SMITHSONIAN MISCELLANEOUS COLLECTIONS
VOLUME 86 (WHOLE VOLUME)

SMITHSONIAN METEOROLOGICAL TABLES

[BASED ON GUYOT'S METEOROLOGICAL AND PHYSICAL TABLES]

FIFTH REVISED EDITION
(Corrected to January, 1931)



(Publication 3116)



CITY OF WASHINGTON
PUBLISHED BY THE SMITHSONIAN INSTITUTION
1931



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SMITHSONIAN MISCELLANEOUS COLLECTIONS

VOL. 86



"EVERY MAN IS A VALUABLE MEMBER OF SOCIETY WHO, BY HIS OBSERVATIONS, RESEARCHES, AND EXPERIMENTS, PROCURES KNOWLEDGE FOR MEN"—SMITHSON

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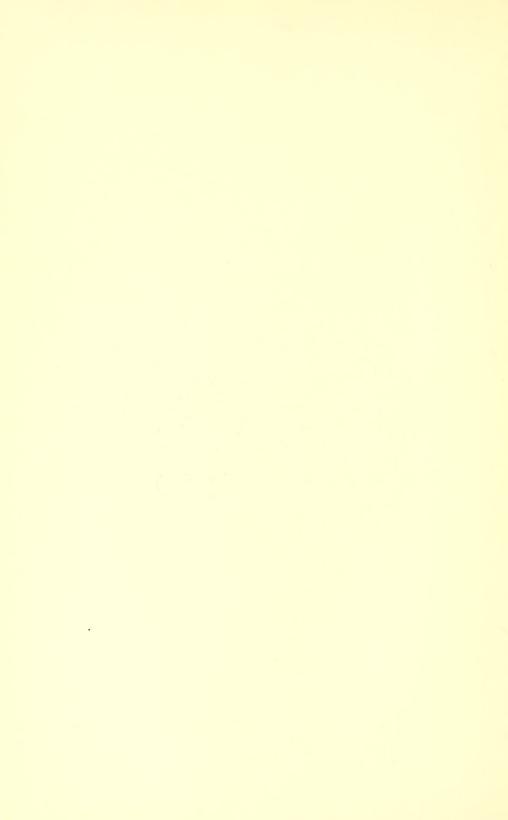
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The present series, entitled "Smithsonian Miscellaneous Collections", is intended to embrace all the octavo publications of the Institution, except the Annual Report. Its scope is not limited, and the volumes thus far issued relate to nearly every branch of science. Among these various subjects zoology, bibliography, geology, mineralogy, anthropology, and astrophysics have predominated.

The Institution also publishes a quarto series entitled "Smithsonian Contributions to Knowledge". It consists of memoirs based on extended original investigations, which have resulted in impor-

tant additions to knowledge.

C. G. Abbot, Secretary of the Smithsonian Institution.



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SMITHSONIAN METEOROLOGICAL TABLES. Fifth Revised Edition. (Corrected to January, 1931.) 282 pages. 1931. (Publ. 3116.) (Whole volume.)







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VOLUME 86 (WHOLE VOLUME)

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CITY OF WASHINGTON

PUBLISHED BY THE SMITHSONIAN INSTITUTION
1931

THE FORD PALTIMORE PRESS
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ADVERTISEMENT TO FIFTH REVISED EDITION.

The original edition of the Smithsonian Meteorological Tables was issued in 1893, and revised editions were published in 1896, 1897, 1907, and 1918. A fifth revised edition is here presented, which has been prepared under the direction of Charles F. Marvin, Chief of the U. S. Weather Bureau, assisted by Herbert H. Kimball, Senior Meteorologist of the same bureau. Officials of the U. S. Bureau of Standards have been consulted relative to the value of certain physical constants that enter into the calculation of the tables. All errata thus far detected in the earlier editions have been corrected.

The great development in the exploration of the free air to the height of the tropopause and even beyond calls for an extension of some tables to adapt them to the low temperatures and pressures experienced at these great heights, and also for a distinction between the symbols for the acceleration of gravity at the surface of the earth and in the free air. Also, the measurement of heights as "geopotentials" in "dynamic meters" calls for five new tables. The table of international meteorological symbols has been revised, and a table of "International code for horizontal visibility" has been added. Much of the work of extension of old tables and the computation of new ones has been done by the Aerological Division of the Weather Bureau.

The complete revision of the "List of meteorological stations," including an alphabetical arrangement by continents, countries, and stations, has been effected by Mr. W. W. Reed of the Climatological Division, U. S. Weather Bureau.

CHARLES G. ABBOT, Secretary.

SMITHSONIAN INSTITUTION, March 21, 1931.

ADVERTISEMENT TO FOURTH REVISED EDITION.

The original edition of the Smithsonian Meteorological Tables was issued in 1893, and revised editions were published in 1896, 1897, and 1907. A fourth revised edition is here presented, which has been prepared under the direction of Professor Charles F. Marvin, Chief of the U.S. Weather Bureau, assisted by Professor Herbert H. Kimball. They have had at their disposal numerous notes left by the late Professor Cleveland Abbe, and have consulted with officials of the U.S. Bureau of Standards and of other Government bureaus relative to the value of certain physical constants that have entered into the calculation of the tables.

All errata thus far detected in the earlier editions have here been corrected. New vapor pressure tables, derived from the latest experimental values by means of a modification of Van der Waals interpolation formula devised by Professor Marvin, have been introduced. The table of relative acceleration of gravity at different latitudes has been recomputed from a new equation based upon the latest investigations of the U.S. Coast and Geodetic Survey. These values have been employed in reducing barometric readings to the standard value of gravity adopted by the International Bureau of Weights and Measures, supplementing a table that has been introduced for directly reducing barometer readings from the value of gravity at the place of observation to its standard value.

The new values of vapor pressure and of gravity acceleration thus obtained, together with a recent and more accurate determination of the density of mercury, have called for an extensive revision of numerous other tables, and especially of those for the reduction of psychrometric observations, and the barometrical tables.

Among the new tables added are those for converting barometric inches and barometric millimeters into millibars, for determining heights from pressures expressed in dynamic units, tables of gradient winds, and tables giving the duration of astronomical and civil twilight, and the transmission percentages of radiation through moist air.

The tables of International Meteorological Symbols, of Cloud Classification, of the Beaufort Scale of Winds, of the Beaufort Weather Notation, and the List of Meteorological Stations, are among those extensively revised.

Tables for reducing barometric readings to sea level, and tables of logarithms of numbers, of natural sines and cosines, of tangents and cotangents, and for dividing by 28, 29, and 31, with a few others, have been omitted from this edition.

This reprint is from the electroplates that were employed in printing the Fourth Revised Edition, after making certain minor corrections.

CHARLES D. WALCOTT.

Secretary.

ADVERTISEMENT TO THIRD REVISED EDITION

The original edition of Smithsonian Meteorological Tables was issued in 1893, and revised editions were published in 1896 and 1897. A third revised edition is here presented, which has been prepared at the request of the late Professor Langley by the coöperation of Professors Alexander McAdie, Charles F. Marvin, and Cleveland Abbe.

All errata thus far detected have been corrected upon the plates, the Marvin vapor tensions over ice have been introduced, Professor F. H. Bigelow's System of Notation and Formulæ has been added, the List of Meteorological Stations has been revised, and the International Meteorological Symbols, together with the Beaufort Notation, are given at the close of the volume.

R. RATHBUN,

Acting Secretary.

Smithsonian Institution, December, 1906.

ADVERTISEMENT TO SECOND REVISED EDITION.

The edition of the Smithsonian Meteorological Tables issued in 1893 having become exhausted, a careful examination of the work has been made, at my request, by Mr. Alexander McAdie, of the United States Weather Bureau, and a revised edition was published in 1896, with corrections upon the plates and a few slight changes. The International Meteorological Symbols and an Index were also added.

The demand for the work has been so great that it becomes necessary to print a new edition of the revised work, which is here presented with corrections to date.

S. P. Langley, Secretary.

SMITHSONIAN INSTITUTION, WASHINGTON CITY, October 30, 1897.



PREFACE TO EDITION OF 1893.

In connection with the system of meteorological observations established by the Smithsonian Institution about 1850, a collection of meteorological tables was compiled by Dr. Arnold Guyot, at the request of Secretary Henry, and published in 1852 as a volume of the Miscellaneous Collections.

Five years later, in 1857, a second edition was published after careful revision by the author, and the various series of tables were so enlarged as to extend the work from 212 to over 600 pages.

In 1859 a third edition was published, with further amendments. Although designed primarily for the meteorological observers reporting to the Smithsonian Institution, the tables obtained a much wider circulation, and were extensively used by meteorologists and physicists in Europe and in the United States.

After twenty-five years of valuable service, the work was again revised by the author; and the fourth edition, containing over 700 pages, was published in 1884. Before finishing the last few tables, Dr. Guvor died, and the completion of the work was intrusted to his assistant, Prof. Wm. Libber, Jr., who executed the duties of final editor.

In a few years the demand for the tables exhausted the edition, and thereupon it appeared desirable to recast entirely the work. After very careful consideration, I decided to publish the new tables in three parts: Meteorological Tables, Geographical Tables, and Physical Tables, each representative of the latest knowledge in its field, and independent of the others; but the three forming a homogeneous series.

Although thus historically related to Dr. Guyot's Tables, the present work is so substantially changed with respect to material, arrangement, and presentation that it is not a fifth edition of the older tables, but essentially a new publication.

In its preparation the advantage of conformity with the recently issued *International Meteorological Tables* has been kept steadily in view, and so far as consistent with other decisions, the constants and methods there employed have been followed. The most important difference in constants is the relation of the yard to the metre. The value provisionally adopted by the Bureau of Weights and Measures of the United States Coast and Geodetic Survey,

I metre = 39.3700 inches,

has been used here in the conversion-tables of metric and English linear measures, and in the transformation of all formulæ involving such conversions.

A large number of tables have been newly computed; those taken from the *International Meteorological Tables* and other official sources are credited in the introduction.

To Prof. WM. LIBBEY, JR., especial acknowledgments are due for a large amount of attention given to the present work. Prof. LIBBEY had already completed a revision, involving considerable recomputation, of the meteorological tables contained in the last edition of Guyot's Tables, when it was determined to adopt new values for many of the constants, and to have the present volume set with new type. This involved a large amount of new computation, which was placed under the direction of Mr. George E. Curtis, who has also written the text, and has carefully prepared the whole manuscript and carried it through the press. To Mr. Curtis's interest, and to his special experience as a meteorologist, the present volume is therefore largely due.

Prof. Libber has contributed Tables 38, 39, 55, 56, 61, 74, 77, 89, and 90, and has also read the proof-sheets of the entire work.

I desire to express my acknowledgments to Prof. CLEVELAND ABBE, for the manuscript of Tables 32, 81, 82, 83, 84, 85, 86; to Mr. H. A. HAZEN, for Tables 49, 50, 94, 95, 96, which have been taken from his Hand-book of Meteorological Tables; and also to the Superintendent of the United States Coast and Geodetic Survey, the Chief Signal Officer of the Army, and the Chief of the Weather Bureau, for much valuable counsel during the progress of the work.

S. P. LANGLEY,

Secretary.

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INTRODUCTION.

DESCRIPTION AND USE OF TABLES.

THERMOMETRY.

The present standard for exact thermometry is the normal centigrade scale of the constant-volume hydrogen thermometer as defined by the International Bureau of Weights and Measures. The constant volume is one liter and the pressure at the freezing point is one meter of mercury reduced to freezing and standard gravity. The scale is completely defined by designating the temperature of melting ice, o°, and of condensing steam, 100°, both under standard atmospheric pressure. All other thermometric scales that depend upon the physical properties of substances may by definition be made to coincide at the ice point and the boiling point with the normal scale as above defined, but they will diverge more or less from it and from each other at all other points. However, by international consent it is customary in most cases to refer other working scales to the hydrogen scale.

The absolute or thermodynamic scale. To obviate the difficulty which arises because thermometers of different type and substance inherently disagree except at the fixed points, Lord Kelvin proposed that temperatures be defined by reference to certain thermodynamic laws. This course furnishes a scale independent of the nature or properties of any particular substance. The resulting scale has been variously named the absolute, the thermodynamic, and, more recently, in honor of its author, the Kelvin scale. The temperature of melting ice by this scale on the centigrade basis is not as yet accurately known, but it is very nearly 273°13, and that of the boiling point, 373°13.

Many problems in physics and meteorology call for the use of the absolute scale; but it is not convenient, and in many cases not necessary, to adhere strictly to the true thermodynamic scale. In fact, the general requirements of science will very largely be met by the use of an approximate absolute scale which for the centigrade system is defined by the equation

$$T = (273^{\circ} + t^{\circ} \text{ C.})$$

The observed quantity, t° , may be referred to the normal hydrogen centigrade scale or be determined by any acceptable thermometric method.

This scale differs from the true Kelvin scale, first, because 273° is not the exact value of the ice point on the Kelvin scale, second, because each observed value of t° other than o° or 100° requires a particular correction to

convert it to the corresponding value on the Kelvin scale. These corrections will differ according to the kind of thermometer used in obtaining the value t° , and while they are small for temperatures between 0° and 100° they are large at extreme temperatures and are important in all questions involving thermometric precision.

Since, however, the approximate absolute scale is sufficiently exact for nearly all purposes, and especially since it is most convenient in computations and in the publication of results, much confusion and uncertainty of terminology and meaning will be obviated if scientists will agree to give the approximate absolute scale a particular name of its own.

For the purpose of these tables the name *Approximate Absolute* will be employed, and in accordance therewith thermometric scales may be designated as follows:—

Scale.	Ice point.	Boiling point.	Symbol.		
Centigrade	o°	100°	С.		
Fahrenheit	32	212	F. or Fahr.		
Reaumur	0	80	R.		
Thermodynamic Absolute Kelvin	(Names sti	373.13 $C.\pm$ 671.6 $F.\pm$ rictly synonymous	A. or K . and strictly		
	one ideal scale.)				
Approximate Absolute	273	373	A.A.		

Table 1. Conversion of the Approximate Absolute thermometric scale to the Centigrade, Fahrenheit, and Reaumur scales.

The equivalent values of the four scales are given for every degree on the Approximate Absolute scale from 375° to 0°.

By the help of the table of proportional parts preceding this table, it is also convenient for converting Fahrenheit to Centigrade and Reaumur, and Centigrade to Fahrenheit and Reaumur.

The formulæ expressing the relations between the different scales are also given, in which

 $A.A.^{\circ}$ = Temperature — Approximate Absolute Scale.

 $C.^{\circ}$ = Temperature — Centigrade Scale.

F.° = Temperature — Fahrenheit Scale.

 $R.^{\circ}$ = Temperature — Reaumur Scale.

Examples:

To convert 285.5 Approximate Absolute into Centigrade, Fahrenheit, and Reaumur.

From the table,
$$285^{\circ}$$
 $A.A. = 12^{\circ}$ $C. = 53^{\circ}6$ $F. = 9^{\circ}6$ $R.$ From the proportional parts, $0.5 = 0.5 = 0.9 = 0.4$ 285.5 $A.A. = 12.5$ $C. = 54.5$ $F. = 10.0$ $R.$

To convert 16°9 Centigrade to Approximate Absolute, Fahrenheit, and Reaumur.

From the table,
$$16^{\circ} C. = 289^{\circ} A.A. = 60^{\circ} 8 F. = 12^{\circ} 8 R.$$

From the proportional parts $0.9 = 0.9 = 1.6 = 0.7$
 $16.9 C. = 289.9 A.A. = 62.4 F. = 13.5 R.$

Or,
$$16^{\circ}.9 \times 2 \left(1 - \frac{I}{10}\right) + 32 = 33.8 \\ - 3.4 \\ - \frac{32.0}{62.4} F.$$

To convert 147°7 Fahrenheit to Approximate Absolute, Centigrade, and Reaumur.

From the table, I40°.
$$F. = 333$$
°. $A.A. = 60$ °. $C. = 48$ °. $R.$
From the proportional parts $7.7 = 4.3 = 4.3 = 4.3 = 3.4$
 $147.7 F. = 337.3 A.A. = 64.3 C. = 51.4 R.$

Or,
$$\frac{147.7 - 32.0}{2} \left(1 + \frac{1}{10} + \frac{1}{100} + \frac{1}{1000} \text{ etc.}\right) = 57.85 + 5.78 + .58 + .06 - 64.27 C.$$

Fahrenheit may also be reduced to Approximate Absolute by obtaining its equivalent in Centigrade from Table 2 and adding 273 to the result.

To convert 18°3 Reaumur to Approximate Absolute, Centigrade, and Fahrenheit.

From the table,
$$16^{\circ}$$
 R. = 293° A.A. = 20° C. = 68° F. From the proportional parts, $2.3 = 2.9 = 2.9 = 5.2 = 18.3$ R. = 295.9 A.A. = 22.9 C. = 73.2 F.

Or,
$$18.3 \times \frac{5}{4} = \frac{91.5}{4} = 22.9 \ C$$
, and $(18.3 \times \frac{9}{4}) + 32 = \frac{164.7}{4} + 32 = 73.2 \ F$.

TABLE 2.

 TABLE 2. Conversion of readings of the Fahrenheit thermometer to readings

 Centigrade.

The conversion of Fahrenheit temperatures to Centigrade temperatures is given for every tenth of a degree from $+ 130^{\circ}.9 F$. to $- 120^{\circ}.9 F$. The side argument is the whole number of degrees Fahrenheit, and the top argument, tenths of a degree Fahrenheit; interpolation to hundredths of a degree, when desired, is readily effected mentally. The tabular values are given to hundredths of a degree Centigrade.

The formula for conversion is

$$C^{\circ} = \frac{5}{9} (F^{\circ} - 32^{\circ})$$

where F° is a given temperature Fahrenheit, and C° the corresponding temperature Centigrade.

Example:

To convert 79°7 Fahrenheit to Centigrade.

The table gives directly 26°50 C.

For conversions of temperatures outside the limits of the table use Table 1.

Table 3. Conversion of readings of the Centigrade thermometer to readings Fahrenheit.

The conversion of Centigrade temperatures to Fahrenheit temperatures is given for every tenth of a degree Centigrade from $+60^{\circ}$ 9 to -90° 9 C. The tabular values are expressed in hundredths of a degree Fahrenheit.

The formula for conversion is

$$F^{\circ} = \frac{9}{5} C^{\circ} + 32^{\circ}$$

where C° is a given temperature Centigrade, and F° the corresponding temperature Fahrenheit.

For conversions of temperatures outside the limits of the table, use Table I or 4.

Table 4. Conversion of readings of the Centigrade thermometer near the boiling point to readings Fahrenheit.

This is an extension of Table 3 from 90°0 to 100°9 Centigrade.

Example:

To convert 95°74 Centigrade to Fahrenheit.

 $95.70 \ C. = 204.26 \ F.$ From the table,

 $\frac{0.04}{95.74} = \frac{0.07}{204.33} = \frac{0.07}{204$ By interpolation,

Conversion of differences Fahrenheit to differences Centigrade.

The table gives for every tenth of a degree from o° to 20.9 F. the corresponding lengths of the Centigrade scale.

TABLE 6.

Table 6. Conversion of differences Centigrade to differences Fahrenheit.

The table gives for every tenth of a degree from 0° to $9^{\circ}9$ C. the corresponding lengths of the Fahrenheit scale.

Example:

To find the equivalent difference in Fahrenheit degrees for a difference of 4°.72 Centigrade.

From the table, From the table by moving the decimal point for 0.2, $\frac{0.02}{4^{\circ}72} = \frac{0.04}{C.} = \frac{0.04}{8^{\circ}50} F.$

TABLES 7, 8.

Tables 7, 8. Correction for the temperature of the emergent mercurial column of thermometers.

When the temperature of the thermometer stem containing a portion of the mercury column is materially different from that of the bulb, a correction needs to be applied to the observed reading unless the instrument has been previously graduated for the condition of use. This correction frequently becomes necessary in physical experiments where the bulb only, or else the bulb with a portion of the stem, is immersed in a bath whose temperature is to be determined. In meteorological observations the correction may become appreciable in wet-bulb, dew-point, and solar-radiation thermometers, when the temperature of the bulb is considerably above or below the air temperature.

If t' be the average temperature of the emergent mercury column, t the observed reading of the thermometer, n the length of the mercury in the emergent stem in scale degrees, and a the apparent expansion of mercury in glass for 1° , the correction is given by the expression

$$an(t-t')$$
, or $-an(t'-t)$

which latter may be the more convenient form when t' is greater than t.

The value of a varies with the composition of the glass of which the thermometer stem is composed. For glass of unknown composition the best average value for centigrade temperatures appears to be 0.000155, while for stems of Jena 16¹¹¹, or similar glasses, or Jena 59¹¹¹, the values 0.00016 for the former and 0.000165 for the latter may be preferred. (Letter from U.S. Bureau of Standards dated January 5, 1918.)

The use of the formula given above presupposes that the mean temperature of the emergent column has been determined. This temperature may be approximately obtained in one of three ways. (1) By a "fadenthermometer" (Buckingham, Bulletin, Bureau of Standards, 8, 239, 1911, Scientific Paper 170); (2) by exploring the temperature distribution along the stem and calculating the mean temperature; (3) by suspending along the side of, or attaching to the stem, a single thermometer. If properly placed this

thermometer will indicate the temperature of the emergent mercurial column to an accuracy sufficient for many purposes. Under conditions ordinarily met with in practice it is desirable to place the bulb of the auxiliary thermometer at some point below the middle of the emergent column.

It is to be noted that the correction sought is directly proportional to the value of α, and that this may vary for glass stems of different composition from 0.00015 to 0.000165 for Centigrade temperatures. For thermometers ordinarily used in meteorological work, however, 0.000155 appears to be a good average value for Centigrade temperatures (0.000086 for Fahrenheit temperatures), and the correction formulæ, therefore, are,

T = t - 0.000086 n (t' - t) Fahrenheit temperatures. T = t - 0.000155 n (t' - t) Centigrade temperatures.

In the above, T =Corrected temperature.

t =Observed temperature.

t' = Mean temperature of the glass stem and emergent mercury column.

n = Length of mercury in the emergent stem in scale degrees.

When t' is $\begin{cases} \text{higher} \\ \text{lower} \end{cases}$ than t the numerical correction is to be $\begin{cases} \text{subtracted.} \\ \text{added.} \end{cases}$

Table 7 gives corrections computed to 0°01 for Fahrenheit thermometers from the equation C = -0.000086 n (t'-t). The side argument, n, is given for 10° intervals from 10° to 130°; the top argument, t'-t, for 10° intervals from 10° to 100°.

Table 8 gives corrections computed to 0.01 for Centigrade thermometers from the equation C = -0.000155 n (t' - t). The side argument, n, is given for 10° intervals from 10° to 100°; the top argument, t' - t, for 10° intervals from 10° to 80°.

Example:

The observed temperature of a black-bulb thermometer is 120°.4 F., the temperature of the glass stem is 55°.2 F., and the length of mercury in the emergent stem is 130° F. To find the corrected temperature. With $n = 130^{\circ}$ F. and $t' - t = -65^{\circ}$ F., as arguments, Table 7 gives the correction 0°.7 F., which by the above rule is to be added to the observed temperature. The corrected temperature is therefore 121°.1 F.

CONVERSIONS INVOLVING LINEAR MEASURES.

The fundamental unit of length is the meter, the length of which is equal to the distance between the defining lines on the international prototype meter at the International Bureau of Weights and Measures (near Paris) when this standard is at the temperature of melting ice (o° C). The relation

here adopted between the meter and the yard, the English measure of length, is I meter = 39.3700 inches, as legalized by Act of U.S. Congress, July 28, 1866. This U.S. Standard of length must be distinguished from the British Imperial yard, comparisons of which with the international prototype meter give the relation I meter = 39.370113 inches. (See Smithsonian Physical Tables, 1916, p. 7, Table 3.)

TABLE 9. Inches into millimeters.

TABLE 9.

I inch = 25.40005 millimeters.

The argument is given for every hundredth of an inch up to 32.00 inches, and the tabular values are given to hundredths of a millimeter. A table of proportional parts for thousandths of an inch is added on each page.

Example:

To convert 24.362 inches to millimeters.

The table gives (p. 20).

$$(24.36 + .002)$$
 inches = $(618.75 + 0.05)$ mm. = 618.80 mm.

TABLE 10. Millimeters into inches.

TABLE 10.

From 0 to 400 mm. the argument is given to every millimeter, with subsidiary interpolation tables for tenths and hundredths of a millimeter. The tabular values are given to four decimals. From 400 to 1000 mm., covering the numerical values which are of frequent use in meteorology for the conversion of barometric readings from the metric to the English barometer, the argument is given for every tenth of a millimeter, and the tabular values to three decimals.

Example:

To convert 143.34 mm. to inches.

The table gives

(143 + .3 + .04) mm. = (5.6299 + 0.0118 + 0.0016) inches = 5.6433 inches.

Tables 11, 12. Conversion of barometric readings into standard units of pressure.

The equation for the pressure in millibars, P_{mb} , corresponding to the barometric height, B, is

$$P_{mb} = B \frac{\Delta g_0}{1000}$$

where Δ is the density of mercury and g_0 is the standard value of gravity.

¹ The value of the *bar* as here defined is a pressure of 1,000,000 dynes per square centimeter, and is that employed by meteorological services, and recommended by inter-

In order that pressures thus derived shall be expressed in C.G.S. units it is evident that the recognized standard values of the constants of the equation must be employed. It therefore becomes necessary to abandon the values for the density of mercury and for standard gravity heretofore employed, which had the sanction of the International Meteorological Committee, in favor of the more recently determined values that have been adopted by the International Bureau of Weights and Measures.

The value adopted for Δ is 13.5951 grams per cubic centimeter; ¹ and for g_0 , 980.665 dynes.²

By the use of these constants in the above equation we obtain

$$P_{mb} = 1.333224 \ B$$
 (millimeters), and $P_{mb} = \frac{1.333224}{0.03937} \ B = 33.86395 \ B$ (inches)

where B is the height of the barometer in the units indicated, after reduction to standard temperature and the standard value of gravity.

Table 11. Barometric inches to millibars.

The argument is for 0.01 inch. From 0.00 to 2.49 inches the tabulated values are given to the nearest hundredth of a millibar, so that by removing the decimal one place to the right the value in millibars of every tenth inch from 0.0 to 24.9 inches may be obtained to the nearest tenth of a millibar. From 25.00 to 31.99 inches the tabular values are given to the nearest tenth of a millibar.

The first part of the table may be used as a table of proportional parts for interpolation.

Example:

To convert 23.86 barometric inches into millibars of pressure.

TABLE 12. Barometric millimeters to millibars.

The argument is for each millimeter from 1 to 799, and the tabular values are given to the nearest tenth of a millibar.

This table may also be used to convert millibars into millimeters of mercury.

national meteorological and aerological conferences. It is 1,000,000 times greater than that given in the Smithsonian Physical Tables, 6th ed., 1914, p. 346. The smaller value is generally employed by physicists and chemists. See Marvin, Charles F. Nomenclature of the Unit of Absolute Pressure. Monthly Weather Review, 1918, 46:73-75.

¹ Chappuis, Recueil de Constantes Physiques, Soc. Fr. Phys., 1913, p. 139. Leduc, Trav. et Mém., Bur. Int. Poids et Mes., xvi, p. 36, 1917.

² Comptes Rendus des Séances, Troisième Conférence Générale, p. 68. Trav. et Mém., Bur. Int. Poids et Mes., XII, 1902.

Example:

To convert 1003.5 millibars into millimeters of mercury. 1003.5 mb. = (1002.6 + 0.9) mb. = (752 + 0.68) mm. = 752.68 mm.

TABLE 13. Feet into meters.

TABLE 13.

From the adopted value of the meter, 39.3700 inches—
I English foot = 0.3048006 meter.

Table 13 gives the value in meters and thousandths (or millimeters) for every foot from 0 to 99 feet; the value to hundredths of a meter (or centimeters) of every 10 feet from 100 to 4090 feet; and the value to tenths of a meter of every 10 feet from 4000 to 9090 feet. In using the latter part, the first line of the table serves to interpolate for single feet.

Example:

To convert 47 feet 7 inches to meters. The table gives 47 feet 7 inches = 47.583 feet. By moving the decimal point 6.583 " = 6.178 " 6.583 feet = 6.178 " 6.188 feet = 6.188 fee

TABLE 14. Meters into feet.

TABLE 14.

I meter = 39.3700 inches = 3.280833 + feet.

From 0 to 509 meters the argument is given for every unit, and the tabular values to two decimals; from 500 to 5090 the argument is given to every 10 meters, and the tabular values to one decimal. The conversion for tenths of a meter is added for convenience of interpolation.

Example:

Convert 4327 meters to feet.

The table gives

$$(4320 + 7)$$
 meters = $(14173.2 + 23.0)$ feet = 14196.2 feet.

TABLE 15. Miles into kilometers.

TABLE 15.

I mile = 1.609347 kilometers.

The table extends from 0 to 1009 miles with argument to single miles, and from 1000 to 20000 miles for every 1000 miles. The tabular quantities are given to the nearest kilometer.

TABLE 16. Kilometers into miles.

TABLE 16.

I kilometer = 0.621370 mile.

The table extends to 1009 kilometers with argument to single kilometers, and from 1000 to 20000 kilometers for every 1000 kilometers. Tabular values are given to tenths of a mile.

Example:

Convert 3957 kilometers into miles.

The table gives

(3000 + 957) kilometers = (1864.1 + 594.7) miles = 2458.8 miles.

TABLE 17. Interconversion of nautical and statute miles.

The nautical mile as defined by the U.S. Coast and Geodetic Survey (Tables for a polyconic projection of maps. U.S. Coast and Geodetic Survey, Special Publication No. 5, page 4) is "A minute of arc of a great circle of a sphere whose surface equals that of the Clarke representative spheroid of 1866," and the value given is 1853.25 meters, or 6080.20 feet.

Table 18. Continental measures of length with their metric and English equivalents.

This table gives a miscellaneous list of continental measures of length, alphabetically arranged, with the name of the country to which they belong and their metric and English equivalents.

CONVERSION OF MEASURES OF TIME AND ANGLE.

TABLE 19. Arc into time.

$$I^{\circ} = 4^{m}; I' = 4^{s}; I'' = \frac{1}{15}^{s} = 0.067.$$

Example:

Change 124° 15′ 24″7 into time.

From the table,

$$124^{\circ} = 8^{h} \quad 16^{m} \quad 0^{s}$$

$$15' = I \quad 0$$

$$24'' = I.600$$

$$0''7 = .047$$

$$8^{h} \quad 17^{m} \quad 1.647$$

TABLE 20. Time into arc.

$$I^{h} = I5^{\circ}; I^{m} = I5'; I^{s} = I5''.$$

Example:

Change 8h 17m 1s647 into arc.

From the table, $8^{h} = 120^{\circ}$ $17^{m} = 4 15'$ $1^{s} = 0.64 = 9.60$ By moving the decimal point, .007 = 0.10

Table 21. Days into decimals of a year and angle.

The table gives for the beginning of each day the corresponding decimal of the year to five places. Thus, at the epoch represented by the beginning of the 15th day, the decimal of the year that has elapsed since January 1.0 is computed from the fraction $\frac{14}{365.25}$. The corresponding value in angle obtained by multiplying this fraction by 360°, is given to the nearest minute.

Two additional columns serve to enter the table with the day of the month either of the common or the bissextile year as the argument, and may be used also for converting the day of the month to the day of the year, and *vice versa*.

Example:

To find the number of days and the decimal of a year between February 12 and August 27 in a bissextile year.

Aug. 27: Day of year = 240; decimal of a year =
$$0.65435$$

Feb. 12: " " = 0.11499
Interval in days = 0.53936

The decimal of the year corresponding to the interval 197 days may also be taken from the table by entering with the argument 198.

TABLE 22. Hours, minutes and seconds into decimals of a day. TABLE 22.

The tabular values are given to six decimals.

Example:

Convert 5^h 24^m 23^s,4 to the decimal of a day:

$$5^{\text{m}} = 0.208333$$
 $24^{\text{m}} = 016667$
 $23^{\text{s}} = 266$
 $0.4 = 5$

By interpolation, or by moving the decimal for $4^{\rm s}$

Table 23. Decimals of a day into hours, minutes and seconds. Table 23

Example:

Convert 0.225271 to hours, minutes and seconds:

0.22 day =
$$4^{h} 48^{m} + 28^{m} 48^{s} = 5^{h} 16^{m} 48^{s}$$

0.0052 day = $7^{m} 12^{s} + 17^{s}28 = 7$ 29 28
0.000071 day = $6^{s}05 + 0.09 = \frac{6.14}{5^{h} 24^{m} 23^{s}4}$

Table 24. Minutes and seconds into decimals of an hour.

TABLE 24

The tabular values are given to six decimals.

Example:

Convert 34^m 28^s,7 to decimals of an hour.

$$34^{m} = 0^{h}566667$$
 $28^{s} = 7778$
 $0.77 = 194$
 0.574639

TABLE 25. Local mean time at apparent noon.

This table gives the local mean time 1 that should be shown by a clock when the center of the sun crosses the meridian, on the 1st, 8th, 16th, and 24th days of each month. The table is useful in correcting a clock by means of a sundial or noon mark.

Example:

To find the correct local mean time when the sun crosses the meridian on December 15, 1891.

The table gives for December 16, 11^h 56^m. By interpolating, it is seen that the change to December 15 would be only one-half minute; the correct clock time is therefore 4 minutes before 12 o'clock noon.

TABLE 26. Sidereal time into mean solar time.

TABLE 27. Mean solar time into sidereal time.

According to Newcomb, the length of the tropical year is 365.24220 mean solar days,² whence

365.24220 solar days = 366.24220 sidereal days.

Any interval of mean time may therefore be changed into sidereal time

by increasing it by its $\frac{1}{365.24220}$ part, and any interval of sidereal time may

be changed into mean time by diminishing it by its $\frac{I}{366.24220}$ part.

Table 26 gives the quantities to be subtracted from the hours, minutes and seconds of a sidereal interval to obtain the corresponding mean time interval, and Table 27 gives the quantities to be added to the hours, minutes and seconds of a mean time interval to obtain the corresponding sidereal interval. The correction for seconds is sensibly the same for either a sidereal or a mean time interval and is therefore given but once, thus forming a part of each table.

Examples:

Change 14^h 25^m 36^s.2 sidereal time into mean solar time.

mge 14 25 30.2 sidered time	THEO THECH COREST CH			
Given sidereal time		$14^{\rm h}$	25 ^m	36 ^s .2
Correction for 14 ^h	$= -2^{m} 17.61$			
25 ^m	= - 4.10			
36°.2	=10			
	- 2 21.81		-2	21.8
Corresponding mean time	=	14	23	14.4

¹ Derived from the equation of time for Washington apparent noon for the year 1899. See the American Ephemeris and Nautical Almanac, 1899, pages 377–84.

² The length of the tropical year is not absolutely constant. The value here given is for the year 1900. Its decrease in 100 years is about 0.5s. (See the American Ephemeris and Nautical Almanac 1918, page xvi.)

2. Change 13^h 37^m 22^s7 mean solar time into sidereal time.

Given mean time =
$$13^{h}$$
 37^{m} 22^{s} .7

Correction for 13^{h} = $+2^{m}$ 8^{s} . 13 = $+6.08$
 22^{s} .7

Corresponding sidereal time = 13^{h} 37^{m} 22^{s} .7

 $= +2^{m}$ 0.06
 $= +2^{m}$ 14.27
 $= +2^{m}$ 14.3
 $= +2^{m}$ 13^{h} 37^{m} 22^{s} .7

CONVERSION OF MEASURES OF WEIGHT.

TABLE 28.

Table 28. Conversion of avoirdupois pounds and ounces into kilograms.

The comparisons of July, 1893, made by the International Bureau of Weights and Measures between the Imperial standard pound and the "kilogram prototype" resulted in the relation:

I pound avoirdupois = 453.592 427 7 grams.

For the conversion of pounds, Table 28 gives the argument for every tenth of a pound up to 9.9, and the tabular conversion values to ten-thousandths of a kilogram.

For the conversion of ounces, the argument is given for every tenth of an ounce up to 15.9, and the tabular values to ten-thousandths of a kilogram.

TABLE 29.

Table 29. Conversion of kilograms into avoirdupois pounds and ounces.

From the above relation between the pound and the kilogram,

The table gives the value to thousandths of a pound of every tenth of a kilogram up to 9.9; the values of tenths of a kilogram in ounces to four decimals; and the values of hundredths of a kilogram in pounds and ounces to three and two decimals respectively.

TABLE 30. Conversion of grains into grams.

TABLES 30, 31,

TABLE 31. Conversion of grams into grains.

From the above relation between the pound and the kilogram,

I gram = I5.432356 grains. I grain = 0.06479892 gram.

TABLE 30 gives to ten-thousandths of a gram the value of every grain from I to 99, and also the conversion of tenths and hundredths of a grain for convenience in interpolating.

TABLE 31 gives to hundredths of a grain the value of every tenth of a gram from 0.1 to 9.9, and the value of every gram from 1 to 99. The values of hundredths and thousandths of a gram are added as an aid to interpolation.

WIND TABLES.

CONVERSION OF VELOCITIES.

TABLE 32. Synoptic conversion of velocities.

This table,¹ contained on a single page, converts miles per hour into meters per second, feet per second and kilometers per hour. The argument, miles per hour, is given for every half unit from o to 78. Tabular values are given to one decimal. For the rapid interconversion of velocities, when extreme precision is not required, this table has proved of marked convenience and utility.

TABLE 33. Conversion of miles per hour into feet per second.

The argument is given for every unit up to 149 and the tabular values are given to one decimal.

TABLE 34. Conversion of feet per second into miles per hour.

The argument is given for every unit up to 199 and the tabular values are given to one decimal.

TABLE 35. Conversion of meters per second into miles per hour.

The argument is given for every tenth of a meter per second up to 60 meters per second, and the tabular values are given to one decimal.

TABLE 36. Conversion of miles per hour into meters per second.

The argument is given for every unit up to 149, and the tabular values are given to two decimals.

TABLE 37. Conversion of meters per second into kilometers per hour.

The argument is given for every tenth of a meter per second up to 60 meters per second, and the tabular values are given to one decimal.

TABLE 38. Conversion of kilometers per hour into meters per second.

The argument is given for every unit up to 200, and the tabular values are given to two decimals.

Table 39. Scale of velocity equivalents of the so-called Beaufort scale of wind.

The personal observation of the estimated force of the wind on an arbitrary scale is a method that belongs to the simplest meteorological records and is widely practiced. Although anemometers are used at meteorological observatories, the majority of observers are still dependent upon estimates based largely upon their own judgment, and so reliable can such estimates be made that for many purposes they abundantly answer the needs of meteorology as well as of climatology.

A great variety of such arbitrary scales have been adopted by different observers, but the one that has come into the most general use and received

¹ From Hand-Book of Meteorological Tables. By H. A. Hazen. Washington, 1888.

the greatest definiteness of application is the duodecimal scale introduced into the British navy by Admiral Beaufort about 1800.

Table 39 is taken from the Observer's Handbook of the Meteorological Office, London, edition of 1917, and the Marine Observer's Handbook of Meteorology, edition of 1930. The velocity equivalents in meters per second and miles per hour are based on extensive observational data collected by Dr. G. C. Simpson and first published by the Meteorological Office in 1906. Several other sets of equivalents have been published in different countries. For a history of this subject see "Rept. 10th Meeting International Meteorological Committee," Rome, 1913, Appendix VII (London, 1914), and a paper by G. C. Simpson on "The velocity equivalents of the Beaufort scale," Professional Notes No. 44, Air Ministry, Meteorological Office, London, 1926.

Simpson points out that the Beaufort scale has been used by sailors for many generations to describe the effect of the air in motion on ships and their rigging, and upon the sea. With change in the rig of ships there still remains the effect of wind upon the surface of the sea, and to this has been added the effect upon objects on land.

Finally, it became desirable to interpret wind force on the Beaufort scale in terms of wind velocity as measured by the anemometer. For this purpose experiments with the anemometer both on land and on sea were made. The results showed considerable discrepancies in the velocity equivalents of winds indicated by different numbers on the Beaufort scale, but Simpson attributes these discrepancies to differences in anemometer exposures during the tests. For example, the Meteorological Office equivalents represent velocities measured by an anemometer not less than 10 meters above the ground level, while the Deutsche Seewarte equivalents represent velocities measured by anemometers as ordinarily exposed.

Simpson proposed a scale of equivalents about midway between those determined by the Meteorological Office and by the Seewarte, respectively, and this compromise scale was adopted by the Commission for Synoptic Weather Information of the International Meteorological Organization at its meeting in Zurich in 1926, with the proviso that the velocity equivalents correspond on land with the wind speed at a height of approximately 6 meters above a level surface. Since, however, the International Commission for Air Navigation has taken as the surface wind that measured at a height of 10 to 15 meters above the ground, it has seemed best in these tables to continue to adhere to the British Meteorological Office equivalents, which are based on the equation $V = 0.836\sqrt{B^3}$, where B is the Beaufort number representing the wind force, and V is the velocity equivalent in meters per second.

The velocity equivalents adopted by the Commission for Synoptic Weather Information, referred to above, expressed in statute miles per hour, correspond very closely to the values in Table 39 expressed in nautical miles (knots) per hour.

In the Quarterly Journal of the Royal Meteorological Society, volume xxx, No. 132, October, 1904, Prof. A. Lawrence Rotch has described an instrument for obtaining the true direction and velocity of the wind at sea aboard a moving vessel. If a line A B represents the wind due to the motion of a steamer in an opposite direction, and A C the direction of the wind relative to the vessel as shown by the drift of its smoke, then, by measuring the angle D B A that the true wind makes with the vessel—which is easily done by watching the wave crests as they approach it—we obtain the third side, B C, of the triangle. This represents, in direction and also in length, on the scale used in setting off the speed of the ship, the true direction of the wind relative to the vessel and also its true velocity. The method fails when the wind direction coincides with the ship's course and becomes inaccurate when the angle between them is small.

GRADIENT WINDS.

When the motions of the atmosphere attain a state of complete equilibrium of flow under definite systems of pressure gradients, the winds blow across the isobars at small angles of inclination depending upon the retarding effects of friction. At the surface of the earth friction is considerable and the angle across the isobars is often great. In the free air, however, the friction is small, and for some purposes may be disregarded entirely. Under an assumption of complete equilibrium of motion and frictionless flow the winds will blow exactly parallel to the isobars—that is, perpendicular to the gradient which produces and sustains the motion. Such winds are called gradient winds. The anomalous condition of flow of terrestrial winds perpendicular to the moving force is the result of the modifications of atmospheric motions due to the deflective influence of the earth's rotation, and to that other influence due to the inertia reaction of matter when it is constrained to move in a curved path, and commonly called centrifugal force. The equations for gradient wind motions have long been known to meteorologists from the work of Ferrel and others, and may be written in the following form:

For Cyclones

$$V = r \left[\sqrt{\omega^2 \sin^2 \phi + \frac{\Delta P}{\rho r}} - \omega \sin \phi \right]$$
 (1)

For Anticyclones

$$V = r \left[\omega \sin \phi - \sqrt{\omega^2 \sin^2 \phi - \frac{\Delta P}{\rho r}} \right]$$
 (2)

In C. G. S. Units, V= velocity of the gradient wind in centimeters per second; r= radius of curvature of isobars in centimeters; $\Delta P=$ pressure gradient in dynes per square centimeter per centimeter; $\rho=$ density of air in grams per cubic centimeter; $\omega=$ angular velocity of the earth's rotation

per second = $\frac{2\pi}{86164}$, and ϕ = latitude. In the Northern Hemisphere the winds gyrate counterclockwise in cyclones and clockwise in anticyclones.

These gyrations are in the reversed direction each to each in the Southern Hemisphere.

In equation (2) the values of V are imaginary for values of $\frac{\Delta P}{\rho r}$ greater than $\omega^2 \sin^2 \phi$. The equality $\frac{\Delta P}{\rho r} = \omega^2 \sin^2 \phi$, or $r = \frac{\Delta P}{\rho \omega^2 \sin^2 \phi}$ defines and

fixes an isobar with minimum curvature in anticyclones. Winds cannot flow parallel to the isobars within this critical isobar. For this isobar the gradient wind has its maximum value $V_c = \frac{\Delta P}{\rho\omega\,\sin\phi}$. For the same gradient and for an isobar with the same curvature in a cyclone the gradient velocity is $V_l = V_c\,(\sqrt{2}-1) = 0.414\,V_c$.

When the isobars are parallel straight lines, a condition very often closely realized in nature, $r = \infty$ and the gradient winds have the value given by either (1) or (2) after squaring, namely,

$$V_{r=\infty} = V_s = \frac{\Delta P}{2 \rho \omega \sin \phi} = \frac{I}{2} V_c.$$

For practical units equation (1) becomes

Units of pressure.

pressure.

$$V = R \begin{bmatrix} \sqrt{.0053173 \sin^2 \phi + \frac{1}{10R\rho d}} - .07292 \sin \phi \end{bmatrix}$$
 (I) (Millibars)
$$\sqrt{.0053173 \sin^2 \phi + \frac{.13333}{R\rho d}} - .07292 \sin \phi \end{bmatrix}$$
 (II) (Millimeters)
$$\sqrt{.068914 \sin^2 \phi + \frac{1.6946}{R\rho d}} - .26252 \sin \phi \end{bmatrix}$$
 (III) (Inches)

V = velocities in meters per second in (I) and (II) and in miles per hour in (III).

R = radius of curvature of isobar (wind path) in kilometers in (I) and (II) and in miles in (III).

The gradient is to be deduced from isobars drawn for pressure intervals of I millibar in (I), I millimeter in (II) and $\frac{I}{IO}$ inch in (III); d, is the perpendicular distance between isobars (as above defined) in kilometers in (I) and (II), and in miles in (III). $\rho = \text{density of air} = \text{grams per cubic centimeter in all cases.}$

Also Units of pressure.
$$V_c = \begin{bmatrix} \frac{1.3713}{\rho d \sin \phi} \text{ (IV)} \\ \frac{1.8284}{\rho d \sin \phi} \text{ (V)} & \text{and } R_c = \begin{bmatrix} \frac{18.806}{\rho d \sin^2 \phi} \text{ (VII) (Millibars)} \\ \frac{25.073}{\rho d \sin^2 \phi} \text{ (VIII) (Millimeters)} \\ \frac{24.500}{\rho d \sin^2 \phi} \text{ (IX) (Inches)} \end{bmatrix}$$

Radius of critical curvature and velocities of gradient winds for frictionless motion in Highs and Lows.

TABLE 40. English Measures.

TABLES 40, 41.

TABLE 41. Metric Measures.

These tables give the radius of curvature of the critical isobar in anticyclones, computed from the equation

$$R_c = \frac{\Delta P}{\rho \omega^2 \sin^2 \phi},$$

the velocity of the wind on this isobar, computed from the equation

$$V_c = \frac{\Delta P}{\rho \omega \sin \phi};$$

the velocity of the wind on a straight isobar, computed from the equation

$$V_s = \frac{\Delta P}{2 \rho \omega \sin \phi} = \frac{I}{2} V_c$$
; and

the velocity of the wind in a cyclone having the same gradient as the anticyclone, and on an isobar having a radius of curvature equal to R_c , computed from the equation

$$V_1 = V_c (\sqrt{2} - 1) = 0.414 V_c$$

Table 40, English measures, gives values of R_c , in miles, and of V_c High, V_s , and V Low, in miles per hour. The side argument is the latitude for 10°, and at 5° intervals from 20° to 90°, inclusive. The top argument, d, is the perpendicular distance in miles between isobars drawn for pressure

intervals of $\frac{1}{10}$ inch. For values of d one tenth as great as given in the

heading of the table the values of R_c , V_c High, V_s , and V Low are increased tenfold.

Table 41, metric measures, gives values of R_c in kilometers, and of V_c High, V_s , and V Low, in meters per second. The side argument is the same as in Table 40. The top argument, d, is the perpendicular distance in kilometers between isobars drawn for pressure intervals of 1 millimeter. For values of d one tenth as great as given in the heading of the table the values of R_c , V_c High, V_s , and V Low are increased tenfold.

FOOF F

TEMPERATURE TABLES.

REDUCTION OF TEMPERATURE TO SEA LEVEL.

Table 42. English Measures.

TABLE 43. Metric Measures.

These tables give for different altitudes and for different uniform rates of decrease of temperature with altitude, the amount in hundredths of a degree Fahrenheit and Centigrade, which must be added to observed temperatures in order to reduce them to sea level.

The rate of decrease of temperature with altitude varies from one region to another, and in the same region varies according to the season and the meteorological conditions; being in general greater in warm latitudes than in cold ones, greater in summer than in winter, and greater in areas of falling pressure than in areas of rising pressure. For continental plateau regions, the reduction often becomes fictitious or illusory. The use of the tables therefore requires experience and judgment in selecting the rate of decrease of temperature to be used. Much experimental work is now in progress with kites and balloons to determine average vertical gradients. It must be remembered that the tables here given are not tables giving the data as recently determined for various elevations.

The tables are given in order to facilitate the reduction of temperature either upward or downward in special investigations, but the reduction is not ordinarily applied to meteorological observations.

The tables, 42 and 43, are computed for rates of temperature change ranging from 1° Fahrenheit in 200 feet to 1° Fahrenheit in 900 feet, and from 1° Centigrade in 100 meters to 1° Centigrade in 500 meters; and for altitudes up to 5000 feet and 3000 meters respectively.

Observed temperature at an elevation of 2 500 feet

Example, Table 42.

Exa

Observed temperature at an elevation of 2,500 feet,	52.5 F.
Reduction to sea level for an assumed decrease in tem-	
perature of 1° F. for every 300 feet,	+ 8°.3
Temperature reduced to sea level,	60°.8 F.
ample, Table 43.	
Observed temperature at an elevation of 500 meters,	12°5 C.
Reduction to sea level for an assumed decrease in temperature	era-
ture of 1° C. for every 200 meters,	+ 2°5
Temperature reduced to sea level,	15°0 C.

BAROMETRICAL TABLES.

REDUCTION TO A STANDARD TEMPERATURE OF OBSERVATIONS MADE WITH MERCURIAL BAROMETERS HAVING BRASS SCALES.

The indicated height of the mercurial column in a barometer varies not only with changes of atmospheric pressure, but also with variations of the temperature of the mercury and of the scale. It is evident therefore that if

the height of the barometric column is to be a true relative measure of atmospheric pressure, the observed readings must be reduced to the values they would have if the mercury and scale were maintained at a constant standard temperature. This reduction is known as the reduction for temperature, and combines both the correction for the expansion of the mercury and that for the expansion of the scale, on the assumption that the attached thermometer gives the temperature both of the mercury and of the scale.

The freezing point is universally adopted as the standard temperature of the mercury, to which all readings are to be reduced. The temperature to which the scale is reduced is the normal or standard temperature of the adopted standard of length. For English scales, which depend upon the English yard, this is 62° Fahrenheit. For metric scales, which depend upon the meter, it is 0° Centigrade. As thus reduced, observations made with English and metric barometers become perfectly comparable when converted by the ordinary tables of linear conversion, viz: inches to millimeters and millimeters to inches (see Tables 9, 10), for these conversions refer to the meter at 0° Centigrade and the English yard at 62° Fahrenheit.

Prof. C. F. Marvin in the Monthly Weather Review for July, 1898, has pointed out the necessity of caution in conversion of metric and English barometer readings:

Example:

Attached thermometer, 25.4 C. Barometer reading, 762.15 mm.

If the temperature is converted to Fahrenheit = 77.7 and the reading to 30.006 in., the temperature correction according to table 44 would be -0.133 inch and the reduced reading 29.873. This would be erroneous. The correct conversion is found by taking the correction corresponding to 25.4 C. and 762 mm., i.e., -3.15 mm., which gives a corrected reading of 759 mm., and converted into inches gives 29.882 which is the correct result.

Professor Marvin further remarks that circumstances sometimes arise in which a Centigrade thermometer may be used to determine the temperature of an English barometer, or a Fahrenheit attached thermometer may be used with a metric scale. In all such cases the temperature must be brought into the same system of units as the observed scale reading before corrections can be applied, and the observed reading must then be corrected for temperature before any conversion can be made.

With aneroid barometers corrections for temperature and instrumental error must be determined for each instrument.

The general formula for reducing mercurial barometers with brass scales to the standard temperature is

$$C = -B \frac{m (t - T) - l (t - \theta)}{1 + m (t - T)},$$

in which C =Correction for temperature.

B =Observed height of the barometric column.

t =Temperature of the attached thermometer.

T =Standard temperature of the mercury.

m = Coefficient of expansion of mercury.

l = Coefficient of linear expansion of brass.

 θ = Standard temperature of the scale.

The accepted determination of the coefficient of expansion of mercury is that given by Broch's reduction of Regnault's experiments, viz:

$$m \text{ (for I}^{\circ} C.) = IO^{-9} (181792 + 0.175t + 0.035116t^2).$$

As a sufficiently accurate approximation, the intermediate value

$$m = 0.0001818$$

has been adopted uniformly for all temperatures in conformity with the usage of the *International Meteorological Tables*.

Various specimens of brass scales made of alloys of different composition show differences in their coefficients of expansion amounting to eight and sometimes ten per cent. of the total amount. The *Smithsonian Tables* prepared by Prof. Guyot were computed with the average value l (for $l \circ C$.) = 0.0000188; for the sake of uniformity with the *International Meteorological Tables*, the value

$$l = 0.0000184$$

has been used in the present volume. For any individual scale, either value may easily be in error by four per cent.

A small portion of the tables has been independently computed, but the larger part of the values have been copied from the *International Meteorological Tables*, one inaccuracy having been found and corrected.

Table 44. Reduction of the barometer to standard temperature — English measures.

For the English barometer the formula for reducing observed readings to a standard temperature becomes

$$C = -B \frac{m (t - 32^{\circ}) - l (t - 62^{\circ})}{1 + m (t - 32^{\circ})}$$

in which B = Observed height of the barometer in English inches.

t = Temperature of attached thermometer in degrees Fahrenheit.

$$m = 0.0001818 \times \frac{5}{9} = 0.000101$$

$$l = 0.0000184 \times \frac{5}{9} = 0.0000102$$

The combined reduction of the mercury to the freezing point and of the scale to 62° Fahrenheit brings the point of no correction to approximately 28.5 Fahrenheit. For temperatures above 28.5 Fahrenheit, the correction is subtractive, and for temperatures below 28.5 Fahrenheit, the correction is additive, as indicated by the signs (+) and (-) inserted throughout the table.

The table gives the corrections for every half degree Fahrenheit from 0° to 100°. The limits of pressure are 19 and 31.6 inches, the corrections being computed for every half inch from 19 to 24 inches, and for every two-tenths of an inch from 24 to 31.6 inches.

Example:

Observed height of barometer = 29.143

Attached thermometer, 54.5 F.

Reduction for temperature = -0.068Barometric reading corrected for temperature = -0.068

TABLE 45.

Table 45. Reduction of the barometer to standard temperature — Metric measures.

For the metric barometer the formula for reducing observed readings to the standard temperature, o° C., becomes

$$C = -B \frac{(m-l)t}{1+mt}$$

in which C and B are expressed in millimeters and t in Centigrade degrees. $m = 0.0001818; \quad l = 0.0000184.$

In the table, the limits adopted for the pressure are 440 and 795 millimeters, the intervals being 10 millimeters between 440 and 600 millimeters, and 5 millimeters between 600 and 795 millimeters.

The limits adopted for the temperature are o° and + 35.8, the intervals being 0.5 and 1.0 from 440 to 560 millimeters, and 0.2 from 560 to 795 millimeters.

For temperatures above o° Centigrade the correction is *negative*, and hence is to be subtracted from the observed readings.

For temperatures below o° Centigrade the correction is *positive*, and from o° C. down to -20° C. the numerical values thereof, for ordinary barometric work, do not materially differ from the values for the corresponding temperatures above o° C. Thus the correction for -9° C. is *numerically* the same as for $+9^{\circ}$ C. and is taken from the table. In physical work of extreme precision, the numerical values given for positive temperatures may be used for temperatures below o° C. by applying to them the following corrections:

Corrections to be applied to the tabular values of Table 45 in order to use them when the temperature of the attached thermometer is below 0° Centigrade.

Temper-	PRESSURE IN MILLIMETERS.							
ature.	450	500	550	600	650	700	750	800
C.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.
- 1°	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
- 9	.00	.00	.00	.00	.00	.00	.00	.00
-10	0.00	0.00	0.00	0.00	0.00	+0.01	+0.01	+0.01
11	.00	.00	.00	.00	+0.01	.01	.01	.01
12	.00	.00	.00	+0.01	.01	.01	.01	.01
13	.00	.00	+0.01	10.01	10.	.01	.01	.01
-14	.00	+0.01	.01	.01	.01	.01	.01	.01
-15	+0.01	+001	+0.01	+0.01	+0.01	+0.01	+0.01	+0.01
16	.01	10.01	.01	.01	.01	.01	10.	10.
	.01	.01	.01	.01	.01	.01	.01	.02
17 18	.01	.01	.01	.01	10.	.01	.01	.02
-19	.01	.01	.01	.01	.01	.01	.02	.02
-20	+0.01	+0.01	+0.01	+0.01	+0.01	+0.02	+0.02	+0.02
21	10.01	10.01	10.01	.02	.02	.02	,02	.02
22	.01	10.	.02	.02	.02	.02	.02	.02
23	10.	.02	.02	.02	.02	.02	.02	.02
-24	10.	.02	.02	.02	.02	.02	.02	.03
,								

Example:

Observed height of barometer, 763.17^{mm}: Temperature of the attached thermometer, -12° C.

Numerical value of the reduction for $+ 12^{\circ} C$. = 1.50 Correction for temperature below $0^{\circ} C$. = + 0.01Reduction for $- 12^{\circ} C$. = + 1.51Observed height of barometer = 763.17Barometer corrected for temperature = 764.68

Table 46. Reduction of the mercurial column in U-shaped manometers with brass scales to standard temperature. English measures.

This is in reality an extension of Table 44 to the small differences in height of the mercurial columns as determined with a U-shaped manometer and is used especially in the calibration of instruments for upper-air investigations. Since the corrections are directly proportional to the observed height of the mercurial column, they have been obtained by multiplying corrections given in Table 44 by the appropriate decimal. They have been computed for each inch of pressure from 1 inch to 20 inches, inclusive, and for intervals of temperature of 2 degrees, from 0° to 100° Fahrenheit.

Example:

Observed heights	of the	mercury	in the	manometer	tubes	(in.),	+6.258
and -4.375 .							

Difference in height of the two columns 10.633

Attached thermometer, 72°4 F.

Correction for temperature - .042

Manometer reading corrected for temperature

10.591

For temperatures above $28^{\circ}.5$ Fahrenheit, the correction is subtractive, and for temperatures below $28^{\circ}.5$ Fahrenheit, the correction is additive, as indicated by the signs (+) and (-) inserted throughout the table.

Table 47. Reduction of the mercurial column in U-shaped manometers with brass scales to standard temperature. Metric measures.

This table is an extension of Table 45 to the small differences in height of the mercurial columns as determined with a U-shaped manometer. The values have been obtained from the corrections given in that table by the same process as those given in Table 46 were obtained from Table 44.

Example:

Observed heights of the mercury in the manometer tubes (mm.), +121.5 and -86.7.

Difference in height of the two columns 208.2

Attached thermometer, 18°4 C.

Correction for temperature – 0.6

Manometer reading corrected for temperature

207.6

For temperatures above o° C, the correction is negative, and hence is to be subtracted from the observed readings. For negative temperatures see the explanation of Table 45.

REDUCTION OF THE MERCURIAL BAROMETER TO STANDARD GRAVITY.

TABLES 48, 49, 50.

The mercurial barometer does not directly measure the atmospheric pressure. The latter is proportional to the weight of the mercurial column, and also to its height after certain corrections have been applied. Since the height of the barometric column is easily measured, by common consent the pressures are expressed in terms of this corrected height.

The observed height of the barometer changes with the temperature of the mercury as already shown, and also with the variations in the value of gravity, as well as with the pressure. Therefore, to obtain a height that shall be a true relative measure of the atmospheric pressure, the observed height of the mercurial column must not only be reduced to what its height would be if at a standard temperature, but also to what it would be at a standard value of gravity.

As stated on page xxii, the standard value of gravity adopted is 980.665 dynes. At the time of its adoption this value was assumed to apply for "latitude 45° and sea-level" on the basis of the absolute determination of g at the International Bureau by Defforges, 1887–1890 (Procés-Verbaux, Comité Inter. d. Poids et Mesures, 1887, pp. 27–28, 86; 1891, p. 135).

More recent determinations, based upon numerous measurements in all parts of the world, and assuming a certain ideal figure for the earth, give for the mean value of g at latitude 45° and sea level the value 980.621dynes. This differs from the standard value by 0.044 dyne. Departures of this magnitude from the mean sea-level gravity of a given latitude are frequently encountered, and in some cases surpassed. They are attributed to topography and isostatic compensation, and to gravity anomalies. For example, according to Bowie,2 at Pikes Peak, Colo., the correction for topography and compensation is +0.187 dyne, while the gravity anomaly 3 is +0.021 dyne, giving a total gravity departure of +0.208 dyne. Also, at Seattle, Wash., from the mean of measurements at two stations, the correction for topography and compensation is -0.019 dyne 4 and the gravity anomaly is -0.093 dyne,5 giving a total gravity departure of -0.112 dyne. The gravity departure at Pikes Peak is sufficient to cause the barometer to read 0.004 inch or 0.10 mm. low, while the departure at Seattle is sufficient to cause the barometer to read 0.003 inch or 0.00 mm. high, as compared with what the readings would have been with gravity at normal intensity for the latitudes of the respective stations.

From the foregoing it is evident that the value of local gravity, g_l , at the observing station must be determined before the barometer reading can be accurately reduced to standard gravity. In many cases, and especially at sea, it is not practicable to measure g_l . In the United States its value may frequently be determined with sufficient accuracy in the following manner:

(1) Compute g_{ϕ} , mean gravity at sea level for the latitude of the station, from the equation 6

```
g_{\phi} = 978.039 \text{ (I} + 0.005294 \sin^2 \phi - 0.000007 \sin^2 2\phi),}
= 980.621 (I - 0.002640 cos 2\phi + 0.000007 cos^2 2\phi)
```

(2) Correct g_{ϕ} for altitude by the equation 7 c (dynes) = -0.0003086 h (meters), or c (dynes) = -0.000094 h (feet),

¹ Investigations of gravity and isostasy, by William Bowie. U. S. Coast and Geodetic Survey, Special Publication No. 40, 1917, p. 134.

² Op. cit., p. 50. ³ Op. cit., p. 59. ⁴ Op. cit., p. 50. ⁵ Op. cit., p. 59. ⁶ Bowie, op. cit., p. 134. ⁷ Bowie, op. cit., p. 93.

where h is the altitude of the station above sea level.

(3) Correct g_{ϕ} for gravity anomaly.¹

(4) Finally, g_{ϕ} is to be corrected for topography and isostatic compensation.²

Example:

To determine the value of local gravity, g_1 , at the Weather Bureau Office, Atlanta, Ga., latitude 33° 45′ N., longitude 84° 23′ W., height of barometer above sea level, 1218 feet.

From Table 90, mean sea level gravity for latitude 33° 45′

itude 33° 45' = 979.631 dynes. Correction for height of barometer (-0.000094×1218) = -0.0114 " = -0.023 " = +0.014 "

Local gravity at Weather Bureau Office, Atlanta,

Ga. = 979.508 dynes.

Having determined g_l , the reduction of barometer readings to standard gravity is easily and accurately accomplished by multiplying by the ratio g_l/g_0 , or by applying a correction to the barometer reading, otherwise corrected, derived from the expression $\frac{(g_l-g_0)}{g_0}B$. With $g_l< g_0$ the correction is to be subtracted; with $g_l> g_0$ the correction is to be added. In general, sufficient accuracy will be attained by computing the gravity correction for a station once for all from the equation $C=B_n$ $\frac{(g_l-g_0)}{g_0}$,

in which B_n is the normal station barometer pressure, and C is expressed in the same units as B_n .

TABLE 48 gives corrections to reduce barometer readings to standard gravity. The top argument is the barometer reading. The side argument is the difference, $g_l - g_0$, for each tenth of a dyne up to 4.0 dynes. The relation is a linear function of both $g_l - g_0$ and B, and for barometer readings 10 or 100 times greater than those given in the argument the correction may be obtained by removing the decimal point in the tabulated values one or two places, respectively, to the right. The correction obtained will be expressed in the same units as the barometer reading to be corrected.

Example 1.

The barometer reading corrected for temperature is 29.647 inches, and the local value of gravity is 978.08. The difference, g_1-g_0 , = -2.585. From the table,

the correction for a barometer reading of 20 inches the correction for a barometer reading of 9 inches the correction for a barometer reading of 0.65 inches = -0.0237 in. Correction for a barometer reading of 29.65 inches = -0.078 in. Corrected barometer reading = 29.647 in. = -0.078 in. = -0.078 in. = -0.078 in.

¹ In most cases the gravity anomaly may be obtained from Bowie's paper, op. cit., figure 11.

² In some cases this correction may be obtained from Bowie's paper, op. cit., pp. 50-52, but in many cases, and especially in mountainous districts, it must be separately computed for each station.

Example 2.

The barometer reading reduced to 0° C. is 637.42 mm., and the local value of gravity is 981.51. The difference, $g_1 - g_0 = +0.845$. From the table,

the correction for a barometer reading of 600 mm. =+ 0.517 mm. the correction for a barometer reading of 30 mm. =+ 0.026 mm. =+ 0.006 mm. Correction for a barometer reading of 637.4 mm. =+ 0.55 mm. Corrected barometer reading =637.42+0.55 =+637.97 mm.

In the case of barometer readings made at sea, and also at some land stations, it is not practicable to determine local gravity with greater accuracy than it can be computed from the equations for variations with latitude and altitude given above. The reduction to standard gravity, accordingly, consists of two parts—a correction for altitude, and a correction from the computed sea-level gravity for the latitude of the station to standard gravity. The first part of the correction, or the correction for altitude, may be computed once for all from the expression $c=-0.0003086\ h\ B_n$ (metric measures), or $c=-0.000094\ h\ B_n$ (English measures), and is usually combined with the reduction of the barometer to sea level or to some other reference plane. The second part has heretofore consisted of a correction for the difference between the mean value of gravity for the latitude of the station and for latitude 45°; and, in accordance with the equation given above, it may be derived from the expression

$$(-0.002640\cos 2\phi + 0.000007\cos^2 2\phi)B$$

where ϕ is the latitude of the station, and B is the barometer reading. The value of the ratio $\frac{g_{45} \cdot - g_0}{g_0} = \frac{980.621 - 980.665}{980.665} = -0.000045$. Therefore, the expression for the gravity correction becomes

$$(-0.00264\cos 2\phi + 0.000007\cos^2 2\phi - 0.000045)B$$

Table 49 (English measures) gives the corrections in thousandths of an inch for every degree of latitude and for each inch of barometric pressure from 19 to 30 inches, to reduce barometer readings to standard gravity, computed from the equation

$$C = (-0.00264 \cos 2 \phi + 0.000007 \cos^2 2 \phi - 0.000045)B$$

TABLE 50 (*metric measures*) gives the same corrections in hundredths of a millimeter for each 20 millimeters barometric pressure from 520 to 780 millimeters.

Example:

Barometric reading (corrected for temperature) at latitude

63° 55', = 27.434 inches
Correction to standard gravity, Table 49, = 0.043 inches
Barometer reduced to standard gravity, = 27.477 inches

The adoption of this new value for standard gravity may require a slight correction to old barometric records in order to make the entire series of readings homogeneous. The amount of this correction will be the difference between the gravity correction computed by these new tables and by the old tables.

Example:

Seattle, Wash., Lat. 47° 38′ N., Long. 122° 20′ W., height of barometer above sea level 125 feet, normal station barometer 29.89 inches.

 g_{ϕ} (Table 90) = 980.859 dynes. Correction for height (-0.000094×125) = -012 "
Correction for topography and compensation = -0.019 "
Correction for gravity anomaly = -0.093 "
Value of level gravity.

Value of local gravity 980.735 dynes. Correction to reduce barometer readings to standard gravity,

980.735 - 980.665 $B_n = +0.002$ inch. Old correction, +0.007; correction to old

records = 0.002 in. - 0.007 in. = -0.005 in.

For correcting back records of readings at sea, or at any place where the value of local gravity cannot be determined, the correction is equal to

the ratio $\frac{980.599 - 980.665}{980.665}$ B = -0.000067 B. The corrections are as follows:

 Barometer reading.
 Correction.

 From 8 to 22 inches
 -0.001 in.

 From 23 to 32 inches
 -0.002 in.

 From 380 to 520 mm.
 -0.03 mm.

 From 530 to 670 mm.
 -0.04 mm.

 From 680 to 820 mm.
 -0.05 mm.

REDUCTION OF BAROMETER READINGS TO SEA LEVEL.

Tables 51 to 63 inclusive, "Determinations of Heights by the Barometer," may be used for reducing barometric readings to sea level, provided the mean temperature and vapor pressure of the atmosphere between the observing station and sea level are known.

See "Example: (English Measures)," p. xlix.

Barometer at upper station corrected for temperature =23.61 in. Mean temperature of air column, θ , $=35^{\circ}$ 0 F. Latitude of station, ϕ , $=44^{\circ}$ 16′ Altitude of station above mean sea level, Z, =6320 ft.

The equation for computing the altitude Z is given on p. xlvii. This equation is simplified after justifiable approximations to the form (in English units)

 $62583.6 \left(\log \frac{29.9}{B} - \log \frac{29.9}{B_0} \right) = Z - Z \left[0.002039 (\theta - 50^\circ) + 0.378 \frac{e}{b} + (\gamma + \eta) + \frac{Z + 2h_0}{R} \right],$

where the terms are as defined on pp. xliv to xlvi, inclusive. Calling the terms in the bracket (a), (b), (c) and (d), respectively, to compute B_0 we have:

from Table 52 with Z=6320 feet and $\theta=35^{\circ}$ 0 F., Z(a)=-194 from Table 54 with Z=6320 feet and average humidity, from Table 53 with Z=6320 feet and $\phi=44^{\circ}$ 16', $Z(c)=+16^{\circ}$ from Table 55 with Z=6320 feet and $h_0=0$, Z(d)=+2 Z(d)=+2 Z(d)=+2

Then since Z=6320 feet we have

$$62583.6 \left(\log \frac{29.9}{B} - \log \frac{29.9}{B_0} \right) = 6320 + 160 = 6480.$$

From Table 51 for B = 23.61 in., we have

62583.6
$$\log \frac{29.9}{B} = 6420$$
, hence
62583.6 $\log \frac{29.9}{B_0} = 6420 - 6480 = -60$.

Referring to Table 51 for the value of B_0 corresponding to this, we find $B_0 = 29.966$ in.

See "Example: (Metric Measures)," p. lii.

Let, the barometric reading (reduced to 0° C.), B=655.7 mm., the mean temperature of the air column, the mean vapor pressure of the air column, the latitude, the altitude of the station, E=0 mm., E=0 mm.

The equation for computing Z is simplified to the closely approximate form (from p. 1; for metric units)

$$18400 \left(\log \frac{760}{B} - \log \frac{760}{B_0} \right) = Z - Z \left[0.00367\theta + 0.378 \frac{c}{b} + (\gamma + \eta) + \frac{Z + 2h_0}{R} \right]$$

where the terms are as defined on pp. xliv-xlvi.

Again calling the terms in the bracket (a), (b), (c) and (d), respectively, to compute B_0 we have:

from Table 59, with
$$Z=1379$$
 m. and $\theta=12^{\circ}3$ C., $Z(a)=62$ from Table 60, with $Z=1379$ m. and $e=9$ mm., $Z(b)=7$ from Table 62, with $Z=1379$ m. and $\phi=32^{\circ}$, $Z(c)=5^{\circ}$ from Table 63, with $Z=1379$ m. and $h_0=0$, $Z(d)=0$ $Z(a)=0$ $Z(a)=0$ $Z(a)=0$ $Z(a)=0$ $Z(a)=0$

Since Z = 1379 m., we have

$$18400 \left(\log \frac{-760}{B} - \log \frac{-760}{B_0} \right) = 1379 - 74 = 1305.$$

From Table 56 for B = 655.7 mm., we have 18400 $\log \frac{760}{B} = 1179$, hence

18400
$$\log \frac{760}{B_0} = 1179 - 1305 = -126.$$

Referring to Table 56 for the value of B_0 corresponding to this, we find $B_0 = 772.1$ mm.

There are no difficulties connected with the use of these tables to reduce barometric readings to sea level, but serious difficulties are often encountered in attempting to determine θ and e from observations at the elevated station only (see pp. xxxiii and lxxii).

¹ Indicated values for latitude and gravity correction apply only to mercurial barometers. For the case of aneroid barometers the η is omitted (see pp. xlviii and xlix).

TABLES FOR DETERMINING HEIGHTS, AND CONVERSIONS INVOLVING GEOPOTENTIAL.

THE HYPSOMETRIC FORMULA AND ITS CONSTANTS.

The fundamental formula for reducing the barometer to sea level and for determining heights by the barometer is the original formula of Laplace, amplified into the following form —

$$(I) \quad Z = K \left(I + \alpha \theta \right) \left(\frac{I}{I - 0.378 \frac{e}{h}} \right) \left(I + \frac{g_0 - g_l}{g_0} \right) \left(I + \frac{h + h_0}{R} \right) \log \frac{p_0}{p},$$

or, where g_l , the value of local gravity is unknown,

(2)
$$Z = K (I + \alpha \theta) \left(\frac{I}{I - 0.378_b^e} \right) (I + k \cos 2 \phi - k' \cos^2 2 \phi + C) \left(I + \frac{h + h_o}{R} \right) \log \frac{p_o}{p}$$

in which

h = Height of the upper station.

 h_{\circ} = Height of the lower station.

 $Z = h - h_o$.

p = Atmospheric pressure at the upper station.

 p_{\circ} = Atmospheric pressure at the lower station.

R =Mean radius of the earth.

 θ = Mean temperature of the air column between the altitudes h and h_0 .

e = Mean pressure of aqueous vapor in the air column.

b = Mean barometric pressure of the air column.

 ϕ = Latitude of the stations.

K = Barometric constant.

 α = Coefficient of the expansion of air.

k and k' = Constants depending on the figure of the earth.

 $C = \text{Constant} = \text{the ratio } \frac{g_{45}^{\circ} - g_0}{g_0}$.

 g_0 = Standard value of gravity = 980.665 dynes.

 g_l = Local value of gravity.

The pressures p_o and p are computed from the height of the column of mercury at the two stations; the ratio $\frac{B_o}{B}$ of the barometric heights may be substituted for the ratio $\frac{p_o}{p}$, if B_o and B are reduced to the values that would be measured at the same temperature and under the same relative value of gravity.

The correction of the observed barometric heights for instrumental temperature is always separately made, but the correction for the variation of gravity with altitude is generally introduced into the formula itself.

If B_o , B represent the barometric heights corrected for temperature only, we have the equation

$$\frac{p_{o}}{p} = \frac{B_{o}}{B} \left(\mathbf{I} + \mu \, \frac{Z}{R} \right),$$

 μ being a constant depending on the variation of gravity with altitude $\left(\frac{\mu}{R} = 0.0000003\right)$, and

$$\log \frac{p_o}{p} = \log \frac{B_o}{B} + \log \left(\mathbf{I} + \mu \frac{Z}{R} \right).$$

Since $\frac{\mu Z}{R}$ is a very small fraction, we may write

Nap.
$$\log\left(1 + \frac{\mu Z}{R}\right) = \frac{\mu Z}{R}$$
, and $\log\left(1 + \frac{\mu Z}{R}\right) = \frac{\mu Z}{R}M$,

M being the modulus of common logarithms.

By substituting for Z its approximate value $Z = K \log \frac{B_o}{B}$, we have

$$\log\left(1 + \frac{\mu Z}{R}\right) = \frac{\mu K}{R} M \log \frac{B_{\circ}}{B}.$$

With these substitutions the barometric formula becomes

(1)
$$Z = K \left(\mathbf{I} + \alpha \theta \right) \left(\frac{\mathbf{I}}{\mathbf{I} - 0.378_{\overline{b}}^{e}} \right) \left(\mathbf{I} + \frac{g_{0} - g_{1}}{g_{0}} \right) \left(\mathbf{I} + \frac{h + h_{0}}{R} \right) \times \left(\mathbf{I} + \frac{\mu K}{R} M \right) \log \frac{B_{0}}{B}, \text{ or }$$

(2)
$$Z = K \left(\mathbf{I} + \alpha \theta \right) \left(\frac{\mathbf{I}}{\mathbf{I} - 0.378_b^e} \right) \left(\mathbf{I} + k \cos 2\phi - k' \cos^2 2\phi + C \right) \left(\mathbf{I} + \frac{h + h_o}{R} \right) \times \left(\mathbf{I} + \frac{\mu K}{R} M \right) \log \frac{B_o}{B}.$$

As a further simplification we shall put

$$\beta = 0.378 \frac{e}{b}$$
, $\gamma = k \cos 2 \phi - k' \cos^2 2 \phi + C$ and $\eta = \frac{\mu K}{R} M$,

and write for the second form, (2), the formula --

$$Z = K(\mathbf{I} + \alpha\theta) \left(\frac{\mathbf{I}}{\mathbf{I} - \beta}\right) (\mathbf{I} + \gamma) \left(\mathbf{I} + \frac{h + h_o}{R}\right) (\mathbf{I} + \eta) \log \frac{B_o}{B}$$

Values of the constants. — The barometric constant K is a complex quantity defined by the equation

$$K = \frac{\Delta \times B_n}{\delta \times M}.$$

 B_n is the normal barometric height of Laplace, 760 mm.

 Δ is the density of mercury at the temperature of melting ice. The value adopted by the International Meteorological Committee, and which has been employed in previous editions of these tables is $\Delta = 13.5956$. The

most probable value, taking into account the recently determined relation between the liter and the cubic decimeter, is as already stated, $\Delta = 13.5951$ and this value is here adopted.

 δ is the density of dry air at o°C under the pressure of a column of mercury B_n and under standard gravity. The value adopted by the International Bureau of Weights and Measures for air under the above conditions and free from CO_2 is $\delta = 0.0012928$ grams per cubic centimeter. This is in close agreement with the value ($\delta = 0.00129278$) used in previous editions of these tables. For air containing 4 parts in 10000 of CO_2 it gives a density of 0.00129307, and for air containing 3 parts in 10000 of CO_2 , the proportion adopted by Hann, it gives a density of 0.00129301. Therefore, the value adopted for the density of air containing an average amount of CO_2 is

$$\delta = 0.0012930$$

M (Modulus of common logarithms) = 0.4342945. These numbers give for the value of the barometric constant

$$K = 18400$$
 meters.

For the remaining constants, the following values have been used:

α = 0.00367 for 1° Centigrade. (International Bureau of Weights and Measures: Travaux et Mémoires, t. I, p. A. 54.)

 $\gamma = k \cos 2\phi - k' \cos^2 2\phi + C = 0.002640 \cos 2\phi - 0.000007 \cos^2 2\phi + 0.000045$

R = 6367324 meters. (A. R. Clarke: Geodesy, 8°, Oxford, 1880.)

$$\eta = \frac{\mu KM}{R} = 0.002396$$
. (Ferrel: Report Chief Signal Officer, 1885, pt. 2, pp. 17 and 393.)

TABLES 51, 52, 53, 54, 55.

THE DETERMINATION OF HEIGHTS BY THE BAROMETER.

TABLES 51, 52, 53, 54, 55.

English Measures.

Since a barometric determination of the height will rarely be made at a place where g_l is known, the discussion which follows will be confined to the second form of the barometric formula developed in the preceding section (see page xlv). For convenience in computing heights it is arranged in the following form:

$$Z = K \left(\log B_{\circ} - \log B\right) \begin{bmatrix} (\mathbf{I} + \alpha \theta) \\ (\mathbf{I} + \beta) \\ (\mathbf{I} + k \cos 2 \phi - k' \cos^{2} 2 \phi + C) (\mathbf{I} + \eta) \\ \left(\mathbf{I} + \frac{Z + 2 h_{\circ}}{R}\right) \end{bmatrix}$$

¹ Comptes Rendus, Quatrième Conférence Générale Poids et Mesures, 1907, pp. 60-61.

² Leduc, A. La masse du litre d'air dans les conditions normales. Comite international des poids et mesures. Travaux et mémoires, T. 16, 1917.

³ Lehrbuch der Meteorologie, dritte Auflage, 1915, s. 5.

in which K (log B_{\circ} – log B) is an approximate value of Z and the factors in the brackets are correction factors depending respectively on the air temperature, the humidity, the variation of gravity with latitude, the variation of gravity with altitude in its effect on the weight of mercury in the barometer, and the variation of gravity with altitude in its effect on the weight of the air. With the constants already given, the formula becomes in English measures:

In order to make the temperature correction as small as possible for average air temperatures, 50° F. will be taken as the temperature at which the correction factor is zero. This is accomplished by the following transformation:

$$1 + 0.002039 (\theta - 32^{\circ}) = [1 + 0.002039 (\theta - 50^{\circ})][1 + 0.0010195 \times 36^{\circ}].$$

The second factor of this expression combines with the constant, and gives $60368 (1 + 0.0010195 \times 36^{\circ}) = 62583.6$.

The first approximate value of Z is therefore

$$62583.6 (\log B_{\circ} - \log B).$$

In order further to increase the utility of the tables, we shall make a further substitution for $\log B_{\circ} - \log B$, and write

62583.6 (log
$$B_{\circ}$$
 – log B) = 62583.6 (log $\frac{29.9}{B}$ – log $\frac{29.9}{B_{\circ}}$).

TABLE 51 contains values of the expression

$$62583.6 \log \frac{29.9}{B}$$

for values of B varying by intervals of 0.01 inch from 12.00 inches to 30.90 inches.

The first approximate value of Z is then obtained by subtracting the tabular value corresponding to B_{\circ} from the tabular value corresponding to B (B and B_{\circ} being the barometric readings observed and corrected for temperature at the upper and lower stations respectively).

TABLE 52 gives the temperature correction

$$Z \times 0.002039 (\theta - 50^{\circ}).$$

¹ In accordance with the relation between the meter and the foot given on p. xxiii, this constant should be 60367. (See Table 14.)

The side argument is the mean temperature of the air column (θ) given for intervals of 1° from 0° to 100° F. The top argument is the approximate difference of altitude Z obtained from Table 51.

For temperatures above 50° F., the correction is to be added, and for temperatures below 50° F., the correction is to be subtracted. It will be observed that the correction is a linear function of Z, and hence, for example, the value for Z = 1740 is the sum of the corrections in the columns headed 1000, 700, and 40.

In general, accurate altitudes cannot be obtained unless the temperature used is freed from diurnal variation.

Table 53 gives the correction for gravity, and for the effect of the variation of gravity with altitude on the weight of the mercury. When altitudes are determined with aneroid barometers the second factor does not enter the formula. In this case the effect of the latitude factor can be obtained by taking the difference between the tabular value for the given latitude and the tabular value for latitude 45° 29'. The side argument is the latitude of the station given for intervals of 2° . The top argument is the approximate difference of height Z.

Table 54 gives the correction for the average humidity of the air at different temperatures. In evaluating the humidity factor as a function of the air temperature, the tables given by Prof. Ferrel have been adopted (Meteorological researches. Part iii. — Barometric hypsometry and reduction of the barometer to sea level. Report, U.S. Coast Survey, 1881. Appendix 10.) These tables by interpolation, and by extrapolation below $0^{\circ}F$, give the following values for β :

For Fahrenheit temperatures,

θ	β	θ	β	θ	β	θ	β
F20° -16 -12 -8 -6 -4 -2 -2 46 8	0.00008 .00020 .00032 .00044 0.00050 .00056 .00062 .00068 .00075 .00082 .00089	F. 10° 12 14 16 18 20 22 24 26 28 30 32 34	0.00104 .00111 .00118 .00126 .00134 .00143 .00153 .00163 .00174 .00187 .00203 .00222	F. 36° 38 40 42 44 46 48 50 52 54 56 58 60	0.00267 .00293 .00322 .00353 .00386 .00421 .00458 .00496 .00534 .00572 .00610 .00648	F. 62° 644 66 688 70 72 76 80 84 88 92 96	0.00724 .00762 .00801 .00839 .00877 .00914 0.00990 .01065 .01141 .01217 .01293

This correction could have been incorporated with the temperature factor in Table 52, but it is given separately in order that the magnitude of the correction may be apparent, and in order that, when the actual hu-

midity is observed, the correction may be computed if desired, by the expression

$$Z\left(0.378 \frac{e}{\bar{b}}\right)$$

where e is the mean pressure of vapor in the air column, and b the mean barometric pressure.

The side argument is the mean temperature of the air column, varying by intervals of 2° from -20° F. to 96° F., except near the extremities of the table where the interval is 4° . The top argument is the approximate difference of altitude Z.

Table 55 gives the correction for the variation of gravity with altitude in its effect on the weight of the air. The side argument is the approximate difference of altitude Z, and the top argument is the elevation of the lower station h_0 .

The corrections given by Tables 53, 54, and 55 are all additive.

Example:

Let the barometric pressure observed, and corrected for temperature, at the upper and lower stations be, respectively, B = 23.61 and $B_{\circ} = 29.97$. Let the mean temperature of the air column be 35° F, and the latitude 44° 16′. To determine the difference of height.

	Feet.
Table 51, argument 23.61, gives	6420
Table 51, " 29.97, "	- 64
Approximate difference of height (Z)	$= \overline{6484}$
Table 52, with $Z = 6484$ and $\theta = 35^{\circ} F$., gives	- 198
Table 53, with $Z=6300$ and $\phi=44^{\circ}$, gives	+ 16
Table 54, with $Z = 6300$ and $\theta = 35^{\circ}$ F., gives	+ 16
Table 55, with $Z = 6300$ and $h_0 = 0$, gives	+ 2
Final difference of height (Z)	= 6320

If in this example the barometric readings be observed with aneroid barometers, the correction to be obtained from Table 53 will be simply the portion due to the latitude factor, and this will be obtained by subtracting the tabular value for 45° 29' from that for 44° , the top argument being Z = 6300. This gives 16 - 15 = 1.

TABLES 56, 57, 58, 59, 60, 61, 62, 63.

Metric and Dynamic Measures.

The barometric formula developed on page xlvi is, in metric and dynamic units,

$$Z \text{ (meters)} = 18400 \text{ (log } B_{\circ} - \log B) \boxed{ (1 + 0.00367 \ \theta \ C.) }$$

$$(1 + 0.378 \frac{\epsilon}{b})$$

$$(1 + 0.002640 \cos 2 \phi - 0.000007 \cos^{2} 2 \phi$$

$$+ 0.000045) (1 + 0.00239)$$

$$(1 + \frac{Z + 2 \ h_{\circ}}{6 \ 367 \ 324})$$

The approximate value of Z (the difference of height of the upper and lower station) is given by the factor 18400 (log B_{\circ} – log B). This expression is computed by means of two entries of a table whose argument is the barometric pressure. In order that the two entries may result at once in an approximate value of the elevation of the upper and lower stations, a transformation is made, which gives the following identities:

18400 (
$$\log B_{\circ} - \log B$$
) = 18400 ($\log \frac{760}{B} - \log \frac{760}{B_{\circ}}$) — Metric measures, and 18400 ($\log B_{\circ} - \log B$) = 18400 ($\log \frac{1013.3}{B} - \log \frac{1013.3}{B_{\circ}}$) — Dynamic measures.

Table 56 gives values of the expression 18400 $\log \frac{760}{B}$ for values of B varying by intervals of I mm. from 300 mm. to 779 mm. The first approximate value of Z is then obtained by subtracting the tabular value corresponding to B_0 from the tabular value corresponding to B (B and B_0 being the barometric readings observed and reduced to 0° C. at the upper and lower stations respectively). The first entry of Table 56 with the argument B gives an approximate value of the elevation of the upper station

above sea level, and the second entry with the argument B_0 gives an ap-

proximate value of the elevation of the lower station.

Table 57 gives values of the expression 18400 log $\frac{1013.3}{B}$ for values of

B varying by intervals of I mb. from 0 mb. to 1049 mb. The approximate value of Z is then obtained by subtracting the tabular value corresponding to B_0 from the tabular value corresponding to B (B and B_0 being the barometric readings observed and reduced to 0° C. at the upper and lower stations respectively). The first entry of Table 57 with the argument B gives an approximate value of the elevation of the upper station above sea level, and the second entry with the argument B_0 gives an approximate value of the elevation of the lower station.

TABLE 58 gives the temperature correction factor, $a = 0.00367\theta$, for each tenth of a degree centigrade, from 0° C. to 50.9° C. To find the correction corresponding to any mean temperature of the air column, θ , multiply the approximate altitude as determined from Table 56 or 57 by the value of a obtained from this table, and add the result if θ is above 0° C.; subtract, if below 0° C.

Attention is called to the fact that the formula is linear with respect to θ , and hence that the correction, for example, for 59.8 C. equals the correction for 50.8 plus the correction for 9° or .186 + .033 = .219, and is to be added.

Table 59 is an amplification of Table 58 and gives the temperature correction 0.00367 $\theta \times Z$.

The side argument is the approximate difference of elevation Z and the top argument is the mean temperature of the air column. The values of Z vary by intervals of 100 m. from 100 to 4000 meters and the temperature varies by intervals of 1° from 1° C. to 10° C. with additional columns for 20°, 30°, and 40° C. This formula also is linear with respect to θ , and hence the correction, for example, for 27° equals the correction for 20° plus the correction for 7°. When the table is used for temperatures below 0° C. the tabular correction must be subtracted from, instead of added to, the approximate value of Z.

TABLE 60 (pp. 148 and 149) gives the correction for humidity resulting from the factor 0.378 $\frac{e}{h} \times Z = \beta Z$.

Page 148 gives the value of 0.378 $\frac{e}{b}$ multiplied by 10000. The side argument is the mean pressure of aqueous vapor, e, which serves to represent the mean state of humidity of the air between the two stations. $e = \frac{1}{2}(e_1 + e_0)$ (e_1 and e_0 being the vapor pressures observed at the two stations) has been written at the head of the table, but the value to be assigned to e is in reality left to the observer, independently of all hypothesis. The top argument is the mean barometric pressure $\frac{1}{2}$ ($B + B_0$).

The vapor pressure varies by millimeters from 1 to 40, and the mean barometric pressure varies by intervals of 20 mm. from 500 mm. to 760 mm.

The tabular values represent the humidity factor β , or 0.378 $\frac{e}{b}$, multiplied by 10000.

. Page 149 gives the correction for humidity, with Z and 10000 \times 0.378 $\frac{e}{b}$ (derived from page 148) as arguments.

The approximate difference of altitude is given by intervals of 100 meters from 100 to 4000 meters, with additional lines for 5000, 6000, and 7000 meters. The values of 10000 β vary by intervals of 25 from 25 to 300. The tabular values are given in tenths of meters to facilitate and increase the accuracy of interpolation.

Table 61. Humidity correction: Value of $\frac{1}{2} \left(\frac{0.378_b^e}{0.00367} \right)$. It has been found advantageous to express the humidity term, βZ , as a correction to the temperature term, $\alpha \theta Z$.

Let
$$\alpha \Delta \theta Z = \beta Z$$
; then,
$$\Delta \theta = \frac{\beta}{\alpha} = \frac{0.378 \frac{e}{b}}{0.00367}$$

For convenience in computing, the tabulated values of $\Delta \theta$ are for $\frac{1}{2} \left(\frac{0.378_b^e}{0.00367} \right)$. The side and top arguments are air and vapor pressures, respectively, in mm. on p. 150 and in mb. on p. 151. Instead of computing $\Delta \theta$ from the mean of the values of B and e at the upper and lower stations it is computed for each station separately, and the sum of the two determinations is added to θ .

TABLE 62 gives the correction for gravity, and for the effect of the variation of gravity with altitude on the weight of the mercurial column. When altitudes are determined with aneroid barometers the latter factor does not enter the formula. In this case the effect of the latitude factor can be obtained by subtracting the tabular value for latitude 45° 29′ from the tabular value for the latitude in question.

The side argument is the approximate difference of elevation Z varying by intervals of 100 meters from 100 to 4000, and by 500 meters from 4000 to 7000. The top argument is the latitude, varying by intervals of 5° from 0° to 75.°

TABLE 63 gives the correction for the variation of gravity with altitude in its effect on the weight of the air.

The side argument is the same as in Table 62; the top argument is the height of the lower station, varying by intervals of 200 meters from 0 to 2000, with additional columns for 2500, 3000 and 4000 meters.

The corrections given in Table 62 and Table 63 apply to the approximate heights computed from metric or dynamic measures by the use of Tables 56 to 61, inclusive, and are additive.

Example: (Metric Measures.)

Let the barometric reading (reduced to 0° C.) at the upper station be 655.7 mm.; at the lower station, 772.4 mm. Let the mean temperature of the air column be $\theta = 12^{\circ}.3$ C., the mean vapor pressure e = 0 mm. and the latitude $\phi = 32^{\circ}$.

Table 56, with argument 655.7, gives	1179 meters.
Table 56, " " 772.4, "	- 129
Approximate value of Z	= 1308
Table 59, with $Z = 1308$ and $\theta = 12^{\circ}3$ C, gives	59
Table 60, with $e = 9$ mm. and $Z = 1370$, gives	7
Table 62, with $Z = 1370$ and $\phi = 32^{\circ}$, gives	5
Table 63, with $Z = 1370$ and $h_0 = 0$, gives	O
Corrected value of Z	= 1379 meters.

Example: (Dynamic Measures.)

Let the barometer reading (reduced to 0° C.) at the upper station be 448.6 mb.; at the lower station, 1000.3 mb. Let the vapor pres-

sure at the upper station be 2.4 mb.; at the lower station 7.3 mb. Let the mean temperature of the air column be $\theta = 5^{\circ}8$ C. and the latitude $\phi = 39^{\circ}$ 25' N.

Table 57, with argument 448.6, gives	6511 meters.
Table 57, with argument 1000.3, gives	104
Approximate value of Z	6407 meters.
Table 61, with arguments 449 and 2.4 gives $\Delta\theta = 0.3$	
Table 61, with arguments 1000 and 7.3 gives $\Delta\theta = 0.4$	
Table 58, with $\theta = 5^{\circ}8 + 0^{\circ}7 = 6^{\circ}5$, and $Z = 6407$ gives	
6407 × 0.024=	154
Table 62 with $Z = 6561$ and $\phi = 39^{\circ}$ 25', gives	19
Table 63 with $Z = 6561$ and $h_0 = 0$, gives	7
Corrected value of Z	$=\overline{6587}$ meters.

GEOPOTENTIAL: DYNAMIC HEIGHTS.

In accordance with the "Règlement" of the Commission Internationale de la Haute Atmosphère adopted at the meeting held in London in April, 1925, heights in all forms and publications of the International Commission are to be measured as "geopotentials" in "dynamic meters" above sea level.

The geopotential or gravity potential of a point is defined numerically as the value of the potential energy relative to sea level of a unit-mass situated at the point.

The application of geopotential as a measure of height becomes more evident when it is seen that surfaces of equal geopotential are identical with horizontal or level surfaces, and due to the geographical variation of gravity, they are not surfaces equally distant from sea level. In this regard it may be emphasized that energy is involved in displacing a mass of air from one position to another in which the potential energy of the mass is different, whereas the displacement of air may take place along horizontal or equigeopotential surfaces without the gain or expenditure of potential energy once the air is in a state of uniform motion. The latter statement, on the contrary, does not hold for surfaces of equal geometric height above sea level.

For the purposes of dynamical meteorology, in making comparisons of vertical positions, certain advantages are derived by defining the height of points above sea level in terms of geopotential. Heights measured in this way

¹ A fuller account of this Règlement may be found in the Avant-Propos of the Commission Internationale de la Haute Atmosphère, Comptes Rendus des Jours Internationaux 1923, published in 1927. This may be had on application to the Secretary of this Commission, c/o the Royal Meteorological Society, London.

are called "dynamic heights," after Prof. V. Bjerknes, and indicate relative potential energies of unit-mass. Thus, points of equal "dynamic height" lie in horizontal or geopotential surfaces.

The geopotential of a point, from the definition, is equal to the work done in lifting a unit-mass from sea level to the point, and is defined precisely by the expression:

$$\Gamma = -\int_{0}^{h} g \ dh$$

where

g = acceleration of gravity

and h = geometric height of the point above sea level.

The dimensions of geopotential in the absolute system are l^2/t^2 . Following the proposal of Prof. Bjerknes,¹ the unit of dynamic height is called the "dynamic meter" and has the magnitude 10 m^2/\sec^2 where g is measured in m/\sec^2 , and h in meters.

The unit is chosen with this magnitude for convenience, since a change in elevation of one meter geometric height produces a change in dynamic height of approximately 98 per cent of one "dynamic meter," *i. e.*, within the range of the majority of present atmospheric observations.

CALCULATION OF DYNAMIC HEIGHTS.

Equation (1) may be solved by substituting in it Helmert's ² equation for the decrease of acceleration of gravity with height:

(2)
$$g = -(g_{\phi} - 0.000003086 h)$$

where

 g_{ϕ} = acceleration of gravity below given point at sea level, in m/\sec^2 . g = acceleration of gravity at point whose elevation is h above sea level. h = geometric height in meters, above sea level.

The minus sign is used because gravity is directed downwards and heights are measured upwards positively.

Equation (1) becomes:

(3)
$$H_d = \frac{1}{10} \int_0^h (g_\phi - 0.000003086 \, h) \, dh$$

where $H_d = \text{dynamic}$ height, in dynamic meters.

¹ The claim for the use of geopotential in measuring heights was set forth by Prof. V. Bjerknes and his collaborators in Vol. I of Dynamical Meteorology and Hydrography, published in English in 1910 by the Carnegie Institution of Washington. The terms "dynamic height" and "dynamic meter" were therein proposed.

² Helmert: Über die Reduction der auf der physischen Erdoberfläche beobachteten Schweerebeschleunigungen auf ein gemeinsames Niveau, Zweite Mitteilung. Sitzungsberichte der Akademie der Wissenschaften, Berlin, 1903, p. 650.

The factor $\frac{1}{10}$ is substituted in eq. (1) to convert to units of dynamic height in dynamic meters (10 m^2/sec^2).

Integrating (3), we obtain

(4)
$$H_d = \frac{g_\phi}{10} h - 1.543 \times 10^{-7} h^2$$

For a first approximation, we may neglect the term in h^2 and take $g_{\phi} = 9.8 \text{ m/sec}^2$,

whence

(5)
$$H_d = 0.98 h$$
, approximately, and (6) $h = 1.02 H_d$, approximately.

Geometric heights (h) may be expressed in terms of dynamic heights (H_a) by a convenient approximate relationship.

Substituting (6) in the h^2 term of (4) we obtain

(7)
$$h = \frac{10}{g_{\phi}} H_d + \frac{10}{g_{\phi}} 1.543 (1.02)^2 \cdot 10^{-7} \cdot H_d^2$$

which is simplified for computation by taking 9.8062 as g_{ϕ} in the second term, this being the mean value at latitude 45° and sea level.

Thus (7) becomes

(8)
$$h = \frac{10}{g_{\phi}} H_a + 1.637 \times 10^{-7} H_a^2$$
 approximately.

We are indebted to Prof. V. Bjerknes and his collaborators for the above formulation, and for tables 64, 65, 67 and 68, which are copied directly from their "Dynamical Meteorology and Hydrography." ¹

description and use of tables 64 to 68 inclusive.

The purpose of these tables is to convert from geometric heights to dynamic heights and vice versa. Tables 64, 65, and 66 are used to convert geometric meters to dynamic meters. Tables 66, 67, and 68 are used to convert dynamic meters to geometric meters.

Table 64. Heights reduced from meters to dynamic meters, the acceleration of gravity at sea level being 9.80.

This table, computed by means of equation (4) above, makes possible the reduction of geometric heights to dynamic heights, the acceleration of gravity at sea level being 9.80 m/sec². In this table the side argument is geometric height above sea level by intervals of 1000 m., and the top argument is geometric height by intervals of 100 m. The proportionality table at the foot of the main table makes it possible to obtain dynamic heights corresponding to any integral number of geometric meters from 0 to 30.000.

¹ Bjerknes, V., and colleagues, Carnegie Inst. Washington, 1910.

Table 65. Corrections to Table 64 for values of the acceleration of gravity at sea level different from 9.80.

This table is computed from a modification of equation (4) arranged to give the increments of dynamic height corresponding to changes in g_{ϕ} from 9.80 m/sec^2 . This form is $H_d = (0.980 \, h - 1.543 \times 10^{-7} \, h^2) + \frac{g_{\phi} - 9.80}{10} \, h$ the latter factor being the increment.

Corrections obtained from this table are applied to values obtained from Table 64 for stations whose latitude is such that g_{ϕ} differs from 9.80 m/\sec^2 . The side argument here is geometric height by intervals of 1000 m. and the top argument is g_{ϕ} , the acceleration of gravity at sea level. Interpolations must be made for geometric heights which are not in even km. and for values of g_{ϕ} which lie between the values given at the top.

Table 66. Normal value of the acceleration of gravity at sea level.

This table has been computed by means of the U. S. Coast and Geodetic Survey Formula

$$g_{\phi} = 9.80621 \ (1 - 0.002640 \cos 2 \phi + 0.000007 \cos^2 2 \phi)$$

where

 $g_{\phi} =$ normal value of acceleration of gravity in m/\sec^2 at latitude ϕ at sea level. and $\phi =$ latitude in degrees.

The side argument is latitude by intervals of 10°, and the top argument is latitude by unit degrees from 0 to 9. Thus the value of g_{ϕ} may be obtained for every degree of latitude. For stations whose latitude cannot be expressed in whole degrees, interpolations may be made for fractional parts of degrees, or reference may be made to Table 90.

Table 67. Heights reduced from dynamic meters to geometric meters, the acceleration of gravity being 9.80.

This table, computed by means of equation (8) converts dynamic heights to geometric heights, where $g_{\phi} = 9.80 \ m/sec^2$. The side argument is dynamic height by intervals of 1000 dynamic meters and the top argument is dynamic height by intervals of 1000 dynamic meters. A proportionality table is added as in Table 64.

Table 68. Corrections to Table 67 for values of the acceleration of gravity at sea level different from 9.80.

This table is computed from a modification of equation (8). The modified form employed is

(8a)
$$h = \left(\frac{10}{9.80} H_d + 1.637 \times 10^{-7} H_d^2\right) + \frac{9.80 - g_\phi}{0.98 g_\phi} H_d$$

Table 67 represents values obtained from the expression within the parentheses and Table 68 represents values computed from the latter factor, taking 0.98 g_{ϕ} as equal to 9.60 for a close approximation of the denominator. This table thus gives increments of geometric height which are applied as corrections to values obtained from Table 67 for stations whose acceleration of gravity at sea level differs from 9.80. The side argument is dynamic height by intervals of 1000 dynamic meters and the top argument is g_{ϕ} , acceleration of gravity, by intervals of 0.01 m/\sec^2 Interpolations must be made for dynamic heights which are not in even thousands and for values of g_{ϕ} lying between those given at the top.

Table 69. Difference of height corresponding to a change of 0.1 inch in the barometer—English measures.

If we differentiate the barometric formula, page xlvii, we shall obtain, neglecting insensible quantities,

$$dZ = -26281 \frac{dB}{B} \left(1 + 0.002039 (\theta - 32^{\circ}) \right) (1 + \beta),$$

in which B represents the mean pressure of the air column dZ.

Putting dB = 0.1 inch,

$$dZ = -\frac{2628.1}{B} \left(1 + 0.002039 (\theta - 32^{\circ}) \right) (1 + \beta).$$

The second member, taken positively, expresses the height of a column of air in feet corresponding to a tenth of an inch in the barometer under standard gravity. Since the last factor $(I+\beta)$, as given on page xlviii, is a function of the temperature, the function has only two variables and admits of convenient tabulation

Table 69, containing values of dZ for short intervals of the arguments B and θ , has been taken from the Report of the U. S. Coast Survey, 1881, Appendix 10,—Barometric hypsometry and reduction of the barometer to sea level, by Wm. Ferrel.¹

The temperature argument is given for every 5° from 30° F. to 85° F., and the pressure argument for every 0.2 inch from 22.0 to 30.8 inches.

This table may be used in computing small differences of altitude, and, up to a thousand feet or more, very approximate results may be obtained.

$$d~Z = -\frac{2628.4}{B} \Big(1 + 0.002034 \; (\theta - 32^{\circ}) \Big) (1 + \beta).$$

¹ Due to the use of a slightly different value for the coefficient of expansion, Prof. Ferrel's formula, upon which the table is computed, is

Example:

Mean pressure at Augusta, October, 1891, 29.94; temperature, 60.8 F. Mean pressure at Atlanta, October, 1891, 28.97; temperature, 59.4 Mean pressure of air column B = 29.455; $\theta = 60.1$

Entering the table with 29.455 and 60°.1 as arguments, we take out 94.95 as the difference of elevation corresponding to a tenth of an inch difference of pressure. Multiplying this value by the number of tenths of inches difference in the observed pressures, viz. 97, we obtain the difference of elevation 921 feet.

TABLE 70.

Table 70. Difference of height corresponding to a change of one millimeter in the barometer — Metric measures.

This table has been computed by converting Table 69 into metric units. The temperature argument is given for every 2° from -2° C. to $+36^{\circ}$ C.; the pressure argument is given for 10-mm. intervals from 760 to 560 mm.

TABLE 71.

TABLE 71. Babinet's formula for determining heights by the barometer.

Babinet's formula for computing differences of altitude ¹ represents the formula of Laplace quite accurately for differences of altitude up to 1000 meters, and within one per cent for much greater altitudes. As it has been quite widely disseminated among travelers and engineers, and is of convenient application, the formula is here given in English and metric measures. It might seem desirable to alter the figures given by Babinet so as to conform to the newer values of the barometrical constants now adopted; but this change would increase the resulting altitudes by less than one-half of one per cent without enhancing their reliability to a corresponding degree, on account of the outstanding uncertainty of the assumed mean temperature of the air.

The formula is, in English measures,

$$Z ext{ (feet)} = 52494 \left[1 + \frac{t_o + t - 64^\circ}{900} \right] \frac{B_o - B}{B_o + B};$$

and in metric measures,

$$Z \text{ (meters)} = 16000 \left[1 + \frac{2(t_o + t)}{1000} \right] \frac{B_o - B}{B_o + B}$$

in which Z is the difference of elevation between a lower and an upper station at which the barometric pressures corrected for all sources of instrumental error are B_o and B, and the observed air temperatures are t_o and t, respectively.

For ready computation the formula is written

$$Z = C \times \frac{B_{\circ} - B}{B_{\circ} + B},$$

¹ Comptes Rendus, Paris, 1850, vol. xxx., page 309.

and the factor C, computed both in English and metric measures, has been kindly furnished by the late Prof. Cleveland Abbe. The argument is $\frac{1}{2}(t_0+t)$ given for every 5° Fahrenheit between 10° and 100° F., and for every 2° Centigrade between - 10° and 36° Centigrade.

In using the table, it should be borne in mind that on account of the uncertainty in the assumed temperature, the last two figures in the value of C are uncertain, and are here given only for the sake of convenience of interpolation. Consequently one should not attach to the resulting altitudes a greater degree of confidence than is warranted by the accuracy of the temperatures and the formula. The table shows that the numerical factor changes by about one per cent of its value for every change of five degrees Fahrenheit in the mean temperature of the stratum of air between the upper and lower stations; therefore the computed difference of altitude will have an uncertainty of one per cent if the assumed temperature of the air is in doubt by $5^{\circ}F$. With these precautions the observer may properly estimate the reliability of his altitudes whether computed by Babinet's formula or by more elaborate tables.

Example:

Let the barometric pressure observed and corrected for temperature at the upper and lower stations be, respectively, B=635 mm. and $B_{\circ}=730$ mm. Let the temperatures be, respectively, $t=15^{\circ}$ C., $t_{\circ}=20_{\circ}$ C. To find the approximate difference of height.

With $\frac{1}{2}(t_0 + t) = \frac{20^\circ + 15^\circ}{2} = 17^\circ 5$ C., the table in metric measures gives $B_\circ - B = 95$

C = 17120 meters. $\frac{B_{\circ} - B}{B_{\circ} + B} = \frac{95}{1365}.$

The approximate difference of height = $17120 \times \frac{95}{1365} = 1191.5$ meters.

THERMOMETRICAL MEASUREMENT OF HEIGHTS BY OESERVATION OF THE TEMPERATURE OF THE BOILING POINT OF WATER.

When water is heated in the open air, the elastic force of its vapor gradually increases, until it becomes equal to the incumbent weight of the atmosphere. Then, the pressure of the atmosphere being overcome, the steam escapes rapidly in large bubbles and the water boils. The temperature at which water boils in the open air thus depends upon the weight of the atmospheric column above it, and under a less barometric pressure the water will boil at a lower temperature than under a greater pressure. Now, as the weight of the atmosphere decreases with the elevation, it is obvious that, in ascending a mountain, the *higher* the station where an observation is made, the *lower* will be the temperature of the boiling point.

The difference of elevation between two places therefore can be de-

duced from the temperature of boiling water observed at each station. It is only necessary to find the barometric pressures which correspond to those temperatures, and from these to compute the difference of height by the tables given herein for computing heights from barometric observations.

From the above, it may be seen that the heights determined by means of the temperature of boiling water are less reliable than those deduced from barometric observations. Both derive the difference of altitude from the difference of atmospheric pressure. But the temperature of boiling water is a less accurate measurement of the atmospheric pressure than is the height of the barometer. In the present state of thermometry it would hardly be safe, indeed, to rely, in the most favorable circumstances, upon quantities so small as hundredths of a degree, even when the thermometer has been constructed with the utmost care; moreover, the quality of the glass of the instrument, the form and substance of the vessel containing the water, the purity of the water itself, the position at which the bulb of the thermometer is placed, whether in the current of the steam or in the water, — all these circumstances cause no inconsiderable variations to take place in the indications of thermometers observed under the same atmospheric pressure. Owing to these various causes, an observation of the boiling point, differing by one-tenth of a degree from the true temperature, ought to be still admitted as a good one. Now, as the tables show, an error of one-tenth of a degree Centigrade in the temperature of boiling water would cause an error of 2 millimeters in the barometric pressure, or of from 70 to 80 feet in the final result, while with a good barometer the error of pressure will hardly ever exceed one-tenth of a millimeter, making a difference of 3 feet in altitude.

Notwithstanding these imperfections, the hypsometric thermometer is of the greatest utility to travellers and explorers in rough countries, on account of its being more conveniently transported and much less liable to accidents than the mercurial barometer. A suitable form for it, designed by Regnault (Annales de Chimie et de Physique, Tome xiv, p. 202), consists of an accurate thermometer with long degrees, subdivided into tenths. For observation the bulb is placed about 2 or 3 centimeters above the surface of the water, in the steam arising from distilled water in a cylindrical vessel, the water being made to boil by a spirit-lamp.

TABLES 72, 73.

Barometric pressures at standard gravity corresponding to the temperature of boiling water.

Table 72. English Measures.

TABLE 73. Metric Measures.

Table 72 is copied directly from Table 75. The argument is the temperature of boiling water for every tenth of a degree from 185°0 to 214°9 Fahrenheit. The tabular values are given to the nearest 0.001 inch.

Table 73 is copied directly from Table 77. The argument is given for every tenth of a degree from 80°0 to 100°9 C. The tabular values are given to the nearest 0.01 mm.

HYGROMETRICAL TABLES.

PRESSURE OF SATURATED AQUEOUS VAPOR.

In former editions of these tables the values of aqueous vapor pressures at temperatures between -29° and 100° C. were based upon Broch's reduction of the classic observations of Regnault. (Travaux et Mémoires du Bureau international des Poids et Mesures, t. I, p. A 19–39). In these computations the same continuous mathematical function was employed to calculate the values of vapor pressure both above and below the point of change of state on freezing. This resulted in a systematic disagreement between observed and computed vapor pressures below the freezing point, and confirmed the inference from the laws of diffusion following from the kinetic theory of gases, namely, that the pressure of the vapor is different according as it is in contact with its liquid or its solid.

Seeking to remove the uncertainty of the values of vapor pressures at temperatures below freezing, Marvin (Annual Report Chief Signal Officer, 1891, Appendix No. 10) made direct experimental determinations thereof, in the course of which the specimens of water were cooled to temperatures of from -10° to -12° C. while still retaining the liquid state, thus affording opportunity for measurements of vapor pressure over ice and over water at various temperatures below the freezing point. The results of these investigations, confirmed by similar independent studies by Juhlin, were printed in the third revised edition of these tables.

Since 1907, especially, several extended series 1 of entirely new determinations, together covering the whole range of temperature from - 70° C. to + 374° C., have been made at the Physikalische-Technischen Reichsanstalt. Because of the elaborate instrumental means available and the extreme effort to eliminate all possible errors these results may be presumed to represent the most accurate series of experimental values of this important physical datum available to science.

Hitherto no satisfactory mathematical equation has been offered adequate to give computed values of vapor pressures with an order of precision comparable to the systematic self consistency of the observations

¹ Scheel, Karl und Heuse, Wilhelm. Bestimmung des Sättigungsdrucks von Wasserdampf unter o°. Annalen der Physik, 1909, 29: 723–737.

Bestimmung des Sättigungsdrucks von Wasserdampf zwischen o° und \pm 50°. Annalen der Physik, 1910, 31: 715–736.

Holborn, L. und Henning, F. Über das Platinthermometer und den Sättigungsdruck des Wasserdampfes zwischen 50 und 200°. Annalen der Physik, 1908, 26: 833–883.

Holborn, L. und Baumann, A. Über den Sättigungsdruck des Wasserdampfes oberhall. 200°. Annalen der Physik, 1910, 31: 945–970.

themselves. This is particularly the case with the more recent data over the whole range of temperature from o° to the critical temperature at about 374° Centigrade. Two remedies have been utilized to overcome this difficulty. First, the employment of separate equations of interpolation adjusted to fit the observations accurately over a short range of temperature, o° to 100° for example, as in the case of Broch's computations. (It has already been mentioned that theory requires the function for vapor pressures over ice to differ from the one for pressures over water, so that the values for ice offer no difficulty.) The second remedy sometimes employed consists in fitting any reasonably accurate equation as closely as possible to the observations. The differences between the observed and computed values are then charted and a smooth curve drawn by hand through the points thus located. This method has been employed notably by Henning¹ and others, using an empirical equation proposed by Thiesen.

For the purpose of these tables Marvin has found it possible from among a multitude of equations to develop a modification of the theoretical equation of Van der Waals which fits the whole range of observations much better than any hitherto offered and with an order of precision quite comparable to the data itself. In fact, the equation serves to disclose inconsistencies in the observations, more particularly between 50° and 80° C., which seem to suggest the need for further experimental determination of values possibly over the range between 0° and 100°.

Although it is not difficult to show, as Cederberg ² has done, that the simple form of general theoretical equation for all vapors developed by Van der Waals is inadequate to represent experiments on water vapor with sufficient accuracy for practical requirements, nevertheless a somewhat simple elaboration of its single constant suffices to remove this limitation in a very satisfactory manner.

The resulting equation is:

(1)
$$\log e = \log \pi - [A - bX + mX^2 - nX^3 + sX^4] \frac{\theta - T}{T}$$
, where $X = \frac{T - 453}{10}$.

The quantity within the square brackets in this equation replaces a single term of the Van der Waals equation which was regarded by him as a constant.

In Van der Waals's original equation π and θ are respectively the critical pressure and temperature (absolute). In the present state of physical science, and from the very nature of the data, these quantities cannot be evaluated exactly. Moreover it is unnecessary to do so for the mere purpose of accurately fitting a mathematical curve to the observational data,

¹ Annalen der Physik, 1907, 22: 609-630.

² Cederberg, Ivar W. Über eine exakte Dampfdruckberechnungsmethode. Physik. Zeitschr. xv: 697, 1914; Über die Temperaturabhängigkeit einiger physikalischen Eigenschaften des Wassers in seinen vershiedenen Aggregatzuständen. Physik. Zeitschr. xv: 824, 1914.

because the same result is attained by simply passing the curve through a point more accurately known and as near as may be to the critical point. This is equivalent to defining π and θ by an "equation of condition." Another "equation of condition" fixes the pressure at the boiling point which by definition must be 760 mm. From the considerations given on page xv computations are greatly facilitated by taking all temperatures on the approximate absolute scale represented by $T=273\times t^\circ$.

A careful preliminary analysis of the observational data in the vicinity of the critical temperature resulted in assigning values to θ and π as follows:

$$\theta = 643^{\circ}$$
, log. $\pi = 5.1959000$

It is emphasized here again that these data do not represent critical temperature conditions, but simply a convenient point on the pressure curve slightly below the critical temperature, the value of which is fixed with considerable accuracy by the observational data.

The value of the constant A was fixed by the equation of condition, e=760 mm. when T=373 (X=-8). The remaining constants (b, m, n, s) are computed by the method of least squares. The results are as follows:

A = 3.1473172 b = .00295944 m = .0004191398 n = .0000001829924s = .00000008243516

The number of significant figures in the constants is obviously greater than the accuracy of the data justifies, but is justified to facilitate computation and to secure accuracy in the interpolation of values which should themselves be as accurate as the data.

Observations of the pressure of aqueous vapor over ice have not been as numerous as those over water. Among the observations which have been used in recent times for the development of formulas to express the values of vapor pressures over ice there may be mentioned those of K. Scheel and W. Heuse ¹ at the Physikalisch-Technischen Reichsanstalt at Charlottenburg, those of W. Nernst ² at the Physikalisch-Chemischen Institut of the University of Berlin, and those of S. Weber ³ at the Physical Laboratory of the Uni-

¹ Scheel, K., and Heuse, W., op. cit., p. 1xi.

² Nernst, W. Verhandlungen der Deutschen Physikalischen Gesellshaft, vol. 11, no. 15, p. 313, Aug. 15, 1909.

Nernst, W. Kinetische Theorie fester Körper; Vorträge über die kinetische Theorie der Materie und der Elektrizität. B. G. Teubner.

³ Weber, S. Communications from the Physical Laboratory at the University of Leiden, no. 150; p. 37.

versity of Leiden. M. Thiesen, making use of the data of Scheel and Heuse, has developed a formula for vapor pressures over ice. This is given by the equation,

(2)
$$\log_{10} e = \log_{10} e_0 + 9.632(1 - 0.00035 t) \frac{t}{T}$$

where

$$e_0 = 4.5785$$
 and $T = 273 + t$,

the vapor pressures, e, being in millimeters and temperatures, t, in degrees Centigrade.

For convenience in computing this equation, for metric units it may be written

(3)
$$\log_{10} e = 0.66072 + \left(\frac{9.632 - 0.0033712 t}{273 + t}\right) t.$$

For English units the equation becomes

(4)
$$\log_{10} e_1 = \overline{1.255888} + \left(\frac{9.69193 - 0.00187289 t_1}{459.4 + t_1}\right) (t_1 - 32)$$

e = vapor pressure in millimeters.

 e_1 = vapor pressure in inches.

t =degrees Centigrade.

 $t_1 = \text{degrees Fahrenheit.}$

Although the Scheel and Heuse observations extended down to -67.9 C., the pressure readings between -60° C. and that temperature were not very accurate, being discarded by Thiesen ¹ in obtaining the constants in equation (2).

Nernst has made determinations of vapor pressure down to at least -50° C., good agreement being found with Scheel and Heuse's measurements. By making use of accurate determinations of the heat of vaporization of ice at o. C., and attributing the deviations of water vapor from the gas laws to the existence of double water molecules 2 Nernst with the collaboration of H. Levy has found for the vapor pressure over ice the formula

(5)
$$\log_{10} e = -\frac{2611.7}{T} + 1.75 \log_{10} T - 0.00210 T + 6.5343,$$
 where $e = \text{vapor pressure in mm. of mercury}$ and $T = 273.09 + t$ $t = \text{degrees Centigrade.}$

This formula has been checked by the accurate determinations of Weber the results of whose observations show good agreement with the values

Knudson, M. Annalen der Physik. Vierte Folge, Band 44, p. 536, 1914.

¹ Thiesen, M. Die Dampfspannung über Eis. (Mitteilung aus der Physikalisch—Technischen Reichsanstalt.) Annalen der Physik, vol. 29, p. 1057, 1909.

² Weber, S. Loc. cit., pp. 50-52.

calculated therefrom between the highest temperature at which he made observations, -22.75° C., and -96° C. Below the latter temperature the agreement does not appear so good. Comparisons between Weber's data and the values calculated by means of Thiesen's formula indicate that the latter formula most probably gives values which are slightly too high above -40° C., and slightly too low below that temperature.

Nernst 1 has also developed a more complicated formula than (5), making use of Pollitzer's quantum-formula for the specific heat of ice. The agreement with Weber's data in this case is not quite as good on the whole as in the case of equation (5), and therefore it is not given here.

More recently, E. W. Washburn 2 has developed a formula for the vapor pressure over ice, making use of Scheel and Heuse's, and Weber's observational data. Tables computed on the basis of this formula have been published in the Monthly Weather Review 2 and in the International Critical Tables.3 Formula (5) gives slightly better agreement with the Weber data than does the last formula referred to. Further determinations are necessary to settle the question as to the most representative equation, especially within the range of temperatures between $0^{\circ}C$, and $-20^{\circ}C$. Some work has been done by Holborn, Scheel, and Henning 4 to correct the values of Scheel and Heuse between 0° C. and -50° C.

Table 76 has been computed by means of Thiesen's formula (3), from 0° C. to -49.5 C. inclusive, and by means of Nernst's formula (5), from -50° C. to -70° C. inclusive.

The vapor pressures in the tables here given are expressed in standard manometric units.

TABLE 74.

Table 74. Pressure of aqueous vapor over ice. English measures.

The pressure, computed by equation (4) above, are given to 0.00001 inch for each degree of temperature from -60° to -15° , for each half degree from -15 to $\pm 0^{\circ}$, and for each tenth of a degree from $\pm 0^{\circ}$ 0 to +32°0.

TABLE 75.

Pressure of aqueous vapor over water. English measures.

This table has been computed by converting Table 77 into English units. The temperature argument is given for every 0°1 from 32°0 to 214°9 F. The vapor pressures are to 0.0001 inch from 32.0 to 130.9 F., and to 0.001 inch from 130°0 to 214°9 F.

¹ Nernst, W. Verhandlungen der Deutschen Physikalischen Gesellshaft, vol. 12, p. 568, 1910.

² Washburn, E. W. Monthly Weather Review, vol. 52, p. 488, 1924.

³ International Critical Tables, vol. III, p. 210, McGraw-Hill Book Company, 1928. ⁴ Holborn, L., Scheel, K., and Henning, F. "Wärmetabellen der Physikalisch-Technischen Reichsanstalt," Braunschweig, 1919.

TABLE 76. Pressure of aqueous vapor over ice. Metric measures.

The pressures, given to the nearest 0.0001 mm., are computed by Nernst's Formula (5), above, for each degree of temperature from -70° to -50° inclusive, and by Thiesen's Formula (3), above, for each half degree from $-49^{\circ}.5$ to -35° inclusive, and each tenth of a degree from $-36^{\circ}.0$ to $\pm 0.0^{\circ}.0$

TABLE 77.

TABLE 77. Pressure of aqueous vapor over water. Metric measures.

The pressures, computed by equation (1) above, are given for each tenth of a degree to 0.001 mm. from 0°0 to 59°9, and to 0.01 mm. from 50°0 to 100°9. They are given for each degree to 0.1 mm. from 100° to 189°, and in millimeters from 190° to 374°.

TABLE 78

TABLE 78. Pressure of aqueous vapor over ice. Dynamic measures.

The pressures given in Table 78, in millibars, have been obtained by multiplying the pressures given in Table 76, in millimeters, by 1.333224, the value of one millimeter in millibars (see page xxii). The values are given for each tenth of a degree between -70° C. and 0° C., inclusive. It may be noted as in the case of Table 76 that the values between temperatures -50° C. and -70° C. inclusive have been obtained by means of the Nernst Formula for the vapor pressure over ice (equation (5), p. lxiv), whereas the values between -50° C. and 0° C. have been obtained by means of the Thiesen Formula (equation (3), p. lxiv). Over the range of temperatures between -50° C. and -36° C., the values for tenths of degrees have been obtained by linear interpolation between whole degrees and half degrees.

TABLE 79.

Table 79. Pressure of aqueous vapor over water. Dynamic measures.

Similarly, the vapor pressures in Table 79, in millibars, have been obtained by multiplying the pressures given in Table 77 by 1.333224, and are given for each tenth of a degree between 0° C. and 44°9 C., inclusive.

TABLES 80, 81.

Table 80. Weight of a cubic foot of saturated aqueous vapor. English measures.

TABLE 81. Weight of a cubic meter of saturated aqueous vapor. Metric measures.

For many years it has been customary to assume that the specific gravity of water vapor relative to dry air is a constant whose theoretical value computed from the accurately known densities of its constituent gases is 0.6221. Direct experimental determinations of the specific volume of dry saturated steam (as yet but few observations are available at moderate temperatures) show conclusively (1) that this theoretical specific gravity is true only for saturated vapor at very low temperatures or when the vapor is in a very attenuated state of partial saturation; (2) that at increasingly higher temperatures the specific gravity is increasingly greater than 0.6221. These assertions are in accord with the values of weight per cubic foot of

water vapor tabulated by Marks & Davis ¹ from the most recent determinations of the specific volume of water vapor. However, owing to the paucity of data, and its inaccuracy for the range of atmospheric temperatures and conditions, the values derived from densities given by Marks and Davis between 10° and 50° are probably too low and require revision. The basis on which this assertion is made is the generalization that the theoretical value 0.6221 is probably a minimum specific gravity towards which actual values asymptotically tend at low temperature and low relative humidity in the meteorological sense, or high super heats in the steam engineering sense. This generalization affords a very helpful "control" in harmonizing and combining experimental determinations of specific volume. It was thus employed in a recomputation, from the original experimental data on specific volumes, of the accompanying table of specific gravities, d, of saturated water vapor.

$T. (C^{\circ})$	d	$T. (C^{\circ})$	d
- 60	0.6226	60	0.6273
50	0.6227	70	0.6283
40	0.6229	80	0.6296
30	0.6230	90	0.6311
20	0.6232	IOO	0.6329
- 10	0.6235	110	0.6351
± 0	0.6238	120	0.6377
+ 10	0.6241	130	0.6408
20	0.6246	140	0.6446
30	0.6251	150	0.6491
40	0.6257	160	0.6545
50	0.6264	170	0.6609
		180	0.6687

The weight of a cubic meter of saturated vapor is given by the expression

$$W = \frac{d \cdot \delta}{1 + \alpha t} \cdot \frac{e}{760},$$

 δ is the weight of a cubic meter of dry air (free from carbonic acid) at temperature o° C., and pressure of 760 millimeters of mercury of standard density under standard gravity: $\delta = 1.2928$ kg. (Bureau International des Poids et Mesures: Travaux et Mémoires, t. I, p. A 54.)

d is the density of aqueous vapor relative to dry air: d = 0.6221.

While, as stated above, there is reason for believing that this value is too low, for atmospheric temperatures the error is less than one per cent. For practical work in meteorology and at moderate temperatures, it seems best to retain the theoretical value until the actual value has been determined

¹ Marks, Lionel S., and Davis, Harvey N. Tables and diagrams of the thermal properties of saturated and superheated steam. New York, 1909.

with greater accuracy. For all important calculations except those at low temperatures the values of d in the Table on page lxvii should be employed.

e is the pressure of saturated aqueous vapor at temperature t, taken from Tables 76 and 77.

a is the coefficient of expansion of air for C° : $\alpha = 0.003670$.

t is the temperature in Centigrade degrees.

Whence we have

$$W ext{ (grams)} = {}^{1} 1.05821 \times \frac{e}{1 + 0.003670 t}$$

TABLE 81 is computed from this formula and gives the weight of saturated vapor in grams in a cubic meter for dew-points from -70° to $+40^{\circ}9$ C., the intervals from -35° to $40^{\circ}9$ C., being $0.^{\circ}1$ C. The tabular values are given to three decimals for temperatures above $-41^{\circ}5$, and to four decimal places for temperatures below $-41.^{\circ}5$.

The weight W_1 of a *cubic foot* of saturated vapor is obtained by converting the foregoing constants into English measures.

The weight of a cubic foot of dry air at temperature 32° F. and at a pressure of 760 mm. or 29.921 inches is

$$\delta_1 \text{ (grains)} = \frac{1292.78 \times 15.43235}{(3.280833)^3} = {}^2 564.94.$$

We have therefore,

$$W_1 \text{ (grains)} = \frac{\delta_1 d}{29.921} \times \frac{c_1}{1 + a_1(t_1 - 32^\circ)} = 11.7459 \frac{c_1}{1 + 0.002039(t_1 - 32^\circ)}$$

The temperature t_1 is expressed in degrees Fahrenheit; the vapor pressure e_1 , expressed in inches, is obtained from Tables 74 and 75.

TABLE 80 gives the weight of saturated aqueous vapor in grains per cubic foot for dew-points given to every degree from -30° to $+20^{\circ}$, to each half degree from $+20^{\circ}$ to $+70^{\circ}$, and for every 0.2 from 70.0 to 119.8 F., the values being computed to the thousandth of a grain.

REDUCTION OF OBSERVATIONS WITH THE PSYCHROMETER AND DETERMINATION OF RELATIVE HUMIDITY.

The psychrometric formula derived by Maxwell, Stefan, August, Regnault and others is, in its simplest form,

$$e = e' - AB(t - t'),$$

in which t = Air temperature.

t' = Temperature of the wet-bulb thermometer.

e =Pressure of aqueous vapor in the air.

e' = Vapor pressure, saturated, at temperature t'.

B = Barometric pressure.

A=A quantity which, for the same instrument and for certain conditions, is a constant, or a function depending in a small measure on t'.

¹ The latest adopted value of $\delta = 1.2028$ makes this factor 1.05822, and in a few cases, especially at high temperatures, increases W by 0.001 over the values given in Tables 81 and 80.

² 564.95 with $\delta = 1.2928$.

³ 11.7461 with $\delta = 1.2928$.

All pressures are expressed in heights of mercurial column under standard gravity.

The important advance made since the time of Regnault consists in recognizing that the value of A differs materially according to whether the wet-bulb is in quiet or moving air. This was experimentally demonstrated by the distinguished Italian physicist, Belli, in 1830, and was well known to Espy, who always used a whirled psychrometer. The latter describes his practice as follows: "When experimenting to ascertain the dew-point by means of the wet-bulb, I always swung both thermometers moderately in the air, having first ascertained that a moderate movement produced the same depression as a rapid one."

The principles and methods of these two pioneers in accurate psychrometry have now come to be adopted in the standard practice of meteorologists, and psychrometric tables are adapted to the use of a whirled or ventilated instrument.

The factor A depends in theory upon the size and shape of the thermometer bulb, largeness of stem and velocity of ventilation, and different formulæ and tables would accordingly be required for different instruments. But by using a ventilating velocity of three meters or more per second, the differences in the results given by different instruments vanish, and the same tables can be adapted to any kind of a thermometer and to all changes of velocity above that which gives sensibly the greatest depression of the wet-bulb temperature; and with this arrangement there is no necessity to measure or estimate the velocity in each case further than to be certain that it does not fall below the assigned limit.

The formula and tables here given for obtaining the vapor pressure and dew-point from observations of the whirled or ventilated psychrometer are those deduced by Prof. Wm. Ferrel (Annual Report Chief Signal Officer, 1886, Appendix 24) from a discussion of a large number of observations.

Taking the psychrometric formula in metric units, pressures being expressed in millimeters and temperatures in centigrade degrees, Prof. Ferrel derived for A the value

$$A = 0.000656 (1 + 0.0019 t').$$

In this expression for A, the factor depending on t' arises from a similar term in the expression for the latent heat of water, and the theoretical value of the coefficient of t' is 0.00115. Since it would require a very small change in the method of observing to cause the difference between the theoretical value and that obtained from the experiments, Prof. Ferrel adopted the theoretical coefficient 0.00115 and then recomputed the observations, obtaining therefrom the final value

$$A = 0.000660 (1 + 0.00115 t').$$

With this value the psychrometric formula in metric measures becomes

$$c = c' - 0.000660 B(t - t') (1 + 0.00115 t').$$

Expressed in English measures, the formula is

$$e = e' - 0.000367 B(t - t') [1 + 0.00064(t' - 32^{\circ})]$$

= $e' - 0.000367 B(t - t') \left(1 + \frac{t' - 32}{1571}\right)$

in which e = Vapor pressure in inches.

e' = Pressure of saturated aqueous vapor at temperature t'.

t = Temperature of the air in Fahrenheit degrees.

t' = Temperature of the wet-bulb thermometer in Fahrenheit degrees

B = Barometric pressure in inches.

TABLE 82.

Table 82. Reduction of Psychrometric Observations—English measures.

Values of
$$e = e' - 0.000367 B(t - t') \left(1 + \frac{t' - 32}{1571}\right)$$

This table provides for computing the vapor pressure, *e*, from observations of ventilated wet- and dry-bulb Fahrenheit thermometers. From the vapor pressure thus computed the dew-point and relative humidity of the atmosphere may be obtained.

The tabular values of the vapor pressure, e, are computed for degree intervals of t' from -20° to $+110^{\circ}$ F. Below $+10^{\circ}$ the interval for t-t' is 0.2, and above 10° the interval is 1°.

Corrections for barometric pressure. The computation has been made for B=30.0 inches, but at the bottom, and usually, also, at the top of each page of the table is given a correction, $\Delta e \times \Delta B$, computed for B=29.0 inches or $\Delta B=1$ inch, and for the value of t' indicated. The correction is a linear function of ΔB . For atmospheric pressures less than 30.0 inches, it is to be added to the tabular values of e, while for atmospheric pressures greater than 30.0 inches it is to be subtracted.

The values of e are given to 0.0001 inch for t' less than 10°, and to 0.001 inch for t' greater than 10°.

Examples:

- I. Given, $t=84^{\circ}3$; $t'=66^{\circ}7$, and B=30.00 inches. With $t'=66^{\circ}7$ and $t-t'=17^{\circ}6$ as arguments, Table 82 gives for e the value 0.462 inch. On page 182, for $t-t'=0^{\circ}0$ it is seen that a vapor presure of 0.462 inch corresponds to a temperature $t'=t=57^{\circ}$, which is the saturation, or dew-point temperature for the data given.
- 2. Given, $t=34^{\circ}5$; $t'=29^{\circ}4$; B=22.3 inches. With $t'=29^{\circ}4$ and $t-t'=5^{\circ}1$ as arguments, Table 82 gives for e the value 0.104. $\Delta B=30.0-22.3=7.7$, and $\Delta e\times \Delta B=0.0018\times 7.7=0.014$. Correct value of e

For t-t'=0° o a vapor pressure of 0.118 inch corresponds to a temperature t'=t=23° (see page 182), which is the saturation or dewpoint temperature for the data given.

TABLE 83. Relative humidity—Temperature Fahrenheit.

The table gives the vapor pressure corresponding to air temperatures from -30° to $+120^{\circ}$ at degree intervals (side argument) and for percentages of saturation at 10 per cent intervals (top argument). It is computed from the formula

$e = e_s \times \text{relative humidity}$,

where e_s is the saturation vapor pressure at the given air temperature. Below a temperature of 20° the values of e are given to 0.0001 inch; above 20° they are given to 0.001 inch.

Examples:

1. In dew-point example 1, above, the computed vapor pressure is 0.462 inch. Entering Table 83 with air temperature 84°3 as side argument, we obtain vapor pressure

o.356 inch = relative humidity 30 and

2. In dew-point example 2, above, the computed vapor pressure is 0.118 inch. Entering Table 83 with air temperature 34°5 as side argument, we obtain, vapor pressure

o.100 inch = relative humidity 50 and

0.118 inch - 0.100 inch = 0.018 inch = " " $\frac{90}{10}$ = 9 therefore, vapor pressure - 0.118 inch with t=34.5 F. = " " 59

Table 84. Reduction of Psychrometric Observations—Metric measures.

Values of
$$e = e' - 0.000660 B(t - t') (1 + 0.00115 t')$$

This table provides for computing the vapor pressure from observations of ventilated wet- and dry-bulb Centigrade thermometers. From the vapor pressure thus computed the dew-point and relative humidity of the atmosphere may be obtained.

The tabular values of the vapor pressure, e, are computed for degree intervals of t' from -30° to $+45^{\circ}$ C. Below $-5.^{\circ}$ 0 the interval for t-t' is $0.^{\circ}$ 1, and above $-5.^{\circ}$ 0 the interval is $1.^{\circ}$.

Corrections for barometric pressure. The computation has been made for B=760 mm. but on each page of the table is given a correction, $\Delta e \times \Delta B$, computed for B = 660, or $\Delta P = 100$ mm., and for the values of t' indicated. The correction is a linear function of ΔB . For atmospheric pressures less than 760 mm. it is to be added to the tabular values of e, while for atmospheric pressures greater than 760 mm. it is to be subtracted. The values of e are given to 0.001 mm. for t' less than -5° 0, and to 0.01 mm. for t' greater than -5° 0.

Example:

Given, $t=10^{\circ}4$ C.; $t'=8^{\circ}3$ C., and B=740 mm. With $t'=8^{\circ}3$ and t-t'=2° 1 as arguments, Table 84 gives for e the value 7.15 mm.

$$\Delta B = \frac{760 - 740}{100} = 0.2. \quad \Delta e \times \Delta B = 0.14 \times 0.2$$
 = 0.03.

Corrected value of e =7.18 mm.

For t-t'=0 a vapor pressure of 7.18 mm. corresponds to a temperature $t'=t=6^{\circ}3$ C., which is the saturation, or dew-point temperature for the data given.

TABLE 85. Relative humidity—Temperature Centigrade.

This table gives the vapor pressure corresponding to air temperatures from -45° C. to $+55^{\circ}$ C. at degree intervals (side argument) and for percentage of saturation at 10 per cent intervals (top argument). It is computed from the same formula as Table 83, namely,

$$e = e_s \times \text{relative humidity.}$$

Below a temperature of +5° o the values of e are given to 0.01 mm.; above 5°0 they are given to 0.1 mm.

Example:

In the dew-point example given above, the computed vapor pressure is 7.18 mm. Entering Table 85 with air temperature 10.4 as side argument, we obtain vapor pressure

$$7.18 - 6.6 = 0.58 \text{ mm.}$$
 = " " $\frac{60}{10} = 60$

therefore, vapor pressure

7.18 mm. with
$$t = 10.4$$
 $C. =$ " = 76

TABLE 85.

Rate of decrease of vapor pressure with altitude for mountain TABLE 86.

From hygrometric observations made at various mountain stations on the Himalayas, Mount Ararat, Teneriffe, and the Alps, Dr. J. Hann (Lehrbuch der Meteorologie Dritte Auflage, S. 230) has deduced the following empirical formula showing the average relation between the vapor pressure e_0 at a lower station and e the vapor pressure at another station at an altitude h meters above it:

$$\frac{e}{e_0} = 10^{-\frac{h}{6300}}.$$

This is of course an average relation for all times and places from which the actual rate of decrease of vapor pressure in any individual case may widely differ.

Table 86 gives the values of the ratio $\frac{e}{e_o}$ for values of h from 200 to 6000 meters. An additional column gives the equivalent values of h in feet.

REDUCTION OF SNOWFALL MEASUREMENT.

The determination of the water equivalent of snowfall has usually been made by one of two methods: (a) by dividing the depth of snow by an arbitrary factor ranging from 8 to 16 for snow of different degrees of compactness; (b) by melting the snow and measuring the depth of the resulting water. The first of these methods has always been recognized as incapable of giving reliable results, and the second, although much more accurate, is still open to objection. After extended experience in the trial of both these methods, it has been found that the most accurate and most convenient measurement is that of weighing the collected snow, and then converting the weight into depth in inches. The method is equally applicable whether the snow as it falls is caught in the gage, or a section of the fallen snow is taken by collecting it in an inverted gage.

Table 87. Depth of water corresponding to the weight of a cylindrical snow core, 2.655 inches in diameter.

This table is prepared for convenience in making surveys of the snow layer on the ground, particularly in the western mountain sections of the country. The weighing method is the only one found to be practicable. Present Weather Bureau practice is to take out a sample by means of a special tube, whose diameter, 2.655 inches, has been selected by reason of convenience in manipulation and simplicity in relation to the pound. Table 87 gives the depth of water in inches and hundredths corresponding to given weights. The argument is given in hundredths of a pound from 0.01 pound to 2.99 pounds.

TABLE 88. Depth of water corresponding to the weight of snow (or rain) collected in an 8-inch gage.

The table gives the depth to hundredths of an inch, corresponding to the weight of snow or rain collected in a gage having a circular collecting mouth 8 inches in diameter — this being the standard size of gage used throughout the United States.

The argument is given in hundredths of a pound from 0.01 pound to 0.99 pound. When the weight of the collected snow or rain is one pound or more, the depth corresponding to even pounds may be obtained from the equivalent of one pound given in the heading of the table.

Example:

The weight of the snow collected in a gage having a circular collecting mouth 8 inches in diameter is 3.48 pounds. Find the corresponding depth of water.

A weight of 3 lbs. corresponds to a depth of water of 1.65 in. 0.5507×3 , equals A weight of 0.48 lbs. corresponds to a depth of water of 0.26 A " " 3.48 " " 1.91 in

Quantity of rainfall corresponding to given depths.

This table gives for different depths of rainfall in inches over an acre the total quantity of water expressed in cubic inches, cubic feet, gallons, and tons. (See Henry, A. J. "Quantity of Rainfall corresponding to Given Depths." Monthly Weather Review, 1898, 26: 408-09.)

GEODETICAL TABLES.

Table 90. Value of apparent gravity on the earth at sea level.

The value of apparent gravity on the earth at sea level is given for every twenty minutes of latitude from 5° to 86°, and for degree intervals near the equator and the poles. It is computed to 0.001 dyne from the equation 2

 $g_{\phi} = 978.039 (1 + 0.005294 \sin^2 \phi - 0.000007 \sin^2 2 \phi)$ $= 980.621 (1 - 0.002640 \cos 2 \phi + 0.000007 \cos^2 2 \phi)$

in which g_{ϕ} is the value of the gravity at latitude ϕ .

The second form of the equation is the more convenient for the computation.

TABLE 91. Relative acceleration of gravity at sea level at different latitudes.

The formula adopted for the variation with latitude of apparent gravity at sea level is that of the U.S. Coast and Geodetic Survey, given above.

The table gives the values of the ratio $\frac{g_{\phi}}{g_{45^{\circ}}}$ to six decimals for every 10'

of latitude from the equator to the pole.

¹ Gravity is here considered in terms of force (expressed in dynes) that is exerted on a mass of one gram rather than its numerical equivalent, acceleration (expressed in centimeters and seconds), for which there is no convenient expression.

² See Bowie, William, Investigations of Gravity and Isostasy. U.S. Coast and Geodetic Survey, Special Publication No. 40, 1917, page 134.

LENGTH OF A DEGREE OF THE MERIDIAN AND OF ANY PARALLEL.

The dimensions of the earth used in computing lengths of the meridian and of parallels of latitude are those of Clarke's spheroid of 1866.¹ This spheroid undoubtedly represents very closely the true size and shape of the earth, and is the one to which nearly all geodetic work in the United States is now referred.

The values of the constants are as follows:

a, semi-major axis = 20926062 feet; $\log a$ = 7.3206875. b, semi-minor axis = 20855121 feet; $\log b$ = 7.3192127. $e^2 = \frac{a^2 - b^2}{a^2}$ = 0.00676866; $\log e^2$ = 7.8305030 - 10.

With these values for the figure of the earth, the formula for computing any portion of a quadrant of the meridian is

Meridional distance in feet = $[5.5618284] \Delta \phi$ (in degrees), - $[5.0269880] \cos 2 \phi \sin \Delta \phi$, + $[2.0528] \cos 4 \phi \sin 2 \Delta \phi$, in which $2\phi = \phi_2 + \phi_1$, $\Delta \phi = \phi_2 - \phi_1$; ϕ_1 , ϕ_2 = end latitudes of arc.

For the length of I degree, the formula becomes:

I degree of the meridian, in feet = $364609.9 - 1857.1 \cos 2 \phi + 3.94 \cos 4 \phi$. The length of the parallel is given by the equation I degree of the parallel at latitude ϕ , in feet =

I degree of the parallel at latitude ϕ , in feet = $365538.48 \cos \phi - 310.17 \cos 3 \phi + 0.39 \cos 5 \phi$.

