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1   **Quenching of steam-charged pumice: Implications for submarine pyroclastic  
2   volcanism**

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16    **Abstract**

17

18         Huge quantities of silicic pumice have been deposited in intra-oceanic convergent  
19 margin settings throughout Earth's history. The association of submarine silicic calderas  
20 with thick proximal accumulations of pumice lapilli suggests that these pyroclasts were  
21 deposited as a direct result of submarine eruptions. Yet when first erupted, these highly  
22 vesicular, gas-filled clasts had densities significantly less than seawater. Experiments  
23 carried out 1-atm on heated pumice samples whose vesicles were charged with steam, the  
24 dominant component of magmatic volatiles show that buoyancy of freshly erupted  
25 submarine pumice is transient. Upon quenching, the phase change of steam to liquid  
26 water creates strong negative pore pressures within the pumice vesicles that accelerate the  
27 absorption of surrounding water, generating high-density pumice and promoting rapid  
28 clast sinking. Variations in the physical properties of steam with temperature and pressure  
29 have important implications for submarine pyroclastic eruptions. Firstly, highly vesicular  
30 pumice can be deposited on the seafloor at temperatures elevated significantly above  
31 ambient if they are erupted at sufficient depths to remain wholly submarine ( $>\sim 200$  m)  
32 and either the fluid in which they cool contains heated water and/or they only absorb  
33 sufficient water to sink. Secondly, the rapid increase in density of the eruption column  
34 caused by condensation and the transition from buoyant (gas-filled) to denser (water-  
35 saturated) pumice lapilli, together with turbulent mixing with the surrounding seawater  
36 favour collapse and transport of pyroclasts in water-supported gravity currents. Finally,  
37 this mixing of the ejecta with seawater and the ease of water ingestion into permeable  
38 pumice clasts suggest that water-supported transport mechanisms can operate as primary  
39 dispersal processes in explosive submarine eruptions.

40

41         *Keywords:* submarine pumice, steam condensation, submarine pyroclastic eruption,  
42 quenching, welding.

43

44    **1. Introduction**

45

46 Pumice is highly vesicular volcanic glass formed during eruptions of water-rich silicic  
47 magma. When the vesicles in pumice are filled with gas, these clasts are buoyant in  
48 water. Historic emergent and ocean-island silicic eruptions have generated extensive rafts  
49 of floating pumice that were widely dispersed, such as those that followed the August  
50 2006 eruption at Home Reef submarine volcano (Smithsonian Institution, 2006) and the  
51 1883 eruption of Krakatau (Simkin and Fiske, 1983). Yet exploration of present-day  
52 submarine arcs shows that aprons of pumice surround submarine explosive calderas (e.g.,  
53 Izu-Bonin arc, Nishimura et al., 1991; Fiske et al., 2001; Kermadec arc, Wright et al.,  
54 2003, Wright et al., 2006). Uplifted successions of modern submarine arcs also attest to  
55 the pumice-rich nature of the deposits (e.g., Hellenic arc, Allen and McPhie, 2000;  
56 Rinaldi and Campos Venuti, 2003; Stewart and McPhie, 2004, 2006), as do thick seafloor  
57 pumice deposits in marine sedimentary sequences associated with ancient volcanic arcs  
58 (e.g., Cambrian Mount Read Volcanics, Australia, McPhie and Allen, 2003; Mesozoic  
59 Mineral King pendant, California, Busby-Spera, 1984; Miocene Green-Tuff Belt, Japan,  
60 Fiske and Matsuda, 1964). These submarine pumice deposits are highly prospective, as  
61 many host VHMS (volcanic-hosted massive sulfide) ore bodies (e.g., Morton et al., 1991;  
62 Gibson et al., 1999; Iizasa et al., 1999; Hudak et al. 2003). The common occurrence of  
63 pumice in the marine record raises important questions about the origin of these deposits.  
64 In particular, because pumice is known to float, its occurrence in large volumes on the  
65 seafloor must be explained.

66 To address this problem, we investigate water ingestion by hot pumice clasts  
67 having variable pore structures (porosity and permeability) and differing proportions of  
68 steam and liquid water in their vesicles. These experiments demonstrate that the influx of  
69 water into steam-charged pumice is rapid during quenching. Extrapolation of our findings  
70 to pressures appropriate for magmatic-volatile-driven explosive eruptions in deep water  
71 suggests that: (1) at least the quenched margins of submarine eruption columns can  
72 transform rapidly from buoyant to collapsing, the latter generating water-supported,  
73 pyroclastic density currents; (2) both the clast cooling history (related to pumice size) and  
74 internal pumice structure (permeability) will influence whether a single pumice clast is  
75 deposited by settling through the water column or from collapse-generated submarine  
76 gravity currents; and (3) the emplacement temperature is influenced by the depth at

77 which the clast becomes water saturated and porosity of the pumice. Our work on steam-  
78 charged pumice extends and expands the experimental work of Whitham and Sparks  
79 (1986) and Dufek et al. (2007) on the interaction of subaerial (air-filled) pumice with  
80 seawater to the submarine environment, providing a quantitative framework for eruptive  
81 and depositional processes in intra-oceanic convergent margin settings.

82

### 83 *1.1 Background and previous work*

84

85 The discovery of pumice clasts in ancient marine volcanic successions now uplifted onto  
86 land, and the concept that some of these pumice lapilli tuffs were derived directly from  
87 submarine explosive eruptions, were highlighted in the pioneering work of RS Fiske  
88 (Fiske, 1963; Fiske and Matsuda, 1964; Fiske 1969). Since that time, several submarine  
89 calderas formed by explosive eruptions of silicic magma and their infilling syn-caldera  
90 pumice deposits have been interpreted in ancient successions (e.g., De Rosen-Spence et  
91 al., 1980; Busby-Spera, 1984; Hudak et al., 2003). It is only recently, however, that  
92 seismic profiles and submarine bathymetric data have confirmed the presence of calderas  
93 on the modern seafloor (e.g., Izu-Bonin arc, Murakami and Ishihara, 1985; Yuasa et al.,  
94 1991; Yuasa and Kano, 2003; Kermadec arc, Wright and Gamble, 1999; Wright et al.,  
95 2006; Mariana Arc, Stern et al., 2008). Dedicated submersible and/or remotely operated  
96 vehicle dives on Myojin Knoll caldera (Fiske et al., 2001), Sumisu caldera (Tani et al.,  
97 2008) and West Rota Volcano (Stern et al., 2003), and dredge-sampling on Healy caldera  
98 (Wright et al., 2003) have shown that these calderas have produced substantial volumes  
99 of highly vesicular pumice deposits on the seafloor. In particular, the eruption that  
100 produced the Sumisu caldera is considered to be the source of the thick, pumice lapilli-  
101 tuffs that were discovered during ODP drilling in the Sumisu rift basin, 70 km away  
102 (Nishimura et al., 1991, Tani et al., 2008).

103 The lithofacies characteristics of well preserved, uplifted Miocene to Recent  
104 eruption-fed, submarine pyroclastic pumice deposits include, (1) double grading, where  
105 each bed is density graded, and the bedsets are normally graded overall (Fiske and  
106 Matsuda, 1964), (2) hydraulic sorting (Cashman and Fiske, 1991), and (3) well-defined  
107 organisation into lithic-rich bases, pumice lapilli-rich main parts, and upper pumice block

108 and/or ash facies (Kano et al., 1996; Allen and McPhie, 2000; Stewart and McPhie,  
109 2004). Such features indicate that the transport and depositional dynamics of the erupted  
110 ejecta are strongly influenced by cooling and mixing with the surrounding seawater.  
111 Theoretical considerations of the eruption dynamics have focussed on the effects of this  
112 turbulent mixing on column stability, leading to the conclusion that the ejecta from  
113 submarine eruptions quickly become negatively buoyant and collapse (Kano et al., 1996;  
114 Head and Wilson 2003). Recent review papers on subaqueous eruption-fed density  
115 currents and their deposits (White 2000), historic submarine pumice eruptions (Kano  
116 2003), and explosive submarine eruptions (White et al., 2003), discuss the processes by  
117 which pumice can be erupted and deposited on the seafloor, including the role of  
118 magmatic gases and external steam production on plume behaviour.

119 Moreover, understanding of the mechanisms that cause submarine-erupted low-  
120 density pumice lapilli to sink has been heavily dependent on the experimental study of  
121 Whitham and Sparks (1986), who addressed a different problem, that is, the behaviour of  
122 hot subaerially erupted pumice that enters the ocean in pyroclastic density currents.  
123 Whitham and Sparks (1986) heated air-filled, highly vesicular pumice (densities 200-300  
124 kg/m<sup>3</sup>) before forcing them under water. When heated to temperatures  $\geq 400^{\circ}\text{C}$ , these air-  
125 filled clasts absorbed water and sank by a two step process: firstly, air was flushed out of  
126 the vesicles by steam generated from the interaction of the hot clast with water. Secondly,  
127 ingestion of water resulted from contraction and condensation of the steam. Pumice at  
128 lower temperatures ( $<300^{\circ}\text{C}$ ) was much less efficient at generating steam and therefore  
129 remained sufficiently air-filled to float. For this reason, it has been generally assumed that  
130 only hot ( $\geq 400^{\circ}\text{ C}$ ) pumice can sink efficiently in water.

