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# PRECISION ORBITS OF 413 PHOTOGRAPHIC METEORS

by LUIGI G. JACCHIA and FRED L. WHIPPLE



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> FRED L. WHIPPLE, Director, Astrophysical Observatory, Smithsonian Institution.

Cambridge, Mass.

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# Precision Orbits of 413 Photographic Meteors

By LUIGI G. JACCHIA<sup>1</sup> and FRED L. WHIPPLE<sup>1</sup>

The 413 doubly photographed meteors discussed here represent a selection of the longest and brightest trails from 3.500 such meteors obtained in the Harvard Meteor Program. The meteors were selected to give the greatest precision in derived velocity and deceleration. in order to establish with high certainty the immediate origin of meteors in the visual range and to provide exact data for studies of meteoric processes, meteoroid characteristics, and the properties of the upper atmosphere. The present paper considers orbital characteristics and associated problems of meteoritic origin, while physical problems will be discussed by L. G. Jacchia in other papers. A preliminary discussion of 308 of the present meteors was presented previously (Whipple and Jacchia, 1957a).

#### The observational material

The meteor orbits presented here are based on precise reductions of selected photographs taken simultaneously at two Harvard stations in New Mexico with the Baker Super-Schmidt meteor cameras. The first of these cameras was installed during the summer of 1951 at Soledad Canyon, but the double-station program did not get under way until March 1952, when a second camera started operations at Dofia Ana. In July 1954 the cameras were moved to Sacramento Peak and Mayhill. All the meteors included in this paper were photographed prior to the move, between March 1952 and July 1954, with the exception of Nos. 4702 and 2961, which were photographed in September and October 1951 with a Super-Schmidt camera at

Soledad and smaller meteor cameras at Doña Ana. The Super-Schmidt meteor cameras and the details of the program have been described elsewhere (Jacchia and Whipple, 1956).

In all, approximately 4,500 meteors were photographed during this period, about 3,500 of them from both stations. Of these meteors, 413 were selected for accurate reduction on the basis of trail length and quality of image.

The shutters of the Super-Schmidt cameras have two 45° openings and rotate at 1,800 rpm; the meteor trail is thus interrupted 60 times a second and presents the aspect of a row of segments separated by wider breaks. In making the selection we deliberately chose only those meteors that were likely to yield excellent decelerations. On this basis we discarded nearly all meteor trails showing fewer than 20 clearly discernible segments and those whose segments were too closely spaced, as well as trails appearing against rich star fields or too faint to be measured with accuracy. The selected meteors have an average of 40 wellmeasured segments on the better of the two films, and 34 on the other, and for all but 17 meteors the instant of appearance was recorded visually. A secondary criterion for selection was that comparable numbers of meteors should be chosen in the low, the medium, and the highvelocity groups, and for each month of the year. For months particularly rich in meteors the standards of acceptance were set a little higher. so that the month in question should not exert an overwhelming weight in the analysis of seasonal effects on decelerations.

As a result of this selection, the orbits presented here do not represent a random sample, and this fact should be kept in mind in evaluating the analysis. Thus, while statistical corre-

<sup>&</sup>lt;sup>1</sup> Smithsonian Astrophysical Observatory and Harvard College Observatory, Cambridge, Mass.

lations between the various orbital elements are justified, frequency distributions of orbital elements should be accepted with some degree of caution. In particular, it should be remembered that by excluding meteors with closely spaced segments we have, in all likelihood, eliminated more of the low-velocity than of the high-velocity meteors. The bias introduced by our selection is added, of course, to the bias already inherent in meteor photography, allowed for in the calculated quantity, cosmic weight.

### **Reduction techniques**

A detailed description of the reduction methods for Super-Schmidt meteors has been given by the authors (Whipple and Jacchia, 1957b). For all but five meteors the radiant was determined from the intersection of the two great circles of motion of the meteor as seen from the two stations. The five exceptions were meteors for which the angle of intersection Q of the great circles was small enough to impair the accuracy of the solution by this method. For these meteors direct triangulation was used (Whipple and Jacchia, 1957b). When a good common point is available, this method can lead to quite accurate results.

The velocity  $V_{\infty}$  of the meteor outside the atmosphere was computed as a by-product of the deceleration; an equation of the type

$$D = a + bt + ce^{kt} \tag{1}$$

was fitted to the distances D on the meteor trajectory, observed in function of time t at the instants corresponding to shutter segments.

The parameter k is computed from four equidistant points on a graph, and a, b, and c are evaluated by least squares. The value of b, which represents the velocity of the meteor at  $t=-\infty$ , was taken as  $V_{\infty}$ . In general, the aim was to obtain decelerations greater than their inner probable error by a factor of 20 to 40; therefore when it appeared likely that the factor would be greater if a single solution were to be computed for the whole meteor, the trajectory was divided into two, three, or more sections and separate least-squares solutions were computed for each of them. In such cases the value of b from the earliest solution was taken as  $V_{\infty}$ . In practically all cases  $V_{\infty}$  was computed independently from each of the two trails, and a weighted mean taken.

### Sources of error

The main sources of error in the individual solutions are briefly described as follows.

The assumed instant of the meteor.-Without a recording aid the error of a time observation can be estimated at  $\pm 2$  seconds. After August 1952 the New Mexico observers used a printing chronograph, accurate to 0<sup>m</sup>.01. A comparison of the records from the two stations shows that when the same meteor was observed simultaneously by both stations (as happened for approximately three-quarters of all meteors), the recorded instants agreed within 0"01 to 0.02. Verv seldom did the discrepancy amount to 0"03. For average geometric conditions an error of 2 seconds in time is reflected in an error of 0.01 percent in the meteor velocity. In the reduction method based on the intersection of the circles of motion, the error varies as the inverse of  $\sin Q$ . The average value of sin Q for our meteors is approximately 0.3. Only 37 meteors had sin Q less than 0.1, and, as a rule, when  $\sin Q$  was found to be less than 0.03, direct triangulation was used, in which the error is independent of Q.

When no visual observations were available, the instant of the meteor had to be computed from one or more points that could be identified as common on both photographic trails. Under good conditions the error of such a determination is not more than 1 minute (0.3 percent in the velocities), but it can occasionally be as large as 6 minutes (one-half of the standard exposure time) when no definite common point can be found.

The determination of the radiant.—A source of error lies in the uncertainty with which the straight line, representing the great circle of motion of the meteor, can be determined in gnomonic projection. For a good meteor the error in the direction of motion is of the order of 10'', but 20'' is probably closer to the average. Under average conditions (center of visible trails 45° from the radiant; sin Q=0.3), an error of 10'' in the direction of each of the trails is reflected in a maximum error of 1' in the radiant position and in a relative error of 0.06 percent in the velocity. This error also varies as the inverse of sin Q; it does not apply when direct triangulation is used.

The extrapolation to  $V_{\infty}$ .—The inner probable error of  $V_{\infty}$ , as computed by the least-squares method for a great number of meteors, appears to be of the order of 0.01 percent for a good, long meteor, and close to 0.03 percent for an average good meteor. In the worst cases on record (short, poor meteors), this type of error amounts to 0.3 percent. These errors refer to a single photographic trail. The fact that a weighted mean was taken between two values of  $V_{\infty}$  should reduce the error in the final value; on the other hand, uncertainty of the parameter k of equation (1) should add a little to the error. It is quite safe to assume that, when the two effects are added together, the final error is not greater than the values given above for individual trails.

Shutter flutter.—After a number of Super-Schmidt meteors had been completely reduced, there was clear evidence that a "flutter" affected the rotation of all camera shutters. Although this instrumental trouble was later eliminated by the installation of more powerful motors, it was nevertheless present during all the period of time covered by the meteors included in this paper.

The shutter flutter was semiregular in character and exhibited widely different amplitudes, ranging mostly from zero to 5°, with a fundamental period of 0.23, but with occasional lapses into cycles half or twice that length. When two or more cycles of the flutter are covered by the photographic trail, its effect can easily be eliminated with relative confidence (Whipple and Jacchia, 1957b). For shorter trails, however, the process becomes more questionable, and a few meteors had to be rejected for this reason. The uncertainty in the correction for shutter flutter is, by a reasonable estimate, of the same order of magnitude as that arising from observational scatter; the two effects also depend in very similar manner on the duration of the meteor.

Speed of rotation of the shutters. The rotating shutters of the Super-Schmidt cameras are driven by synchronous motors fed by a 60-cycle a.c. current whose frequency is regulated by a quartz crystal. Theoretically the shutter speed should not vary more than 0.01 percent but occasional dips in speed as high as 0.1 percent have been observed. The shutter speed, always checked at the start and at the end of an observing night, and occasionally at intervals during the night, is recorded to the nearest tenth of one rpm. It is safe to assume that no error larger than 0.05 percent can come from this source.

### Orbital data

Table 1 presents orbital data for the 413 photographic meteors. The column heads have the following meanings:

- Trail No.: Number of trail photographed at the Doña Ana station.
- Day: Day of the month in Universal Time given to 0<sup>4</sup>01.
- Yr.: Year of observation minus 1900.
- Mo.: Number of the month of the observation.
- Sh. No.: Identification of associated meteor shower, if any, as indicated in tables 3 and 4; the letter "Q" after the number indicates a questionable association.
- a: Semimajor axis, in a.u.
- e: Eccentricity.
- q: Perihelion distance, in a.u.
- q': Aphelion distance, in a.u.
- ω: Argument of perihelion; angle from the ascending node to perihelion along direction of motion, in degrees. Equinox 1950.0.
- $\Omega$ : Longitude of the ascending node along the ecliptic from the vernal equinox of 1950.0, in degrees.
- *i*: Inclination of the orbit plane to the ecliptic 1950.0, in degrees.
- $\pi$ : Longitude of perihelion  $\pi = \omega + \Omega$ , in degrees.
- True radiant: Radiant after correction for the earth's attraction in degrees and minutes:  $\alpha$ , right ascension;  $\delta$ , declination; equinox 1950.0.
- $V_{\infty}$ : Velocity with respect to the stations, corrected for atmospheric drag, in km/sec.
- $V_{\sigma}$ : Velocity with respect to the center of the earth, corrected for earth's attraction, in km/sec.
- $V_{H}$ : Heliocentric velocity, fully corrected, in km/sec.

#### Day Ir. Mo. Sh. ٩! ω ይ 1 Trail 8 . q -No. No. .890 45.4 1+665 .465 2.441 100+3 38.7 9880 1.31 54 145.7 1 .727 9888 54 3.493 .952 6.033 202.3 280.4 18.8 122.7 ī 88 9900 2.27 54 2.900 . 690 .898 4.903 218.1 281.3 29.5 139.3 1 3.21 9917 54 1.861 .533 .870 2.852 48.1 102.2 7.8 150.3 1 9925 54 6.650 .958 .281 13.020 117.4 102-4 57.5 219.7 3.32 1 10 .682 .970 5.123 165.2 282.5 68.6 87.6 0045 54 3-046 3.42 1 9951 11.480 .969 .361 22.600 286.6 282.5 124.6 209.1 3.45 54 1 9953 3.45 54 10 2.906 .664 .978 4.833 170.3 282.5 72.7 92.8 1 9955 3.45 54 1 10 3.119 .685 .983 5 . 254 180.4 282.5 72.6 102.9 9974 3-48 54 1 10 2.999 . 674 .978 5.020 170.4 282.5 72.5 92.9 169.6 9983 3.49 54 3.002 .675 .977 5.027 282.5 72.4 92.1 1 10 .975 9985 3.50 54 1 3.074 .683 5 . 173 168.3 282.5 70.8 90.8 10 9997 3.52 54 3.274 .701 .980 5.568 282.6 73.4 1 172.8 95.4 10 10006 4.45 54 3.170 .692 .975 5.364 168.6 283.5 72.5 92.1 1 10 10012 4.53 54 1 18.920 .971 .556 37.280 263.2 283.6 136.4 186.8 30 3.955 10064 9-42 54 1 2.198 .799 - 441 103-9 108.6 13.8 212.5 .977 3.097 11.4 109.6 13.3 10.13 53 .520 6062 1 2.037 120.9 11.37 .770 .542 4.169 91.8 110.6 10070 54 2.355 1 6.9 202.4 6093 13.39 53 ī 36.467 .975 .920 72.020 150.2 292.9 67.5 83.1 100 6095 13.41 53 1 .839 .177 .690 .987 349.1 292.9 56.3 282.0 6105 13.46 53 1 100 2.361 .630 .874 3.850 135.4 293.0 75.2 68.4 6218 16.44 53 1 216.638 .995 .976 432.300 169.6 296.0 161.5 105.6 - 99.500 6275 20.31 53 1 31 - 49.400 1.015 .737 239.9 299.9 113.6 179.8 6329 23.38 53 1 320 2.413 .725 -664 4.162 77.0 123.1 4.2 200.0 6376 5.14 53 2 33 2.707 .858 -384 5.030 108.8 136.0 0.8 244.8 .959 .697 6398 10.27 53 2 16.870 33.050 246.4 321.2 15.8 207.6 6429 12.47 53 .896 .131 2.390 326.7 323.4 14.4 290.1 2 1.261 9.229 .893 17.470 148.1 6433 12.49 53 2 34 .986 184.7 323.4 130.5 159.100 .928 28.5 143.5 171.9 6437 12.50 53 2 80.030 .988 154.5 18.40 6491 53 2 .737 .805 5.320 235.8 329.4 19.3 205.3 3.064 53 34 11.089 .916 . 933 151.7 332.5 125.0 6546 21.46 2 21.250 124.2 10173 27.16 54 1.889 - 550 -850 2.928 233.2 338.0 2.5 211.1 2 .799 10218 5.30 54 2.561 .515 4.607 274.7 0.8 258.9 344.1 3 5.33 32.480 .984 10222 54 3 .533 64.420 266.2 344 . 2 162.1 250.3 5.45 54 .926 120.6 10240 3 3.695 .272 7.117 164.3 38.6 284.9 10273 6.37 54 3 2.867 .658 .980 4.755 194.5 345.2 60.1 179.7 54 110 .888 .252 165.3 2.7 291.2 10247 6.42 3 2.239 4.225 126.0 10252 6.48 .989 54 3 88.640 .966 176.300 198.7 184.0 10255 6.49 54 3 1.935 .587 .800 3.071 118.4 345.3 18.3 103.7 9815 8.29 54 3 7.816 .894 14.800 229.6 111.2 216.7 .828 347.1 . 549 10279 -446 8.44 54 3 .987 1.529 123.8 291.0 167.3 1.6 8.47 110 10281 54 3 3.289 .822 .585 5.993 84.9 167.3 7.7 252.2 9.47 9804 54 -391.457 .974 -783.875 3 1.002 195.9 348.3 169.0 184.2 2.790 53 6795 12.22 3 . 645 .993 4.590 183.2 351.3 17.7 174.5 6802 53 238.6 12.27 3 20.780 .967 .694 40.860 247.3 351.4 95.1 6811 53 10.670 .984 •175 155.9 12.30 3 21.160 131.4 171.4 302.8 36 .941 6842 13.38 53 3 36 2.671 •159 5.183 137.2 172.5 147.2 309.6 6882 14.30 53 3 37 1.528 .351 .992 2.064 187.0 353.1 7.2 180.1 6904 14.44 53 3 4.416 .913 •386 8.445 73.6 353.5 128.9 67.1 6915 18.21 53 3 38(39,40) 3.780 . 786 .810 6.760 234.8 357.3 12.6 232.0 53 6932 18.34 3 5-347 .820 .963 9.731 201.9 357.4 46.2 199.3 6949 18.43 53 110 3 2.461 .790 •518 4.404 275.0 357.5 5.4 272.5 6959 18.47 53 40(38,39) -156.200 - INF 3 1.004 .556 96.8 357.5 76.7 94.3 6961 19.22 53 .976 197.7 3 2.085 .532 3.194 19.6 178.1 25.9 38(39,40) 2.908 6971 19.31 53 3 .731 .783 5.033 240.4 358.4 11.5 238.8 6992 19.39 53 8.491 .913 3 .736 16.250 243.1 358.4 9.5 241.5 6998 19.43 53 10.280 .948 3 •536 20.020 87.1 178.5 9.0 265.6

.880

.663

.722

.864

2.913

3.586

.104

.983

.996

1.625

4.843

6.176

156+0

14.9

180.0

178.5

179.5

359.4

334.5

194.4

179.4

2.9

12.0

39.3

7002

3053

7022

19.44

20.16

20.35

53

52

53

3 41(42)