Table 92. Length of one degree of the meridian at different latitudes.

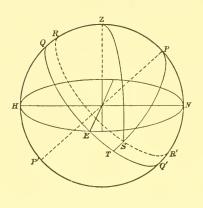
This gives for every degree of latitude the length of one degree of the meridian in statute miles to three decimals, in meters to one decimal, and in geographic miles to three decimals—the geographic mile being here defined to be one minute of arc on the equator. The values in meters are computed from the relation: I meter = 39.3700 inches. The tabular values represent the length of an arc of one degree, the middle of which is situated at the corresponding latitude. For example, the length of an arc of one degree of the meridian, whose end latitudes are 29° 30′ and 30° 30′, is 68.879 statute miles.

Table 93. Length of one degree of the parallel at different latitudes.

This table is similar to Table 92.

¹ Comparisons of Standards of Length, made at the Ordnance Survey Office, Southampton, England, by Capt. A. R. Clarke, R. E., 1866.

Table 94. Duration of sunshine at different latitudes for different values of the sun's declination.



Let Z be the zenith, and NH the horizon of a place in the northern hemisphere.

P the pole;

QEQ' the celestial equator;

RR' the parallel described by the sun on any given day;

S the position of the sun when its upper limb appears on the horizon;

PN the latitude of the place, ϕ .

ST the sun's declination, δ .

PS the sun's polar distance, $90^{\circ} - \delta$.

ZS the sun's zenith distance, z.

ZPS the hour angle of the sun from meridian, t.

r the mean horizontal refraction = 34' approximately.

s the mean solar semi-diameter = 16'

$$z = 90^{\circ} + r + s = 90^{\circ} 50'$$

In the spherical traingle ZPS, the hour angle ZPS may be computed from the values of the three known sides by the formula

$$\sin \frac{1}{2} ZPS = \sqrt{\frac{\sin \frac{1}{2} (ZS + PZ - PS) \sin \frac{1}{2} (ZS + PS - PZ)}{\sin PZ \sin PS}}$$

$$\sin \frac{1}{2} t = \sqrt{\frac{\sin \frac{1}{2} (z + \delta - \phi) \sin \frac{1}{2} (z - \delta + \phi)}{\cos \phi \cos \delta}}$$

or

The hour angle t, converted into mean solar time and multiplied by 2 is the duration of sunshine.

Table 94 has been computed for this volume by Prof. Wm. Libbey, Jr. It is a table of double entry with arguments δ and ϕ . For north latitudes northerly declination is considered positive and southerly declination as negative. The table may be used for south latitudes by considering southerly declination as positive and northerly declination as negative.

The top argument is the latitude, given for every 5° from 0° to 40°, for every 2° from 40° to 60°, and for every degree from 60° to 80°.

The side argument is the sun's declination for every 20' from S 23° 27' to N 23° 27'.

The duration of sunshine is given in hours and minutes.

To find the duration of sunshine for a given day at a place whose latitude is known, find the declination of the sun at mean noon for that day in the *Nautical Almanac*, and enter the table with the latitude and declination as arguments.

Example:

To find the duration of sunshine, May 18, 1892, in latitude 49° 30' North.

From the Nautical Almanac, $\delta = 19^{\circ}$ 43′ N., at Greenwich apparent noon. From the table, with $\delta = 19^{\circ}$ 43′ N. and $\phi = 49^{\circ}$ 30′, the duration of sunshine is found to be 15^{h} 31^m.

Table 95. Declination of the sun for the year 1899, at Greenwich apparent noon.

This table is an auxiliary to Table 94, and gives the declination of the sun for every third day of the year 1899. These declinations may be used as approximate values for the corresponding dates of other years when the exact declination cannot readily be obtained. Thus, in the preceding example, the declination for May 18, 1892, may be taken as approximately the same as that for the same date in 1899, viz. 19° 34′.

THE DURATION OF TWILIGHT.

A review of the literature ¹ indicates that from an early date astronomical twilight has been considered to end in the evening and begin in the morning when the true position of the sun's center is 18° below the horizon. At this time stars of the sixth magnitude are visible near the zenith, and generally there is no trace on the horizon of the twilight glow.

It also appears that *civil* twilight ends in the evening and begins in the morning when the true position of the sun's center is 6° below the horizon. At this time stars and planets of the first magnitude are just visible. In the evening the first purple light has just disappeared, and darkness compels the suspension of outdoor work unless artificial lighting is provided. In the morning the first purple light is beginning to be visible, and the illumination is sufficient for the resumption of outdoor occupations.

Some confusion has arisen in the computation of tables of the duration of both astronomical and civil twilight, due to the fact that in some instances the time of sunrise or sunset has been considered to be that instant when the *center* of the sun is on the true horizon; in others, when its center *appears* to be on the true horizon; and in still others when the *upper limb* of the sun appears to coincide with the true horizon. In the United States this latter is regarded as defining the time of sunrise and sunset.

In the tables here presented the duration of astronomical twilight is the interval between sunrise or sunset, according to this latter definition, and the instant the true position of the sun's center is 18° below the horizon. Likewise, the duration of civil twilight is the interval from sunrise or sunset to the instant the true position of the sun's center is 6° below the horizon.

¹ Kimball, Herbert H. "Duration and Intensity of Twilight," *Monthly Weather Review* 1916, 44: 614-620.

The computations may be made from the equation

$$\cos t = \frac{\sin a - \sin \phi \sin \delta}{\cos \phi \cos \delta}$$

where t is the sun's hour angle from the meridian, a is the sun's altitude, considered minus below the horizon, δ is the solar declination, and ϕ is the latitude of the place of observation.

The solar declinations employed are those given in the American Ephemeris and Nautical Almanac, 1899, pp. 377–384, Solar Ephemeris for Washington.

The atmospheric refraction with the sun on the horizon has been assumed to be 34', and 16' has been allowed for the sun's semi-diameter, so that at the instant of sunrise or sunset, as defined above, the true position of the sun's center is about 50' below the horizon. The difference between this value of t and its value with the sun 6° and 18° below the horizon gives, respectively, the duration of civil and astronomical twilight.

The computations have been simplified by the use of Ball's Altitude Tables, from which the value of t has been determined for true altitudes of the sun of -50', -6° , and -18° .

TABLE 96. Duration of astronomical twilight.

TABLE 96.

The duration of astronomical twilight is given to the nearest minute for the 1st, 11th, and 21st day of each month for north latitudes, 0°, 10°, 20°, 25°, and at 2° intervals from 30° to 50°, inclusive. The absence of data for latitude 50° from June 1 to July 11, inclusive, indicates that between these dates at this latitude astronomical twilight continues throughout the night.

TABLE 97. Duration of civil twilight.

TABLE 97.

The duration of civil twilight is given to the nearest minute for the 1st, 11th and 21st day of each month for north latitudes 0°, 10°, 20°, 25°, and at 2° intervals from 30° to 50°, inclusive.

RELATIVE INTENSITY OF SOLAR RADIATION AT DIFFERENT LATITUDES.

TABLE 98.

Table 98. Mean intensity for 24 hours of solar radiation on a horizontal surface at the top of the atmosphere.

This table is that of Prof. Wm. Ferrel, published in the *Annual Report* of the Chief Signal Officer, 1885, Part 2, p. 427, and computed from formulæ and constants given in Chapter II of the above publication, pages 75 to 82. It gives the mean intensity, *J*, for 24 hours of solar radiation received by a horizontal surface at the top of the atmosphere, in terms of the mean solar

¹ Ball, Frederick. Altitude Tables for let. 31° to 60°. London, 1907; [same] for lat. 0° to 30°, London, 1910.

constant A_o , for each tenth parallel of latitude of the northern hemisphere, and for the first and sixteenth day of each month; also the values of the solar constant A in terms of A_o , and the longitude of the sun for the given dates.

Table 99. Relative amounts of solar radiation received on a horizontal surface during the year at different latitudes.

The second column of this table is obtained from the last line of Table 98 by multiplying by 1440, the number of minutes in 24 hours. It therefore gives the average daily amount of radiation that would be received from the sun on a horizontal surface at the surface of the earth if none were absorbed or scattered by the atmosphere, expressed in terms of the mean solar constant. The following columns give similar data, except that the atmospheric transmission coefficient is assumed to be 0.9, 0.8, 0.7 and 0.6, respectively, and have been computed by utilizing Angot's work (Recherches théoretiques sur la distribution de la chaleur à la surface du globe, par M. Alfred Angot, Annales du Bureau Central Météorologique de France, Année 1883. v. 1. B 121-B 169), which leads to practically the same values as Ferrel's when expressed in the same units.

The vertical argument of the table is for 10° intervals of latitude from the equator to the north pole, inclusive.

Table 100. Air mass, m, corresponding to different renith distances of the sun.

For homogenous rays, the intensity of solar energy after passing through an air mass, m, is expressed by the equation $I = I_o a^m$, where I_o is the intensity before absorption, a is the atmospheric transmission coefficient, or the proportion of the energy transmitted by unit air mass, and m is the air mass passed through. If we take for unit air mass the atmospheric mass passed through by the rays when the sun is in the zenith, then for zenith distances of the sun less than 80° the air mass is nearly proportional to the secant of the sun's zenith distance. In general, the secant gives air masses that are too high by an increasing amount as the zenith distance of the sun increases.

The equation by which air masses are sometimes computed is $m = \frac{atmospheric\ refraction}{K\sin Z}$

where Z is the sun's zenith distance and K is a constant. The uncertain factor in this equation is the atmospheric refraction. Table 100 gives values of m computed by Bemporad ($Rend.\ Acc.\ Lincei.$, Roma, Ser. 5, V. 16, 2 Sem. 1907, pp. 66–71) from the above formula, using for K the value 58''.36. The argument is for each degree of Z from 20° to 89°, with values of m added for $Z=0^\circ$, 10°, and 15°. The values of m are given to two decimal places.

TABLE 101. Relative illumination intensities.

TABLE 101.

The table gives illumination intensities in foot-candles for zenithal sun, sky at sunset, sky at end of civil twilight, zenithal full moon, quarter moon, and starlight, and the ratio of these intensities to the illumination from the zenithal full moon. For the sources of the data see Kimball, Herbert H., "Duration and Intensity of Twilight," Monthly Weather Review, 1916, 44:614-620.

MISCELLANEOUS TABLES.

WEIGHT IN GRAMS OF A CUBIC CENTIMETER OF AIR.

The following tables (102 to 107) give the factors for computing the weight of a cubic centimeter of air at different temperatures, humidities and pressures.

$$\delta = \frac{0.0012930}{1 + 0.00367 t} \left(\frac{B - 0.378 e}{760} \right)$$

in which δ is the weight of a cubic centimeter of air expressed in grams, under the standard value of gravity (g=980.665)

B is the atmospheric pressure in millimeters, under standard gravity;

e is the pressure of aqueous vapor in millimeters, under standard gravity;

t is the temperature in Centigrade degrees.

For dry atmospheric air (containing 0.0004 of its weight of carbonic acid) at a pressure of 760 mm. and temperature o° C., the absolute density, or the weight of one cubic centimeter, is 0.0012930 gram. See p. xlvi.

The weight of a cubic centimeter may also be written as follows:

$$\delta = \frac{0.0012930}{1 + 0.002039(t - 32^{\circ})} \left(\frac{B - 0.378 e}{29.921} \right)$$

where δ is defined as before, but B and c are expressed in inches and t in Fahrenheit degrees. Thus by the use of tables based on these two formulæ, lines of equal atmospheric density may be drawn for the whole world, no matter whether the original observations are in English or metric measures.

ENGLISH MEASURES.

TABLES 102, 103, 104.

Table 102. Temperature Term.

This table gives the values and logarithms of the expression

$$\delta_{t, 29.921} = \frac{0.0012930}{1 + 0.002039 (t - 32^{\circ})}$$

for values of t extending from -45° F. to $+140^{\circ}$ F., the intervals between 0° F. and 110° F. being 1° .

The tabular values are given to five significant figures.

Table 103. Term for humidity; auxiliary to Table 102.

TABLE 104. Humidity and pressure term.
$$\frac{h}{29.921} = \frac{B - 0.378 \text{ e}}{29.921}$$

TABLE 103 gives values of 0.378 e to three decimal places as an aid to the use of Table 104. The argument is the dew-point given for every degree from $-60^{\circ} F$. to $+140^{\circ} F$. The second column gives the corresponding values of the vapor pressure (e) derived from Tables 74 and 75.

TABLE 104 gives values and logarithms of $\frac{h}{29.921} = \frac{B - 0.378 \, e}{29.921}$ for values of h extending from 10.0 to 31.7 inches. The logarithms are given to five significant figures and the corresponding numbers to four decimals.

Example:

The air temperature is 68° F., the pressure is 29.36 inches and the dewpoint 51° F. Find the logarithm of the density.

Table 102, for
$$t = 68^{\circ} F$$
., gives 7.08085 – 10
Table 103, for dew-point 51°, gives 0.378 $e = 0.142$ inch,
Table 104, for $h = B - 0.378$ $e = 29.36 - 0.14 = 29.22$, gives 9.98941 – 10
Logarithm of density = $\frac{30}{7.07056 - 10}$

METRIC MEASURES.

Table 105. Temperature term.

This table gives values and logarithms of the expression

$$\delta_t, \,_{760} = \frac{0.0012930}{1 + 0.00367} \, t$$

for values of t extending from $-34^{\circ}C$, to $+69^{\circ}C$. The tabular values are given to five significant figures.

TABLE 106. Term for humidity; auxiliary to Table 107.

TABLE 107. Humidity and pressure terms.
$$\frac{h}{760} = \frac{B - 0.378 e}{760}$$
.

Table 106 gives the values of 0.378 e to hundredths of a millimeter for dew-points extending from -50° C. to $+60^{\circ}$ C. Above -25° C. the interval is one degree. The values of the vapor pressure, e, corresponding to these dew-points, given in the second column, are taken from tables 76 and 77.

Table 107 gives values and logarithms of
$$\frac{h}{760} = \frac{B - 0.378 e}{760}$$
 for

values of h extending from 300 to 799 mm. The atmospheric pressure B is the barometer reading corrected for gravity and 0.378 e is the term for humidity obtained from Table 106. The logarithms are given to five significant figures and the corresponding numbers to four decimal places.

TABLE 108. Atmospheric water-vapor lines in the visible spectrum.

Table 108, prepared by the Astrophysical Observatory at Washington, gives a summary of lines in St. John's (1928) revision of Rowland's "Preliminary Table of Solar Spectrum Wave Lengths," recorded as of atmospheric water vapor origin. There are more than 400 such lines in Rowland's table, but an abridgment is here made as follows:

Only lines of intensity "I" or greater are here separately given, but the total number and average intensity of the fainter lines lying between these are inserted. The scale of intensities is such that a line of intensity "I" is "just clearly visible" on Rowland's map; the H and K lines are of intensity, I,000; D_1 (the sodium line of greater wave length), 20; C_2 , 40. "Lines more and more difficult to see" are distinguished by 0, -1, -2, and -3.

TABLE 109.

TABLE 109. Atmospheric water-vapor bands in the infra-red spectrum.

The values of Table 109 relate to the transmission of energy in the minima of various water-vapor bands, when there is I cm. of precipitable water in the path through the air. For other amounts of water-vapor, the depths of these minima may be taken as equal to a^{δ} , where a is the coefficient taken from the third column of Table 109 and δ is the amount of precipitable water in cm. in the path. For average conditions in the transmission of radiation through the atmosphere, δ may be determined by the modification of Hann's formula $\delta = 2.0 e$ sec. Z, where e is the vapor pressure in cms. as determined by wet and dry thermometers and Z is the angle which the path makes with the vertical.

For the use of the transmissions observed in such bands for the inverse process of determining the amount of water-vapor in the atmosphere, see Fowle, *Astrophysical Journal*, 35, p. 149, 1912; 37, p. 359, 1913.

TABLE 110.

Table 110. Transmission percentages of radiation through moist air.

The values of Table 110 will be of use when the transmission of energy through the atmosphere containing a known amount of water-vapor is under consideration. An approximate value for the energy transmitted may be had if the amount of energy from the source between the wavelengths of the first column is known and is multiplied by the corresponding transmission coefficients of the subsequent columns of the table. The table is compiled from Fowle, "Water-vapor Transparency," *Smithsonian Miscellancous Collections*, 68, No. 8, 1917; see also, Fowle, "The Transparency of Aqueous Vapor," *Astrophysical Journal*, 42, p. 394, 1915.

TABLE 111

TABLE 111. The spectral distribution of solar radiation and its transmission by the atmosphere.

The measured relative intensity of radiation at a given wave length depends not only upon the source, but also upon the prismatic dispersion.

Usually, a dispersion coefficient is used to reduce the intensities to what they would have been had the dispersion been the same at all wave lengths, but in Table III it is that of the ultra-violet glass prism employed by the Astrophysical Observatory of the Smithsonian Institution in making Solar radiation measurements. Column I gives the deviation from ω_1 in minutes of arc at which the energy was measured. Column 2 gives the corresponding wave length. Column 3 gives transmission coefficients, $a_{a\lambda}$, for pure dry air at 760 mm. pressure, with the sun in the zenith. They have been computed by means of Rayleigh's equation as modified by King. Fowle's values of $a_{w\lambda}$, the transmission coefficient for that amount of atmospheric water vapor which if precipitated would produce a layer of water one centimeter thick, have been employed to compute the transmission of solar radiation through moist air. Column 5 gives what Abbot considers the most reliable value for the relative energy outside the atmosphere, $e_{0\lambda}$, at the wave lengths corresponding to the deviations of Column I.

The data in the upper part of Columns 6, 7, and 8 have been computed by means of the factors shown in their respective headings. They give the energy distribution with the sun in the zenith and atmospheric pressure of 760 mm., column 6 with no moisture present, and columns 7 and 8 with sufficient moisture to produce a layer of water 1.0 cm. and 2.0 cm. thick, respectively, if precipitated.

Fowle 4 has shown that for average conditions the precipitable water in the atmosphere above a given place may be approximately determined from the equation w=2.3 e to $\frac{-h}{22000}$, where e is the surface water vapor pressure in centimeters and h is the altitude of the place above sea level, in meters. The Aerological Division of the U. S. Weather Bureau is developing equations that more accurately express the relation between surface vapor pressure and the water-vapor content of the atmosphere, utilizing for this purpose its valuable accumulation of free-air data. It's results, which are approaching completion, will probably be published in the Monthly Weather Review during the current year.

Similarly, the data in the upper part of columns 9 and 10 have been computed for the sun at zenith distances 60 and 70.7 degrees, and the moisture content of the atmosphere equivalent to 1.0 cm., and 3.0 cm., of precipitable water, respectively.

¹ King, Louis Vessot. On the scattering and the absorption of light in gaseous media with applications to the intensity of sky radiation. Phil. Trans. Roy. Soc., London, A. 212, p. 375, 1919.

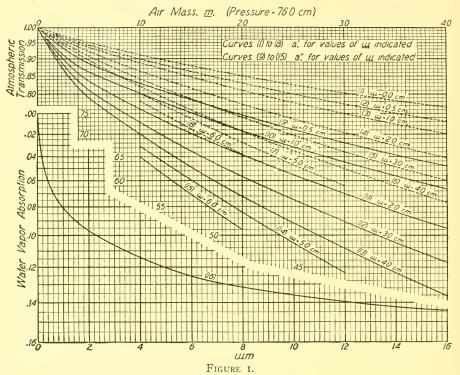
² Fowle, F. E. Water vapor transparency to low-temperature radiation. Smithsonian Misc. Coll., vol. 68, no. 8, 1917.

³ Abbot, C. G., and others. The distribution of energy in the spectrum of the sun and stars. Smithsonian Misc. Coll., vol. 74, no. 7, 1923.

⁴ Fowle, F. E. Atmospheric transparency for radiation. Monthly Weather Review, vol. 42, pp. 2-4, 1914.

These computations take account of the depletions of solar radiation by scattering only. We now proceed to compute the energy in the total solar spectrum after passing through dust-free air containing the amounts of atmospheric moisture specified, and with the sun at the distances from the zenith indicated.

The wave lengths given in column 2 do not cover the entire range of wave lengths included in the solar spectrum. It is therefore necessary to apply a correction to the measured energy so as to include the energy not



measured. Abbot's ¹ method of determining these corrections has been followed in computing the corrections for u. v. (ultra-violet) and i. r. (infra-red) energy not measured, which are given in the lower part of Table III. The absorption by water vapor in the great water vapor bands in the infra-red (w. v. absorption) had been computed by the method developed by Fowle.² Finally, Fowle has computed for this table the absorption by the permanent gases of the atmosphere.

The relative energy in different parts of the solar spectrum may now be determined by summing up the energies at different wave lengths, giving

¹ Abbot, C. G. Smithsonian Solar Researches. Gerland's Beitrage zur Geophysik, Bd. XVI, Heft 4, pp. 344-353, 1927.

² Fowle, F. E. Water vapor transparency to low-temperature radiation. Smithsonian Misc. Coll., vol. 68, no. 8, 1917.

double weight to those 10' in deviation apart. It will be noted that the summation includes the following spectral bands, namely, below 0.346μ , between 0.346 and 0.405μ , between 0.405 and 0.704μ , and above 0.704μ ; or the short-wave ultra violet, the long-wave ultra violet, the visible radiation, and the infra-red radiation. The percentage of the energy included in each of these sections to the total energy is given, and the percentage of the total to the total before it enters the atmosphere, or the atmospheric transmission corresponding to the conditions as specified, is also given.

By means of computations such as are given in Table III the curves of Figure I, showing the depletion by scattering in passing through dry air, curve I, and through air containing different amounts of moisture, curves 2 to 8, and the depletion by both scattering and absorption, curves 9-15, have been constructed. The ordinates give atmospheric transmission; the abscissas, air masses, m, corresponding to zenith distances of the sun 0°, 60°, 70.7°, and 75.7°. The values for m less than I represent depletions at elevations above sea level.

For a more complete description of this figure see the Monthly Weather Review, 55: 167, 1927, and 56: 394, 1928, and 58: 43, 1930.

Abbot's correction for u. v. radiation below 0.346μ , which is not measured, includes the radiation absorbed at these wave lengths by an average amount of atmospheric ozone, but does not take account of variations in the ozone content of the atmosphere. Fowle has shown that the absorption by ozone in the visible spectrum varies in amount with both time and place, and that it causes a depletion of solar radiation by about 0.2 to 0.4 per cent of the solar constant. This depletion has not been included in "Absorption by permanent gases," near the bottom of Table 112. The values of atmospheric transmission in the last line of the table are therefore too high by from 0.2 to 0.4 per cent, more or less, depending upon the ozone absorption in the visible spectrum, and disregarding the possible error, probably small in amount, due to variations in the ozone absorption in the ultra-violet.

Example of the use of Figure 1. The atmospheric pressure is 76.0 cm., the water vapor pressure 0.87 cm., the zenith distance of the sun is 60° (m=2.0), and the elevation of the station is only slightly above sea level. The

precipitable water= $2.3 \times 0.87 \times 10^{\frac{-n}{22000}}$ =2.0 cm. From Figure 1 the transmission read from curve 11, for m=2, is 0.653.

Table 112. International meteorological symbols.

TABLE 112.

The information under this heading has been compiled for the present edition by the librarian of the United States Weather Bureau, and represents current practice in the use of the symbols approved by the International Meteorological Organization. For further information on the sub-

¹ Fowle, F. E. Atmospheric ozone: Its relation to some solar and terrestrial phenomena. Smithsonian Misc. Coll., vol. 81, No. 11, 1929.

ject of meteorological symbols, see *Monthly Weather Review* (Wash., D. C.), May, 1916, pp. 265-274.

TABLE 113. International Cloud Classification.

In the "International Atlas of Clouds and of State of the Sky, Abridged edition for the use of Observers, Paris, 1930," the Commission of the International Meteorological Committee for the Study of Clouds has proposed a classification of clouds under Families A, B, C, and D, Forms a, b, and c, and Genera I to 10 inclusive. But since the definitions of most of these latter differ but little from those given in the International Cloud Atlas, 2d edition, Paris. 1910, and since the new Atlas has not yet been generally accepted, the well known definitions of the older Atlas are adhered to in Table 113.

TABLE 114. Beaufort weather notation.

This table has been revised in the library of the United States Weather Bureau, and represents the current practice of American and British observers in the use of the Beaufort letters.

TABLE 115. International code for horizontal visibility.

The code for horizontal visibility is used by a large number of Nations and was adopted by the International Commission for Air Navigation. Reference: Convention relating to the Regulation of Aerial Navigation dated October 13, 1919; corrected text of May 1929. The seat of the Commission and of its permanent Secretariat has been fixed at No. 20 Avenue Kléber, Paris.

TABLE 116. List of meteorological stations.

This list has been extensively revised, mainly by large additions for the continents of South America, Asia, and Africa. It includes stations for which data appear in the "Réseau Mondial" of the British Meteorological Office for 1922 (published 1929), which were selected to represent, as far as available data permitted, the meteorology of all land areas of the globe, on the basis of two, or in some cases three, stations for each ten-degree square of latitude and longitude. Many additional stations are included for some countries, and especially for the United States.

No attempt has been made in this edition of the Smithsonian Tables to indicate the "order" of the several stations, according to the definitions adopted at the Vienna Congress of 1873; as, owing to the present wide-spread use of self-recording instruments, the old distinction between first and second order stations has lost much of its importance.

Several stations included in the list are no longer in operation. Data concerning the locations and altitudes of these stations are still valuable, in view of the frequent use made of their records in meteorological and climatological studies.

In general, the established English spellings of geographical names in foreign countries have been followed. Where no English name was established, native orthography has been followed.

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Centigrade scale to Fahrenheit		Table 3
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TABLE 1.

APPROXIMATE ABSOLUTE, CENTIGRADE, FAHRENHEIT, AND REAUMUR

SCALES.

Conversion Formulæ for Approximate Absolute (A.A), Centigrade (C), Fahrenheit (F), and Reaumur (R) Scales.

1 1 1	(F), and Readmur (K) Scales.											
$A.A = 5/9 (F - 3^2) + 273 = C + 273 = 5/4 R + 273$												
								$\left(1+\frac{1}{2}\right)$	+-1	$+\frac{1000}{1}$	+)	
		/5C + 32										
		/9 (F - 1)					3/ 1 32 -	- 20 (10/	1 32		
	N — 4,	/9 (F — ,	32) — 4/	· 5 C — .	1 5 (-1	1 - 273)						
	,			PI	ROPORTIO	ONAL PAR						
A.A) 1		3		4	5	6	7			9	
F R					.2	9 C 4.0	10.8 4.8	12.6 5.6	14. 6.	•	.2	
F	' I	2		,	4	5	6	7		3 (
C	٦.	5* 1.1			.22*	2.77*	3.33*	3.88*			00*	
A.A)	.4* .8			.77*	2.22*	2.66*	3.11*			00*	
 R				,	4	5	6	7	. 8	9		
C	1		3. ₁			5 6.25	7.50	8.75	10.	,	.25	
A.A F)	-				_	13.50	15.75	18.		.25	
				* These	last figure	s repeated	indefinitel	٧.				
A.A.	c.	F.	R.	A.A.	c.	F.	R.	A.A.	c.	F.	R.	
375°	102°	215.6	81°.6	350°	77°	170°.6	61.6	325°	52°	125°.6	41°.6	
374	101	213.8	80.8 80.0	349 348	76	168.8	60.8 60.0	324	51	123.8	40.8	
373 372	99	210.2	79.2	347	75 74	165.2	59.2	323 322	50 49	I 20.2	40.0 39.2	
371	98	208.4	78.4	346	73	163.4	58.4	321	48	118.4	38.4	
370 360	97 06	206.6	77.6 76.8	345 344	72 71	161.6 150.8	57.6 56.8	320 310	47 46	116.6 114.8	37.6 36.8	
368	95	203.0	76.0	343	70	158.0	56.0	318	45	113.0	36.0	
367 366	94 93	201.2 100.4	75.2 74.4	342 341	69 68	156.2 154.4	55.2 54.4	317 316	44 43	111.2	35·2 34·4	
365	02	197.6	73.6	340	67	152.6	53.6	315	42	107.6	33.6	
364	91	195.8	72.8	339	66	150.8	52.8	314	41	105.8	32.8	
363 362	90 80	194.0	72.0 71.2	338 337	65 64	140.0 147.2	52.0 51.2	313 312	40 39	104.0	32.0	
361	88	190.4	70.4	336	63	145.4	50.4	311	38	100.4	30.4	
360	87	188.6	69.6	335	62	143.6	49.6	310	37	98.6	29.6	
359	87 86 85	188.6 186.8 185.0	69.6 68.8 68.0	334	62 61 60	143.6 141.8 140.0	49.6 48.8 48.0	310 309 308	36	98.6 96.8 95.0	29.6 28.8 28.0	
359 358 357	86 85 84	186.8 185.0 183.2	68.8 68.0 67.2	334 333 332	61 60 59	141.8 140.0 138.2	48.8 48.0 47.2	309 308 307	36 35 34	96.8 95.0 93.2	28.8 28.0 27.2	
359 358 357 356	86 85 84 83	186.8 185.0 183.2 181.4	68.8 68.0 67.2 66.4	334 333 332 331	61 60 59 58	141.8 140.0 138.2 136.4	48.8 48.0 47.2 46.4	309 308 307 306	36 35 34 33	96.8 95.0 93.2 91.4	28.8 28.0 27.2 26.4	
359 358 357 356 355	86 85 84	186.8 185.0 183.2 181.4	68.8 68.0 67.2	334 333 332	61 60 59	141.8 140.0 138.2	48.8 48.0 47.2	309 308 307	36 35 34	96.8 95.0 93.2 91.4 89.6 87.8	28.8 28.0 27.2	
359 358 357 356 355 354 353	86 85 84 83 82 81 80	186.8 185.0 183.2 181.4 179.6 177.8 176.0	68.8 68.0 67.2 66.4 65.6 64.8 64.0	334 333 332 331 330 329 328	61 60 59 58 57 56 55	141.8 140.0 138.2 136.4 134.6 132.8 131.0	48.8 48.0 47.2 46.4 45.6 44.8 44.0	309 308 307 306 305 304 303	36 35 34 33 32 31 30	96.8 95.0 93.2 91.4 89.6 87.8 86.0	28.8 28.0 27.2 26.4 25.6 24.8 24.0	
359 358 357 356 355 354	86 85 84 83 82 81	186.8 185.0 183.2 181.4 179.6 177.8	68.8 68.0 67.2 66.4 65.6 64.8	334 333 332 331 330 329	61 60 59 58 57 56	141.8 140.0 138.2 136.4 134.6 132.8	48.8 48.0 47.2 46.4 45.6 44.8	309 308 307 306 305 304	36 35 34 33 32 31	96.8 95.0 93.2 91.4 89.6 87.8	28.8 28.0 27.2 26.4 25.6 24.8	
359 358 357 356 355 354 353 352	86 85 84 83 82 81 80	186.8 185.0 183.2 181.4 179.6 177.8 176.0 174.2	68.8 68.0 67.2 66.4 65.6 64.8 64.0 63.2	334 333 332 331 330 329 328 327	61 60 59 58 57 56 55 54	141.8 140.0 138.2 136.4 134.6 132.8 131.0 129.2	48.8 48.0 47.2 46.4 45.6 44.8 44.0 43.2	309 308 307 306 305 304 303 302	36 35 34 33 32 31 30 29	96.8 95.0 93.2 91.4 89.6 87.8 86.0 84.2	28.8 28.0 27.2 26.4 25.6 24.8 24.0 23.2	

TABLE 1

APPROXIMATE ABSOLUTE, CENTICRADE, FAHRENHEIT, AND REAUMUR

SCALES.

A.A.	c.	F.	R.	A.A.	c.	F.	R.	A.A.	C.	F.	R.
300°	27°	80°.6	21°.6	250°	-23°	- 9°4	-18.°4	200°	-73°	- 99.4	-58.4
299	26	78.8	20.8	249	24	11,2	19.2	199	74	101.2	59.2
298	25	77.0	20.0	248	25	13.0	20.0	198	75	103.0	60.0
297	24	75.2	10.2	247	26	14.8	20.8	197	76	104.8	60.8
296	23	73.4	18.4	246	27	16.6	21.6	196	77	106.6	61.6
295	22	71.6	17.6	245	-28	-18.4	-22.4	195	-78	-108.4 110.2	-62.4 63.2
294	2 I 20	69.8 68.0	16.8	244	29	20.2	23.2	194	79 80	112.0	64.0
293	10	66.2	15.2	243	30 31	23.8	24.8	193	81	113.8	64.8
291	18	64.4	14.4	241	32	25.6	25.6	191	82	115.6	65.6
290	17	62.6	13.6	240	-33	-27.4	-26.4	190	-83	-117.4	-66.4
280	16	60.8	12.8	239	34	20.2	27.2	189	84	119.2	67.2
288	15	59.0	12.0	238	35	31.0	28.0	188	85	121.0	68.0
287	14	57.2	11.2	237	36	32.8	28.8	187	86	122.8	68.8
286	13	55.4	10.4	236	37	34.6	29.6	186	87	124.6	69.6
285	I 2	53.6	9.6	235	-38	-36.4	-30.4	185	-88	-126.4	-70.4
284	II	51.8	8.8	234	39	38.2	31.2	184	89	128.2	71.2
283	10	50.0	8.0	233	40	40.0	32.0	183 182	90	130.0	72.0
282	9	48.2 46.4	7.2 6.4	232 231	4I 42	41.8	32.8 33.6	181	91	133.6	73.6
	-							100	00	725 4	-74.4
280	7 6	44.6	5.6 4.8	230	-43	-45.4	-34.4	170	-93 94	-135.4 137.2	75.2
279	5	42.8	4.0	229	44 45	47.2	35.2 36.0		95	139.0	76.0
277	4	39.2	3.2	227	45	50.8	36.8		95	140.8	76.8
276	3	37.4	2.4	226	47	52.6	37.6		97	142.6	77.6
275	+ 2	35.6	+ 1.6	225	-48	-54.4	-38.4	175	-98	-144.4	-78.4
274	+ 1	33.8	+ 0.8	224	49	56.2	39.2	174	99	146.2	79.2
273	士。	32.0	± 0.0	223	50	58.0	40.0		100	148.0	80.0
272	- I	30.2	- 0.8	222	51	59.8	40.8		101	149.8	80.8
271	- 2	28.4	- 1.6	221	52	61.6	41.6	171	102	151.6	81.6
270	- 3	26.6	- 2.4	220	-53	-63.4	-42.4	170	-103	-153.4	-82.4
269	4	24.8	3.2	219	54	65.2	43.2	169	104	155.2	83.2
268	5	23.0	4.0	218	55	67.0	44.0		105	157.0	84.0
267	6	21.2	4.8	217	56	68.8	44.8		106	158.8	84.8
266	7	19.4	5.6	216	57	70.6	45.6	166	107	160.6	85.6
265	- 8	17.6	- 6.4	215	-58	-72.4	-46.4		-108	-162.4	-86.4
264	9	15.8	7.2	214	59	74.2	47.2		100	164.2	87.2 88.0
263	10	14.0	8.o 8.8	213	60	76.0	48.8		111	167.8	88.8
261	12	10.4	9.6	212 211	61 62	77.8	49.6		112	169.6	89.6
260	-13	8.6	-10.4	210	-63	-81.4	-50.4	160	-113	-171.4	-90.4
250	14	6.8	11.2	200	64	83.2	51.2		114	173.2	91.2
258	15	5.0	12.0	208	65	85.0	52.0		115	175.0	92.0
257	16	3.2	12.8	207	66	86.8	52.8		116	176.8	92.8
256	17	+ 1.4	13.6	206	67	88.6	53.6	156	117	178.6	93.6
255	-18	-0.4	-14.4	205	-68	-90.4	-54.4		-118	-180.4	-94.4
254	19	2.2	15.2	204	69	92.2	55-2		119	182.2	95.2
253	20 2 I	4.0	16.0		70	94.0	56.0	153	120	184.0	96.0
252 251	21	5.8 7.6	16.8		71	95.8	56.8 57.6		121	187.6	97.6
					72					-189.4	-98.4
250	-23	-9.4	-18.4	-	-73	-99.4	-58.4		-123	F.	R.
A.A	. С.	F.	R.	A.A.	C.	F.	R.	A.A.	C.		Ν.

TABLE 1
APPROXIMATE ABSOLUTE, CENTICRADE, FAHRENHEIT, AND REAUMUR
SCALES.

A.A.	c.	F.	R.	A.A.	c.	F.	R.	A.A.	c.	F.	R.
150°	-123°	-189°.4	- 98°.4	100°	-173°	-270°4	-138°.4	50°	-223°	-360°4	-178°4
149	124	101.2	99.2	99	174	281.2	130.2	49	224	371.2	179.2
148	125	193.0	100.0	98	175	283.0	140.0	48	225	373.0	180.0
147	126	194.8	100.8	97	176	284.8	140.8	47	226	374.8	180.8
146	127	196.6	101.6	96	177	286.6	141.6	46	227	376.6	181.6
	,										
145	-128	-198.4	-102.4	95	-178	-288.4	-142.4	45	-228	-378.4	-182.4
144	129	200.2	103.2	94	179	290.2	143.2	44	229	380.2	183.2
143	130	202.0	104.0	93	180	292.0	144.0	43	230	382.0	184.0
142	131	203.8	104.8	92	181	293.8	144.8	42	231	383.8	184.8
141	132	205.6	105.6	91	182	295.6	145.6	41	232	385.6	185.6
140			***6 .	90	-183	-207.4	-146.4	40	022	-387.4	-186.4
140	-133	-207.4	-106.4	80	184	299.2	147.2		-233	389.2	187.2
139	134	209.2	107.2	88	185	301.0	147.2	39 38	234	301.0	188.0
138	135	211.0	108.8	87	186	302.8	148.8		235 236	391.8	188.8
137	136	214.6	100.6	86	187	302.6	140.6	37 36	237	394.6	180.6
130	13/	214.0	109.0		107	304.0	149.0	30	231	394.0	109.0
135	-138	-216.4	-110.4	85	-188	-306.4	-150.4	35	-238	-396.4	-190.4
134	139	218.2	111.2	84	180	308.2	151.2	34	239	398.2	101.2
133	140	220.0	112.0	83	100	310.0	152.0	33	240	400.0	192.0
132	141	221.8	112.8	82	101	311.8	152.8	32	241	401.8	192.8
131	142	223.6	113.6	81	192	313.6	153.6	31	242	403.6	193.6
											1
130	-143	-225.4	-114.4	80	-193	-315.4	-154.4	30	-243	-405.4	-194.4
129	144	227.2	115.2	79	194	317.2	155.2	29	244	407.2	195.2
128	145	229.0	116.0	78	195	319.0	156.0	28	245	409.0	196.0
127	146	230.8	116.8	77	196	320.8	156.8	27	246	410.8	196.8
126	147	232.6	117.6	76	197	322.6	157.6	26	247	412.6	197.6
125	-148	221.4	-118.4	75	-198	-324.4	-158.4	25	-248	-414.4	-108.4
		-234.4 236.2	110.2	74	199	326.2	150.4	24	240	416.2	100.2
124	149 150	238.0	120.0	73	200	328.0	160.0	23	250	418.0	200.0
123	151	230.8	120.8	72	201	329.8	160.8	22	25I	419.8	200.8
121	152	241.6	121.6	71	202	331.6	161.6	2 I	252	421.6	201.6
121	-3-	24210		′ -		33-11			,	7	
120	-153	-243.4	-122.4	70	-203	-333.4	-162.4	20	-253	-423.4	-202.4
IIO	154	245.2	123.2	69	204	335.2	163.2	19	254	425.2	203.2
118	155	247.0	124.0	68	205	337.0	164.0	18	255	427.0	204.0
117	156	248.8	124.8	67	206	338.8	164.8	17	256	428.8	204.8
116	157	250.6	125.6	66	207	340.6	165.6	16	257	430.6	205.6
				0.5	0		-66		0		
115	-158	-252.4	-126.4	65	-208	-342.4	-166.4	15	-258	-432.4	-206.4
114	159	254.2	127.2	64	209	344.2	167.2	14	259	434.2	207.2
113	160	256.0	128.0 128.8	63	210	346.0	168.0	13	260 261	436.0	208.0
II2	161 162	257.8 259.6	128.8	61	2II 2I2	347.8 349.6	160.6	11	262	437.8 439.6	200.6
III	102	259.0	129.0	01	212	349.0	109.0	11	202	439.0	209.0
110	-163	-261.4	-130.4	60	-213	-351.4	-170.4	10	-263	-441.4	-210.4
100	164	263.2	131.2	59	214	353.2	171.2	9	264	443.2	211.2
108	165	265.0	132.0	58	215	355.0	172.0	8	265	445.0	212.0
107	166	266.8	132.8	57	216	356.8	172.8	7	266	4.16.8	212.8
106	167	268.6	133.6		217	358.6	173.6	6	267	448.6	213.6
105	-168	-270.4	-134.4	55	-218	-360.4	-174.4	5	-268	-450.4	-214.4
104	169	272.2	135.2	54	219	362.2	175.2	4	269	452.2	215.2
103	170	274.0	136.0	53	220	364.0	176.0	3	270	454.0	216.0
102	171	275.8	136.8	52	221	365.8	176.8	2	271	455.8	216.8
IOI	172	277.6	137.6	51	222	367.6	177.6	Ι	272	457.6	217.6
100	-173	-279.4	-138.4	50	-223	-369.4	-178.4	0	-273	-459.4	-218.4
A.A.	c.	F.	R.	A.A.	C.	F.	R.	A.A.	C.	F.	R.

Fahren- heit.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
+130° 129 128 127 126	c. +54°.44 53.89 53.33 52.78 52.22	c. +54°.50 53.94 53.39 52.83 52.28	c. +54°.56 54.00 53.44 52.89 52.33	c. +54.61 54.06 53.50 52.94 52.39	c. +54.67 54.11 53.56 53.00 52.44	53.06	c. +54°.78 54.22 53.67 53.11 52.56	c. +54.83 54.28 53.72 53.17 52.61	c. +54.89 54.33 53.78 53.22 52.67	c. +54°94 54·39 53·83 53·28 52·72
+125	+51.67	+ 51.72	+51.78	+51.83	+51.89	+51.94	+52.00	+52.06	+52.11	+52.17
124	51.11	51.17	51.22	51.28	51.33	51.39	51.44	51.50	51.56	51.61
123	50.56	50.61	50.67	50.72	50.78	50.83	50.89	50.94	51.00	51.06
122	50.00	50.06	50.11	50.17	50.22	50.28	50.33	50.39	50.44	50.50
121	49.44	49.50	49.56	49.61	49.67	49.72	49.78	49.83	49.89	49.94
+120 119 118 117 116	+48.89 48.33 47.78 47.22 46.67	+43.94 48.39 47.83 47.28 46.72	+49.00 48.44 47.89 47.33 46.78	+49.06 48.50 47.94 47.39 46.83	+49.11 48.56 48.00 47.44 46.89	48.06	+49.22 48.67 48.11 47.56 47.00	+49.28 48.72 48.17 47.61 47.06	48.78 48.22 47.67	+49.39 48.83 48.28 47.72 47.17
+115	+46.11	+46.17	+46.22	+46.28	+46.33	+46.39	+46.44	+46.50	+46.56	+46.61
114	45.56	45.61	45.67	45.72	45.78	45.83	45.89	45.94	46.00	46.06
113	45.00	45.06	45.11	45.17	45.22	45.28	45.33	45.39	45.44	45.50
112	44.44	44.50	44.56	44.61	44.67	44.72	44.78	44.83	44.89	44.94
111	43.89	43.94	44.00	44.06	44.11	44.17	44.22	44.28	44.33	44.39
+ II0	+43.33	+43.39	+43.44	+43.50	+43.56		+43.67	+43.72	+43.78	+43.83
109	42.78	42.83	42.89	42.94	43.00		43.11	43.17	43.22	43.28
108	42.22	42.28	42.33	42.39	42.44		42.56	42.61	42.67	42.72
107	41.67	41.72	41.78	41.83	41.89		42.00	42.06	42.11	42.17
106	41.11	41.17	41.22	41.28	41.33		41.44	41.50	41.56	41.61
104 103 102 101	+40.56 40.00 39.44 38.89 38.33	+40.61 40.06 39.50 38.94 38.39	+40.67 40.11 39.56 39.00 38.44	+40.72 40.1 7 39.61 39.06 38.50	+40.78 40.22 39.67 39.11 38.56	+40.83 40.28 39.72 39.17 38.61	+40.89 40.33 39.78 39.22 38.67	+40.94 40.39 39.83 39.28 38.72	+41.00 40.44 39.89 39.33 38.78	+41.06 40.50 39.94 39.39 38.83
+ 100 99 98 97 96	+37.78	+37.83	+37.89	+37.94	+38.00	+38.06	+38.11	+38.17	+38.22	+38.28
	37.22	37.28	37.33	37.39	37.44	37.50	37.56	37.61	37.67	37.72
	36.67	36.72	36.78	36.83	36.89	36.94	37.00	37.06	37.11	37.17
	36.11	36.17	36.22	36.28	36.33	36.39	36.44	36.50	36.56	36.61
	35.56	35.61	35.67	35.72	35.78	35.83	35.89	35.94	36.00	36.06
+ 95 94 93 92 91	+35.00	+35.06	+35.11	+35.17	+35.22	+35.28	+35.33	+35.39	+35.44	+35.50
	34.44	34.50	34.56	34.61	34.67	34.72	34.78	34.83	34.89	34.94
	33.89	33.94	34.00	34.06	34.11	34.17	34.22	34.28	34.33	34.39
	33.33	33.39	33.44	33.50	33.56	33.61	33.67	33.72	33.78	33.83
	32.78	32.83	32.89	32.94	33.00	33.06	33.11	33.17	33.22	33.28
+ 90 89 88 87 86	+32.22	+32.28	+32.33	+32.39	+32.44	+32.50	+32.56	+32.61	+32.67	+32.72
	31.67	31.72	31.78	31.83	31.89	31.94	32.00	32.06	32.11	32.17
	31.11	31.17	31.22	31.28	31.33	31.39	31.44	31.50	31.56	31.61
	30.56	30.61	30.67	30.72	30.78	30.83	30.89	30.94	31.00	31.06
	30.00	30.06	30.11	30.17	30.22	30.28	30.33	30.39	30.44	30.50
+ 85 84 83 82 81 ·	+29.44 28 89 28.33 27.78 27.22 +26.67	+29.50 28.94 28.39 27.83 27.28 +26.72	+29.56 29.00 28.44 27.89 27.33 +26.78	+29.61 29.06 28.50 27.94 27.39 +26.83	+29.67 29.11 28.56 28.00 27.44 +26.89	29.17 28.61 28.06 27.50	29.22 28.67 28.11 27.56	+29.83 29.28 28.72 28.17 27.61 +27.06	+29.89 29.33 28.78 28.22 27.67 +27.11	+29.94 29.39 28.83 28.28 27.72 +27.17
	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9

Fahren- heit.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
+80° 79 78 77 76	c.	c.	c.	c.	c.	c.	c.	c.	c.	C.
	+26.67	+26°.72	+26.78	+26.83	+26.89	+26.94	+27°.00	+27.06	+27°.11	+27.17
	26.11	26.17	26.22	26.28	26.33	26.39	26.44	26.50	26.56	26.61
	25.56	25.61	25.67	25.72	25.78	25.83	25.89	25.94	26.00	26.06
	25.00	25.06	25.11	25.17	25.22	25.28	25.33	25.39	25.44	25.50
	24.44	24.50	24.56	24.61	24.67	24.72	24.78	24.83	24.89	24.94
+- 75 74 73 72 71	+23.89	+23.94	+24.00	+24.06	+24.11	+24.17	+24.22	+24.28	+24.33	+24.39
	23.33	23.39	23.44	23.50	23.56	23.61	23.67	23.72	23.78	23.83
	22.78	22.83	22.89	22.94	23.00	23.06	23.11	23.17	23.22	23.28
	22.22	22.28	22.33	22.39	22.44	22.50	22.56	22.61	22.67	22.72
	21.67	21.72	21.78	21.83	21.89	21.94	22.00	22.06	22.11	22.17
+70	+21.11	+21.17	+21.22	+21.28	+21.33	+21.39	+21.44	+21.50	+21.56	†21.61
69	20.56	20.61	20.67	20.72	20.78	20.83	20.89	20.94	21.00	21.06
68	20.00	20.06	20.11	20.17	20.22	20.28	20.33	20.39	20.44	20.50
67	19.44	19.50	19.56	19.61	19.67	19.72	19.78	19.83	19.89	19.94
66	18.89	18.94	19.00	19.06	19.11	19.17	19.22	19.28	19.33	19.39
+65	+18.33	+18.39	+18.44	+18.50	+18.56	+18.61	+18.67	+18.72	+18.78	+18.83
64	17.78	17.83	17.89	17.94	18.00	18.06	18.11	18.17	18.22	18.28
63	17.22	17.28	17.33	17.39	17.44	17.50	17.56	17.61	17.67	17.72
62	16.67	16.72	16.78	16.83	16.89	16.94	17.00	17.06	17.11	17.17
61	16.11	16.17	16.22	16.28	16.33	16.39	16.44	16.50	16.56	16.61
+ 60 59 58 57 56	+15.56	+15.61	+15.67	+15.72	+15.78	+15.83	+15.89	+15.94	+16.00	+16.06
	15.00	15.06	15.11	15.17	15.22	15.28	15.33	15.39	15.44	15.50
	14.44	14.50	14.56	14.61	14.67	14.72	14.78	14.83	14.89	14.94
	13.89	13.94	14.00	14.06	14.11	14.17	14.22	14.28	14.33	14.39
	13.33	13.39	13.44	13.50	13.56	13.61	13.67	13.72	13.78	13.83
+55	+12.78	+12.83	+12.89	+12.94	+13.00	+13.06	+13.11	+13.17	+13.22	13.28
54	12.22	12.28	12.33	12.39	12.44	12.50	12.56	12.61	12.67	12.72
53	11.67	11.72	11.78	11.83	11.89	11.94	12.00	12.06	12.11	12.17
52	11.11	11.17	11.22	11.28	11.33	11.39	11.44	11.50	11.56	11.61
51	10.56	10.61	10.67	10.72	10.78	10.83	10.89	10.94	11.00	11.06
+50	+10.00	+10.06	+10.11	+10.17	+10.22	+10.28	+10.33	+10.39	+10.44	+10.50
49	9.44	9.50	9.56	9.61	9.67	9.72	9.78	9.83	9.89	9.94
48	8.89	8.94	9.00	9.06	9.11	9.17	9.22	9.28	9.33	9.39
47	8.33	8.39	8.44	8.50	8.56	8.61	8.67	8.72	8.78	8.83
46	7.78	7.83	7.89	7.94	8.00	8.06	8.11	8.17	8.22	8.28
+45	+ 7.22	+ 7.28	+ 7.33	+ 7.39	+ 7.44	+ 7.50	+ 7.56	+ 7.61	+ 7.67	+ 7.72
44	6.67	6.72	6.78	6.83	6.89	6.94	7.00	7.06	7.11	7.17
43	6.11	6.17	6.22	6.28	6.33	6.39	6.44	6.50	6.56	6.61
42	5.56	5.61	5.67	5.72	5.78	5.83	5.89	5.94	6.00	6.06
41	5.00	5.06	5.11	5.17	5.22	5.28	5.33	5.39	5.44	5.50
+ 40 39 38 37 36	+ 4.44 3.89 3.33 2.78 2.22	+ 4.50 3.94 3.39 2.83 2.28	+ 4.56 4.00 3.44 2.89 2.33	+ 4.61 4.06 3.50 2.94 2.39	+ 4.67 4.11 3.56 3.00 2.44	+ 4.72 4.17 3.61 3.06 2.50	+ 4.78 4.22 3.67 3.11 2.56	+ 4.83 4.28 3.72 3.17 2.61	+ 4.89 4.33 3.78 3.22 2.67	+ 4.94 4.39 3.83 3.28 2.72
+35 34 33 32 31 +30			+ I.22 + 0.67 + 0.11 - 0.44	+ 1.83 + 1.28 + 0.72 + 0.17 - 0.39 - 0.94		+ 0.83 + 0.28 - 0.28		+ 2.06 + 1.50 + 0.94 + 0.39 - 0.17 - 0.72		+ 2.17 + 1.61 + 1.06 + 0.50 - 0.06 - 0.61
1	.0	.1	.2	.з	.4	.5	.6	.7	.8	.9

SMITHSONIAN TABLES.

Fahren- heit.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
+30° 29 28 27 26	c 1°.11 1.67 2.22 2.78 3.33	c. - 1.06 1.61 2.17 2.72 3.28	c. - 1.00 1.56 2.11 2.67 3.22	c. - 0.94 1.50 2.06 2.61 3.17	c. - 0.89 1.44 2.00 2.56 3.11	c. - 0.83 1.39 1.94 2.50 3.06	c 0.78 1.33 1.89 2.44 3.00	c 0.72 1.28 1.83 2.39 2.94	c 0.67 1.22 1.78 2.33 2.89	c 0.61 1.17 1.72 2.28 2.83
+25 24 23 22 21	- 3.89 4.44 5.00 5.56 6.11	- 3.83 4.39 4.94 5.50 6.06	- 3.78 4.33 4.89 5.44 6.00	- 3.72 4.28 4.83 5.39 5.94	- 3.67 4.22 4.78 5.33 5.89	- 3.61 4.17 4.72 5.28 5.83	- 3.56 4.11 4.67 5.22 5.78	- 3.50 4.06 4.61 5.17 5.72	- 3.44 4.00 4.56 5.11 5.67	- 3.39 3.94 4.50 5.06 5.61
+20 19 18 17 16	- 6.67 7.22 7.78 8.33 8.89	- 6.61 7.17 7.72 8.28 8.83	- 6.56 7.11 7.67 8.22 8.78	- 6.50 7.61 8.17 8.72	- 6.44 7.00 7.56 8.11 8.67	- 6.39 6.94 7.50 8.06 8.61	- 6.33 6.89 7.44 8.00 8.56	- 6.28 6.83 7.39 7.94 8.50	- 6.22 6.78 7.33 7.89 8.44	- 6.17 6.72 7.28 7.83 8.39
+ 15 14 13 12 11	- 9.44 10.00 10.56 11.11 11.67	- 9.39 9.94 10.50 11.06	- 9.33 9.89 10.44 11.00	- 9.28 9.83 10.39 10.94 11.50	- 9.22 9.78 10.33 10.89	9.17 9.72 10.28 10.83	- 9.11 9.67 10.22 10.78 11.33	- 9.06 9.61 10.17 10.72 11.28	- 9.00 9.56 10.11 10.67 11.22	- 8.94 9.50 10.06 10.61 11.17
+ 10 9 8 7 6	12.22 12.78 13.33 13.89 14.44	-12.17 12.72 13.28 13.83 14.39	-12.11 12.67 13.22 13.78 14.33	-12.06 12.61 13.17 13.72 14.28	-12.00 12.56 13.11 13.67 14.22	-11.94 12.50 13.06 13.61 14.17	-11.89 12.44 13.00 13.56 14.11	-11.83 12.39 12.94 13.50 14.06	-11.78 12.33 12.89 13.44 14.00	-11.72 12.28 12.83 13.39 13.94
+ 5 4 3 2 1 + 0	-15.00 15.56 16.11 16.67 17.22 17.78	14.94 15.50 16.06 16.61 17.17 17.72	-14.89 15.44 16.00 16.56 17.11 17.67	-14.83 15.39 15.94 16.50 17.06 17.61	-14.78 15.33 15.89 16.44 17.00 17.56		-14.67 15.22 15.78 16.33 16.89 17.44	-14.61 15.17 15.72 16.28 16.83 17.39	-14.56 15.11 15.67 16.22 16.78 17.33	-14.50 15.06 15.61 16.17 16.72 17.28
- 0 1 2 3 4	-17.78 18.33 13.89 19.44 20.00	-17.83 18.39 18.94 19.50 20.06	-17.89 18.44 19.00 19.56 20.11	-17.94 18.50 19.06 19.61 20.17	-18.00 18.56 19.11 19.67 20.22	-18.06 18.61 19.17 19.72 20.28	-18.11 18.67 19.22 19.78 20.33	-18.17 18.72 19.28 19.83 20.39	-18.22 18.78 19.33 19.89 20.44	
- 5 6 7 8 9	-20.56 21.11 21.67 22.22 22.78	-20.61 21.17 21.72 22.28 22.83	-20.67 21.22 21.78 22.33 22.89	-20.72 21.28 21.83 22.39 22.94	-20.78 21.33 21.89 22.44 23.00		-20.89 21.44 22.00 22.56 23.11	22.61 23.17	21.56 22.11 22.67 23.22	-21.06 21.61 22.17 22.72 23.28
- 10 11 12 13 14	-23.33 23.89 24.44 25.00 25.56	-23.39 23.94 24.50 25.61	-23.44 24.00 24.56 25.11 25.67	-23.50 24.06 24.61 25.17 25.72	-23.56 24.11 24.67 25.22 25.78	24.17 24.72 25.28 25.83	-23.67 24.22 24.78 25.33 25.89	-23.72 24.28 24.83 25.39 25.94	-23.78 24.33 24.89 25.44 26.00	26.06
- 15 16 17 18 19 -20	-26.11 26.67 27.22 27.78 28.33 -28.89	-26.17 26.72 27.28 27.83 28.39 -28.94	-26.22 26.78 27.33 27.89 28.44 -29.00	-26.28 26.83 27.39 27.94 28.50 -29.06	-26.33 26.89 27.44 28.00 28.56 -29.11	-26.39 26.94 27.50 28.06 28.61 -29.17	-26.44 27.00 27.56 28.11 28.67 -29.22	-26.50 27.06 27.61 28.17 28.72 -29.28	-26.56 27.11 27.67 28.22 28.78 -29.33	-26.61 27.17 27.72 28.28 28.83 -29.39
	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9

Fahren- heit.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
-20°	c. -28.89 29.44 30.00	c. -28°94 29.50	c. -29.00 29.56	c. 29.06 29.61	c. -29.11 29.67 30.22	c. -29°17 29.72 30.28	c. -29°22 29.78	c. -29.28 29.83	c. -29°33 29.89	c. -29°39 29.94 30.50
22 23 24 - 25	30.56 31.11 -31.67	30.06 30.61 31.17	30.11 30.67 31.22 -31.78	30.72 31.28 -31.83	30.78 31.33 31.89	30.83 31.39	30.33 30.89 31.44	30.39 30.94 31.50	30.44 31.00 31.56	31.06 31.61 -32.17
26	32.22	32.28	32.33	32.39	32.44	32.50	32.56	32.61	32.67	32.72
27	32.78	32.83	32.89	32.94	33.00	33.06	33.11	33.17	33.22	33.28
28	33.33	33.39	33.44	33.50	33.56	33.61	33.67	33.72	33.78	33.83
29	33.89	33.94	34.00	34.06	34.11	34.17	34.22	34.28	34.33	34.39
-30	-34.44	-34.50	-34.56	-34.61	-34.67	-34.72	-34.78	-34.83	-34.89	-34.94
31	35.00	35.06	35.11	35.17	35.22	35.28	35.33	35.39	35.44	35.50
32	35.56	35.61	35.67	35.72	35.78	35.83	35.89	35.94	36.00	36.06
33	36.11	36.17	36.22	36.28	36.33	36.39	36.44	36.50	36.56	36.61
34	36.67	36.72	36.78	36.83	36.89	36.94	37.00	37.06	37.11	37.17
-35	-37.22	-37.28	-37.33	-37.39	-37.44	-37.50	-37.56	-37.61	-37.67	-37.72
36	37.78	37.83	37.89	37.94	38.00	38.06	38.11	38.17	38.22	38.28
37	38.33	38.39	38.44	38.50	38.56	38.61	38.67	38.72	38.78	38.83
38	38.89	38.94	39.00	39.06	39.11	39.17	39.22	39.28	39.33	39.39
39	39.44	39.50	39.56	39.61	39.67	39.72	39.78	39.83	39.89	39.94
-40	-40.00	-40.06	-40.11	-40.17	-40.22	-40.28	-40.33	-40.39	-40.44	-40.50
41	40.56	40.61	40.67	40.72	40.78	40.83	40.89	40.94	41.00	41.06
42	41.11	41.17	41.22	41.28	41.33	41.39	41.44	41.50	41.56	41.61
43	41.67	41.72	41.78	41.83	41.89	41.94	42.00	42.06	42.11	42.17
44	42.22	42.28	42.33	42.39	42.44	42.50	42.56	42.61	42.67	42.72
-45	-42.78	-42.83	-42.89	-42.94	-43.00	-43.06	-43.11	-43.17	-43.22	-43.29
46	43.33	43.39	43.44	43.50	43.56	43.61	43.67	43.72	43.78	43.83
47	43.89	43.94	44.00	44.06	44.11	44.17	44.22	44.28	44.33	44.39
48	44.44	44.50	44.55	44.61	44.67	44.72	44.78	44.83	44.89	44.94
49	45.00	45.06	45.11	45.17	45.22	45.28	45.33	45.39	45.44	45.50
-50	-45.56	-45.61	-45.67	-45.72	-45.78	-45.83	-45.89	-45.94	-46.00	-46.06
51	46.11	46.17	46.22	46.28	46.33	46.39	46.44	46.50	46.56	46.61
52	46.67	46.72	46.78	46.83	46.89	46.94	47.00	47.06	47.11	47.17
53	47.22	47.28	47.33	47.39	47.44	47.50	47.56	47.61	47.67	47.72
54	47.78	47.83	47.89	47.94	48.00	48.06	48.11	48.17	48.22	48.28
-55	-48.33	-48.39	-48.44	-48.50	-48.56	-48.61	-48.67	-48.72	-48.78	-48.83
56	48.89	48.94	49.00	49.06	49.11	49.17	49.22	49.28	49.33	49.39
57	49.44	49.50	49.56	49.61	49.67	49.72	49.78	49.83	49.89	49.94
58	50.00	50.06	50.11	50.17	50.22	50.28	50.33	50.39	50.44	50.50
59	50.56	50.61	50.67	50.72	50.78	50.83	50.89	50.94	51.00	51.06
-60	-51.11	-51.17	-51.22	-51.28	-51.33	-51.39	-51.44	-51.50	-51.56	-51.61
61	51.67	51.72	51.78	51.83	51.89	51.94	52.00	52.06	52.11	52.17
62	52.22	52.28	52.33	52.39	52.44	52.50	52.56	52.61	52.67	52.72
63	52.78	52.83	52.89	52.94	53.00	53.06	53.11	53.17	53.22	53.28
64	53.33	53.39	53.44	53.50	53.56	53.61	53.67	53.72	53.78	53.83
-65 66 67 68 69 -70	-53.89 54.44 55.00 55.56 56.11 -56.67	-53.94 54.50 55.06 55.61 56.17 -56.72	-54.00 54.56 55.11 55.67 56.22 -56.78	-54.06 54.61 55.17 55.72 56.28 -56.83	-54.11 54.67 55.22 55.78 56.33 -56.89	-54.17 54.72 55.28 55.83 56.39 -56.94	-54.22 54.78 55.33 55.89 56.44 -57.00	-54.28 54.83 55.39 55.94 56.50 -57.06	-54.33 54.89 55.44 56.00 56.56 -57.11	-54·39 54·94 55·50 56.06 56.61
	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9

Fahren- heit.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	С.	C.	С.							
-70°	-56°.67	-56.72	-56.°78	-56°.83	-56.89	- , .	−57.°00	-57.°06	-57°11	-57.17
71 72	57.22 57.78	57.28 57.83	57.33 57.89	57.39 57.94	57.44	57.50 58.06	57.56	57.61	57.67 58.22	57.72 58.28
73	58.33	58.39	58.44	58.50	58.56	58.61	58.67	58.72	58.78	58.83
74	58.89	58.94	59.00	59.06	59.11	59.17	59.22	59.28	59.33	59.39
- 75 76	-59.44 60.00	-59.50 60.06	-59.56 60.11	-59.61 60.17	-59.67 60.22	-59.72 60.28	-59.78 60.33	-59.83 60.39	-59.89 60.44	-59.94 60.50
77	60.56	60.61	60.67	60.72	60.78	60.83	60.89	60.94	61.00	61.06
78 79	61.11	61.17	61.22	61.28	61.33	61.39	61.44	61.50	61.56	61.61
-80	-62.22	-62.28	-62.33	-62.39	-62.44	-62.50	-62.56	-62.61	-62.67	-62.72
81	62.78	62.83	62.89	62.94	63.00	63.06	63.11	63.17	63.22	63.28
82 83	63.33	63.39	63.44	63.50	63.56	63.61	63.67	63.72	63.78	63.83
84	64.44	64.50	64.56	64.61	64.67		64.78	64.83	64.89	64.39
-85	-65.00	-65.06	-65.11	-65.17	-65.22		-65.33	-65.39	-65.44	-65.50
86 87	65.56	65.61	65.67	65.72 66.28	65.78	65.83	65.89	65.94	66.00 66.56	66.61
88	66.67	66.72	66.78	66.83	66.89	66.94	67.00	67.06	67.11	67.17
89	67.22	67.28	67.33	67.39	67.44	67.50	67.56	67.61	67.67	67.72
-90	-67.78	-67.83	-67.89	-67.94	-68.00	-68.06 68.61	-68.11	-68.17	-68.22	-68.28
91 92	68.33 68.89	68.39 68.94	68.44	68.50 69.06	68.56	69.17	68.67	68.72	68.78	68.83 69.39
93	69.44	69.50	69.56	69.61	69.67	69.72	69.78	69.83	69.89	69.94
94	70.00	70.06	70.11	70.17	70.22	70.28	70.33	70.39	70.44	70.50
-95 96	-70.56 71.11	-70.61	-70.67 71.22	-70.72 71.28	-70.78 71.33	-70.83 71.39	-70.89 71.44	-70.94 71.50	71.56	-71.06 71.61
97	71.67	71.72	71.78	71.83	71.89	71.94	72.00	72.06	72.11	72.17
98	72.22 72.78	72.28 72.83	72.33 72.89	72.39 72.94	72.44 73.00	72.50 73.06	72.56	72.61	72.67	72.72 73.28
-100										
101	-73.33 73.89	-73.39 73.94	74.00	-73.50 74.06	-73.56 74.11	-73.61 74.17	-73.67 74.22	74.28	-73.78 74.33	-73.83 74.39
102	74.44	74.50	74.56	74.61	74.67	74.72	74.78	74.83	74.89	74.94
103	75.00 75.56	75.61	75.11	75.17 75.72	75.22 75.78	75.28 75.83	75.33 75.89	75.39 75.94	75.44 76.00	75.50 76.06
-105	-76.11	-76.17	-76.22	-76.28	-76.33	-76.39	-76.44	-76.50	-76.56	-76.61
106	76.67	76.72	76.78	76.83	76.89	76.94	77.00	77.06	77.11	77.17
107	77.22 77.78	77.28	77.33 77.89	77·39 77·94	77.44 78.00	77.50 78.06	77.56 78.11	77.61 78.17	77.67 78.22	77.72 78.28
109	78.33	78.39	78.44	78.50	78.56	78.61	78.67	78.72	78.78	78.83
-110	-78.89	-78.94	-79.00	-79.06	-79.11	-79.17	-79.22	-79.28	-79.33	-79.39
111 112	79·44 80.00	79.50 80.06	79.56	79.61 80.17	79.67 80.22	79.72 80.28	79.78 80.33	79.83 80.39	79.89 80.44	79.94 80.50
113	80.56	80.61	80.67	80.72	80.78	80.83	80.89	80.94	81.00	81.06
114	81.11	81.17	81.22	81.28	81.33	81.39	81.44	81.50	81.56	81.61
-115 116	-81.67 82.22	-81.72 82.28	-81.78 82.33	-81.83 82.39	-81.89 82.44	-81.94 82.50	-82.00 82.56	-82.06 82.61	-82.11 82.67	-82.17 82.72
117	82.78	82.83	82.89	82.94	83.00	83.06	83.11	83.17	83.22	83.28
118	83.33 83.89	83.39 83.94	83.44	83.50 84.06	83.56 84.11	83.61 84.17	83.67	83.72 84.28	83.78 84.33	83.83
-120	-84.44	-84.50	-84.56	-84.61	-84.67	-84.72	-84.78	-84.83	-84.89	-84.94
	.0	.1	.2	.3	.4	.5	,6	.7	.8	.9

CENTIGRADE SCALE TO FAHRENHEIT.

Centi- grade.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	F.	F.	F.	F.	F.	F.	F.	F.	F.	F.
+60°		+140.18	+140.36	+140.54	+140.72					+141.62
59	138.20	138.38		138.74		139.10	139.28	139.46		139.82
58	136.40	136.58 134.78		136.94 135.14		137.30	137.48 135.68	137.66		136.22
57 56	132.80	132.98						134.06		134.42
		,								
					+131.72	+131.90				+132.62
54	129.20			129.74		130.10	130.28 128.48	130.46 128.66		130.82
53 52	127.40	127.58 125.78			1 -					127.22
51	123.80			124.34						125.42
+50					+122.72	+122.90 121.10		+123.20 121.46		+123.62 121.82
49 48	120.20	120.38 118.58		120.74	120.92	119.30	_			120.02
47	116.60			117.14	_	, ,				118.22
46	114.80	114.98	115.16	115.34	115.52	115.70	115.88	116.06	116.24	116.42
145		1,172,10	LII 2 26	L II 2 5 .	+113.72	+11200	+11108	+111 26	+114.41	+114.62
+45 44	111.20	111.38						112.46	112.64	112.82
43	100.40			100.04						111.02
42	107.60			108.14	108.32					
41	105.80	105.98	106.16	106.34	106.52	106.70	106.88	107.06	107.24	107.42
+40	+101.00	+104.18	+101.36	+104.54	+104.72	+104.00	+105.08	+105,26	+105.44	+105.62
39	102.20							103.46	103.64	103.82
38	100.40			100.94	101.12	101.30	101.48	101.66		102.02
37	98.60						99.68	99.86		08.42
36	96.80	96.98	97.16	97.34	97.52	97.70	97.88	98.06	90.24	90.42
+35	+ 95.00	+ 95.18	+ 95.36	+ 95.54	+ 95.72	+ 95.90	+ 96.08	+ 96.26	+ 96.44	+ 96.62
34	93.20			93.74	93.92	94.10	94.28	94.46		94.82
. 33	91.40			91.94				92.66		93.02
32 31	89.60 87.80			90.14 88.34		90.50 88.70		90.86 89.06		91.22 89.42
31	07.00	07.90	00.10							
+30			+ 86.36		+ 86.72				+ 87.44	+ 87.62
29	84.20	84.38		84.74						85.82 84.02
28 27	82.40 80.60	82.58 80.78		82.94 81.14						
26	78.80			79.34	_					
	+ 77.00		+ 77.36		+ 77.72				+ 78.44	
24	75.20 73.40			75.74 73.94						
23	71.60									
21	69.80									
100	1 60	1 60 -0	1 60 -6	1 60	1 60		1 60	1 60 06	1 60 11	1 60 60
+20	+ 68.00 66.20				+ 68.72 66.92					
18	64.40									66.02
17	62.60	62.78	62.96				63.68	63.86	64.04	64.22
16	60.80	60.98	61.16	61.34	61.52	61.70	61.88	62.06	62.24	62.42
+15	+ 59.00	+ 59.18	+ 59.36	+ 59.54	+ 50.72	+ 59.90	+ 60.08	+ 60.26	+ 60.14	+ 60.62
14	57.20							58.46	58.64	
13	55.40	55.58	55.76	55.94	56.12	56.30	56.48	56.66	56.84	
12	53.60									
II	51.80	51.98	52.16	52.34	52.52	52.70	52.88	53.06	53.24	53.42
+10	+ 50.00	+ 50.18	+ 50.36	+ 50.54	+ 50.72	+ 50.90	+ 51.08	+ 51.26	+ 51.44	+ 51.62
	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9

CENTIGRADE SCALE TO FAHRENHEIT.

+ 0	Centi- grade.	.0		.1	.2	.3	.4	.5	.6	.7	.8	.9
8 46.40 46.58 46.70 46.04 47.12 47.30 47.48 47.66 47.8 6 42.80 42.80 43.10 43.34 45.52 45.50 45.68 46.0 5 41.00 41.18 41.30 41.54 41.72 41.00 42.08 42.26 42.4 4 4 43.92 +30.38 +30.50 37.74 43.92 +40.10 +40.28 +40.40 +40.6 42.68 42.26 42.4 4 4 43.92 +30.74 +30.92 +40.10 +40.28 +40.40 +40.66 38.8 38.66 38.8 38.66 38.8 38.66 38.8 38.66 38.8 38.66 38.8 38.66 38.8 38.66 38.8 38.06 38.8 38.66 38.8 38.66 38.8 38.06 38.8 38.06 38.2 38.2 38.2 38.2 38.2 38.2 38.2 38.2 38.2 38.2 38.2	+10°										F. +51.44	F, +51.62
+ 4	8 7 6	46.40 44.60 42.80	46.40 44.60 42.80	46.58 44.78 42.98	46.76 44.96 43.16	46.94 45.14 43.34	47.12 45.32 43.52	47.30 45.50 43.70	47.48 45.68 43.88	47.66 45.86 44.06	+49.64 47.84 46.04 44.24	+49.82 48.02 46.22 44.42 42.62
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	+ 4 3 2 1	+39.20 37.40 35.60 33.80	+39.20 37.40 35.60 33.80	+39.38 37.58 35.78 33.98	+39.56 37.76 35.96 34.16	+39.74 37.94 36.14 34.34	+39.92 38.12 36.32 34.52	+40.10 38.30 36.50 34.70	+40.28 38.48 36.68 34.88	+40.46 38.66 36.86 35.06	+40.64 38.84 37.04 35.24 33.44	+40.82 39.02 37.22 35.42 33.62
6 21.20 21.02 20.84 20.66 20.48 20.30 20.12 19.94 19.77 19.40 10.22 19.04 18.86 18.68 18.50 18.32 18.14 17.0 15.80 15.62 15.44 15.26 15.08 14.90 14.72 14.54 14.34 17.10 14.72 14.54 14.34 17.10 14.72 14.54 14.34 17.10 14.72 14.54 14.34 17.10 14.72 14.54 14.34 17.10 17.20 17.	1 2 3	30.20 28.40 26.60	30.20 28.40 26.60	+31.82 30.02 28.22 26.42	29.84 28.04 26.24	29.66 27.86 26.06	29.48 27.68 25.88	29.30 27.50 25.70	+30.92 29.12 27.32 25.52	28.94 27.14 25.34	+30.56 28.76 26.96 25.16 23.36	+30.38 28.58 26.78 24.98 23.18
11 12.20 12.02 11.84 11.66 11.48 11.30 11.12 10.94 10.74 12 10.40 10.22 10.04 9.86 9.68 9.50 9.32 9.14 8.9 13 8.60 8.42 8.24 8.06 7.88 7.70 7.52 7.34 7.1 14 6.80 6.62 6.44 6.26 6.08 5.90 5.72 5.54 5.3 -15 + 5.00 + 4.82 + 4.64 + 4.46 + 4.28 + 4.10 + 3.92 + 3.74 + 3.5 16 + 3.20 + 2.84 + 2.66 + 2.48 + 2.30 + 2.12 + 1.94 + 1.7 17 + 1.40 + 1.22 + 1.04 + 0.86 + 0.68 + 0.55 + 0.32 + 0.14 - 0.0 18 - 0.40 - 0.58 - 0.76 - 0.94 - 1.12 - 1.30 1.48 - 1.66 - 1.8 19 - 2.20 - 2.38 - 2.56<	6 7 8	21.20 19.40 17.60	21.20 19.40 17.60	21.02 19.22 17.42	20.84 19.04 17.24	20.66 18.86 17.06	20.48 18.68 16.88	20.30 18.50 16.70	20.12 18.32 16.52	19.94 18.14 16.34	+21.56 19.76 17.96 16.16 14.36	+21.38 19.58 17.78 15.98 14.18
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11 12 13	12.20 10.40 8.60	12.20 10.40 8.60	12.02 10.22 8.42	11.84 10.04 8.24	9.86 8.06	9.68 7.88	9.50 7.70	9.32 7.52	10.94 9.14 7.34	+12.56 10.76 8.96 7.16 5.36	+12.38 10.58 8.78 6.98 5.18
21 5.80 5.98 6.16 6.34 6.52 6.70 6.88 7.06 7.2 22 7.60 7.78 7.96 8.14 8.32 8.50 8.68 8.86 9.0 23 9.40 9.58 9.76 9.94 10.12 10.30 10.48 10.60 10.8 24 11.20 11.38 11.56 11.74 11.92 12.10 12.28 12.46 12.6 -25 -13.00 -13.18 -13.36 -13.54 -13.72 -13.90 -14.08 -14.26 14.26 16.06 16.2 15.70 15.88 16.06 16.2 15.70 15.88 16.06 16.2 18.06 18.04 19.12 19.30 19.48 19.66 19.8 19.60 19.8 19.12 19.30 19.48 19.66 19.8 19.12 19.30 19.48 19.66 19.8 21.46 21.6 21.6 21.6 21.6 21.6 21.6 21.6	16 17 18	+ 3.20 + 1.40 - 0.40	+ 3.20 + 1.40 - 0.40	+ 3.02 + 1.22 - 0.58	+ 2.84 + 1.04 - 0.76	+ 2.66 + 0.86 - 0.94	+ 2.48 + 0.68 - 1.12	+ 2.30 + 0.50 - 1.30	+ 2.12 + 0.32 - 1.48	+ 1.94 + 0.14 - 1.66	+ 1.76 - 0.04 - 1.84	+ 3.38 + 1.58 - 0.22 - 2.02 - 3.82
26	21 22 23	5.80 7.60 9.40	5.80 7.60 9.40	5.98 7.78 9.58	6.16 7.96 9.76	6.34 8.14 9.94	6.52 8.32 10.12	6.70 8.50 10.30	6.88 8.68 10.48	7.06 8.86 10.66	- 5.44 7.24 9.04 10.84 12.64	- 5.62 7.42 9.22 11.02 12.82
31 23.80 23.98 24.16 24.34 24.52 24.70 24.88 25.06 25.2 32 25.60 25.78 25.96 26.14 26.32 26.50 26.68 26.86 27.0 33 27.40 27.58 27.76 27.94 28.12 28.30 28.48 28.66 28.8 34 29.20 29.38 29.56 29.74 29.92 30.10 30.28 30.46	26 27 28	14.80 16.60 18.40	14.8c	14.98 16.78 18.58	15.16 16.96 18.76	15.34 17.14 18.94	15.52 17.32 19.12	15.70 17.50 19.30	15.88 17.68 19.48	16.06 17.86 19.66	-14.44 16.24 18.04 19.84 21.64	-14.62 16.42 18.22 20.02 21.82
25 27 28 27 26 27 24 27 22 27 20 27 28 -22 26 -22 4	31 32 33	23.80 25.60 27.40	23.8c 25.6c 27.4c	23.98 25.78 27.58	24.16 25.96 27.76	24.34 26.14 27.94	24.52 26.32 28.12	24.70 26.50 28.30	24.88 26.68 28.48	25.06 26.86 28.66	-23.44 25.24 27.04 28.84 30.64	-23.62 25.42 27.22 29.02 30.82
36 32.80 32.98 33.16 33.34 33.52 33.70 33.88 34.06 34.2 37 34.60 34.78 34.96 35.14 35.32 35.50 35.68 35.86 36.0 38 36.40 36.58 36.76 36.94 37.12 37.30 37.48 37.66 37.8	37 38	34.60 36.40	32.8c 34.6c 36.4c	32.98 34.78 36.58	34.96 36.76	35.14 36.94	33.52 35.32 37.12	33.70 35.50 37.30	35.68 37.48	35.86 37.66	-32.44 34.24 36.04 37.84 39.64	-32.62 34.42 36.22 38.02 39.82
-40	-40 		_									-41.62 .9

CENTICRADE SCALE TO FAHRENHEIT.

Centi- grade.	.0	.1	.2	.3	.4	,5	,6	.7	.8	.9
	F.	F.	F.	F.	F.	F.	F.	F,	F.	F.
- 40°	- 40°.00									
4 I	41.80		42.16	42.34		42.70	42.88	43.06	43.24	43.42
42	43.60									
43 44	45.40 47.20									
44	47.20	47.30	47.30	4/./4	47.92	40.10	40.20	40.40	40.04	40.02
- 45	- 49.00									- 50.62
46	50.80									52.42
47 48	52.60 54.40									
49	56.20									57.82
li l										
- 50	- 58.00 59.80				- 58.72		- 50.08 60.88			
51 52	61.60						62.68			61.42 63.22
53	63.40				64.12					65.02
54	65.20				65.92					66.82
5.5	- 67.00	60	6	6	6	6-	60 -0	60 -6	60	60 (
- 55 56	68.80		- 67.36 69.16		- 67.72 69.52			- 68.26 70.06	1 1	- 68.62 70.42
57	70.60		70.06	71.14	71.32		71.68			72.22
58	72.40	72.58	72.76		73.12		73.48	73.66		74.02
59	74.20	74.38	74.56	74.74	74.92	75.10	75.28	75.46	75.64	75.82
- 60	- 76.00	- 76.18	~6 a6	76 74	- 76.72	76.00	- 77.08	77.06		- 77.62
61	77.80		- 76.36 78.16	- 76.54 78.34	78.52		78.88		- 77.44 79.24	79.42
62	79.60		79.96	80.14	80.32		80.68	80.86	81.04	81.22
63	81.40	81.58	81.76	81.94	82.12	82.30	82.48	82.66	82.84	83.02
64	83.20	83.38	83.56	83.74	83.92	84.10	84.28	84.46	84.64	84.82
- 65	- 85.00	- 85.18	- 85.36	- 85.54	- 85.72	- 85.90	- 86.08	- 86.26	- 86.44	- 86.62
66	86.80	86.98	87.16	87.34	87.52	87.70	87.88	88.06	88.24	88.42
67	88.60		88.96		89.32		89.68	89.86	90.04	90.22
68	90.40				91.12		91.48	91.66		92.02
69	92.20	92.38	92.56	92.74	92.92	93.10	93.28	93.46	93.64	93.82
- 70	- 94.00	- 94.18	- 94.36	- 94.54	- 94.72	- 04.90	- 95.08	- 95.26	- 95.44	- 95.62
71	95.80	95.98	96.16	96.34	96.52		96.88	97.06	97.24	97-12
72	97.60				98.32		98.68	98.86	99.04	99.22
73	99.40	99.58		99.94	100.12		100.48	100.66	100.84	101.02
74	101.20	101.38	101.56	101.74	101.92	102.10	102.28	102.46	102.64	102.82
- 75	-103.00	-103.18	-103.36	-103.54	-103.72	-103.90	-104.08	-104.26	-104.44	-104.62
76	104.80	104.98	105.16	105.34	105.52	105.70	105.88	106.06	106.24	106.42
77	106.60	106.78	106.96	107.14	107.32	107.50	107.68	107.86	108.04	108.22
78 79	108.40	108.58	108.76	108.94	109.12		109.48	109.66	109.84	110.02
19	110.20	110.30	110.50	110.74	110.92				·	111.02
- 80			-112.36		-112.72			-113.26		-113.62
81	113.80	113.98	114.16	114.34	114.52		114.88	115.06	115.24	115.42
82 83	115.60	115.78	115.96	116.14	116.32	116.50	116.68	116.86	117.04	117.22
84	110.20				110.12	120.10	120.28	120.46	120.64	120.82
- 85		-121.18				-121.90				
86 87	122.80	122.98 124.78	123.16 124.96	123.34	123.52		123.88	124.06	I 24.24 I 26.04	124.42
88	126.40	126.58	124.90	126.94	127.12		127.48	127.66	127.84	128.02
89	128.20	128.38		128.74	128.92		129.28	129.46	129.64	129.82
- 90	-130.00	-130.18	-130.36	-130.54	-130.72	-130.90	-131.08	-131.26	-131.44	-131.62
	.0	.1	.2	.3	.4	.5	,6	.7	.8	.9
		• 1	124		. 7		, ,	. ,		

SMITHSONIAN TABLES.

TABLE 4.

CENTIGRADE SCALE TO FAHRENHEIT - Near the Boiling Point.

Centi- grade.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	F.									
100°	212.00	212.18	212°36	212°54	212°72	212°90	213.08	213.26	213.44	213.62
99	210.20	210.38	210.56	210.74	210.92	211.10	211.28	211.46	211.64	211.82
98	208.40	208.58	208.76	208.94	209.12	209.30	209.48	209.66	209.84	210.02
97	206,60	206.78	206.96	207.14	207.32	207.50	207.68	207.86	208.04	208.22
96	204.80	204.98	205.16	205.34	205.52	205.70	205.88	206.06	206.24	206.42
95	203.00	203.18	203.36	203.54	203.72	203.90	204.08	204.26	204.44	204.62
94	201.20	201.38	201.56	201.74	201.92	202.10	202.28	202.46	202.64	202.82
93	199.40	199.58	199.76	199.94	200.12	200.30	200,48	200,66	200.84	201.02
92	197.60	197.78	197.96	198.14	198.32	198.50	198.68	198.86	199.04	199.22
91	195.80	195.98	196.16	196.34	196.52	196.70	196.88	197.06	197.24	197.42
90	194.00	194.18	194.36	194.54	194.72	194.90	195.08	195.26	195.44	195.62

TABLE 5.
DIFFERENCES FAHRENHEIT TO DIFFERENCES CENTIGRADE.

Fahren- heit.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
0° 1 2 3 4	c.	c.	c.	c.	c.	c.	c.	c.	c.	C.
	0.00	0.06	0.11	0.17	0.22	o.º28	0°.33	0°39	0°.44	0.50
	0.56	0.61	0.67	0.72	0.78	o.83	0.89	0.94	1.00	1.06
	1.11	1.17	1.22	1.28	1.33	1.39	1.44	1.50	1.56	1.61
	1.67	1.72	1.78	1.83	1.89	1.94	2.00	2.06	2.11	2.17
	2.22	2.28	2.33	2.39	2.44	2.50	2.56	2.61	2.67	2.72
5	2.78	2.83	2.89	2.94	3.00	3.06	3.11	3.17	3.22	3.28
6	3.33	3.39	3.44	3.50	3.56	3.61	3.67	3.72	3.78	3.83
7	3.89	3.94	4.00	4.06	4.11	4.17	4.22	4.28	4.33	4.39
8	4.44	4.50	4.56	4.61	4.67	4.72	4.78	4.83	4.89	4.94
9	5.00	5.06	5.11	5.17	5.22	5.28	5.33	5.39	5.44	5.50
10	5.56	5.61	5.67	5.72	5.78	5.83	5.89	5.94	6.00	6.06
11	6.11	6.17	6.22	6.28	6.33	6.39	6.44	6.50	6.56	6.61
12	6.67	6.72	6.78	6.83	6.89	6.94	7.00	7.06	7.11	7.17
13	7.22	7.28	7.33	7.39	7.44	7.50	7.56	7.61	7.67	7.72
14	7.78	7.83	7.89	7.94	8.00	8.06	8.11	8.17	8.22	8.28
15 16 17 18 19 20	8.33 8.89 9.44 10.00 10.56	8.39 8.94 9.50 10.06 10.61	8.44 9.00 9.56 10.11 10.67	8.50 9.06 9.61 10.17 10.72 11.28	8.56 9.11 9.67 10.22 10.78	8.61 9.17 9.72 10.28 10.83	8.67 9.22 9.78 10.33 10.89	8.72 9.28 9.83 10.39 10.94 11.50	8.78 9.33 9.89 10.44 11.00	8.83 9.39 9.94 10.50 11.06

TABLE 6.
DIFFERENCES CENTIGRADE TO DIFFERENCES FAHRENHEIT.

Centi- grade.	.0	.1	.2	.3	.4	.5	.6	.7	.8	9
0° 1 2 3 4	F. 0.00 1.80 3.60 5.40 7.20	F. 0.18 1.98 3.78 5.58 7.38	F. 0°.36 2.16 3.96 5.76 7.56	F. 0°.54 2.34 4.14 5.94 7.74	F. 0.72 2.52 4.32 6.12 7.92	F. 0.90 2.70 4.50 6.30 8.10	F. 1°08 2.88 4.68 6.48 8.28	F. 1°26 3.06 4.86 6.66 8.46	F. 1°44 3.24 5.04 6.84 8.64	F. 1.62 3.42 5.22 7.02 8.82
5 6 7 8 9	9.00 10.80 12.60 14.40 16.20	9.18 10.98 12.78 14.58 16.38	9.36 11.16 12.96 14.76 16.56	9.54 11.34 13.14 14.94 16.74	9.72 11.52 13.32 15.12 16.92	9.90 11.70 13.50 15.30 17.10	10.08 11.88 13.68 15.48 17.28	10.26 12.06 13.86 15.66 17.46	10.44 12.24 14.04 15.84 17.64	10.62 12.42 14.22 16.02 17.82

CORRECTION FOR THE TEMPERATURE OF THE EMERCENT MERCURIAL COLUMN OF THERMOMETERS.

T=t – 0.00086 n(t'-t) – Fahrenheit temperatures, T=t – 0.000155 n(t'-t) – Centigrade temperatures.

T =Corrected temperature. t =Observed temperature.

t' = Mean temperature of the glass stem and emergent mercury column.

n = Length of mercury in the emergent stem in scale degrees.

When t' is $\left\{\frac{\text{higher}}{lower}\right\}$ than t the numerical correction is to be $\left\{\frac{\text{subtracted.}}{added.}\right\}$

TABLE 7.

CORRECTION FOR FAHRENHEIT THERMOMETERS.

Values of 0.000086 n(t' - t)

n					t'-t					
	10°	20°	30°	40	50°	60°	70°	80°	90°	100°
F. 10° 20 30 40 50	F. 0.01 0.02 0.03 0.03 0.04	F. 0.02 0.03 0.05 0.07 0.09	F. 0.03 0.05 0.08 0.10 0.13	F. 0.03 0.07 0.10 0.14 0.17	F. 0.04 0.09 0.13 0.17 0.22	F. 0.05 0.10 0.15 0.21 0.26	F. 0.06 0.12 0.18 0.24 0.30	F. 0.07 0.14 0.21 0.28 0.34	F. 0.08 0.15 0.23 0.31 0.39	F. 0.09 0.17 0.26 0.34 0.43
60 70 80 90 100 110 120 130	0.05 0.06 0.07 0.08 0.09 0.09 0.10	0.10 0.12 0.14 0.15 0.17 0.10 0.21	0.15 0.18 0.21 0.23 0.26 0.28 0.31	0.21 0.24 0.28 0.31 0.34 0.38 0.41	0.26 0.30 0.34 0.39 0.43 0.47 0.52 0.56	0.31 0.36 0.41 0.46 0.52 0.57 0.62 0.67	0.36 0.42 0.48 0.54 0.60 0.66 0.72 0.78	0.41 0.48 0.55 0.62 0.69 0.76 0.83 0.90	0.46 0.54 0.62 0.70 0.77 0.85 0.93 1.01	0.52 0.60 0.69 0.77 0.86

TABLE 8.

CORRECTION FOR CENTICRADE THERMOMETERS.

Values of 0.000155 n(t'-t)

n				t'-t				
	10	20°	30°	40	50	60°	70°	80°
C.	C.	C.	C.	C.	С.	C.	C.	C,
10	0.02	0.03	0.05	0.00	0.08	0.00	0.11	0.°12
20	0.03	0.06	0.00	0.12	0.16	0.10	0.22	0.25
30	0.05	0.00	0.14	0.10	0.23	0.28	0.33	0.37
40	0.06	0.12	0.10	0.25	0.31	0.37	0.43	0.50
50	0.08	0.16	0.23	0.31	0.30	0.46	0.54	0.62
60	0.00	0.10	0.28	0.37	0.46	0.56	0.65	0.74
70	0.11	0.22	0.33	0.43	0.54	0.65	0.76	0.87
80	0.12	0.25	0.37	0.50	0.62	0.74	0.87	0.00
90	0.14	0.28	0.42	0.56	0.70	0.84	0.08	1.12
100	0.10	0.31	0.46	0.62	0.78	0.93	1.08	1.24

CONVERSIONS INVOLVING LINEAR MEASURES.

Inches into millimeters	•	•		•	•	•	•	•	•	•	•	•		٠	Table 9
Millimeters into inches						•	•			•	٠	•	•		TABLE 10
Barometric inches (merc	eur	y)	into	o m	illi	bar	S	•	•	•	•	•	•		TABLE II
Barometric millimeters	(1110	21°C1	ury) i	nto	mi	illib	ars	S .	•	•		•		TABLE 12
Feet into meters		•			•	•	•	•	•	•	•	•	•		TABLE 13
Meters into feet	4		•			•		۰	•	•	•	•		٠	TABLE 14
Miles into kilometers							•	•	•		•		•		TABLE 15
Kilometers into miles										•		٠			Table 16
Interconversion of naut	ical	ar	nd s	stat	tute	e m	ile	s							Table 17
Continental measures o	f 16	ng	th	wit	h i	the	ir 1	me	tric	aı	nd	En	glis	sh	
equivalents															TABLE 18

-	Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
		mm.	111111.	mm.							
L	0.00	0.00	0.25	0.51	0.76	1.02	1.27	1.52	1.78	2.03	2.29
ı	0.10	2.54	2.79	3.05	3.30	3.56 6.10	3.81	4.06 6.60	4.32 6.86	4.57	4.83
i.	0.20	5.08 7.62	5.33 7.87	5.59 8.13	5.84 8.38	8.64	6.35 8.89	9.14	9.40	7.11 9.65	7.37
H	0.40	10.16	10.41	10.67	10.92	11.18	11.43	11.68	11.94	12.19	12.45
İ.	0.50	12.70	12.95	13.21	13.46	13.72	13.97	14.22	14.48	14.73	14.99
	0.60	15.24	15.49	15.75	16.00	16.26	16.51	16.76	17.02	17.27	17.53
L	0.70	17.78	18.03	18.29	18.54	18.80	19.05	19.30	19.56	19.81	20.07
L	0.80	20.32	20.57	20.83	21.08	21.34	21.59	21.84	22.10	22.35	22.61
	0.90	22.86	23.11	23.37	23.62	23.88	24.13	24.38	24.64	24.89	25.15
l.	1.00	25.40	25.65	25.91	26.16	26.42	26.67	26.92	27.18	27.43	27.69
L	1.10	27.94	28.19	28.45	28.70	28.96	29.21	29.46	29.72	29.97	30.23
	1.20	30.48	30.73	30.99	31.24	31.50	31.75	32.00	32.26	32.51	32.77
	1.30 1.40	33.02 35.56	33.27 35.81	33.53 36.07	33.78 36.32	34.04 36.58	34.29 36.83	34.54 37.08	34.80 37.34	35.05 37.59	35.31
	·				38.86					}	
L	1.50 1.60	38.10 40.64	38.35 40.89	38.61	41.40	39.12 41.66	39.37 41.91	39.62 42.16	39.88 42.42	40.13	40.39
L	1.70	43.18	43.43	43.69	43.94	44.20	44.45	44.70	44.96	45.21	45.47
L	1.So	45.72	45.97	46.23	46.48	46.74	46.99	47.24	47.50	47.75	48.01
П	1.90	48.26	48.51	48.77	49.02	49.28	49.53	49.78	50.04	50.29	50.55
	2.00	50.80	51.05	51.31	51.56	51.82	52.07	52.32	52.58	52.83	53.09
	2.10	53.34	53.59	53.85	54.10	54.36	54.61	54.86	55.12	55.37	55.63
L	2.20	55.88	56.13	56.39	56.64	56.90	57.15	57.40	57.66	57.91	58.17
Н	2.30	58.42	58.67	58.93	59.18	59.44	59.69	59.94	60.20	60.45	60.71
ı	2.40	60.96	61.21	61.47	61.72	61.98	62.23	62.48	62.74	62.99	63.25
П	2.50	63.50	63.75	64.01	64.26	64.52	64.77	65.02	65.28	65.53	65.79
Ш	2.60	66.04	66.29 68.83	66.55	66.80	67.06 69.60	67.31	67.56	67.82	68.07	68.33
II.	2.70 2.80	68.58	71.37	71.63	69.34 71.88	72.14	69.85	70.10	70.36	70.61	70.87
	2.90	73.66	73.91	74.17	74.42	74.68	74.93	75.18	75.44	75.69	75.95
ı	3.00	76.20	76.45	76.71	76.96	77.22	77.47	77.72	77.98	78.23	78.49
L	3.10	78.74	78.99	79.25	79.50	79.76	So.01	So.26	80.52	80.77	81.03
	3.20	81.28	81.53	81.79	\$2.04	82.30	82.55	82.80	83.06	83.31	83.57
li.	3.30	83.82	84.07	84.33	84.59	84.84	85.09	85.34	85.60	85.85	86.11
	3.40	86.36	86.61	86.87	87.12	87.38	87.63	87.88	88.14	88.39	88.65
1	3.50	88.90	89.15	89.41	89.66	89.92	90.17	90.42	90.68	90.93	91.19
1	3.60	91.44	91.69	91.95	92.20	92.46	92.71	92.96	93.22	93.47	93.73
	3.70 3.80	93.98 96.52	94.23	94.49	94.74 97.28	95.00 97.54	95.25 97.79	95.50 98.04	95.76 98.30	96.01	96.27 98.81
	3.90	99.06	99.31	99.57	99.82	100.08	100.33	100.58	100.84	101.09	101.35
	4.00	101.60	101.85	102.11	102.36	102.62	102.87	103.12	103.38	103.63	103.89
	4.10	101.00	104.39	104.65	102.30	102.02	102.37	103.12	103.30	103.03	103.39
	4.20	106.68	106.93	107.19	107.44	107.70	107.95	108.20	108.46	108.71	108.97
	4.30	109.22	109.47	109.73	109.98	110,24	110.49	110.74	111.00	111.25	111.51
	4.40	111.76	112.01	112.27	112.52	112.78	113.03	113.28	113.54	113.79	114.05
	4.50	114.30	114.55	114.81	115.06	115.32	115.57	115.82	116.08	116.33	116.59
	4.60	116.84	117.09	117.35	117.60	117.86	118.11	118.36	118.62	118.87	119.13
	4.70 4.80	119.38	119.63	119.89	120.14	120.40	120.65	120.90	121.16	121.41	121.67
	4.90	124.46	124.71	124.97	125.22	122.94	123.19	123.44	123.70	123.95	124.21
	5.00	127.00	127.25	127.51	127.76	128.02	128.27	128.52	128.78	129.03	129.29
-											
	Proport	ional Part	s. Inch.				0.00		0.007		0.009
			mm.	0.025	0.051	0.076 0.	102 0.12	7 0.152	0.178	0.203	0.229

Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
5.00 5.10 5.20 5.30	mm. 127.00 129.54 132.08 134.62	mm. 127.25 129.79 132.33 134.87	mm. 127.51 130.05 132.59 135.13 137.67	mm. 127.76 130.30 132.84 135.38 137.92	mm. 128.02 130.56 133.10 135.64 138.18	mm. 128.27 130.81 133.35 135.89 138.43	mm. 128.52 131.06 133.60 136.14 138.68	mm. 128.78 131.32 133.86 136.40 138.94	mm. 129.03 131.57 134.11 136.65 139.19	mm. 129.29 131.83 134.37 136.91 139.45
5.40 5.50 5.60 5.70 5.80 5.90	137.16 139.70 142.24 144.78 147.32 149.86	137.41 139.95 142.49 145.03 147.57 150.11	140.21 142.75 145.29 147.83 150.37	140.46 143.00 145.54 148.08 150.62	140.72 143.26 145.80 148.34 150.88	140.97 143.51 146.05 148.59 151.13	141.22 143.76 146.30 148.84 151.38	141.48 144.02 146.56 149.10 151.64	141.73 144.27 146.81 149.35 151.89	141.99 144.53 147.07 149.61 152.15
6.00 6.10 6.20 6.30 6.40	152.40 154.94 157.48 160.02 162.56	152.66 155.19 157.73 160.27 162.81	152.91 155.45 157.99 160.53 163.07	153.16 155.70 158.24 160.78 163.32	153.42 155.96 158.50 161.04 163.58	153.67 156.21 158.75 161.29 163.83	153.92 156.46 159.00 161.54 164.08	154.18 156.72 159.26 161.80 164.34	154.43 156.97 159.51 162.05 164.59	154.69 157.23 159.77 162.31 164.85
6.50 6.60 6.70 6.80 6.90	165.10 167.64 170.18 172.72 175.26	165.35 167.89 170.43 172.97 175.51	165.61 168.15 170.69 173.23 175.77	165.86 168.40 170.94 173.48 176.02	166.12 168.66 171.20 173.74 176.28	166.37 168.91 171.45 173.99 176.53	166.62 169.16 171.70 174.24 176.78	166.88 169.42 171.96 174.50 177.04	167.13 169.67 172.21 174.75 177.29	167.39 169.93 172.47 175.01 177.55
7.00 7.10 7.20 7.30 7.40	177.80 180.34 182.88 185.42 187.96	178.05 180.59 183.13 185.67 188.21	178.31 180.85 183.39 185.93 188.47	178.56 181.10 183.64 186.18 188.72	178.82 181.36 183.90 186.44 188.98	179.07 181.61 184.15 186.69 189.23	179.32 181.86 184.40 186.94 189.48	179.58 182.12 184.66 187.20 189.74	179.83 182.37 184.91 187.45 189.99	180.09 182.63 185.17 187.71 190.25
7.50 7.60 7.70 7.80 7.90	190.50 193.04 195.58 198.12 200.66	190.75 193.29 195.83 198.37 200.91	191.01 193.55 196.09 198.63 201.17	191.26 193.80 196.34 198.88 201.42	191.52 194.06 196.60 199.14 201.68	191.77 194.31 196.85 199.39 201.93	192.02 194.56 197.10 199.64 202.18	192.28 194.82 197.36 199.90 202.44	192.53 195.07 197.61 200.15 202.69	192.79 195.33 197.87 200.41 202.95
8.00 8.10 8.20 8.30 8.40	203.20 205.74 208.28 210.82 213.36	203.45 205.99 208.53 211.07 213.61	203.71 206.25 208.79 211.33 213.87	203.96 206.50 209.04 211.58 214.12	204.22 206.76 209.30 211.84 214.38	204.47 207.01 209.55 212.09 214.63	207.26 209.80 212.34	204.98 207.52 210.06 212.60 215.14	205.23 207.77 210.31 212.85 215.39	205.49 208.03 210.57 213.11 215.65
8.50 8.60 8.70 8.80 8.90	215.90 218.44 220.98 223.52 226.06	216.15 218.69 221.23 223.77 226.31	216.41 218.95 221.49 224.03 226.57	216.66 219.20 221.74 224.28 226.82	216.92 219.46 222.00 224.54 227.08	219.71 222.25 224.79	219.96 222.50 225.04	220.22 222.76 225.30	217.93 220.47 223.01 225.55 228.09	218.19 220.73 223.27 225.81 228.35
9.00 9.10 9.20 9.30 9.40	228.60 231.14 233.68 236.22 238.76	228.85 231.39 233.93 236.47 239.01	234.19 236.73 239.27	231.90 234.44 236.98 239.52	229.62 232.16 234.70 237.24 239.78	232.41 234.95 237.49	232.66 235.20 237.74 240.28	232.92 235.46 238.00 240.54	235.71 238.25 240.79	230.89 233.43 235.97 238.53 241.05
9.50 9.60 9.70 9.80 9.90	241.30 243.84 246.38 248.92 251.46	244.09 246.63 249.17	244.35 246.89 249.43	244.60 247.14 249.68	244.86 247.40 249.94	245.11 247.65 250.19 252.73	245.36 247.90 250.44 252.98	245.62 248.16 250.70 253.24	245.87 248.41 250.95 253.49	248.67 251.2 253.7
10.00	254.00	Tne	<u></u>		1	1	255-52	1	0.008	0.009

Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
	mm.	mm.	mm.	mm.	mm.	mm.	mm,	mm.	mm.	mm.
10.00	254.00	254.25	254.51	254.76	255.02	255.27	255.52	255.78	256.03	256.29
10.10	256.54 259.08	256.79 259.33	257.05 259.59	257.30 259.84	257.56	257.81 260.35	258.06 260.60	258.32 260.86	258.57	258.83
10.30	261.62	261.87	262.13	262.38	262.64	262.89	263.14	263.40	263.65	263.91
10.40	264.16	264.41	264.67	264.92	265.18	265.43	265.68	265.94	266.19	266.45
10.50	266.70	266.95	267.21	267.46	267.72	267.97	268.22	268.48	268.73	268.99
10.60	269.24	269.49	269.75	270.00	270.26	270.51	270.76	271.02	271.27	271.53
10.70 10.80	271.78	272.03 274.57	272.29	272.54 275.08	272.So 275.34	273.05 275.59	273.30 275.84	273.56	273.81 276.35	276.61
10.90	276.86	277.11	277.37	277.62	277.88	278.13	278.38	278.64	278.89	279.15
11.00	279.40	279.65	279.91	280.16	280.42	2So.67	280.92	281.18	281.43	281.69
II.IG	281.94	282.19	282.45	282.70	282.96	283.21	283.46	283.72 286.26	283.97 286.51	284.23 286.77
11,20 11,30	284.48 287.02	284.73 287.27	284.99 287.53	285.24 287.78	285.50 288.04	285.75 288.29	288.54	288.80	289.05	289.31
11.40	289.56	289.81	290.07	290.32	290.58	290.83	291.08	291.34	291.59	291.85
11.50	292.10	292.35	292.61	292.86	293.12	293.37	293.62	293.88	294.13	294.39
11.60	294.64	294.89	295.15	295.40	295.66	295.91	296.16 298.70	296.42 298.96	296.67	296.93
11.70 11.80	297.18 299.72	297.43	297.69 300.23	297.94 300.48	300.74	298.45 300.99	301.24	301.50	301.75	299.47 302.01
11.90	302.26	302.51	302.77	303.02	303.28	303.53	303.78	304.04	304.29	304.55
12.00	304.80	305.05	305.31	305.56	305.82	306.07	306.32	306.58	306.83	307.09
12.10	307.34	307.59	307.85	308.10	308.36	308.61	308.86	309.12	309.37	309.63
12.20	309.88	310.13	310.39	310.64	310.90	311.15	311.40	311.66	314.45	312.17
12.40	314.96	315.21	315.47	315.72	315.98	316.23	316.48	316.74	316.99	317.25
12.50	317.50	317.75	318.01	318.26	318.52	318.77	319.02	319.28	319.53	319.79
12.60	320.04	320.29	320.55	320.80	321.06	321.31	321.56	321.82	322.07	322.33
12.70 12.80	322.58 325.12	322.83 325.37	323.09 325.63	323.34 325.88	323.60	323.85	324.10	324.36	324.61	324.87
12.90	327.66	327.91	328.17	328.42	328.68	328.93	329.18	329.44	329.69	329.95
13.00	330.20	330.45	330.71	330.96	331.22	331.47	331.72	331.98	332.23	332.49
13.10 13.20	332.74	332.99	333-25	333.50	333.76	334.01	334.26 336.80	334·52 337.06	334·77 337·31	335.03
13.30	335.28 337.82	335·53 338.07	335·79 338.33	338.58	338.84	339.09	339.34	339.60	339.85	337·57 340.11
13.40	340.36	340.61	340.87	341.12	341.38	341.63	341.88	342.14	342.39	342.65
13.50	342.90	343.15	343.41	343.66	343.92	344.17	344.42	344.68	344.93	345.19
13.60	345.44	345.69	345.95	346.20	346.46	346.71	346.96	347.22	347-47	347.73
13.70 13.80	347.98 350.52	348.23	348.49	348.74	349.00 351.54	349.25 351.79	349.50	349.76	350.01 352.55	350.27 352.81
13.90	353.06	353.31	353-57	353.82	354.08	354.33	354.58	354.84	355.09	355-35
14.00	355.60	355.85	356.11	356.36	356.62	356.87	357.12	357.38	357.63	357.89
14.10	358.14	358.39	358.65	358.90	359.16	359.41	359.66	359.92	360.17	360.43
14.20 14.30	360.68 363.22	360.93 363.47	361.19	361.44	361.70	361.95 364.49	362.20	362.46	362.71 365.25	362.97 365.51
14.40	365.76	366.01	366.27	366.52	366.78	367.03	367.28	367.54	367.79	368.05
14.50	368.30	368.55	368.81	369.06	369.32	369.57	369.82	370.08	370.33	370.59
14.60	370.84	371.09	371.35	371.60	371.86	372.11	372.36	372.62	372.87	373.13
14.70 14.80	373.38 375.92	373.63	373.89	374.14	374.40	374.65	374.90	375.16	375.41	375.67 378.21
14.90	378.46	378.71	378.97	379.22	379.48	379.73	379.98	380.24	380.49	380.75
15.00	381.00	381.25	381.51	381.76	382.02	382.27	382.52	382.78	383.03	383.29
Propo	rtional Pa	rts. Incl				.004 0.00	_	0.007 0.178		0.009

Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
15.00 15.10 15.20 15.30 15.40	mm. 381.00 383.54 386.08 388.62 391.16	mm. 381.25 383.79 386.33 388.87 391.41	mm. 381.51 384.05 386.59 389.13 391.67	mm. 381.76 384.30 386.84 389.38 391.92	mm. 382.02 384.56 387.10 389.64 392.18	mm. 382.27 384.81 387.35 389.89 392.43	mm. 382.52 385.06 387.60 390.14 392.68	mm. 382.78 385.32 387.86 390.40 392.94	mm. 383.03 385.57 388.11 390.65 393.19	nim. 383.29 385.83 388.37 390.91 393.45
15.50	393.70	393.95	394.21	394.46	394.72	394.97	395.22	395.48	395.73	395.99
15.60	396.24	39.649	396.75	397.00	397.26	397.51	397.76	398.02	398.27	398.53
15.70	398.78	399.03	399.29	399.54	399.80	400.05	400.30	400.56	400.81	401.07
15.80	401.32	401.57	401.83	402.08	402.34	402.59	402.84	403.10	403.35	403.61
15.90	403.86	404.11	404.37	404.62	404.88	405.13	405.38	405.64	405.89	406.15
16.00	406.40	406.65	406.91	407.16	407.52	407.67	407.92	408.18	408.43	408.69
16.10	408.94	409.19	409.45	409.70	409.96	410.21	410.46	410.72	410.97	411.23
16.20	411.48	411.73	411.99	412.24	412.50	412.75	413.00	413.26	413.51	413.77
16.30	414.02	414.27	414.53	414.78	415.04	415.29	415.54	415.80	416.05	416.31
16.40	416.56	416.81	417.07	417.32	417.58	417.83	418.08	418.34	418.59	418.85
16.50	419.10	419.35	419.61	419.86	420.12	420.37	420.62	420.88	421.13	421.39
16.60	421.64	421.89	422.15	422.40	422.66	422.91	423.16	423.42	423.67	423.93
16.70	424.18	424.43	424.69	424.94	425.20	425.45	425.70	425.96	426.21	426.47
16.80	426.72	426.97	427.23	427.48	427.74	427.99	428.24	428.50	428.75	429.01
16.90	429.26	429.51	429.77	430.02	430.28	430.53	430.78	431.04	431.29	431.55
17.00	431.80	432.05	432.31	432.56	432.82	433.07	433.32	433.58	433.83	434.09
17.10	434.34	434.59	434.85	435.10	435.36	435.61	435.86	436.12	436.37	436.63
17.20	436.88	437.13	437.39	437.64	437.90	438.15	438.40	438.66	438.91	439.17
17.30	439.42	439.67	439.93	440.18	440.44	440.69	440.94	441.20	441.45	441.71
17.40	441.96	442.21	442.47	442.72	442.98	443.23	443.48	443.74	443.99	444.25
17.50	444.50	444.75	445.01	445.26	445.52	445.77	446.02	446.28	446.53	446.79
17.60	447.04	447.29	447.55	447.80	448.06	448.31	448.56	448.82	449.07	449.33
17.70	449.58	449.83	450.09	450.34	450.60	450.85	451.10	451.36	451.61	451.87
17.80	452.12	452.37	452.63	452.88	453.14	453.39	453.64	453.90	454.15	454.41
17.90	454.66	454.91	455.17	455.42	455.68	455.93	456.18	456.44	456.69	456.95
18.00	457.20	457.45	457.71	457.96	458.22	458.47	458.7 2	458.98	459.23	459.49
18.10	459.74	459.99	460.25	460.50	460.76	461.01	461.26	461.52	461.77	462.03
18.20	462.28	462.53	462.79	463.04	463.30	463.55	463.80	464.06	464.31	464.57
18.30	464.82	465.07	465.33	465.58	465.84	466.09	466.34	466.60	466.85	467.11
18.40	467.36	467.61	467.87	468.12	468.38	468.63	468.88	469.14	469.39	469.35
18.50	469.90	470.15	470.41	470.66	470.92	471.17	471.42	471.68	471.93	472.19
18.60	472.44	472.69	472.95	473.20	473.46	473.71	473.96	474.22	474.47	474.73
18.70	474.98	475.23	475.49	475.74	476.00	476.25	476.50	476.76	477.01	477.27
18.80	477.52	477.77	478.03	478.28	478.54	478.79	479.04	479.30	479.55	479.81
18.90	480.06	480.31	480.57	480.82	481.08	481.33	481.58	481.84	482.09	482.35
19.00	482.60	482.85	483.11	483.36	483.62	483.87	484.12	484.38	484.63	484.89
19.10	485.14	485.39	485.65	485.90	486.16	486.41	486.66	486.92	487.17	487.43
19.20	487.68	487.93	488.19	488.44	488.70	488.95	489.20	489.46	489.71	489.97
19.30	490.22	490.47	490.73	490.98	491.24	491.49	491.74	492.00	492.25	492.51
19.40	492.76	493.01	493.27	493.52	493.78	494.03	494.28	494.54	494.79	495.05
19.50	495.30	495.55	495.81	496.06	496.32	496.57	496.82	497.08	497.33	497.59
19.60	497.84	498.09	498.35	498.60	498.86	499.11	499.36	499.62	499.87	500.13
19.70	500.38	500.34	500.89	501.14	501.40	501.65	501.91	502.16	502.41	502.67
19.80	502.92	503.18	503.43	503.68	503.94	504.19	504.45	504.70	504.95	505.21
19.90	505.46	505.72	505.97	506.22	506.48	506.73	506.99	507.24	507.49	507.75
Propos	508.00	508.26		0.002	-	509.27 .004 0.00	-	0.007 0.178		510.29

Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
	mm.	mm.	mm.	mm.	111111.	mm.	mm.	mm.	mm.	mm.
20.00	508.00	508.26	508.51	508.76	509.02	509.27	509.53	509.78	510.03	510.29
20.10 20.20	510.54 513.08	510.80	511.05	511.30	511.56	511.81	512.07	512.32	512.57	512.83
20.20	515.62	513.34 515.88	513.59	516.38	514.10	514.35 516.89	514.61	517.40	517.65	515.37
20.40	518.16	518.42	518.67	518.92	519.18	519.43	519.69	519.94	520.19	520.45
20.50	520.70	520.96	521.21	521.46	521.72	521.97	522.23	522.48	522.73	522.99
20.60	523.24	523.50	523.75	524.00	524.26	524.51	524.77	525.02	525.27	525.53
20.70 20.80	525.78	526.04	526.29	526.54	526.80	526.95	527.31	527.56	527.81	528.07
20.90	528.32 530.86	528.58 531.12	528.83 531.37	529.08 531.62	529.34 531.88	529.59 532.13	529.85	530.10 532.64	530.35	530.61
21.00	533.40	533.66	533.91	534.16	534.42	534.67	534.93	535.18	535.43	535.69
21.10	535.4	536.20	536.45	536.70	536.96	537.21	537.47	537.72	537.98	538.23
21.20	538.48	538.74	538.99	539.24	539.50	539.75	540.01	540.26	540.51	540.77
21.30	541.02	541.28	541.53	541.78	542.04	542.29	542.55	542.80	543.05	543.31
21.40	543.56	543.82	544.07	544.32	544.58	544.83	545.09	545.34	545.59	545.85
21.50 21.60	546.10 548.64	546.36 548.90	546.61	546.86 549.40	547.12 549.66	547·37 549·91	547.63 550.17	547.88 550.42	548.13	548.39
21.70	551.18	551.44	551.69	551.94	552.20	552.45	552.71	552.96	553.21	553.47
21.80	553.72	553.98	554.23	554.48	554.74	554.99	555.25	555.50	555.75	556.01
21.90	556.26	556.52	556.77	557.02	557.28	557-53	557.79	558.04	558.29	558.55
22.00	558.80	559.06	559.31	559.56	559.82	560.07	560.03	560.58	560.83	561.09
22.10	561.34 563.88	561.60 564.14	561.85	562.10 564.64	562,36 564.90	562.61	562.87	563.12 565.66	563.37	563.63
22.30	566.42	566.68	566.93	567.18	567.44	565.15 567.69	565.41	568.20	565.91 568.45	566.17
22.40	568.96	569.22	569.47	569.72	569.98	570.23	570.49	570.74	570.99	571.25
22.50	571.50	571.76	572.01	572.26	572.52	572.77	573.03	573.28	573-53	573.79
22.60	574.04	574.30	574.55	574.80	575.06	575.31	575-57	575.82	576.07	576.33
22.70 22.80	576.58 579.12	576.84	577.09	577.34	577.60 580.14	577-95	578.11 580.65	578.36 580.90	578.61 581.15	578.87
22.90	581.66	579.38 581.92	579.63 582.17	579.88 582.42	582.68	580.39 582.93	583.19	583.44	583.69	581.41
23.00	584.20	584.46	584.71	584.96	585.22	585.47	585.73	585.98	586.23	586.49
23.10	586.74	587.00	587.25	587.50	587.76	588.01	588.27	588.52	588.77	589.03
23.20	589.28	589.54	589.79	590.04	590.30	590.55	590.81	591.06	591.31	591.57
23.30 23.40	591.82 594.36	592.08 594.62	592.33 594.87	592.58 595.12	592.84 595.38	593.09	593-35 595.89	593.60	593.85 596.39	594.11
23.50	596.90	597.16		597.66	1			598.68		
23.60	599.44	599.70	597.41	600.20	597.92 600.46	598.17	598.43	601.22	598.93 601.47	599.19
23.70	601.98	602.24	602.49	602.74	603.00	603.25	603.51	603.76	604.01	604.27
23.80	604.52	604.78	605.03	605.28	605.54 608.08	605.79	606.05	606.30	606.55	606.81
23.90	607.06	607.32	607.57	607.82		608.33	608.59	608.84	609.09	609.35
24.00 24.10	609.60	609.86	610.11	610.36	610.62	610.87 613.41	611.13	611.38	611.63	611.89
24.20	614.68	614.94	615.19	615.44	615.70	615.95	616.21	616.46	616.71	614.43
24.30	617.22	617.48	617.73	617.98	618.24	618.49	618.75	619.00	619.25	619.51
24.40	619.76	620.02	620.27	620.52	620.78	621.03	621.29	621.54	621.79	622.05
24.50	622.30	622.56	622.81	623.06	623.32	623.57	623.83	624.08	624.33	624.59
24.00	624.84	627.64	625.35 627.89	625.60	625.86	628.65	626.37 628.91	626.62	626.S7 629.41	627.13
24.So	629.92	630.18	630.43	630.68	630.94	631.19	631.45	631.70	631.95	632.21
24.90	632.46	632.72	632.97	633.22	633.48	633.73	633.99	634.24	634.49	634.75
25.00	635.00	635.26	635.51	635.76	636.02	636.27	636.53	636.78	637.03	637.29
Proport	lional Par	is. Inch				0.00		0.007 0.178		.009

Inches.	.00	10.	.02	.03	.04	.05	.06	.07	.08	.09
25.00 25.10 25.20 25.30 25.40	mm. 635.00 637.54 640.08 642.62 645.16	mm. 635.26 637.80 640.34 642.88 645.42	mm. 635.51 638.05 640.59 643.13 645.67	mm. 635.76 638.30 640.84 643.38 645.92	mm. 636.02 638.56 641.10 643.64 646.18	mm. 636.27 638.81 641.35 643.89 646.43	mm. 636.53 639.07 641.61 644.15 646.69	mm. 636.78 639.32 641.86 644.40 646.94	mm. 637.03 639.57 642.11 644.65 647.19	mm. 637.29 639.83 642.37 644.91 647.45
25.50 25.60 25.70 25.80 25.90 26.00	647.70 650.24 652.78 655.32 657.86	647.96 650.50 653.04 655.58 658.12 660.66	648.21 650.75 653.29 655.83 658.37	648.46 651.00 653.54 656.08 658.62 661.16	648.72 651.26 653.80 656.34 658.88 661.42	648.97 651.51 654.05 656.59 659.13	649.23 651.77 654.31 656.85 659.39 661.93	649.48 652.02 654.56 657.10 659.64 662.18	649.73 654.27 654.81 657.35 659.89 662.43	649.99 652.53 655.07 657.61 660.15
26.10 26.20 26.30 26.40 26.50	662.94 665.48 668.02 670.56	663.20 665.74 668.28 670.82	663.45 665.99 668.53 671.07	663.70 666.24 668.78 671.32	663.96 666.50 669.04 671.58	664.21 666.75 669.29 671.83	664.47 667.01 669.55 672.09	664.72 667.26 669.80 672.34 674.88	664.97 667.51 670.05 672.59	665.23 667.77 670.31 672.85 675.39
26.60 26.70 26.80 26.90 27.00	675.64 678.18 680.72 683.26 685.80	675.90 678.44 680.98 683.52 686.06	676.15 678.69 681.23 683.77 686.31	676.40 678.94 681.48 684.02 686.56	676.66 679.20 681.74 684.28	676.91 679.45 681.99 684.53	677.17 679.71 682.25 684.79	677.42 679.96 682.50 685.04 687.58	677.67 680.21 682.75 685.29 687.83	677.93 680.47 683.01 685.55 688.09
27.10 27.20 27.30 27.40 27.50 27.60	688.34 690.88 693.42 695.96 698.50 701.04	688.60 691.14 693.68 696.22 698.76 701.30	688.85 691.39 693.93 696.47 699.01 701.55	689.10 691.64 694.18 696.72 699.26 701.80	689.36 691.90 694.44 696.98 699.52 702.06	689.61 692.15 694.69 697.23 699.77 702.31	689.87 692.41 694.95 697.49 700.03 702.57	690.12 692.66 695.20 697.74 700.28 702.82	690.37 692.91 695.45 697.99 700.53 703.07	690.63 693.17 695.71 698.25 700.79
27.70 27.80 27.90 28.00 28.10	703.58 706.12 708.66 711.20 713.74	703.84 706.38 708.92 711.46 714.00	704.09 706.63 709.17 711.71 714.25	704.34 706.88 709.42 711.96 714.50	704.60 707.14 709.68 712.22 714.76	704.85 707.39 709.93 712.47 715.01	705.11 707.65 710.19 712.73 715.27	705.36 707.90 710.44 712.98 715.52	705.61 708.15 710.69 713.23 715.77	705.87 708.41 710.95 713.49 716.03
28.20 28.30 28.40 28.50 28.60	716.28 718.82 721.36 723.90 726.44	716.54 719.08 721.62 724.16 726.70	716.79 719.33 721.87 724.41 726.95	717.04 719.58 722.12 724.66 727.20	717.30 719.84 722.39 724.92 727.46	717.55 720.09 722.63 725.17 727.71	717.81 720.35 722.89 725.43 727.97	718.06 720.60 723.14 725.68 728.22	718.31 720.85 723.39 725.93 728.47	718.57 721.11 723.65 726.19 728.73
28.70 28.80 28.90 29.00 29.10 29.20	728.98 731.52 734.06 736.60 739.14	729.24 731.78 734.32 736.86 739.40	729.49 732.03 734.57 737.11 739.65	729.74 732.28 734.82 737.36 739.90	730.00 732.54 735.08 737.62 740.16	730.25 732.79 735.33 737.87 740.41	730.51 733.05 735.59 738.13 740.67	730.76 733.30 735.84 738.38 740.92	731.01 733.55 736.09 738.63 741.17	731.27 733.81 736.35 738.89 741.43
29.20 29.30 29.40 29.50 29.60 29.70	741.68 744.22 746.76 749.30 751.84 754.38	741.94 744.48 747.02 749.56 752.10 754.64	742.19 744.73 747.27 749.81 752.35 754.89	742.44 744.98 747.52 750.06 752.60 755.14	742.70 745.24 747.78 750.32 752.86 755.40	742.95 745.49 748.03 750.57 753.11 755.65	743.21 745.75 748.29 750.83 753.37 755.91	743.46 746.00 748.54 751.08 753.62 756.16	743.71 746.25 748.79 751.33 753.87 756.41	743.97 746.51 749.05 751.59 754.13 756.67
29.80 29.90 30.00	756.92 759.46 762.00	757.18 759.72 762.26	757.43 759.97 762.51	757.68 760.22 762.76	757.94 760.48 763.02	758.19 760.73 763.27	758.45 760.99 763.53	758.70 761.24 763.78	758.95 761.49 764.03	759.21 761.75 764.29
Propo	tional Par	ts. Incl			_	.102 0.12	-	0.007		0.009

TABLE 9.

INCHES INTO MILLIMETERS.

1 inch = 25.40005 mm.

Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
	mm.	mm.	mm.	mm.	111111.	mm.	1111111.	mm.	mm.	mm.
30.00	762.00	762.26	762.51	762.76	763.02	763.27	763.53	763.78	764.03	764.29
30.10	764.54	764.80	765.05	765.30	765.56	765.81	766.07	766.32	766.57	766.83
30.20	767.08	767.34	767.59	767.84	768.10	768.35	768.61	768.86	769.11	769.37
30.30	769.62	769.88	770.13	770.38	770.64	770.89	771.15	771.40	771.65	771.91
30.40	772.16	772.42	772.67	772.92	773.18	773.43	773.69	773.94	774.19	774.45
30.50	774.70	774.96	775.21	775.46	775.72	775.97	776.23	776.48	776.73	776.99
30.60	777.24	777.50	777.75	778.00	778.26	778.51	778.77	779.02	779.27	779.53
30.70	779.78	780.04	780.29	780.54	780.80	781.05	781.31	781.56	781.81	782.07
30.80	782.32	782.58	782.83	783.08	783.34	783.59	783.85	784.10	784.35	784.61
30.90	784.86	785.12	785.37	785.62	785.88	786.13	786.39	786.64	786.89	787.15
31.00	787.40	787.66	787.91	788.16	788.42	788.67	788.93	789.18	789.43	789.69
31.10	789.94	790.20	790.45	790.70	790.96	791.21	791.47	791.72	791.97	792.23
31.20	792.48	792.74	792.99	793.24	793.50	793.75	794.01	794.26	794.51	794.77
31.30	795.02	795.28	795.53	795.78	796.04	796.29	796.55	796.80	797.05	797.31
31.40	797.56	797.82	798.07	798.32	798.58	798.83	799.09	799.34	799.59	799.85
31.50	\$00.10	800.36	Soo.61	800.86	Soi.12	801.37	801.63	So1.88	802.13	802.39
31.60	\$02.64	802.90	So3.15	803.40	Soj.66	803.91	804.17	So4.42	804.67	804.93
31.70	\$05.18	805.44	So5.69	805.94	Soi.20	806.45	806.71	So6.96	807.21	807.47
31.80	\$07.72	807.98	So8.23	808.48	Soi.74	808.99	809.25	So9.50	809.75	810.01
31.90	\$10.26	810.52	S10.77	811.02	Sii.28	811.53	811.79	S12.04	812.29	812.55
Propo	Proportional Parts. Inch. 0.001 0.002 0.003 0.004 0.005 0.006 0.007 0.008 0.009 mm. 0.025 0.051 0.076 0.102 0.127 0.152 0.178 0.203 0.229									

Milli- meters.	0	1	2	3	4	5	6	7	8	9
	Inches.	Inches.	Inches.	Inches	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
0	0.0000	0.0394	0.0787	0.1181	0.1575	0.1968	0.2362	0.2756	0.3150	0.3543
10	0.3937	0.4331	0.4724	0.5118		0.5906	0.6299	0.6693	0.7087	0.7480
20	0.7874	0.8268	0.8661	0.9055		0.9842	1.0236	1.0630		1.1417
30	1.1811	1.2205	1.2598	1.2992		1.3780	1.4173	1.4567		1.5354
40	1.5748	1.6142	1.6535	1.6929	1.7323	1.7716	1,8110	1.8504	1.8898	1.9291
50	1.9685	2.0079	2.0472	2.0866	2.1260	2.1654	2.2047	2.2441		2.3228
60	2.3622	2.4016	2.4409	2.480		2.5590	2.5984	2.6378	2.6772	2.7165
70	2.7559	2.7953	2.8346	2.8740		2.9528	2.9921	3.0315		3.1102
80	3.1496	3.1890	3.2283	3.267		3.3464	3.3858	3.4252		3.5039
90	3.5433	3.5828	3.6220	3.6612	3.7008	3.7402	3.7795	3.8189	3.8583	3.8976
100	3.9370	3.9764	4.0157	4.055		4.1338	4.1732	4.2126		4.2913
110	4.3307	4.3701	4.4094	4.4488		4.5276	4.5669	4.6063		4.6850
120	4.7244	4.7638	4.8031	4.842		4.9212	4.9606	5.0000		5.0787
130	5.1181	5.1575	5.1968	5.2362		5.3150	5.3543	5.3937	5.4331 5.8268	5.4724
140	5.5118	5.5512	5.5905	5.6299	5.6693	5.7086	5.7480	5.7874	5.0200	5.0001
150	5.9055	5.9449	5.9842	6.0230		6.1024	6.1417	6.1811		6.2598
160	6.2992	6.3386	6.3779	6.417		6.4960	6.5354	6.5748		6.6535
170	6.6929	6.7323	6.7716	6.8110	0	6.8898	6.9291	6.9685		7.0472
180	7.0866	7.1260	7.1653	7.204	1 2 1 0	7.2834	7.3228	7.3622		7.4409
190	7.4803	7.5197	7.5590	7.598	7.6378	7.6772	7.7165	7.7559	7.7953	7.8346
200	7.8740	7.9134	7.9527	7.992	8.0315	8.0708	8.1102	8.1496	8.1890	8.2283
210	8.2677	8.3071	8.3464	8.3858		8.4646	8.5039	8.5433		8.6220
220	8.6614	8.7008	8.7401	8.779	5 8.8189	8.8582	8.8976	8.9370	8.9764	9.0157
230	9.0551	9.0945	9.1338	9.173		9.2520	9.2913	9.3307	1 0	9.4094
240	9.4488	9.4882	9.5275	9.566	9.6063	9.6456	9.6850	9.7244	9.7638	9.8031
250	9.8425	9.8819	9.9212	9.960	0.0000	10.0394	10.0787	10.1181	10.1575	10.1968
260		10.2756		10.354			10.4724			
270	10.6299	10.6693	10.7086	10.748	10.7874	10.8268	10.8661	10.9055	10.9449	10.9842
				11.141					11.3338	11.3779
290	11.4173	11.4568	11.4960	11.535	1 11.5748	11.6142	11.6535	11.6929	11.7323	11.7716
300	11.8110	11.8504	11.8897	11.929	11.9685	12.0078	12.0472	12.0866	12.1260	12.1653
310	12.2047	12.2441	12.2834		12.3622				12.5197	
320		12.6378	12.6771	12.716	12.7559	12.7952	12.8346	12.8740	12.9134	12.9527
330			13.0708	13.110			13.2283			13.3464
340	13.3858	13.4252	13.4645	13.503	13.5433	13.5826	13.6220	13.6614	13.7008	13.7401
350	13.7795	13.8189	13.8582	13.8976	5 13.9370	13.9764	14.0157	14.0551	14.0945	14.1338
360	14.1732	14.2126	14.2519	14.291	3 14.3307	14.3700	14.4094	14.4488	14.4882	
370	10 2	14.6063	1	14 685		14.7638		14.8425		
		15.0000	15.0393	15.078			15.1968			
390	15.3543	15.3937	15.4330	15.472	4 15.5118	15.5512	15.5905	15.6299	15.6693	15.7086
400	15.7480	15.7874	15.8267	15.866	1 15.9055	15.9448	15.9842	16.0236	16.0630	16.1023
		Tenth	s of a mill	imeter.			Hundred	ths of a r	nillimeter.	
	mm.	Inch	ı. m	ım.	Inch.	mm.	Inch	, n	ım.	Inch.
	0.1	0.003		0.6	0.0236	0.01	0,000		.06	0.0024
	.2	.007	*	.7	.0676	.02	,000		.07	.0028
	-3	.011		.s	.0315	.03	.001		.08	.0031
	-4	.015		.9	.0354	.04	.001		.09	.0035
	∙5	.019	97	0.1	.0394	.05	.002	0	.10	.0039
		1					1		!	