131 Interpretations based on these experiments may be less applicable to the behaviour  
132 of pumice produced in submarine environments, where vesicles are filled with magmatic  
133 gases (mostly steam) rather than air. Nitrogen and oxygen, the chief components of air, are  
134 not magmatic gases, and in contrast to steam, do not undergo a phase change while cooling  
135 through temperature ranges encountered by submarine eruptions. Condensation of steam  
136 causes a dramatic change in volume creating negative pore pressures that accelerate  
137 ingestion of the surrounded seawater fluid (e.g., Kato, 1987; Kano et al., 1996; Cashman  
138 and Fiske, 1991; Fiske et al., 2001). To test the efficiency of this mechanism, we have

139 performed a series of 1 atm experiments on steam-charged rhyolitic pumice samples that  
140 were initially fully water-saturated. The physics of steam condensation is universal  
141 regardless of the pressure conditions, hence, results of quenching experiments undertaken  
142 at atmospheric pressure can be realistically extrapolated to higher pressure conditions  
143 below the critical point.

144

## 145 **2. Steam experiments**

146

### 147 *2.1 Sample properties*

148

149 Four blocks of unaltered, fully water-saturated rhyolitic pumice were collected from  
150 thick, coarse unconsolidated pumice breccias on the seafloor at depths of 1470-320 m in  
151 the Izu-Bonin arc and back arc by Remotely Operated Vehicle (ROV) and dredging  
152 during JAMSTEC research cruises KV04-04 and NT04-10 (Table 1). As these clasts are  
153 fresh (unaltered and without manganese crusts), large (>30 cm across), and contain  
154 relatively homogeneous vesicle populations, their textures are similar in the multiple 2  
155 cm-cubes that were cut. Seawater was flushed out and replaced by fresh water by suction.  
156 The water-saturated pumice cubes were individually numbered and weighed while  
157 suspended in water [ $m_{sat}(\text{water})$ ] (dabbed for ~2 seconds on moist chamois to remove  
158 excess water), and then weighed again in air [ $m_{sat}(\text{air})$ ]. Water saturated specific gravities  
159 were calculated as:

160

$$161 S.G_{sat} = m_{sat}(\text{air}) / [m_{sat}(\text{air}) - m_{sat}(\text{water})]$$

162

163 The variation in water saturated S.G. due to vesicle heterogeneities within each  
164 block was less than 5% (Table 1, Fig. 1). On completion of the steam experiments, the  
165 cubes were furnace dried (1-2 hr at 200-400°C) and weighed to calculate their specific  
166 gravity when dry, where

167

$$168 S.G_{dry} = m_{dry}(\text{air}) / [m_{sat}(\text{air}) - m_{sat}(\text{water})]$$

169

170 Dense-rock S.G. for each pumice clast were measured by He-pycnometer using powdered  
171 samples. Theoretical water-saturated S.G. were calculated for each cube, where

172

173  $S.G_{\text{sat}} \text{ (theoretical)} = 1 + S.G_{\text{dry}} - (S.G_{\text{dry}} / S.G_{\text{dense rock}})$

174

175 Variations in measured water-saturated S.G. from theoretical values were <3%  
176 and attributed to leakage from large pores during weight-in-air measurements (Table 1,  
177 Fig. 1). Bulk and connected porosities and abundances of isolated vesicles of dry (air-  
178 filled) samples were measured by He-pycnometer following the method of Klug and  
179 Cashman (1996). We also measured the permeability of 25 mm-diameter cores cut from  
180 the pumice clasts with a permeameter/porometer following the method of Rust and  
181 Cashman (2004).

182

183 *2.1 Experimental method*

184

185 The experiments were designed to measure the effects of steam condensation on the  
186 uptake of water during quenching of pumice clasts. They involved two stages: (1) Steam  
187 experiments, where the fully water-saturated cubes were heated in a furnace at a set  
188 temperature so that a fraction of the pore water was replaced with steam. At the desired  
189 water/steam ratio, the cubes were quenched in room-temperature (21°) water and  
190 reweighed to determine the efficiency of water absorption. (2) Air experiments where the  
191 same pumice cubes were then dried, heated to the same temperature as the steam run,  
192 quenched, and reweighed to determine the efficiency of water resorption in the cube in  
193 the absence of interstitial steam.

194

195 At 1 atm the phase change from steam to liquid water occurs at 100°C, so that  
196 experiments to measure the effects of steam condensation were undertaken at  
197 temperatures elevated slightly above 100°C (110, 125 and 150°C). To distinguish the  
198 effects of steam condensation from capillary action and gas contraction, the steam  
199 experiments included runs at higher temperatures (200 to 500°C). Air experiments were  
200 performed at temperatures that ranged between 21 °C and 500°C.

201 *Steam experiments:*

- 202 1) Initially, samples from each pumice clast were furnace dried to permit calculation of  
203 their dry specific gravities. Then for each cube used in the steam experiments, the  
204 approximate mass could be calculated to reflect the desired steam/water ratio prior to  
205 quenching. Steam/water ratios were chosen at 30/70, 50/50 and 70/30 to reflect stages in  
206 water ingestion in a theoretically cooling pumice clast. Ratios were chosen to reduce the  
207 proportion of water sufficiently to make the cube initially buoyant ( $\leq 70\%$ ), but with  
208 minimum contamination of air ( $\geq 30\%$ ). The cubes were tightly wrapped in aluminium-  
209 foil to further reduce contamination with air.
- 210 2) Experimental runs were conducted at furnace temperatures of 110°C, 125°C, 150°C,  
211 200°C, 300°C, 400°C and 500°C. A total of 12 cubes were used for each temperature run  
212 - three cubes from each pumice block; one at each steam/water ratio. Because the  
213 experiments were designed to retain some liquid water in the cube, each cube  
214 experienced a temperature gradient that ranged from below 100°C in the cube interior to  
215 the furnace temperature towards the cube margin.
- 216 3) As each cube was heated, the interstitial water boiled and was progressively  
217 transformed to steam. The mass of water-loss for each cube was measured periodically by  
218 rapid (5 sec round trip) removal and weighing on an adjacent top-loading balance. The  
219 rate of water loss was plotted to predict the time when the desired steam/water ratio  
220 would be reached (Fig. 2a).
- 221 4) At the desired steam/water ratio, the steamy cube was quenched by plunging into 21°C  
222 water; the Al-foil was quickly removed while being held under water. After a set time  
223 interval (5 minutes was chosen to allow the clast to fully cool and reach an equilibrium  
224 saturation), the cube was removed from water, dabbed for ~2 seconds on moist chamois,  
225 and weighed to determine the resaturation mass.
- 226 5) The cubes were then dried and weighed dry to permit calculation of their dry specific  
227 gravities and determine their actual steam/water ratio on quenching.

228

229 *Air experiments:*

- 230 6) Each (Al-clad) dried cube was reheated to the same temperature as its water-saturated  
231 run, with additional temperature runs of 21°C and 70°C. The air-filled cube was then

232 weighed and quenched in water following the procedure for the steam-charged cubes to  
233 determine the comparative re-saturation mass.  
234 7) As a control, 12 dry cubes (the same 3 cubes selected from each pumice clast) were  
235 heated, quenched and weighed for saturation after quenching at each of the temperature  
236 runs. These experiments tested the variability in saturation on quenching of the same clast  
237 when heated to different temperatures (Fig. 2b).

238

### 239 **3. Results and interpretation**

240

241 The primary goal of our experiments was to determine controls on the efficiency of water  
242 resorption by pumice clasts when immersed in water. In all experiments, we define the  
243 efficiency of water absorption as the extent to which a pumice cube re-saturates after  
244 heating, quenching and immersion in water for 5 minutes compared to its fully water-  
245 saturated, pre-experiment mass. The absorption factor ( $\alpha$ ) was defined as  $\alpha = (m_{\text{resaturated}}$   
246  $- m_{\text{air-filled}})/(m_{\text{saturated}} - m_{\text{air-filled}})$  where  $m$  is the mass of the cube;  $\alpha$  can therefore vary  
247 between 0 (no resorption) and 1 (fully resorption; Fig. 3).

248

#### 249 *3.1 Water and steam-filled pumice*

250

251 When heated above the liquid water-steam transition (100°C at 1-atm), all steam-charged  
252 pumice cubes sank quickly when quenched regardless of their pre-quench temperature,  
253 re-absorbing most of the water temporarily displaced by steam (Fig. 3). Ideally, the  
254 uptake of water due to steam condensation in the pore spaces during quenching should  
255 have returned all cubes to full saturation (absorption factors of 1). However, saturation  
256 was commonly less than 100% and varied predictably with pre-quenching conditions.  
257 Pumice cubes having the highest pre-quench water/steam ratios (70/30; red dots) had the  
258 highest re-absorption factors ( $\alpha \geq 0.95$ ). All but two of those having 50/50 water/steam  
259 ratios had  $\alpha \geq 0.90$  (blue dots), and only one of those having 30/70 ratios (green dots) had  
260  $\alpha < 0.8$ . In the latter two sets of experiments,  $\alpha$  increased with increasing pre-quench  
261 temperature. We have identified two sources of experimental error that probably

262 contributed to less than perfect water resorption; differences in resorption potential  
 263 generated by details of the pore structure are discussed later.

264 (1) *Air contamination.* Our experiments did not prevent the loss of steam from the  
 265 cubes, and resulting contamination by air, during the repeated out-and-into-furnace  
 266 weighings because of leakage through the aluminium foil wrap enclosing each cube. The  
 267 data points representing steam/water ratios of 30/70 (red), 50/50 (blue), and 70/30 (green)  
 268 (Fig. 3), show progressive decreasing re-absorption factors, indicating that errors were  
 269 greater with increasing time in the furnace and increasing numbers of weighing cycles.