3 44

3 45

for double-station meteors

Trail	True I	adiant	V _	V.	٧.,	λ	Sin Q	C.V.	ĸ	м	•	Onel.
No.	a	δ	00	U	н				-	τ'p	•	diment .
	· · ·	• •								-		
9880	106 45	-45 12	25.97	23.49	35.64	82.0	- 039	9.90	24	-0.1	1 00	2.0
9888	19 49	48 57	18 92	15 45	20 25	114 0	171	10.10		-0-1	1477	2.0
7000	04 22	00 27	10.75	19049	37.33	114.0	+1/1	10.10	• 34	0.2	2.5/6	1.0
9900	00 33	05 51	23.01	21.14	20.09	90.0	. 200	11+20	•20	0+2	1.14	1.0
9917	80 Z	0 4	16.44	12.07	36.42	111.1	.173	8.00	21	1.8	1.17	1.5
9925	126 0	- 7 33	44.57	43.08	40+85	65.0	• 058	10.50	1.49	-1.2	. 46	2.0
											• ••	
0045	224 49	49 15	41.45	20.68	29.90	66 0	26.2	2 5 4	21			
0051	144 25	28 21	10.40	59.00	30.00	03.9	.202	2.50	•21	0.4	+42	1+2
9921	100 35	20 21	60.40	22.35	41+53	41+0	• 249	4+00	1.86	0+0	• 29	3.0
9953	229 21	48 48	43+15	41+45	38.70	63.0	• 299	2.00	•16	0.4	.42	2.5
9955	225 16	51 32	43.25	41.58	38.96	63.4	A228	1.70	.22	0.7	- 36	3.0
9974	229 37	48 57	43.14	A1.47	38.82	63.3	. 224	2.00	.19	-1.0	42	1.0
		40 21		41041	20005	0,00	•	2.00	•17	-1.0	.02	1+0
9983	230 5	48 48	43.07	41+40	38.82	63+4	• 230	Z+00	•19	-1.3	• 50	1.5
9985	231 56	49 14	42.40	40.71	38.91	64.5	.167	2.20	•21	-0.4	.45	2.0
9997	228 22	49 19	43.72	42.10	39.14	63.0	.353	1.80	.27	1.1	. 35	2.0
10006	231 12	48 20	43.30	A1.61	39.02	42.5	. 277	2.10	. 24	0.4	50	1 6
10000	176 47	22 45	45.50	41.001	57002	03.9		2.10	• 2 •	0.4	• 50	1.5
10012	112 41	23 43	04+02	03.13	41+20	33.3	• 764	2.30	2.10	~1+0	•37	1.5
10064	116 52	79	29.01	27.05	37.40	81.2	• 356	7.90	•29	-0.6	• 58	1.5
6062	58 51	-35 19	15.33	10.51	36.97	122.3	. 191	6.62	19	1.2	.58	1.0
10070	112 58	12 3	26.03	22.72	37.74	87.9	245	4.90	. 26	2.2	1 44	1.0
6003	252 10	42 61	43 60	41 70	42.14			4070		0.2	1.40	1.0
6093	252 10	42 21	43.30	41+/8	42.10	07+5	.219	4.4/	2.40	0+7	• 51	2.0
6095	222 57	43 51	29.73	27.31	27.30	56.3	• 322	INF	- •92	-0.3	.69	1.0
6105	243 44	35 56	43.95	42.22	37.77	60-1	. 344	4.27	e02	0-7	. 67	2-0
6218	210 45	- 1 2	72 79	71 67	43 40	11 2	112	10	2 00	1 4	4.7	1 6
0210	210 45	- 1 3	12.10	11.01	42.40	11.02	•115	•10	3.70	-1+4	• • 4	1.9
6215	198 44	29 19	61.60	60+26	42.65	41.6	.291	2.80	INF	-1+1	• > >	2.0
6329	117 52	14 0	22.70	20.06	37.86	95.5	•412	3.70	•18	1.7	• 65	1.0
6376	147 15	12 27	31.67	29.30	38.34	80.2	.260	• 39	.55	-0.1	.89	1.0
				_			_			-		
1000	112 11		27 25	a. a.			(12	0.00	1 00	2.0	3 6 9	1
0398	142 14	38 51	21033	24.95	41+/2	97.9	•412	9.29	1.90	-2.9	1.40	1+0
6429	174 21	9 21	35+40	33.82	33+04	61.9	•652	5.24	• 36	-0.1	•48	1.0
6433	236 25	9 46	66.06	64.97	41.22	28.9	.101	• 39	1.21	-0+7	•40	1.5
6437	217 2	-30 1	71.07	70.20	42.23	16.8	.226	.33	3.14	-0.6	.45	3.0
4401	155 15	40 30	22.49	10.93	38.77	99.5	. 157	13.01	. 31	0.4	.82	1.0
0471	122 12	47 50	22.07	17073	20.011	7703	+131	13.01	• 51	0.4	.02	1.0
6546	254 53	8 54	64.45	63.22	41.37	33.0	• 207	1.06	1+40	-0.6	•40	1.5
10173	142 17	22 8	17.07	12.73	36.33	109.4	.395	2.60	- •19	1.4	.68	1.5
10218	168 8	6 4	27.44	25.09	37.95	86.6	.234	.50	. 36	0.4	.65	1.5
10222	228 5	- 0 22	67 00	44 40	41 94	26.2	108	. 90	2.69	-0.3	47	2.0
10222	220 3	- 9 23	07.90	00.07	41+74	20.3	• 108	• 70	2.037	-0.5	• • /	5+0
10240	176 35	-21 17	39+51	38.18	39.33	69.2	•311	10+/0	• 9 9	0+9	1+04	1+0
10273	252 23	49 14	37.10	35.17	38.43	71.8	.173	2.60	+14	-0.2	• 59	3.0
10247	180 59	- 2 16	34.49	32.84	37.29	72.6	.117	1.10	.57	0.1	.47	3.0
10257	250 51	20 10	55 30	54 04	42 14	50.0	124	1.50	2.21	-1.4	. 27	2.0
10252	250 51	28 19	22020	24+04	42.14	20.7	• 1 3 4	1050	3021	-1.0	• • • •	2.00
10255	337 46	32 36	20.66	17.06	30.44	97.7	. 239	13.00	- +13	-0.0	• 91	2.0
9815	242 22	16 37	59.73	58.32	40.89	41.3	•234	Z+40	1.15	-2.3	• 38 G	1+5
10279	182 55	- 3 41	20.56	17.55	29.79	72.3	.357	1.50	47	2.4	.97	1.5
10201	162 1	2 25	26 47	24 42	38 03	90.8	474	5.30	. 53	0.3	. 90	1.5
10201	103 1	- 5 25	20.41	67076	50.75	· · · · ·		11	245	2.0		2.2
9804	252 40	-16 2	12.18	/1.80	42.21	1 + 1	•072	• 1 1	INF	-3.0	+ 24	2.0
6795	101 53	83 11	17.39	13.42	38.29	118.9	•274	4.20	•11	-0.1	•28	Z•0
6802	235 33	22 25	54.84	53.36	41.72	51+2	• 238	4.50	2.09	0.9	• 39	2.0
6011			(1. 25		41 33	28 0	012	2.20	2.11	0.9	27	2 0
0011	211 21	-22 2	01.22	24.40	41+23	30.7	•015	2.20	2011	0.7	• 5 7	3.0
6842	218 40	-24 47	57.90	56.72	38.09	38+4	•111	3.10	• 74	0.0	• 4 4	4.5
6882	112 31	65 11	12.72	6.41	34.68	133.5	.346	2.24	- •50	2.2	1.12	1.0
6904	294 44	- 1 11	59.86	58.46	39.77	38.7	.176	3.60	.98	0.8	.56	1.0
6015	171 45		20.26	10 00	20 22	105 1	544	12.90	. 50	2.2	. 45	1.5
0915	1/1 42	30 32	20.30	10.00	37036	102+1	• 200	12.070	• 20		• • • •	
6932	240 53	58 52	31.77	29.62	40.18	84.9	•248	5.14	• 73	0.3	•61	1.0
6949	182 48	5 32	27-07	24.97	37.68	86-2	•442	3.60	• 32	-0+5	1.30	1.0
6959	308 3	22 22	48.71	47.09	42.24	61-9	.276	7.70	INF	-0-5	.73	2.0
60737	500 5	23 23	40011		72020	00.0	2.02	7.20	17	0.8	1.90	1.0
0701	11/ 4	-52 15	20.12	10.94	30.01	77.7	• 202	1.20		0.0	1.70	1.0
6971	174 46	26 20	21.60	18.59	38+40	102•Z	• • 7 5	¥•40	•21	TeA	• 38	∠•0
6992	172 12	20 1	24-68	22.30	40.93	102.3	.450	6.90	1+27	2.1	.87	1.0
6998	174 16		20.25	28.44	41.15	89-6	.378	4.90	1.58	1.3	.97	1.0
70.00	714 15	- 0 0	50.63	20040	77 12	55 1	. 202	1.20	.13	1.2	. 52	2.5
1002	210 4	-13 39	31+40	27.22	21.40	52+1	• 376	1.20		102		2
3053	113 35	-21 29	16.10	11.80	38.41	128.8	• 6 0 5	2.23	+10	-0+2	2.02	3.0
7022	267 7	67 30	27.29	24.78	39.14	90.9	.316	2.10	• 35	1.1	•74	1.0

NO. 4

Day	ĭr.	Mo. Sh. No.		e	q	ď,	۵	ß	i	R
20.38	53	3	16.784	. 957	.723	32.845	243.9	359.4	56.6	243.4
20.30	53	3 4 3	4.771	. 794	985	8.558	193.1	359.4	150.0	192.5
20.45	53	3 38/30.40	1 2.553	.685	.804	4.302	238.4	359.5	19.3	237.9
20.47	53	3	39.550	.984	•648	78.460	252.9	359.5	67.7	252.4
21.35	53	3	2.847	• 702	.850	4.845	50.0	180•4	5.7	230.4
21.38	53	3	53.050	.983	.879	105.200	220.3	0•4	93.5	220.7
21.40	52	3	1.457	.941	.086	2.829	332.3	0.7	15.6	333.0
21.41	52	3	61.397	.997	•158	122.637	133.3	180.7	104.5	314.0
22.41	52	3 39(38,40	) 2.638	.654	•912	4.364	218.2	1.7	7.0	219.9
26.27	54	3 37	1.541	• 353	.997	2.084	183.0	5.0	9•3	188.0
28.34	52	3 4 5	2.938	•663	.989	4.886	167.6	7.6	37.2	175.2
30.39	52	3	219.000	•998	•475	437.500	92.9	189.6	116.6	282•5
1.30	- 54	4 47 (48)	3.078	•841	.489	5.667	276.8	11.0	9.7	287.8
1.33	52	4 (43)	6.358	.851	•946	11.770	207.9	11.5	150•3	219.5
1.34	54	4 46	2.716	•750	•678	4.753	75.6	191.0	17.6	266.6
1.37	54	4 48(47)	3.063	.844	.479	5.647	98.0	191.0	19.8	289.0
2.34	54	4 -	6.080	1.002	•103	- INF	142.4	192.0	24.9	334.4
2.37	54	4 42(41)	1.740	•859	•246	3.237	129.2	192.0	8•7	321.3
2.42	54	4 39(38+40	2.835	• 65 7	•971	4.698	201.9	12+1	5.7	214.0
3.13	23	4 30(3994)	2.002	• 688	•893	4+830	222.4	13.0	9.5	232+5
3.19	53	4	3.470	.744	.891	6.060	221.9	13.1	36.0	235.0
3.45	52	4	- INF	1.000	•972	- INF	160.7	13.6	82.3	174 • 3
4.17	53	4 49	2.473	.882	•291	4.656	300.9	$14 \cdot 1$	1.7	314.9
4.17	53	4 52	3.142	• 690	•975	5.309	200•4	14 • 1	16•2	214.4
5.19	54	4 44	2.620	• 635	•957	4.284	27.5	194.8	13.2	222•3
5.38	54	4 42(41)	2.577	.896	•267	4.886	123.4	195.0	6.0	318.4
5.41	54	4 42(41)	3.251	.894	.343	6.159	113.1	195.0	15.2	308.1
6.23	54	4	42•680	• 990	•419	84 • 940	279.7	15.8	63.2	295•5
6.26	54	4 46	2.804	•738	•734	4.873	68.1	195.9	16.5	263.9
6.29	54	4	2.594	•671	•852	4.335	50.9	195.9	24+1	246.8
7.28	53	4	1.980	.809	•378	3.580	293.0	17.1	27.4	310.1
7.46	54	4 60	39.300	• 976	•942	77.658	208.3	17.0	86.1	225 • 3
9 • 37	53	4 50	2.669	•746	•678	4.660	75.9	199.2	0.6	275•1
9•38	53	4 40 (38,39	) INF	1.000	•692	INF	112.5	19+2	79.9	131•7
10•14	53	4	2.800	• 679	•899	4.700	138.3	19•9	12.8	158•2
10.27	53	4 50	2.035	•688	•634	3.436	264•2	20•1	1.3	284•3
10.33	53	4	62•340	•989	•679	124.002	249.4	20•1	51.5	269•6
10.35	53	4	19.770	•963	•728	38.810	243.7	20.1	27.1	263.8
10.47	54	4 40(38,39)	167.700	•996	•677	334.700	110.5	20+0	80+4	130•4
11.18	53	4 51	2.606	•618	•996	4.216	169.8	21.0	2.8	190•8
11.20	53	4 48 (47)	6.830	•925	•511	13.150	91.2	201.0	17.9	292.1
11+34	53	4 50	2.295	• 6 9 4	• 703	3.887	254+3	21+1	4.2	215+4
12+42	54	4 52	3+163	•683	1.003	5.323	179.4	21+9	19.0	201•3
13.38	53	4 49	2.381	•831	•401	4.360	288.8	23+1	14.4	311+9
13+40	53	4	15.550	•989	•164	30.940	133.0	203.1	156+8	336 • 2
15.27	53	4	3.010	•729	•815	5.204	236.3	25.0	28.4	261.2
15.28	53	4 49	2.787	•861	.388	5.186	289.0	25.0	2 • 3	314•0
15 • 32	53	4	21.938	•990	•227	43.649	123.8	205.0	49.0	328.8
16+13	53	4 50	4.854	•834	•806	8 • 902	55.5	205 • 8	5.2	261+3
16+15	53	4 50	2.481	•695	• 757	4.205	66•4	205+8	3.0	272•2

2.157

2.717

28.233

10.117

31.640

10.208 1.706 3.037

2.729

10.353

16.30 53 4 50

53 4 45

53 4

52 4 6

52 4 6

16.33

21.44

22.35

22.43

23.32

23.36

28.45

1.36

7392

7454

3271

3217

3228

3234 3250

10127

3265

.707

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.971

•907 •765 •841 •907

• 920

•631

.994

•305

.919

.915

.946

•401 •484

.254

.833

3.683

4.439

56.160

19.316

62.360

19.471

3.011 5.591 5.204

19.874

26.0

26.0 31.0

32.1

32.2

33•1

33•1

36•0 37•6 40•9

264.0

167.3

66.4

215.0

215.2

208.9

292•8 277•9 304•9

129.6

3•2 41•2

68.4

78.5

79.1

63.8

14.9 9.8 31.7

64.3

290.0

193.3

97.4

247.1

247.4

242.0

325•9 313•9

342•4 170•5

TABLE 1.-Basic orbital data

Trail No.	True	radiant 5	~~	v <sub>G</sub>	v <sub>H</sub>	λ	Sin Q	C • W •	K	мр	t	Qual.
7026	223 37	37 15	39.99	38.33	41.55	73.9	.778	9.10	1.88	0.8	- 68	2.0
5688	265 37	- 6 14	68.64	67.42	39.92	17.4	.125	.24	.62	-5.7	1.166	1.0
7040	186 27	37 13	22.15	19.42	37.84	98.0	.238	13.40	.14	0.6	.53	1.0
7044	227 47	30 22	44.95	43.64	41.91	66.5	.544	8.20	2.68	-0.9	. 35	1.0
7046	154 4	- 3 37	18.72	15.39	38.31	111.5	.439	5.60	•21	1.1	.94	2.5
7052	252 12	25 59	54.40	53.03	41.98	52.2	.318	2.90	2.80	-0.3	. 28	2.0
3072	209 36	- 6 43	38.90	37.34	34-21	60.0	•137	4+71	•68	-0.6	• 45	3.0
3074	213 11	-31 51	55.35	54.27	42.00	50+2	.188	7.23	3.68	-0.8	.53	1.5
3076	159 27	30 30	16.82	13.00	37.98	119+4	•072	6.63	•10	0.9	1.33	3.0
10342	120 49	12 22	13.15	/•1/	34+60	127•4	•612	1.70	- •49	1.3	. 98	1+0
3088	288 6	68 5	25.93	23.28	38.38	91.7	.282	3.56	.16	1.2	1.01	1.0
3037	234 47	-46 27	59.92	58.84	42.07	42+6	•155	4.20	4.31	0.2	•97G	3.0
10358	197 50	3 20	29.43	27.21	38 • 54	84.9	•024	5.40	• 5 5	1.1	. 86	3.0
3024	272 59	- 6 36	68.85	67.58	40+42	18.4	.155	+45	• 90	0+4	•70	2.0
10365	176 11	-26 35	25.04	22.64	38.04	92+0	•270	11.70	•28	1.3	1.17	1.5
10106	189 0	-24 53	30.71	28.81	38.52	82.2	.253	9.80	• 56	-0.2	1.15	2.0
10380	210 28	-20 13	45.93	44.54	42.28	65.9	•030	5.70	INF	-0.2	.34	3.0
10384	206 16	-16 47	33.38	31.56	35.55	70.8	•020	3.80	• 36	-0.1	1.34	3.0
10394	150 56	33 49	15.11	10.68	38.21	136.1	+ 004	3.90	+14	1.4	1.29	3.0
7067	176 28	28 13	18,58	14.63	38.24	114.6	.387	7.70	•19	0.5	•65	1+0
7069	222 18	49 15	27.65	25.07	38.95	90.1	.322	10.10	•37	0.7	•70	2.0
3000	288 19	37 0	49.58	48.17	42.10	60.0	.311	1.86	INF	-0.9	• 42	2.0
7073	206 31	- 9 40	34.14	31.94	37.60	75 • 0	•170	•73	•60	1+7	• 72	1.5
7075	175 48	57 23	18.04	14.10	38.60	118.9	• 694	6.90	• 23	1.8	.63	1.0
10414	140 15	-27 47	17.03	13.03	37.86	119•1	• 234	8.20	•07	-0+9	3.84	1.0
10439	206 47	-15 12	34.71	33.01	37.78	73.8	.014	2.52	•67	-0.5	1.04	2.0
10447	200 50	-20 56	33.85	32.20	38.71	77.2	.133	6.60	• 77	-0+4	. 94	1.0
10098	231 35	15 53	45.71	44+01	41.83	65.8	• 256	9.60	2.94	-2.9	•71G	1.0
10478	175 52	-27 58	23.71	21.00	38.14	95 • 9	• 209	11.50	•27	-1.7	.61	1.5
10480	160 57	-43 32	22.70	19.98	37.80	97.0	• 205	13.40	+12	1.9	1.22	2.0
7097	218 22	7 54	32.71	30.59	36.36	74+1	.269	11.10	•27	0.0	•65	1.0
10531	267 2	31 0	51.07	49.78	41.80	56 . 9	.333	2.45	2.51	-0.9	.48	1.0
7158	190 29	- 5 37	23.07	20.47	37.91	96.4	.366	.50	• 26	-0.7	.46	1.0
7161	317 7	32 42	49.19	47.59	42.06	60.8	.272	6.30	8+14	-2.0	1.49	1.0
7169	33 13	49 46	18.00	14.46	38.11	114+8	• 052	11.10	•17	1+2	. 83	2.0
7184	196 35	- 4 51	23.12	20.23	36.51	91.9	.006	1.10	.04	0.6	.70	2.0
7188	231 59	29 38	38.93	37.21	41.88	76.6	.430	10.10	3.06	-1.3	.44	1.0
7190	208 52	27 18	29.49	27.38	41.52	93.2	.831	11.90	2.02	-1.6	.93	1.0
10094	318 21	32 13	49.31	47.77	41.99	60.4	.174	6.45	3.92	-2.6	.92	1.5
7210	97 46	36 3	13.71	8.42	37.79	161.5	.301	.80	• 04	1.5	.85	1.0
7216	195 26	-25 47	31.89	29.72	40.48	85.9	-020	8.20	1.25	-1.9	1.64	1.5
7240	194 52	1 26	21.89	19-04	37.17	97.0	.409	3.70	.10	-0.6	.42	1.0
10555	166 44	78 18	18.02	14.28	38.57	118.3	. 249	INF	.23	-0.2	.60	2.0
7272	215 26	- 0 44	30.92	28.99	37.35	79.0	.450	7.30	• 41	-0.9	.93	1.5
7277	250 36	-28 43	60.68	59.61	41.35	39.7	+154	2.20	2.47	-0.6	• 56	1+0
7331	218 18	35 6	25-65	22.99	38.36	92.6	.485	12.80	•28	0.6	•47	1.0
7333	212 12	-10 54	31.46	29.35	38.05	80.3	.267	1.20	• 57	1.3	. 64	1.0
7339	219 56	-37 0	44.63	43.20	41.54	66.5	.131	10.10	2.63	1.2	. 38	2.0
7367	181 23	-11 39	21.94	18.68	39.79	108+6	.028	4.10	• 73	1.0	.79	2.5
7372	189 49	-10 19	21.12	17.72	37.53	101.8	•224	2.60	•14	0.7	• 74	1.5
7388	203 0	- 4 34	23.51	20.74	36.81	92.1	.359	2.50	.10	-0+7	• 36	1.5
7392	287 12	65 53	27.56	25.07	37.94	87.3	.275	2.40	.08	-0+2	.66	1.0
7454	347 23	25 20	47.21	45.53	41+61	63.1	•307	9.90	2.72	0.1	•69G	1.5
3271	271 54	33 32	47.37	45.83	40.93	61.3	.330	3.42	1.33	-1.5	• 52	1.5
3217	271 16	33 19	48.04	46.67	41+65	61+5	•451	3.44	2.33	-0.6	• 30	Z•0
3228	266 5	42 47	40.76	39.02	40.93	71.7	.501	3.96	1.32	1.3	. 48	1.5
3234	226 55	- 3 14	28.94	26.79	35.25	77.2	.271	8.23	•11	0+4	.47	1.5
3250	221 12	- 5 22	29.37	27.22	38.33	84.7	.309	5.52	• 55	1.0	• 70	1.5
10127	239 38	- 2 42	37.55	36.10	37.88	76.6	.198	10.23	• 75	-1.8	• 29	2.0
3265	328 30	51 34	41.45	39.69	40.90	70.7	.288	6.69	1.39	0+1	+54	Z+0