Milli- meters.	.0	. 1	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.									
400	15.748	15.752	15.756	15.760	15.764	15.768	15.772	15.776	15.779	15.783
40I 402	15.787 15.827	15.791 15.831	15.795 15.835	15.799 15.839	15.803	15.807 15.846	15.811	15.815	15.819	15.823 15.862
403	15.866	15.870	15.874	15.878	15.882	15.886	15.890	15.894	15.898	15.902
404	15.905	15.909	15.913	15.917	15.921	15.925	15.929	15.933	15.937	15.941
405 406	15.945 15.984	15.949	15.953 15.992	15.957 15.996	15.961 16.000	15.965 16.004	15.968 16.008	15.972 16.012	15.976 16.016	15.980 16.020
407	16.024	15.988 16.028	16.031	16.035	16.039	16.043	16.047	16.051	16.055	16.059
408	16.063 16.102	16.067 16.106	16.071 16.110	16.075 16.114	16.079 16.118	16.083 16.122	16.087 16.126	16.091 16.130	16.094 16.134	16.098 16.138
409					16.157	16.161	16.165		16.173	
410	16.142	16.146 16.185	16.150 16.189	16.154 16.193	16.157	16.201	16.205	16.169 16.209	16.173	16.177 16.217
412	16.220	16.224	16.228	16.232	16.236	16.240	16.244	16.248	16.252	16.256
413 414	16.260 16.299	16.264 16.303	16.268 16.307	16.272	16.276 16.315	16.279	16.283	16.287 16.327	16.291 16.331	16.295
415	16.339	16.342	16.346	16.350	16.354	16.358	16.362	16,366	16.370	16.374
416	16.378	16.382	16.386	16.390	16.394	16.398	16.402	16.405	16.409	16.413
417 418	16.417 16.457	16.421 16.461	16.425 16.465	16.429 16.468	16.433 16.472	16.437 16.476	16.441 16.480	16.445 16.484	16.449	16.453
419	16.496	16.500	16.504	16.508	16.512	16.516	16.520	16.524	16.528	16.531
420	16.535	16.539	16.543	16.547	16.551	16.555	16.559	16.563	16.567	16.571
42I 422	16.575	16.579 16.618	16.583 16.622	16.587 16.626	16.591	16.594 16.634	16.598 16.638	16.602 16.642	16.606 16.646	16.610 16.650
423	16.654	16.657	16.661	16.665	16.669	16.673	16.677	16.681	16.685	16.689
424	16.693	16.697	16.701	16.705	16.709	16.713	16.717	16.720	16.724	16.728
425 426	16.732 16.772	16.736 16.776	16.740 16.779	16.744 16.783	16.748 16.787	16.752 16.791	16.756 16.795	16.760 16.799	16.764 16.803	16.768 16.807
427	16.811	16.815	16.819	16.823	16.827	16.831	16.835	16.839	16.842	16.846
428 429	16.850 16.890	16.854 16.894	16.858 16.898	16.862 16.902	16.866 16.905	16.870 16.909	16.874 16.913	16.878 16.917	16.882	16.886
430	16.929	16.933	16.937	16.941	16.945	16.949	16.953	16.957	16.961	16.965
431	16.929	16.933	16.937	16.980	16.984	16.988	16.953	16.996	17.000	17.004
432	17.008	17.012	17.016	17.020	17.024	17.02S 17.067	17.031	17.035	17.039	17.043
433 434	17.047 17.087	17.051	17.055	17.059	17.102	17.106	17.071	17.075	17.079	17.083
435	17.126	17.130	17.134	17.138	17.142	17.146	17.150	17.154	17.157	17.161
436	17.165	17.169	17.173	17.177	17.181	17.185	17.189	17.193	17.197	17.201
437 438	17.205	17.209	17.213	17.217	17.260	17.264	17.268	17.232	17.236	17.240
439	17.283	17.287	17.291	17.295	17.299	17.303	17.307	17.311	17.315	17.319
440	17.323	17.327	17.331	17.335	17.339	17.342	17.346	17.350	17.354	17.358
441 442	17.362	17.366	17.370	17.374	17.378	17.382	17.386	17.390	17.394	17.398
443	17.441	17.445	17.449	17.453	17.457	17.461	17.465	17.468	17.472	17.476
444	17.480	17.484	17.488	17.492	17.496	17.500	17.504	17.508	17.512	17.516
445 446	17.520	17.524	17.528	17.531	17.535	17.539	17.543	17.547	17.551	17.555
447	17.598	17.602	17.606	17.610	17.614	17.618	17.622	17.626	17.630	17.634
448	17.638	17.642	17.646	17.650	17.654	17.657	17.661	17.665	17.669	17.673
450	17.717	17.720	17.724	17.728	17.732	17.736	17.740	17.744	17.748	
430	17.717	17.720	17.724	17.720	1.732	1.735	17.745	17.744	17.740	17.752

Milli- meters.	.0	1.	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.	Inches.	Inches.							
450	17.717	17.720	17.724	17.728	17.732	17.736	17.740	17.744	17.748	17.752
451	17.756	17.760	17.764	17.768	17.772	17.776	17.779	17.783	17.787	17.791
452	17.795	17.799	17.803	17.807	17.811	17.815	17.819	17.823	17.827	17.831
453	17.835	17.839	17.842	17.846	17.850	17.854	17.858	17.862	17.866	17.870
454	17.874	17.878	17.882	17.886	17.890	17.894	17.898	17.902	17.905	17.909
455	17.913	17.917	17.921	17.925	17.929	17.933	17.937	17.941	17.945	17.949
456	17.953	17.957	17.961	17.965	17.968	17.972	17.976	17.980	17.984	17.988
457	17.992	17.996	18.000	18.004	18.008	18.012	18.016	18.020	18.024	18.028
458	18.031	18.035	18.039	18.043	18.047	18.051	18.055	18.059	18.063	18.067
459	18.071	18.075	18.079	18.083	18.087	18.091	18.094	18.098	18.102	18.106
460	18.110	18.114	18.118	18.122	18.126	18.130	18.134	18.138	18.142	18.146
461	18.150	18.154	18.157	18.161	18.165	18.169	18.173	18.177	18.181	18.185
462	18.189	18.193	18.197	18.201	18.205	18.209	18.213	18.216	18.220	18.224
463	18.228	18.232	18.236	18.240	18.244	18.248	18.252	18.256	18.260	18.264
464	18.268	18.272	18.276	18.279	18.283	18.287	18.291	18.295	18.299	18.303
465	18.307	18.311	18.315	18.319	18.323	18.327	18.331	18.335	18.339	18.342
466	18.346	18.350	18.354	18.358	18.362	18.366	18.370	18.374	18.378	18.382
467	18.386	18.390	18.394	18.398	18.402	18.405	18.409	18.413	18.417	18.421
468	18.425	18.429	18.433	18.437	18.441	18.445	18.449	18.453	18.457	18.461
469	18.465	18.468	18.472	18.476	18.480	18.484	18.488	18.492	18.496	18.500
470	18.504	18.508	18.512	18.516	18.520	18.524	18.528	18.531	18.535	18.539
471	18.543	18.547	18.551	18.555	18.559	18.563	18.567	18.571	18.575	18.579
472	18.583	18.587	18.591	18.594	18.598	18.602	18.606	18.610	18.614	18.618
473	18.622	18.626	18.630	18.634	18.638	18.642	18.646	18.650	18.654	18.657
474	18.661	18.665	18.669	18.673	18.677	18.681	18.685	18.689	18.693	18.697
475 476 477 478 479	18.701	18.705	18.709	18.713	18.716	18.720	18.724	18.728	18.732	18.736
	18.740	18.744	18.748	18.752	18.756	18.760	18.764	18.768	18.772	18.776
	18.779	18.783	18.787	18.791	18.795	18.799	18.803	18.807	18.811	18.815
	18.819	18.823	18.827	18.831	18.835	18.839	18.842	18.846	18.850	18.854
	18.858	18.862	18.866	18.870	18.874	18.878	18.882	18.886	18.890	18.894
480	18.898	18.902	18.905	18.909	18.913	18.917	18.921	18.925	18.929	18.933
481	18.937	18.941	18.945	18.949	18.953	18.957	18.961	18.965	18.968	18.972
482	18.976	18.980	18.984	18.988	18.992	18.996	19.000	19.004	19.008	19.012
483	19.016	19.020	19.024	19.028	19.031	19.035	19.039	19.043	19.047	19.051
484	19.055	19.059	19.063	19.067	19.071	19.075	19.079	19.083	19.087	19.091
485	19.094	19.098	19.102	19.106	19.110	19.114	19.118	19.122	19.126	19.130
486	19.134	19.138	19.142	19.146	19.150	19.154	19.157	19.161	19.165	19.169
487	19.173	19.177	19.181	19.185	19.189	19.193	19.197	19.201	19.205	19.209
488	19.213	19.216	19.220	19.224	19.228	19.232	19.236	19.240	19.244	19.248
489	19.252	19.256	19.260	19.264	19.268	19.272	19.276	19.279	19.283	19.287
490	19.291	19.295	19.299	19.303	19.307	19.311	19.315	19.319	19.323	19.327
491	19.331	19.335	19.339	19.342	19.346	19.350	19.354	19.358	19.362	19.366
492	19.370	19.374	19.378	19.382	19.386	19.390	19.394	19.398	19.402	19.405
493	19.409	19.413	19.417	19.421	19.425	19.429	19.433	1 9.437	19.441	19.445
494	19.449	19.453	19.457	19.461	19.465	19.468	19.472	19.476	19.480	19.484
495	19.488	19.492	19.496	19.500	19.504	19.508	19.512	19.516	19.520	19.524
496	19.528	19.531	19.535	19.539	19.543	19.547	19.551	19.555	19.559	19.563
497	19.567	19.571	19.575	19.579	19.583	19.587	19.591	19.594	19.598	19.602
498	19.606	19.610	19.614	19.618	19.622	19.626	19.630	19.634	19.638	19.642
499	19.646	19.650	19.654	19.657	19.661	19.665	19.669	19.673	19.677	19.681
500	19.685	19.689	19.693	19.697	19.701	19.705	19.709	19.713	19.716	19.720

Milli-	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
meters.	.0									
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
500	19.685	19.689	19.693	19.697	19.701	19.705	19.709	19.713	19.716	19.720
501	19.724 19.764	19.728 19.768	19.732	19.736	19.740	19.744	19.748 19.787	19.752	19.756	19.760
502 503	19.704	19.807	19.7/2	19.815	19.819	19.823	19.827	19.831	19.835	19.839
504	19.842	19.846	19.850	19.854	19.858	19.862	19.866	19.870	19.874	19.878
505	19.882	19.886	19.890	19.894	19.898	19.902	19.905	19.909	19.913	19.917
506	19.921	19.925	19.929	19.933	19.937	19.941 19.980	19.945	19.949	19.953	19.957
507 508	19.961	19.965	19.968	19.972	20.016	20.023	20.024	20.028	20.031	19.996
509	20.039	20.004	20.047	20.051	20.055	20.059	20.063	20.067	20.071	20.075
510	20.079	20.083	20.087	20.091	20.094	20.098	20.102	20.106	20.110	20.114
511	20.118	20, 122	20.126	20.130	20.134	20.138	20,142	20.146	20.150	20.154
512	20.157	20,161	20,165	20,169	20.173	20.177	20.181	20.185	20.189	20.193
513 514	20.197	20,201	20,205	20.209	20.213	20.216 20.256	20.220	20.224	20.228	20,232
515	20.276	20.279	20,283	20.287	20.291	20.295	20.299	20.303	20.307	20.311
516	20.315	20.319	20.323	20.327	20.331	20.335	20.339	20.342	20.346	20.350
517	20.354	20.358	20 362	20.366	20.370	20.374	20.378	20.382	20.386	20.390
518 519	20.394	20.398	20.402	20.405	20.409	20.413	20.417	20,421	20.425	20.429
520	20.472	20.476	20.480	20.484	20,488	20.492	20.496	20.500	20.504	20.508
521	20.512	20.516	20.520	20.524	20.528	20.531	20.535	20.539	20.543	20.547
522	20.551	20.555	20.559	20.563	20.567	20.571	20.575	20.579	20.583	20.587
523 524	20.591	20.594	20.598 20.638	20.602	20,606	20.650	20.654	20.657	20.661	20.665
525	20.669	20.673	20.677	20.681	20.685	20.689	20,693	20.697	20.701	20.705
526	20.709	20.713	20.716	20.720	20.724	20.728	20.732	20.736	20.740	20.744
527 528	20.748 20.787	20.752	20.756	20.760	20.764 20.803	20.768 20.807	20.772 20.811	20.776 20.S15	20.779	20.783
529	20.707	20.791	20.793	20.799	20.842	20.846	20.850	20.854	20.858	20.862
530	20.866	20.870	20.874	20.878	20.882	20,886	20,890	20.894	20.898	20.902
531	20,905	20.909	20.913	20.917	20.921	20.925	20.929	20.933	20.937	20.941
532 533	20.945	20.949	20.953	20.957	20,961	20.965	20.968	20.972	20.976	20.980
534	21.024	21.028	21.031	21.035	21.039	21.043	21.047	21.051	21.055	21.059
535	21.063	21.067	21.071	21.075	21.079	21.083	21.087	21.091	21.094	21.098
536	21.102	21.106	21.110	21.114	21.118	21.122	21.126	21.130	21.134	21.138
537 538	21.142	21.140	21.150	21.154	21.157	21.201	21.105	21.109	21.213	21.216
539	21,220	21.224	21.228	21.232	21.236	21.240	21.244	21.248	21.252	21.256
540	21.260	21.264	21.268	21.272	21.276	21.279	21.283	21.287	21.291	21.295
541	21.299	21.303	21.307	21.311		21.319	21.323	21.327	21.331	21.335
542 543	21.339	21.342	21.346	21.350			21.402			
544	21.417	21,421	21.425	21.429	21.433		21.441	21.445	21.449	21.453
545	21.457	21.461	21.465	21.468	21.472	21.476	21.480	21.484	21.488	21.492
546	21.496	21.500	21.504	21.508	21.512	21.516	21.520	21.524 21.563	21.528	21.531
547 548	21.535	21.539	21.583	21.587	21.591	21.594	21.598	21.602	21.606	21.610
549	21.614	21.618	21.622	21.626	21.630	21.634	21.638	21.642	21.646	21.650
550	21.654	21.657	21.661	21.665	21.669	21.673	21.677	21,681	21.685	21.689
	I			4	1					

Milli- meters.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
550	21.654		21.661	21.665	21.669	21.673	21.677	21.681	21.685	21.689
551	21.693		21.701	21.705	21.709	21.713	21.716	21.720	21.724	21.728
552	21.732		21.740	21.744	21.748	21.752	21.756	21.760	21.764 21.803	21.703
553 554	21.772 21.811	21.776	21.779	21.783	21.787 21.827	21.791	21.795 21.835	21.799	21.842	21.846
555	21.850	21.854	21.858	21.862	21.866	21.870	21.874	21.878	21.882	21.886
556	21.890	21.894	21.898	21.902	21.905	21.909	21.913	21.917	21.921	21.925
557	21.929	21.933	21.937	21.941	21.945	21.949	21.953	21 957 21.996	21.961	21.965
558	21.968	21.972	21.976	21.980 22.020	21.984	21.988	21.992	22.035	22.039	22.043
559	22.008				22.063	22.067	22.071	22.075	22.079	22.083
560	22.047	22.051	22.055	22.059 22.098	22.102	22.106	22.110	22.114	22.118	22.122
561 562	22.087	22.091	22.134	22.138	22.142	22.146	22.150	22.153	22.157	22.161
563	22.165	22.169	22.173	22.177	22.181	22.185	22.189	22.193	22.197	22.201
564	22.205	22.209	22.213	22.216	22.220	22.224	22.228	22.232	22.236	22.240
565	22.244	22.248	22,252	22.256	22.260	22.264	22,268	22.272	22.276	22.279
566	22.283	1 /	22.291	22.295	22.299	22.303				22.319
567	22.323		22.331	22.335	22.339	22.342		22.350		0
568	22.362		22.370	22.374	22.378	22.382 22.42I	1		1	22.437
569					22.457			22.468	22.472	22.476
570	22.441	1	22.449 22.488	22.453	22.496	1	1			
571	22.480		22.528	1	22.535					
572 573	22.559	1 -	22.567	22.571	22.575	22.579				
574	22.598		22.606			1 .		1		
575	22.638		22.646					1 -	,) -	1
576	22.677		22.685	1 0			. 1		1	
577	22.716				1		- 1	0.		
578 579	22.795		1 0	22.807	22.811	22.81				
580	22.83									
581	22.87							1		, , , ,
582	22.91				' I :			- 1 - 6		
583 584	22.95	-	.		' [23.020		
585	23.03	1 23.035	23.039	23.043	3 23.04	7 23.05	1 23.05			
586	23.03				3 23.08	7 23.09	1 23.09			
587	23.11			3 23.12		6 23.13		1		
588	23.15							o	2 -	1 4 7
589	23.18	9 23.193	23.19							
590	23.22			c	1 0				1 0	
591	23.26								5 23.33	9 23.342
592 593	23.30	(8 23.36		6 23.37	0 23.37		
593	23.38	23.39					5 23.40			
595	23.42	25 23.429	9 23.43	3 23.43		1 23.44		9 23.45		
596	23.46		8 23.47	2 23.47	6 23.48	30 23.48				
597	23.50									
598 599						01 6		23.61		1 60
600	- 1					- 1	12 23.64	16 23.65	50 23.65	23.657

845115										
Milli- meters.	.0	1.	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
600 601	23.622	23.626	23.630 23.669	23.634	23.638	23.642	23.646 23.685	23.650	23.653	23.657
602	23.701	23.705	23.709	23.713	23.716	23.720	23.724	23.728	23.732	23.736
603 604	23.740 23.779	23.744 23.783	23.748 23.787	23.752 23.791	23.756 23.795	23.760 23.799	23.764 23.803	23.768 23.807	23.772 23.811	23.776 23.815
605	23.819	23.823	23.827	23.831	23.835	23.839	23.842	23.846	23.850	23.854
606 607	23.858 23.898	23.862	23.866	23.S70 23.909	23.874 23.913	23.878	23.882 23.921	23.886	23.890	23.894
608 609	23.937 23.976	23.941 23.980	23.945 23.984	23.949 23.988	23.953 23.992	23.957 23.996	23.961 24.000	23.965 24.004	23.968 24.008	23.972 24.012
610	24.016	24.020	21.021	24.028	24.031	24.035	24.039	24.043	24.047	24.051
611	24.055	24.059 24.098	24.063	24.067 24.106	24.071 24.110	24.075 24.114	24.079 24.118	24.083	24.087	24.091
613	24.134	24.138	24.142	24.146	24.150	24.153	24.157	24.161	24.165	24.169
614	24.173	24.177	24.181	24.224	24.189	24.193	24.197	24.201	24.205	24.209
616	24.252	24.256	24.260	24.264	24.268	24.232	24.236	24.279	24.244 24.283	24.248 24.287
617 618	24.291 24.331	24.295 24.335	24.299 24.339	24.303	24.307 24.346	24.311	24.315 24.354	24.319 24.358	24.323 24.362	24.327 24.366
619	24.370	24.374	24.378	24.382	24.386	24.390	24.394	24.398	24.402	24.405
620 621	24.409	24.413 24.453	24.417	24.42I 24.46I	24.425 24.465	24.429 24.468	24.433 24.472	24.437 24.476	24.441 24.480	24.445 24.484
622	24.488	24.492	24.496	24.401	24.403	24.508	24.472	24.516	24.400	24.404
623 624	24.528 24.567	24.531 24.571	24.535 24.575	24.539 24.579	24.543 24.583	24.547 24.587	24.551 24.591	24.555 24.594	24.559 24.598	24.563 24.602
625 626	24.606 24.646	24.610 24.650	24.614	24.618	24.622	24.626	24.630	24.634	24.638	24.642
627	24.685	24.689	24.653 24.693	2 4.657 24.697	24.661 24.701	24.665 24.705	24.669 24.709	24.673	24.677 24.716	24.681
62S 629	24.724	24.728 24.768	24.732 24.772	24.736 24.776	24.740 24.779	24.744 24.783	24.748 24.787	24.752 24.791	24.756 24.795	24.760 24.799
630	24.803	24.807	24.811	24.815	24.819	24.823	24.827	24.831	24.835	24.839
631 632	24.842 24.882	24.846 24.886	24.850 24.890	24.854 24.894	24.858 24.898	24.862	24.866 24.905	24.870	24.874	24.878
633	24.921	24.925	24.929	24.933	24.937	24.941	24.945	24.949	24.913 24.953	24.917 24.957
634 635	24.961	24.965	24.968	24.972	24.976	24.980	24.984	24.988	24.992	24.996
636	25.000 25.039	25.004	25.00S 25.047	25.012 25.051	25.016 25.055	25.020 25.059	25.024 25.063	25.028 25.067	25.031 25.071	25.035 25.075
637 638	25.079 25.118	25.083 25.122	25.087 25.126	25.091 25.130	25.094 25.134	25.098 25.138	25.102 25.142	25.106 25.146	25.110	25.114
639	25.157	25.161	25.165	25.150	25.134	25.177	25.142	25.140	25.150 25.189	25.153 25.193
640 641	25.197	25.201	25.205	25.209	25.213	25.216	25.220	25.224	25.228	25.232
642	25.236 25.276	25.240 25.279	25.244 25.283	25.248 25.287	25.252 25.291	25.256 25.295	25.260 25.299	25.264 25.303	25.268 25.307	25.27 2 25.311
643 644	25.315 25.354	25.319 25.358	25.323	25.327 25.366	25.331 25.370	25.335 25.374	25.339 25.378	25.342 25.382	25.346 25.386	25.350 25.390
645	25.394	25.398	25.402	25.405	25.409	25.413	25.417	25.421	25.425	25.429
646 647	25.433	25.437	25.441	25.445	25.449	25.453	25.457	25.461	25.465	25.468
648	25.472 25.512	25.476 25.516	25.480	25.484 25.524	25.488 25.528	25.492 25.531	25.496 25.535	25.500 25.539	25.504 25.543	25.508 25.547
649	25.551	25.555	25.559	25.563	25.567	25.571	25.575	25.579	25.583	25.587
650	25.591	25.594	25.598	25.602	25.606	25.610	25.614	25.618	25.622	25.626

		1	1					(
Milli- meters.	.0	ا.	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
650 651	25.591 25.630	25.594 25.634	25.598 25.638	25.602 25.642	25.606 25.646	25.610 25.650	25.614	25.618	25.622	25.626
652	25.669	25.673	25.677	25.681	25.685	25.689	25.653	25.657 25.697	25.661 25.701	25.665 25.705
653	25.709	25.713	25.716	25.720	25.724	25.728	25.732	25.736	25.740	25.744
654	25.748	25.752	25.756	25.760	25.764	25.768	25.772	25.776	25.779	25.783
655 656	25.787 25.827	25.791	25.795 25.835	25.799	25.803	25.807	25.811	25.815	25.819	25.823
657	25.866	25.831 25.870	25.874	25.839 25.878	25.842 25.882	25.846 25.886	25.850 25.890	25.854 25.894	25.858 25.898	25.862 25.902
658	25.905	25.909	25.913	25.917	25.921	25.925	25.929	25.933	25.937	25.941
659	25.945	25.949	25.953	25.957	25.961	25.965	25.968	25.972	25.976	25.980
660 661	25.984 26.024	25.988 26.028	25.992 26.031	25.996 26.035	26.000	26.004	26.008 26.047	26.012	26.016	26.020 26.059
662	26.063	26.067	25.071	26.075	26.079	26.083	26.087	26.090	26.094	26.098
663 664	26.102 26.142	26.106 26.146	26.110 26.150	26.114	26.11S 26.157	26.122	26.126 26.165	26.130	26.134	26.138 26.177
665	26.181	26,185	26.189	26.193	26.197	26.201	26.205	26.209	26.213	1
666	26.220	26.224	26.228	26.232	26.236	26.240	26.244	26.248	26.252	26.216 26.256
667 668	26.260 26.299	26.264	26.268	26.272	26.276	26.279	26.283	26.287	26.291	26.295
669	26.339	26.303 26.342	26.307 26.346	26.311	26.315 26.354	26.319 26.358	26.323	26.327 26.366	26.33I 26.370	26.335 26.374
670	26.378	26.382	26.386	26.390	26.394	26.398	26.402	26.405	26.409	26.413
671	26.417	26.421	26.425	26.429	26.433	26.437	26.441	26.445	26.449	26.453
672 673	26.457 26.496	26.461 26.500	26.465 26.504	26.468 26.508	26.472 26.512	26.476 26.516	26.4So 26.520	26.484 26.524	26.488 26.528	26.49 2 26.531
674	26.535	26.539	26.543	26.547	26.551	26.555	26.559	26.563	26.567	26.571
675	26.575	26.579	26.583	26.587	26.590	26.594	26.598	26.602	26,606	26.610
676 677	26.614 26.653	26.618 26.657	26.622 26.661	26.626 26.665	26.630 26.669	26.634 26.673	26.638 26.677	26.642 26.681	26.646 26.685	26.650 26.689
678	26.693	26.697	26.701	26.705	26.709	26.713	26.716	26.720	26.724	26.728
679	26.732	26.736	26.740	26.744	26.748	26.752	26.756	26.760	26.764	26.768
680 681	26.772 26.811	26.776 26.815	26.779 26.819	26.783 26.823	26.787 26.827	26.791 26.831	26.795 26.835	26 799 26.838	2 6.803	26.807 26.846
682	26.850	26.854	26.858	26.862	26.866	26.870	26.S74	26.878	26.882	26.886
683	2 6.890 2 6.929	26.894 26.933	2 6.898 2 6.937	26.902 26.941	26.905 26.945	26.909 26.949	26.913 26.953	26.917 26.957	26.921 26.961	26.925 26.965
685	26.968	26.972	26.976	26.980	26.984	26.988				
686	27.008	27.012	27.016	27.020	27.024	27.028	26.992 27.031	26.996 27.035	27.000 27.039	27.004
687 688	27.047	27.051	27.055	27.059	27.063	27.067	27.071	27.075	27.079	27.083
689	27.087 27.126	27.090 27.130	27.094 27.134	27.098 27.138	27. I 02 27. I 42	27.106 27.146	27.110 27.150	27.114	27.11S 27.157	27.122
690	27.165	27.169	27.173	27.177	27.181	27.185	27.189	27.193	27.197	27.201
691 692	27.205 27.244	27.209 27.248	27.213 27.252	27.216	27.220 27.260	27.224 27.264	27.228	27.232	27.236	27.240
693	27.283	27.287	27.291	27.256 27.295	27.299	27.303	27.268 27.307	27.272 27.311	27.276 27.315	27.279
694	27.323	27.327	27.331	27.335	27.339	27.342	27.346	27.350	27.354	27.358
695 696	27.362 27.402	27.366 27.405	27.370 27.409	27.374	27.378	27.382	27.386	27.390	27.394	27.398
697	27.402 27.44I	27.445	27.449	27.413 27.453	27.417 27.457	27.421 27.461	27.425 27.465	27.429 27.468	27.433 27.472	27.437 27.476
698	27.480	27.484	27.488	27.492	27.496	27.500	27.504	27.508	27.512	27.516
699	27.520	27.524	27.528	27.531	27.535	27.539	27.543	27.547	27.551	27-555
700	27.559	27.563	27.567	27.571	27.575	27.579	27.583	27.587	27.590	27-594

				(,					
Milli- meters.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.									
700	27.559	27.563	27.567	27.571	27.575	27.579	27.583	27.587	27.590	27.594
701	27.598	27.602	27.606	27.610	27.614	27.618	27.622 27.661	27.626	27.630	27.634
702 703	27.638 27.677	27.642 27.681	27.646	27.650	27.653	27.657 27.697	27.701	27.665	27.709	27.673
704	27.716	27.720	27.724	27.728	27.732	27.736	27.740	27.744	27.748	27.752
705	27.756	27.760	27.764	27.768	27.772	27.776	27.779	27.783	27.787	27.791
706	27.795	27.799	27.803	27.807	27.811	27.815	27.819	27.823	27.827	27.831
707	27.835	27.839	27.842	27.846	27.850	27.854 27.894	27.858 27.898	27.862	27.866	27.870
708 709	27.874	27.878 27.917	27.882 27.921	27.886 27.925	27.929	27.933	27.937	27.902 27.941	27.905 27.945	27.949
710	27.953	27.957	27.961	27.965	27.968	27.972	27.976	27.980	27.984	27.988
711	27.992	27.996	28.000	28,004	28,008	28.012	28.016	28.020	28.024	28.028
712	28.031	28.035	28.039	28.043	28.047	28.051	28.055	28.059	28.063	28.067
713 714	28.071 28.110	28.075 28.114	28.079 28.118	28.083 28.122	28.087 28.126	28.090 28.130	28.094 28.134	28.098 28.138	28.102 28.142	28.106 28.146
715	28.150	28.153	28.157	28.161	28.165	28.169	28.173	28.177	28.181	28.185
716	28.189	28.193	28.197	28.201	28.205	28.209	28.213	28.216	28,220	28.224
717	28.228	28.232	28.236	28.240	28.244	28.248	28.252	28.256	28.260	28.264
718 719	28.268 28.307	28.272 28.311	28.276 28.315	28.279 28.319	28.283 28.323	28.287 28.327	28.291 28.331	28.295 28.335	28.299 28.339	28.303 28.342
720	28.346	28.350	28.354	28.358	28.362	28.366	28.370	28.374	28.378	28.382
721	28.386	28.390	28.394	28.398	28,402	28.405	28.409	28.413	28.417	28.421
722	28.425	28.429	28.433	28.437	28.441 28.480	28.445	28.449 28.488	28.453	28.457 28.496	28.461
723 724	28.465 28.504	28.468 28.508	28.472 28.512	28.476 28.516	28.520	28.484 28.524	28.528	28.492 28.531	28.535	28.500 28.539
725	28.543	28.547	28.551	28.555	28.559	28.563	28.567	28.571	28.575	28.579
726	28.583	28.587	28.590	28.594	28.598	28.602	28.606	28.610	28.614	28.618
727 728	28.622 28.661	28.626 28.665	28.630 28.669	28.634 28.673	28.638 28.677	28.642 28.681	28.646 28.685	28.650 28.689	28.653 28.693	28.657 28.697
729	28.701	28.705	28.709	28.713	28.716	28.720	28.724	28.728	28.732	28.736
730	28.740	28.744	28.748	28.752	28.756	28.760	28.764	28.768	28.772	28.776
731	28.779	28.783	28.787	28.791	28.795	28.799	28.So3	28.807	28.811	28.815
732 733	28.819 28.858	28.823 28.862	28.827 28.866	28.831 28.870	28.835 28.874	28.839 28.878	28.842 28.882	28.846 28.886	28.850 28.890	28.854 28.894
734	28.898	28.902	28.905	28.909	28.913	28.917	28.921	28.925	28.929	28.933
735	28.937	28.941	28.945	28.949	28.953	28.957	28.961	28.965	28.968	28.972
736	28.976	28.980	28.984	28.988	28.992	28.996	29.000	29.004	29.008	29.012
737 738	29.016 29.055	29.020	29.024 29.063	29.028 29.067	29.03I 29.07I	29.035	29.039	29.043 29.083	29.047 29.087	29.051
739	29.033	29.098	29.102	29.106	29.110	29.114	29.118	29.122	29.126	29.130
740	29.134	29.138	29.142	29.146	29.150	29.153	29.157	29.161	29.165	29.169
741	29.173	29.177	29.181	29.185	29.189 29.228	29.193	29.197	29.201	29.205	29.209
742 743	29.213 29.252	29.256	29.260	29.224	29.228	29.232	29.236 29.276	29.240 29.279	29.244 29.283	29.243
743	29.291	29.295	29.299	29.303	29.307	29.311	29.315	29.319	29.323	29.327
745	29.331	29.335	29.339	29.342	29.346	29.350	29.354	29.358	29.362	29.366
746 747	29.370 29.409	29.374 29.413	29.378	29.382 29.421	29.386 29.425	29.390	29.394	29.398	29.402 29.44I	29.405
748	29.449	29.453	29.417	29.421	29.425	29.429	29.433	29.437	29.480	29.484
749	29.488	29.492	29.496	29.500	29.504	29.508	29.512	29.516	29.520	29.524
750	29.528	29.531	29.535	29.539	29-543	29.547	29.551	29.555	29.559	29.563
							2			

Milli- meters	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
750 751 752 753 754	29.528	29.531	29.535	29.539	29.543	29.547	29.551	29.555	29.559	29.563
	29.567	29.571	29.575	29.579	29.583	29.587	29.590	29.594	29.598	29.602
	29.606	29.610	29.614	29.618	29.622	29.626	29.630	29.634	29.638	29.642
	29.646	29.650	29.653	29.657	29.661	29.665	29.669	29.673	29.677	29.681
	29.685	29.689	29.693	29.697	29.701	29.705	29.709	29.713	29.716	29.720
755 756 757 758 759	29.724	29.728	29.732	29.736	29.740	29.744	29.748	29.752	29.756	29.760
	29.764	29.768	29.772	29.776	29.779	29.783	29.787	29.791	29.795	29.799
	29.803	29.807	29.811	29.815	29.819	29.823	29.827	29.831	29.835	29.839
	29.842	29.846	29.850	29.854	29.858	29.862	29.866	29.870	29.874	29.878
	29.882	29.886	29.890	29.894	29.898	29.902	29.905	29.909	29.913	29.917
760 761 762 763 764	29.921 29.961 30.000 30.039 30.079	29.925 29.965 30.004 30.043 30.083	29.929 29.968 30.008 30.047 30.087	29.933 29.972 30.012 30.051 30.090	29.937 29.976 30.016 30.055 30.094	29.941 29.980 30.020 30.059 30.098	29.945 29.984	29.949 29.988 30.027 30.067 30.106	29.953 29.992 30.031 30.071 30.110	29.957 29.996 30.035 30.075 30.114
765	30.118	30.122	30.126	30.130	30.134	30.138	30.142	30. 146	30.150	30.153
766	30.157	30.161	30.165	30.169	30.173	30.177	30.181	30. 185	30.189	30.193
767	30.197	30.201	30.205	30.209	30.213	30.216	30.220	30. 224	30.228	30.232
768	30.236	30.240	30.244	30.248	30.252	30.256	30.260	30. 264	30.268	30.272
769	30.276	30.279	30.283	30.287	30.291	30.295	30.299	30. 303	30.307	30.311
770	30.315	30.319	30.323	30.327	30.331	30.335	30.339	30.342	30.346	30.350
771	30.354	30.358	30.362	30.366	30.370	30.374	30.378	30.382	30.386	30.390
772	30.394	30.398	30.402	30.405	30.409	30.413	30.417	30.421	30.425	30.429
773	30.433	30.437	30.441	30.445	30.449	30.453	30.457	30.461	30.465	30.468
774	30.472	30.476	30.480	30.484	30.488	30.492	30.496	30.500	30.504	30.508
775	30.512	30.516	30.520	30.524	30.528	30.531	30.535	30.539	30.543	30.547
776	30.551	30.555	30.559	30.563	30.567	30.571	30.575	30.579	30.583	30.587
777	30.590	30.594	30.598	30.602	30.606	30.610	30.614	30.618	30.622	30.626
778	30.630	30.634	30.638	30.642	30.646	30.650	30.653	30.657	30.661	30.665
779	30.669	30.673	30.677	30.681	30.685	30.689	30.693	30.697	30.701	30.705
780	30.709	30.713	30.716	30.720	30.724	30.728	30.732	30.736	30.740	30.744
781	30.748	30.752	30.756	30.760	30.764	30.768	30.772	30.776	30.779	30.783
782	30.787	30.791	30.795	30.799	30.803	30.807	30.811	30.815	30.819	30.823
783	30.827	30.831	30.835	30.839	30.842	30.846	30.850	30.854	30.858	30.862
784	30.866	30.870	30.874	30.878	30.882	30.886	30.890	30.894	30.898	30.902
785	30.905	30.909	30.913	30.917	30.921	30.925	30.929	30.933	30.937	30.941
786	30.945	30.949	30.953	30.957	30.961	30.965	30.968	30.972	30.976	30.980
787	30.984	30.988	30.992	30.996	31.000	31.004	31.008	31.012	31.016	31.020
788	31.024	31.027	31.031	31.035	31.039	31.043	31.047	31.051	31.055	31.059
789	31.063	31.067	31.071	31.075	31.079	31.083	31.087	31.090	31.094	31.098
790	31.102	31.106	31.110	31.114	31.118	31.122	31.126	31.130	31.134	31.138
791	31.142	31.146	31.150	31.153	31.157	31.161	31.165	31.169	31.173	31.177
792	31.181	31.185	31.189	31.193	31.197	31.201	31.205	31.209	31.213	31.216
793	31.220	31.224	31.228	31.232	31.236	31.240	31.244	31.248	31.252	31.256
794	31.260	31.264	31.268	31.272	31.276	31.279	31.283	31.287	31.291	31.295
795	31.299	31.303	31.307	31.311	31.315	31.319	31.323	31.327	31.331	31.335
796	31.339	31.342	31.346	31.350	31.354	31.358	31.362	31.366	31.370	31.374
797	31.378	31.382	31.380	31.390	31.394	31.398	31.402	31.405	31.409	31.413
798	31.417	31.421	31.425	31.429	31.433	31.437	31.441	31.445	31.449	31.453
799	31.457	31.461	31.465	31.468	31.472	31.476	31.480	31.484	31.488	31.492
800	31.496	31.500	31.504	31.508	31.512	31.516	31.520	31.524	31.527	31.531

Milli- meters.	.0	1.	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.	Inches.								
800	31.496	31.500	31.504	31.508	31.512	31.516	31.520	31.524	31.527	31.531
801	31.535	31.539	31.543	31.547	31.551	31.555	31.559	31.563	31.567	31.571
802	31.575	31.579	31.583	31.587	31.590	31.594	31.598	31.602	31.606	31.610
803	31.614	31.618	31.622	31.626	31.630	31.634	31.638	31.642	31.646	31.650
804	31.653	31.657	31.661	31.665	31.669	31.673	31.677	31.681	31.685	31.689
805	31.693	31.697	31.701	31.705	31.709	31.713	31.716	31.720	31.724	31.728
806	31.732	31.736	31.740	31.744	31.748	31.752	31.756	31.760	31.764	31.768
807	31.772	31.776	31.779	31.783	31.787	31.791	31.795	31.799	31.803	31.807
808	31.811	31.815	31.819	31.823	31.827	31.831	31.835	31.839	31.842	31.846
809	31.850	31.854	31.858	31.862	31.866	31.870	31.874	31.878	31.882	31.886
810	31.890	31.894	31.898	31.902	31.905	31.909	31.913	31.917	31.921	31.925
811	31.929	31.933	31.937	31.941	31.945	31.949	31.953	31.957	31.961	31.965
812	31.968	31.972	31.976	31.980	31.984	31.988	31.992	31.996	32.000	32.004
813	32.008	32.012	32.016	32.020	32.024	32.027	32.031	32.035	32.039	32.043
814	32.047	32.051	32.055	32.059	32.063	32.067	32.071	32.075	32.079	32.083
815	32.087	32.090	32.094	32.098	32.102	32.106	32.110	32.114	32.118	32.122
816	32.126	32.130	32.134	32.138	32.142	32.146	32.150	32.153	32.157	32.161
817	32.165	32.169	32.173	32.177	32.181	32.185	32.189	32.193	32.197	32.201
818	32.205	32.209	32.213	32.216	32.220	32.224	32.228	32.232	32.236	32.240
819	32.244	32.248	32.252	32.256	32.260	32.264	32.268	32.272	32.276	32.279
820	32.283	32.287	32.291	32.295	32.299	32.303	32.307	32.311	32.315	32.319
821	32.323	32.327	32.331	32.335	32.339	32.342	32.346	32.350	32.354	32.358
822	32.362	32.366	32.370	32.374	32.378	32.382	32.386	32.390	32.394	32.398
823	32.402	32.405	32.409	32.413	32.417	32.421	32.425	32.429	32.433	32.437
824	32.441	32.445	32.449	32.453	32.457	32.461	32.465	32.468	32.472	32.476
825	32.480	32.484	32.488	32.492	32.496	32.500	32.504	32.508	32.512	32.516
\$26	32.520	32.524	32.527	32.531	32.535	32.539	32.543	32.547	32.551	32.555
\$27	32.559	32.563	32.567	32.571	32.575	32.579	32.583	32.587	32.590	32.594
\$28	32.598	32.602	32.606	32.610	32.614	32.618	32.622	32.626	32.630	32.634
\$29	32.638	32.642	32.646	32.650	32.653	32.657	32.661	32.665	32.669	32.673
830	32.677	32.681	32.685	32.689	32.693	32.697	32.701	32.705	32.709	32.713
831	32.716	32.720	32.724	32.728	32.732	32.736	32.740	32.744	32.748	32.752
832	32.756	32.760	32.764	32.768	32.772	32.776	32.779	32.783	32.787	32.791
833	32.795	32.799	32.803	32.807	32.811	32.815	32.819	32.823	32.827	32.831
834	32.835	32.839	32.842	32.846	32.850	32.854	32.858	32.862	32.866	32.870
835	32.874	32.878	32.882	32.886	32.890	32.894	32.898	32.902	32.905	32.909
836	32.913	32.917	32.921	32.925	32.929	32.933	32.937	32.941	32.945	32.949
837	32.953	32.957	32.961	32.965	32.968	32.972	32.976	32.980	32.984	32.988
838	32.992	32.996	33.000	33.004	33.008	33.012	33.016	33.020	33.024	33.027
839	33.031	33.035	33.039	33.043	33.047	33.051	33.055	33.059	33.063	33.067
840	33.071	33.075	33.079	33.083	33.087	33.090	33.094	33.098	33.102	33.106
841	33.110	33.114	33.118	33.122	33.126	33.130	33.134	33.138	33.142	33.146
842	33.150	33.153	33.157	33.161	33.165	33.169	33.173	33.177	33.181	33.185
843	33.189	33.193	33.197	33.201	33.205	33.209	33.213	33.216	33.220	33.224
844	33.228	33.232	33.236	33.240	33.244	33.248	33.252	33.256	3 3.260	33.264
845	33.268	33.272	33.276	33.279	33.283	33.287	33.291	33·295	33.299	33.303
846	33.307	33.311	33.315	33.319	33.323	33.327	33.331	33·335	33.339	33.342
847	33.346	33.350	33.354	33.358	33.362	33.366	33.370	33·374	33.378	33.382
848	33.386	33.390	33.394	33.398	33.402	33.405	33.409	33·413	33.417	33.421
849	33.425	33.429	33.433	33.437	33.441	33.445	33.449	33·453	33.457	33.461
850	33.464	33.468	33.472	33.476	33.480	33.484	33.488	33.492	33.496	33.500

Milli- meters.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.									
850	33.464	33.468	33.472	33.476	33.480	33.484	33.488	33.492	33.496	33.500
\$51	33.504	33.508	33.512	33.516	33.520	33.524	33.527	33.531	33.535	33.539
852	33.543	33.547	33.551	33.555	33.559	33.563	33.567	33.571	33.575	33.579
853	33.583	33.587	33.590	33.594	33.598	33.602	33.606	33.610	33.614	33.618
854	33.622	33.626	33.630	33.634	33.638	33.642	33.646	33.650	33.653	33.657
855	33.661	33.665	33.669	33.673	33.677	33.681	33.685	33.689	33.693	33.697
856	33.701	33.705	33.709	33.713	33.716	33.720	33.724	33.728	33.732	33.736
857	33.740	33.744	33.748	33.752	33.756	33.760	33.764	33.768	33.772	33.776
858	33.779	33.783	33.787	33.791	33.795	33.799	33.803	33.807	33.811	33.815
859	33.819	33.823	33.827	33.831	33.835	33.839	33.842	33.846	33.850	33.854
860	33.858	33.862	33.866	33.870	33.874	33.878	33.882	33.886	33.890	33.894
861	33.898	33.902	33.905	33.909	33.913	33.917	33.921	33.925	33.929	33.933
862	33.937	33.941	33.945	33.949	33.953	33.957	33.961	33.964	33.968	33.972
863	33.976	33.980	33.984	33.988	33.992	33.996	34.000	34.004	34.008	34.012
864	34.016	34.020	34.024	34.027	34.031	34.035	34.039	34.043	34.047	34.051
865	34.055	34.059	34.063	34.067	34.071	34.075	34.079	34.083	34.087	34.090
866	34.694	34.098	34.102	34.106	34.110	34.114	34.118	34.122	34.126	34.130
867	34.134	34.138	34.142	34.146	34.150	34.153	34.157	34.161	34.165	34.169
868	34.173	34.177	34.181	34.185	34.189	34.193	34.197	34.201	34.205	34.209
869	34.213	34.216	34.220	34.224	34.228	34.232	34.236	34.240	34.244	34.248
870	34.252	34.256	34.260	34.264	34.268	34.272	34.276	34.279	34.283	34.287
871	34.291	34.295	34.299	34.303	34.307	34.311	34.315	34.319	34.323	34.327
872	34.331	34.335	34.339	34.342	34.346	34.350	34.354	34.358	34.362	34.366
873	34.370	34.374	34.378	34.382	34.386	34.390	34.394	34.398	34.402	34.405
874	34.409	34.413	34.417	34.421	34.425	34.429	34.433	34.437	34.441	34.445
875	34.449	34·453	34·457	34.461	34.464	24.468	34.472	34.476	34.480	34.484
876	34.488	34·492	34·496	34.500	34.504	34.508	34.512	34.516	34.520	34.524
877	34.527	34·531	34·535	34.539	34.543	34.547	34.551	34.555	34.559	34.563
878	34.567	34·571	34·575	34.579	34.583	34.587	34.590	34.594	34.598	34.602
879	34.606	34·610	34·614	34.618	34.622	34.626	34.630	34.634	34.638	34.642
880	34.646	34.650	34.653	34.657	34.661	34.665	34.669	34.673	34.677	34.681
881	34.685	34.689	34.693	34.697	34.701	34.705	34.709	34.713	34.716	34.720
882	34.724	34.728	34.732	34.736	34.740	34.744	34.748	34.752	34.756	34.760
883	34.764	34.768	34.772	34.776	34.779	34.783	34.787	34.791	34.795	34.799
884	34.803	34.807	34.811	34.815	34.819	34.823	34.827	34.831	34.835	34.839
885	34.842	34.846	34.850	34.854	34.858	34.862	34.866	34.870	34.874	34.878
886	34.882	34.886	34.890	34.894	34.898	34.902	34.905	34.909	34.913	34.917
887	34.921	34.925	34.929	34.933	34.937	34.941	34.945	34.949	34.953	34.957
888	34.961	34.964	34.968	34.972	34.976	34.980	34.984	34.988	34.992	34.996
889	35.000	35.004	35.008	35.012	35.016	35.020	35.024	35.027	35.031	35.035
890	35.039	35.043	35.047	35.051	35.055	35.059	35.063	35.067	35.071	35.075
891	35.079	35.083	35.087	35.090	35.094	35.098	35.102	35.106	35.110	35.114
892	35.118	35.122	35.126	35.130	35.134	35.138	35.142	35.146	35.150	35.153
893	35.157	35.161	35.165	35.169	35.173	35.177	35.181	35.185	35.189	35.193
894	35.197	35.201	35.205	35.209	35.213	35.216	35.220	35.224	35.228	35.232
895	35.236	35.240	35.244	35.248	35.252	35.256	35.260	35.264	35.268	35.272
896	35.276	35.279	35.283	35.287	35.291	35.295	35.299	35.303	35.307	35.311
897	35.315	35.319	35.323	35.327	35.331	35.335	35.339	35.342	35.346	35.350
898	35.354	35.358	35.362	35.366	35.370	35.374	35.378	35.382	35.386	35.390
899	35.394	35.398	35.402	35.405	35.409	35.413	35.417	35.421	35.425	35.429
900	35-433	35.437	35.441	35-445	35-449	35-453	35-457	35.461	35.464	35.468

1 mm. = 0.03937 inch.

Milli- meters.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	Iuches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
900	35.433	35-437	35.441	35.445	35.449	35.453	35-457	35.461	35.464	35.468
901 902	35.472 35.512	35.476 35.516	35.480 35.520	35.484 35.524	35.488 35.527	35·492 35·531	35.496 35.535	35.500	35.504 35.543	35.508 35.547
903	35.551	35.555	35-559	35.563	35.567	35.571	35.575	35.579	35.583	35.587
904	35.590	35.594	35.598	35.602	35.606	35.610	35.614	35.618	35.622	35.626
905	35.630	35.634	35.638	35.642	35.646	35.650	35.653	35.657	35.661	35.665
906 907	35.669	35.673 35.713	35.677 35.716	35.681	35.685 35.724	35.689 35.728	35.693 35.732	35.697 35.736	35.701 35.740	35.705
908	35.748	35.752	35.756	35.760	35.764	35.768	35.772	35.776	35.779	35.783
909	35.7 ⁸ 7	35.791	35.795	35.799	35.803	35.So7	35.811	35.815	35.819	35.823
910	35.827	35.831	35.835	35.839	35.842	35.846	35.850	35.854	35.858	35.862
911	35.866 35.905	35.870 35.909	35.874 35.913	35.878 35.917	35.882 35.921	35.886 35.925	35.890 35.929	35.894 35.933	35.898 35.937	35.902 35.941
913	35.945	35.949	35.953	35.957	35.961	35.964	35.968	35.972	35.976	35.980
914	35.984	35.988	35.992	35.996	36.000	36.004	36.008	36.012	36.016	36.020
915	36.024	36.027	36.031	36.035	36.039	36.043	36.047	36.051	36.055	36.059
916	36.063 36.102	36.067 36.106	36.071 36.110	36.075 36.114	36.079 36.118	36.083 36.122	36.087 36.126	36.090 36.130	36.094 36.134	36.098 36.138
918	36.142	36.146	36.150	36.153	36.157	36.161	36.165	36.169	36.173	36.177
919	36, 181	36.185	36.189	36.193	36.197	36,201	36,205	36,209	36.213	36.216
920 921	36.220 36.260	36.224 36.264	36.228 36.268	36.232 36.272	36.236 36.276	36.240 36.279	36.244 36.283	36.248 36.287	36.252 36.291	36.256 36.295
921	36.299	36.303	36.307	36.311	36.315	36.319	36.323	36.327	36.331	36.335
923	36.339	36.342	36.346	36.350	36.354	36.358	36.362	36.366	36.370	36.374
924	36.378	36.382	36.386	36.390	36.394	36.398	36.402	36.405	36.409	36.413
9 25 926	36.417 36.457	36.421 36.461	36.425 36.464	36,429 36,468	36.433 36.472	36.437 36.476	36.441 36.480	36.445 36.484	36.449 36.488	36.453 36.492
927	36.496	36.500	36.504	36.508	36.512	36.516	36.520	36.524	36.527	36.531
928 929	36.535 36.575	36.539 36.579	36.543 36.583	36.547 36.587	36.551 36.590	36.555 36.594	36.559 36.598	36.563	36.567 36.606	36.571 36.610
930	36.614									
931	36.653	36.618 36.657	36.622 36.661	36.626 36.665	36.630 36.669	36.634 36.673	36.638 36.677	36.642 36.681	36.646 36.685	36.650 36.689
932	36.693	36.697	36.701	36.705	36.709	36.713	36.716	36.720	36.724	36.728
933	36.732 36.772	36.736 36.776	36.740 36.779	36.744 36.783	36.748 36.787	36.752 36.791	36.756 36.795	36.760 36.799	36.764 36.803	36.768 36.807
935	36.811	36.815	36.819	36.823	36.827	36.831	36.835	36.839	36.842	36.846
936	36.850	36.854	36.858	36.862	36.866	36.870	36.874	36.878	36.882	36.886
937 938	36.890 36.929	36.894 36.933	36.898 36.937	36.902 36.941	36.905 36.945	36,909 36,949	36.913 36.953	36.917 36.957	36.921 36.961	36.925 36.964
939	36.968	36.933	36.976	36.980	36.984	36.988	36,992	36.937	37.000	37.004
940	37.008	37.012	37.016	37.020	37.024	37.027	37.031	37.035	37.039	37.043
941	37.047	37.051	37.055	37.059	37.063	37.067	37.071	37.075	37.079	37.083
942 943	37.087 37.126	37.090 37.130	37.094 37.134	37.098 37.138	37.102 37.142	37.106 37.146	37.110	37.114 37.153	37.118	37.122 37.161
944	37.165	37.169	37.173	37.177		37.185	37.189	37.193	37.197	37.201
945	37.204	37.208	37.212	37.216	37.220	37.224	37.228	37.232	37.236	37.240
946 947	37.244 37.283	37.248 37.287	37.25 2 37.291	37.256 37.295	37.260 37.299	37.264 37.303	37.268 37.307	37.272 37.311	37.276 37.315	37.279 37.319
948	37.323	37.327	37.331	37.335	37.299	37.342	37.346	37.350	37.354	37.358
949	37.362	37.366	37.370	37.374	37.378	37.382	37.386	37-390	37-394	37.398
950	37.402	37.405	37.409	37.413	37.417	37.421	37.425	37.429	37-433	37.437

	-									
Milli- meters.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	Inches.									
950	37.402	37.405	37.409	37.413	37.417	37.421	37.425	37.429	37.433	37.437
951	37.441	37.445	37.449	37.453	37.457	37.461	37.464	37.468	37.472	37.476
952	37.480	37.484	37.488	37.492	37.496	37.500	37.504	37.508	37.512	37.516
953	37.520	37.524	37.527	37.531	37.535	37.539	37.543	37.547	37.551	37.555
954	37.559	37.563	37.567	37.571	37.575	37.579	37.583	37.587	37.590	37.594
955	37.598	37.602	37.606	37.610	37.614	37.618	37.622	37.626	37.630	37.634
956	37.638	37.642	37.646	37.650	37.653	37.657	37.661	37.665	37.669	37.673
957	37.677	37.681	37.685	37.689	37.693	37.697	37.701	37.705	37.709	37.713
958	37.716	37.720	37.724	37.728	37.732	37.736	37.740	37.744	37.748	37.752
959	37.756	37.760	37.764	37.768	37.772	37.776	37.779	37.783	37.787	37.791
960	37.795	37·799	37.803	37.807	37.811	37.815	37.819	37.823	37.827	37.831
961	37.835	37·839	37.842	37.846	37.850	37.854	37.858	37.862	37.866	37.870
962	37.874	37·878	37.882	37.886	37.890	37.894	37.898	37.901	37.905	37.909
963	37.913	37·917	37.921	37.925	37.929	37.933	37.937	37.941	37.945	37.949
964	37.953	37·957	37.961	37.964	37.968	37.972	37.976	37.980	37.984	37.988
965	37.992	37.996	38.000	38.004	38.008	38.012	38.016	38.020	38.024	38.027
966	38.031	38.035	38.039	38.043	38.047	38.051	38.055	38.059	38.063	38.067
967	38.071	38.075	38.079	38.083	38.087	38.090	38.094	38.098	38.102	38.106
968	38.110	38.114	38.118	38.122	38.126	38.130	38.134	38.138	38.142	38.146
969	38.150	38.153	38.157	38.161	38.165	38.169	38.173	38.177	38.181	38.185
970	38.189	38.193	38.197	38.201	38.205	38.209	38.213	38.216	38.220	38.224
971	38.228	38.232	38.236	38.240	38.244	38.248	38.252	38.256	38.260	38.264
972	38.268	38.272	38.276	38.279	38.283	38.287	38.291	38.295	38.299	38.303
973	38.307	38.311	38.315	38.319	38.323	38.327	38.331	38.335	38.339	38.342
974	38.346	38.350	38.354	38.358	38.362	38.366	38.370	38.374	38.378	38.382
975	38.386	38.390	38.394	38.398	38.401	38.405	38.409	38.413	38.417	38.421
976	38.425	38.429	38.433	38.437	38.441	38.445	38.449	38.453	38.457	38.461
977	38.464	38.468	38.472	38.476	38.480	38.484	38.488	38.492	38.496	38.500
978	38.504	38.508	38.512	38.516	38.520	38.524	38.527	38.531	38.535	38.539
979	38.543	38.547	38.551	38.555	38.559	38.563	38.567	38.571	38.575	38.579
980	38.583	38.587	38.590	38.594	38.598	38.602	38.606	38.610	38.614	38.618
981	38.622	38.626	38.630	38.634	38.638	38.642	38.646	38.650	38.653	38.657
982	38.661	38.665	38.669	38.673	38.677	38.681	38.685	38.689	38.693	38.697
983	38.701	38.705	38.709	38.713	38.716	38.720	38.724	38.728	38.732	38.736
984	38.740	38.744	38.748	38.752	38.756	38.760	38.764	38.768	38.772	38.776
985	38.780	38.783	38.787	38.791	38.795	38.799	38.803	38.807	38.811	38.815
986	38.819	38.823	38.827	38.831	38.835	38.839	38.842	38.846	38.850	38.854
987	38.858	38.862	38.866	38.870	38.874	38.878	38.882	38.886	38.890	38.894
988	38.898	38.901	38.905	38.909	38.913	38.917	38.921	38.925	38.929	38.933
989	38.937	38.941	38.945	38.949	38.953	38.957	38.961	38.964	38.968	38.972
990	38.976	38.980	38.984	38.988	38.992	38.996	39.000	39.004	39.008	39.012
991	39.016	39.020	39.024	39.027	39.031	39.035	39.039	39.043	39.047	39.051
992	39.055	39.059	39.063	39.067	39.071	39.075	39.079	39.083	39.087	39.090
993	39.094	39.098	39.102	39.106	39.110	39.114	39.118	39.122	39.126	39.130
994	39.134	39.138	39.142	39.146	39.150	39.153	39.157	39.161	39.165	39.169
995	39.173	39.177	39.181	39.185	39.189	39.193	39.197	39.201	39.205	39.209
996	39.213	39.216	39.220	39.224	39.228	39.232	39.236	39.240	39.244	39.248
997	39.252	39.256	39.260	39.264	39.268	39.272	39.276	39.279	39.283	39.287
998	39.291	39.295	39.299	39.303	39.307	39.311	39.315	39.319	39.323	39.327
999	39.331	39.335	39.339	39.342	39.346	39.350	39.354	39.358	39.362	39.366
1000	39-370	39.374	39.378	39.382	39.386	39.390	39-394	39.398	39.401	39.405

TABLE 11.

BAROMETRIC INCHES (MERCURY) INTO MILLIBARS.

1 inch = 33.86395 mb.

										'
Inches	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
	mb.	mb.	mb.	mb.	mb.	nıb.	mb.	mb.	mb.	mb.
0.0	0.00	0.34	0.68	1.02	1.35	1.69	2.03	2.37	2.7 I	3.05
0.1	3.39	3.73	4.06	4.40	4.74	5.08	5.42	5.76	6.10	6.43
0.2	6.77	7.11	7.45	7.79	8.13	8.47	8.80	9.14	9.48	9.82
0.3	10.16	10.50	10.84	11.18	11.51	11.85	12.10	12.53	12.87	13.21
0.4	13.55	13.88	14.22	14.56	14.90	15.24	15.58	15.92	16.25	16.59
0.5	16.93	17.27	17.61	17.95	18.29	18.63	18.96	19.30	19.64	19.98
0.6	20.32	20.66	21.00	21.33	21.67	22.01	22.35	22.69	23.03	23.37
0.7	23.70	24.04	24.38	24.72	25.06	25.40	25.74	26.08	26.41	26.75
0.8	27.00	27.43	27.77	28.11	28.45	28.78	29.12	29.46	29.80	30.14
0.9	30.48	30.82	31.15	31.49	31.83	32.17	32.51	32.85	33.19	33.53
1.0	33.86	34.20	34.54	34.88	35.22	35.56	35.90	36.23	36.57	36.91
1.1	37.25	37.59	37.93	38.27	38.60	38.94	39.28	39.62	39.96	40.30
1.2	40.64	40.98	41.31	41.65	41.99	42.33	42.67	43.01	43.35	43.68
1.3	44.02	44.36	44.70	45.04	45.38	45.72	46.05	46.39	46.73	47.07
1.4	47.41	47.75	48.09	48.43	48.76	49.10	49.44	49.78	50.12	50.46
1.5	50.80	51.13	51.47	51.81	52.15	52.49	52.83	53.17	53.51	53.84
1.6	54.18	54.52	54.86	55.20	55.54	55.88	56.21	56.55	56.89	57.23
1.7	57.57	57.91	58.25	58.58	58.92	59.26	59.60	59.94	60.28	60.62
1.8	60.96	61.20	61.63	61.97	62.31	62.65	62.99	63.33	03.66	64.00
1.9	64.34	64.68	65.02	65.36	65.70	66.03	66.37	66.71	67.05	67.39
2.0	67.73	68.07	68.41	68.74	69.08	69.42	69.76	70.10	70.44	70.78
2.1	71.11	71.45	71.79	72.13	72.47	72.81	73.15	73.48	73.82	74.16
2.2	74.50	74.84	75.18	75.52	75.86	76.19	76.53	76.87	77.21	77.55
2.3	77.89	78.23	78.56	78.90	79.24	79.58	79.92	80.26	80.60	80.93
2.4	81.27	81.61	81.95	82.29	82.63	82.97	83.31	83.64	83.98	84.32
25.0	846.6	846.9	847.3	847.6	848.0	848.3	848.6	849.0	849.3	849.6
25.1	850.0	850.3	850.7	851.0	851.3	851.7	852.0	852.4	852.7	853.0
25.2	853.4	853.7	854.0	854.4	854.7	855.1	855.4	855.7	856.1	856.4
25.3	8,56.8	857.1	857.4	857.8	858.1	858.5	858.8	859.1	859.5	859.8
25.4	860.1	860.5	860.8	861.2	861.5	861.8	862.2	862.5	862.9	863.2
25.5	863.5	863.9	864.2	864.5	864.9	865.2	865.6	865.9	866.2	866.6
25.6	866.9	867.3	867.6	867.9	868.3	868.6	868.9	869.3	869.6	870.0
25.7	870.3	870.7	871.0	871.3	871.7	872.0	872.3	872.7	873.0	873.4
25.8	873.7	874.0	874.4	874.7	875.0	875.4	875.7	876.1	876.4	876.7
25.9	877.1	877.4	877.8	878.1	878.4	878.8	879.1	879.4	879.8	880.1
26.0	880.5	880.8	881.1	881.5	881.8	882.2	882.5	882.8	883.2	883.5
26.1	883.8	884.2	884.5	884.9	885.2	885.5	885.9	886.2	886.6	886.9
26.2	887.2	887.6	887.9	888.3	888.6	888.9	889.3	889.6	889.9	890.3
26.3	890.6	891.0	891.3	891.6	892.0	892.3	892.7	893.0	893.3	893.7
26.4	894.0	894.3	894.7	895.0	895.4	895.7	896.0	896.4	896.7	897.1
26.5	897.4	897.7	898.1	898.4	898.7	899.1	899.4	899.8	900.1	900.4
26.6	900.8	901.1	901.5	901.8	902.1	902.5	902.8	903.2	903.5	903.8
26.7	904.2	904.5	904.8	905.2	905.5	905.9	906.2	906.5	906.9	907.2
26.8	907.6	907.9	908.2	908.6	908.9	909.2	909.6	909.9	910.3	910.6
26.9	910.9	911.3	911.6	912.0	912.3	912.6	913.0	913.3	913.6	914.0
27.0	914.3	914.7	915.0	915.3	915.7	916.0	916.4	916.7	917.0	917.4
27.1	917.7	918.1	918.4	918.7	919.1	919.4	919.7	920.1	920.4	920.8
27.2	921.1	921.4	921.8	922.I	922.5	922.8	923.I	923.5	923.8	924.I
27.3	924.5	924.8	925.2	925.5	925.8	926.2	926.5	926.9	927.2	927.5
27.4	927.9	928.2	928.5	928.9	929.2	929.6	929.9	930.2	930.6	930.9

TABLE 11.

BAROMETRIC INCHES (MERCURY) INTO MILLIBARS.

ı inch=33.86395 mb.

Inches.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
				mb.	mb.	mb.	mb.	mb.	mb.	mb.
1	mb.	mb.	mb.	932.3	932.6	933.0	933.3	933.6	934.0	934-3
27.5	931.3	931.6	931.9		936.0	936.3	936.7	937.0	937.4	937.7
27.6	934.6	935.0	935.3	935.7	939.4	939.7	9.10.1	940.4	940.7	941.1
27.7	938.0	938.4	938.7	939.0	939.4	943.I	943.4	943.8	944.1	944.5
27.8	941.4	941.8	942.1	942.4	946.2	946.5	946.8	947.2	947.5	947.9
27.9	944.8	945.1	945.5	945.8	1940.2	943				
1 1		_	0	210.2	949.5	949.9	950.2	950.6	950.9	951.2
28.0	948.2	948.5	948.9	949.2	952.9	953.3	953.6	953.9	954.3	954.6
28.1	951.6	951.9	952.3	952.6	956.3	956.7	957.0		957.7	958.0
28.2	955.0	955.3	955.6	956.0	959.7	960.0	960.4		961.1	961.4
28.3	958.3	958.7	959.0	959.4	959.7	963.4	963.8		964.4	964.8
28.4	961.7	962.1	962.4	962.8	903.1	9-3-4				
			(0	066.I	066.5	066.8	967.2	967.5		968.2
28.5	965.1	965.5	965.8	I	950.3	970.2	970.5	970.9		971.6
28.6	968.5	968.8	969.2	969.5	973.2	973.6	973.9		974.6	974.9
28.7	971.9	972.2	972.6	972.9	975.2	977.0	977.3		978.0	978.3
28.8	975.3	975.6	976.0	976.3	980.0	980.4	980.		981.4	981.7
28.9	978.7	979.0	979.3	979.7	900.0	955.4	1			0
			0	083.1	983.4	983.7	084.	1 984		
29.0	982.1	982.4	982.7		086.8	987.1		5 987.		
20.1	985.4	985.8	986.1	986.5	000.2	990.5		991.		
20.2	988.8	989.2	989.5	989.8		993.9			6 994.9	995.3
29.3	992.2	992.6	992.9	993.2	993.6	993.9				998.6
29.4	995.6	995.9	996.3	996.6	997.0	997.5	1			
	1				1000.4	1000.7	1001.	0 1001.	4 1001.7	
29.5	999.0	999.3	999.7	1000.0	1000.4	1004.1		4 1004		
29.6	1002.4	1002.7	1003.1	1003.4	1007.1	1007.				
29.7	1005.8	1006.1	1006.4	1006.8	1010.5	1010.8	,		5 1011.0	
29.8	1000.1	1009.5	1009.8	1010.2	1013.9	1014.			.9 1015.	2 1015.6
20.0	1012.5	1012.9	1013.2	1013.5	1013.9	1				. 1
	1			1016.9	1017.3	1017.	6 1018	.0 1018		
30.0	1015.9	1016.3	1016.6		1020.7			.3 1021	.7 1022.	
30.1	1019.3		1020.0	1020.3	1024.0			.7 1025		
30.2	1022.7		1023.4	1023.7				.1 1028		
30.3	1026.1		1026.8	1027.1	1030.8	. 1			.8 1032.	2 1032.5
30.4	1029.5	1029.8	1030.1	1030.5	1030.0	1232.				
1 "				10220	1034.2	1034	5 1034			
30.5	1032.9									
30.6	1036.2						7	1.7 104		
30.7	1039.0							5.0 104		
30.8	1043.0							3.4 104	8.8 1049	.1 1049.
30.9	1046	1 1046.7	1047.1	1047.4	1047.0					
				1050.8	1051.	1 1051	.5 105			
31.0	1049.				_	1		5.2 105		
31.1	1053.									
31.2				1 2		2				
31.3	1059.			1 /	6.			5.4 106	5.7 1066	1066.
31.4		3 1063.	7 1064.0	1004.	1004.	1				6-
				1 1067.	7 1068.	1 1068	3.4 106		9.1 1069	
31.5	1066			T '				2.1 107	12.5 107	
31.6							5.2 107	5.5 10	75.9 107	- 1
31.7					- 0			8.9 10	79.2 107	
		.0 1077.	2 1077.		7 1 6			32.3 108	32.6 108	3.0 1083
31.8	10/0	.3 1080.	6 1080.	0 1081.						

TABLE 12.

BAROMETRIC MILLIMETERS (MERCURY) INTO MILLIBARS.

l mm. = 1.33322387 mb.

Milli- meters.	0	1	2	3	4	5	6	7	8	9
	mb.									
10	13.3	1.3	2.7	4.0 17.3	5·3 18.7	6.7 20.0	8.0	9.3	10.7	25.3
20	20.7	28.0	29.3	30.7	32.0	33.3	34.7	36.0	37.3	38.7
30	40.0	41.3	42.7	44.0	45.3	46.7	48.0	49.3	50.7	52.0
40	53.3	54.7	56.0	57.3	58.7	60.0	61.3	62.7	64.0	65.3
50	66.7	68.0	69.3	70.7	72.0	73.3	74.7	76.0	77-3	78.7
60	80.0	81.3	82.7 96.0	84.0 97.3	85.3 98.7	86.7	88.0	89.3	90.7	92.0
80	93.3 106.7	94.7	100.3	110.7	112.0	113.3	114.7	116.0	117.3	118.7
90	120.0	121.3	122.7	124.0	125.3	126.7	128.0	129.3	130.7	132.0
100	133.3	134.7	136.0	137.3	138.7	140.0	141.3	142.7	144.0	145.3
110	146.7	148.0	149.3	150.7	152.0	153.3	154.7	156.0	157.3	158.7
120	160.0	161.3	162.7	164.0	165.3	166.7	168.0	169.3	170.7	172.0
130	173.3	174.7	176.0	177.3	178.7	180.0 193.3	181.3	182.7	184.0	185.3
	100.7	100.0	109.3	190.7	192.0					190.7
150	200.0	201.3	202.7	204.0	205.3	206.6	208.0	209.3	210.6	212.0
160	213.3	214.6	216.0	217.3 230.6	218.6	220.0	221.3	222.6	224.0	225.3
180	240.0	241.3	242.6	244.0	245.3	246.6	248.0	240.3	250.6	252.0
190	253.3	254.6	256.0	257.3	258.6	260.0	261.3	262.6	264.0	265.3
200	266.6	268.0	269.3	270.6	272.0	273.3	274.6	276.0	277.3	278.6
210	280.0	281.3	282.6	284.0	285.3	286.6	288.0	289.3	290.6	292.0
220	293.3	294.6	296.0	297.3	298.6	300.0	301.3	302.6	304.0	305.3
230 240	306.6 320.0	308.0	309.3 322.6	310.6 324.0	312.0	313.3 326.6	314.6	316.0	317.3 330.6	318.6
							Ü			
250 260	333·3 346.6	334.6 348.0	336.0 349.3	337·3 350.6	338.6 352.0	340.0 353.3	341.3 354.6	342.6 356.0	344.0 357.3	345·3 358.6
270	360.0	361.3	362.6	364.0	365.3	366.6	368.0	369.3	370.6	372.0
280	373.3	374.6	376.0	377-3	378.6	380.0	381.3	382.6	384.0	385.3
290	386.6	388.0	389.3	390.6	392.0	393.3	394.6	396.0	397.3	398.6
300	400.0	401.3	402.6	404.0	405.3	406.6	408.0	409.3	410.6	412.0
310	413.3	414.6	416.0	417.3	418.6	420.0	421.3	422.6	424.0	425.3
320	426.6	428.0	429.3 442.6	430.6	432.0	433·3 446.6	434.6	436.0 449.3	437.3 450.6	438.6 452.0
330 340	440.0 453-3	441.3 454.6	456.0	457.3	445·3 458.6	460.0	461.3	462.6	464.0	465.3
350	466.6	468.0	469.3	470.6	472.0	473.3	474.6	476.0	477.3	478.6
300	480.0	481.3	482.6	484.0	485.3	486.6	488.0	489.3	490.6	492.0
370	493.3	494.6	496.0	497-3	498.6	500.0	501.3	502.6	504.0	505.3
380	506.6	508.0	509.3	510.6	512.0	513.3	514.6	516.0	517.3	518.6
390	520.0	521.3	522.6	524.0	525.3	526.6	528.0	529.3	530.6	532.0
400	533.3	534.6	536.0	537.3	538.6	540.0	541.3	542.6	544.0	545.3
410 420	546.6 560.0	548.0 561.3	549.3 562.6	550.6 564.0	552.0 565.3	553·3 566.6	554.6 568.0	556.0 569.3	557·3 570.6	558.6 572.0
430	573.3	574.6	576.0	577.3	578.6	580.0	581.3	582.6	584.0	585.3
440	586.6	588.0	589.3	590.6	592.0	593.3	594.6	596.0	597.3	598.6
						-				

TABLE 12.
BAROMETRIC MILLIMETERS (MERCURY) INTO MILLIBARS.

1 mm. = 1.33322387 mb.

Milli- meters.	0	1	2	3	4	5	6	7	8	9
-	ļ ———				-	-	l		-	
	mb.									
450	600.0	601.3	602.6	604.0	605.3	606.6	608.0	609.3	610.6	611.9
460	613.3	614.6	615.9	617.3	618.6	619.9	621.3	622.6	623.9	625.3
470	626.6	627.9	629.3	630.6	631.9	633.3	634.6	635.9	637.3	638.6
480	639.9	641.3	642.6	643.9	645.3	646.6	647.9	649.3	650.6	651.9
490	653.3	654.6	655.9	657.3	658.6	659.9	661.3	662.6	663.9	665.3
500	666.6	667.9	669.3	670.6	671.0	673.3	674.6	675.0	677.3	678.6
510	679.9	681.3	682.6	683.9	685.3	686.6	687.9	689.3	600.6	601.0
520	693.3	694.6	695.9	697.3	698.6	699.9	701.3	702.6	703.0	705.3
530	706.6	707.9	709.3	710.6	711.9	713.3	714.6	715.0	717.3	718.6
540	719.9	721.3	722.6	723.9	725.3	726.6	727.9	729.3	730.6	731.9
550	733.3	734.6	735.9	737-3	738.6	739.9	741.3	742.6	743.9	745-3
560	746.6	747.9	749.3	750.6	751.0	753.3	754.6	755.9	757.3	758.6
570	759.9	761.3	762.6	763.9	765.3	766.6	767.9	760.3	770.6	771.0
580	773.3	774.6	775.9	777.3	778.6	779.9	781.3	782.6	783.9	785.3
590	786.6	787.9	789.3	790.6	791.9	793.3	794.6	795.9	797.3	798.6
600		0	0	0	0	0.66	0	0	0 (
600	799.9	801.3	802.6	803.9	805.3	806.6	807.9	809.3	810.6	811.9
620	813.3	814.6	815.9	817.3	818.6	819.9	821.3	822.6	823.9	825.3
	826.6	827.9	829.3	830.6	831.9	833.3	834.6	835.9	837.3	838.6
630	839.9	841.3	842.6	843.9	845.3	846.6	847.9	849.3	850.6	851.9
040	853.3	854.6	855.9	857.3	858.6	859.9	861.3	862.6	863.9	865.3
650	866.6	867.9	869.3	870.6	871.9	873.3	874.6	875.9	877.3	878.6
660	879.9	881.3	882.6	883.9	885.3	886.6	887.9	889.3	890.6	891.9
670	893.3	894.6	895.9	897.3	898.6	899.9	901.3	902.6	903.9	905.3
680	906.6	907.9	909.3	910.6	911.9	913.3	914.6	915.9	917.3	918.6
69 0	919.9	921.3	922.6	923.9	925.3	926.6	927.9	929.3	930.6	931.9
700	933.3	934.6	935-9	937.3	938.6	939.9	041.3	942.6	943.9	945.3
710	946.6	947.9	949.3	950.6	951.9	953.3	954.6	955.9	957.3	958.6
720	959.9	961.3	962.6	963.9	965.3	966.6	967.9	969.3	970.6	971.9
730	973-3	974.6	975.9	977.3	978.6	979.9	981.3	982.6	983.9	985.3
740	986.6	987.9	989.3	990.6	991.9	993.3	994.6	995.9	997-3	998.6
750	0.000	1001.3	1002.6	1003.0	1005.3	1006.6	1007.0	1000.3	1010.6	1011.0
760	1013.3	1014.6	1015.0	1017.2	1018.6	1010.0	1021.2	1022.6	1023.0	1025.2
770	1026.6	1027.0	1020.2	1030.6	1031.0	1033.2	1034.6	1035.0	1023.9	1038.6
780	1030.0	1041.2	1042.6	1043.0	1045.2	1046.6	1047.0	1040.2	1050.6	1051.0
790	1053.2	1054.6	1055.9	1057.2	1058.6	1050.0	1061.2	1062.6	1063.0	1065.2
7.7	- 55	- 54.0	-33.9	-37-2		-39.9			2.3.9	3.2

FEET INTO METERS.

r foot = 0 3048006 meter.

Feet, O	2000											
0		Feet.	0	1	2	3	4	5	6	7	8	9
10	ı		m.	m.	m.	111.	m.	m.	m.	m.	m.	m.
20	H	0	0.000	0.305	0.610	0.914	1.219	1.524	1.829	2.134	2.438	
20	l	10	3.048	3-353	3.658	3.962	4.267	4.572	4.877	5,182	5.486	5,701
The color of the	H											
15.240	H										1	
60	ı		12.192	12.497	12.502	13.100	13.411	13.716	14.021	14.326	14.630	14.935
Too 21,336 21,641 21,946 22,250 23,556 23,165 23,470 23,774 24,079 27,127 28,249 28,346 25,598 25,693 25,598 26,213 26,518 26,578 29,870 20,970 21,336 216,41 219,46 222,50 225,55 228,60 231,65 234,70 237,74 24,079 20,970 27,432 27,737 28,042 225,95 225,55 228,60 231,65 234,70 237,74 24,079 20,970 27,432 27,737 28,042 239,94 252,98 256,03 259,08 262,13 265,18 265,22 27,12 20,179 20,422 20,726 20,422 20,726 20,422 20,726 20,422 20,726 20,422 20,726 20,422 20,726 20,422 20,726 20,422 20,726 20,422 20,726 20,422 20,726 20,422 20,726 20,422 20,726 20,422 20,726 20,422 20,42	L											
\$\begin{array}{c c c c c c c c c c c c c c c c c c c	L					(-	201					
100	Ь											
100		90	27.432	27.737	28.042						29.870	
200			0	10	20	30	40	50	60	70	80	90
200	ı											
300												
\$\frac{400}{500} 121.92 124.97 128.02 131.06 134.11 137.16 140.21 143.26 146.30 149.35 \$\frac{500}{600} 152.40 155.45 158.50 161.54 164.59 167.64 170.69 173.74 176.78 179.83 \$700 213.36 216.41 219.46 222.50 225.55 228.60 231.65 234.70 237.74 240.79 \$800 243.84 246.89 249.94 252.98 256.03 259.08 262.13 265.18 268.22 271.27 \$900 274.32 277.37 280.42 283.46 286.51 289.56 292.61 295.66 298.70 301.75 \$1000 304.80 307.85 310.90 313.94 316.99 320.04 323.09 326.14 339.31 334.38 344.42 347.47 350.52 355.57 356.62 359.07 390.17 \$1300 365.76 368.81 371.86 374.90 377.95 381.00 384.05 387.10 390.14 399.29 402.34 405.38 405.38 408.43 411.48 414.53 417.58 420.62 423.67 \$1400 426.72 429.77 432.82 435.86 438.91 441.66 445.01 448.06 451.10 454.15 \$1500 457.20 460.25 463.30 466.34 469.39 472.44 475.49 478.54 481.58 484.63 \$1600 487.68 490.73 493.78 496.82 499.87 502.92 505.97 509.02 512.07 515.11 \$1800 548.64 551.69 554.74 557.79 560.83 563.88 566.93 569.85 573.03 576.07 \$1900 579.12 582.17 585.22 588.27 591.31 594.36 597.41 600.46 603.51 606.55 \$2000 609.66 612.65 615.70 618.75 618.75 655.32 658.80 688.85 619.90 609.49 676.66 679.71 682.75 685.80 688.85 619.90 697.99 \$2300 761.04 704.09 707.14 710.19 713.23 716.28 719.33 722.38 725.43 728.47 \$2600 792.48 795.53 798.58 801.63 804.67 807.72 810.77 813.82 816.87 819.91 \$2600 792.48 795.53 798.58 801.63 804.67 807.72 810.77 813.82 806.82 809.83 809.02 803.07 806.11 899.16 902.21 905.26 908.31 \$3000 914.48 947.93 950.98 950.98 950.98 950.98 950.98 950.98 950.98 950.98 950.98 950.98 950.98 960.29 90.50 90.50 90.75			-									
182.88 185.93 188.98 192.02 195.07 198.12 201.17 204.22 207.26 210.31 204.69 246.89 246.89 249.94 252.98 256.03 259.08 262.13 265.18 268.22 271.27 204.29 207.26 237.74 240.79 204.29 207.26 237.74 240.79 204.29 207.26 2							0 0				1	
The color The	ı	500	152.40	155.45	158.50	161.54	164.59	167.64	170.69	173.74	176.78	179.83
\$\frac{800}{900}	Ш					192.02	195.07		201.17		207.26	210.31
1000	H											
1000	ı											
1100		1000	304.80	307.85	310.00	312 04						
1200	ı.				-							
1400	L					374.90			384.05			
1500	ı	~										
1600												
1800 548.64 551.69 554.74 557.79 560.83 563.88 566.93 569.98 573.03 576.07 2000 609.60 612.65 615.70 618.75 621.79 624.84 627.89 630.94 633.99 637.03 2100 640.08 643.13 646.18 649.23 652.27 655.32 658.37 661.42 664.47 667.51 2200 670.56 673.61 676.66 679.71 682.75 685.80 688.85 691.90 694.95 697.99 2300 701.04 704.09 707.14 710.19 713.23 716.28 719.33 722.38 725.43 728.47 2400 731.52 734.57 737.62 740.67 743.71 774.79 779.43 772.24 780.29 783.34 786.39 789.43 2500 762.00 765.05 768.10 771.15 774.19 777.24 780.29 783.34 786.39 789.43 2700 <th></th> <th>1600</th> <th>487.68</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>		1600	487.68									
1900 579.12 582.17 585.22 588.27 591.31 594.36 597.41 600.46 603.51 606.55	Į.											
2000 609.60 612.65 615.70 618.75 621.79 624.84 627.89 630.94 633.99 637.03 2100 640.08 643.13 646.18 649.23 652.27 655.32 658.37 661.42 664.47 667.51 2200 670.56 673.61 676.66 679.71 682.75 685.80 688.85 691.90 694.95 697.99 2300 701.04 704.09 707.14 710.19 713.23 746.76 749.81 752.86 755.91 728.43 728.47 2400 762.00 765.05 768.10 771.15 774.10 777.24 780.29 783.34 786.39 755.91 758.95 2500 792.48 795.53 798.58 801.63 804.67 807.72 810.77 813.82 816.87 819.91 2700 822.96 826.01 829.06 832.11 835.15 838.20 841.25 844.30 847.35 850.39 3000 <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>- 0</th> <th></th> <th></th> <th></th> <th></th> <th></th>							- 0					
2100 640.08 643.13 646.18 649.23 652.27 658.37 661.42 664.47 667.51 670.56 673.61 676.66 679.71 682.75 685.80 688.85 691.90 694.95 697.99 2400 731.52 734.57 737.62 740.67 743.71 746.76 749.81 752.86 755.91 758.95 749.81 752.86 755.91 758.95 759.00 822.96 826.01 829.06 832.11 835.15 838.20 841.25 844.30 847.35 850.39 886.97 890.02 893.07 896.11 897.99 905.26 998.31 911.35 944.88 947.93 950.98 954.03 995.05 941.83 947.93 950.98 954.03 995.05 975.36												
2200	1	1										
2400 731.52 734.57 737.62 740.67 743.71 746.76 749.81 752.86 755.91 758.95 2500 762.00 765.05 768.10 771.15 774.19 777.24 780.29 783.34 786.39 789.43 2600 792.48 795.53 798.58 801.63 804.67 807.72 813.82 816.87 819.91 2700 822.96 826.01 829.06 832.11 835.15 838.20 841.25 844.30 847.35 850.39 2800 833.44 856.49 859.54 862.59 865.63 868.68 871.73 874.78 877.83 880.87 2900 883.92 886.97 890.02 923.55 926.59 929.64 932.69 935.74 938.79 911.35 3000 914.40 917.45 920.50 923.55 926.59 929.64 932.69 935.74 938.79 911.35 3200 975.36 978.41 981.46 <th>ı</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>682.75</th> <th>685.8o</th> <th>688.85</th> <th></th> <th>694.95</th> <th>697.99</th>	ı						682.75	685.8o	688.85		694.95	697.99
2500 762.00 765.05 768.10 771.15 774.19 777.24 780.29 783.34 786.39 789.43 2600 792.48 795.53 798.58 801.63 804.67 807.72 810.77 813.82 816.87 819.91 2700 822.96 826.01 829.06 832.11 835.15 838.20 841.25 844.30 847.35 850.39 2800 853.44 856.49 859.54 862.59 865.63 868.68 871.73 874.78 877.83 880.87 2900 883.92 886.97 890.02 893.07 896.11 891.6 902.21 905.26 908.31 911.35 3000 914.40 917.45 920.50 923.55 926.59 929.64 932.69 935.74 938.79 941.83 3200 975.36 978.41 981.46 984.51 987.55 1960.12 963.17 966.22 969.27 972.31 3400 1005.84 1008.89 </th <th></th>												
2600 792.48 795.53 798.58 801.63 804.67 807.72 810.77 813.82 816.87 819.91 2700 822.96 826.01 829.06 832.11 835.15 838.20 841.25 844.30 847.35 850.39 853.44 856.49 859.54 862.59 865.63 868.68 871.73 874.78 877.83 880.87 890.00 914.40 917.45 920.50 923.55 926.59 929.64 932.69 935.74 938.79 941.83 3100 944.88 947.93 950.98 954.03 957.07 960.12 963.17 966.22 969.27 972.31 933.00 1005.84 1008.89 1011.94 1014.99 1018.03 1005.84 1008.89 1011.94 1014.99 1018.03 1036.32 1039.37 1042.42 1045.47 1048.51 1051.56 1054.61 1057.66 1060.71 1063.75 1097.28 1100.33 1103.38 1103.38 1103.38 1103.38 1103.38 1133.86 1136.43 1109.47 1143.00 1146.05 1149.10 1152.15 1155.51 1155.19 1188.26 1158.24 1161.29 1164.34 1107.39 1170.43 1175.34 1176.35 1179.58 1182.63 1185.67 1213.11 1216.15												
2700 822.96 826.01 829.06 832.11 835.15 838.20 841.25 844.30 847.35 850.39 2800 853.44 856.49 859.54 862.59 865.63 868.68 871.73 874.78 877.83 886.87 2900 914.40 917.45 920.50 923.55 926.59 941.85 947.93 954.98 954.93 954.93 954.93 954.93 954.93 955.96 935.74 938.79 941.85 3200 975.36 978.41 981.46 984.51 987.55 960.12 963.17 966.22 969.27 972.31 3300 1005.84 1008.89 1011.94 1014.99 1018.03 1036.32 1036.32 1039.37 1042.42 1045.47 1048.51 1051.56 1057.66 1060.71 1063.75 3500 1066.80 1069.85 1072.90 1075.95 1078.99 1112.57 1118.62 1121.67 1124.71 3700 1127.76 130.81 133.86 136.91 1139.95 1143.00 1146.05 1149.10 1152.15 1155.19 3800 1158.24 1161.29 1164.34 1107.39 1170.43 1170.38 1175.38 1176.53 1179.58 1182.63 1185.67 1188.72 1191.77 1194.82 1197.87 1200.91 1203.96 1207.01 1210.06 1213.11 1216.15	ı											
2900 883.92 886.97 890.02 893.07 896.11 899.16 902.21 905.26 908.31 911.35 3000 914.40 917.45 920.50 923.55 926.59 929.64 932.69 935.74 938.79 941.83 3100 944.88 947.93 950.98 954.03 957.07 966.12 963.17 966.22 969.27 972.31 3200 975.36 978.41 981.46 984.51 987.55 990.60 993.65 996.70 999.75 1002.79 3300 1005.84 1008.89 1011.94 1014.99 1018.03 1021.08 1024.13 1027.18 1030.23 1033.27 1036.32 1039.37 1042.42 1045.47 1048.51 1051.56 1054.61 1057.66 1060.71 1063.75 3500 1066.80 1069.85 11072.90 1075.95 1078.99 1112.52 1115.57 1118.62 1121.67 1124.71 3700 1127.76 1130.81 1133.86 1136.94 1139.95 1143.00 1175.41 116.53 1179.58 1182.63 1155.19 1155.67 1186.22 11161.29 1164.34 1107.39 1170.43 1170.43 1170.43 1170.43 1170.43 1170.43 1170.43 1170.45 1120.06 1213.11 1216.15	ı		822.96	826.01	829.06							
3000 914.40 917.45 920.50 923.55 926.59 929.64 932.69 935.74 938.79 941.83 3100 944.88 947.93 950.98 954.03 957.07 960.12 963.17 966.22 969.27 972.31 3200 975.36 978.41 981.46 984.51 987.55 990.60 ,993.65 996.70 999.75 1002.79 3300 1005.84 1008.89 1011.94 1014.99 1018.03 1021.08 1024.13 1027.18 1030.23 1033.27 3500 1066.80 1069.85 1672.90 1075.95 1078.99 1082.04 1085.09 1088.14 1091.19 1094.23 3700 1127.76 1130.81 1133.86 1136.91 1139.95 1143.00 1146.05 1149.10 1152.15 1155.51 3800 1158.24 1161.29 1164.34 1107.39 1170.43 1173.48 1120.06 1213.11 1216.15												
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3200 975.36 978.41 981.46 984.51 987.55 990.60 ,993.65 996.70 999.75 1002.79 3300 1005.84 1030.89 1011.94 1014.99 1018.03 1021.08 1021.18 1027.18 1030.23 1033.27 3500 1066.80 1069.85 1072.90 1075.95 1078.99 1082.04 1085.09 1088.14 1091.19 1094.23 3700 1127.76 130.81 1133.86 1136.91 1139.95 1144.30 1146.05 1149.10 1152.15 1155.19 3800 1158.24 1161.29 1164.34 1107.39 1170.43 1173.48 1176.53 1179.58 1182.63 1185.67 1188.72 1191.77 1194.82 1197.87 1200.91 1203.96 1207.01 1210.06 1213.11 1216.15												
3500 1066.80 1069.85 1072.90 1075.95 1078.99 1082.04 1085.09 1088.14 1091.19 1094.23 3700 3700 3800 1158.24 1161.29 1164.34 1167.39 1170.43 3900 1188.72 1191.77 1194.82 1197.87 1200.91 1200.91 1210.06 1213.11 1216.15			975.36	978.41	981.46							
3500 1066.80 1069.85 1672.90 1075.95 1078.99 1082.04 1085.09 1088.14 1091.19 1094.23 3700 1127.76 1130.81 1133.86 1136.91 1139.95 1143.00 1146.05 1149.10 1152.15 1155.19 3800 1188.72 1191.77 1194.82 1197.87 1200.91 1207.01 1207.01 1210.06 1213.11 1216.15			1005.84	1008.89								
3600 1097.28 1100.33 1103.38 1106.43 1109.47 1112.52 1115.57 1118.62 1121.67 1122.71 130.81 1133.86 1136.91 1139.95 1143.00 1158.24 1161.29 1164.34 1107.39 1170.43 1170.43 1170.53 1179.58 1182.63 1185.67 1188.72 1191.77 1194.82 1197.87 1200.91 1203.96 1207.01 1210.06 1213.11 1216.15												
3700 1127.76 1130.81 1133.86 1136.91 1139.95 1143.00 1146.05 1149.10 1152.15 1155.19 1158.24 1161.29 1164.34 1167.39 1170.43 1173.48 1176.53 1179.58 1182.63 1185.67 1188.72 1191.77 1194.82 1197.87 1200.91 1203.96 1207.01 1210.06 1213.11 1216.15			1097.28	1100.33	1103.38	1106.13	1109.47	1112.52	1115.57	1118.62	1121.67	1124.71
3900 1158.72 1191.77 1194.82 1197.87 1200.91 1203.96 1207.01 1210.06 1213.11 1216.15			1127.76	1130.81	1133.86	1136.91	1139.95	1143.00	1146.05	1149.10	1152.15	1155.19
			1150.24	1161.29	1164.34	1107.39	1170.43	1173.48	1176.53	1179.58	1182.63	1185.67
1225.30 1225.30 1225.35 1231.39 1234.44 1237.49 1240.54 1243.59 1240.03											1	-
		.000	1219.20	1222.23	1225.30	1220.35	1231.39	1234.44	1237.49	1240.54	1243.59	1240.03

FEET INTO METERS.

1 foot == 0.3048006 meter.

Feet.	0	10	20	30	40	50	60	70	80	90
	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
4000	1219.2	1222.3	1225.3	1228.3	1231.4	1234.4	1237.5	1240.5	1243.6	1246.6
4100 4200	1249.7	1252.7	1255.8	1258.8	1261.9	1264.9	1268.0	1271.0	1274.1	1277.1
4300	1310.6	1313.7	1316.7	1319.8	1322.8	1325.9	1328.9	1332.0	1335.0	1338.1
4400	1341.1	1344.2	1347.2	1350.3	1353.3	1356.4	1359.4	1362.5	1365.5	1368.6
4500	1371.6	1374.7	1377.7	1380.7	1383.8	1386.8	1389.9	1392.9	1396.0	1399.0
4600	1402.1	1405.1	1408.2	1411.2	1414.3	1417.3	1420.4	1423.4	1426.5	1429.5
4700 4800	1432.6	1435.6	1438.7	1441.7	1444.8	1447.8	1450.9	1453.9	1456.9	1460.0
4900	1493.5	1496.6	1499.6	1502.7	1505.7	1508.8	1511.8	1514.9	1517.9	1521.0
5000	1524.0	1527.1	1530.1	1533.1	1536.2	1539.2	1542.3	1545.3	1548.4	1551.4
5100	1554.5	1557.5	1560.6	1563.6	1566.7	1569.7	1572.8	1575.8	1578.9	1581.9
5200	1585.0	1588.0	1591.1	1594.1	1597.2	1600.2	1603.3	1606.3 1636.8	1639.8	1612.4
5300 5400	1615.4	1618.5 1649.0	1621.5. 1652.0	1624.6 1655.1	1627.6 1658.1	1661.2	1633.7	1667.3	1670.3	1673.4
5500	1676.4	1679.5	1682.5	1685.5	1688.6	1691.6	1694.7	1697.7	1700.8	1703.8
5600	1706.9	1709.9	1713.0	1716.0	1719.1	1722.1	1725.2	1728.2	1731.3	1734.3
5700	1737.4 1767.8	1740.4	1743.5	1746.5	1749.6	1752.6	1755.7 1786.1	1758.7	1761.7 1792.2	1764.8
5800 5900	1798.3	1770.9 1801.4	1773.9 1804.4	1807.5	1810.5	1813.6	1816.6	1819.7	1822.7	1825.8
6000	1828.8	1831.9	1834.9	1837.9	1841.0	1844.0	1847.1	1850.1	1853.2	1856.2
6100	1859.3	1862.3	1865.4	1868.4	1871.5	1874.5	1877.6	1880.6	1883.7	1886.7
6200 6300	1889.8	1892.8	1895.9	1898.9	1902.0	1905.0	1908.1	1911.1	1914.1	1917.2
6400	1950.7	1953.8	1956.8	1959.9	1962.9	1966.0	1969.0	1972.1	1975.1	1978.2
6500	1981.2	1984.3	1987.3	1990.3	1993.4	1996.4	1999.5	2002.5	2005.6	2008.6
6600 6700	2011.7	2014.7	2017.8	2020.8	2023.9	2026.9	2030.0	2033.0	2036.1	2039.1
6800	2072.6	2075.7	2078.7	2081.8	2084.8	2087.9	2090.9	2094.0	2097.0	2100.I
6900	2103.1	2106.2	2109.2	2112.3	2115.3	2118.4	2121.4	2124.5	2127.5	2130.6
7000	2133.6	2136.7	2139.7	2142.7	2145.8	2148.8	2151.9	2154.9	2158.0	2161.0
7100 7200	2164.1 2194.6	2167.1	2170.2	2173.2	2176.3	2179.3	2182.4	2185.4	2188.5	2191.5
7300	2225.0	2228.1	2231.1	2234.2	2237.2	2240.3	2243.3	2246.4	2249.4	2252.5
7400	2255.5	2258.6	2261.6	2264.7	2267.7	2270.8	2273.S	2276.9	2279.9	2283.0
7500	2286.0	2289.1	2292.1	2295.1	2298.2	2301.2	2304.3	2307.3	2310.4	2313.4
7600 7700	2316.5	2319.5	2322.6 2353.1	2325.6 2356.1	2328.7	2331.7 2362.2	2334.8	2337.8	2340.9	2343.9
7800	2377.4	2380.5	2383.5	2386.6	2389.6	2392.7	2395.7	2398.8	2401.8	2404.9
7900	2407.9	2411.0	2414.0	2417.1	2420.1	2423.2	2426.2	2429.3	2432.3	2435.4
8000	2438.4	2441.5	2444.5	2447.5	2450.6	2453.6	2456.7	2459.7	2462.8	2465.8
8100 8200	2468.9 2499.4	2471.9 2502.4	2475.0 2505.5	2478.0 2508.5	2481.1 2511.6	2484.1 2514.6	2487.2	2490.2 2520.7	2493.3 2523.7	2496.3 2526.8
8300	2529.8	2532.9	2535.9	2539.0	2542.0	2545. I	2548.1	2551.2	2554.2	2557.3
8400	2560.3	2563.4	2566.4	2569.5	2572.5	2575.6	2578.6	2581.7	2584.7	2587.8
8500	2590.8	2593.9	2596.9	2599.9	2603.0	2606.0	2609.1	2612.1	2615.2	2618.2
8600 8700	2621.3	2624.3 2654.8	2627.4	2630.4	2633.5 2664.0	2636.5	2639.6 2670.1	2642.6 2673.1	2645.7 2676.1	2648.7
8800	2682.2	2685.3	2688.3	2691.4	2694.4	2697.5	2700.5	2703.6	2706.6	2709.7
8900	2712.7	2715.8	2718.8	2721.9	2724.9	2728.0	2731.0	2734. I	2737.1	2740.2
9000	2743.2	2746.3	2749.3	2752.3	2755.4	2758.4	2761.5	2764.5	2767.6	2770.6

METERS INTO FEET.

I meter = 39.3700 inches = 3.280833 feet.

Meters.	0	1	2	3	4	5	6	7	8	9
	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
0	0.00	3.28	6.56	9.84	13.12	16.40	19.68	22.97	26.25	29.53
10	32.81	36.09	39.37	42.65	45.93	49.21	52.49	55.77	59.05	62.34
20	65.62	68.90	72.18	75.46	78.74	82.02	85.30	88.58	91.86	95.14
30	98.42	101.71	104.99	108.27	111.55	114.83	118.11	121.39	124.67	12 7.9 5 160.76
40	131.23	134.51	137.79	141.08	144.36	147.64	150.92	154.20	137.40	100.70
50	164.04	167.32	170.60	173.88	177.16	180.45	183.73	187.01	190.29	193.57
60	196.85	200.13	203.41	206.69	209.97	213.25	216.53	219.82	223.10	226.38
70	229.66	232.94	236.22	239.50 272.31	242.78 275.59	246.06 278.87	249.34 282.15	252.62 285.43	255.90 28 \$. 71	259.19
80 90	262.47 295.27	265.75 298.56	269.03 301.84	305.12	308.40	311.68	314.96	318.24	321.52	324.80
		331.36	334.64	337.93	341.21	344.49	347.77	351.05	354.33	357.61
110	328.08 360.89	364.17	367.45	370.73	374.01	377.30	380.58	383.86	387.14	390.42
120	393.70	396.98	400.26	403.54	406.82	410.10	413.38	416.67	419.95	423.23
130	426.51	429.79	433.07	436.35	439.63	442.91	446.19	449.47	452.75	456.04
140	459.32	462.60	465.88	469.16	472.44	475.72	479.00	482.28	485.56	488.84
150	492.12	495.41	498.69	501.97	505.25	508.53	511.81	515.09	518.37	521.65
160	524.93	528.21	531.49	534.78	538.06	541.34	544.62	547.90	551.18	554.46
170	557.74	561.02	564.30	567.58	570.86	574.15	577.43	580.71	583.99	587.27
180	590.55	593.83	597.11	600.39	603.67	606.95	610.23	613.52	616.So	620.08
190	623.36	626.64	629.92	633.20	636.48	639.76	643.04	646.32	649.60	652.89
200	656.17	659.45	662.73	666.01	669.29	672.57	675.85	679.13	682.41	685.69
210	688.97	692.26	695.54	698.82	702.10	705.38	708.66	711.94	715.22	718.50
220	721.78	725.06	728.34	731.63	734.91	738.19	741.47	744.75	748.03 780.84	751.31 784.12
230	754-59	757.87 790.68	761.15	764.43	767.71 Soo.52	771.00 So3.So	807.08	810.37	813.65	816.93
240	787.40									
250	820.21	823.49	826.77	830.05	833.33	836.61	839.89	843.17	846.45	849.74
260	853.02	856.30	859.58	862.86 895.67	866.14	\$69.42 902.23	872.70 905.51	875.98 908.79	879.26	882.54 915.35
270 280	\$85.82 918.63	921.91	892.39 925.19	928.48	931.76	935.04		941.60	944.88	948.16
290	951.44	954.72	958.00		964.56	967.85	971.13	974.41	977.69	980.97
						1000 65	1002 02	1007.22	1010 50	1013.78
300	984.25	987.53	990.81	994.09	1030.18	1033.46	1036.74	10/0.02	1043.30	1046.59
320	1049.87			1059.71	1062.99	1066.27	1069.55	1072.83	1076.11	1079.39
330	1082.67	1085.96						1105.64		1112.20
340	1115.48	1118.76	1122.04	1125.33	1128.61	1131.89	1135.17	1138.45	1141.73	1145.01
350	1148.29	1151.57						1171.26		1177.82
360			1187.66	1190.94				1204.07		1210.63
370	0, 1	1217.19		1223.75				1236.87		1243.44
380	1246.72	1250.00		1256.56				1269.68		1276.24
390			1286.09					1302.49		1309.05
400	1312.33	1315.61	1318.89	1322.18	1325.46	1328.74	1332.02	1335.30		1341.86
410	1345.14	1348.42	1351.70	1354.98	1358.26	1361.55	1304.83	1368.11		1374.67
420	1377.95	1301.23	1384.51	1420.60	1422 88	1127 16	1430 44	1432.72	1437.00	1440.20
430 440	1443.57	1446.85	1417.32	1453.41	1456.69	1459.97	1463.25	1466.53	1469.81	1473.09
450	1476.37	1479.66	1482.94	1486.22	1489.50	1492.78	1496.06	1499.34	1502.62	1505.90
460	1509.18	1512.46	1515.74	1519.03	1522.31	1525.59	1528.87	1532.15	1535.43	1538.71
470	1541.99	1545.27	1548.55	1551.83	1555.11	1558.40	1561.68	1564.96	1568.24	1571.52
480	1574.80	1578.08	1581.36	1584.64	1587.92	1591.20	1594.48	1597.77	1601.05	1604.33
490						1			1	1637.14
500	1640.42	1643.70	1646.98	1650.26	1653.54	1656.82	1660.10	1663.38	1666.66	1669.94

METERS INTO FEET.

I meter = 39.3700 inches = 3 280833 feet.

Meters.	0	10	20	30	40	50	60	70	80	90
	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
500	1640.4	1673.2	1706.0	1738.8	1771.6	1804.5	1837.3	1870.1	1902.9	1935.7
600 700	1968.5	2001.3	2034.1	2066.9	2099.7 2427.8	2132.5	2165.3	2198.2 2526.2	2231.0	2263.8
800	2624.7	2329.4 2657.5	2690.3	2395.0 2723.I	2755.9	2788.7	2821.5	2854.3	2559.0 2887.1	2591.9 2919.9
900	2952.7	2985.6	3018.4	3051.2	3084.0	3116.8	3149.6	3182.4	3215.2	3248.0
1000	3280.8	3313.6	3346.4	3379-3	3412.1	3444.9	3477-7	3510.5	3543-3	3576.1
1100	3608.9	3641.7	3674.5	3707.3	3740.1	3773.0	3805.8	3838.6	3871.4	3904.2
1200 1300	3937.0 4265.1	3969.8	4002.6	4035.4	4396.3	4101.0	4133.8	4166.7	4199.5	4232.3
1400	4593.2	4626.0	4658.8	4691.6	4724.4	4757.2	4790.0	4822.8	4855.6	4888.4
1500	4921.2	4954.1	4986.9	5019.7	5052.5	5085.3	5118.1	5150.9	5183.7	5216.5
1600	5249.3	5282.1	5314.9	5347.8	5380.6	5413.4	5446.2	5479.0	5511.8	5544.6
170 0 1800	5577.4	5610.2	5643.0	5675.8	5708.6	5741.5	5774-3	5807.1	5839.9 6168.0	5872.7 6200.S
1900	5905.5 6233.6	5938.3 6266.4	5971.1 6 2 99.2	6332.0	6364.8	6069.5 6397.6	6102.3	6135.2	6496.0	6528.9
2000	6561.7	6594.5	6627.3	6660.1	6692.9	6725.7	6758.5	6791.3	6824.1	6856.9
2100	6889.7	6922.6	6955.4	6988.2	7021.0	7053.8	7086.6	7119.4	7152.2	7185.0
2200	7217.8	7250.6	7283.4	7316.3	7349.1	7381.9	7414.7	7447.5	7480.3	7513.1 7841.2
2300 2400	7545.9 7874.0	7578.7 7906.8	7611.5 7939.6	7644.3 7972.4	7677.1 8005.2	7710.0 8038.0	7742.8 8070.8	7775.6 S103.7	7808.4 8136.5	8169.3
2500	8202.1	8234.9	8267.7	8300.5	8333.3	S366.1	8398.9	8431.7	8464.5	8497.4
2600	8530.2	8563.0	8595.8	8628.6	8661.4	8694.2	8727.0		8792.6	8825.4
2700	8858.2	8891.1	8923.9	8956.7	8989.5	9022.3	9055.1	9087.9	9120.7	9153.5
2800 2900	9186.3 9514.4	9219.1	9251.9	9284.8	9317.6	9350.4 9678.5	9383.2	9416.0	9448.8	9809.7
3000	9842.5	9875.3	9908.1	9940.9	9973.7	10006.5	10039.3	10072.2	10105.0	10137.8
3100		10203.4								10465.9
3200	10498.7			10597.1		10662.7		10728.3	10761.1	10793.9
3300 3400	10826.7	10859.6		10925.2		11318.9	11023.6	11384.5	11417.3	11450.1
3500	11482.9	11515.7	11548.5	11581.3	11614.1	11647.0	11679.8	11712.6	11745.4	11778.2
3600		11843.8								12106.3
3700	12139.1	12171.9					12335.9		12401.5	12434.4
3800 3900	12467.2 12795.2			12565.6		12031.2		_	12729.6	13090.5
4000	13123.3	13156.1	13188.9	13221.8	13254.6	13287.4	13320.2	13353.0	13385.8	13418.6
4100		13484.2	13517.0	13549.8	13582.6	13615.5	13648.3	13681.1	13713.9	13746.7
4200	13779.5			13877.9				1 -	14042.0	
4300 4400	14107.6	14140.4	14173.2	14206.0		14271.6			14370.0	14402.9
4500	14763.7	14796.6	14829.4	14862.2	14895.0	14927.8	14960.6	14993.4	15026.2	15059.0
	15091.8	15124.6	15157.4	15190.3	15223.1	15255.9	15288.7	15321.5	15354.3	15387.1
4700		15452.7								
4800 4900	16076.1	15780.8 16108.9	16141.7	16174.5	16207.3	16240.1	16272.9	16305.7	16338.5	16371.4
5000	16404.2	16437.0	16469.8	16502.6	16535.4	16568.2	16601.0	16633.8	16666.6	16699.4
Ten Fee	ths of a me	eter.		0.2 0.3 0.656 0.9	3 0.4 984 1.31	0.5 2 1.640	o.6 1.968		0.8 0.9 1.625 2.9	

MILES INTO KILOMETERS.

1 mile = 1.609347 kilometers.

						,				
Miles.	0	1	2	3	4	5	6	7	8	9
0 10 20 30	km. 0 16 32 48	km. 2 18 34 50	km. 3 19 35 51	km. 5 21 37 53	km. 6 23 39 55	km. 8 24 40 56	km. 10 26 42 58	km. 11 27 43 60	km. 13 29 45 61	14 31 47 63
40 50 60 70 80 90	64 80 97 113 129 145	66 82 98 114 130 146	68 84 100 116 132 148	69 85 101 117 134 150	71 87 103 119 135	72 89 105 121 137 153	74 90 106 122 138 154	76 92 108 124 140 156	77 93 109 126 142 158	79 95 111 127 143 159
100	161	163	16.4	166	167	169	171	172	174	175
110	177	179	180	182	183	185	187	188	190	192
120	193	195	196	198	200	201	203	204	206	208
130	209	211	212	214	216	217	219	220	222	224
140	225	227	229	230	232	233	235	237	238	240
150	241	243	245	246	248	249	251	253	254	256
160	257	259	261	262	264	266	267	269	270	272
170	274	275	277	278	280	282	283	285	286	288
180	290	291	293	295	296	298	299	301	303	304
190	306	307	309	311	312	314	315	317	319	320
200	322	323	325	327	328	330	332	333	335	336
210	338	340	341	343	344	346	348	349	351	352
220	354	356	357	359	360	362	364	365	367	369
230	370	372	373	375	377	378	380	381	383	385
240	386	388	389	391	393	394	396	398	399	401
250	402	404	406	407	409	410	412	414	415	417
260	418	420	422	423	425	426	428	430	431	433
270	435	436	438	439	441	443	444	446	447	449
280	451	452	454	455	457	459	460	462	463	465
290	467	468	470	472	473	475	476	478	480	481
300	483	484	486	488	489	491	492	494	496	497
310	499	501	502	504	505	507	509	510	512	513
320	515	517	518	520	521	523	525	526	528	529
330	531	533	534	536	538	539	541	542	544	546
340	547	549	550	552	554	555	557	558	560	562
350	563	565	566	568	570	571	573	575	576	578
360	579	581	583	584	586	587	589	591	592	594
370	595	597	599	600	602	604	605	607	608	610
380	612	613	615	616	618	620	621	623	624	626
390	628	6 2 9	631	632	634	636	637	639	641	642
400	644	645	647	649	650	652	653	655	657	658
410	660	661	663	665	666	668	669	671	673	674
420	676	678	679	681	682	684	686	687	689	690
430	692	694	695	697	698	700	702	703	705	706
440	708	710	711	713	715	716	718	719	721	723
450	724	726	727	729	73 I	732	734	735	737	739
460	740	742	744	745	747	748	750	752	753	755
470	756	758	760	761	763	764,	766	768	769	771
480	772	774	776	778	779	781	782	784	785	787
490	789	790	792	793	795	797	798	800	801	803
510 520 530 540	805 821 837 853 869	806 822 838 855 871	808 824 840 856 872	809 826 842 858 874	811 827 843 859 875	813 829 845 861 877	\$14 \$30 \$47 863 879	\$16 832 848 864 880	818 834 850 866 882	819 835 851 867 884
550	885	887	888	890	892	893	895	896	898	

MILES INTO KILOMETERS.

Miles.	0	1	2	3	4	5	6	7	8	9
550 560 570 580 590	km. 885 901 917 933 950	km. 887 903 919 935 951	km. 888 904 921 937 953	km. 890 906 922 938 954	km. 892 908 924 940 956	km. 893 909 925 941 958	km. 895 911 927 943 959	km. 896 912 929 945 961	km. 898 914 930 946 962	km. 900 916 932 948 964
600 610 620 630 640	966 98 2 998 1014 1030	967 983 999 1015 1032	969 985 1001 1017 1033	970 987 1003 1019	972 988 1004 1020 1036	974 990 1006 1022 1038	975 991 1007 1024 1040	977 993 1009 1025 1041	978 995 1011 1027 1043	980 996 101 2 10 2 8 1044
650 660 670 680 690	1046 1062 1078 1094 1110	1048 1064 1080 1096 1112	1049 1065 1081 1098 1114	1051 1067 1083 1099 1115	1053 1069 1085 1101 1117	1054 1070 1086 1102 1118	1056 1072 1088 1104 1120	1057 1073 1090 1106 1122	1059 1075 1091 1107 1123	1061 1077 1093 1109 1125
700 710 720 730 740	1127 1143 1159 1175 1191	1128 1144 1160 1176 1193	1130 1146 1162 1178 1194	1131 1147 1164 1180 1196	1133 1149 1165 1181	1135 1151 1167 1183 1199	1136 1152 1168 1184 1201	1138 1154 1170 1186 1202	1139 1156 1172 1188 1204	1141 1157 1173 1189 1 2 05
750 760 770 780 790	1207 1223 1239 1255 1271	1209 1225 1241 1257 1273	1210 1226 1242 1259 1275	1212 1228 1244 1260 1276	1213 1230 1246 1262 1278	1215 1231 1247 1263 1279	1217 1233 1249 1265 1281	1218 1234 1250 1267 1283	1220 1236 1252 1268 1284	1221 1238 1254 1270 1286
800 810 820 830 840	1287 1304 1320 1336 1352	1289 1305 1321 1337 1353	1291 1307 1323 1339 1355	1292 1308 1324 1341 1357	1294 1310 1326 1342 1358	1296 1312 1328 1344 1360	1297 1313 1329 1345 1362	1299 1315 1331 1347 1363	1300 1316 1333 1349 1365	1302 1318 1334 1350 1366
850 860 870 880 890	1368 1384 1400 1416 1432	1370 1386 1402 1418 1434	1371 1387 1403 1419 1436	1373 1389 1405 1421 1437	1374 1390 1407 1423 1439	1376 1392 1408 1424 1440	1378 1394 1410 1426 1442	1379 1395 1411 1427 1444	1381 1397 1413 1429 1445	1382 1399 1415 1431 1447
900 910 920 930 940	1448 1464 1481 1497 1513	1450 1466 1482 1498 1514	1452 1468 1484 1500 1516	1453 1469 1485 1502 1518	1455 1471 1487 1503 1519	1456 1473 1489 1505 1521	1458 1474 1490 1506 1522	1460 1476 1492 1508 1524	1461 1477 1493 1510 1526	1463 1479 1495 1511 1527
950 960 970 980 990	1529 1545 1561 1577 1593	1530 1547 1563 1579 1595	1532 1548 1564 1580 1596	1534 1550 1566 1582 1598	1535 1551 1567 1584 1600	1537 1553 1569 1585 1601	1539 1555 1571 1587 1603 1619	1540 1556 1572 1588 1605	1542 1558 1574 1590 1606	1543 1559 1576 1592 1608
1000	Miles 1000 2000 3000 4000 5000	0 1609 0 3219 0 4828 0 6437	60° 70° 80° 90°	00 96 00 112 00 128 00 144	556 1 265 12 375 13 484 14	2000 3000 4000	km. 17703 19312 20922 22531 24140	Miles. 16000 17000 18000 19000 20000	km. 25750 27359 28968 30578 32187	1024

KILOMETERS INTO MILES.

1 kilometer = 0.621370 mile.

KIIo-	1						
meters. 0 1 2	3	4	5	6	7	8	9
Miles. Miles. Miles.	Miles.	Miles.	Miles.	Miles.	Miles.	Miles.	Miles.
0 0.0 0.6 1.2	1.9	2.5	3.1	3.7	4.3	5.0	5.6
10 6.2 6.8 7.5 20 12.4 13.0 13.7	8.1	8.7 14.9	9.3	9.9 16.2	10.6 16.8	11.2 17.4	11.8 18.0
20 12.4 13.0 13.7 30 18.6 19.3 19.9	14.3	21.1	15.5	22.4	23.0	23.6	24.2
40 24.9 25.5 26.1	26.7	27.3	28.0	28.6	29.2	29.8	30.4
50 31.1 31.7 32.3	32.9	33.6	34.2	34.8	35.4	36.0	36.7
60 37.3 37.9 38.5 70 43.5 44.1 44.7	39. I	39.8 46.0	40.4 46.6	41.0 47.2	41.6 47.8	42.3 48.5	42.9
70 43.5 44.1 44.7 80 49.7 50.3 51.0	45.4 51.6	52.2	52.8	53.4	54.1	54.7	49. I 55. 3
90 55.9 56.5 57.2	57.8	58.4	59.0	59.7	60.3	60.9	61.5
100 62.1 62.8 63.4	64.0	64.6	65.2	65.9	66.5	67.1	67.7
110 68.4 69.0 69.6 120 74.6 75.2 75.8	70.2 76.4	70.8 77.0	71.5 77.7	72.1 78.3	72.7 78.9	73·3 79·5	73.9 80.2
130 80.8 81.4 82.0	82.6	83.3	83.9	84.5	85.1	85.7	86.4
140 87.0 87.6 88.2	88.9	89.5	90. I	90.7	91.3	92.0	92.6
150 93.2 93.8 94.4	95.1	95.7	96.3	96.9	97.6	98.2	98.8
160 99.4 100.0 100.7 170 105.6 106.3 106.9	101.3	101.9	102.5	103.1	103.8	104.4 110.6	105.0
180 111.8 112.5 113.1	113.7	114.3	115.0	115.6	116.2	116.8	117.4
190 118.1 118.7 119.3	119.9	120.5	121.2	121.8	122.4	123.0	123.7
	126.1	126.8	127.4	128.0	128.6	129.2	129.9
	132.4	133.0 139.2	133.6	134.2	134.8	135.5	136.1
230 142.9 143.5 144.2	144.8	145.4	146.0	146.6	147.3	147.9	148.5
240 149.1 149.8 150.4	151.0	151.6	152.2	152.9	153.5	154.1	154.7
250 155.3 156.0 156.6	157.2	157.8	158.4	159.1	159.7	160.3	160.9
260 161.6 162.2 162.8 270 167.8 168.4 169.0	163.4	164.0 170.3	164.7 170.9	165.3	165.9 172.1	166.5 172.7	167.1
280 174.0 174.6 175.2	175.8	176.5	177.1	177.7	178.3	179.0	179.6
290 180.2 180.8 181.4	182.1	182.7	183.3	183.9	184.5	185.2	185.8
300 186.4 187.0 187.7	188.3	188.9	189.5	190.1	190.8	191.4	192.0
310 192.6 193.2 193.9 198.8 199.5 200.1	194.5	195.1 201.3	195.7	196.4 202.6	197.0	197.6 203.8	198.2
330 205.1 205.7 206.3	206.9	207.5	208.2	203.8	209.4	210.0	210.6
340 211.3 211.9 212.5	213.1	213.8	214.4	215.0	215.6	216.2	216.9
350 217.5 218.1 218.7	219.3	220.0	220.6	221.2	221.8	222.5	223. I
360 223.7 224.3 224.9 370 229.9 230.5 231.1	225.6	226.2	226.8 233.0	227.4 233.6	228.0 234.3	228.7 234.9	229.3 235.5
380 236.1 236.7 237.4	238.0	238.6	239.2	239.8	240.5	241.1	241.7
390 242.3 243.0 243.6	244.2	244.8	245.4	246.1	246.7	247.3	247.9
400 248.5 249.2 249.8	250.4	251.0	251.7	252.3	252.9	253.5	254.1
410 254.8 255.4 256.0 420 261.0 261.6 262.2	256.6 262.8	257.2 263.5	257.9 264.1	258.5 264.7	259. I 265. 3	259.7 265.9	260.4 266.6
430 267.2 267.8 268.4	269.1	269.7	270.3	270.9	271.5	272.2	272.8
440 273.4 274.0 274.6	275.3	275.9	276.5	277.1	277.8	278.4	279.0
	281.5		282.7		284.0		
460 285.8 286.5 287.1 470 292.0 292.7 293.3	287.7	288.3	288.9 295.2	·289.6 295.8	290.2 296.4	290.8 297.0	291.4
480 298.3 298.9 299.5	300.1	300.7	301.4	302.0	302.6	303.2	303.8
490 304.5 305.1 305.7	306.3	307.0	307.6	308.2	308.8	309.4	310.1
500 310.7 311.3 311.9 510 316.9 317.5 318.1	312.5 318.8	313.2 319.4	313.8	314.4 320.6	315.0	315.7	316.3
520 323.1 323.7 324.4	325.0	325.6	326.2	326.8	327.5	328.1	328.7
530 329.3 329.9 330.6	331.2	331.8	332.4	333. I	333.7	334.3	334.9
540 335.5 336.2 336.8	337-4	338.0	338.6	339-3	339.9	340.5	341.1

KILOMETERS INTO MILES.

Kilo- meters.	0	1	2	3	4	5	6	7	8	9
550 560 570 580 590	Miles. 341.8 348.0 354.2 360.4 366.6	Miles. 342.4 348.6 354.8 361.0 367.2	Miles. 343.0 349.2 355.4 361.6 367.9	Miles. 343.6 349.8 356.0 362.3 368.5	Miles. 344.2 350.5 356.7 362.9 369.1	Miles. 344.9 351.1 357.3 363.5 369.7	Miles. 345.5 351.7 357.9 364.1 370.3	Miles. 346.1 352.3 358.5 364.7 371.0	Mile ·. 346.7 352.9 359.2 365.4 371.6	Miles. 347·3 353·6 359·8 366.0 372.2
600 610 620 630 640	372.8 379.0 385.2 391.5 397.7	373·4 379·7 385·9 392·1 398·3	374.1 380.3 386.5 392.7 398.9	374·7 380.9 387.1 393·3 399·5	375·3 381.5 387·7 393·9 400.2	375.9 382.1 388.4 394.6 400.8	376.6 382.8 389.0 395.2 401.4	377.2 383.4 389.6 395.8 402.0	377.8 384.0 390.2 396.4 402.6	378.4 384.6 390.8 397.1 403.3
650 660 670 680 690	403.9 410.1 416.3 422.5 428.7	404.5 410.7 416.9 423.2 429.4	405.1 411.3 417.6 423.8 430.0	405.8 412.0 418.2 424.4 430.6	406.4 412.6 418.8 425.0 431.2	407.0 413.2 419.4 425.6 431.9	407.6 413.8 420.0 426.3 432.5	408.2 414.5 420.7 426.9 433.1	408.9 415.1 421.3 427.5 433.7	409.5 415.7 421.9 428.1 434.3
710 720 730 740	435.0 441.2 447.4 453.6 459.8 466.0	435.6 441.8 448.0 454.2 460.4	436.2 442.4 448.6 454.8 461.1	436.8 443.0 449.3 455.5 461.7	437.4 443.7 449.9 456.1 462.3	438.1 444.3 450.5 456.7 462.9	438.7 444.9 451.1 457.3 463.5	439·3 445·5 451·7 457·9 464·2	439.9 446.1 452.4 458.6 464.8	440.6 446.8 453.0 459.2 465.4
760 770 780 790	472.2 478.5 484.7 490.9	466.6 472.9 479.1 485.3 491.5	467.3 473.5 479.7 485.9 492.1	467.9 474.1 480.3 486.5 492.7	468.5 474.7 480.9 487.2 493.4	469. 1 475. 3 481. 6 487. 8 494. 0	469.8 476.0 482.2 488.4 494.6	470.4 476.6 482.8 489.0 495.2	471.0 477.2 483.4 489.6 495.9	471.6 477.8 484.0 490.3 496.5
810 820 830 840	497.1 503.3 509.5 515.7 522.0	497.7 503.9 510.1 516.4 522.6	498.3 504.6 510.8 517.0 523.2	499.0 505.2 511.4 517.6 523.8	499.6 505.8 512.0 518.2 524.4	500.2 506.4 512.6 518.8 525.1	500.8 507.0 513.3 519.5 525.7	501.4 507.7 513.9 520.1 526.3	502.1 508.3 514.5 520.7 526.9	502.7 508.9 515.1 521.3 527.5
850 860 870 880 890	528.2 534.4 540.6 546.8 553.0	528.8 535.0 541.2 547.4 553.6	529.4 535.6 541.8 548.0 554.3	530.0 536.2 542.5 548.7 554.9	530.6 536.9 543.1 549.3 555.5	531.3 537.5 543.7 549.9 556.1	531.9 538.1 544.3 550.5 556.7	532.5 538.7 544.9 551.2 557.4	533.1 539.3 545.6 551.8 558.0	533.8 540.0 546.2 552.4 558.6
910 920 930 940 950	559.2 565.4 571.7 577.9 584.1	559.9 566.1 572.3 578.5 584.7	560.5 566.7 572.9 579.1 585.3	561.1 567.3 573.5 579.7 586.0	561.7 567.9 574.1 580.4 586.6	562.3 568.6 574.8 581.0 587.2	563.0 569.2 575.4 581.6 587.8	563.6 569.8 576.0 582.2 588.4	564.2 570.4 576.6 582.8 589.1	564.8 571.0 577.3 583.5 589.7
960 970 980 990	590.3 596.5 602.7 608.9 615.2	590.9 597.1 603.4 609.6 615.8	591.5 597.8 604.0 610.2 616.4	592.2 598.4 604.6 610.8 617.0	592.8 599.0 605.2 611.4 617.6	593.4 599.6 605.8 612.0 618.3 624.5	594.0 600.2 606.5 612.7 618.9	594.7 600.9 607.1 613.3 619.5 625.7	595.3 601.5 607.7 613.9 620.1	595.9 602.1 608.3 614.5 620.7
	km. 1000 2000 3000 4000 5000	Miles. 621.4 1242.7 1864.1	km. 4 600 7 700 8 800 5 900	Mile 3728 00 4349 00 4971 5592	es. k 3.2 II 9.6 I2 1.0 I3 2.3 I4	m. M 000 68 000 74 000 86	(iles. 335.1 156.4 277.8	km. 16000 17000 18000 19000 20000	Miles. 9941.9 10563.3 11184.7 11806.0 12427.4	02/10

INTERCONVERSION OF NAUTICAL AND STATUTE MILES.

1 nautical mile* = 6080.20 feet.

Nautical Miles.	Statute Miles.	Statute Miles.	Nautical Miles.		
1 2 3 4 5 6 7 8 9	1.1516 2.3031 3.4547 4.6062 5.7578 6.9093 8.0609 9.2124 10.3640	2 3 4 5 6 7 8 9	0.8684 1.7368 2.6052 3.4736 4.3420 5.2104 6.0787 6.9471 7.8155		

^{*} As defined by the United States Coast Survey.

TABLE 18.

CONTINENTAL MEASURES OF LENGTH WITH THEIR METRIC AND ENGLISH EQUIVALENTS.

The asterisk (*) indicates that the measure is obsolete or seldom used.

Measure,	Metric Equivalent.	English Equivalent.		
El (Netherlands) Fathom, Swedish = 6 feet Foot, Austrian* old French* Russian Rheinlandisch or Rhenish (Prussia*, Denmark, Norway*). Swedish* Spanish* = ½ vara *Klafter, Wiener (Vienna) *Line, old French = ½ foot Mile, Austrian post* = 24000 feet German sea Swedish = 36000 feet Norwegian = 36000 feet Norwegian = 36000 feet Netherlands (mijl) Prussian (law of 1868) Danish Palm, Netherlands *Rode, Danish *Ruthe, Prussian, Norwegian Sagene (Russian) *Toise, old French = 6 feet *Vara, Spanish Mexican Werst, or versta (Russian) = 500 sashjene	I meter. 1.7814 " 0.31608 " 0.32484 " 0.30480 " 0.2969 " 0.2786 " 1.89648 " 0.22558 cm. 7.58594 km. 1.852 " 10.69 " 11.2986 " 1 " 7.500 " 7.5324 " 0.1 meter. 3.7662 " 2.1336 " 1.9490 " 0.8359 " 0.8380 " 1.0668 km.	3.2808 feet. 5.8445 " 1.0370 " 1.0657 " 1 " 1.0297 " 0.9741 " 0.9140 " 6.2221 " 0.0888 inch. 4.714 statute miles. 1.1508 " " 6.642 " " 7.02 " " 0.6214 " " 4.660 " " 4.6804 " " 0.3281 feet. 12.356 " 12.356 " 7 " 6.3943 " 2.7424 " 2.7493 " 3.500 "		

CONVERSION OF MEASURES OF TIME AND ANGLE.

Arc into time	٠			TABLE 19
Time into arc				TABLE 20
Days into decimals of a year and angle				TABLE 21
Hours, minutes and seconds into decimals of a day				TABLE 22
Decimals of a day into hours, minutes and seconds				TABLE 23
Minutes and seconds into decimals of an hour .				TABLE 24
Local mean time at apparent noon				TABLE 25
Sidereal time into mean solar time		•	٠	TABLE 26
Mean solar time into sidereal time	0	•		TABLE 27

ARC INTO TIME.

		,													
0	h. m.	0	h. m.	0	h. m.	0	h m.	0	h. m.	٥	h. m.		m. s.	//	s.
0	0 0	60	4 0	120	8 0	180	12 0	240	16 o	300	20 0	0	0 0	0	0.000
I	0 4	61	4 4	121	8 4	181	12 4	241	16 4	301	20 4	I	0 4	I	0.067
3	0 8	62	4 8 4 12	122 123	8 8	182 183	12 8 12 12	242	16 8	302 303	20 S 20 I2	3	0 S 0 I2	3	0.133
4	0 16	64	4 16	124	8 16	184	12 16	244	16 16	304	20 16	4	0 16	4	0.267
5	0 20	65	4 20	125	8 20	185	12 20	245	16 20	305	20 20	5	0 20	5	0.333
6	0 24	66	4 24 4 28	126	8 24 8 28	186 187	12 24	246	16 24	306	20 24 20 28	6	0 24	6	0.400
7 8	0 32	67 68	4 28	127 128	8 32	188	12 32	247 248	16 28 16 32	307 308	20 32	7 8	0 32	7 8	0.467
9	0 36	69	4 36	129	8 36	189	12 36	249	16 36	309	20 36	9	0 36	9	0.600
10	0 40	70	4 40	130	8 40	190	12 40	250	16 40	310	20 40	10	0 40	10	0.667
11	0 44	71	4 44	131	8 44	191	12 44	251	16 44	311	20 44	II	0 44	11	0.733
12	0 48	72 73	4 48	132 133	8 48 8 52	192 193	12 48 12 52	252 253	16 48 16 52	312 313	20 48	12	0 48	12	o.800 o.867
14	0 56	74	4 56	134	8 56	194	12 56	2 54	16 56	314	20 56	14	0 56	14	0.933
15	I O	75	5 0	135	9 0	195	13 0	255	17 0	315	21 0	15	I O	15	1.000
16	I 4 I 8	76	5 4 5 8	136	9 4	196	13 4	256	17 4 17 8	316	2I 4 2I 8	16	I 4	16	1.067
18	I 12	77 78	5 8	137 138	9 8	197	13 8	257 258	17 S	317 318	21 12	18	I 12	17 18	1.133
19	1 16	79	5 16	139	9 16	199	13 16	259	17 16	319	21 16	19	1 16	19	1.267
20	I 20	80	5 20	140	9 20	200	13 20	260	17 20	320	21 20	20	I 20	20	1.333
21	I 24	81	5 24	141	9 24	201	13 24	261	17 24	321	21 24	21	I 24	21	1.400
22	I 28	82 83	5 28	142 143	9 28	202	13 28 13 32	262 263	17 28	322 323	21 28	22	I 28	22 23	1.467 1.533
24	1 36	84	5 36	144	9 36	204	13 36	264	17 36	324	21 36	24	1 36	24	1.600
25	I 40	85	5 40	145	9 40	205	13 40	265	17 40	325	21 40	25	1 40	25	1.667
26	I 44 I 48	86 87	5 44 5 48	146	9 44	206 207	13 44	266	17 44	326	21 44	26	I 44	26	1.733
27 28	1 52	88	5 48	147 148	9 48	208	13 48 13 52	267 268	17 48	327 328	21 48 21 52	27 28	1 48	27 28	1.800
29	1 56	89	5 56	149	9 56	209	13 56	269	17 56	329	21 56	29	1 56	29	1.933
30	2 0	90	6 0	150	10 0	210	14 0	270	18 o	330	22 0	30	2 0	30	2.000
31	2 4	91	6 4	151	10 4	211	14 4	271	18 4	331	22 4	31	2 4	31	2.067
32	2 8	92	6 8	152	10 8	212	14 S 14 I2	272	18 8	332	22 8	32	2 8	32	2.133
33 34	2 16	93 94	6 16	153 154	10 12	213 214	14 16	273 274	18 12	333	22 12	33	2 12 2 16	33 34	2.200
35	2 20	95	6 20	155	10 20	215	14 20	275	18 20	335	22 20	35	2 20	35	2.333
36	2 24 2 28	96	6 24	156	10 24	216	14 24	276	18 24	336	22 24	36	2 24	36	2.400
37 38	2 32	97 98	6 28	157 158	10 28	217 218	14 28 14 32	277 278	18 28 18 32	337 338	22 28	· 37 38	2 28	37 38	2.467
39	2 36	99	6 36	159	10 36	219	14 36	279	18 36	339	22 36	39	2 36	39	2.600
40	2 40	100	6 40	160	10 40	220	14 40	280	18 40	340	22 40	40	2 40	40	2.667
41	2 44	IOI	6 44	161	10 44	221	14 44	281	18 44	341	22 44	41	2 44	41	2.733
42	2 48 2 52	102	6 48	162 163	10 48	222	14 48 14 52	282 283	18 48 18 52	342	22 48	42	2 48	42	2.867
43	2 56	104	6 56	164	10 52	224	14 52	284	18 56	343	22 52 22 56	43	2 56	43	2.933
45	3 0	105	7 0	165	11 0	225	15 0	285	19 0	345	23 0	45	3 0	45	3.000
46	3 4 8	106	7 4	166	II 4	226	15 4 15 8	286	19 4	346	23 4	46	3 4	46	3.067
47 48	3 8	107		167 168	11 8 11 12	227 228	15 S 15 12	287 288	19 8	347 348	23 8 23 I2	47 48	3 8	47 48	3.133
49	3 16	109	7 16	169	11 16	229	15 16	289	19 16	349	23 16	49	3 16	49	3.267
50	3 20	110	7 20	170	II 20	230	15 20	290		350	23 20	50	3 20	50	3.333
51	3 24	111	7 24	171	II 24	231	15 24	291	19 24	351	23 24	51	3 24	51	3.400
52	3 28 3 32	112	7 28 7 32	172	11 28 11 32	232	15 28	292	19 28	352		52	3 28	52	3.467
	3 36	114		173 174	11 32	233 234	15 32 15 36	293 294	19 32 19 36	353 354		53 54	3 32 36	53 54	3.533 3.600
54 55	3 40	115	7 40	175	II 40	235	15 40	295	19 40	355	23 40	55	3 40	55	3.667
56	3 44	116	1 1 1	176	11 44	236	15 44	296	19 44	356	23 44	56	3 44	56	3.733
57 58	3 48	117		177 178	11 48 11 52	237 238	15 48 15 52	297 298	19 48	357 358	23 48	57 58	3 48	57 58	3.867
59	3 56	119	7 56	179	11 56	239	15 56	299	19 56	355		59	3 56	59	3.933
60	4 0	120	8 0	180	I2 O	240	16 0	300	20 0	360	24 0	60	4 0	60	4.000
													1		

TIME INTO ARC.

						ı	Hours	ii	nto A	rc.					
Time.	Arc.	Ti	me.	Arc.		Time.	Arc.		Time.	A	rc.	Time.	Arc.	Time,	Arc.
hrs.	0	h	rs.	٥		hrs.	0		hrs.		0	hts.	0	hrs.	0
1	15		5	75		9	135 150		13 14		95	17 18	255	21 22	315
2 3 4	30 45 60		6 7 8	90 105 120		11	165	;	15 16	2	10 25 40	19 20	270 285 300	23 24	330 345 360
	Minu	tes	of	Time	int	to A	rc.		Seconds of Time into Arc.						
m.	0 /	n	n.	0 /		m.	s.	/	//	s	, ,,	S.	/ //		
1 0 15 21 5 15 41 10 15 1 0 15 21 5 15 41 10 15 2 0 30 22 5 30 42 10 30 2 0 30 22 5 30 42 10 30 2 0 45 23 5 45 43 10 45															
5	I 15		5	6 I 6 3	~	45 46		15	5	I I	15 30	25 26	6 15		11 15 11 30
7 8	I 45	2	7 8	6 4		47 48		15	7 8	I 2	45	27 28	6 45		11 45 12 0
9	2 15	١.	9	·	5	49		15	9	2	15	30	7 15		12 15
10 11 12	2 30 2 45 3 0	3	0 1	7 4	5	50 51 52	12 4	30 45 0	10 11 12	2 2 3	30 45 0	31 32	7 30 7 45 8 6	5 51	12 30 12 45 13 0
13	3 I5 3 30	5 3	32 33 34	8 1	5	52 53 54		15	13 14	3 3	15 30	33 34	8 15	5 53	13 15 13 30
15 16	3 45	/	3 5		5	55 56	13 4	45 O	15 16	3 4	45 o	35 36	8 4		13 45
17 18	4 1	5 3	37 38	9 1	5 0	57 58	14	15 30	17 18	4	15	37	9 1	5 57	14 15 14 30
19	4 4.	5	39	9 4	15	59	14	45	19 4 45 39 9 45 59			14 45			
20	5	0 4	10	10	0	60	15	0	20	5	0	40	10	0 60	15 0
			Н	undre	dth	s of	a S	Sec	ond	of -	Γim	e into	Arc.		
Hundre of a S ond of 1	Sec-	.00		01	.0	2	.03		04	.0	5	.06	.07	.08	.09
s. 0.0		ó.oo		0.15	0,3		ó.45		,, 60	0.7		ó.go	1.05	1.20	
.I .2	0	1.50 3.00		3.15	3.3	80 30	1.95 3.45		2.10 3.60	2.1 3.1	·	2.40 3.90	2.55 4.05	4.20	4.35
		4.50 6.00	4	1.65 5.15		80 30	4.95 6.45	1	5.10 5.60	5. 6.	25	5.40 6.90	5.55 7.05	5.70 7.20	
0.5		7.50		7.65		So	7.95		8.10	8.:		8.40	8.55	8.70	
.7	70 1	9.00	I			80	9.45 10.95	I	9.60	9.	25	9.90	10.05	11.70	11.85
	.70 10.50 10.65 10.80 10.90 .80 12.00 12.15 12.30 12.4 .90 13.50 13.65 13.80 13.9								2.60 4.10	12.		12.90 14.40	13.05		
1			1			1		J			1		1		

Day of	Decimal of	Amalo	Day of	Month.	Day	Decimal of	Angle.	Day of	Month.
Year.	a Year.	Angle.	Common Year,	Bissextile Year.	Year.	a Year.	Angie.	Common Year.	Bissextile Year.
1 2 3 4	0.00000 .00274 .00548 .00821	o° o′ o 59 i 58 2 57	Jan. 1 2 3 4	Jan. 1 2 3 4	51 52 53 54	0.13689 .13963 .14237 .14511	49° 17′ 50 16 51 15 52 14	Feb. 20 21 22 23	Feb. 20 21 22 23
5 6 7 8 9	0.01095 .01369 .01643 .01916	3 57 4 56 5 55 6 54 7 53	5 6 7 8 9	5 6 7 8	55 56 57 58 59	0.14784 .15058 .15332 .15606 .15880	53 13 54 13 55 12 56 11 57 10	24 25 26 27 28	24 25 26 27 28
10 11 12 13 14	0.02464 .02738 .03011 .03285	8 52 9 51 10 51 11 50 12 49	10 11 12 13 14	10 11 12 13 14	60 61 62 63 64	0.16153 .16427 .16701 .16975 .17248	58 9 59 8 60 7 61 7 62 6	Mar. 1 2 3 4 5	Mar. 1 2 3 4
15 16 17 18 19	0.03833 .04107 .04381 .04654 .04928	13 48 14 47 15 46 16 45 17 44	15 16 17 18	15 16 17 18	65 66 67 68 69	0.17522 .17796 .18070 .18344 .18617	63 5 64 4 65 3 66 2 67 I	6 7 8 9	5 6 7 8
20 21 22 23 24	0.05202 .05476 .05749 .06023 .06297	18 44 19 43 20 42 21 41 22 40	20 21 22 23 24	20 21 22 23 24	70 71 72 73 74	0.18891 .19165 .19439 .19713 .19986	68 o 69 o 69 59 70 58 71 57	11 12 13 14	10 11 12 13
25 26 27 28 29	0.06571 .06845 .07118 .07392 .07666	23 39 24 38 25 38 26 37 27 36	25 26 27 28 29	25 26 27 28 29	75 76 77 78 79	0.20260 .20534 .20808 .21081 .21355	72 56 73 55 74 54 75 54 76 53	16 17 18 19 20	15 16 17 18
30 31 32 33 34	0.07940 .08214 .08487 .08761 .09035	28 35 29 34 30 33 31 32 32 32	30 31 Feb. 1 2 3	30 31 Feb. 1 2 3	80 81 82 83 84	0.21629 .21903 .22177 .22450 .22724	77 52 78 51 79 50 80 49 81 48	21 22 23 24 25	20 21 22 23 24
35 36 37 38 39	0.09309 .09582 .09856 .10130	33 31 34 30 35 29 36 28 37 27	4 5 6 7 8	4 5 6 7 8	85 86 87 88 89	0.22998 .23272 .23546 .23819 .24093	\$2 48 \$3 47 \$4 46 \$5 45 \$6 44	26 27 28 29 30	25 26 27 28 29
40 41 42 43 44	0.10678 .10951 .11225 .11499	38 26 39 26 40 25 41 24 42 23	9 10 11 12 13	9 10 11 12 13	90 91 92 93 94	0.24367 :24641 .24914 .25188 .25462	87 43 88 42 89 42 90 41 91 40	Apr. 31 2 3 4	30 31 Apr. 1 2 3
45 46 47 48 49	0.12047 .12320 .12594 .12868 .13142	43 22 44 21 45 20 46 19 47 19	14 15 16 17 18	14 15 16 17 18	95 96 97 98 99	0.25736 .26010 .26283 .26557 .26831	92 39 93 38 94 37 95 36 96 35	5 6 7 8 9	4 5 6 7 8
50	0.13415	48 18	19	19	100	0.27105	97 35	10	9

Day	Decimal		Day of	Month.	Day	Decimal		Day of	Month.
of Year.	ot a Year.	Angle.	Common Year.	Bissextile Year.	of Year.	of a Year.	Angle.	Common Year.	Bissextile Year.
101 102 103 104	0.27379 .27652 .27926 .28200	98°34′ 99 33 100 32 101 31	Apr. 11 12 13 14	Apr. 10 11 12 13	151 152 153 154	0.41068 .41342 .41615 .41889	147° 51′ 148 50 149 49 150 48	May 31 June 1 2 3	May 30 June 1 2
105 106 107 108 109	0.28474 .28747 .29021 .29295 .29569	102 30 103 29 104 29 105 28 106 27	15 16 17 18	14 15 16 17 18	155 156 157 158 159	0.42163 .42437 .42710 .42984 .43258	151 47 152 46 153 45 154 45 155 44	4 5 6 7 8	3 4 5 6 7
110 111 112 113 114	0.29843 .30116 .30390 .30664 .30938	107 26 108 25 109 24 110 23 111 23	20 21 22 23 24	19 20 21 22 23	160 161 162 163 164	0.43532 .43806 .44079 .44353 .44627	156 43 157 42 158 41 159 40 160 39	9 10 11 12 13	8 9 10 11 12
115 116 117 118 119	0.31211 .31485 .31759 .32033 .32307	112 22 113 21 114 20 115 19 116 18	25 26 27 28 29	24 25 26 27 28	165 166 167 168 169	0.44901 -45175 -45448 -45722 -45996	161 39 162 38 163 37 164 36 165 35	14 15 16 17 18	13 14 15 16
120 121 122 123 124	0.32580 .32854 .33128 .33402 .33676	117 17 118 17 119 16 120 15 121 14	May 1 2 3 4	29 30 May 1 2 3	170 171 172 173 174	0.46270 .46543 .46817 .47091 .47365	166 34 167 33 168 33 169 32 170 31	19 20 21 22 23	18 19 20 21 22
125 126 127 128 129	0.33949 .34223 .34497 .34771 .35044	122 13 123 12 124 11 125 10 126 10	5 6 7 8 9	4 5 6 7 8	175 176 177 178 179	0.47639 .47912 .48186 .48460 .48734	171 30 172 29 173 28 174 27 175 26	24 25 26 27 28	23 24 25 26 27
130 131 132 133 134	0.35318 ·35592 ·35866 ·36140 ·36413	127 9 128 8 129 7 130 6 131 5	10 11 12 13	9 10 11 12 13	180 181 182 183 184	0.49008 .49281 .49555 .49829 .50103	176 26 177 25 178 24 179 23 180 22	29 30 July 1 2 3	28 29 30 July 1 2
135 136 137 138 139	0.36687 .36961 .37235 .37509 .37782	132 4 133 4 134 3 135 2 136 1	15 16 17 18	14 15 16 17 18	185 186 187 188 189	0.50376 .50650 .50924 .51198	181 21 182 20 183 20 184 19 185 18	4 5 6 7 8	3 4 5 6 7
140 141 142 143 144	0.38056 .38330 .38604 .38877 .39151	137 0 137 59 138 58 139 58 140 57	20 21 22 23 24	19 20 21 22 23	190 191 192 193 194	0.51745 .52019 .52293 .52567 .52841	186 17 187 16 188 15 189 14 190 14	9 10 11 12	8 9 10 11 12
145 146 147 148 149	0.39425 .39699 .39973 .40246 .40520	141 56 142 55 143 54 144 53 145 52	25 26 27 28 29	25 26 27	195 196 197 198 199	0.53114 .53388 .53662 .53936 .54209	191 13 192 12 193 11 194 10 195 9	14 15 16 17 18	14 15 16 17
150	0.40794	146 51	30	29	200	D.54483	196 8	19	18

Day	Decimal		Day of	Month.	Day	Decimal		Day of	Month.
of Year.	of a Year.	Angle.	Common Year.	Bissextile Year.	of Year.	of a Year.	Angle.	Common Year.	Bissextile Year.
201 202 203 204	0.54757 .55031 .55305 .55578	197° 8′ 198 7 199 6 200 5	July 20 21 22 23	July 19 20 21 22	251 252 253 254	0.68446 .68720 .68994 .69268	246°24′ 247 24 248 23 249 22	Sept. 8 9 10	Sept. 7 8 9 10
205 206 207 208 209	0.55852 .56126 .56400 .56674 .56947	20I 4 202 3 203 2 204 I 205 I	24 25 26 27 28	23 24 25 26 27	255 256 257 258 259	0.69541 .69815 .70089 .70363 .70637	250 21 251 20 252 19 253 18 254 17	12 13 14 15 16	11 12 13 14 15
210 211 212 213 214	0.57221 ·57495 ·57769 ·58042 ·58316	206 0 206 59 207 58 208 57 209 56	29 30 31 Aug. 1 2	28 29 30 31 Aug. 1	260 261 262 263 264	0.70910 .71184 .71458 .71732 .72005	255 17 256 16 257 15 258 14 259 13	17 18 19 20 21	16 17 18 19 20
215 216 217 218 219	0.58590 .58864 .59138 .59411 .59685	210 55 211 55 212 54 213 53 214 52	3 4 5 6	2 3 4 5 6	265 266 267 268 269	0.72279 •72553 •72827 •73101 •73374	260 12 261 11 262 11 263 10 264 9	22 23 24 25 26	21 22 23 24 25
220 221 222 223 224	0.59959 .60233 .60507 .60780 .61054	215 51 216 50 217 49 218 49 219 48	8 9 10 11 12	7 8 9 10	270 271 272 273 274	0.73648 .73922 .74196 .74470 .74743	265 8 266 7 267 6 268 5 269 5	27 28 29 30 <i>Oct.</i> 1	26 27 28 29 30
225 226 227 228 229	0.61328 .61602 .61875 .62149 .62423	220 47 221 46 222 45 223 44 224 43	13 14 15 16	12 13 14 15	275 276 277 278 279	0.75017 .75291 .75565 .75838 .76112	270 4 271 3 272 2 273 I 274 0	2 3 4 5 6	Oct. 1 2 3 4 5
230 231 232 233 234	0.62697 .62971 .63244 .63518 .63792	225 43 226 42 227 41 228 40 229 39	18 19 20 21 22	17 18 19 20 21	280 281 282 283 284	0.76386 .76660 .76934 .77207 .77481	274 59 275 59 276 58 277 57 278 56	7 8 9 10	6 7 8 9
235 236 237 238 239	0.64066 .64339 .64613 .64887	230 38 231 37 232 36 233 36 234 35	23 24 25 26 27	22 23 24 25 26	285 286 287 288 289	0.77755 .78029 .78303 .78576 .78850	279 55 280 54 281 53 282 52 283 52	12 13 14 15	11 12 13 14
240 241 242 243 244	0.65435 .65708 .65982 .66256 .66530	235 34 236 33 237 32 238 31 239 30	28 29 30 31 Sept. 1	27 28 29 30 31	290 291 292 293 294	0.79124 .79398 .79671 .79945 .80219	284 51 285 50 286 49 287 48 288 47	17 18 19 20 21	16 17 18 19 20
245 246 247 248 249	0.66804 .67077 .67351 .67625 .67899	240 30 241 29 242 28 243 27 244 26	2 3 4 5 6	Sept. I 2 3 4 5	295 296 297 298 299	0.80493 .80767 .81040 .81314 .81588	289 46 290 46 291 45 292 44 293 43	22 23 24 25 26	21 22 2 3 24 25
250	0.68172	245 25	7	6	300	0.81862	294 42	27	26

Day	Decimal		Day of	Month.	Day	Decimal			Day of	Month.
of Year.	of a Year.	Angle.	Common Year	Bissextile Year.	of Year.	of a Year.	Angle		ommon Year.	Bissextile Year.
301 302 303 304	0.82136 .82409 .82683 .82957	295°41′ 296 40 297 40 298 39	Oct. 28 29 30 31	Oct. 27 28 29 30	351 352 353 354	0.95825 .96099 .96372 .96646	344° 5 345 5 346 5 347 5	57	Dec. 17 18 19 20	Dec. 16
305 306 307 308 309	0.83231 .83504 .83778 .84052 .84326	299 38 300 37 301 36 302 35 303 34	Nov. 1 2 3 4 5	Nov. 1 2 3 4	355 356 357 358 359	0.96920 .97194 .97467 .97741 .98015	348 5 349 5 350 5 351 5 352 5	54 53 52	21 22 23 24 25	20 21 22 23 24
310 311 312 313 314	0.84600 .84873 .85147 .85421 .85695	304 34 305 33 306 32 307 31 308 30	6 7 8 9 10	5 6 7 8 9	360 361 362 363 364	0.98289 .98563 .98836 .99110	353 5 354 5 355 4 356 2 357 4	50 19 18	26 27 28 29 30	25 26 27 28 29
315 316 317 318	0.85969 .86242 .86516 .86790	309 29 310 28 311 27 312 27	11 12 13 14	10 11 12 13	365 366	0.99658 •99932	358 ² 359 ²	15	31	30
319 320 321 322 323	.87064 0.87337 .87611 .87885 .88159	313 26 314 25 315 24 316 23 317 22	15 16 17 18	14 15 16 17 18	Hrs.	Dec. of Year.	Angle.	Min.	Dec. of Year.	
324 325 326 327 328 329	.88433 o.88706 .8898o .89254 .89528 .89802	318 21 319 21 320 20 321 19 322 18 323 17	20 21 22 23 24 25	20 21 22 23 24	1 2 3 4 5	0.00011 23 34 46	2.5 4.9 7.4 9.9	1 2 3 4 5	1	.08
330 331 332 333	0.90075 .90349 .90623 .90897	324 16 325 15 326 15 327 14 328 13	26 27 28 29 30	25 26 27 28 29	6 7 8 9	68 80 91 103	14.8 17.2 19.7 22.2	6 7 8 9	2	1 .25 1 .29 2 .33 2 .37 2 0.41
334 335 336 337 338	0.91444 .91718 .91992 .92266	329 12 330 11 331 10 332 9	Dec. 1 2 3 4	Dec. 1 2 3	11 12 13 14	126 137 148 160	27.1 29.6 32.0 34.5	20 30 40 50	2 6 8	1 .82 5 1.23 6 1.64 2.05
339 340 341 342 343	.92539 0.92813 .93087 .93361 .93634	333 9 334 8 335 7 336 6 337 5	5 6 7 8 9	5 6 7 8	15 16 17 18 19	0.00171 183 194 205 217	37.0 39.4 41.9 44.4 46.8	60	0.0001	2.46
344 345 346 347 348	.93908 0.94182 .94456 .94730 .95003	338 4 339 3 340 2 341 2 342 1	10 11 12 13 14	9 10 11 12 13	20 21 22 23 24	0.00228 240 251 262 274	49·3 51·7 54·2 56·7 59·1			
349 3 50	.95277 0.95551	343 ° 343 59	15	14						

Table 22.
HOURS, MINUTES AND SECONDS INTO DECIMALS OF A DAY.

Hours.	Day.	Min.	Day.	Min.	Day.	Sec.	Day.	Sec.	Day.
	0.041 667	-	0,000 694	31	0.021 528		0,000 012	31	0.000 359
2	.083 333	2	.001 389	32	,022 222	2	.000 023	32	.000 370
3	.125 000	3	.002 083	33	.022 917	3	.000 035	33	.000 382
4	.166 667	4	.002 778	34	.023 611	4	.000 046	34	.000 394
5	0.208 333	5	0.003 472	35	0.024 305	5	0.000 058	35	0.000 405
6	.250 000	6	.004 167	36	.025 000	6	.000 069	36	.000 417
7	.291 667	7	.004 861	37	.025 694	7	.000 081	37	.000 428
8	-333 333	8	.005 556	38	.026 389	8	.000 093	38	.000 440
9	.375 000	9	.006 250	39	.027 083	9	.000 104	39	.000 451
10	0.416 667	10	0.006 944	40	0.027 778	10	0.000 116	40	0.000 463
11	.458 333	11	.007 639	41	.028 472	II	.000 127	41	.000 475
12	.500 000	12	.008 333	42	.029 167	12	.000 139	42	.000 486
13	.541 667	13	.009 028	43	.029 861	13	.000 150	43	.000 498
1.4	-5 ⁸ 3 333	14	.009 722	44	.030 556	14	,000 162	44	.000 509
15	0.625 000	15	0.010 417	45	0.031 250	15	0.000 174	45	0.000 521
16	.666 667	16	III IIO.	46	.031 944	16	.000 185	46	.000 532
17	.708 333	17	.011 806	47	.032 639	17	.000 197	47	.000 544
18	.750 000	18	.012 500	48	.033 333	18	.000 208	48	.000 556
19	.791 667	19	.013 194	49	.034 028	19	,000 220	49	.000 567
20	0.833 333	20	0.013 889	50	0.034 722	20	0.000 231	50	0.000 579
21	.875 000	21	.014 583	51	.035 417	21	.000 243	51	.000 590
22	.916 667	22	.015 278	52	.036 111	22	.000 255	52	.000 602
23	.958 333	23	.015 972	53	.036 806	23	.000 266	53	.000 613
24	1.000 000	24	.016 667	54	.037 500	2.1	.000 278	54	.000 625
		25	0.017 361	55	0.038 194	25	0.000 289	55	0.000 637
		26	.018 056	56	.038 889	26	.000 301	56	.000 648
		27	.018 750	57	.039 583	27	.000 313	57	.000 660
		28	.019 444	58	.040 278	28	.000 324	58	.000 671
		29	.020 139	59	.040 972	29	.000 336	59	.000 683
		30	0.020 833	60	0.041 667	30	0.000 347	60	.000 694

TABLE 23.

DECIMALS OF A DAY INTO HOURS, MINUTES AND SECONDS.