270 (2) *Weighing error.* Measurement of pumice mass (both saturated and re-  
 271 saturated) generated errors of  $\leq 2\%$ . Greater errors were associated with samples  
 272 containing larger coalesced vesicles because of rapid water drainage from vesicles.

273 3.2 *Air-filled pumice*

274 Absorption characteristics of the air-filled pumice cubes differ markedly from the steam-  
 275 charged cubes (open circles; Fig. 3). Between 21°C and  $\sim 300^\circ\text{C}$ ,  $\alpha$  of air-filled cubes  
 276 increase as temperature increases. Above 300°C, less vesicular cubes (337-1, 339-8; 73  
 277 vol% vesicles; Figs. 3c, 3d) are almost completely water-saturated whereas cubes with  
 278 higher vesicularities (D7, 337-5; 80 vol% vesicles; Figs. 3a, 3b) fail to reach complete  
 279 water-saturation, even at temperatures of 500°C.

280 At room temperature (21°C), where there is no temperature change on immersion  
 281 in water, absorption may occur by capillary forces (related to pressure and surface  
 282 tension); our data suggest that capillarity can account for absorption factors of  $\sim 0.4$   
 283 (capillary+ field; Fig. 3a). With increasing initial temperature, absorption is enhanced by  
 284 cooling contraction of the air within the vesicles. According to the ideal gas law  
 285 (assuming that pressure and mole fraction of air remain constant):

286

287 
$$V_1 / V_2 = T_1 / T_2,$$

288

289 where  $V_1$  and  $V_2$  and  $T_1$  and  $T_2$  are volumes and temperatures (in Kelvin) after heating  
 290 (just before quenching) and on quenching to ambient temperatures. For example, on

291 quenching from temperatures of 573K (300°C), air contracts to about half its volume,  
292 giving an absorption factor of ~0.5 (1-T<sub>2</sub>/T<sub>1</sub> contraction field; Fig. 3a). At temperatures  
293 ≥400°C (673K), the absorption process is overshadowed by the phase change of steam  
294 (steam field; Fig. 3a) generated from the interaction of the hot glass with water (e.g.,  
295 Whitham and Sparks, 1986; Dufek et al., 2007).

296

297 *3.3 Behaviour of air- versus steam-charged hot pumice*

298

299 The differences in absorption efficiency between air-filled and steam-charged pumice  
300 illustrate the importance of the volatile phase composition on quenching behaviour.  
301 Steam-charged pumice ingests water rapidly, reaching essentially full saturation as soon  
302 as the steam condenses (at the steam-liquid water phase transition temperature) and sinks  
303 (grey field in Fig. 3). In contrast, air-filled pumice partially saturates to a degree that  
304 depends on the initial temperature and vesicularity. For this reason, the largest differences  
305 in  $\alpha$  between steam-charged and air-filled pumice occurs at the lowest temperatures  
306 (<300°C), where the steam generated is not sufficient to cause saturation of pumice clasts  
307 on quenching and water ingestion occurs by cooling contraction of air and capillary  
308 action (e.g., Whitham and Sparks, 1986).

309 As noted by Whitham and Sparks (1986), the initial vesicularity of hot air-filled  
310 pumice clasts dictates the absorption factor required for the clast density to exceed that of  
311 seawater. This relationship is illustrated by comparing air-filled clasts with 80% vesicles,  
312 which sank at T > 300°C ( $\alpha \geq 0.7$ ; Figs. 3a, 3b) with those with 73% vesicles, which sank  
313 at T > 125°C ( $\alpha \geq 0.58$ ; Fig. 3c, 3d). This vesicularity dependence is not observed in  
314 steam-charged pumice, where all clasts had  $\alpha >> 0.7$  and therefore sank as soon as the  
315 steam-liquid water phase transition was reached.

316 Our results thus show that pumice can absorb water and sink at the steam-liquid  
317 water phase change temperature if the vesicles are initially charged with steam.  
318 Moreover, cooling from temperatures far above this phase transition does not further  
319 increase the absorption efficiency, in contrast to the strong dependence of sinking  
320 efficiency on the temperature of air-filled clasts. Finally, air-filled clasts never achieved  
321 full saturation, although all clasts sank when heated to sufficiently high temperatures.

322 Thus we expect pumice cooled from magmatic temperatures and flushed by air prior to  
323 contact with water to have very different water-ingestion capabilities than submarine-  
324 erupted pumice filled with H<sub>2</sub>O-rich magmatic gases that never reaches sea level.

325

326 *3.4 Influence of pore structure on water absorption*

327

328 Our experiments suggest that textural variations in the seafloor pumice blocks  
329 influenced the absorption characteristics of the cubes sawn from them. To assess the  
330 importance of pore structure on  $\alpha$ , we measured the connected porosity, isolated porosity,  
331 and permeability of all analysed samples. All pumice clasts are highly vesicular (73-80  
332 vol% vesicles); these vesicles are mostly (>97%) connected. Both the high porosities and  
333 high degree of interconnectivity lead to high clast permeabilities ( $2.5 - 10 \times 10^{-12} \text{ m}^2$ ). In  
334 detail, sample D7 exhibits both high vesicularities and uniform vesicle geometries,  
335 resulting in both high permeability ( $9.9 \times 10^{-12} \text{ m}^2$ ; Table 1) and high water absorption  
336 efficiency of this sample ( $T < 200^\circ\text{C}$ ,  $\alpha \geq 0.87$ ; Fig. 3a). The other three pumice samples  
337 comprise both elongate and round coalesced vesicle domains and/or display a greater  
338 range in vesicle size (up to 5 mm) and lower permeabilities ( $2.4-3.2 \times 10^{-12} \text{ m}^2$ ). As a  
339 result, these cubes have slightly lower absorption efficiencies ( $T < 200^\circ\text{C}$ ,  $\alpha \geq 0.74$ ) than  
340 the D7 cubes, particularly as the phase change temperature is approached.

341

342 *3.5 Submarine-erupted pumice properties*

343

344 The pumice blocks used in the experiments have vesicularities and permeabilities typical  
345 of submarine erupted and deposited pumice clasts collected from knolls on the modern  
346 sea floor of the Izu-Bonin Arc, Japan and from uplifted successions in the Aegean Arc,  
347 Greece (Fig. 4). Our suite of over 200, highly vesicular, silicic pyroclastic and quenched-  
348 dome margin samples, have typical vesicularities of 60-80 vol%, permeabilities of  $>10^{-13}$   
349  $\text{m}^2$  and are dominated by connected vesicles (>90 vol%). These high permeability and  
350 vesicularity ranges appear typical of silicic pumice regardless of whether they were  
351 erupted in the submarine or subaerial environment (cf. Klug and Cashman, 1996). Such

352 high permeabilities are equivalent to those of well-sorted sands and glacial outwash,  
353 although the porosities of sediments are much lower (25-50 vol%; Fetter 1988).

354 There are however two unusual characteristics of submarine erupted and  
355 deposited pumice that affect clast dispersal characteristics. Firstly, a feature that was first  
356 recognised by Fiske (1969) in ancient submarine successions is that much of the pumice  
357 is the long-tube variety. The vesicles have a dominant elongation direction, and range  
358 from elongate to being highly attenuated (Fig. 5a). In these clasts, permeabilities can vary  
359 by up to 4 orders of magnitude depending on the orientation of the measurement;  
360 important for settling properties is the very high permeability measured parallel to vesicle  
361 elongation. In contrast, submarine-erupted pumice clasts with a high percentage of  
362 spherical and isolated vesicles tend to float for long periods of time (Fiske, 1969), and are  
363 thus washed up at coastlines or deposited from floating rafts at substantial distances from  
364 source. For example Kato (1987) found that pumice that remained floating from the  
365 submarine eruption off Iriomote Island in 1924 had very high proportions (37 vol%) of  
366 isolated vesicles. Saturation of pumice with spherical vesicles is governed by capillary  
367 pressure required for water to move through the very small pores formed during partial  
368 vesicle coalescence (Klug and Cashman, 1996). Secondly, there is a tendency for coarse  
369 lapilli and larger clasts to fracture as a result of quenching in water. Fracturing is  
370 manifested as intensely shattered to jointed (at a cm-scale) margins and polyhedral or  
371 curviplanar internal fracture surfaces (Fig. 5b). The effect of this process is illustrated by  
372 large m-sized pumice blocks that rose to the surface from the 1934-1935 deep submarine  
373 eruptions of Shin-Iwojima, Japan (Kano et al., 2003) and floated only briefly while  
374 steaming and cracking before sinking. Thus, fracture-controlled permeability appears to  
375 allow effective and rapid saturation of large hot pumice clasts.

376

#### 377 **4. Implications for submarine pyroclastic eruptions**

378

379 Magmatic-volatile-driven explosive eruptions are triggered by overpressures related to  
380 the decompression of volatiles in the magma (McBirney, 1963; Wilson et al., 1980)  
381 which drives the ejecta upwards at high exit velocities. In subaerial eruptions, further  
382 ascent occurs as a result of mixing of this turbulent jet with air, which considerably

383 lowers the density of the ejecta and generates a buoyant plume. Subaqueous pyroclastic  
384 eruptions however, are expected to behave differently from their subaerial counterparts.  
385 For example, the pressure exerted by the overlying water column retards volatile  
386 exsolution, vesiculation and decompression-driven exit velocities; the high heat capacity  
387 and thermal conductivity of water accelerates cooling; and, the greater viscosity and  
388 density of seawater relative to air affects buoyancy and patterns of clast transport  
389 (Cashman and Fiske, 1991; Kokelaar and Busby, 1992; Kano et al., 1996; Head and  
390 Wilson, 2003; White et al., 2003; Stewart and McPhie, 2004).