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# TABLE 1.—Basic orbital data

Trail No.	Day	¥r•	Мо	Sh. No.		e	٩	đ,	ω	ይ	i	n
11816	3.15	54	5		2.481	.610	•968	3.995	26.7	222.1	22.9	248.8
11818	3.17	54	5		5.124	.808	.984	9.264	161.2	42 • 1	2.6	203.4
11825	3.23	54	5	57 (56,58)	2.716	•743	•697	4.734	73.9	222.2	3+5	296.1
11856	3.43	54	- 5	57(56,58)	2.255	•675	•734	3.776	71.1	222 • 4	1.8	293.5
11862	3.45	54	5		13.190	• 958	•560	25.820	95.2	42 • 4	163.5	137.6
7474	5.28	53	5	54(53,55)	2.949	• 925	•220	5.679	128.8	224 • 4	3.2	353.3
7476	5.30	53	5	53(54,55)	1.840	.868	•242	3.438	309.4	44.5	7.9	353.9
7478	5.30	53	5	55(53,54)	2.166	.844	.338	3.993	116.9	224.5	11.6	341.3
7480	6.15	53	5	57(56,58)	2.713	• 657	•850	4.576	52+2	225 • 3	1+4	277.5
7494	6.28	53	5	57 ( 56 , 58 )	2.151	•6/1	• /0 /	3. 340	12.3	223 • 4	0.5	300.6
7496	6.29	53	5		1.249	• 195	1.006	1.492	168.6	45.4	13.7	214.0
11973	6.29	54	5	50.51 57	6.131	. 884	• / 1 1	11.550	248.3	42 • 2	10.3	293.4
7499	0.27	52	2	58(50,57.58	) 1.907	• 100	• 4 4 0	3.200	227.5	45.4	3.4	273.0
7520	7.27	53	5	52	2.339	.569	1.009	3.670	182.5	46.4	28.1	278.8
			ĺ	52								
7524	7.28	53	5	59	9.613	• 896	1.002	18.220	190.0	46.4	55•Z	236.3
7534	/•31	53	5	53 (54,55	) 2.781	• 901	•276	5.280	302.2	40.4	12+0	348.6
7562	8.27	52	2		21.501	. 957	•/10	42.570	242.7	47.3	20+4 0.8	293.0
7592	9.33	53	5	51	2.402	.580	1.009	3.796	176.3	48.4	1.8	224.6
7407	0.07				5 207	015		0 4 4 0	164 6	4.9.4		202.0
7607	9.31	52	2	50/54 57	2.875	.828	• 700	9.449	280.5	40 • 4	40+0	202.9
7637	12.24	53	5	55153.54	2.489	.850	. 372	4-606	112-0	231.2	4.1	343.1
7664	13.16	53	5	56(57,58)	2.697	• 676	.873	4.521	228.5	52 • 1	3.1	280.5
7666	13.18	53	5	50(57458	.870	• 162	•733	1.020	14.3	52 • 1	17.8	66.4
3344	21.21	52	5	52	2.981	•661	1.010	4 • 952	173.6	60•1	22 • 5	233•7
3340	21.30	52	- 5		16.561	• 947	•884	32.238	222.4	60.1	121.1	282.5
3342	21.31	52	5	60	2.321	• 648	•818	3.825	59.2	240.2	9.7	299.4
3334	21.32	52	5	-	20.761	1.027	•556	- 42.080	263.6	60 • Z	91+5	323.8
3332	21.34	52	5		2.713	• /3/	• /13	4.713	252.3	60 • 2	19.5	312.5
3327	21.36	52	5	54(53,55	2.622	•915	•223	5.020	129.2	240 • 2	4.5	9.4
3312	22.25	52	5	52	2.768	• 635	1.011	4.524	174.3	61.1	15.8	235+4
3307	22.27	52	5	52	2.892	•650	1.012	4.772	182.8	61.1	22.7	243.9
3303	22.20	22	2	56(5/+58	2.040	• 281	•822	3.220	234.8	61+1	2.02	242.9
5277	23033	52			2.100	• / 7 /	• 4 4 2	3.717	20501	02 • 1	13.5	541.00
3295	23+40	52	5	53(54,55	) 1.792	•826	•311	3.272	302.1	62 • 2	21+7	4.3
3288	24 • 28	52	2	60	1.932	•619	• / 3 /	3.128	13.3	243.0	12+2	310+3
3200	22.22	52	25		75.118	.940	+098	3+072	190.1	69.8	85.9	259.8
12342	31.35	54	5	66	2.844	•759	•686	5.001	255.5	69.3	1.3	324.8
12261	1 10	E 4			6 612	821	804	0 310	57.0	250 1	12.0	207 1
12363	1+10	54	6		4.512	+021	•000	5.111	127.7	200+1	8.2	197.8
4103	1.37	52	6	62(61)	2.322	.580	.976	3.669	206.3	70.8	21.8	277.0
12399	2.23	54	6	61(62)	2.867	•667	.954	4.779	211.5	71+1	21.2	282.6
7726	4.20	53	6	01.02.	2.343	.838	•379	4.307	112.0	253•2	3.0	5+2
7734	4.24	53	6	63	2.460	•610	•959	3.960	31.2	253•2	0.8	284•4
10587	4.39	54	6	59	89.970	•989	1.008	178.900	170.7	73.2	55+5	243.8
10583	4.39	54	6		42.820	• 984	•686	84.960	290.3	253.2	178.1	183.4
7742	5+17	53	6	64	3.464	•717	•979	5.949	203.7	14.2	/1.6	21/+9
//44	5.11		0	00	20312	• • • • • •	• / 9 5	3.949	24201	14•2	1+1	310.7
7750	5.21	53	6	63	2.367	•620	•900	3.833	45.2	254.2	1.2	299.4
1754	5.25	53	6	66	Z • 059	•667	•686	3.432	259.0	74•2	7.0	333.2
12504	5+26	54	6		3.008	• 703	•894	5.122	135.3	74.0	14.9	209+3
7797	2•28	53		67	2.770	+ Y53	• 505	20.830	211.7	14.3	130+9	340+0
7.07	0.20			04	20110	• 143	• 70 4	0.372	200.1		10.0	20000
7820	9.23	53	6	62(61)	2.806	•645	•995	4.616	198.5	78.0	20.8	276.5
7838	9.34	53	6		1.921	•491	•978	2.864	207.1	78.2	15+7	285.3
12577	11.41	50	4	67	2.162	+0/4	• 912	14+521	24+6	200 • 2	10.2	10.4
7871	13.35	53	6	* ·	1.691	•725	•464	2.917	106.9	262.0	6+6	8.9

Trail No.	True	$radiant \delta$	200	▼ <sub>G</sub>	▼ <sub>H</sub>	λ	Sin Q	C.W.	K	Mp	t	Qual.
11816	151 23	-56 4	19.87	16.56	37.43	105.0	• 156	8.20	•01	1.1	2.16	2.0
11818	105 40	31 57	15.58	11.33	39.81	150.7	.175	1.40	.68	-0.1	2.19	1.5
11825	209 26	-18 1	22.96	20.03	37.83	97.7	• 004	2.80	•27	0.3	1.03	2.5
11856	208 47	-15 20	20.73	17.88	36.94	99.4	•474	1.80	•06	1.0	1.32	1.0
11862	335 34	- 1 53	66.76	65+49	41+12	26+2	•127	.85	1.78	-0.7	•58	2.5
7474	239 7	-22 13	36.83	34.99	38.16	72 • 0	.160	1.20	.88	0.8	•65	1.0
7476	241 28	-15 51	33.77	31.80	35.71	71.1	•171	3.40	•42	0.2	.94	1.0
7478	232 54	-28 23	31.95	29.93	36.71	76.3	•195	5.50	•41	1.4	•75	1.0
7400	214 42	-11 40	21.45	12.10	3/ 01	111.8	•064	1.30	•16	0.5	• 94	1.0
1434	214 42	-14 51	21043	10.39	30.01	7/02	+151	•50	•04	1+4	•60	1+0
7496	236 44	77 39	13.67	7.94	32.36	104+0	•331	INF	- •73	0.7	• 33	1.5
11973	267 24	25 9	44.93	43.29	40.15	63.7	.266	7.10	1.00	-0.8	.67	1.0
7499	234 10	- 8 33	28.11	25+76	35.94	80.8	•132	6.10	•16	0.8	•78	1.5
7520	201 49	-09	21.03	14+45	37.94	112.0	• 293	3.20	•18	1.5	.93	1.0
1322	241 20	09 0	21003	11019	57011	100+5	• 590	INF	- •07	0+0	• 07	1+0
7524	275 38	54 28	36.11	34.17	40.79	79.3	.305	INF	1.24	-1.8	.87	1.0
7534	241 2	-12 57	35.05	33.19	37.91	74 • 2	•164	4.83	•73	1.1	• 46	1.0
7560	251 50	26 58	37.75	35.87	41.41	77+9	•401	10.00	2.10	0+2	•48	1.0
7562	225 8	- 3 43	26.43	23.94	38.84	92.7	•114	6.40	• 58	1.1	.87	1.0
1292	140 2	24 30	12022	1.02	31023	1/1+1	•122	146	- +04	1.5	•	3.0
7607	311 50	69 13	31.58	29.44	39.81	85.0	.293	5.10	•71	0.2	.44	1.0
7635	236 32	-10 14	29.70	27.38	38.02	83.9	.108	5.20	•51	0+4	•69	1.0
7637	238 18	-23 47	31.36	29.17	37.38	79•2	•009	2.10	+49	-1.7	1.10	2.0
7666	207 25	- 3 /	10.20	14+35	3/0/5	114+2	•113	2.80	+17	1+1	• 67	1+5
1000	305 55	50 41	14035	7007	21022	00+7	•410	4040	- •72	0.3	• 02	1.0
3344	205 43	72 15	19.25	15.74	38.12	111.6	.392	INF	•16	2.3	• 54	2.0
3340	306 43	14 37	62.80	61.18	41.20	36 • 0	.299	1.58	1.78	-0.9	• 46	2.0
3342	214 3	-35 43	19.54	16.27	37.00	104+5	.388	8.90	•04	-0.7	1.56	1.5
3334	283 28	14 3	53.57	52+19	42+35	54+2	•1/4	6+05	100	-0.6	• 4 9	4+0
2222	240 23	9 40	24+00	22.007	3/0/4	9302	.011	12.01	• 2 3	0+4	.02	1.0
3327	256 22	-25 24	35.96	34.25	37.58	71.9	.222	1.76	•77	1.3	.38	2.0
3312	180 54	63 33	16.57	12.45	37.82	124.1	• 090	INF	•09	2.1	•92	1.5
3307	217 36	64 9	19.24	15.76	38.00	110-9	•140	INF	•13	1.2	.81	1.5
3303	219 36	- 9 40	17.33	13.42	36.28	110+1	• 390	2021	- •11	2.02	• 67	2.0
2299	200 00	- 9 14	27.03	20.73	30.03	01+0	+421	1025	• 2 7	1.0	.01	200
3295	259 58	- 7 29	32.27	30+45	35.43	72.6	.333	9.71	.28	1.1	.52	1.5
3288	227 7	-40 48	21.02	17.92	35.93	95.8	.281	10+44	- •09	1.5	1.20	3.0
3286	274 27	-34 57	41.37	39.58	35.73	60.3	•031	9.42	•84	1+1	• 94	4+0
3277	309 44	41 54	50.70	49+26	41.66	57.5	• 348	1.10	3+05	-0+9	+42	2.0
12342	239 29	-18 27	23.04	20.37	37070	77.00	• 204	1.10	• 32		•05	200
12361	222 44	-41 8	22.62	19.63	39.38	105.3	.088	9.20	•66	0.5	1.44	1.0
12363	93 33	42 11	18.93	15.65	38.08	111.9	• 044	7.90	•25	0.2	2.34	2.0
4103	236 24	42 41	18.98	15.62	36.96	106.5	• 266	7.45	- +06	2.3	.43	2.0
12399	235 41	35 52	20.07	16.68	37.92	10/•/	• • • • •	9+10	+10	0.4	- 04	1.5
//26	262 22	-25 53	30.76	20.44	30.99	1900	•071	1.00	• • • 3	1.02	• / 0	100
7734	207 49	-14 14	15.19	10.57	37.23	131.8	+411	•60	• 01	1.9	•71	1.0
10587	297 37	66 18	36.63	34.88	41.68	80.4	•419	INF	3+20	-2.0	•67	1.5
10583	3 26	0 26	68.98	67.70	41.55	20.6	.161	·08	2.72	-1.2	1.00	1.5
7742	300 53	44 45	42.39	40.63	38.61	64.6	•298	2.07	• 52	0.9	1 02	1.0
1144	236 34	-17 35	19.76	10+10	51000	102+4	•110	1.01	•07	1.04	1.02	101
7750	221 58	-19 38	16.83	12.66	37.04	118.2	.183	1.10	•00	1.7	.80	1.0
7754	248 45	-10 14	22.01	18.94	36.28	95.0	•432	6.00	•01	0+1	•77	1.0
12504	105 11	58 35	19.32	15.98	38.10	111.0	•121	11.30	•24	-0.5	2.95	1.0
7758	310 0	3 44	61.82	60+48	40.78	36.4	•141	3.00	1+64	-0.3	• 55	2.0
1187	306 12	41 16	45+68	44+07	30.01	00+0	.510	2030	• • 1	1.0	• 23	107
7820	232 34	44 35	18.92	15.34	37.81	111.8	.255	3.50	•11	-0+4	1.17	1.0
7838	234 1	34 52	16.25	12.12	35.84	113.0	.212	6.80	- •25	0.5	•79	1.0
7841	343 22	- 8 37	70.57	69.38	40.39	6.6	• 106	•03	1.06	-0.2	•49	1.0
12577	269 58	-14 14	29.65	27.70	36.55	19+7	+152	5.50	e 0 3	0.6	1.14	1-0
1011	204 51	-30 46	20.00	23+01	34034	0100			105			