Hundre	dths of a	Day.	Ten Thousa	ndths of a Day.	Millionths of a Day.				
d.	h. m	l. s.	d,	min. sec.	d.	sec.			
0.01	I	4 24	0.0001	8.64	0.000001	0.09			
.02	28		2	17.28	2	0.17			
.03	4,	,	3	25.92	3	0.26			
.04	5		4	34.56	4	0.35			
0.05	I I	2 0	0.0005	43.20	0.000005	0.43			
.06	I 2	6 24	6	51.84	6	0.52			
.07	I 40	0 48	7 8	I 0.48	7 8	0,60			
.08	I 5.	5 12	8	I 9.12	Š	0.69			
.09	2	9 36	9	1 17.76	9	0.78			
0.10	2 2.	4 0	0.0010	1 26.40	0.000010	0.86			
.20	4 4	8 0	20	2 52.80	20	1.73			
.30	7 I:	2 0	30	4 19.20	30	2.59			
.40	9 3	6 о	40	5 45.60	40	3.46			
0.50	12	0 0	0.0050	7 12.00	0.000050	4.32			
.60	1.4 2	4 0	60	8 38.40	60	5.18			
.70	16 4	8 0	70	10 4.80	70	6.05			
.80	19 1		So	11 31.20	So	6.91			
.90	21 3	6 0	90	12 57.60	90	7.78			

TABLE 24.

MINUTES AND SECONDS INTO DECIMALS OF AN HOUR.

Min.	Decimals of an hour.	Min.	Decimals of an hour.	Sec.	Decimals of an hour.	Sec.	Decimals of an hour.
1 2 3 4	0.016 667 .033 333 .050 000 .066 667	31 32 33 34	0.516 667 ·533 333 ·550 000 ·566 667	2 3 4	0.000 278 .000 556 .000 833 .001 111	31 32 33 34	0.008 611 .008 889 .009 167 .009 444
5	0.083 333	35	0.583 333	5	0.001 389	35	0.009 722
6	.100 000	36	.600 000	6	.001 667	36	.010 000
7	.116 667	37	.616 667	7	.001 944	37	.010 278
8	.133 333	38	.633 333	8	.002 222	38	.010 556
9	.150 000	39	.650 000	9	.002 500	39	.010 833
10	0.166 667	40	o.666 667	10	0.002 778	40	0.011 111
11	.183 333	41	.683 333	11	.003 056	41	.011 389
12	.200 000	42	.700 000	12	.003 333	42	.011 667
13	.216 667	43	.716 667	13	.003 611	43	.011 944
14	.233 333	44	.733 333	14	.003 889	44	.012 222
15	0.250 000	45	0.750 000	15	0.004 167	45	0.012 500
16	.266 667	46	.766 667	16	.004 444	46	.012 778
17	.283 333	47	.783 333	17	.004 722	47	.013 056
18	.300 000	48	.800 000	18	.005 000	48	.013 333
19	.316 667	49	.816 667	19	.005 278	49	.013 611
20	0.333 333	50	o.833 333	20	0.005 556	50	0.013 SS9
21	.350 000	51	.850 000	21	.005 833	51	.014 167
22	.366 667	52	.866 667	22	.006 111	52	.014 444
23	.383 333	53	.883 333	23	.006 389	53	.014 722
24	.400 000	54	.900 000	24	.006 667	54	.015 000
25	0.416 667	55	0.916 667	25	0.006 944	55	0.015 278
26	·433 333	56	·933 333	26	.007 222	56	.015 556
27	·450 000	57	·950 000	27	.007 500	57	.015 833
28	·466 667	58	·966 667	28	.007 778	58	.016 111
29	·483 333	59	·983 333	29	.008 056	59	.016 389
30	0,500 000	60	1.000 000	30	0.008 333	60	0.016 667

TABLE 25.

LOCAL MEAN TIME AT APPARENT NOON.

Day of Month.	JAN.	FEB.	MAR.	APR.	MAY.	JUNE.
1 8 16 24	h. m. 12 4 12 7 12 10 12 12	h. m. 12 14 12 14 12 14 12 13	h. m. 12 12 12 11 12 9 12 6	h. m. 12 4 12 2 12 0 11 58	h. m. 11 57 11 56 11 56 11 57	h. m. 11 58 11 59 12 0 12 2
	JULY.	AUG.	SEPT.	oct.	NOV.	DITC.
1 8 16 24	h. m. 12 4 12 5 12 6 12 6	h. m. 12 6 12 5 12 4 12 2	h. m. 12 0 11 58 11 55 11 52	h. m. 11 50 11 48 11 46 11 44	h. m. 11 44 11 44 11 45 11 47	h. m. 11 49 11 52 11 56 12 0

TABLE 27.

SIDEREAL TIME INTO MEAN SOLAR TIME.

MEAN SOLAR TIME INTO SIDEREAL TIME.

The tabular values are to be *subtracted* from a sidereal time interval.

The tabular values are to be added to a mean solar time interval.

	nom a sid					7		mean so				
Hrs.	Reduction to Mean Time.	Min.	Reduc- tion to Mean Time.	Min.	Reduc- tion to Mean Time.		Hrs.	Reduction to Sidereal Time.	Min.	Reduc- tion to Sidereal Time.	Min.	Reduc- t on to Sidereal Time.
h. 1 2 3 4	m. s. 0 9.83 0 19.66 0 29.49 0 39.32	m. 1 2 3 4	s. 0.16 0.33 0.49 0.66	m. 31 32 33 34	s. 5.08 5.24 5.41 5.57		h. 2 3 4	m. s. o 9.86 o 19.71 o 29.57 o 39.43	m. 1 2 3 4	s. 0.16 0.33 0.49 0.66	m. 31 32 33 34	s. 5.09 5.26 5.42 5.59
5 6 7 8 9	0 49.15 0 58.98 1 8.81 1 18.64 1 28.47	5 6 7 8 9	0.82 0.98 1.15 1.31 1.47	35 36 37 38 39	5.73 5.90 6.06 6.23 6.39		5 6 7 8 9	0 49.28 0 59.14 1 9.00 1 18.85 1 28.71	5 6 7 8 9	0.82 0.99 1.15 1.31 1.48	35 36 37 38 39	5.75 5.91 6.08 6.24 6.41
10 11 12 13 14	1 38.30 1 48.13 1 57.95 2 7.78 2 17.61	10 11 12 13 14	1.64 1.80 1.97 2.13 2.29	40 41 42 43 44	6.55 6.72 6.88 7.04 7.21		10 11 12 13 14	1 38.56 1 48.42 1 58.28 2 8.13 2 17.99	10 11 12 13 14	1.64 1.81 1.97 2.14 2.30	40 41 42 43 44	6.57 6.74 6.90 7.06 7.23
15 16 17 18 19	2 27.44 2 37.27 2 47.10 2 56.93 3 6.76	15 16 17 18 19	2.46 2.62 2.79 2.95 3.11	45 46 47 48 49	7·37 7·54 7·70 7.86 8.03		15 16 17 18 19	2 27.85 2 37.70 2 47.56 2 57.42 3 7.27	15 16 17 18	2.46 2.63 2.79 2.96 3.12	45 46 47 48 49	7.39 7.56 7.72 7.89 8.05
20 21 22 23 24	3 16.59 3 26.42 3 36.25 3 46.08 3 55.91	20 21 22 23 24	3.28 3.44 3.60 3.77 3.93	50 51 52 53 54	8.19 8.36 8.52 8.68 8.85		20 21 22 23 24	3 17.13 3 26.99 3 36.84 3 46.70 3 56.56	20 21 22 23 24	3.29 3.45 3.61 3.78 3.94	50 51 52 53 54	8.21 8.38 8.54 8.71 8.87
		25 26 27 28 29	4.10 4.26 4.42 4.59 4.75	55 56 57 58 59	9.01 9.17 9.34 9.50 9.67				25 26 27 28 29	4.11 4.27 4.41 4.60 4.76	55 56 57 58 59	9.04 9.20 9.36 9.53 9.69
		30	4.91	60	9.83				30	4.93	60	9.86

Reduction for Seconds-sidereal or mean solar.

The tabular values are to be $\begin{cases} subtracted \text{ from a sidereal} \\ added \text{ to a mean solar} \end{cases}$ time interval.

Sidereal or Mean Time.	0	I	2	3	4	5 -	6	7	8	9
s. 0	s. 0.00	s. 0.00	s. 0.01	s. 0.01	s. o.oi	s. O.OI	s. 0.02	s. 0.02	s. 0.02	s. 0.02
10 20 30	.03 .05 .08	.03 .06 .08	.03 .06 .09	.04 .06 .09	.04 .07 .09	.04 .07	.04 .07	.05 .07 .10	.05 .08	.05 .08
40	.11	.11	.11	.12	.12	.12	.13	.13	.13	.13
50	0.14	0.14	0.14	0.15	0.15	0.15	0.15	0.16	0.16	0.16

^{*} Subtract 0.14 from a sidereal time interval.

CONVERSION OF MEASURES OF WEIGHT.

Conversion of avoirdupois pound	s a	nd	ou	nce	s ii	ıto	kil	ogi	an	ıs	٠	TABLE 28
Conversion of kilograms into avo	ird	up	ois	poi	unc	ls a	ınd	ou	псе	es		TABLE 29
Conversion of grains into grams												TABLE 30
Conversion of grams into grains			0									TABLE 31

TABLE 28.

AVOIRDUPOIS POUNDS AND OUNCES INTO KILOGRAMS.

ı avoirdupois pound = 0.4535924 kilogram. ı avoirdupois ounce = 0.0283495 kilogram.

Pounds.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	kg.									
0	0.0000	0.0454	0.0907	0.1361	0.1814	0.2268	0.2722	0.3175	0.3629	0.4082
I	0.4536	0.4990	0.5443	0.5897	0.6350	0.6804	0.7257	0.7711	0.8165	0.8618
2	0.9072	0.9525	0.9979	1.0433	1.0886	1.1340	1.1793	1.2247	1.2701	1.3154
3	1.3608	1.4061	1.4515	1.4969	1.5422	1.5876	1.6329	1.6783	1.7237	1.7690
4	1.8144	1.8597	1.9051	1.9504	1.9958	2.0412	2.0865	2.1319	2.1772	2.2226
5	2.2680	2.3133	2.3587	2.4040	2.4494	2.4948	2.5401	2.5855	2.6308	2.6762
6	2.7216	2.7669	2.8123	2.8576	2.9030	2.9484	2.9937	3.0391	3.0844	3.1298
7	3.1751	3.2205	3.2659	3.3112	3.3566	3.4019	3.4473	3.4927	3.5380	3.5834
8	3.6287	3.6741	3.7195	3.7648	3.8102	3.8555	3.9009	3.9463	3.9916	4.0370
9	4.0823	4.1277	4.1731	4.2184	4.2638	4.3091	4.3545	4.3998	4.4452	4.4906
Ounces.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
	kg.									
0	0,0000	0.0028	0.0057	0.0085	0.0113	0.0142	0.0170	0.0198	0.0227	0.0255
I	.0283	.0312	.0340	.0369	.0397	.0425	.0454	.0482	.0510	.0539
2	.0567	.0595	.0624	.0652	.0680	.0709	.0737	.0765	.0794	.0822
3	.0850	.0879	.0907	.0936	.0964	.0992	.1021	.1049	.1077	.1106
4	.1134	.1162	.1191	.1219	.1247	.1276	.1304	.1332	.1361	.1389
5	0.1417	0.1446	0.1474	0.1503	0.1531	0.1559	0.1588	0.1616	0.1644	0.1673
6	.1701	.1729	.1758	.1786	.1814	.1843	.1871	.1899	.1928	.1956
7	.1984	.2013	.2041	.2070	.2098	.2126	.2155	.2183	.2211	.2240
8	.2268	.2296	.2325	.2353	.2381	.2410	.2438	.2466	.2495	.2523
9	.2551	.2580	.2608	.2637	.2665	.2693	.2722	.2750	.2778	.2807
10	0.2835	0.2863	0.2892	0.2920	0.2948	0.2977	0.3005	0.3033	0.3062	0.3090
II	.3118	.3147	.3175	.3203	.3232	.3260	.3289	.3317	-3345	•3374
12	.3402	.3430	•3459	.3487	-3515	-3544	.3572	.3600	.3629	.3657
13	.3685	.3714	-3742	.3770	-3799	.3827	.3856	.3884	.3912	-3941
14	.3969	-3997	.4026	.4054	.4082	.4111	.4139	.4167	.4196	.4224
1										

KILOGRAMS INTO AVOIRDUPOIS POUNDS AND OUNCES.

I kilogram = 2.204622 avoirdupois pounds.

Kilograms.	0.0	1.0	0.2	0.3	3	0.4	0.5	0.6	0.7	0.8	0.9
	Av. lbs.	Av. 1bs.	Av. 1bs.	Av. I	bs.	Av. 1bs.	Av. 1bs	. Av.1bs.	Av. 1bs	. Av. lbs.	Av. 1bs.
0	0.000	0.220	0.441	0.6	61	0.882	1.102	1.323	1.543	1.764	1.984
1	2.205	2.425	2.646	2.8	66	3.086	3.307		3.748		1 - 1
2	4.409	4.630	4.850	5.0	71	5.291	5.512	5.732	5.952	1 -	1
3	6.614	6.834	7.055	7.2	75	7.496	7.716	7.937	8.157		
4	8.818	9.039	9.259	9.4	So	9.700	9.921	10.141	10.362	10.582	10.803
5	11.023	11.244	11.464	11.6	84	11.905	12.125	12.346	12.566	12.787	13.007
6	13.228	13.448	13.669	13.8	- 1	14.110	14.330		14.771		15.212
7	15.432	15.653	15.873	16.0	94	16.314	16.535		16.976	1	
8	17.637	17.857	18.078	18.20	98	18.519	18.739		19.180	1	19.621
9	19.842	20.062	20.283	20.5	03	20.723	20.944	21.164	21.385		21.826
		Tenths of a	Kilogram i	nto Oun	nces.		i	Hundre nto Decimals	dths of a of a Pou	Kilogram nd and Ounc	es.
	kg.	Oz.		g.		Oz.	kg.	Av. 1bs.	Oz. 1	g. Av. 1	os. Oz.
	0.1	3.527		.6		1.1644	0.01	0.022 = 0	-	-	2 = 2.12
	.2 .3	7.054 10.582		·7		4.6918 8 . 2192	.02	.044 = 0 .066 = 1			4 = 2.47 5 = 2.82
	•4	14.109		.9		1.7466	.03	.088 = 1			3 = 2.02 3 = 3.17
	-5	17.637	0 1	.0	-	5.2740	.05	.110 = 1		-	0 = 3.53

TABLE 30.

CRAINS INTO CRAMS.

1 grain = 0.06479892 gram.

Grains.	0	ı	2	3		4	5	6	7	7	8	9
	grams.	grams.	grams.	gran	ns.	grams.	grams.	grams.	gra	ms.	grams.	grams.
0	0.0000	0.0648	0.1296	0.19	44	0.2592	0.3240	0.3888	0.4	536	0.5184	0.5832
10	0.6480	0.7128	0.7776	0.84	24	0.9072	0.9720	1.0368	1.10	016	1.1664	1.2312
20	1.2960	1.3608	1.4256	1.49	04	1.5552	1.6200	1.6848	1.74	196	1.8144	1.8792
30	1.9440	2.0088	2.0736	2.13	84	2.2032	2.2680	2.3328	2.39	976	2.4624	
40	2.5920	2.6568	2.7216	2.78	64	2.8512	2.9160	2.9808	3.04	155	3.1103	3.1751
50	3.2399	3.3047	3.3695	3.43	43	3.4991	3.5639	3.6287	3.60	935	3.7583	3.8231
60	3.8879	3.9527	4.0175	4.68		4.1471	4.2119	4.2767	4.34		4.4063	1 - 1
70	4.5359	4.6007	4.6655	4.73	03	4.7951	4.8599	4.9247	4.98	395	5.0543	
80	5.1839	5.2487	5.3135	5.37	83	5-4431	5.5079	5.5727	5.6	375	5.7023	5.7671
90	5.8319	5.8967	5.9615	6.02	63	6.0911	6.1559	6.2207	6.28	355	6.3503	6.4151
		Tent	hs of a G	rain.				Hundre	edths	of a	Grain.	
	Grain,	gram.	Gr	ain.	-	gram.	Grain;	gran	1.	Gı	rain.	gram.
	0.1	0.0065		- 1	C	.0389	0,01	0.000			.06	0.0039
	.2	.0130		·7		.0454	.02	100.	~		.07	.0045
	•3 •4	.0194	·	.9		.0513	.03	.002	- 1		.09	.0052
	-5	.0324	- 1	.0		.0648	.05	.003	2		.10	.0065

CRAMS INTO CRAINS.

1 gram = 15.432356 grains.

Grams.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
0 1 2 3 4 5 6 7 8	Grains. 0.00 15.43 30.86 46.30 61.73 77.16 92.59 108.03 123.46 138.89	Grains. 1.54 16.98 32.41 47.84 63.27 78.71 94.14 109.57 125.00 140.43	Grains. 3.09 18.52 33.95 49.38 64.82 80.25 95.68 111.11 126.55 141.98	Grains 4.6; 20.06 35.49 50.93 66.36 81.79 97.22 112.66 128.09	6.17 21.61 37.04 52.47 67.90 83.33 98.77 114.20 129.63	Grains. 7.72 23.15 38.58 54.01 69.45 84.88 100.31 115.74 131.18 146.61	Grains. 9.26 24.69 40.12 55.56 70.99 86.42 101.85 117.29 132.72 148.15	Grains. 10.80 26.24 41.67 57.10 72.53 87.96 103.40 118.83 134.26 149.69	12.35 27.78 43.21 58.64 74.08 89.51 104.94 120.37 135.80	Graius. 13.89 29.32 44.75 60.19 75.62 91.05 106.48 121.92 137.35 152.78
	0	ı	2	3	4	5	6	7	8	9
0 10 20 30 40 50 60 70 80 90	1234.59		Grains. 30.86 185.19 339.51 493.84 648.16 802.48 956.81 1111.13 1265.45 1419.78	Grains 46.30 200.62 354.94 509.27 663.50 817.91 972.22 1126.56 1280.89	61.73 216.05 370.38 524.70 679.02 833.35 987.67 1141.99 1296.32	1157.43	Grains. 92.59 246.92 401.24 555.56 709.89 864.21 1018.54 1172.86 1327.18 1481.51	Grains. 108.03 262.35 416.67 571.00 725.32 879.64 1033.97 1188.29 1342.61	123.46 277.78 432.11 586.43 740.75 895.08 1049.40 1203.72 1358.05	Grains. 138.89 293.21 447.54 601.86 756.19 910.51 1064.83 1219.16 1373.48 1527.80
	gram. 0.01 .02 .03 .04 .05	Grain 0.154 .309 .463 .617 .772	0.0	- 1	Grain. 0.926 1.080 1.235 1.389 1.543	gram. 0.001 .002 .003 .004 .005	Grain 6.015 .031 .046 .062	0	ram, .006 .007 .008 .009	Grain. 0.093 .108 .123 .139 .154

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SYNOPTIC CONVERSION OF VELOCITIES.

Miles per hour into meters per second, feet per second and kilometers per hour.

Miles per hour.	Meters per second.	Feet per second.	Kilome- ters per hour.	Miles per hour.	Meters per second.	Feet per second,	Kilome- ters per hour,	Miles per hour.	Meters per second.	Feet per second.	Kilome- ters per hour.
0.0 0.5 1.0 1.5 2.0 2.5	0.0 0.2 0.4 0.7 0.9 1.1	0.0 0.7 1.5 2.2 2.9 3.7	0.0 0.8 1.6 2.4 3.2 4.0	26.0 26.5 27.0 27.5 28.0 28.5	11.6 11.8 12.1 12.3 12.5	38.1 38.9 39.6 40.3 41.1 41.8	41.8 42.6 43.5 44.3 45.1 45.9	52.0 52.5 53.0 53.5 54.0 54.5	23.2 23.5 23.7 23.9 24.1 24.4	76.3 77.0 77.7 78.5 79.2 79.9	83.7 84.5 85.3 86.1 86.9 87.7
3.0 3.5 4.0 4.5 5.0 5.5	1.3 1.6 1.8 2.0 2.2 2.5	4.4 5.1 5.9 6.6 7.3 8.1	4.8 5.6 6.4 7.2 8.0 8.9	29.0 29.5 30.0 30.5 31.0 31.5	13.0 13.2 13.4 13.6 13.9 14.1	42.5 43.3 44.0 44.7 45.5 46.2	46.7 47.5 48.3 49.1 49.9 50.7	55.0 55.5 56.0 56.5 57.0 57.5	24.6 24.8 25.0 25.3 25.5 25.7	80.7 81.4 82.1 82.9 83.6 84.3	88.5 89.3 90.1 90.9 91.7 92.5
6.0 6.5 7.0 7.5 8.0 8.5	2.7 2.9 3.1 3.4 3.6 3.8	8.8 9.5 10.3 11.0 11.7 12.5	9.7 10.5 11.3 12.1 12.9 13.7	32.0 32.5 33.0 33.5 34.0 34.5	14.3 14.5 14.8 15.0 15.2 15.4	46.9 47.7 48.4 49.1 49.9 50.6	51.5 52.3 53.1 53.9 54.7 55.5	58.0 58.5 59.0 59.5 60.0 60.5	25.9 26.2 26.4 26.6 26.8 27.0	85.1 85.8 86.5 87.3 88.0 88.7	93·3 94·1 95·0 95.8 96.6 97·4
9.0 9.5 10.0 10.5 11.0	4.0 4.2 4.5 4.7 4.9 5.1	13.2 13.9 14.7 15.4 16.1 16.9	14.5 15.3 16.1 16.9 17.7 18.5	35.0 35.5 36.0 36.5 37.0 37.5	15.6 15.9 16.1 16.3 16.5 16.8	51.3 52.1 52.8 53.5 54.3 55.0	56.3 57.1 57.9 58.7 59.5 60.4	61.0 61.5 62.0 62.5 63.0 63.5	27.3 27.5 27.7 27.9 28.2 28.4	89.5 90.2 90.9 91.7 92.4 93.1	98.2 99.0 99.8 100.6 101.4 102.2
12.0 12.5 13.0 13.5 14.0 14.5	5.4 5.6 5.8 6.0 6.3 6.5	17.6 18.3 19.1 19.8 20.5 21.3	19.3 20.1 20.9 21.7 22.5 23.3	38.0 38.5 39.0 39.5 40.0 40.5	17.0 17.2 17.4 17.7 17.9 18.1	55.7 56.5 57.2 57.9 58.7 59.4	61.2 62.0 62.8 63.6 64.4 65.2	64.0 64.5 65.0 65.5 66.0 66.5	28.6 28.8 29.1 29.3 29.5 29.7	93.9 94.6 95.3 96.1 96.8 97.5	103.0 103.8 104.6 105.4 106.2 107.0
15.0 15.5 16.0 16.5 17.0 17.5	6.7 6.9 7.2 7.4 7.6 7.8	22.0 22.7 23.5 24.2 24.9 25.7	24.1 24.9 25.7 26.6 27.4 28.2	41.0 41.5 42.0 42.5 43.0 43.5	18.3 18.6 18.8 19.0 19.2	60.1 60.9 61.6 62.3 63.1 63.8	66.0 66.8 67.6 68.4 69.2 70.0	67.0 67.5 68.0 68.5 69.0 69.5	30.0 30.2 30.4 30.6 30.8 31.1	98.3 99.0 99.7 100.5 101.2	107.8 108.6 109.4 110.2 111.0 111.8
18.0 18.5 19.0 19.5 20.0 20.5	8.0 8.3 8.5 8.7 8.9 9.2	26.4 27.1 27.9 28.6 29.3 30.1	29.0 29.8 30.6 31.4 32.2 33.0	44.0 44.5 45.0 45.5 46.0 46.5	19.7 19.9 20.1 20.3 20.6 20.8	64.5 65.3 66.0 66.7 67.5 68.2	70.8 71.6 72.4 73.2 74.0 74.8	70.0 70.5 71.0 71.5 72.0 72.5	31.3 31.5 31.7 32.0 32.2 32.4	102.7 103.4 104.1 104.9 105.6 106.3	112.7 113.5 114.3 115.1 115.9 116.7
21.0 21.5 22.0 22.5 23.0 23.5	9.4 9.6 9.8 10.1 10.3 10.5	30.8 31.5 32.3 33.0 33.7 34.5	33.8 34.6 35.4 36.2 37.0 37.8	47.0 47.5 48.0 48.5 49.0 49.5	21.0 21.2 21.5 21.7 21.9 22.1	68.9 69.7 70.4 71.1 71.9 72.6	75.6 76.4 77.2 78.1 78.9 79.7	73.0 73.5 74.0 74.5 75.0 75.5	32.6 32.9 33.1 33.3 33.5 33.5	107.1 107.8 108.5 109.3 110.0	117.5 118.3 119.1 119.9 120.7 121.5
24.5 25.0 25.5 26.0	10.7 11.0 11.2 11.4 11.6	35.2 35.9 36.7 37.4 38.1	38.6 39.4 40.2 41.0 41.8	50.0 50.5 51.0 51.5 52.0	22.4 22.6 22.8 23.0 23.2	73.3 74.1 74.8 75.5 76.3	80.5 81.3 82.1 82.9 83.7	76.0 76.5 77.0 77.5 78.0	34.0 34.2 34.4 34.6 34.9	111.5 112.2 112.9 113.7 114.4	122.3 123.1 123.9 124.7 125.5

MILES PER HOUR INTO FEET PER SECOND.

r mile per hour $=\frac{44}{30}$ feet per second.

Miles per hour.	0	1	2	3	4	5	6	7	8	9
	Feet per sec.	Feet per								
0	0.0	1.5	2.9	4.4	5.9	7.3	8.8	10.3	11.7	13.2
IO	14.7	16.1	17.6	19.1	20.5	22.0	23.5	24.9	26.4	27.9
20	29.3	30.8	32.3	33.7	35.2	36.7	38. 1	39.6	41.1	42.5
30	44.0	45.5	46.9	48.4	49.9	51.3	52.8	54.3	55-7	57.2
40	58.7	60.1	61.6	63.1	64.5	66.0	67.5	68.9	70.4	71.9
50	73.3	74.8	76.3	77.7	79.2	80.7	82.1	83.6	85.1	86.5
60	88.0	89.5	90.9	92.4	93.9	95.3	96.8	98.3	99.7	IOI.2
70 80	102.7	104.1	105.6	107.1	108.5	110.0	111.5	112.9	114.4	115.9
	117.3	118.8	120.3	121.7	123.2	124.7	126.1	127.6	129.1	130.5
90	132.0	133.5	134.9	136.4	137.9	139.3	140.8	142.3	143.7	145.2
100	146.7	148.1	149.6	151.1	152.5	154.0	155.5	156.9	158.4	159.9
110	161.3	162.8	164.3	165.7	167.2	168.7	170.1	171.6	173.1	174.5
120	176.0	177.5	178.9	180.4	181.9	183.3	184.8	186.3	187.7	189.2
130	190.7	192.1	193.6	195.1	196.5	198.0	199.5	200.9	202.4	203.9
140	205.3	206.8	208.3	209.7	211.2	212.7	214.1	215.6	217.1	218.5

TABLE 34.

FEET PER SECOND INTO MILES PER HOUR.

I foot per second $=\frac{30}{44}$ miles per hour.

Feet per sec.	0	1	2	3	4	5	6	7	8	9
	Miles per hr. 0.0 6.8 13.6 20.5 27.3 34.1 40.9 47.7 54.5 61.4 68.2 75.0 81.8 88.6 95.5	Miles per hr. 0.7 7.5 14.3 21.1 28.0 34.8 41.6 48.4 55.2 62.0 68.9 75.7 82.5 89.3 96.1	Miles per hr. 1.4 8.2 15.0 21.8 28.6 35.5 42.3 49.1 55.9 62.7 69.5 76.4 83.2 90.0 96.8	Miles per hr. 2.0 8.9 15.7 222.5 29.3 36.1 43.0 49.8 56.6 63.4 70.2 77.0 83.9 90.7 97.5	Miles per hr. 2.7 9.5 16.4 23.2 30.0 36.8 43.6 50.5 57.3 64.1 70.9 77.7 84.5 91.4 98.2	Miles per hr. 3.4 10.2 17.0 23.9 30.7 37.5 44.3 51.1 58.0 64.8 71.6 78.4 85.2 92.0 98.9	Miles per hr. 4.1 10.9 17.7 24.5 31.4 38.2 45.0 51.8 58.6 65.5 72.3 79.1 85.9 92.7 99.5	Miles per hr. 4.8 11.6 18.4 25.2 32.0 38.9 45.7 52.5 59.3 66.1 73.0 79.8 86.6 93.4 100.2	Miles per hr. 5.5 12.3 19.1 25.9 32.7 39.5 46.4 53.2 60.0 66.8 73.6 80.5 87.3 94.1 100.9	Miles per hr. 6. I 13.0 19.8 26.6 33.4 40 2 47.0 53.9 60.7 67.5 74.3 81. I 88.0 94.8 101.6
160 170 180 190	102.3 109.1 115.9 122.7 129.5	103.0 109.8 116.6 123.4 130.2	103.6 110.5 117.3 124.1 130.9	104.3 111.1 118.0 124.8 131.6	105.0 111.8 118.6 125.5 132.3	105.7 112.5 119.3 126.1 133.0	106.4 113.2 120.0 126.8 133.6	107.0 113.9 120.7 127.5 134.3	107.7 114.5 121.4 128.2 135.0	108.4 115.2 120.0 128.9 135.7

METERS PER SECOND INTO MILES PER HOUR.

1 meter per second = 2.236932 miles per hour.

Meters per second.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
	Miles	Miles	Miles							
	per hr.	per hr.	per hr.							
0 1 2 3 4	0.0 2.2 4.5 6.7 8.9	0.2 2.5 4.7 6.9 9.2	0.4 2.7 4.9 7.2 9.4	0.7 2.9 5.1 7.4 9.6	0.9 3.1 5.4 7.6 9.8	1.1 3.4 5.6 7.8 10.1	3.6 5.8 8.1	1.6 3.8 6.0 8.3	1.8 4.0 6.3 8.5 10.7	2.0 4.3 6.5 8.7 11.0
5 6 7 8 9	11.2 13.4 15.7 17.9 20.1	11.4 13.6 15.9 18.1	11.6 13.9 16.1 18.3 20.6	11.9 14.1 16.3 18.6 20.8	12.1 14.3 16.6 18.8 21.0	12.3 14.5 16.8 19.0 21.3	12.5 14.8 17.0 19.2 21.5	12.8 15.0 17.2 19.5 21.7	13.0 15.2 17.4 19.7 21.9	13.2 15.4 17.7 19.9 22.1
10	22.4	22.6	22.8	23.0	23.3	23.5	23.7	23.9	24.2	24.4
11	24.6	24.8	25.1	25.3	25.5	25.7	25.9	26.2	26.4	26.6
12	26.8	27.1	27.3	27.5	27.7	28.0	28.2	28.4	28.6	28.9
13	29.1	29.3	29.5	29.8	30.0	30.2	30.4	30.6	30.9	31.1
14	31.3	31.5	31.8	32.0	32.2	32.4	32.7	32.9	33.1	33.3
15	33.6	33.8	34.0	34.2	34.4	34.7	34.9	35.1	35·3	35.6
16	35.8	36.0	36.2	36.5	36.7	36.9	37.1	37.4	37.6	37.8
17	38.0	38.3	38.5	38.7	38.9	39.1	39.4	39.6	39.8	40.0
18	40.3	40.5	40.7	40.9	41.2	41.4	41.6	41.8	42.1	42.3
19	42.5	42.7	43.0	43.2	43.4	43.6	43.8	44.1	44·3	44.5
20	44.7	45.0	45.2	45.4	45.6	45.9	46.1	46.3	46.5	46.8
21	47.0	47.2	47.4	47.6	47.9	48.1	48.3	48.5	48.8	49.0
22	49.2	49.4	49.7	49.9	50.1	50.3	50.6	50.8	51.0	51.2
23	51.5	51.7	51.9	52.1	52.3	52.6	52.8	53.0	53.2	53.5
24	53.7	53.9	54.1	54.4	54.6	54.8	55.0	55.3	55.5	55.7
25	55.9	56.1	56.4	56.6	56.8	57.0	57·3	57.5	57·7	57.9
26	58.2	58.4	58.6	58.8	59.1	59.3	59·5	59.7	60.0	60.2
27	60.4	60.6	60.8	61.1	61.3	61.5	61.7	62.0	62.2	62.4
28	62.6	62.9	63.1	63.3	63.5	63.8	64.0	64.2	64.4	64.6
29	64.9	65.1	65.3	65.5	65.8	66.0	66.2	66.4	66.7	66.9
30	67.1	67.3	67.6	67.8	68.0	68.2	68.5	68.7	68.9	69.1
31	69.3	69.6	69.8	70.0	70.2	70.5	70.7	70.9	71.1	71.4
32	71.6	71.8	72.0	72.3	72.5	72.7	72.9	73.1	73.4	73.6
33	73.8	74.0	74.3	74.5	74.7	74.9	75.2	75.4	75.6	75.8
34	76.1	76.3	76.5	76.7	77.0	77.2	77.4	77.6	77.8	78.1
35	78.3	78.5	78.7	79.0	79.2	79.4	79.6	79.9	So. I	80.3
36	80.5	So.8	S1.0	81.2	81.4	81.6 .	81.9	82.1	S2. 3	82.5
37	82.8	83.0	83.2	83.4	83.7	84.0	84.1	84.3	S4. 6	84.8
38	85.0	85.2	85.5	85.7	85.9	86.1	86.3	86.6	S6. 8	87.0
39	87.2	87.5	87.7	87.9	88.1	88.4	88.6	88.8	S9. 0	89.3
40 41 42 43 44	89.5 91.7 94.0 96.2 98.4	89.7 91.9 94.2 96.4 98.7	89.9 92.2 94.4 96.6 98.9	90.2 92.4 94.6 96.9 99.1	90.4 92.6 94.8 97.1 99.3	90.6 92.8 95.1 97.3 99.5	90.8 93.1 95.3 97.5 99.8	91.0 93.3 95.5 97.8 100.0	91.3 93.5 95.7 98.0 100.2	91.5 93.7 96.0 98.2

METERS PER SECOND INTO MILES PER HOUR.

Meters per second.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
	Miles per hr.									
45	100.7	100.9	IOI.I	101.3	101.6	101.8	102.0	102.2	102.5	102.7
46	102.9	103.1	103.3	103.6	103.8	104.0	104.2	104.5	104.7	104.9
47	105.1	105.4	105.6	105.8	106.0	106.3	106.5	106.7	106.9	107.2
48	107.4	107.6	107.8	108.0	108.3	108.5	108.7	108.9	109.2	109.4
49	109.6	109.8	IIO.I	110.3	110.5	110.7	III.O	III.2	111.4	111.6
50 51 52 53 54	111.8 114.1 116.3 118.6 120.8	112.1 114.3 116.6 118.8 121.0	112.3 114.5 116.8 119.0 121.3	112.5 114.8 117.0 119.2 121.5	112.7 115.0 117.2 119.5 121.7	113.0 115.2 117.4 119.7 121.9	113.2 115.4 117.7 119.9 122.1	113.4 115.7 117.9 120.1 122.4	113.6 115.9 118.1 120.4 122.6	113.9 116.1 118.3 120.6 122.8
55	123.0	123.3	123.5	123.7	123.9	124.2	124.4	124.6	124.8	125.1
56	125.3	125.5	125.7	126.0 128.2	126.2 128.4	126.4 128.6	126.6 128.9	126.8	127.1	127.3
57 58	127.5	127.8	130.2	130.4	130.7	130.9	131.1	129.1	129.3	129.5
59	132.0	132.2	132.5	132.7	132.9	133.1	133.3	131.3	133.8	134.0

TABLE 36.

MILES PER HOUR INTO METERS PER SECOND.

I mile per hour = 0.4470409 meters per second.

Miles per hour.	0	1	2	3	4	5	6	7	8	9
	meters per sec.									
0	0.00	0.45	0.89	1.34	1.79	2.24	2.68	3.13	3.58	4.02
10	4.47	4.92	5.36	5.81	6.26	6.71	7.15	7.60	8.05	8.49
20	8.94	9.39	9.83	10.28	10.73	11.18	11.62	12.07	12.52	12.96
30	13.41	13.86	14.31	14.75	15.20	15.65	16.09	16.54	16.99	17.43
40	17.88	18.33	18.78	19.22	19.67	20,12	20,56	21.01	21.46	21.90
50 60	22.35 26.82	22.80 27.27	23.25 27.72	23.69 28.16	24.14 28.61	24.59 29.06	25.03 29.50	25.48 29.95	25.93 30.40	26.37 30.85
70	31.29	31.74	32.19	32.63	33.08	33.53	33.98	34.42	34.87	35.32
80	35.76	36.21	36.66	37.10	37.55	38.00	38.44	38.89	39.34	39.79
90	40.23	40.68	41.13	41.57	42.02	42.47	42.92	43.36	43.81	44.26
100	44.70	45.15	45.60	46.04	46.49	46.94	47.39	47.83	48.28	48.73
110	49.17	49.62	50.07	50.51	50.96	51.41	51.86	52.30	52.75	53.20
120	53.64	54.09	54.54	54.98	55.43	55.88	56.33	56.77	57.22	57.67
130	58.12	58.56	59.01	59.46	59.90	60.35	60.80	61.24	61.69	62.14
140	62.59	63.03	63.48	63.93	64.37	64.82	65.27	65.72	66.16	66.61

METERS PER SECOND INTO KILOMETERS PER HOUR.

I meter per second = 3.6 kilometers per hour.

Meters per second.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
	km.	km.	km.	km.	km.	km.	km.	km.	km.	km.
	per hr.	per hr.	per hr.	per hr.	per hr.	per hr.	per hr.	per hr.	per hr.	per hr.
0 I 2 3 4	0.0 3.6 7.2 10.8 14.4	0.4 4.0 7.6 11.2 14.8	0.7 4.3 7.9 11.5 15.1	1.1 4.7 8.3 11.9	1.4 5.0 8.6 12.2 15.8	1.8 5.4 9.0 12.6 16.2	2.2 5.8 9.4 13.0 16.6	2.5 6.1 9.7 13.3 16.9	2.9 6.5 10.1 13.7 17.3	3.2 6.8 10.4 14.0 17.6
5	18.0	18.4	18.7	19.1	19.4	19.8	20.2	20.5	20.9	21.2
6	21.6	22.0	22.3	22.7	23.0	23.4	23.8	24.1	24.5	24.8
7	25.2	25.6	25.9	26.3	26.6	27.0	27.4	27.7	28.1	28.4
8	28.8	29.2	29.5	29.9	30.2	30.6	31.0	31.3	31.7	32.0
9	32.4	32.8	33.1	33.5	33.8	34.2	34.6	34.9	35.3	35.6
10	36.0	36.4	36.7	37.1	37.4	37.8	38.2	38.5	38.9	39.2
11	39.6	40.0	40.3	40.7	41.0	41.4	41.8	42.1	42.5	42.8
12	43.2	43.6	43.9	44.3	44.6	45.0	45.4	45.7	46.1	46.4
13	46.8	47.2	47.5	47.9	48.2	48.6	49.0	49.3	49.7	50.0
14	50.4	50.8	51.1	51.5	51.8	52.2	52.6	52.9	53.3	53.6
15 16 17 18	54.0 57.6 61.2 64.8 68.4	54.4 58.0 61.6 65.2 68.8	54.7 58.3 61.9 65.5 69.1	55.1 58.7 62.3 65.9 69.5	55.4 59.0 62.6 66.2 69.8	55.8 59.4 63.0 66.6 70.2	56.2 59.8 63.4 67.0 70.6	56.5 60.1 63.7 67.3 70.9	56.9 60.5 64.1 67.7 71.3	57.2 60.8 64.4 68.0 71.6
20	72.0	72.4	72.7	73.1	73.4	73.8	74.2	74.5	74.9	75.2
21	75.6	76.0	76.3	76.7	77.0	77.4	77.8	78.1	78.5	78.8
22	79.2	79.6	79.9	80.3	80.6	81.0	81.4	81.7	82.1	82.4
23	82.8	83.2	83.5	83.9	84.2	84.6	85.0	85.3	85.7	86.0
24	86.4	86.8	87.1	87.5	87.8	88.2	88.6	88.9	89.3	89.6
25 26 27 28 29	90.0 93.6 97.2 100.8 104.4	90.4 94.0 97.6 101.2 104.8	90.7 94·3 97·9 101.5	91.1 94.7 98.3 101.9	91.4 95.0 98.6 102.2 105.8	91.8 95.4 99.0 102.6 106.2	92.2 95.8 99.4 103.0 106.6	92.5 96.1 99.7 103.3 106.9	92.9 96.5 100.1 103.7 107.3	93.2 96.8 100.4 104.0 107.6
30	108.0	108.4	108.7	109.1	109.4	109.8	110.2	110.5	110.9	111.2
31	111.6	112.0	112.3	112.7	113.0	113.4	113.8	114.1	114.5	114.8
32	115.2	115.6	115.9	116.3	116.6	117.0	117.4	117.7	118.1	118.4
33	118.8	119.2	119.5	119.9	120.2	120.6	121.0	121.3	121.7	122.0
34	122.4	122.8	123.1	123.5	123.8	124.2	124.6	124.9	125.3	125.6
35	126.0	126.4	126.7	127.1	127.4	127.8	128.2	128.5	128.9	129.2
36	129.6	130.0	130.3	130.7	131.0	131.4,	131.8	132.1	132.5	132.8
37	133.2	133.6	133.9	134.3	134.6	135.0	135.4	135.7	136.1	136.4
38	136.8	137.2	137.5	137.9	138.2	138.6	139.0	139.3	139.7	140.0
39	140.4	140.8	141.1	141.5	141.8	142.2	142.6	142.9	143.3	143.6
40	144.0	144.4	144.7	145.1	145.4	145.8	146.2	146.5	146.9	147.2
41	147.6	148.0	148.3	148.7	149.0	149.4	149.8	150.1	150.5	150.8
42	151.2	151.6	151.9	152.3	152.6	153.0	153.4	153.7	154.1	154.4
43	154.8	155.2	155.5	155.9	156.2	156.6	157.0	157.3	157.7	158.0
44	158.4	158.8	159.1	159.5	159.8	160.2	160.6	160.9	161.3	161.6

METERS PER SECOND INTO KILOMETERS PER HOUR.

Meters per second.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
45 46 47	km. per hr. 162.0 165.6 169.2	km. per hr. 162.4 166.0 169.6	km. per hr. 162.7 166.3 169.9	km. per hr. 163.1 166.7 170.3	km. per hr. 163.4 167.0 170.6	km. per hr. 163.8 167.4 171.0	km. per hr. 164.2 167.8	km. per hr. 164.5 168.1	km. per hr. 164.9 168.5 172.1	km. per hr. 165.2 168.8 172.4
48 49 50	172.8 176.4 180.0	173.2 176.8	173.5 177.1	173.9 177.5	174.2 177.8	174.6 178.2 181.8	175.0 178.6	175.3 178.9	175.7 179.3	176.0 179.6
51 52 53 54	183.6 187.2 190.8	184.0 187.6 191.2 194.8	184.3 187.9 191.5 195.1	184.7 188.3 191.9	185.0 188.6 192.2 195.8	185.4 189.0 192.6	185.8 189.4 193.0 196.6	186.1 189.7 193.3	186.5 190.1 193.7 197.3	186.8 190.4 194.0
55 56 57	198.0 201.6 205.2 208.8	198.4 202.0 205.6	198.7 202.3 205.9	199.1 202.7 206.3	199.4 203.0 206.6	199.8 203.4 207.0	200.2 203.8 207.4	200.5 204.1 207.7	200.9 204.5 208. I	201.2 204.8 208.4
58 59	212.4	209.2	209.5	209.9	210.2	210.6	211.0 214.6	211.3	211.7	212.0

TABLE 38.

KILOMETERS PER HOUR INTO METERS PER SECOND.

I kilometer per hour $=\frac{10}{36}$ meters per second.

Kilcmeters per hour.	. 0	1	2	3	4	5	6	7	8	9
	meters per sec.	meters per sec,	meters per sec.	meters per sec.						
0	0.00	0.28		0.83	1.11	•	1.67	1.94	2.22	2.50
			0.56	3.61	3.89	1.39			5.00	5.28
10 20	2.78	3.06 5.83	3.33 6.11	6.39	6.67	4.17 6.94	4.44 7.22	4.72 7.50	7.78	8.06
	5.56	8.61	8.89				10.00	10.28	10.56	10.83
30	8.33			9.17	9.44	9.72	_			
40	11.11	11.39	11.67	11.94	12.22	12.50	12.78	13.06	13.33	13.61
50	13.89	14.17	14.44	14.72	15.00	15.28	15.56	15.83	16.11	16.39
60	16.67	16.94	17.22	17.50	17.78	18.06	18.33	18.61	18.89	19.17
70	19.44	19.72	20.00	20.28	20.56	20.83	21.11	21.39	21.67	21.94
So	22,22	22.50	22.78	23.06	23.33	23.61	23.89	24.17	24.44	24.72
90	25.00	25.28	25.56	25.83	26.11	26.39	26.67	26.94	27.22	27.50
,	_5,	-5	-5.5-	-00			,			1.0-
100	27.78	28.06	28.33	28.61	28.89	29.17	29.44	29.72	30.00	30.28
110	30.56	30.83	31.11	31.39	31.67	31.94	32.22	32.50	32.78	33.06
120	33.33	33.61	33.89	34.17	34.44	34.72	35.00	35.28	35.56	35.83
130	36.11	36.39	36.67	36.94	37.22	37.50	37.78	38.06	38.33	38.61
140	38.89	39.17	39.44	39.72	40.00	40.28	40.56	40.83	41.11	41.39
							-			
150	41.67	41.94	42.22	42.50	42.78	43.06	43-33	43.61	43.89	44.17
160	44.44	44.72	45.00	45.28	45.56	45.83	46.11	46.39	46.67	46.94
170	47.22	47.50	47.78	48.06	48.33	48.61	48.89	49.17	49.44	49.72
180	50.00	50.28	50.56	50.83	51.11	51.39	51.67	51.94	52.22	52.50
190	52.78	53.06	53-33	53.61	53.89	54.17	54.44	54.72	55.00	55.28
								1		

SCALE OF VELOCITY EQUIVALENTS OF THE SO-CALLED BEAUFORT SCALE OF WIND.

	Beaufort			I.	imits of ve	locity
Beaufort Number,	description of wind,	Deep Sea Criterion, 1874, International	Specification for use on land	Miles 1	er hour	Meters
Interna- tional	Interna- tional	1874, International	tor use on land	Nautical (knots)	Statute	per sec.
0	Calm		Calm, smoke rises vertically.	Less than 1	Less than 1	Less than 0.4
1	Light air	Just sufficient to give steer- age way. ¹	Direction of wind shown by smoke drift, but not by wind vanes.	1 to 3	1 to 3	0.4 to 1.5
2	Light breeze	That in which a well-conditioned man-of-	leaves rustle; ordi- nary vane moved	4 to 6	4 to 7	1.6 to 3.3
3	Gentle breeze	war, with all sail set, and clean full, would go in smooth water from—	by wind. Leaves and small twigs in constant motion; wind extends light flag.	7 to 10	8 to 12	3.4 to 5.4
4	Moderate breeze	5 to 6 knots	Raises dust and loose paper; small branches are moved.	11 to 16	13 to 18	5.5 to 7.9
5	Fresh breeze	That to which she could just carry in chase, full and by—	Small trees in leaf begin to sway; crested wavelets form on inland waters.	17 to 21	19 to 24	8.0 to 10.7
6	Strong breeze	Top gallant sails.	Large branches in motion; whistling heard in telegraph wires; umbrellas used with difficulty.	22 to 27	25 to 31	10.8 to 13.8
7	Moderate gale	That to which she could just carry in chase, full and by—	Whole trees in mo- tion; inconvenience felt when walking against wind.	28 to 33	32 to 38	13.9 to 17.1
8	Fresh gale	Reefed up- per top- sails and	Breaks twigs off trees; generally impodes progress.	34 to 40	39 to 46	17.2 to 20.7
9	Strong gale	courses Lower top- sails and courses.	Slight structural damage occurs (chimney pots and slate removed).	41 to 47	47 to 54	20.8 to 24.4
10	Whole gale	That with which she could scarcely bear lower maintop- sail and reefed foresail.	Seldom experienced inland; trees up- rooted; considerable structural damage occurs.	48 to 55	55 to 63	24.5 to 28.4
11	Storm	That which would reduce her to storm stay-sails.	Very rarely experi- enced, accompanied by wide-spread damage.	56 to 65	64 to 75	28.5 to 33.5
12	Hurri- cane	That which no canvas could withstand.		Above 65	Above 75	Above 33.5

¹ A full-rigged ship of 1874.

RADIUS OF CRITICAL CURVATURE AND VELOCITIES OF CRADIENT WINDS FOR FRICTIONLESS MOTION IN HIGHS AND LOWS.

ENGLISH MEASURES.

 R_c = radius of critical curvature in miles. V_c High = maximum speed in miles per hour on isobar of critical curvature. V_s = speed along straight line isobars = 0.5 V_c . V Low = speed in Low along isobar of curvature R_c . V Low = 0.4142 V_c .

The table is computed for a density of the air, $\rho = .0010$, which represents the conditions in the free air at an elevation of, roughly, one mile. Values for any other density can be readily found by dividing each or any of the tabulated values by the ratio of the densities, as, for example, for surface conditions divide by $1.2 = \frac{.0010}{.0012}$ and so on.

Lati-						d (m	niles)					
tude:		100	125	150	175	200	250	300	400	500	600	800
10°	R_c V_c High V_s V Low	8160 372 186 154	6530 298 149 123	5440 248 124 103	4660 212 106 88.0	4080 186 93.0 77.0	3260 149 74.4 61.6	2720 124 62.0 51.3	2040 93.0 46.5 38.5	1630 74 · 4 37 · 2 30 · 8	1360 62.0 31.0 25.7	1020 46.5 23.2 19.2
20	R_c V_c High V_s V Low	2100 189 94 · 4 78 · 2	1680 151 75.5 62.5	1400 126 62.9 52.1	1200 108 54.0 44.7	1050 94 · 4 47 · 2 39 · 1	841 75·5 37·8 31·3	701 62.9 31.4 26.1	526 47.2 23.6 19.6	420 37.8 18.9 15.7	350 31.5 15.8 13.0	263 23.6 11.8 9.8
25	R_c V_c High V_s V Low	1380 153 76.4 63.3	1100 122 61.1 50.6	918 102 50.9 42.2	787 87.3 43.6 36.2	688 76.4 38.2 31.6	551 61.1 30.6 25.3	459 50.9 25.4 21.1	344 38.2 19.1 15.8	275 30.6 15.3 12.7	230 25.5 12.8 10.6	172 19.1 9.5 7.9
30	R_c V_c High V_s V Low	984 129 64.5 53.5	787 103 51.6 42.8	656 86. I 43. 0 35. 7	562 73.8 36.9 30.6	49 ² 64.5 32.2 26.7	393 51.6 25.8 21.4	328 43.0 21.5 17 8	246 32.3 16.2 13.4	197 25.8 12.9 10.7	164 21.5 10.8 8.9	123 16.1 8.1 6.7
35	R_c V_c High V_s V Low	747 112 56.3 46.6	598 90.0 45.0 37.3	498 75.0 37.5 31.1	427 64.3 32.2 26.6	374 56.3 28.2 23.3	299 45.0 22.5 18.6	249 37·5 18.8 15.5	187 28. I 14. 0 11. 6	150 22.5 11.2 9.3	125 18.8 9.4 7.8	93·4 14.1 7.0 5.8
40	$R_c \ V_c \ ext{High} \ V_s \ ext{Low}$	595 100 50.2 41.6	476 80.3 40.2 33.3	397 66.9 33.4 27.7	340 57·4 28·7 23.8	298 50. 2 25. I 20. 8	238 40. 2 20. 1 16. 7	198 33·5 16.8 13.9	149 25.1 12.6 10.4	119 20. 1 10. 0 8. 3	99.2 16.7 8.4 6.9	74.4 12.6 6.3 5.2
45	R_c V_c High V_s V Low	492 91.3 45.6 37.8	393 73.0 36.5 30.2	328 60.9 30.4 25.2	281 52.2 26.1 21.6	246 45.6 22.8 18.9	197 36.5 18.2 15.1	164 30.4 15.2 12.6	123 22.8 11.4 9.4	98.4 18.3 9.2 7.6	82.0 15.2 7.6 6.3	61.5 11.4 5.7 4.7
50	R_c V_c High V_s V Low	419 84.3 42.1 34.9	335 67.4 33.7 27.9	279 56.2 28.1 23.3	240 48.2 24. I 20.0	210 42.1 21.0 17.4	168 33·7 16.8 14.0	140 28.1 14.0 11.6	105 21.1 10.6 8.7	83.8 16.9 8.4 7.0	69.9 14.0 7.0 5.8	52.4 10.5 5.3 4.4
55	R_c V_c High V_s V Low	366 78.8 39.4 32.6	293 63.0 31.5 26.1	244 52.5 26.2 21.7	209 45.0 22.5 18.6	183 39·4 19.7 16.3	147 31.5 15.8 13.0	122 26.3 13.2 10.9	91.6 19.7 9.8 8.2	73.3 15.8 7.9 6.5	61.1 13.1 6.6 5.4	45.8 9.8 4.9 4.1
60	R _c V _c High V _s V Low	328 74·5 37·3 30·9	262 59.6 29.8 24.7	219 49.7 24.8 20.6	187 42.6 21.3 17.6	164 37·3 18.6 15.5	131 29.8 14.9 12.3	100 24.8 12.4 10.3	82.0 18.6 9.3 7.7	65.6 14.9 7.4 6.2	54·7 12.4 6.2 5.1	41.0 9.3 4.7 3.9
65	R_c V_c High V_s V Low	299 71.2 35.6 29.5	240 57.0 28.5 23.6	200 47·5 23.8 19·7	171 40.7 20.4 16.0	150 35.6 17.8 14.7	120 28.5 14.2 11.8	99.8 23.7 11.8 9.8	74.8 17.8 8.9 7.4	59.9 14.2 7.1 5.9	49.9 11.9 6.0 4.9	37·4 8.9 4·4 3·7

TABLE 40.

RADIUS OF CRITICAL CURVATURE AND VELOCITIES OF GRADIENT
WINDS FOR FRICTIONLESS MOTION IN HIGHS AND LOWS.

ENGLISH MEASURES.

Lati-						d (mile	s)					
tude:		100	125	150	175	200	250	300	400	500	600	800
70°	R _c V _c High V _s V Low	278 68.7 34.3 28.5	223 55.0 27.5 22.8	186 45.8 22.9 19.0	159 39·3 19.6 16.3	130 34·3 17·2 14·2	111 27.5 13.8 11.4	92.8 22.9 11.4 9.5	60.6 17.2 8.6 7.1	55·7 13.7 6.8 5·7	46.4 11.4 5.7 4.7	34.8 8.6 4.3 3.6
75	$egin{array}{l} R_c \ V_c \ ext{High} \ V_s \ V \ ext{Low} \end{array}$	264 66.8 33.4 27.7	211 53·5 26.8 22.2	176 44.6 22.3 18.5	151 38.2 19.1 15.8	132 33·4 16.7 13.8	105 20.7 13.4 11.1	87.0 22.3 11.2 9.2	65.0 16.7 8.4 6.0	52·7 13·4 6·7 5·6	43.0 11.1 5.6 4.0	33.0 8.4 4.2 3.5
80	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ ext{Low} \end{array}$	254 65.5 32.8 27.1	203 52.4 26.2 21.7	169 43·7 21.8 18.1	145 37·5 18.8 15.5	127 32.8 16.4 13.6	101 20.2 13.1 10.9	84.5 21.8 10.0 9.0	63.4 16.4 8.2 6.8	50.7 13.1 6.6 5.4	10.9 5.4 4.5	31.7 8.2 4.1 3.4
85	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ ext{V} \ ext{Low} \end{array}$	248 64 8 32.4 26.8	198 51.8 25.9 21.5	165 43.2 21.6 17.9	142 37.0 18.5 15.3	124 32.4 16.2 13.4	00. I 25. 0 13. 0 10. 7	82.6 21.6 10.8 8.9	62.0 16.2 8.1 6.7	49.6 13.0 0.5 5.4	41.3 10.8 5.4 4.5	31.0 8.1 4.0 3.4
90	R _c V _c High V _s V Low	246 64.6 32.3 26.8	197 51.6 25.8 21.4	164 43.0 21.5 17.8	30.9	123 32·3 16.2	98.4 25.8 12.9 10.7	82.0 21.5 10.8 8.9	61.5 16.1 8.0 6.7	49.2 12.0 6.4 5.3	41.0 10.8 5.4 4.5	30.7 8.1 4.0 3.3

TABLE 41.

RADIUS OF CRITICAL CURVATURE AND VELOCITIES OF GRADIENT

WINDS FOR FRICTIONLESS MOTION IN HIGHS AND LOWS.

METRIC MEASURES.

 R_c = radius of critical curvature in kilometers. V_c High = maximum speed in meters per second on isobar of critical curvature. V_s = speed along straight line isobars = 0.5 V_c . V Low = speed in Low along isobar of curvature R_c . V Low = 0.4142 V_c .

The remarks in heading of Table 40 relative to the density of the air apply equally to Table 41.

Lati-					d (1	kilomete	ers)					
tude:		100	125	150	175	200	250	300	400	500	600	800
10°	V_c High V_s V Low R_c V_c High V_s	8330 105 52·7 43·5 2140 53·5 26.7	6660 84.3 42.2 34.9 1710 42.8 21.4	5550 70.2 35.1 29.1 1430 35.6 17.8	4760 60.2 30.1 24.9 1220 30.5 15.2	4160 52.7 26.4 21.8 1070 26.7 13.4	3330 42.1 21.0 17.4 857 21.4 10.7	2780 35.1 17.6 14.5 714 17.8 8.9	2080 26.3 13.2 10.0 536 13.4 6.7	1670 21.1 10 6 8.7 429 10.7 5.4	1390 17.6 8.8 7·3 357 8.9 4·4	1040 13.2 6.6 5.5 268 6.7 3.4
25	V Low R_c V_c High V_s Low	22. 2 .1400 43. 3 21. 6 17. 9	17.7 1120 34.6 17.3 14.3	936 28.8 14.4 11.9	802 24.7 12.4 10.2	702 21.6 10.8 8.9	562 17.3 8.6 7.2	7·4 468 14·4 7·2 6.0	5.6 351 10.8 5.4 4.5	281 8.7 4.4 3.6	3·7 234 7·2 3.6 3.0	2.8 175 5.4 2.7 2.2
30	R _c V _c High V _s V Low	1003 36.6 18.3 15.2	802 29.3 14.6 12.1	669 24.4 12.2 10.1	573 20.9 10.4 8.7	501 18.3 9.2 7.6	401 14.6 7.3 6.0	334 12.2 6.1 5.1	251 9.1 4.6 3.8	7·3 3.6 3.0	167 6. 1 3.0 2.5	125 4.6 2.3 1.9

TABLE 41.

RADIUS OF CRITICAL CURVATURE AND VELOCITIES OF GRADIENT WINDS FOR FRICTIONLESS MOTION IN HIGHS AND LOWS.

METRIC MEASURES.

	Ī				d (kilomet	ers)					
Lati- tude:		4.00	400	450	<u> </u>				1			
-		100	125	150	175	200	250	300	400	500	600	800
35°	V _s V Low	762 31.9 15.9 13.2	610 25.5 12.8 10.6	508 21.3 10.6 8.8	435 18.2 9.1 7.5	381 15.9 8.e 6.6	305 12.8 6.4 5.3	254 10.6 5·3 4·4	8.0 4.0 3.3	152 6.4 3.2 2.7	5·3 2.6 2.2	95·3 4·0 2.0 1.7
40	V_c High V_s Low	607 28.4 14.2 11.8	485 22.8 11.4 9.4	405 19.0 9.5 7.9	347 16.3 8.2 6.8	303 14.2 7.1 5.9	243 11.4 5·7 4·7	202 9·5 4.8 3·9	152 7. I 3. 6 2. 9	5.7 2.8 2.4	101 4·7 2·4 1.9	75.8 3.6 1.8
45	$egin{array}{c} R_c \ V_c \ ext{High} \ V_s \ ext{Low} \end{array}$	50I 25.9 I2.9 I0.7	40I 20.7 I0.4 8.6	334 17.2 8.6 7.1	287 14.8 7.4 6.1	251 12.9 6.4 5.3	201 10.3 5.2 4.3	167 8.6 4.3 3.6	125 6.5 3.2 2.7	100 5.2 2.6 2.2	83.6 4.3 2.2 1.8	62.7 3.2 1.6 1.3
50	R_c V_c High V_s V Low	427 23.9 11.9 9.9	342 19. 1 9. 6 7. 9	285 15.9 8.0 6.6	244 13.6 6.8 5.6	214 11.9 6.0 4.9	9·5 4.8 3·9	142 8.0 4.0 3.3	107 6.0 3.0 2.5	85.5 4.8 2.4 2.0	71.2 4.0 2.0 1.7	53·4 3.0 1.5 1.2
55	R_c V_c High V_s V Low	374 22.3 11.2 9.2	299 17.9 9.0 7.4	249 14.9 7.4 6.2	213 12.8 6.4 5·3	187 11.2 5.6 4.6	149 8.9 4.4 3.7	125 7·4 3·7 3.1	93.4 5.6 2.8 2.3	74·7 4·5 2.2 1.9	62.3 3.7 1.8 1.5	46.7 2.8 1.4 1.2
60	$ \begin{array}{c} R_c \\ V_c \\ V_s \\ V \\ Low \end{array} $	334 21.1 10.6 8.7	267 16.9 8.4 7.0	223 14. I 7. 0 5. 8	191 12.1 6.0 5.0	167 10.6 5.3 4.4	134 8.4 4.2 3.5	7.0 3.5 2.9	83.6 5.3 2.6 2.2	66.9 4.2 2.1 1.7	55·7 3·5 1.8 1.4	41.8 2.6 1.3 1.1
65	$egin{array}{l} R_c \ V_c \ ext{High} \ V_s \ ext{Low} \end{array}$	305 20, 2 10, 1 8, 4	244 16. 1 8. 0 6. 7	20.4 13.4 6.7 5.6	174 11.5 5.8 4.8	153 10. 1 5. 0 4. 2	122 8. I 4. O 3. 4	102 6.7 3.4 2.8	76.3 5.0 2.5 2.1	61.0 4.0 2.0 1.7	50.9 3.4 1.7 1.4	38. 2 2. 5 1. 2 1. 0
70	R_c V_c High V_s V Low	284 19.5 9.7 8.1	227 15.6 7.8 6.5	189 13.0 6.5 5.4	162 11.1 5.6 4.6	142 9·7 4.8 4·0	7.8 3.9 3.2	94.6 · 6.5 3.2 2.7	71.0 4.9 2.4 2.0	56.8 3.9 2.0 1.6	47·3 3·2 1.6 1.3	35·5 2·4 I.2 I.0
75	R_c V_c High V_s V Low	269 18.9 9.5 7.8	215 15.1 7.6 6.3	179 12.6 6.3 5.2	154 10.8 5.4 4.5	134 9·5 4.8 3·9	107 7.6 3.8 3.1	89.6 6.3 3.2 2.6	67.2 4.7 2.4 1.9	53·7 3.8 1.9 1.6	44.8 3.2 1.6 1.3	33.6 2.4 1.2 1.0
80	R_c V_c High V_s V Low	259 18.6 9.3 7.7	207 14.9 7.4 6.2	172 12.4 6.2 5.1	148 10.6 5 3 4·4	129 9.3 4.6 3.9	103 7 · 4 3 · 7 3 · 1	86. 2 6. 2 3. I 2. 6	64.6 4.6 2.3 1.9	51.7 3.7 1.8 1.5	43. I 3. I 1. 6 I. 3	32·3 2·3 I.2 I.0
85	R_c V_c High V_s V Low	253 18.4 9.2 7.6	202 14.7 7.4 6.1	168 12.2 6.1 5.1	144 10.5 5.2 4.3	126 9.2 4.6 3.8	101 7·3 3.6 3.0	84. 2 6. I 3. 0 2. 5	63.2 4.6 2.3 1.9	50. 5 3. 7 1. 8	42. I 3. I 1. 6 I. 3	31.6 2.3 1.2 1.0
90	R_c V_c High V_s V Low	251 18.3 9.1 7.6	201 14.6 7.3 6.0	167 12.2 6.1 5.1	143 10.4 5.2 4.3	9. I 4. 6 3. 8	7·3 3.6 3.0	83.6 6.1 3.0 2.5	62.7 4.6 2.3 1.9	50. I 3.7 I.8 I.5	41.8 3.0 1.5 1.2	31.3 2.3 1.2 1.0



REDUCTION OF TEMPERATURE TO SEA LEVEL.

English measures	٠	٠	٠	٠	•	•	4	٠	٥	٠	•	۰	٠	٠	٠	٠	TABLE 42
Metric measures								٠	•	•		٠				•	TABLE 43

REDUCTION OF TEMPERATURE TO SEA LEVEL.

ENGLISH MEASURES.

Rate of decrease of temper-		DIF	FERE	NCES	BETW		THE D AT				AT AN	Y ALTI	TUDE			
ature.						A	LTITU	E IN	FEET.							
for every	100	200	300	400	500	600	700	800	900	100 0	2000	3000	4000	5000		
Feet.	F.	F.	F.	F.	F.	F.	F.	F.	F.	F.	F.	F. 15.00	F.	F.		
200	0.50	1,00	1.50	2,00	2°50	3.°00	3°50	4.00	4°50	5°.00 4.88	9.76	14.63	20,00	25.00		
205 210	0.49	0.98	1.46	I.95 I.90	2.44	2.93 2.86	3.41	3.90 3.81	4.39 4.29	4.76	9.70	14.03	19.51	24.39 23.81		
215	0.47	0.93	I.43 I.40	1.86	2.33	2.79	3.26	3.72	4.19	4.65	9.30	13.95	18.60	23.26		
220	0.45	0.93	1.36	1.82	2.27	2.73	3.18	3.64	4.09		9.09	13.63	18.18	22.72		
220	0.43	0.91	1.30	1.02	2.27	2.73	3.20	3,04	4.09	4.33		13.03	10,10	22.72		
230	0.43	0.87	1.30	1.74	2.17	2.61	3.04	3.48	3.91	4-35	8.70	13.04	17.39	21.74		
240	0.42	0.83	1.25	1.67	2.08	2.50	2.92	3.33	3.75	4	8.33	12.50	16.67	20.83		
250	0.40	0.80	1.20	1.60	2.00	2.40	2.80	3.20	3.60	4.00	8.00	12.00		20.00		
260	0.38	38 0.77 1.15 1.54 1.92 2.31 2.69 3.08 3.46 3.85 7.69 11.54 15.38 19.23														
270	0.37															
280	0.36	0.71	1.07	1.43	1.79	2.14	2.50	2.86	3.21	3.57	7.14	10.71	14.29	17.86		
290	0.34	0.69	1.03	1.38	1.73	2.07	2.41	2.76	3.10	3.45	6.90	10.34	13.79	17.24		
300	0.33	0.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	6.67	10.00	13.33	16.67		
310	0.32	0.65	0.97	1.29	1.61	1.94	2.26	2.58	2.90	3.23	6.45	9.68	12.90	16.13		
320	0.31	0.62	0.94	1.25	1.56	1.87	2.19	2.50	2.81	3.12	6.25	9.37	12.50	15.62		
340	0.29	0.59	0.88	1.18	1.47	1.76	2.06	2.35	2.65	2.94	5.88	8.82	11.76	14.71		
360	0.28	0.56	0.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	5.56	8.33	11.11	13.89		
380	0.26	0.53	0.79	1.05	1.32	1.58	1.84	2.10	2.37	2.63	5.26	7.89	10.53	13.16		
400	0, 25	0.50	0.75	1.00	1.25	1.50	1.75	2.00	2.25	2.50	5.00	7.50	10.00	12.50		
420	0.24	0.48	0.71	0.95	1.19	1.43	1.67	1.90	2.14	2.38	4.76	7.14	9.52	11.90		
140						6		- 0-			,	(0-				
440	0.23	0.45	0.68	0.91	1.14	1.36	1.59	1.82	2.05	2.27	4.55	6.82	9.09	11.36		
460	0.22	0.43	0.65	0.87	1.09	1.30	1.52	1.74	1.96	2.17	4.35	6.52	8.70	10.87		
480	0.21	0.42	0.62	0.83	1.04	1.25	1.46	1.67	1.87	2.08	4.17	6.25	8.33	10.42		
500	0.20	0.40	0.60	0.80	1.00	1.20	1.40	1.60	1.80	2,00	3.85	6.00	8.00	10.00		
520	0.19	0.38	0.58	0.77	0.96	1.15	1.35	1.54	1.73	1.92	3.03	5.77	7.69	9.62		
540	0.19	0.37	0.56	0.74	0.93	1.11	1.30	1.48	1.67	1.85	3.70	5.56	7.41	9.26		
560	0.18	0.36	0.54	0.71	0.89	1.07	1.25	1.43	1.61	1.79	3.57	5.36	7.14	8.93		
580	0.17	0.34	0.52	0.69	0.86	1.03	1.21	1.38	1.55	1.72	3.45	5.17	6.90	8.62		
600	0.17	0.33	0.50	0.67	0.83	1.00	1.17	1.33	1.50	1.67	3.33	5.00	6.67	8.33		
620	0.16	0.32	0.48	0.65	0.81	0.97	1.13	1.29	1.45	1.61	3.23	4.84	6.45	8.06		
650	0.15	0.31	0.46	0.62	0.77	0.92	1.08	1.23	1.38	1.54	3.08	4.62	6.15	7.69		
700	0.14	0.29	0.43	0.57	0.71	0.86	1.00	1.14	1.29	1.43	2.86	4.29	5.71	7.14		
750	0.13	0.27	0.40	0.53	0.67	0.80	0.93	1.07	1.20	1.33	2.67	4.00	5.33	6.67		
800	0.12	0.25	0.37	0.50	0.62	0.75	0.87	1.00	1.12	1.25	2.50	3.75	5.00	6.25		
850	0.12	0.24	0.35	0.47	0.59	0.71	0.82	0.94	1.06	1.18	2.35	3.53	4.71	5.88		
900	0.11	0.22	0.33	0.44	0.56	0.67	0.78	0.89	1.00	1.11	2.22	3.33	4.44	5.56		
	1	1	1.33		3.33		1 7			1	1	3.33	7.44	0.00		

Tabular values are to be added to the observed temperature to obtain the temperature at sea level.

REDUCTION OF TEMPERATURE TO SEA LEVEL.

METRIC MEASURES.

Rate of decrease of		DIFFE	ERENCI	S BET		THE T			AT AN	IY ALT	ITUDE	
temper- ature. 1°C.					A	LTITUDE	IN METER	RS.				
for every	100	200	300	400	500	600	700	800	900	1000	2000	3000
m. 100	C. 1.00	C. 2°,00	C.	C. 4.00	c. 5°00	c. 6.00	C. 7.00	c. 8°00	C.	C.	c. 20,00	c. 30.00
102	0.98	1.96	2.94	3.92	4.90	5.88	6.86	7.84	8.82	9.80	19.61	29.41
104	0.96	1.92	2.88	3.85	4.81	5.77	6.73	7.69	8.65	9.62	19.23	28.85
106	0.94	1.89	2.83	3.77	4.72	5.66	6.60	7.55	8.49	9.43	18.87	28.30
108	0.93	1.85	2.78	3.70	4.63	5.56	6.48	7.41	8.33	9.26	18.52	27.78
110	0.91	1.82	2.73	3.64	4.55	5-45	6.36	7.27	8.18	9.09	18.18	27.27
115	0.87	1.74	2.61	3.48	4.35	5.22	6.09	6.96	7.83	8.70	17.39	26.09
120	0.83	1.67	2.50	3.33	4.17	5.00	5.83	6.67	7.50	8.33	16.67	25.00
125	0.80	1.60	2.40	3.20	4.00	4.80	5.60	6.40	7.20	8.00	16.00	24.00
130	0.77	1.54	2.31	3.08	3.85	4.62	5.38	6.15	6.92	7.69	15.38	23.08
135	0.74	1.48	2,22	2.96	3.70	4.44	5.19	5.93	6.66	7.41	14.81	22.22
140	0.71	1.43	2.14	2.86	3.57	4.29	5.00	5.71	6.43	7.14	14.29	21.43
145	0.69	1.38	2.07	2.76	3.45	4.14	4.83	5.52	6.21	6,90	13.79	20.69
150	0.67	1.33	2.00	2.67	3.33	4.00	4.67	5.33	6.00	6.67	13.33	20.00
155	0.65	1.29	1.94	2.58	3.23	3.87	4.52	5.16	5.81	6.45	12.90	19.35
160	0.62	1.25	1.87	2.50	3.12	3-75	4.37	5.00	5.62	6.25	12.50	18.75
170	0.59	1.18	1.76	2.35	2.94	3.53	4.12	4.70	5.29	5.88	11.76	17.65
180	0.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.56	11.11	16.67
190	0.53	1.05	1.58	2.10	2.63	3.16	3.68	4.21	4.74	5.26	10.53	15.79
200	0.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	10,00	15.00
210	0.48	0.95	1.43	1.90	2.38	2.86	3.33	3.81	4.29	4.76	9.52	14.29
220	0.45	0.91	1.36	1.82	2.27	2.73	3.18	3.64	4.09	4.55	9.09	13.64
230	0.43	0.87	1.30	1.74	2.17	2.61	3.04	3.48	3.91	4.35	8.70	13.04
240	0.42	0.83	1.25	1.67	2.08	2.50	2.92	3.33	3.75	4.17	8.33	12.50
250	0,40	0.80	1.20	1.60	2,00	2.40	2.80	3.20	3.60	4.00	8.00	12.00
260	0.38	0.77	1.15	1.54	1.92	2.31	2.69	3.08	3.46	3.85	7.69	11.54
270	0.37	0.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	7.41	II.II
280	0.36	0.71	1.07	1.43	1.79	2.14	2.50	2.86	3.21	3.57	7.14	10.71
290	0.34	0.69	1.03	1.38	1.72	2.07	2.41	2.76	3.10	3.45	6.90	10.34
300	0.33	0.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	6.67	10.00
320	0.31	0.62	0.94	1.25	1.56	1.87	2.19	2.50	2.81	3.12	6.25	9.37
340	0.29	0.59	0.88	1.18	1.47	1.76	2.06	2.35	2.65	2.94	5.88	8.82
360	0.28	0.56	0.83	1.11	1.39	1.67	1.94	2,22	2.50	2.78	5.56	8.33
38o	0.26	0.53	0.79	1.05	1.32	1.58	1.84	2.10	2.37	2.63	5.26	7.89
400	0.25	0.50	0.75	1.00	1.25	1.50	1.75	2.00	2.25	2.50	5.00	7.50
420	0.24	0.48	0.71	0.95	1.19	1.43	1.67	1.90	2.14	2.38	4.76	7.14
440	0.23	0.45	0.68	0.91	1.14	1.36	1.59	1.82	2.05	2.27	4-55	6.82
460	0.22	0.43	0,65	0.87	1.09	1.30	1.52	1.74	1.96	2.17	4.35	6.52
480	0.21	0.42	0.62	0.83	1.04	1.25	1.46	1.67	1.87	2.08	4.17	6.25
500	0.20	0.40	0.60	o.So	1.00	1.20	1.40	1.60	1.80	2.00	4.00	6,00
·	77.1.1		1	to bo	-11-1	1	1	1 4	rnomati		-1-4-1	

Tabular values are to be added to the observed temperature to obtain the temperature at sea level.



REDUCTION OF BAROMETER READINGS TO STANDARD UNITS

Reduction of the barometer to standard temperature—	
English measures	TABLE 44
Metric measures	TABLE 45
Reduction of the mercurial column to standard temperature. (For U-shaped manometers with brass scales.)	
English measures	TABLE 46
Metric measures	TABLE 47
Reduction of the mercurial barometer to standard gravity.	
Direct reduction from local to standard gravity	Table 48
Reduction through variation with latitude—	
English measures	Table 49
Metric measures	

TABLE 44.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

ENGLISH MEASURES.

	Attached	HEIGHT OF THE BAROMETER IN INCHES.										
	Ther- mometer		1	HEIG	HT OF	THE BA	ROMETE	R IN II	NCHES.	1		
	Fahren- heit.	19.0	19.5	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	
l	F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	
	0°0		+0.051			+0.055				+0.060		
ĺ	+ 0.5	+0.049 .048	+0.050	+0.051	+0.053	+0.054	+0.055	+0.056	+0.058	+0.059	+0.060	
	1.5	.047	.048	.049	.051	.052	.053	.054	.056	.057	.058	
	2.0	.046 .045	.047	.049	.050	.050	.052	.053	.055	.056	.057	
		+0.044			1 .		+0.050			+0.054		
ł	3.5 4.0	.043	.045	.046	.047	.048	.049	.050	.051	.053	.054	
Ì	4.5	.042	.043	.044	.045	.046	.047	.048	.049	.051	.052	
I	5.0	.041	.042	.043	.044	.045	.046	.047	.048	.049	.051	
	5.5 6.0	+0.040	+0.041	+0.042	+0.043	+0.044	+0.045 .044	+0.046	+0.047 .046	+0.048	+0.049 .048	
ľ	6.5	.038	.039	.040	.041	.042	.043	.0.14	.045	.046	.047	
١	7.0	.037	.038	.039	.040	.041	.042	.043	.044	.045	.046	
	7.5	.037	.038	.038	.039	.040	.041	.042	.043	.044	.045	
ı	8.0 8.5	+0.036	+0.037		+0.038	+0.039	+0.040	+0.041	+0.042	+0.043	+0.044 .043	
ı	9.0	.034	.035	.037	.037	.038	.039	.039	.040	.042	.043	
	9.5	.033	.034	.035	.036	.037	.037	.038	.039	.040	.041	
Į	10.0	.032	.033	.034	.035	.036	.036	.037	.038	.039	.oto	
١	10.5		+0.032				+0.035			+0.038		
	11.0	.030	.031	.032	.033	.034	.034	.035	.036	.037	.038	
Į	11.5	.030	.030	.031	.032	.033	.034	.034	.035	.036	.037	
ĺ	12.5	.028	.029	.029	.030	.031	.032	.032	.033	.034	.034	
		+0.027		+0.028	+0.029				+0.032		+0.033	
ı	13.5	.026	.027	.028	.028	.029	.030	.030	.031	.032	.032	
ı	14.0	.025	.026	.027	.027	.028	.029	.029	.030	.031	.031	
	15.0	.024	.024	.025	.025	.026	.027	.027	.028	.029	.029	
ı	15.5	+0.023			+0.024			+0.026		+0.027	+0.028	
	16.0	.022	.023	.023	.024	.024	.025	.025	.026	.026	.027	
ı	16.5 17.0	.021	.022	.022 .02I	.023	.023	.024	.024	.025	.025	.026	
	17.5	.019	.020	.020	.021	.021	.022	.022	.023	.023	.024	
ı		+0.018	+0.019		+0.020	+0.020	+0.021	+0.021	+0.022	+0.022	+0.023	
ı	18.5	.017	.018	.018	.019	.019	.020	.020	.021	.021	.022	
İ	19.0	.017	.017	.018	.018	.018	.019	.019	.020	.020	.02I	
ı	20.0	.015	.015	.016	.016	.016	.017	.017	.019	.019	.018	
		+0.014	+0.014			+0.016	+0.016					
	21.0	.013	.014	.014	.014	.015	.015	.015	.016	.016	.016	
	22.0	.012	.013	.013	.013	.014	.013	.014	.015	.015	.015	
	22.5	.011	.011	.011	.011	.012	.012	.012	.013	.013	.013	
	23.0	+0.010	+0.010	+0.010	+0.010	+0.011	+0.011	+0.011	+0.012	+0.012	+0.012	
	23.5	.009	.009	.009	.009	.010	.010	.010	.010	.010	.010	
	24.5	.007	.007	.008	.008	.008	.008	.008	.009	.009	.009	
	25.0	,006	.006	.007	.007	.007	.007	.007	.00Ś	.00Š	.008	
			1			1			1	1		

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

Attached Ther-	HEIGHT OF THE BAROMETER IN INCHES.									
mometer Fahren- heit.	19.0	19.5	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
25°5	+0.005	+0.006	+0.006	+0.006	-1-0.006	+0.006	+0.006	+0.006	+0.007	+0.007
26.0	.005	.005	.005	.005	.005	.005	.005	,005	.005	.006
26.5	.004	.004	.004	.004	.004	.004	.004	.004	.004	.005
27.0	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003
27.5	.002	.002	.002	.002	.002	.002	.002	.002	.002	,002
28.0	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001
28.5	0.000	0.000	0,000	0,000	0,000	0.000	0,000	0,000	0,000	0,000
29.0	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001
29.5	.002	.002	.002	.002	.002	.002	,002	.002	.002	.002
30.0	,002	.002	.002	.003	.003	.003	.003	.003	.003	.003
30.5	-0.003	-0.003	-0.003	-0.003	-0.004	-0.004	-0.004	-0.004	-0.004	-0.004
31.0	.004	.004	,004	.004	.005	.005	.005	.005	,005	,005
31.5	.005	.005	.005	.005	.005	.006	.006	.006	,006	.006
32.0 32.5	.006	.006	.006	.006	.006	.007	.007	.007	.007	.007
32.3	.007	.007	.007	.007	.007	.000	.000	.000	.000	,000
33.0	-0.008	-0.008	-0.008	-0.008	-0.008	-0.009	-0.009	-0.009	-0.009	-0.009
33.5	.008	.009	.009	.009	.009	.010	.010	.010	.010	.010
34.0	.009	.010	.010	.010	.010	.010	.011	.011	.011	110.
34.5	.010	.010	.011	.011	110.	.011	.012	.012	.012	.013
35.0	.011	.011	.012	.012	.012	.012	.013	.013	.013	.014
35.5	-0.012	-0.012	-0.012	-0.013	-0.013	-0.013	-0,014	-0.014	-0.014	-0.015
36.0	.013	.013	.013	.014	.014	.014	.015	.015	.015	.016
36.5	.014	.014	.014	.015	.015	.015	.016	.016	.016	.017
37.0	.014	.015	.015	.016	.016	.016	.017	.017	.017	.018
37.5	.015	.016	.016	.017	.017	.017	.018	.018	.019	.019
38.0	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.019	-0.019	-0.020	-0.020
38.5	.017	.017	.018	.018	.019	.019	.020	.020	.02 I	.021
39.0	.018	.018	.019	.019	.020	.020	.021,	.021	.022	.022
39.5	.019	.019	.020	,020	.021	.021	.022	.022	.023	.023
40.0	.020	.020	.021	.021	.022	,022	.023	.023	.024	.024
40.5	-0.020	-0.021	-0.022	-0.022	-0.023	-0.023	-0.024	-0.024	-0.025	-0.025
41.0	.021	.022	.022	.023	.024	.024	.025	.025	.026	.026
41.5	.022	.023	.023	.024	.025	.025	.026	.026	.027	.027
42.0	.023	.024	.024	.025	.025	.026	.027	.027	.028	.029
42.5	.024	.025	.025	.026	.026	.027	.028	.028	.029	.030
43.0	-0.025	-0.025	-0.026	-0.027	-0.027	-0.028	-0,029	-0.029	-0.030	-0.031
43.5	.026	.026	.027	.028	.028	.029	.030	.030	.031	.032
44.0	.026	.027	.028	.029	.029	.030	.031	.031	.032	.033
44.5	.027	.028	.029	.030	.030	.031	.032	.032	.033	.034
45.0	.028	.029	.030	.030	.031	.032	.033	.033	.034	.035
45.5	-0.029	-0.030	-0.031	-0.031	-0.032	-0.033	-0.034	-0.034	-0.035	-0.036
46.0	.030	.031	.031	.032	.033	.034	.035	.035	.036	.037
46.5	.031	.032	.032	.033	.034	.035	.036	.036	.037	.038
47.0	.032	.032	.033	.034	.035	.036	.037	.037	.038	.039
47.5	.033	.033	.034	.035	.036	.037	.038	.038	.039	,040
48.0	-0.033	-0.034	-0.035	-0.036	-0.037	-0.038	-0.039	-0.040	-0.040	-0.041
48.5	.034	.035	.036	.037	.038	.039	.040	.041	.041	.042
49.0	.035	.036	.037	.038	.039	.040	.0.11	.042	.042	.043
49.5	.036	.037	.038	.039	.040	.041	.042	.043	.044	.044
50.0	.037	.038	.039	.040	.041	.042	.043	.044	0.45	.046
L	·									

TABLE 44.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

ENGLISH MEASURES.

Attached Ther- mometer	HEIGHT OF THE BAROMETER IN INCHES.										
Fahren- heit.	19.0	19.5	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5	
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch	Inch.	
50°5	-0.038		-0.040		-0.042	-0.043	-0.044	-0.045	-0.046		
51.0	.039	.040	.041	.042	.043	.044	.045	.046	0.47	.048	
51.5	.039	.040	.041	.042	.044	.045	.046	.047	.048	.049	
52.0	.040	.041	.042	.043	.044	.046	.047	.048	.049	.050	
52.5	.041	.042	.043	.044	.045	.047		.049	.050	.051	
53.0			-0.044	-0.045	-0.046	-0.047	-0.049	-0.050	-0.051	-0.052	
53.5	.043	.044	.045	.046	.047	.048	.050	.051	.052	.053	
54.0	.044	.045	.046	.047	.048	.049	.051	.052	.053	.054	
54·5 55.0	.045	.046	.047 .048	.048	.049	.050	.052	.053	.054	.055 .056	
						_					
55.5 - 56.0	-0.046	-0.047	-0.049	-0.050	-0.051	-0.052	-0.054	-0.055	-0.056	-0.057	
56.5	.047	.048	.050	.051	.052	.053	.055	.056	.057	.058	
57.0	.048	.049	.050	.052	.053	.054	.056	.057	.058	.059	
57.5	.049	.050 .051	.051	.053	.054	.055	.058	.058	.059	.061	
	.030	.001	.032	.034	.000	.000	.030	•~39	.000	.001	
58.0	-0.051	-0.052	-0.053	-0.055	-0.056	-0.057	-0.059	-0.060	-0.061	-0.063	
58.5	.051	.053	.054	.055	.057	.058	.060	.061	.062	.064	
59.0	.052	.054	.055	.056	.058	.059	.061	.062	.063	.065	
59·5 60.0	.053	.055	.056	.057	.059	.060	.061	.063 .064	.064	.066	
00.0	.054	.055	.057	.058	.060	.001	.002	.004	.005	.007	
60.5	-0.055	-0.056	-0.058	-0.059	-0.061	-0.062	-0.063	-0.065	-0.066	-0.068	
61.0	.056	.057	.059	.060	.062	.063	.064	.066	.067	.069	
61.5	.057	.058	.060	.061	.062	.064	.065	.067	.068	.070	
62.0	.057	.059	.060	.062	.063	.065	.066	.068	.069	.071	
62.5	.058	.060	.061	.063	.064	.066	.067	.069	.071	.072	
63.0	-0.059	-0.061	-0.062	-0.064	-0.065	-0.067	-0.068	-0.070	-0.072	-0.073	
63.5	.060	.062	.063	.065	.066	0.68	.069	.071	.073	.074	
64.0	.061	.062	.064	.066	.067	.069	.070	.072	.074	.075	
64.5 65.0	.062	.063	.065	.067	.068	.070	.071	.073	.075	.076	
05.0	.063	.064	.066	.067	.069	.071	.072	.074	.076	.077	
65.5	-0.063	-0.065	-0.067	-0.068	-0.070	-0.072	-0.073	-0.075	-0.077	-0.078	
66.0	.064	.066	.068	.069	.071	.073	.074	.076	.078	.079	
66.5	.065	.067	.069	.070	.072	.074	.075	.077	.079	.081	
67.0	.066	.068	.069	.071	.073	.075	.076	.078	.080	.082	
67.5	.067	.069	.070	.072	.074	.076	.077	.079	.081	.083	
68.0	-0.068	-0,069	-0.071	-0.073	-0.075	-0.077	-0.078	-0.080	-0.082	-0.084	
68.5	.069	.070	.072	.074	.076	.078	.079	.081	.083	.085	
69.0 69.5	.069	.07 I	.073	.075	.077	.079	.080	.082	.084	.086	
70.0	.070	.072	.074	.076	.078	.079	.081	.083	.085	.087 .088	
	.071	.073	.075	.077	.079	.080	.082	.084	.086	.000	
70.5	-0.072	-0.074	-0.076	-0.078							
71.0	.073	.075	.077	.079	,080	.082	.084	.086	.088	.090	
71.5 72.0	.074	.076	.078	.079	.081	.083	.085	.087	.089	.091	
72.5	.075	.076	.078	.080	.082	.084	.086 .087	.088	.090	.092	
									.091		
73.0	-0.076	-0.078	-0.080	-0.082	-0.084	-0.086	-0.088	-0.090	-0.092	-0.094	
73.5 74.0	.077	.079	.081	.083	.085	.087	.089	.091	.093	.095	
74.5	.078	.080	.082	.084	.086	.088	.090	.092	.094	.096	
75.0	.079 .080	.081	.083	.085	.087 .088	.089	.091	.093	.095 .096	.097	
	.000	.002	.004	,000	.000	.090	.092	.094	.090	.099	

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

Attached Ther- mometer	HEIGHT OF THE BAROMETER IN INCHES.									
Fahren- heit.	19.0	19.5	20.0	20.5	21.0	21.5	22.0	22.5	23.0	23.5
F.	Inch.	Inch.	Inch	Inch.	Inch.	Inch.	Inch.		Inch.	Inch.
75°.5	-o.oSı			-0.087		-0.091	-0.093		-0.097	-0.100
76.0	.081	.084	.086	.088	.090	.092	.094	.096	.098	.101
76.5	.082	.084	.087 .087	.089	.091	.093	.095	.097	.100	.102
77.0	.083	.086	.088	.090	.092	.094	.096	.098	.101	.103
77.5	· ·				.093	.095	.097			
78.0	-0.085	-0.087	-0.089	-0.091	-0.094	-0.096	-0.098	-0.100		-0.105
78.5	.086	.088	.090	.092	.095	.097	.099	.101	.104	.106
79.0	.086	.089	.091	.093	.096	.098	.100	.102	.105	.107
79.5	.087	.090	.092	.094	.097	.099	.101	.103	.106	.108
80,0	.088	.091	.093	.095	.097	.100	. 102	.104	. 107	.109
80.5	-0.089	-0.091	-0.094	-0.096			-0.103		-0.108	
81.0	.090	.092	.095	.097	.099	,102	.104	.106	.109	.111
81.5	.091	.093	.096	.098	.100	.103	.105	.107	.110	.112
82.0	.092	.094	.096	.099	.101	.104	.106	.108	.111	.113
S2.5	.092	.095	.097	.100	.102	.105	.107	. 109	.112	.114
83.0	-0.093	-0.096	-0.098	-0.101	-0.103	-0.106	-0.108	-0.111	-0.113	-0.115
83.5	.094	.097	.099	. 102	.104	.107	.109	.112	.114	.117
84.0	.095	.098	.100	. 103	. 105	.108	.110	.113	.115	811.
84.5	.096	.098	.101	.103	.106	. 108	.111	.114	.116	.119
85.0	.097	.099	.102	. 104	. 107	.109	.112	.115	.117	.120
85.5	-0.09S	-0.100	-0.103	-0.105	-0.108	-0.110	-0.113	-0.116	-0.118	-0.121
86.0	.098	,101	.104	.106	.109	.111	.114	.117	.119	.122
86.5	.099	.102	.105	.107	.110	,112	.115	.118	.120	.123
87.0	.100	.103	. 105	.108	.111	.113	.116	.119	.121	.124
87.5	.101	. 104	.106	, 109	.112	.114	.117	. I 20	.122	.125
88.0	-0. IO2	-0.105	-0.107	-0.110	-0.113	-0.115	-0.118	-0.121	-0.123	-0.126
88.5	. 103	. 105	.108	.111	.114	.116	.119	.122	. 124	. 127
89.0	.104	.106	.109	.112	.114	.117	.120	.123	.125	.128
89.5	. 104	.107	.110	.113	.115	.118	.121	.124	.126	.129
90.0	. 105	. 108	.111	.114	.116	.119	.122	.125	.127	.130
90.5	-0.106	-0.109	-0.112	-0.114	- 0.117	-0.120	-0.123	-0.126	-0.128	-0.131
91.0	.107	.110	.113	.115	.118	.121	.124	.127	.129	.132
91.5	.108	.111	.113	.116	.119	.122	.125	.128	.131	.133
92.0	.109	.112	.114	.117	.120	.123	.126	.129	.132	.134
92.5	.110	.112	.115	.118	.121	. 1 2.4	.127	.130	.133	.135
93.0	-0.110	-0.113	-0.116	-0.119	-0.122	-O.125	-0.128	-0.131	-0.134	-0.137
93.5	.111	.114	.117	.120	.123	.120	.129	.132	.135	. 138
94.0	.112	.115	.118	.121	.124	.127	.130	.133	.136	.139
94.5	.113	.116	.119	.122	.125	.128	.131		.137	.140
95.0	.114	.117	.120	.123	. 126	.129	.132	.135	.138	.141
95.5	-0.115	-0.118	-0.121	-0.124	-o.127	-0.130	-0.133	-0.136	-0.139	-0.142
96.0	.115	.119	.122	.125	.128	.131	.134	.137	.140	.143
96.5	.116		.122	.126	.129	.132	.135	.138	. 141	.144
97.0	.117		.123	.126	.130	.133	.136	.139	.142	.145
97.5	.118	.121	.124	.127	.130	.134	.137	.140	.143	.146
98.0	-0.119	-O.I22		-0.128	-0.131		-0.138		-0.144	
98.5	.120	.123	.126	. 129	.132	. 135	.139	.142	.145	.148
99.0	.121	.124	.127	.130	.133	.136	.140	.143	.146	.149
99.5	.121	.125	.128	.131	.134	.137	.141	.144	.147	.150
100.0	.122	.126	.129	.132	.135	.138	.142	.145	.148	.151

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

	. ENGLISH WEASURES.										
Attached Ther- mometer	HEIGHT OF THE BAROMETER IN INCHES.										
Fahren- heit.	24.0	24.2	24.4	24.6	24.8	25.0	25.2	25.4	25.6	25.8	
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	
0.0	+0.063	+0.063	+0.064	+0.064	+0.065	+0.065	+0.066	+0.066	+0.067	+0.067	
+0.5	+0.061	+0.062				+0.064		+0.065		+0.066	
1.0	.060	.061		.062	.062	.063	.063	.064		.065	
1.5	.059	.060	.060	.061	.060	.062	.062	.063	.063	.064	
2.5	.057	.058	.058	.059	.059	.059	.060	.060	.061	.061	
3.0	+0.056	+0.056	+0.057	+0.057	+0.058	+0.058	10.050	10.050	+0.060	+0.060	
3.5	.055	.055	.056	.056	.057	.057	.058	.058	.059	.059	
4.0	.054	.054	.055	.055	.056	.056	.057	.057	.057	.058	
4.5	.053	.053	.054	.054	.054	.055	.055	.056	.056	.057	
5.0	.052	.052	.052	.053	.053	.054	.054	.055	.055	.056	
5.5		+0.051		+0.052					+0.054		
6.0	.049	.050	.050	.051	.051	.052	.052	.052	.053	.053	
7.0	.047	.048	.048	.048	.049	.049	.050	.050	.050	.051	
7.5	.046	.047	.047	.047	.048	.048	.048	.049	.049	.050	
8.0	+0.045	+0.045	+0.046	+0.046	+0.047	+0.047	+0.047	+0.048	+0.048	+0.048	
8.5	.044	.044	.045	.045	.045	.046	.046	.047	.047	.047	
9.0 9.5	.043	.043	.044	.044	.044	.045	.045	.045	.046	.046	
10.0	.041	.041	.042	.043	.043	.042	.043	.043	.043	.043	
10.5	+0.040	+0.040	·			+0.041		+0.042		+0.043	
11.0	.039	.039	.039	.039	.040	.040	.040	.041	.041	.041	
11.5	.037	.038	.038	.038	.039	.039	.039	.040	.040	.040	
12.0	.036	.037	.037	.037	.038	.038	.038	.038	.039	.039	
12.5	.035	.036	.036	.036	.036	.037	.037	.037	.038	.038	
13.0		+0.034							+0.036		
13.5 14.0	.033	.033	.034	.034	.034	.034	.035	.035	.035	.036	
14.5	.031	.031	.031	.032	.032	.032	.032	.033	.033	.033	
15.0	.030	.030	.030	.030	.031	.031	.031	.031	.032	.032	
15.5	+0.029	+0.029	+0.029	+0.029	+0.030	+0.030	+0.030	+0.030	+0.031	+0.031	
16.0	.028	.028	.028	.028	.028	.029	.029	.029	.029	.030	
16.5 17.0	.026	.027	.027	.027	.027	.028	.028	.028	.028	.028	
17.5	.023	.024	.025	.025	.025	.025	.027	.027	.027	.026	
		+0.023	_		1	ľ				+0.025	
18.5	.022	.022	.022	.023	.023	.023	.023	.023	.024	.024	
19.0	.021	.021	.021	.022	.022	.022	.022	.022	.022	.023	
19.5	.020	.020	.020	.020	.021	.021	.021	.021	.021	.021	
20,0	.019		.019	.019	.019		.020	.020	.020		
	+0.018	+0.018							+0.019	+0.019 810.	
21.0	.017	.017	.017	.017	.017	.017	.017	.018	.018	.017	
22.0	.014	.015	.015	.015	.015	.015	.015	.015	.015	.016	
22.5	.013	.013	.014	.014	.014	.014	.014	.014	.014	.014	
23.0	+0.012	+0.012	+0.012	+0.013	+0.013	+0.013	+0.013	+0.013	+0.013	+0.013	
23,5	.011	.011	.011	.011	.012	.012	.012	.012	.012	.012	
24.5	.010	.010	.010	.010	.010	.001	.011	.010.	110.	110.	
25.0	.008	.008	.008	.008	.008	.008	.0(8	.008	.008	.009	
	l	1		l							

Attached Ther- mometer			HEIC	HT OF	THE BA	ROMETE	R IN I	NCHES.		
Fahren- heit.	24.0	24.2	24.4	24.6	24.8	25.0	25.2	25.4	25.6	25.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
25°.5	+0.007	+0.007	+0.007	+0.007	+0.007	+0.007	+0.007	+0.007	+0.007	+0.007
26.0	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006
26.5	.005	.005	.005	.005	.005	.005	.005	.005	.005	.005
27.0 27.5	.002	.002	.003	.003	.003	.004	.004	.004	.004	.004
28.0	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001	+0.001	+0.∞1	+0.001	+0.001
28.5	0,000	0.000	0,000	0.000	0.000	0.000	0,000	0.000	0.000	0,000
29.0	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001
29.5	,002	,002	,002	,002	.002	,002	.002	.002	,002	.002
30.0	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003
30.5	-0.004	-0.004	-0.004	-0.004	-0.004	-0.004	→0.004	-0.004	-0.004	-0.004
31.0	.005	.005	.005	.005	.005	.005	.005	.005	.006	.006
31.5	.006	.006	.006	.006	.006	.007	.007	.007	.007	.007
32.0 32.5	.007	.007	.007	.008	.008	.008	.008	.008	.008	.008
								.009		.009
33.0	-0,010	-0.010	-0.010	-0.010	-0.010	-0.010	-0.010	-0.010	-0.010	-0.010
33.5	.011	.011	.011	.011	.011	.011	110.	.011	.011	.011
34.0	.012	.013	.012	.012	.012	.012	.012	.012 .014	.012	.013
34.5 35.0	.014	.014	.014	.014	.013	.014	.015	.015	.015	.015
35.5	-0.015	-0.015	-0.015	-0.015	-0.015	-0.016	-0.016	-0.016	-0.016	-0.016
36.0	.016	.016	.016	.016	.017	.017	.017	.017	.017	.017
36.5	.017	.017	.017	.018	.018	.018	.018	.018	.018	.018
37.0	.018	.018	.019	.019	.019	.019	.019	.019	.019	.019
37.5	.019	.019	.020	.020	.020	.020	.020	.020	.021	.021
38.0	-0.020	-0.021	-0.021	-0.021	-0.021	-0. 021	-0.02I	-0.022	-0.022	-0.022
38.5	.021	.022	.022	.022	.022	.022	.023	.023	.023	.023
39.0	.023	.023	.023	.023	.023	.024	.024	.024	.024	.024
39·5 40.0	.025	.025	.025	.025	.024	.025	.025	.025	.025 .026	.025
40.5	-0.026	-0.026	-0.026	-0.026	-0.027	-0.027	-0.027	-0.027	-0.028	-0.028
41.0	.027	.027	.027	.028	.028	.028	.028	.029	.029	.029
41.5	.028	.028	.028	.029	.029	.029	.029	.030	.030	.030
42.0	.029	.029	.030	.030	.030	.030	.031	.031	.031	.031
42.5	.030	.030	.031	.031	.031	.031	.032	.032	.032	.032
43.0	-0.031	-0.032	-0.032	-0.032	-0.032	-0.033	-0.033	-0.033	-0.033	-0.034
43.5	.032	.033	.033	.033	.033	.034	.034	.034	.035	.035
44.0	.035	.034	.034	.034	.035	.035	.035	.035	.036	.037
45.0	.036	.036	.036	.037	.037	.037	.037	.038	.038	.038
45.5	-0.037	-0.037	-0.037	-0.038	-0.038	-0.038	-0.039	-0.039	-0.039	-0.039
46.0	.038	.038	.038	.039	.039	.039	.040	.040	.040	.041
46.5	.039	.039	.040	.040	.040	.041	.041	.041	.041	.042
47.0 47.5	.040	.040 .041	.041	.041 .042	.041	.042	.042	.042	.043	.043
48.0	-0.042	-0.042	-0.043	-0.043	-0.044	-0.044	-0.044	-0.045	-0.045	-0.045
48.5	.043	.044	.044	.044	.045	.045	.045	.046	.046	.046
49.0	.044	.045	.045	.045	.046	.046	.047	.047	.047	.048
49.5	.045	.046	.046	.047	.047	.047	.048	.048	.048	.049
50.0	.046	.047	.047	.048	.048	.048	.049	.049	.050	.050

TABLE 44.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

ENGLISH MEASURES.

Attached Fahren-hatt					ENGL	ISH ME	ASURE	5.			
Fahrene	Ther-			HEIC	HT OF	THE BA	ROMETI	ER IN I	NCHES.		
\$\frac{50.5}{51.0}	Fahren-	24.0	24.2	24.4	24.6	24.8	25.0	25.2	25.4	25.6	25.8
51.0	F.	Inch.	Inch.	Inch.	Inch.						
51.5 0.95 0.	50°5	-0.048	-0.048	-0.048	-0.049	-0.049	-0.050	-0.050	-0.050	-0.051	-0.051
52.0											
52.5											
\$3.0				1							
53.5 .054 .055 .055 .055 .056 .057 .057 .058 .058 .058 .055 .056 .057 .057 .058 .059 .058 .0		.052	.032	.053	.053	•054	.054	.055	.033	.055	.050
54-0 .055 .056 .057 .057 .058 .058 .059 .050 .061 .061 .062 55.5 -0.058 -0.059 -0.060 .061 .061 .062 .062 .063 .063 .064 .065 .065 .065 .065 .065 .065 .065 .065 .065 .065 .065 .065 .065 .065 .065 .065 .065 .065 .066 .067 .065 .065 .066 .067 .066 .067 .066 .067 .066 .066 .067 .066 .066 .069 .070 .070 .070 .070 .071 .072 .072 .072 .072 .072 .072 .072 .072 .072 .072								_			
\$\frac{5}{55.0}\$ \ \ \ \. 0.056 \ \ \ \ \. 0.057 \ \ \ \. 0.58 \ \ \ \. 0.058 \ \ \ \. 0.058 \ \ \ \. 0.058 \ \ \. 0.058 \ \ \. 0.058 \ \ \. 0.059 \ \ \. 0.050 \ \ \. 0.060 \ \ \. 0.061 \ \. 0.061 \ \ \. 0.062 \ \ \$\frac{55.5}{55.0}\$ \ \ \ \. 0.058 \ \ \. 0.059 \ \ \. 0.059 \ \ \. 0.060 \ \ \. 0.061 \ \ \. 0.061 \ \. 0.062 \ \\ \. 0.058 \ \\ \. 0.059 \ \ \. 0.059 \ \\ \. 0.059 \ \\ \. 0.058 \ \\ \. 0.059 \ \\ \. 0.059 \ \\ \. 0.059 \ \\ \. 0.060 \ \\ \. 0.061 \ \\ \. 0.062 \ \\ \. 0.062 \ \\ \. 0.062 \ \\ \. 0.062 \ \\ \. 0.063 \ \\ \. 0.060 \ \\ \. 0.060 \ \\ \. 0.060 \ \\ \. 0.060 \ \\ \. 0.060 \ \\ \. 0.060 \ \\ \. 0.060 \ \\. 0.060 \ \\ \. 0.060 \ \\ \. 0.061 \ \\ \. 0.062 \ \\ \. 0.63 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.063 \ \\ \. 0.064 \ \\ \. 0.065 \ \\ \. 0.065 \ \\ \. 0.066 \ \\ \. 0.065 \ \\ \. 0.066 \ \\ \. 0.065 \ \\ \. 0.066 \ \\ \. 0.065 \ \\ \. 0.066 \ \\ \. 0.065 \ \\ \. 0.066 \ \\ \. 0.065 \ \\ 0.066 \ \\ \. 0.067 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.069 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.069 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.069 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.068 \ \\ \. 0.069 \ \\ \. 0.069 \ \\ \. 0.069 \ \\ \. 0.069 \ \\ \. 0.069 \ \\ \. 0.069 \ \\ \. 0.069 \ \\ \. 0.069 \ \\ \. 0.069 \ \\ \. 0.069 \ \\ \. 0.069 \\ \. 0.069 \\ \. 0.069 \\ \\ \. 0.069 \\ \\ \.											
55.5 0.057 0.058 0.059 0.059 0.060 0.061 0.061 0.062 55.5 0.058 0.059 0.059 0.060 0.061 0.061 0.062 0.062 0.063 56.0 0.060 0.060 0.061 0.061 0.062 0.062 0.063 56.5 0.061 0.061 0.062 0.062 0.063 0.063 0.063 0.063 0.063 0.063 0.063 0.064 0.065 0.065 57.0 0.062 0.062 0.063 0.063 0.064 0.064 0.065 0.065 0.065 57.5 0.063 0.064 0.064 0.064 0.065 0.065 0.066 0.067 0.065 58.0 0.064 0.064 0.065 0.065 0.066 0.066 0.067 0.068 0.069 0.065 58.0 0.066 0.067 0.068 0.068 0.068 0.069 0.070 0.071 59.0 0.066 0.067 0.068 0.068 0.069 0.070 0.071 0.072 0.072 60.0 0.068 0.069 0.070 0.071 0.072 0.071 0.072 0.072 0.073 0.073 60.5 0.060 0.070 0.070 0.071 0.072 0.073 0.074 0.074 0.074 61.0 0.070 0.071 0.072 0.072 0.073 0.074 0.074 0.074 0.074 0.075 0.076 0.076 0.074 0.074 0.074 0.074 0.074 0.074 0.074 0.074 0.074 0.074 0.074 0.074 0.074 0.074 0.075 0.076 0.076 0.077 0.			-								
55.5 -0.058 -0.059 -0.059 -0.060 -0.061 -0.061 -0.062 -0.062 -0.063 56.5 56.5 .060 .060 .060 .061 .062 .062 .063 .063 .063 .064 .065 .56.5 .061 .061 .062 .063 .063 .063 .063 .064 .065 .065 .065 .065 .065 .065 .065 .065 .065 .065 .065 .065 .065 .066 .066 .066 .066 .066 .066 .066 .066 .067 .067 .068 .069 .069 .069 .069 .069 .069 .069 .069 .069 .069 .069 .069 .070 .071 .072 .0											
56.0 .060 .060 .060 .061 .061 .062 .062 .063 .064 .065 .066 .066 .066 .067 .067 .068 .064 .065 .065 .066 .066 .067 .067 .068 .065 .065 .066 .066 .067 .067 .068 .065 .066 .066 .067 .067 .068 .068 .069 .069 .070 .070 .071 .072 .072 .073 .074 .075 .068 .068 .069 .069 .070 .070 .071 .072 .072 .073 .073 .074 .075 .076 .076 .076 .077 .078 .074 .075 .076 .077 .078 .074 .075 .076 .076 .076 .076 .077 .078 .076 .077 .078 .075 .076 .077 .077 .078 .076				_							
56.5											
57.0 .062 .062 .063 .063 .064 .064 .065 .065 .065 .066 .066 .066 .066 .066 .066 .066 .066 .066 .066 .067 .067 58.0 .065 .065 .066 .067 .068 .068 .068 .069 .069 .069 .070 .071 59.0 .066 .067 .068 .068 .069 .069 .070 .071 .072 .072 .071 59.5 .067 .068 .068 .069 .069 .070 .071 .072 .072 .073 .071 .072 .073 .071 .072 .073 .073 .074 .074 .074 .075 .076 .076 .076 .076 .076 .076 .076 .076 .076 .076 .077 .077 .077 .077 .077 .077 .077 .077 .077 .077 .077 <th></th> <td></td> <td>1</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>			1								
57.5 .063 .063 .064 .064 .065 .066 .066 .067 .067 58.0 -0.064 -0.064 -0.065 -0.065 -0.065 -0.066 -0.067 .067 .068 .068 .069 .069 .069 .069 .069 .069 .069 .069 .070 .071 .072 .072 .072 .072 .071 .072 .072 .072 .072 .072 .072 .072 .072 .072 .072 .073 .073 .073 .073 .074 .074 .075 .076 .076 .074 .075 .076 .074 .075 .073 .073 .074 .074 .075 .076 .076 .074 .075 .076 .076 .076 .076 .076 .076 .076 .076 .077 .077 .077 .077 .077 .077 .077 .077 .077 .077 .077 .077 .077 .077											
58.0 -0.064 -0.065 -0.065 -0.066 -0.066 -0.067 -0.068 -0.068 -0.069 .070 .070 .070 .070 .070 .070 .070 .070 .070 .070 .071 .072 .072 .071 .072 .072 .071 .072 .073 .074 .074 .074 .074 .074 .074 .074 .074 .075 .076 .075 .074 .077 .077 .077 .077 .077 .077 .07											
58.5 .065 .065 .066 .067 .067 .068 .068 .069 .069 .070 .071 59.0 .066 .067 .068 .069 .069 .070 .070 .071 .072 .072 60.0 .068 .069 .069 .070 .070 .071 .072 .072 .072 .073 .073 .073 .073 .074 .074 .075 .076 .071 .072 .073 .073 .074 .074 .075 .076 .076 .071 .072 .073 .073 .074 .074 .075 .076 .076 .076 .077 .076 .076 .077 .077 .078 .076 .077 .077 .078 .076 .077 .077 .078 .079 .080 .081 .081 .082 .082 .083 .081 .081 .082 .082 .083 .084 .085 .085 .081 .082<	37.3							,,,,,		,	,
59.0 .066 .067 .068 .068 .069 .069 .070 .070 .071 59.5 .067 .068 .068 .069 .069 .070 .070 .070 .071 .072 .072 .073 .073 .070 .070 .071 .072 .073 .073 .074 .074 .074 .074 .074 .074 .074 .074 .074 .074 .074 .074 .074 .074 .075 .076 .077 .072 .073 .074 .074 .074 .075 .076 .076 .076 .076 .077 .077 .078 .072 .073 .074 .074 .074 .074 .074 .074 .074 .074 .075 .076 .076 .076 .077 .078 .079 .079 .080 .081 .082 .082 .082 .082 .082 .083 .084 .084 .085 .081 .082 .0					-0.065	-0.066	-0.066	-0.067	-0.068	-0.068	-0.069
59.5 .067 .068 .068 .069 .069 .070 .070 .071 .072 .072 60.0 .068 .069 .069 .070 .071 .072 .071 .072 .073 .073 60.5 -0.069 -0.070 -0.071 -0.072 -0.072 -0.073 -0.073 -0.074 -0.075 -0.076 -0.076 -0.076 -0.076 -0.076 -0.076 -0.076 -0.076 -0.076 -0.076 -0.077 -0.078 -0.079 -0.079 -0.079 -0.079 -0.079 -0.079 -0.079 -0.079 -0.079 -0.080 -0.080 -0.080 -0.080 -0.081 -0.081 -0.077 -0.078 -0.079 -0.080 .081 .082 .083 <										1	
60.0 .068 .069 .069 .070 .070 .071 .072 .072 .073 .073 60.5 -0.069 -0.070 -0.071 -0.072 -0.072 -0.073 -0.074 -0.074 -0.074 61.5 -071 .072 .073 .074 .074 .075 .076 .076 .071 .072 .073 .074 .074 .075 .076 .076 .077 .078 .079 .077 .078 .079 .077 .078 .079 .077 .078 .079 .077 .078 .079 .079 .078 .079 .078 .079 .079 .080 .081 .081 .082 .082 .082 .082 .082 .082 .083 .081 .081 .082 .083 .084 .085 .085 .081 .081 .082 .083 .084 .085 .085 .081 .081 .082 .083 .084 .085 .086							/				
60.5											
61.0	00,0	.003	.009	.009	.070	.070	.071	.072	.072	.073	.073
61.0	60.5	-0.069	-0,070	-0.070	-0.071	-0.072	-0.072	-0.073	-0.073	-0.071	-0.074
61.5			,		,						
62.5	61.5	.071	.072	.073						.076	.077
63.0											
63.5 .076 .076 .077 .078 .078 .079 .080 .081 .081 64.0 .077 .077 .078 .079 .079 .080 .081 .081 .082 .082 .082 .082 .083 .084 .082 .083 .084 .084 .085 .084 .084 .084 .084 .084 .084 .084 .084 .084 .084 .084 .085 .084 .084 .085 .084 .084 .085 .084 .085 .084 .085 .084 .085 .085 .085 .085 .085 .085 .085 .085 .085 .085 .085 .086 .087 .088 .088 .089 .090 .091 .092 .093 .090 .091 .092 .093 .090 .091 .092 .093 .094 .092 .093 .094 .092 .093 .094 .092 .093 .094 .0	62.5	.074	.074	.075	.075	.076	.077	.077	.078	.078	.079
63.5 .076 .076 .077 .078 .078 .079 .080 .081 .081 64.0 .077 .077 .078 .079 .079 .080 .081 .081 .082 .082 .082 .082 .083 .084 .082 .083 .084 .084 .085 .084 .084 .084 .084 .084 .084 .084 .084 .084 .084 .084 .085 .084 .084 .085 .084 .084 .085 .084 .085 .084 .085 .084 .085 .085 .085 .085 .085 .085 .085 .085 .085 .085 .085 .086 .087 .088 .088 .089 .090 .091 .092 .093 .090 .091 .092 .093 .090 .091 .092 .093 .094 .092 .093 .094 .092 .093 .094 .092 .093 .094 .0	63.0	-0.075	-0.075	-0.076	-0.077	-0.077	-0.078	-0.078	-0.070	-0.080	-0.080
64.0 .077 .077 .078 .079 .079 .080 .081 .081 .082 .082 64.5 .078 .079 .079 .080 .081 .081 .082 .082 .083 .084 65.0 .079 .080 .080 .081 .082 .082 .083 .084 .084 .085 65.5 -0.080 -0.081 -0.082 -0.083 -0.084 -0.085 -0.085 -0.085 -0.085 -0.085 -0.085 -0.085 -0.085 -0.085 -0.085 .087 .087 .087 .087 .088 .089 .089 .089 .089 .089 .089 .089 .089 .089 .089 .090 .091 .092 .092 .092 .093 .094 .095 .088 .089 .090 .091 .092 .093 .094 .095 .096 .097 .090 .091 .092 .093 .094 .095											
65.0 .079 .080 .080 .081 .082 .082 .083 .084 .084 .085 65.5 -0.080 -0.081 -0.081 -0.082 -0.083 -0.083 -0.084 -0.085 -0.085 -0.085 -0.085 -0.085 -0.085 -0.085 -0.085 -0.086 66.0 .081 .082 .083 .084 .085 .085 .085 .085 .085 .086 .087 .088 .089 .089 .090 .091 .088 .089 .090 .091 .092 .092 .093 .094 .094 .095 .089 .090 .091 .092 .092 .092 .093 .094 .094 .092 .093 .094 .094 .092 .093 .094 .094 .092 .093 .094 .094 .095 .096 .097 .098 .099 .091 .092 .093 .094 .094 .092 .093 .094 .094			.077					.081	.081	.082	
65.5 -0.080 -0.081 -0.082 -0.083 -0.083 -0.084 -0.085 -0.085 -0.086 66.0 .081 .082 .083 .084 .085 .085 .086 .087 .087 .087 .087 .088 .088 .088 .089 .089 .089 .090 .091 .083 .084 .085 .085 .086 .087 .087 .088 .089 .090 .091 .089 .090 .091 .092 .092 .093 .091 .092 .092 .093 .094 .094 .094 .094 .094 .092 .093 .094 .094 .095 .096 .097 .098 .089 .090 .091 .092 .093 .094 .092 .093 .094 .092 .093 .094 .092 .093 .094 .095 .096 .097 .098 .099 .091 .092 .093 .094 .094 .095 .096 </td <th></th> <td></td>											
66.0	65.0	.079	.080	.080	.081	.082	.082	.083	.084	.084	.085
66.0	65.5	-0.080	-0.08I	-0.0SI	-0.082	-0.082	-0.082	-0.084	-0.085	-0.085	-0.086
66.5											
67.0						.085					
68.0	67.0		.084	.085	.085	.086	.087				.090
68.5	67.5	.084	.085	.086	.087	.087	.oss	.089	.089	.090	.091
68.5	68.0	0.08=	0.006	-0.08-	0.000	0.000	0.080	0.000	0.000	0.001	0.000
69.0 .088 .088 .089 .090 .091 .091 .092 .093 .093 .094 69.5 .089 .089 .090 .091 .092 .092 .093 .094 .095 .095 70.0 .090 .091 .092 .093 .094 .095 .096 .097 .095 .096 .097 70.5 .0091 -0.092 -0.093 -0.094 -0.095 -0.095 -0.096 -0.097 .098 .099 71.0 .092 .093 .094 .094 .095 .096 .097 .098 .099 .099 71.5 .093 .094 .095 .096 .097 .098 .098 .099 .098 .099 .098 .099 .098 .099 .100 .100 .101 .102 .103 .104 .105 .104 .105 73.0 .096 -0.097 -0.098 -0.099 -0.100								-	-		-
69.5 .089 .089 .090 .091 .092 .092 .093 .094 .095 .095 .095 70.0 .090 .091 .091 .092 .093 .094 .094 .095 .096 .097 70.5 -0.091 -0.092 -0.093 -0.094 -0.095 -0.095 -0.096 -0.097 -0.098 71.0 .092 .093 .094 .095 .096 .097 .098 .099 .099 .099 71.5 .093 .094 .095 .096 .097 .098 .098 .099 .100 .100 72.0 .094 .095 .096 .097 .098 .099 .100 .101 .102 .102 72.0 .094 .095 .096 .097 .098 .099 .100 .101 .102 .102 73.0 -0.096 -0.097 -0.098 -0.099 -0.100 -0.101 -0.102									- 1	-	
70.0				-				-			
70.5 -0.091 -0.092 -0.093 -0.094 -0.095 -0.095 -0.096 -0.097 -0.098 71.0 .092 .093 .094 .095 .096 .097 .098 .098 .099 71.5 .093 .094 .095 .096 .097 .098 .098 .099 .100 72.0 .094 .095 .096 .096 .097 .098 .099 .100 .101 .102 .101 72.5 .095 .096 .097 .098 .099 .100 .101 .102 .102 .103 .104 .102 .103 73.0 -0.096 -0.097 -0.098 -0.099 -0.100 -0.101 -0.102 -0.103 -0.104 73.5 .097 .098 .099 .100 .101 .102 .103 .104 .105 .105 74.0 .098 .099 .100 .101 .102 .103 .104 .105 .106 .107		/	,	-	- 1						
71.0	70 -						1	1			
71.5		- 1	-	-					-0.096		-0.098
72.0											.099
72.5											
73.0 -0.096 -0.097 -0.098 -0.099 -0.100 -0.100 -0.101 -0.102 -0.103 -0.104 73.5 .097 .098 .099 .100 .101 .101 .102 .103 .104 .105 74.0 .098 .099 .100 .101 .102 .103 .104 .105 .105 .106 74.5 .100 .100 .101 .102 .103 .104 .105 .105 .106 .107											
73.5		750	1290			7.7			, 1071	.102	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$									-0.102	0.103	
74.5 .100 .100 .101 .102 .103 .104 .105 .105 .106 .107											
100 .100 .100 .100 .100											
	73.0	-101	. 101	.102	.103	,104	,103	.100	,100	.107	.100

					SH WE					
Attached Ther- mometer			HEIG	HT OF	THE BA	ROMETE	R IN IN	CHES.		
Fahren- heit,	24.0	24.2	24.4	24.6	24.8	25.0	25.2	25.4	25.6	25.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
75.5	-0.102		-0.103 .104	.105	.106	-0.106	. 107	-0.108	-0.108	-0.109
76.5	.103	.104	.104	.105	.107	.107	.109	.110	.110	.110
77.0	.104	.105	.107	.108	.108	.100	.110	.111	.112	.113
77.5	.106	.107	.108		.110	.110	.111	.112	.113	.114
78.0							-0.112			
78.5	. 108	.109	.110	.111	.112	.113	.114	.114	.115	.116
79.0	.109	.110	III.	.112	.113	.114	.115	.116	.117	.117
79.5	011.	.111	.112	.113	.114	.115	.110	.117	.113	.119
80.0										
80.5					-0.116		-0.118			
81.0	.114	.115	.115	.116	.117	.118	.119	.120	.121	.122
81.5	.115	.116	.117	.118	.118	.119	.120	.121	.122	.123
82.0 82.5	.116	.117	.118	.119	.120	.121	.122	.122	.123	.124
								·		
83.0							-0.124			
83.5	.119	.120	.121	.122	.123	. I 24	.125	.126	.127	.128
84.0	. 120	.121	.122	.123	.124	.125	.126	.127	.128	.129
84.5	.121	.122		.124	.125	.126	.127	.128	.129	.130
85.0	.122	.123	.124	ŭ			1	.129	_	131
85.5		-O. I 24					-0.129			
86.0	. 124	.125	.126	.127	. 128	.130	.131	.132	.133	.134
86.5	.125	.126	.128	.129	.130	.131	.132	.133	.134	.135
87.0	.126	.128	.129	.130	.131	.132		.134		.136
87.5	.128	.129		.131	.132	.133		.135	.136	.137
88.0					-0.133		-0.135	-0.136	-0.137	-0.138
SS.5	.130	.131	.132	.133	.134	.135		.137	.138	.139
89.0	.131	.132	.133	.134	.135	.136		.138	.140	.141
89.5	.132	.133	.134	.135	.136	.137	.138	.140	.141	.142
90.0	.133	.134	.135	.136	.137	.138				
90.5	-0.134		-0.136		-01.39				-0.143	-0.144
91.0	.135	.136	.137	.138	.140	.141	.142	.143	.144	.145
91.5	. 136	.137	.138	.140	.141	.142	.143	.144	.145	.146
92.0 92.5	.137	.138	.140	.141	.142	.143		.145	.148	.149
93.0			-0.142		-0.144		-0.146		-0.149	
l i	-0.139 .140	.142	.143	.144	.145	.146	.148	.149	.150	.151
93.5 94.0	.140	.143	.144	.145	.146	.147	.149	.150	.151	.152
94.5	.143	.144		.146		.149		.151		.153
95.0	.144	.145	.146	.147	.149	.150		.152	.153	.154
				1	0.150	-0.151	-0.152	-0.152	-0.154	-0.156
95.5 96.0	.146	-0.146	.148	.150	.151	.152	.153	.154	.156	.157
96.5	.147	.148	.149	.151	.152	.153	.154	.156	.157	.158
97.0	.148	.149	.150	.152	.153	.154	.155	.157	.158	.159
97.5	.149	.150	.152	.153	.154	.155	.157	.158	.159	.160
98.0	-0.150	-0.151	-0.153	-0.154	-0.155	-0.156	-0.158	-0.159	-0.160	-0.161
98.5	.151	.153	.154	.155	.156	.158	.159	.160	.161	. 163
99.0	.152	.154	.155	.156	.157	.159	.160	.161	.162	.164
99.5	.153	.155	.156	.157	.159	.160	.161	.162	.164	.165
100,0	.154	.156	.157	.158	.160	.161	.162	.163	.165	. 166
	I		1	1			-			1

TABLE 44.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

ENGLISH MEASURES.

					,					
Attached Ther- mometer			HEIG	HT OF	THE BA	ROMETE	R IN I	NCHES.		
Fahren- heit.	26.0	26.2	26.4	26.6	26.8	27.0	27.2	27.4	27.6	27.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
0.0	+0.068	+0.068	+0.069	+-0.069	+0.070	+0.070	+0.071	+0.071	+0.072	+0.072
	+0.067	+0.067	+0.068		+0.069		+0.070		+0.071	+0.071
I.O I.5	.065	.066	.066	.067	.067	.068	.068	.069	.069	.070
2.0	.063	.064	.064	.065	.065	.065	.066	.066	.067	.067
2.5	.062	.062	.063	.063	.064	.064	.065	.065	.066	.066
3.0	+0.061	+0.061	+0.062	+0.062	+0.063	+0.063	+0.063	+0.064	+0.064	+0.065
3.5	.059	.060	.060	.061	.061	.062	.062	.063	.063	.064
4.0	.058	.059	.059	.060	.060	.061	.061	.061	.062	.062 .061
4.5 5.0	.057 .056	.056	.057	.057	.058	.058	.059	.059	.059	.060
				1	+0.056		+0.057		+0.058	
6.0	+0.055 .054	+0.055	.054	.055	.055	+0.057	.056	.056	.057	+0.059
6.5	.052	.053	.053	.054	.054	.054	.055	.055	.056	.056
7.0	.051	.052	.052	.052	.053	.053	.054	.054	.054	.055
7.5	.050	.050	.051	.051	.052	.052	.052	.053	.053	.053
8.0	+0.049		+0.050		+0.050		+0.051		+0.052	+0.052
8.5 9.0	.048	.048	.048	.049	.049	.049	.050	.050	.051	.051
9.5	.045	.046	.046	.046	.047	.047	.049	.048	.049	.048
10.0	.044	.044	.045	.045	.045	.0.16	.046	.046	.047	.047
10.5	+0.043	+0.043	+0.044	+0.044	+0.044	+0.045	+0.045	+0.045	+0.046	+0.046
11.0	.042	.042	.042	.043	.043	.043	.04.4	.044	.044	.045
11.5	.041	.041	.041	.041	.042	.042	.042	.043	.043	.043
12.5	.039 .038	.040	.039	.040	.041	.041 .040	.041	.041	.042	.042 .041
		+0.037	+0.038							
13.5	+0.037 .036	.036	.036	.037	.037	.037	+0.039	+0.039	+0.039	+0.040
14.0	.035	.035	.035	.035	.036	.036	.036	.036	.937	.037
14.5	.033	.034	.034	.034	.034	.035	.035	.035	.035	.036
15.0	.032	.032	.033	.033	.033	.033	.034	.034	.034	.034
	+0.031		+0.032		+0.032		+0.032		+0.033	+0.033
16.0 16.5	.030	.030	.030	.031	.031	.031	.031	.031	.032	.032
17.0	.027	.028	.028	.028	.028	.029	.029	.029	.029	.029
17.5	.026	.027	.027	.027	.027	.027	.028	.028	.028	.028
	+0.025	+0.025	+0.026	+0.026	+0.026	+0.026	+0.026	+0.026	+0.027	+0.027
18.5	.024	.024	.024	.024	.025	.025	.025	.025	.025	.026
19.0	.023	.023	.023	.023	.023	.024	.024	.024	.024	.024
20.0	.020	.021	.021	.021	.021	.021	.021	.021	.022	.023
20.5	+0.019	+0.019	+0.020	+0.020	+0.020	+0.020	+0.020	+0.020	+0.0 2 0	+0.021
21.0	310.	.018	.018	.018	.019	.019	.019	.019	.019	.019
21.5	.017	.017	.017	.017	.017	.017	.018	.018	.018	.018
22.0	.016	.016	.016	.016	.016	.016	.016	.017	.017	.017
23.0 23.5	+0.0I3 .0I2	+0.013	+0.014	+0.014	+0.014	+0.014	+0.014		+0.014	+0.014
23.5	.012	.012	.012	.012	.012	.013	.013	.013	.013	.013
24.5	.010	.010	.010	.010	.010	.010	.010	.010	.010	.110
25.0	.009	.009	.009	.009	.009	.009	.009	.009	.009	.009

						ROURES				
Attached Ther- mometer			HEIG	HT OF	THE BA	ROMETE	R IN I	NCHES.		
Fahren- heit.	26.0	26.2	26.4	26.6	26.8	27.0	27.2	27.4	27.6	27.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
25°.5			+0.008	+0.008	+0.008	+0.008	+0.008		+-0.00S	+0.008
26.0	.006	.006	.006	.006	.006	.006	.006	.007	.007	.007
26.5	.005	.005	.005	.005	.005	.005	.005	.005	.005	.005
27.0	.004	.004	.00.1	.004	.001	.004	.004	.00.1	.004	.004
27.5	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003
	+·0.001	+0.001	+0.002	+0.002		+0.002	+0.002	+0.002	+0.002	+0.002
28.5	0,000	0.000	0.000	0,000	0.000	0.000	0.000	0,000	0.000	0.000
29.0	-0.00I	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001
29.5	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
30.0	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003
30.5	-0.004	-0.004	-0.004	-0 005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005
31.0	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006
31.5	.007	.007	.007	.007	.007	.007	.007	.007	.007	.007
32.0	.008	.008	.008	.008	.008	.008	.008	.008	.008	.009
32.5	.009	.009	.009	.009	.009	.009	.010	.010	.010	.010
22.0	-0.010	0.010	-0.010	0.011	0.077	-0.011		-0.011		0.011
33.0	.010	-0.0I0 .0I2	.012	.012	-0.011	-0.0II .0I2	-0.0II .0I2	.012	-0.0II .0I2	-0.011 .012
33.5 34.0	.013	.012	.012	.012	.012	.013	.012	.013	.013	.012
34.5	.013	.014	.014	.014	.014	.014	.014	.015	.015	.015
35.0	.015	.015	.015	.015	.015	.016	.016	.016	.016	.016
00.1										
35.5	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.017	-0.017	-0.017	-0.017
36.0	.017	.018	.018	.018	.018	.018	.018	.018	.018	.019
36.5	.019	.019	.019	.019	.019	.019	.019	.020	.020	.020
37.0	.020	.020	.020	.020	.020	.021	.021	.021	.021	.021
37.5	.021	.021	.021	.021	.022	.022	.022	.022	.022	.022
38.0	-0.022	-0.022	-0.022	-0.023	-0.023	-0.023	-0.023	-0.023	-0.023	-0.024
38.5	.023	.023	.024	.024	.024	.024	.024	.025	.025	.025
39.0	.024	.025	.025	.025	.025	.025	.026	.026	.026	.026
39.5	.026	.026	.026	.026	.026	.027	.027	.027	.027	.027
40.0	.027	.027	.027	.027	.028	.028	.028	.028	.028	.029
40.5	-0.028	-0.028	-0.028	-0.020	0.020	-0.029	-0.029	_0.020	_0.020	-0.030
41.0	.029	.029	.030	-0.029	-0.029	.030	.031	-0.030	-0.030	.031
41.5	.030	.031	.030	.031	.031	.032	.032	.032	.032	.032
42.0	.032	.032	.032	.032	.033	.033	.033	.033	.033	.034
42.5	.033	.033	.033	.033	.034	.034	.034	.034	.035	.035
40.0									((
43.0	-0.034	-0.034	-0.034	-0.035	-0.035	-0.035	-0.035	-0.036	-0.036	-0.036
43.5	.035	.035	.036	.036	.036	.036	.037	.037	.037	.037
44.0	.036	.037	.037	.037	.037	.038	.038	.038	.030	.039
44.5 45.0	.037	.038	.039	.039	.040	.040	.040	.041	.041	.041
45.0	.039	.039	.039	.039	.040	1040	, , ,			*
45.5	-0,040	-0.040	-0.040	-0.041	-0.041	-0.041	-0.042	-0.042	-0.042	-0.043
46.0	.041	.041	.042	.042	.042	.043	.043	.043	.043	.044
46.5	.042	.042	.043	.043	.043	.044	.044	.044	.045	.045
47.0	.043	.044	.044	.044	.045	.045	.045	.046	.046	.046
47.5	.045	.045	.045	.046	.046	.046	.047	.047	.047	.048
48.0	-0.046	-0.046	-0.046	-0.047	-0.047	-0.047	-0.048	-0.048	-0.048	-0.049
48.5	.047	.047	.048	.048	.048	.049	.0.19	.049	.050	.050
49.0	.048	.048	.049	.049	.049	.050	.050	.051	.051	.051
49.5	.049	.050	.050	.050	.051	.051	.051	.052	.052	.053
50.0	.050	.051	.051	.052	.052	.052	.053	.053	.053	.054
		1	1	1	1					

TABLE 44.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

ENGLISH MEASURES.

				ENGLI	SH ME	ASURES	· .			
Attached Ther- mometer			HEIG	HT OF	THE BA	ROMETE	R IN I	CHES.		
Fahren- heit.	26.0	26.2	26.4	26.6	26.8	27.0	27.2	27.4	27.6	27.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
50°5	-0.052	-0.052	-0.052	-0.053	-0.053	-0.054	-0.054	-0.054	-0.055	-0.055
51.0	.053	.053	.054	.054	.054	.055	.055	.056	.056	.056
51.5	.054	.054	.055	.055	.056	.056	.056	.057	.057	.058
52.0	.055	.055	.056	.056	.057	.057	.058	.058	.058	.059
52.5	.056	.057	.057	.058	.058	.058	.059	.059	.060	.060
53.0	-0.057	-0.058	-0.058	-0.059	-0.059	-0.060	-0.060	-0.061	-0.061	-0.061
53.5	.059	.059	.059	.060	.060	.061	.061	.062	.062	.063
54.0	.060	.060	.061	.061	.062	.062	.063	.063	.063	.064
54.5	.061	.061	.062	.062	.063	.063	.064	.064	.065	.065
55.0	.062	.063	.063	.064	.064	.064	.065	.065	.066	.066
55.5	-0.063	-0.064	-0.064	-0.065	-0.065	-0.066	-0.066	- 0.067	-0.067	-0.068
56.0	.064	.065	.065	.066	.066	.067	.067	.068	.068	.069
56.5	.066	.066	.067	.067	.068	.068	.069	.069	.070	.070
57.0	.067	.067	.068	.068	.069	.069	.070	.070	.071	.071
57-5	.068	.069	.069	.070	.070	.071	.071	.072	.072	.073
58.0	-0.069	-0.070	-0.070	-0.071	-0.071	-0.072	-0.072	-0.073	-0.073	-0.074
58.5	.070	.071	.071	.072	.072	.073	.074	.074	.075	.075
59.0	.072	.072	.073	.073	.074	.074	.075	.075	.076	.076
59.5	.073	.073	.074	.074	.075	.075	.076	.077	.077	.078
60.0	.074	.074	.075	.076	.076	.077	.077	.078	.078	.079
60.5	-0.075	-0.076	-0.076	-0.077	-0.077	-0.078	-0.078	-0.079	- 0.080	-0.080
61.0	.076	.077	.077	.078	.079	.079	.080	.oSo	.081	.081
61.5	.077	.078	.079	.079	.oSo	.oSo	.081	.082	.082	.083
62.0	.079	.079	.080	.oSo	.oSı	.082	.082	.083	.083	.084
62.5	.080	.oSo	.081	.082	.082	.083	.083	.084	.085	.085
63.0	-0.081	-0.082	-0.082	-0.083	-0.083	-0.084	_o.oS5	-0.085	-0.086	-0.086
63.5	.082	.083	.083	.084	.085	.085	.086	.086	.087	.088
64.0	.083	.084	.085	.085	.086	.086	.087	.088	.088	.089
64.5	.084	.085	.086	.086	.087	.088	.088	.089	.090	.090
65.0	.086	.086	.087	.088	.088	.089	.090	.090	.091	.092
65.5	-0.0S7	-0.087	0.088	-0.0S9	-0.089	-0.090	-0.091	-0.091	-0.092	-0.093
66.0	.088	.089	.089	.090	.091	.091	.092	.093	.093	.094
66.5	.089	.090	.090	.091	.092	.093	.093	.094	.095	.095
67.0	.090	.091	.092	.092	.093	.094	.094	.095	.096	.097
67.5	.092	.092	.093	.094	.094	.095	.096	.096	.097	.098
68.0	-0.093	-0.093	-0.094	-0.095	-0.095	-0.096	-0.097	-0.098	-0.098	-0.099
68.5	.094	.095	.095	.096	.097	.097	.098	.099	.100	.100
69.0	.095	.096	.096	.097	.098	.099	.099	.100	. IOI	.102
69.5	.096	.097	.098	.098	.099	.100	.IOI	.101	.102	.103
70.0	.097	.098	.099	.100	.100	.101	.102	.103	.103	.10.1
70.5	-0.098	-0.099	-0.100	-0.101	-0.101	-0.102	-0,103	-0.104	-0.105	-0,105
71.0	.100	.100	.IOI	.102	.103	.103	.104	.105	.106	.107
71.5	.IOI	.102	.102	.103	.104	.105	.105	.106	.107	.108
72.0	.102	.103	.104	.104	.105	.106	.107	.107	.108	.109
72.5	.103	.104	.105	.106	.106	.107	.108	.109	.109	.110
73.0	-0.104	-0.105	-0.106	-0.107	-o. 10S	-0.108	-0.109	-0.110	-0.111	-0.112
73.5	.105	.106	.107	.108	.109	.IIO	.110	.III	.112	.113
74.0	.107	.107	.108	.109	.110	.III	.112	.112	.113	.114
74.5	.108	.109	.109	.110	.III	.112	.113	.114	114	.115
75.0	.109	.110	.111	.112	.112	.113	.114	.115	116	.117
		1		1	·					

Father Neth	Attached Ther- mometer			HEIG	HT OF	THE BAI	ROMETE	R IN IN	CHES.		
75.5	Fahren-	26.0	26.2	26.4	26.6	26.8	27.0	27.2	27.4	27.6	27.8
76.0									3		Inch.
76.5											11
77.5											.119
77.5											.120
78.0 -0.116 -0.117 -0.118 -0.119 -0.120 -0.120 -0.121 -0.122 -0.123 -0.123 -0.123 -0.123 -0.124 -122 .123 .123 .124 .125 .126 .127 .125 .120 .121 .122 .123 .124 .125 .126 .127 .128 80.0 .121 .122 .123 .124 .125 .126 .127 .128 .123 .124 .125 .126 .127 .128 .123 .131 .132 .131 .132 .138 .135 .131 .132 .138 .135 .131 .132 .133 .134 .132 .133 .134 .132 .133 .134 .132 .133 .131 .132 .133 .134 .132 .133 .134 .132 .133 .134 .132 .133 .134 .132 .133 .134 .135 .136 .137 .138 .139 <t< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>.122</th></t<>											.122
78.5		.115	.116	.117	.117	.118	.119			.122	.123
79.0	78.0	-0.116	- 0.117	-0.118	-0.119	-0.120	-0. I 20	-0.121	-0.122	-0.123	-0.I24
79.5	78.5	.117	.118	.119	.120	.121	.122	.123	.123	.124	.125
80.0	79.0	.118	.119	.120	.121	.122	.123	.124	.125	.126	.127
80.0	79.5	.120	.120	.121	.122	.123	.124	.125	.126	.127	.128
St. 1.23					.123		.125	.126	.127	.128	.129
S1.5		-0.122	-0.123	-0.124		-0.126			-0.128	-0.129	-0.130
82.0	81.0	.123	.124	.125	.126	.127	.128			.131	.132
82.0		.124	.125	.126	.127		.129	.130	.131	.132	.133
82.5 .127 .128 .128 .129 .130 .131 .132 .133 .134 .132 83.0 -0.128 -0.129 -0.130 -0.131 -0.132 -0.133 -0.134 -0.135 -0.136 -0.138 83.5 .129 .130 .131 .132 .133 .134 .135 .136 .137 .138 84.5 .131 .132 .133 .134 .135 .136 .137 .138 .139 .141 .12 85.0 .132 .133 .134 .135 .136 .137 .138 .139 .141 .142 .143 .141 .142 .143 .141 .142 .143 .141 .142 .143 .141 .142 .143 .141 .142 .143 .144 .145 .146 .147 .148 .149 .14 .142 .143 .144 .145 .146 .147 .148 .149 .15				.127		.129	.130				.134
83.5	82.5										.135
83.5	83.0	-0.700	-0 TOO	-0 T20	_0 T27	-0 T22	-0 T22	-0 T24	-0 I25	-0 T26	-0.127
84.0 .130 .131 .132 .133 .134 .135 .136 .137 .138 .137 85.0 .132 .133 .134 .135 .136 .137 .138 .139 .141 .12 85.5 -0.134 -0.135 -0.136 -0.137 -0.138 -0.140 -0.141 -0.142 -0.12 86.0 .135 .136 .137 .138 .139 .140 .141 .142 .143 .144 .145 .146 .147 .143 .144 .145 .144 .145 .146 .147 .148 .144 .145 .146 .147 .148 .144 .145 .146 .147 .148 .149 .15 .146 .147 .148 .149 .15 .15 .15 .15 .15 .14 .142 .143 .144 .145 .146 .147 .148 .149 .15 .14 .142 .143 .144 .145 .146 .147 .148 .149 .150 .15 .15 .15											
84.5 .131 .132 .133 .134 .135 .136 .137 .138 .139 .141 .12 85.5 -0.134 -0.135 -0.136 -0.137 -0.138 -0.139 -0.140 -0.141 -0.142 -0.14 86.0 .135 .136 .137 .138 .139 .140 .141 .142 .143 .144 .142 86.5 .136 .137 .138 .139 .140 .141 .142 .143 .144 .142 87.5 .138 .139 .140 .141 .142 .143 .144 .145 .146 .147 .148 .144 .145 .146 .147 .148 .149 .150 .14 .145 .146 .147 .148 .149 .150 .15 .152 .153 .15 .152 .153 .15 .152 .153 .15 .152 .153 .15 .152 .153 .15	03.5					+133					
85.0 .132 .133 .134 .135 .136 .137 .138 .139 .141 .142 85.5 -0.134 -0.135 -0.136 -0.137 -0.138 -0.139 -0.140 -0.141 -0.142 -0.142 86.5 .136 .137 .138 .139 .140 .141 .142 .143 .144 .142 87.5 .138 .139 .140 .141 .142 .143 .144 .145 .12 87.5 .138 .139 .140 .141 .142 .143 .144 .145 .146 .147 .143 .144 .145 .146 .147 .143 .144 .145 .146 .147 .148 .149 .150 .15						•134					
85.5 -0.134 -0.135 -0.136 -0.137 -0.138 -0.139 -0.140 -0.141 -0.142 -0.142 -0.142 86.5 1.36 1.37 1.38 1.39 1.40 1.41 1.42 1.43 1.44 1.42 1.43 1.44 1.42 1.43 1.44 1.45 1.46 1.47 1.42 1.43 1.44 1.45 1.46 1.47 1.42 1.43 1.44 1.45 1.46 1.47 1.42 1.43 1.44 1.45 1.46 1.47 1.48 1.44 1.45 1.46 1.47 1.48 1.49 1.5 1.46 1.47 1.48 1.49 1.5 1.46 1.47 1.48 1.49 1.50 1.5<								.137			.140
86.0	85.0	.132	.133	.134	.135	.135	.137	.138	.139	.141	.142
86.0	85.5	-0.134	-0.135	-0.136	-0.137	-0.138	-0.139	-0.140	-0.141	-0.142	-0.143
86.5	86.0				.138				.142		.144
87.0 .137 .138 .139 .140 .141 .142 .143 .144 .145 .14 87.5 .138 .139 .140 .141 .142 .144 .145 .146 .147 .14 88.0 -0.139 -0.140 -0.142 -0.143 -0.144 -0.145 -0.146 -0.147 -0.148 -0.14 89.5 .141 .142 .143 .144 .145 .146 .147 .148 .149 .150 .15 89.5 .143 .144 .145 .146 .147 .148 .149 .150 .15 .152 .153 .15 .152 .153 .15 .152 .153 .15 .152 .153 .15 .152 .153 .154 .155 .146 .147 .148 .150 .151 .152 .153 .154 .150 .151 .152 .153 .151 .152 .153 .151 .152		.136		.138							.145
87.5 .138 .139 .140 .141 .142 .144 .145 .146 .147 .148 88.0 -0.139 -0.140 -0.142 -0.143 -0.144 -0.145 -0.146 -0.147 -0.148 -0.148 89.5 .141 .142 .143 .144 .145 .146 .147 .148 .149 .150 .152 .153 .152 .153 .152 .153 .152 .153 .152 .153 .152 .153 .152 .153 .152 .153 .154 .155 .146 .147 .148 .149 .151 .152 .153 .152 .153 .152 .153 .152 .153 .154 .155 .15 .152 .153 .154 .155 .15 .152 .153 .154 .155 .157 .15 .152 .153 .154 .155 .157 .158 .159 .16 .157 .158 .159 .16				.130							.147
88.5											.148
88.5	88.0	-0.130	- 0, I40	-0. I42	-0.143	-0.144	-0.145	-0.146	-0.147	-0.148	-0.149
89.0 .142 .143 .144 .145 .146 .147 .148 .149 .150 .15 .152 .15 .152 .15 .152 .15 .152 .15 .152 .15 .152 .15 .152 .15 .152 .15 .152 .15 .152 .153 .15 .152 .153 .15 .152 .153 .15 .152 .153 .15 .152 .153 .154 .155 .15 .15 .152 .153 .154 .155 .15 .15 .152 .153 .154 .155 .15 .15 .152 .153 .154 .155 .157 .158 .159 .15 .152 .153 .154 .155 .157 .158 .159 .15 .152 .153 .155 .157 .158 .159 .16 .157 .158 .159 .16 .157 .158 .159 .16 .157 .158 .159 .1	88.5										.150
89.5 .143 .144 .145 .146 .147 .148 .149 .151 .152 .153 .152 .153 .152 .153 .152 .153 .152 .153 .152 .153 .152 .153 .152 .153 .152 .153 .154 .155 .153 .154 .155 .153 .154 .155 .153 .154 .155 .157 .158 .159 .151 .152 .153 .154 .155 .157 .158 .159 .159 .159 .151 .152 .153 .154 .155 .157 .158 .159 <td< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>.152</th></td<>											.152
90.0											.153
91.0											.154
91.0 1.46 1.47 1.49 1.50 1.51 1.52 1.53 1.54 1.55 1.57 1.59 1.50 1.51 1.52 1.53 1.54 1.55 1.57 1.58 1.59 1.50 1.51 1.52 1.53 1.54 1.55 1.57 1.58 1.59 1.50 1.51 1.52 1.53 1.54 1.56 1.57 1.58 1.59 1.50 1.51 1.52 1.53 1.54 1.56 1.57 1.58 1.59 1.50 1.	90.5	-0.145	-0.146	-0.1.17	-0.149	-0.150	-0.151	-0.152	-0.153	-0.154	-0.155
91.5 148 149 150 151 152 153 154 155 157 158 159 160 152 153 154 155 157 158 159 150 151 152 153 154 156 157 158 159 150 151 152 153 154 156 157 158 159 160 152 153 155 156 157 158 159 160 162 163 164 165 165 167 168 169 170 171											.157
92.0 92.0 92.5 149 150 151 152 153 154 156 157 158 159 160 162 163 154 165											.158
92.5 .150 .151 .152 .153 .154 .156 .157 .158 .159 .16 93.0 -0.151 -0.152 -0.153 -0.155 -0.156 -0.157 -0.158 -0.159 -0.160 -0.16 93.5 .152 .153 .155 .156 .157 .158 .159 .160 .162 .163 .16 94.0 .153 .155 .156 .157 .158 .159 .160 .162 .163 .16 .162 .163 .16 .162 .163 .164 .165 .16 .162 .163 .164 .165 .16 95.5 -0.157 -0.158 -0.159 -0.160 -0.162 -0.163 -0.164 -0.165 -0.167 -0.16 95.5 -0.157 -0.158 -0.159 -0.160 -0.162 -0.163 -0.164 -0.165 -0.167 -0.167 96.0 .158 .159 .160 .162											.159
93.5									.158		.160
93.5	93.0	-0.151	-0.152	-0.153	-0.155	-0.156	-0.157	-0.158			
94.0 94.5 94.5 94.5 94.5 95.0 94.5 95.0 94.5 95.5 95.0 94.5 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.0 95.5 95.5 95.0 95.5 95	93.5							.159			.163
94.5 95.0 155 156 157 158 159 160 162 163 164 165 164 165 169 160 162 163 164 165 160 162 163 164 165 160 162 163 164 165 160 162 163 164 165 160 162 163 164 165 167 168 160 162 163 164 165 167 168 169 170 170 171 171 172 173 174 175									.162		.164
95.0 .156 .157 .158 .159 .160 .162 .163 .164 .165 .16 95.5 -0.157 -0.158 -0.159 -0.160 -0.162 -0.163 -0.164 -0.165 -0.167 -0.167 96.0 .158 .159 .160 .162 .163 .164 .165 .167 .168 .16 96.5 .159 .160 .162 .163 .164 .165 .167 .168 .169 .17 97.0 .160 .162 .163 .164 .165 .167 .168 .169 .170 .171 .17 97.5 .162 .163 .164 .165 .166 .168 .169 .170 .171 .17									.163	.164	.165
96.0											.166
96.0	95.5	-0,157	-0.158	-0.150	-0.160	-0.162	-0.163	-0.164	-0.165	-0.167	-0.168
96.5						162	.164	, 165	.167	, 168	.169
97.0											.170
97.5 .162 .163 .164 .165 .166 .168 .169 .170 .171 .17				162	164						.171
98 0 0 162 0 164 0 165 0 166 0 168 0 160 0 170 0 171 0 172 0 17					.165						.173
-0.103 -0.104 -0.105 -0.100 -0.109 -0.170 -0.171 -0.173 -0.1	98.0	-0.163	-0.164	-0.165	-0. 166	-0.168	-0.169	-0.170	-0.171	-0.173	-0.174
98.5 .164 .165 .166 .168 .169 .170 .171 .173 .174 .17	98.5										.175
99.0 .165 .166 .168 .169 .170 .171 .173 .174 .175 .17											.176
											.178
								.175			.179
	230,5	1 .10/	'109	1 .1/0	1/1	1 1/2	1 -74	-73			1

Attached Ther- mometer			HEIG	HT OF	THE BA	ROMETE	R IN II	NCHES.		
Fahren- heit.	28.0	28.2	28.4	28.6	28.8	29.0	29.2	29.4	29.6	29.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
0.0	+0.073	+0.074	+0.074	+0.075	+0.075	+0.076	+0.076	+0.077	+0.077	+0.078
+0.5	+0.072	+0.072	+0.073		+0.074	+0.074	+0.075	+0.075	+0.076	+0.076
1.0	.070	.071	.071	.072	.072	.073	.073	.074	.074	.075
1.5 2.0	.069	.070	.070	.071	.071	.072	.072	.073	.073	.074
2.5	.067	.067	.068	.068	.069	.069	.069	.070	.070	.071
3.0	+0.065	+0.066	+0.066	+0.067	+0.067	+0.068	±0.068	+0.069	+0.069	+0.070
3.5	.064	.065	.065	.065	.066	.066	.067	.067	.068	.068
4.0 4.5	.063	.063	.064	.064	.065	.065	.065	.066	.066	.067
5.0	,060	.061	.061	.062	.062	.062	.063	.063	.064	.064
5.5	+0.059	+0.059	+0.060	+0.060	+0.061	+0.061	+0.062	+0.062	+0.062	+0.063
6.0	.058	.058	.059	.059	.059	.060	.060	.061	.061	.061
6.5	.056	.057	.057	.058	.058	.058	.059	.059	.060	.060
7.0 7.5	.055 .054	.056	.056	.056	.057	.057 .056	.057 .056	.058	.058	.059
8.0	+0.053	+0.053	+0.053	+0.054	+0.054	+0.054	+0.055	+0.055	+0.056	+0.056
8.5	.051	.052	.052	.052	.053	.053	.053	.054	.054	.055
9.0	.050	.050	.051	.051	.051	.052	.052	.053	.053	.053
9.5 10.0	.049 .047	.049	.049	.050	.050	.050	.051	.051	.052	.052
10.5	+0.046	+0.047	+0.047	+0.047	+0.048	+0.048	+0.048	+0.049	+0.049	+0.049
0.11	.0.15	.045	.046	.046	.046	.047	.047	.047	.047	.048
11.5	.044	.044	.044	.045	.045	.045	.046	.046	.046	.046
12.0 12.5	.042	.043	.043	.043	.044	.044	.044	.044	.045	.045
	+0.040	+0.040	+0.040	+0.041	+0.041	+0.041	+0.042	+0.042	+0.042	+0.042
13.5	.039	.039	.039	.039	.040	.040	.040	.040	.041	.041
14.0	.037	.038	.038	.038	.038	.039	.039	.039	.039	.040
14.5	.036	.036	.037	.037	.037	.037	.038	.038	.038	.038
15.0	.035	.035	.035	.035	.036	.036	.036	.036	.037	.037
15.5	+0.033	+0.034	+0.034	+0.034	+0.034	+0.035	+0.035	+0.035		+0.036
16.0 16.5	.032	.032	.033	.033	.033	.033	.034	.034	.034	.034
17.0	.030	.030	.030	.030	.030	.031	.032	.031	.031	.032
17.5	.028	.029	.029	.029	.029	.029	.030	.030	.030	.030
18.0	+0.027	+0.027	+0.027	+0.028	+0.028	+0.028	+0.028	+0.028	+0.029	+0.029
18.5	.026	.026	.026	.026	.027	.027	.027	.027	.027	.027
19.0	.025	.025	.025	.025	.025	.025	.026	.026	.026	.026
19.5 20.0	.023	.023	.024	.024	.024	.024	.024	.024	.025	.025
									+0.022	
21.0	.019	.020	.020	.020	.020	.020	.020	.020	.021	.021
21.5	.018	810.	.018	.019	.019	.019	.019	.019	.019	.019
22.0 22.5	.017	.017	.017	.017	.017	.017	.018	.018	.018	.018
23.0										
23.5	+0.014	+0.014	.013	+0.015	+0.015	+0.015	+0.015	+0.015	+0.015	+0.015 .014
24.0	.012	.012	,012	,012	,013	.012	.012	.012	.012	.013
24.5	110.	110.	110,	110,	.011	110.	.011	.011	.011	110.
25.0	.009	.009	.009	.009	.009	.010	.010	.010	.010	.010

Table 44.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

ENGLISH MEASURES.