391 Quantitative analysis of the behaviour of submarine pyroclastic eruptions predicts  
392 that the jet mixes extensively with water through turbulence (Head and Wilson, 2003).  
393 The thermal diffusivity of steam varies with temperature and pressure ( $2 \times 10^{-5} \text{ m}^2/\text{s}$  for  
394 steam at  $100^\circ\text{C}$  and  $0.1 \text{ MPa}$ ;  $2 \times 10^{-6} \text{ m}^2/\text{s}$  for steam at  $180^\circ\text{C}$  at  $1 \text{ MPa}$ ), but is  
395 significantly higher than that of pumice ( $\sim 2.5 \times 10^{-7} \text{ m}^2/\text{s}$ ). Hence, the inter-particle steam  
396 will rapidly cool and condense, accelerating the mixing of the ejecta with seawater due to  
397 negative pressures created during condensation. This change in plume composition from  
398 gas-dominated to water-dominated is therefore likely to occur quickly, at least at the  
399 margins of the jet. Furthermore, Head and Wilson (2003) predict that this cooling and  
400 mixing with water will cause the jet to collapse and segregate from the ash, which will be  
401 elutriated to form a plume. However, Head and Wilson (2003) did not trace fate of ejecta  
402 dominated by highly vesicular pumice clasts. Here we explore the ramifications of the  
403 steam-liquid water phase change on the behaviour and depositional processes  
404 accompanying submarine explosive eruptions where pumice is the dominant clast type.  
405

#### 406 *4.1 Transient buoyancy*

407

408 On eruption, vesicles in the pumice clasts are filled with magmatic gases and rise  
409 through the water column as a result of the combined effects of initial eruption flux and  
410 buoyancy. However, steam, the dominant component of magmatic gas, which has a low  
411 density and high buoyancy, condenses to higher density liquid water once it cools  
412 through the phase-change temperature, drawing in the surrounding water. Theoretically,  
413 on cooling, pumice clasts will begin to fill with seawater, gradually at first because of the

414 combined effects of capillary forces and the volume change of magmatic gases due to  
415 contraction and then abruptly because of the condensation of magmatic steam. For  
416 example, in order to sink, pumice with 60 vol% vesicles needs only 10% of the vesicles  
417 to be water-saturated whereas clasts with 85 vol% vesicles requires saturation of 75% of  
418 the vesicles (Figs. 6, 7). Therefore, in order for pumice clasts to remain buoyant, they  
419 must be sufficiently hot to remain steam-filled (Cashman and Fiske, 1991; Kano et al.,  
420 1996; Fiske et al., 2001). The rate of cooling of pumice is also dependent on clast size,  
421 and larger clasts cool more slowly because of their greater thermal mass (Thomas and  
422 Sparks, 1992; Kano et al., 1996). Kano et al. (1996) used equations of Carslaw and Jaeger  
423 (1959) to calculate times required for complete cooling of pumice clasts to condensation  
424 temperatures for different clast sizes. These calculations give maximum cooling rates  
425 from conductive cooling. The results suggest that cooling the clast interiors to 180°C, the  
426 phase change temperature at 1 MPa (100 mbsl), for coarse ash ( $\leq 2$  mm), fine lapilli ( $\leq 16$   
427 mm) and coarse lapilli ( $\leq 64$  mm) would take no longer than 1.6 seconds, 1.7 minutes  
428 and 27 minutes, respectively. These calculations led Kano et al. (1996) to suggest that  
429 smaller pumice clasts cool on contact with water and become water-logged. As the  
430 behaviour of eruption columns is sensitive to density changes, the cooling and mixing of  
431 the ejecta with seawater together with the dramatic increase in density of pumice lapilli  
432 during cooling is predicted to destabilize the column, promoting collapse, and initiating  
433 transport of negatively buoyant pyroclasts in water-supported gravity currents, essentially  
434 conforming with the model of Head and Wilson (2003). Therefore, pumice lapilli that  
435 cool and absorb water more readily than larger clasts, will be over-represented in deposits  
436 resulting from collapse-generated flows. Such pumice lapilli-rich flow deposits have  
437 been reported in field studies of uplifted successions in Japan and Greece (e.g., Shinjima  
438 pumice, Kano et al., 1996; Yali pumice, Allen and McPhie, 2000; Filakopi pumice unit  
439 B, Stewart and McPhie, 2004) (Fig. 5c).

440 In contrast, coarse lapilli and blocks that remain sufficiently hot to be buoyant,  
441 rise out of the collapsing fountain in thermal convecting plumes of heated water (e.g.  
442 Kano et al., 1996). We suggest that, for these large buoyant clasts, magmatic steam and  
443 other gases filling vesicles at depth will continue to decompress, acting to accelerate their  
444 rise rate and inhibit contact with the surrounding water. Once these large clasts reach the

surface and decompression is complete, they begin to cool. Hot pumice clasts were observed to billow steam as they floated on the sea surface during the 1934 eruption at Shin-Iwojima, south of Kyushu, Japan (Kano, 2003) and the 1953-1957 eruption of Tuluman volcano, northern Bismarck Sea (Reynolds et al., 1980). In this low-pressure environment, the steam to liquid water phase change is accompanied by a 1600-fold volume decrease, and thermal-contraction fractures that form in the pumice, accelerate the ingestion of water into the clast. Hence, these fractured clasts quickly begin to saturate and sink. While doing so, any remaining gas in the vesicles continues to contract while settling through the increasing pressures in the water column, causing settling velocities to increase. For example, large pumice blocks (10-100+ cm) within the Yali pumice cobble-boulder facies (Allen and McPhie, 2000) and Filakopi pumice unit C (Stewart and McPhie, 2004) (Fig. 5d), are interpreted to have separated from the collapsing column and ascended buoyantly to the sea surface before settling to the seafloor and are deposited after the collapse generated deposits. Deposits derived from quenched, submarine pumice eruption columns therefore tend to show an overall reverse grading in pumice clast size from lapilli (base) to blocks (upper part), reflecting differing cooling rates and transport mechanisms.

In addition, dense conduit- and vent-derived lithic clasts are too heavy to be entrained in the jet and, fall out rapidly to form basal lithic breccias (Stewart and McPhie, 2004). Furthermore, fine ash particles, having low settling velocities, are readily elutriated during eruption and transport and can be transported many kilometres from the eruption site as water-settled fallout or in sufficient concentrations form ash-rich density currents. Many submarine-erupted pumice deposits are therefore fines-poor (e.g., Fiske, 1963; Fiske and Matsuda, 1964; Fiske, 1969; Kano et al., 1996; Allen and McPhie, 2000; Stewart and McPhie, 2004).

The patterns of pyroclast transport and deposition outlined above also differ from those resulting from subaerial eruptions that enter the sea. In this environment, pumice lapilli cool in air, ingests air, and falls to the sea surface with their vesicles filled with air. Large proportions of these pumice lapilli float and can be rafted far from the eruption site (e.g., Simkin and Fiske, 1983; Bryan et al., 2004). In contrast, negatively buoyant clasts

475 settle through the water column generating submarine deposits that are rich in dense lithic  
476 clasts.

477 Our findings reinforce the concept first proposed by Fiske and Matsuda (1964),  
478 that the direct products of explosive submarine eruptions can form primary seafloor  
479 pyroclastic deposits. However, these submarine eruption-fed deposits differ markedly in  
480 facies characteristics from their subaerial counterparts.

481

#### 482 *4.2 Effect of increasing water depth*

483

484 A major challenge to understanding submarine eruptions is determining the effect of  
485 increasing water depth (pressure) on the style of eruptive activity. The reduction in water  
486 exsolved from the magma with pressure controls the volatiles available to drive explosive  
487 submarine eruptions (McBirney, 1963). Using the model of Wilson et al., (1980), we  
488 calculate that for rhyolites with magmatic water contents of 5-7 wt%, exit velocities will  
489 be reduced by ~1/2 at 500 m water depth, and by ~1/4 at 1000 m water depth because of  
490 variations in water solubility, alone. In addition, Head and Wilson (2003) predict that  
491 although the density of the ejecta increases with water depth, less thermal energy is lost  
492 during mixing with ambient seawater and hence lower but hotter fountain mixtures are  
493 generated. Several weakly vesiculated rhyolites in ancient successions have been  
494 interpreted to be sourced from these deep-water dense fountains (e.g., Kokelaar and  
495 Busby, 1992; Mueller and White, 1992; Busby, 2005).