TABLE 1.—Basic orbital data

Trail No.	Day	ĭr.	Mo.	Sh. No.	<b>a</b>	e	ą	ď,	ω	ß	i	A
7873	13.36	53	6	65	9.277	.925	.695	17.858	249.9	82.0	131.0	331.9
7882	13.41	53	6	61(62)	3.371	.721	•940	5.801	214.6	82.0	18.7	296.6
4111	14.19	52	6	63	2.461	.630	•911	4.011	42.8	263.0	4.3	305.8
7902	16.35	53	6		5.778	.957	.251	11.300	302.7	84.8	147.3	27.5
4125	19.30	52	6	61(62)	2.838	•660	•966	4.710	209.0	87.9	17.5	296.9
7929	20.39	53	6		191.000	.996	• 732	381.300	243.9	88.7	174.4	332.6
4136	21.41	52	6		17.310	.947	•911	33.700	218.2	89.9	94 • 4	308.1
4138	21.42	52	6	68	18.010	•951	•886	35.130	137.4	89•9	153.6	227.3
4141	22.18	52	6	52	2.502	•603	•994	4.010	160.4	90•7	16.3	251.0
4143	22.19	52	6	67	2.937	.839	•473	5.401	279.9	90•7	14.4	10.6
4147	22•22	52	6	66	2.229	• 702	•665	3 • 792	260.7	90•7	3.6	351.4
4151	22.38	52	6	68	78.887	•988	•968	156.807	154.6	90.8	163.1	245.5
4153	23.28	52	6	66	2.773	.720	•778	4.769	244.0	91.7	3.0	335.7
4181	25.22	52	6	67	3.923	.878	•480	7.366	277.4	93.6	13.0	11.0
12714	25.26	54	6		2.009	• 717	• 568	3.449	273.2	93.1	16.9	6•3
4199	29.43	52	6	3	1.502	.852	• 223	2.780	314.2	97.6	7.4	51.8
10566	30.25	54	6		55.990	• 982	1.009	110.960	189.7	97.9	33.6	287.6
7944	6.30	53	7	69	3.092	.761	•738	5.446	248.5	103.9	7.2	352•4
7946	6.31	53	7	72(73)	2.491	•621	• 94 5	4.038	215.4	103.9	18.1	319.3
8012	15.25	53	7		3.898	•862	•537	7.258	271.1	112•4	21.8	23.5
8017	15.26	53	7	69	3.042	• 756	•741	5.343	68.2	292•4	2.5	0.7
8054	16.28	53	7		26+200	•967	•859	51.530	133.3	113.4	95.5	246.7
8068	16.38	53	7		26.230	.978	•588	51.860	278.5	293.5	147.8	212.0
8075	16.41	53	7	20	1.553	•925	•117	2 • 988	327.4	113.5	26.5	80.9
8083	16.43	53	7		7.045	•919	•571	13.519	265.2	113.5	166.9	18.7
3355	19.41	52	7	3	2.489	•901	•248	4.730	126.6	296.6	0.9	63.2
8089	20.36	53	7		- 80.920	1.012	•973	-162.800	203.7	117.3	43.6	321.0
3360	21.35	52	7	5	2.795	• 983	•047	5.542	157.5	298.5	33.1	95.9
8106	21•39	53	7		1.285	.812	• 242	2 • 328	134.5	298.3	6.3	72.7
8108	21.40	53	7		12.150	•916	1.015	23.290	177.1	118.3	72.9	295.4
8110	21.41	53	7	3	2.559	.860	.358	4.760	293.7	118.3	5.4	52.0
8113	23.42	53	7	68	22.880	.957	.986	44.770	160.1	120.2	164.3	280.3
3377	24.34	52	7		34.060	•971	• 994	67.130	197.1	121.3	129.8	318.4
3379	24.36	52	7	1	2.528	.765	• 594	4.461	267.6	121.3	7.7	28.9
3386	25.27	52	7	1	2.134	•732	•573	3.694	271.9	122.2	7.6	34•1
3393	25.42	52	7	70	6.208	•912	• 545	11.870	268.4	122.4	44.1	30.7
3399	25.44	52	7	5	2.848	•978	•063	5.632	153.8	302.4	27.3	96.2
3405	26.22	52	7	1	2.447	.775	•551	4.344	272.8	123.1	7.6	35.9
3407	26.25	52	7	3	3.337	•920	•266	6.408	122.7	303.2	1.9	65.9
3411	26.27	52	7	1	2.069	•725	• 568	3.569	272.7	123.2	5.3	35.9
3416	26.35	52	7	1	2.536	•774	.574	4.499	269.9	123.3	7.2	33.1
3424	27.27	52	7	5	3.001	•977	• 069	5.933	152.4	304.1	26.1	96.5
3450	28.31	52	7	5	2.358	•973	• 06 4	4.652	154.2	305.1	30.1	99.3
3463	28.31	52	7	5	3.084	•979	•064	6.105	153.3	305.1	25.6	98.4
3487	29•42	52	7	5	2.179	•969	•067	4.291	153.8	306•2	28.5	100.0
8127	3.19	53	8		2.305	•725	•635	3.970	263.7	130.5	25.3	34.2
8143	4.21	53	8	73(72)	3.582	•737	• 942	6.222	213.7	131.5	29.4	345.1
8147	4.22	53	8	1	2.482	.801	•495	4.469	278.7	131.5	6.7	50.2
8149	4 - 25	53	8	ī	2 • 588	•768	.601	4.575	266.5	131.5	7.0	38.0
8153	4.29	53	8	7	22.370	•958	•942	43.790	148.6	131.6	112•4	280•1
3497	4.46	52	8		2.751	•635	1.005	4.496	167.4	132.0	43.1	299.4
8168	5.24	53	8	50	2.751	.976	.065	5.437	333.4	132.5	23.8	105.8
8187	5.33	53	8	5	2.950	•967	•098	5.801	146.9	312.6	24.1	99.4
8189	5.34	53	8		3.126	.750	•781	5.470	242.4	132.6	13.0	15.0
8192	5.35	53	8	71	• 947	•723	•263	1.631	140.1	312.6	10.2	92.6
8215	5.43	53	8		19.527	•954	• 908	38.147	141.7	132.6	69.8	274.4
8224	5.45	53	8	7	23.080	.958	.960	45.200	152.8	132.7	111.2	285.5
8238	6.21	53	8	5	2.779	.961	•109	5.450	145.2	313.4	25.4	98.6
8240	6.22	53	8		5.844	.854	.854	10.830	229.0	133.4	36.2	2 • 4
8244	6.24	53	8	74(75)	2.950	•662	• 995	4.900	197.8	133.4	13.9	331.2

Trail	True	radian	nt	V	v <sub>G</sub>	v <sub>H</sub>	λ	Sin Q	C.W.	K	M	t	Qual.
NO.	• •	•	1								ſ		
7873	322 9	10	56	63.03	61.81	40.61	33.2	•238	2.20	1.38	-0.4	. 42	1.5
7882	240 23	26	43	19.62	16+54	38.50	111+1	.125	10.40	•32	1+0	1.10	4+0
4111	226 18	-30	0	16.82	12.64	37.21	119.7	.414	3.85	•03	-0.8	1.34	1.0
1902	317 33	- 4	27	60.17	58+93	39.89	37•5	•004	2.80	1+41	-0+2	• 38	3.0
4125	240 33	29	21	10+31	14+02	5/+84	114+0	+427	8.29	+14	1.3	• 56	1.5
7929	340 14	- 5	15	69.42	68.30	41.70	18.9	-015	.20	A-00	-1.8	- 51	2.5
4136	319 27	35	35	53.45	52.25	41.14	51.7	.147	2.52	1.81	-1.2	.37	2.0
4138	5 42	18	28	68.79	67.60	38+67	19.5	.327	•63	1.85	-0.6	.38	2.0
4141	179 5	61	9	16.92	12.94	37.28	118.7	.099	3.70	•00	0.3	.70	2.5
4143	276 40	- 8	59	29.90	27.49	37.97	83.9	.198	7.60	• 53	1+4	• 79	1.5
4147	265 13	-17	25	22.70	10.45	26.60	05 1	0.94	2 . 65	10		1	
4151	3 45	12	15	70.97	69.76	41.67	12.4	. 229	- 20	2.11	-1.9	1.00	2.0
4153	256 0	-17	2	20.58	17.42	37.74	104-9	. 393	2.75	.23	0.1	.81	1.5
4181	278 5	-10	22	30.45	28.15	38.95	85.4	.058	6.77	.78	-1.6	. 79	3.0
12714	276 53	- 2	4	25.92	23.31	36.09	85.9	.211	10.90	•09	0.1	.81	1.5
		• •											
4199	299 18	-16	-	32.12	30.32	33.96	69.4	•466	3.51	+27	1+5	•67	3.0
7044	270 11	-11	2	20.18	230//	41.70	102+6	• 337	INF	2.19	-3.2	1.30	2.0
7946	257 33	25	23	18.49	15.08	37.25	110-0	. 798	10.40	• 30	-0-7	2.55	1.0
8012	294 48	1	51	30.09	27.86	38.94	85.9	.087	10.90	•72	-0.6	.97	1.0
											0.0		
8017	281 1	-27	35	21.77	18.74	38.11	102.8	.186	2.20	• 34	1.6	.94	1.0
8054	23 59	60	25	54.13	52.79	41.35	51+3	.198	3.20	2.20	-1+5	•60	1+0
8075	321 42		50	27.57	26.00	41+32	67.3	. 200	1.60	2+30	0.3	- 50	2.0
8083	357 25		34	65.99	64.95	40.22	24.6	.103	.70	1.22	-0.9	• 35	2.0
		-					2				007	•	200
3355	315 41	-17	27	34.28	32.58	37.25	73.8	.504	+41	.68	0.9	+40	3.0
8089	280 58	50	43	31.38	29.53	41.89	90+8	• 099	4.90	INF	-0.9	.88	3.0
3360	333 49	-17	52	44.34	42.85	37.78	59.7	• 291	7.54	1.52	-0+8	• 22	Z.0
8106	323 15	-19	10	29.91	27.84	32.47	69•Z	• 321	3.38	+09	1+5	+ 12	1+0
0100	334 1	67	34	44+11	42+70	40+08	00+2	• 330	LINE	1+43	-0+4	• 55	1+0
8110	310 25	-13	44	31.05	29.22	37.39	79.4	.325	2.90	.53	1.4	.76	1.0
8113	30 36	22	8	70.85	69.72	41.30	10.7	.401	.10	2.02	-2.2	.43	2.0
3377	10 28	36	46	65.33	64.14	41.46	30.0	.552	•30	2.36	-0.8	.38	1.5
3379	300 13	-10	0	24.84	22.42	37.34	91.4	.385	5.88	•28	1.0	•51	2.0
3386	303 11	- 9	39	24.72	22.02	30.40	89+3	•14/	2+11	+14	1+0	+42	2.0
3303	309 48	20	10	36.05	34.54	60-03	77.2	. 309	12.68	1.13	0.6	. 45	1.5
3399	335 53	-17	4	43.05	41.73	37.86	61.5	.517	6.89	1.41	0.1	.44	2.0
3405	304 39	-10	- i -	26.10	23.44	37.19	88.9	.036	5.21	•29	-1.7	.95	2.0
3407	320 38	-16	40	35.16	33.16	38.46	75.7	.082	.80	•91	-0.9	.25	2.5
3411	304 54	-12	22	24.47	21.75	36.29	89.3	•035	4+07	•11	1.5	• 35	2.5
34.14	202.20	.10	34	38 34	22.05	27 26	00 4	220	6.25	. 20	1.0	. 54	2.0
3434	326 64	-10	42	42 22	41.54	38.08	62.2	.008	6-48	1.41	-1-4	. 62	2-0
3450	330 30	-16	28	42.71	41+06	37.01	60.8	.068	7.45	1.23	-0.7	.29	2.5
3463	337 57	-15	55	43.42	41.83	38.18	62.0	.118	6.33	1.47	-0.8	.52	2.0
3487	340 33	-16	2	41.82	40.41	36.59	60.9	.466	7.48	1+14	0.1	• 37	2.0
8127	307 57	15	5	26.80	24.18	36.91	86.6	.228	13.77	•16	1.8	• 50	1.5
8143	282 58	39	24	23.67	20+91	38+12	99.4	- 150	4.20	- 35	1.7	- 30	2.0
8140	313 37		25	2/072	29.77	37.48	92.2	-223	5.20	• 29	1.1	.65	2.0
8153	37 50	56	9	60.10	58.85	41.32	40.7	.280	1.40	2.02	-1.3	• 52	2.0
	5. 50									-			
3497	262 9	74	52	28.17	25.99	37.75	85+8	•072	INF	•09	0+5	• 38	2.5
8168	340 21	- 1	55	42.99	41.26	37.75	62.0	.232	5.98	1.36	-1.1	• 62	2.5
8187	343 25	-15	14	41.61	40.00	38+04	103 0	. 54 3	10.80	1+24	2-2	. 40	3.0
6169	296 8	-14	15	21.65	22-84	28+20 28+48	64.7	.169	6.70	- •23	1.0	.41	2.0
0172	343 40	-10	20	23040	22.00	20040							
8215	59 33	83	10	43.62	42.15	41.25	67.8	.277	4.60	1.91	1.3	. 58	2.0
8224	36 26	56	57	59.70	58.57	41.34	41.3	.411	1.20	2.04	-0+2	.28	3.0
8238	344 18	-15	54	41.26	39.41	37.80	64 . 8	.088	7.00	1+14	0+5	• 95	Z+0
8240	297 48	36	1	28.77	26.48	39.95	91+Z	. 6/0	3,20	+6/	1-8	1,17	2-0
6244	228 39	24	1	10.00	12+40	<b>50 + 0</b> 4	12342	• UO I	2020	410	100	****	2.40

# TABLE 1.—Basic orbital data

Trail No.	Day	Ir.	Мо	• Sh• No•	٠	e	đ	đ,	ω	ռ	i	R
8254	6.29	53	8	5	3.814	•972	•109	7.520	144.3	313.5	19•2	97.8
8294	7.39	53	8	74(75)	2.063	•515	1.000	3.125	196.2	134.5	7.7	330.7
8307	8.19	53	8	3	3.316	•927	• 243	6.390	125.5	315.3	7.5	80.8
8344	8.39	53	8	5	2 • 4 5 8	• 963	•092	4.820	148+/	136.3	20.9	104+2
8360	9.21	23	0	10	2.525	•004	• • 70	+• • • • • •	21005	19049	11.40	2401
8394	10.22	53	8	75(74)	2.362	•587	•976	3.747	205.8	137.2	4 • 3	343•1
8401	10.24	53	8	7	51.492	•982	•949	102.034	150+6	137.3	110.9	287.9
8413	10.30	53	8	120	2.870	•647	1.012	4.728	184.8	137.3	39+2	322.1
8415	10.30	53	8	75(74)	2+4//	•603	• 984	3+970	202+9	137.3	1+2	340+2
0411	10+52	22	•	/1	1+100	• / 0 /	• 2 • 7	2.000	51505	15145	1404	7207
8658	10.44	53	8	7	25.750	• 964	•935	50.560	147.3	137.4	113.5	284.7
8668	10.45	53	8	1	2.672	•748	•673	4.671	257.6	137.5	7.2	35.1
8447	11.42	53	8	72(73)	4 • 175	• 174	•944	7.40/	212.5	138 • 4	22+1	350+9
8449	13.24	53	8	7	28.250	• 995	.039	55.560	148.3	140.1	113.5	289.4
0407	13424		Ŭ	'	200230	• > 0 ·	• / 2 /	550500	1,005	14001	11303	20004
8476	13.28	53	8	12073(	72) 3.171	•688	•990	5 • 352	199.2	140.2	28 • 9	339.4
8510	13.42	53	8	72(73)	2.495	•617	•955	4.034	211.8	140.3	17•3	352.1
8463	13.45	53	8	1	1/./38	• 946	•958	34.517	152.7	140+3	113+8	293.0
8726	14+19	53	8	י ד	10+189	• 908	•957	19+442	147+4	141+0	114+0	200+2
0.20	1402/		Ŭ		1000000	• / 40	• / 0 0	500240	17501			27402
8546	14.29	53	8		2.793	•701	.834	4.753	55.1	321.1	3.6	16.3
8572	14.43	53	8		10.720	• 960	•425	21.010	100.7	321.3	159.7	62+0
8576	14.43	53	8		- 10.272	1.075	•770	- 21.314	27.05	321.03	89+1	18.8
3573	15.37	52	9	1	3+105	.925	+ 2 2 0	2.614	330-6	142.4	22.1	113.0
5575	17031	12	0		10000	• 725	.102	20014	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	142.04	~~~	11300
8609	17.32	53	8	70	6.134	•840	•982	11.287	200.9	144 • 1	121.6	345.0
3604	18.25	52	8		20 • 917	•952	1.011	40.823	183.4	145.2	44.7	328.6
3610	18.34	52	8	5	2.48/	•970	+0/5	4.898	331.7	145.3	16+9	11/+0
3629	18.46	52	8	20	2.183	.906	•225	4.142	310.2	145.4	5.3	95+6
							1	. 7.5	100.1			225 2
3633	20+21	52	8	12073(	72) 2.600	• 0 0 1	1.008	4 • / 5 7 5	188+1	14/+1	0.1	55202
3640	20.24	52	8	1 741751	3.359	• 704	.994	5.724	196.7	147.1	9.6	343.8
3643	21 • 19	52	8	1	2.735	.808	.525	4.945	274.4	148.0	4.3	62.4
3651	21.29	52	8	10	2.746	•787	.586	4 • 906	267.5	148 • 1	1.2	55.6
3655	21.30	52	8	10	6.313	.902	•621	12.010	259.3	148 • 1	8.0	47.4
3657	21.40	52	8		16.815	.946	.905	32.720	141.5	148 . 2	100 • 2	289.7
3663	21•46	52	8	71	1.431	•824	•252	2.610	311.5	148.3	6 • 8	99•8
3784	22.24	52	8	3	2.580	•931	•178	4.982	135.2	329.0	13.8	104+2
3/86	22.021	22	8		1.015	•024	•630	2.119	88.9	329 • 1	3.8	58+0
4216	25.26	52	8	70	56.500	• 982	1.010	112+000	182.1	152.0	111.8	334 • 0
3813	25 • 44	52	8	12073(	72) 2.758	•634	1.011	4.507	178.6	152 • 1	32.4	330•7
3847	30•36	52	8	70	43.673	•977	1.009	86 • 337	178.9	156.9	107.6	335•7
3861	30.46	52	8	~ .	6.879	•868	•909	12.849	218.2	157.0	93.2	15+2
3877	31+47	52	8	/1	• 758	• / 52	•231	1+6/8	321+3	158.0	4 • 2	119+3
3886	1.47	52	9	2	1.640	•806	•318	2 • 962	302.3	158.9	1.9	101.2
4289	10+15	52	9	76(77)	3.780	•769	•874	6 • 687	225.9	167.3	5 • 8	33.2
4311	13+27	52	2	77/7/1	2.590	•690	•804	4 • 377	59.5	350.4	11+4	49.9
4328	14-21	52	9	79/201	2.094 3.800	• 04 3	• 901	4 • 4 26	207+6	171-2	13-6	18+0
1720	14451	72		171001	50000	*0.74	•055	0.007	27703	11103	1300	1040
4330	14.23	52	9	00/7-	59.005	•985	•903	117.107	217.5	171.3	125.4	28.8
4340	14+51	52	9	80(79)	2+3/4	• 724	•654	4.093	80.3	351.4	6+1	11+1
4360	16-15	52	9	78	3.970	.884	• 2 • 1	J + J21 7-479	278.7	173.2	73.1	91_9
4369	16.33	52	9	79(80)	2.961	.818	•537	5.383	271.9	173.4	7.2	85•2
4388	17-27	5.2	0	771761	3.374	.717	. 940	5.711	212.2	174 2	3.6	26.5
4394	17.31	52	9	20	2.470	.894	.263	4-678	124-4	354-2	500	118.7
4229	19.20	52	9		3.385	•718	.956	5.815	152.1	176.2	53.6	328 . 2
4454	19.36	52	9	81	23.080	.957	.997	45.170	170.3	176.3	144.6	346.6
4464	19.43	52	9	79(80)	2.307	• 707	•675	3.938	257.9	176.4	7.5	74.3