Attache	d)					ASURE				
Ther- momete Fahren-	г		HEI	GHT OF	THE BA	ROMET	ER IN I	NCHES.		
heit.	28.0	28.2	28.4	28.6	28.8	29.0	29.2	29.4	29.6	29.8
F. 25°5	Inch.	Inch.	_	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
26.0	+0.008			, .		+0.008	+0.008	+0.008	+0.008	+0.008
26.5	.007	,		.007	.007	.007	.007	.007	.007	.007
27.0	.003		-	.006	1		.006	.006	.006	.006
27.5	.003			.004			.004	.00.1	.004	.004
-7.5	1 .003	.003	.003	.003	.003	.003	.003	.003	.003	.003
28.0	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002	
28.5	0,000		0.000	0.000	0,000	0.000	0.000	0.000	0.000	+0.002 0.000
29.0	-0.001		-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001
29.5	.002			.002	.002	.002	.002	.002	.002	.002
30.0	.003	.004	.004	.004	.004	,004	.004	.004	.004	.004
30.5	-0.005	-0.005	0.00	0						-
31.0	.006			-0.005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005
31.5	.007	.007		.006	.006	.006	.006	.006	.006	.006
32.0	.009	.009		.007	.008	.008	.008	.008	.008	.008
32.5	.010	.010	1	.010	.010	.009	.009	009	.009	.009
			1	.010	.010	.010	.010	.010	.010	.010
33.0	-0.011	-0.011	-0.011	-0.011	-0.011	-0.012	-0.012	-0.012	-0.012	-0.012
33.5	.012	.012		.013	.013	.013	.013	.013	.013	.013
34.0	.014	.014	.014	.014	.014	.014	.014	.014	.014	.015
34.5	.015	.015	.015	.015	.015	.015	.016	.016	.016	.016
35.0	.016	.016	.016	.017	.017	.017	.017	.017	.017	.017
35.5	-0.017	-0.018	0.070	0						·
36.0	.019	.019	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.019
36.5	.020	.020	.019	.019	.019	.019	.020	.020	.020	.020
37.0	.021	.021	.022	.020	.021	.021	.021	.02 I	.O2 I	.021
37.5	.023	.023	.023	.023	.023	.022	.022	.022	.022	.023
		3	1 1 2	.023	.023	.023	.024	.024	.024	.024
38.0	-0.024	-0.024	-0.024	-0.024	-0.024	-0.025	~0.025	-0.025	-0.025	-0.025
38.5	.025	.025	.025	.026	.026	.026	.026	.026	.027	.027
39.0	.026	.027	.027	.027	.027	.027	.027	.028	.028	.028
39.5	.028	.028	.028	.028	.028	.029	.029	.029	.029	.029
40.0	.029	.029	.029	.030	.030	.030	.030	.030	.031	.031
40.5	-0.030	-0.030	-0.031	0.007			j			1
41.0	.031	.032	.032	-0.031	-0.031	-0.031	-0.031	-0.032 -	-0.032	-0.032
41.5	.033	.033	.032	.032	.032	.033	.033	.033	.033	.033
42.0	.034	.034	.034	.035	.034	.034	.034	.034	.035	.035
42.5	.035	.035	.036	.036	.036	.036	.035	.036	.036	.036
40.					. 330	.030	.037	.037	.037	.037
43.0	-0.036	-0.037	-0.037 -	-0.037	-0.038	-0.038	-0.038 -	-0.038	-0.039	-0.039
43.5	.038	.038	.038	.039	.039	.039	.039	.040	.040	.040
44.0	.039	.039	.040	.040	.040	.040	.041	.041	.041	.042
44.5	.040	.041	.041	.041	.041	.042	.042	.042	.043	.043
45.0	.042	.042	.042	.042	.043	.043	.043	.044	.044	.044
45.5	-0.043	-0.013	-0.043	-0.011	-0.044	-0.014	-0.015	-0.015	0.045	
46.0	.044	.044	.045	.045	.045	.046	.046	.046	-0.045 -	-0.046
46.5	.045	.046	.046	.046	.047	.047	.047	.048	.047	.047
47.0	.047	.047	.047	.048	.048	.048	.049	.049	.049	.048
47.5	.048	.048	.049	.049	.049	.050	.050	.050	.051	.051
48.0	-0.040	-0.050	0.070			-				,00,
48.5	-0.049	-0.050		-0.050 -		-0.051 -				-0.052
49.0	.050	.051	.051	.052	.052	.052	.053	.053	.053	.054
49.5	.053	.052	.052	.053	.053	.054	.054	.054	.055	.055
50.0	.054	.055	.054	.054	.054	.055	.055	.056	.056	.056
				.033	.050	.056	.057	.057	.057	.058

TABLE 44.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

ENGLISH MEASURES.

				ENGLI	O. IVIE	ASURES				
Attached Ther- mometer		,	нею	SHT OF	THE BA	ROMETE	R IN I	NCHES.		
Fahren- heit.	28.0	28.2	28.4	28.6	28.8	29.0	29.2	29.4	29.6	29.8
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
50°5	-0.055	-0.056	-0.056	-0.057	-0.057	-0.057	-0.058	-0.058	-0.059	-0.059
51.0	.057	.057	.058	.058	.058	.059	.059	.060	.060	.060
51.5	.058	.058	.059	.059	.060	.060	.061	.061	.061	.062
52.0 52.5	.059	.061	.061	.062	.061	.063	.063	.064	.064	.064
53.0	-0.062	-0.062	-0.063	-0.063	-0.064	-0.064	-0.064	-0.065	-0.065	-0.066
53.5	.063	.064	.064	.064	.065	.065	.066	.066	.067	.067
54.0	.064	.065	.065	.066	.066	.067	.067	.068	.068	.068
54.5	.066	.066	.067	.067	.067	.068	.068	.069	.069	.070
55.0	.067	.067	.068	.068	.069	.069	.070	.070	.071	.071
55.5	-0.068	-0.069	-0.069	-0.070	-0.070	-0.071	-0.071	-0.072	-0.072	-0.073
56.0	.069	.070	.070	.071	.071	.072	.072	.073	.073	.074
56.5	.071	.071	.072	.072	.073	.073	.074	.074	.075	.075
57.0 57.5	.072	.072	.073	.073	.074	.075 .076	.075	.077	.077	.077
58.0	-0.074	-0.075	-0.076	-0.076	-0.077	-0.077	-0.078	-0.078	-0.079	-0.079
58.5	.076	.076	.077	.077	.078	.078	.079	,080	.080	.081
59.0	.077	.078	.078	.079	.079	.080	.080	.081	.081	.082
59.5 60.0	.078 .080	.079 .080	.079	.080	.081	.081	.082	.082	.083 .084	.083
60.5	-0.081	-0.081	-0.082	-0.083	-0.083	-0.084	-0.084	-0.085	-0.085	-0.086
61.0	.082	.083	.083	.084	.084	.085	.086	.086	.087	.087
61.5	.083	.084	.085	.085	.086	.086	.087	.087	.088	.089
62.0 62.5	.o85 .o86	.085 .086	.086 .087	.o86 .o88	.087 .088	.088	.088	.089	.089	.090
63.0	-0.087	-0.088	-o.o88	-0.089	-0.090	-0.090	-0.091	-0.091	-0.092	-0.093
63.5	.088	.089	.090	.090	.091	.092	.092	.093	.093	.094
64.0	.090	.090	.091	.092	.092	.093	.093	.094	.095	.095
64.5 65.0	.091	.092	.092	.093	.093	.094	.095	.095	.096	.097
		.093	.093	.094	.095	.095				
65.5 66.0	-0.093	-0.094	-0.095	-0.095	-0.096	-0.097	-0.097	-0. 098	-0.099	-0.099 .101
66.5	.095	.095	.096	.097	.097	.098	.099	.099	.100	.101
67.0	.097	.098	.099	.099	.100	.101	.101	.102	.103	.103
67.5	.098	.099	.100	.IOI	.IOI	.102	.103	.103	.104	.105
68.0	-0.100	-0.100	-0.101	-0.102	-0.103	-0.103	-0.104	-0.105	-0.105	-0.106
68.5	.IOI	.102	.102	.103	.104	.105	.105	.106	.107	.107
69.0 69.5	.102	.103	.104	.104	.105 .106	.106	.107	.107	.108	.109
70.0	.105	.104	.105	.107	.108	.109	.109	.110	.111	.112
70.5	-0.106	-0.107	-0.108	-0.108	-0.109	-0,110	-0.111	-0.111	-0.112	-0.113
71.0	.107	.108	.109	OII.	011.	III.	.112	.113	.113	.114
71.5 72.0	.109	.109	.110	.111	.112	.112	.113	.114	.115	.116
72.5	.110	.112	.113	.112	.114	.115	.116	.117	.117	.117
73.0	-0.112	-0.113	-0,114	-0.115	-0.116	-0.116	-0.117	-0.118	-0.119	-0.120
73.5	.114	.114	.115	.116	.117	.118	.118	.119	.120	.121
74.0	.115	.116	.117	.117	.118	.119	.120	.121	.121	.122
74·5 75.0	.117	.117	.110	.119	.119	.120	.121	.123	.123	.124
, 5.0	***/	.110	.119	,120	,		,,,,,,		, , , ,	

Attached Ther- mometer			HEIC	HT OF	THE BA	ROMETE	R IN II	NCHES.		
Fahren- heit.	28.0	28.2	28.4	28 6	28 8	29.0	29.2	29.4	29.6	29.8
F. 75°.5 76.0 76.5 77.0 77.5	Inch0.119 .120 .121 .122 .124	Inch0.119 .121 .122 .123 .125	Inch0.120 .122 .123 .124 .125	Inch0.121 .122 .124 .125 .126	Inch0.122 .123 .125 .126 .127	Inch0.123 .124 .125 .127 .128	Inch0.124 .125 .126 .128 .129	Inch0.125 .126 .127 .129 .130	Inch0.125 .127 .128 .129 .131	Inch0.126 .128 .129 .130 .132
78.0 78.5 79.0 79.5 80.0	-0.125 .126 .127 .129 .130	-0.126 .127 .128 .130	-0.127 .128 .129 .131 .132	-0.128 .129 .130 .131 .133	-0.129 .130 .131 .132 .134	-0.129 .131 .132 .133 .135	-0.130 .132 .133 .134 .136	.133 .134 .135 .136	-0.132 .133 .135 .136	-0.133 .134 .136 .137 .138
80.5 81.0 81.5 82.0 82.5	.132 .134 .135 .136	-0.132 .133 .135 .136 .137	-0.133 .134 .136 .137 .138	-0.134 .135 .137 .138 .139	-0.135 .136 .138 .139 .140	-0.136 .137 .139 .140 .141	-0.137 .138 .139 .141 .142	-0.138 .139 .140 .142 .143	-0.139 .140 .141 .143	-0.140 .141 .142 .144 .145
83.0 83.5 84.0 84.5 85.0	-0.138 .139 .140 .141 .143	-0.139 .140 .141 .142 .144	-0.139 .141 .142 .143 .145	-0.140 .142 .143 .144 .146	-0.141 .143 .144 .145 .147	-0.142 .144 .145 .146 .148	-0.143 .145 .146 .147 .149	-0.144 .146 .147 .148 .150	-0.145 .147 .148 .149 .151	-0.146 .148 .149 .150 .152
85.5 86.0 86.5 87.0 87.5	-0.144 .145 .146 .148	-0.145 .146 .147 .149 .150	-0.146 .147 .148 .150 .151	-0.147 .148 .149 .151 .152	-0.148 .149 .151 .152 .153	-0.149 .150 .152 .153 .154	-0.150 .151 .153 .154 .155	-0.151 .152 .154 .155 .156	-0.152 .153 .155 .156	-0.153 .154 .156 .157 .158
88.0 83.5 89.0 89.5 90.0	-0.150 .151 .153 .154 .155	-0.151 .152 .154 .155 .156	-0.152 .154 .155 .156	-0.153 .155 .156 .157 .158	-0.154 .156 .157 .158 .160	-0.155 .157 .158 .159 .161	-0.157 .158 .159 .160	-0.158 .159 .160 .162 .163	-0.159 .160 .161 .163 .164	-0.160 .161 .162 .164 .165
90.5 91.0 91.5 92.0 92.5	-0.156 .158 .159 .160	-0.157 .159 .160 .161	-0.159 .160 .161 .162 .164	-0.160 .161 .162 .164 .165	-0.161 .162 .163 .165	-0.162 .163 .165 .166	-0.163 .164 .166 .167 .168	-0.164 .166 .167 .168 .169	-0.165 .167 .168 .169	-0.166 .168 .169 .170
93.0 93.5 94.0 94.5 95.0	-0.163 .164 .165 .166	-0.164 .165 .166 .168	-0.165 .166 .168 .169	-0.166 .167 .169 .170	-0.167 .169 .170 .171	-0.168 .170 .171 .172 .174	-0.170 .171 .172 .174 .175	-0.171 .172 .173 .175 .176	-0.172 .173 .175 .176 .177	-0.173 .174 .176 .177 .178
95.5 96.0 96.5 97.0 97.5	-0.169 .170 .171 .173	-0.170 .171 .173 .174 .175	-0.171 .173 .174 .175 .176	-0.173 .174 .175 .176 .178	-0.174 .175 .176 .178	-0.175 .176 .178 .179 .180	-0.176 .177 .179 .180	-0.177 .179 .180 .181 .183	-0.179 .180 .181 .183 .184	-0.180 .181 .182 .184 .185
98.0 98.5 99.0 99.5 100.0	-0.175 .176 .178 .179 .180	-0.176 .178 .179 .180 .182	-0.178 .179 .180 .182 .183	-0.179 .180 .182 .183 .184	-0.180 .181 .183 .184 .185	-0.181 .183 .184 .185 .187	-0.183 .184 .185 .187 .188	-0.184 .185 .187 .188	-0.185 .187 .188 .189	-0.186 .188 .189 .190

TABLE 44.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE

ENGLISH MEASURES.

				EITGE	SH ME	1001120				
Attached Ther- mometer			HEIG	HT OF	THE BA	ROMETE	R IN II	NCHES.		
Fahren- heit.	29.8	30.0	30.2	30.4	30.6	30.8	31.0	31.2	31.4	31.6
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
0.0	+0.078	+0.078	+0.079	+0.079	+0.080	+0.080	+0.081	+0.081	+0.082	+0.082
0.5	+0.076	+0.077	+0.077		+0.078		+0.079	+0.080		+0.081
1.0	.075	.076	.076	.077	.077	.078	.078	.079	.079	.oSo .o7S
1.5 2.0	.074	.074	.075	.075	.074	.075	.077	.077	.076	.077
2.5	.071	.071	.072	.072	.073	.073	.074	.074	.075	.075
3.0	+0.070	+0.070	+0.070	+0.071	+0.071	+0.072	+0.072	+0.073	+0.073	+0.074
3.5	.068	.069	.069	.070	.070	.070	.071	.071	.072	.072
4.0	.067	.067	.068	.068	.069	.069	.070	.070	.070	.071
4.5	.065 .064	.066	.066	.067	.067	.068	.068	.069	.069	.069
5.0		1		_ ~						
5.5 6.0	+0.063 .061	+0.063	+0.064	+0.064	+0.064	+0.065 .063	+0.065	+0.066	+0.066	+0.067 .065
6.5	.060	.060	.062	.061	.062	.062	.062	.063	.063	.064
7.0	.059	.059	.059	.060	.060	.061	.061	.061	.062	.062
7.5	.057	.058	.058	.058	.059	.059	.060	.060	.060	.061
8.0	+0.056	+0.056	+0.057	+0.057	+0.057	+0.058	+0.058	+0.059	+0.059	+0.059
8.5	.055	.055	.055	.056	.056	.056	.057	.057	.058	.058
9.0	.053	.054	.054	.054	.055	.055	.055	.056	.056	.056
9.5 10.0	.052	.052	.053	.053	.053	.054	.054	.054	.055	.055
		-		_					_	i
10.5 11.0	+0.049 .048	+0.049	+0.050 .048	+0.050	+0.050	+0.051 .049	+0.051	+0.051	+0.052	.051
11.5	.046	.047	.047	.047	.048	.048	.048	.049	.049	.049
12.0	.045	.045	.046	.046	.046	.047	.047	.047	.048	.048
12.5	.044	.044	.044	.045	.045	.045	.045	.046	.046	.046
	+0.042		+0.043				+0.044	+0.044		+0.045
13.5	.041	.041	.042	.042	.042	,042	.043	.043	.043	.043
14.0 14.5	.040 .038	.040	.040	.040	.041	.041	.041	.042	.042	.042 .041
15.0	.037	.037	.037	.038	.038	.038	.038	.039	.039	.039
15.5	+0.036	+0.036	+0.036	+0.036	+0.037	+0.037	+0.037	+0.037	+0.037	+0.038
16.0	.034	.034	.035	.035	.035	.035	.036	.036	.036	.036
16.5	.033	.033	.033	.034	.034	.034	.034	.034	.035	.035
17.0	.032	.032	.032	.032	.032	.033	.033	.033	.033	.033
17.5	.030	.030	.031	.031	-					.032
	+0.029	1.	+0.029 .028	+0.029	+0.030	+0.030	+0.030		+0.030	+0.031
18.5	.027	.028	.028	.028	.023	.025	.029	.029	.029	.029
19.5	.025	.025	.025	.025	.025	.026	.026	.026	.026	.026
20.0	.023	.024	.024	.024	.024	.024	.024	.024	.025	.025
20.5	+0.022	+0.022	+0.022	+0.022	+0.023	+0.023	+0.023	+0.023	+0.023	+0.023
21.0	.021	.021	.021	,02 I	.021	.021	.022	.022	.022	.022
21.5	.019	.019	.020	.020	.020	.020	.020	.020	.020	.020
22.0	.018	.018	.018	.017	.017	.019	.019	.019	.017	.019
23.0	1			+0.016	+0.016		+0.016	+0.016	+0.016	+0.016
23.5	+0.015	.014	+0.015	.014	,014	.014	.014	.015	.015	.015
24.0	.013	.013	.013	.013	.013	.013	.013	.013	.013	.013
24.5	.011	.011	.011	.011	.011	.012	.012	.012	.012	.012
25.0	.010	.010	.010	.010	.010	.010	.010	.010	0.10	.010

Attacher Ther- momete			HEI	GHT OF	THE BA	ROMET	ER IN I	NCHES.		
Fahren- heit.		30.0	30.2	30.4	30.6	30.8	31.0	31.2	31.4	31.6
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
25°.5	+0.008		+0.009	+0.009	+0.009	+0.009	+0.009	+0.009	+0.000	+0.009
26.0	.007	.007	.007	.007	.007	.007	.007	.007	.008	.008
26.5 27.0	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006
27.5	.004	.004	.004	.005	.005	,005	.005	.005	.005	.005
-7.5	1 .003	1 .003	.003	.003	1 .003	.003	.003	.003	.003	.003
28.0	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002	+0.002
28.5	0.000	0.000	0,000	0,000	0.000	0.000	0,000	0.000	0.000	0.000
29.0	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001
30.0	.004	.002	.002	.002	.002	.002	.002	.002	.002	.002
		1004	1004	1004		.004	.004	1 .004	.00.4	.004
30.5	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005	-0.005
31.0 31.5	.006	.006	.006	.007	.007	.007	.007	.007	.007	.007
32.0	.003	.009	.009	.009	.009	.008	.008	.008	.008	.008
32.5	.010	.011	.011	.011	.011	.011	.009	010.	.010.	.010.
00.0						1			.011	.011
33.0	-0.012	-0.012	-0.012	-0.012	-0.012	-0.012	-0.012	-0.012	-0.012	-0.013
33.5 34.0	.013	.013	.013	.013	.014	.014	.014	.014	.014	.014
34.5	.015	.015	.015	.015	.015	.015	.015	.015	.015	.015
35.0	.017	.017	.017	.018	.018	.018	.017	.017	.017	.017 .018
25.5										.010
35.5 36.0	-0.019	-0.019	-0.019	-0.019	-0.019	-0.019	-0.019	-0.019	-0.020	-0.020
36.5	.020	.020	.020	.020	.020	.021	.021	.021	.021	.021
37.0	.023	.023	.023	.023	.023	.022	.022	.022	.022	.023
37-5	.024	.024	.024	.024	.025	.025	.025	.025	.025	.024
38.0	0.005	0.006	2 226		((
38.5	-0.025 027	-0.026 .027	-0.026 .027	-0.026 .027	-0.026 .027	-0.026 .028	-0.026 .028	-0.027 .028	-0.027	-0.027
39.0	.028	.028	.028	.029	.029	.020	.029	.029	.028	.028
39.5	.029	.030	.030	.030	.030	.030	.031	.031	.031	.031
40.0	.031	.031	.031	.031	.032	.032	.032	.032	.032	.033
40.5	-0.032	-0.032	-0.033	-0.033	-0.033	-0.033	-0.033	-0.034	-0.024	0.004
41.0	.033	.034	.034	.034	.034	.035	.035	.035	-0.034	-0.034
41.5	.035	.035	.035	.035	.036	.036	.036	.036	.037	.035
42.0	.036	.036	.037	.037	.037	.037	.038	.038	.038	.038
42.5	.037	.038	.038	.038	.038	.039	.039	.039	.040	.040
43.0	-0.039	-0.039	-0.039	-0.040	-0.040	-0.040	-0.040	-0.041	-0.041	-0.041
43.5	.040	.040	.041	.041	.041	.042	.042	.042	.042	.043
44.0	.042	.042	.042	.042	.043	.043	.043	.043	.044	.044
44.5 45.0	.043	.043	.043	.044	.044	.044	.045	.045	.045	.045
	.044	.045	.045	.045	.045	.046	.046	.046	.047	.047
45.5	-0.046		-0.046		-0.047	-0.047	-0.047	-0.048 -	-0.048 -	0.048
46.0 46.5	.047	.047	.048	.048	.048	.049	.049	.049	.049	.050
47.0	.050	.049	.049	.049	.050	.050	.050	.051	.051	.051
47.5	.051	.051	.052	.052	.052	.053	.053	.053	.054	.054
48.0	-0.052	-0.053		i		-0.054		- }	- 1	- 1
48.5	.054	.054	-0.053 - .054	-0.053 -055	-0.054 .055	.055	-0.054 -056	-0.055 - .056	-0.055 - .057	-0.055 .057
49.0	.055	.055	.056	.056	.057	.057	.057	.058	.058	.058
49.5	.056	.057	.057	.058	.058	.058	.059	.059	.059	.060
50.0	.058	.058	.058	.059	.059	.060	.060	.060	.061	.061
						1				

TABLE 44.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

ENGLISH MEASURES.

Attached Thermonder 29.8 30.0 30.2 30.4 30.6 30.8 31.0 31.2 31.4 31.6						SH ME						
Fahren 19.8 30.0 30.2 30.4 30.6 30.8 31.0 31.2 31.4 31.6	Ther-	HEIGHT OF THE BAROMETER IN INCHES.										
50.75	Fahren-	29.8	30.0	30.2	30.4	30.6	30.8	31.0	31.2	31.4	31.6	
S1.0			}		1	1	Į.	1	1		ſ	
\$1.5 .062 .0662 .0663 .0663 .0663 .0665												
\$2.0 .063 .064 .065 .066 .067 .077 .073 .073 .074 .075 .076 .077 .077 .078 .079 .079 .079 .080 .081 .081 .081 .081 .081 .081 .081 .081 .081 .081 .081 .081 .082 .083 .084 .084 .085 .086 .086 .087 .088 .089 .099 .091 .091 .092 .093 .094 .094 .095 .096												
52-5												
\$53.5 .066 .066 .066 .066 .069 .070 .070 .071 .071 .071 .071 .071 .071 .071 .071 .071 .071 .071 .072 .072 .073 .073 .074 .075 .076 .077 .077 .078 .078 .079 .080 .081 .081 .082 .082 .083 .081 .082 .082 .083 .081 .082 .082 .083 .081 .082 .085												
\$3.5	53.0	-0.066	-0.066	-0.067	-0.067	-0.068	-0.068	-0.068	-0.069	-0.069	-0.070	
\$\frac{5}{5}.5 \cdot 0.071 0.072 0.073 0.073 0.074 0.075 0.085	53.5				.069	.069		.070	.070	.071		
55.6	54.0							.071	.072	.072	.073	
\$55.5										.074		
\$6.0	55.0	.071	.072	.072	.073	.073	.074	.074	•075	.075	.075	
56.5 .075 .076 .076 .077 .078 .079 .079 .080 .081 .081 .081 .081 .081 .081 .081 .081 .081 .081 .082 .083 .081 .081 .081 .082 .083 .081 .081 .082 .083 .081 .081 .082 .083 .084 .084 .085	55.5	-0.073	-0.073	-0.074	-0.074				-0.076	-0.076		
\$57.0		.074							.077			
\$7.5					.077		.078		.079			
58.0 -0.079 -0.080 -0.081 -0.081 -0.082 -0.083 -0.084 -0.084 58.5 .081 .081 .082 .083 .084 .084 .085 .085 .085 .085 .085 .085 .085 .086 .086 .086 .086 .086 .086 .086 .086 .086 .087 .083 .084 .085 .086 .086 .086 .087 .088 .089 .089 .090 .090 .087 .088 .089 .090 .090 .091 .091 .092 .093 .090 .091 .091 .092 .093 .093 .090 .091 .091 .092 .093 .093 .093 .094 .094 .095 .095 .096 .097 .097 .098 .0090 .091 .091 .092 .093 .093 .094 .095 .095 .095 .095 .096 .097 .097 .098 .099 <th></th> <td></td> <td></td> <td></td> <td></td> <td></td> <td>.079</td> <td></td> <td></td> <td></td> <td></td>							.079					
58.5	57.5	.078	.078	.079	.079	.080	.051	.081	.082	.082	.083	
59.0	58.0	-0,079	-0.0So	-0.0So	-0.081	-0.081	-0.082	-0.082	-0.083	-0.084	-0.084	
59.5	58.5									.085	.085	
60.0					.084							
60.5	59.5				.085							
61.0	60.0	.085	.085	.086	.086	.087	.087	.088	.089	.089	.090	
61.0	60.5	-0.086	-o.oS7	-0.087	-0.088	-0.088	-0.089	-0.0Sq	-0.000	-0.001	-0.001	
61.5	61.0										1 -	
62.0	61.5	.089	.oS9	.090	.090							
63.0	62.0		.091		.092	.092	.093	.094				
63.5	62.5	.091	.092	.093	.093	.094	.094	.095	.096	.096	.097	
64.0		-0.093	-0.093	-0.094	-0.095	-0.095	-0.096	-0.096	-0.097	-0.09S	-0.098	
64.5	63.5	.094					.097	.098	.098	.099		
65.0 .098 .099 .099 .100 .101 .101 .102 .103 .103 .104 65.5 -0.099 -0.100 -0.101 -0.102 -0.103 -0.103 -0.104 -0.105 -0.105 66.0 .101 .101 .102 .103 .103 .104 .105 .106 .106 .107 .108 .108 .109 .110 .110 .110 .110 .110 .110 .110 .110 .110 .111 .112 .113 .114 .105 .106 .106 .107 .108 .108 .109 .110 .110 .111 .111 .112 .113 .114 .115 .110 .111 .112 .113 .114 .115 .115 .115 .115 .115 .115 .115 .115 .115 .116 .117 .118 .112 .113 .114 .115 .115 .116 .117 .118 .119 .120												
65.5 -0.099 -0.100 -0.101 -0.101 -0.102 -0.103 -0.103 -0.104 -0.105 -0.105 66.0 .101 .102 .103 .103 .104 .105 .106 .106 .107 .108 .108 .109 .108 .108 .109 .110 .110 .111 .112 .113 .114 .115 .106 .106 .107 .108 .108 .109 .110 .110 .111 .112 .113 .114 .115 .116 .106 .107 .108 .108 .109 .110 .111 .111 .112 .113 .114 .115 .116 .110 .111 .112 .113 .114 .115 .115 .115 .115 .115 .115 .115 .115 .115 .115 .116 .117 .118 .119 .120 .121 .121 .121 .121 .122 .123 .124 .125 .125 .121 .									l .	1		
66.0	05.0	.098	.099	.099	.100	.101	.IOI	.102	.103	.103	.10.1	
66.5							-0.103	-0.103			-0.105	
67.0 .103 .104 .105 .106 .106 .107 .108 .108 .109 .110 .110 .111 68.0 -0.106 -0.107 -0.108 -0.109 -0.110 -0.111 -0.112 -0.113 68.5 .107 .108 .109 .110 .110 .111 .112 .113 .114 .115 .113 .114 .115 .115 .115 .115 .115 .116 .117 .118 .119 .112 .113 .114 .115 .116 .117 .118 .119 .120 .121 .121 .121 .118 .119 .120 .121 .122 .123 .124 .125 .126 .127 .128 .129 .129 .120 .121 70.0 .112 .114 -0.114 -0.115 -0.116 -0.117 -0.118 -0.119 -0.120 .121 .122 .122 .123 .124 .122 .123												
67.5 .105 .106 .106 .107 .108 .108 .109 .110 .110 .111 68.0 -0.106 -0.107 -0.108 -0.108 -0.109 -0.110 -0.111 -0.112 -0.113 68.5 .107 .108 .109 .110 .110 .111 .112 .113 .114 .115 .115 .115 .115 .115 .115 .115 .115 .115 .115 .116 .117 .118 .119 .120 .121 .121 .121 .121 .117 .118 .119 .120 .121 .121 .118 .119 .120 .121 .121 .121 .122 .123 .124 .125 .125 .124 .125 .123 .124 .125 .125 .126 .127 .128 .129 .130 70.5 -0.113 -0.114 -0.114 -0.115 -0.116 -0.117 -0.118 -0.119 -0.120												
68.0 -0.106 -0.107 -0.108 -0.108 -0.109 -0.110 -0.110 -0.111 -0.112 -0.113 68.5 .107 .108 .109 .110 .110 .111 .112 .113 .114 .115 .115 .116 .117 .113 .114 .115 .115 .116 .117 .115 .116 .117 .118 .115 .116 .117 .118 .119 .120 .121 .121 .121 .121 .121 .117 .118 .119 .120 .121 .121 .118 .119 .120 .121 .121 .121 .121 .122 .123 .124 .125 .126 .127 .128 .129 .120 .121 .121 .122 .123 .124 .125 .126 .127 .128 .129 .130 .131												
68.5 .107 .108 .109 .110 .110 .111 .112 .113 .113 .114 69.0 .109 .110 .110 .111 .112 .112 .113 .114 .115 .115 .115 .115 .115 .115 .115 .116 .117 .117 .118 .117 .118 .116 .117 .118 .119 .120 .121 .121 .121 .121 .121 .121 .121 .121 .122 .123 .124 .125 .125 .126 .127 .128 .129 .129 .130 .114 .115 .116 .117 .118 .119 .120 .121 .120 .121 .120 .121 .120 .121 .122 .123 .124 .122 .123 .124 .125 .125 .125 .125 .125 .126 .127 .128 .129 .130 .131 70.5 .116 .117<			.100	.100	.10/	.103	.103	109	,110	,110	.111	
69.0	68.0											
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	60.0											
70.0 .112 .112 .113 .114 .115 .115 .116 .117 .117 .118 70.5 -0.113 -0.114 -0.114 -0.115 -0.116 -0.117 -0.117 -0.118 -0.119 -0.120 71.0 .114 .115 .116 .116 .117 .118 .119 .120 .121 .120 .121 .122 .123 .121 .122 .123 .124 .125 .125 72.0 .117 .118 .118 .119 .120 .121 .122 .123 .124 .125 .125 72.0 .118 .119 .120 .121 .122 .123 .124 .125 .125 73.0 -0.120 -0.121 -0.122 -0.123 -0.124 -0.124 -0.125 -0.126 -0.127 73.5 .121 .122 .123 .124 .125 .126 .127 .128 .129 .130												
70.5 -0.113 -0.114 -0.114 -0.115 -0.116 -0.117 -0.117 -0.118 -0.119 -0.120 71.0 .114 .115 .116 .116 .117 .118 .119 .120 .121 .122 .121 71.5 .116 .116 .117 .118 .119 .120 .121 .122 .122 .123 .124 72.0 .117 .118 .118 .119 .120 .121 .122 .122 .123 .124 .125 .125 72.5 .118 .119 .120 .121 .121 .122 .123 .124 .125 .125 73.0 -0.120 -0.120 -0.121 -0.122 -0.123 -0.124 -0.124 -0.125 -0.126 -0.127 73.5 .121 .122 .123 .123 .124 .125 .126 .127 .128 .129 .130 .130 74.5 .1												
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$									· ·			
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					-0.115		-	-0.117				
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$												
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$												
73.5 .121 .122 .123 .123 .124 .125 .126 .127 .127 .128 74.0 .122 .123 .124 .125 .126 .126 .127 .128 .129 .130 74.5 .124 .124 .125 .126 .127 .128 .129 .130 .131		.118										
73.5 .121 .122 .123 .123 .124 .125 .126 .127 .127 .128 74.0 .122 .123 .124 .125 .126 .126 .127 .128 .129 .130 74.5 .124 .124 .125 .126 .127 .128 .129 .130 .131	73.0	-0.120	-0.120	-0.121	-0.122	-0.122	- 0.124	-0 124	-0 725	-0 T26	-0 I27	
74.0												
74.5 .124 .125 .126 .127 .128 .129 .129 .130 .131												
10 10 10 10 10 10 10 10 10 10 10 10 10 1	75.0	.125	.126	.127	.127	.128	.129	.130	.131	.132	.132	

					311 WE	ASURES	•			
Attached Ther- mometer			HEIG	HT OF T	HE BAR	COMETE	R IN IN	CHES.		
Fahren- heit.	29.8	30.0	30.2	30.4	30.6	30.8	31.0	31.2	31.4	31.6
F.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
75°5	-0. 126	-0.127	-0.128	-0.129	-0.130	-0.131	-0.131	-0.132	-0.133	-0.134
76.0	.128	.128	.129	.130	.131	.132	.133	.134	.134	.135
76.5	.129	.130	.131	.132	.132	.133	.134	.135	.136	.137
77.0 77.5	.130	.131	.132	.133	.134	.13 5 .136	.136	.136	.137	.138
78.0	-0.133	-0.134	-0.135	-0.136	-0.137	-0.137	-0.138	-0.139	- 0.140	-0.141
78.5	.134	.135	.136	.137	.138	.139	.140	.141	.142	.142
79.0	.136	.137	.137	.138	.139	.140	.141	.142	.143	.144
79.5	.137	.138	.139	.140	.141	.142	.143	.143	.144	.145
80.0	.138	.139	.140	.141	.142	.143	.144	.145	.146	.147
80.5	-0. 140	-0.141	-0.142	-0.142	-0.143	-0.144		- 0.146	-0.147	-0.148
81.0	.141	.142	.143	.144	.145	.146	.147	.148	.149	.150
81.5	.142	.143	.144	.145	.146	.147	.148	.149	.150	.151
82.0	.144	.145	.146	.147	.148	.149	.149	.150	.151	.152
82.5	.145	.146	.147	.148	.149	.150	.151	.152	.153	.154
83.0	-0.146	-0.147	-0.148	-0.149	-0.150	-0.151	-0.152	-0.153	-0.154	-0.155
83.5	.148	.149	.150	.151	.152	.153	.154	.155	.156	.157
84.0	.149	.150	.151	.152	.153	.154	.155	.156	.157	.158
84.5	.150	.151	.152	.153	.154	.155	.156	.157	.158	.159
85.0	.152	.153	.154	.155	.156	.157	.158	.159	.160	.161
85.5	-0.153	-0.154	-0.155	-0.156	-0.157	- 0.158		- 0.160		-0.162
86.0	.154	.155	.156	.158	.159	.160	.161	.162	.163	.164
86.5	.156	.157	.158	.159	.160	.161	.162	.163	.164	.165
87.0	.157	.158	.159	.160	.161	.162	. 163	.164	.166	.167
87.5	.158	.159	.161	.162	.163	.164	.165	.166	.167	.168
88.0	-0.160	-0.161	-0.162	-0.163	-0.164	-0.165	-0.166	− 0.167	- 0.168	-0. 169
88.5	.161	.162	.163	.164	.165	.166	.168	.169	.170	.171
89.0	.162	.164	.165	.166	.167	.168	.169	.170	.171	.172
89.5	.164	.165	.166	.167	.168	.169	.170	.171	.173	.174
90.0	.165	.166	.167	.168	.170	.171	.172	.173	.174	.175
90.5	-0.166	-0.168	-0.169		-0.171	-0.172			-0.175	-0.176
91.0	.168	.169	.170	.171	.172	.173	.175	.176	.177	.178
91.5	.169	.170	.171	.173	.174	.175	.176	.177	.178	.179
92.0	.170	.172	.173	.174	.175	.176 .178	.177	.178 .180	.180	.182
92.5	.172	.173	.174	.175	.176		.179			
93.0	-0.173	-0.174		-0.177		-0.179		-o.181		-0.184
93.5	.174	.176	.177	.178	.179	.180	.181	.183		.185
94.0	.176	.177	.178	.179	.180	.182	.183	.184		.186
94.5	.177	.178	.179	.181	.182	.183	.184	.185	.187	.188
95.0	.178	.180	.181	.182	.183	.184	.186	.187	.188	.189
95.5 96.0	-0.180 .181	-0.181 .182	-0.182 .184	-0.183 .185	-0.185 .186	-0.186 .187	-0.187 .188	-0.188	-0 189	-0.191 .192
96.5	.182	.184	.185	.186	.187	.189	.190	.190	.192	.193
97.0	.184	.185	.186	.187	.189	.190	.191	.192	.194	.195
97.5	.185	.186	.188	.189	.190	.191	.193	.194	.195	.196
98.0	-0.186	-0.188	-0.189	-0.190	-0.191	-0.193	-0.194	-0.195	-0.196	-0.198
98.5	.188	.189	.190	.192	.193	.194	.195	.197	.198	.199
99.0	.189	.190	.192	.193	.194	.195	.197	.198	.199	.201
99.5	.190	.192	.193	.194	.196	.197	.198	.199	.201	.202
100.0	.192	.193	.194	.196	.197	.198	,200	.201	.202	.203
				1	!			i	L	<u> </u>

Attached Ther-			F	HEIGHT	OF T	не ва	ROME	TER IN	MILL	IMETEI	RS.		
mometer Centi- grade.	440	450	460	470	480	490	500	510	520	530	540	550	560
c.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.
0°0 0.5 1.0 1.5 2.0	0.00 .04 .07 .11	0.00 .04 .07 .11	0.00 .04 .08 .11	0.00 .04 .08 .12	0.00 .04 .08 .12	0.00 .04 .08 .12	0.00 .04 .08 .12 .16	0.00 .04 .08 .12	0.00 .04 .08 .13 .17	0.00 .04 .09 .13	0.00 .04 .09 .13	0.00 .04 .09 .13	0.00 .05 .09 .14
2.5	0.18	0.18	0. 19	0.19	0.20	0.20	0.20	0.21	0.21	0.22	0.22	0.22	0.23
3.0	.22	.22	.23	.23	.24	.24	.24	.25	.25	.26	.26	.27	.27
3.5	.25	.26	.26	.27	.27	.28	.29	.29	.30	.30	.31	.31	.32
4.0	.29	.29	.30	.31	.3I	.32	.33	.33	.34	.35	.35	.36	.37
4.5	.32	.33	.34	.35	.35	.36	.37	.37	.38	.39	.40	.40	.41
5.0	0.36	0.37	0.38	0.38	0.39	0.40	0.41	0.42	0.42	0.43	0.44	0.45	0.46
5.5	.40	.40	.41	.42	.43	.44	·45	.46	.47	.48	48	.49	.50
6.0	.43	.44	.45	.46	.47	.48	·49	.50	.51	.52	·53	.54	.55
6.5	.47	.48	.49	.50	.51	.52	·53	.54	.55	.56	·57	.58	.59
7.0	.50	.51	.53	.54	.55	.56	·57	.58	.59	.61	.62	.63	.64
7.5 8 o 8.5 9.0 9.5	0.54 .57 .61 .65 .68	0.55 .59 .62 .66	0.56 .60 .64 .68	0.58 .61 .65 .69 .73	0.59 .63 .67 .70	0.60 .64 .68 .72 .76	0.61 .65 .69 .73 .77	0.62 .67 .71 .75 .79	0.64 .68 .72 .76 .81	0.65 .69 .73 .78 .82	0.66 .70 .75 .79 .84	0.67 .72 .76 .81 .85	0.69 .73 .78 .82 .87
10.0 10.5 11.0 11.5 12.0	0.72 ·75 ·79 .83 .86	0.73 .77 .81 .84 .88	0.75 .79 .83 .86	0.77 .80 .84 .88 .92	0.78 .82 .86 .90	0.80 .84 .88 .92 .96	0.82 .86 .90 .94 .98	0.83 .87 .91 .96	0.85 .89 .93 .98 1.02	0.86 .91 .95 .99 1.04	0.88 .92 .97 1.01 1.06	0.90 ·94 ·99 1.03 1.08	0.91 .96 1.00 1.05 1.10
13.0	0 93	0.95	0.97	I.00	I.02	1.04	1.06	1.08	1.10	1.12	1.14	1.17	1.19
14.0	1.00	1.03	1.05	I.07	I.10	1.12	1.14	1.16	1.19	1.21	1.23	1.25	1.28
15.0	1.08	1.10	1.12	I.15	I.17	1.20	1.22	1.25	1.27	1.30	1.32	1.34	1.37
16.0	1.15	1.17	1.20	I.23	I.25	1.28	1.30	1.33	1.36	1.38	1.41	1.43	1.46
17.0	1.22	1.25	1.27	I.30	I.33	1.36	1.38	1.41	1.44	1.47	1.50	1.52	1.55
18.0	1.29	1.32	1.35	1.38	1.41	1.44	1.47	1.50	1.52	1.55	1.58	1.61	1.64
19.0	1.36	1.39	1.42	1.45	1.49	1.52	1.55	1.58	1.61	1.64	1.67	1.70	1.73
20.0	1.43	1.47	1.50	1.53	1.56	1.60	1.63	1.66	1.69	1.73	1.76	1.79	1.82
21.0	1.50	1.54	1.57	1.61	1.64	1.67	1.71	1.74	1.78	1.81	1.85	1.88	1.91
22.0	1.58	1.61	1.65	1.68	1.72	1.75	1.79	1.83	1.86	1.90	1.93	1.97	2.01
23.0	1.65	1.68	1.72	1.76	1.80	1.83	1.87	I 9I	1.95	1.98	2.02	2.06	2.10
24.0	1.72	1.76	1.80	1.84	1.87	1.91	1.95	I.99	2.03	2.07	2.11	2.15	2.19
25.0	1.79	1.83	1.87	1.91	1.95	1.99	2.03	2.07	2.11	2.16	2.20	2.24	2.28
26.0	1.86	1.90	1.95	1.99	2.03	2.07	2.11	2.16	2.20	2.24	2.28	2.33	2.37
27.0	1.93	1.98	2.02	2.06	2.11	2.15	2.20	2.24	2.28	2.33	2.37	2.41	2.46
28.0	2.00	2.05	2.09	2.14	2.18	2.23	2.28	2.32	2.37	2.41	2.46	2.50	2.55
29.0	2.07	2.12	2.17	2.22	2.26	2.31	2.36	2.40	2.45	2.50	2.55	2.59	2.64
30.0	2.15	2.19	2.24	2.29	2.34	2.39	2.44	2.49	2.54	2.58	2.63	2.68	2.73
31.0	2.22	2.27	2.32	2.37	2.42	2.47	2.52	2.57	2.02	2.67	2.72	2.77	2.82
32.0	2.29	2.34	2.39	2.44	2.50	2.55	2.60	2.65	2.70	2.76	2.81	2.86	2.91
33.0	2.36	2.41	2 47	2.52	2.57	2.63	2.68	2.73	2.79	2.84	2.89	2.95	3.00
34.0	2.43	2.48	2.54	2.60	2.65	2.71	2.76	2.82	2.87	2.93	2.98	3.04	3.09
35.0	2.50	2.55	2.61	2.67	2.73	2.78	2.84	2.90	2.96	3.01	3.07	3.13	3.18

METRIC MEASURES.

	Н		ог тие в 560 mn		ER	Н	EIGHT O	F ТНЕ Е		ER
Attached Ther- mometer.	0°0	0.2	0°.4	0.6	0°8	0°0	0°2	0°4	0.6	0.8
C. 0° 1 2 3 4	mm. 0.00 .09 .18 .27 .37	mm. 0.02 .11 .20 .29 .38	mm. 0.04 .13 .22 .31 .40	mm. 0.05 .15 .24 .33 .42	mm. 0.07 .16 .26 .35 .44	mm. 0.00 .09 .19 .28	mm. 0.02 .11 .20 .30 .39	mm. 0.04 .13 .22 .32 .41	mm. 0.06 .15 .24 .34 .43	mm. 0.07 .17 .26 .35 .45
5 6 7 8 9	0.46 •55 .64 •73 .82	0.48 •57 •66 •75 •84	0.49 .58 .68 .77 .86	0.51 .60 .69 .79 .88	0.53 .62 .71 .80	0.47 .56 .65 .74 .84	0.48 .58 .67 .76 .86	0.50 .60 .69 .78 .87	0.52 .61 .71 .80 .89	0.54 .63 .73 .82 .91
10	0.91	0.93	0.95	0.97	0.99	0.93	0.95	0.97	0.99	1.00
11	1.00	1.02	1.04	1.06	1.08	1.02	1.04	1.06	1.08	1.10
12	1.10	1.11	1.13	1.15	1.17	1.12	1.13	1.15	1.17	1.19
13	1.19	1.20	1.22	1.24	1.26	1.21	1.23	1.25	1.26	1.28
14	1.28	1.30	1.31	1.33	1.35	1.30	1.32	1.34	1.36	1.37
15	1.37	1.39	1.41	1.42	1.44	1.39	1.41	1.43	1.45	1.47
16	1.46	1.48	1.50	1.51	1.53	1.49	1.50	1.52	1.54	1.56
17	1.55	1.57	1.59	1.61	1.62	1.58	1.60	1.62	1.63	1.65
18	1.64	1.66	1.68	1.70	1.71	1.67	1.69	1.71	1.73	1.75
19	1.73	1.75	1.77	1.79	1.81	1.76	1.78	1.80	1.82	1.84
20	1.82	1.84	1.86	1.88	1.90	1.86	1.87	1.89	1.91	1.93
21	1.91	1.93	1.95	1.97	1.99	1.95	1.97	1.99	2.00	2.02
22	2.01	2.02	2.04	2.06	2.08	2.04	2.06	2.08	2.10	2.11
23	2.10	2.11	2.13	2.15	2.17	2.13	2.15	2.17	2.19	2.21
24	2.19	2.20	2.22	2.24	2.26	2.23	2.24	2.26	2.28	2.30
25	2.28	2.30	2.31	2.33	2.35	2.32	2.34	2.35	2.37	2.39
26	2.37	2.39	2.40	2.42	2.44	2.41	2.43	2.45	2 47	2.48
27	2.46	2.48	2.49	2.51	2.53	2.50	2.52	2.54	2.56	2.58
28	2.55	2.57	2.59	2.60	2.62	2.59	2.61	2.63	2.65	2.67
29	2.64	2.66	2.68	2.69	2.71	2.69	2.71	2.72	2.74	2.76
30	2.73	2.75	2.77	2.78	2.80	2.78	2.80	2.82	2.83	2.85
31	2.82	2.84	2.86	2.87	2.89	2.87	2.89	2.91	2.93	2.94
32	2.91	2.93	2.95	2.97	2.98	2.96	2.98	3.00	3.02	3.04
33	3.00	3.02	3.04	3.06	3.07	3.06	3.07	3.09	3.11	3.13
34	3.09	3.11	3.13	3.15	3.16	3.15	3.17	3.18	3.20	3.22
35	3.18	3.20	3.22	3.24	3.25	3.24	3.26	3.28	3.29	3.31

TABLE 45.

METRIC MEASURES.

	Н		F ТНЕ В 580 m n		ER	Н	EIGHT O	г тне в 90 m n		ER
Attached Ther- mometer.	0.0	0.2	0.4	0 °6	0.8	0.0	0°2	0?4	0.6	0°8
C. O° I 2 3 4	mm. 0.00 .09 .19 .28	mm. 0.02 .11 .21 .30 .40	mm. 0.04 .13 .23 .32 .42	mm. 0.06 .15 .25 .34 .44	mm. 0.08 .17 .27 .36 .45	mm. 0.00 .10 .19 .29 .39	mm. 0.02 .12 .21 .31 .40	mm. 0.04 .13 .23 .33 .42	mm. 0.06 .15 .25 .35 .44	mm. 0.08 .17 .27 .37
5 6 7 8 9	0.47 •57 .66 .76 .85	0.49 •59 •68 •78 •87	0.51 .61 .70 .79 .89	0.53 .62 .72 .81	0.55 .64 .74 .83 .93	0.48 .58 .67 .77 .87	0.50 .60 .69 .79 .89	0.52 .62 .71 .81	0.54 .64 .73 .83 .92	0.56 .65 .75 .85
10 11 12 13 14	0.95 1.04 1.13 1.23 1.32	0.96 1.06 1.15 1.25 1.34	0.98 1.08 1.17 1.27 1.36	1.00 1.10 1.19 1.29 1.38	1.02 1.12 1.21 1.30 1.40	0.96 1.06 1.15 1.25 1.35	0.98 1.08 1.17 1.27 1.37	1.00 1.10 1.19 1.29 1.38	I.02 I.12 I.21 I.31 I.40	1.04 1.14 1.23 1.33 1.42
15 16 17 18	1.42 1.51 1.61 1.70 1.79	1.44 1.53 1.62 1.72 1.81	1.46 1.55 1.64 1.74 1.83	1.47 1.57 1.66 1.76 1.85	1.49 1.59 1.68 1.78 1.87	1.44 1.54 1.63 1.73 1.83	1.46 1.56 1.65 1.75 1.84	1.48 1.58 1.67 1.77 1.86	1.50 1.60 1.69 1.79 1.88	1.52 1.61 1.71 1.81 1.90
20 21 22 23 24	1.89 1.98 2.08 2.17 2.26	1.91 2.00 2.10 2.19 2.28	1.93 2.02 2.11 2.21 2.30	1.95 2.04 2.13 2.23 2.32	1.96 2.06 2.15 2.25 2.34	1.92 2.02 2.11 2.21 2.30	1.94 2.04 2.13 2.23 2.32	1.96 2.06 2.15 2.25 2.34	1.98 2.07 2.17 2.27 2.36	2.00 2.09 2.19 2.28 2.38
25 26 27 28 29	2.36 2.45 2.55 2.64 2.73	2.38 2.47 2.57 2.66 2.75	2.40 2.49 2.58 2.68 2.77	2.41 2.51 2.60 2.70 2.79	2.43 2.53 2.62 2.72 2.81	2.40 2.49 2.59 2.69 2.78	2.42 2.51 2.61 2.70 2.80	2.44 2.53 2.63 2.72 2.82	2.46 2.55 2.65 2.74 2.84	2.48 2.57 2.67 2.76 2.86
30 31 32 33 34	2.83 2.92 3.02 3.11 3.20	2.85 2.94 3.03 3.13 3.22	2.87 2.96 3.05 3.15 3.24	2.88 2.98 3.07 3.16 3.26	2.90 3.00 3.09 3.18 3.28	2.88 2.97 3.07 3.16 3.26	2.90 2.99 3.09 3.18 3.2 8	2.91 3.01 3.11 3.20 3.30	2.93 3.03 3.12 3.22 3.31	2.95 3.05 3.14 3.24 3.33
35	3.30	3.31	3.33	3.35	3.37	3.35	3.37	3.39	3.41	3.43

METRIC MEASURES.

	II		F ТНЕ 1 600 mn	BAROMET	ER	н	EIGHT O	F ТИЕ Е 805 mm		ER
Attached Ther- mometer.	0.0	0.2	0?4	0 .6	0.8	0°0	0°2	0.4	0.6	0°8
C. 0° 1 2 3 4	mm. 0.00 .10 .20 .29	mm. 0.02 .12 .22 .31 .41	mm. 0.04 .14 .24 .33 .43	mm. 0.06 .16 .25 .35 .45		mm. 0.00 .10 .20 .30 .40	nnn. 0.02 .12 .22 .32 .41	mm. 0.04 .14 .24 .34 .43		mm. 0.08 .18 .28 .38
5 6 7 8 9	0.49 .59 .69 .78 .88	0.51 .61 .70 .80	0.53 .63 .72 .82	0.55 .65 .74 .84	0.57 .67 .76 .86	0.49 .59 .69 .79 .89	0.51 .61 .71 .81	0.53 .63 .73 .83 .93	0.55 .65 .75 .85	0.57 .67 .77 .87 .97
10	0.98	1.00	1.02	1.04	1.06	0.99	I.01	1.03	1.05	1.07
11	1.08	1.10	1.12	1.13	1.15	1.09	I.10	1.12	1.14	1.16
12	1.17	1.19	1.21	1.23	1.25	1.18	I.20	1.22	1.24	1.26
13	1.27	1.29	1.31	1.33	1.35	1.28	I.30	1.32	1.34	1.36
14	1.37	1.39	1.41	1.43	1.45	1.38	I.40	1.42	1.44	1.46
15	1.47	1.49	1.51	1.53	1.54	1.48	1.50	1.52	1.54	1.56
16	1.56	1.58	1.60	1.62	1.64	1.58	1.60	1.62	1.64	1.66
17	1.66	1.68	1.70	1.72	1.74	1.68	1.70	1.71	1.73	1.75
18	1.76	1.78	1.80	1.82	1.84	1.77	1.79	1.81	1.83	1.85
19	1.86	1.88	1.90	1.91	1.93	1.87	1.89	1.91	1.93	1.95
20	1.95	1.97	1.99	2.01	2.03	1.97	1.99	2.0I	2.03	2.05
21	2.05	2.07	2.09	2.11	2.13	2.07	2.09	2.1I	2.13	2.15
22	2.15	2.17	2.19	2.21	2.23	2.17	2.19	2.2I	2.23	2.24
23	2.25	2.26	2.28	2.30	2.32	2.26	2.28	2.30	2.32	2.34
24	2.34	2.36	2.38	2.40	2.42	2.36	2.38	2.40	2.42	2.44
25	2.44	2.46	2.48	2.50	2.52	2.46	2.48	2.50	2.52	2.54
26	2.54	2.56	2.58	2.60	2.61	2.56	2.58	2.60	2.62	2.64
27	2.63	2.65	2.67	2.69	2.71	2.66	2.68	2.70	2.71	2.73
28	2.73	2.75	2.77	2.79	2.81	2.75	2.77	2.79	2.81	2.83
29	2.83	2.85	2.87	2.89	2.91	2.85	2.87	2.89	2.91	2.93
30	2.93	2.94	2.96	2.98	3.00	2.95	2.97	2.99	3.01	3.03
31	3.02	3.04	3.06	3.08	3.10	3.05	3.07	3.09	3.11	3.13
32	3.12	3.14	3.16	3.18	3.20	3.15	3.16	3.18	3.20	3.22
33	3.22	3.24	3.25	3.27	3.29	3.24	3.26	3.28	3.30	3.32
34	3.31	3.33	3.35	3.37	3.39	3.34	3.36	3.38	3.40	3.42
35	3.41	3-43	3-45	3-47	3.49	3.44	3.46	3.48	3.50	3.52

TABLE 45.

METRIC MEASURES.

FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	11		F THE B	AROMET.	ER	II		F ТПЕ В 615 m n	BAROMET	ER
Attached Ther- mometer.	0.0	0°2	0.4	0.6	0°.8	0.0	0.2	0°4	0°.6	0°8
c. 0° 1 2 3 4	mm. 0.00 .10 .20 .30 .40	mm. 0.02 .12 .22 .32 .42	mm. 0.04 .14 .24 .34 .44	mm. 0.06 .16 .26 .36 .46	mm. 0.08 .18 .28 .38 .48	mm. 0.00 .10 .20 .30 .40	mm. 0.02 .12 .22 .32 .42	mm. 0.04 .14 .24 .34 .44	nim. 0.06 .16 .26 .36 .46	mm. 0.08 .18 .28 .38 .48
5 6 7 8 9	0.50 .60 .70 .80	0.52 .62 .72 .82 .92	0.54 .64 .74 .84	0.56 .66 .76 .86	0.58 .68 .78 .88 .98	0.50 .60 .70 .80	0.52 .62 .72 .82 .92	0.54 .64 .74 .84 .94	0.56 .66 .76 .86	0.58 .68 .78 .88
10	0.99	1.01	1.03	1.05	1.07	1.00	I.02	1.04	1.06	1.08
11	1.09	1.11	1.13	1.15	1.17	1.10	I.12	1.14	1.16	1.18
12	1.19	1.21	1.23	1.25	1.27	1.20	I.22	1.24	1.26	1.28
13	1.29	1.31	1.33	1.35	1.37	1.30	I.32	1.34	1.36	1.38
14	1.39	1.41	1.43	1.45	1.47	1.40	I.42	1.44	1.46	1.48
15	1.49	1.51	1.53	1.55	1.57	1.50	1.52	1.54	1.56	1.58
16	1.59	1.61	1.63	1.65	1.67	1.60	1.62	1.64	1.66	1.68
17	1.69	1.71	1.73	1.75	1.77	1.70	1.72	1.74	1.76	1.78
18	1.79	1.81	1.83	1.85	1.87	1.80	1.82	1.84	1.86	1.88
19	1.89	1.91	1.93	1.95	1.97	1.90	1.92	1.94	1.96	1.98
20	1.99	2.01	2.03	2.05	2.07	2.00	2.02	2.04	2.06	2.08
21	2.09	2.10	2.12	2.14	2.16	2.10	2.12	2.14	2.16	2.18
22	2.18	2.20	2.22	2.24	2.26	2.20	2.22	2.24	2.26	2.28
23	2.28	2.30	2.32	2.34	2.36	2.30	2.32	2.34	2.36	2.38
24	2.38	2.40	2.42	2.44	2.46	2.40	2.42	2.44	2.46	2.48
25	2.48	2.50	2.52	2.54	2.56	2.50	2.52	2.54	2.56	2.58
26	2.58	2.60	2.62	2.64	2.66	2.60	2.62	2.64	2.66	2.68
27	2.68	2.70	2.72	2.74	2.76	2.70	2.72	2.74	2.76	2.78
28	2.78	2.80	2.82	2.84	2.86	2.80	2.82	2.84	2.86	2.88
29	2.88	2.90	2.91	2.93	2.95	2.90	2.92	2.94	2.96	2.98
30	2.97	2.99	3.01	3.03	3.05	3.00	3.02	3.04	3.06	3.08
31	3.07	3.09	3.11	3.13	3.15	3.10	3.12	3.14	3.16	3.18
32	3.17	3.19	3.21	3.23	3.25	3.20	3.22	3.24	3.26	3.28
33	3.27	3.29	3.31	3.33	3.35	3.30	3.32	3.34	3.36	3.38
34	3.37	3.39	3.41	3.43	3.45	3.40	3.42	3.44	3.46	3.48
35	3.47	3.49	3.51	3.53	3.55	3.49	3.51	3-53	3.55	3.57

	H		F ТНЕ В 320 mn	BAROMET.	ER	II	EIGHT O	F THE B		ER
Attached Ther- mometer.	0°0	0.2	0°4	0.6	0°3	0°0	0°2	0°4	0°.6	0.8
c. 0° 1 2 3 4	mm. 0.00 .10 .20 .30 .40	mm. 0.02 .12 .22 .32 .43	mm. 0.04 .14 .24 .34 .45	mm. 0.06 .16 .26 .36	mm. 0.08 .18 .28 .38 .49	mm. 0.00 .10 .20 .31 .41	mm. 0.02 .12 .22 .33 .43	mm. 0.04 .14 .24 .35 .45	mm. 0.06 .16 .27 .37	mm. 0.08 .18 .29 .39
5 6 7 8 9	0.51 .61 .71 .81	0.53 .63 .73 .83 .93	0.55 .65 .75 .85 .95	0.57 .67 .77 .87 .97	0.59 .69 .79 .89	0.51 .61 .71 .82	0.53 .63 .73 .84 .94	0.55 .65 .75 .86 .96	0.57 .67 .78 .88 .98	0.59 .69 .80 .90
10	1.01	1.03	1.05	1.07	1.09	1.02	1.04	1.06	1.08	I.10
11	1.11	1.13	1.15	1.17	1.19	1.12	1.14	1.16	1.18	I.20
12	1.21	1.23	1.25	1.27	1.29	1.22	1.24	1.26	1.28	I.30
13	1.31	1.33	1.35	1.37	1.39	1.32	1.34	1.37	1.39	I.41
14	1.41	1.43	1.46	1.48	1.50	1.43	1.45	1.47	1.49	I.51
15	1.52	1.54	1.56	1.58	1.60	1.53	1.55	1.57	1.59	1.61
16	1.62	1.64	1.66	1.68	1.70	1.63	1.65	1.67	1.69	1.71
17	1.72	1.74	1.76	1.78	1.80	1.73	1.75	1.77	1.79	1.81
18	1.82	1.84	1.86	1.88	1.90	1.83	1.85	1.87	1.89	1.91
19	1.92	1.94	1.96	1.98	2.00	1.93	1.95	1.97	1.99	2.01
20	2.02	2.04	2.06	2.08	2.10	2.04	2.06	2.08	2.10	2.12
21	2.12	2.14	2.16	2.18	2.20	2.14	2.16	2.18	2.20	2.22
22	2.22	2.24	2.26	2.28	2.30	2.24	2.26	2.28	2.30	2.32
23	2.32	2.34	2.36	2.38	2.40	2.34	2.36	2.38	2.40	2.42
24	2.42	2.44	2.46	2.48	2.50	2.44	2.46	2.48	2.50	2.52
25	2.52	2.54	2.56	2.58	2.60	2.54	2.56	2.58	2.60	2.62
26	2.62	2.64	2.66	2.68	2.70	2.64	2.66	2.68	2.70	2.72
27	2.72	2.74	2.76	2.78	2.80	2.74	2.76	2.78	2.80	2.82
28	2.82	2.84	2.86	2.88	2.90	2.85	2.87	2.89	2.91	2.93
29	2.92	2.94	2.96	2.98	3.00	2.95	2.97	2.99	3.01	3.03
30	3.02	3.04	3.06	3.08	3.10	3.05	3.07	3.09	3.11	3.13
31	3.12	3.14	3.16	3.18	3.20	3.15	3.17	3.19	3.21	3.23
32	3.22	3.24	3.26	3.28	3.30	3.25	3.27	3.29	3.31	3.33
33	3.32	3.34	3.36	3.38	3.40	3.35	3.37	3.39	3.41	3.43
34	3.42	3.44	3.46	3.48	3.50	3.45	3.47	3.49	3.51	3.53
35	3.52	3.54	3.56	3.58	3.60	3.55	3.57	3-59	3.61	3.63

TABLE 45.

METRIC MEASURES.

FOR TEMPERATURES ABOVE 0° CENTIGRADE. THE CORRECTION IS TO BE SUBTRACTED

	н	EIGHT O	F THE В		ER	II	EIGHT O	F ТИЕ В 35 mm		ER ,
Attached Ther- mometer.	0.0	0.2	0°4	0.6	0°8	0:0	0°2	0°4	0.6	0°.8
C. 0° 1 2 3 4	mm. 0.00 .10 .21 .31 .41	mm. 0.02 .12 .23 .33 .43	mm. 0.04 .14 .25 .35 .45	mm. 0.06 .16 .27 .37 .47	mm. 0.08 .19 .29 .39	mm. 0.00 .10 .21 .31 .41	mm. 0.02 .12 .23 .33 .44	mm. 0.04 .15 .25 .35 .46	mm. 0.06 .17 .27 .37 .48	mm. 0.08 .19 .29 .39
5 6 7 8 9	0.51 .62 .72 .82 .92	0.53 .64 .74 .84 .95	0.56 .66 .76 .86	0.58 .68 .78 .88	0.60 .70 .80 .90 I.0I	0.52 .62 .73 .83 .93	0.54 .64 .75 .85 .95	0.56 .66 .77 .87 .97	0.58 .68 .79 .89	0.60 .70 .81 .91
10 11 12 13 14	1.03 1.13 1.23 1.34 1.44	1.05 1.15 1.25 1.36 1.46	1.07 1.17 1.27 1.38 1.48	1.09 1.19 1.29 1.40 1.50	1.11 1.21 1.31 1.42 1.52	1.04 1.14 1.24 1.35 1.45	1.06 1.16 1.26 1.37 1.47	1.08 1.18 1.28 1.39 1.49	1.10 1.20 1.30 1.41 1.51	I.12 I.22 I.33 I.43 I.53
15 16 17 18	1.54 1.64 1.74 1.85 1.95	1.56 1.66 1.77 1.87	1.58 1.68 1.79 1.89 1.99	1.60 1.70 1.81 1.91 2.01	1.62 1.72 1.83 1.93 2.03	1.55 1.66 1.76 1.86 1.96	1.57 1.68 1.78 1.88	1.59 1.70 1.80 1.90 2.01	1.61 1.72 1.82 1.92 2.03	1.63 1.74 1.84 1.94 2.05
20 21 22 23 24	2.05 2.15 2.26 2.36 2.46	2.07 2.17 2.28 2.38 2.48	2.09 2.19 2.30 2.40 2.50	2.11 2.21 2.32 2.42 2.52	2.13 2.24 2.34 2.44 2.54	2.07 2.17 2.27 2.38 2.48	2.09 2.19 2.29 2.40 2.50	2.11 2.21 2.31 2.42 2.52	2.13 2.23 2.34 2.44 2.54	2.15 2.25 2.36 2.46 2.56
25 26 27 28 29	2.56 2.66 2.77 2.87 2.97	2.58 2.68 2.79 2.89 2.99	2.60 2.70 2.81 2.91 3.01	2.62 2.73 2.83 2.93 3.03	2.64 2.75 2.85 2.95 3.05	2.58 2.69 2.79 2.89 2.99	2.60 2.71 2.81 2.91 3.01	2.62 2.73 2.83 2.93 3.03	2.64 2.75 2.85 2.95 3.05	2.66 2.77 2.87 2.97 3.08
30 31 32 33 34	3.07 3.17 3.28 3.38 3.48	3.09 3.19 3.30 3.40 3.50	3.11 3.21 3.32 3.42 3.52	3.13 3.23 3.34 3.44 3.54	3.15 3.25 3.36 3.46 3.56	3.10 3.20 3.30 3.40 3.51	3.12 3.22 3.32 3.42 3.53	3.14 3.24 3.34 3.44 3.55	3.16 3.26 3.36 3.47 3.57	3.18 3.28 3.38 3.49 3.59
35	3.58	3.60	3.62	3.64	3.66	3.61	3.63	3.65	3.67	3.69

SMITHGUNIAN TABLES.

METRIC MEASURES.

FOR TEMPERATURES ABOVE 0° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	II		ғ тне в 640 mm	BAROMET	ER	Н		F THE E 645 mm		ER
Attached Ther- mometer.	0.0	0°2	0.4	0 °6	0.8	0°0	0°2	0°4	0.6	0.8
C. 0° 1 2 3 4	mm. 0.00 .10 .21 .31 .42	mm. 0.02 .13 .23 .33 .44	mm. 0.04 .15 .25 .36 .46	mm. 0.06 .17 .27 .38 .48	mm. 0.08 .19 .29 .40	mm. 0.00 .11 .21 .32 .42	mm. 0.02 .13 .23 .34 .44	mm. 0.04 .15 .25 .36 .46	mm. 0.06 .17 .27 .38 .48	mm. 0.08 .19 .29 .40
5 6 7 8 9	0.52 .63 .73 .84 .94	0.54 .65 .75 .86 .96	0.56 .67 .77 .88 .98	0.59 .69 .79 .90	0.61 .71 .81 .92	0.53 .63 .74 .84 .95	0.55 .65 .76 .86	0.57 .67 .78 .88 .99	0.59 .69 .80 .90	0.61 .72 .82 .93 1.03
10	1.04	1.06	1.09	1.11	1.13	1.05	1.07	1.09	1.12	I.14
11	1.15	1.17	1.19	1.21	1.23	1.16	1.18	1.20	1.22	I.24
12	1.25	1.27	1.29	1.31	1.34	1.26	1.28	1.30	1.32	I.35
13	1.36	1.38	1.40	1.42	1.44	1.37	1.39	1.41	1.43	I.45
14	1.46	1.48	1.50	1.52	1.54	1.47	1.49	1.51	1.53	I.56
15	1.56	1.59	1.61	1.63	1.65	1.58	1.60	1.62	1.64	1.66
16	1.67	1.69	1.71	1.73	1.75	1.68	1.70	1.72	1.74	1.77
17	1.77	1.79	1.81	1.83	1.86	1.79	1.81	1.83	1.85	1.87
18	1.88	1.90	1.92	1.94	1.96	1.89	1.91	1.93	1.95	1.97
19	1.98	2.00	2.02	2.04	2.06	2.00	2.02	2.04	2.06	2.08
20	2.08	2.10	2.13	2.15	2.17	2.10	2.12	2.14	2.16	2.18
21	2.19	2.21	2.23	2.25	2.27	2.20	2.23	2.25	2.27	2.29
22	2.29	2.31	2.33	2.35	2.37	2.31	2.33	2.35	2.37	2.39
23	2.40	2.42	2.44	2.46	2.48	2.41	2.43	2.46	2.48	2.50
24	2.50	2.52	2.54	2.56	2.58	2.52	2.54	2.56	2.58	2.60
25	2.60	2.62	2.64	2.66	2.69	2.62	2.64	2.66	2.69	2.71
26	2.71	2.73	2.75	2.77	2.79	2.73	2.75	2.77	2.79	2.81
27	2.81	2.83	2.85	2.87	2.89	2.83	2.85	2.87	2.89	2.92
28	2.91	2.93	2.95	2.98	3.00	2.94	2.96	2.98	3.00	3.02
29	3.02	3.04	3.06	3.08	3.10	3.04	3.06	3.08	3.10	3.12
30	3.12	3. 14	3.16	3.18	3.20	3.14	3.17	3.19	3.21	3.23
31	3.22	3.24	3.27	3.29	3.31	3.25	3.27	3.29	3.31	3.33
32	3.33	3.35	3.37	3.39	3.41	3.35	3.37	3.39	3.42	3.44
33	3.43	3.45	3.47	3.49	3.51	3.46	3.48	3.50	3.52	3.54
34	3.53	3.55	3.58	3.60	3.62	3.56	3.58	3.60	3.62	3.64
35	3.64	3.66	3.68	3.70	3.72	3.67	3.69	3.71	3.73	3.75

FOR TEMPERATURES ABOVE 0° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	II		F THE 1 550 mr	BAROMET	ER	II		F THE 1 555 m n		ER
Attached Ther- mometer.	0°.0	0°2	0°4	0°6	0°8	0°0	0°2	0°.4	0°6	0.8
C. 0° I 2 3	mm. 0.00 .11 .21 .32 .42	mm. 0.02 .13 .23 .34 .45	mm. 0.04 .15 .25 .36 .47	mm. 0.06 .17 .28 .38 .49	mm. 0.08 .19 .30 .40	mm. 0.00 .11 .21 .32 .43	mm. 0.02 .13 .24 .34 .45	mm. 0.04 .15 .26 .36 .47	mm. 0.06 .17 .28 .39	mm. 0.09 .19 .30 .41
5 6 7 8 9	0.53 .64 .74 .85 .95	0.55 .66 .76 .87 .98	0.57 .68 .78 .89	0.59 .70 .81 .91	0.62 .72 .83 .93	0.53 .64 .75 .85 .96	0.56 .66 .77 .88	0.58 .68 .79 .90	0.60 .71 .81 .92 1.03	0.62 ·73 .83 ·94 I.05
10	1.06	1.08	1.10	1.12	1.14	1.07	1.09	1.11	1.13	1.15
11	1.17	1.19	1.21	1.23	1.25	1.17	1.20	1.22	1.24	1.26
12	1.27	1.29	1.31	1.34	1.36	1.28	1.30	1.32	1.35	1.37
13	1.38	1.40	1.42	1.44	1.46	1.39	1.41	1.43	1.45	1.47
14	1.48	1.50	1.53	1.55	1.57	1.49	1.52	1.54	1.56	1.58
15	1.59	1.61	1.63	1.65	1.67	1.60	1.62	1.64	1.66	1.69
16	1.69	1.72	1.74	1.76	1.78	1.71	1.73	1.75	1.77	1.79
17	1.80	1.82	1.84	1.86	1.88	1.81	1.84	1.86	1.88	1.90
18	1.91	1.93	1.95	1.97	1.99	1.92	1.94	1.96	1.98	2.01
19	2.01	2.03	2.05	2.07	2.10	2.03	2.05	2.07	2.09	2.11
20	2.12	2.14	2.16	2.18	2.20	2.13	2.15	2.18	2.20	2.22
21	2.22	2.24	2.26	2.29	2.31	2.24	2.26	2.28	2.30	2.32
22	2.33	2.35	2.37	2.39	2.41	2.35	2.37	2.39	2.41	2.43
23	2.43	2.45	2.47	2.50	2.52	2.45	2.47	2.49	2.52	2.54
24	2.54	2.56	2.58	2.60	2.62	2.56	2.58	2.60	2.62	2.64
25	2.64	2.66	2.69	2.71	2.73	2.66	2.68	2.71	2.73	2.75
26	2.75	2.77	2.79	2.81	2.83	2.77	2.79	2.81	2.83	2.85
27	2.85	2.87	2.90	2.92	2.94	2.88	2.90	2.92	2.94	2.96
28	2.96	2.98	3.00	3.02	3.04	2.98	3.00	3.02	3.05	3.07
29	3.06	3.08	3.11	3.13	3.15	3.09	3.11	3.13	3.15	3.17
30	3.17	3.19	3.21	3.23	3.25	3.19	3.21	3.24	3.26	3.28
31	3.27	3.30	3.32	3.34	3.36	3.30	3.32	3.34	3.36	3.38
32	3.38	3.40	3.42	3.44	3.46	3.41	3.43	3.45	3.47	3.49
33	3.48	3.51	3.53	3.55	3.57	3.51	3.53	3.55	3.57	3.60
34	3.59	3.61	3.63	3.65	3.67	3.62	3.64	3.66	3.68	3.70
35	3.69	3.71	3.74	3.76	3.78	3.72	3.74	3.76	3.79	3.81

METRIC MEASURES.

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	n	EIGHT O	F THE 1		ER	П		F THE E	BAROMET	ER
Attached Ther- mometer.	0:0	0.2	0.4	0°6	0°8	0°0	0.2	0.4	0.6	0.8
c. 0° t 2 3 4	mm. 0.00 .11 .22 .32 .43	mm. 0.02 .13 .24 .34 .45	1mm. 0.04 .15 .26 .37 .47	mm. 0.06 .17 .28 .39	mm. 0.09 .19 .30 .41	mm. 0.00 .11 .22 .33 .43	mm. 0.02 .13 .24 .35 .46	mm. 0.04 .15 .26 .37 .48	mm. 0.07 .17 .28 .39 .50	mm. 0.09 .20 .30 .41
5 6 7 8 9	0.54 .65 .75 . 8 6 .97	0.56 .67 .78 .88	0.58 .69 .80 .90	0.60 .71 .82 .93 1.03	0.62 •73 •84 •95 1.05	0.54 .65 .76 .87	0.56 .67 .78 .89	0.59 .69 .80 .91	0.61 .72 .82 .93 1.04	0.63 •74 •85 •95 1.06
10 11 12 13 14	1.08 1.18 1.29 1.40 1.51	1.10 1.21 1.31 1.42 1.53	1.12 1.23 1.33 1.44 L55	1.14 1.25 1.36 1.46 1.57	1.16 1.27 1.38 1.48 1.59	1.08 1.19 1.30 1.41 1.52	1.11 1.21 1.32 1.43 1.54	1.13 1.24 1.34 1.45 1.56	1.15 1.26 1.37 1.47 1.58	1.17 1.28 1.39 1.50 1.60
15 16 17 18	1.61 1.72 1.83 1.93 2.04	1.63 1.74 1.85 1.96 2.06	1.66 1.76 1.87 1.98 2.08	1.68 1.78 1.89 2.00 2.11	1.70 1.81 1.91 2.02 2.13	1.63 1.73 1.84 1.95 2.06	1.65 1.76 1.86 1.97 2.08	1.67 1.78 1.88 1.99 2.10	1.69 1.80 1.91 2.01 2.12	1.71 1.82 1.93 2.04 2.14
20 21 22 23 24	2.15 2.26 2.36 2.47 2.58	2.17 2.28 2.38 2.49 2.60	2.19 2.30 2.41 2.51 2.62	2.21 2.32 2.43 2.53 2.64	2.23 2.34 2.45 2.56 2.66	2.17 2.27 2.38 2.49 2.60	2.19 2.29 2.40 2.51 2.62	2.2I 2.32 2.42 2.53 2.64	2.23 2.34 2.45 2.55 2.66	2.25 2.36 2.47 2.57 2.68
25 26 27 28 29	2.68 2.79 2.90 3.00 3.11	2.71 2.81 2.92 3.03 3.13	2.73 2.83 2.94 3.05 3.15	2.75 2.85 2.96 3.07 3.18	2.77 2.88 2.98 3.09 3.20	2.70 2.81 2.92 3.03 3.13	2.73 2.83 2.94 3.05 3.16	2.75 2.85 2.96 3.07 3.18	2.77 2.88 2.98 3.09 3.20	2.79 2.90 3.01 3.11 3.22
30 31 32 33 34	3.22 3.32 3.43 3.54 3.64	3.24 3.35 3.45 3.56 3.67	3.26 3.37 3.47 3.58 3.69	3.28 3.39 3.49 3.60 3.71	3.30 3.41 3.52 3.62 3.73	3.24 3.35 3.46 3.56 3.67	3.26 3.37 3.48 3.59 3.69	3.29 3.39 3.50 3.61 3.71	3.31 3.41 3.52 3.63 3.74	3·33 3·44 3·54 3.65 3.76
35	3.75	3.77	3.79	3.81	3.84	3.78	3.80	3.82	3.84	3.86

TABLE 45.

FOR TEMPERATURES ABOVE 0° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	Ш		тне в 70 mm		Н	EIGHT OF	75 mm		ER	
Attached Ther- mometer.	0°0	0°2	0.4	0.6	0.8	0.0	0.2	0.4	0.6	0°8
C. 0° 1 2 3 4	mm. 0.00 .11 .22 .33 .44	mm. 0.02 .13 .24 .35 .46	mm. 0.04 .15 .26 .37 .48	mm. 0.07 .18 .28 .39 .50	mm. 0.09 .20 .31 .42 .53	mm. 0.00 .11 .22 .33 .44	mm. 0.02 .13 .24 .35 .46	mm. 0.04 .15 .26 .37 .48	mm. 0.07 .18 .29 .40 .51	mm. 0.09 .20 .31 .42 .53
5 6 7 8 9	0.55 .66 .77 .87 .98	0.57 .68 .79 .90	0.59 .70 .81 .92 1.03	0.61 .72 .83 .94 1.05	0.63 •74 •85 •96	0.55 .66 .77 .88 .99	0.57 .68 .79 .90	0.60 .71 .82 .93	0.62 •73 •84 •95 1.06	0.64 •75 •86 •97 1.08
10	1.09	1.11	1.14	1.16	1.18	1.10	1.12	1.14	1.17	1.19
11	1.20	1.22	1.25	1.27	1.29	1.21	1.23	1.25	1.28	1.30
12	1.31	1.33	1.35	1.38	1.40	1.32	1.34	1.36	1.39	1.41
13	1.42	1.44	1.46	1.49	1.51	1.43	1.45	1.47	1.50	1.52
14	1.53	1.55	1.57	1.59	1.62	1.54	1.56	1.58	1.61	1.63
15	1.64	1.66	1.68	1.70	1.72	1.65	1.67	1.69	1.72	1.74
16	1.75	1.77	1.79	1.81	1.83	1.76	1.78	1.80	1.83	1.85
17	1.86	1.88	1.90	1.92	1.94	1.87	1.89	1.91	1.94	1.96
18	1.96	1.99	2.01	2.03	2.05	1.98	2.00	2.02	2.04	2.07
19	2.07	2.09	2.12	2.14	2.16	2.09	2.11	2.13	2.15	2.18
20	2.18	2.20	2.23	2.25	2.27	2.20	2.22	2.24	2.26	2.29
21	2.29	2.31	2.33	2.36	2.38	2.31	2.33	2.35	2.37	2.39
22	2.40	2.42	2.44	2.46	2.49	2.42	2.44	2.46	2.48	2.50
23	2.51	2.53	2.55	2.57	2.59	2.53	2.55	2.57	2.59	2.61
24	2.62	2.64	2.66	2.68	2.70	2.64	2.66	2.68	2.70	2.72
25	2.72	2.75	2.77	2.79	2.81	2.74	2.77	2.79	2.81	2.83
26	2.83	2.85	2.88	2.90	2.92	2.85	2.88	2.90	2.92	2.94
27	2.94	2.96	2.98	3.01	3.03	2.96	2.99	3.01	3.03	3.05
28	3.05	3.07	3.09	3.11	3.14	3.07	3.09	3.12	3.14	3.16
29	3.16	3.18	3.20	3.22	3.24	3.18	3.20	3.23	3.25	3.27
30	3.27	3.29	3.3½	3.33	3.35	3.29	3.31	3.33	3.36	3.38
31	3.37	3.40	3.42	3.44	3.46	3.40	3.42	3.44	3.47	3.49
33	3.48	3.50	3.53	3.55	3.57	3.51	3.53	3.55	3.57	3.60
33	3.59	3.61	3.63	3.66	3.68	3.62	3.64	3.66	3.68	3.71
34	3.70	3.72	3.74	3.76	3.79	3.73	3.75	3.77	3.79	3.81
35	3.81	3.83	3.85	3.87	3.89	3.84	3.86	3.88	3.90	3.92

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	Н	EIGHT O	F THE В		ER	11	EIGHT O	F THE В 8 85 mn		ER
Attached Ther- mometer.	0.0	0.2	0.4	0 °.6	0.8	0:0	0.2	0 °.4	0.6	0.8
c. 0° 1 2 3 4	mm. 0.00 .11 .22 .33 .44	mm. 0.02 .13 .24 .36 .47	mm. 0.04 .16 .27 .38 .49	mm. 0.07 .18 .29 .40 .51	mm. 0.09 .20 .31 .42 .53	mm. 0.00 .II .22 .34 .45	mm. 0.02 .13 .25 .36 .47	mm. 0.04 .16 .27 .38 .49	mm. 0.07 .18 .29 .40 .51	mm. 0.09 .20 .31 .43 .54
5 6 7 8 9	0.56 .67 .78 .89	0.58 .69 .80 .91	0.60 .71 .82 .93 1.04	0.62 .73 .84 .95 1.06	0.64 .75 .87 .98	0.56 .67 .78 .89	0.58 .69 .80 .92 I.03	0.60 .72 .83 .94 1.05	0.63 .74 .85 .96	0.65 .76 .87 .98 I.09
10	I.II	1.13	1.15	1.18	1.20	1.12	1.14	1.16	1.18	1.21
11	I.22	1.24	1.26	1.29	1.31	1.23	1.25	1.27	1.30	1.32
12	I.33	1.35	1.37	1.40	1.42	1.34	1.36	1.38	1.41	1.43
13	I.44	1.46	1.49	1.51	1.53	1.45	1.47	1.50	1.52	1.54
14	I.55	1.57	1.60	1.62	1.64	1.56	1.59	1.61	1.63	1.65
15	1.66	1.68	1.71	1.73	1.75	1.67	1.70	1.72	1.74	1.76
16	1.77	1.79	1.82	1.84	1.86	1.79	1.81	1.83	1.85	1.87
17	1.88	1.91	1.93	1.95	1.97	1.90	1.92	1.94	1.96	1.99
18	1.99	2.02	2.04	2.06	2.08	2.01	2.03	2.05	2.07	2.10
19	2.10	2.13	2.15	2.17	2.19	2.12	2.14	2.16	2.19	2.21
20	2.21	2.24	2.26	2.28	2.30	2.23	2.25	2.27	2.30	2.32
21	2.32	2.35	2.37	2.39	2.41	2.34	2.36	2.39	2.41	2.43
22	2.43	2.46	2.48	2.50	2.52	2.45	2.47	2.50	2.52	2.54
23	2.54	2.57	2.59	2.61	2.63	2.56	2.59	2.61	2.63	2.65
24	2.66	2.68	2.70	2.72	2.74	2.67	2.70	2.72	2.74	2.76
25	2.77	2.79	2.81	2.83	2.85	2.79	2.81	2.83	2.85	2.87
26	2.88	2.90	2.92	2.94	2.96	2.90	2.92	2.94	2.96	2.99
27	2.99	3.01	3.03	3.05	3.07	3.01	3.03	3.05	3.07	3.10
28	3.10	3.12	3.14	3.16	3.18	3.12	3.14	3.16	3.18	3.21
29	3.21	3.23	3.25	3.27	3.29	3.23	3.25	3.27	3.30	3.32
30	3.32	3.34	3.36	3.38	3.40	3.34	3.36	3.38	3.41	3.43
31	3.43	3.45	3.47	3.49	3.51	3.45	3.47	3.49	3.52	3.54
32	3.54	3.56	3.58	3.60	3.62	3.56	3.58	3.61	3.63	3.65
33	3.64	3.67	3.69	3.71	3.73	3.67	3.69	3.72	3.74	3.76
34	3.75	3.78	3.80	3.82	3.84	3.78	3.80	3.83	3.85	3.87
35	3.86	3.89	3.91	3.93	3.95	3.89	3.91	3.94	3.96	3.98

TABLE 45.

FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	11		F ТИЕ В 90 m n	ROMET.	ÐR	п	EIGHT O	F ТПЕ В 95 m n		ER
Attached Ther- mometer.	C°0	0.2	0°4	0.6	0.8	0°.0	0.2	0°4	0.6	0.8
C. 0° 1 2 3 4	mm. 0.00 .11 .23 .34 .45	mm. 0.02 .14 .25 .36 .47	mm. 0.05 .16 .27 .38 .50	mm. 0.07 .18 .29 .41 .52	mm. 0.09 .20 .32 .43 .54	mm. 0.00 .11 .23 .34 .45	mm. 0.02 .14 .25 .36 .48	mm. 0.05 .16 .27 .39 .50	mm. 0.07 .18 .30 .41 .52	mm. 0.09 .20 .32 .43 .54
5 6 7 8 9	0.56 .68 .79 .90	0.59 .70 .81 .92 1.04	0.61 .72 .83 .95	0.63 •74 •86 •97	0.65 •77 .88 •99	0.57 .68 .79 .91	0.59 .70 .82 .93 1.04	0.61 •73 •84 •95	0.64 .75 .86 .98	0.66 •77 •88 •1.00
10	1.13	1.15	1.17	1.19	1.22	1.13	1.16	1.18	1.20	1.22
11	1.24	1.26	1.28	1.31	1.33	1.25	1.27	1.29	1.31	1.34
12	1.35	1.37	1.39	1.42	1.44	1.36	1.38	1.41	1.43	1.45
13	1.46	1.48	1.51	1.53	1.55	1.47	1.50	1.52	1.54	1.56
14	1.57	1.60	1.62	1.64	1.66	1.59	1.61	1.63	1.65	1.68
15	1.69	1.71	1.73	1.75	1.78	1.70	1.72	1.74	1.77	1.79
16	1.80	1.82	1.84	1.87	1.89	1.81	1.83	1.86	1.88	1.90
17	1.91	1.93	1.96	1.98	2.00	1.92	1.95	1.97	1.99	2.01
18	2.02	2.05	2.07	2.09	2.11	2.04	2.06	2.08	2.11	2.13
19	2.13	2.16	2.18	2.20	2.22	2.15	2.17	2.20	2.22	2.24
20	2.25	2.27	2.29	2.31	2.34	2.26	2.29	2.31	2.33	2.35
21	2.36	2.38	2.40	2.43	2.45	2.38	2.40	2.42	2.44	2.47
22	2.47	2.49	2.52	2.54	2.56	2.49	2.51	2.53	2.56	2.58
23	2.58	2.60	2.63	2.65	2.67	2.60	2.62	2.65	2.67	2.69
24	2.69	2.72	2.74	2.76	2.78	2.71	2.74	2.76	2.78	2.80
25	2.81	2.83	2.85	2 87	2.90	2.83	2.85	2.87	2.89	2.92
26	2.92	2.94	2.96	2.99	3.01	2.94	2.96	2.98	3.01	3.03
27	3.03	3.05	3.07	3.10	3.12	3.05	3.07	3.10	3.12	3.14
28	3.14	3.16	3.19	3.21	3.23	3.16	3.19	3.21	3.23	3.25
29	3.25	3.27	3.30	3.32	3.34	3.28	3.30	3.32	3.34	3.37
30	3.36	3.39	3.41	3.43	3.45	3.39	3.41	3.43	3.46	3.48
31	3.48	3.50	3.52	3.54	3.56	3.50	3.52	3.55	3.57	3.59
32	3.59	3.61	3.63	3.65	3.68	3.61	3.64	3.66	3.68	3.70
33	3.70	3.72	3.74	3.77	3.79	3.73	3.75	3.77	3.79	3.81
34	3.81	3.83	3.85	3.88	3.90	3.84	3.86	3.88	3.90	3.93
35	3.92	3.94	3.97	3.99	4.01	3.95	3.97	3.99	4.02	4.04

METRIC MEASURES

FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	Н		ог тне 1 700 mr	BAROMET n.	'ER	II	EIGHT C) F ТИЕ 1 705 mm		ER
Attached Ther- mometer.	0.0	0°2	0°.4	0°.6	0°8	0.0	0°2	0°4	0°6	0.8
c. 0° 1 2 3 4	mm. 0.00 .11 .23 .34 .46	mm. 0.02 .14 .25 .37 .48	mm. 0.05 .16 .27 .39 .50	mm. 0.07 .18 .30 .41 .53	mm. 0.09 .21 .32 .43 .55	mm. 0.00 .12 .23 .35 .46	mm. 0.02 .14 .25 .37 .48	mm. 0.05 .16 .28 .39 .51	mm. 0.07 .18 .30 .41 .53	mm. 0.09 .21 .32 .44 .55
5 6 7 8 9	0.57 .69 .80 .91	0.59 .71 .82 .94 1.05	0.62 •73 •85 •96	0.64 •75 •87 •98	0.66 .78 .89 1.00	0.58 .69 .81 .92 1.04	0.60 .71 .83 .94 1.06	0.62 .74 .85 .97 1.08	0.64 .76 .87 .99	0.67 .78 .90 I.01 I.13
10 11 12 13 14	1.14 1.26 1.37 1.48 1.60	1.16 1.28 1.39 1.51 1.62	1.19 1.30 1.42 1.53 1.64	1.21 1.32 1.44 1.55 1.67	1.23 1.35 1.46 1.57 1.69	1.15 1.26 1.38 1.49 1.61	1.17 1.29 1.40 1.52 1.63	1.20 1.31 1.43 1.54 1.65	1.22 1.33 1.45 1.56 1.68	1.24 1.36 1.47 1.59 1.70
15 16 17 18	1.71 1.82 1.94 2.05 2.17	I.73 I.85 I.96 2.07 2.19	1.76 1.87 1.98 2.10 2.21	1.78 1.89 2.01 2.12 2.23	1.80 1.92 2.03 2.14 2.26	1.72 1.84 1.95 2.07 2.18	1.75 1.86 1.98 2.09 2.20	1.77 1.88 2.00 2.11 2.23	1.79 1.91 2.02 2.14 2.25	1.81 1.93 2.04 2.16 2.27
20 21 22 23 24	2.28 2.39 2.51 2.62 2.73	2.30 2.42 2.53 2.64 2.76	2.32 2.44 2.55 2.67 2.78	2.35 2.46 2.57 2.69 2.80	2.37 2.48 2.60 2.71 2.82	2.30 2.41 2.52 2.64 2.75	2.32 2.43 2.55 2.66 2.78	2.34 2.46 2.57 2.68 2.80	2.36 2.48 2.59 2.71 2.82	2.39 2.50 2.62 2.73 2.84
25 26 27 28 29	2.85 2.96 3.07 3.19 3.30	2.87 2.98 3.10 3.21 3.32	2.89 3.01 3.12 3.23 3.34	2.91 3.03 3.14 3.25 3.37	2.94 3.05 3.16 3.28 3.39	2.87 2.98 3.10 3.21 3.32	2.89 3.00 3.12 3.23 3.35	2.91 3.03 3.14 3.25 3.37	2.94 3.05 3.16 3.28 3.39	2.96 3.07 3.19 3.30 3.41
30 31 32 33 34	3.41 3.53 3.64 3.75 3.87	3.44 3.55 3.66 3.77 3.89	3.46 3.57 3.68 3.80 3.91	3.48 3.59 3.71 3.82 3.93	3.50 3.62 3.73 3.84 3.96	3.44 3.55 3.66 3.78 3.89	3.46 3.57 3.69 3.80 3.92	3.48 3.60 3.71 3.82 3.94	3.51 3.62 3.73 3.85 3.96	3.53 3.64 3.76 3.87 3.98
35	3.98	4.00	4.02	4.05	4.07	4.01	4.03	4.05	4.07	4.10

TABLE 45.

METRIC MEASURES.

FOR TEMPERATURES ABOVE 0° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	111		г тне в. '10 mm		ER	111	EIGHT O	тие в 15 mm		ER
Attached Ther- mometer.	0.0	0.2	0°4	0.6	0.8	0:0	0°2	0.4	0.6	0.8
C. 0° 1 2 3 4	mm. 0.00 .12 .23 .35 .46	mm. 0.02 .14 .26 .37 .49	mm. 0.05 .16 .28 .39 .51	mm. 0.07 .19 .30 .42 .53	mm. 0.09 .21 .32 .44 .56	mm. 0.00 .12 .23 .35 .47	mm. 0.02 .14 .26 .37 .49	mm. 0.05 .16 .28 .40 .51	mm. 0.07 .19 .30 .42 .54	mm. 0.09 .21 .33 .44 .56
5 6 7 8 9	0.58 .70 .81 .93 1.04	0.60 .72 .83 .95	0.63 •74 .86 •97	0.65 .76 .88 1.00	0.67 •79 •90 1.02 1.13	0.58 .70 .82 .93 1.05	0.61 •72 •84 •96	0.63 .75 .86 .98	0.65 •77 .89 1.00 1.12	0.68 .79 .91 1.03 1.14
10 11 12 13 14	1.16 1.27 1.39 1.50 1.62	1.18 1.30 1.41 1.53 1.64	1.20 1.32 1.44 1.55 1.67	1.23 1.34 1.46 1.57 1.69	1.25 1.37 1.48 1.60	1.17 1.28 1.40 1.52 1.63	1.19 1.31 1.42 1.54 1.65	1.21 1.33 1.45 1.56 1.68	1.24 1.35 1.47 1.58 1.70	1.26 1.38 1.49 1.61 1.72
15 16 17 18 19	1.74 1.85 1.97 2.08 2.20	1.76 1.87 1.99 2.10 2.22	1.78 1.90 2.01 2.13 2.24	1.80 1.92 2.04 2.15 2.27	1.83 1.94 2.06 2.17 2.29	1.75 1.86 1.98 2.10 2.21	1.77 1.89 2.00 2.12 2.24	1.79 1.91 2.03 2.14 2.26	1.82 1.93 2.05 2.17 2.28	1.84 1.96 2.07 2.19 2.30
20 21 22 23 24	2.31 2.43 2.54 2.66 2.77	2.33 2.45 2.57 2.68 2.80	2.36 2.47 2.59 2.70 2.82	2.38 2.50 2.61 2.73 2.84	2.40 2.52 2.63 2.75 2.86	2.33 2.44 2.56 2.68 2.79	2.35 2.47 2.58 2.70 2.81	2.37 2.49 2.61 2.72 2.84	2.40 2.51 2.63 2.75 2.86	2.42 2.54 2.65 2.77 2.88
25 26 27 28 29	2.89 3.00 3.12 3.23 3.35	2.91 3.03 3.14 3.25 3.37	2.93 3.05 3.16 3.28 3.39	2.96 3.07 3.19 3.30 3.42	2.98 3.09 3.21 3.32 3.44	2.91 3.02 3.14 3.25 3.37	2.93 3.05 3.16 3.28 3.39	2.95 3.07 3.19 3.30 3.42	2.98 3.09 3.21 3.32 3.44	3.00 3.12 3.23 3.35 3.46
30 31 32 33 34	3.46 3.58 3.69 3.81 3.92	3.48 3.60 3.71 3.83 3.94	3.51 3.62 3.74 3.85 3.97	3.53 3.65 3.76 3.87 3.99	3.55 3.67 3.78 3.90 4.01	3.49 3.60 3.72 3.83 3.95	3.51 3.62 3.74 3.86 3.97	3.53 3.65 3.76 3.88 3.99	3.56 3.67 3.79 3.90 4.02	3.58 3.69 3.81 3.92 4.04
35	4.03	4.06	4.08	4.10	4.13	4.06	4.09	4.11	4.13	4.16

FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	п	IEIGHT (720 mr		ER	I		725 mr	BAROMET	ER
Attached Ther- mometer.	0.0	0°2	0°4	0°6	0°8	0.0	0.2	0°.4	0°6	0°8
C. 0° 1 2 3 4	mm. 0.00 .12 .24 .35 .47	mm. 0.02 .14 .26 .38 .49	mm. 0.05 .16 .28 .40 .52	mm. 0.07 .19 .31 .42 .54	mm. 0.09 .21 .33 .45 .56	mm. 0.00 .12 .24 .36 .47	mm. 0.02 .14 .26 .38	mm. 0.05 .17 .28 .40 .52	mm. 0.07 .19 .31 .43 .54	mm. 0.09 .21 .33 .45 .57
5 6 7 8 9	0.59 .71 .82 .94 1.06	0.61 .73 .85 .96 1.08	0.63 .75 .87 .99	0.66 .78 .89 I.01 I.13	0.68 .80 .92 I.03 I. I5	0.59 .71 .83 .95 1.06	0.62 •73 •85 •97 I.09	0.64 .76 .88 .99	0.66 .78 .90 I.02 I.14	0.69 .80 .92 I.04 I.16
11 12 13 14	1.17 1.29 1.41 1.53 1.64	1.20 1.31 1.43 1.55 1.67	1.22 1.34 1.46 1.57 1.69	1.24 1.36 1.48 1.60 1.71	1.27 1.39 1.50 1.62 1.74	1.18 1.30 1.42 1.54 1.65	1.21 1.32 1.44 1.56 1.68	1.23 1.35 1.47 1.58 1.70	1.25 1.37 1.49 1.61 1.73	1.28 1.39 1.51 1.63 1.75
15 16 17 18 19	1.76 1.88 1.99 2.11 2.23	1.78 1.90 2.02 2.13 2.25	1.81 1.92 2.04 2.16 2.27	1.83 1.95 2.06 2.18 2.30	1.85 1.97 2.09 2.20 2.32	1.77 1.89 2.01 2.13 2.24	1.80 1.91 2.03 2.15 2.27	1.82 1.94 2.05 2.17 2.29	1.84 1.96 2.08 2.20 2.31	1.87 1.98 2.10 2.22 2.34
20 21 22 23 24	2.34 2.46 2.58 2.69 2.81	2.37 2.48 2.60 2.72 2.83	2.39 2.51 2.62 2.74 2.86	2.41 2.53 2.65 2.76 2.88	2.44 2.55 2.67 2.79 2.90	2.36 2.48 2.60 2.71 2.83	2.38 2.50 2.62 2.74 2.85	2.41 2.53 2.64 2.76 2.88	2.43 2.55 2.67 2.78 2.90	2.45 2.57 2.69 2.81 2.92
25 26 27 28 29	2.93 3.04 3.16 3.28 3.39	2.95 3.07 3.18 3.30 3.42	2.97 3.09 3.21 3.32 3.44	3.00 3.11 3.23 3.35 3.46	3.02 3.14 3.25 3.37 3.49	2.95 3.07 3.18 3.30 3.42	2.97 3.09 3.21 3.32 3.44	3.00 3.11 3.23 3.35 3.46	3.02 3.14 3.25 3.37 3.49	3.04 3.16 3.28 3.39 3.51
30 31 32 33 24	3.51 3.63 3.74 3.86 3.98	3.53 3.65 3.77 3.88 4.00	3.56 3.67 3.79 3.91 4.02	3.58 3.70 3.81 3.93 4.05	3.60 3.72 3.84 3.95 4.07	3.53 3.65 3.77 3.89 4.00	3.56 3.68 3.79 3.91 4.03	3.58 3.70 3.82 3.93 4.05	3.60 3.72 3.84 3.96 4.07	3.63 3.75 3.86 3.98 4.10
35	4.09	4.11	4.14	4.16	4.18	4.12	4.14	4.17	4.19	4.21

TABLE 45.

FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н		г тие в 730 m n	AROMETI	ER	HI	EIGHT OF	7 THE B.		ER
Attached Ther- mometer.	0°0	0°2	0 °.4	0°6	0°8	0.0	0°2	0.4	0°.6	0.8
C. 0° 1 2 3 4	mm. 0.00 .12 .24 .36 .48	mm. 0.02 .14 .26 .38 .50	mm. 0.05 .17 .29 .41 .52	mm. 0.07 .19 .31 .43 .55	mm. 0.10 .21 .33 .45 .57	mm. 0.00 .12 .24 .36 .48		mm. 0.05 .17 .29 .41 .53	mm. 0.07 .19 .31 .43 .55	mm. 0.10 .22 .34 .46 .58
5 6 7 8 9	0.60 .71 .83 .95 I.07	0.62 .74 .86 .98	0.64 .76 .88 I.00	0.67 •79 •91 1.02 1.14	0.69 .81 .93 1.05	0.60 .72 .84 .96	0.62 •74 •86 •98	0.65 •77 .89 I.01 I.13	0.67 •79 •91 1.03 1.15	0.70 .82 .94 1.06 1.17
10	I. 19	1.21	1.24	1.26	1.29	1.20	1.22	1.25	1.27	1.29
11	I. 31	1.33	1.36	1.38	1.40	1.32	1.34	1.37	1.39	1.41
12	I. 43	1.45	1.48	1.50	1.52	1.44	1.46	1.49	1.51	1.53
13	I. 55	1.57	1.59	1.62	1.64	1.56	1.58	1.61	1.63	1.65
14	I. 67	1.69	1.71	1.74	1.76	1.68	1.70	1.72	1.75	1.77
15	1.78	1.81	1.83	1.86	1.88	1.80	1.82	1.84	1.87	1.89
16	1.90	1.93	1.95	1.97	2.00	1.92	1.94	1.96	1.99	2.01
17	2.02	2.05	2.07	2.09	2.12	2.04	2.06	2.08	2.11	2.13
18	2.14	2.16	2.19	2.21	2.23	2.15	2.18	2.20	2.23	2.25
19	2.26	2.28	2.31	2.33	2.35	2.27	2.30	2.32	2.35	2.37
20	2.38	2.40	2.42	2.45	2.47	2.39	2.42	2.44	2.46	2.49
21	2.50	2.52	2.54	2.57	2.59	2.51	2.54	2.56	2.58	2.61
22	2.61	2.64	2.66	2.68	2.71	2.63	2.66	2.68	2.70	2.73
23	2.73	2.76	2.78	2.80	2.83	2.75	2.77	2.80	2.82	2.85
24	2.85	2.87	2.90	2.92	2.94	2.87	2.89	2.92	2.94	2.97
25	2.97	2.99	3.02	3.04	3.06	2.99	3.01	3.04	3.06	3.08
26	3.09	3.11	3.13	3.16	3.18	3.11	3.13	3.16	3.18	3.20
27	3.20	3.23	3.25	3.28	3.30	3.23	3.25	3.27	3.30	3.32
28	3.32	3.35	3.37	3.39	3.42	3.35	3.37	3.39	3.42	3.44
29	3.44	3.46	3.49	3.51	3.54	3.46	3.49	3.51	3.54	3.56
30	3.56	3.58	3.61	3.63	3.65	3.58	3.61	3.63	3.65	3.68
31	3.68	3.70	3.72	3.75	3.77	3.70	3.73	3.75	3.77	3.80
32	3.79	3.82	3.84	3.87	3.89	3.82	3.84	3.87	3.89	3.92
33	3.91	3.94	3.96	3.98	4.01	3.94	3.96	3.99	4.01	4.03
34	4.03	4.05	4.08	4.10	4.12	4.06	4.08	4.11	4.13	4.15
35	4.15	4.17	4.20	4.22	4.24	4.18	4.20	4.22	4.25	4.27

METRIC MEASURES.

	11	EIGHT O	г тце в 40 mm		ER	п		F ТПЕ В '45 mm	AROMET	ER
Attached Ther- mometer.	0.0	0.2	0°.4	0.6	0°8	0°0	0°2	0°4	0°6	0.8
C. 0° 1 2 3 4	mm. 0.00 .12 .24 .36 .48	mm. 0.02 .15 .27 .39	mm. 0.05 .17 .29 .41 .53	mm. 0.07 .19 .31 .44	mm. 0.10 .22 .34 .46 .58	mm. 0.00 .12 .24 .37 .49	mm. 0.02 .15 .27 .39 .51	mm. 0.05 .17 .29 .41 .54	mm. 0.07 .19 .32 .44 .56	mm. 0.10 .22 .34 .46 .58
5 6 7 8 9	0.60 .72 .85 .97 1.09	0.63 -75 -87 -99	0.65 .77 .89 1.01	0.68 .80 .92 1.04 1.16	0.70 .82 .94 1.06	0.61 •73 •85 •97	0.63 .75 .88 1.00	0.66 .78 .90 1.02	0.68 .80 .92 1.05	0.71 .83 .95 1.07 1.19
10	1.21	1.23	1.26	1.28	1.30	1.22	1.24	1.26	1.29	1.31
11	1.33	1.35	1.38	1.40	1.42	1.34	1.36	1.38	1.41	1.43
12	1.45	1.47	1.50	1.52	1.54	1.46	1.48	1.51	1.53	1.55
13	1.57	1.59	1.62	1.64	1.66	1.58	1.60	1.63	1.65	1.68
14	1.69	1.71	1.74	1.76	1.78	1.70	1.72	1.75	1.77	1.80
15	1.81	1.83	1.86	1.88	1.90	1.82	1.85	1.87	1.89	1.92
16	1.93	1.95	1.98	2.00	2.03	1.94	1.97	1.99	2.01	2.04
17	2.05	2.07	2.10	2.12	2.15	2.06	2.09	2.11	2.14	2.16
18	2.17	2.19	2.22	2.24	2.27	2.18	2.21	2.23	2.26	2.28
19	2.29	2.31	2.34	2.36	2.39	2.31	2.33	2.35	2.38	2.40
20	2.41	2.43	2.46	2.48	2.51	2.43	2.45	2.47	2.50	2.52
21	2.53	2.55	2.58	2.60	2.63	2.55	2.57	2.59	2.62	2.64
22	2.65	2.67	2.70	2.72	2.75	2.67	2.69	2.72	2.74	2.76
23	2.77	2.79	2.82	2.84	2.87	2.79	2.81	2.84	2.86	2.88
24	2.89	2.91	2.94	2.96	2.99	2.91	2.93	2.96	2.98	3.01
25	3.01	3.03	3.06	3.08	3.11	3.03	3.05	3.08	3.10	3.13
26	3.13	3.15	3.18	3.20	3.22	3.15	3.17	3.20	3.22	3.25
27	3.25	3.27	3.30	3.32	3.34	3.27	3.29	3.32	3.34	3.37
28	3.37	3.39	3.42	3.44	3.46	3.39	3.42	3.44	3.46	3.49
29	3.49	3.51	3.54	3.56	3.58	3.51	3.54	3.56	3.58	3.61
30	3.61	3.63	3.66	3.68	3.70	3.63	3.66	3.68	3.70	3.73
31	3.73	3.75	3.78	3.80	3.82	3.75	3.78	3.80	3.82	3.85
32	3.85	3.87	3.89	3.92	3.94	3.87	3.90	3.92	3.95	3.97
33	3.97	3.99	4.01	4.04	4.06	3.99	4.02	4.04	4.07	4.09
34	4.09	4.11	4.13	4.16	4.18	4.11	4.14	4.16	4.19	4.21
35	4.21	4.23	4.25	4.28	4.30	4.23	4.26	4.28	4.31·	4.33

METRIC MEASURES.

FOR TEMPERATURES ABOVE 0° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	11:		F ТИЕ В 50 mm	AROMETI	ER	н		F ТНЕ В. ' 55 mm	AROMETI	ER
Attached Ther- mom-ter.	0.0	0°2	0°4	0.6	0.8	0.0	0°2	0.4	0°6	8.0
C. 0° 1 2 3 4	min. 0.00 .12 .25 .37 .49	mm. 0.02 .15 .27 .39 .51	mm. 0.05 .17 .29 .42 .54	mm. 0.07 .20 .32 .44 .56	mm. 0.10 .22 .34 .47 .59	mm. 0.00 .12 .25 .37 .49	mm. 0.02 .15 .27 .39 .52	mm. 0.05 .17 .30 .42 .54	mm. 0.07 .20 .32 .44 .57	mm. 0.10 .22 .35 .47 .59
5 6 7 8 9	0.61 •73 .86 .98 1.10	0.64 .76 .88 1.00	0.66 .78 .91 1.03	0.69 .81 .93 1.05	0.71 .83 .95 1.08	0.62 •74 •86 •99	0.64 .76 .89 I.01 I.13	0.67 .79 .91 1.03	0.69 .81 .94 1.06 1.18	0.71 .84 .96 1.08
10	1.22	1.25	1.27	1.30	1.32	1.23	1.26	1.28	1.31	1.33
11	1.35	1.37	1.39	1.42	1.44	1.35	1.38	1.40	1.43	1.45
12	1.47	1.49	1.52	1.54	1.56	1.48	1.50	1.53	1.55	1.58
13	1.59	1.61	1.64	1.66	1.69	1.60	1.62	1.65	1.67	1.70
14	1.71	1.74	1.76	1.78	1.81	1.72	1.75	1.77	1.80	1.82
15	1.83	1.86	1.88	1.91	1.93	1.85	1.87	1.89	1.92	1.94
16	1.96	1.98	2.00	2.03	2.05	1.97	1.99	2.02	2.04	2.07
17	2.08	2.10	2.13	2.15	2.17	2.09	2.12	2.14	2.16	2.19
18	2.20	2.22	2.25	2.27	2.30	2.21	2.24	2.26	2.29	2.31
19	2.32	2.34	2.37	2.39	2.42	2.34	2.36	2.38	2.41	2.43
20	2.44	2.47	2.49	2.52	2.54	2.46	2.48	2.51	2.53	2.56
21	2.56	2.59	2.61	2.64	2.66	2.58	2.61	2.63	2.65	2.68
22	2.69	2.71	2.73	2.76	2.78	2.70	2.73	2.75	2.78	2.80
23	2.81	2.83	2.86	2.88	2.90	2.83	2.85	2.87	2.90	2.92
24	2.93	2.95	2.98	3.00	3.03	2.95	2.97	3.00	3.02	3.05
25	3.05	3.07	3.10	3.12	3.15	3.07	3.09	3.12	3.14	3.17
26	3.17	3.20	3.22	3.24	3.27	3.19	3.22	3.24	3.27	3.29
27	3.29	3.32	3.34	3.37	3.39	3.31	3.34	3.36	3.39	3.41
28	3.41	3.44	3.46	3.49	3.51	3.44	3.46	3.49	3.51	3.53
29	3.54	3.56	3.58	3.61	3.63	3.56	3.58	3.61	3.63	3.66
30	3.66	3.68	3.71	3.73	3.75	3.68	3.71	3.73	3.75	3.78
31	3.78	3.80	3.83	3.85	3.87	3.80	3.83	3.85	3.88	3.90
32	3.90	3.92	3.95	3.97	4.00	3.92	3.95	3.97	4.00	4.02
33	4.02	4.04	4.07	4.09	4.12	4.05	4.07	4.10	4.12	4.14
34	4.14	4.17	4.19	4.21	4.24	4.17	4.19	4.22	4.24	4.27
35	4.26	4.29	4.31	4.33	4.36	4.29	4.31	4.34	4.36	4.39

METRIC MEASURES.

FOR TEMPERATURES ABOVE 0° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	н)F THE 1		ER	II	EIGHT O	F ТПЕ 1 765 mm		ER
Attached Ther- mometer.	0.0	0°2	0.4	0°.6	0°.8	0°0	0°2	0°4	0°6	0.8
c. 0° 1 2 3 4	mm. 0.00 .12 .25 .37 .50	mm. 0.02 .15 .27 .40 .52	mm. 0.05 .17 .30 .42 .55	mm. 0.07 .20 .32 .45 .57	mm. 0.10 .22 .35 .47 .60	mm. 0.00 .13 .25 .37	mm. 0.03 .15 .27 .40	mm. 0.05 .17 .30 .42 .55	mm. 0.07 .20 .32 .45 .57	mm. 0.10 .22 .35 .47
5 6 7 8 9	0.62 .74 .87 .99	0.65 .77 .89 I.02 I.14	0.67 .79 .92 I.04 I.17	0.69 .82 •94 1.07 1.19	0.72 .84 .97 I.09	0.62 .75 .87 1.00	0.65 .77 .90 1.02 1.15	0.67 .80 .92 1.05	0.70 .82 .95 I.07	0.72 .85 .97 1.10
10 11 12 13 14	1.24 1.36 1.49 1.61 1.73	1.26 1.39 1.51 1.64 1.76	1.29 1.41 1.54 1.66 1.78	1.31 1.44 1.56 1.68 1.81	1.34 1.46 1.59 1.71 1.83	1.25 1.37 1.50 1.62 1.75	1.27 1.40 1.52 1.65	1.30 1.42 1.55 1.67 1.80	I.32 I.45 I.57 I.70 I.82	1.35 1.47 1.60 1.72 1.85
15 16 17 18 19	1.86 1.98 2.10 2.23 2.35	1.88 2.01 2.13 2.25 2.38	1.91 2.03 2.15 2.28 2.40	1.93 2.06 2.18 2.30 2.43	1.96 2.08 2.20 2.33 2.45	1.87 1.99 2.12 2.24 2.37	1.89 2.02 2.14 2.27 2.39	1.92 2.04 2.17 2.29 2.42	1.94 2.07 2.19 2.32 2.44	1.97 2.09 2.22 2.34 2.47
20 21 22 23 24	2.47 2.60 2.72 2.84 2.97	2.50 2.62 2.75 2.87 2.99	2.52 2.65 2.77 2.89 3.02	2.55 2.67 2.80 2.92 3.04	2.57 2.70 2.82 2.94 3.07	2.49 2.62 2.74 2.86 2.99	2.52 2.64 2.76 2.89 3.01	2.54 2.66 2.79 2.91 3.04	2.57 2.69 2.81 2.94 3.06	2.59 2.71 2.84 2.96 3.09
25 26 27 28 29	3.09 3.21 3.34 3.46 3.58	3.12 3.24 3.36 3.48 3.61	3.14 3.26 3.39 3.51 3.63	3.16 3.29 3.41 3.53 3.66	3.19 3.31 3.43 3.56 3.68	3.11 3.23 3.36 3.48 3.61	3.14 3.26 3.38 3.51 3.63	3.16 3.28 3.41 3.53 3.66	3.19 3.31 3.43 3.56 3.68	3.21 3.33 3.46 3.58 3.70
30 31 32 33 34	3.71 3.83 3.95 4.07 4.20	3.73 3.85 3.98 4.10 4.22	3.75 3.88 4.00 4.12 4.25	3.78 3.90 4.02 4.15 4.27	3.80 3.93 4.05 4.17 4.29	3.73 3.85 3.98 4.10 4.22	3.75 3.88 4.00 4.13 4.25	3.78 3.90 4.03 4.15 4.27	3.80 3.93 4.05 4.17 4.30	3.83 3.95 4.08 4.20 4.32
35	4.32	4.34	4.37	4.39	4.42	4.35	4.37	4.40	4.42	4.45

TABLE 45.

METRIC MEASURES.

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	II	EIGHT O	F ТПЕ В		ER	II	еі дпт о 7	F ТНЕ В 75 mm		ER
Attached Ther- mometer.	0°0	0°2	0°4	0.6	0.8	0:0	0°2	0°4	0°6	0.8
c. 0° 1 2 3 4	mm. 0.00 .13 .25 .38 .50	mm. 0.03 .15 .28 .40 .53	mm. 0.05 .18 .30 .43 .55	mm. 0.08 .20 •33 •45 •58	mm. 0.10 .23 .35 .48 .60	mm. 0.00 .13 .25 .38 .51	mm. 0.03 .15 .28 .40 .53	mm. 0.05 .18 .30 .43 .56	mm. 0.08 .20 .33 .46 .58	mm. 0.10 .23 .35 .48 .61
5 6 7 8 9	0.63 .75 .88 1.01 1.13	0.65 .78 .90 1.03 1.16	0.68 .80 .93 1.06 1.18	0.70 .83 .95 1.08	0.73 .85 .98 1.11 1.23	0.63 .76 .89 I.01 I.14	0.66 .78 .91 1.04 1.16	0.68 .81 .94 1.06 1.19	0.71 .83 .96 1.09	0.73 .86 .99 I.II I.24
10	1.26	1.28	1.31	1.33	1.36	1.26	1.29	1.31	1.34	1.36
11	1.38	1.41	1.43	1.46	1.48	1.39	1.42	1.44	1.47	1.49
12	1.51	1.53	1.56	1.58	1.61	1.52	1.54	1.57	1.59	1.62
13	1.63	1.66	1.68	1.71	1.73	1.64	1.67	1.69	1.72	1.74
14	1.76	1.78	1.81	1.83	1.86	1.77	1.79	1.82	1.84	1.87
15	1.88	1.91	1.93	1.96	1.98	1.89	1.92	1.94	1.97	2.00
16	2.01	2.03	2.06	2.08	2.11	2.02	2.05	2.07	2.10	2.12
17	2.13	2.16	2.18	2.21	2.23	2.15	2.17	2.20	2.22	2.25
18	2.26	2.28	2.31	2.33	2.36	2.27	2.30	2.32	2.35	2.37
19	2.38	2.41	2.43	2.46	2.48	2.40	2.42	2.45	2.47	2.50
20	2.51	2.53	2.56	2.58	2.61	2.52	2.55	2.57	2.60	2.62
21	2.63	2.66	2.68	2.71	2.73	2.65	2.67	2.70	2.72	2.75
22	2.76	2.78	2.81	2.83	2.86	2.77	2.80	2.83	2.85	2.88
23	2.88	2.91	2.93	2.96	2.98	2.90	2.93	2.95	2.98	3.00
24	3.01	3.03	3.06	3.08	3.11	3.03	3.05	3.08	3.10	3.13
25	3.13	3.16	3.18	3.21	3.23	3.15	3.18	3.20	3.23	3.25
26	3.26	3.28	3.31	3.33	3.36	3.28	3.30	3.33	3.35	3.38
27	3.38	3.41	3.43	3.46	3.48	3.40	3.43	3.45	3.48	3.50
28	3.51	3.53	3.56	3.58	3.60	3.53	3.55	3.58	3.60	3.63
29	3.63	3.65	3.68	3.70	3.73	3.65	3.68	3.70	3.73	3.75
30	3.75	3.78	3.80	3.83	3.85	3.78	3.80	3.83	3.85	3.88
31	3.88	3.90	3.93	3.95	3.98	3.90	3.93	3.95	3.98	4.00
32	4.00	4.03	4.05	4.08	4.10	4.03	4.05	4.08	4.10	4.13
33	4.13	4.15	4.18	4.20	4.23	4.15	4.18	4.20	4.23	4.25
34	4.25	4.28	4.30	4.33	4.35	4.28	4.30	4.33	4.35	4.38
35	4.38	4.40	4.43	4.45	4.48	4.40	4.43	4.45	4.48	4.50

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

METRIC MEASURES.

FOR TEMPERATURES ABOVE O' CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	,,,	TELCUT (тие н		T.O.					
			780 mr		EK	"		785 mr	BAROMET n.	ER
Attached Ther- mometer.	0.0	0°2	0 °.4	0°6	0°8	0°0	0°2	0°4	0°6	0.8
C. 0° 1 2 3 4	mm. 0.00 .13 .25 .38 .51	mm. 0.03 .15 .28 .41 .53	mm. 0.05 .18 .31 .43 .56	mm. 0.08 .20 ·33 .46 ·59	mm. 0.10 .23 .36 .48 .61	mm. 0.00 .13 .26 .38 .51	mm. 0.03 .15 .28 .41 .54	mm. 0.05 .18 .31 .44 .56	mm. 0.08 .21 .33 .46 .59	mm. 0.10 .23 .36 .49 .62
5 6 7 8 9	0.64 .76 .89 1.02	0.66 .79 .92 I.04 I.17	0.69 .81 .94 1.07 1.20	0.71 .84 .97 1.09	0.74 .87 .99 1.12 1.25	0.64 .77 .90 1.02 1.15	0.67 .79 .92 1.05 1.18	0.69 .82 .95 I.08	0.72 .85 .97 I.10 I.23	0.74 .87 I.00 I.13 I.25
10 11 12 13 14	1.27 1.40 1.53 1.65 1.78	1.30 1.42 1.55 1.68 1.81	1.32 1.45 1.58 1.70 1.83	1.35 1.48 1.60 1.73 1.86	1.37 1.50 1.63 1.75 1.88	1.28 1.41 1.54 1.66 1.79	1.31 1.43 1.56 1.69 1.82	1.33 1.46 1.59 1.71 1.84	1.36 1.48 1.61 1.74 1.87	1.38 1.51 1.64 1.77 1.89
15 16 17 18	1.91 2.03 2.16 2.29 2.41	1.93 2.06 2.19 2.31 2.44	1.96 2.08 2.21 2.34 2.46	1.98 2.11 2.24 2.36 2.49	2.01 2.13 2.26 2.39 2.51	1.92 2.05 2.17 2.30 2.43	1.94 2.07 2.20 2.33 2.45	1.97 2.10 2.22 2.35 2.48	2.00 2.12 2.25 2.38 2.51	2.02 2.15 2.28 2.40 2.53
20 21 22 23 24	2.54 2.67 2.79 2.92 3.05	2.57 2.69 2.82 2.94 3.07	2.59 2.72 2.84 2.97 3.10	2.62 2.74 2.87 3.00 3.12	2.64 2.77 2.89 3.02 3.15	2.56 2.68 2.81 2.94 3.07	2.58 2.71 2.84 2.96 3.09	2.61 2.73 2.86 2.99 3.12	2.63 2.76 2.89 3.01 3.14	2.66 2.79 2.91 3.04 3.17
25 26 27 28 29	3.17 3.30 3.42 3.55 3.68	3.20 3.32 3.45 3.58 3.70	3.22 3.35 3.47 3.60 3.73	3.25 3.37 3.50 3.63 3.75	3.27 3.40 3.53 3.65 3.78	3.19 3.32 3.45 3.57 3.70	3.22 3.34 3.47 3.60 3.73	3.24 3.37 3.50 3.62 3.75	3.27 3.40 3.52 3.65 3.78	3.29 3.42 3.55 3.67 3.80
30 31 32 33 34	3.80 3.93 4.05 4.18 4.31	3.83 3.95 4.08 4.21 4.33	3.85 3.98 4.11 4.23 4.36	3.88 4.00 4.13 4.26 4.38	3.90 4.03 4.16 4.28 4.41	3.83 3.95 4.08 4.21 4.33	3.85 3.98 4.11 4.23 4.36	3.88 4.00 4.13 4.26 4.39	3.90 4.03 4.16 4.28 4.41	3.93 4.06 4.18 4.31 4.44
35	4.43	4.46	4.48	4.51	4.53	4.46	4.49	4.51	4.54	4.56

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE O° CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

	D		F ТНЕ 1 790 mn		ER	Н		F THE 1	BAROMET	ER
Attached Ther- mometer.	0.0	0°2	0°4	0.6	0.8	0°0	0°2	0°4	0.6	0°8
C. 0° I 2 3 4	nini. 0.00 .13 .26 .39	mm. 0.03 .15 .28 .41 .54	mm. 0.05 .18 .31 .44 .57	mm. 0.08 .21 .34 .46	mm. 0.10 .23 .36 .49 .62	mm. 0.00 .13 .26 .39 .52	mm. 0.03 .16 .29 .42 .55	mm. 0.05 .18 .31 .44 .57	mm. 0.08 .21 .34 .47	mm. 0.10 .23 .36 .49 .62
5 6 7 8 9	0.64 .77 .90 1.03 1.16	0.67 .80 .93 1.06 1.19	0.70 .83 .95 1.08	0.72 .85 .98 I.II I.24	0.75 .88 1.01 1.13 1.26	0.65 .78 .91 1.04 1.17	0.67 .80 .93 1.06	0.70 .83 .96 I.09 I.22	0.73 .86 .99 I.12 I.24	0.75 .88 I.01 I.14 I.27
10	1.29	1.31	1.34	1.37	1.39	1.30	1.32	1.35	1.37	1.4e
11	1.42	1.44	1.47	1.49	1.52	1.43	1.45	1.48	1.50	1.53
12	1.55	1.57	1.60	1.62	1.65	1.56	1.58	1.61	1.63	1.66
13	1.67	1.70	1.73	1.75	1.78	1.68	1.71	1.74	1.76	1.79
14	1.80	1.83	1.85	1.88	1.91	1.81	1.84	1.87	1.89	1.92
15	1.93	1.96	1.98	2.01	2.03	1.94	1.97	1.99	2.02	2.05
16	2.06	2.09	2.11	2.14	2.16	2.07	2.10	2.12	2.15	2.18
17	2.19	2.21	2.24	2.26	2.29	2.20	2.23	2.25	2.28	2.30
18	2.32	2.34	2.37	2.39	2.42	2.33	2.36	2.38	2.41	2.43
19	2.44	2.47	2.50	2.52	2.55	2.46	2.49	2.51	2.54	2.56
20	2.57	2.60	2.62	2.65	2.67	2.59	2.61	2.64	2.67	2.69
21	2.70	2.73	2.75	2.78	2.80	2.72	2.74	2.77	2.79	2.82
22	2.83	2.85	2.88	2.91	2.93	2.85	2.87	2.90	2.92	2.95
23	2.96	2.98	3.01	3.03	3.06	2.98	3.00	3.03	3.05	3.08
24	3.08	3.11	3.14	3.16	3.19	3.10	3.13	3.16	3.18	3.21
25	3.21	3.24	3.26	3.29	3.31	3.23	3.26	3.28	3.31	3.34
26	3.34	3.37	3.39	3.42	3.44	3.36	3.39	3.41	3.44	3.46
27	3.47	3.49	3.52	3.54	3.57	3.49	3.52	3.54	3.57	3.59
28	3.60	3.62	3.65	3.67	3.70	3.62	3.64	3.67	3.70	3.72
29	3.72	3.75	3.77	3.80	3.83	3.75	3.77	3.80	3.82	3.85
30	3.85	3.88	3.90	3.93	3.95	3.88	3.90	3.93	3.95	3.98
31	3.98	4.00	4.03	4.06	4.08	4.00	4.03	4.06	4.08	4.11
32	4.11	4.13	4.16	4.18	4.21	4.13	4.16	4.18	4.21	4.24
33	4.23	4.26	4.29	4.31	4.34	4.26	4.29	4.31	4.34	4.36
34	4.36	4.39	4.41	4.44	4.46	4.39	4.42	4.44	4.47	4.49
35	4.49	4.51	4.54	4.57	4.59	4.52	4.54	4.57	4.59	4.62

SMIT ISCNIAN TABLES.

REDUCTION OF THE MERCURIAL COLUMN TO STANDARD TEMPERATURE.

ENGLISH MEASURES

Table reconstructed from Table 44 to adapt it to U-shaped manometers with brass scales.

ed eter		Differe	NCE IN	HEIGHT	OF THE 1	WO COL	IIMNS I	F THE		AIC
Attached thermometer Fahrenheit		1	DIFF.	ERENCE	OF THEI	R READII	NGS, IN I	NCHES.	ALGEBR	A1C
	1	2	3	4	5	6	7	8	9	10
F. 0	Inch. +0.003	Inch.	Inch. +0.008	Inch. +0.010	Inch. +0.013	Inch.	Inch.	Inch.	Inch.	Inch.
2	+0.002		+0.007	'		1	1		+0.023	+0.026
4 6	.002	.004	.007			+0.015	+0.017	+0.019 810.	+0.022 0.20	+0.024
8	.002	, ,				.012	.015	.017	.019	.021
10	.002	.003			1	110.	.013	.015	.017	.019
12	+0.002	+0.003	+0.005	+0.006	+0.008	+0.009		+0.012		
14 16	100.	.003	.004	.005	.007	.008	.009	.011	+0.014	+0.015
18	100.	.002	0	.005	.006	.007	.008	.009	.010	.012
20	.001	.002		.003		.005	.006	.006	.009	.010
22	+0.001	+0.001	+0.002		+0.003	+0.004	+0.004	+0.005	+0.005	+0.006
24 26	.000	100.	100.	.002	.002	.002	.003	.003	.004	.004
28	.000	.000	.000	.000	.000	.000	.002	.002	.002	.003
30	.000	.000	.000	001	001	001	100.—	001	001	001
32	0.000	-0.001	-0.001	-0.001	-0.002	-0.002	-0.002	-0.003	-0.003	-0.003
34 36	100.	100.	.002	.002	.003	.003	.004	.004	.005	.005
38	100.	.002	.003	.003	.004	.005	.005	.005	.006	.007
40	100.	.002	.003	.004	.005	.006	.007	.008	.009	.010
42 44	100.001	-0.002 .003	-0.004 .004	-0.005	-0.006	-0.007	-0.009	-0.010	-0.011	-0.012
46	.002	.003	.005	.006	.007	.008	.010.	.013	.012	.014
48 50	.002	.004	.005	.007	.009	.011	.012	.014	.014	.010
52		1	.006	.008	.010	.012	.014	.016	.018	.019
54	.002	-0.004 .005	-0.006 .007	-0.008 .009	110.0—	-0.013 .014	-0.015 -016	-0.017	-0.019	-0.021
56	.002	.005	.007	.010	.012	.015	.017	.018	.021	.023
58 60	.003	.005	.008	110.	.013	.016	.019	.021	.024	.027
62	-0.003	-0.006			1	.017	.020	.023	.025	.028
64	.003	.006	-0.009	-0.012	-0.015 -0.016	-810.0—	-0.021 -	-0.024 .026	-0.027 -029	-0.030
66 68	.003	.007	.010	.014	.017	.020	.024	.027	.031	.032
70	.004	.007	110.	.014	.018	.021	.025	.028	.032	.036
72	-0.004	-0.008	-0.012	-0.016	-0.020	-0.024	-0.027	1)
74	.004	.008	.012	.016	.020	.025	.029	-0.031 -	-0.035 .037	-0.039 .041
76 78	.004	.009	.013	.017	.021	.026	.030	.034	.038	.043
80	.005	.009	.014	.019	.023	.027	.031	.036	.040	.045
82	-0.005	-0.010	-0.014	-0.019	-0.024	-0.029	-0.034			-0.048
84 86	.005	.010	.015	.020	.025	.030	.035	.040	.045	.050
88	.005	010.	.016	.021	.026	.031	.036	.042	.047	.052
90	.006	110.	.017	.022	.028	.033	.039	.043	.050	.053
92	-0.006	-0.011	-0.017	-0.023	-0.029	-0.034	-0.040	-0.046	-0.052 -	-0.057
94 96	.006	.012	.018	.024	.030	.035	.041	.047	.053	.059
98	.006	.013	.019	.025	.030	.036	.043	.049	.055	.063
100	.006	.013	.019	.026	.032	.039	.045	.052	.058	.064

REDUCTION OF THE MERCURIAL COLUMN TO STANDARD TEMPERATURE.

ENGLISH MEASURES

Table reconstructed from Table 44 to adapt it to U-shaped manometers with brass scales.