496 Submarine eruptions that generate highly vesicular pumice at a few hundred meters  
497 water depth are fairly common, as indicated by both vent depth estimates for well  
498 exposed uplifted submarine pyroclastic pumice deposits (e.g., Fiske and Matsuda, 1964;  
499 Kano et al., 1996; Allen and McPhie, 2000; Stewart and McPhie, 2004) and historic  
500 pumice-forming submarine eruptions (Kano, 2003). The submarine caldera-forming  
501 eruption that deposited the Shinjima Pumice was sourced in as little as 200 m of water,  
502 indicating that this depth was sufficient to suppress jet heights and cause column collapse  
503 (Kano et al. 1996). While studies of calderas on the modern seafloor suggest that  
504 magmatic volatile-driven eruptions generating highly vesicular pumice have occurred at  
505 depths of 500 m and possibly as much as 1000 m (Fiske et al., 2001; Wright et al., 2003,

506 Yuasa and Kano, 2003; Wright et al., 2006). At a depth of 200 m (2 MPa) the steam-  
507 liquid water phase transition temperature is 212°C, more than 100°C greater than at sea  
508 level, and at 500-1000 m the phase transition is in the range 260-310°C. What is the  
509 effect of such elevated temperatures on pumice erupted and deposited at these depths?

510

511 *4.3 Hot submarine pumice deposits?*

512

513 As the critical point of H<sub>2</sub>O is approached, the density change across the steam-to-liquid  
514 water phase transition decreases, and the temperature increases. Although unlikely to  
515 have a major effect on the process of magmatic vesiculation, which typically occurs at  
516 much higher temperatures and pressures, changes in the physical properties of steam will  
517 affect post-eruptive interaction of pumice with seawater. The cooling interval over which  
518 submarine-erupted pumice exceeds the density of seawater and begins to sink depends on  
519 vesicularity and ambient pressure, which determine the steam volume and temperature of  
520 the steam-liquid water phase transition.

521 Theoretically, pumice clasts can remain substantially above 100°C and still sink  
522 (Fig. 6). Our experiments show that sufficient water is ingested in clasts that have less  
523 than ~ 80 vol% during cooling to initiate sinking, even above the phase transition  
524 temperature (Fig. 6a). Furthermore, highly vesicular clasts (those with >81 vol% vesicles)  
525 that require cooling to the phase change temperature to induce sinking can theoretically  
526 be deposited hot (that is, at T > 100°C) as a result of the increase in the phase change  
527 temperature with water depth (Fig. 6b). For example, at sea level pumice containing  
528 81 vol% vesicles will sink at 100°C, whereas at 1000 m water depth (10 MPa) the same  
529 pumice will begin to sink at 311°C. At sea level, dense pumice with a specific gravity of  
530 0.82 (65 vol% vesicles) when first erupted will sink at ~550°C and at 1000 m water depth  
531 the clast will begin to sink at ~600°C.

532 Variability in pumice deposition rate will also be controlled by non-uniformity in  
533 processes of cooling and water-saturation of pumice. On contact of the hot pumice with  
534 seawater, small clasts (lapilli) and the margins of larger clasts (blocks) cool rapidly,  
535 whereas the interior of coarser clasts can remain hot, forming a steep within-clast  
536 temperature gradient. This gradient is clearly demonstrated in the spacing and intensity of

537 fractures in pumice clasts deposited on the seafloor. The outer ~1-2 cm margin is  
 538 intensely cracked and may even show breadcrust texture whereas the interior has more  
 539 widely spaced incipient fractures (Fig. 5b). Furthermore, water is ingested into the  
 540 interior of the clast along the most permeable pathways, producing an irregular wet front  
 541 (e.g., Manville et al., 1998). In addition, cooling of pumice within submarine eruption  
 542 columns will be influenced by the temperature of the surrounding fluid, which is  
 543 controlled by the rate of heat transfer from the magmatic ejecta.

544 Submarine pumice lapilli can therefore be deposited hot if the clasts are erupted at  
 545 depth, sink quickly (close to the eruption and depositional depth), and ingest heated  
 546 water. This is not an unrealistic scenario for pumice deposits resulting from the collapse  
 547 of submarine eruption columns. Would deposition temperatures be sufficient for highly  
 548 vesicular pumice deposited on the seafloor to thermally weld? Our assessment of an  
 549 ~300°C maximum depositional temperature for highly vesicular pumice is far lower than  
 550 that expected for thermal welding in subaerial settings (650-750°C, Grunder et al., 2005),  
 551 although the decreased viscosity of the hydrous glass due to the reduced exsolution of  
 552 water in the magma at high hydrostatic pressures needs also to be considered (e.g., Sparks  
 553 et al., 1980). However, if the erupted pumice clasts are also relatively dense (<~65 vol%  
 554 vesicles), then hot deposition, and even welding, may be possible (cf. Kokelaar and  
 555 Busby, 1992). This leads to the possibility that welding in submarine deposits may be  
 556 possible in partially water-saturated clasts negating the perceived difficulties of  
 557 transporting and depositing hot, buoyant gas-filled pumice on the seafloor.

558

## 559 **5. Conclusions**

560

561 Pumice clasts, when first erupted from submarine vents, are hot, filled with magmatic gas  
 562 (mostly steam), and are buoyant. Our experiments with steam-charged pumice, performed  
 563 at 1-atm pressure, show that buoyancy is transient as the pumice is quenched in water and  
 564 becomes water-logged. Moreover, steam-charged pumice need not be super-hot (>400°C)  
 565 to sink, in contrast to air-filled pumice (Whitham and Sparks, 1986).

566 Water is first ingested into cooling pumice when steam and other magmatic gases  
 567 in the vesicles cool and contract. Regardless of the temperature at which pumice begins to

568 sink, the greatest and most rapid density increase occurs once the clast cools through the  
569 steam-liquid water phase transition; this phase change triggers in an abrupt increase in  
570 clast settling velocity. Hence, during a submarine eruption, pumice clasts change from  
571 being buoyant and hot on eruption, to being negatively buoyant and cooler while mixing  
572 with water in the column, at which point they are transported in collapse-generated  
573 gravity currents or by water settling. This behaviour contrasts with pumice clasts in  
574 subaerial explosive eruptions, which regardless of their temperature, are always more  
575 dense than the surrounding air.

576 Our experiments can be extrapolated to show that the phase change of magmatic  
577 steam to liquid water in the vesicles of hot pumice and in the submarine eruption column  
578 has an important influence on eruption behaviour and pyroclast dispersal. Condensation  
579 of steam causes a rapid change in density and mixing with ambient seawater that  
580 promotes collapse. Lapilli and coarse ash, being small, tend to quench rapidly and  
581 completely and are therefore likely to be transported in water-supported gravity currents.  
582 Larger pumice blocks cool more slowly and may rise to sea level before settling through  
583 the water column along with fine ash.

584 Because the temperature at which pumice becomes saturated and sinks increases  
585 with water depth, submarine pumice clasts can be deposited both hot and waterlogged in  
586 eruptions sourced in several hundred metres of water and if they cool within the heated  
587 water of the eruption column. The resulting deposits, having internal temperatures above  
588 that of the surrounding seawater, will be too cool to weld ( $\leq 300^{\circ}\text{C}$ ) unless the pumice  
589 clasts are also poorly vesicular ( $\sim 65$  vol% vesicles).

590 Our quantitative analysis explains the physical processes accompanying  
591 submarine pyroclastic eruptions and demonstrates that they can form primary seafloor  
592 pyroclastic deposits, a conclusion reached by others from qualitative studies in ancient  
593 terrains now uplifted onto land.

594

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596

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604

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- 778
- 779 **FIGURE CAPTIONS**
- 780

781 Fig. 1. Measured specific gravities of pumice clasts re-saturated with water compared to  
782 measured specific gravities of dry pumice clasts. The expected relationship for fully  
783 water-saturated clasts is shown as a dashed line and based on measured solid densities;  
784 deviations from this curve are assumed to result from either pore water leakage (low  
785 values) or excess water remaining on the clast (high values).

786

787 Fig. 2. Experimental data. (a) Examples of the rate of water loss and steam generation  
788 during an experimental run at 150°C of three D7 pumice cubes: #13 cube at 30% steam  
789 70% water, #14 cube at 50% steam 50% water, #15 cube at 70% steam 30% water. Filled  
790 symbols show the heating track of initially water-saturated cubes to pre-determined ratios  
791 of water and steam within the pores; symbols enclosed in squares denote saturation  
792 percentages after quenching of water-and-steam-filled clasts in water for 5 minutes. Open  
793 symbols show the comparable saturation levels for the same cubes when they had been  
794 dried, heated to 150°C, plunged in water, and weighed after 5 minutes. Shaded domain;  
795 pumice sufficiently water-saturated to sink. (b) Resaturation mass of the air-filled control  
796 experiments of the three 337-5 (80 vol% vesicles) cubes and three 339-8 (74 vol%  
797 vesicles) cubes showing higher degrees of water saturation with increasing temperature.

798

799 Fig. 3. Absorption factors after quenching of heated steam-charged pumice cubes (filled  
800 circles) and repeated experiments with dry air-filled cubes (open circles; colour identifies  
801 the same steam-charged cube). Each dot is the result of a single experiment. (a) D7, 80  
802 vol% vesicles, (b) 337-5, 80 vol% vesicles, (c) 337-1, 73 vol% vesicles, and, (d) 339-8,  
803 73 vol% vesicles. Yellow circles represent dry air-filled experimental runs at both higher  
804 and lower temperatures than the steam-filled runs. 70w/30s; represents 70% water, 30%  
805 steam. Labeled fields show the degree of absorption anticipated for **contraction** of air  
806 alone, **contraction + capillary forces**, and additional saturation due to the **steam-liquid**  
807 water phase change.