Trail	True	radiant	₹	<b>v</b> <sub>G</sub>	v <sub>H</sub>	λ	Sin Q	C.W.	K	Mp	t	Qual.
8264	342 7	-14 30	A1.72	** **	28.02							
8294	253 58	11 34	13.73	8.68	36.31	138.3	.183	5+30 INF	1.42	1.6	.42	3.0
8307	335 7	-15 6	36.06	33.99	38.48	74.4	.093	2.91	. 94	0.8	1.02	1.0
8344	347 41	-14 9	41.23	39.73	37.25	63.2	.407	7.40	1.11	0.7	.46	1.0
8368	319 38	- 2 13	27.99	25.48	37.38	85.6	• 004	7.10	•37	0.5	•70	2.0
8394	266 52	- 6 35	14.52	9.57	37.06	138.1	.497	2.70	- •04	1.0	1.03	1.0
8401	273 54	28 47	26 20	28.70	41.61	41.6	• 266	1.30	2.74	-1.6	•90	1.0
8415	262 5	-18 30	14.12	9.19	37.29	90.1	.403	170	•13	1.6		2.0
8417	338 5	2 2	29.18	26.92	31.46	67.8	.207	7.72	01	-1.1	.28	2.5
8658	46 46	57 16	60.46	59.31	41.40	40+1	.560	1.40	2.14	-0.9	. 40	2.0
8668	310 23	- 6 30	22.78	20.29	37.64	96.8	.260	6.40	• 27	1.2	.97	1.0
8447	281 17	29 43	20.83	18.02	39.20	109.2	.095	10.60	• 52	1.2	1.50	1.0
8679	47 73	57 33	60.80	59.69	41.74	40+1	•501	1.25	3.59	-2.5	•72	3.0
0487	47 30	38 U	00.39	37+37	41+42	40+1	.269	1.40	2.22	-2.0	1.35	1.5
8476	275 42	48 3	22.19	19.40	38.34	101.6	• 069	4.51	•23	-0.1	.85	2.0
8510	280 8	26 33	17.74	14.26	37.34	112.9	•138	10.00	• 02	-1.5	.93	1.0
8710	51 5	57 30	60.12	58.02	41+22	39.0	• 219	1.19	1.80	-0+1	• 67	1.5
8726	48 28	56 54	61.10	59.87	41.25	38.7	. 223	1.07	1.85	-2.0	. 96	1.5
							• • • • •	1007	1005	- 510		
8546	303 46	-28 22	18.79	15.28	37.85	111.9	• 345	3.70	• 20	0.8	1.89	1.0
8576	25 34	-36 8	52.70	51.50	40+83	50.9	• 2 3 3	4.69	1072	-0.5	. 56	3.0
3567	325 10	-13 24	26.85	24.50	38.27	90.0	.427	.28	.52	0.3	.74	1.0
3573	349 46	4 20	36.80	35.11	33.13	61.0	•462	7.45	• 54	-1.6	•60	1.0
8609	30 39	48 38	61.91	60.70	40.08	34.5	.310	. 60	.85	-1.2	•37	2.0
3604	273 28	65 37	31.01	29.06	41.34	89.9	.309	INF	1.93	-0.3	.44	2.0
3610	351 48	1 36	41.56	40.00	37+35	62.9	+134	4.70	1.21	0.2	.46	Z.0
3612	22 29	61 26	34 30	27.48	40.79	42.2	• 322	1.22	1+31	-0+3	• 4 3	2.0
3029	393 39	- 3 31	34+20	32.03	30+08	12.5	• 329	2.33	••1	1.4	• 22	2+0
3633	271 46	59 10	23.91	21.27	38.00	95.8	.255	INF	•13	0.8	.83	1.0
3636	324 16	-14 2	23.46	20.55	37.58	95.8	•121	•08	•27	0.1	1.42	1.0
3640	265 10	11 4	15.59	11.34	38.57	137.6	.355	2.88	. 29	-2.0	2.000	1.0
3651	330 19	- 6 40	27+00	24+30	37.81	92.4	+083	2.04	. 36	0.0	+ 62	1.5
5051	520 9	-11 17		22075	31001	/204						
3655	321 43	- 3 59	26.74	24.42	40+14	95.9	• 543	5+42	1.09	0.3		1.0
3657	68 49	67 22	55.84	54+59	41+22	48.1	+280	2.30	1.78	-0+1	. 89	2+0
3784	367 13	-10 1	37.50	35.56	37.54	69.8	.055	4.83		-0.6	. 37	2.0
3786	332 40	-17 59	21.28	18.09	34.98	91.6	.278	3.62	- +14	-0.3	. 64	1.0
4216	44 9	59 45	60.51	59.29	41.69	40.8	.332	INF	2.80	0.2	.48	2.0
3813	259 25	60 54	23.11	20.44	37.85	97.0	.107	INF	•09	1.6	1.18	1.5
3847	51 45	63 54	59.03	57.85	41.66	43.3	.283	INF	2.57	-0+2	•17	2.5
3861	17 11	61 32	52.24	51+12	40.33	52.0	•241	2.72	• 97	-2.4	.52	2.0
3877	2 29	4 58	25.95	23.73	28.84	04+0	•314	3.02	- •17	1+2	. 6 3	1+0
3886	353 57	- 0 54	29.16	27.29	34.87	75.7	.292	1.14	•18	0.7	1.16	1.0
4289	316 37	- 1 33	18.82	15+04	39.06	118+6	+114	5+29	• 46	0.5	1.00	1.0
4311	346 20	-31 59	20.13	16.77	37.68	105+3	- 167	6-01	• 15	1.6	1.14	2.0
4328	276 27	12 22	25.81	23.18	39,10	94.9	423	9.35	+62	-0.3	.73	1.0
4320	341 1	12 25	27001	23010	,,,,,,							
4330	57 58	51 48	64.16	63.00	41.80	33.8	• 253	1.33	2.88	-2.5	. 60	1.5
4340	351 26	-14 10	22.74	19+90	36.10	92 . 1	• 3 3 3	3.96	.07	0-3	.72	1-5
4340	2 30	-13 41	45-40	43.77	39.24	61-1	.326	9.25	.81	0.1	. 34	2.0
4369	351 41	5 49	26.73	24.43	38.26	89.6	• 4 30	4.96	.47	1.1	.77	1.0
4388	310 36	- 6 40	16.02	11.85	38.69	132.9	.530	3.17	• 31	1.6	1.08	1.0
4394	10 39	1 24	33.85	31.93	37.48	74.9	•174	2.00	• 64	0.8	.48	1.5
4229	213 28	73 16	34.18	32.44	38.76	77.1	.123	4.86	• 31	1.0	• 76	1.0
4454	89 48	44 8	69.05	67.90	41.55	20.0	• 250	+21	2.01	0.0	• 27	3.0
4464	346 25	7 44	21.89	19.25	57.15	70.0	• 337	/+03	•13	-0.9	2021	1.0

Trail No.	Day	Yr.	Мо	Sh. No.		•	q	۹'	ω	ß	1	π
4472	20.25	52	9	120	3.580	•720	1.001	6.150	186.7	177.2	32.0	3.8
4505	20.37	52	9	80(79)	3.121	•817	•572	5.669	87.6	357.3	1.1	84.9
4507	20.38	52	9	20	1.254	• / 92	+ 317	2.720	123+3	177.3	24.3	351.7
4702	20.39	51	9	82	3.012	.680	•965	5.059	205.0	180.3	49.0	25.2
4534	25.28	52	9	82	4.431	.777	.988	7.875	195.0	182.1	48.4	17.1
4542	25.33	52	9	80(79)	1.983	.713	.568	3.398	92.3	2 • 2	5.8	94.5
4574	26.22	52	9	2	1.154	• 782	•252	2.056	134.9	3.0	5.3	138.0
4596	27.28	52	9		2.220	•575	•913	3.730	72.5	4.1	29.6	44•0 76•6
4622	27.29	52	9	81	78.830	.988	•949	156.700	153.2	184.1	137.9	337.3
4624	27.30	52	9	76(77)	2.986	•721	.833	5.139	233.3	184.1	1.6	57.4
4645	27.40	52	9		51.248	•991	•463	102.000	94.7	4.2	115•4	98.9
4657	27.46	52	9	80(79)	3.004	• 788	•638	5.371	79.9	4 • 2	5.7	84.1
4677	28.38	52	9		35.480	•972	1.002	69.960	181.7	185.2	64.9	6.8
4679	28.39	52	9	76(77)	3.527	• 749	.884	6.169	223.4	185.2	3 • 1	48.6
4683	28.41	52	9	81	75.109	.987	.945	149.273	152.4	185.2	134.9	337.6
8766	30.19	53	9	80(79)	2.311	•737	•607	4.016	85+9	6.7	5.5	92.5
4701	50+48	52	9	2	1.010	.020	•300	5.050	12507	1.02	0.5	130.9
2961	2.22	51	10	20	2.701	. 864	• 366	5.036	291.6	188 • 2	2.7	119.8
8793	2.28	53	10		5.242	.048	• / 6 /	9.111	240+5	188.8	2/+0	218.5
8819	2.35	53	10	79	13.990	.973	.373	27.600	285.8	188.8	66+1	114.6
8881	6.24	53	10	90	3.356	• 705	•990	5.722	167.5	192.6	15.4	0.1
8891	6.29	53	10		8.554	. 886	•971	16.140	200.0	192.7	48.4	32.7
8917	7.39	53	10		1.919	• 649	•673	3.166	80.2	13.8	1.9	93.9
8943	9+19	53	10	9	3.3/1	• 704	• 9 9 8	5 • 7 4 3	17/+0	195+5	24+0	142.7
8951	9.23	53	10	9	3.293	.697	•998	5.587	176.9	195.6	24.6	12.5
8976	9.31	53	10		19.447	• 949	•998	37.896	177.0	195.7	104.0	12.7
8974	9.31	53	10	85	2.029	• 744	•520	3.539	97+1	15.7	9.7	112.8
8990	9.47	53	10	20	1.109	. 929	•271	1.947	133.8	15.8	4.1	149.6
9030	10.39	53	10	2	1.898	.715	•540	3.255	275.7	196.7	3.6	112.5
9062	12.44	53	10		5.385	• 940	• 324	10.447	246.8	18.8	146.0	265.6
9087	16.46	53	10		1.671	• 548	•756	2.585	71.5	22.7	16.9	94.3
4952	19.44	52	10	2	•948	+127	•82/	1.069	119.9	26+0	2.8	145.9
4962	21.20	52	10	83	3.693	• 756	•902	6.484	218.5	207.7	22.8	66•2
4964	21.20	52	10	84	3.237	•693	.994	5.479	176.4	207.7	13.0	24.1
4966	21.22	52	10	85	2.118	•762	• 504	3.733	98.1	27+7	6.4	125.9
4974	21.24	52	10	80	5/.1/6	• 988	• 664	113.688	70.1	27.8	145.1	90.5
5022	21.40	52	10	2	2.055	.830	• 349	3.760	115.6	27.9	5 • 8	143.5
5045	21.48	52	10		3.514	• 729	.952	6.075	206.2	208•0	71.2	54.1
5047	22.13	52	10		1.583	•479	.825	2.342	61.8	28.6	4.0	90.5
5073	22.20	52	10	80	26.//3	. 686	.946	5.087	236+8	208.8	23.1	57.2
5079	22.31	52	10	8	12.667	.953	• 5 9 2	24.743	80.2	28.8	164.3	109.0
5083	22.33	52	10	8	18.935	.972	•533	37.337	86.7	28.8	163.8	115.5
5101	22.37	52	10	8	11.178	.949	.574	21.781	82.5	28.9	163.8	111.3
5112	22.43	52	10	8	29.377	•981	•546	58.209	84.9	28.9	165.5	113.8
5176	23.42	52	10	2	2.022	.836	•473	3.712	99•1 117•5	29•0 29•9	5+3 5+5	128.1
5180	23.44	52	10	17	2.258	.865	• 305	4.211	299.7	209.9	3.9	149.6
5195	23.48	52	10	2	2.046	.813	•383	3.710	111.8	30.0	5.0	141.8
5231	24.27	52	10	80	22.758	•973	•609	44.908	257.6	210.8	158.0	108.4
5257	24.30	52	10	17	2.153	.875	•269	4.036	304+2	210.9	3.2	155+1