Attached thermometer Fahrenheit	DIFFERENCE IN HEIGHT OF THE TWO COLUMNS, I. E., THE ALGEBRAIC DIFFERENCE OF THEIR READINGS, IN INCHES. 11 12 13 14 15 16 17 18 19 20												
Atta therm Fahr	11	12	13	14	15	16	17	18	19	20			
F.0°	Inch. +0.029	Inch. +0.031	Inch. +0.034	Inch. +0.037	Inch. +0.039	Inch. +0.042	Inch. +0.044	Inch. +0.047	Inch. +0.050	Inch. +0.052			
2	+0.027	+0.029	+0.031	+0.034	+0.036	+0.039	+0.041	+0.044	+0.046	+0.049			
4	.025	.027	.029	.031	.033	.036	.038	.040	.043	.045			
6	.023	.025	.027	.029	.031	.033	.035	.037	.039	.041			
10 8	.021	.023	.025	.026 .024	.028 .025	.030 .027	.032	.034	.036	.038 .034			
12	+0.017	+0.018	+0.020	+0.021	+0.023	+0.024	+0.026	+0.027	+0.029	+0.030			
14	.015	.016	.017	.018	.020	.021	.023	.024	.025	.027			
16	.013	.014	.015	.016	.017	.019	.020	.021	.022	.023			
18	.011	.012	.013	.014	.015	.016	.016	.017	.018	.019			
20	.009	.009	.010	.011	.012	.013	.013	.014	.015	.016			
22	+0.007	+0.007	+0.008	+0.008	+0.009	+0.010	+0.010	110.0+	+0.011	+0.012			
24 26	.005	.005	.006	.006	.006	.007	.007	.004	.005	.008			
28	.003	.003	.003	.004	100.	100.	.001	100.	100.	.003			
30	0.001	-0.002	-0.002	-0.002	0.002	-0.002	0.002	-0.002	0.002	0.002			
32	0.003	-0.004	-0.004	-0.004	-0.005	-0.005	-0.005	-0.006	-0.006	-0.006			
34	.005	.006	.007	.007	.008	.008	.008	.009	.009	.010			
36	.007	.008	.009	.009	.010	.011	.011	.012	.013	.013			
38	.009	.010	.011	.012	.013	.014	.014	.015	.016	.017			
40	.011	.012	.013	.015	.016	.017	.018	.019	.020	.021			
42		-0.015	-0.016	-0.017	-0.018	-0.020	0.021	-0.022	-0.023	0.024			
44	.015	.017	.018	.019	.021	.022	.024	.025	.026	.028			
46 48	.017	.019	.020	.022	.024	.025	.030	.032	.030	.031			
50	.021	.023	.025	.023	.029	.031	.033	.035	.037	.039			
52	-0.023	-0.025	-0.027	-0.030	-0.032	-0.034	-0.036	-0.038	0.040	-0.042			
54	.025	.028	.030	.032	.034	.037	.039	.041	.014	.046			
56	.027	.030	.032	.035	.037	.040	.042	.045	.047	.050			
58	.029	.032	.035	.037	.040	.043	.045	.048	.051	.053			
60	.031	.034	.037	.040	.042	.045	.048	.051	.054	.057			
62	-0.033	-0.036	-0.039	0.042	-0.045	-0.048	-0.051	-0.054	-0.057	-0.060			
64	.035	.038	.042	.045	.048	.051	.054	.058	.061	.064			
66 68	.037	.041	.044	.048	.051	.054 .057	.057	.061	.064 .068	.068 .071			
70	.039	.043	.046	.050 .052	.053 .056	.060	.064	.067	.071	.075			
72	0.043	-0.047	-0.051	-0.055	-0.059	-0.063	-o.o67	-0.071	-0.075	-o.o78			
	.043	.049	.053	.057	.061	.065	.070	.074	.078	.082			
74 76	.047	.051	.056	.060	.064	.068	.073	.077	.081	.086			
78	.049	.054	.058	.062	.067	.071	.076	.080	.085	.089			
80	.051	.056	.060	.065	.070	.074	.079	.084	.088	.093			
82		-0.058	-0.063	-o.o67	-0.072		-0.082	-0.087		-0.096			
84	.055	.060		.070	.075	.080	.085 .088	.090	.095 .098	.100			
\$ 6 88	.057	.062	.067	.073	.080	.083 .086	.000	.093 .096	.102	.104			
90	.059 .061	.066	.072	.075 .078		.089	.091	.100	.105	.111			
92	-0.063	-0.069	-0.074	-0.080	-0.086	0.092	-0.097	-0.103	-0.109	-0.114			
94	.065	.071	.077	.083	.089	.095	.100	.106	.112	.118			
96	.067	.073	.079	.085	.091	.097	.103	.109	.115	.122			
98	.069	.075	.081	.088	.094	.100	.106	.113	.119	.125			
100	.071	.077	.084	.090	.097	.103	.109	.116	.122	.129			

REDUCTION OF THE MERCURIAL COLUMN TO STANDARD TEMPERATURE.

METRIC MEASURES

Table reconstructed from Table 45 to adapt it to U-shaped manometers with brass scales. For temperatures above 0°C., the correction is to be subtracted; for temperatures below, added.

Attached thermometer	Dı	FFERE	NCE IN	HEIG DIFFER	HT OF	THE T	WO COI	LUMNS,	, I. E., 5 (MM.)	THE A	LGEBR	AIC
	20	40	60	80	100	120	140	160	180	200	220	240
C.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.
0°	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
2	.0	0.	.0	.0	.0	.0	.0	.I	.I	. I	.I	.I
3	.0	0.	.0	.0 .1	0. I.	I. I.	.1	.I	ı.	1.	.I	·I
4	1 .0	.0	.0	.1	.1	• 1	.I	.I	1.	1.	.I	.2
5	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0,2	0.2	0.2
6	.0	.0	1.	.1	ı.	.1	.1	.2	.2	.2	.2	.2
7 8 .	.0	.0	.1	ı.	.I	1.	.2	.2	.2	.2	-3	-3
	.0	.I	.I	. I	1.	.2	.2	.2	.2	-3	•3	-3
9	.0	1.	ı.	.I	Ι.	.2	.2	.2	-3	•3	•3	-4
10	0.0	0.1	0.1	0.1	0.2	0.2	0.2	0.3	0.3	0.3	0.4	0.4
11	.0	.I.	1.0	.1	.2	.2	-3	-3	-3	.4	•4	0.4
12	.0	.1	.I	.2	.2	.2	•3	-3	.4	.4	-4	.5
13	.0	.I	.I	.2	.2	.3	.3	.3	-4	.4	.5	.5
14	.0	.1	.I	.2	.2	.3	.3	-4	.4	.5	·š	·š
15	0.0	0.1	0.1	0.2	0.2	0.3	0.3	0.4	0.4	0.5	0.5	0.6
16	1.1	1.0	.2	.2	.3	-3	•4	0.4	0.4 ·5	0.5	0.5 .6	.6
17	ı.	ı.	.2	.2	.3	•3	-4	.4	•5	.6	.6	.7
18	.I	.ı	.2	.2	.3	.4	.4	.5	-5	.6	.6	.7
19	.I	.1	.2	.2	.3	•4	.4	-5	.6	.6	.7	.7
20	0.1	0.1	0.2	0.3	0.3	0.4	0.5	0.5	0.6	0.7	0.7	0.8
21	.I	.I	.2	.3	-3	-4	.5	-5	.6	-7	.8	.8
22	.I	I.	.2	.3	.4	.4	-5	.6	.6	-7	8	.9
23	.I	I.	.2	.3	•4	.4	-5	.6	.7	.7	.8	.9
24	.I	.2	.2	-3	•4	.5	-5	.6	.7	.8	.9	.9
25	0.1	0.2	0.2	0.3	0.4	0.5	0.6	0.7	0.7	0.8	0.9	1.0
26	.I	.2	.3	•3	-4	.5	.6	.7	.8	.8	.9	1.0
27	.I	.2	-3	•4	-4	-5	.6	.7	.8	.9	0.1	1.1
28	. I	.2	.3	.4	-5	-5	.6	.7	.8	.9	0.1	I.I
29	.I	.2	.3	-4	-5	.6	.7	.8	.8	.9	1.0	1.1
30	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	1.2
31	.ı	.2	.3	.4	.5	.6	.7	.8	.9	1.0	I.I	1.2
32	·I	.2	.3	-4	-5	.6	.7	.8	.9	1.0	1.1	1.2
33	.1	.2	.3	4	.5	.6	.8	.9	0.1	I.I	1.2	1.3
34	.I	.2	.3	.4	.6	.7	.8	.9	1.0	1.1	1.2	1.3

TABLE 47.

REDUCTION OF THE MERCURIAL COLUMN TO STANDARD TEMPERATURE.

METRIC MEASURES

Table reconstructed from Table 45 to adapt it to U-shaped manometers with brass scales. For temperatures above 0°C. , the correction is to be subtracted; for temperatures below, added.

Attached thermometer		Diffe	ERENCI		EIGHT (E ALGE	BRAIC	
At	260	280	300	320	340	360	380	400	420	440	460	480	500
C. 0° 1 2 3 4	mm. 0.0 .0 .1 .1	mm. 0.0 .0 .1 .1	mm. 0.0 .0 .1 .1	mm. 0.0 .I .I .2 .2	mm. 0.0 .I .I .2 .2	mm, 0.0 .I .I .2 .2	mm. 0.0 .I .I .2 .2	mm. 0.0 .I .I .2 .3	mm. 0.0 .I .I .2 .3	mm. 0.0 .I .I .2 .3	mm. 0.0 .1 .2 .2 .3	mm. 0.0 .I .2 .2	mm. 0.0 .I .2 .2
5 6 7 8 9	0.2 ·3 ·3 ·3 ·4	0.2 ·3 ·3 ·4 ·4	0.2 ·3 ·3 ·4 ·4	0.3 ·3 ·4 ·4 ·5	.03 .3 .4 .4 .5	0.3 .4 .4 .5 .5	0.3 ·4 ·4 ·5 .6	0.3 .4 .5 .5	0.3 ·4 ·5 ·5 .6	0.4 .4 .5 .6 .6	0.4 .5 .5 .6 .7	0.4 ·5 ·5 ·6 ·7	0.4 .5 .6 .7 .7
10 11 12 13 14	0.4 .5 .5 .5	0.5 •5 •5 •6 .6	0.5 .5 .6 .6	0.5 .6 .6 .7 .7	0.6 .6 .7 .7	0.6 .6 .7 .8 .8	0.6 •7 •7 •8 •9	0.7 .7 .8 .8 .9	0.7 .8 .8 .9	0.7 .8 .9 .9	0.8 .8 .9 1.0	0.8 .9 .9 1.0	0.8 .9 I.0 I.I
15 16 17 18 19	0.6 •7 •7 •8 •8	0.7 .7 .8 .8 .9	0.7 .8 .8 .9	0.8 .8 .9 .9	0.8 .9 .9 I.0	0.9 1.0 1.1 1.1	0.9 1.0 1.1 1.1 1.2	I.0 I.0 I.I I.2 I.2	1.0 1.1 1.2 1.2 1.3	I.I I.I I.2 I.3 I.4	I.I I.2 I.3 I.3 I.4	1.2 1.2 1.3 1.4 1.5	1.2 1.3 1.4 1.5 1.5
20 21 22 23 24	0.8 .9 .9 I.0	0.9 I.0 I.0 I.1	I.0 I.0 I.I I.I I.2	I.0 I.I I.I I.2 I.2	I.I I.2 I.2 I.3 I.3	1.2 1.3 1.3 1.4	1.2 1.3 1.4 1.4 1.5	1.3 1.4 1.4 1.5 1.6	1.4 1.4 1.5 1.6 1.6	1.4 1.5 1.6 1.6	1.5 1.6 1.6 1.7 1.8	1.6 1.6 1.7 1.8 1.9	1.6 1.7 1.8 1.9 1.9
25 26 27 28 29	I.I I.I I.I I.2 I.2	I.I I.2 I.2 I.3 I.3	1.2 1.3 1.3 1.4 1.4	1.3 1.4 1.4 1.5	1.4 1.4 1.5 1.5	1.5 1.6 1.6 1.7	1.5 1.6 1.7 1.7	1.6 1.7 1.8 1.8 1.9	1.7 1.8 1.8 1.9 2.0	1.8 1.9 1.9 2.0 2.1	1.9 1.9 2.0 2.1 2.2	2.0 2.0 2.1 2.2 2.3	2.0 2.1 2.2 2.3 2.4
30 31 32 33 34	I.3 I.4 I.4 I.4	I.4 I.4 I.5 I.5 I.5	1.5 1.5 1.6 1.6	1.6 1.6 1.7 1.7 1.8	1.7 1.7 1.8 1.8 1.9	1.8 1.8 1.9 1.9 2.0	1.9 1.9 2.0 2.0 2.1	2.0 2.0 2.1 2.1 2.2	2.0 2.1 2.2 2.2 2.3	2.I 2.2 2.3 2.4 2.4	2.2 2.3 2.4 2.5 2.5	2.3 2.4 2.5 2.6 2.6	2.4 2.5 2.6 2.7 2.8

CORRECTIONS TO REDUCE BAROMETRIC READINGS TO STANDARD GRAVITY.

$$C = \frac{(g - g_0)}{g_0} B$$

(WITH $g_z < g_0$ THE CORRECTION IS TO BE SUBTRACTED; WITH $g_z > g_0$ IT IS TO BE ADDED.)

	BAROMETER READING B .												
g1-g0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0			
		2.0	3.0	7.0	0.0	0.0	7.0	0.0	3.0	10.0			
Dynes.													
0.1	0.00010	0.00020	0.00031	0.00041	0.00051	0.00061	0.00071	0.00082	0.00002	0.00102			
0.2	00020	00041	00061	00082	00102	00122	00143	00163	00184	00204			
0.3	00031	00061	00003	00122	00153	00184	00214	00245	00275	00306			
0.4	00041	00082	00122	00163	00204	00245	00286	00326	00367	00408			
0.5	00051	00102	00153	00204	00255	00306	00357	00408	00459	00510			
0.6	0.00061	0.00122	0.00184	0.00245	0.00306	0.00367	0.00128	0.00480	0.00551	0.00612			
0.7	00071	00143	00214	00286	00357	00428	00500	00571	00642	00714			
0.8	00082	00163	00245	00326	00408	00489	00571	00653	00734	00816			
0.9	00092	00184	00275	00367	00459	00551	00642	00734	00826	00918			
1.0	00102	00204	00306	00408	00510	00612	00714	00816	00918	01020			
1.1	0.00112		0.00337	0.00449	0.00561	0.00673	0.00785	0.00897	0.01010				
1.2	00122	00245	00367	00489	00612	00734	00857	00979	01101	01224			
1.3	00133	00265	00398	00530	00663	00795	00928	01061	01193	01326			
1.4	00143	00286	00428	00571	00714	00857	00000	01142	01285	01428			
1.5	00153	00306	00459	00012	00703	00018	01071	01224	01377	01530			
1.6	0.00163	0.00326	0.00489	0.00653	0.00816	0.00979	0.01142	0.01305	0.01468	0.01632			
1.7	00173	00347	00520	00693	00867	01040	01213	01387	01560	01734			
1.8	00184	00367	00551	00734	00018	01101	01285	01468	01652	01835			
1.9	00194	00387	00581	00775	00969	01162	01356	01550	01744	01937			
2.0	00204	00408	00012	00810	01020	01224	01420	01632	01035	02039			
2.1	0.00214	0.00428	0.00642	0.00857	0.01071		0.01499	0.01713	0.01927	0.02141			
2.2	00224	00449	00673	00897	01122	01346	01570	01705	02019	02243			
2.3	00235	00469	00704	00938	01173	01407	01642	01876	02111	02345			
2.4	00245	00489	00734	00979	01224	01468	01713	01958	02203	02447			
2.5	00255	00510	00765	01020	01275	01530	01/05	02039	02294	02549			
2.6	0.00265	0.00530	0.00795	0.01061	0.01326	0.01591	0.01856	0.02121	0.02386	0.02651			
2.7	00275	00551	00826	01101	01377	01652	01927	02203	02478	02753			
2.8	00286	00571	00857	01142	01428	01713	01999	02284	02570	02855			
2.9	00296	00591	00887	01183	01479	01774	02070	02366	02661	02958			
3.0	00300	00012	00013	01224	01530	01835	02141	02447	02753	03059			
3.1		0.00632	0.00948	0.01264		0.01897	0.02213	0.02529	0.02845	0.03161			
3.2	00326	00653	00079	01305	01632	01958	02284	02610	02937	03263			
3.3	00337	00673	01010	01346	01683	02019	02356	02692	03029	03365			
3.4	00347	00693	01040	01387	01734	02080	02427	02774	03120	03467			
3.5	00357	00/14	010/1	01428	01785	02141	02498	02055	03212	03300			
3.6	0.00367	0.00734		0.01468		0.02203		0.02937	0.03304	0.03671			
3.7	00377	00755	01132	01500	01886	02264	02641	03018	03396	03773			
3.8	00387	00775	01162	01550	01037	02325	02712	03100	03487	03875			
3.9	00398	00795	01193	01591	01988	02386	02784	03182	03579	03977			
4.0	00408	00010	01224	01632	02039	02447	02855	03203	03071	04079			
			<u></u>	<u>'</u>									

REDUCTION OF THE BAROMETER TO STANDARD CRAVITY. ENGLISH MEASURES.

FROM LATITUDE 0° TO 45°, THE CORRECTION IS TO BE SUBTRACTED.

HEIGHT OF THE BAROMETER IN INCHES.												
Lati-				HEIG	HT OF T	HE BAR	OMETE	R IN INC	HES.	_		
tude.	19	20	21	22	23	24	25	26	27	28	29	30
	Inch.	. Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.
o°	-0.051	-0.054	-0.056	-0.059	-0.062	-0.064	-0.067	-0.070	-0.072	-0.075	-0.078	-0.080
5		-0.053				-0.063	-0.066	-0.069	-0.071	-0.074	-0.077	
6	0.050		0.055	0.058	0.060	0.063	0.066	0.068	0.071	0.073	0.076	0.079
7 8	0.049	-	0.055	0.057	0.060		0.064	0.067	0.070		0.075	0.077
9	0.048		0.054		0.050	0.061	0.064	0.066	0.069	0.071	0.074	0.076
10	-0.0.18	-0.050	-0.053	-0.055	-0.058	-0.060	-0.063	-0.066	-0.068	-0.07 I	-0.073	-0.076
11	0.047	0.050	0.052	0.055	0.057	0.060	0.062	0.065	0.067	0.070		0.075
I 2	0.047	0.049	0.051	0.054	0.056	0.059	0.061	0.064	0.066	0.069	,	0.074
13	0.046			0.053	0.055	0.058	0.060		0.065	0.068		,
14	0.045	0.047	0.050	0.052	0.055	0.057	0.059	0.062	0.064	0.066	0.069	0.07
15	-0.044	-0.047	-0.049	-0.051	-0.053	-0.056	-0.058		-0.063			-0.070
16	0.043		0.048	0.050		0.055	0.057	0.059	0.062	0.064	0.066	
17	0.042		0.047	0.049	0.051	0.053	0.056					
18	0.041	0.044		0.048		0.052	0.054	0.057	0.059	0.061	0.063	
19	0.010	0.042	0.045	0.047	0.049	0.051						
20		-0.041				-0.050	-0.052	-0.054	-0.056	-0.058	-0.060	-0.06
2 I		0.040	0.042							0.056		
22	0.037	0.039	0.041				0.049	_		0.054		
23	0.036		0.039	0.041		0.045	0.047	0.049	-	0.053	0.054	0.050
								1				
25	-0.033	-0.035	-0.037							-0.049		
26	0.032		0.035	0.037	0.038	0.040	0.042		0.045	0.047	0.048	
27 28	0.030		0.033	0.035	0,	0.038 0.036	0.040			0.045	0.046	
20	0.029	0	0.032	0.033	0.035	0.035	0.036			0.040	0.044	0.04
30	0.006	-0.027	0.020	0.020	-0.031	0.022	-0.024	-0.035	-0.037	-0.028	-0.040	-0.01
31	0.024					0.031	0.032					
32	0.023		0.025	0.026	_		0.030		0.032	0.034	, ,	
33	0.021	0.022		0.025			0.028			0.031	0.032	0.03
34	0.020	0.021	0.022	0.023	0.024	0.025	0.026	0.027	0.028	0.029	0.030	0.03
35	-0.018	-0.019	-0.020	-0.021	-0.022	-0.023	-0.024	-0.025	-0.026	-0.027	-0.027	-0.02
36	0.016			0.019			0.022			0.024		
37	0.015			0.017						0.022		
38	0.013			0.015	1)		_	0.019		
39	0.011	0.012	0.012	0.013	0.014	0.014	0.015	0.015	0.016	0.017	0.017	0.01
40		-0.010							-0.014			
41	0.008		_	_			0.010			0.012	i	
42	0.000			0.007		0.008	0.008					
43	0.003			0.003		0.003	0.003			0.004	0.004	0.00
45	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.00

REDUCTION OF THE BAROMETER TO STANDARD GRAVITY.

ENGLISH MEASURES.

FROM LATITUDE 46° TO 90° THE CORRECTION IS TO BE ADDED.

Loti-	HEIGHT OF THE BAROMETER IN INCHES.												
tude.	19	20	21	22	23	24	25	26	27	28	29	30	
	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch.	Inch,	Inch.	
45°	-0.001	-0.001	-0.001	-0.00 I	-0.001	-0.001			-0.001		-0.001	1	
46													
47	0.003										+0.001		
48	0.003						0		0.004			0.004	
49	0.006			0.007	0.007			1	0.000			0.007	
50	0.008	0.008	0.000	0.000	0.010	0.010	0.010	0.011	0.011			- 1	
51	10010	+0.010	10011	±0.011	±0.013	+0.013	±0.013	10013	10011	10071	+0.015		
52	0.011						0.015	0.013	0.016			0.018	
53	0.013		0.011	U		0.016		0.018	0.018		,	0.020	
54	0.015	0.015	0.016		0.018	0.010				0.022	0.022	0.023	
55	0.016	0.017	0.018	0.019	0.020	0.021	0.021	0.022				0.026	
56	1 0		10000		(0 000								
1	0.020		+0.020								+0.027		
57	0.020		0.022	0	0.024	0	0.026			0.020	0.030	0.031	
59	0.023		U	0	0.028	,			0.032	0.031	0.032	0.033	
60	0.024		-				U	-	0.034	0.036	0.033	0.038	
	i								(,,			1	
61	+0.026	+0.027	+0.028	+0.030	+0.031	+0.033	+0.034	+0.035	+0.037	+0.038	+0.039	+0.041	
62	0.027	0.029	0.030	0.032	0.033	0.034	0.036		0.039	0.010	0.0.12	0.043	
63	0.029	0.030	0.032	0.033	0.035	0.036			0.041	0.042	0.044	0.045	
64	0.030	0.032	0.033	0.035	0.036	· ·			10	0.011	0.046	0.047	
65	0.031	0.033	0.035	0.036	0.038	0.010	0.041	0.043	0.045	0.046	0.048	0.050	
66	+0.033	+0.034	+0.036	+0.038	+0.040	+0.041	+0.043	+0.045	+0.047	+0.048	+0.050	+0.052	
67	0.034			0.039	0.041	0.043			0.048	0.050	0.052	0.054	
68	0.035	0.037	0.039	0.041	0.043	0.045	0.046		0.050	0.052	0.054	0.056	
69	0.036	0.038	0.010	0.042	0.044	0.046		0.050	0	0.054	0.056	0.058	
70	0.038	0.010	0.042	0.044	0.046	0.048	0.050	0.052	0.053	0.055	0.057	0.059	
71	+0.030	+0.041	+0.043	+0.045	+0.047	+0.040	+0.051	+0.053	+0.055	+0.057	+0.059	+0.061	
72	0.040	0.012	0.011	0.046		0.050		0.054		0.050	0.061	0.063	
73	0.041	0.043	0.045	0.047	0.040	0.052	0.054	0.056	0.058	0.060	0.062	0.064	
74	0.042		0.046		0.051	0.053	0.055	0.057	0.059	0.062	0.064	0.066	
75	0.043	0.045	0.047	0.049	0.052	0.054	0.056	0.058	0.061	0.063	0.065	0.067	
76	+0.011	+0.016	+0.018	+0.050	+0.053	+0.055	+0.057	+0.060	+0.062	+0.061	+0.066	10.060	
77		0.047	0.040	0.051	0.054				0.063	0.065	0.068	0.070	
78	0.045	0.047	0.050	0.052	0.055	0.057	0.050	0.062	0.064	0.066	0.060	0.071	
79	0.046	0.048		0.053	0.055	0.058	0.060	0.063	0.065	0.067	0.070	0.072	
80	0.046	0.049	0.051	0.054	0.056	0.059	0.061	0.063	0.066	0.068	0.071	0.073	
81	±0.017	+0.010	+0.053	+0.051	+0.057	+0.050	10.062	10.064	±0.067	+0.060	+0.072	10.074	
82	0.047	0.050	0.052	0.055	0.057	0.050		0.065	0.067	0.070		0.075	
83	0.048	0.050	0.053	0.055	0.058	0.061	0.063	- 1	0.068		0.072	0.075	
84	0.048		0.053	0.056	0.050	0.061	0.064			0.071	0.074	0.076	
85	0.049	_	0.054	0.056	0.059	0.061	0.064		0.069	0.072	0.074	0.077	
90	+0.040	+0.052	+0.055	+0.057	+0.060	+0.062	+0.065	+0.068	+0.070	+0.073	+0.075	+0.078	

TABLE 50.
REDUCTION OF THE BAROMETER TO STANDARD CRAVITY.

METRIC MEASURES.

FROM LATITUDE 0° TO 45°, THE CORRECTION IS TO BE SUBTRACTED.

1 - 1	HEIGHT OF THE BAROMETER IN MILLIMETERS.													
tude.	520	540	560	580	600	620	640	660	680	700	720	740	760	780
	mm.	mm.	mm,	mm.	mm.	mm.	mm,	mm.	mm.	mm.	mm.	mm.	mm.	mm,
0°			-1.50			-1.66	-1.71	-1.77	-1.82	-1.87	-1.93	-1.98	-2.04	-2.09
5	-1.37	-1.42	-1.48	-1.53	-1.58	-1.64	-1.60	-1.74	-1.70	-1.85	-1.00	-1.05	-2.00	-2.06
6	1.36	1.42	1.47	1.52	1.57	1.63	1.68	1.73	1.78	1.83	1.89	1.94	1.99	2.04
7 8	1.35	1.40	1.46	1.51	1.56	1.61	1.66	1.72	1.77	1.82	1.87	. 1.92	1.98	2.03
8	1.34	1.30	1.44	1.49	1.55	1.60	1.65	1.70	1.75	1.80	1.85	1.01	1.96	2.01
9	1.33	1.38	1.43	1.48	1.53	1.58	1.63	1.68	1.73	1.78	1.84	1.89	1.94	1.99
10	-1.31	-1.36	-1.41	-1.46	-1.51	-1.56	-1.61	-1.66	-1.71	-1.76	-1.81	-1.86	-1.02	-1.07
11	1.20	1.34	1.39	1.44	1.49	1.54	1.59	1.64	1.69	1.74	1.79	1.84	1.89	1.94
12	1.27	1.32	1.37	1.42	1.47	1.52	1.57	1.62	1.67	1.72	1.76	1.8:	1.86	1.01
13	1.25	1.30	1.35	1.40	1.45	1.50	1.54	1.59	1.64	1.69	1.74	1.78	1.83	1.88
14	1.23	1.28	1.33	1.38	1.42	1.47	1.52	1.56	1.61	1.66	1.71	1.75	1.80	1.85
15	-1.21	-1.26	-1.30	-1.35	1.40	-1.44	-1.40	-1.54	-1.58	-1.63	-1.67	-1.72	-1.77	-1.81
16	1.10	1.23	1.28	1.32	1.37	1.41	1.46	1.50	1.55	1.60	1.64	1.69	1.73	1.78
17	1.16	1.20	1.25	1.29	1.34	1.38	1.43	1.47	1.52	1.56	1.60	1.65	1.69	1.74
18	1.13	1.18	1.22	1.26	1.31	1.35	1.39	1.44	1.48	1.52	1.57	1.61	1.65	1.70
19	1.10	1.15	1.19	1.23	1.27	1.32	1.36	1.40	1.44	1.48	1.53	1.57	1.61	1.65
20	-1.07	-1.11	-1.16	-1.20	-1.24	-1.28	-1.32	-1.36	-1.40	-1.44	-1.40	-1.53	-1.57	-1.61
21	1.04	1.08	1.12	1.16	1.20	1.24	1.28	1.32	1.36	1.40	1.44	1.48	1.52	1.56
22	1.01	1.05	1.09	1.13	1.16	1.20	1.24	1.28	1.32	1.36	1.40	1.44	1.48	1.51
23	0.98	1.01	1.05	1.00	1.13	1.16	1.20	1.24	1.28	1.31	1.35	1.39	1.43	1.46
24	0.94	0.98	1.01	1.05	1.08	1.12	1.16	1.19	1.23	1.27	1.30	1.34	1.37	1.41
25	-0.00	-0.04	-0.07	-1.01	-1.04	-1.08	-1.11	-1.15	-1.18	-1.22	-1.25	-1.20	-1.32	-1.36
26	0.87	0.90	0.93	0.97			1.07	1.10	1.13	1.17	1.20	1.23	1.27	1.30
27	0.83	0.86	0.89	0.92	0.96	0.99	1.02	1.05	1.08	1.12	1.15	1.18	1.21	1.24
28	0.79	0.82	0.85	0.88	0.91	0.94	0.97	1.00	1.03	1.06	1.00	1.12	1.15	1.18
29	0.75	0.78	0.81	0.84	0.86	0.89	0.92	0.95	0.98	10.1	1.04	1.07	1.10	1.12
30	-0.71	-0.74	-0.76	-0.70	-0.82	-0.85	-0.87	-0.00	-0.93	-0.95	-0.98	-1.01	-1.04	-1.06
31	0.67	0.69	0.72			0.80	0.82	0.85	0.87	0.90	0.92	0.95	0.98	1.00
32	0.62		0.67	0.70			0.77	0.79	0.82	0.84	0.86	0.89	0.91	0.94
33	0.58				0.67			0.74	0.76	0.78	0.80	0.83	0.85	0.87
34	0.54	0.56	0.58	0.60	0.62	0.64	0.66	0.68	0.70	0.72	0.74	0.76	0.79	0.81
35	-0.49	-0.51	-0.53	-0.55	-0.57	-0.50	-0.61	-0.63	-0.64	-0.66	-0.68	-0.70	-0.72	-0.74
36	0.45		0.48					0.57	0.58		0.62	0.64		0.67
37	0.40	0.42				0.48	0.49		0.52		0.56		0.59	1
38	0.36	1	0.38					0.45			0.49		0.52	
39	0.31	0.32	0.33	0.34	0.36	0.37	0.38	0.39	0.40	0.42	0.43	0.44	0.45	0.40
40	-0.26	-0.27	-0.28	-0.20	-0.30	-0.31	-0.32	-0.33	-0.34	-0.35	-0.36	-0.37	-0.38	-0.39
41	0.21		0.23	0.24	0.25	0.26	0.26	0.27	0.28	0.29	0.30		0.31	0.32
42	0.17										0.23			1 0
43	0.12		1 6								0.10		0.17	
44	0.07	0.07	0.08	0.08	0.08	0.08	0.09	0.00	0.00	0.10	0.10	0.10	0.10	0.11
45	-0.02	-0.02	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.04
											1			
1	·		•											

REDUCTION OF THE BAROMETER TO STANDARD CRAVITY.

METRIC MEASURES.

FROM LATITUDE 46° TO 90°, THE CORRECTION IS TO BE ADDED.

	HEIGHT OF THE BAROMETER IN MILLIMETERS.													
Lati- tude.		540	560	580	600	620	640	660	680	700	720	740	760	780
	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.
45°	-0.02	-0.02	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.04
46	-0.02 0.07	1. 0	+0.03	. 0								+0.03		
47 48	0.12			0.08	0.08	0.09	. 2	1 - 2			0.10		0.10	0.11
49	0.17	0.17		0.10				0.21		0.23	0.23	0.24	0.25	0.25
50	0.22	0.22	0.23	0.24	0.25	0.26	0.26	0.27	0.28	0.29	0.30	0.31	0.31	0.32
51 52	+0.26 0.31	+0.27	+0.28	+0.29	+0.30	+0.31	+0.32			+0.35			+0.38	+0.39
53	0.36	0.37	0.0	0.40	0.41	0.42	0.44	0.39	0.40		0.43	0.44	0.45	0.46
54	0.40	0.42	0.43	0.45	0.46	0.48	0.49	0.51	0.52	0.54	0.56	0.57	0.59	0.60
55	0.45	0.46	0.48	0.50	0.52	0.53	0.55	0.57	0.58	0.60	0.62	0.64	0.65	0.67
56	+0.49		+0.53	+0.55	+0.57		+0.60	+0.62	+0.64	+0.66	+0.68	+0.70	+0.72	+0.74
57	0.54	0.56		0.60	0.62	0.64	0.66	0.68	0.70	0.72	0.74	0.76	0.78	0.80
58 59	0.58	0.60	0.62	0.65	0.67	0.69	0.71	0.74	0.76	0.78	0.80	0.82	0.85	0.87
60	0.66	0.69	0.72	0.74	0.77	0.79	0.82	0.84	0.87	0.89	0.92	0.94	0.91	0.93
61	+0.71	+0.72	+0.76	+0.70	+0.81	+0.84	±0.87	±0.80	±0.03	±0.0-	±0.08	+1.00	1.00	1 7 06
62	0.74	0.77	0.80	0.83	0.85	0.88	0.01	0.04	0.07	1.00	1.02	1.05	1.08	1.11
63	0.78	0.81	0.85	0.88	0.91	0.94	0.97	1.00	1.03	1.06	1.00	1.12	1.15	1.18
64	0.82	0.85	0.89	0.92	0.95	0.98	1.01	1.04	1.08	I.II	1.14	1.17	1.20	1.23
65	0.80	0.09	0.93	0.96	0.99	1.03	1.06	1.09	1.13	1.16	1.19	1.22	1.26	1.29
66	+0.90		- •	+1.00	+1.04					+1.21			+1.31	
67	0.93	0.97	1.00	1.04	1.08	1.11	1.15	1.18	I.22 I.26	1.25	I.29 I.34	1.33	1.36	1.40
69	1.00	1.04	1.08	1.11	1.15	1.10	1.23	1.27	1.31	1.34	1.38	1.42	1.46	1.45
70	1.03	1.07	1.11	1.15	1.19	1.23	1.27	1.31	1.35	1.39	1.43	1.47	1.51	1.55
71	+1.06	+1.10	+1.14	+1.18	+1.22	+1.26	+1.31	+1.35	+1.30	+1.43	+1.47	+1.51	+1.55	+1.50
72	1.00	1.13	1.17	I.22	1.26	1.30	1.34	1.38	1.42	1.47	1.51	1.55	1.59	1.63
73	I.I 2	1.16	1.20	1.25	1.29	1.33	1.37	1.42	1.46	1.50	1.55	1.59	1.63	1.67
74 75	1.14	1.19	1.23	1.28	I.32 I.35	1.36	1.41	1.45	1.50	1.54	1.58	1.63	1.67	1.72
								1.40	1.33	1.57	1.02	1.00	1.71	1.75
76			+1.28	+1.33								+1.70		
77	1.21	1.26	1.31	1.35 1.38	I.40 I.42	1.45	I.49 I.52	1.54	1.59	1.63	1.68	1.73	1.77	1.82
79	1,25	1.30	1.35	1.40	1.45	1.40	1.54	1.59	1.64	1.60	I.7I I.73	1.76 1.78	1.80	1.85
80	1.27	1.32	1.37	1.42	.147	1.51	1.56	1.61	1.66	1.71	1.76	1.81	1.86	1.90
81	+1.29	+1.33	+1.38	+1.43	+1.48	+1.53	+1.58	+1.63	+1.68	+1.73	+1.78	+1.83	+1.88	+1.03
82	1.30	1.35	1.40	1.45	1.50	1.55	1.60	1.65	1.70	1.75	1.80	1.85	1.90	1.95
83	1.31	1.36	1.41	1.46	1.51	1.56	1.61	1.67	1.72	1.77	1.82	1.87	1.92	1.97
84 85	1.32	1.37 1.38	1.42	1.48	1.53 1.54	1.58	1.63	1.68	1.73	1.78	1.83	1.88	1.93	1.98
									1	11				
90	+1.35	+1.41	+1.46	+1.51	+1.56	+1.61	+1.67	+1.72	+1.77	+1.82	+1.87	+1.93	+1.98	+2.03

TABLES FOR DETERMINING HEIGHTS, AND CONVERSIONS INVOLVING GEOPOTENTIAL

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ENGLISH MEASURES.

Values of 60368 [1 + 0.0010195 \times 36] log $\frac{29.90}{8}$.

								R		-
Barometric Pressure. B.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
Inches.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
12.00	24814	24791	24769	24746	24723	24701	24678	24656	24633	24611
12.10	24588	24566	24543	24521	24499	24476	24454	24431	24409	24387
12.20	24365	24342	24320	24298	24276	24253	24231	24209	24187	24165
12.30	24143	24121	24098	24076	24054	24032	24010	23988	23966	23944
12.40	23923	23901	23879	23857	23835	23813	23791	23770	23748	23726
12.50	23704	23682	23661	23639	23617	23596	23574	23552	23531	23509
12.60 12.70	23488	23466	23445	23423	23402	23380	23359	23337	23316	23294
12.70	23273 23060	2325I 23038	23230	23209	23187	23166 22954	23145	23123	23102	23081
12.90	22848	22827	22806	22785	22764	22743	22933	22911 22701	22890 22680	22869 22659
13.00	22638	22617	22596	22576	22555	22534	22513	22492	20477	
13.10	22430	22409	22388	22368	22347	22326	22306	22285	22471	22451 22244
13.20	22223	22203	22182	22162	22141	22121	22100	22080	22059	22039
13.30	22018	21998	21977	21957	21937	21916	21896	21876	21855	21835
13.40	21815	21794	21774	21754	21734	21713	21693	21673	21653	21633
13.50	21612	21592	21572	21552	21532	21512	21492	21472	21452	21432
13.60	21412	21392	21372	21352	21332	21312	21292	21272	21252	21233
13.70	21213	21193	21173	21153	21134	21114	21094	21074	21054	21035
13.80	20819	20995	20976 20780	20956 20760	20936 20741	20917	20897 20702	20878 20682	20858	20838
1 1	- 1					, i			20663	20643
14.00 14.10	20624 20431	20605 20411	20585	20566	20546	20527	20508	20488	20469	20450
14.20	20238	20219	20200	20373 20181	20354 20162	20334	20315	20296	20277 20086	20258
14.30	20048	20029	20010	19991	19972	19953	19934	19915	19896	19877
14.40	19858	19839	19821	19802	19783	19764	19745	19727	19708	19689
14.50	19670	19651	19633	19614	19595	19577	19558	19539	19521	19502
14.60	19483	19465	19446	19428	19409	19390	19372	19353	19335	19316
14.70	19298	19279	19261	19242	19224	19206	19187	19169	19150	19132
14.90	18931	18912	19077	19059	18858	19022 18840	19004 18821	18985 18803	18967 18785	18949 18767
15.00	18749	18731	18713	18694	18676	18658	18640	18622	18604	18586
15.10	18568	18550	18532	18514	18496	18478	18460	18442	18425	18407
15.20	18389	18371	18353	18335	18317	18300	18282	18264	18246	18228
15.30	18211	18193	18175	18157	18140	18122	18104	18086	18069	18051
15.40	18033	18016	17998	17981	17963	17945	17928	17910	17893	17875
15.50	17858	17840	17823	17805	17788	17770	17753	17735	17718	17700
15.60	17683	17665	17648	17631	17613	17596	17578	17561	17544	17526
15.70 15.80	17509	1749 2 17319	17474	17457	17440	17423 17251	17405	17388 17216	17371 17199	17354 17182
15.90	17165	17148	17131	17114	17097	17080	17063	17046	17029	17012
16.00	16995	16978	16961	16944	16927	16910	16893	16876	16859	16842
16.10	16825	16808	16792	16775	16758	16741	16724	16707	16691	16674
16.20	16657	16640	16623	16607	16590	16573	16557	16540	16523	16506
16.30 16.40	16490 163 2 4	16473 16307	16456 16 2 90	16440 16274	16423 16257	16406 16241	16390 16224	16373	16357	16340 16175
16.50	16158	16142	16125	16109	16092	16076	16060	16043	16027	16010
16.60	15994	15978	15961	15945	15929	15912	15896	15880	15863	15847
16.70	15831	15815	15798	15782	15766	15750	15733	15717	15701	15685
16.80	15669	15652	15636	15620	15604	15588	15572	15556	15539	15523
16.90	15507	15491	15475	15459	15443	15427	15411	15395	15379	15363
17.00	15347	15331	15315	15299	15283	15267	15251	15235	15219	15203
				!						

TABLE 51.

ENGLISH MEASURES.

Values of 60368 [1+0.0010195 \times 36] $\log \frac{29.90}{B}$.

								В		
Barometric Pressure B.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
Inches.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
17.00	15347	15331	15315	15299	15283	15267	15251	15235	15219	15203
17.10	15187	15172	15156	15140	15124	15108	15092	15076	15061	15045
17.20	15029	15013	14997	14982	14966	14950	14934	14919	14903	14887
17.30	14871	14856	14840	14824	14809	14793	14777	14762	14746	14730
17.40	14715	14699	14004	14003	14652	14637	14621	14606	14590	14575
17.50	14559	14544	14528	14512	14497	14481	14466	14451	14435	14420
17.60	14404 14250	14389	14373	14358	14342	14327	14312	14296	14281 14128	14266 1411 2
17.80	14230	14082	14219	14051	14036	14021	14006	13990	13975	13960
17.90	13945	13930	13914	13899	13884	13869	13854	13839	13824	13808
18.00	13793	13778	13763	13748	13733	13718	13703	13688	13673	13658
18.10	13643	13628	13613	13598	13583	13568	13553	13538	13523	13508
18.20	13493	13478	13463	13448	13433	13418	13404	13389	13374	13359
18.30	13314	13329	13314	13300	13285	13270	13255	13240	13226	13211
18.40	13196	13181	13166	13152	13137	13122	13107	13093	13078	13063
18.50	13049	13034	13019	13005	12990	12975	12961	12946	12931	12917
18.60	12902	12888	12873	12858	12844	12829	12815	12800	12785	12771
18.70 18.80	12756	12742 12597	12727 12583	12713	1269S 12554	12684	12669 12525	12655 12510	12640 12496	12626 12482
18.90	12467	12453	12438	12424	12410	12395	12381	12367	12352	12338
19.00	12324	12310	12295	12281	12267	12252	12238	12224	12210	12195
19.10	12181	12167	12153	12138	12124	12110	12096	12082	12068	12053
19.20	12039	12025	12011	11997	11983	11969	11954	11940	11926	11912
19.30	11898	11884	11870	11856 11716	11842	11828 11688	11814 11674	11800 11660	11786 11646	11772
19.40	11758	11744								
1 9.50	11618	11604 11465	11590	11576	11562 11423	11548	11534 11396	11520 11382	11507	11493
19.70	11340	11327	11313	11299	11285	11272	11258	11244	11230	11217
19.80	11203	11189	11175	11162	11148	11134	11121	11107	11093	11080
19.90	11066	11052	11039	11025	IIOII	10998	10984	10970	10957	10943
20.00	10930	10916	10903	10889	10875	10862	10848	10835	10821	10808
20.10	10794	10781	10767	10754	10740	10727	10713	10700	10686	10673
20.20	10659	10646	10632 10498	10619	10605 10472	10592	10579	10565	10552 10418	10538
20.40	10525	10378	10365	10352	10338	10325	10445	10431 10298	10285	10272
20.50	10259	10245	10232	10219	10206	10192	10179	10166	10153	10139
20,60	10126	10113	10100	10087	10074	10060	10047	10034	10021	10008
20.70	9995	9982	9968	9955	9942	9929	9916	9903	9890	9877
20.So 20.90	9864 9733	9851 97 2 0	9838 9707	9825 9694	9812 9681	9799 9668	9786 9655	9772 9642	9759 9629	9746
21.00	9604	9591	9578	9565	9552	9539	9526	9513	9500	9487
21.10	9474	9391	9370	9303	9552	9539	9320	9313	9372	9359
21.20	9346	9333	9320	9307	9295	9282	9269	9256	9244	9231
21.30	9218	9205	9193	9180	9167	9154	9142	9129	9116	9103
21.40	9091	9078	9065	9053	9040	9027	9015	9002	8989	8977
21.50 21.60	8964 8838	8951 8825	8939 8813	8926 8800	8913 8788	8901 8775	8888 8762	8876 8750	8863 8737	8850 8725
21.70	8712	8700	8687	8675	8662	8650	8637	8625	8612	8600
21.80	8587	8575	8562	8550	8538	8525	8513	8500	8488	8475
21.90	8463	8451	8438	8426	8413	8401	8389	8376	8364	8352
22.00	8339	8327	8314	8302	8290	8277	8265	8253	8240	8228
							1			

ENGLISH MEASURES.

Values of 60368 [1 + 0.0010195 \times 36] $\log \frac{29.90}{B}$.

								B		
Barometric Pressure. B.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
Inches.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
22.00	8339	8327	8314	8302	8290	8277	8265	8253	8240	8228
22.10	8216	8204	8191	8179	8167	8154	8142	8130	8118	8105
22.20	8093	8081	8069	8056	8044	8032	8020	8008	7995	7983
22.30	7971	7959	7947	7935	7922	7910	7898	7886	7874	7862
22.40	7849	7837	7825	7813	7801	7789	7777	7765	7753	7740
22.50	7728	7716	7704	7692	7680	7668	7656	7644	7632	7620
22.60	7608	7596	7584	7572	7560	7548	7536	7524	7512	7500
22.70	7488	7476	7464	7452	7440	7428	7416	7404	7392	7380
22.80	7368	7356	7345	7333	7321	7309	7297	7285	7273	7261
22.90	7249	7238	7226	7214	7202	7190	7178	7166	7155	7143
23.00	7131	7119	7107	7096	7084	7072	7060	7048	7037	7025
23.10	7013	7001	6990	6978	6966	6954	6943	6931	6919	6907
23.20	6896	6884	6872	6861	6849	6837	6825	6814	6802	6790
23.30	6779	6767	6755	6744	6732	6721	6709	6697	6686	6674
23.40	6662	6651	6639	6628	6616	6604	6593	6581	6570	6558
23.50	6546	6535	6523	6512	6500	6489	6477	6466	6454	6443
23.60	6431	6420	6408	6397	6385	6374	6362	6351	6339	6328
23.70	6316	6305	6293	6282	6270	6259	6247	6236	6225	6213
23.80	6202	6190	6179	6167	6156	6145	6133	6122	6110	6099
23.90	6088	6076	6065	6054	6042	6031	6020	6008	5997	5986
24.00	5974	5963	5952	5940	5929	5918	5906	5895	5884	5872
24.10	5861	5850	5839	5827	5816	5805	5794	5782	5771	5760
24.20	5749	5737	5726	5715	5704	5693	5681	5670	5659	5648
24.30	5637	5625	5614	5603	5592	5581	5570	5558	5547	5536
24.40	5525	5514	5503	5492	5480	5469	5458	5447	5436	5425
24.50	5414	5403	5392	5381	5369	5358	5347	5336	5325	5314
24.60	5303	5292	5281	5270	5259	5248	5237	5226	5215	5204
24.70	5193	5182	5171	5160	5149	5138	5127	5116	5105	5094
24.80	5083	5072	5061	5050	5039	5028	5017	5006	4995	4985
24.90	4974	4963	4952	4941	4930	4919	4908	4897	4886	4876
25.00	4865	4854	4843	4832	4821	4810	4800	4789	4778	4767
25.10	4756	4745	4735	4724	4713	4702	4691	4681	4670	4659
25.20	4648	4637	4627	4616	4605	4594	4584	4573	4562	4551
25.30	4540	4530	4519	4508	4498	4487	4476	4465	4455	4444
25.40	4433	4423	4412	4401	4391	4380	4369	4358	4348	4337
25.50	4326	4316	43°5	4295	4284	4273	4263	4252	4241	4231
25.60	4220	4209	4199	4188	4178	4167	4156	4146	4135	4125
25.70	4114	4104	4093	4082	4072	4061	4051	4040	4030	4019
25.80	4009	3998	3988	3977	3966	3956	3945	3935	3924	3914
25.90	3903	3893	3882	3872	3861	3851	3841	3830	3820	3809
26.00	3799	3788	3778	3767	3757	3746	3736	3726	3715	3705
26.10	3694	3684	3674	3663	3653	3642	3632	3622	3611	3601
26.20	3590	3580	3570	3559	3549	3539	3528	3518	3508	3497
26.30	3487	3477	3466	3456	3446	3435	3425	3415	3404	3394
26.40	3384	3373	3363	3353	3343	3332	3322	3312	3301	3291
26.50	3281	3270	3260	3250	3240	3230	3219	3209	3199	3189

TABLE 51.

DETERMINATION OF HEIGHTS BY THE BAROMETER.

ENGLISH MEASURES.

Values of 60368 $[1+0.0010195 \times 36] \log \frac{29.90}{9}$.

					0.0010			В		
Barometric Pressure. B.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
Inches.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
26.50	3281	3270	3260	3250	3240	3230	3219	3209	3199	3189
26.60 26.70	3179 3077	3168 3066	3158 3056	3148 3046	3138 3036	3128 3026	3117	3107 3005	3097 2995	3087 2985
26.80	2975	2965	2955	2945	2934	2924	2914	2904	2 894	2884
26.90	2874	2 864	2854	2843	2833	2823	2813	2803	2793	2783
27.00	2773	2763	2753	2743	2733	2723	2713	2703	2692	2682
27.10	2672	2662	2652	2642	2632	2622	2612	2602	2592	2582
27.20 27.30	2572 2473	2562 2463	2552 2453	2542 2443	2532 2433	2522 2423	2512 2413	2502 2 403	2493 2393	2483 2383
27.40	2373	2363	2353	2343	2334	2324	2314	2304	2 294	2284
27.50	2274	2264	2254	2245	2235	2225	2215	2205	2195	2185
27.60 27.70	2176 2077	2166 2067	2156 2058	2146 2048	2136 2038	2126 2028	2116 2018	2107 2009	2097 1999	268 7 198 9
27.50 27.80	1979	1970	1960	1950	1940	1930	1921	1911	1901	1891
27.90	1882	1872	1862	1852	1843	1833	1823	1814	1804	1794
28.00	1784	1775	1765	1755	1746	1736	1726	1717	1707	1697
28.10	1688	1678	1668	1659	1649	1639	1630	1620	1610	1601
28.20 28.30	1591 1495	1581 1485	1572 1476	1562 1466	1552 1456	1543 1447	1533 1437	1524 1428	1514 1418	1504
28.40	1399	1389	1380	1370	1361	1351	1342	1332	1322	1313
28.50	1303	1294	1284	1275	1265	1256	1246	1237	1227	1218
28.60 28.70	1208 1113	1199 1104	1189	1180 1085	1170 1075	1161	1151	114 2 1047	1132 1038	1123
2 8.80	1019	1009	1000	990	981	972	962	953	943	9.34
28.90	925	915	906	896	887	878	868	859	849	840
29.00	831	821	812	803	793	784	775 681	765	756	746
29.10 29.20	737 644	728 635	718 625	709 616	700 607	690 597	588	672 579	663 570	653 560
29.30	551	542	532	523	514	505	495	486	477	468
29.40	458	449	440	431	421	412	403	394	384	375
29.50	366	357	348	338	329	320	311	302	292	283
29.60 29.70	274 182	265 173	256 164	247 155	237 146	228 137	219 128	210 118	201 109	192 100
29.80	+ 91	+ 82	+ 73	+ 64	+ 55	+ 45	+ 36	+ 27	+ 18	+ 9
29.90	0	- 9	- 18	- 27	- 36	- 45	– 55	- 64	- 73	- 82
30.00	- 91 - 181	- 100	- 109	- 118 - 208	- 127	- 136 - 226	- 145	- 154	- 163	- 172 - 262
30.10 30.20	-181 -271	- 190 - 280	- 199 - 289	- 208 - 298	- 217 - 307	- 226 - 316	-235 $ -325$	- 244 - 334	$\frac{-253}{-343}$	-352
30.30	- 361	- 370 - 460	- 379 - 460	- 388 - 478	- 397	- 406	-415	- 424	- 433	- 442
30.40	- 451	– 460	— 469	– 478	– 486	— 495	- 504	-513	- 522	-531
30.50	- 540 - 630	- 549 - 628	- 558 - 647	- 567 - 656	- 576 - 665	- 585 - 671	- 593 - 682	- 602 - 691	- 611 - 700	- 620 - 709
30.60 30.70	- 629 - 718	- 63S - 727	- 647 - 735	- 656 - 744	- 665 - 753	- 673 - 762	- 771	- 780	- 788	- 797
30.80	- 806	-815	- S24	- \$ ₃₃	- S41	-850	-859	- 868	- S77	- 885
								1		

DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.

Term for Temperature: 0.002039 $(\theta - 50^{\circ})$ z.

For temperatures $\left\{ \begin{array}{ll} above \ 50^{\circ} \ \mathrm{F.} \\ below \ 50^{\circ} \ \mathrm{F.} \end{array} \right\}$ the values are to be $\left\{ \begin{array}{ll} added. \\ subtracted. \end{array} \right.$

Me Tempe	rature.	AF	PROX	IMATI	E DIFF	EREN	CE OI	HEIC	энт о	BTAIN	ED FI	ROM T	ABLE	51.
	9.	20	40	60	08	100	200	300	400	500	600	700	800	900
F.	F.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
49° 48	51° 52	0	0	0	0	0	O	I	I 2	I 2	I 2	3	3	2
47	53	0	0	0	0	I	I	2	2	3	4	4 6	5	4 6
46	54	0	0	0	I	I	2	2	3	4	5		7	7
45 44	55 56	0	0	I I	I I	I	2 2	3 4	4	5 6	6 7	7	8	9
43	57	0	I	I	I	I	3	4	5 6	7 8	9	9	11	13
42 41	58 59	0	I I	I	I	2	3 4	5 6	7	8	IO	II	13	15
40	60	0	I	I	2	2	4	6	8	10	12	13	15 16	18
39 38	61	0	I	I	2	2	4	7	9	II	13	16	18	20
38	62 63	O	I	I 2	2 2	3	5 5 6	7 8	10	12	15 16	17 19	20 21	22
36	64	I	I	2	2	3	6	9	II	14	17	20	23	24 26
35	65 66	I	I	2	2	3	6	9	12	15	18	21	24	28
34	67	I I	I I	2 2	3	3 3 4	7	IO	13	16 17	20 2 I	23 24	26 28	29 31
32	68	I	I	2	3 3 3		7 8	II	15	18	22	26	29	33
31	69	I	2	2		4		12	15	19	23	27	31	35
30 29	70 71	I	2 2	3	3	4	8 9	12	16 17	20 21	24 26	29 30	33 34	37 39
28	72	I	2	3	4	4	9	13	18	22	27	31	36	40
27 26	73 74	I	2 2	3	4	5 5	9 10	14 15	19 20	23 24	28 29	33 34	38 39	42 44
25	75	I	2	3	4		10	15	20	25	31	36	41	46
24	76	I	2 2	3	4	5 6 6	II	16	2 I 2 2	27 28	32	37	42	48
23 22	77 78	I	2	3	4 5	6	II	17	23	29	33 34	39 40	44 46	50 51
21	79	I	2	4	5	6	12	18	24	30	35	41	47	53
20	80 18	I	3	4	5	6	12 13	18	24 25	31 32	37 38	43	49	55
19 18	82	I	3	4	5	7	13	20	26	33	39	44 46	51 52	57 59 61
17 16	83 84	I	3	4 4	5 5 5	7 7	13 14	20 2 I	27 28	34 35	40 42	47 49	54 55	61 62
15	85	I	3	4	6	7	14	21	29	36	43	50	57	
14	86	I	3	4	6	7 8	15	22	29	37	44	51	59	64 66
13	87 88	2 2	3	5 5	6	8	15 15	23 23	30 31	38 39	45 46	53 54	60 62	68 70
II	89	2	3	5	6	8	16	24	32	40	48	56	64	72
10	90 91	2 2	3	5 5	7 7	8	16 17	24	33 33	41 42	49 50	57	65 67	73
9 8	92	2	3	5	7	9	17 18	25 26	34	43	51	59 60	69	75 77
7 6	93 94	2	4	5 5	7 7	9	18 18	26 27	35 36	44 45	53 54	61 63	70 72	77 79 81
5	95	2	4	6		9	18	28	37	45 46	55	64	73	83
4	96	2 2	4	6	7 8 8	9	19	28	38	47 48	56	66	75	83 84
3 2	97 98	2	4 4	6	8	10	20	29 29	38 39	49	57 59	67 69	77 78	86 88
1	99	2	4	6	8	10	20	30	40	50	60	70	80	90
0	100	2	4	6	8	IO	20	31	41	51	61	71	82	92

DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.

Term for Temperature: $0.002039 (\theta - 50^{\circ})$ z.

For temperatures $\left\{ \begin{array}{ll} above \ 50^{\circ} \ F. \\ below \ 50^{\circ} \ F. \end{array} \right\}$ the values are to be $\left\{ \begin{array}{ll} added. \\ subtracted. \end{array} \right.$

-				(Subtracti									
	Tempe	ean rature.	APPR	OXIMA	TE DIF	FEREN	CE OF	HEIGI	нт овт	AINED	FROM	TABLE	51.
	t	9.	1000	2000	3000	4000	5000	6000	7000	8000	9000	10000	20000
	F.	F.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
	49° 48	51° 52	2 4	4 8	6 12	8 16	10 20	12 24	14 2 9	16 33	18 37	20 41	41 82
	47 46	53 54	6 8	12 16	18 24	24 33	31 41	37 49	43 57	49 65	55 73	61 8 2	122 163
	45	55	10 12	20	31	41	51 61	61	71 86	82	92	102	204
	44 43	56 57	14	24 29	37 43	49 57	71	73 86	100	98 114	110 128	122 143	245 285
	42 41	58 59	16 18	33 37	49 55	65 73	82 92	98 110	114 1 2 8	130 147	147 165	163 184	3 2 6 367
	40 39	60 61	20 22	41 45	61 67	8 2 90	IO2 II2	122 135	143 157	163 179	184 202	2 04 22 4	408 449
	38	62	2.1	49	73 So	98	122	147	171	196	220	245	489
	37 36	63 64	27 29	53 57	86 86	106 114	133 143	159 171	186 2 00	212 228	239 257	265 285	530 571
	35 34	65 66	31 33	61 65	9 2 98	122 130	153 163	184 196	214 228	245 261	275 294	306 3 2 6	612 65 2
	33	67 68	35	69	104	139	173	208	243	277	312	347	693
	3 ² 3 ¹	69	37 39	73 77	110	147	184 194	220 232	257 27 I	2 94 310	330 349	3 ⁶ 7 3 ⁸ 7	734 775
	30	70 71	41 43	8 2 86	122 128	163 171	2 04 2 14	245 257	285 300	3 2 6 343	367 385	408 4 2 8	816 856
	28	72	45	90	135	179	224	269	314	359	404	449	897
	27 26	73 74	47 49	94 98	141	196	234 245	281 294	3 2 8 343	375 391	4 22 440	469 489	938 979
	25 24	75 76	51 53	102 106	153 159	204 212	255 265	306 318	357 371	408 4 2 4	459 477	510 530	1020
1	23	77 78	55	110	165	220 228	275 285	330	385	440	495	551	IOI
	21	79	57 59	118	171	236	2 96	343 355	400	457 473	514 532	571 591	1142
	20	80 81	61 63	122 126	184	245 253	306 316	367 379	428 442	489 506	551 569	61 2 63 2	1223 1264
	18	82 83	65 67	130	196	261 269	326	391	457	522	587 606	652	1305
	17	84	69	135	208	277	336 347	404 416	471 485	538 555	624	673 693	1346 1387
	15	85 86	71 73	143 147	214 220	2 85 2 94	357 367	4 2 8 440	500 514	571 587	642 661	714 734	1427 1468
	13	87 88	75 77	151	226 232	302 310	377 387	453 465	528	604 620	679	754	1509 1550
	II	89	So !	155 159	239	318	398	477	54 2 557	636	697 716	775 795	1590
	10	90 91	82 84	163 167	245 251	3 2 6	408 418	489 502	571 585	65 2 669	734 752	816 836	1631 1672
	9 8	92 93	86 88	171 175	257 263	343	4 2 8 438	514 526	599 614	685 701	771 789	856 877	1713
	7	94	90	179	2 69	351 359	449	538	628	718	807	897	1794
	5 4	95 96	92 94	184 188	275 281	367 375	459 469	551 563	64 2 657	734 750	826 844	918 938	1835
	3 2	97 98	96	192 196	287 294	383	479 489	575 587	671 685	767 783	862 881	958 979	1917
	ī	99	100	200	300	400	500	599	699	799	899	999	1998
1	0 [100	102	204	306	408	510	612	714	816	918	1020	2039

ENGLISH MEASURES.

Correction for Gravity and Weight of Mercury: z (0.002640 $\cos 2 \phi$ - 0.000007 $\cos^2 2 \phi$ + 0.00244).

Latitude.	API	PROXIM	ATE DI	FFERE	NCE OF	HEIGH	IT OBT	AINED	FROM	TABLES	51-52.
φ	500	1000	1500	2000	2500	3000	3500	4000	4500	5000	5500
0° 2 4 6 8	Feet. +3 3 3 3 2	Feet. +5 5 5 5 5 5	Feet. +8 8 8 8 7	Feet. + 10 10 10	Feet. +13 13 13 13	Feet. + 15 15 15 15 15	Feet. + 18 18 18 18	Feet. +20 20 20 20 20	Feet. +23 23 23 23 23 22	Feet. +25 25 25 25 25	Feet. +28 28 28 28
10 12 14 16 18	+2 2 2 2 2 2	+5 5 5 5 5	+7 7 7 7 7	+10 10 10 9	+ 1 2 1 2 1 2 1 2 1 1	+15 15 14 14 14	+17 17 17 16 16	+20 19 19 19	+22 22 21 21 21	+25 24 24 23 23	+27 27 26 26 25
20 22 24 26 28	+2 2 2 2 2	+4 4 4 4 4	+7 6 6 6 6	+ 9 9 8 8 8	10 10	+13 13 13 12 12	+16 15 15 14 14	+18 17 17 16 16	+20 19 19 18 18	+22 22 21 20 20	+24 24 23 22 21
30 32 34 36 38	+2 2 2 2 2 2	+4 4 3 3 3	+6 5 5 5 5	+ 8 7 7 6 6	+ 9 9 9 8 8	11 10 10	+13 13 12 11	+15 14 14 13 12	+17 16 15 15	+19 18 17 16 15	+21 20 19 18 17
40 42 44	+ I	+3 3 3	+4 4 4	+ 6 5 5	+ 7 7 6	+ 9 8 8	+10 9 9	+ 1 2 1 I 10	+13 12 11	+14	+16 15 14
45	+1	+2	+4	+ 5	+ 6	+ 7	+ 9	+10	+11	+12	+13
46 48 50	+ I I	+2 2 2	+4 3 3	+ 5 4 4	+ 6 5 5	+ 7 6 6	+ 8 8 7	+ 9 9 8	+11	+12 11 10	+13
52 54 56 58 60	+1 1 1	+2 2 I I	+3 2 2 2 2 2	+ 4 3 3 3 2	+ 4 4 4 3 3	+ 5 5 4 4 3	+ 6 6 5 4 4	+ 7 6 6 5 4	+ 8 7 7 6 5	+ 9 8 7 6 6	+10 9 8 7 6
62 64 66 68 70	0 0 0	+ I I I O	+ I I I I I I I I I I I I I I I I I I I	+ 2 2 I I I	+ 2 2 1 1	+ 3 2 2 2 2 1	+ 3 3 2 2 1	+ 4 4 3 2 2	+ 4 3 3 2 2 2	+ 5 4 3 3 2	+ 5 4 3 3 2 1
72 74 76 78 80	0 0 0 0	0 0 0 0 0	0 0 0 0	0 0 0	0 0	1 0 0	+ I	+ I 0 0	+ I 0 0	+ I I O O O	+ I

ENGLISH MEASURES.

Correction for Gravity and Weight of Mercury: $z = (0.002640 \cos 2 \phi - 0.000007 \cos^2 2 \phi + 0.00244)$.

Feet	Latitude.				1		HEIGH					
0°	φ	6000	7000	8000	9000	10000	11000	12000	13000	14000	15000	20000
2	_		Feet.									Feet.
4 30 35 40 45 50 55 61 66 71 76 101 8 30 35 40 45 50 55 01 66 71 76 70 99 10					1 1 1							1 '
8 30 35 40 45 50 55 60 66 71 76 100 8 30 35 40 45 50 55 60 665 70 75 99 10 +20 +34 +30 +44 +40 +54 +50 +64 +60 +74 +98 12 29 34 30 44 48 53 58 63 68 73 99 16 28 33 37 42 47 51 56 61 65 70 93 18 27 32 37 41 46 50 55 59 64 68 20 +27 +31 +36 +40 +45 +40 +53 +58 +62 +67 +80 22 26 30 35 30 43 48 52 55 66 61 65 70 93 18 27 32 37 41 46 50 55 59 64 68 91 20 +27 +31 +36 +40 +45 +40 +53 +58 +62 +67 +80 24 25 29 34 38 42 46 50 55 59 63 84 26 24 28 32 37 41 45 40 45 30 55 59 63 30 +23 +26 +30 +34 +38 +41 +45 +40 +53 +56 59 78 30 +23 +26 +30 +34 +38 +41 +45 +40 +53 +56 +75 34 21 24 27 31 34 38 41 44 48 51 68 36 20 23 26 20 32 36 40 43 47 51 55 59 78 30 +21 +22 +22 +22 +22 +27 +29 +32 +34 +37 +49 46 +14 +16 +19 +21 +23 +26 +20 +32 +35 +38 +41 +43 +57 50 12 14 16 18 20 22 24 26 28 30 32 36 40 48 13 15 17 10 22 24 26 28 30 32 36 30 32 43 41 51 51 18 20 23 25 28 31 34 15 17 10 22 24 26 28 30 32 25 28 30 33 35 38 41 40 43 46 61 40 +17 +20 +23 +26 +20 +32 +35 +38 +41 +43 +57 42 16 10 22 24 27 30 33 33 35 38 41 54 40 43 46 61 40 +17 +20 +23 +26 +20 +32 +35 +38 +41 +43 +57 42 16 10 22 24 27 30 33 33 35 38 41 54 40 65 61 61 61 61 61 61 61 61 61 61 61 61 61												
8						-		1				
12												1
14 20 33 38 43 48 52 57 62 67 71 95 16 28 33 37 42 47 51 56 61 65 70 93 18 27 32 37 41 46 50 55 59 64 68 91 20 +27 +31 +36 +40 +45 +40 +53 +58 +62 +67 +80 22 26 30 35 39 43 48 52 56 61 65 87 24 25 29 34 38 42 46 50 55 59 63 84 26 24 28 32 37 41 45 49 53 57 61 81 28 23 27 31 35 39 43 47 50 55 59 63 84 30 +23 +26 +30 34 36	10	+29	+34	+39	+44	+49	+54	+59	+64		+74	+ 98
16	12	29	34		44							97
18 27 32 37 41 46 50 55 59 64 68 91 20 +27 +31 +36 +40 +45 +40 +53 +58 +62 +67 +80 22 26 30 35 39 43 48 52 56 61 65 87 24 25 29 34 38 42 40 50 55 59 61 81 28 23 27 31 35 39 43 47 51 55 59 78 30 +23 +26 +30 +34 +38 +41 +45 +40 +53 +56 +75 32 22 25 29 32 36 40 43 47 50 54 48 34 21 24 27 31 34 38 41 44 48 51 68 38 18 22 25 28 31 34 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>												
22												
22	20	1 27			+ 10	+15	+ 10		+58	+62	167	+ 80
24							149					
26	24	25	29							59	63	84
30						1					61	81
32 22 25 29 32 36 40 43 47 50 54 72 34 21 24 27 31 34 38 41 44 48 51 68 36 20 23 26 29 32 36 39 42 46 49 65 38 18 22 25 28 31 34 37 40 43 46 49 65 40 +17 +20 +23 +26 +20 +32 +35 +38 +41 +43 +57 42 16 19 22 24 27 30 33 35 38 41 54 44 15 18 20 23 25 28 30 33 35 38 41 54 44 15 18 20 23 25 28 30 33 35 38 41 54 45 +15 +17 +19	28	23	27	31	35	39	43	47	51	55	59	78
34			1 '									
36 20 23 26 20 32 36 39 42 46 49 65 40 +17 +20 +23 +26 +20 +32 +35 +38 +41 +43 +57 42 16 19 22 24 27 30 33 35 38 41 54 44 15 18 20 23 25 28 30 33 35 38 41 54 45 +15 +17 +19 +22 +24 +27 +29 +32 +34 +37 +49 46 +14 +16 +19 +21 +23 +26 +28 +30 +33 +35 +46 48 13 15 17 19 22 24 26 28 30 32 43 50 12 14 16 18 20 22 24 26 28 30 32 24 43 50 0 10										50		
38 18 22 25 28 31 34 37 40 43 46 61 40 +17 +20 +23 +26 +20 +32 +35 +38 +41 +43 +57 42 16 10 22 24 27 30 33 35 38 41 54 44 15 18 20 23 25 28 30 33 35 38 41 45 +15 +17 +19 +22 +24 +27 +29 +32 +34 +37 +49 46 +14 +16 +19 +21 +23 +26 +28 +30 +33 +35 +46 48 13 15 17 19 22 24 26 28 30 32 43 50 12 14 16 18 20 22 24 26 28 30 32 43 54 10 11 13 15 16 18 10 21 23 24 32 55 9 10 11 13 14 16 17 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td> <td></td> <td></td> <td></td>									1			
42 16 19 22 24 27 30 33 35 38 41 54 44 15 18 20 23 25 28 30 33 35 38 41 54 45 +15 +17 +19 +22 +24 +27 +29 +32 +34 +37 +49 46 +14 +16 +19 +21 +23 +26 +28 +30 +33 +35 +46 48 13 15 17 19 22 24 26 28 30 32 43 50 12 14 16 18 20 22 24 26 28 30 40 52 +11 +13 +14 +16 +18 +20 +22 +23 +25 +27 +36 54 10 11 13 14 16 17 19 20 22 29 58 8 0 10 11 13												
42 16 19 22 24 27 30 33 35 38 41 54 44 15 18 20 23 25 28 30 33 35 38 41 54 45 +15 +17 +19 +22 +24 +27 +29 +32 +34 +37 +49 46 +14 +16 +19 +21 +23 +26 +28 +30 +33 +35 +46 48 13 15 17 10 22 24 26 28 30 32 43 50 12 14 16 18 20 22 24 26 28 30 40 52 +11 +13 +14 +16 +18 +20 +22 +23 +25 +27 +36 54 10 11 13 14 16 17 19 20 22 29 58 8 0 10 11 13	40	+17	+20	+23	+26	+20	+32	+35	+38	+41	+43	+ 57
45			19				30				41	
46	44	15	18	20	23	25	28		33	35	38	50
48	45	+15	+17	+19	+22	+24	+27	+29	+32	+34	+37	+ 49
48		+14	+16	+19	+21	+23	+26	+28	+30	+33	+35	+ 46
50	48		15				24	26	28	30		
54		I 2		16	18	20	22	24	26	28	30	40
56	52	+11	+13	+14								+ 36
58												
60 7 8 9 10 11 12 13 14 16 17 22 62 +6 +7 +8 +9 +10 +11 +11 +12 +13 +14 +19 64 5 6 6 7 7 8 0 9 10 11 12 16 60 4 5 5 6 7 7 8 0 9 10 13 68 3 4 4 5 5 6 6 7 7 8 11 70 2 3 3 4 4 4 5 5 6 6 8 72 +2 +2 +2 +3 +3 8 74 +1 +1 +1 +1 +1 +1 +1 +1 +1 76 +1						1			1			
64												
64 5 6 6 7 8 9 10 10 11 12 16 66 4 5 5 6 7 7 8 9 9 10 13 68 3 4 4 5 5 6 6 7 7 8 11 70 2 3 3 4 4 4 5 5 6 6 72 + 2 + 2 + 2 + 2 + 74 + 1 <td>62</td> <td>+ 6</td> <td>+ 7</td> <td>+ 8</td> <td>+ 0</td> <td>+10</td> <td>+11</td> <td>+11</td> <td>+12</td> <td>+13</td> <td>+14</td> <td>+ 10</td>	62	+ 6	+ 7	+ 8	+ 0	+10	+11	+11	+12	+13	+14	+ 10
66							1	1 .				
68 70 2 3 4 4 5 5 6 6 7 7 8 8 11 8 72 +2 +2 +2 +2 +3 +3 76 +1 +1 +1 +1 +1 +1 +1 +1 +1 +1	66		5	5			7		, 0	9		13
72		3	4	4		5	6					II
74	70	2	3	3	4	4	4	5	5	6	6	8
76 + 1 + 1 + 1 + 1 + 1					+ 3	+ 3						
						+ 2 + 1						

ENGLISH MEASURES.

Correction for an Average Degree of Humidity.

Mean Temper-	APPF	ROXIMA	TE DI	FFERE	NCE OI	HEIG	нт ов:	TAINEI	FROM	TABL	ES 51-	52
ature.	500	1000	2000	3000	4000	5000	6000	7000	8000	9000	10000	20000
F. -20° - 16 - 12	Feet. O O	Feet. O O	Feet. O O + I	Feet. O + I I	Feet. O + I I	Feet. 0 + 1 2	Feet. 0 + I 2	Feet. + I I 2	Feet. + 1 2 3	Feet. + I 2 3	Feet. + I 2 3	Feet. + 2 4 6
- 8 - 6 - 4 - 2	0 0 0	0 0 + 1	I I I	I I 2 2	2 2 2 2	2 2 3 3	3 3 3 4	3 3 4 4	4 4 4 5	4 4 5 6	4 5 6 6	9 10 11 12
0 + 2 4 6 8	0 0 0	I I I	I I 2 2 2	2 2 2 3 3	3 3 4 4	3 4 4 4 5	4 4 5 5 6	5 5 6 6 7	5 6 7 7 8	6 7 7 8 9	7 7 8 9	14 15 16 18
10 12 14 16 18	1 1 1 1	I I I	2 2 2 3 3	3 3 4 4 4	4 4 5 5 5	5 6 6 6 7	6 7 7 8 8	7 8 8 9 9	9 10 11	9 10 11 11	10 11 12 13 13	2I 22 24 25 27
20 22 24 26 28	I I I	I 2 2 2 2	3 3 3 4	4 5 5 5 6	6 7 7 7	7 8 8 9	10 10 10	10 11 11 12 13	11 12 13 14 15	13 14 15 16 17	14 15 16 17	29 31 33 35 37
30 32 34 36 38	I I I	2 2 2 3 3	4 4 5 5 6	6 7 7 8 9	8 9 10 11 12	10 11 12 13 15	12 13 15 16 18	14 16 17 19 21	16 18 19 21 23	18 20 22 ·24 26	20 22 24 27 29	41 44 49 53 59
40 42 44 46 48	2 2 2 2 2	3 4 4 4 5	6 7 8 8 9	10 11 12 13 14	13 14 15 17 18	16 18 19 21 23	19 21 23 25 27	23 25 27 29 32	26 28 31 34 37	29 32 35 38 41	32 35 39 4 2 46	64 71 77 84 92
50 52 54 56 58	2 3 3 3 3	5 5 6 6 6	10 11 11 12 13	15 16 17 18	20 21 23 24 26	25 27 29 30 32	30 32 34 37 39	35 37 40 43 45	40 43 46 49 52	45 48 51 55 58	50 53 57 61 65	99 107 114 122 130
60 62 64 66 68	3 4 4 4 4	7 7 8 8 8	14 14 15 16 17	21 22 23 24 25	27 29 30 32 34	34 36 38 40 42	41 43 46 48 50	48 51 53 56 59	55 58 61 64 67	62 65 69 72 76	69 72 76 80 84	137 145 152 160 168
70 72	4 5	9	18 18	26 27	35 37	44 46	53 55	61 64	70 73	79 82	88 91	175
76 80 84 88 92 96	5 6 6 6 7	10 11 11 12 13 14	20 21 23 24 26 27	30 32 34 37 39 41	40 43 46 49 52 55	49 53 57 61 65 68	59 64 68 73 78 82	69 75 80 85 91 96	79 85 91 97 103 110	89 96 103 110 116 123	99 106 114 122 129 137	198 213 228 243 259 274

ENGLISH MEASURES.

Correction for the Variation of Gravity with Altitude: $\frac{z(z+2h_0)}{R}$.

Approx- imate			Н	EIGHT	of Lo	WER S	TATIO	N IN F	EET (A	i _o).		
difference of height. Z.	0	1000	2000	3000	4000	5000	6000	7000	8000	9000	10000	12000
Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.
500	0	0	0	0	0	0	0	0	0	0	0	+ 1
1000	0	0	0	0	0	+ 1	+1	+1	+1	+1	+ 1	I
1500	0	0	0	+ 1	+ 1	I	I	I	I	I	2	2
2000	0	0	+ 1	I	I	I	Ι	2	2	2	2	2
2500	0	+ 1	I	I	I	I	2	2	2	2	3	3
3000	0	I	I	I	2	2	2	2	3	3	3	4
3500	+ 1	I	I	2	2	2	3	3	3	4	4	5
4000	I	I	2	2	2	3	3	3	4	4	5	5 6
4500	I	I	2	2	3	3	4	4	4	5	5	6
5000	I	2	2	3	3	4	4	5	5	6	6	7
5500	I	2	3	3	4	4	5	5	6	6	7	8
6000	2	2	3	3	4	5	5	6	6	7 8	7 S	9
6500	2	3	3	4	5	5 6	6	7	7 8	8	9	9 10
7000	2	3	4	4	5	0	0	1	0	0	9	10
7500	3	3	4	5	6	6	7	8	8	9	10	ΙI
8000	3	4	5	5	6	7	8	8	9	10	II	12
8500	3	4	5	6	7	8	8	9	10	11	12	13
9000	4	5	6	6	7	8	9	10	ΙΙ	12	12	14
9500	4	5	6.	7	8	9	10	11	12	13	13	15
10000	5	6	7	8	9	IO	II	11	12	13	14	16
11000	6	7	8	9	10	11	12	13	14	15	16	18
12000	7	8	9	10	II	13	14	15	16	17	18	2 I
13000	S	9	ΙΙ	12	13	14	16	17	18	19	21	23
14000	9	II	12	13	15	16	17	19	20	21	23	25
15000	11	12	1.4	15	17	18	19	21	22	24	25	28
16000	12	14	15	17	18	20	21	23	25	26	28	31
17000	14	15	17	19	20	22	2.1	25	27	28	30	
18000	16	17	19	21	22	24	26	28	30	31		
19000	17	19	21	23	25	26	28	30	32			
20000	19	21	23	25	27	29	31					

METRIC MEASURES.

Values of 18400 log 760.

		1									
	rometric essure.	0	1	2	3	4	5	6	7	8	9
	300 310 320 330 340	m. 7428 7166 6912 6666 6428	m. 7401 7140 6887 6642 6405	m. 7375 7115 6862 6618 6381	m. 7348 7089 6838 6594 6358	m. 7322 7064 6813 6570 6334	7296 7038 6789 6546 6311	m. 7270 7013 6764 6522 6288	6987	7218 6962 6715 6475 6242	111. 7192 6937 6691 6451 6219
	350 360 370 380 390	6196 5971 5752 5539 5332	6173 5949 5730 5518 5311	6151 5927 5709 5497 5291	6128 5905 5687 5476 5270	6106 5883 5666 5455 5250	6083 5861 5644 5434 5229	6061 5839 5623 5414 5209	6038 5817 5602 5393 5189	6016 5795 5581 5373 5169	5993 5773 5560 5352 5149
4	100 410 420 430 440	5129 4932 4739 4551 4368	5109 4912 4720 4532 4350	5089 4893 4701 4514 4332	5069 4873 4682 4495 4314	5049 4854 4663 4477 4296	5029 4834 4644 4458 4278	5010 4815 4625 4440 4260	4990 4796 4606 4422 4242	4971 4777 4588 4404 4224	4951 4758 4569 4386 4206
4	150 160 170 180 190	4188 4012 3840 3672 3507	4170 3994 3823 3655 3490	4152 3977 3806 3639 3474	4134 3959 3789 3622 3458	4117 3942 3772 3606 3442	4099 3925 3755 3589 3426	4082 3908 3738 3573 3410	4064 3891 3721 3556 3394	4047 3874 3705 3540 3378	4029 3 ⁸ 57 3688 3523 3362
5 5 5	00 510 520 530 540	3346 3188 3033 2880 2731	3330 3172 3017 2865 2716	3314 3157 3002 2850 2701	3298 3141 2986 2835 2687	3282 3126 2971 2820 2672	3266 3110 2955 2805 2657	3250 3095 2940 2790 2643	3235 3079 2925 2775 2628	3219 3064 2910 2760 2613	3203 3048 2895 2745 2599
5 5 5	50 60 70 80 90	2584 2440 2299 2160 2023	2570 2426 2285 2146 2010	2555 2411 2271 2133 1996	2541 2397 2257 2119 1983	2526 2383 2243 2105 1969	2512 2369 2229 2092 1956	2497 2355 2215 2078 1942	2483 2341 2201 2064 1929	2468 2327 2188 2051 1915	2454 2313 2174 2037 1902
6 6 6	00 10 20 30 40	1889 1757 1627 1499 1373	1875 1744 1614 1486 1361	1862 1731 1601 1474 1348	1848 1718 1588 1461 1336	1835 1705 1576 1448 1323	1822 1692 1563 1436	1809 1679 1550 1423 1298	1796 1666 1537 1411 1286	1783 1653 1525 1398 1273	1770 1640 1512 1386 1261
6 6	50 60 70 80 90	1249 1127 1007 889 772	1236 1115 995 877 761	1224 1103 983 866 749	1212 1091 971 854 738	1199 1079 960 842 726	1187 1067 948 831 715	1175 1055 936 819 703	1163 1043 924 807 692	1151 1031 913 796 680	1139 1019 901 784 669
7 74 73	00 10 20 30 40	657 544 432 322 213	646 533 421 311 202	635 521 410 300 192	623 510 399 2 89 181	612 499 388 278 170	601 487 377 267 160	589 476 366 256 149	578 465 355 245 138	567 454 344 234 128	555 443 333 224 117
76	50	0	- 10	- 21	- 31	+ 64 - 42 - 146	+ 53 - 52 - 156	+ 43 - 63 - 166	+ 3 ² - 73 - 177	+ 22 - 83 - 187	+ 11 - 94 - 197

TABLE 57.

DETERMINATION OF HEICHTS BY THE BAROMETER.

DYNAMIC MEASURES.

Values of 18400 log $\frac{1013.3}{B}$

						B				
Baro- metric Pressure	0	1	2	3	4	5	6	7	8	9
mb.	m.	m.	m.	m.	m,	m.	m.	m.	m,	m.
0	ω	55306	49767	46527	44228	42445	40988	39756	38689	37748
IO	36906	36144	35448	34809	34217	33666	33150	32665	32200	31777
20	31367	30977	30605	30250	29910	29584	29270	28969	28678	28397
30	28127	27865	27611	27365	27126	26895	26670	26451	26238	2603 I
40	25828	25630	25438	25250	25066	24887	24711	24539	24371	24206
50	24043	23886	23731	23579	23430	23283	23139	22998	22859	22722
60	22588	22456	22326	22198	22072	21948	21827	21706	21587	21471
70	21356	21242	21131	21021	20012	20805	20699	20594	20491	20389
80	20289	20189	20092	19995	19899	19804	19711	19618	19527	19437
90	19348	19259	19172	19086	19000	18916	10032	18749	18667	18586
100	18506	18426	18347	18269	18192	18116	18040	17965	17891	17817
110	17744	17672	17600	17529	17459	17389	17320	17251	17183	17115
120	17040	16982	16917	16851	16787	16722	16659	16596	16533	16471
130	16409	16348	16287	16227	16167	16108	16048	15990	15932	15874
140	15817	15760	15703	15647	15592	15536	15482	15427	15373	15319
150	15266	15212	15160	15107	15055	15004	14952	14901	14850	14800
160	14750	14700	14650	14601	14553	14504	14456	14408	14360	14312
170	14265	14218	14172	14125	14079	14034	13988	13943	13898	13853
180	13809	13764	13720	13677	13633	13590	13547	13504	13461	13419
190	13377	13335	13293	13251	13210	13169	13128	13087	13047	13007
200	12967	12927	12887	12848	12808	12769	12730	12692	12653	12615
210	12577	12539	12501	12463	12426	12389	12352	12315	12278	12242
220	12205	12169	12133	12007	12061	12026	11990	11955	11920	11885
230	11850	11815	11781	11746	11712	11678	11644	11610	11577	11543
240	11510	11476	11443	11410	11378	11345	11312	11280	11248	11216
250	11184	11152	11120	11088	1.1057	11025	10004	10963	10032	10001
260	10870	10839	10809	10778	10748	10718	10688	10658	10628	10598
270	10569	10539	10510	10480	10451	10422	10393	10364	10335	10307
280	10278	10249	10221	10193	10165	10137	10108	10081	10053	10025
290	9997	9970	9943	9915	9888	9861	9834	9807	9780	9753
300	9727	9700	9674	9647	9621	9594	9568	9542	9516	9490
310	9465	9439	9413	9388	9362	9337	9311	9286	9261	9236
320	9211	9186	9161	9136	9111	9087	9062	9038	9014	8989
330	8965	8941	8917	8893	8869	8845	8821	8797	8773	8750
340	8726	8703	8679	8656	8633	8610	8587	8564	8541	8518
350	8495	8472	8449	8427	8404	8381	8359	8336	8314	8292
360	8270	8247	8225	8203	8181	8159	8138	8116	8094	8073
370	8051	8029	8008	7986	7965	7943	7922	7901	7880	7859
380	7838	7817	7796	7775	7754	7733	7712	7692	7671	7651
390	7630	7610	7589	7569	7548	7528	7508	7488	7468	7448
400	7428	7408	7388	7368	7348	7328	7300	7289	7269	7250
410	7230	7211	7191	7172	7153	7133	7114	7095	7076	7057
420	7038	7019	7000	6704	6776	67.77	6720	6721		6868
430	6850	6831	6813	6794	6776	6757 6576	6739	6721	6703	6504
11										
450	6487	6469	6451	6433	6416	6398	6381	6363	6346	6328
460	6311	6294	6276	6259	6242	6225	6207	6021	6004	5987
480	6139 5071	5954	5937	5921	5904	5888	5871	5855	5839	5822
490	5806	5790	5773	5757	5741	5725	5709	5693	5677	5661
1490	3000	3190	3113	3131	3142	3,733	3139	3.93	3.77	

SMITHSONIAN TABLES.

DYNAMIC MEASURES.

Values of 18400 log $\frac{1013.3}{B}$

						<u> </u>				
Barometric Pressure	0	1	2	3	4	5	6	7	8	9
mb.	m.	m.	m.	m.	m.	m,	m.	m.	m.	m.
500	5645	5629	5613	5597	5581	5565	5549	5533	5518	5502
510	5486	5471	5455	5439	5424	5408	5393	5377	5362	5346
520	5331	5316	5300	5285	5270	5255	5239	5224	5200	5194
530	5179	5164	5149	5134	5119	5104	5089	5074	5059	5044
540	5030	5015	5000	4985	4971	4956	4941	4927	4912	4898
550	4883	4868	4854	4839	4825	4811	4796	4782	4768	4753
560	4739	4725	4710	4696	4682	4668	4654	4640	4626	4612
570	4598	4583	4569	4556	4542	4528	4514	4500	4486	4472
580	4459	4445	4431	4417	4404	4390	4376	4363	4349	4335
590	4322	4308	4295	4281	4268	4254	4241	4228	4214	4201
600	4188	4174	4161	4148	4134	4121	4108	4095	4082	4069
610	4056	4042	4029	4016	4003	3990	3977	3964	3951	3939
620	3926	3913	3900	3887	3874	3861	3849	3836	3823	3810
630	3798	3785	3772	3760	3747	3735	3722	3700	3697	3684
640	3672	3659	3647	3635	3622	3610	3597	3585	3573	3560
650	3548	3536	3523	3511	3499	3487	3475	3462	3450	3438
660	3426	3414	3402	3390	3378	3366	3354	3342	3330	3318
670	3306	3294	3282	3270	3258	3246	3235	3223	3211	3199
680	3187	3176	3164	3152	3141	3129	3117	3106	3094	3082
690	3071	3059	3048	3036	3025	3013	3002	2990	2979	2967
700	2956	2944	2933	2922	2910	2899	2888	2876	2865	2854
710	2842	2831	2820	2800	2798	2786	2775	2764	2753	2742
720	2731	2720	2708	2697	2686	2675	2664	2653	2642	2631
730	2621	2609	2599	2588	2577	2566	2555	2544	2533	2523
740	2512	2501	2490	2479	2469	2458	2447	2437	2426	2415
750	2405	2394	2383	2373	2362	2351	2341	2330	2320	2309
760	2299	2288	2278	2267	2257	2246	2236	2225	2215	2 205
770	2194	2184	2173	2163	2153	2142	2132	2122	2112	2101
78o	2001	2081	2071	2060	2050	2040	2030	2020	2009	1000
790	1989	1979	1969	1959	1949	1939	1929	1919	1909	1899
800	1889	1879	1869	1859	1849	1839	1829	1819	1809	1799
810	1789	1780	1770	1760	1750	1740	1731	1721	1711	1701
820	1692		1672	1662 1566	1653	1643	1633	1623	1614	1604
830 840	1595	1585	1575 1480	1470	1556	1547	1537	1527	1518	1508
11	1499	1			1	1451	1442	1433	1423	1414
850	1404	1395	1386	1376	1367	1357	1348	1330	1329	1320
860	1311	1302	1292	1283	1274	1264	1255	1246	1237	1228
870 880		1209	I 200 I 100	1101	1001	1173 1082	1164	1154	1145	1136
890	1127	1028	1010	1010	1001	992	983	974	1055 965	956
1								886	, -	868
900	948	939	930	92I 822	912 824	903	894	798	877 789	781
910	859	850 763	842	833		815	807 720	798		694
920	772 686	677	755 668	746 660	737 651	729 643	634	626	7 0 3 617	608
930	600	592	583	575	566	558	549	541	532	524
950				490	482		465		448	- 1
950	516	507 424	499 415	490	399	474 390	382	457 374	365	440 357
970	432 349	34I	332	324	316	398	300	292	283	275
980	267	259	251	243	234	226	218	210	202	194
990	186	178	170	162	154	146	138	130	122	114
1000	106	98	90	82	74	66	58	50	42	
1000	26	. 18	10	2	- 6	- 13	- 21	- 20	$-\frac{42}{37}$	- 34 - 45
1010	- 53	- 61	- 68	- 76	- 84	- 92	-100	-107	-115	-123
1030	-131	-138	-146	-154	- 162	-169	-177	- 185	-192	- 200
1040	- 208	-215	-223	-231	-238	-246	- 254	-261	- 269	- 277
			1							

DETERMINATION OF HEIGHTS BY THE BAROMETER. METRIC MEASURES.

Temperature correction factor, $a = .00367 \theta$.

Multiply approximate altitudes, determined from table 56 or 57. by values of a corresponding to mean temperature, θ , of air column. Add, if θ is above o° C; subtract, if below o° C.

Mean										
Temp. θ	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
°c.	a.	a.	a.	a,	a.	a.	a.	a.	a.	a.
0	0.000	0.000	0.001	0.001	0.001	0.002	0.002	0.003	0.003	0.003
I	.004	.004	.004	.005	.005	.006	.006	.006	.007	.007
2	.007	.008	.008	.008	.000	.000	.010	.010	.010	110.
3	.011	.011	.012	.012	.012	.013	.013	.014	.014	.014
4		_								
5	.018	.019	.019	.019	.020	.020	.021	.021	.02 I	.022
	.022 .026	.022	.023	.023	.023	.024	.024	.025	.025	.025
7 8	.020	.030	.030	.030	.031	.031	.032	.032	.032	.033
9	.033	.033	.034	.034	.034	.035	.035	.036	.036	.036
10	.037	.037	.037	.038	.038	.039	.039	.039	.040	.040
11	.040	.041	.041	.041	.042	.042	.043	.043	.043	.044
12	.044	.041	.045	.045	.046	.046	.046	.047	.047	.047
13	.048	.048	.048	.049	.040	.050	.050	.050	.051	.051
14	.051	.052	.052	.552	.053	.053	.054	.054	.054	.055
15	.055	.055	.056	.056	-057	.057	.057	.058	.058	.058
16	.059	.059	.059	.060	.060	.061	.061	.061	.062	.062
17	.062	.063	.003	.063	.064	.064	.065	.065	.065	.066
18	.066	.066	.067	.067	.068	.068	.068	.069	.069	.069
19	.070	.070	.070	.071	.071		.072	.072	.073	.073
20	.073	.074	.074	.075	.075	.075	.076	.076	.076	.077
2 I 2 2	.077	.077	.078	.078	.079	.079	.079	.080 .083	.080	.080
22	.081	.085	.085	.086	.086	.086	.087	.087	.087	.088
24	.088	.088	.080	.080	.000	.000	.000	.007	.001	.001
25	.002	.002	.002	.003	.003	.004	.004	.004	.005	.005
26	.005	.006	.006	.007	.097	.097	.008	.008	.008	.000
27	.000	.000	.100	.100	.101	.101	.101	.102	.102	.102
28	.103	.103	.103	.104	.104	.105	.105	.105	.106	.106
29	.106	.107	.107	.108	.108	.108	.109	.109	.109	.110
30	.110	.110	.111	111.	.112	.112	.112	.113	.113	.113
31	.114	.114	.115	.115	.115	.116	.116	.116	.117	.117
32	.117	.118	.118	.119	.119	.119	.120	.120	.120	.121
33	.121	.121	.122	.122	.123	.123	.123	.124	.124	.124
34	.125	.125	.126	.126		.127	.127	.127		
35	.128	.129	.120	.130	.130	.130	.131	.131	.131	.132
36	.132	.132	.133	.133	.134	.134	.134	.135 .138	.135	.135
37 38	.136	.130	.137	.141	.141	.130	.142	.142	.142	.143
39	.139	.143	.144	.144	.145	.145	.145	.146	.146	.146
40	.147	.147	.148	.148	.148	.140	.140	.140	.150	.150
41	.150	.151	.151	.152	.152	.152	.153	.153	.153	.154
42	.154	.155	.155	.155	.156	.156	.156	.157	.157	.157
43	.158	.158	.159	.159	.159	.160	.160	.160	.161	.161
44	.161	.162	.162	.163	.163	.163	.164	.164	.164	.165
45	.165	.166	.166	.166	.167	.167	.167	.168	.168	.168
46	.169	.169	.170	.170	.170	.171	.171	.171	.172	.172
47	.172	.173	.173	.174	.174	.174	.175	.175	.175	.176
48	.176 .180	.177	.177	.177	.178	.178 .182	.178	.179	.179	.179
49	1							.186	.186	.187
50	.184	.184	.184	.185	.185	.185	.186	.180	.180	.187
1		-								

METRIC MEASURES.

Term for Temperature: $0.00367 \theta \times z$.

For temperatures { above o° C. } the values are to be { added. subtracted.

Approx-													
imate differ-	M	IEAN	TEMP	ERATU	JRE O	F AIR	COLU	MN IN	CENT	IGRADI	E DEGI	REES (9).
ence of height. Z.	l°	2°	3°	4°	5°	6°	7 °	8°	9°	I0°	20°	30°	40°
m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.	m.
100 200 300 400	O I I I	1 1 2 3	1 2 3 4	3 4 6	2 4 6 7	2 4 7 9	3 5 8 10	3 6 9 12	3 7 10 13	4 7 11 15	7 15 22 29	11 22 33 44	15 29 44 59
500 600 700 800 900	2 2 3 3 3	4 4 5 6 7	6 7 8 9	7 9 10 12 13	9 11 13 15	11 13 15 18 20	13 15 18 21 23	15 18 21 23 26	17 20 23 26 30	18 22 26 29 33	37 44 51 59 66	55 66 77 88 99	73 88 103 117 132
1000 1100 1200 1300 1400	4 4 4 5 5	7 8 9 10	11 12 13 14 15	15 16 18 19 21	18 20 22 24 26	22 24 26 29 31	26 28 31 33 36	29 32 35 38 41	33 36 40 43 46	37 40 44 48 51	73 81 88 95 103	110 121 132 143 154	147 161 176 191 206
1500 1600 1700 1800 1900	6 6 7 7	11 12 12 13 14	17 18 19 20 21	22 23 25 26 28	28 29 31 33 35	33 35 37 40 42	39 41 44 46 49	44 47 50 53 56	50 53 56 59 63	55 59 62 66 70	110 117 125 132 139	165 176 187 198 209	220 235 250 264 279
2000 2100 2200 2300 2400	7 8 8 9	15 15 16 17 18	22 23 24 25 26	29 31 32 34 35	37 39 40 42 44	44 46 48 51 53	51 54 57 59 62	59 62 65 68 70	66 69 73 76 79	73 77 81 84 88	147 154 161 169 176	220 231 242 253 264	294 308 323 338 352
2500 2600 2700 2800 2900	9 10 10	18 19 20 21 21	28 29 30 31 32	37 38 40 41 43	46 48 50 51 53	55 57 59 62 64	64 67 69 72 75	73 76 79 82 85	83 86 89 92 96	92 95 99 103 106	184 191 198 206 213	275 286 297 308 319	367 382 396 411 426
3000 3100 3200 3300 3400	11 11 12 12 12	22 23 23 24 25	33 34 35 36 37	44 46 47 48 50	55 57 59 61 62	66 68 70 73 75	77 80 82 85 87	88 91 94 97 100	99 102 106 109 112	110 114 117 121 125	220 228 235 242 250	330 341 352 363 374	440 455 470 484 499
3500 3600 3700 3800 3900	13 13 14 14 14	26 26 27 28 29	39 40 41 42 43	51 53 54 56 57	64 66 68 70 72	77 79 81 84 86	90 92 95 98 100	103 106 109 112 115	116 119 122 126 129	128 132 136 139 143	257 264 272 279 286	385 396 407 418 429	514 528 543 558 573
4000 5000 6000 7000	15 18 22 26	29 37 44 51	44 55 66 77	59 73 88 103	73 92 110 128	88 110 132 154	103 128 154 180	117 147 176 206	132 165 198 231	147 183 220 257	294 367 440 514	440 551 661 771	587 734 881 1028

METRIC MEASURES.

Correction for Humidity: Values of 10000 β .

$$\beta = 0.378 \frac{e}{b} = 0.378 \frac{e_1 + e_0}{B + B_0}$$

Mean Vapor			MEAN	BARC	METR	IC PRI	ESSURI	E IN M		ETER:	$s\left(\frac{B}{a}\right)$	$+B_{\circ}$		
Pressure. $e = \frac{e_1 + e_0}{2}$	500	520	540	560	580	600	620	640	660	680	700	720	740	760
mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm,	mm.	mm.	mm.	mm.
1	8	7	7	7	7	6	6	6	6	6	5	5	5	5
2	15	15	14	14	13	13	12	12	11	11	11	11	10	10
3	23	22	21	20	20	19	18	18	17	17	16	16	15	15
4	30	29	28	27	26	25	24	24	23	22	22	21	20	20
5	38	36	35	34	33	31	30	30	29	28	27	26	26	25
6	45	44	42	41	39	38	37	35	34	33	32	32	31	30
7	53	51	49	47	46	44	43	41	40	39	38	37	36	35
8	60	58	56	54	52	50	49	47	46	44	43	42	41	40
9	68	65	63	61	59	57	55	53	52	50	49	47	46	45
10	76	73	70	68	65	63	61	59	57	56	54	53	51	50
11	83	80	77	74	72	69	67	65	63	61	59	58	56	55
12	91	87	84	81	78	76	73	71	69	67	65	63	61	60
13	98	95	91	88	85	82	79	77	74	72	70	68	66	65
14	106	102	98	95	91	88	85	83	80	78	76	74	72	70
15 16 17 18	113 121 129 136 144	109 116 124 131 138	105 112 119 126 133	101 108 115 122 128	98 104 111 117 124	95 101 107 113 120	91 98 104 110 116	89 94 100 106 112	86 92 97 103 109	83 89 94 100 106	81 86 92 97 103	79 84 89 95 100	77 82 87 92 97	75 80 85 90 95
20	151	145	140	135	130	126	122	118	115	111	108	105	102	99
21	159	153	147	142	137	132	128	124	120	117	113	110	107	104
22	166	160	154	149	143	139	134	130	126	122	119	116	112	109
23	174	167	161	155	150	145	140	136	132	128	124	121	117	114
24	181	174	168	162	156	151	146	142	137	133	130	126	123	119
25	189	182	175	169	163	157	152	148	143	139	135	131	128	124
26	197	189	182	175	169	164	159	154	149	145	140	137	133	129
27	204	196	189	182	176	170	165	159	155	150	146	142	138	134
28	212	204	196	189	182	176	171	165	160	156	151	147	143	139
29	219	211	203	196	189	183	177	171	166	161	157	152	148	144
30	227	218	210	203	196	189	183	177	172	167	162	158	153	149
31	234	225	217	209	202	195	189	183	178	172	167	163	158	154
32	242	233	224	216	209	202	195	189	183	178	173	168	163	159
33	249	240	231	223	215	208	201	195	189	183	178	173	169	164
34	257	247	238	230	222	214	207	201	195	189	184	179	174	169
35	265	254	245	236	228	220	213	207	200	195	189	184	179	174
36	272	262	252	243	235	227	219	213	206	200	194	189	184	179
37	280	269	259	250	241	233	226	219	212	206	200	194	189	184
38	287	276	266	257	248	239	232	224	218	211	205	200	194	189
39	295	283	273	263	254	246	238	230	223	217	211	205	199	194
40	302	291	280	270	261	252	244	236	229	222	216	210	204	199

METRIC MEASURES.

Correction for Humidity: 10000 $\beta \times z$.

Top argument: Values of 10000 β obtained from page 148 Side argument: Approximate difference of height (z).

Approximate Difference						IC	οοοο β.					
of Height.	25	50	75	100	125	150	175	200	225	250	275	300
m.	m,	m.	m.	m.	m.	m.	111.	m.	m.	m.	m.	m.
100 200 300 400	0.3 0.5 0.8 1.0	0.5 1.0 1.5 2.0	0.8 1.5 2.3 3.0	1.0 2.0 3.0 4.0	1.3 2.5 3.8 5.0	1.5 3.0 4.5 6.0	1.8 3.5 5.3 7.0	2.0 4.0 6.0 8.0	2.3 4.5 6.8 9.0	2.5 5.0 7.5 10.0	5.5 8.3	3.0 6.0 9.0 12.0
500	I.3	2.5	3.8	5.0	6.3	7.5	8.8	10.0	11.3	12.5	13.8	15.0
600	I.5	3.0	4.5	6.0	7.5	9.0	10.5	12.0	13.5	15.0	16.5	18.0
700	I.8	3.5	5.3	7.0	8.8	10.5	12.3	14.0	15.8	17.5	19.3	21.0
800	2.0	4.0	6.0	8.0	10.0	12.0	14.0	16.0	18.0	20.0	22.0	24.0
900	2.3	4.5	6.8	9.0	11.3	13.5	15.8	18.0	20.3	22.5	24.8	27.0
1000	2.5	5.0	7.5	10.0	12.5	15.0	17.5	20.0	22.5	25.0	27.5	30.0
1100	2.8	5.5	8.3	11.0	13.8	16.5	19.3	22.0	24.8	27.5	30.3	33.0
1200	3.0	6.0	9.0	12.0	15.0	18.0	21.0	24.0	27.0	30.0	33.0	36.0
1300	3.3	6.5	9.8	13.0	16.3	19.5	22.8	26.0	29.3	32.5	35.8	39.0
1400	3.5	7.0	10.5	14.0	17.5	21.0	24.5	28.0	31.5	35.0	38.5	42.0
1500	3.8	7.5	11.3	15.0	18.8	22.5	26.3	30.0	33.8	37.5	41.3	45.0
1600	4.0	8.0	12.0	16.0	20.0	24.0	28.0	32.0	36.0	40.0	44.0	48.0
1700	4.3	8.5	12.8	17.0	21.3	25.5	29.8	34.0	38.3	42.5	46.8	51.0
1800	4.5	9.0	13.5	18.0	22.5	27.0	31.5	36.0	40.5	45.0	49.5	54.0
1900	4.8	9.5	14.3	19.0	23.8	28.5	33.3	38.0	42.8	47.5	52.3	57.0
2000	5.0	10.0	15.0	20.0	25.0	30.0	35.0	40.0	45.0	50.0	55.0	60.0
2100	5.3	10.5	15.8	21.0	26.3	31.5	36.8	42.0	47.3	52.5	57.8	63.0
2200	5.5	11.0	16.5	22.0	27.5	33.0	38.5	44.0	49.5	55.0	60.5	66.0
2300	5.8	11.5	17.3	23.0	28.8	34.5	40.3	46.0	51.8	57.5	63.3	69.0
2400	6.0	12.0	18.0	24.0	30.0	36.0	42.0	48.0	54.0	60.0	66.0	72.0
2500	6.3	12.5	18.8	25.0	31.3	37·5	43.8	50.0	56.3	62.5	68.8	75.0
2600	6.5	13.0	19.5	26.0	32.5	39.0	45.5	52.0	58.5	65.0	71.5	78.0
2700	6.8	13.5	20.3	27.0	33.8	40.5	47.3	54.0	60.8	67.5	74.3	81.0
2800	7.0	14.0	21.0	28.0	35.0	42.0	49.0	56.0	63.0	70.0	77.0	84.0
2900	7.3	14.5	21.8	29.0	36.3	43·5	50.8	58.0	65.3	72.5	79.8	87.0
3000 3100 3200 3300 3400	7.5 7.8 8.0 8.3 8.5	15.0 15.5 16.0 16.5 17.0	22.5 23.3 24.0 24.8 25.5	30.0 31.0 32.0 33.0 34.0	37.5 38.8 40.0 41.3 42.5	45.0 46.5 48.0 49.5 51.0	52.5 54.3 56.0 57.8 59.5	60.0 62.0 64.0 66.0 68.0	67.5 69.8 72.0 74.3 76.5	75.0 77.5 80.0 82.5 85.0	82.5 85.3 88.0 90.8 93.5	90.0 93.0 96.0 99.0
3500	8.8	17.5	26.3	35.0	43.8	52.5	61.3	70.0	78.8	87.5	96.3	105.0
3600	9.0	18.0	27.0	36.0	45.0	54.0	63.0	72.0	81.0	90.0	99.0	108.0
3700	9.3	18.5	27.8	37.0	46.3	55.5	64.8	74.0	83.3	92.5	101.8	111.0
3800	9.5	19.0	28.5	38.0	47.5	57.0	66.5	76.0	85.5	95.0	104.5	114.0
3900	9.8	19.5	29.3	39.0	48.8	58.5	68.3	78.0	87.8	97.5	107.3	117.0
4000	10.0	20.0	30.0	40.0	50.0	60.0	70.0	So.0	90.0	100.0	110.0	120.0
5000	12.5	25.0	37.5	50.0	62.5	75.0	87.5	100.0	112.5	125.0	137.5	150.0
6000	15.0	30.0	45.0	60.0	75.0	90.0	105.0	120 0	135.0	150.0	165.0	180.0
7000	17.5	35.0	52.5	70.0	87.5	105.0	122.5	140.0	157.5	175.0	192.5	210.0

TABLE 61

DETERMINATION OF HEIGHTS BY THE BAROMETER.

METRIC MEASURES.

Correction for Humidity: Values of $\frac{1}{2} \left(\frac{0.378 \frac{\epsilon}{\delta}}{0.00367} \right)$

Top argument: Values of e. Side argument: Values of b. Auxiliary to Table 58.

Air					V.	APOR P	RESSUF	RE mm.					
Pres- sure.	0.5	1	2	3	4	5	6	7	8	9	10	20	30
mm. 780 760 740 720 700	°C.	°C. O. I . I . I . I	°C. O.I .I .I .I	°C 0.2 .2 .2 .2 .2 .2	°c. 0.3 ·3 ·3 ·3	°C. 0.3 .3 .4 .4	°C. 0.4 .4 .4 .4	°c. 0.5 ·5 ·5 ·5	°C, 0.5 .5 .6 .6	°c. o.6 .6 .6 .6	°c. 0.7 ·7 ·7 ·7 ·7	°C. 1.3 1.4 1.4 1.4 1.5	°C. 2.0 2.0 2.1 2.1 2.2
680 660 640 620 600	.0	. I . I . I . I	.2 .2 .2 .2 .2 .2	.2 .2 .2 .2 .3	.3 .3 .3 .3	•4 •4 •4 •4	.4 .5 .5 .5	·5 ·5 .6 .6	.6 .6 .6 .7	·7 ·7 ·7 ·8 .8	.8 .8 .8 .8	1.5 1.6 1.6 1.7	
580 560 540 520 500	.0	.I .I .I .I	.2 .2 .2 .2 .2 .2	·3 ·3 ·3 ·3	.4 .4 .4 .4	•4 •5 •5 •5	.5 .6 .6 .6	.6 .5 .7 .7	.7 .7 .8 .8	.8 .8 .9	.9 .9 I.0		
480 460 440 420 400	.I .I .I .I	. I . I . I . I	.2 .2 .2 .2 .3	·3 ·3 ·4 ·4	.4 .4 .5 .5	.5 .6 .6 .6	.6 •7 •7	.8 .8					
380 360 340 320 300	.I .I .I	.I .I .2 .2	·3 ·3 ·3 ·3	·4 ·4 ·4	.5 .6								
280 260 240 220 200	. I . I . I	.2 .2 .2 .2 .3	·4 ·4 ·4										
180 160 140 120 100	.I .2 .2 .2 .2	·3 ·3 ·4 ·4 ·5											
80 60 40 20 10	.3 .4 .6 I.3 2.6												

DETERMINATION OF HEICHTS BY THE BAROMETER. TABLE 61. DYNAMIC MEASURES.

Correction for Humidity: Values of $\frac{1}{2} \left(\frac{0.378_b^c}{0.00367} \right)$

Top argument: Values of e. Side argument: Values of b. Auxiliary to Table 58.

Air Pres-						VAPO	R PRI	ESSURI	E mb.					
sure.	0.5	1	2	3	4	5	6	7	8	9	10	20	30	40
mb. 1080 1060 1040 1020 1000	°C. 0.0 .0 .0	°C. 0.0 .0 .0	°C. O.I .I .I .I	°C. O.I .I .I .2 .2	°C. 0.2 .2 .2 .2	°C. 0.2 .2 .2 .3 .3	°c. •3 •3 •3 •3	°c. °c. °3 ·3 ·4 ·4	°C. 0.4 .1 .1	°C. 0.4 ·4 ·5 ·5	°c. 0.5 .5 .5 .5	°C. I.O I.O I.O	°c. 1.4 1.5 1.5 1.5	°C. I.0 I.0 2.0 2.0 2.1
980 960 940 920 900	.0	.I .I .I .I	. I . I . I . I	.2 .2 .2 .2 .2	.2 .2 .2 .2 .2 .2	·3 ·3 ·3 ·3 ·3	·3 ·3 ·3 ·3 ·3	·4 ·4 ·4 ·4 ·4	·4 ·4 ·4 ·4	•5 •5 •5 •5	·5 ·5 ·5 .6 .6	1.1 1.1 1.1 1.1	1.6 1.6 1.7	2.I 2.I 2.2 2.2 2.2
880 860 840 820 800	.0	I. I. I. I.	. I . I . I . I	.2 .2 .2 .2 .2	.2 .2 .2 .3 .3	·3 ·3 ·3 ·3	.4 .4 .4 .4	·4 ·4 ·4 ·4 ·5	•5 •5 •5 •5	·5 ·5 .6 .6	.6 .6 .6	I.2 I.2 I.2 I.3 I.3	1.8 1.8 1.8 1.9	2.3
780 760 740 720 700	.0	. I . I . I . I	. I . I . I . I	.2 .2 .2 .2 .2	·3 ·3 ·3 ·3	·3 ·3 ·3 ·4 ·4	·4 ·4 ·4 ·4	·5 ·5 ·5 ·5	·5 ·5 .6 .6	.6 .6 .6 .6	.7 .7 .7 .7	I.3 I.4 I.4 I.4 I.5	2.0	
680 660 640 620 600	.0	.I .I .I .I	.2 .2 .2 .2 .2	.2 .2 .2 .2 .3	·3 ·3 ·3 ·3	·4 ·4 ·4 ·4	•5 •5 •5	·5 ·5 .6 .6	.6 .6 .6 .7	·7 ·7 ·7 ·7	.8 .8 .8			
580 560 540 520 500	.0 .0 .0	.I .I .I .I	.2 .2 .2 .2 .2 .2	·3 ·3 ·3 ·3	·4 ·4 ·4 ·4	·4 ·5 ·5 ·5	·5 .6 .6 .6	.6 .6 .7 .7	.7 .7 .8 .8	.8				
480 460	.I .I	. I	.2	•3	·4 ·4	.5	.6	.8			Air Pres-	VAPOI	R PRES	SURE
440 420 400	.I .I	.I .I .I	.2 .2	·4 ·1 ·4	·5	.6	·7 ·7 .8			-	sure.	0.5	1	2
380 360 340 320 300	.I .I .I .I	.I .I .2 .2 .2	·3 ·3 ·3 ·3 ·3	·4 ·4 ·5 ·5 ·5	·5 .6 .6 .6	·7 ·7 .8					mb, 180 160 140 120 100	°CI .2 .2 .2 .3	°c. •3 •3 •4 •4 •5	°c. .6
280 260 240 220 200	.I .I .I .I	.2 .2 .2 .2 .2	·4 ·4 ·4 ·5 ·5	.6 .6 .6	.7						80 60 40 20 10	·3 ·4 .6 I.3 2.6		

METRIC MEASURES.

Correction for Gravity and Weight of Mercury: $z(0.002640 \cos 2\phi - 0.000007 \cos^2 2\phi + 0.00244)$.

Approximate							I	ATIT	JDE ((ϕ)						
difference of Height. Z.	0°	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°	75
Meters. 100 200 300 400	m. I I 2	m, I I 2	m. O I I 2	m. 0 1 1 2	m. 0 I I 2	m. O I I 2	m. O I I 2	m. O I I	m. 0 I I	m. 0 0 I	m. O O I I	m. 0 0	m. 0 0	m. 0 0	m. 0 0	m. 0 0
500 600 700 800 900	3 3 4 4 5	3 3 4 4 5	2 3 3 4 4	2 3 3 4 4	2 3 3 4 4	2 2 ·3 3 4	2 2 3 3 3	2 2 2 3 3	1 2 2 2 3	I 1 2 2 2	I I I 2	I I I I	I	0 0 I I	0 0 0 0	0 0 0
1000 1100 1200 1300 1400	5 6 6 7 7	5 6 6 7 7	5 6 6 7	5 6 6 7	4 5 5 6 6	4 5 5 6	4 4 5 5 5	3 4 4 4 5	3 3 4 4	2 3 3 3 3	2 2 2 3 3	2 2 2 2 2 2	I I I I 2	I I I I	0 0 I I	0 0 0
1500 1600 1700 1800 1900	8 8 9 9	8 8 9 9	7 8 8 9	7 8 8 8	7 7 8 8 8	6 7 7 7 8	6 6 7 7	5 5 6 6 6	4 5 5 5 5	4 4 4 4 5	3 3 4 4	2 2 3 3 3	2 2 2 2 2	I I I I	I I I I	0 0 0 0
2000 2100 2200 2300 2400	10 11 11 12 12	10 11 11 12 12	IO IO II II II	10 10 11	9 9 10 10	8 9 9 9	8 8 8 9	7 7 7 8 8	6 6 6 7 7	5 5 6 6	4 4 4 5 5	3 3 4 4	2 2 2 3 3	I 2 2 2 2 2	I I I I	0 0 0 0
2500 2600 2700 2800 2900	13 13 14 14 15	13 13 14 14 15	12 13 13 14 14	12 12 13 13	11 12 12 12 13	10 11 11 12 12	9 10 11	8 9 9 9	7 8 8 8 8	6 6 7 7 7	5 5 6 6	4 4 4 4 4	3 3 3 3 3	2 2 2 2 2 2 2	I I I I	0 0 0
3000 3100 3200 3300 3400	15 16 16 17	15 16 16 17 17	15 16 16 16	14 15 15 16 16	13 14 14 15 15	12 13 13 14 14	11 12 12 12 13	11 11 10	9 9 9 10	7 8 8 8	6 6 6 7 7	5 5 5 5	3 3 4 4 4	2 2 2 2	I I I I	0 0 0
3500 3600 3700 3800 3900	18 18 19 19	18 18 19 19	17 18 18 19	17 17 17 18 18	16 16 16 17	14 15 15 16 16	13 14 14 14 15	12 12 12 13	11 11 01	9 9 9 9	7 7 7 8 8	5 5 6 6 6	4 4 4 4	3 3 3 3	I I 2 2 2	I I I
4000 4500 5000 5500 6000	20 23 25 28 30	20 23 25 28 30	20 22 25 27 29	19 21 24 26 28	18 20 22 24 27	17 19 21 23 25	15 17 19 21 23	13 15 17 18 20	12 13 14 16	10 11 12 13 15	8 9 10 11 12	6 7 8 8	4 5 6 6 7	3 3 4 4 4	2 2 2 2 2	I I I
6500 7000	33	33 35	32 34	31	29 31	27 29	24 26	22	10	16 17	13	10	7 8	5	3 3	1

METRIC MEASURES.

Correction for the variation of gravity with altitude: $\frac{z (z + 2 h_o)}{R}$

Approxi- mate difference				Н	EIGH	T OF L	OWER	STATI	ON IN	METE	RS (ho).		
of height.	0	200	400	600	800	1000	1200	1400	1600	1800	2000	2500	3000	4000
meters	m.	m.	m.	m.	m.	m.	111.	m.	m.	m.	m.	m.	m.	m,
200	0	0	0	0	0	0	0	0	0	0	0	0	0	0
300 400	0	0	0	0	0	0	0	0	0	0	0	0	0	0
										0	1	0		I
500 600	0	0	0	0	0	0	0	0	0	0	0	0	I	I
700	0	0	0	0	0	0	0	0	0	0	0	I	I	I
800	0	0	0	0	0	0	0	0	I	I	Î	Î	I	I
900	0	0	0	0	0	0	0	I	I	1	I	I	I	I
1000	0	0	0	0	0	0	I	I	1	I	I	I	I	ı
1100	0	0	0	0	0	I	I	1	1	I	I	I	I	2
1200 1300	0	0	0	0	I	I	I	I	I	I	I	I	I	2
1400	0	0	0	I	I	I	I	I	I	I	I	I	I 2	2 2
1500	О	0	I	I	I	I	I	I	1	I	I	2	2	2
1600 1700	0	I	I	I	I	I	I	I	I	I	I	2	2	2
1800	O	I	I	I	I	I I	I I	I	I	I 2	2 2	2 2	2 2	3
1900	I	I	I	I	I	Ī	I	Ī	2	2	2	2	2	3 3 3
2000	I	I	I	I	I	* I	I	2	2	2	2	2	3	3
2100 2200	I	I	I	I	I	I I	I 2	2 2	2 2	2 2	2 2	2 2	3	3 3 4 4
2300	I	I	I	I	I	2	2	2	2	2	2	3	3	4 4
2400	1	I	I	I	2	2	2	2	2	2	2	3	3	4
2500	ī	I	I	I	2	2	2	2	2	2	3	3	3	4
2600 2700	I	I	I	2 2	2 2	2 2	2 2	2 2	3	3	3 3 3	3	4	4 5 5 5
2800	I	I	2	2	2	2	2	2	3	3 3	3	3	4 4	5
2900	I	2	2	2	2	2	2	3	3	3	3	4	4	5
3000	I	2	2	2	2	2	3	3	3	3	3	4	4	5
3100 3200	2 2	2	2 2	2 2	2 2	2	3	3 3	3	3 3 3	3	4	4	5
3300	2	2	2	2	3	3	3	3	3 3 3	4	4	4 4	5 5	5 5 6 6
3400	2	2	2	2	3	3	3	3	4	4	4	4	5	6
3500	2	2	2	3	3	3	3	3	4	4	4	5	5	6
3600 3700	2	2 2	3	3	3	3	3 4	4 4	4 4	4	4	5 5 5	5 6	7 7 7
3800	2	3	3	3	3	3	4	4	4	4	5	5	6	7
3900	2	3	3	3	3	4	4	4	4	5	5	5	6	7
4000	3	3	3	3	4	4	4	4	5	5	5 6	6	6	8
4500 5000	3 4	3 4	5	4	4	5 5 6	5 6	5 6	5 6			7 8	7 9	9
5500	5 6			5	5		7	7 S	8	7 8	7 8	9	10	12
6000	6	5 6	5 6	7	7	8	7 8	8	9	9 .	9	IÓ	11	13
6500	7 8	7 8	7	8	8	9	9	9	10	10	11	12	13	15
7000	8	8	9	9	9	10	10	II	II	12	12	13	14	16
		1												

TABLE 64.

HEIGHTS REDUCED FROM METERS TO DYNAMIC METERS, THE ACCELERATION OF GRAVITY AT SEA LEVEL BEING 9.80.

Height (meters)	0	100	200	300	400	500	600	700	800	900
29000	28290	28387	28484	28582	28679	28776	28873	28970	29067	29164
28000	27319	27416	27513	27610	27708	27805	27902	27999	28096	28193
27000	26347	26445	26542	26639	26736	26833	26930	27028	27125	27222
26000	25376	25473	25570	25667	25764	25862	25959	26056	26153	26250
25000	24404	24501	24598	24695	24792	24890	24987	25084	25181	25279
2,000	24404	24301	24390	24093	-4/9-	24090	24301	23004	23101	23219
24000	23431	23528	23626	23723	23820	23917	24015	24112	24209	24306
23000	22458	22556	22653	22750	22847	22945	23042	23139	23237	23334
22000	21485	21583	21680	21777	21875	21972	22069	22166	22264	22361
21000	20512	20609	20707	20804	20901	20999	21096	21193	21291	21388
20000	19538	19636	19733	19830	19928	20025	20122	20220	20317	20415
19000	18564	18662	18759	18856	18954	TOOFT	19149	19246	10244	10117
18000	17590	17687		17882	17980	19051	18175	18272	19344	19441
17000	16615	16713	17785	16908	17905		17200			18467
16000						17103 16128		17298	17395	17493
	15640	15738	15835	15933	16030		16225	16323	16420	16518
15000	14665	14763	14000	14958	15055	15153	15250	15348	15446	15543
14000	13690	13787	13885	13982	14080	14178	14275	14373	14470	14568
13000	12714	12811	12909	13007	13104	13202	13299	13397	13495	13592
12000	11738	11835	11933	12031	12128	12226	12323	12421	12519	12616
11000	10761	10859	10957	11054	11152	11250	11347	11445	11543	11640
10000	9785	9882	9980	10078	10175	10273	10371	10468	10566	10664
9000	8807	8905	9003	1010	9198	9296	9394	9492	9589	9687
8000	7830	7928	8026	8123	8221	8319	8417	8514	8612	8710
7000	6852	6950	7048	7146	7244	7341	7439	7537	7635	7732
6000	5874	5972	6070	8616	6266	6363	6461	6559	6657	6755
5000	4896	4994	5092	5190	5287	5385	5483	5581	5679	5777
1000	3918	4015	4113	4211	4309	4407	4505	4603	4700	4798
4000 3000	2939	3037	3134	3232	3330	3428	4505 3526	3624	3722	3820
2000	1959	2057	2155	2253	2351	2449	2547	2645	2743	2841
1000	980	1078	1176	1274	1372	1470	1568	1666	1763	1861
0	900	98	196	294	392	490	588	686	784	882
	0	100	200	300	400	500	600	700	800	900
			Р	ROPORT	IONALIT	y Tabli	ε.			
Meters	0	1	2	3	4	5	6	7	8	9
90	88	89	90	91	92	93	94	95	96	97
8o	78	79	80	81	82	93 83	94 84	85	86	87
70	69	70	71	72	73	74	74	75	76	77
60	59	60	61	62	63	64	65	66	67	68
50	49	50	51	52	53	54	55	56	57	58
40	39 -	40	41	42	43	44	45	46	47	48
30	29	30	31	32	33	34	35	36	37	38
20	20	21	22	23	24	24	25	26	27	28
10	01	11	12	13	14	15	16	17	18	19
0	0	I	2	3	4	5	6	7	8	9
	0	1	2	3	4	5	6	7	8	9

CORRECTIONS TO TABLE 64 FOR VALUES OF THE ACCELERATION OF GRAVITY AT SEA LEVEL DIFFERENT FROM 9.80.

Height		1	Acceler	ATION O	F GRAVIT	Y AT SE	A LEVEL	•	
(meters)	9.76	9.77	9.78	9.79	9.80	9.81	9.82	9.83	9.84
29000 28000 27000 26000 25000	-116 -112 -108 -104 -100	-87 -84 -81 -78 -75	58 56 54 52 50	-29 -28 -27 -26 -25	0 0 0 0	29 28 27 26 25	58 56 54 52 50	87 84 81 78 75	116 112 108 104 100
24000 23000 22000 21000 20000	- 96 - 92 - 88 - 84 - 80	-72 -69 -66 -63 -60	-48 -46 -44 -42 -40	-24 -23 -22 -21 -20	0 0 0 0	24 23 22 21 20	48 46 44 42 40	72 69 66 63 60	96 92 88 84 80
19000 18000 17000 16000 15000	- 76 - 72 - 68 - 64 - 60	-57 -54 -51 -48 -45	$ \begin{array}{r} -38 \\ -36 \\ -34 \\ -32 \\ -30 \end{array} $	-19 -18 -17 -16 -15	0 0 0 0	19 18 17 16	38 36 34 32 30	57 54 51 48 45	76 72 68 64 60
14000 13000 12000 11000 10000	- 56 - 52 - 48 - 44 - 40	-42 -39 -36 -33 -30	-28 -26 -24 -22 -20	-14 -13 -12 -11 -10	0 0 0 0	14 13 12 11 10	28 26 24 22 20	42 39 36 33 30	56 52 48 44 40
9000 8000 7000 6000 5000	- 36 - 32 - 28 - 24 - 20	-27 -24 -21 -18 -15	-18 -16 -14 -12 -10	- 9 - 8 - 7 - 6 - 5	0 0 0 0	9 8 7 6 5	18 16 14 12	27 24 21 18 15	36 32 28 24 20
4000 3000 2000 1000	- 16 - 12 - 8 - 4	-12 - 9 - 6 - 3 0	- 8 - 6 - 4 - 2 0	- 4 - 3 - 2 - 1 0	0 0 0 0	4 3 2 1 0	8 6 4 2 0	12 9 6 3 0	16 12 8 4 0
	9.76	9.77	9.78	9.79	9.80	9.81	9.82	9.83	9.84

TABLE 66.

NORMAL VALUE OF THE ACCELERATION OF GRAVITY AT SEA LEVEL, $\mathbf{G}_{\phi},~\mathbf{M}/\text{SEC}.^2$

Latitude (degrees)	O°	1°	2°	3°	4°	5°	6°	7°	8°	9°
70° 60° 50° 40° 30° 20°	9.8306 9.8261 9.8192 9.8107 9.8017 9.7933 9.7864 9.7819 9.7804	9.8266 9.8200 9.8116 9.8026 9.7941 9.7870	9.8272 9.8207 9.8125 9.8035 9.7949 9.7876	9.8277 9.8214 9.8134 9.8044 9.7957 9.7883	9.8282 9.8222 9.8142 9.8053 9.7965 9.7889 9.7834	9.8287 9.8229 9.8151 9.8062 9.7974 9.7896 9.7838	9.8291 9.8236 9.8159 9.8071 9.7982 9.7903 9.7843	9.8295 9.8242 9.8168 9.8080 9.7991 9.7910 9.7848	9.8299 9.8249 9.8176 9.8089 9.8000 9.7918 9.7853	9.8303 9.8255 9.8184 9.8098 9.8008 9.7925 9.7858

 g_{ϕ} at $90^{\circ} = 9.8322$

HEIGHTS REDUCED FROM DYNAMIC METERS TO GEOMETRIC METERS, THE ACCELERATION OF GRAVITY AT SEA LEVEL BEING 9.80.

Height (dynamic meters)	0	100	200	300	400	500	600	700	800	900
29000	29729	29832	29935	30038	30141	30244	30347	30451	30554	30657
28000	28700	28803	28906	29009	29112	29215	29318	29420	29523	29626
27000	27670	27773	27876	27979	28082	28185	28288	28391	28494	28597
26000	26641	26744	26847	26950	27053	27156	27259	27362	27464	27567
25000	25612	25715	25818	25921	26024	26127	26230	26333	26435	26538
24000	24584	24687	24790	24893	24995	25098	25201	25304	25407	25510
23000	23556	23659	23762	23864	23967	24070	24173	24276	24378	24481
22000	22528	22631	22734	22836	22939	23042	23145	23248	23350	23453
21000	21501	21603	21706	21809	21912	22014	22117	22220	22323	22425
20000	20474	20576	20679	20782	20884	20987	21090	21193	21295	21398
19000	19447	19549	19652	19755	19858	19960	20063	20166	20268	20371
18000	18420	18523	18626	18728	18831	18934	19036	19139	19242	19344
17000	17394	17497	17599	17702	17805	17907	18010	18112	18215	18318
16000	16368	16471	16574	16676	16779	16881	16984	17086	17189	17292
15000	15343	15445	15548	15651	15753	15856	15958	16061	16163	16266
14000	14318	14420	14523	14625	14728	14830	14933	15035	15138	15240
13000	13293	13395	13498	13600	13703	13805	13908	14010	14113	14215
12000	12268	12371	12473	12576	12678	12781	12883	12986	13088	13190
11000	11244	11347	11449	11552	11654	11756	11859	11961	12064	12166
10000	10220	10323	10425	10528	10630	10732	10835	10937	11040	11142
9000	9197	9299	9402	9504	9606	9709	9811	9913	10016	10118
8000	8174	8276	8378	8481	8583	8685	8788	8890	8992	9095
7000	7151	7253	7355	7458	7560	7662	7765	7867	7969	8071
6000	6128	6231	6333	6435	6537	6640	6742	6844	6946	7049
5000	5106	5208	5311	5413	5515	5617	5719	5822	5924	6026
4000	4084	4186	4289	4391	4493	4595	4697	4800	4902	5004
3000	3063	3165	3267	3369	3471	3573	3676	3778	3880	3982
2000	2042	2144	2246	2348	2450	2552	2654	2756	2858	2961
1000	1021	1123	1225 204	1327 306	1429 408	1531	1633 612	1735 714	1837 816	919
	0	100	200	300	400	500	600	700	800	900
Proportionality Table.										
Meters	0	1	2	3	4	5	6	7	8	9
90	92	93	94	95	96	97	98	99	100	101
80	82	83	84	85	86	87	88	89	90	91
70	71	72	73	74	76	77	78	79	80	81
60	16	62	63	64	65	66	67	68	69	70
50	51	52	53	54	55	56	57	58	59	60

SMITHSONIAN TABLES

CORRECTIONS TO TABLE 67 FOR VALUES OF THE ACCELERATION OF GRAVITY AT SEA LEVEL DIFFERENT FROM 9.80.

Height (dynamic			Acceler	ATION O	F GRAVIT	TY AT SE	A LEVEL		
meters)	9.76	9.77	9.78	9.79	9.80	9.81	9.82	9.83	9.84
29000 28000 27000 26000 25000	121 117 113 108 104	91 88 84 81 78	60 58 56 54 52	- 30 29 28 27 26	0 0 0 0	-30 -29 -28 -27 -26	60 58 56 54 52	91 88 84 81 78	-121 -117 -113 -108 -104
24000 23000 22000 21000 20000	100 96 92 87 83	75 72 69 66 62	50 48 46 44 42	25 24 23 22 21	0 0 0 0	-25 -24 -23 -22 -21	-50 -48 -46 -44 -42	-75 -72 -69 -66 -62	-100 - 96 - 92 - 87 - 83
19000 18000 17000 16000 15000	79 75 71 67 62	59 56 53 50 47	40 37 35 33 31	20 19 18 17 16	0 0 0 0	-20 -19 -18 -17 -16	-40 -37 -35 -33 -31	-59 -56 -53 -50 -47	— 79 — 75 — 71 — 67 — 62
14000 13000 12000 11000 10000	58 54 50 46 42	44 41 37 34 31	29 27 25 23 21	15 14 13 11	0 0 0 0	-15 -14 -13 -11 -10	-29 -27 -25 -23 -21	-44 -41 -37 -34 -31	- 58 - 54 - 50 - 46 - 42
9000 8000 7000 6000 5000	37 33 29 25 21	28 25 22 19 16	19 17 15 12 10	9 8 7 6 5	0 0 0 0	- 9 - 8 - 7 - 6 - 5	-19 -17 -15 -12 -10	-28 -25 -22 -19 -16	- 37 - 33 - 29 - 25 - 21
4000 3000 2000 1000	17 13 8 4	9 6 3 0	8 6 4 2 0	4 3 2 I 0	0 0 0 0	- 4 - 3 - 2 - 1	- 8 - 6 - 4 - 2 0	-12 - 9 - 6 - 3 0	- 17 - 13 - 8 - 4 0
	9.76	9.77	9.78	9.79	9.80	9.81	9.82	9.83	9.84

Examples to tables 67 and 68.

	1			
1	2	3	4	5
1614	1633	14	+ 2	1649
2804	2858	4	+ 3	2865
4704	4800	4	+ 6	4810
12140	12371	41	+16	12428

Column

- Heights above sea level given in dynamic meters.
- 2. Values of table 67 for the dynamic heights, 1600, 2800, 4700, 12100.
- Values of proportionality table for dynamic heights 14, 4, 4, 40.
- 4. Corrections from table 68 for g = 9.7873 at sea level and for the heights of column 1.
- Sum of numbers in columns 2, 3 and 4, giving the geometrical heights corresponding to the dynamic heights of column 1.

Examples to tables 64 and 65.

í					
١	1	2	3	4	5
	1649	1568	48	- 2	1614
	2865	2743	64	— 3	2804
ı	4810	4700	10	— 6	4704
ı	12428	12128	27	-15	12140

Column

- 1. Heights above sea level given in meters.
- Values of table 64 for the heights 1600, 2800, 4800, 12400.
- Values of proportionality table for the heights 49, 65, 10, 28.
- 4. Corrections from table 65 for g = 9.7873 at sea level and for the heights of column 1.
- Sum of numbers in columns 2, 3 and 4, giving the dynamic heights corresponding to the geometrical heights of column 1.

DIFFERENCE OF HEIGHT CORRESPONDING TO A CHANGE OF 0.1 INCH IN THE BAROMETER.

ENGLISH MEASURES.

Baro- metric		MEAN	N TEMI	PERATU	JRE OF	THE	AIR IN	FAHR	ENHEI'	r degr	REES.		
Pres-	30°	35°	40°	45°	50°	55°	60°	65°	70°	75°	80°	85°	
Inches	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	Feet.	
22.0	119.2	120.5	121.8	123. I 122.0	124.4	125.8	127.1 126.0	128.5	129.8	131.2	132.5	133.9	
.2	117.1	119.4	119.6	120.9	123.3	124.7 123.6	124.9	127.3 126.2	127.5	130.0	131.3	132.7 131.5	
.6	116.1	117.3	118.6	119.8	121.1	122.5	123.8	125.1	125.3	127.7	129.0	130.3	
23.0	114.0	115.3	116.5	117.8 116.8	119.0	120.3	121.6	122.9	124.2	1 25 .5	126.8	128.1	
.4	112.1	113.3	114.5	115.8	117.0	118.3	119.5	120.8	122.1	123.3	124.6	125.9	
.6	111.1	111.4	113.5	114.8	116.0	117.3	118.5	119.8	121.0	122.3	123.5	124.8	
24.0	109.3	110.5	111.7	112.9	114.1	115.3	116.5	117.8	119.0	120.2	121.5	122.7	
.2	107.5	109.5	109.8	111.9	113.1	114.4	114.6	115.9	117.1	118.3	119.5	121.7	
.6	106.6	107.8	108.9	110.1	111.3	112.5	113.7	114.9	116.1	117.3	118.5	119.7	
25.0	104.9 104.1	106.0	107.2	108.3	109.5	110.7	111.9	113.1	114.2	115.4	116.6 115.7	117.8	
-4	103.3	104.4	105.5	107.5	107.8	109.0	IIO.I	111.3	112.4	113.6	114.8	116.0	
.6	102.5	103.6	104.7	105.8	107.0	108.1	109.3	10.4	111.6	112.7	113.9	115.1	
26.0	100.9	IO2.0 IOI.2	103.1 102.3	104.2	105.3	106.4	107.6	108.7	109.9	111.0 110.1	112.1 111.3	113.3	
.2	99.4	100.4	101.5	103.4	103.7	104.8	106.0	107.1	108.2	109.3	110.4	111.6	
.6	98.6 97.9	99.7 98.9	100.7	101.8	102.9	104.0	105.2	105.5	107.4	108.5	109.6	110.7	
27.0	97.1 96.4	98.2 97.5	99.2 98.5	100.3	101.4	102.5	103.6	104.7	105.8	106.9	108.0	109.1	
-4	95.7	96.8	97.8	98.9	99.9	101.0	102.1	103.2	104.2	105.3	106.4	107.5	
.6	95.0 94.3	96.1 95.4	97.1 96.4	98.1 97.4	99.2 98.5	100.3	101.3	102.4	103.5	104.6	105.6	105.9	
28.0	93.7	94.7	95.7 95.0	96.7 96.1	97.8 97.1	98.8 98.1	9 9.9	101.0	102.0	103.1 102.3	104.1	105.2	
-4	93.0	94.0	94.4	95.4	96.4	97.5	98.5	99.5	100.6	101.6	102.7	103.7	
.6	91.7 91.1	92.7 92.1	93.7 93.1	94.7 94.1	95·7 95. I	96.8 96.1	97.8 97.1	98.8 98.2	99.9	100.9	101.9 101.2	103.0	
29.0	90.4 89.8	91.4	92.4	93.4 92.8	94.4	95·4 94.8	96.5 95.8	97·5 96.8	98.5 97.8	99.5 98.8	100.5	101.6	
•4	89.2 88,6	90.2	91.1	92.1	93. I	94.1	95.1	96.1	97.1 96.5	98.2	99.2	100.2	
.6	88.0	89.0	90.5	91.5	92.5 91.9	93.5 92.9	94.5	95·5 94·9	95.8	97·5 96.8	97.8	98.8	
30.0	87.4 86.8	88.4 87.8	89.3 88.7	90.3	91.3	92.3 91.7	93.2 92.6	94. 2 93.6	95.2 94.6	96.2 95.6	97.2 96.5	98.2 97.5	
.4	86.3 85.7	87.2 86.7	88.2 87.6	89.1 88.5	90.1 89.5	91.1	92.0	93.0	94.0	94.9	95·9 95·3	96.9	
.8	85.2	86.1	87.0	88.0	88.9	89.9	90.8	91.8	93.3	93.7	94.7	95.6	
	I	1	1	<u> </u>			1	1		1			

DIFFERENCE OF HEIGHT CORRESPONDING TO A CHANGE OF 1 MILLIMETER IN THE BAROMETER.

METRIC MEASURES.