808

809 Fig. 4. Graphs of vesicularity and permeability for samples of submarine erupted and  
810 deposited rhyolitic pumice. (a) Connected vesicularity versus total vesicularity for  
811 pyroclastic pumice from Yali and Milos, Greece and Sumisu, Izu-Bonin Arc, (crosses),

812 and quench fragmented pumice from Sumisu (plus signs). Pumice clasts used in the  
813 experiments (solid symbols) lie at the high end of the vesicularity spectrum and are  
814 dominated by connected vesicles. (b) Permeability vs. total vesicularity for pyroclastic  
815 and quench fragmented pumice (as in a). Most samples are highly permeable ( $>10^{-13} \text{ m}^2$ ).  
816

817 Fig. 5. Uplifted submarine erupted and deposited pumice. (a) Elongate vesicular pumice  
818 block from Yali, Greece. (b) Internally fractured pumice block with a quenched margin  
819 from Milos, Greece. (c) Weakly stratified pumice lapilli from Yali, Greece. (d) Reversely  
820 graded pumice from Milos, Greece. Lower part; weakly stratified pumice lapilli, upper  
821 part; water-settled pumice blocks and ash. Scale bar, 5 m.  
822

823 Fig. 6. Theoretical cooling and specific gravity trajectories of submarine-erupted pumice  
824 clasts. (a) Calculated trajectories show saturation paths for pumice clasts of different  
825 vesicularities; the temperature at which pumice is sufficiently water-saturated to sink  
826 (shaded region) decreases as the initial clast vesicularity increases. (b) Calculated  
827 cooling and density trajectories for highly vesicular pumice (81 vol% vesicles) as a  
828 function of initial water depth; saturation temperature increases with increasing water  
829 depth because of changes in the temperature of the steam-to-liquid water phase transition.  
830

831 Fig. 7. Schematic cartoon of the saturation front required to allow pumice clasts with  
832 variable initial vesicularities (60, 77 and 85 vol%) to sink.  
833

Table 1 Location and properties of the pumice blocks.

| Sample | latitude | longitude | sample   | max    | variation in specific gravity |                      |             | porosity^ |     | vol%  |          |
|--------|----------|-----------|----------|--------|-------------------------------|----------------------|-------------|-----------|-----|-------|----------|
|        | (N)      | (E)       | depth    | length |                               | (kg/m <sup>3</sup> ) | theoretical | saturated | dry | total | isolated |
|        |          |           |          | (m)    | (cm)                          |                      |             |           |     | vol%  |          |
| D7*    | 30.2833  | 139.1833  | 1348-700 | 23     | 1.25±0.01                     | 1.25±0.05            | 0.45±0.03   | 80.5      | 2.0 |       |          |
| 337-1# | 31.6188  | 139.7227  | 1466     | 31     | 1.32±0.03                     | 1.33±0.07            | 0.6±0.03    | 72.6      | 2.4 |       |          |
| 337-5# | 31.6187  | 139.7240  | 1343     | 35     | 1.24±0.02                     | 1.24±0.02            | 0.44±0.03   | 80.2      | 3.0 |       |          |
| 339-8# | 31.5391  | 139.8369  | 323      | 46     | 1.33±0.03                     | 1.33±0.06            | 0.63±0.08   | 73.8      | 1.7 |       |          |

\*dredge, #ROV, <sup>^</sup>He pycnometer measurements

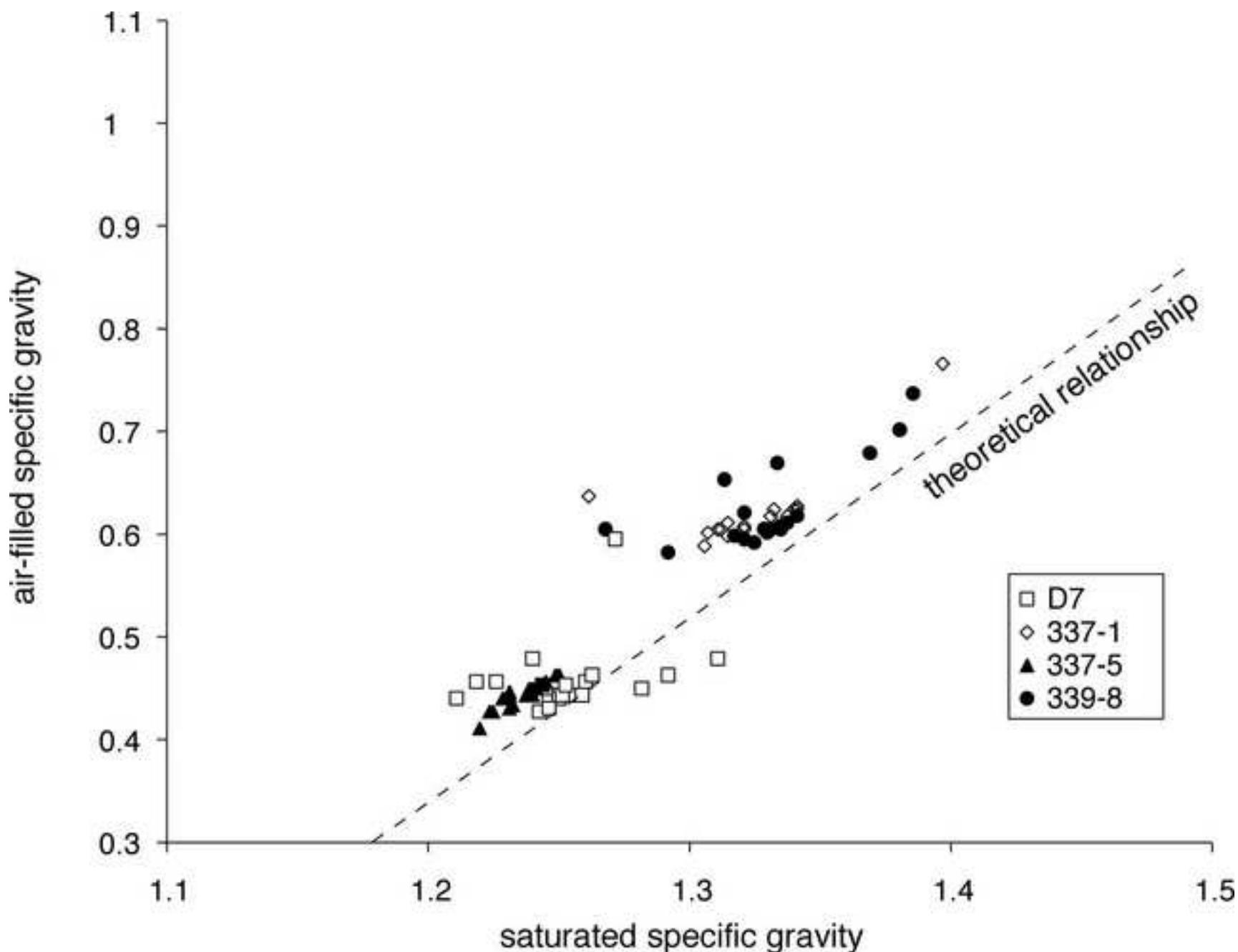
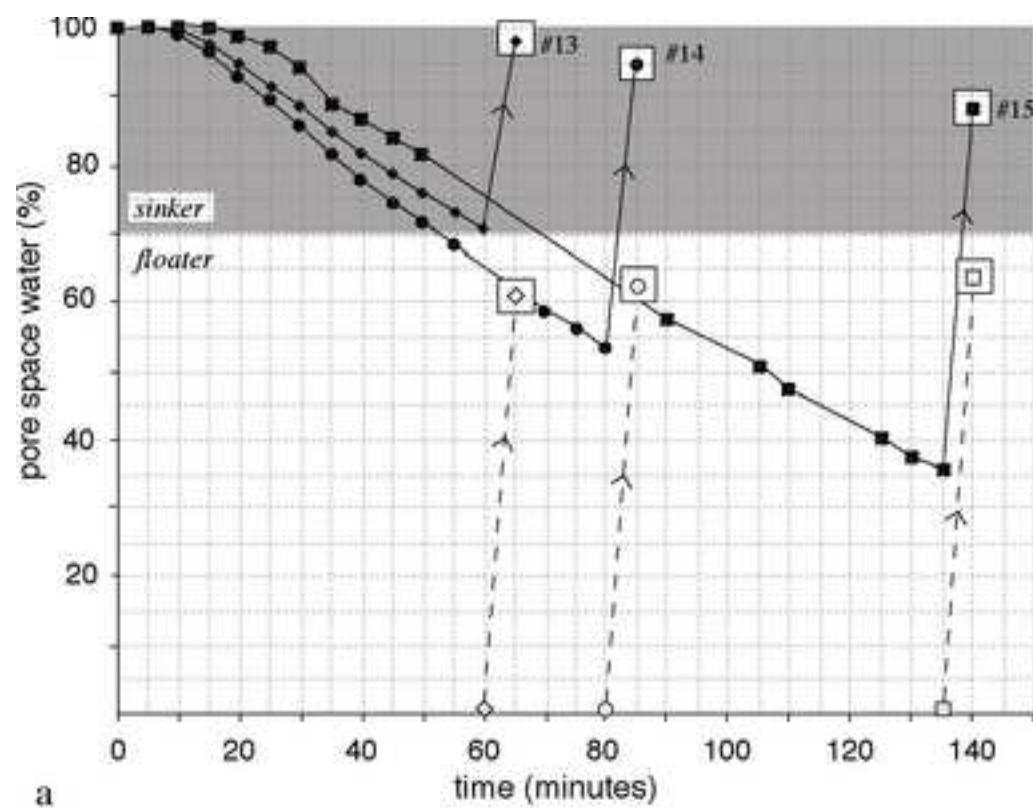
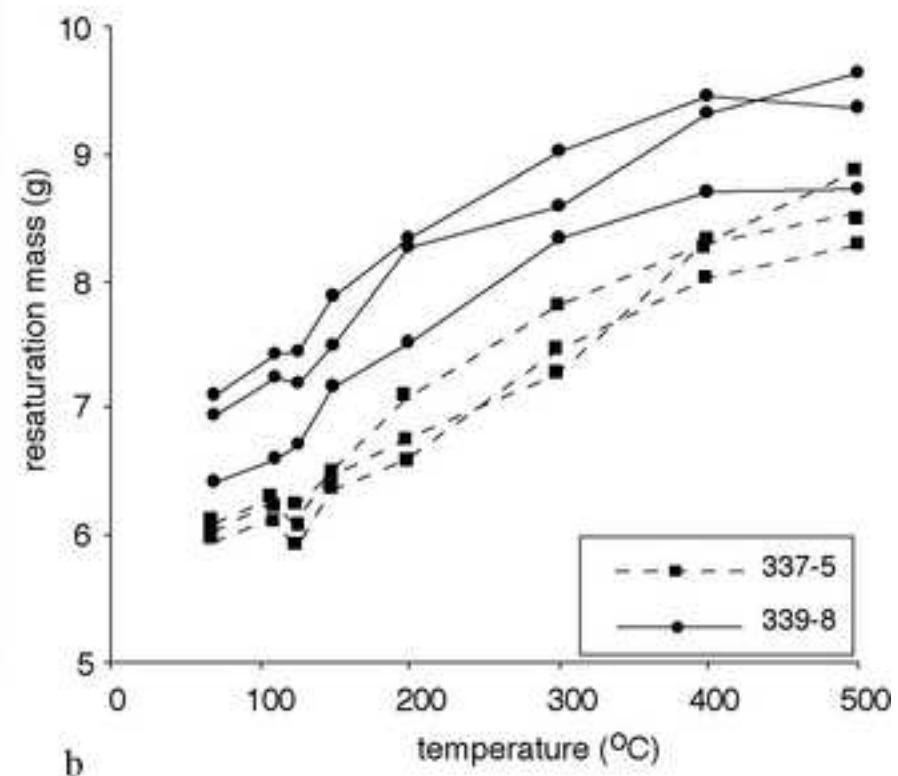