Trail	True	radiant	V	V <sub>G</sub>	V <sub>H</sub>	λ	Sin Q	C.W.	К	M_	t	Qual.
No.	α	δ		u	**					P		
44.73	376 16		22 60	20.00								
4412	2/0 15	5/ 1	23.50	20.93	38.95	99 • 2	•016	INF	•34	0.8	•91	2+0
4505	356 51	- 2 58	25+66	23.36	38.48	92.3	• 525	•83	+49	1.9	.82	1.0
4507	15 20	-13	29.03	26 • 95	34.39	74+6	•636	4.94	•12	2.0	• 55	3.0
4513	258 33	50 36	19.30	16.00	37.27	105.5	•083	INF	- •06	-0.3	. 84	2.0
4702	312 17	71 49	31.62	29.60	38.37	80.7	.288	4.84	• 20	-2.1	.78	2.0
4534	295 6	72 10	31.78	29.90	39.59	83.3	.156	2.98	.55	-1.8	1.00	1.0
4542	6 33	- 5 56	23.86	21.22	36.34	89.5	.307	4.77	•07	1.2	-60	1.0
4574	24 58	6 3	28.62	26.09	31.63	68.7	.177	2.97	03	1.9	.80	1.0
4596	319 2	53 27	22.41	19.71	36.80	94.1	.005	12.00	- 10	2 0	02	1.0
4618	356 19	- 5 36	20.50	17.28	37.02	100.6	209	2.00	- •10	2.00	. 72	3.0
4010		, ,,,	20030	11020	57002	100+0	• 2 70	2.00	•00	1		1+0
46.22	108 22	46 46	67.87	66.60	41.02	28 6	202	67	3 11			
46.26	263 6	2 40	10 57	15 00	41072	23.0	• 205	•07	3+11	0.5	+ 31	1+2
4024	341 0	- 3 40	10.57	15.09	38.30	113.9	. 529	1.70	•21	0.9	.88	1.0
4047	01 2/	- 0 0	28.85	5/.69	41.85	44+1	+114	4.48	3.05	-1+1	• 45	2.0
4659	10 31	- 9 16	18.16	14+75	33.06	89 • 5	•387	7.32	- +41	0+4	.88	1.0
4657	2 41	- 8 8	23.79	21+43	38.39	96 • 0	•317	4.90	+40	0.8	2.11	1.0
4677	256 27	83 54	41.15	39.65	41.76	72.4	.149	1.41	2.39	-0.5	.87	1.0
4679	332 44	- 2 21	17.50	13.99	38.96	121.9	.274	3.36	.39	-0.2	1.89	1.0
4683	110 54	48 16	67.16	66.01	41.92	27.4	.433	. 76	3.07	-1-2	.40	1.5
8766	7 36	- 5 22	24.01	21.05	37.24	92.7	.224	4.30	.18	-0.4	1.30	1.0
4701	22 22	4 24	30 01	28.21	36 10	74 7	414	3 50	22	1 5	02	2.0
4701	23 33	4 50	30.01	20.21	33.13	17+1	.414	3.50	• 2 3	1.02	• 72	2.0
2011	16.16	0.24	31 33	28 04	27.00	00 1	245	1 (0				
2901	10 14	9 24	51.22	28.90	57.98	80.0	• 205	1.40	+27	-2.02	• 08	2.0
8793	342 58	38 30	20.59	24+28	40+02	95+0	•028	13.80	•82	1+2	• 13	2.0
8817	119 47	36 33	68.89	67.68	41+41	21.3	•287	•83	1.77	0.7	•49	1.5
8819	24 4	44 35	45.45	44+11	41.32	64+7	•202	10.30	2.02	0.3	• 38	1.0
8881	258 58	27 30	17.02	13.34	38.84	123.9	•132	5+10	•29	0.0	3.48G	1.0
8891	303 45	71 45	32.72	30+90	40.86	84 . 6	•152	4.60	1+15	-0.2	.85	1.0
8917	9 18	0.18	20.63	17-68	36.22	96.0	.424	2.00	04	0.6	. 78	1.0
ROAS	270 56	47 14	20.20	17.16	38.88	108.7	-087	2.20	. 29	0.1	1.10	2.0
9045	22 12	9 54	21.06	28.60	34.42	72.5	206	2.00	. 21	1.7	. 90	1.0
0747	33 13	0 24	31.00	20.07	34002	12.00	•200	2.50	• 2 1	1.1		1.0
9421	210 50	4/ 10	20.11	1/+08	30.00	100+0	•005	2.20	• 21	0+1	1.33	1+3
							245	20	1	~ /	2.0	2.0
8976	123 8	66 42	57.96	20+14	41+28	42+3	• 240	• 30	1.87	0.0	• 30	2.0
8974	23 15	- 3 8	25.66	23.15	30.58	80.4	• 320	1.00	+14	-1.9	• • 2	1.0
8990	36 35	10 55	26.95	24.85	31+24	69+0	•221	2.70	- •10	1.6	• 90	1.0
9015	32 24	7 23	30.88	28.71	35.61	74.9	•084	3.60	•27	-0.1	1.05	1.0
9030	16 29	12 10	24.07	21.61	36.17	87.9	•349	3.00	•06	1.2	1.09	1.0
9062	140 44	2 10	62.23	60.87	40.14	34.8	.186	2 • 50	1+24	0.2	.52	1.5
9087	30 36	-24 21	19.80	16.73	35.32	94.4	.328	15.30	24	0.2	•61	1.5
4952	50 31	- 6 42	11.49	3.41	29.07	72.5	. 564	1.10	92	1.4	.79	2.0
9104	41 22	11 2	30.30	28.51	35.65	75.2	.225	3.40	• 26	-0.1	. 96	1.0
4062	226 0	47 3	21.65	18.69	39.25	105.4	.058	12.58		0.0	.82	2.0
4702	330 9	-1 5	21.05	10.07	37025	10304		12050		0.00		2.00
4044	202 41	24.24	15 02	11 84	29 82	121 7	244	3.62	. 25	1.7	1 00	1.0
4704	202 41	24 34	12092	11.04	30.02	131+1	• 2 40	3002	• 2 7		1.00	1.0
4966	32 52	56	26.29	23.64	36+91	86+3	•121	4.45	•20	1+4	•12	1+2
4974	95 22	5 56	67.05	65.75	42.01	28.6	•199	1.52	2.99	-0+5	•77	1.0
5006	96 1	15 57	68.17	66.98	41.49	24+1	.185	•69	1.85	-0.3	.37	2.5
5022	39 42	10 17	30.13	28.20	36.74	78.3	.442	3.30	• 35	-0.6	.90	1.0
5045	126 59	85 11	42.42	40.93	39.10	64.8	•197	3.14	•35	-1.2	.44	2.0
5047	16 30	- 5 32	16.26	11.55	34.95	106.2	.321	4.47	35	0.3	.73	1.0
5043	106 16	26 22	70.64	69.41	41-81	17.3	.252	.22	2.26	0.1	.55	2.0
5003	104 10	20 32	20.26	17.20	38.57	104.7	.102	10.85	.21	-1.0	1.82	1.0
5075	522 40	50 40	20.20	11.20	41 37	24 9	205	. 74	1.72	-1.1	38	1.6
5079	96 16	15 49	01.03	00.00	41+37	2400	•205	• / •	1012	-1+1	• 30	102
						24.0	270		2 1 2	-2.4	44	1 5
2083	93 57	15 5/	01.21	00.0/	41.07	20.9	.210	• 0 5	1 1 2	-2.04		2.42
5101	95 45	15 40	67.40	66.26	41.25	25.3	•317	• 80	1+03	-1+3	+ 34	2.0
5112	94 30	16 38	67.51	66.50	41.85	26.3	•739	•75	2.50	-2.3	• 39	1.5
5124	33 37	7 26	27.88	25.94	38.21	86.0	•304	3.50	•47	0+4	1.50	1.0
5176	42 20	11 35	30.47	28.62	36.66	77.5	.370	3.01	• 35	-0.8	• 90	1.0
5180	40 50	18 55	31.88	30.15	37.27	76.7	.149	1.99	.49	-0.6	•60	1.0
5195	30 55	10 43	28.92	27.05	36.73	80.1	.306	3.05	.30	0.9	.95	1.0
5221	99 20	32 40	67.82	66-60	41.75	25.8	.230	1.02	2.22	-0.6	.52	1.5
5227	21 20	- 9 4	28.41	26.20	41.56	94.9	.636	9.00	1.92	0.8	.77	1.0
5257	51 39	- 0 0	20.01	21	37.03	74 7	. 340	1.52	. 51	-1-7	.78	1-0
2221	44 2	13 4	52.01	21009	37+02	17441		1072				1.0

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TABLE	1.—Basic	orbital	data

Trail No.	Day	Yr.	Mo.	Sh. No.	*	•	٩	d,	ω	ß	i	R
5273	24.42	52	10		58.588	.989	•635	116.542	105.8	210.9	124.0	316.7
5289	24.49	52	10		327.815	.999	• 204	655 • 426	233.9	31.0	177•2	264.8
9130	2.12	53	11	84	4.017	• 755	.983	7.050	168.4	219 • 3	17•2	27.8
9147	2.29	53	11		10.660	•971	•314	21.000	292.8	219+5	121+1	152.3
9149	2.30	53	11		15.909	.981	•307	31.511	293.3	219.5	74 • 1	152.8
9170	3.20	53	11		6.507	.903	•633	12.381	76.3	40.4	39.4	116.7
9172	3.21	53	11		14.540	.951	•713	28.370	245.0	220.4	8.0	105.4
5332	7.09	52	11	18Q	2 • 790	• 732	•749	4.830	245.0	224.6	17.4	109•6
9238	7.37	53	11	2	1.970	.793	•405	3.530	109.6	44.6	6.0	154.2
9240	7.37	53	11	2	1.881	•751	•469	3 • 293	103.2	44 • 6	5+2	147.8
9246	7.43	53	11	2	2.191	.823	.387	3.994	110.4	44 . 7	4.9	155.1
9252	7.46	53	11	180	2 • 292	.679	.735	3.849	248.8	224 . 7	0.0	113.5
9257	7.48	53	11	17	2.257	. 844	• 353	4.161	294.0	224.7	2.5	158.7
9265	9.25	53	11	17	2.326	.841	• 369	4.283	291.9	226.5	3.5	158.4
9284	10.36	53	11		2.434	•722	•676	4.191	75.9	47.6	27.0	123.5
5346	11.21	52	11	2	2.000	• 796	•409	3.600	109.0	48.7	5.8	157.7
5370	12.18	52	11	-	3.860	.748	.974	6.750	195.7	229.7	8.1	65.4
9331	13.35	53	11	17	2.073	.838	.336	3.810	296.7	230.6	3.1	167.3
9335	13.35	53	11		17.860	.978	.394	35.320	102.5	50.6	114.4	153.1
5450	15.48	52	11	13	12.557	•922	.983	24.131	171.0	233•0	161.8	44•0
5472	19.50	52	11		4.209	•770	.968	7.451	197.5	237.1	79.4	74.6
5511	21.44	52	11	17	3.540	.887	.400	6.670	105.4	59.1	0.4	164.5
9375	26.17	53	11		2.240	.697	.679	3.801	76.1	63.6	3.8	139.7
9379	1.13	53	12		3.501	•748	.882	6.121	221.2	248.6	14.7	109.8
9411	4.44	53	12	16	56.660	.995	•279	113.050	116.0	72.0	128.7	187.9
9416	7.39	53	12	20	2.167	.756	.529	3.805	94.3	74.9	6.5	169.2
9418	7.40	53	12	4	1.383	.903	.134	2.631	325.1	254.9	21.4	220.1
5551	9.25	52	12		34.874	.994	.220	69.527	303.9	257.1	135.2	201.0
5557	9.27	52	12		3.452	.773	.782	6.122	58.1	77.1	16.9	135.2
9451	9.37	53	12	4	1.244	.885	•143	2.345	325.1	256.9	23.4	222•0
5572	10.21	52	12	88	3.170	. 696	.964	5.376	198.5	258.1	15.3	96.6
5601	11.19	52	12	4	1.379	.898	.141	2.617	324.2	259.1	24.3	223.3
5605	11.21	52	12	4	1.310	.894	.139	2.480	325.0	259.1	23.5	224.1
9507	11.39	53	12	4	1.263	.886	.144	2.381	35.2	259.0	24.1	223.8
5640	12.21	52	12	4	1.472	• 904	•141	2.802	323.6	260.1	23.8	223.6
5644	12.22	52	12	4	1.275	. 887	-144	2.405	324.7	260-1	21.7	224.8
5648	12.23	52	12	4	1.335	.893	.143	2.527	324.3	260.1	23.8	224.4
9547	12.35	53	12	4	1.376	. 997	.142	2.610	324.0	260.0	23.6	224.0
5759	13.14	52	12	4	1.348	.894	.142	2.554	324.3	261.0	23.9	225.3
9611	13.31	53	12	4	1.471	.904	•141	2.801	323.5	261.0	23.5	224.5
8645	13.34	53	12	4	1.355	.896	•141	2.570	324.4	261.0	23.4	225.4
9627	13.36	53	12	4	1.412	• 903	•137	2.687	324.5	261.0	22.8	225 • 5
9631	13.36	53	12	4	1.380	.897	•142	2.617	324.0	261.0	23.5	225.0
9656	13.43	53	12	4	1.362	.896	+141	2.582	324.3	261.1	23.2	225•4
<b>96</b> 60	13.43	53	12	16	11.178	• 980	•225	22.130	124.0	81.1	125.0	205•1
9709	13.52	53	12	4	1.361	.896	•142	2.580	324.3	261.2	23.6	225.4
9719	14.34	53	12	4	1.403	.899	•141	2.664	324.0	262.0	22.8	226 • 0
9725	14.37	53	12	4	1.353	.895	•142	2.564	324.3	262.0	23.5	226 • 3
9742	14.40	53	12	4	1.463	• 904	•140	2.787	323.7	262.1	23.4	225 .8
9749	14.40	53	12	4	1.394	.897	•143	2.644	323.8	262.1	23.5	225 • 9
8640	14.43	53	12		22.731	.957	.980	44.481	352.6	82.1	96.7	74.7
8648	15.48	53	12	16	11.870	.981	.225	23.520	123.9	83.2	124.9	207.0
9833	29.24	53	12		2.596	•740	•675	4.518	74.8	97.2	18.6	172.0
	•				•	•	•	•	•	•	•	•
	•				•	•	•	•	•	•	•	•
	•				•	•	•	•	•	•	•	•

Trail No.	True	radiant <sup>δ</sup>	∙	₹ <sub>G</sub>	v <sub>H</sub>	λ	Sin Q	C.W.	K	M P	t	Qual.
5273	162 10	36 4	6 63.05	61.75	42.04	37.3	•239	2.75	3.03	-0.8	.34	3.0
5289	160 6	72	8 63.40	62.10	42.18	36 • 9	•223	•24	5.02	0.2	. 35	2.0
9130	278 34	30 4	0 17.98	14.48	39.57	121.6	•258	6.50	• 46	1.4	. 88	1.0
9147	91 30	44	1 58.79	57.51	41.27	43.5	• 321	4.70	1.85	-0.1	.47	2.0
9149	67 55	50 4	7 48.46	47.07	41.60	60.6	.516	9.50	2.21	-1.9	• 39	2.0
9170	59 43	-21 4	8 33.83	31.66	40.63	82.3	• 095	12.30	1.10	1.3	.86	1.0
9172	20 21	22 1	3 25.10	22.46	41.54	103.7	•265	5.80	1.76	-1.7	1.07	1.0
5332	20 13	42	9 23.04	19.96	38.36	98 • 2	.375	12.50	•26	1.1	.85	1.0
9238	53 48	13 1	.8 28.35	26.23	36.58	80.8	•472	3.70	•23	0 • 2	• 72	1.0
9240	50 52	12 3	1 26.20	23.90	36.30	83.7	•460	3.70	• 12	0.3	• 79	1.5
9246	53 45	14 4	1 29.34	27.43	37.20	80.5	. 568	2.90	• 35	1.1	.81	1.5
9252	31 4	12 4	0 19.84	16.87	37.44	102.2	•357	• 02	•08	1.7	.81	1.0
9257	53 39	21 2	4 30.40	28.63	37.36	79 . 0	.289	1.40	•42	-1.2	1.51	1.0
9265	54 19	22 3	3 30.53	28.31	37.53	80.0	• 387	1.90	•43	1.0	•57	1.5
9284	58 29	-18 3	4 26.34	23.99	37.76	87.8	•003	14.70	•18	-1.2	1.05	2.5
5346	57 33	14 1	8 28.75	26.28	36.72	81.0	•274	3.40	• 25	0.7	.83	1.0
5370	334 50	21 2	6 15.58	11.20	39.51	142.0	•409	5.40	•43	1.3	.65	1.0
9331	61 8	23 2	4 30.75	28.75	36.93	77.7	• 097	1.70	•37	-1.9	. 92	1.0
9335	101 40	- 2	4 58.52	57.28	41.73	44.8	•149	4.80	2.20	-1.5	• 50	1.0
5450	152 0	22 4	6 71.73	70•69	41.49	10.7	•435	• 15	1.49	-3.3	• 64	2.5
5472	180 47	68 3	3 46.75	45.30	39.79	59.7	.394	2.06	•51	-1.2	.60	1.0
5511	65 4	21	7 31.00	29.23	39.29	82.9	.287	•20	.77	-0.2	1.05	1.0
9375	56 13	13	0 21.96	18.72	37.42	97.1	.230	3.40	•10	1.0	.81	2.0
9379	22 22	48 3	9 19.63	16.14	39.30	112.4	.429	11.50	• 39	-0.3	.93	1.0
9411	121 38	23	9 60.39	59+40	42.22	42.2	• 066	4.20	3.36	-0.9	• 50	2.0
9416	77 49	14 5	2 25.61	23.30	37.28	87.3	.085	4.80	•19	-0.4	1.05	1.5
9418	105 3	32	3 36.30	34.61	34.03	62.9	.205	7.40	•43	-0.9	.58	1.0
5551	133 53	31 3	9 60.76	59.42	42.12	42.0	.261	3.80	3.04	0.6	.40	2.0
5557	67 40	-10 1	2 22.67	19.78	39.28	101.5	.192	12.41	.43	-0.6	1.22	1.0
9451	108 33	33 1	1 35.23	33.41	32.98	62.2	.234	8.30	• 31	0.0	. 56	1.5
5572	353 9	53 1	9 17.19	13.35	38.99	122.0	.146	9.03	•25	1.4	1.15	1.0
5601	110 9	32 5	8 36.66	34.63	34.02	62.8	.301	7.92	. 41	0.4	.58	1.0
5605	110 36	32 3	9 36.18	34.14	33.52	62.4	- 366	7.84	.37	-2.7	1.14	1.0
9507	110 55	22 1	2 25.29	33.63	33.14	62.2	. 293	8.50	- 32	-0.4	. 48	1.5
5640	110 33	32 3	5 37.13	35.14	34.61	63.4	.318	7.66	•47	0.9	.44	2.0
5644	111 24	12	8 35.56	33-51	33.24	62.6	- 390	7.53	. 33	-0.4	• 60	1.0
5648	111 28	32 4	0 34.21	34.20	33.71	62.7	438	7.96	• 37	-0.7	.74	1.0
9547	110 58	32 4	0 36.26	34.46	34.00	63.0	.189	8.00	.40	-1.0	.55	1.0
5759	112 20	32 3	8 36.41	34.34	33.81	62.8	.273	7.86	. 38	1.0	.67	1.0
9611	111 28	32 2	3 36.92	35.08	34.61	63.5	.351	7.70	• 46	-0.8	.55	1.0
8645	112 20	32 2	3 36-20	34- 39	33.86	62.8	.148	7.95	• 39	-3.5	1.10	1.0
9627	111 67	31 6	6 36.41	34.85	34.25	63.0	.171	7.60	.44	-0.8	.48	2.0
94 31	112 4	32 2	0 36.27	34.49	34.03	63.0	.232	8.00	.40	-0.2	.51	1.0
9454	112 18	22 1	36.04	34.40	33.90	62.9	.315	8.00	.40	-1.3	.63	1.0
9660	128 19	1 3	5 58.66	57.63	41.49	43.8	•036	4+80	2.04	-0.5	•45	2.5
9709	11 2 20	12 2	7 35.80	34-41	33.90	62.9	.154	8.30	• 39	-0.2	.58	1.0
9710	112 44	21 6	9 36.42	34.62	34.19	63.2	.355	7.70	.42	0.9	.50	2.0
0725	112 20	22.2	A 24.10	34.34	11.85	62.8	. 336	8.00	. 39	-2.4	.956	1.0
9123	113 44	22 6	A 24.74	25.00	34.47	63.4	405	7.80	.46	-1-0	. 54	1.0
9749	113 9	32 2	0 36+23	34.55	34.13	63.2	.271	8.00	•41	-2.5	. 84	1.0
					41 87	40.0	.0.84	1.09	2-01	-1-4	1.186	1-0
8640	152 22	-43 1	7 77+/4	59+72	41.66	42.0	-041	4.90	2.09	-0-8	.43	2.0
0840	150 9		3 30.39	22-22	38-22	92.2	.176	12.10	.24	-0-2	.50	1.0
/ = ] ]				<u></u>								

- **λ**: Elongation of the true radiant from the apex of the earth's motion, in degrees.
- sin Q: Q is the angle between the apparent great circles of motion as seen from the two stations.
- C.W.: Cosmic weight, a weighting factor intended to be inversely proportional to the probability that meteoroids of constant mass in their observed orbits will, in one revolution, collide with the earth and produce photographable meteors. C.W. is calculated from the expression,

$$C.W. = \frac{V_o \sin i}{V_{\bullet}^4} \left(2 - \frac{1}{a} - p\right)^{\mu},$$

where  $p=a(1-e^2)$ ; p and a are expressed in a.u. and the velocities in units of 100 km/sec (see Whipple, 1954).