		MEAN TEMPERATURE OF THE AIR IN CENTIGRADE DEGREES.											
Barometric Pressure.	-2°	0°	2°	4°	6°	8°	10°	12°	14°	16°			
mm.	Meters.	Meters.	Meters.	Meters.	Meters.	Meters.	Meters.	Meters.	Meters.	Meters.			
760	10.48	10.57	10.65	10.73	10.81	10.89	10.9S	11.06	11.15	11.23			
750	10.62	10.71	10.79	10.87	10.95	11.04	11.13	11.21	11.30	11.38			
740	10.77	10.85	10.93	11.02	11.10	11.19	11.28	11.36	11.45	11.54			
730 720	10.91	II.00 II.15	11.08	11.17	11.26	11.35	11.43	11.52	11.61	11.70			
710	11.22	11.31	11.40	11.48	11.58	11.67	11.75	11.85	11.77	12.03			
700	11.38	11.47	11.56	11.65	11.74	11.83	11.92	12.02	12.11	12.20			
690	11.55	11.63	11.72	11.82	11.91	12.00	12.09	12.19	12.28	12.38			
680 670	11.72	11.80	11.89	11.99	12.08	12.18	12.27	12.37	12.46	12.56			
660	11.89	11.98	12.07	12.17	12.26	12.36	12.46 12.65	12.55	12.65	12.75			
650	12.26	12.35	12.45	12.54	12.64	12.74	12.84	12.94	13.04	13.14			
640	12.45	12.55	12.64	12.74	12.84	12.94	13.04	13.14	13.24	13.35			
630	12.65	12.75	12.84	12.94	13.04	13.15	13.25	13.35	13.45	13.56			
620 610	12.85 13.06	12.96	13.05 13.27	13.15	13.25	13.36	13.46	13.57	13.67	13.78			
600	13.28	13.39	13.49	13.59	13.70	13.80	13.91	14.02	14.13	14.24			
590	13.51	13.62	13.72	13.82	13.93	14.03	14.15	14.26	14.13	14.48			
580	13.74	13.85	13.96	14.06	14.17	14.28	14.39	14.51	14.62	14.73			
570	13.98	14.09	14.20	14.31	14.42	14.53	14.64	14.76	14.88	14.99			
560	14.23	14.34	14.45	14.57	14.68	14.79	14.90	15.02	15.14	15.25			
Barometric		MEAN T	EMPERA	TURE O	F THE	AIR IN			1				
Barometric Pressure.	18°	MEAN T	EMPERA	TURE O	F THE 26°	AIR IN			1				
Pressure.	18° Meters.			24° Meters.	26° Meters.	28°	CENTIG 30° Meters.	RADE D	EGREES 34° Meters.	36° Meters.			
Pressure.	18°	20°	22°	24°	26°	28°	CENTIG	RADE D	EGREES 34°	36°			
mm. 760	18° Meters. 11.32 11.47	20° Meters. 11.41 11.56	22° Meters. 11.49 11.64	24° Meters. 11.58 11.73	26° Meters. 11.66 11.82	28° Meters. 11.75 11.91	30° Meters. 11.84 12.00	32° Meters. 11.92 12.08	34° Meters. 12.01 12.17	36° Meters. 12.10 12.26			
mm. 760 750 740	18° Meters. 11.32 11.47 11.63	20° Meters. 11.41 11.56 11.72	22° Meters. 11.49 11.64 11.80	24° Meters. 11.58 11.73 11.89	26° Meters. 11.66 11.82 11.98	28° Meters. 11.75 11.91 12.07	30° Meters. 11.84 12.00 12.16	32° Meters. 11.92 12.08 12.24	34° Meters. 12.01 12.17 12.33	36° Meters. 12.10 12.26 12.42			
mm. 760 750 740 730	Meters. 11.32 11.47 11.63 11.79	20° Meters. 11.41 11.56 11.72 11.88	22° Meters. 11.49 11.64 11.80 11.96	24° Meters. 11.58 11.73 11.89 12.05	26° Meters. 11.66 11.82 11.98 12.15	28° Meters. 11.75 11.91 12.07 12.23	30° Meters. 11.84 12.00 12.16 12.32	32° Meters. 11.92 12.08 12.24 12.41	34° Meters. 12.01 12.17	36° Meters. 12.10 12.26 12.42 12.59			
mm. 760 750 740	18° Meters. 11.32 11.47 11.63	20° Meters. 11.41 11.56 11.72	22° Meters. 11.49 11.64 11.80	24° Meters. 11.58 11.73 11.89	26° Meters. 11.66 11.82 11.98	28° Meters. 11.75 11.91 12.07	30° Meters. 11.84 12.00 12.16	32° Meters. 11.92 12.08 12.24	34° Meters. 12.01 12.17 12.33 12.50	36° Meters. 12.10 12.26 12.42			
mm. 760 750 740 730 720 710 700	Meters. 11.32 11.47 11.63 11.79 11.95	20° Meters. 11.41 11.56 11.72 11.88 12.04 12.21	22° Meters. 11.49 11.64 11.80 11.96 12.13 12.30 12.48	24° Meters. 11.58 11.73 11.89 12.05 12.22 12.39 12.57	26° Meters. 11.66 11.82 11.98 12.15 12.32 12.49 12.67	28° Meters. 11.75 11.91 12.07 12.23 12.40 12.58 12.76	30° Meters. 11.84 12.00 12.16 12.32 12.49 12.67	32° Meters. 11.92 12.08 12.24 12.41 12.58 12.76	34° Meters. 12.01 12.17 12.33 12.50 12.68 12.86	36° Meters. 12.10 12.26 12.42 12.59 12.77 12.95 13.13			
mm. 760 750 740 730 720 710 700 690	Meters. 11.32 11.47 11.63 11.79 11.95 12.12 12.29 12.47	20° Meters. 11.41 11.56 11.72 11.88 12.04 12.21 12.39 12.57	22° Meters. 11.49 11.64 11.80 11.96 12.13 12.30 12.48 12.66	24° Meters. 11.58 11.73 11.89 12.05 12.22 12.39 12.57 12.75	26° Meters. 11.66 11.82 11.98 12.15 12.32 12.49 12.67 12.85	Meters. 11.75 11.91 12.07 12.23 12.40 12.58 12.76 12.94	30° Meters. 11.84 12.00 12.16 12.32 12.49 12.67 12.85 13.04	32° Meters. 11.92 12.08 12.24 12.41 12.58 12.76 12.94 13.13	34° Meters. 12.01 12.17 12.33 12.50 12.68 12.86 13.04 13.23	36° Meters. 12.10 12.26 12.42 12.59 12.77 12.95 13.13 13.32			
mm. 760 750 740 730 720 710 700 690 680	Meters. 11.32 11.47 11.63 11.79 11.95 12.12 12.29 12.47 12.66	20° Meters. 11.41 11.56 11.72 11.88 12.04 12.21 12.39 12.57 12.75	22° Meters. 11.49 11.64 11.80 11.96 12.13 12.30 12.48 12.66 12.85	24° Meters. 11.58 11.73 11.89 12.05 12.22 12.39 12.57 12.75 12.94	26° Meters. 11.66 11.82 11.98 12.15 12.32 12.49 12.67 12.85 13.04	28° Meters. 11.75 11.91 12.07 12.23 12.40 12.58 12.76 12.94 13.13	30° Meters. 11.84 12.00 12.16 12.32 12.49 12.67 12.85 13.04 13.23	32° Meters. 11.92 12.08 12.24 12.41 12.58 12.76 12.94 13.13 13.32	34° Meters. 12.01 12.17 12.33 12.50 12.68 12.86 13.04 13.23 13.42	36° Meters. 12.10 12.26 12.42 12.59 12.77 12.95 13.13 13.32 13.52			
mm. 760 750 740 730 720 710 700 690	Meters. 11.32 11.47 11.63 11.79 11.95 12.12 12.29 12.47	20° Meters. 11.41 11.56 11.72 11.88 12.04 12.21 12.39 12.57	22° Meters. 11.49 11.64 11.80 11.96 12.13 12.30 12.48 12.66	24° Meters. 11.58 11.73 11.89 12.05 12.22 12.39 12.57 12.75	26° Meters. 11.66 11.82 11.98 12.15 12.32 12.49 12.67 12.85	Meters. 11.75 11.91 12.07 12.23 12.40 12.58 12.76 12.94	30° Meters. 11.84 12.00 12.16 12.32 12.49 12.67 12.85 13.04	32° Meters. 11.92 12.08 12.24 12.41 12.58 12.76 12.94 13.13	34° Meters. 12.01 12.17 12.33 12.50 12.68 12.86 13.04 13.23	36° Meters. 12.10 12.26 12.42 12.59 12.77 12.95 13.13 13.32			
mm. 760 750 740 730 710 700 690 680 670	Meters. 11.32 11.47 11.63 11.79 11.95 12.12 12.29 12.47 12.66 12.85	20° Meters. 11.41 11.56 11.72 11.88 12.04 12.21 12.39 12.57 12.75 12.94	22° Meters. 11.49 11.64 11.80 11.96 12.13 12.30 12.48 12.66 12.85 13.04	24° Meters. 11.58 11.73 11.89 12.05 12.22 12.39 12.57 12.75 12.94 13.14	26° Meters. 11.66 11.82 11.98 12.15 12.32 12.49 12.67 12.85 13.04 13.23	28° Meters. 11.75 11.91 12.07 12.23 12.40 12.58 12.76 12.94 13.13 13.33	30° Meters. 11.84 12.00 12.16 12.32 12.49 12.65 13.04 13.23 13.43	Meters. 11.92 12.08 12.24 12.41 12.58 12.76 12.94 13.13 13.32 13.52	34° Meters. 12.01 12.17 12.33 12.50 12.68 12.86 13.04 13.23 13.42 13.62	Meters. 12.10 12.26 12.42 12.59 12.77 12.95 13.13 13.32 13.52 13.72			
mm. 760 750 740 730 710 700 690 680 670 660 650 640	Meters. 11.32 11.47 11.63 11.79 11.95 12.12 12.29 12.47 12.66 12.85 13.04 13.24 13.45	20° Meters. 11.41 11.56 11.72 11.88 12.04 12.21 12.39 12.57 12.75 12.94 13.14 13.34 13.55	22° Meters. 11.49 11.64 11.80 11.96 12.13 12.30 12.48 12.66 12.85 13.04 13.24 13.44 13.65	24° Meters. 11.58 11.73 11.89 12.05 12.22 12.39 12.57 12.75 12.94 13.14 13.34 13.54 13.54	26° Meters. 11.66 11.82 11.98 12.15 12.32 12.49 12.67 12.85 13.04 13.23 13.43	28° Meters. 11.75 11.91 12.07 12.23 12.40 12.58 12.76 12.94 13.13 13.33 13.53	30° Meters. 11.84 12.00 12.16 12.32 12.49 12.67 12.85 13.04 13.23 13.43 13.63	32° Meters. 11.92 12.08 12.24 12.41 12.58 12.76 12.94 13.13 13.32 13.52 13.73	34° Meters. 12.01 12.17 12.33 12.50 12.68 12.86 13.04 13.23 13.42 13.62 13.83	Meters. 12.10 12.26 12.42 12.59 12.77 12.95 13.13 13.32 13.52 13.72 13.93 14.15			
mm. 760 750 740 730 710 700 690 680 670 660 650 640 630	18° Meters. 11.32 11.47 11.63 11.79 11.95 12.12 12.29 12.47 12.66 12.85 13.04 13.45 13.66	20° Meters. 11.41 11.56 11.72 11.88 12.04 12.21 12.39 12.57 12.75 12.94 13.14 13.34 13.55 13.76	22° Meters. 11.49 11.64 11.80 11.96 12.13 12.30 12.48 12.66 12.85 13.04 13.24 13.44 13.65 13.87	24° Meters. 11.58 11.73 11.89 12.05 12.22 12.39 12.57 12.75 12.94 13.14 13.34 13.54 13.75 13.97	26° Meters. 11.66 11.82 11.98 12.15 12.32 12.49 12.67 12.85 13.04 13.23 13.43 13.64 13.85 14.07	28° Meters. 11.75 11.91 12.07 12.23 12.40 12.58 12.76 12.94 13.13 13.53 13.74 13.96 14.18	30° Meters. 11.84 12.00 12.16 12.32 12.49 12.67 12.85 13.04 13.23 13.43 13.63 13.84 14.06 14.28	Meters. 11.92 12.08 12.24 12.41 12.58 12.76 12.94 13.13 13.32 13.52 13.73 13.94 14.15 14.38	34° Meters. 12.01 12.17 12.33 12.50 12.68 12.86 13.04 13.23 13.42 13.62 13.83	36° Meters. 12.10 12.26 12.42 12.59 12.77 12.95 13.13 13.32 13.52 13.72 13.93 14.15 14.37 14.60			
mm. 760 750 740 730 710 700 690 680 670 660 650 640	Meters. 11.32 11.47 11.63 11.79 11.95 12.12 12.29 12.47 12.66 12.85 13.04 13.24 13.45	20° Meters. 11.41 11.56 11.72 11.88 12.04 12.21 12.39 12.57 12.75 12.94 13.14 13.34 13.55	22° Meters. 11.49 11.64 11.80 11.96 12.13 12.30 12.48 12.66 12.85 13.04 13.24 13.44 13.65	24° Meters. 11.58 11.73 11.89 12.05 12.22 12.39 12.57 12.75 12.94 13.14 13.34 13.54 13.54	26° Meters. 11.66 11.82 11.98 12.15 12.32 12.49 12.67 12.85 13.04 13.23 13.43	28° Meters. 11.75 11.91 12.07 12.23 12.40 12.58 12.76 12.94 13.13 13.33 13.53	30° Meters. 11.84 12.00 12.16 12.32 12.49 12.67 12.85 13.04 13.23 13.43 13.63	32° Meters. 11.92 12.08 12.24 12.41 12.58 12.76 12.94 13.13 13.32 13.52 13.73	34° Meters. 12.01 12.17 12.33 12.50 12.68 12.86 13.04 13.23 13.42 13.62 13.83	Meters. 12.10 12.26 12.42 12.59 12.77 12.95 13.13 13.32 13.52 13.72 13.93 14.15			
mm. 760 750 740 730 720 710 700 690 680 670 660 650 640 630 620 610	18° Meters. 11.32 11.47 11.63 11.79 11.95 12.12 12.29 12.47 12.66 12.85 13.04 13.45 13.66 13.88 14.11	20° Meters. 11.41 11.56 11.72 11.88 12.04 12.21 12.39 12.57 12.75 12.94 13.14 13.34 13.55 13.76 13.98 14.21	22° Meters. 11.49 11.64 11.80 11.96 12.13 12.30 12.48 12.66 12.85 13.04 13.24 13.44 13.65 13.87 14.09 14.32	24° Meters. 11.58 11.73 11.89 12.05 12.22 12.39 12.57 12.75 12.94 13.14 13.34 13.54 13.75 13.97 14.20 14.43	26° Meters. 11.66 11.82 11.98 12.15 12.32 12.49 12.67 12.85 13.04 13.23 13.43 13.64 13.85 14.07 14.30 14.54	28° Meters. 11.75 11.91 12.07 12.23 12.40 12.58 12.76 12.94 13.13 13.33 13.53 13.74 13.96 14.18 14.41	30° Meters. 11.84 12.00 12.16 12.32 12.49 12.67 12.85 13.04 13.23 13.43 13.63 13.84 14.06 14.28 14.51 14.75	32° Meters. 11.92 12.08 12.24 12.41 12.58 12.76 12.94 13.13 13.32 13.52 13.73 13.94 14.15 14.38 14.62 14.86	34° Meters. 12.01 12.17 12.33 12.50 12.68 12.86 13.04 13.23 13.42 13.62 13.83 14.04 14.26 14.49 14.72 14.96	Meters. 12.10 12.26 12.42 12.59 12.77 12.95 13.13 13.32 13.52 13.72 13.93 14.15 14.37 14.60 14.83 15.07			
mm. 760 750 740 730 720 710 700 690 680 670 660 650 640 630 620 610 600	18° Meters. 11.32 11.47 11.63 11.795 12.12 12.29 12.47 12.66 12.85 13.04 13.24 13.45 13.66 13.88 14.11 14.35	20° Meters. 11.41 11.56 11.72 11.88 12.04 12.21 12.39 12.57 12.75 12.94 13.14 13.55 13.76 13.98 14.21 14.45	Meters. 11.49 11.64 11.80 12.13 12.30 12.48 12.66 12.85 13.04 13.44 13.65 13.87 14.09	24° Meters. 11.58 11.73 11.89 12.05 12.22 12.39 12.57 12.75 12.94 13.14 13.34 13.54 13.75 13.97 14.20	26° Meters. 11.66 11.82 11.98 12.15 12.32 12.49 12.67 12.85 13.04 13.23 13.43 13.64 13.85 14.07 14.30	28° Meters. 11.75 11.91 12.07 12.23 12.40 12.58 12.76 12.94 13.13 13.53 13.74 13.96 14.18 14.41 14.64	Meters. 11.84 12.00 12.16 12.32 12.49 12.67 12.85 13.04 13.23 13.43 13.63 13.84 14.06 14.28 14.51	Meters. 11.92 12.08 12.24 12.41 12.58 12.76 12.94 13.13 13.32 13.52 13.73 13.94 14.15 14.38 14.62	34° Meters. 12.01 12.17 12.33 12.50 12.68 13.04 13.23 13.42 13.62 13.83 14.04 14.26 14.49 14.72	Meters. 12.10 12.26 12.42 12.59 12.77 12.95 13.13 13.32 13.52 13.72 13.93 14.15 14.37 14.60 14.83 15.07			
mm. 760 750 740 730 710 700 690 680 670 660 650 640 630 620 610 600 590 580	Meters. 11.32 11.47 11.63 11.79 11.95 12.12 12.29 12.47 12.66 12.85 13.04 13.45 13.68 14.11 14.35 14.59 14.84	20° Meters. 11.41 11.56 11.72 11.88 12.04 12.21 12.39 12.57 12.75 12.94 13.14 13.34 13.55 13.76 13.98 14.21 14.45 14.70 14.95	Meters. 11.49 11.64 11.80 11.96 12.13 12.30 12.48 12.66 12.85 13.04 13.24 13.44 13.65 13.87 14.09 14.32 14.56 14.81 15.07	24° Meters. 11.58 11.73 11.89 12.05 12.22 12.39 12.57 12.75 12.94 13.14 13.34 13.54 13.75 13.97 14.20 14.43 14.67 14.92 15.17	26° Meters. 11.66 11.82 11.98 12.15 12.32 12.49 12.67 12.85 13.04 13.23 13.43 13.64 13.85 14.07 14.30 14.54 14.78 15.03 15.29	Meters. 11.75 11.91 12.07 12.20 12.40 12.58 12.76 12.94 13.13 13.33 13.53 13.74 13.96 14.18 14.41 14.64 14.89 15.14 15.40	CENTIG 30° Meters. 11.84 12.00 12.16 12.32 12.49 12.67 12.85 13.04 13.23 13.43 13.63 13.84 14.06 14.25 14.75 15.00 15.25 15.52	Meters. 11.92 12.08 12.24 12.41 12.58 12.76 12.94 13.13 13.32 13.52 13.73 13.94 14.15 14.38 14.62 14.86 15.11 15.36 15.63	34° Meters. 12.01 12.17 12.33 12.50 12.68 12.86 13.04 13.23 13.42 13.62 13.83 14.04 14.26 14.49 14.72 14.96 15.21 15.47 15.71	Meters. 12.10 12.26 12.42 12.59 12.77 12.95 13.13 13.32 13.52 13.72 13.93 14.15 14.37 14.60 14.83 15.07			
mm. 760 750 740 730 720 710 700 690 680 670 660 650 640 630 620 610 600 590	Meters. 11.32 11.47 11.63 11.79 11.95 12.12 12.29 12.47 12.66 12.85 13.04 13.24 13.45 13.66 13.88 14.11 14.35 14.59	Meters. 11.41 11.56 11.72 11.88 12.04 12.21 12.39 12.57 12.75 12.94 13.14 13.34 13.55 13.76 13.98 14.21 14.45 14.70	Meters. 11.49 11.64 11.80 11.96 12.13 12.30 12.48 12.66 12.85 13.04 13.24 13.44 13.65 13.87 14.09 14.32	24° Meters. 11.58 11.73 11.89 12.05 12.22 12.39 12.57 12.75 12.94 13.14 13.34 13.54 13.54 13.75 13.97 14.20 14.43 14.67 14.92	26° Meters. 11.66 11.82 11.98 12.15 12.32 12.49 12.67 12.85 13.04 13.23 13.43 13.64 13.85 14.07 14.30 14.54 14.78 15.03	28° Meters. 11.75 11.91 12.07 12.23 12.40 12.58 12.76 12.94 13.13 13.33 13.53 13.74 13.96 14.18 14.41 14.64 14.89 15.14	Meters. 11.84 12.00 12.16 12.32 12.49 12.67 12.85 13.04 13.23 13.43 13.63 13.84 14.06 14.28 14.51 14.75	Meters. 11.92 12.08 12.24 12.41 12.58 12.76 12.94 13.13 13.32 13.52 13.73 13.94 14.15 14.38 14.62 14.86	Meters. 12.01 12.17 12.33 12.50 12.68 12.86 13.04 13.23 13.42 13.62 13.83 14.04 14.26 14.49 14.72 14.96	Meters. 12.10 12.26 12.42 12.59 12.77 12.95 13.13 13.32 13.52 13.72 13.93 14.15 14.37 14.60 14.83 15.07			

DETERMINATION OF HEIGHTS BY THE BAROMETER.

Formula of Babinet.

$$\mathbf{Z} = C \frac{B_{\text{o}} - B}{B_{\text{o}} + B}$$

$$C \text{ (in feet)} = 52494 \left[\mathbf{I} + \frac{t_{\text{o}} + t - 64}{900} \right] - \text{English Measures.}$$

$$C \text{ (in metres)} = 16000 \left[\mathbf{I} + \frac{2(t_{\text{o}} + t)}{1000} \right] - \text{Metric Measures.}$$

In which Z = Difference of height of two stations in feet or metres.

 $B_{\rm o},\,B$ = Barometric readings at the lower and upper stations respectively, corrected for all sources of instrumental error.

 t_0 , t = Air temperatures at the lower and upper stations respectively.

Values of C.

ENGLISH MEASURES.

METRIC MEASURES.

F.	$\frac{1}{2}(\mathbf{t}_{0}+\mathbf{t}).$	log C.	C.	
15	F.		Feet.	
20	10°	4.69834	49928	
25	15	.70339	50511	
30 .71818 52261 35 4.72300 52844 40 .72777 53428 45 .73248 54011 50 .73715 54595 55 .74177 55178 60 4.74633 55761 65 .75085 56344 70 .75532 56927 75 .75975 57511 80 .76413 58094 85 4.76847 58677 90 .77276 59260 95 .77702 59844	20	.70837	51094	
35 4.72300 52844 40 .72777 53428 45 .73248 54011 50 .73715 54595 55 .74177 55178 60 4.74633 55761 65 .75085 56344 70 .75532 56927 75 .75975 57511 80 .76413 58094 85 4.76847 58677 90 .77276 59260 95 .77702 59844	25	.71330	51677	
40 .72777 53428 45 .73248 54011 50 .73715 54595 55 .74177 55178 60 4.74633 55761 65 .75085 56344 70 .75532 56927 75 .75975 57511 80 .76413 58094 85 4.76847 58677 90 .77276 59260 95 .77702 59844	30	.71818	52261	
40 .72777 53428 45 .73248 54011 50 .73715 54595 55 .74177 55178 60 4.74633 55761 65 .75085 56344 70 .75532 56927 75 .75975 57511 80 .76413 58094 85 4.76847 58677 90 .77276 59260 95 .77702 59844				
45 .73248 54011 50 .73715 54595 55 .74177 55178 60 4.74633 55761 65 .75085 56344 70 .75532 56927 75 .75975 57511 80 .76413 58094 85 4.76847 58677 90 .77276 59260 95 .77702 59844	35	4.72300	52844	
50 .73715 54595 55 .74177 55178 60 4.74633 55761 65 .75085 56344 70 .75532 56927 75 .75975 57511 80 .76413 58094 85 4.76847 58677 90 .77276 59260 95 .77702 59844	40	.72777	53428	
60 4.74633 55761 65 .75085 56344 70 .75532 56927 75 .75975 57511 80 .76413 58094 85 4.76847 58677 90 .77276 59260 95 .77702 59844	45	.73248	54011	
60 4.74633 55761 65 .75085 56344 70 .75532 56927 75 .75975 57511 80 .76413 58094 85 4.76847 58677 90 .77276 59260 95 .77702 59844	50	.73715	54595	
65 .75085 56344 70 .75532 56927 75 .75975 57511 80 .76413 58094 85 4.76847 58677 90 .77276 59260 95 .77702 59844	55	.74177	55178	
65 .75085 56344 70 .75532 56927 75 .75975 57511 80 .76413 58094 85 4.76847 58677 90 .77276 59260 95 .77702 59844				
70 .75532 56927 75 .75975 57511 80 .76413 58094 85 4.76847 58677 90 .77276 59260 95 .77702 59844	60	4.74633	55761	
75 .75975 57511 80 .76413 58094 85 4.76847 58677 90 .77276 59260 95 .77702 59844	65	.75085	56344	
85 4.76847 58677 90 .77276 59260 95 .77702 59844	70	-75532	56927	
85 4.76847 58677 90 .77276 59260 95 .77702 59844	75	.75975	57511	
90 .77276 59260 95 .77702 59844	So	.76413	58094	
90 .77276 59260 95 .77702 59844				
95 .77702 59844	85	4.76847	58677	
	90	.77276	59260	
100 .78123 60427	95	.77702	59844	
	100	.78123	60427	

$\frac{1}{2}(t_{o}+t).$	log C.	c.
c.		Metres.
-10°	4.18639	15360
-8	.19000	15488
- 6	.19357	15616
-4	.19712	15744
- 2	.20063	15872
0	4.20412	16000
+ 2	.20758	16128
4	.21101	16256
6	.21442	16384
8	.21780	16512
10	4.22115	16640
12	.22448	16768
14	.22778	16896
16	.23106	17024
18	.23431	17152
20	4.00554	x ma20
	4.23754	17280
22	.24075	17408
24 26	.24393	17536
28	.24709	17664
20	.25022	17792
30	4.25334	17920
32	.25643	18048
34	.25950	18176
36	.26255	18304
3-		- 55 4

TABLE 72.

BAROMETRIC PRESSURES CORRESPONDING TO THE TEMPERATURE OF THE BOILING POINT OF WATER.

ENGLISH MEASURES.

Tempera-	0.	.1	.2	.3	.4	1 ,5	.6	.7	.8	.9
F.	Inches.	Inches.	Inches,	Inches						
185°				Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
186	17.075	17.112	17.150	17.187	17.224	17.262	17.300	17.337	17.375	17.413
187	17.450	17.400	17.526	17.564	17.602	17.641	17.679	17.717	17.756	17.794
188	18.221	18.261	17.910	17.948	17.987	18.026	18.065	18.104	18.143	18.182
180	18.618	18.658	18.300	18.340	18.379	18.419	18.458	18.498	18.538	18.578
	l .		_	18.738	18.778	18.818	18.859	18.899	18.940	18.980
190	19.021	19.062	19.102	19.143	19.184	19.225	19.266	19.308	19.349	19.390
191	19.431	19.473	19.514	19.556	19.598	19.639	19.681	19.723	19.765	10.807
192	19.849	19.892	19.934	19.976	20.019	20.061	20.104	20.146	20.189	20.232
193	20.275	20.318	20.361	20.404	20.447	20.490	20.533	20.577	20.620	20.664
194	20.707	20.751	20.795	20.839	20.883	20.927	20.971	21.015	21.059	21.103
195	21.148	21.192	21.237	21.282	21.326	21.371	21.416	21.461	21.506	21.551
196	21.597	21.642	21.687	21.733	21.778	21.824	21.870	21.015	21.961	22.007
197	22.053	22.000	22.145	22.192	22.238	22.284	22.331	22.377	22.424	22.471
198	22.517	22.564	22.611	22.658	22.706	22.753	22.800	22.847	22.805	22.042
199	22,990	23.038	23.085	23.133	23.181	23.229	23.277	23.325	23.374	23.422
200	23.470	23.519	23.568	23.616	23.665	23.714	23.763	23.812	23.861	23.010
201	23.959	24.000	24.058	24.108	24.157	24.207	24.257	24.307	24.357	24.407
202	24.457	24.507	24.557	24.608	24.658	24.700	24.759	24.810	24.861	24.912
203	24.963	25.014	25.065	25.116	25.168	25.219	25.271	25.322	25.374	25.426
204	25.478	25.530	25.582	25.634	25.686	25.738	25.791	25.843	25.896	25.948
205	26.001	26.054	26.107	26.160	26.213	26.266	26.319	26.373	26.426	26,480
206	26.534	26.587	26.641	26.695	26.749	26.803	26.857	26.912	26.066	27.021
207	27.075	27.130	27.184	27.239	27.294	27.349	27.404	27.460	27.515	27.570
208	27.626	27.681	27.737	27.793	27.848	27.904	27.960	28.016	28.073	28.129
209	28.185	28.242	28.298	28.355	28.412	28.469	28.526	28.583	28.640	28.697
210	28.754	28.812	28.869	28.927	28.985	29.042	20.100	20.158	20.216	20.275
211	29.333	29.391	29.450	29.508	29.567	29.626	29.685	29.744	29.803	20.862
212	29.921	29.981	30.040	30.100	30.159	30.219	30.279	30.339	30.399	30.459
213	30.519	30.580	30.640	30.701	30.761	30.822	30.883	30.944	31.005	31.066
214	31.127	31.199	31.250	31.311	31.373	31.435	31.497	31.559	31.621	31.683
-										

METRIC MEASURES.

TABLE 73.

Tempera-l	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
C.	mm.									
80°	355.40	356.84	358.28	359.73	361.19	362.65	364.11	365.58	367.06	368.54
81	370.03	371.52	373.01	374.51	376.02	377.53	379.05	380.57	382.09	383.62
82	385.16	386.70	388.25	389.80	391.36	392.92	394.49	396.06	397.64	399.22
83	400.81	402.40	404.00	405.61	407.22	408.83	410.45	412.08	413.71	415.35
84	416.99	418.64	420.29	421.95	423.61	425.28	426.95	428.64	430.32	432.01
85	433.71	435.41	437.12	438.83	440.55	442.28	444.01	445.75	447.49	449.24
86	450.99	452.75	454.51	456.28	458.06	459.84	461.63	463.42	465.22	467.03
87	468.84	470.66	472.48	474.3I	476.14	477.99	479.83	481.68	483.54	485.41
88	487.28	489.16	491.04	492.93	494.82	496.72	498.63	500.54	502.46	504.39
89	506.32	508.26	510.20	512.15	514.11	516.07	518.04	520.01	521.99	523.98
90	525.97	527.97	529.98	531.99	534.01	536.04	538.07	540.11	542.15	544.21
91	546.26	548.33	550.40	552.48	554.56	556.65	558.75	560.85	562.96	565.08
92	567.20	569.33	571.47	573.61	575.76	577.92	580.08	582.25	584.43	586.61
93	588.80	591.00	593.20	595.41	597.63	599.86	602.09	604.33	606.57	608.82
94	611.08	613.35	615.62	617.90	620.19	622.48	624.79	627.09	629.41	631.73
95	634.06	636.40	638.74	641.09	643.45	645.82	648.19	650.57	652.96	655.35
96	657.75	660.16	662.58	665.00	667.43	669.87	672.32	674.77	677.23	679.70
97	682.18	684.66	687.15	689.65	692.15	694.67	697.19	699.71	702.25	704.79
98	707.35	709.90	712.47	715.04	717.63	720.22	722.81	725.42	728.03	730.65
99	733.28	735.92	738.56	741.21	743.87	746.54	749.22	751.90	754.59	757.29
100	760.00	762.72	765.44	768.17	770.91	773.66	776.42	779.18	781.95	784.73



HYGROMETRICAL TABLES.

Pressure of aqueous vapor over ice—English measures	Table 74
Pressure of aqueous vapor over water—English measures .	Table 75
Pressure of aqueous vapor over ice—Metric measures	Table 76
Pressure of aqueous vapor over water—Metric measures .	Table 77
Pressure of aqueous vapor over ice—Dynamic measures .	Table 78
Pressure of aqueous vapor over water—Dynamic measures .	Table 79
Weight of a cubic foot of saturated vapor—English measures	Table So
Weight of a cubic meter of saturated vapor—Metric measures	Table 81

PRESSURE OF AQUEOUS VAPOR OVER ICE.

ENGLISH MEASURES.

											_		_	
Tempera ture.	- Vapor Pressur	Tempera ture,	- Vapor Pressu	r Tempe re. ture		r ire.	Tempe ture		Va Pres	ssure.		mpera- ture.	F	Vapor ressure.
F.	Inches	. F.	Inche	s. F.	Inche	s.	F.		Inc	ches.		F.		Inches.
-60°	0.0000		0.002				-15	o°		1600		7 5°		02556
59	.0010	7 44	.002				14.			1738		7.0		.02626
58	.0011		. 003				14.			1787		6.5		. 02698
57	.0012		.003				13.			1838	6.0			02771
56	.0013	41	.003	56 26	. 008	96	13.	0	.0	1890	5 · 5			. 02847
-55	.0014	1 -40	. 003	79 -25	. 000	51	-12.	5	. 0	1943	-	5.0		02924
54	.0015		. 004				12.			1998		4.5		03003
53	.0016		. 004				11.			2054		4.0		. 03084
52	.0017		. 004				11.			2111		3.5		03168
51	.0018		. 004	- 1		- 1	10.	_		2170		3.0		.03253
-50	.0019		. 005				-10.			2230	-	2.5		.03340
49 48	.0021		.005				9. 9.			2292 2356		2.0 I.5		03429
47	.0022	00	.006			1	8.			2421		1.0		.03520
46	.0025		.006				8.	0		2487		0.5		.03710
		l °		.		0	i					3		
Tem- perat.	.0	.1	.2	.3	.4		.5		6	.7		.8		.9
F.	Inches.	Inches.	Inches.	Inches.	Inches.	ı	nches.	Inc	hes.	Inche	s.	Inche	s.	Inches.
0		0.03820											- 1	0.03002
1	. 04013	. 04034	. 04055	.04076	. 04097		04118	. 04	140	.041	61	. 04 18	33	. 04204
2	.04226	. 04248	. 04270	.04292	.04314		04337		359	. 043		. 0440		. 04427
3	.04450	. 04473	. 04496	.04519	.04543		04566		590	. 046		. 0463		.0466r
4	. 04685	. 04709	. 04733	.04758	. 04782		04807	. 04	831	. 048	50	. 0488	1	. 04906
5	. 04931	. 04956	. 04982	. 05007	. 05033		05058		084	. 051		.051		.05162
6	.05189	.05215	.05242	. 05269			05322		350	.053		. 0540		. 05431
7 8	.05459	. 05487	.05514	. 05542			05598 05887		627 917	. 056 . 059		. 0568		. 05712
9	.05741	. 05770	. 06008	.05028			05007		221	. 062		.0628		.06315
											_			
10	.06346	. 06378	. 06410	. 06442	. 06474		06507		539	. 065	72	. 0660		. 06638
11	.06670	. 06703	. 06737	.06770	. 06804		06838 07184		872 220	.069		. 069.		. 06975
12	.07009	.07044	. 07436	.07114	.07149		07134		583	.072		.076		.07328
14	.07303		. 07800	.07848	.07886		07925		964	. 080		. 080.		. 08082
15	.08121	.08161	. 08201	. 08241	.08281		08321		362	. 084		. 0842 . 0886		. 08484
16 17	. 08525 . 08948	. 08566	. 000035	.00070	.00092		08734 00167		777 211	.003		. 0030		.00345
18	.00340	.00435	. 00481	.09526			09107		664	. 007		. 097		.00804
19	.09851	. 00898	. 09946				10090		138	. 101		. 102		. 10284
20	.10333	. 10383	, 10432	. 10482	. 10532		10582	. 10	633	. 106	82	. 107	3.4	. 10785
21	. 10333	. 10388	. 10432				11006		140	. 112		. 112		. 11308
22	.11361	.11415	. 11469				11632		687	.117		. 1170		. 11853
23	. 11909		. 1 202 2	. 12078	. 12135	١.	12192	. I 2	250	. 123	07	. 123	55	. 12423
24	. 12481	. 12540	. 12598	. 12657	. 12717		12776		836	. 128	96	. 129.	56	. 13017
25	. 13077	. 13138	. 13200	. 13261	. 13323		13385	. 13	447	. 135	10	. 135	73	. 13636
26	. 13699		. 13827	. 13891	. 13956	١.	14021		086	. 141	51	. 142	16	. 14282
27	. 14348	. 14415	. 14481				14683		751	. 148		. 148		. 14956
28	. 15024		. 15163	. 15233			15374		444	. 155		. 155		. 15658
29	. 15729	. 15801	. 15874	. 15947	. 16020		16093	. 10	167	. 162	41	. 163	15	. 16389
30	. 16463	. 16538	. 16614	. 16690	. 16766		16842	. 16	919	. 169	96	. 170		. 17150
31	. 17228	. 17306	. 17386				17626		7707	. 177		. 178		. 17950
32	. 18032													
-													_	

PRESSURE OF AQUEOUS VAPOR OVER WATER. ENGLISH MEASURES.

Tempera-										
ture.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
F.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
32°	0.1803	0.1810	0.1818	0.1825	0.1833	0.1840	0.1847	0.1855	0.1862	0.1870
33	.1877	.1885	.1893	.1900	.1908	.1915	.1923	.1931	.1030	1046
34	.1954	.1962	.1970	.1978	.1986	.1994	.2002	.2010	.2018	.2026
35	.2034	.2042	.2050	.2059	.2067	.2075	.2083	.2001	.2100	.2108
36	.2117	.2125	.2133	.2142	.2150	.2159	.2168	.2176	.2185	.2193
37	.2202	.2211	.2220	.2228	.2237	.2246	.2255	.2264	.2273	.2282
38	.2201	.2300	.2309	.2318	.2327	.2336	.2345	.2355	.2364	.2373
. 39	.2382	.2392	.2401	.2410	.2420	.2429	.2439	.2448	.2458	.2467
40	.2477	.2487	.2496	.2506	.2516	.2526	.2536	.2545	.2555	.2565
41	.2575	.2585	.2595	.2606	.2616	.2626	.2636	.2646	.2656	.2667
42	.2677	.2687	.2698	.2708	.2719	.2729	.2740	.2750	.2761	.2771
43	.2801	.2793	.2804	.2814	.2825	.2836	.2847	.2858	.2869	.2880
	.2091	.2902	.2913	.2924	.2935	.2946	.2958	.2969	.2981	.2992
45	.3003	.3014	.3026	.3037	.3049	.3061	.3073	.3084	.3096	.3108
46	.3120	.3132	.3144	.3156	.3167	.3179	.3191	.3203	.3216	.3228
47 48	.3240	.3252	.3265	-3277	.3289	.3301	.3314	-3326	-3339	-3352
49	.3365	·3377 ·3506	.3390	.3402	.3415	.3428	.3441	•3454	.3467	.3480
	13493	.3300	.3519	-3532	.3546	-3559	·357 ²	.3585	-3599	.3612
50	.3626	.3639	.3653	.3666	.3680	.3694	.3708	.3722	.3736	-3749
51	.3763	-3777	.3791	.3805	.3820	.3834	.3848	.3862	.3876	.3890
52	.3905	.3919	-3934	.3948	.3963	.3978	-3993	.4007	.4022	.4037
53	.4052	.4067	.4082	.4097	.4112	.4127	.4142	.4157	.4172	.4187
54	.4203	.4218	.4234	.4249	.4265	.4280	.4296	.4312	.4328	-4343
55	·4359	-4375	.4391	-4407	.4423	-4439	.4455	.4471	.4488	.4504
56	.4521	-4537	.4554	.4570	.4587	.4603	.4620	.4637	.4654	.4670
57	.4687	.4704	.4721	.4738	·4755	-4772	.4790	.4807	.4824	.4841
58	.4859	.4876	.4894	.4912	.4930	•4947	.4965	.4983	.5001	.5019
59	.5037	.5055	.5073	.5091	.5110	.5128	.5146	.5164	.5183	.5201
60	.5220	.5239	-5258	.5276	.5295	.5314	-5333	-5352	.5371	.5390
61	.5409	.5428	-5448	.5467	.5486	-5505	-5525	-5545	.5565	.5584
62	.5604	.5624	.5644	.5663	.5683	.5703	-5724	-5744	.5764	-5784
64	.5805	.5825	.5846	.5866 .6076	.5887	.5908	.5929	.5950	.5971	.5992
	.0013	.0034	.6055	.0070	.6097	.6118	.6140	.6161	.6183	.6204
65	.6226	.6248	.6270	.6292	.6314	.6336	.6358	.6380	.6402	.6424
66	.6447	.6469	.6492	.6514	.6537	.6559	.6582	.6605	.6628	.6651
67 68	.6674	.6697	.6721	.6744	.6767	.6790	.6814	.6837	.6861	.6885
69	.6909	.6932	.6956	.6980	.7004	.7028	.7053	.7077	.7101	.7125
	.7150	.7174	.7199	.7224	.7249	.7274	.7299	.7324	.7348	.7373
70	.7399	.7424	.7449	.7474	.7500	.7526	.7552	-7577	.7603	.7629
71	.7655	.7681	.7707	.7733	.7760	.7786	.7813	.7839	.7866	.7892
72	.7919	.7946	.7973	.8000	.8027	.8054	.8081	.8108	.8136	.8163
73 74	.8191	.8219	8247	.8274	.8302	.8330	.8358	.8386	.8414	.8442
	.8471	.8499	.8528	.8556	.8585	.8614	.8643	.8672	.8701	.8730
75	.8760	.8789	.8818	.8847	.8877	.8907	.8937	.8966	.8996	.9026
76	.9056	.9086	.9117	.9147	.9178	.9208	.9239	.9269	.9300	.9331
77 78	.9362	.9393	.9424	-9455	.9487	.9518	.9550	.9581	.9613	.9645
	.9677	.9709	.9741	.9773	.9805	.9837	.9870	.9902	-9935	.9968
79	1.0001	1.0033	1.0066	1.0099	1.0133	1.0166	1.0199	1.0232	1.0266	1.0300
80	1.0334	1.0367	1.0401	1.0435	1.0470	1.0504	1.0538	1.0572	1.0607	1.0641
1	l							J		

PRESSURE OF AQUEOUS VAPOR OVER WATER. ENGLISH MEASURES.

Tempera- ture.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
F.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
80°	1.0334	1.0367	1.0401	1.0435	1.0470	1.0504	1.0538	1.0572	1.0607	1.0641
81	1.0676	1.0711	1.0746	1.0781	1.0816	1.0851	1.0887	1.0022	1.0058	1.0003
82	1.1020	1.1005	1.1101	1.1137	1.1173	1.1200	1.1246	1.1282	1.1319	1.1355
83	1.1302	1.1420	1.1466	1.1503	1.1540	1.1577	1.1615	1.1652	1.1600	1.1727
84	1.1765	1.1803	1.1841	1.1879	1.1917	1.1955	1.1994	1.2032	1.2071	1.2110
0.5		00					. 0		. (.)	
85 86	1.2149	1.2188	1.2227	1.2266	1.2305	1.2344	1.2384	1.2423	1.2463	1.2503
87	I.2543	1.2583	1.2623	1.2663	1.2704 1.3114	1.2744	1.2785	1.2826	1.3281	1.2908
88	1.3365	1.3407	1.3450	1.3492	1.3535	1.3155	1.3197	1.3239	1.3707	1.3323
89	1.3794	1.3837	1.3881	1.3025	1.3969	1.4013	1.4057	1.4101	1.4146	1.4100
	5194	3-57				43	4-57			
90	1.4234	1.4279	1.4324	1.4360	1.4414	1.4459	1.4505	1.4550	1.4596	1.4642
91	1.4688	1.4734	1.4780	1.4826	1.4872	1.4918	1.4965	1.5012	1.5059	1.5106
92	1.5153	1.5200	1.5247	1.5294	1.5342	1.5390	1.5438	1.5486	1.5534	1.5582
93	1.5630	1.5678 1.6171	1.5727 1.6221	1.5776	1.5825	1.5874	1.5923 1.6422	1.5972	1.6022	1.6574
94	1.0121	1.01/1		1.02/1	1.0321	1.6371	1.0422	1.04/2	1.6523	1.03/4
95	1.6625	1.6676	1.6728	1.6779	1.6831	1.6882	1.6934	1.6986	1.7038	1.7000
96	1.7143	1.7195	1.7248	1.7301	1.7354	1.7407	1.7460	1.7513	1.7567	1.7620
97	1.7674	1.7728	1.7782	1.7836	1.7891	1.7945	1.8000	1.8055	1.8110	1.8165
98	1.8220	1.8275	1.8331	1.8386	1.8442	1.8498	1.8554	1.8610	1.8667	1.8723
99	1.8780	1.8837	1.8894	1.8951	1.9008	1.9065	1.9123	1.9181	1.9239	1.9297
100	1.9355	1.9413	1.9472	1.9530	1.9589	1.9648	1.9707	1.9766	1.9826	1.9885
101	1.9945	2.0005	2.0065	2.0125	2.0185	2.0245	2.0306	2.0367	2.0428	2.0489
102	2.0550	2.0611	2.0673	2.0735	2.0797	2.0859	2.0021		2.1046	2.1108
103	2.1171	2.1234	2.1298	2.1301	2.1425	2.1488	2.1552	2.1616	2.1680	2.1744
104	2.1809	2.1874	2.1939	2.2004	2.2069	2.2134	2.2200	2.2265	2.233I	2.2397
105	2.2463	2.2529	2.2596	2.2663	2.2730	2.2797	2.2864	2.2931	2.2000	2.3067
106	2.3135	2.3203	2.3271	2.3339	2.3408	2.3477	2.3546	2.3615	2.3684	2.3753
107	2.3823	2.3893	2.3963	2.4033	2.4103	2.4173	2.4244	2.4315	2.4386	2.4457
108	2.4529	2.4600	2.4672	2.4744	2.4816	2.4888	2.4961	2.5033	2.5106	2.5179
109	2.5252	2.5325	2.5399	2.5473	2.5547	2.5621	2.5695	2.5770	2.5845	2.5919
110	2.5994	2.6069	2.6145	2.6220	2.6296	2.6372	2.6448	2.6524	2.6601	2.6678
III	2.6755	2.6832	2.6909	2.6986	2.7064	2.7142	2.7220	2.7298	2.7377	2.7456
112	2.7535	2.7614	2.7693	2.7772	2.7852	2.7932	2.8012	2.8002	2.8173	2.8253
113	2.8334	2.8415	2.8496	2.8577	2.8659	2.8741	2.8823	2.8905	2.8988	2.9070
114	2.9153	2.9236	2.9320	2.9403	2.9487	2.9571	2.9655	2.9739	2.9823	2.9908
115	2.9993	3.0078	3.0163	3.0248	3.0334	3.0420	3.0506	3.0592	3.0679	3.0766
116	3.0853	3.0940	3.1027	3.1115	3.1203	3.1291	3.1379	3.1467	3.1556	3.1645
117	3.1734	3.1823	3.1913	3.2003	3.2093	3.2183	3.2273	3.2364	3.2455	3.2546
118	3.2637	3.2728	3.2820	3.2912	3.3004	3.3096	3.3189	3.3282	3.3375	3.3468
119	3.3562	3.3655	3.3749	3.3843	3.3938	3.4032	3.4127	3.4222	3.4318	3.4413
120	3.4509	3.4605	3.4701	3.4797	3.4894	3.4991	3.5088	3.5185	3.5283	3.5381
121	3.5479	3.5577	3.5676	3.5774	3.5873	3.5972	3.6072	3.6172	3.6272	3.6372
122	3.6472	3.6573	3.6674	3.6775	3.6876	3.6977	3.7079	3.7181	3.7284	3.7386
123	3.7489	3.7592	3.7695	3.7799	3.7903	3.8007	3.8111	3.8215	3.8320	3.8425
124	3.8530	3.8636	3.8742	3.8848	3.8954	3.9060	3.9167	3.9274	3.9381	3.9488
125	3.9596	3.9704	3.9813	3.9921	4.0030	4.0139	4.0248	4.0357	4.0467	4.0577
126	4.0687	4.0797	4.0908	4.1019	4.1131	4.1242	4.1354	4.1466	4.1578	4.1690
127	4.1803	4.1916	4.2030	4.2143	4.2256	4.2370	4.2485	4.2599	4.2714	4.2829
128	4.2945	4.3061	4.3177	4.3293	4.3410	4.3527	4.3645	4.3762	4.3880	4.3998
129	4.4116	4.4235	4.4354	4.4473	4.4592	4.4711	4.4831	4.4951	4.5072	4.5192
130	4.5313	4.5434	4.5555	4.5677	4.5798	4.5921	4.6043	4.6166	4.6289	4.6412

PRESSURE OF AQUEOUS VAPOR OVER WATER.

ENGLISH MEASURES.

Temper- ature.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
F,	Inches.	Inches	Leaber				1 1			
		Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
130°	4.531	4.543	4.556	4.568	4.580	4.592	4.604	4.617	4.629	4.641
131	4.654	4.666	4.678	4.691	4.703	4.716	4.728	4.741	4.754	4.766
132	4.779	4.792	4.804	4.817	4.830	4.843	4.855	4.868	4.881	4.894
133	4.907	4.920	4.933	4.946	4.959	4.972	4.985	4.998	5.012	5.025
134	5.038	5.051	5.065	5.078	5.091	5.105	5.118	5.132	5.145	5.158
135	5.172	5.186	5.190	5.213	5.226	5.240	5.254	5.268	5.281	5.295
136	5.309	5.323	5.337	5.351	5.365	5.379	5.392	5.407	5.421	5-435
137	5.449	5.463	5.477	5.492	5.506	5.520	5.535	5.549	5.563	5.578
138	5.592	5.607	5.621	5.636	5.650	5.665	5.680	5.694	5.709	5.724
139	5.739	5.754	5.768	5.783	5.798	5.813	5.828	5.843	5.858	5.873
140	5.889	5.904	5.919	5.934	5.949	5.965	5.980	5.995	6.011	6.026
141	6.041	6.057	6.072	6.088	6.104	6.119	6.135	6.151	6.166	6.182
142	6.198	6.214	6.229	6.245	6.261	6.277	6.293	6.300	6.325	6.341
143	6.358	6.374	6.390	6.406	6.422	6.439	6.455	6.472	6.488	6.504
144	6.521	6.537	6.554	6.571	6.587	6.604	6.621	6.637	6.654	6.671
145	6.688	6.705	6.722	6.730	6.756	6.773	6.790	6.807	6.824	6.841
146	6.858	6.876	6.803	6.010	6.928	6.945	6.962	6.080	6.997	7.015
147	7.032	7.050	7.068	7.085	7.103	7.121	7.139	7.156	7.174	7.192
148	7.210	7.228	7.246	7.264	7.282	7.300	7.319	7.337	7.355	7.374
149	7.392	7.410	7.429	7-447	7.466	7.484	7.503	7.521	7.540	7.559
150	7.577	7.596	7.615	7.634	7.653	7.672	7.601	7.710	7.729	7.748
151	7.767	7.786	7.805	7.824	7.844	7.863	7.882	7.002	7.921	7.941
152	7.960	7.980	8.000	8.010	8.039	8.050	8.078	8.008	8.118	8.138
153	8.158	8.178	8.108	8.218	8.238	8.258	8.278	8.298	8.319	8.339
154	8.360	8.380	8.400	8.421	8.441	8.462	8.482	8.503	8.524	8.545
155	8.565	8.586	8.607	8.628	8.649	8.670	8.601	8.712	8.733	8.754
156	8.776	8.707	8.818	8.839	8.861	8.882	8.904	8.925	8.947	8.968
157	8.000	0.012	0.034	9.055	9.077	9.000	0.121	9.143	9.165	9.187
158	9.200	9.231	9.253	9.276	9.298	9.320	0.342	9.365	9.387	9.410
159	9.432	9.455	9.233	9.500	9.523	9.546	9.569	9.592	9.507	9.638
160	0.661	0.684	9.707	9.730	9.753	9.776	9.799	9.823	0.846	9.870
161	9.893	9.004	9.707	9.730	9.733	10.011	10.035	10.059	10.082	10.106
162	10.130	10.154	10.178	10.203	10.227	10.251	10.275	10.299	10.324	10.348
163	0		10.178	10.446	10.227	10.495	10.520	10.545	10.570	10.595
164	10.373	10.397	10.422	10.695	10.720	10.745	10.770	10.795	10.821	10.393
			·							
165	10.872	10.897	10.922	10.948	10.974	10.999	11.025	11.051	11.077	11.102
166	11.128	11.154	11.180	11.206	11.232	11.258	11.284	11.311	11.337	11.363
167	11.300	11.417	11.444		11.497	11.523	11.550	11.577	11.604	11.631
168	11.658	11.685	11.712	11.739	11.766	11.793	11.821	11.848	11.875	11.903
169	11.930	11.957	11.985	12.013	12.040	12.068	12.096	12.124	12.152	12.180
170	12.208	12.236	12.264	12.292	12.320	12.349	12.377	12.406	12.434	12.463
171	12.491	12.520	12.548	12.577	12.606	12.635	12.664	12.693	12.722	12.751
172	12.780	12.809	12.838	12.868	12.897	12.927	12.956	12.986	13.015	13.045
173	13.074	13.104	13.134	13.164	13.194	13.224	13.254	13.284	13.314	13.344
174	13.374	13.405	13.435	13.465	13.496	13.527	13.557	13.588	13.619	13.649
175	13.680	13.711	13.742	13.773	13.804	13.835	13.867	13.898	13.929	13.961
176	13.992	14.024	14.055	14.087	14.118	14.150	14.182	14.214	14.246	14.278
177	14.310	14.342	14.374	14.406	14.438	14.471	14.503	14.536	14.568	14.601
178	14.633	14.666	14.699	14.731	14.764	14.797	14.830	14.864	14.897	14.930
179	14.963	14.996	15.030	15.063	15.097	15.130	15.164	15.197	15.231	15.265
180	15.299	15.333	15.367	15.401	15.435	15.469	15.504	15.538	15.572	15.607

TABLE 75.

PRESSURE OF AQUEOUS VAPOR OVER WATER. ENGLISH MEASURES.

Tempera- ture.	.0	.1	.2	.3	.4	.5	.6	.7	،8	.9
F.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
180°	15.200	15.333	15.367	15.401	15.435	15.460	15.504	15.538	15.572	15.607
181	15.641	15.676	15.710	15.745	15.780	15.815	15.850	15.885	15.920	15.955
182	15.990	16.025	16.060	16.096	16.131	16.167	16.202	16.238	16.274	16.309
183	16.345	16.381	16.417	16.453	16.489	16.525	16.561	16.598	16.634	16.670
184	16.707	16.743	16.780	16.817	16.853	16.890	16.927	16.964	17.001	17.038
185	17.075	17.112	17.150	17.187	17.224	17.262	17.300	17.337	17.375	17.413
186	17.450	17.488	17.526	17.564	17.602	17.641	17.679	17.717	17.756	17.794
187	17.832	17.871	17.910	17.948	17.987	18.026	18.065	18.104	18.143	18.182
188	18.221	18.261	18.300	18.340	18.379	18.419	18.458	18.498	18.538	18.578
189	18.618	18.658	18.698	18.738	18.778	18.818	18.859	18.899	18.940	18.980
190	19.021	19.062	19.102	19.143	19.184	19.225	19.266	19.308	19.349	19.390
191	19.431	19.473	19.514	19.556	19.598	19.639	19.681	19.723	19.765	19.807
192	19.849	19.892	19.934	19.976	20.019	20.061	20.104	20.146	20.189	20.232
193	20.275	20.318	20.361	20.404	20.447	20.490	20.533	20.577	20.620	20.664
194	20.707	20.751	20.795	20.839	20.883	20.927	20.971	21.015	21.059	21.103
195	21.148	21.102	21.237	21.282	21.326	21.371	21.416	21.461	21.506	21.551
196	21.597	21.642	21.687	21.733	21.778	21.824	21.870	21.915	21.961	22.007
197	22.053	22.000	22.145	22.192	22.238	22.284	22.331	22.377	22.424	22.471
198	22.517	22.564	22.611	22.658	22.706	22.753	22.800	22.847	22.895	22.942
199	22.990	23.038	23.085	23.133	23.181	23.229	23.277	23.325	23.374	23.422
200	23.470	23.519	23.568	23.616	23.665	23.714	23.763	23.812	23.861	23.910
201	23.959	24.009	24.058	24.108	24.157	24.207	24.257	24.307	24.357	24.407
202	24.457	24.507	24.557	24.608	24.658	24.709	24.759	24.810	24.86 I	24.912
203	24.963	25.014	25.065	25.116	25.168	25.219	25.271	25.322	25.374	25.426
204	25.478	25.530	25.582	25.634	25.686	25.738	25.791	25.843	25.896	25.948
205	26.001	26.054	26.107	26.160	26.213	26.266	26.319	26.373	26.426	26.480
206	26.534	26.587	26.641	26.695	26.749	26.803	26.857	26.912	26.966	27.021
207	27.075	27.130	27.184	27.239	27.294	27.349	27.404	27.460	27.515	27.570
208	27.626	27.681	27.737	27.793	27.848	27.904	27.960	28.016	28.073	28.129
209	28.185	28.242	28.298	28.355	28.412	28.469	28.526	28.583	28.640	28.697
210	28.754	28.812	28.869	28.927	28.985	29.042	29.100	29.158	29.216	29.275
211	29.333	29.391	29.450	29.508	29.567	29.626	29.685	29.744	29.803	29.862
212	29.921	29.981	30.040	30.100	30.159	30.219	30.279	30.339	30.399	30.459
213	30.519	30.580	30.640	30.701	30.761	30.822	30.883	30.944	31.005	31.066
214	31.127	31.189	31.250	31.311	31.373	31.435	31.497	31.559	31.621	31.683

PRESSURE OF AQUEOUS VAPOR OVER ICE.

METRIC MEASURES

Tempe	ra- Vapo	Tom	pera- V	арог	Tempera-	Va	por 1	Tempera-	Vapor	Tomposo	Vanas
ture	press			ssure	ture		ssure	ture	bressnie	Tempera- ture	Vapor pressure
C. 70 69 68 67 66	0.00 0.00 0.00	19 —6 22 26 30	50° 0.6 59 0.6 58 0.6 57 0.6	0080 0092 0105 0120	C. -50.0° 49.5 49.0 48.5 48.0	0.0 0.0 0.0	m. 294 308 329 350 373	C. -45.0° 44.5 44.0 43.5 43.0	mm. 0.0537 0.0570 0.0605 0.0642 0.0680	-40.0° 39.5 39.0 38.5 38.0	mm. 0.0964 0.1020 0.1080 0.1143 0.1209
—65 64 63 62 61	0.00	46 53 61	54 0.6 53 0.6 52 0.6	0156 0178 0202 0229 0260	-47.5 47.0 46.5 46.0 45.5	0.0	396 421 448 476 506	-42.5 42.0 41.5 41.0 40.5	0.0721 0.0765 0.0811 0.0859 0.0910	-37.5 37.0 36.5 36.0 35.5	0.1279 0.1352 0.1430 0.1511 0.1596
Tem- pera- ture	.0	.1	.2	.3	.4		.5	.6	.7	.8	.9
-35° 34 33 32 31	mm. 0.1686 0.1880 0.2094 0.2331 0.2591	mm. 0.1668 0.1860 0.2072 0.2306 0.2564	mm. 0.1650 0.1840 0.2050 0.2281 0.2537	0.18 0.20 0.22	32 0.16 20 0.18 28 0.20 57 0.22	00 06 33	mm. 0.1596 0.1781 0.1984 0.2209 0.2458	0.1761 0.1963 0.2186	mm. 0.1562 0.1742 0.1942 0.2163 0.2406	0.1723 0.1921 0.2140	mm. 0.1528 0.1705 0.1901 0.2117 0.2355
-30 29 28 27 26	0.2878 0.3194 0.3541 0.3923 0.4341	0.2848 0.3161 0.3505 0.3883 0.4297	0.2818 0.3128 0.3469 0.3843 0.4254	0.30	96 0.30 33 0.33 04 0.37	64 98 66	0.2731 0.3032 0.3363 0.3727 0.4127	0.3001 0.3329 0.3689	0.2674 0.2970 0.3295 0.3652 0.4044	0.2939 0.3261 0.3615	0.2619 0.2908 0.3227 0.3578 0.3963
-25 24 23 22 21	0.4800 0.5303 0.5854 0.6456 0.7115	0.4752 0.5251 0.5796 0.6393 0.7046	0.4705 0.5199 0.5739 0.6331 0.6978	0.51	47 0.50 83 0.56 70 0.62	96 28 09	0.4565 0.5046 0.5572 0.6148 0.6778	0.4996 0.5517 0.6088	0.4474 0.4946 0.5463 0.6029 0.6648	0.4897 0.5409 0.5970	0.4385 0.4848 0.5356 0.5912 0.6519
-20 19 18 17 16	0.7834 0.8618 0.9474 1.0406 1.1421	0.7759 0.8537 0.9385 1.0309 1.1316	0.7685 0.8456 0.9297 1.0213 1.1211	0.76 0.83 0.920 1.01	76 0.82 09 0.91 18 1.00	96 0 23 0 24 0	0.7466 0.8217 0.9037 0.9930 1.0903	0.8139	0.7324 0.8062 0.8867 0.9745 1.0702		0.7184 0.7909 0.8701 0.9563 1.0504
-15 14 13 12 11	1.2525 1.3726 1.5029 1.6444 1.7979	1.2411 1.3601 1.4894 1.6297 1.7820	1.2297 1.3477 1.4759 1.6151 1.7662	1.21 1.33 1.46 1.60 1.75	55 1.32 26 1.44 07 1.58	33 95 64	1.1962 1.3113 1.4364 1.5722 1.7196	1.2993 1.4234 1.5581	1.1743 1.2875 1.4105 1.5441 1.6892	1.1635 1.2757 1.3978 1.5302 1.6741	1.1527 1.2641 1.3851 1.5165 1.6592
—10 9 8 7 6	1.9643 2.1445 2.3395 2.5505 2.7785	1.9470 2.1258 2.3193 2.5287 2.7549	1.9299 2.1073 2.2993 2.5070 2.7315	1.91 2.08 2.27 2.48 2.70	89 2.07 94 2.25 55 2.46	07 2 96 2 42 2	1.8794 2.0526 2.2401 2.4430 2.6623		1.8464 2.0168 2.2014 2.4011 2.6171	1.8301 1.9992 2.1823 2.3804 2.5947	1.8139 1.9817 2.1633 2.3599 2.5725
- 5 4 3 2 1	3.0248 3.2907 3.5775 3.8868 4.2199	2.9993 3.2632 3.5479 3.8548 4.1854	2.9740 3.2359 3.5184 3.8230 4.1513	2.94 3.20 3.48 3.79 4.11	88 3.18 92 3.46 16 3.76	19 02 03	2.8993 3.1552 3.4314 3.7292 4.0502	2.8747 3.1287 3.4028 3.6985 4.0171	2.8504 3.1025 3.3745 3.6678 3.9841	2.8262 3.0764 3.3463 3.6375 3.9515	2.8023 3.0505 3.3184 3.6074 3.9190
<u> </u>	4.5802	4.5428	4.5057	4.46	90 4.43	25	4.3962	4.3604	4.3248	4.2896	4.2546

TABLE 77.

PRESSURE OF AQUEOUS VAPOR OVER WATER. METRIC MEASURES.

				IVICI	RIC ME	45UKES.				
Tem- pera- ture.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
C.	mm.	mm.	mm,	mm.	mm,	mm.	mm.	mm.	mm.	mm.
0°	4.580	4.614	4.647	4.681	4.715	4.750	4.784	4.810	4.854	4.889
I	4.924	4.060	4.996	5.032	5.068	5.105	5.142	5.179	5.216	5.254
2	5.201	5.329	5.368	5.406	5.445	5.484	5.523	5.562	5.602	5.642
3	5.682	5.723	5.763	5.804	5.846	5.887	5.929	5.071	6.013	6.056
4	6.098	6.141	6.185	6.228	6.272	6.316	6.361	6.406	6.450	6.496
II T	11190		1	0,220	0.272	0.520	0.301	0.400	0.430	0.490
5	6.541	6.587	6.633	6.680	6.726	6.773	6.820	6.868	6.916	6.964
6	7.012	7.061	7.110	7.150	7.200	7.259	7.300	7.360	7.410	7.462
7	7.513	7.565	7.617	7.669	7.722	7.775	7.828	7.882	7.936	7.001
7 8	8.045	8.100	8.156	8.211	8.267	8.324	8.380	8.437	8.404	8.552
9	8.610	8.669	8.727	8.786	8.846	8.906	8.966	9.026	9.087	9.148
	1									
10	9.210	9.272	9.334	9.397	9.460	9.523	9.587	9.651	9.716	9.781
II	9.846	9.912	9.978	10.044	10.111	10.178	10.246	10.314	10.382	10.451
I 2	10.521	10.590	10.660	10.731	10.801	10.873	10.044	11.016	11.080	11.162
13	11.235	11.300	11.383	11.458	11.533	11.608	11.684	11.761	11.837	11.915
14	11.992	12.070	12.149	12.228	12.307	12.387	12.468	12.549	12.630	12.712
15	12.794	12.877	12.960	13.043	13.127	13.212	13.207	13.383	13.460	13.555
16	13.642	13.720	13.817	13.006	13.995	14.084	14.174	14.265	14.356	14.447
17	14.539	14.632	14.725	14.818	14.012	15.007	15.102	15.197	15.203	15.390
18	15.487	15.585	15.683	15.782	15.882	15.981	16.082	16.183	16.285	16.387
19	16.489	16.593	16.696	16.801	16.906	17.011	17.117	17.224	17.331	17.439
00	T = 1.0		66	0	0-	=0 ===	-0	-0	-0	-0
20	17.548	17.657	17.766	17.877	17.987	18.000	18.211	18.323	18.437	18.551
21	18.665	18.780	18.896	19.012	19.129	19.247	10.365	19.484	19.603	10.723
22	21.087	19.965	,	21.473	20.333	20.457	20.582	20.707	20.833	20,960
23	22.308	22.533	21.344	22.805	21.604	21.734	23.210	23.358	22.131	22,264
2.4	22.390	22.333	22.009	22.003	22.942	23.000	23.219	23.330	23.490	23.030
25	23.780	23.022	24.065	24.200	24.353	24.498	24.644	24.701	24.938	25.086
26	25.235	25.385	25.535	25.687	25.839	25.001	26.145	26.200	26.455	26.610
27	26.767	26.925	27.083	27.242	27.402	27.563	27.725	27.887	28.051	28.215
28	28.380	28.546	28.712	28.880	29.048	29.217	29.387	29.558	29.730	29.903
29	30.076	30.251	30.426	30.602	30.779	30.957	31.136	31.315	31.496	31.678
	96-		0			0.0		6		
30	31.860	32.043	32.228	32.413	32.599	32.786	32.974	33.163	33.353	33.543
31	33.735	33.928	34.121	34.316	34.512	34.708	34.906	35.104	35.303	35.504
32	35.705	35.908	36.111	36.315	36.521	36.727	36.935	37.143	37.353	37.563
33	37.775	37.987	38.201	38.415 40.610	38.631 40.846	38.848	39.065	39.284	39.504	39.725
34	39.947	40.170	40.394	40.019	40.040	41.073	41.302	41.531	41.762	41.994
35	42.227	42.461	42.696	42.932	43.170	43.408	43.648	43.889	44.131	44.374
36	44.619	44.864	45.111	45.358	45.608	45.858	46.100	46.362	46.615	46.870
37	47.127	47.384	47.643	47.902	48.163	48.426	48.689	48.954	49.220	49.487
38	49.756	50.025	50.296	50.569	50.842	51.117	51.393	51.670	51.949	52.229
39	52.510	52.793	53.077	53.362	53.649	53-937	54.226	54.516	54.808	55.101
10	FF 206	== 600	55.080	56 agg	-6 -88	56.88o	E77 702	FF 106	En 802	~8 TOO
40	55.396	55.692	55.989 59.038	56.288	56.588 59.665	50.081	57.102 60.208	57.496 60.616	57.80 <i>2</i> 60.036	58.109
41	58.417	58.727		59.351	62.886	63.216		63.880		61.257
42	64.889	65.228	62.230	62.557 65.911	66.255	66.600	63.547 66.947	67.295	64.215	64.551
43	68.350	68.704	69.061	69.419	69.778	70.139	70.502	70.866	71.232	71.599
44		00.704	9.001	9.4.4	-9.77	7-1139	7 5 - 2	75.500	72.232	7399
45	71.968	72.339	72.712	73.086	73.461	73.839	74.218	74.598	74.981	75.365
46	75.751	76.138	76.527	76.918	77.311	77.705	78.101	78.499	78.898	79.300
47	79.703	80.107	80.514	80.922	81.332	81.744	82.158	82.573	82.990	83.409
48	83.830	84.253	84.677	85.104	85.532	85.962	86.304	86.828	87.263	87.701
49	88.140	88.581	80.024	89.470	89.916	90.365	90.816	91.269	91.723	92.180
50	92.639	93.099	93.562	94.026	94.492	94.961	95.431	95.903	96.378	96.854
50	92.039	93.099	93.302	94.020	94.492	94.901	93,431	93.903	90.370	90.034

PRESSURE OF AQUEOUS VAPOR OVER WATER.

METRIC MEASURES.

Tem- pera- ture.	.0	-1	.2	.3	.4	.5	.6	.7	.8	.9
C.	mm,	mm.	mm,	mm.	mm.	mm,	mm.	mm.	mm.	mm.
50°	92.64	93.10	93.56	94.03	94.49	94.96	95.43	95.90	96.38	96.85
51	97.33	97.81	98.30	98.78	99.27	99.76	100.25	100.74	101.23	101.73
52	102.23	102.73	103.23	103.74	104.25	104.75	105.27	105.78	106.30	106.81
53	107.33	107.86	108.38	108.91	109.44	100.07	110.50	111.04	111.57	112.11
54	112.66	113.20	113.75	114.30	114.85	115.40	115.96	116.51	117.07	117.64
55	118.20	118.77	119.34	119.91	120.40	121.06	121.64	122.22	122.81	123.39
56	123.98	124.57	125.16	125.76	126.36	126.96	127.56	128.17	128.77	129.38
57	130.00	130.61	131.23	131.85	132.47	133.10	133.73	134.36	134.99	135.62
58	136.26	136.90	137.54	138.19	138.84	139.49	140.14	140.80	141.46	142.12
59	142.78	143.45	144.12	144.79	145.46	146.14	146.82	147.50	148.19	148.88
60	140.57	150.26	150.95	151.65	152.35	153.06	153.77	154.48	155.10	155.90
бі	156.62	157.34	158.07	158.79	159.52	160.26	160.00	161.73	162.47	163.21
62	163.96	164.71	165.46	166.22	166.98	167.74	168.50	169.27	170.04	170.81
63	171.50	172.37	173.15	173.93	174.72	175.51	176.31	177.10	177.91	178.71
64	179.52	180.32	181.14	181.95	182.77	183.50	184.42	185.25	186.08	186.91
	, , , , ,				/ '	0.09				
65	187.75	188.59	189.44	190.28	191.13	191.99	192.85	193.71	194.57	195.44
66	196.31	197.18	198.06	198.94	199.82	200.71	201.60	202.49	203.39	204.29
67	205.19	206.10	207.01	207.92	208.84	209.76	210.68	211.61	212.54	213.47
68	214.41	215.35	216.30	217.24	218.20	219.15	220.11	221.07	222.04	223.01
69	223.98	224.96	225.94	226.92	227.91	228.90	229.89	230.89	231.89	232.90
70				226.26	227.00	200.07	240.04	241.08	242.12	242.76
70	233.91	234.92	235.94	236.96	237.98	239.01	240.04	251.64	252.72	243.16 253.80
71 72	244.21 254.88	245.26 255.97	246.31 257.07	258.16	250.27	260.37	261.48	262.50	263.71	264.83
	265.96	255.97	268.22	269.35	270.50	271.64	272.79	273.94	275.10	276.26
73 74	277.43	278.60	279.77	280.95	282.13	283.32	284.51	285.71	286.90	288.11
/4	211.43	270.00	219.11	200.93	202.13	203.32	204.31	203.71	200.90	200.11
75	280.32	290.53	291.74	292.97	294.19	295.42	296.65	297.89	299.13	300.38
76	301.63	302.89	304.15	305.41	306.68	307.95	309.23	310.51	311.80	313.00
77	314.38	315.68	316.99	318.30	319.61	320.93	322.25	323.58	324.91	326.25
78	327.59	328.93	330.28	331.64	333.00	334.36	335.73	337.10	338 48	339.86
79	341.25	342.65	344.04	345.44	346.85	348.26	349.68	351.10	352.53	353.96
00			0 0			.6.6.	-6	-60	-66	-60 -
80	355.40	356.84	358.28	359.73	361.19	362.65	364.11	365.58	367.06	368.54
81	370.03	371.52	373.01	374.51	376.02	377.53	379.05	380.57	382.09	383.62
82	385.16	386.70	388.25	389.80	391.36	392.92	394.49	396.06	397.64	399.22
83	400.81	402.40	404.00	405.61	407.22	408.83	410.45	412.08	413.71	415.35
84	416.99	418.64	420.29	421.95	423.61	425.28	426.95	420.04	430.32	432.01
85	433.71	435.41	437.12	438.83	440.55	442.28	444.01	445.75	447.49	449.24
86	450.00	452.75	454.51	456.28	458.06	459.84	461.63	463.42	465.22	467.03
87	468.84	470.66	472.48	474.31	476.14	477.99	479.83	481.68	483.54	485.41
88	487.28	489.16	491.04	492.93	494.82	496.72	498.63	500.54	502.46	504.39
89	506.32	508.26	510.20	512.15	514.11	516.07	518.04	520.01	521.99	523.98
90	525.97	527.97	529.98	531.99	534.01	536.04	538.07	540.11	542.15	544.21
91	546.26	548.33	550.40	552.48	554.56	556.65	558.75	560.85	562.96	565.08
92	567.20	569.33	571.47	573.61	575.76	577.92	580.08	582.25	584.43	586.61
93	588.80	591.00	593.20	595.41	597.63	599.86	602.09	604.33	606.57	608.82
94	611.08	613.35	615.62	617.90	620.19	622.48	624.79	627.09	629.41	631.73
95	634.06	636.40	638.74	641.00	643.45	645.82	648.19	650.57	652.96	655.35
96	657.75	660.16	662.58	665.00	667.43	669.87	672.32	674.77	677.23	679.70
97	682.18	684.66	687.15	689.65	602.15	694.67	697.19	699.71	702.25	704.79
98	707.35	709.90	712.47	715.04	717.63	720.22	722.81	725.42	728.03	730.65
99	733.28	735.92	738.56	741.21	743.87	746.54	749.22	751.90	754.59	757.29
1	1	, 03)			,					
100	760.00	762.72	765.44	768.17	770.91	773.66	776.42	779.18	781.95	784.73
	I			1	1		!			

TABLE 77.

PRESSURE OF AQUEOUS VAPOR OVER WATER. METRIC MEASURES.

Temperature.	O°	1°	2 °	3°	4°	5°	6°	7 °	8°	9°
G.	mm.	mm.	mm,	mm.	mm.	mm.	mm.	mm,	mm.	mm.
100°	760.0	787.5	815.0	845.0	875.1	906.0	937.8	970.5	1004.2	1038.8
110	1074.4	1111.0	1148.6	1187.2	1226.9	1267.7	1309.6		1396.8	1442.1
120	1488.7	1536.4	1585.4	1635.7	1687.3	1740.2	1704.4		1907.0	1965.4
130	2025.2	2086.5	2149.3	2213.7	2279.6	2347.0	2416. I	2486.8	2559.2	2633.2
140	2709.0	2786.5	2865.8	2947.0	3029.9	3114.7	3201.4	3290. 1	3380.7	3473 - 3
150°	3507.9	3664.6	3763.3	3864.2	3967.2	4072.4	4179.8	4289.5	4401.5	4515.7
160	4632.4	4751.4	4872.8	4996.7		5252.0	5383.4	5517.5	5654.2	5793.5
170	5935.6	6080.4	6228.0	6378.4	6531.7		6846.9	7009.0	7174.0	7342. I
180	7513.3	7687.7	7865.2	8045.9	8229.8		8607.6	8801.5	8998.9	9199.6
100	13-3.3	1001.1	73	40.9		' '				111
190°	9404	9612	0823	10038	10257	10479	10705	10935	11169	11407
200	11648	11894	12143	12397	12654	12916	13182	13452	13727	14006
210	14289	14577	14860	15165	15467	15772	16083	16398	16718	17043
220	17372	17707	18046	18391	18740	19095	19454	19819	20190	20565
									•	
230°	20946	21332	21724	22121	22524	22932	23347	23766	24192	24623
240	25061	25504	25953	26408	26870	27337	27811	28291	28778	29270
250	29770	30275	30787	31306	31832		32903	33449	34002	34562
260	35128	35702	36283	36872	37467	38070	38680	39298	39923	40556
270	41197	41845	42501	43165	43836	44516	45204	45899	46603	47316
280°	48036	48765	49593	50248	51003	51766	52538	53318	54108	54906
290	55714	56530	57356	58191	59035	59888	60751	61624	62506	63398
300	64200	65211	66132	67063	68005	68956	69918	70890	71872	72865
310	73869	74883	75907	76943	77990	79047	80116	81195	82286	83389
320	84503	85628	86765	87913	89074	90246	91430	92626	93835	95056
330°	g628g	97534	98793	100060	101350	102640	103050	105280	106610	107960
340		110700	112000		114910		117780		120720	122210
350	123710	125220	126760	128310	120870		133030		136270	137000
360	130560	-	142020	144620		148070	149820		153380	155180
370		158840		162560	164450		1			
1			-		1					

SMITHSONIAN TABLES.

PRESSURE OF AQUEOUS VAPOR OVER ICE.

DYNAMIC MEASURES

Temp.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
C.	mb.									
—70°	0.0026	0.0025	0.0025	0.0025	0.0024	0.0024	0.0024	0.0023	0.0023	0.0023
-69	0.0030	0.0029	0.0029	0.0029	0.0028	0.0028	0.0027	0.0027	0.0027	0.0026
-68	0.0035	0.0034	0.0034	0.0033	0.0033	0.0032	0.0032	0.0031	0.0031	0.0030
67	0.0040	0.0040	0.0039	0.0038	0.0038	0.0037	0.0037	0.0036	0.0036	0.0035
66	0.0046	0.0046	0.0045	0.0044	0.0044	0.0043	0.0043	0.0042	0.0041	0.0041
65	0.0054	0.0053	0.0052	0.0051	0.0051	0.0050	0.0049	0.0048	0.0048	0.0047
64	0.0062	0.0061	0.0060	0.0059	0.0058	0.0057	0.0057	0.0056	0.0055	0.0054
63	0.0071	0.0070	0.0069	0.0068	0.0067	0.0066	0.0065	0.0064	0.0063	0.0063
62	0.0082	0.0080	0.0079	0.0078	0.0077	0.0076	0.0075	0.0074	0.0073	0.0072
<u>61</u>	0.0094	0.0092	0.0091	0.0090	0.0089	0.0087	0.0086	0.0085	0.0084	0.0083
60	0.011	0.011	0.010	0.010	0.010	0.010	0.0099	0.0097	0.0096	0.0095
— 59	0.012	0.012	0.012	0.012	0.012	0.011	0.011	0.011	0.011	0.011
-58	0.014	0.014	0.014	0.013	0.013	0.013	0.013	0.013	0.013	0.012
-57	0.016	0.016	0.016	0.015	0.015	0.015	0.015	0.015	0.014	0.014
— 56	0.018	0.018	0.018	0.018	0.017	0.017	0.017	0.017	0.016	0.016
55	0.021	0.021	0.020	0.020	0.020	0.020	0.019	0.019	0.019	0.019
	0.024	0.023	0.023	0.023	0.022	0.022	0.022	0.022	0.021	0.021
-53	0.027	0.027	0.026	0.026	0.026	0.025	0.025	0.025	0.024	0.024
	0.031	0.030	0.030	0.029	0.029	0.029	0.028	0.028	0.028	0.027
<u>—51</u>	0.035	0.034	0.034	0.033	0.033	0.033	0.032	0.032	0.031	0.031
-50	0.039	0.039	0.038	0.038	0.037	0.037	0.036	0.036	0.036	0.035
-49	0.044	0.043	0.043	0.042	0.042	0.041	0.041	0.040	0.040	0.039
- 48	0.050	0.049	0.049	0.048	0.047	0.047	0.046	0.046	0.045	0.044
-47	0.056	0.055	0.055	0.054	0.053	0.053	0.052	0.052	0.051	0.050
	0.063	0.063	0.062	0.061	0.060	0.060	0.059	0.058	0.058	0.057
45	0.072	0.071	0.070	0.069	0.068	0.067	0.067	0.066	0.065	0.064
44	0.081	0.080	0.079	0.078	0.077	0.076	0.075	0.074	0.073	0.072
43	0.091	0.090	0.089	0.088	0.087	0.086	0.085	0.084	0.083	0.082
12	0.102	0.101	0.100	0.098	0.097	0.096	0.095	0.094	0.093	0.092
-41	0.115	0.113	0.112	0.111	0.109	0.108	0.107	0.106	0.104	0.103
<u>-40</u>	0.129	0.127	0.126	0.124	0.123	0.121	0.120	0.119	0.117	0.116
—39	0.144	0.142	0.141	0.139	0.138	0.136	0.134	0.133	0.132	0.130
— 38	0.161	0.159	0.158	0.156	0.154	0.152	0.151	0.149	0.147	0.146
-37	0.180	0.178	0.176	0.174	0.172	0.171	0.169	0.167	0.165	0.163
— 36	0.201	0.199	0.197	0.195	0.193	0.191	0.189	0.186	0.184	0.182

PRESSURE OF AQUEOUS VAPOR OVER ICE.

DYNAMIC MEASURES

	1	1		1	1		1	ı	1	
Temp.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
C.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.	mb.
 −35°	0.225	0.222	0.220	0.218	0.215	0.213	0.211	0.208	0.206	0.204
-34 -33	0.251	0.248	0.245	0.243	0.240	0.237	0.235	0.232	0.230	0.227
-32	0.311	0.307	0.304	0.301	0.298	0.295	0.291	0.288	0.285	0.282
-31	0.345	0.342	0.338	0.335	0.331	0.328	0.324	0.321	0.317	0.314
30	0.384	0.380	0.376	0.372	0.368	0.364	0.360	0.357	0.353	0.349
-29	0.426	0.421	0.417	0.413	0.408	0.404	0.400	0.396	0.392	0.388
-28 -27	0.472 0.523	0.467	0.462	0.458	0.453	0.448	0.444	0.439	0.435	0.430
-26	0.579	0.573	0.567	0.561	0.556	0.550	0.545	0.539	0.534	0.528
25	0.640	0.634	0.627	0.621	0.615	0.609	0.602	0.596	0.590	0.585
-24	0.707	0.700	0.693	0.686	0.679	0.673	0.666	0.659	0.653	0.646
-23	0.780	0.773	0.765	0.758	0.750	0.743	0.736	0.728	0.721	0.714 0.788
—22 —2I	0.861	0.852	0.844	0.836	0.828	0.820	0.812	0.804 0.886	0.796 0.878	0.700
		, , ,				, ,			, i	
—20 —19	1.04	1.03	1.02	1.0I 1.12	1.00	1.10	0.986	0.976 1.07	0.967 1.06	0.958 1.05
—19 —18	1.15 1.26	I.14 I.25	I.13 I.24	1.12	1.11	1.10	1.19	1.18	1.17	1.16
-17	1.39	1.37	1.36	1.35	1.34	1.32	1.31	1.30	1.29	1.27
16	1.52	1.51	1.49	1.48	1.47	1.45	1.44	1.43	1.41	1.40
15	1.67	1.65	1.64	1.62	1.61	1.59	1.58	1.57	1.55	1.54
-14	1.83	1.81	1.80	1.78	1.76	1.75	1.73	1.72 1.88	1.70 1.86	1.69
—13 —12	2.00	1.99 2.17	1.97 2.15	1.95 2.13	1.93	1.92	1.90 2.08	2.06	2.04	2.02
-11	2.40	2.38	2.35	2.33	2.31	2.29	2.27	2.25	2.23	2.21
10	2.62	2.60	2.57	2.55	2.53	2.51	2.48	2.46	2.44	2.42
- 9	2.86	2.83	2.81	2.78	2.76	2.74	2.71	2.69	2.67	2.64
— 8	3.12	3.09	3.07	3.04	3.01	2.99	2.96	2.93	2.91	2.88
$\begin{bmatrix} -7 \\ -6 \end{bmatrix}$	3.40	3.37	3.34	3.31 3.61	3.29 3.58	3.26	3.23 3.52	3.20 3.49	3.17 3.46	3.15
	3.70	3.67	3.64			3.55				
— 5	4.03	4.00	3.97	3.93	3.90	3.87	3.83	3.80	3.77	3.74
— 4 — 3	4.39	4·35 4·73	4.31 4.69	4.28 4.65	4.24 4.61	4.21 4.58	4.17 4.54	4.14 4.50	4.10 4.46	4.07 4.42
— 3 — 2	4.77 5.18	5.14	5.10	5.06	5.01	4.97	4.93	4.89	4.85	4.81
— 1	5.63	5.58	5.53	5.49	5.44	5.40	5.36	5.31	5.27	5.23
- 0	6.11	6.06	6.01	5.96	5.91	5.86	5.81	5.77	5.72	5.67
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PRESSURE OF AQUEOUS VAPOR OVER WATER.

DYNAMIC MEASURES

				,	,		-			
Temp.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
C. 0° 1 2 3	mb. 6.11 6.56 7.05 7.58	mb. 6.15 6.61 7.10 7.63	mb. 6.20 6.66 7.16 7.68	mb. 6.24 6.71 7.21 7.74	mb. 6.29 6.76 7.26 7.79	mb. 6.33 6.81 7.31 7.85	mb. 6.38 6.86 7.36 7.90	mb. 6.42 6.90 7.42 7.96	mb. 6.47 6.95 7.47 8.02	mb. 6.52 7.00 7.52 8.07
5 6 7 8 9	8.13 8.72 9.35 10.02 10.73 11.48	8.19 8.78 9.41 10.09 10.80 11.56	8.25 8.84 9.48 10.16 10.87 11.64	8.30 8.91 9.54 10.22 10.95 11.71	8.36 8.97 9.61 10.30 11.02 11.79	9.03 9.68 10.37 11.10 11.87	9.09 9.74 10.44 11.17 11.95	9.16 9.81 10.51 11.25 12.03	9.22 9.88 10.58 11.32 12.12	8.66 9.28 9.95 10.65 11.40 12.20
10	12.28	12.36	12.44	12.53	12.61	12.70	12.78	12.87	12.95	13.04
11	13.13	13.21	13.30	13.39	13.48	13.57	13.66	13.75	13.84	13.93
12	14.03	14.12	14.21	14.31	14.40	14.50	14.59	14.69	14.78	14.88
13	14.98	15.08	15.18	15.28	15.38	15.48	15.58	15.68	15.78	15.89
14	15.99	16.09	16.20	16.30	16.41	16.51	16.62	16.73	16.84	16.95
15	17.06	17.17	17.28	17.39	17.50	17.61	17.73	17.84	17.96	18.07
16	18.19	18.30	18.42	18.54	18.66	18.78	18.90	19.02	19.14	19.26
17	19.38	19.51	19.63	19.76	19.88	20.01	20.13	20.26	20.39	20.52
18	20.65	20.78	20.91	21.04	21.17	21.31	21.44	21.58	21.71	21.85
19	21.98	22.12	22.26	22.40	22.54	22.68	22.82	22.96	23.11	23.25
20	23.40	23.54	23.69	23.83	23.98	24.13	24.28	24.43	24.58	24.73
21	24.88	25.04	25.19	25.35	25.50	25.66	25.82	25.98	26.14	26.30
22	26.46	26.62	26.78	26.94	27.11	27.27	27.44	27.61	27.78	27.94
23	28.11	28.28	28.46	28.63	28.80	28.98	29.15	29.33	29.51	29.68
24	29.86	30.04	30.22	30.40	30.59	30.77	30.96	31.14	31.33	31.51
25	31.70	31.89	32.08	32.28	32.47	32.66	32.86	33.05	33.25	33.45
26	33.64	33.84	34.04	34.25	34.45	34.65	34.86	35.06	35.27	35.48
27	35.69	35.90	36.11	36.32	36.53	36.75	36.96	37.18	37.40	37.62
28	37.84	38.06	38.28	38.50	38.73	38.95	39.18	39.41	39.64	39.87
29	40.10	40.33	40.56	40.80	41.04	41.27	41.51	41.75	41.99	42.23
30	42.48	42.72	42.97	43.21	43.46	43.71	43.96	44.21	44.47	44.72
31	44.98	45.23	45.49	45.75	46.01	46.27	46.54	46.80	47.07	47.33
32	47.60	47.87	48.14	48.42	48.69	48.97	49.24	49.52	49.80	50.08
33	50.36	50.65	50.93	51.22	51.50	51.79	52.08	52.37	52.67	52.96
34	53.26	53.56	53.85	54.15	54.46	54.76	55.06	55.37	55.68	55.99
35	56.30	56.61	56.92	57.24	57.56	57.87	58.19	58.51	58.84	59.16
36	59.49	59.81	60.14	60.47	60.81	61.14	61.47	61.81	62.15	62.49
37	62.83	63.17	63.52	63.86	64.21	64.56	64.91	65.27	65.62	65.98
38	66.34	66.69	67.06	67.42	67.78	68.15	68.52	68.89	69.26	69.63
39	70.01	70.38	70.76	71.14	71.53	71.91	72.30	72.68	73.07	73.46
40	73.86	74.25	74.65	75.04	75.44	75.85	76.25	76.66	77.06	77.47
41	77.88	78.30	78.71	79.13	79.55	79.97	80.39	80.81	81.24	81.67
42	82.10	82.53	82.97	83.40	83.84	84.28	84.72	85.17	85.61	86.06
43	86.51	86.96	87.42	87.87	88.33	88.79	89.26	89.72	90.19	90.66
44	91.13	91.60	92.07	92.55	93.03	93.51	93.99	94.48	94.97	95.46

TABLE 80.

WEICHT OF A CUBIC FOOT OF SATURATED VAPOR. ENGLISH MEASURES.

						LASURE		,		
Temper- ature.		Temper- ature.	.0	.5	Tempera- ature.	.0	.2	.4	.6	.8
F.	Grains	F.	Grains	Grains	F.	Grains	Grains	Grains	Grains	Grains
-30°	0.095	+20°	1.244	1.273	+70°	8.066	8.117	8.170	8.223	8.276
29	0.100	21	1.301	1.332	7 I	8.329	8.383	8.437	8.491	8.546
28	0.106	22	1.362	1.393	72	8.600	8.656	8.711	8.766	8.823
27	0.112	23	1.425	1.457	73	8.879	8.936	8.992	9.050	9.107
26	0.119	24	1.490	1.524	7-1	9.165	9.223	9.281	9.341	9.400
-25	0.126	+25	1.558	1.593	+75	9.460	0.519	9.579	9.640	9.700
24	0.134	26	1.629	1.666	76	9.761	9.823	9.885	9.947	10.009
23	0.141	27 28	1.703	1.741	77	10.072	10.135	10.199	10.263	10.327
21	0.150	20	1.779 1.859	1.819	78	10.302	10.457	10.521	10.587	10.653
			1.059	1.900	79	10.720	10.765	10.853	10.921	10.987
-20	0.167	+30	1.942	1.984	+80	11.056	11.124	11.193	11.262	11.331
19	0.176	31	2.028	2.072	81	11.401	11.471	11.542	11.613	11.685
18	0.187	32	2.118	2.159	82	11.756	11.828	11.000	11.974	12.047
17	0.197	33	2,200	2,242	83	12.121	12.195	12.269	12.344	12.419
10	0.208	34	2.286	2.330	84	12.494	12.570	12,646	12.723	12.800
-15	0.220	+35	2.375	2.420	+85	12.878	12.956	13.034	13.113	13.192
14	0.232	36	2.466	2.513	86	13.272	13.351	13.432	13.512	13.594
13	0.244	37	2.560	2.609	87	13.676	13.758	13.840	13.923	14.006
I 2	0.258	38	2.658	2.708	88	14.090	14.174	14.258	14.344	14.429
II	0.272	39	2.759	2.810	89	14.515	14.601	14.689	14.776	14.864
-10	0.286	+40	2.863	2.916	+90	14.951	15.040	15.120	15.219	15.309
9	0.302	41	2.970	3.026	91	15.400	15.490	15.581	15.673	15.766
8	0.318	42	3.082	3.138	92	15.858	15.951	16.045	16.139	16.234
7 6	0.335	43	3.196	3.254	93	16.328	16.423	16.520	16.616	16.713
6	0.353	44	3.315	3-374	94	16.810	16.909	17.007	17.106	17.205
- 5	0.371	+45	3.436	3.499	+95	17.305	17.406	17.506	17.607	17.709
4	0.301	46	3.563	3.627	96	17.812	17.914	18.018	18.121	18.226
3	0.411	47	3.693	3.759	97	18.330	18.436	18.542	18.648	18.755
2	0.433	48	3.828	3.895	98	18.863	18.971	19.079	19.188	19.298
- I	0.455	49	3.965	4.036	99	19.407	19.518	19.629	19.741	19.853
± 0	0.479	+50	4.108	4.181	+100	19.966	20.079	20.193	20,307	20.422
+ 1	0.503	51	4.255	4.331	101	20.538	20.654	20.770	20.887	21.005
2	0.529	52	4.407	4.485	102	21.123	21.242	21.362	21.481	21.602
3	0.556	53	4.564	4.644	103	21.723	21.845	21.967	22.000	22.213
4	0.584	54	4.725	4.807	104	22.337	22.462	22.588	22.714	22.839
5	0.613	+55	4.891	4.976	+105	22.966	23.095	23.223	23.351	23.481
6	0.644	56	5.062	5.149	106	23.611	23.742	23.873	24.005	24.138
7 8	0.676	57	5.238	5.328	107	24.271	24.405	24.539	24.673	24.809
1 1	0.709	58	5.420	5.513	108	24.946	25.082	25.220	25.358	25.497
9	0.744	59	5.607	5.703	109	25.636	25.776	25.917	26.058	26.201
10	0.780	+60	5.800	5.899	+110	26.343	25.486	26.630	26.775	26.920
II	0.818	61	5.999	6.099	III	27.066	27.213	27.360	27.508	27.657
12	0.858	62	6.203	6.306	112	27.807	27.956	28.107	28.259	28.411
13	0.900	63	6.413	6.521	113	28.563	28.717	28.871	29.026	29.181
1.1	0.943	64	6.630	6.740	114	29.338	29.495	29.653	29.812	29.970
15	0.988	+65	6.852	6.966	+ 115	30.130	30.291	30.452	30.614	30.777
16	1.035	66	7.082	7.198	116	30.940	31.104	31.270	31.435	31.601
17	1.084	67	7.317	7.437	117	31.768	31.937	32.106	32.274	32.445
+10	1.135	68 +69	7.560 7.809	7.683	118	32.616	32.787	32.960	33.133	33.307
10	1.100	700	7.009	7.937	+110	33.482	33.657	33.834	34.010	34.189

WEIGHT OF A CUBIC METER OF SATURATED VAPOR OVER ICE.

METRIC MEASURES

Temper	a-	Temp			mpera-			Tempera-		Tempera- ture	
C70° 69 68 67 66 -65° 64 63 62 61	0.003 0.003 0.004 0.004	s C. 88 —66 2 55 55 56 —55 4 55 4	gra 0° 0.00 9 0.00 8 0.00 7 0.00 6 0.00 5° 0.00 4 0.00 3 0.00 2 0.00	ms 109 —5 124 142 161 183 207 —4 234 265 300	C. 50°.0 49.5 49.0 48.5 48.0 17°.5 47.0 46.5 46.0 45.5	0.0 0.0 0.0 0.0 0.0 0.0	ams 0381 0398 0424 0451 0479 0508 0538 0572 0606 0643	C45°.0 44.5 44.0 43.5 43.0 -42°.5 42.0 41.5 41.0 40.5	grams 0.0681 0.0721 0.0763 0.0808 0.0854 0.0904 0.0957 0.101 0.107 0.113	C40°.0 39.5 39.0 38.5 38.0 -37°.5 37.0 36.5 36.0 35.5	grams 0.120 0.126 0.133 0.141 0.149 0.157 0.166 0.175 0.184 0.194
Temp.	.0	.1	.2	.3	.4		.5	.6	.7	.8	.9
C. -35° 34 33 32 31	grams 0.205 0.227 0.252 0.280 0.309	grams 0.203 0.225 0.250 0.277 0.306	grams 0.200 0.223 0.247 0.274 0.303	grams 0.198 0.220 0.244 0.271 0.300	gran 0.19 0.21 0.24 0.26 0.29)6 18 12 58	grams 0.194 0.216 0.239 0.265 0.294	0.192 0.214 0.237 0.263	0.190 0.211 0.234 0.260	grams 0.188 0.209 0.232 0.258 0.285	grams 0.186 0.207 0.230 0.255 0.282
-30° 29 28 27 26	0.342 0.378 0.418 0.461 0.508	0.339 0.374 0.414 0.456 0.503	0.335 0.371 0.410 0.452 0.498	0.332 0.367 0.405 0.447 0.493	0.32 0.36 0.40 0.44 0.48)4)1 3	0.325 0.360 0.398 0.439 0.484	0.356 0.394 0.434	0.353 0.390 0.430	0.316 0.349 0.386 0.426 0.470	0.313 0.346 0.382 0.422 0.465
-25° 24 23 22 21	0.559 0.615 0.677 0.743 0.816	0.554 0.610 0.670 0.736 0.808	0.549 0.604 0.664 0.729 0.801	0.543 0.598 0.658 0.723 0.793	0.53 0.59 0.65 0.71 0.78	12 132 16 16 16	0.533 0.587 0.645 0.709 0.779	0.581 0.639 0.702 0.772	0.576 0.633 0.696 0.764	0.518 0.570 0.627 0.689 0.757	0.513 0.565 0.621 0.683 0.750
-20° 19 18 17 16	0.894 0.980 1.073 1.174 1.284	0.886 0.972 1.064 1.164 1.273	0.878 0.963 1.054 1.154 1.261	0.870 0.954 1.045 1.143 1.250	0.86 0.94 1.03 1.13 1.23	5 5 3	0.854 0.936 1.026 1.123 1.228	0.928 1.017 1.113	0.920 1.008 1.103	0.831 0.911 0.998 1.093	0.823 0.903 0.989 1.083 1.185
-15° 14 13 12 11	1.403 1.531 1.671 1.820 1.983	1.390 1.518 1.656 1.805 1.966	1.378 1.505 1.641 1.789 1.949	1.366 1.492 1.627 1.774 1.933	1.35 1.47 1.61 1.75 1.91	8 3 9	1.342 1.466 1.599 1.744 1.900	I.453 I.585 I.729	1.440 1.572	1.307 1.428 1.558 1.699 1.852	1.295 1.415 1.545 1.685 1.836
-10° 9 8 7 6	2.158 2.347 2.551 2.770 3.006	2.140 2.327 2.530 2.748 2.982	2.122 2.308 2.509 2.725 2.958	2.104 2.289 2.488 2.703 2.934	2.08 2.27 2.46 2.68 2.91	7 30	2.069 2.251 2.447 2.658 2.886	2.232 2.426 2.636	2.034 2.213 2.406 2.615 2.839	2.016 2.194 2.386 2.593 2.816	2.000 2.176 2.366 2.572 2.793
- 5° 4 3 2 1	3.261 3.534 3.828 4.144 4.482	3.234 3.506 3.798 4.111 4.447	3.208 3.478 3.767 4.078 4.412	3.182 3.450 3.737 4.046 4.378	3.15 3.42 3.70 4.01 4.34	2 8 5	3.131 3.395 3.678 3.983 4.310	3.649 3.951	3.081 3.341 3.620 3.920 4.242	3.056 3.314 3.591 3.889 4.209	3.031 3.287 3.562 3.858 4.176
- 0°	4.847	4.809	4.771	4.734	4.69	7	4.661	4.624	4.588	4.553	4.517

TABLE 81.

WEIGHT OF A CUBIC METER OF SATURATED VAPOR OVER WATER. METRIC MEASURES

Temp.	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
C.	grams									
+ 0°	4.847	4.881	4.914	4.948	4.982	5.017	5.051	5.086	5.121	5.157
I	5.192	5.228	5.264	5.300	5.336		5.410	5.447	5.483	5.521
2	5.559	5.596	5.634 6.028	5.673 6.068	5.711	5.750 6.151	5.789	5.828 6.234	5.868 6.275	5.908
3 4	5.947 6.360	5.988 6.402	6.445	6.488	6.532		6.619	6.664	6.708	6.753
+ 5	6.797	6.842	6.888	6.934	6.979		7.072	7.119	7.166	7.213
6	7.261	7.309	7.357	7.405	7.453	7.502	7.552	7.601	7.651	7.701
7 8	7.751 8.271	7.802 8.324	7.853 8.378	7.904 8.432	7.956 8.487	8.007 8.542	8.059 8.597	8.112	8.164 8.708	8.217 8.764
9	8.821	8.877	8.934	8.991	9.049		0.,.	9.223	9.282	9.341
			,,,,							
+10	9.401	9.461 10.078	9.521 10.142	9.582	9.643 10.270	9.704 10.334	9.765	9.827	9.889 10.530	9.952 10.597
12	10.664	10.730	10.797	10.865	10.932		11.069	11.138	11.208	11.278
13	11.348	11.418	11.489	11.561	11.632	11.704	11.777	11.850	11.922	11.997
14	12.070	12.144	12.219	12.295	12.370	12.446	12.523	12.600	12.677	12.754
+15	12.832	12.911	12.990	13.068	13.148	13.229	13.309	13.390	13.472	13.553
16	13.635	13.718	13.801	13.885	13.969		14.139	14.224	14.309	14.395
17	14.482	14.569	14.657	14.744	14.833	14.922	15.011	15.101	15.191	15.282
18	15.373	15.465	15.557	15.650	15.743		15.931 16.898	16.025	16.121	16.216
19	16.311	16.409	16.505	16.603	16.701	16.799	10.090	10.990	17.097	17.190
+20	17.300	17.401	17.503	17.606	17.708	17.812	17.917	18.021	18.126	18.232
21	18.338	18.445	18.553	18.660	18.768	18.878	18.987	19.097	19.207	19.319
22	19.430	19.542	19.655	19.769	19.882	19.996	20.112	20.227	20.343	20.461
23	20.578	20.695	20.814	20.933	21.053 22.282	21.173	21.295 22.536	21.416	21.538	21.660
24	21.783									
+25 26	23.049	23.179	23.310	23.442	23.573	23.706 25.066	23.839 25.206	23.973	24.107 25.488	24.242
27	24.378 25.771	24.514 25.915	24.651 26.058	24.790 26.203	24.929 26.348	26.494	26.641	25.346 26.787	26.936	27.084
28	27.234	27.384	27.534	27.686	27.837	27.990	28.143	28.298	28.453	28.609
29	28.765	28.923	29.081	29.239	29.399	29.559	29.720	29.881	30.044	30.207
+30	30.371	30.535	30.701	30.867	31.034	31.202	31.371	31.540	31.710	31.880
31	32.052	32.225	32.398	32.572	32.747	32.923	33.100	33.277	33.454	33.633
32	33.812	33.993	34.175	34.356	34.540	34.723	34.909	35.094	35.280	35.467
33	35.656	35.844	36.034	36.224	36.416	36.609	36.801	36.995	37.190	37.386
34	37.583	37.780	37.979	38.178	38.378	38.579	38.782	38.984	39.187	39-395
+35	39.599	39.805	40.013	40.221	40.430	40.640	40.851	41.064	41.277	41.491
36	41.706	41.921	42.139	42.356	42.575	42.795	43.015	43.237	43.459	43.683
37	43.908	44.134	44.360	44.587	44.815	45.046	45.277	45.507	45.740	45.973
38	46.208	46.443	46.680	46.918	47.156 49.600	47.396	47.636	47.878 50.353	48.121 50.606	48.365
39	40.009	48.855	49.103	49.350	49.000	49.050	30.101	30.333	30.000	30.001
+40	51.117	51.373	51.631	51.890	52.150	52.410	52.673	52.936	53.200	53.466

HYGROMETRICAL TABLES.

Reduction of psychrometric observations — English measures.	
Values of $e = e' - 0.000367 B(t - t') \left(1 + \frac{t' - 32}{1571}\right)$.	TABLE 82
Relative humidity — Temperature Fahrenheit	Table 83
Reduction of psychrometric observations — Metric Measures.	
Values of $e = e' - 0.000660 B (t - t') (1 + 0.00115 t')$.	Table 84
Relative humidity — Temperature Centigrade	TABLE 85
Rate of decrease of vapor pressure with altitude	Table 86
Reduction of snowfall measurements.	
Depth of water corresponding to the weight of a cylindrical snow core 2.655 inches in diameter	Table 87
Depth of water corresponding to the weight of snow (or rain) collected in an 8-inch gage	Table 88
Quantity of rainfall corresponding to given depths	Table 89

TABLE 82.

REDUCTION OF PSYCHROMETRIC OBSERVATIONS.

ENGLISH MEASURES.

Values of
$$e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 32}{1571} \right)$$

Pressure of Saturated Aqueous Vapor, e.

	Intersal of Saturated Figure 1, 200													
Tempera- ture.	0	1	2	3	4	5	6	7	8	9				
F.	Inches.	Inches.	Inches.	Inches.	Inches	Inches.	Inches.	Inches.	Inches.	Inches.				
−60° 5°	.0010	.0018	.0017	.0016	.0015	.0014	.0013	.0012	.0011	.0011				
40	38	36	33	31	20	28	26	24	23	21				
30	71	66	62	59	55	52	49	46	43	40				
20	.0127	.0120	.0113	.0107	.0101	.0095	.0090	.0084	.0080	.0075				
			e = e'		= 30.0 i1	1.0	$\frac{t'-32}{1571}$)						
						- t'		_						
<i>t'</i>	.0 .2 .4 .6 .8 1.0 1.2 1.4 1.6 1.8													
	Inches.	Inches,	Inches,	Inches.	Inches,	Inches,	Inches.	Inches.	Inches.	Inches.				
-20°	.0127	.0106	.0085	.0063	.0042	.0021								
19	135	113	92	71	49	28	.0007							
18	143	I 2 I	.0100	79	57	36	.0015							
17	151	130	108	87	66	44	23	,0002						
10	160	138	117	96	74	53	32	.0010						
15	160	148	126	.0105	84	62	41	19						
14	179	157	136	115	93	72	50	20	.0008					
13	180	168	146	125	.0103	82	61	39	.0018					
12	200	178	157	136	114	93	71	50	29	.0007				
11	211	190	168	147	125	.0104	83	61	40	.0018				
10	223	202	180	159	137	116	94	73	52	30				
9	236	214	193	171	150	128	.0107	85	64	43				
8	249	227	206	184	163	141	I 20	98	77	56				
7	263	241	220	198	177	155	134	.0112	91	69				
6	277	256	234	213	191	170	148	127	.0105	84				
5	202	271	249	228	206	185	163	142	120	.0099				
4	308	287	265	244	222	201	179	158	136	.0115				
3	325	304	282	261	239	218	196	175	153	132				
2	343	321	300	278	257	235	214	192	171	149				
- I	361	340	318	297	275	254	232	210	189	167				
± 0	381	359	338	316	204	273	251	230	208	187				
+ r	401	380	358	337	315	293	272	250	229	207				
2	423	401	379	358	336	315	293	271	250	228				
3	445	423	402	380	359	337	315	294	272	250				
4	468	447	425	404	382	360	339	317	295	274				
5	493	471	450	428	407	385	363	342	320	298				
6	519	497	476	454	432	411	389	367	346	324				
7 8	546	524	503	481	459	438	416	394	373	351				
8	574	552	531	509	487	466	444	422	401	379				
9	604	582	560	539	517	495	474	452	430	408				
10	.0635	.0613	.0591	.0569	.0548	.0526	.0504	.0483	.0461	.0439				
-20 + 10	$\Delta c \times \Delta B$	+.0001	+.0001	+.0002	+.0003	+.0004	+.0004	+.0005	+.0006	+.0007				

Values of
$$e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 32}{1571} \right)$$

 $B = 30.0$ inches

				o.o inche	-				
				t	- t'				
2.0	2.2	2.4	2.6	2.8	3.0	3.2	3.4	3.6	3.8
Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
21									
48	26	.0005							
			0012						
93	72	50	29	.0007	.0002				
127	.0106	84	63	41	.0020	.0016			
165	144	122			57	36	.0014		
185	164 185	142 163	121	.0120	78 .0099		34 55	.0013	.0012
229 252	207 231	186 209	164 187	142 166	.0121 144	.01 22	.0101	56 79	34 58
277	255	233	212	190	168	147	125	.0104	82
329	308	286	264	243	221	199	178	156	.0107
357 387	330 365	343	322	300	249 278	227 257	205 235	184	162 191
.0417	.0396	.0374	.0352	.0331	.0309	.0287	.0266	.0244	.0222
+.0007	+.0008	+.0009	+.0009	+.0010	+.0011	+.0012	+.0012	+.0013	+.0014
				t-	-t'				
4.0	4.2	4.4	4.6	4.8	5.0	5.2	5.4	5,6	5.8
Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
36	.0014								
60 86	39	.0017	0027						
.0113	91	69	47	.0026	.0004	0010			
170	148	.0126	.0105	83	61	40	.0018		
.0200	.0179	.0157	.0135	.0114	.0092	.0070	.0048	.0027	.0005
+.0014	0015	+.0016 -	+.0017	+.0017	0018 -	0019	0020 -	0020	+.0021
	Inches0009 21 34 48 62 77 93 .0110 127 146 165 185 207 229 252 277 302 329 357 387 .0417 +.0007 Inches0013 36 60 86 .0113 140 170 .0200	Inches. Inches0000 21 34 .0013 48 26 62 41 77 56 93 72 .0110 88 127 .0106 146 124 165 144 185 207 252 231 277 255 302 281 329 308 357 336 387 365 .0417 .0396 +.0007 +.0008 4.0 4.2 Inches. Inches0013 36 64 .0113 91 140 .0119 170 148	Inches. Inches. Inches. .0009 21 34 .0013 48 26 .0005 62 41 .0019 77 56 34 .0100 88 67 127 .0100 84 122 125 163 129 207 185 163 229 207 186 252 231 209 277 255 233 302 281 259 329 308 286 357 336 314 387 365 343 .0417 .0396 .0374 +.0007 +.0008 +.0009 4.0013 36 .0014 60 39 .0017 60 42 4.0113 91 69 140 .0119 97 170 148 .0126 .0200 .0179 .0157	2.0 2.2 2.4 2.6 Inches. Inches. Inches. Inches	2.0 2.2 2.4 2.6 2.8	1	Column C	Column C	Column C

Values of
$$c = c' - 0.000367 B(t - t') \left(1 + \frac{t' - 3^2}{15^7 1}\right)$$

 $B = 30.0 \text{ inches}$

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$					B =	= 30.0 in	ches				
F.						t-t'					
10°	t'	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0
10	F.		Inches.	Inches.	Inches.	Inches.			Inches.	Inches.	Inches.
11								+.0022	+.0025	+.0029	+.0033
12				1 '	1			0.000			
13				45							
T4								8			
16		77	66	56	45		23	.012	0.001		
17			70		49	38	27		5		
18						42					
19											
20		- '									0.000
1.108			0.2		7.1				27		
22											
125				92			59	48		26	
25		-									
26 .137 .126 .115 .104 93 82 71 60 49 38 27 .143 .133 .122 .111 .100 89 78 67 56 45 28 .150 .139 .128 .117 .100 95 84 73 62 51 29 .157 .140 .135 .124 .113 .102 91 80 69 58 30 .165 .154 .143 .132 .121 .110 99 88 77 66 31 .172 .161 .150 .139 .128 .117 .106 95 84 73 32 .180 .169 .158 .147 .130 .125 .114 .103 92 81 33 .185 .177 .106 .155 .144 .133 .122 .111 .100 .80 .148 .137 <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>											
143		_		-							
28			1								
29											
31		.157	.146	.135	.124	.113		91		69	
31	30	.165	.154	.143	.132	.121	.110	99	88	77	66
33											
334			1								
35											
36 .212 .201 .190 .170 .168 .157 .145 .134 .123 .112 37 .220 .200 .198 .187 .176 .165 .154 .143 .132 .121 38 .220 .218 .207 .196 .185 .174 .163 .152 .141 .130 39 .238 .227 .216 .205 .194 .183 .172 .161 .150 .139 40 .248 .237 .226 .215 .203 .192 .181 .170 .159 .148 41 .258 .246 .235 .224 .213 .202 .191 .180 .169 .158 42 .268 .257 .246 .234 .223 .212 .201 .190 .179 .168 43 .278 .267 .256 .245 .234 .223 .211 .200 .179											
37 .220 .200 .198 .187 .176 .165 .154 .143 .132 .121 38 .229 .218 .207 .196 .185 .174 .163 .152 .141 .130 39 .238 .227 .216 .205 .194 .183 .172 .161 .150 .139 40 .248 .237 .226 .215 .203 .192 .181 .170 .159 .148 41 .258 .246 .235 .224 .213 .202 .191 .180 .169 .158 42 .268 .257 .246 .234 .223 .212 .201 .190 .179 .168 43 .278 .267 .256 .245 .234 .223 .211 .200 .178 44 .289 .278 .267 .256 .245 .234 .223 .211 .200 .189			_								
38 .229 .218 .207 .196 .185 .174 .163 .152 .141 .130 39 .238 .227 .216 .205 .194 .183 .172 .161 .150 .139 40 .248 .237 .226 .215 .203 .192 .181 .170 .159 .148 41 .258 .246 .235 .224 .213 .202 .191 .180 .169 .158 42 .268 .257 .246 .234 .223 .212 .201 .190 .179 .168 43 .278 .267 .256 .245 .234 .223 .211 .200 .178 44 .289 .278 .267 .256 .245 .234 .223 .211 .200 .189 45 .300 .289 .278 .267 .256 .245 .234 .223 .211 .200											
40 .248 .237 .226 .215 .203 .192 .181 .170 .159 .148 41 .258 .246 .235 .224 .213 .202 .191 .180 .169 .158 42 .268 .257 .246 .234 .223 .212 .201 .190 .179 .168 43 .278 .267 .256 .245 .234 .223 .212 .201 .190 .179 .168 44 .289 .278 .267 .256 .245 .234 .223 .211 .200 .179 45 .300 .289 .278 .267 .256 .245 .234 .223 .211 .200 .189 45 .300 .289 .278 .267 .256 .245 .234 .223 .211 .200 46 .312 .313 .302 .291 .280 .268 .257		<			-			-			
41 .258 .246 .235 .224 .213 .202 .191 .180 .169 .158 42 .268 .257 .246 .234 .223 .212 .201 .190 .179 .168 43 .278 .267 .256 .245 .234 .223 .212 .201 .190 .179 .168 44 .289 .278 .267 .256 .245 .234 .223 .211 .200 .179 45 .300 .289 .278 .267 .256 .245 .234 .223 .211 .200 .189 46 .312 .301 .290 .279 .268 .256 .245 .234 .223 .211 .200 47 .324 .313 .302 .291 .280 .268 .257 .246 .235 .224 48 .336 .325 .314 .303 .292 .281	39	l .			_		_			_	
42 .268 .257 .246 .234 .223 .212 .201 .190 .179 .168 43 .278 .267 .256 .245 .234 .223 .212 .201 .190 .179 .168 44 .289 .278 .267 .256 .245 .234 .223 .211 .200 .189 45 .300 .289 .278 .267 .256 .245 .234 .223 .211 .200 .189 46 .312 .301 .290 .279 .268 .256 .245 .234 .223 .211 .200 47 .324 .313 .302 .291 .280 .268 .257 .246 .235 .224 48 .336 .325 .314 .303 .292 .281 .270 .259 .248 .236 49 .349 .333 .327 .316 .305 .294											
43 .278 .267 .256 .245 .234 .223 .212 .201 .190 .178 44 .289 .278 .267 .256 .245 .234 .223 .211 .200 .189 45 .300 .289 .278 .267 .256 .245 .234 .223 .211 .200 .189 46 .312 .301 .290 .279 .268 .256 .245 .234 .223 .211 .200 47 .324 .313 .302 .291 .280 .268 .257 .246 .233 .212 48 .336 .325 .314 .303 .292 .281 .270 .259 .248 .236 49 .349 .338 .327 .316 .305 .294 .283 .271 .260 .249 50 .363 .351 .340 .329 .318 .307 .296										-	
44 .289 .278 .267 .256 .245 .234 .223 .211 .200 .189 45 .300 .289 .278 .267 .256 .245 .234 .223 .211 .200 .189 46 .312 .301 .290 .279 .268 .256 .245 .234 .223 .211 .200 47 .324 .313 .302 .291 .280 .268 .257 .246 .235 .212 48 .336 .325 .314 .303 .292 .281 .270 .259 .248 .236 49 .349 .388 .327 .316 .305 .294 .283 .271 .260 .249 50 .363 .351 .340 .329 .318 .307 .296 .285 .274 .262 51 .376 .365 .354 .343 .332 .321 .309						_					
45 .300 .289 .278 .267 .256 .245 .234 .223 .211 .200 46 .312 .301 .290 .279 .268 .256 .245 .234 .223 .212 47 .324 .313 .302 .291 .280 .268 .257 .246 .235 .224 48 .336 .325 .314 .303 .292 .281 .270 .259 .248 .236 49 .349 .338 .327 .316 .305 .294 .283 .271 .260 .249 50 .363 .351 .340 .329 .318 .307 .296 .285 .274 .262 51 .376 .365 .354 .343 .332 .321 .309 .298 .287 .276 52 .390 .379 .368 .357 .346 .335 .324 .312 .301							-			-	
46 .312 .301 .290 .270 .268 .256 .245 .234 .223 .212 47 .324 .313 .302 .291 .280 .268 .257 .246 .235 .224 48 .336 .325 .314 .303 .292 .281 .270 .259 .248 .236 49 .349 .338 .327 .316 .305 .294 .283 .271 .260 .249 50 .363 .351 .340 .329 .318 .307 .296 .285 .274 .262 51 .376 .365 .354 .343 .332 .321 .309 .298 .287 .276 52 .390 .379 .368 .357 .346 .335 .324 .312 .301 .290 53 .495 .394 .383 .372 .361 .349 .338 .327 .316	E!	.300	.289	.278	.267		.245	.234	.223	.211	.200
48 .336 .325 .314 .363 .292 .281 .270 .259 .248 .236 49 .349 .338 .327 .316 .305 .294 .283 .271 .260 .249 50 .363 .351 .340 .329 .318 .307 .296 .285 .274 .262 51 .376 .365 .354 .343 .332 .321 .309 .298 .287 .276 52 .390 .379 .368 .357 .346 .335 .324 .312 .301 .290 53 .405 .394 .383 .372 .361 .349 .338 .327 .316 .305 54 .420 .409 .398 .387 .376 .364 .353 .342 .331 .320 55 .436 .425 .414 .402 .391 .380 .369 .358 .347		.312		.290							}
49 .349 .338 .327 .316 .305 .294 .283 .271 .260 .249 50 .363 .351 .340 .329 .318 .307 .296 .285 .274 .262 51 .376 .365 .354 .343 .332 .321 .309 .298 .287 .276 52 .390 .379 .368 .357 .346 .335 .324 .312 .301 .290 53 .405 .394 .383 .372 .361 .349 .338 .327 .316 .305 54 .420 .409 .398 .387 .376 .364 .353 .342 .331 .320 55 .436 .425 .414 .402 .391 .380 .360 .358 .347 .335 56 .452 .441 .430 .419 .407 .396 .385 .374 .363											
50 .3649 .367 .367 .368 .351 .340 .329 .318 .307 .296 .285 .274 .262 51 .366 .365 .354 .343 .332 .321 .309 .298 .287 .276 52 .390 .379 .368 .357 .346 .335 .324 .312 .301 .290 53 .495 .394 .383 .372 .361 .349 .338 .327 .316 .305 54 .420 .409 .398 .387 .376 .364 .353 .342 .331 .320 55 .436 .425 .414 .402 .391 .380 .360 .358 .347 .335 56 .452 .441 .430 .419 .407 .396 .385 .374 .363 .352 57 .469 .458 .446 .435 .424 .413						-					
51 .376 .365 .354 .343 .332 .321 .309 .298 .287 .276 52 .390 .379 .368 .357 .346 .335 .324 .312 .301 .290 53 .405 .394 .383 .372 .361 .349 .338 .327 .316 .305 54 .420 .409 .398 .387 .376 .364 .353 .342 .331 .320 55 .436 .425 .414 .402 .391 .380 .360 .358 .347 .335 56 .452 .441 .430 .409 .396 .385 .374 .363 .352 57 .469 .458 .446 .435 .424 .413 .402 .300 .379 .368 58 .486 .475 .464 .452 .441 .430 .419 .408 .396 .385											
52 .390 .379 .368 .357 .346 .335 .324 .312 .301 .290 53 .495 .394 .383 .372 .361 .349 .338 .327 .316 .305 54 .420 .499 .398 .387 .376 .364 .353 .342 .331 .320 55 .436 .425 .414 .492 .391 .380 .360 .358 .347 .335 56 .452 .441 .430 .419 .458 .374 .363 .352 57 .469 .458 .446 .455 .424 .413 .402 .300 .379 .368 58 .486 .475 .464 .452 .441 .430 .419 .408 .396 .385 59 .504 .493 .481 .470 .459 .448 .437 .425 .414 .403											
53 .405 .394 .383 .372 .361 .349 .338 .327 .316 .305 54 .420 .409 .398 .387 .376 .364 .353 .342 .331 .320 55 .436 .425 .414 .402 .391 .380 .360 .358 .347 .335 56 .452 .441 .430 .419 .407 .396 .385 .374 .363 .352 57 .469 .458 .446 .435 .424 .413 .402 .390 .379 .368 58 .486 .475 .464 .452 .441 .430 .419 .408 .396 .385 59 .504 .493 .481 .470 .459 .448 .437 .425 .414 .403 60 0.522 0.511 0.500 0.488 0.477 0.466 0.455 0.444 0.432<		.390		.368		.346			.312	.301	.290
55 .436 .425 .414 .402 .391 .380 .360 .358 .347 .335 56 .452 .441 .430 .419 .407 .396 .385 .374 .363 .352 57 .469 .458 .446 .435 .424 .413 .402 .390 .379 .368 58 .486 .475 .464 .452 .441 .430 .419 .408 .396 .385 59 .504 .493 .481 .470 .459 .448 .437 .425 .414 .403 60 0.522 0.511 0.500 0.488 0.477 0.466 0.455 0.444 0.432 0.421	53	.405	•394	.383							
56 .452 .441 .430 .419 .407 .396 .385 .374 .363 .352 57 .469 .458 .446 .435 .424 .413 .402 .390 .379 .368 58 .486 .475 .464 .452 .441 .430 .419 .408 .396 .385 59 .504 .493 .481 .470 .459 .448 .437 .425 .414 .403 60 0.522 0.511 0.500 0.488 0.477 0.466 0.455 0.444 0.432 0.421	i I										
57 .469 .458 .446 .435 .424 .413 .402 .390 .379 .368 58 .486 .475 .464 .452 .441 .430 .419 .408 .396 .385 59 .504 .493 .481 .470 .459 .448 .437 .425 .414 .403 60 0.522 0.511 0.500 0.488 0.477 0.466 0.455 0.444 0.432 0.421		.436									
58 .486 .475 .464 .452 .441 .430 .410 .408 .396 .385 59 .504 .493 .481 .470 .459 .448 .437 .425 .414 .403 60 0.522 0.511 0.500 0.488 0.477 0.466 0.455 0.444 0.432 0.421											
59 .504 .493 .481 .470 .459 .448 .437 .425 .414 .403 60 0.522 0.511 0.500 0.488 0.477 0.466 0.455 0.444 0.432 0.421	58										
60 0.522 0.511 0.500 0.488 0.477 0.466 0.455 0.444 0.432 0.421											
		0.522	0.511	0.500	0.488	0.477	0.466	0.455	0.444	0.432	0.421
00 1	60	$\Delta c \times \Delta B$	+.0004	+.0007	+.0011	+.0015	+.0019	+.0022	+.0026	+.0030	+.0034

Values of $e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 32}{1571} \right)$

B = 30.00

					t -	· t'				
t'	10	11	12	13	14	15	16	17	18	19
F. 30° Δε× ΔΒ	Inches. +.0037	Inches. +.0040	Inches. +.0044	Inches. +.0048	Inches. +.0051	Inches. +.0055	Inches. +.0050	Inches. +.0062	Inches. +.0066	Inches. +.0070
22° 23 24	0.004									
25 26 27 28 29	21 27 34 40 47	0.010 16 23 29 36	0.005 .012 18 25	0.001 7	0.003					
30 31 32 33 34	55 62 70 78 85	44 51 59 67 74	33 40 48 55 63	22 29 37 44 52	.011 18 26 33 41	0.000 .007 .015 22 30	0.004	0.000		
35 36 37 38 39	93 .101 .110 .110	82 90 99 .108 .117	71 79 88 96	60 68 77 85 94	49 57 66 74 83	38 46 55 63 72	27 35 43 52 61	.016 24 32 41 50	0.005 .013 21 30 39	0.002 .010 IQ 28
40 41 42 43 44	.137 .147 .157 .167	.126 .136 .146 .156 .167	.115 .125 .135 .145 .156	.104 .114 .124 .134 .145	93 .103 .113 .123	82 91 .101 .112 .123	71 80 90 .101	60 69 79 90	49 58 68 79 89	37 47 57 68 78
45 46 47 48 49	.189 .201 .213 .225 .238	.178 .190 .202 .214	.167 .179 .191 .203	.156 .168 .180 .192	.145 .156 .168 .181	.134 .145 .157 .170	.123 .134 .146 .159	.112 .123 .135 .147 .160	.100 .112 124 .136 .149	89 .101 .113 .125 .138
50 51 52 53 54	.251 .265 .279 .294 .309	.240 .254 .268 .282 .297	.229 .243 .257 .271 .286	.218 .231 .246 .260	.207 .220 .234 .249 .264	.196 .209 .223 .238 .253	.184 .198 .212 .227 .242	.173 .187 .201 .216	.162 .176 .190 .204	.151 .165 .179 .193 .208
55 56 57 58 59	•324 •340 •357 •374 •392	.313 .329 .346 .363 .381	.302 .318 .334 .352 .369	.201 .307 .323 .340 .358	.280 .296 .312 .329 .347	.268 .285 .301 .318 .336	.257 .273 .290 .307 .325	.246 .262 .279 .296 .313	.235 .251 .267 .284 .302	.224 .240 .256 .273 .291
60	0.410	0.399	0.388	0.376	0.365	0.354	0.343	0.331	0.320	0.309
$60 \ \Delta e \times \Delta B$	+.0037	+.0041	+.0045	+.0049	+.0052	+.0056	+.0060	+.0064	+.0067	+.0071

TABLE 82. REDUCTION OF PSYCHROMETRIC OBSERVATIONS.

Values of e = e' - 0.000367 $B(t-t')\left(1 + \frac{t' - 32}{1571}\right)$

					B = 30.00					
t'						t-t'				
,	20	21	22	23	24	25	26	27	28	29
F.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
$40^{\circ} \Delta e \times \Delta B$	+.0074	+.0077	+.0081	+.0085	+.0089	+.0092	+.0096	+.0100	+.0103	+.010
38°	0.008									
39	.017	0.006								
40	26	.015	0.004	0.003						
4I 42	36 46	25 35	.014	.013	0.002					
43	56	45	34	23	.012	0.001				
44	67	56	45	34	23	.012	0.001			
45	78	67	56	45	34	23	.012	0.001		
46	.102	79 91	68 79	57 68	45	34 46	23	.012 24	0.001	0.002
47 48	.114	.103	92	81	57 70	58	35 47	36	25	.014
49	.127	.116	.104	93	82	71	60	49	38	27
50	.140	.129	.118	.106	95	84	73	62	51	40
51	.153	.142	.131	.120	.109	98	87	75	64	53
52	.167	.156	.145	.134	.123	.112	.101	.104	78 93	67 82
53 54	.102	.186	.175	.164	.152	.141	.130	.119	.108	97
55	.212	.201	.100	.179	.168	.157	.145	.134	.123	.112
56	.229	.218	.206	.195	.184	.173	.162	.150	.139	.128
57	.245	.234	.223	.211	.200	.189	.178	.167	.156	.144
58 59	.262	.251	.240	.228	.217	.206	.195	.184	.173	.161
60	0.208	0.287	0.275	0.264	0.253	0.242	0.231	0.210	0.208	0.197
$60 \Delta e \times \Delta B$		+.0078		+.0086	+.0000	+.0093	+.0007	+.0101	+.0105	+.010
	111173	110070	110002	1.0000	-	t-t'	1.0097	1.0101	1.0105	7.0100
t'	30	31	32	33	-		36	37	38	39
<i>t'</i>						t-t'				
$ \begin{array}{c c} \hline F. \\ 50^{\circ} \Delta e \times \Delta B \end{array} $	30	31	32 Inches.	33 Inches.	34	<i>t−t′</i> 35	36	37	38	39 Inches.
$ \begin{array}{c c} \hline F. \\ 50^{\circ} \Delta e \times \Delta B \\ 48^{\circ} \end{array} $	30 Inches. +.0111	31 Inches. +.0115	32 Inches.	33 Inches.	34 Inches.	35 Inches.	36 Inches.	37 Inches.	38 Inches.	39 Inches.
F. 50° Δε× ΔΒ 48° 49	30 Inches. +.0111 0.003 .015	31 Inches. +.0115	32 Inches. +.0119	33 Inches.	34 Inches.	35 Inches.	36 Inches.	37 Inches.	38 Inches.	39 Inches.
F. 50° Δε× ΔΒ 48° 49 50	30 Inches. +.0111 0.003 .015	31 Inches. +.0115	32 Inches. +.0119	33 Inches. +.0122	34 Inches.	35 Inches.	36 Inches.	37 Inches.	38 Inches.	39 Inches.
F. 50° Δe × ΔB 48° 49 50	30 Inches. +.0111 0.003 .015 29 42	31 Inches. +.0115 .004 .017 31	32 Inches. +.0119	33 Inches. +.0122	34 Inches.	35 Inches.	36 Inches.	37 Inches.	38 Inches.	39 Inches.
F. 50° Δε× ΔΒ 48° 49 50 51 52 53	30 Inches. +.0111 0.003 .015 29 42 56 70	31 Inches. +.0115 .004 .017 31 45 59	32 Inches. +.0119 0.006 .020 34 48	33 Inches. +.0122	34 Inches. +.0126	1-l' 35 Inches. +.0130 0.000 .015	36 Inches. +.0134	37 Inches. +.0137	38 Inches.	39 Inches.
F. 50° Δε× ΔΒ 48° 49 50 51 5 ² 53 54	30 Inches. +.0111 0.003 .015 29 42 56 70 85	31 Inches. +.0115 .004 .017 31 45 59 74	32 Inches. +.0119 0.006 .020 34 48 63	33 Inches. +.0122	34 Inches. +.0126	1-l' 35 Inches. +.0130 0.000 .015 30	36 Inches. +.0134	37 Inches. +.0137	38 Inches. +.0141	39 Inches. +.0145
F. 50° Δe× ΔB 48° 49 50 51 52 53 54 55	30 Inches. +.0111 0.003 .015 29 42 56 70 85 .101	31 Inches. +.0115 .004 .017 31 45 59 74 90	32 Inches. +.0119 0.006 .020 34 48 63 78	33 Inches. +.0122 0.009 .023 37 52 67	34 Inches. +.0126	1-1' 35 Inches. +.0130 0.000 .015 30 45	36 Inches. +.0134	37 Inches. +.0137	38 Inches. +.0141	39 Inches. +.0145
F. 50° Δe× ΔB 48° 49 50 51 52 53 54 55 56	30 Inches. +.0111 0.003 .015 29 42 56 70 85 .101 .117	31 Inches. +.0115 .004 .017 31 45 59 74 90 .106	32 Inches. +.0119 0.006 .020 34 48 63 78 95	0.009 0.023 37 52 67 83	34 Inches. +.0126	0.000 0.000 0.015 30 45 61	36 Inches. +.0134	37 Inches. +.0137	38 Inches. +.0141	39 Inches. +.0145
F. 50° Δe× ΔB 48° 49 50 51 52 53 54 55	30 Inches. +.0111 0.003 .015 29 42 56 70 85 .101	31 Inches. +.0115 .004 .017 31 45 59 74 90	32 Inches. +.0119 0.006 .020 34 48 63 78	33 Inches. +.0122 0.009 .023 37 52 67	34 Inches. +.0126	1-1' 35 Inches. +.0130 0.000 .015 30 45	36 Inches. +.0134	37 Inches. +.0137	38 Inches. +.0141	39 Inches. +.0145
F. 50° Δe× ΔB 48° 49 50 51 52 53 54 55 56 57 58 59	30 Inches. +.OIII 0.003 .015 29 42 56 70 85 .IOI .II7 .I33 .I50 .I68	31 Inches. +.0115 .004 .017 31 45 59 74 90 .106 .122	32 Inches. +.0119 0.006 .020 34 48 63 78 95 .111	0.009 0.23 37 52 67 83 .100	0.011 26 41 56 72 88	0.000 0.015 30 0.77	36 Inches. +.0134	0.007 0.003 0.007	38 Inches. +.0141	39 Inches. +.0145
F. 50° Δe× ΔB 48° 49 50 51 52 53 54 55 56 57 58 59 60	30 Inches. +.OIII 0.003 .015 29 42 56 70 85 .IOI .II7 .I33 .I50 .I68	31 Inches. +.0115 .004 .017 .31 .45 .59 .74 .90 .106 .122 .139 .157 0.175	0.006 .020 34 48 63 78 95 .111 .128 .145 0.163	0.009 0.023 37 52 67 83 .100 .117 .134 0.152	0.011 26 41 56 72 88 .105 .123	0.000 0.000 0.015 30 45 61 77 94 .112 0.130	36 Inches. +.0134 0.004 .018 34 50 66 83 .101 0.119	0.007 0.007 0.23 39 55 72 89 0.107	38 Inches. +.0141	0.000 0.000 0.016 32 49 67 0.085
F. 50° Δε× ΔB 48° 49 50 51 52 53 54 55 56 57 58 59	30 Inches. +.OIII 0.003 .015 29 42 56 70 85 .IOI .II7 .I33 .I50 .I68	31 Inches. +.0115 .004 .017 .31 .45 .59 .74 .90 .106 .122 .139 .157	0.006 .020 34 48 63 78 95 .111 .128 .145 0.163	0.009 0.023 37 52 67 83 .100 .117 .134 0.152	0.011 26 41 56 72 88 .105 .123 0.141 +.0127	0.000 0.000 0.015 30 45 61 77 94 .112 0.130 +.0131	0.004 0.018 0.018 0.018 0.018	0.007 0.007 0.23 39 55 72 89	38 Inches. +.0141 0.011 28 44 61 78	0.000 0.16 32 49 67 0.085
F. 50° Δε× ΔΒ 48° 49 50 51 52 53 54 55 56 67 58 59 60 60 Δε × ΔΒ	30 Inches. +.OIII 0.003 .015 29 42 56 70 85 .IOI .II7 .I33 .I50 .I68	31 Inches. +.0115 .004 .017 .31 .45 .59 .74 .90 .106 .122 .139 .157 0.175	0.006 0.020 34 48 63 78 95 .111 .128 .145 0.163 +.0120	0.009 .023 .37 .52 .67 .83 .100 .117 .134 0.152 +.0123	0.011 26 41 56 72 88 .105 .123 0.141 +.0127	0.000 0.000 0.015 30 45 61 77 94 .112 0.130	36 Inches. +.0134 0.004 .018 34 50 66 83 .101 0.119	0.007 0.007 0.23 39 55 72 89 0.107	38 Inches, +.0141 0.011 28 44 61 78 0.096	0.000 0.000 0.016 32 49 67 0.085
F. 50° Δε× ΔΒ 48° 49 50 51 52 53 54 55 56 57 58 59 60 60 Δε× ΔΒ	30 Inches. +.OIII 0.003 .015 29 42 56 70 85 .IOI .II7 .I33 .I50 .I68	31 Inches. +.0115 .004 .017 .31 .45 .59 .74 .90 .106 .122 .139 .157 0.175	0.006 .020 34 48 63 78 95 .111 .128 .145 0.163	0.009 0.023 37 52 67 83 .100 .117 .134 0.152	0.011 26 41 56 72 88 .105 .123 0.141 +.0127	0.000 0.000 0.015 30 45 61 77 94 .112 0.130 +.0131	36 Inches. +.0134 0.004 .018 34 50 66 83 .101 0.119	0.007 0.007 0.23 39 55 72 89 0.107	38 Inches, +.0141 0.011 28 44 61 78 0.096	0.000 0.16 32 49 67 0.085
F. 50° Δe× ΔB 48° 49 50 51 52 53 54 55 56 57 58 59 60 60 Δe × ΔB	30 Inches. +.0111 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186 +.0112	31 Inches. +.0115 .004 .017 31 45 59 74 .0106 .122 .139 .157 0.175 +.0116	0.006 0.020 34 48 63 78 95 .111 .128 .145 0.163 +.0120	0.009 .023 .37 .52 .67 .83 .100 .117 .134 0.152 +.0123	0.011 26 41 56 72 88 .105 .123 0.141 +.0127	0.000 .015 30 45 61 77 94 .112 0.130 +.0131	0.004 .018 34 50 66 83 .101 0.119 +.0134	0.007 0.007 0.23 39 55 72 89 0.107	38 Inches, +.0141 0.011 28 44 61 78 0.096	0.000 0.16 32 49 67
F. 50° Δe× ΔB 48° 49 50 51 52 53 54 55 56 57 58 59 60 60 Δe × ΔB t' F. 56°	30 Inches. +.0111 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186 +.0112 40 Inches. 0.005	31 Inches. +.0115	32 Inches. +.0119 0.006 .020 34 48 63 78 95 .111 .128 0.163 +.0120	0.009 .023 .37 .52 .67 .83 .100 .117 .134 0.152 +.0123	0.011 26 41 56 72 88 .105 .123 0.141 +.0127	0.000 .015 30 45 61 77 94 .112 0.130 +.0131	0.004 .018 34 50 66 83 .101 0.119 +.0134	0.007 0.007 0.23 39 55 72 89 0.107	38 Inches, +.0141 0.011 28 44 61 78 0.096	0.000 0.16 32 49 67
F. 50° Δe× ΔB 48° 49 50 51 52 53 54 55 56 57 58 59 60 60 Δe× ΔB t' F. 56° 57	30 Inches. +.0111 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186 +.0112	31 Inches	32 Inches. +.0119 0.006 .020 34 48 63 78 95 .111 .128 0.163 +.0120 42 Inches.	0.000 0.000 0.023 37 52 67 83 .100 .117 .134 0.152 +.0123	0.011 26 41 56 72 88 .105 .123 0.141 +.0127	0.000 .015 30 45 61 77 94 .112 0.130 +.0131	0.004 .018 34 50 66 83 .101 0.119 +.0134	0.007 0.007 0.23 39 55 72 89 0.107	38 Inches, +.0141 0.011 28 44 61 78 0.096	0.000 0.16 32 49 67
F. 50° Δe× ΔB 48° 49 50 51 52 53 54 55 56 60 60 Δe × ΔB t' F. 56°	30 Inches. +.0111 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186 +.0112 40 Inches. 0.005	31 Inches. +.0115	0.006 .020 34 48 63 78 95 .111 .128 0.163 +.0120	0.009 .023 .37 .52 .67 .83 .100 .117 .134 0.152 +.0123	0.011 26 41 56 72 88 .105 .123 0.141 +.0127	0.000 .015 30 45 61 77 94 .112 0.130 +.0131	0.004 .018 34 50 66 83 .101 0.119 +.0134	0.007 0.007 0.23 39 55 72 89 0.107	38 Inches, +.0141 0.011 28 44 61 78 0.096	0.000 0.000 0.016 32 49 67 0.085
F. 50° Δε × ΔΒ 48° 49 50 51 52 53 54 55 56 57 58 60 60 Δε × ΔΒ t' F. 56° 57 58	30 Inches. +.0111 0.003 .015 29 42 56 70 85 .101 .117 .133 .150 .168 0.186 +.0112 40 Inches. 0.005 .021 38	31 Inches. +.oII5 .004 .017 31 45 59 74 90 .106 .122 .139 .157 0.175 +.oII6 41 Inches. 0.010 27	32 Inches. +.0119 0.006 .020 34 48 63 78 95 .111 .128 0.163 +.0120 42 Inches.	0.000 0.000 0.023 37 52 67 83 .100 .117 .134 0.152 +.0123	0.011 26 41 56 72 88 .105 .123 0.141 +.0127	0.000 .015 30 45 61 77 94 .112 0.130 +.0131 -t'	0.004 .018 34 50 66 83 .101 0.119 +.0134	0.007 0.007 0.23 39 55 72 89 0.107	38 Inches, +.0141 0.011 28 44 61 78 0.096	0.000 0.000 0.016 32 49 67 0.085
F. 50° Δε× ΔΒ 48° 49 50 51 52 53 54 55 56 57 58 59 60 60 Δε × ΔΒ t' F. 56° 57 58 59	30 Inches. +.0111 0.003 .015 29 42 56 70 85 .101 .117 .133 .1568 0.186 +.0112 40 Inches. 0.005 .021 38 56 0.074	31 Inches. +.0115 .004 .017 31 45 59 74 90 .106 .122 .139 .157 0.175 +.0116 41 Inches. 0.010 27 45 0.063	0.006 0.020 34 48 63 78 95 .111 .128 .145 0.163 +.0120 42 Inches.	0.000 0.000 0.023 37 52 67 83 .100 .117 .134 0.152 +.0123	0.011 26 41 56 72 88 .105 .123 0.141 +.0127	0.000 0.000 0.015 30 45 61 77 94 .112 0.130 +.0131 -t' 45 Inches.	0.004 .018 34 50 66 83 .101 0.119 +.0134	0.007 0.007 0.23 39 55 72 89 0.107	38 Inches, +.0141 0.011 28 44 61 78 0.096	0.000 0.000 0.016 32 49 67

Values of
$$e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 3^2}{1571}\right)$$

 $B = 30.00$

					B = 30	.00					
t'						t-t'					
	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0
F. 60°	Inches. $\Delta e \times \Delta E$	Inches. +.0004	Inches. +.0007		Inches. +.0015	Inches.	Inches. +.0022	Inches. +.0026	Inches.	Inches. +.0034	Inches. +.0037
60°	0.522	0.511	0.500	0.488	0.477	0.466	0.455	0.444	0.432	0.421	0.410
61	.541	.530	.518	.507	.496	.485	.474	.462	.451	.440	.420
62	.560	-549	.538	-527	.516	.504	•493	.482	·47I	-459	.448
63	.580 .601	569	.558	-547	.536	-524	.513	.502	.491	.479	.468
64 65	.623	.590	.600	.568	.556	•545	-534	.523	.511	.500	.489
66	.645	.633	.622	.589	.578	.566	·555	.544	·533 ·555	.521	.510
67	.667	.656	.645	.634	.622	.611	.600	.589	.577	.566	.532 .555
68	.691	.680	.668	.657	.646	.635	.623	.612	.601	.590	.578
69	.715	.704	.692	.681	.670	.659	.647	.636	.625	.614	.602
70	.740	.729	.717	.706	.695	.684	.672	.661	.650	.638	.627
71	.766	.754	·743	.732	.720	.709	.698	.687	.675	.664	.653
72 73	.792 .819	.781	.709	.758 .785	·747	·735	.724 .751	.713	.702	.690	.679
74	.847	.836	.824	.813	.802	.791	.779	.768	.757	-745	.734
75	.876	.865	.853	.842	.831	.819	.808	.797	.786	.774	.763
76	.906	.894	.883	.872	.860	.849	.838	.826	.815	.804	.792
77	.936	.925	.914	.902	.891	.880	.868	.857	.846	.834	.823
78 79	.968	.956	·945 ·977	-934 -966	.922	.911	.900	.888	.877	.866	.854
80	1.033	1.022	1.011	.999	.988	.943	.952			-	. 1
81	.068	.056	.045	1.034	1.022	1.011	.903	.954 .988	·943 ·977	.931	.920
82	.103	.092	.080	.069	.057	.046	1.035	1.023	1.012	1.001	.989
83	.139	.128	.116	.105	.094	.082	.071	.060	.048	.037	1.026
84	.176	.165	.154	.142	.131	.120	.108	.097	.086	.074	.063
85	1.215	1.204	1.192	1.181	1.169	1.158	1.147	1.135	1.124	1.112	1.101
86 87	.254	.243	.232	.220	.209	.197	.186	.175	.163	.152	.140
88	.336	.325	.314	.302	.201	.279	.268	.257	.245	.234	.222
89	.379	368	-357	·345	-334	.322	.311	.300	.288	.277	.265
90	1.423	1.412	1.401	1.389	1.378	1.366	1.355	1.343	1.332	1.321	1.309
91	.469	-457	.446	.435	.423	.412	.400	.389	-377	.366	-355
92	.515	.504	.492	.481	.470	.458	.447	-435	.424	.412	.401
93 94	.563 .612	.552 .601	.540	.529 .578	.517 .566	.506	∙494 •543	.483	.47I .52I	.460	·449 .498
95	1.662	1.651	1.640	1.628	1.617	1.605	1.594	1.582	1.571	1.559	1.548
96	.714	.703	.691	.680	.668	.657	.646	.634	.623	.611	.600
97	.767	.756	.744	.733	.722	.710	.699	.687	.776	.664	.653
98	.822 .878	.811 .867	·799	.788 .844	.776	.765 .821	.753	.742	.730	.719	.707
99	1.936	1.024	.855	1.001	.832	1.878	.809	.798	.786	.775	.763
101	.994	.983	.972	.960	.949	.937	.926	.014	.903	1.832	1.821
102	2.055	2.043	2.032	2.020	2.009	.997	.986	.974	.963	.951	.940
103	.117	.106	.094	.083	.071	2.060	2.048	2.037	2.025	2.014	2.002
104	.181	.169	.158	.146	.135	.123	.112	.100	.089	.077	.066
105	2.246	2.235	2.223	2.212	2.200	2.189	2.177	2.166	2.154		2.131
106 107	.314 .382	.302 .371	.359	.348	.336	.256	.244	.302	.221	.210	.198
108	·453	.441	.430	.418	.407	·323 ·395	.384	.372	.361	.340	.337
109	-525	.514	.502	.491	.479	.467	.456	-444	+433	.421	.410
110	2.599	2.588	2.576	2.565	2.553	2.542	2.530	2.519	2.507	2.495	2.484
110	$\Delta e \times \Delta B$	+.0004	+.0008	+.0012		+.0019	+.0023	+.0027		+.0035	
						1		-			

Table 82. REDUCTION OF PSYCHROMETRIC OBSERVATIONS. ENGLISH MEASURES.