Figure 1

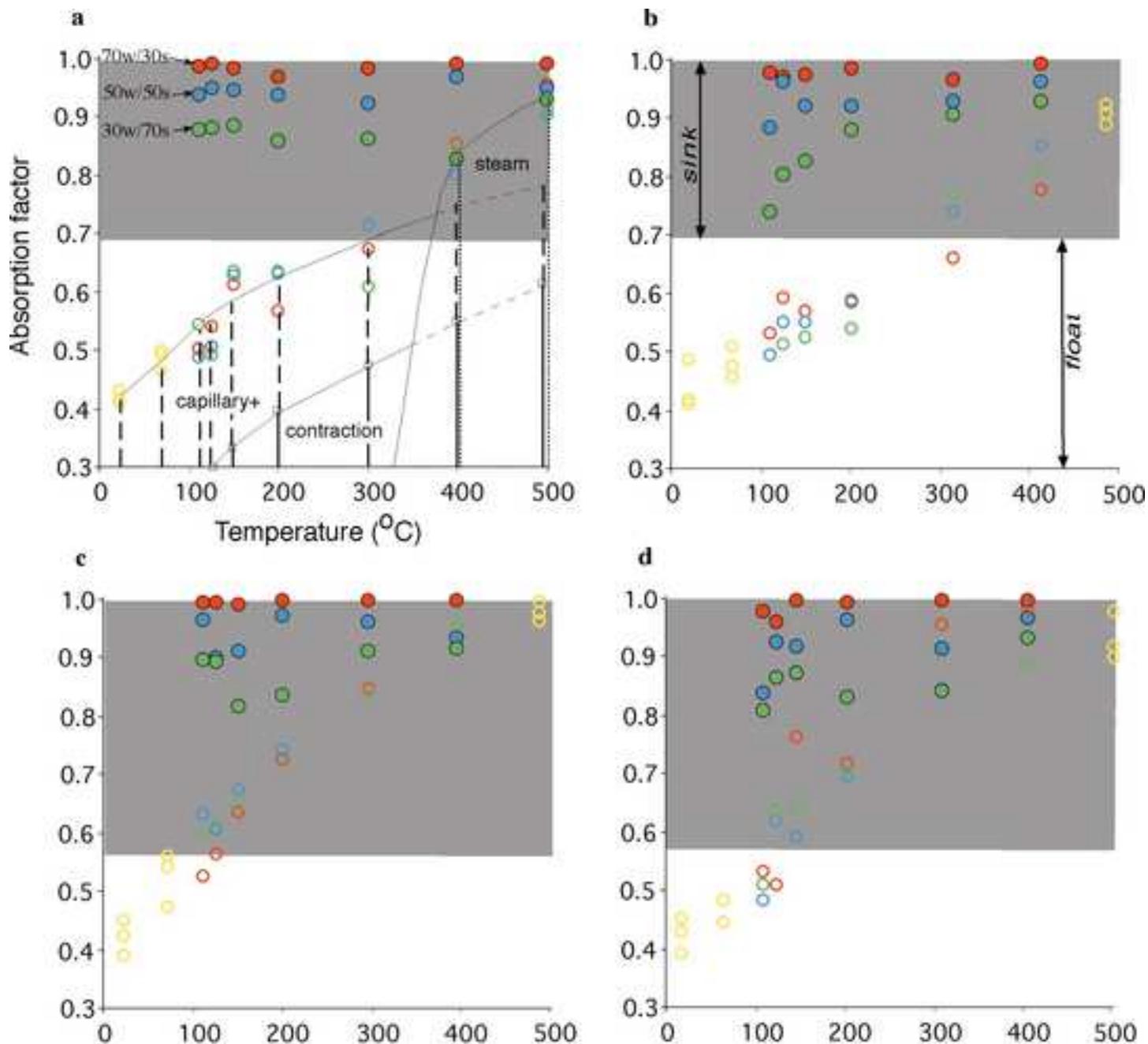


a



b

Figure 2

**Figure 3**

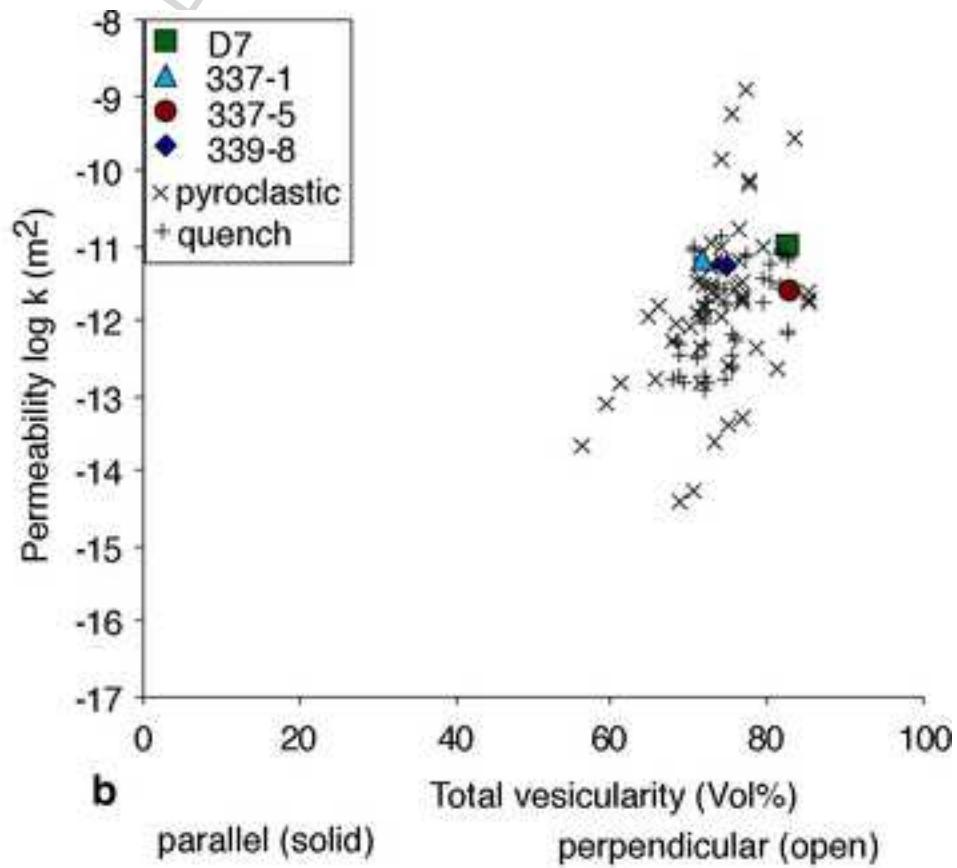
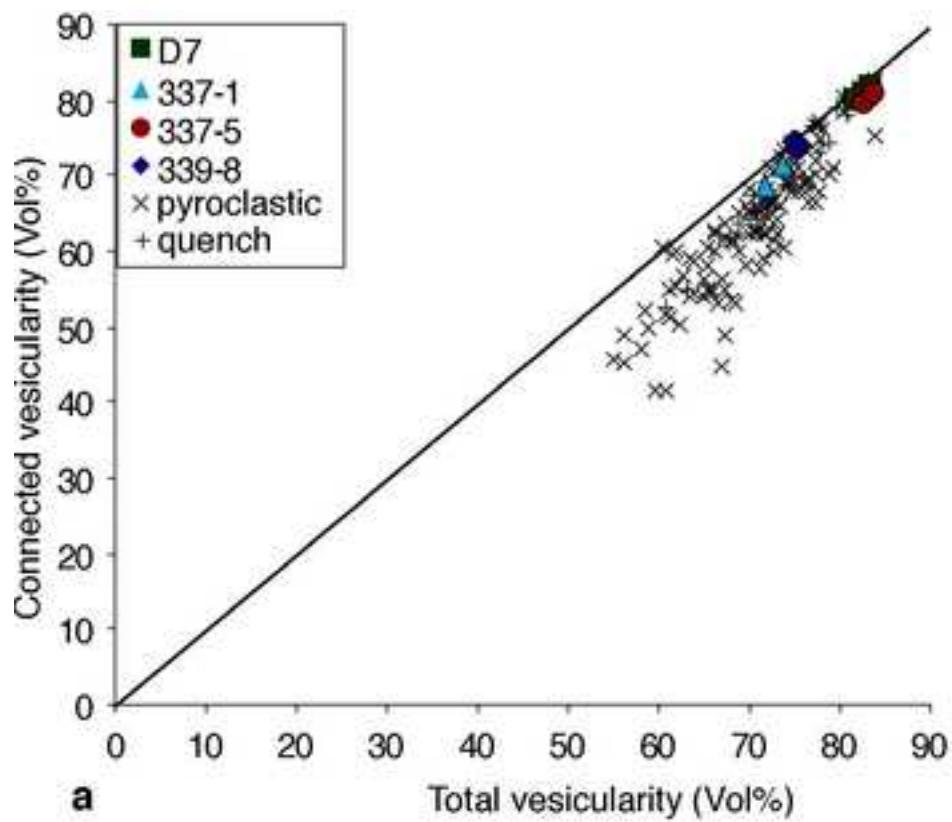