- K: A criterion designed to distinguish statistically between cometary and asteroidal orbits. The K criterion is defined by the expression  $\log_{10}\left(\frac{q'}{1-e}\right)-1$ , where the aphelion distance is measured in a.u. The term q'/(1-e) is proportional to the inverse square of the aphelion velocity. In most cases K>0 for comets and K<0 for asteroids, but the values of K are not well known for asteroids of q<1.
- $M_{p}$ : Photographic absolute magnitude.
- t: Duration of longer photographed trails in seconds of time. Trails both limited by the edge of film are designated by G.
- Qual.: Quality class of velocity and orbit determination, defined in table 2 and in text (below).

### Classification on the basis of quality

When all sources of possible error are added, the velocities of good meteors turn out to be correct to approximately 0.1 percent, those of fair meteors to some 0.4 percent, and those of poor meteors (comprising less than 10 percent of the total) to approximately 1 or 2 percent.

We have tried to assign to each meteor a grade of reliability by which it is classified. Table 2 gives for each quality class in table 1 the most probable value of the relative error and the maximum error to be expected if all causes of error were working in the same direction.

TABLE 2.—E	rrors for meteor tabl	s of various qu e 1	ality classes in
Quality	Most prob- able error	Maximum	No. of such meteors in

Quality class	Most prob- able error (%)	Maximum error (%)	No. of such meteors in table 1
1	0.1	0.13	173
1.5	0.2	0.3	78
2	0.4	0.7	103
2.5	0.7	1.5	23
3	1.0	3	32
3.5	2	6	0
4	3	10	4

### Frequency distributions of orbital elements

On page 97 ff. we discuss certain minor selection factors operating in the choice of the meteoric trails reduced in the present program. A number of strong selection factors, however, enter into the statistical distributions of the orbital elements and, indeed, into the correlations among them. Certain of these factors are included in the quantity, cosmic weight (C.W.). Thus meteors of small orbital inclination or with apsides near the earth's orbit are distinctly favored. Also, the photographic technique appears to favor meteors of higher velocity, exclusive of the geometric factors involved. On the other hand, the effect of the cross-sectional area of the earth is to favor the slow meteors.

Perturbational effects, especially of Jupiter, play important roles in determining the distribution of orbital elements. A selective effect probably operates in the case of meteoric streams, resulting from the fact that the earth moves on a line through the stream. This effect is not well understood and deserves major consideration. Because of the complexity of this problem, however, no attempt will be made here to discuss it. A few of the statistical interrelationships among the observed orbital elements will be treated in the following sections and some of the major selectional factors will be discussed briefly.

Perihelion distance versus argument of perihelion.—Figure 1 is a plot of the perihelion distance against the argument of perihelion  $\omega$  for the observed meteors. A rather amazing correlation results from the fact that meteors must, by definition, be observed at the nodes of their orbits at heliocentric distances near 1 a.u. The effect of this requirement is peculiarly conspicuous in the figure because the eccentricities of

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FIGURE 1.—Argument of perihelion  $\omega$  plotted against perihelion distance q (all meteors).

the orbits are generally large and the aphelion distance much greater than 1 a.u. The concentration near the two parabola-like curves in figure 1 would be even more complete were meteoric observations from a point near the equator possible on a 24-hour basis. A complete discussion would involve the detailed effects resulting from night versus day, northern versus southern hemisphere, and ascending versus descending node. We merely show the diagram as a warning that correlations among orbital elements of meteors as well as among distribution functions must be evaluated carefully in terms of selection effects.

Inclinations of orbits having aphelia within Jupiter's orbit.—One of the authors (Whipple, 1940) investigated the perturbations in the angular elements of meteors derived from Comet Encke and showed that the Taurid meteor shower is associated with this comet. Some of the conclusions apply broadly to all meteors in orbits with aphelion distances less than the perihelion distance of Jupiter. With the secular perturbations in node, for Comet Encke the inclination varies over the range from  $4^{\circ}$  to  $16^{\circ}$ (with respect to the plane of Jupiter's orbit, not far from that of the earth). For similar orbits of small perihelion distance, the condition heliocentric distance r=1 a.u. at the node permits encounters with the earth only when the inclination is relatively low, approximately  $4.6^{\circ}$ .

On the other hand, the rate of change of the node at this orientation is a maximum and strongly influences the chance of encounter with the earth. Hence, any theory dealing with the distribution of inclinations or with the dependence of inclination upon perihelion distance, for orbits with aphelia lying within Jupiter's orbit, must be carefully studied if the observed distribution or correlation is to be of significance. The ramifications of these perturbational relationships are too involved for the present paper. They are mentioned only to indicate that the mean inclinations of the very short-period meteor orbits in space may be seriously underestimated because of the peculiarities of the perturbations of Jupiter.

Inclination versus perihelion distance.—Figure 2 depicts the observed distribution of meteors with respect to perihelion distance and inclination. As is to be expected from geometrical selection effects, a high concentration of observed meteors occurs near q=1 a.u. and near i=0. No conspicuous gaps occur in the

diagram except in the neighborhood of q=0, and possibly near  $i=90^{\circ}$  for small q.

Although there is no dearth of comets with small perihelion distances, the meteoric distribution cuts off sharply at q=.05 a.u. with only 3 sporadic meteors having q<0.1 a.u. The remarkable  $\delta$ -Aquarid shower shows a high concentration near q=0.06 a.u. with a minimum value of 0.047 a.u. Six of the 7 sporadic meteors with q<0.15 a.u. are of short period with aphelion distance <5 a.u. The inclinations are all moderate,  $<40^\circ$ .

We conclude that the sun's energy, possibly heat or corpuscular radiation, eliminates mete-



FIGURE 2.—Orbital inclination *i* plotted against perihelion distance *q*. Major showers (mean values) are indicated by circled dots.

ors rapidly within a distance of .05 a.u. and effectively reduces the numbers with q < 0.1 a.u. The existence of the dense  $\delta$ -Aquarid stream, however, with q < 0.1 a.u. suggests strongly that these effects do not arise from direct melting or destruction but from some slow process such as etching by corpuscular radiation or by sublimation in the range 0.05 < q < 0.10 a.u.

A possibly significant scarcity of meteors, both shower and sporadic, near inclination 90° may be associated with the minimum of comet frequencies in this same range. The effect may well be of a perturbational character and deserves more thorough study.

Inclination versus aphelion distance.—In figure 3 orbital inclinations are plotted against  $q'^{-1/2}$ , where q' is the aphelion distance ex-



FIGURE 3.—Orbital inclination *i* plotted against aphelion distance q'. The variable in abscissa is  $q'^{-1/2}$ ; heliocentric distances of the major planets are marked at the bottom. Major showers (mean values) are indicated by circled dots.

pressed in a.u. This parameter was chosen in preference to q' or  $q'^{-1}$  to avoid the crowding of points at one end of the diagram.

At great aphelion distances the distribution is rather uniform with inclination although there is some scarcity of low inclination orbits. The effect of Jupiter's perturbations shows strikingly for aphelia between Jupiter and the asteroids, where retrograde orbits are absent and the mean inclination falls rapidly as the aphelion distance decreases. The apparent concentration near the orbit of Mars does not seem to be real (see data of Hawkins and Southworth, 1958).

No concentration at all is evident in the region of the asteroid belt. This fact is a powerful argument against an asteroidal origin of an appreciable number of the meteors in this collection. The concentrations of major showers near the ranges 0.1 to 0.2 and 0.4 to 0.6 in  $q'^{-1/2}$  are of some interest. The former concentration may, of course, be fortuitous. The latter indicates a strong dependence of shower comets on Jupiter's perturbations, with some longevity in orbital characteristics attained by those showers with aphelia inside of Jupiter's orbit. It appears to be very difficult for comet aphelia to be reduced much below 2 a.u.; the Geminids represent an extreme case. Figure 3 is very similar to a corresponding figure for comets except for the dearth of comets with very small aphelion distance. Such comets, of course, would be very short lived and it is difficult to see how they could develop. Meteors, on the other hand, subject to physical forces, can theoretically attain quite small aphelion distances.

Aphelion distance versus longitude of aphelion.— We have already seen that aphelia for meteors are highly concentrated near Jupiter's orbit. In figure 4 the aphelion distance is plotted as a. function of longitude of aphelion with the corresponding radius-vector of Jupiter indicated as a curve. There is a slight tendency for the distribution of meteoric aphelia to fall off just beyond Jupiter's orbit. It is not clear, however, that this effect is statistically significant.

Among the asteroids the concentration of aphelia in the direction of Jupiter's aphelion is extremely marked. The effect exists because the perturbations of Jupiter are greater when the asteroidal aphelion is closer to the orbit of Jupiter and the consequent forward motion of the line of apsides is more rapid. Thus, the aphelia tend to concentrate in the direction of Jupiter's aphelion. We should expect such an effect for meteor orbits that lie entirely within Jupiter's orbit. No such tendency is indicated in figure 4. Apparent concentrations appear to be possibly significant some 90° from Jupiter's line of apsides. Three possible explanations for this lack of a well-explained perturbational effect are as follows:

(1) Physical forces change the lines of apsides for meteors more rapidly than do Jupiter's perturbations.

(2) Meteors of small aphelion distance may be contributed by a relatively small number of comets (or other bodies) and show a random distribution because of the small statistical selection of sources.

(3) The lifetimes of meteoroids may be extremely short, appreciably smaller than the revolution period of apsides.

Explanation (1) is purely hypothetical insofar as physical perturbations of meteoroids are concerned. The major physical forces that have been considered are the Poynting-Robertson effect, corpuscular radiation from the sun, and encounters with meteoritic dust. There is no evidence that electromagnetic forces act appreciably on meteoroids while the forces listed above should not generally shift the lines of apsides appreciably. In other words, if physical forces are responsible for the lack of concentration of lines of apsides, these forces must be of a character not yet considered seriously.

The number of recognized meteor streams is relatively small and a few major sources, such as extraordinarily large comets, may indeed play a significant role in providing the observed meteors. Nevertheless, if meteoroids had long lifetimes we should expect the Jupiter effect to be manifest in the distribution of the lines of apsides.

Hence, it seems necessary to conclude that meteors are injected into their orbits without a significant correlation with the lines of apsides of Jupiter's orbit, and that their lifetimes are relatively short. For Comet Encke, with an aphelion distance of 4.1 a.u., the line of apsides revolves in some 13,000 revolutions. The Taurid meteors can be traced back in history by their association with Encke's comet through



FIGURE 4.—Aphelion distances q' plotted against the longitude of aphelion  $\pi + 180^{\circ}$ . Only meteors with q' < 8 a.u. are shown in the diagram. The curve represents Jupiter's heliocentric distance. Major showers (mean values) are indicated by circled dots.

some 1,500 revolutions, not much more than 10 percent of a complete revolution in the line of apsides. Although aphelia near Jupiter will move somewhat more rapidly than that of Comet Encke, nevertheless we clearly should expect no concentration of the lines of apsides for meteors if the ordinary meteor lifetime averages less than perhaps 2,000 to 3,000 revolutions.

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Since meteors (see p. 125) originate almost

entirely from comets, and since the lines of apsides of comets with aphelia near Jupiter or within its orbit appear not to be concentrated by perturbations by Jupiter, we appear to have a satisfactory explanation of figure 4 in terms of short lifetimes for meteors. The fact that some 60 percent of the meteors exist in identifiable streams or associations is added evidence for their short lifetimes because a number of forces, both physical and gravitational, tend to disturb the stream motions and hide the evidence for comet origin.

Geocentric velocity versus elongation of the radiant.-For certain types of meteoritic orbits our only reliable information is the elongation of the radiant. Hence we present the meteor data in figure 5, where the ordinate is geocentric velocity. Va (corrected for earth's attraction), and the abscissa is the elongation,  $\lambda$ , of the corrected radiant from the apex of the earth's motion about the sun. Small values of  $\lambda$  correspond to the high-velocity meteors that make head-on encounters with the earth, while large values correspond to relatively slow meteors that "catch up" with the earth. The continuous curve in figure 5 indicates the parabolic limit in  $V_{\alpha}$ . For elongations up to about 60° the observed values describe a curve parallel to the parabolic one, with a rather narrow scatter. Above about 60° in  $\lambda$  the effect of short-period orbits occurs and extends the range of velocities over an area much below the parabolic limit in geocentric velocity. The asteroids with perihelia inside the earth's orbit would occur near the lower edge of the distribution in figure 5. with a concentration near elongation 90°.

#### Sources of meteors

With the precise material presented in the previous pages, we may now consider possible sources of these photographic meteors.

Interstellar meteors.—Meteoroids of immediate interstellar origin should travel in hyperbolic orbits about the sun. Table 1 lists 7 meteors with hyperbolic velocities and 2 with parabolic velocities. Among the 7 hyperbolic meteors none is of quality as high as 1.5, while the one parabolic case is of quality 1. Hence, among the 251 meteors of highest quality, there are no hyperbolic and only one parabolic velocities measured. Four of the 7 hyperbolic cases lie among the 36 meteors of poorest quality.

All meteors with nearly hyperbolic velocities have been carefully restudied to search for errors in the calculations and to determine whether uncertainties in the instant of the meteor might lead to a spurious determination of a hyperbolic velocity. In all cases an elliptical solution can be obtained by use of an instant within the common interval of exposure. No evidence exists that the velocities of identified shower meteors differ significantly from those of the comets with which they are associated. This fact can be used to indicate that the systematic errors in meteoric velocities are small, not exceeding the errors indicated on page 114.

Any hypothesis that hyperbolic meteors are selectively avoided in the photographic meteor program because of their greater apparent velocities appears to be unfounded. Strong evidence indicates that a given body moving at high velocity through the atmosphere produces more light than a similar body at a lower velocity, and that the luminosity dependence is more than linear with the velocity. For meteors of the same intrinsic brightness the camera's ability to register the meteor varies roughly as the inverse product of distance and velocity. Since faster meteors occur at somewhat higher altitudes than slower meteors, the product is the inverse velocity raised to a power slightly less than unity. Hence the luminosity and the geometric factors combine to favor the photography of more rapidly moving meteors in preference to slower moving ones.

The criteria of selection used here for meteor trails favored the slower meteors because those of highest angular velocity tend to produce fewer shutter breaks; this effect was partially compensated by the inclusion of more of the faster meteors than would have been allowable by strict application of the selection criteria. Hyperbolic meteors, moreover, need not enter the atmosphere with high velocities. The fact that observed borderline cases occur almost entirely in the high-velocity range casts further doubt on the existence of hyperbolic meteors.

The observing program ran continuously through the hours of darkness for more than 2 years; hence any selection factor stemming from a lack of observations in the late night hours versus the early evening hours appears not to be serious.

We conclude, therefore, that hyperbolic meteors constitute, at most, less than 1 percent of our sample—the most precise photographic material yet available—and that there is no strong evidence for the existence of any hyperbolic meteors. This conclusion agrees with that obtained by radio techniques in the researches of



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McKinley (1951) in Canada, and of Lovell (1949) and associates (see Almond, Davies, and Lovell, 1953) in England.

The occurrence of hyperbolic meteors remains to be demonstrated.

Lunar meteoroids .-- It has been suggested recently by Urey (1960) that the encounter between large meteorites and the moon might produce an appreciable number of secondary meteorites from lunar material, which subsequently would have a moderate probability of falling on the earth. In the present collection of 413 meteor orbits only one has a geocentric velocity ( $V_{\sigma}$ , corrected for earth attraction) below 9 km/sec. This is meteor No. 4952, which fell on October 19, 1952, with  $V_o$ =3.41 km/sec. Its hypothetical velocity of ejection from the moon would have been increased by the effect of the earth potential at the moon (1.0 km/sec) and the lunar velocity of escape (2.38 km/sec), so that it would have required a lunar ejection velocity of 4.4 km/sec. The study by Hawkins and Southworth (1958) of randomly selected fainter meteors indicates 6 meteors with velocities of ejection from the moon less than 9 km/sec.

Further criteria are not available for any of these meteors except one. For number 4952, Jacchia (unpublished) finds that its behavior in the upper atmosphere is normal as compared with the average of the other slow meteors.

Of the few meteors that have aphelion distances less than 1.4 a.u.-only 3 out of the 413-all have aphelia less than 1.1 a.u. This fact strongly suggests that the earth, in some manner or other, is responsible for this concentration. This concept is strengthened by the data of Hawkins and Southworth, which indicate that of 12 meteors with aphelia less than 1.3 a.u., 7 have aphelia less than 1.1 a.u. About half the meteors of small q' have geocentric velocities much too great to ascribe to lunar ejection-2 out of 3 among the 413 presented here and 6 out of 12 from the data of Hawkins and Southworth. These ratios suggest that the earth perturbs meteor orbits, possibly by "capture" phenomena as has happened for comets and meteors with aphelia near Jupiter. The capture phenomenon and the concomitant encounter phenomenon are both favored by low orbital inclinations and apsides near the earth's

orbit. Hence the few data available do not answer the question as to whether lunar ejection is likely or not for the very few possible examples.

The lunar ejection theory for meteorites is greatly weakened by the fact that the collisional cross-section of the earth is much greater than that of the moon, by approximately a factor of 16, if we neglect the additional gravitational factors at low relative velocities. Unless the process of formation and ejection of secondary meteorites by encounters between primary meteorites and the moon is extremely efficient, one would expect only a small fraction of the total number of meteorites found on the earth to be of lunar origin. The low velocity of encounter with the atmosphere, required by a lunar ejection mechanism, is not a great compensating factor.

In summary, we find little or no evidence to support the hypothesis of meteoric ejection from the moon, although for photographic meteors the hypothesis is not excluded at approximately the 1 percent level.

Comets and asteroids.—In earlier sections we have shown that no appreciable fraction of the meteors discussed here could have come from sources outside the gravitational control of the sun, or from encounters between larger meteoritic bodies with the moon. Observationally, each of these sources is within the 1 percent level of probability and no evidence proves the existence of either source.