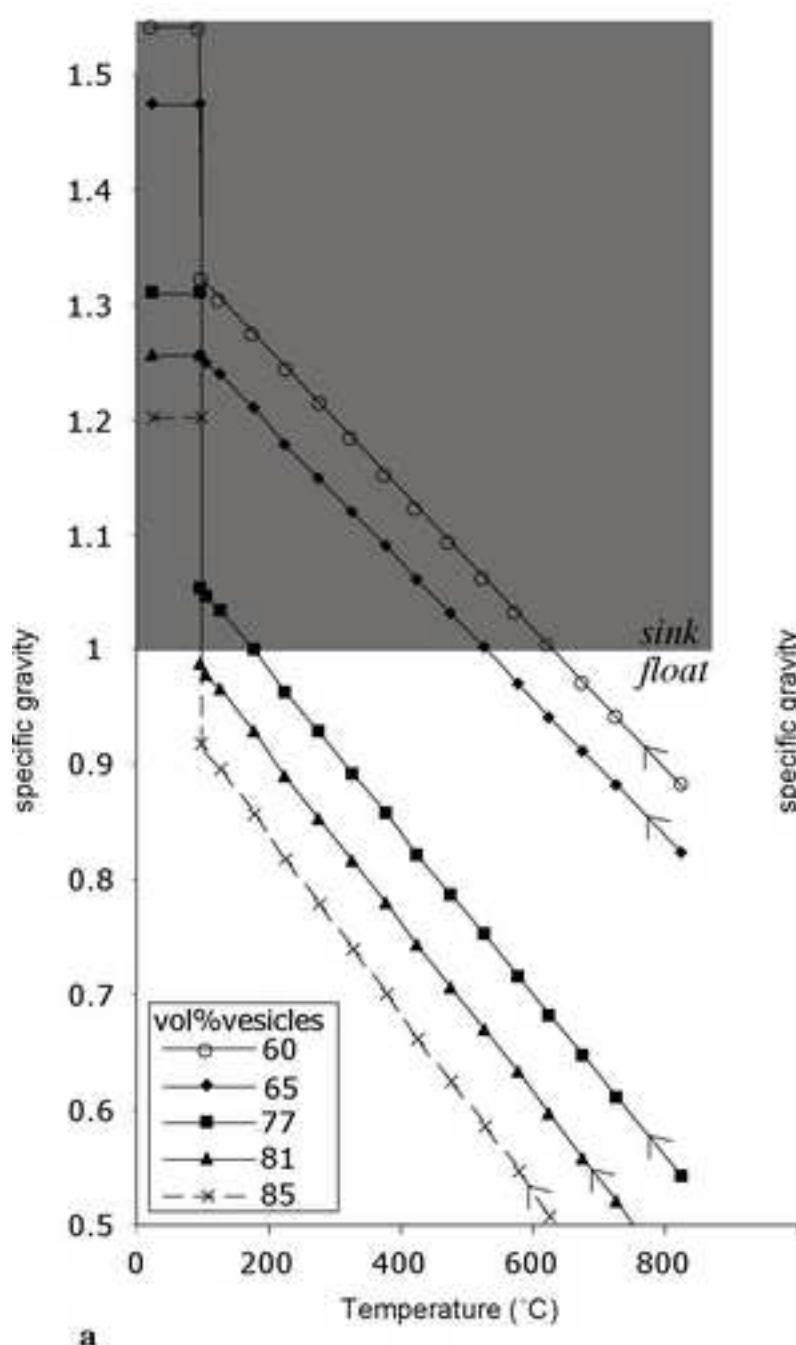
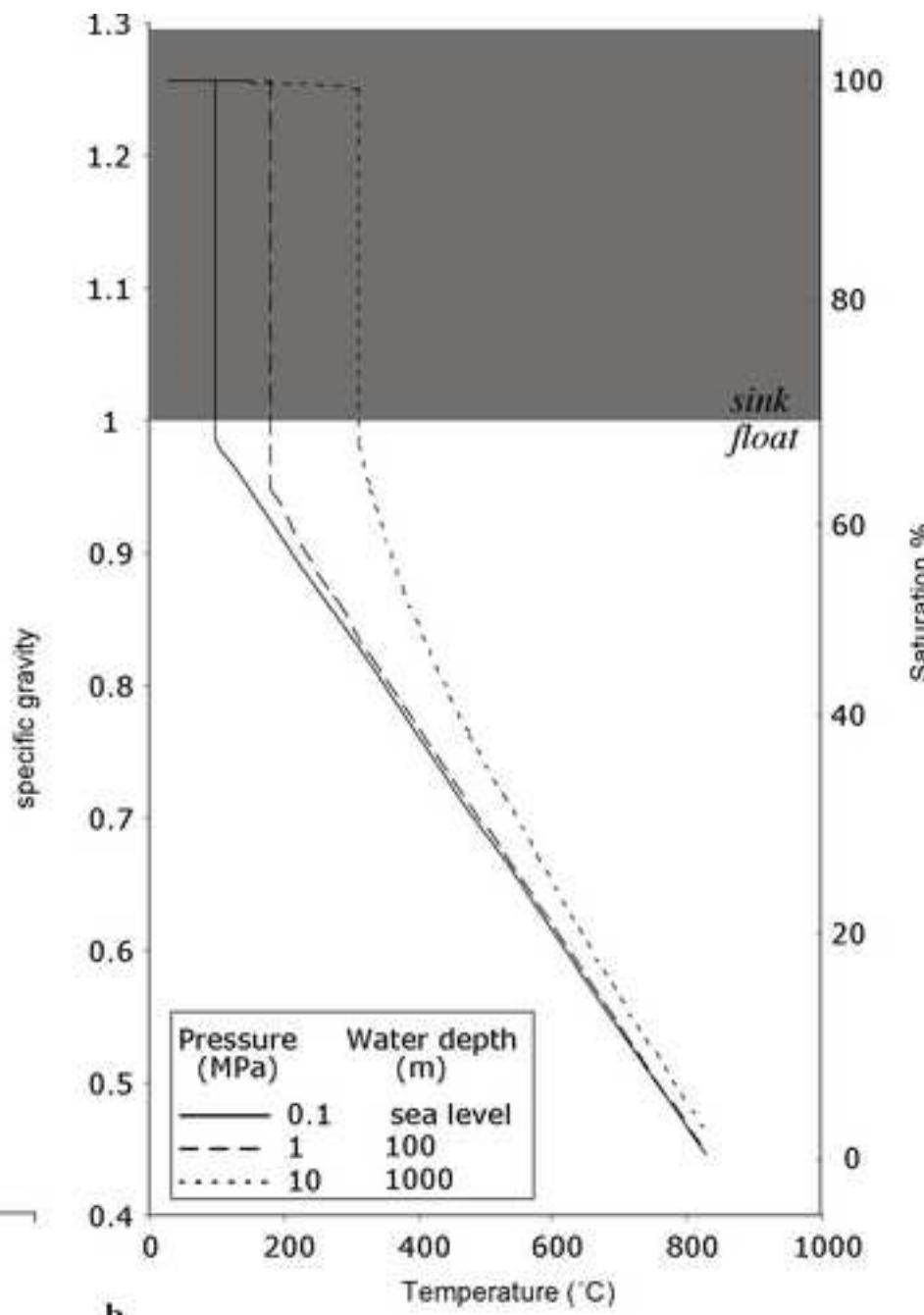


Figure 4

**a****b****c****d**



a



b

Figure 6

RIPT



Figure 7