There remain two obvious sources of meteors: comets and asteroids. The only proven source of meteors is cometary. Whipple and Hawkins (1959) identify 12 meteor streams with 9 comets, the association of the  $\eta$  Aquarids and Orionids with Halley's comet being somewhat uncertain. Tentative identifications of other meteor streams with as many as 20 comets have been made and are fairly probable; the list grows continuously with increasing orbital information on meteors. Incidentally, the present orbital information on meteors now exceeds both in quantity and quality that on comets.

These positive and tentative identifications leave a major fraction of the observed meteors without a known source. In the search for possible asteroidal sources, we must consider the character of asteroid orbits. If an asteroid is to contribute meteors, its perihelion must lie near or within the earth's orbit. Only 7 asteroids have been observed to pass within the earth's orbit; hence our sample for comparison is extremely small. The mean aphelion distance of these asteroids is 2.2 a.u. and the inclinations are generally small. Since we know of only 1 asteroid, Hidalgo, that passes beyond Jupiter's orbit (neglecting, of course, the Trojans), it seems to be a proper assumption that meteors of asteroidal origin should have aphelia well within Jupiter's orbit, perhaps concentrated in the major portion of the asteroid belt or its inner reaches. No asteroidal aphelion is known to lie within the orbit of Mars.

No meteor orbit in the present collection appears to be sufficiently like that of any individual asteroid to suggest a specific genetic association. If, then, we eliminate as of asteroidal origin all meteors with aphelia very close to the orbit of Jupiter and beyond, as well as those definitely associated with known comets, we will have reduced the asteroidal source to less than approximately 40 percent. If we choose aphelion distance near and beyond the environment of Jupiter as a criterion for cometary origin, and if we assume in addition that all meteors in streams or associations are of cometary origin, then we reduce the potential asteroidal contribution to less than 11 percent. Since the percentage of the meteors identifiable with streams will increase as a larger number of accurate meteor orbits becomes available. it seems quite safe to conclude, on the basis of these assumptions, that the asteroidal contribution to the present collection of photographed meteors cannot possibly exceed 10 percent. Let us now seek evidence that any of the remaining 10 percent are actually of asteroidal origin.

A somewhat more vivid picture of the distribution of aphelion distances is shown in figure 6, where the meteoric data have been divided into two groups: sporadic, and showers plus associations. The frequency distributions have been compared with the total number of comet passages in the list by Baldet and De Obaldia (1952), except that the orbits listed as parabolic have been excluded because of the generally poor orbital determinations (comparison is properly made between the distribution of *all* cometary passages and the observed meteoric distribution).<sup>2</sup> The histogram is in terms of the argument  $(q')^{-1/2}$  and the meteor groups reduced to a common basis of 1000. The three sets of curves are very similar in general character, and suggest that the meteoric orbits are shifted towards somewhat smaller values of q' than the comet orbits. In particular, there is a marked absence of very great aphelion distances among the meteors, while the comets show the well-known heavy concentration near the parabolic limit.

The influence of Jupiter's perturbations is markedly shown in all three curves, the most striking feature of the distribution function. One has the impression that meteoric orbits are pressing against the Jupiter barrier (Whipple, 1951, 1955; Öpik, 1951). The sporadic meteors include a considerable number of longer period, in comparison to the shower meteors, but otherwise the two distributions are so nearly identical in form that it is difficult to draw any other conclusion than that the two classes of orbits are similar, and that the bodies are probably of the same origin.

A number of other orbital data are available for a comparison among the three groups of elements, for sporadic meteors, showers plus associations, and comets. The distributions of inclinations are similar in character, as noted earlier, and the lines of apsides appear not to give any clues of importance. The K criterion, used earlier by one of the authors (Whipple, 1954) apparently will not be particularly valuable until we have far greater information concerning the asteroids that cross the earth's orbit. Furthermore, it is not certain that the K criterion is more significant than the distribution of aphelion distances. So many selection factors enter into the cometary statistics as well as the meteor statistics that an exact equality of distributions is hardly to be expected. Other elements than those discussed seem not to add appreciably to a solution of the problem but are entirely consistent with a cometary origin for photographic meteors.

A comparison of the present collection of meteor orbits with those of comets indicates a

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<sup>&</sup>lt;sup>3</sup> More precisely, the frequencies could be properly corrected for the cosmic weight. This has been done but has not been presented here since the histograms are not markedly changed by this weighting factor.



FIGURE 6.—Distribution of aphelion distances for comets, shower meteors, and sporadic meteors. Ordinates are numbers of objects reduced to a standard population of 1,000 in intervals of 0.04 of  $q'^{-1/2}$ . Comets for which only parabolic orbits had been computed were eliminated from the comet distribution.

connetary origin for at least 90 percent of the meteors. If we assume that meteors in streams and associations are of cometary origin, the general similarity of their distribution functions with those of the sporadic meteors would indicate no significant difference in origin; therefore, a cometary origin appears likely for practically all meteors. One of the authors (Jacchia, unpublished) can find no significant difference in physical characteristics among meteors with very small orbits of low inclination, among typical stream meteors, or among meteors with distinctly cometary orbits. Striking evidence exists that photographic meteors are produced by extremely fragile objects (Jacchia, 1955; McCrosky, 1955), and the forward motions in meteoric trains (Cook and Whipple, unpublished) provide strong indications that photographic meteors may be of extremely low density. Such evidence makes it doubtful that the photographic meteoroid is comparable to the iron or stony meteorites that fall on the earth.

The writers are of the opinion that the asteroidal contribution to the photographic meteors probably does not exceed 1 percent of the total and may well be less.

### Meteor streams and associations

The selection of meteor streams and associations given in tables 3 and 4 is not intended to be definitive. The dividing line between the terms "stream" and "association" is not rigidly defined. The intent here is to indicate the nature of the streams and associations to be found by intercomparison of a limited amount of rather precise data, the 413 orbits of the meteors listed in table 1, and the 144 brighter orbits previously published (Whipple, 1954). Other investigators might apply more rigid rules or might be constrained to include even more members in the associations.

TABLE	3.—Code	for	identifying	known	meteor	showers
			listed in to	ible 1		

Shower No.	Shower	
None	Sporadic meteor	
1	a Capricornids	
2	Southern Taurids	
3	، Aquarids (So.)	
4	Geminids	
5	δ Aquarids	
6	Lyrids	
7	Perseids	
8	Orionids	
9	Draconids	
10	Quadrantids	
11	Virginids	
12	« Cygnids	
13	Leonids	
14	χ Orionids	
15	Ursids	
16	σ Hydrids	
17	Northern Taurids	
18	Andromedids	
19	n Aquarids	
20	· Aquarids (No.)	

The large variations that occur in the orbits of certain comets, such as Lexell or Brooks II, must also certainly occur among the orbits of meteors both before and after their ejection from comets. Refined analysis in many cases will undoubtedly indicate widespread variations in the orbital elements of meteors originally produced by the same comets.

We find a number of low inclination streams with components in which the line of nodes is shifted by 180°. This phenomenon was first observed for the Taurid meteors in association with Comet Encke (Whipple, 1940).

# TABLE 4.—Identification of tentative meteor associations listed in table 1

[EXPLANATION: (N), northern branch of the stream; (S), southern branch of the stream; parentheses, small camera meteors not included in table 1 but listed in Whipple (1954).]

Associ- ated Shower No.	Trail No.	Date	Remarks
30	10012	1- 4-54	
	(1918)	(1-20-50)	
31	(2889)	(1-15-51)	
	6275	1-20-53	
32	(1257)	(1-22-44)	
	(1988)	(1-23-50)	
	6329	1-23-53	
33	6376	2- 5-53	
	(1243)	(2- 6-45)	
34	6433	2-12-53	
	6546	2-21-53	
35?	6802	3-12-53	
	7052	3-21-53	
36	6811	3-12-53	
	6842	3-13-53	
37	6882	3-14-53	Same as Association
	10342?	3-26-54	Whipple II, origi-
	(1920)?	(4–21–50)	nally composed of meteors 1920 and 2031. It now seems very doubt
			ful that 2031 belongs to this

group.

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TABLE 4.	Identific listed i	ation of tentation table 1—Con	ive meteor associations ntinued	TABLE 4.—Identification of tentative meteor associations           listed in table 1—Continued				
Associ-				Associ- ated				
Shower		1		Shower	-			
No.	Trail No.	Date	Remarks	No.	Trail No.	Date	Remarks	
(38	6915	3-18-53		51	7210	4-11-53		
	6971	3-19-53			7592	5- 9-53		
	7040	3-20-53						
	(1068)	(2 - 23 - 41)		52	7075	4- 4-53		
	(1000)	( 3-23-31)		01	10555	4-12-54		
1 í	1001	4- 0-00			75999	5		
	00.50	0 00 50	Describbe selected		2244	5 91 59		
39	3076	3-22-52	Possibly related		0044	5-21-52		
	10394	4- 2-54	to No. 38.		3312	5-22-52		
1					3307	5-22-52		
					4141	6-22-52		
40	6959?	<b>3</b> –18–53						
	7161	4-9-53		(53(N)	7476	5- 5-53		
	10094	4-10-54			7534	5- 7-53		
				1	3295	<b>5–23–5</b> 2		
141	7002	3-19-53			(1205)	(5-25-43)		
	(1937)	(3 - 23 - 50)		)				
	(1001)	(,		)54(S)	7474	5- 5-53		
42	10384	4- 2-54	Possibly related		3327	5 - 21 - 53		
12	10430	4 5 54	to No. 41					
	10447	4 5 54		55	7478	5- 5-53	Probably related	
`	10447	4-0-04		l	7637	5-12-53	to Nos. 53, 54.	
49	F 0 0 0	9 90 59						
43	5068	3-20-53		56(N)	7520	5- 7-53		
	3024	4- 1-52			7664	5-13-53		
					3303	5-22-52		
44	3053	3-20-52			0000	0 0-		
	10414	4- 5-54		57(8)	11995	5 2 54		
				101(0)	11020	5 3 54		
45	7022	3-20-53			5490	J- J-J4		
	3088	3-28-52			7480	5-0-53		
	7392	4-16-53			7494	5- 0-53		
				59	7400	5 6 52	Probably related	
46	10365	4-1-54		00	7499	5-0-55	A Neg 56 55	
	10478	4-6-54			1035	5-12-55	10 NOS. 50, 57.	
				-0				
(47(N)	10358	4-1-54		59	7524	5- 7-53		
	(2918)	(4 - 4 - 51)			10587	6- 4-54		
	(3454)	(4-12-51)						
{	(0101)	(1 +2 01)		60	3342	5 - 21 - 52		
10(9)	10106	4 1 54	Polated to No. 47		3288	5 - 24 - 52		
40(0)	7916	4 11 59	Related to No. 47.					
(	7210	4-11-33		61	(2862)	(5-20-50)	Nos. 61, 62 very	
10					12399	6-2-54	probably are one	
49	7073	4- 4-53			(2024)	(6 - 9 - 50)	single diffuse	
	7272	4-13-53			7882	6-13-53	stream : could	
	7333	4-15-53		{	4125	6-10-52	be related to	
	3234	<b>4</b> –2 <b>3</b> –52			4120	0-19-52	No 52	
	3250	4-26-52		60	4109	6 1 50	NO. 52.	
				02	4103	0- 1-52		
50	7158	4-9-53		ι	7820	6- 9-53		
	7184	4-10-53						
	7240	4-11-53		63	7734	6-4-53		
	73677	4-16-53			7750	6- 5-53		
	7372	4-16-53			4111	6-14-52		
	73897	4_16_52						
	(1054)9	(4-17-50)		e A	7749	6 5 59		
	(1994)[	(4-17-30)		04	1144	0- 0-00		
					1181	0-8-53		

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TABLE 4	.—Identifice listed i	ation of tentation table 1—C	ive meteor associations ontinued	TABLE 4.—Identification of tentative meteor associations listed in table 1—Continued				
Associ- ated Shower				Associ- ated Shower				
No.	Trail No.	Date	Remarks	No.	Trail No.	Date	Remarks	
65	7758	6- 5-53		787	4360	9-16-52		
	7873	6-13-53			8819	10- 2-53		
66	(2863)	(5-23-50)		(79(N)	4328	9-14-52		
	12342	5-31-54			4369	9-16-52		
	7744	6- 5-53			4464	9-19-52		
	7754	6- 5-53						
	4147	6 - 22 - 52		80(S)	4340	9-14-52	Nos. 79. 80 are	
	4153	6-23-52		1	4351	9-14-52	related.	
					4505	9-20-52		
67	12577?	6-11-54		1	4542	9-25-52		
•••	4143	6 - 22 - 52		100	4657	9-27-52		
	4181	6-25-52			8766	9-30-53		
68	4138?	6-21-52		81	4454	9-19-52		
	4151	6-22-52			4622	9-27-52		
	8113	7-23-53			4683	9-28-52		
69	<b>7944</b>	7- 6-53	Could be related to	82	4702	9-24-51	,	
	8017	7 - 15 - 53	No. 66.		4534	9-25-52		
-				83	(1180)?	(10-4-42)	Same as Association	
70	3393	7-25-52			(2463)?	(10 - 9 - 50)	Whipple V	
	(2073)	(8-10-50)			4962	10-21-52		
					5073	10-22-52		
71	8192	8- 5-53			0010	10 22 02		
	8417	8-10-53		94	8881	10- 6-53	May be related to	
	3663	8-21-52		04	4064	10-21-52	the Dreconide	
	3877	8-31-52			9130	11- 2-53	(Giacobinida).	
(79	70469	7 4 59						
12	9447	0 11 59		85	8974	10- 9-53		
	8510	8-13-53			4966	10-21-52		
				86	5237	10-24-52		
73	8143	8- 4-53	Nos. 72, 73 possibly		(3134)	(11- 6-51)		
	(2185)	(8- 9-50)	are related					
	8476	8-13-53	streams; asso-	87	(2624)	(11- 6-50)	Same as Association	
	3633	8-20-52	ciated with <i>x</i>		(2622)	(11-7-50)	Whipple VI.	
l	3813	8-25-52	Cygnids?		9252	11- 7-53		
174	8944	8_ 6_52		00		10 10 80		
1.1	8211	0- 0-00 9 7_52		88	0012	12-10-52		
	3640	8-20-52			(2292) 08887	(12-12-50) 1- 1-54		
						1 1 01		
75	8394	8-10-53	Nos. 74, 75 are re-	The f	act that	268 out of 4	413 meteors can be	
	8415	8-10-53	lated streams.	placed i	in associa	tions-ever	h though the crite-	
(76	4289	9-10-52		rion ma	ay be so	mewhat lo	ose—is proof that	
	4624	9-27-52		streamin	ng is a	major ph	enomenon among	
	4679	9-28-52		meteors	This is	not surpri	sing when we con-	
}	(1514)?	(10-12-47)		sider th	nat, on a	stronomica	I time scales, the	

77 Nos. 76, 77 pos-9-13-52 4313 4388 9-17-52 sibly are related streams.

lifetimes of small bodies must be quite finite. On the other hand, the orbital evidences of origin for meteors crossing the orbit of Jupiter

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would be lost long before an appreciable percentage of the bodies would be eliminated by encounter or major perturbational effects. For orbits lying entirely within that of Jupiter the expectations are not so clearcut. Asteroidal families have long been recognized by their orbital characteristics and presumably must persist over periods of time measured possibly in hundreds of millions of years. The Poynting-Robertson effect alone would destroy such associations, in terms of possible identification, in much shorter times for meteors in the photographic range with masses measured in grams. More research along these lines is urgently needed in order to clarify the time scales applicable to the lifetimes of meteors. We can see that these are measured in terms of a very few thousand revolutions, but other approaches to the problem are highly desirable.

Table 5 gives some tentative identifications of known comets with the meteor associations indicated in table 4. Five of these cometary associations appear quite valid and six others fairly probable. Three are in the extremely doubtful category. As a larger number of precise meteor orbits become available, the number of such identifications will undoubtedly increase. A more definitive identification of meteor streams and cometary associations can be made from a combination of the other photographic evidence available, particularly the concurrent publications by Hawkins and Southworth (1961) and by McCrosky and Posen (1961).

 
 TABLE 5.—Possible associations between comets and meteor associations of table 4

Associated Shower	
No.	Comet
33	1833 ?
34	1947 c
36	1826 III ??
40	1886 I ?
44	1858 III (Tuttle-Giacobini)
47, 48	1834
51	1945 c ?
52	1930 VI
61, 62	1930 VI ?
66	1770 I (Lexell)
68	1864 II ?
81	1790 I ???
84	P Giacobini-Zinner?
86	1779 ??

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#### Abstract

Orbital results are presented for 413 long-trail meteors doubly photographed with the Baker Super-Schmidt cameras in New Mexico and reduced by precise methods. The error in velocity probably does not exceed 0.1 percent for 173 meteors, or 0.4 percent for 181 others.

With such exact material it is now possible to determine definitively the source of meteors in the visual range. The obvious possibilities are interstellar, cometary, asteroidal, and secondary lunar sources.

Meteors of interstellar origin would move in hyperbolic orbits about the sun. The 251 orbits of precision 0.2 percent in velocity include no hyperbolic cases; for 7 hyperbolic orbits among the less precise cases, a long-period solution exists within the possible range of each. Hence more than 99 percent, if not all, must have been gravitational members of the solar system. The orbital data alone indicate that more than 90 percent of these, probably more than 99 percent, must be cometary in origin, while the physical data from decelerations and light curves show no unusual characteristics for the remainder. The number of meteoroids produced by the encounter of meteorites with the moon cannot exceed the 1 percent level of probability among the current selection. Thus comets seem to supply essentially all the visual meteors and probably also smaller meteoroids.

A number of statistical correlations among meteor orbital elements are shown and commented on. Also a preliminary study of meteor streams and associations is made. Several new cometary associations with meteor streams are suggested.

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