Values of
$$e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 3^2}{1571}\right)$$

 $B = 30.00$

t'						$t-t^{\prime}$					
	0.0	11	12	13	14	15	16	17	18	19	20
F. 60°	Inches. $\Delta e \times \Delta B$	Inches.	Inches.	Inches. +.0040	Inches. +.0052	Inches. +.0056	Inches. +.0060	Inches. +.0063	Inches. +.0067	Inches. +.0071	Inches. +.0075
60°	0.522	0.399	0.388	0.376	0.365	0.354	0.343	0.331	0.320	0.309	0.298
61	.541	0.418	.406	.395	.384	.373	.361	.350	.339	.328	.317
62	.560	-437	.426	.415	.403	.392	.381	.370	.358	-347	.336
63	.580	.457	.446	-435	.423	.412	.401	.390	.378	.367	.356
64 65	.601	.478	.466	·455	•444	-433	.422	.410	-399	.388	-377
66	.623	.499 .521	.510	.476 .498	.465	·454 .476	·443	.43 I .453	.420	.409 .431	.398
67	.667	-544	.532	.521	.510	.499	.487	.476	.465	-454	.442
68	.691	.567	.556	.544	-533	.522	.511	-499	.488	-477	.466
69	.715	.591	.580	.568	-557	.546	-535	.523	.512	.501	.490
70	.740	.616	.605	-593	.582	·571	-559	.548	-537	.526	-514
71	.766	.641 .668	.630	.619	.608	.596 .623	.585	.574 .600	.562	.551	-540
7 ² 73	.792 .810	.695	.656 .684	.645	.634 .661	.650	.638	.627	.589 .616	-577 -604	.566
74	.847	.723	.711	.700	.689	.678	.666	.655	.644	.632	.621
75	.876	-752	.740	.729	.718	.706	.695	.684	.672	.661	.650
76	.906	.781	.770	.758	.747	.736	.725	.713	.702	.691	.679
77 78	.936	.812	.800	.789	.778	.766	-755	.744	.732	.721	.710
	.968	.843	.832	.820	.809	.798	.786	.775	.764	-752	.741
79	1.000	.875	.864	.853	.841	.830	.819	.807	.796	.785	-773
80 81	1.033	.909	.897	.886	.875	.863	.852 .886	.841	.829 .863	.818 .852	.806
82	.068	.943	.931	.920	.909	.032	.021	.875	.898	.887	.841 .876
83	.139	1.014	1.003	.991	.980	.969	.957	.946	.935	.923	.012
84	.176	.051	.040	1.029	1.017	1.006	-995	.983	.972	.960	.949
85	1.215	1.090	1.078	1.067	1.056	1.044	1.033	I.02 I	1.010	.999	.987
86	.254	.129	.118	.106	.095	.083	.072	.061	.049	1.038	1.027
87	.295	.170	.158	.147	.135	.124	.113	.101	.090	.078	.067
88 89	.336	.211	.200	.231	.177 .220	.208	.154	.143	.131	.120	.108
90	·379 1.423	1.298	1.286	1.275	1.264	1.252	1.241	1.229	1.218	1.206	1.195
91	.469	•343	.332	.320	.309	.297	.286	.275	.263	.252	.240
92	515	.390	.378	.367	·355	.344	-332	.321	.310	.298	.287
93	.563	-437	.426	.414	.403	.391	.380	.369	-357	.346	.334
94	.612	.486	.475	.463	-452	.440	.429	.418	.406	-395	.383
95	1.662	1.537	1.525	1.514	1.502	1.491	1.479	1.468	1.456	1.445	1.433
96	.714	.588 .641	·577	.565 .618	·554 .607	·542 ·595	.531 .584	.520 .572	.508 .561	·497 ·550	.485 .538
97 98	.822	.696	.684	.673	.661	.650	.638	.627	.615	.604	-593
90	.878	.752	.740	.729	.717	.706	.694	.683	.671	.660	.648
100	1.936	1.800	1.798	1.786	1.775	1.763	1.752	1.740	1.729	1.717	1.706
101	.994	.868	.857	.845	.834	.822	.811	.799	.788	.776	.765
102	2.055	.928	.917	.905	.894	.882	.871	.859	.848	.836	.825
103	.117	.991	.979	.968	.956	·944 2.008	.933	.921 .985	.910	.898 .962	.887
104	.181	2.054	2.043	2.031	2.085	2.073	.997 2.062	2.050	·974 2.030	2.027	.951 2.016
105 106	.314	.187	.175	2.097	.152	.141	.120	.118	.106	.004	.083
107	.382	.255	.244	.232	.221	.200	.198	.186	.175	.163	.152
108	.453	.326	.314	.302	.291	.280	.268	.257	.245	.234	.222
109	.525	.398	-387	.375	.364	.352	.340	.329	.317	.306	.294
110	2.599	2.472	2.461	2.449	2.438	2.426	2.414	2.403	2.391	2.380	2.368
110	$\Delta c \times \Delta B$	+.0042	+.0046				+.0062	+.0065			+.0077

Values of $e=e'-0.000367 B (t-t') \left(1 + \frac{t'-3^2}{1571}\right)$ B=30.00

	1				30.0						
t'						t-t'					
	0.0	21	22	23	24	25	26	27	28	29	30
F.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
60°	$\Delta e \times \Delta B$	1	1	+.0086	1	1	1	+.0101	1	1 '	+.0112
60°	0.522	0.287	0.275	0.264	0.253	0.242	0.231	0.219	0.208	0.197	0.186
61 62	.541	0.305	.294	.283	.272 .291	.261	.249	.238	.227	.216	.205
63	.560 .580	-325 -345	.314	.322	.311	.300	.289	.257	.246	.235	.224
64	.601	.365	-354	•343	.332	.320	.309	.298	.287	.276	.264
65	.623	.387	-375	.364	.353	.342	.330	.319	.308	.297	.285
66	.645	.408	-397	.386	-375	.363	.352	.341	.330	.310	.307
67	.667	.431	.420	.409	-397	.386	-375	.364	-352	.341	.330
68	.691	·454	·443 .467	.432 .456	.421	.409	.398	.387	.376	.364	-353
70	.715	.478		.481	.445	·433	.422	.411	-399	.388	-377
70	.740 .766	.503	.492 .517	.506	.409	.458 .483	-447 -472	·435	.424	.413	.402
72	.792	-555	.544	-532	.521	.510	.498	.487	.476	.464	.427 .453
73	.819	.582	.571	-559	.548	-537	-525	.514	.503	.491	.480
74	.847	.610	.598	.587	.576	.564	-553	-542	531	.519	.508
75	.876	.638	.627	.616	.605	-593	.582	.571	-559	.548	-537
76	.906	.668	.657	.645 .676	.634 .664	.623	.611	.600	.589	-577	.566
77 78	.936 .968	.730	.718	.707	.696	.653 .684	.642	.630 .662	.619	.608	.596
79	1.000	.762	.751	-739	.728	.717	.705	.694	.683	.671	.660
80	1.033	.795	.784	.772	.761	.750	.738	.727	.716	.704	.693
8 r	.068	.829	.818	.806	.795	.784	.772	.761	.750	.738	.727
82	.103	.864	.853	.842	.830	.819	.808	.796	.785	.773	.762
83	.139	.900	.889	.878	.866	.855	.844	.832	.821	.810	.798
84	.176	.938	.926	.915	.904	.892	.881	.869	.858	.847	.835
85 86	1.215 •254	.976	.965	.953 .992	.942 .981	.930	.919	.908	.896	.885	.873
87	.295	.056	.044	1.033	1.021	1.010	.999	.947 .987	·935 .976	.924 .964	.913
88	.336	.097	.086	.074	.063	.051	1.040	1.029	1.017	1.006	.933
89	-379	.140	.128	.117	.106	.094	.083	.071	.060	.049	1.037
90	1.423	1.184	1.172	1.161	1.149	1.138	1.127	1.115	1.104	1.092	1.081
91	.469	.229	.217	.206	.195	.183	.172	.160	.149	.138	.126
92	.515	.275	.264	.252	.241	.230	.218	.207	.195	.184	.172
93 94	.612	·323 ·372	.360	-349	.337	.277 .326	.315	.254	.243	.231	.220
95	1.662	1.422	1.411	1.399	1.388	1.376	1.365	1.353	1.342	1.330	1.310
96	.714	.474	.462	.451	.439	.428	.416	.405	393	.382	.371
97	.767	.527	.515	.504	-492	.481	.469	.458	.446	·435	.423
98	.822	.581	.570	.558	.547	·535	.524	.512	.501	.489	.478
99	.878	.637	.625	.614	.602	.591	.580	.568	-557	.545	-534
101	1.936 -994	1.694	1.683	1.671	1.660	1.648	1.637	1.625	1.614	1.602	1.591
101	2.055	·753	.742 .802	.730	.719 .779	.707 .767	.696 .756	.684 ·744	.673 ·733	.661 .721	.650
103	.117	.875	.864	.852	.841	.829	.818	.806	·733	.783	.772
104	.181	.939	.928	.916	.905	.893	.882	.870	.858	.847	.835
105	2.246	2.004	1.993	1.981	1.970	1.958	1.947	1.935	I.024	1.912	1.901
106	.314	.071	2.060	2.048	2.037	2.025	2.014	2.002	.991	.979	.968
107	.382 ·453	.140	.129 .199	.117	.105 .176	.094	.082	.071	2.059	2.048	2.036
100	.525	.283	.271	.260	.248	.236	.153	.141	.130	.118	.107
110	2.500	2.357	2.345	2.334	2.322	2.310	2.299	2.287	2.276	2.264	2.253
110	$\Delta e \times \Delta B$			+.0089	-		+.0100			+.0112	
						,	, .0100	1.0104	,.0100	1.0112	0110

Values of $e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 3^2}{1571}\right)$ B = 30.00

					B = 30	-			:-		
t'						t-t'					
	0.0	31	32	33	34	35	36	37	38	39	40
F.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inche
60°	$\Delta e \times \Delta B$	+.0116	+.0120	+.CI 23	+.0127	+.0131	+.0134	+.0138	+.0142	+.0146	+.01
60°	0.522	0.175	0.163	0.152	0.141	0.130	0.119	0.107	0.096	0.085	0.07
61	.541	.193	.182	.171	.16c	.148	.137	.126	.115	.104	.09
62	.560	.213	.201	.190	.179	.168	.156	.145	.134	.123	.II
63	.580	.232	.22I	.210	.100	.188	.176	.165	.154	.143	.13
64	.601	.253	.242	.231	.219	.208	.197	.186	.174	.163	.15
65	.623	.274	.263	-252	.240	.229	.218	.207	.195	.184	.17
66	.645	.296	.285	.274	.262	.251	.240	.229 .251	.217	.206	.19
67 68	.667 .691	.318	.307	.296	.308	.273	.285	.274	.263	.252	.21
69	.715	.366	-354	.343	.332	.321	.309	.208	.287	.275	.26
70	.740	.300	-379	.368	-357	•345	-334	.323	.311	.300	.28
71	.766	.416	.404	-393	.382	.371	.359	.348	-337	.325	.31
72	.792	.442	.431	.410	.408	.397	.385	.374	.363	•352	-34
73	.819	.460	.458	.446	.435	.424	.412	.401	.390	.379	.36
74	.847	.496	.485	-474	.463	.451	.440	.429	.418	.406	.39
75	.876	-525	.514	.503	.491	.480	.469	.457	.446	-435	.42
76	.906	-555	-543	.532	.521	.509	.498	.487	.476	.464	•45
77	.936	.585	.574	.562	.551	.540	-529	.517	.506	-495	.48
78	.968	.616	.605	-594	.582	.571	.56c	.548	.537	.526	.51
79	1.000	.649	.637	.626	.615	.603	-592	.581	.569	.558	-54
80	1.033	.682	.670	.659	.648	.636	.625	.614	.602	.591	.58
81	.068	.716	.704	.693	.682	.670	.650	.648	.636	.625	.61
82	.103	.751	.739	.728	.717	.705	.694	.683	.671	. 660	.64
83	.139	.787	.775	.764	.753	.741	.730	.719	.707	.696	.68
84	.176	.824	.813	.801	.790	.778	.767	.756	.744	.733	.72
85	1.215	.862	.851	.839	.828	.817	.805	.794	.782	.77I	.76
86	.254	.901	.890	.878	.867	.856	.844	.833	.822	.810	•79
87	.295	.042	.930	.919	.907	.896	.885	.873	.862	.850	.83
88	.336	.983	-972	.960	.949	.937	.926	.915	.903	.892	.88
89	-379	1.026	1.014	1.003	.991	.980	.969	-957	.946	.934	.92
90	1.423	1.069	1.058	1.047	1.035	1.024	1.012	1.001	.990	.978	96
91	.469	.115	.103	.002	.08c	.069	.058	.046	1.035	.070	.05
92	.515	.161	.150	.138 .186	.174	.115	.151	.140	.128	.117	.10
93	.563 .612	.257	.197 .246	.234	.223	.212	.200	.180	.177	.166	.15
94		1.308	1.206	1.285	1.273	1.262	1.250	1.230	1.227	1,216	1.20
95 96	1.662 .714	·359	.348	.336	.325	.313	.302	.290	.279	.267	.25
	.767	.412	.401	.389	.378	.366	.355	.343	.332	.320	.30
97 98	.822	.466	.455	.443	.432	.420	.400	.398	.386	-375	.36
99	.878	.522	.511	•499	.488	.476	.465	.453	.442	.430	.41
100	1.936	1.579	1.568	1.556	1.545	1.533	1.522	1.510	1.499	1.488	1.47
101	.994	.638	.627	.615	.604	.592	.581	.569	.558	.546	-53
102	2.055	.698	.687	.675	.664	.652	.641	.629	.618	.606	.59
103	.117	.760	.749	.737	.720	.714	.703	.691	.680	.668	.65
104	.181	.824	.812	.801	.789	.778	.766	-755	.743	.732	.72
105	2.246	1.889	1.878	1.866	1.855	1.843	1.832	1.820	1.808	1.797	1.78
100	.314	.956	-945	.933	.922	.910	.898	.887	.875	.864	.85
107	.382	2.025	2.013	2.002	.990	-979	.907	-955	.944	.932	.92
108	-453	.005	.084	.072	2.060	2.049	2.037	2.026	2.014	2.003	.99
100	2.525	2.167	2.156	2.144	2.133	2.121	2.109	2.098	2.086	2.075	2.06
110	$\Delta e \times \Delta B$	+.0119	+.0123	+.0127	+.0131	+.c135	+.0130	+.0143	+.0146	+.0150	+.01
				l							

Values of
$$e = e' - 0.000367 B (t - t') \left(1 + \frac{t' - 32}{1571} \right)$$

 $B = 30.00$

	1				-	t-t'					
t'	0.0	41	42	43	44	45	46	47	48	49	50
F. 60°	Inches. $\Delta e \times \Delta B$	Inches.	Inches.	Inches. +.0161	Inches. +.0164	Inches. +.0168	Inches. +.0172	Inches. +.0176	Inches. +.0170	Inches. +.0183	Inches. +.0187
60°	0.522	0.063	0.051	0.040	0.020	0.018	0.007				
61 62	.541	.081	.070	.059	.048	.036	.025	.033	0.003	0.011	
63 64	.580 .601	.120 .141	.100	.co8	.087	.075	.064	.053	.042 .c62	.030	0.019
65	.623	.162	.150	.139	.128	.117	.105	.094	.083	.072	.061
66 67	.645 .667	.184	.172	.161	.150	.139	.127	.116 .138	.105 .127	.094	.105
68	.691	.229	.218	.207	.195	.184	.173	.162	.150	.139	.128
69	.715	.253	.242	.230	.219	.208	.197	.185	.174	.163	.152
70	.740	.278	.266	.255	.244	.232	.221	.210	.100	.187	.176
71 72	.766 .792	.303	.292	.280 .306	.269	.258	.246	.235	.224	.213	.201
73	.819	.356	-345	-333	.322	.311	.299	.288	.277	.266	.254
74	.847	.384	.372	.361	-350	.338	-327	.316	.304	.293	282
75	.876	.412	.401	.390	.378	.367	.356	-344	•333	.322	.310
76	.9c6 .936	.442	.430 .461	.419	.408	.396	.385	·374	.362 .393	.351	.340
77 78	.968	.503	.492	.480	.469	.458	.446	.435	.424	.412	.401
79	1.000	-535	.524	.513	.501	.490	.478	.467	.456	•444	•433
80	1.033	.568	-557	.546	∙534	.523	.511	.500	.489	-477	.466
81 82	.068	.602 .637	.591 .626	·579 .614	.568 .603	·557	·545	•534 •569	.523 .558	.511 .546	.500 ·535
83	.139	.673	.662	.650	.639	.628	.616	.605	.594	.582	.571
84	.176	.710	.699	.687	.676	.665	.653	.642	.631	.619	.608
85	1,215	.748	.737	-725	.714	.703	.691	.680	.669	.657	.646
86 87	.254	.787 .828	.776 .816	.765 .805	·753	.742 .782	.730	.719 ·759	.708	.696 •737	.685
88	.336	.869	.858	.846	.835	.823	.812	.801	.789	.778	.766
89	·379	.912	.900	.889	.877	.866	.855	.843	.832	.820	.809
90	1.423	.955	.944	.932	.921	.910	.898	.887	.875	.864	.853
91	.469	1.000	.989	.978	.966 1.012	.955 1.001	.943	.932	.920 .967	.9 0 9	.898
92 93	.515 .563	.004	.083	.071	.c6o	.048	1.037	1.025	1.014	1.003	.991
94	.612	.143	.131	.1 20	.100	.c97	.086	.074	.c63	.051	1.040
95	1.662	1.193	1.182	1.170	1.159	1.147	1.136	1.124	1.113	I.ICI	1.090
96	.714	.244	.233	.222	.210	.199	.187	.176	.164	.153	.141
97 98	.767 .822	.297	.340	.274	.263	.251	.240	.283	.217	.260	.248
99	1.878	1.407	1.396	1.384	1.373	1.361	1.350	1.338	1.327	1.316	1.304
100	$\Delta e \times \Delta B$	+.0157	+.0161	+.0165	+.0168	+.0172	+.0176	+0.180	+.0184	+.0188	+.0191

Values of
$$e = e' - 0.000367 B (t-t') \left(1 + \frac{t' - 32}{1571}\right)$$

 $B = 30.00$

t'	t-t'											
	0.0	51	52	53	54	55	56	57	58	59	60	
F. 70°	Inches. $\Delta e \times \Delta B$	Inches. +.0192	Inches. +.0195	Inches. +.0199	Inches. +.0203	Inches. +.0207	Inches. +.0210	Inches. +.0214	Inches. +.0218	Inches. +.0222	Inches. +.0226	
62°	0.560 .580	0.008										
64	.601	0.028	0.017	0.006								
65 66	.623 .645	.040	.038	.027	0.016	0.004 .026	0.015	0.001				
67 68	.667	.093	.082	.071	.060	.048	.037	.026	0.015	0.003		
69	.691 .715	.116	.105	.004	.106	.071	.060	.049 .073	.038	.050	.039	
70	.740	.165	.154	.142	.131	.120	.108	.097	.086	.075	.063	
7 I 7 2	.766 .792	.190	.179 .205	.167 .194	.156 .182	.145 .171	.134	.122	.111	.100	.089	
73 74	.819 .847	.243 .271	.232	.220	.209	.198	.186	.175	.164 .191	.153	.141	
75	.876 .906	.299	.288	.276 .306	.265	.254 .283	.243	.231	.220	.209	.197	
76 77 78	.936	-359	-347	.336	.325	.313	.302	.291	.279	.268	.257	
78 79	.968 1.000	.390	.378	.367 .399	.356 .388	·344 .376	·333 ·365	·322 ·354	.310 .342	.299 .331	.288	
80 81	1.03,3	·455	·443 ·477	·432	.421 ·455	.409 •443	.398	.387	•375 •400	.364	·353 .386	
82	.103	-524	-512	.501	.489	.478	.467	.455	-444	.433	.421	
83 84	.139 .176	•559 •596	.548 .585	·537 ·574	.525 .562	.514	.503	.491 .528	.480 .517	.469	∙457 •494	
85 86	1.215	.634	.623 .662	.612 .651	.600 .639	.589	.578	.566	·555 ·594	·543 ·582	·532	
87	.254 .295	.714	.702	.691	.680	.668	.657	.645	.634	.623	.611	
88 89	.336 1.379	·755 0.798	·744 o.786	.732 0.775	.721 0.763	.709 0.752	.698	.687 0.729	.675 0.718	.664 0.706	.652 0.695	
90	$\Delta e \times \Delta B$	+.0194	+.0198	+.0202	+.0205	+.0209	+.0213	+.0217	+.0221	+.0225	+.0228	

RELATIVE HUMIDITY. TEMPERATURES FAHRENHEIT.

Air Temper- ature.	RELATIVE HUMIDITY, OR PERCENTAGE OF SATURATION.										
	10	20	30	40	50	60	70	80	90	100	
F.	Vapor pressure (inches).										
-30°	0.0007	0.0014	0.0021	0.0028	0.0035	0.0042	0.0049	0.0056	0.0063	0.0071	
20	.0007	.0015	.0022	.0030	.0037	.0045	.0052	.0060	.0067	.0075	
28	8000.	.0016	.0024	.0032	.0040	.0048	.0056	.0068	.0072	.0080	
26	.0000	.0017	.0023	.0034	.0042	.0051	.0059	.0072	.0070	.0084	
-25	0.0010	0.0010	0.0020	0.0038	0.0048	0.0057	0.0067	0.0076	0.0086	0.0005	
24	.0010	.0020	.0030	.0040	.0050	.0060	.0071	.0081	.0001	.0101	
23	1100.	.002 I	.0032	.0043	.0053	.0064	.0075	.0086	.0096	.0107	
22 2I	.0011	.0023	.0034	.0048	.0057	.0068	.0079	.0001	.0102	.0113	
	ı						.0084		.0108	.0120	
-20 10	.0013	.0025	0.0038	.0051	.0067	0.0076	0.0089	.0102	.0114	0.0127	
18	.0013	.0027	.0043	.0057	.0071	.0081	.0100	.0114	.0121	.0135	
17	.0015	.0030	.0045	.0060	.0076	.0001	.0106	.0121	.0136	.0151	
16	.0016	.0032	.0048	.0064	.0080	.0096	.0112	.0128	.0144	.0160	
-15	0.0017	0.0034	0.0051	0.0068	0.0084	0.0101	0.0118	0.0135	0.0152	0.0169	
1.4	.0018	.0036	.0054	.0071	.0089	.0107	.0125	.0143	.0161	.0179	
13	.0019	.0038	.0057	.0076	.0094	.0113	.0132	.0151	.0170	.0189	
12 11	.0020	.0040	.0060	.0080	.0100	.0120	.0140	.0160	.0180	.0200	
~10	0.0022	0.0045	0.0067	0.0080	0.0112	0.0134	0.0156	0.0178	0.0201		
9	.0024	.0047	.0071	.0004	.0118	.0141	.0165	.0188	.0212	.0223	
8	.0025	.0050	.0075	.0000	.0124	.0149	.0174	.0199	.0224	.0249	
7 6	.0026	.0053	.0079	.0105	.0131	.0158	.0184	.0210	.0236	.0263	
	.0028	.0055	.0083	.0111	.0139	.0166	.0194	.0222	.0249	.0277	
- 5	0.0029	0.0058	0.0088	0.0117	0.0146	0.0175	0.0205	0.0234	0.0263	0.0292	
4	.0031	.0062	.0093	.0123	.0154	.0185	.0216	.0247	.0278	.0308	
3 2	.0033	.0065	.0098	.0130	.0163	.0195	.0228	.0260	.0293	.0325	
I	.0036	.0072	.0103	.0145	.0181	.0217	.0253	.0274	.0309	.0343 .0361	
±0	0.0038	0.0076	0.0114	0.0152	0.0100	0.0220	0.0267	0.0305	0.0343	0.0381	
1	.0040	.0080	.0120	.0161	.0201	.0241	.0281	.0321	.0361	.0401	
2	.0042	.0085	.0127	.0169	.0211	.0254	.0296	.0338	.0380	.0423	
3	.0044	.0089	.0134	.0178	.0222	.0267	.0312	.0356	.0400	.0445	
4	.0047	.0094	.0141	.0187	.0234	.0281	.0328	.0375	.0422	.0468	
5	0.0049	0.0099	0.0148	0.0197	0.0247	0.0296	0.0345	0.0394	0.0444	0.0493	
6	.0052	.0104	.0156	.0208 .0218	.0259	.0311	.0363	.0415	.0467	.0519	
7 8	.0055	.0109	.0104	.0218	.0273	.0328	.0382	.0437	.0491	.0546	
9	.0060	.0121	.0181	.0241	.0302	.0362	.0402	.0483	.0543	.0604	
10	0.0063	0.0127	0.0100	0.0254	0.0317	0.0381	0.0444	0.0508	0.0571	0.0635	
11	.0067	.0133	.0200	.0267	.0334	.0400	.0467	.0534	.0600	.0667	
12	.0070	.0140	.0210	.0280	.0350	.0421	.0491	.0561	.0631	.0701	
13	.0074	.0147	.0221	.0295	.0368	.0442	.0515	.0589	.0663	.0736	
14	.0077	.0155	.0232	.0309	.0387	.0464	.0541	.0619	.0696	.0773	
15	0.0081	0.0162	0.0244	0.0325	0.0406	0.0487	0.0568	0.0650	0.0731	0.0812	
16 17	.0085	.0170 .0179	.0256	.0341	.0426	.0512	.0597 .0626	.0682	.0767	.0852	
18	.0004	.0188	.0282	.0376	.0470	.0563	.0657	.0751	.0845	.0093	
19	.0099	.0197	.0296	.0394	.0493	.0591	.0690	.0788	.0887	.0985	
20	0.0103	0.0207	0.0310	0.0413	0.0517	0.0620	0.0723	0.0827	0.0930	0.1033	

RELATIVE HUMIDITY. TEMPERATURES FAHRENHEIT.

Air											
Temper- ature,	RELATIVE HUMIDITY, OR PERCENTAGE OF SATURATION.										
	10	20	30	40	50	60	70	80	90	100	
F.	Vapor pressure (inches).										
20°	0.010	0.021	0.031	.043	0.052	0.062 .065	0.072 .076	0.083	0.093	0.103	
22 23	.011 .012	.023 .024 .025	.034	.045 .048 .050	.057 .060 .062	.068 .071 .075	.080 .083 .087	.091	.102 .107	.114	
24 25 26	0.013	0.026	0.039	0.052	0.065	0.078	0.092	0.105	0.118	0.131	
27 28	.014	.029	.043	.057	.072	.086	.100	.115	.129	.143	
29 30	.016	0.033	.047	.063 0.066	.079 0.082	.094	0.115	.126	0.148	0.165	
31 32	.017	.034	.052	.069 .072	.086	.103	.121	.138	.155	.172	
33	.019	.038	.056	.075	.098	.113	.131	.150	.169	.188	
35 36 37	.021 .022	.041 .042	.061 .064 .066	0.081 .085 .088	0.102 .106	0.122 .127 .132	0.142 .148 .154	0.163 .169 .176	0.183	0.203	
38 39	.023	.046	.069 .071	.092	.115	.137	.160	.183	.206	.229	
40 41	0.025	0.050 .052	0.074	0.009	0.124	0.149	0.173	0.198 .206	0.223	0.248	
42 43 44	.027 .028 .029	.054 .056 .058	.080 .083 .087	.107	.134 .139 .145	.161 .167 .173	.187 .195	.214 .223 .231	.24 I .250 .260	.268 .278 .289	
45 46	0.030	0.060	c.090 .094	0.120	0.150	0.180	0.210	0.240	0.270	0.300	
47 48 49	.032 .034 .035	.065 .067 .070	.097 .101 .105	.130 .135 .140	.162 .168 .175	.194	.227 .236 .245	.259 .269 .279	.292 .303 .314	.324 .336 .349	
50	0.036	0.073 .075	0.109	0.145	0.181	0.218	0.254	0.290	0.326	0.363	
5 ² 53	.039 .041	.078 .081 .084	.117	.156 .162 .168	.195	.234 .243 .252	.273 .284 .294	.312 .324 .336	.351 .365 .378	.390 .405 .420	
54 55 56	0.044	0.087	0.131	0.174	0.218	0.262	0.305	0.349	0.392	0.436 •452	
57 58	.047 .049	.094	.141	.187 .194	.234	.281	.328	·375 ·389	.422 .437	.469 .486	
59 60	0.052	0.104	0.157	0.200	0.261	.302	·353 o.365	.403	·453 0.470	0.522	
61 62 63	.054 .056 .058	.108	.162 .168 .174	.216	.270 .280 .200	·325 ·336 ·348	.379 .392 .406	.433 .448 .464	.487 .504 .522	.541 .560 .580	
64	.060	.120	.180	.241	.301	.361	.421	0.498	0.560	0.623	
66 67	.064 .067	.129	.103	.258	.322	.387	.451 .467	.516 ·534	.580 .601	.645 .667	
68 69	.069 .072	.138	.207	.276 .286	·345 ·358	.415 .429	.484	•553 •572	.622	.691	
70	0.074	0.148	0.222	0.296	0.370	0.444	0.518	0.592	0.666	0.740	

RELATIVE HUMIDITY. TEMPERATURES FAHRENHEIT.

Air Temper- ature.]	RELATIVE	HUMIDI	TY, OR P	ERCENTA	GE OF SA	TURATION	V.	
	10	20	30	40	50	60	70	80	90	100
F.					Vapor pres	sure (inches	s).			
70° 71 72 73 74	0.074 .077 .079 .082 .085	0.148 .153 .158 .164 .169	0.222 .230 .238 .246 .254	0.296 .306 .317 .328 .339	0.370 .383 .396 .410	0.444 .459 .475 .491 .508	0.518 .536 .554 .573 .593	0.592 .612 .634 .655 .678	0.666 .689 .713 .737 .762	0.740 .766 .792 .819 .847
75 76 77 78 79	0.088 .091 .094 .097	0.175 .181 .187 .194 .200	0.263 .272 .281 .290 .300	0.350 .362 .374 .387 .400	0.438 .453 .468 .484 .500	0.526 .543 .562 .581 .600	0.613 .634 .655 .677 .700	0.7CI .724 .749 .774 .800	0.788 .815 .843 .871	0.876 .906 .936 .968 1.000
80 81 82 83 84	0.103 .107 .110 .114	0.207 .214 .221 .228 .235	0.310 .320 .331 .342 .353	0.413 .427 .441 .456 .471	0.517 -534 -551 -570 -588	0.620 .641 .662 .684 .706	0.723 ·747 ·772 ·797 .824	0.827 .854 .882 .911	0.930 .961 .993 1.025 1.059	1.033 1.068 1.103 1.139 1.176
85 86 87 88 89	.125 .129 .134 .138	0.243 .251 .259 .267 .276	0.364 .376 .388 .401 .414	0.486 .502 .518 .535 .552	0.607 .627 .647 .668 .690	0.729 •753 •777 .802 .828	0.850 .878 .906 .936 .966	0.972 1.003 1.036 1.069 1.104	1.093 1.129 1.165 1.203 1.241	1.215 1.254 1.295 1.336 1.379
90 91 92 93 94	0.142 .147 .152 .156 .161	0.285 .294 .303 .313 .322	0.427 .441 .455 .469 .484	0.569 .588 .606 .625 .645	0.712 ·734 ·758 ·782 .806	0.854 .881 .909 .938 .967	0.996 1.028 1.061 1.094 1.128	1.130 1.175 1.212 1.250 1.290	1.281 1.322 1.364 1.407 1.451	1.423 1.469 1.515 1.563 1.612
95 96 97 98 99	0.166 .171 .177 .182 .188	•343 •353 •364 •376	0.499 .514 .530 .547 .563	0.665 .686 .707 .729 .751	0.831 .857 .884 .911	0.998 1.029 1.060 1.093 1.127	1.164 1.200 1.237 1.275 1.315	1.330 1.371 1.414 1.458 1.502	1.496 1.543 1.591 1.640 1.690	1.662 1.714 1.767 1.822 1.878
100 101 102 103 104	0.194 .199 .206 .212 .218	0.387 •399 •411 •423 •436	0.581 .598 .616 .635 .654	0.774 .798 .822 .847 .872	0.968 .997 1.028 1.059 1.090	1.161 1.197 1.233 1.270 1.309	1.355 1.396 1.438 1.482 1.527	1.548 1.596 1.644 1.694 1.745	1.742 1.795 1.850 1.905 1.963	1.936 1.994 2.055 2.117 2.181
105 106 107 108 109	0.225 .231 .238 .245 .253	0.449 .463 .476 .491 .505	0.674 .694 .715 .736 .758	0.899 .925 .953 .981	1.123 1.157 1.191 1.226 1.263	1.348 1.388 1.429 1.472 1.515	1.572 1.610 1.668 1.717 1.768	1.797 1.851 1.906 1.962 2.020	2.022 2.082 2.144 2.208 2.273	2.246 2.314 2.382 2.453 2.525
110 111 112 113 114	0.260 .268 .275 .283 .292	0.520 ·535 ·551 ·567 ·583	0.780 .803 .826 .850 .875	1.040 1.070 1.101 1.133 1.166	1.300 1.338 · 1.377 1.417 1.458	1.560 1.605 1.652 1.700 1.749	1.820 1.873 1.927 1.983 2.041	2.080 2.140 2.203 2.267 2.332	2.339 2.408 2.478 2.550 2.624	2.599 2.676 2.754 2.833 2.915
115 116 117 118 119	0.300 .309 .317 .326 .336	0.600 .617 .635 .653 .671	0.900 .926 .952 .979 1.007	1.200 1.234 1.260 1.305 1.342	1.500 1.543 1.587 1.632 1.678	1.800 1.851 1.904 1.958 2.014	2.100 2.160 2.221 2.285 2.349	2.399 2.468 2.539 2.611 2.685	2.699 2.777 2.856 2.937 3.021	2.999 3.085 3.173 3.264 3.356
120	0.345	0.6gc	1.035	1.380	1.725	2.071	2.416	2.761	3.106	3.451

REDUCTION OF PSYCHROMETRIC OBSERVATIONS.

METRIC MEASURES.

Values of e = e' - 0.000660 B (t - t') (1 + 0.00115 t')

Temper- ature.				PRESSI	URE OF	AQUEOU	JS VAPO	R, e.			
	0	1	2	3	4	5		6	7	8	9
C. -50° 40 30	mm. 0.029 0.096 0.288	mm. 0.026 0.086 0.259	mm. 0.023 0.076 0.233	mm. 0.020 0.068 0.209	mm. 0.01 0.06 0.18	0.0	15 o. 54 o.	013 0	mm. 0.012 0.042 0.135	mm. 0.010 0.037 0.121	mm. 0.009 0.033 0.108
	· · · · · · · ·		e = c'		60 B (t	, ,	+0.001	115 t')			
t'						t-t'					
	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
°. −30°	$\Delta e \times \Delta B$	mm. +0.006	mm. +0.013	mm. +0.019	mm. +0.025	mm. +0.032	mm. +0.038	mm. +0.045	mm. +0.051	mm. +0.057	mm. +0.064
-30° 29 28 27 26	0.288 .319 .354 .392 .434	0.239 .271 .306 .344 .385	0.191 .222 .257 .295 .337	0.143 .174 .208 .246 .288	0.094 .125 .160 .198	0.046 .077 .111 .149	0.028 .063 .101	0.014 .052 .093	0.003		
-25 24 23 22 21	0.480 .530 .585 .646	0.431 .482 .537 .597 .663	0.383 .433 .488 .548	0.334 .384 .439 .499 .565	0.285 •335 •390 •450	0.236 .286 .341 .401	0.188 .238 .292 .352 .418	0.139 .189 .244 .303	.140 .195 .254	.091	0.043 .097 .157 .222
-20 19 18 17	0.783 .862 .947 1.041	0.734 .813 .898 .991 1.093	0.685 .764 .849 .942 1.044	0.636 .715 .800 .893	0.587 .666 .751 .844 .945	0.538 .616 .702 .795 .896	0.489 .567 .653 .746 .847	0.440 .518 .604 .696		.420 .505 .598	0.293 .371 .456 .549 .650
-15 14 13 12	1.252 1.373 1.503 1.644 1.798	1.203 1.323 1.453 1.595 1.748	1.154 1.274 1.404 1.545 1.699	1.105 1.225 1.355 1.496 1.649	1.055 1.175 1.305 1.447 1.600	1.006 1.126 1.256 1.397 1.550	1.076 1.206 1.348	C.907 1.027 1.157 1.298 1.451	0.858 .978 1.108 1.249 1.402	.928 1.058 1.199	0.760 .879 1.009 1.150 1.303
-10 9 8 7 6	1.964 2.144 2.340 2.550 2.778	1.915 2.095 2.290 2.501 2.729	1.865 2.045 2.240 2.451 2.670	1.816 1.996 2.190 2.401 2.629	1.766 1.946 2.141 2.351 2.570	1.716 1.896 2.001 2.302 2.529	1.667 1.847 2.041 2.252 2.480	1.617 1.797 1.992 2.202 2.430	1.568 1.747 1.942 2.152 2.380	1.698 1.892 2.103	1.468 1.648 1.843 2.053 2.280
-5 -5	3.025 $\Delta e \times \Delta B$	2.975	2.925	2.875	2.825 +0.026	2.775 +0.033	2.726 +0.039	2.676 +0.046	2.626 +0.052	,	2.526 +0.066

REDUCTION OF PSYCHROMETRIC OBSERVATIONS. METRIC MEASURES.

Values of e = e' - 0.000660 B (t - t') (1 + 0.00115 t')

B = 760 mm.

l t'						t-t'					
	0.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0
C. -20°	mm. $\Delta e \times \Delta B$	mm. +0.071	mm. +0.077	mm. +0.084	mm. +0.090	mm. +0.097	mm. +0.103	mm. +0.110	mm. +0.116	mm. +0.123	mm. +0.129
-25° 24 23 22 21	0.480 .530 .585 .646	0.048	0.059								
-20 19 18 17 16	.783 .862 .947 1.041	.244 .322 .407 .500	.273 .358 .450	.224 .309 .401	.097 .175 .260 .352 .453	.303	0.077 .161 .254	.112	0.063 .155 .256	0.014 .106	0.057
-15 14 13 12 11	1.252 1.373 1.503 1.644 1.798	.710 .830 .959 1.100	.780 .910		.562 .682 .811 .952	.513 .632 .762 .902 1.055	.583 .712 .853	.414 .534 .663 .803	.365 .484 .614 .754	.316 .435 .564 .705 .857	.267 .386 .515 .655
-10 9 8 7 6	+1.964 2.144 2.340 2.550 2.778	1.419 1.598 1.793 2.003 2.231	1.549	1.320 1.499 1.693 1.904 2.131	1.270 1.450 1.644 1.854 2.081	1.221 1.400 1.594 1.804 2.031	1.544	1.495	1.072 1.251 1.445 1.655 1.882	1.022 1.201 1.395 1.605 1.832	.973 1.152 1.346 1.555 1.782
-5 -5	3.025 $\Delta e \times \Delta B$	2.476	2.426	2.376	2.327 +0.092	2.277			2.127	2.077	2.027
	20/20	10.072	10.079	10.003		t-t'	70.103	70.112	70.116	70.123	+0.131
t'	0.0	2.1	2.2	2.3	2,4	2.5	2.6	2.7	2.8	2.9	3.0
C. -15°	mm. $\Delta \varepsilon \times \Delta B$	mm. +0.136	mm. +0.143	mm. +0.149	mm. +0.156	mm. +0.162	mm. +0.169	mm. +0.175	mm. +0.182	mm. +0.188	mm. +0.195
-17°	1.041 1.142	0.008	0.059	0.010							
-I5 14 13 12 11	1.252 1.373 1.503 1.644 1.798	0.217 .336 .465 .606 .758	.168 .287 .416 .556 .708	.119 .237 .366 .507 .659	0.069 .188 .317 .457 .609	0.020 .139 .268 .408	0.089 .218 .358 .510	0.040 .169 .309 .461	0.119 .259 .411	0.070 .210 .362	0.021 .160 .312
-10 9 8 7 6	1.964 2.144 2.340 2.550 2.778	.923 1.102 1.296 1.506 1.732	.873 1.052 1.246 1.456 1.683	.824 1.003 1.196 1.406 1.633	.774 .953 1.147 1.356 1.583	.725 .903 1.097 1.307 1.533	.675 .854 1.047 1.257 1.483	.626 .804 .998 1.207	.576 .755 .948 1.157 1.384	.526 .705 .898 1.108 1.334	.477 .655 .849 1.058 1.284
- 5 - 5	3.025 $\Delta e \times \Delta B$	1.977 +0.138	1.928 +0.144	1.878 +0.151	1.828 +0.157	1.778 +0.164	1.728 +0.171	1.678 +0.177	1.628 +0.184	1.579 +0.190	1.529 +0.197

REDUCTION OF PSYCHROMETRIC OBSERVATIONS.

METRIC MEASURES.

Values of $e=e'-0.000660\ B\ (t-t')\ (1+0.00115\ t')$ $B=760\ {\rm mm}.$

					t	- t'				
<i>t'</i>	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	4.0
0. -10° Δe×ΔB	mm. +0.202	mm. +0.209	mm. +0.215	mm. +0.222	mm. +0.228	mm. +0.235	mm, +0.241	mm, +0.248	mm. +0.254	mm. +0.261
-12°	0.111 .263	0.061	0.012 .164	0.114	0.065	0.015				
-10 9 8 7 6	.427 .606 .799 1.008	.378 .556 .749 .958 1.184	.328 .506 .699 909	.278 .457 .650 .859	.229 .407 .600 .809	.179 •357 •550 •759 •985	0.130 .308 .501 .710	0.080 .258 .451 .660	.209	0.159 .352 .560 .786
-5	1.479	1.429	1.379	1.329	1.279	1.229	1.180	1.130	1.080	1.030
$-5 \Delta e \times \Delta B$	+0.203	+0.210	+0.217	+0.223	+0.230	+0.236	+0.243	+0.249	+0.256	+0.262
t'					t -	- t'				
	4.1	4.2	4.3	4.4	4.5	4.6	4.7	4.8	4.9	5.0
C. -8° Δe×ΔB	mm. +0.268	mm. +0.275	mm. +0.281	mm. +0.288	mm. +0.294	mm. +0.301	mm. +0.307	mm. +0.314	mm. +0.320	mm. +0.327
-9° 8 7 6	0.109 0.302 .510 .736	0.060 0.252 .461 .686	0.010 .202 .411 .637	0.153 .361 .587	0.103 .311 .537	0.053 .262 .487	0.004 .212 ·437	0.162 .387	0.112	0.063
-5	0.980	0.930	0.880	0.830	0.781	0.731	0.681	0.631	0.581	0.531
$-5 \Delta e \times \Delta B$	+0.269	+0.276	+0.282	+0.289	+0.295	+0.302	+0.308	+0.315	+0.322	+0.328
t'					1-	- t'				
	5.1	5.2	5.3	5-4	5.5	5.6	5.7	5.8	5.9	6.0
C. -7° 6	mm. 0.013	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.	mm.
-5	0.481	0.431	0.382	0.332	0.282	0.232	0.182	0.132	0.082	0.033
$-5 \Delta e \times \Delta B$	+0.335	+0.341	+0.348	+0.354	+0.361	+0.367	+0.374	+0.381	+0.387	+0.394

REDUCTION OF PSYCHROMETRIC OBSERVATIONS. METRIC MEASURES.

Values of e = e' - 0.000660 B (t - t') (1 + 0.00115 t')

B = 760 mm.

							t-t'					
	t'	0	1	2	3	4	5	6	7	8	9	10
	C. -5°	mm. $\Delta e \times \Delta B$	mm. +0.07	mm. +0.13	mm, +0.20	mm. +0.26	mm. +0.33	mm. +0.30	mm. +0.46	mm. +0.52	mm. +0.50	mm. +0.66
	-5°	3.02	2.53	2.03	1.53	1.03	0.53	0.03		,	,59	
	4 3	3.29 3.58	2.79 3.08	2.29	1.79 2.08	1.29 1.58	0.79	0.29	0.08)
	2 I	3.89	3·39 3·72	2.89	2.39	1.89 2.22	1.38	0.88	0.38	0.21		
	±0	4.58	4.08	3.58	3.08	2.57	2.07	1.57	1.07	0.57	0.07	
	+1	4.92 5.29	4.42	3.92	3.42 3.78	2.92 3.28	2.41	2.27	1.41	0.91	0.40	0.26
I	3	5.68 6.10	5.18	4.68 5.09	4.17 4.59	3.67 4.08	3.17 3.58	2.66 3.07	2.16	2.07	1.15	0.65
	5	6.54	6.03	5.53	5.03	4.52	4.02	3.51	3.48	2.51	2.00	1.50
I	6 7 8	7.01 7.51	7.01	6.00	6.00	4.99 5.49	4.49 4.98	4.48	3.97	3.47	2.96	2.46
I	8 9	8.05 8.61	7.54 8.10	7.60	7.09	6.02	6.08	5.01	4.50 5.06	4.00	3.49 4.05	3.54
	10	9.21	8.70 9.34	8.20	7.69 8.32	7.18 7.81	6.67 7.31	6.80	5.66	5.15	4.64 5.27	4.14
	12	10.52	10.01	9.50	9.00	8.49 9.20	7.98 8.69	7.47 8.18	6.96 7.67	6.45 7.16	5.94 6.65	5.44 6.14
	14	11.99	11.48	10.97	10.46	9.95 10.75	9.44 10.24	8.93 9.73	8.42	7.91	7.41 8.20	6.90 7.69
	16	13.64	13.13	12.62	12.11	11.60	11.00	10.58	10.07	9.56	9.04	8.53
	17 18	14.54 15.49	14.03	13.52	13.00	12.49 13.44	11.98	11.47	10.96	11.39	9.94	9.42
	19 20	16.49 17.55	15.98	15.46 16.52	14.95 16.01	14.44	13.93 14.98	13.41	12.90	12.39	11.88	12.42
	21 22	18.66 19.84	18.15	17.64 18.82	17.12	16.61	16.10 17.27	15.58 16.76	15.07 16.24	14.56 15.73	14.04	13.53
	23	21.09	20.57	20.06	19.54	19.03	18.51	18.00	17.48	16.97	16.45 17.76	15.94
	24 25	22.40	23.26	22.75	22.23	21.72	21.20	20.68	20.17	19.65	19.14	18.62
	26 27	25.24 26.77	24.72 26.25	24.20 25.73	23.69 25.22	23.17 24.70	22.65 24.18	22.14	21.62	21.10	20.59	20.07
H	28 29	28.38 30.08	27.86 29.56	27.34 29.04	26.83 28.52	26.31	25.79 27.48	25.27 26.97	24.76 26.45	24.24 25.93	23.72 25.41	23.20
	30	31.86	31.34	30.82	30.30	29.78 31.66	29.27 31.14	28.75 30.62	28.23	27.71 20.58	27.19 20.06	
	31 32	33·74 35·70	33.22 35.18	34.66	34.14	33.62	33.10	_ 0	32.06 34.13	31.54	31.02 33.09	30.50
	33 34	37.78 39.95	37·25 39·43	36.73 38.90	36.21 38.38	35.69 37.86	35.17 37.34	36.82	36.30	35.78 38.05	35.26	
	35 36	42.23	41.71	41.18	40.66	40.14	39.62 42.01		38.57 40.96	40.44	37·53 39.92	39.40
	37 38	47.13 49.76	46.60	46.08 48.71	45.56 48.19		44.51 47.14	1 //	43.47 46.09	42.94 45.57	42.42 45.04	
	39 40	52.51 55.40	51.99	51.46 54.35	50.94 53.82	50.41	49.89	49.37	48.84 51.72	48.32 51.20		
	41	58.42	57.89	57-37	56.84	56.32	55.79	55.27	54·74 57.90	54.21 57.37	53.69 56.85	
	42 43	61.58	64.36	63.84	63.31	62.78	62.26	61.73	61.20	60.68	60.15	59.62
	44 45	68.35	67.82	67.30 70.91	66.77 70.39				1	67.75	67.22	66.69
	45	$\Delta e \times \Delta B$	+0.07	+0.14	+0.21	+0.28	+0.35	+0.42	+0.49	+0.56	+0.62	+0.69

REDUCTION OF PSYCHROMETRIC OBSERVATIONS. METRIC MEASURES.

Values of $e = e' - 0.000660 \ B \ (t - t') \ (1 + 0.00115 \ t')$ $B = 760 \ \mathrm{mm}.$

					= 700						
t'						t-t'					
	0	11	12	13	14	15	16	17	18	19	20
C. +5°	$\Delta e \times \Delta B$	mm. +0.73	mm. +0.80	mm. +0.86	mm. +0.93	mm. +1.00	mm. +1.06	mm. +1.13	mm. +1.19	mm, +1.26	mm. +1.33
+3° 4 5	5.68 6.10 6.54	0.15 0.56 0.99	0.05						3		
6 7 8 9 10	7.01 7.51 8.05 8.61 9.21	1.46 1.95 2.48 3.04 3.63	0.95 1.45 1.97 2.53 3.12	0.45 0.94 1.46 2.02 2.61	0.43 0.96 1.52 2.11	0.45 1.01 1.60	0.50	0.58	0.08		
11 12 13 14 15	9.85 10.52 11.24 11.99 12.79	4.26 4.93 5.63 6.39 7.18	3.75 4.42 5.13 5.88 6.67	3.24 3.91 4.62 5.37 6.16	2.73 3.40 4.11 4.86 5.65	2.23 2.89 3.60 4.35 5.14	1.72 2.38 3.09 3.84 4.63	1.21 1.88 2.58 3.33 4.12	0.70 1.37 2.07 2.82 3.61	0.20 0.86 1.56 2.31 3.10	0.35 1.05 1.80 2.59
16 17 18 19 20	13.64 14.54 15.49 16.49 17.55	8.02 8.91 9.86 10.85	7.51 8.40 9.34 10.34 11.39	7.00 7.89 8.83 9.83 10.88	6.49 7.38 8.32 9.31 10.36	5.98 6.87 7.81 8.80 9.85	5.47 6.36 7.30 8.29 9.34	4.96 5.85 6.78 7.78 8.82	4.45 5.33 6.27 7.26 8.31	3.94 4.82 5.76 6.75 7.80	3.43 4.31 5.25 6.24 7.29
21 22 23 24 25	18.66 19.84 21.09 22.40 23.78	13.01 14.19 15.42 16.73 18.10	12.50 13.67 14.91 16.21 17.59	11.99 13.16 14.39 15.70 17.07	11.47 12.64 13.88 15.18 16.56	10.96 12.13 13.36 14.67 16.04	10.45 11.62 12.85 14.15 15.52	9.93 11.10 12.33 13.64 15.01	9.42 10.59 11.82 13.12 14.49	8.90 10.07 11.30 12.60 13.98	8.39 9.56 10.79 12.09 13.46
26 27 28 29 30	25.24 26.77 28.38 30.08 31.86	19.55 21.08 22.68 24.37 26.15	19.04 20.56 22.17 23.86 25.63	18.52 20.04 21.65 23.34 25.11	18.00 19.53 21.13 22.82 24.60	17.49 19.01 20.61 22.30 24.08	16.97 18.49 20.10 21.78 23.56	16.45 17.98 19.58 21.26 23.04	15.94 17.46 19.06 20.75 22.52	15.42 16.94 18.54 20.23 22.00	14.90 16.42 18.02 19.71 21.48
31 32 33 34 35	33.74 35.70 37.78 39.95 42.23	28.02 29.98 32.05 34.21 36.49	27.50 29.46 31.53 33.69 35.97	26.98 28.94 31.01 33.17 35.44	26.46 28.42 30.49 32.65 34.92	25.94 27.90 29.97 32.13 34.40	25.42 27.38 29.44 31.61 33.88	24.90 26.86 28.92 31.09 33.36	24.38 26.34 28.40 30.57 32.83	23.86 25.82 27.88 30.04 32.31	23.34 25.30 27.36 29.52 31.79
36 37 38 39 40	44.62 47.13 49.76 52.51 55.40	38.87 41.37 44.00 46.74 49.62	38.35 40.85 43.47 46.22 49.10	37.83 40.33 42.95 45.70 48.58	37.31 39.81 42.43 45.17 48.05	36.78 39.28 41.90 44.65 47.53	36.26 38.76 41.38 44.12 47.00	35.74 38.24 40.86 43.60 46.48	35.22 37.71 40.33 43.08 45.95		34.17 36.67 39.29 42.03 44.90
41 42 43 44 45	58.42 61.58 64.80 68.35 71.97	52.64 55.80 59.10 62.55 66.16	52.11 55.27 58.57 62.03 65.64	51.59 54.74 58.05 61.50 65.11	51.06 54.22 57.52 60.97 64.58	50.54 53.69 56.99 60.45 64.05	50.01 53.17 56.47 59.92 63.53	49·49 52·64 55·94 59·39 63.00	48.96 52.12 55.41 58.86 62.47	48.44 51.59 54.89 58.34 61.94	47.91 51.06 54.36 57.81 61.42
45	$\Delta c \times \Delta B$	+0.76	+0.83	+0.90	+0.97	+1.04	+1.11	+1.18	+1.25	+1.32	+1.39

REDUCTION OF PSYCHROMETRIC OBSERVATIONS.

METRIC MEASURES

Values of $e = e' - 0.000660 \ B \ (t - t') \ (1 + 0.00115 \ i')$ $B = 760 \ \mathrm{mm}.$

t'		-			t	-t'					
I I	0	21	22	23	24	25	26	27	28	29	30
C. +15°	$\Delta e \times \Delta B$	mm. +1.41	mm. +1.48	mm. +1.54	mm. +1.61	mm. +1.68	mm. +1.75	mm. +1.81	mm. + 1.88	mm. +1.95	mm. +2.01
13°	11.24 11.99 12.79	0.54 1.29 2.08	0.03 0.78 1.57	0.27	0.55	0.04					
+16 17 18 19 20	13.64 14.54 15.49 16.49 17.55	2.91 3.80 4.74 5.73 6.77	2.40 3.29 4.22 5.21 6.26	1.89 2.78 3.71 4.70 5.75	1.38 2.27 3.20 4.19 5.23	0.87 1.75 2.69 3.68 4.72	0.36 1.24 2.18 3.16 4.21	0.73 1.66 2.65 3.69	0.22 1.15 2.14 3.18	0.64 1.62 2.67	0.13 1.11 2.15
J-21 22 23 24 25	18.66 19.84 21.09 22.40 23.78	7.88 9.04 10.27 11.57 12.94	7.36 8.53 9.76 11.06 12.43	6.85 8.02 9.25 10.54 11.91	6.34 7.50 8.73 10.03 11.40	5.82 6.99 8.22 9.51 10.88	5.31 6.47 7.70 9.00 10.36	4.79 5.96 7.19 8.48 9.85	4.28 5.44 6.67 7.97 9.33	3.77 4.93 6.16 7.45 8.82	3.25 4.42 5.64 6.93 8.30
+26 27 28 29 30	25.24 26.77 28.38 30.08 31.86	14.39 15.91 17.51 19.19 20.96	13.87 15.39 16.99 18.67 20.44	13.35 14.87 16.47 18.15 19.93	12.84 14.35 15.95 17.64 19.41	12.32 13.84 15.44 17.12 18.89	11.80 13.32 14.92 16.60 18.37	11.29 12.80 14.40 16.08 17.85	10.77 12.29 13.88 15.56 17.33	10.25 11.77 13.37 15.04 16.81	9.74 11.25 12.85 14.53 16.29
+31 32 33 34 35	33.74 35.70 37.78 39.95 42.23	22.83 24.78 26.84 29.00 31.27	22.31 24.26 26.32 28.48 30.75	21.79 23.74 25.80 27.96 30.23	21.27 23.22 25.28 27.44 29.70	20.75 22.70 24.76 26.92 29.18	20.23 22.18 24.24 26.40 28.66	19.71 21.66 23.72 25.87 28.14	19.19 21.14 23.20 25.35 27.62	18.67 20.62 22.68 24.83 27.10	18.15 20.10 22.16 24.31 26.57
+36 37 38 39 40	44.62 47.13 49.76 52.51 55.40	33.65 36.15 38.76 41.50 44.38	33.13 35.62 38.24 40.98 43.85	32.60 35.10 37.72 40.46 43.33	32.08 34.58 37.19 39.93 42.80	31.56 34.05 36.67 39.41 42.28	31.04 33.53 36.14 38.88 41.75	30.52 33.01 35.62 38.36 41.23	29.99 32.48 35.10 37.84 40.71	29.47 31.96 34.57 37.31 40.18	28.95 31.44 34.05 36.79 39.66
+40	$\Delta e \times \Delta B$	+1.45	+1.52	+1.59	+1.66	+1.73	+1.79	+1.86	+1.93	+2.00	+2.07
t'					t	- t'					
,		31	32	33	34	35	36	37	38	39	40
+2J°	$\Delta e \times \Delta B$	mm. +2.09	mm. +2.16	mm. +2.23	mm. +2.30	mm. +2.36	mm. +2.43	mm. +2.50	mm. +2.57	mm. +2.63	mm. +2.70
20 21 22 23		2.74 3.90 5.13	2.23 3.39 4.61	0.61 1.71 2.87 4.10	0.10 1.20 2.36 3.58	0.69 1.84 3.07	0.17 1.33 2.55	0.82	0.30	1.01	0.49
24 25 +26		6.42 7.78 9.22	5.90 7.27 8.70	5.39 6.75 8.19	4.87 6.24 7.67	4.36 5.72 7.15	3.84 5.20 6.64	3.33 4.69 6.12	2.81 4.17 5.60	2.30 3.66 5.09	1.78 3.14 4.57
27 28 29 30		10.73 12.33 14.01 15.77	10.22 11.81 13.49 15.26	9.70 11.29 12.97 14.74	9.18 10.78 12.45 14.22	8.67 10.26 11.93 13.70	8.15 9.74 11.42 13.18	7.63 9.22 10.90 12.66	7.11 8.71 10.38 12.14	6.60 8.19 9.86 11.62	6.08 7.67 9.34 11.10
+30	$\Delta e \times \Delta B$	+2.12	+2.18	+2.25	+2.32	+2.39	+2.46	+2.53	+2.59	+2.66	+2.73

RELATIVE HUMIDITY. TEMPERATURE CENTIGRADE.

Air		R	RELATIVE	нимирг	ry, or pe	CRCENTAC	GE OF SA	ruratio:	N,	
Temper- ature.	10	20	30	40	50	60	٫70	80	90	100
C.				Vap	or pressure	e (millimete	ers).			
-45° 44 43 42	10.0 10.0 10.0 10.0	0.0I 0.0I 0.0I 0.02 0.02	0.02 0.02 0.02 0.02 0.02 c.03	0. 02 0. 02 0. 03 0. 03	0. c3 0. 03 0. 03 0. 04 0. 04	0.03 0.04 0.04 0.05 0.05	0.04 0.04 0.05 0.05 0.06	0.04 0.05 0.05 0.06 0.07	0.05 0.05 0.06 0.07 0.08	0.05 0.06 0.07 0.08
41 -40 39 38 37 36	0.0I 0.0I 0.0I 0.0I 0.0I	0.02 0.02 0.02 0.02 0.03 0.03	0.03 0.03 0.04 0.04 0.05	0.03 0.04 0.04 0.05 0.05 0.06	0.05 0.05 0.05 0.06 0.07 0.08	0.05 0.06 0.06 0.07 0.08 0.09	0.07 0.08 0.08 0.00 0.11	0.07 0.08 0.00 0.10 0.11	0.00 0.10 0.11 0.12 0.14	0.09 0.10 0.11 0.12 0.14 0.15
-35 34 33 32 31	0.02 0.02 0.02 0.02 0.02	0.03 0.04 0.04 0.05 0.05	0.05 0.06 0.06 0.07 0.08	0.07 0.08 0.08 0.09 0.10	0.08 0.09 0.10 0.12 0.13	0.10 0.11 0.13 0.14 0.16	0.12 0.13 0.15 0.16 0.18	0.13 0.15 0.17 0.19 0.21	0.15 0.17 0.19 0.21 0.23	0. 17 0. 19 0. 21 0. 23 0. 26
-30 20 28 27 26	0.03 0.03 0.04 0.04 0.04	0.06 0.06 0.07 0.08 0.09	0.00 0.10 0.11 0.12 0.13	0. I 2 0. I 3 0. I 4 0. I 6 0. I 7	0. 14 0. 16 0. 18 0. 20 0. 22	0. 17 0. 19 0. 21 0. 24 0. 26	0. 20 0. 22 0. 25 0. 27 0. 30	0. 25 0. 26 0. 28 0. 31 0. 35	0. 26 0. 29 0. 32 0. 35 0. 39	0. 29 0. 32 0. 35 0. 39 0. 43
-25 24 23 22 21	0.05 0.05 0.06 0.06	0. I0 0. II 0. I2 0. I3 0. I4	0. 14 0. 16 0. 18 0. 19 0. 21	0. 19 0. 21 0. 23 0. 26 0. 28	0. 24 0. 27 0. 29 0. 32 0. 36	0. 29 0. 32 0. 35 0. 39 0. 43	0. 34 0. 37 0. 41 0. 45 0. 50	0.38 0.42 0.47 0.52 0.57	0.43 0.48 0.53 0.58 0.64	0.48 0.53 0.59 0.65 0.71
-20 19 18 17 16	0.08 0.09 0.09 0.10	0. 16 0. 17 0. 19 0. 21 0. 23	0. 24 0. 26 0. 28 0. 31 0. 34	0.31 0.34 0.38 0.42 0.46	0.39 0.43 0.47 0.52 0.57	0.47 0.52 0.57 0.62 0.69	0.55 0.60 0.66 0.73 0.80	0.63 0.69 0.76 0.83 0.91	0.71 0.78 0.85 0.94 1.03	0.78 0.86 0.95 1.04
- 15 14 13 12 11	0.13 0.14 0.15 0.16 0.18	0. 25 0. 27 0. 30 0. 33 0. 36	0.38 0.41 0.45 0.49 0.54	0.50 0.55 0.60 0.66 0.72	0.63 0.69 0.75 0.82 0.90	0.75 0.82 0.90 0.99 1.08	0.88 0.96 1.05 1.15	I.00 I.10 I.20 I.32 I.44	I. I3 I. 24 I. 35 I. 48 I. 62	1.25 1.37 1.50 1.64 1.80
- 10 9 8 7 6	0. 20 0. 21 0. 23 0. 26 0. 28	0.39 0.43 0.47 0.51 0.56	0.59 0.64 0.70 0.77 0.83	0.79 0.86 0.94 1.02	0.98 1.07 1.17 1.28 1.39	1.18 1.29 1.40 1.53 1.67	1.38 1.50 1.64 1.79 1.94	I. 57 I. 72 I. 87 2. 04 2. 22	1.77 1.93 2.11 2.30 2.50	1.96 2.14 2.34 2.55 2.78
- 5 4 3 2 1	0.30 0.33 0.36 0.39 0.42	o. 6o o. 66 o. 72 o. 78 o. 84	0.91 0.99 1.07 1.17 1.27	1.21 1.32 1.43 1.55 1.69	1.51 1.65 1.79 1.94 2.11	1.81 1.97 2.15 2.33 2.53	2. 12 2. 30 2. 50 2. 72 2. 95	2.42 2.63 2.86 3.11 3.38	2.72 2.96 3.22 3.50 3.80	3.02 3.29 3.58 3.89 4.22
± 0 + 1 2 3 4	0.46 0.49 0.53 0.57 0.61	0.92 0.98 1.06 1.14 1.22	1.37 1.48 1.59 1.70 1.83	1.83 1.07 2.12 2.27 2.44	2. 29 2. 46 2. 65 2. 84 3. 05	2.75 2.95 3.17 3.41 3.66	3. 21 3. 45 3. 70 3. 98 4. 27	3.66 3.94 4.23 4.55 4.88	4. 12 4. 43 4. 76 5. 11 5. 49	4.58 4.92 5.29 5.68 6.10
+ 5	0.65	1.31	1.96	2.62	3 . 27	3.92	4.58	5.23	5.89	6.54

RELATIVE HUMIDITY. TEMPERATURE CENTIGRADE.

Air Temper- ature.			RELATIV	E HUMII	OITY, OR	PERCEN	TAGE OF	SATURA	TION.	-
	10	20	30	40	50	60	70	80	90	100
C.				Vapor _I	oressure (m	nillimeters)				·
5° 6 7 8 9	0.7 0.7 0.8 0.8 0.9	I.3 I.4 I.5 I.6	2.0 2.1 2.3 2.4 2.6	2.6 2.8 3.0 3.2 3.4	3·3 3·5 3.8 4·0 4·3	3·9 4·2 4·5 4.8 5·2	4.6 4.9 5.3 5.6 6.0	5. 2 5. 6 6. 0 6. 4 6. 9	5.9 6.3 6.8 7.2 7.7	6.5 7.0 7.5 8.0 8.6
10 11 12 13 14	0.9 I.0 I.I I.I I.2	1.8 2.0 2.1 2.2 2.4	2.8 3.0 3.2 3.4 3.6	3·7 3·9 4·2 4·5 4.8	4.6 4.9 5.3 5.6 6.0	5·5 5·9 6.3 6.7 7·2	6.4 6.9 7.4 7.9 8.4	7·4 7·9 8·4 9.0 9.6	8.3 8.9 9.5 10.1 10.8	9. 2 9. 8 10. 5 11. 2 12. 0
15 16 17 18 19	1.3 1.4 1.5 1.5	2.6 2.7 2.9 3. I 3.3	3.8 4.1 4.4 4.6 4.9	5. I 5. 5 5. 8 6. 2 6. 6	6.4 6.8 7·3 7·7 8.2	7.7 8.2 8.7 9.3 9.9	9.0 9.5 10.2 10.8 11.5	10. 2 10. 9 11. 6 12. 4 13. 2	11.5 12.3 13.1 13.9 14.8	12.8 13.6 14.5 15.5 16.5
20 21 22 23 24	1.8 1.9 2.0 2.1 2.2	3·5 3·7 4·0 4·2 4·5	5.3 5.6 6.0 6.3 6.7	7.0 7.5 7.9 8.4 9.0	8.8 9.3 9.9 10.5 11.2	10.5 11.2 11.9 12.7 13.4	12.3 13.1 13.9 14.8 15.7	14.0 14.9 15.9 16.9 17.9	15.8 16.8 17.9 19.0 20.2	17.5 18.7 19.8 21.1 22.4
25 26 27 28 29	2.4 2.5 2.7 2.8 3.0	4.8 5.0 5.4 5.7 6.0	7. I 7. 6 8. 0 8. 5 9. 0	9.5 10.1 10.7 11.4 12.0	11.9 12.6 13.4 14.2 15.0	14.3 15.1 16.1 17.0 18.0	16.6 17.7 18.7 19.9 21.1	19.0 20.2 21.4 22.7 24.1	21.4 22.7 24.1 25.5 27.1	23.8 25.2 26.8 28.4 30.1
30 31 32 33 34	3.2 3.4 3.6 3.8 4.0	6.4 6.7 7.1 7.6 8.0	9.6 10.1 10.7 11.3 12.0	12.7 13.5 14.3 15.1 16.0	15.9 16.9 17.9 18.9 20.0	19.1 20.2 21.4 22.7 24.0	22.3 23.6 25.0 26.4 28.0	25.5 27.0 28.6 30.2 32.0	28.7 30.4 32.1 34.0 36.0	31.9 33.7 35.7 37.8 39.9
35 36 37 38 39	4.2 4.5 4.7 5.0 5.3	8.4 8.9 9.4 10.0	12.7 13.4 14.1 14.9 15.8	16.0 17.8 18.0 19.0 21.0	21. I 22. 3 23. 6 24. 9 26. 3	25.3 26.8 28.3 29.9 31.5	29.6 31.2 33.0 34.8 36.8	33.8 35.7 37.7 39.8 42.0	38.0 40.2 42.4 44.8 47.3	42. 2 44. 6 47. 1 49. 8 52. 5
40 41 42 43 44	5.5 5.8 6.2 6.5 6.8	11.1 11.7 12.3 13.0	16.6 17.5 18.5 19.5 20.5	22. 2 23. 4 24. 6 26. 0 27. 3	27.7 29.2 30.8 32.4 34.2	33.2 35.1 36.9 38.9 41.0	38.8 40.9 43.1 45.4 47.8	44.3 46.7 49.3 51.9 54.7	49.9 52.6 55.4 58.4 61.5	55.4 58.4 61.6 64.9 68.4
45 46 47 48 49	7.2 7.6 8.0 8.4 8.8	14.4 15.2 15.9 16.8 17.6	21.6 22.7 23.9 25.1 26.4	28.8 30.3 31.9 33.5 35.3	36.0 37.9 39.9 41.9 44.1	43.2 45.5 47.8 50.3 52.9	50.4 53.0 55.8 58.7 61.7	57.6 60.6 63.8 67.1 70.5	64.8 68.2 71.7 75.4 79.3	72.0 75.8 79.7 83.8 88.1
50 51 52 53 54	9·3 9·7 10.2 10.7	18.5 19.5 20.4 21.5 22.5	27.8 29.2 30.7 32.2 33.8	37. I 38. 9 40. 9 42. 9 45. I	46.3 48.7 51.1 53.7 56.3	55.6 58.4 61.3 64.4 67.6	64.8 68.1 71.6 75.1 78.9	74. I 77. 9 81. 8 85. 9 90. I	83.4 87.6 92.0 96.6 101.4	92.6 97.3 102.2 107.3 112.7
55	11.8	23.6	35.5	47 - 3	59.1	70.9	82.7	94.6	106.4	118.2

RATE OF DECREASE OF VAPOR PRESSURE WITH ALTITUDE FOR MOUNTAIN STATIONS.

(According to the empirical formula of Dr. J. Hann.)

$$\frac{e}{c} = 10 - \frac{h}{6300}$$

e, e_0 = Vapor pressures at an upper and a lower station respectively. h =Difference of altitude in meters.

Difference	of Altitude.	$\frac{\epsilon}{\epsilon_{\circ}}$.	Difference	of Altitude.	$\frac{\epsilon}{\epsilon_{\circ}}$.	Difference	of Altitude.	$\frac{e}{e_{\circ}}$.
Meters. 200 400 600 800	Feet. 656 1312 1968 2625	0. 93 .86 .80 .75	Meters. 1800 2000 2200 2400	Feet. 5905 0562 7218 7874	0. 52 . 48 . 45 . 42	Meters. 3400 3600 3800 4000	Feet. 11155 11811 12407 13123	0. 29 . 27 . 25 . 23
1000 1200 1000	3281 3937 4593 5249	0.69 .64 .60 .56	2600 2800 3000 3200	\$530 9186 9842 10499	0.30 .36 .33 .31	4500 5000 5500 6000	14764 16404 18045 19685	0.19 .16 .13 .11

TABLE 87.

DEPTH OF WATER CORRESPONDING TO THE WEIGHT OF A CYLINDRICAL SNOW CORE 2.655 INCHES IN DIAMETER. (One-fifth pound equals 1 inch.)

Weight Ibs.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
. 0	0.00	0.05	0. 10	0.15	0. 20	0.25	0.30	0.35	0. 40	0.45
. I	0.50	0.55	0.60	0.65	0.70	0.75	0.80	0.85	0.00	0.95
. 2	1.00	1.05	1.10	1.15	I. 20	1.25	1.30	1.35	1.40	1.45
- 3	1.50	1.55	1.60	1.65	1.70	I.75	1. So	1.85	1.90	1.95
.4	2.00	2.05	2.10	2.15	2.20	2.25	2.30	2.35	2.40	2.45
. 5	2.50	2.55	2.60	2.65	2.70	2.75	2.80	2.85	2.90	2.95
. 6	3.00	3.05	3.10	3.15	3.20	3.25	3.30	3.35	3.40	3 · 45
· 7	3.50	3-55	3.60	3.65	3.70	3 - 75	3.80	3.85	3.90	3.95
.0	4.00	4.05	4.10	4.15	4.70	4.25 4.75	4.80	4.35 4.85	4.40	4·45 4·95
.9	4.30	4.33	4.00	4.03	4.70	4.73	4.00	4.05	4.90	4.93
1.0	5.00	5.05	5.10	5.15	5.20	5.25	5.30	5.35	5.40	5.45
I.I	5.50	5 - 55	5.60	5.65	5.70	5.75	5.80	5.85	5.90	5.95
I.2	6.00	6.05	6.10	6.15	6. 20	6.25	6.30	6.35	6.40	6.45
1.3	6. 50 7. 00	6.55	6.60	6.65	6.70 7.20	6.75 7.25	6.80 7.30	6.85	6.90 7.40	6.95
I.4	7.00	7.05	7.10	7.15	7.20	1.25	7.30	7 · 35	7.40	7.45
5	7.50	7.55	7.60	7.65	7.70	7.75	7.So	7.85	7.90	7.95
1.6	8.00	8.05	8.10	8.15	8.20	8.25	8.30	8.35	8.40	8.45
I. 7	8.50	8.55	8.60	8.65	8.70	8.75	8.80	8.85	8.90	8.95
1.8 1.9	9.00	9.05	9.10	9.15	9.20	9.25 9.75	9.30	9·35 9.85	9.40	9·45 9·95
1.9	9.30	9.55	9.00	9.03	9.70	9.73	9.80	9.05	9.90	9.93
2.0	10.00	10.05	10.10	10.15	10.20	10.25	10.30	10.35	10.40	10.45
2. I	10.50	10.55	10.60	10.65	10.70	10.75	10.80	10.85	10.90	10.95
2.2	11.00	11.05	11.10	11.15	II. 20	11.25	11.30	11.35	11.40	11.45
2.3	11.50	11.55	11.60	11.65	11.70	11.75 12.25	11.80	11.85	11.90	11.95
2.4	12.00	12.05	12.10	12.15	12.20	12.25	12.30	12.33	12.40	12.43
2.5	12.50	12.55	12.60	12.65	12.70	12.75	12.80	12.85	12.90	12.95
2.6	13.00	13.05	13.10	13.15	13.20	13.25	13.30	13.35	13.40	13.45
2.7	13.50	13.55	13.60	13.65	13.70	13.75	13.80	13.85	13.90	13.95
2.8	I4.00	14.05	14.10	14.15	14.20	14.25 14.75	14.30	14.35	14.40	14.45
2.9	14.50	14.55	14.00	14.05	14.70	14.75	14.00	14.05	14.90	14.91

DEPTH OF WATER CORRESPONDING TO THE WEIGHT OF SNOW 'OR RAIN' COLLECTED IN AN 8-INCH CAGE. (One pound equals 0.5507 inch.)

Weight Pounds.	.00	.01	.02	.03	.04	.05	.06	.07	.08	.09
.0 .1 .2 .3 .4 .5 .6 .7 .8	lnch00 .06 .11 .17 .22 .28 .33 .39 .44	Inch01 .06 .12 .17 .23 .28 .34 .39 .45 .50	Inch. . 01 . 07 . 12 . 18 . 23 . 29 . 34 . 40 . 45 . 51	Inch. .02 .07 .13 .18 .24 .29 .35 .40 .46	Inch. . 02 . 08 . 13 . 19 . 24 . 30 . 35 . 41 . 46 . 52	Inch. .03 .08 .14 .19 .25 .30 .36 .41 .47 .52	Inch 03 . 00 . 14 . 20 . 25 . 31 . 36 . 42 . 47 . 53	Inch04 .00 .15 .20 .26 .31 .37 .43 .48 .54	lnch. .04 .10 .15 .21 .26 .32 .38 .43 .49 .54	Inch05 .10 .16 .22 .27 .33 .38 .44 .40 .55

Table 89.

QUANTITY OF RAINFALL CORRESPONDING TO CIVEN DEPTHS.

			Gallons	per acre.	Tons per acre (2000
Depth of rain- fall, inches.	Cubic inches per acre.	Cubic feet per acre.	United States or Queen Anne.	Imperial (British),	pounds). (62° F.)
0.01 0.02 0.03 0.04 0.05	62726.4 125453. 188179. 250905. 313632.	36.3 72.6 108.9 145.2 181.5	271.5 543. 815. 1086. 1358.	226 45 ² 678 904 1130	1. I 2 3 3. 4 4. 5 5. 6
0.06 0.07 0.08 0.09 0.10	370335. 439084. 501810. 564536. 627264.	254. I 290. 4 326. 7 363. 0	1900. 2171. 2442. 2715.	1582 1808 2034 2261	7.9 9.0 10.1 11.3
0.25 0.50 0.75 1.00	1568160. 3136320. 4704480. 6272640. 7840800.	907.5 1815. 2722. 3630. 4538.	6789. 13577. 20366. 27154. 33943.	11303 16955 22607 28259	56. 85. 113. 141.
1 50 1.75 2.00 2.25 2.50	9408960. 10977120. 12545280. 14113440. 15681600.	5445. 6352. 7260. 8168. 9075.	40371. 47520. 54309. 61097. 67866.	33911 39563 45214 50866 56517	198. 226 255. 283.
2.75 3.00 4.00 5.00 6.00	17249760. 18817920. 25090560. 31363200. 37635840.	0982. 10890. 14520. 18150 21780.	74674 81463 108617 135772 162926.	62169 67821 90428 113035 135642	311. 339. 452. 565. 678.



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Relative intensity of solar radiation at different latitudes.		
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Air mass, m, corresponding to different zenith distances of the sun	TABLE	100
Relative illumination intensities	TABLE	101

VALUE OF GRAVITY ON THE EARTH AT SEA LEVEL.

 $g_{\phi} = 978.039 (1 + 0.005294 \sin^2 \phi - 0.000007 \sin^2 2 \phi)$ = 980.621 (1 - 0.002640 cos 2 \phi + 0.000007 cos^2 2 \phi)

ф	g_{ϕ}	ф	g_{ϕ}	ф	g_{ϕ}	ф	g_{ϕ}	ф	g_{ϕ}
0 /	Dynes.	· ,	Dynes.	0 /	Dynes.	0 /	Dynes.	0 /	Dynes.
0 0	978.039	20 00	978.642	37 00	979.908	54 00	981.422	71 00	982.665
I O	.041	20	.661	20	.937	20	.450	20	. 684
2 0	. 045	40	. 681	40	. 966	40	. 479	40	. 702
3 0	. 053	21 00	. 701	38 00	. 995	55 00	. 507	72 00	. 720
4 0	. 064	20	.721	20	980.024	20	- 535	20	. 738
		40	. 742	40	. 054	40	. 564	40	. 755
5 00	.078	22 00	. 762	39 00	. 083	56 00	. 592	73 00	.772
20	. 084	20	. 783	20	. 113	20	. 620	20	. 789
6 00	. 089	40 23 00	. 805	40 40 40	. 142	40 57 00	.647	40 74 00	.805
20	. 102	23 00	. 848	20	. 201	20	. 703	20	. 837
40	. 108	40	. 870	40	. 231	40	. 730	40	. 853
7 00	. 115	24 00	. 802	41 00	. 261	58 00	- 757	75 00	. 868
20	. 123	20	.014	20	. 201	20	. 784	20	. 883
40	. 131	40	. 037	40	. 321	40	. 811	40	. 898
8 00	. 139	25 00	. 960	42 00	. 350	59 00	. 838	76 00	.012
20	. 147	20	. 983	20	. 380	20	. 865	20	. 926
40	. 156	40	979.006	40	.410	40	. 891	40	. 940
9 00	. 165	26 00	. 030	43 00	. 440	60 00	.917	77 00	. 953
20	. 174	20	. 054	20	.47I	20	. 943	20	. 966
40	. 184	40	. 077	40	. 501	40	. 969	40	. 979
10 00	. 194	27 00	. 102	44 00	. 531	61 00	. 995	78 00	. 992
20	. 205	20	. 126	20	. 561	20 40	082.020	20 40	983.004
11 00	. 215	40 28 00	. 151	45 00	. 621	62 00	.040	70 00	.010
20	. 238	20 00	. 201	20	. 651	20	.006	79 00	. 039
40	. 250	40	. 226	40	.681	40	. 121	40	. 049
12 00		20 00	. 251	46 00	. 711	63 00	. 145	80 00	. 060
20	. 274	20	. 277	20	. 741	20	. 160	20	. 070
40	. 287	40	. 302	40	. 772	40	. 194	40	080
13 00	300	30 00	. 328	47 00	. 802	64 00	. 217	81 00	. 090
20	.313	20	- 354	20	. 832	20	. 241	20	. 000
40	. 327	40	. 381	40	. 862	40	. 265	40	. 108
14 00	. 341	31 00	. 407	48 00	. 892	65 co	. 288	82 00	. 116
20	- 355	20	-434	20	. 922	20 40	. 311	20	. 124
40	. 369	32 00	. 460 . 487	40 00	. 952 . 981	66 00	· 334 · 356	83 00	. 132
15 00	. 384	32 00	. 515	20	981.011	20	. 350	20	. 147
10	.415	40	. 542	40	. 0.11	40	. 401	40	. 153
16 00	. 430	33 00	. 560	50 00	.071	67 00	. 423	84 00	. 160
20	. 447	20	. 597	20	. 100	20	.445	20	. 166
40	. 463	40	. 624	40	. 130	40	. 466	40	. 172
17 00	. 479	34 00	. 652	51 00	. 160	68 00	. 487	85 00	. 177
20	. 496	20	. 680	20	. 189	20	. 508	20	. 182
40	. 514	40	. 708	40	. 218	40	. 528	40	. 187
18 00	. 531	35 00	. 736	52 00	. 248	69 00	. 549	86	70.0
20	. 549	20	. 765	20	. 277	20	. 569	86 00	. 102
40	. 567	36 oo	· 793 . 822	40 53 00	. 306	40 70 00	. 589 . 608	88 00	203
19 00	. 585 . 604	20	. 850	53 00	· 335 . 364	20	. 628	80 00	. 215
10	078.623	40	979.879	40	981.393	40	982.647	00 00	083.217
	1,70.003	73	21319				''		

RELATIVE ACCELERATION OF CRAVITY AT DIFFERENT LATITUDES.

Ratio of the acceleration of gravity at sea level for each 10' of latitude, to its acceleration at latitude 45°.

$$\frac{g_{\phi}}{g_{45}} = 1 - 0.002640 \cos 2 \phi + 0.000007 \cos^2 2 \phi$$

	84	15				
Latitude.	0'	10′	20′	30′	40′	50′
0°	0.997367	0.997367	0.007367	0.997367	0.997368	0.997368
I	. 997369	. 997369	. 997370	. 997371	. 997371	. 997372
2	.997373	997374	.997376	997377	.997378	.997380
	.997373	. 997374	.997375	. 997387	. 997388	.997390
3	.997393	997395	.997397	.997399	.997300	. 997494
4	. 997393	1997393	.997397	.997399	.99740-	.997404
5	0.997407	0.997410	0.997412	0.997415	0.997418	0.997421
6	.997424	. 997428	. 997431	. 997434	. 997438	.997441
7 8	. 997445	. 997449	. 997453	. 997456	. 997460	. 997465
8	. 997469	. 997473	. 997477	. 997482	. 997486	. 997491
9	. 997496	. 997500	. 997505	. 997510	. 997515	. 997520
10	0.997525	0.997531	0.997536	0.997541	0.997547	0.997553
11	.997558	. 997564	.997570	. 997576	. 997582	. 997588
12	. 997594	. 997500	. 997607	. 997613	. 997620	. 997626
	. 997594	. 997640	. 997646	. 997653	. 997660	. 997667
13	. 997674	. 997682	. 997689	. 997696	. 997704	.097711
14	.997074	.997002	. 997009	.997090	. 997704	. 99//12
15	0.997719	0.997727	0.997734	0.997742	0.997750	0.997758
16	. 997766	. 997774	. 997783	. 997791	. 997799	. 997808
17	. 997816	. 997825	. 997833	. 997842	. 997851	. 997860
18	. 997869	. 997878	. 997887	. 997896	. 997905	. 997915
IQ	.997924	. 997934	. 997943	. 997953	. 997962	. 997972
7	77.7					
20	0.997982	0.997992	0.998002	0.998012	0.998022	0.998032
2 I	. 998042	. 998052	. 998063	. 998073	. 998084	. 998094
2.2	. 998104	. 998115	. 998126	. 998137	. 998148	. 998159
23	. 998170	. 998181	. 998192	. 998203	. 998214	. 998225
24	. 998237	. 998248	. 998260	. 998271	. 998283	. 998294
25	0.998306	0.998318	0.998330	0.998341	0.998353	0.998365
20	. 998377	. 998389	. 998402	. 998414	. 998426	. 998438
27	. 998451	. 998463	. 998476	. 998488	. 998501	. 998513
28	. 998526	. 998539	. 998551	. 998564	. 998577	. 998590
20	. 998603	. 998616	. 998629	. 998642	. 998655	. 998669
30	0.998682	c. 998695	0.998708	0.998722	0.998735	0.998749
31	. 998762	. 998776	. 998789	. 998803	.998817	. 998830
32	. 998844	. 998858	. 998872	. 998886	. 998899	.998913
33	. 998927	.998941	. 998956	. 998970	. 998984	. 998998
34	. 999012	. 999026	. 999041	. 999055	. 999 0 69	. 999084
35	0.000008	0.000112	0.999127	0.999141	0.999156	0.000170
36	. 999185	. 999199	.999214	. 999229	.999243	. 999258
37	.999273	. 999288	. 999302	.999317	.999332	.999347
38	. 999362	. 999377	. 999392	. 999406	. 999421	. 999436
39	. 999451	. 999466	. 999482	. 999497	.999512	.999527
10		0.000###	0.000 500	0.000.50	0.000600	0 000670
40	0.999542	0.999557	0.999572	0.999587	0.999602	0.999618
41	. 999633	. 999648	. 999663	. 999678		.999709
42	. 999724	. 999739	. 999755	. 999770	.999785	.999801
43	. 999816	.999831	. 999847	. 999862	. 999877	. 999893
44	. 9999 0 8	. 999923	. 999939	. 999954	. 999969	. 999905
45	1.000000	1.000015	1.000031	1.000046	1.000061	1.000077
			L			

TABLE 91.

RELATIVE ACCELERATION OF CRAVITY AT DIFFERENT LATITUDES.

Ratio of the acceleration of gravity at sea level for each 10' of latitude, to its acceleration at latitude 45°.

$$\frac{g_{\phi}}{g_{45}} = 1 - 0.002640 \cos 2 \phi + 0.000007 \cos^2 2 \phi$$

	84					
Latitude. ϕ	0′	10′	20′	30′	40′	50′
45	I.00000	1.000015	1.000031	1.000046	1.000061	1.000077
46	002	108	123	138	153	160
47	184	200	215	230	246	261
48	276	201	307	322	337	352
49	368	383	398	413	428	444
49	300	303	390	413	420	444
50	1.000459	1.000474	1.coc489	1.000504	1.000519	1.000534
51	549	564	579	594	609	624
52	639	654	669	684	699	713
53	728	743	758	773	787	802
54	816	831	846	860	875	889
55	1.000004	1.000918	1.000933	1.000947	1.000061	1.000076
56	0000	1004	1018	1033	1047	1061
57	1075	1089	1103	1117	1131	1145
58	1159	1173	1186	1200	1214	1227
59	1241	1255	1268	1282	1205	1308
39	1241	1233	1200	1202	1293	1300
60	1.001322	1.001335	1.001348	1.001362	1.001375	1.001388
61	1401	1414	1427	1440	1453	1466
62	1478	1491	1504	1517	1529	1542
63	1554	1567	1579	1501	1604	1616
64	1628	1640	1652	1664	1676	1688
65					7 001777	T 0077778
65 66	1.001700	1.001712	1.001723	1.001735	1.co1747 1815	1.001758
	1770	1781	1792		1881	1802
67 68	1837	1848	1859	1870		
	1903	1913	1924	1935	1945	1955
69	1966	1976	1986	1996	2007	2017
70	1.002026	1.002036	1,002046	1.002056	1.002066	1.002075
71	2085	2004	2104	2113	2122	2131
72	2140	2140	2158	2167	2176	2185
73	2194	2202	2211	2210	2227	2236
74	2244	2252	2260	2268	2276	2284
75	1 000000	7 000000	T 000307	1.002314	1.002322	1.002329
	1.002292	1.002299	1.002307			
76	2336	2344	2351	2358	2365	2372
77 78	2378	2385	2392	2398	2405	2411 2448
	2418	2424 2460	2430	2436	2442 2476	2446
79	2454	2400	2465	2471	2470	2402
80	1.002487	1.002492	1.002497	1.002502	1.002507	1.002512
81	2517	2522	2527	2531	2536	2540
82	2544	2548	2553	2557	2561	2564
83	2568	2572	2576	2579	2582	2586
84	2589	2592	2595	2598	2601	2604
85	1,002607	1,002600	1.002612	1.002614	1,002617	1.002610
86	2621	2623	2625	2627	2620	2631
87	2632	2634	2636	2637	2638	2639
88	2641	2642	2643	2643	2644	2645
89	2645	2646	2646	2647	2647	2647
90	1.002647					
1	•			1	1	

LENGTH OF ONE DEGREE OF THE MERIDIAN AT DIFFERENT LATITUDES.

Latitude.	Meters.	Statute Miles.	Geographic Miles. 1' of the Eq.	Latitude.	Meters.	Statute Miles.	Geographic Miles. 1' of the Eq.
0° 1 2 3 4	110 568.5 110 568.8 110 569.8 110 571.5 110 573.9	68.703 68.704 68.705 68.706 68.707	59·594 59·594 59·595 59·596 59·597	45° 46 47 48 49	111 132.1 111 151.9 111 171.6 111 191.3 111 210.9	69.054 69.067 69.079 69.091 69.103	59.898 59.908 59.919 59.929 59.940
5 6 7 8 9	110 577.0 110 580.7 110 585.1 110 590.2 110 595.9	68.709 68.711 68.714 68.717 68.721	59.598 59.600 59.603 59.606 59.609	50 51 52 53 54	111 230.5 111 249.9 111 269.2 111 288.3 111 307.3	69.115 69.127 69.139 69.151 69.163	59.951 59.961 59.972 59.982 59.992
10 11 12 13 14	110 602.3 110 609.3 110 617.0 110 625.3 110 634.2	68.725 68.729 68.734 68.739 68.745	59.612 59.616 59.620 59.625 59.629	55 56 57 58 59	111 326.0 111 344.5 111 362.7 111 380.7 111 398.4	69.175 69.186 69.198 69.209	60.002 60.012 60.022 60.032 60.041
15 16 17 18	110 643.7 110 653.8 110 664.5 110 675.7 110 687.5	68.751 68.757 68.763 68.770 68.778	59.634 59.640 59.646 59.652 59.658	60 61 62 63 64	111 415.7 111 432.7 111 449.4 111 465.7 111 481.5	69.230 69.241 69.251 69.261 69.271	60.051 60.060 60.069 60.077 60.086
20 21 22 23 24	110 699.9 110 712.8 110 726.2 110 740.1 110 754.4	68.786 68.794 68.802 68.810 68.819	59.665 59.672 59.679 59.686 59.694	65 66 67 68 69	111 497.0 111 512.0 111 526.5 111 540.5 111 554.1	69.281 69.290 69.299 69.308 69.316	60.094 60.102 60.110 60.118 60.125
25 26 27 28 29	110 769.2 110 784.5 110 800.2 110 816.3 110 832.8	68.829 68.838 68.848 68.858 68.868	59.702 59.710 59.719 59.727 59.736	70 71 72 73 74	111 567.1 111 579.7 111 591.6 111 603.0 111 613.9	69.324 69.332 69.340 69.347 69.354	60.132 60.139 60.145 60.151 60.157
30 31 32 33 34	110 849.7 110 866.9 110 884.4 110 902.3 110 920.4	68.879 68.889 68.900 68.911 68.923	59·745 59·755 59·764 59·774 59·784	75 76 77 78 79	111 624.1 111 633.8 111 642.8 111 651.2 111 659.0	69.360 69.366 69.372 69.377 69.382	60.163 60.168 60.173 60.177 60.182
35 36 37 38 39	110 938.8 110 957.4 110 976.3 110 995.3	68.934 68.946 68.957 68.969 68.981	59.794 59.804 59.814 59.824 59.834	80 81 82 83 84	111 666.2 111 672.6 111 678.5 111 683.6 111 688.1	69.386 69.390 69.394 69.397 69.400	60.186 60.189 60.192 60.195 60.197
40 41 42 43 44	111 033.9 111 053.4 111 073.0 111 092.6 111 112.4	68.993 69.005 69.017 69.029 69.042	59.845 59.855 59.866 59.876 59.887	85 86 87 88 89	111 691.9 111 695.0 111 697.4 111 699.2 111 700.2	69.402 69.404 69.405 69.407 69.407	60.199 60.201 60.202 60.203 60.204
45	111 132.1	69.054	59.898	90	111700.6	69.407	60.204

LENGTH OF ONE DEGREE OF THE PARALLEL AT DIFFERENT LATITUDES.

Latitude.	Meters.	Statute Miles.	Geographic Miles. 1' of the Eq.	Latitude.	Meters.	Statute Miles.	Geographic Miles. 1' of the Eq.
0° 1 2 3 4	111 321.9 111 305.2 111 254.6 111 170.4 111 052.6	69.171 69.162 69.130 69.078 69.005	60.000 59.991 59.964 59.918 59.855	45° 46 47 48 49	78 850.0 77 466.5 76 059.2 74 628.5 73 174.9	48.995 48.135 47.261 46.372 45.469	42.498 41.753 40.994 40.223 39.440
5	110 901.2	68.911	59.773	50	71 698.9	44.552	38.644
6	110 716.2	68.796	59.673	51	70 200.8	43.621	37.837
7	110 497.7	68.660	59.556	52	68 681.1	42.676	37.018
8	110 245.8	68.593	59.420	53	67 140.3	41.719	36.187
9	109 960.5	68.326	59.266	54	65 578.8	40.749	35.346
10	109 641.9	68.128	59.095	55	63 997. I	39.766	34.493
11	109 290.1	67.909	58.905	56	62 395.7	38.771	33.630
12	108 905.2	67.670	58.697	57	60 775. I	37.764	32.757
13	108 487.3	67.411	58.472	58	59 135.7	36.745	31.873
14	108 036.6	67.131	58.229	59	57 478. I	35.715	30.979
15	107 553.1	66.830	57.969	60	55 802.8	34.674	30.076
16	107 037.0	66.510	57.690	61	54 110.2	33.622	29.164
17	106 488.5	66.169	57.395	62	52 400.9	32.560	28.243
18	105 907.7	65.808	57.082	63	50 675.4	31.488	27.313
19	105 294.7	65.427	56.751	64	48 934.3	30.406	26.374
20	104 649.8	65.026	56.404	65	47 178.0	29.315	25.428
21	103 973.2	64.606	56.039	66	45 407.1	28.215	24.473
22	103 265.0	64.166	55.657	67	43 622.2	27.106	23.511
23	102 525.4	63.706	55.259	68	41 823.8	25.988	22.542
24	101 754.6	63.227	54.843	69	40 012.4	24.862	21.566
25	100 953.0	62.729	54.411	70	38 188.6	23.729	20.583
26	100 120.6	62.212	53.963	71	36 353.0	22.589	19.593
27	99 257.8	61.676	53.498	72	34 506.2	21.441	18.598
28	98 364.8	61.121	53.016	73	32 648.6	20.287	17.597
29	97 441.9	60.548	52.519	74	30 780.9	19.126	16.590
30	96 489.3	59.956	52.006	75	28 903.6	17.960	15.578
31	°5 507.3	59.345	51.476	76	27 017.4	16.788	14.562
32	94 496.2	58.717	50.931	77	25 122.8	15.611	13.541
33	93 456.3	58.071	50.371	78	23 220.4	14.428	12.515
34	92 387.9	57.407	49.795	79	21 310.8	13.242	11.486
35	91 291.3	56.726	49.204	80	19 394.6	12.051	10.453
36	90 166.8	56.027	48.598	81	17 472.4	10.857	9.417
37	89 014.8	55.311	47.977	82	15 544.7	9.659	8.378
38	87 835.6	54.578	47.341	83	13 612.2	8.458	7.337
39	86 629.6	53.829	46.691	84	11 675.5	7.255	6.293
40	85 397.0	53.063	46.027	85	9735.1	6.049	5.247
41	\$4 138.4	52.281	45.349	86	7791.7	4.841	4.200
42	\$2 854.0	51.483	44.656	87	5845.9	3.632	3.151
43	\$1 544.2	50.669	43.950	88	3898.3	2.422	2.101
44	\$0 209.4	49.840	43.231	89	1949.4	1.211	1.051
45	78 850.0	48.995	42.498	90	0.0	0.000	0.000

Declination				LATIT	UDE NO	RTH.			
the Sun.	0°	5°	10°	15°	20°	25°	30°	35°	40°
	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
-23°27′	12 7	11 50	II 32	11 14	10 55	10 35	10 13	9 48	9 19
-23°20	12 7	11 50	II 32	11 14	10 56	10 36	10 14	9 49	9 20
-23°0	12 7	11 50	II 33	11 15	10 57	10 37	10 15	9 51	9 23
$ \begin{array}{c cccc} -22 & 40 \\ -22 & 20 \\ -22 & 0 \end{array} $	12 7	11 50	II 33	11 16	10 58	10 38	10 17	9 53	9 26
	12 7	11 51	II 34	11 17	10 59	10 40	10 19	9 55	9 29
	12 7	11 51	II 34	11 18	11 0	10 41	10 20	9 58	9 31
-21 40	12 7	11 51	11 35	II 19	II I	10 43	10 22	10 0	9 34
-21 20	12 7	11 52	11 35	II 19	II 2	10 44	10 24	10 2	9 37
-21 0	12 7	11 52	11 36	II 20	II 4	10 46	10 26	10 4	9 40
-20 40	12 7	II 52	11 37	II 2I	II 5	10 47	10 28	10 6	9 4 2
-20 20	12 7	II 52	11 37	II 22	II 6	10 49	10 29	10 8	9 45
-20 0	12 7	II 53	11 38	II 23	II 7	10 50	10 31	10 11	9 47
-19 40 -19 20 -19 0	12 7 12 7 12 7	II 53 II 53 II 53	11 38 11 39 11 39	11 23 11 24 11 25	11 8 11 10	10 51 10 53 10 54	10 33 10 35 10 37	10 13 10 15 10 17	9 50 9 53 9 55
-18 40	12 7	11 54	11 40	11 26	11 11	10 55	10 38	10 19	9 58
-18 20	12 7	11 54	11 40	11 27	11 12	10 57	10 40	10 21	10 I
-18 0	12 7	11 54	11 41	11 28	11 13	10 58	10 42	10 23	10 3
-17 40	12 7	11 54	11 41	11 28	11 14	10 59	10 43	10 26	10 5
-17 20	12 7	11 55	11 42	11 29	11 15	11 1	10 45	10 28	10 8
-17 0	12 7	11 55	11 42	11 30	11 16	11 2	10 47	10 30	10 10
-16 40	12 7	11 55	II 43	II 3I	11 17	11 4	10 49	10 32	10 13
-16 20	12 7	11 55	II 43	II 3I	11 18	11 5	10 50	10 34	10 16
-16 0	12 7	11 56	II 44	II 32	11 19	11 6	10 52	10 36	10 18
-15 40	12 7	11 56	II 44	II 33	II 20	11 8	10 53	10 38	10 20
-15 20	12 7	11 56	II 45	II 34	II 2I	11 9	10 55	10 40	10 23
-15 0	12 7	11 56	II 45	II 34	II 22	11 10	10 57	10 42	10 25
-14 40	12 7	11 57	11 46	II 35	II 23	11 11	IO 59	10 44	10 28
-14 20	12 7	11 57	11 46	II 36	II 25	11 13	II O	10 46	10 30
-14 0	12 7	11 57	11 47	II 37	II 26	11 14	II 2	10 48	10 32
-13 40	12 7	11 57	11 47	11 37	11 27	11 16	11 4	10 50	10 35
-13 20	12 7	11 58	11 48	11 38	11 28	11 17	11 5	10 52	10 37
-13 0	12 7	11 58	11 48	11 39	11 29	11 18	11 7	10 54	10 40
-12 40 -12 20 -12 0	12 7 12 7 12 7	11 58 11 58 11 58	11 49 11 49 11 50	II 40 II 40 II 4I	11 30 11 31 11 32	II 19 II 21 II 22	11 10 11 11	10 56 10 58 11 0	10 42 10 44 10 47
-11 40	12 7	11 59	11 50	II 42	11 33	11 23	11 13	11 2	10 49
-11 20	12 7	11 59	11 51	II 43	11 34	11 25	11 15	11 4	10 52
-11 0	12 7	11 59	11 51	II 43	11 35	11 26	11 16	11 6	10 54
-10 40	12 7	11 59	11 52	11 44	11 36	II 27	11 18	11 8	10 56
-10 20	12 7	12 0	11 52	11 45	11 37	II 28	11 20	11 10	10 59
-10 0	12 7	12 0	11 53	11 46	11 38	II 30	11 21	11 12	11 1
- 9 40	12 7	12 O	II 53	11 46	II 39	11 31	11 23	11 14	11 3
- 9 20	12 7	12 O	II 54	11 47	II 40	11 32	11 24	11 16	11 5
- 9 0	12 7	12 I	II 54	11 47	II 41	11 34	11 26	11 17	11 8
- 8 40	12 7	12 I	11 55	11 48	II 42	11 35	II 28	II 19	II 10
8 20	12 7	12 I	11 55	11 49	II 43	11 36	II 29	II 21	II 12
8 0	12 7	12 I	11 56	11 50	II 44	11 37	II 3I	II 23	II 14

Declination of				I,	ATITUD	E NORT	H.			
the Sun.	42°	44°	46°	48°	50°	52°	54°	56°	58°	60°
	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
-23°27′	9 7	8 53	8 38	8 22	8 4	7 44	7 22	6 56	6 27	5 52
-23°20	9 8	8 54	8 39	8 23	8 5	7 45	7 24	6 58	6 29	5 54
-23°0	9 11	8 58	8 43	8 28	8 10	7 50	7 29	7 4	6 36	6 2
-22 40	9 14	9 I	8 46	8 31	8 14	7 55	7 34	7 10	6 43	6 9
-22 20	9 17	9 4	8 50	8 35	8 18	8 0	7 39	7 16	6 49	6 17
-22 0	9 20	9 7	8 53	8 38	8 22	8 4	7 44	7 22	6 55	6 25
-21 40	9 23	9 IO	8 57	S 42	8 26	8 9	7 49	7 27	7 I	6 32
-21 20	9 26	9 I3	9 1	8 46	8 30	8 13	7 54	7 32	7 8	6 38
-21 0	9 28	9 I7	9 4	8 50	8 34	8 18	7 59	7 38	7 I4	6 46
-20 40	9 31	9 20	9 7	8 53	8 38	8 22	8 4	7 43	7 20	6 52
-20 20	9 34	9 23	9 11	8 57	8 42	8 26	8 8	7 49	7 25	6 59
-20 0	9 37	9 26	9 14	9 I	8 46	8 31	8 13	7 54	7 31	7 5
-19 40	9 40	9 29	9 17	9 4	8 50	8 35	8 18	7 59	7 37	7 12
-19 20	9 43	9 32	9 20	9 7	8 54	8 39	8 23	8 4	7 43	7 18
-19 0	9 46	9. 35	9 24	9 II	8 58	8 43	8 27	8 9	7 48	7 25
-18 40	9 48	9 38	9 27	9 I5	9 2	8 47	8 32	8 14	7 54	7 31
-18 20	9 51	9 41	9 30	9 I9	9 6	8 52	8 36	8 19	7 59	7 37
-18 0	9 54	9 44	9 34	9 22	9 10	8 56	8 41	8 24	8 5	7 43
-17 40	9 56	9 47	9 37	9 25	9 13	9 0	\$ 45	8 29	8 10	7 49
-17 20	9 59	9 50	9 40	9 29	9 17	9 4	8 50	8 34	8 15	7 55
-17 0	10 2	9 53	9 43	9 32	9 21	9 8	8 54	8 38	8 20	8 1
16 40	10 5	9 56	9 46	9 35	9 25	9 12	8 58	8 43	8 26	8 6
16 20	10 7	9 59	9 49	9 39	9 28	9 16	9 2	8 47	8 31	8 12
16 0	10 10	10 1	9 52	9 43	9 32	9 20	9 7	8 52	8 36	8 17
15 40	10 12	10 4	9 55	9 46	9 35	9 24	9 II	8 57	8 41	8 23
15 20	10 15	10 7	9 58	9 49	9 39	9 28	9 I5	9 2	8 46	8 29
15 0	10 18	10 10	10 1	9 52	9 43	9 31	9 I9	9 6	8 51	8 34
-14 40	10 20	10 13	10 4	9 56	9 46	9 35	9 23	9 II	8 56	8 40
-14 20	10 23	10 16	10 7	9 59	9 49	9 39	9 28	9 I5	9 I	8 45
-14 0	10 26	10 19	10 10	10 2	9 53	9 43	9 32	9 I9	9 6	8 50
- 13 40	10 28	10 21	10 13	10 5	9 56	9 47	9 36	9 24	9 11	8 56
- 13 20	10 31	10 24	10 16	10 8	10 0	9 50	9 40	9 28	9 16	9 I
- 13 0	10 33	10 26	10 19	10 11	10 3	9 54	9 44	9 33	9 20	9 6
- 12 40	10 36	10 29	IO 22	IO 15	10 7	9 58	9 48	9 37	9 25	9 II
- 12 20	10 38	10 32	IO 25	IO 18	10 10	10 1	9 52	9 41	9 30	9 I7
- 12 0	10 41	10 35	IO 28	IO 21	10 13	10 5	9 56	9 46	9 35	9 22
- II 40	10 44	10 38	IO 3I	IO 25	10 17	10 9	10 0	9 50	9 39	9 27
- II 20	10 46	10 40	IO 34	IO 28	10 20	10 13	10 4	9 55	9 44	9 32
- II 0	10 49	10 43	IO 37	IO 31	10 23	10 16	10 8	9 59	9 49	9 37
-10 40	10 51	10 46	10 40	10 34	IO 27	IO 19	10 12	IO 3	9 53	9 42
-10 20	10 53	10 49	10 43	10 37	IO 31	IO 23	10 16	IO 7	9 58	9 47
-10 0	10 56	10 51	10 46	10 40	IO 34	IO 27	10 19	IO II	10 3	9 52
- 9 40	10 59	10 54	10 49	10 43	10 37	IO 31	IO 23	10 16	10 7	9 57
- 9 20	11 1	10 56	10 52	10 46	10 40	IO 34	IO 27	10 20	10 11	10 2
- 9 0	11 3	10 59	10 55	10 49	10 44	IO 37	IO 3I	10 24	10 16	10 7
- 8 40	11 6	II 2	10 57	10 52	10 47	IO 41	10 34	10 28	10 20	10 11
- 8 20	11 8	II 4	11 0	10 55	10 50	IO 44	10 38	10 32	10 25	10 16
- 8 0	11 10	II 7	11 3	10 58	10 53	IO 48	10 42	10 36	10 29	10 21

				LATIT	UDE NO	RTH.			
Declination of the Sun.	0°	5°	10°	15°	20°	25°	30°	35°	40°
	h. m.	h. m.	h. m.	h. m.	h. m.		h. m.	h. m.	h. m.
-8° 0′	12 7	12 1	11 55	11 50	11 44		11 31	11 23	11 14
-7 40 -7 20 -7 0	12 7 12 7 12 7	12 I 12 I 12 2	11 56	11 51	11 46	-	11 34	II 27 II 29	11 19
-6 40	12 7	12 2	11 57	II 53	11 48	II 42	II 37	11 31	11 24
-6 20	12 7	12 2	11 58	II 53	11 49	II 43	II 38	11 32	11 26
-6 0	12 7	12 2	11 58	II 54	11 50	II 45	II 40	11 34	11 28
-5 40	12 7	12 3	11 59	11 55	11 51	11 46	11 41	11 36	11 31
-5 20	12 7	12 3	11 59	11 55	11 52	11 47	11 43	11 38	11 33
-5 0	12 7	12 3	12 0	11 56	11 53	11 49	11 44	11 40	11 35
-4 40	12 7	12 3	12 O	11 57	11 54	11 50	11 46	11 42	II 37
-4 20	12 7	12 4	12 I	11 58	11 55	11 51	11 47	11 44	II 40
-4 0	12 7	12 4	12 I	11 58	11 56	11 52	11 49	11 46	II 42
-3 40	12 7	12 4	12 2	11 59	11 57	11 53	11 51	11 47	11 44
-3 20	12 7	12 4	12 2	12 0	11 58	11 55	11 52	11 49	11 46
-3 0	12 7	12 5	12 3	12 1	11 58	11 56	11 54	11 51	11 49
-2 40	12 7	12 5	12 3	12 I	11 59	11 58	11 55	11 53	11 51
-2 20	12 7	12 5	12 4	12 2	12 0	11 59	11 57	11 55	11 53
-2 0	12 7	12 5	12 4	12 3	12 1	12 0	11 58	11 57	11 55
- I 40	12 7	12 5	12 4	12 4	12 2	12 I	12 0	11 59	11 58
- I 20	12 7	12 6	12 5	12 4	12 3	12 2	12 2	12 1	12 0
- I 0	12 7	12 6	12 5	12 5	12 4	12 4	12 3	12 2	12 2
-0 40	12 7	12 6	12 6	12 5	12 5	12 5	12 5	12 4	12 4
-0 20	12 7	12 6	12 6	12 6	12 6	12 6	12 6	12 6	
0 0	12 7	12 7	12 7	12 7	12 7	12 7	12 8	12 8	12 9
+0 20	12 7	12 7	12 7	12 8	12 8	12 8	12 9	12 10	12 11
0 40	12 7	12 7	12 8	12 8	12 9	12 10	12 11	12 12	12 13
0	12 7	12 7	12 S	12 9	12 IO	12 11	12 13	12 14	12 15
1 20	12 7	12 8	12 9	12 10	12 II	12 13	12 14	12 16	12 17
1 40	12 7	12 8	12 9	12 10	12 I2	12 14	12 16	12 17	12 20
2 0	12 7	12 8	12 IO	12 II	12 13	12 15	12 17	12 19	12 22
2 20	12 7	12 8	12 IO	12 I2	12 14	12 16	12 19	12 21	12 25
2 40	12 7	12 9	12 II	12 I3	12 15	12 17	12 20	12 23	12 27
3 0	12 7	12 9	12 II	12 13	12 16	12 19	12 22	12 25	12 29
3 20	12 7	12 9	12 I2	12 14	12 17	12 20	12 23	12 27	12 31
3 40	12 7	12 9	12 I2	12 15	12 18	12 21	12 25	12 29	12 33
4 0	12 7	12 IO	12 13	12 16	12 19		12 26	12 31	12 35
4 20	12 7	12 IO	12 13	12 16	12 20		12 28	12 32	12 38
4 40	12 7	12 IO	12 14	12 17	12 21		12 29	12 34	12 40
5 0 5 20 5 40	12 7 12 7 12 7	12 IO 12 IO 12 II	12 14 12 15 12 15	12 19	12 23	12 28 12 29	12 31 12 32 12 34	12 36 12 38 12 40	12 43 12 45 12 47
6 0 6 20 6 40	12 7 12 7 12 7	12 II 12 II 12 II	12 16 12 16 12 16	12 21	12 26	12 31	12 35 12 37 12 39	12 46	12 54
7 0 7 20 7 40	12 7 12 7 12 7	1	12 17 12 17 12 18	12 23	12 29	12 35		12 50	12 58
8 0	12 7	12 13	12 18	3 12 2	1 12 3	1 12 38	12 45	12 53	13 3

TABLE 94.

Declination of				I,	ATITUDI	E NORT	11.			
the Sun.	42°	44°	46°	48°	50°	52°	54°	56°	58°	60°
-8° 0′	h, m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m. 10 36	h. m.	h. m. 10 21
-7 40	11 13	11 10	11 5	11 1	10 57	10 52	10 46	10 40	10 34	10 26
-7 20	11 16	11 12	11 8	11 4	11 0	10 55	10 50	10 44	10 38	10 31
-7 0	11 19	11 15	11 11	11 7	11 3	10 59	10 54	10 48	10 42	10 35
-6 40	II 2I	II 17	II I4	11 10	11 7	11 2	10 58	10 52	10 47	10 40
-6 20	II 23	II 20	II I7	11 13	11 10	11 5	11 1	10 56	10 51	10 45
-6 0	II 26	II 23	II 20	11 16	11 13	11 9	11 5	11 0	10 55	10 50
-5 40	11 28	II 25	II 23	II 19	11 16	11 13	11 8	II 4	10 59	10 55
-5 20	11 31	II 28	II 25	II 22	11 19	11 16	11 13	II 8	11 4	10 59
-5 0	11 33	II 31	II 28	II 25	11 23	11 19	11 16	II 12	11 8	11 4
-4 40	11 35	11 33	II 3I	11 28	II 26	11 23	11 20	II 16	II 13	11 8
-4 20	11 38	11 36	II 34	11 31	II 29	11 26	11 23	II 20	II 17	11 13
-4 0	11 40	11 38	II 37	11 34	II 32	11 30	11 27	II 24	II 21	11 18
-3 40	II 43	11 41	II 39	II 37	II 35	II 33	11 31	11 28	11 26	II 22
-3 20	II 45	11 43	II 42	II 40	II 38	II 37	11 35	11 32	11 30	II 27
-3 0	II 47	11 46	II 45	II 43	II 42	II 40	11 38	11 36	11 34	II 32
-2 40	II 50	11 49	11 47	11 46	11 45	11 44	II 42	11 40	II 38	11 37
-2 20	II 52	11 51	11 50	11 49	11 48	11 47	II 46	11 44	II 43	11 41
-2 0	II 55	11 54	11 53	11 52	11 52	11 50	II 49	11 48	II 47	11 46
- I 40	11 57	11 56	11 55	11 55	11 55	11 54	11 53	11 52	11 51	11 50
- I 20	11 59	11 59	11 58	11 58	11 58	11 57	11 57	11 56	11 56	11 55
- I 0	12 2	12 2	12 1	12 1	12 1	12 1	12 1	12 0	12 0	11 59
-0 40	12 4	12 4	12 4	12 4	12 4	12 4	12 4	12 4	12 4	12 4
-0 20	12 7	12 7	12 7	12 7	12 7	12 7	12 S	12 8	12 S	12 9
+0 0	12 9	12 9	12 10	12 10	12 IO	12 11	12 11	12 12	12 13	12 13
0 20	12 11	12 12	12 13	12 13	12 I4	12 14	12 15	12 16	12 17	12 18
0 40	12 14	12 14	12 15	12 16	12 I7	12 17	12 19	12 20	12 21	12 23
l 0	12 16	12 17	12 18	12 19	12 20	12 21	12 22	12 24	12 25	12 27
I 20	12 19	12 20	12 20	12 22	12 23	12 25	12 26	12 28	12 29	12 32
I 40	12 21	12 22	12 23	12 25	12 26	12 28	12 30	12 32	12 34	12 37
2 0	12 23	12 25	12 26	12 28	12 29	12 31	12 34	12 36	12 38	12 41
2 20	12 26	12 28	12 29	12 31	12 32	12 35	12 37	12 40	12 43	12 46
2 40	12 28	12 30	12 32	12 34	12 36	12 38	12 41	12 44	12 47	12 50
3 0	12 31	12 32	12 35	12 37	12 39	12 41	12 44	12 48	12 51	12 55
3 20	12 33	12 35	12 37	12 40	12 42	12 45	12 48	12 52	12 55	13 0
3 40	12 35	12 38	12 40	12 43	12 46	12 49	12 52	12 56	13 0	13 4
4 0	12 38	12 40	12 43	12 46	12 49	12 52	12 56	13 0	13 4	13 9
4 20	12 40	12 43	12 46	12 49	12 52	12 55	12 59	13 4	13 8	13 14
4 40	12 43	12 46	12 49	12 52	12 55	12 59	13 3	13 8	13 13	13 19
5 0	12 45	12 48	12 51	12 55	12 58	13 2	13 7	13 12	13 17	13 23
5 20	12 47	12 51	12 54	12 58	13 2	13 6	13 11	13 16	13 22	13 28
5 40	12 50	12 53	12 57	13 1	13 5	13 10	13 14	13 20	13 26	13 33
6 0	12 53	12 56	12 59	13 4	13 8	13 13	13 18	13 24	13 31	13 38
6 20	12 55	12 59	13 2	13 7	13 11	13 16	13 22	13 28	13 35	13 43
6 40	12 58	13 1	13 5	13 10	13 14	13 20	13 26	13 32	13 39	13 47
7 0	13 0	13 4	13 S	13 13	13 18	I3 23	13 29	13 36	13 44	13 52
7 20	13 2	13 7	13 II	13 16	13 21	I3 27	13 33	13 40	13 48	13 57
7 40	13 5	13 9	13 I4	13 19	13 25	I3 3I	13 37	13 44	13 53	14 2
8 0	13 7	13 12	13 17	13 22	13 28	13 34	13 41	13 48	13 57	14 7

Declination				LATI	TUDE NO	ORTH.			
the Sun.	0°	5°	10°	15°	20°	25°	30°	35°	40°
	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
+8° 0′	12 7	12 13	12 18	12 24	12 31	12 38	12 45	12 53	13 3
8 20	12 7	12 13	12 19	12 25	12 32	12 39	12 47	12 55	13 5
8 40	12 7	12 13	12 19	12 26	12 33	12 40	12 48	12 57	13 8
9 0	12 7	12 13	12 20	12 26	12 34	12 41	12 50	12 59	13 10
9 20	12 7	12 13	12 20	12 27	12 35	12 43	12 52	13 1	13 13
9 40	12 7	12 14	12 21	12 28	12 36	12 44	12 53	13 3	13 14
10 0	12 7	12 14	12 21	12 29	12 37	12 45	12 55	13 5	13 17
10 20	12 7	12 14	12 22	12 29	12 38	12 47	12 56	13 7	13 19
10 40	12 7	12 14	12 22	12 30	12 39	12 48	12 58	13 9	13 22
0	12 7	12 15	12 23	12 31	12 40	12 49	12 59	13 11	13 24
11 20	12 7	12 15	12 23	12 32	12 41	12 50	13 1	13 13	13 26
11 40	12 7	12 15	12 24	12 32	12 42	12 52	13 2	13 15	13 29
12 0	12 7	12 15	12 24	12 33	12 43	12 53	13 4	13 17	13 31
12 20	12 7	12 16	12 25	12 34	12 44	12 55	13 6	13 19	13 34
12 40	12 7	12 16	12 25	12 35	12 45	12 56	13 8	13 21	13 36
13 0	12 7	12 16	12 26	12 35	12 46	12 57	13 9	13 23	13 38
13 20	12 7	12 16	12 26	12 36	12 47	12 58	13 11	13 25	13 41
13 40	12 7	12 17	12 27	12 37	12 48	13 0	13 13	13 27	13 43
14 0	12 7	12 I7	12 27	12 38	12 49	13 I	13 14	13 29	13 46
14 20	12 7	12 I7	12 28	12 39	12 50	13 2	13 16	13 31	13 48
14 40	12 7	12 I7	12 28	12 40	12 51	13 4	13 17	13 33	13 51
15 0	12 7	12 18	12 29	12 40	12 52	13 5	13 19	13 35	13 53
15 20	12 7	12 18	12 29	12 41	12 53	13 7	13 21	13 37	13 56
15 40	12 7	12 18	12 30	12 41	12 54	13 8	13 23	13 39	13 58
16 0	12 7	12 19	12 30	12 42	12 55	13 9	13 2 5	13 41	14 I
16 20	12 7	12 19	12 31	12 43	12 56	13 11	13 2 6	13 43	14 3
16 40	12 7	12 19	12 31	12 44	12 58	13 12	13 28	13 45	14 6
17 0	12 7	12 19	12 32	12 45	12 59	13 13	13 29	13 47	14 8
17 20	12 7	12 20	12 32	12 46	13 0	13 15	13 31	13 50	14 11
17 40	12 7	12 20	12 33	12 46	13 1	13 16	13 33	13 52	14 14
18 0	12 7	I2 20	12 33	12 47	13 2	13 17	13 35	13 54	14 16
18 20	12 7	I2 20	12 34	12 48	13 3	13 19	13 37	13 56	14 19
18 40	12 7	I2 2I	12 34	12 49	13 4	13 20	13 38	13 58	14 22
19 0	12 7	12 2I	12 35	12 50	13 5	I3 22	13 40	14 0	14 24
19 20	12 7	12 2I	12 35	12 51	13 6	I3 23	13 42	14 2	14 26
19 40	12 7	12 22	12 36	12 52	13 7	I3 25	13 44	14 5	14 29
20 0	12 7	12 22	12 36	12 52	13 S	13 26	13 46	14 7	14 32
20 20	12 7	12 22	12 37	12 53	13 10	13 28	13 47	14 10	14 35
20 40	12 7	12 22	12 37	12 54	13 11	13 29	13 49	14 12	14 37
21 0	12 7	12 23	12 38	12 55	13 12	13 31	13 51	14 14	14 40
21 20	12 7	12 23	12 39	12 56	13 13	13 32	13 53	14 16	14 43
21 40	12 7	12 23	12 39	12 56	13 14	13 34	13 55	14 19	14 46
22 0	12 7	I2 24	12 40	12 57	13 16	13 35	13 56	14 21	14 49
22 20	12 7	I2 24	12 41	12 58	13 17	13 37	13 58	14 23	14 52
22 40	12 7	I2 24	12 41	12 59	13 18	13 38	14 0	14 25	14 54
23 0	12 7	12 25	12 42	13 0	13 19	13 40	14 2	14 28	14 57
23 20	12 7	12 25	12 42	13 1	13 20	13 41	14 4	14 30	15 0
23 27	12 7	12 25	12 43	13 1	13 20	13 41	14 5	14 31	15 1

Declination				L	ATITUDI	E NORT	н.			
the Sun.	42°	44°	46°	48°	50°	52°	54°	56°	58°	60°
	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
+8° 0′	13 7	13 12	13 17	13 22	13 28	13 34	13 41	13 49	13 58	14 7
8 20	13 10	13 14	13 20	13 25	13 31	13 38	13 45	13 53	14 2	14 12
8 40	13 12	13 17	13 23	13 28	13 34	13 41	13 49	13 57	14 6	14 17
9 0	13 15	I3 20	13 25	13 31	13 38	13 45	13 53	14 I	14 11	14 22
9 20	13 17	I3 23	13 28	13 34	13 41	13 49	13 56	14 5	14 15	14 26
9 40	13 20	I3 25	13 31	13 38	13 44	13 52	14 0	14 IO	14 20	14 31
10 0	13 22	13 28	13 34	13 41	13 48	13 56	14 4	14 14	14 25	14 36
10 20	13 25	13 31	13 37	13 44	13 51	13 59	14 8	14 18	14 29	14 41
10 40	13 28	13 34	13 40	13 47	13 55	14 3	14 12	14 22	14 34	14 47
11 0	13 30	13 36	13 43	13 50	13 58	14 7	14 16	14 27	14 38	14 52
11 20	13 32	13 39	13 46	13 53	14 1	14 10	14 20	14 31	14 43	14 57
11 40	13 35	13 41	13 49	13 56	14 5	14 14	14 24	14 35	14 48	15 2
12 0	13 38	13 44	13 52	14 0	14 8	14 18	14 28	14 40	14 53	15 8
12 20	13 40	13 47	13 55	14 3	14 12	14 22	14 32	14 44	14 58	15 13
12 40	13 43	13 50	13 58	14 6	14 16	14 25	14 37	14 49	15 2	15 18
13 0	13 46	13 53	14 I	14 10	14 19	14 29	14 41	14 53	15 7	15 23
13 20	13 48	13 56	14 4	14 13	14 22	14 33	14 45	14 58	15 13	15 29
13 40	13 50	13 58	14 7	14 16	14 26	14 37	14 49	15 2	15 17	15 35
14 0	13 53	14 1	14 10	14 19	14 29	14 41	14 53	15 7	15 22	15 40
14 20	13 56	14 4	14 13	14 23	14 33	14 45	14 57	15 11	15 28	15 46
14 40	13 59	14 7	14 16	14 26	14 37	14 49	15 2	15 16	15 33	15 51
15 0	14 1	14 10	14 19	14 29	14 40	14 52	15 6	15 21	15 38	15 57
15 20	14 4	14 13	14 22	14 33	14 44	14 56	15 10	15 26	15 43	16 2
15 40	14 7	14 16	14 26	14 36	14 48	15 0	15 14	15 30	15 48	16 8
16 0	14 IO	14 19	14 29	14 40	14 52	15 4	15 19	15 35	15 53	16 14
16 20	14 I2	14 22	14 32	14 43	14 55	15 8	15 23	15 40	15 59	16 20
16 40	14 I5	14 25	14 35	14 46	14 59	15 13	15 28	15 45	16 4	16 26
17 0	14 17	14 28	14 38	14 50	15 3	15 17	15 32	15 50	16 10	16 32
17 20	14 20	14 31	14 41	14 53	15 7	15 21	15 37	15 55	16 15	16 38
17 40	14 23	14 34	14 45	14 57	15 10	15 25	15 41	16 0	16 20	16 45
18 0	14 26	14 37	14 48	15 I	15 14	15 29	15 46	16 5	16 26	16 51
18 20	14 29	14 40	14 52	15 4	15 18	15 34	15 50	16 10	16 32	16 58
18 40	14 32	14 43	14 55	15 8	15 22	15 38	15 55	16 15	16 38	17 4
19 0	14 35	14 46	14 58	15 11	15 26	15 42	16 0	16 20	16 44	17 11
19 20	14 37	14 49	15 1	15 15	15 30	15 46	16 5	16 25	16 50	17 17
19 40	14 40	14 52	15 5	15 19	15 34	15 51	16 10	16 31	16 56	17 24
20 0	14 43	14 55	15 8	15 22	15 38	15 55	16 15	16 37	17 2	17 31
20 20	14 46	14 58	15 11	15 26	15 42	16 0	16 20	16 42	17 8	17 38
20 40	14 49	15 2	15 15	15 30	15 46	16 4	16 25	16 47	17 14	17 46
21 0	14 52	15 5	15 19	15 34	15 50	16 9	16 30	16 53	17 20	17 53
21 20	14 55	15 8	15 22	15 38	15 55	16 13	16 35	16 59	17 27	18 1
21 40	14 58	15 11	15 26	15 42	15 59	16 18	16 40	17 5	17 34	18 8
22 0	15 1	15 14	15 29	15 46	16 3	16 23	16 45	17 11	17 40	18 16
22 20	15 4	15 18	15 33	15 49	16 7	16 28	16 50	17 17	17 47	18 24
22 40	15 7	-5 22	15 37	15 53	16 12	16 32	16 56	17 23	17 54	18 32
23 0	15 10	15 25	15 40	15 57	16 16	16 37	17 I	17 29	18 1	18 41
23 20	15 13	15 28	15 44	16 1	16 21	16 42	17 7	17 35	18 8	18 49
23 27	15 14	15 29	15 46	16 3	16 23	16 44	17 9	17 37	18 11	18 52

Declination					L,ATIT	UDE N	ORTH.				
of the Sun.	60°	61°	62°	63°	64°	65°	66°	67°	68°	69°	70°
	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
$ \begin{array}{c cccc} -23^{\circ} 27' \\ -23 & 20 \\ -23 & 0 \end{array} $	5 52 5 55 6 2	5 31 5 34 5 43	5 8 5 12 5 21	4 42 4 46 4 56	4 11 4 16 4 28	3 34 3 40 3 53	2 46 2 53 3 II	I 29 I 41 2 II			
-22 40 -22 20 -22 0	6 10 6 17 6 25	5 51 5 59 6 7	5 30 5 39 5 47	5 6 5 16 5 25	4 39 4 50 5 I	4 7 4 20 4 32	3 27 3 43 3 58	2 35 2 56 3 14	0 59 I 43 2 I3		
-21 40	6 32	6 14	5 56	5 34	5 11	4 43	4 11	3 3I	2 38	I I	
-21 20	6 39	6 22	6 4	5 43	5 20	4 55	4 24	3 47	2 59	I 45	
-21 0	6 46	6 29	6 12	5 52	5 30	5 5	4 36	4 I	3 18	2 16	
-20 40	6 52	6 37	6 20	6 I	5 40	5 16	4 48	4 16	3 35	2 4I	1 2
-20 20	6 59	6 44	6 27	6 9	5 49	5 26	4 59	4 29	3 51	3 2	1 47
-20 0	7 5	6 51	6 34	6 I7	5 58	5 35	5 10	4 41	4 6	3 22	2 19
-19 40	7 12	6 58	6 42	6 25 6 33 6 41	6 6	5 45	5 21	4 53	4 20	3 39	2 44
-19 20	7 18	7 4	6 49		6 14	5 54	5 31	5 5	4 34	3 55	3 6
-19 0	7 25	7 11	6 56		6 23	6 3	5 41	5 16	4 47	4 11	3 26
-18 40	7 3 ¹	7 17	7 4	6 48	6 31	6 12	5 51	5 26	4 59	4 25	3 44
-18 20	7 37	7 24	7 10	6 55	6 39	6 20	6 1	5 37	5 11	4 39	4 1
-18 0	7 43	7 31	7 17	7 3	6 47	6 29	6 10	5 47	5 22	4 52	4 16
-17 40	7 49	7 37	7 24	7 IO	6 55	6 38	6 19	5 57	5 33	5 5	4 31
-17 20	7 55	7 43	7 31	7 I7	7 2	6 46	6 28	6 7	5 43	5 17	4 45
-17 0	8 I	7 49	7 37	7 24	7 9	6 53	6 36	6 16	5 54	5 28	4 58
-16 40	8 6	7 55	7 44	7 31	7 17	7 I	6 44	6 26	6 4	5 40	5 11
- 16 20	8 12	8 1	7 50	7 38	7 24	7 9	6 52	6 35	6 14	5 51	5 23
- 16 0	8 17	8 7	7 56	7 44	7 31	7 I7	7 1	6 44	6 24	6 2	5 35
-15 40	8 23	8 13	8 2	7 51	7 38	7 25	7 9	6 52	6 34	6 12	5 47
-15 20	8 29	8 19	8 8	7 58	7 45	7 32	7 17	7 1	6 43	6 22	5 59
-15 0	8 34	8 25	8 15	8 4	7 52	7 39	7 25	7 9	6 52	6 32	6 10
-14 40	8 40	8 31	8 21	8 10	7 59	7 46	7 32	7 17	7 I	6 42	6 20
-14 20	8 45	8 36	8 27	8 17	8 5	7 53	7 40	7 26	7 IO	6 51	6 31
-14 0	8 50	8 42	8 33	8 23	8 12	8 I	7 47	7 34	7 IS	7 1	6 41
-13 40	8 56	8 47	8 38	8 29	8 19	8 7	7 55	7 41	7 26	7 10	6 51
-13 20	9 1	8 53	8 44	8 35	8 25	8 14	8 2	7 49	7 35	7 19	7 1
-13 0	9 6	8 58	8 50	8 41	8 32	8 21	8 10	7 57	7 43	7 28	7 10
-12 40	9 11	9 4	8 56	8 47	8 38	8 28	8 17	8 5	7 51	7 37	7 20
-12 20	9 17	9 10	9 2	8 53	8 44	8 34	8 24	8 12	7 59	7 45	7 29
-12 0	9 22	9 15	9 7	8 59	8 50	8 41	8 31	8 20	8 7	7 53	7 38
- II 40	9 27	9 20	9 13	9 5	8 56	8 47	8 38	8 27	8 15	8 2	7 47
- II 20	9 32	9 25	9 19	9 11	9 3	8 54	8 44	8 34	8 23	8 10	7 56
- II 0	9 37	9 31	9 24	9 17	9 9	9 0	8 51	8 41	8 31	8 18	8 5
-10 40	9 42	9 36	9 29	9 22	9 15	9 7	8 58	8 49	8 38	8 26	8 14
-10 20	9 47	9 41	9 35	9 28	9 21	9 13	9 5	8 56	8 46	8 34	8 22
-10 0	9 52	9 46	9 40	9 34	9 27	9 19	9 11	9 3	8 53	8 42	8 31
- 9 40	9 57	9 51	9 46	9 40	9 33	9 26	9 18	9 10	9 0	8 50	8 39
- 9 20	10 2	9 56	9 51	9 45	9 39	9 32	9 25	9 16	9 8	8 58	8 47
- 9 0	10 7	10 2	9 56	9 50	9 44	9 38	9 31	9 23	9 15	9 5	8 55
- 8 40	10 11	10 7	IO 2	9 56	9 50	9 44	9 37	9 30	9 22	9 13	9 3
- 8 20	10 16	10 12	IO 7	10 2	9 56	9 50	9 44	9 37	9 29	9 21	9 11
- 8 0	10 21	10 17	IO I2	10 7	10 2	9 56	9 50	9 43	9 36	9 28	9 19

Declination				L	ATITUDI	E NORT	н.			
of the Sun.	71°	72°	73°	74°	75°	76°	77°	78°	79°	80°
-23°27′ -23°20 -23°0 -22°40 -22°20 -22°0	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
-21 40 -21 20 -21 0 -20 40 -20 20 -20 0 -19 40 -19 20	I 3 I 50									
- 19 0 - 18 40 - 18 20 - 18 0 - 17 40 - 17 20 - 17 0	2 22 2 47 3 10 3 30 3 49 4 6 4 22	I 5 I 52 2 25 2 52 3 I4 3 35	I 6 I 55 2 29							
-16 40 -16 20 -16 0 -15 40 -15 20 -15 0	4 37 4 52 5 6 5 19 5 32 5 44	3 54 4 12 4 28 4 44 4 59 5 13	2 56 3 20 3 41 4 1 4 19 4 36	I 8 I 58 2 32 3 I 3 25 3 47	I 10 2 2 2 37					
-14 40 -14 20 -14 0 -13 40 -13 20 -13 0	5 56 6 8 6 19 6 29 6 40 6 51	5 27 5 40 5 52 6 5 6 17 6 29	4 52 5 7 5 21 5 35 5 49 6 2	4 7 4 26 4 43 5 0 5 16 5 31	3 6 3 31 3 54 4 14 4 34 4 52	1 13 2 5 2 42 3 12 3 38 4 2	I 15 2 10 2 48			
-12 40 -12 20 -12 0 -11 40 -11 20 -11 0	6 I 7 II 7 2I 7 3I 7 40 7 50	6 40 6 50 7 1 7 12 7 23 7 33	6 15 6 27 6 39 6 51 7 3 7 14	5 45 5 59 6 13 6 26 6 38 6 51	5 9 5 25 5 41 5 56 6 11 6 25	4 23 4 43 5 2 5 19 5 38 5 54	3 19 3 46 4 10 4 32 4 53 5 13	1 18 2 15 2 55 3 27 3 55 4 20	1 21 2 20 3 2	
-10 40 -10 20 -10 0 -9 40 -9 20 -9 0 -8 40	7 59 8 8 8 17 8 26 8 35 8 44 8 53	7 43 7 53 8 3 8 13 8 22 8 31 8 41	7 25 7 35 7 46 7 56 8 7 8 17 8 27	7 3 7 15 7 27 7 38 7 50 8 1	6 34 6 52 7 4 7 17 7 29 7 41 7 53	6 9 6 23 6 38 6 52 7 6 7 20 7 33	5 31 5 49 6 6 6 22 6 38 6 53 7 8	4 43 5 5 5 25 5 44 6 3 6 21 6 38	3 35 4 5 4 31 4 56 5 19 5 40 6 0	1 25 2 27 3 10 3 46 4 17 4 44 5 10
- 8 20 - 8 0	9 10	8 50 8 59	8 37 8 47	8 22 8 33	8 5 8 17	7 46 7 59	7 22 7 36	6 55	6 19 6 38	5 34 5 5 6

Declination of					LATITU	UDE N	ORTH.				
the Sun.	60°	61°	62°	63°	64°	65°	66°	67°	68°	69°	70°
-8° 0′	h. m.	h. m.	h. m.	h. m.	h. m.	h. m. 9 56	h. m. 950	h. m. 9 43	h. m. 9 36	h. m. 9 2 8	h. m. 9 19
-7 40 -7 20	10 26	10 22	10 17 10 23 10 28	10 13 10 18 10 23	10 8 10 13 10 19	10 2 10 8 10 14	9 56 10 3 10 9	9 50 9 57 10 4	9 43 9 50 9 57	9 35 9 43 9 50	9 27 9 35 9 43
-7 0 -6 40 -6 20 -6 0	10 35 10 40 10 45 10 50	10 32 10 37 10 42 10 47	10 33 10 38 10 43	10 29 10 34 10 40	10 25 10 31 10 36	10 20 10 26 10 32	10 15 10 22 10 28	10 10 10 16 10 23	10 4 10 11 10 18	9 57 10 5 10 12	9 51 9 58 10 6
-5 40 -5 20 -5 0	10 55 10 59	10 52 10 56	10 49 10 54 10 59	10 45 10 50 10 56	10 41 10 47 10 53	10 38 10 44 10 50	10 34 10 40 10 46	10 29 10 36 10 42	10 25 10 31 10 38	10 19 10 26 10 34	10 14 16 21 10 29
-4 40 -4 20 -4 0	11 8 11 13 11 18	11 6 11 11	11 4 11 9 11 14	II I II 7 II I2	10 58 11 4 11 10	10 55 11 1 11 7	10 52 10 58 11 4	10 49 10 55 11 1	10 45 10 52 10 58	10 41 10 48 10 55	10 36 10 44 10 51
-3 40 -3 20 -3 0	11 22 11 27 11 32	11 21 11 26 11 31	11 19 11 24 11 29	11 17 11 22 11 28	11 15 11 20 11 26	11 13 11 19 11 24	11 10 11 16 11 2 2	11 8 11 14 11 20	11 5 11 11 11 18	11 2 11 9 11 16	10 59 11 6 11 13
-2 40 -2 20 -2 0	11 37 11 41 11 46	11 35 11 40 11 45	11 34 11 39 11 44	11 33 11 38 11 43	11 31 11 37 11 43	11 30 11 36 11 41	11 28 11 34 11 40	11 27 11 33 11 40	11 25 11 32 11 38	11 23 11 30 11 37	11 21 11 28 11 35
-! 40 -! 20 -! 0	11 50 11 55 11 59	11 50 11 55 11 59	11 49 11 54 11 59	11 49 11 54 11 59	11 48 11 53 11 59	11 47 11 53 11 59	11 46 11 52 11 58	11 46 11 52 11 58	11 45 11 52 11 58	11 44 11 51 11 58	11 43 11 50 11 58
-0 40 -0 20	12 4 12 9	12 4 12 9	12 4	12 4 12 10	12 4 12 10	12 4 12 10	12 4 12 10	12 4 12 II	12 5 12 II	12 5 12 12	12 5 12 12
0 0 +0 20 0 40	12 13 12 18 12 22	12 14 12 19 12 23	12 14 12 19 12 24	12 15 12 20 12 25	12 15 12 20 12 26	12 16 12 22 12 27	12 16 12 22 12 28	12 17 12 23 12 29	12 18 12 25 12 31	12 19 12 26 12 33	12 19 12 27 12 34
I 0 I 20 I 40	12 27 12 32 12 37	12 28 12 33 12 38	12 29 12 34 12 39	12 31 12 36 12 41	12 32 12 37 12 43	12 33 12 39 12 44		12 36 12 42 12 49	12 38 12 44 12 51	12 40 12 47 12 54	12 41 12 49 12 56
2 0 2 20 2 40	12 41 12 46 12 50	12 43 12 47 12 52	12 44 12 49 12 54	12 46 12 52 12 57	12 48 12 53 12 59	12 56	12 59	12 55 13 1 13 7	12 58 13 4 13 11	13 I 13 8 13 15	13 4 13 11 13 19
3 0 3 20 3 40	12 55 13 0 13 4	12 57 13 2 13 7	12 59 13 5 13 10	13 2 13 7 13 13	13 5 13 10 13 16	13 13	13 17		13 17 13 24 13 31	13 22 13 29 13 36	13 26 13 34 13 41
4 0 4 20 4 40	13 14 13 14	13 17	13 20	13 18 13 23 13 29	13 22 13 27 13 32	13 31	13 35	13 40	13 38 13 45 13 52	13 43 13 50 13 58	14 4
5 0 5 20 5 40	13 23 13 28 13 33	13 32	13 35	13 34 13 40 13 45	13 44	13 49	13 54	13 59	14 12	14 12	14 19
6 0 6 20 6 40	13 38 13 43 13 47	3 13 47	13 51	13 56	14 1	14 1	7 14 12	14 19	14 26 14 33	14 34	14 43
7 0 7 20 7 40	13 52 13 57 14	7 14 2	14 7		14 18	3 14 2 1 14 3	14 3	14 39 14 46	14 48	14 57	15 7
8 0	14	7 44 12	14 17	14 23	14 30	14 3	7 14 4	5 14 52	15 2	15 13	15 23

Declination of				I,,	ATITUDI	E NORT	`H.			
the Sun.	71°	72°	73°	74°	75°	76°	77°	78°	79°	80°
-8° 0′	h. m.	h. m. 8 59	h. m. S 47	h. m. 8 33	h. m. 8 17	h. m. 7 58	h. m. 7 37	h. m. 7 10	h. m. 6 38	h. m. 5 56
-7 40	9 18	9 oS	8 56	8 43	S 2S	S 11	7 50	7 26	6 56	6 18
-7 20	9 26	9 17	9 6	8 53	S 39	8 23	8 4	7 41	7 14	6 38
-7 0	9 35	9 26	9 16	9 3	8 50	8 35	8 17	7 56	7 31	6 58
-6 40	9 43	9 34	9 25	9 14	9 1	8 47	8 30	8 11	7 47	7 17
-6 20	9 51	9 43	9 34	9 24	9 12	8 59	8 43	8 25	8 3	7 36
-6 0	9 59	9 52	9 43	9 34	9 23	9 11	8 56	8 39	8 19	7 54
-5 40	10 7	10 I	9 53	9 44	9 34	9 22	9 9	8 53	8 34	8 11
-5 20	10 15	10 9	10 2	9 53	9 44	9 34	9 22	9 7	8 50	8 28
-5 0	10 23	10 17	10 11	10 3	9 55	9 45	9 34	9 20	9 5	8 46
-4 40	10 31	10 26	10 20	10 13	10 5	9 56	9 46	9 34	9 19	9 2
-4 20	10 39	10 34	10 29	10 22	10 15	10 7	9 58	9 47	9 34	9 18
-4 0	10 47	10 43	10 38	10 32	10 26	10 18	10 10	10 0	9 49	9 34
-3 40	10 55	10 51	10 46	10 4I	10 36	10 29	IO 22	10 13	10 3	9 50
-3 20	11 3	10 59	10 55	10 51	10 46	10 40	IO 34	10 26	10 17	10 6
-3 0	11 11	11 8	11 4	11 0	10 56	10 51	IO 45	10 39	10 31	10 22
-2 40	11 19	11 16	II 13	11 10	11 6	II 2	10 57	10 52	10 45	10 37
-2 20	11 2 6	11 24	II 22	11 19	11 16	II 13	11 8	11 4	10 59	10 52
-2 0	11 34	11 32	II 31	11 28	11 26	II 23	11 20	11 17	11 13	11 8
- I 40	11 42	11 41	11 39	11 38	11 36	II 34	11 32	11 29	11 26	11 23
- I 20	11 49	11 49	11 48	11 47	11 46	II 45	11 43	11 42	11 40	11 38
- I 0	11 57	11 57	11 56	11 56	11 56	II 55	11 55	11 55	11 54	11 53
-0 40	12 5	12 5	12 5	12 5	12 6	12 6	12 7	12 7	12 8	12 8
-0 20	12 13	12 13	12 14	12 15	12 16	12 17	12 18	12 20	12 21	12 2 3
9 0	12 20	12 22	12 22	12 24	12 26	12 28	12 29	12 32	12 35	12 38
+ 0 20	12 28	12 30	12 31	12 34	12 36	12 38	12 41	12 44	12 49	12 53
0 40	12 36	12 38	12 40	12 43	12 46	12 49	12 53	12 57	13 2	13 9
I 0	12 44	12 46	12 49	12 52	12 56	13 O	13 5	13 10	13 16	13 24
I 20	12 52	12 55	12 58	13 2	13 6	13 II	13 16	13 2 3	13 30	13 40
I 40	12 59	13 3	13 7	13 11	13 16	13 22	13 28	13 36	13 44	13 55
2 0	13 7	13 11	13 16	13 20	13 26	13 3 2	13 40	13 49	13 5 9	14 11
2 20	13 15	13 19	13 25	13 30	13 36	13 43	13 52	14 1	14 13	14 27
2 40	13 23	13 28	13 33	13 40	13 46	13 54	14 4	14 14	14 2 8	14 43
3 0	13 31	13 36	13 42	13 49	13 57	14 5	14 16	14 28	14 42	14 59
3 20	13 39	13 44	13 51	13 59	14 7	14 17	14 28	14 41	14 56	15 16
3 40	13 47	13 53	14 I	14 8	14 17	14 28	14 40	14 55	15 11	15 33
4 0	13 55	I4 2	14 10	14 18	14 28	I4 40	14 53	15 8	15 27	15 50
4 20	14 3	I4 I0	14 19	14 28	14 38	I4 5I	15 5	15 22	15 ·43	16 7
4 40	14 11	I4 I9	14 28	14 38	14 49	I5 2	15 18	15 36	15 58	16 25
5 0	14 19	14 28	14 37	14 48	15 O	15 14	15 31	15 50	16 14	16 44
5 20	14 27	14 37	14 46	14 58	15 II	15 26	15 44	16 5	16 31	17 3
5 40	14 35	14 45	14 56	15 8	15 22	15 38	15 57	16 2 0	16 47	17 22
6 0	I4 44	14 54	15 5	15 19	15 33	15 50	16 11	16 35	17 5	17 43
6 20	I4 52	15 3	15 15	15 29	15 44	16 3	16 25	16 51	17 23	18 5
6 40	I5 I	15 12	15 25	15 40	15 56	16 16	16 39	17 7	17 41	18 27
7 0	15 10	15 22	15 35	15 50	16 8	16 29	16 53	17 23	18 1	18 50
7 20	15 18	12 31	15 45	16 1	16 20	16 42	17 8	17 40	18 21	19 16
7 40	15 27	15 40	15 55	16 12	16 32	16 55	17 23	17 58	18 42	19 44
8 0	15 35	15 50	16 5	16 23	16 44	17 9	17 39	18 16	19 5	20 15

Declination					LATITU	JDE N	ORTH.				
of the Sun.	60°	61°	62°	63°	64°	65°	66°	67°	68°	69°	70°
	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.	h. m.
+ 8° 0′ 8 20 8 40	14 7 14 12 14 17	14 12 14 1; 14 22	14 17 14 23 14 28	14 23 14 29 14 35	14 30 14 36 14 42	14 37 14 43 14 50	14 45 14 52 14 58	14 53 15 0 15 7	15 2 15 10 15 17	15 12 15 20 15 28	15 23 15 32 15 40
9 0 9 20 9 40	14 22 14 27 14 32	14 27 14 32 14 38	14 34 14 39 14 45	14 41 14 46 14 52	14 48 14 54 15 0	14 56 15 2 15 9	15 5 15 11 15 18	15 14 15 21 15 28	15 25 15 32 15 40	15 36 15 44 15 52	15 49 15 57 16 6
10 0 10 20 10 40	14 37 14 42 14 47	14 43 14 49 14 54	14 50 14 56 15 2	14 58 15 4 15 10	15 6 15 13 15 19	15 15 15 22 15 28	15 25 15 32 15 39	15 35 15 43 15 5 0	15 47 15 55 16 3	16 0 16 8 16 17	16 15 16 24 16 33
11 0 - 11 20 - 11 40	14 52 14 57 15 2	14 59 15 5 15 10	15 7 15 13 15 19	15 16 15 22 15 28	15 25 15 31 15 38	15 35 15 41 15 48	15 46 15 53 16 0	15 58 16 5 16 13	16 11 16 19 16 27	16 26 16 34 16 43	16 42 16 52 17 1
12 0 12 20 12 40	15 8 15 13 15 18	15 16 15 21 15 27	15 25 15 31 15 36	15 34 15 40 15 46	15 44 15 50 15 57	15 55 16 2 16 9	16 7 16 15 16 22	16 21 16 2 9 16 37	16 35 16 44 16 53	16 52 17 1 17 11	17 11 17 21 17 31
13 0 13 20 13 40	15 23 15 29 15 35	15 33 15 39 15 44	15 42 15 48 15 55	15 53 15 59 16 5	16 4 16 11 16 17	16 16 16 23 16 31	16 30 16 37 16 45	16 45 16 53 17 1	17 2 17 10 17 19	17 20 17 30 17 40	17 41 17 52 18 3
14 0 14 20 14 40	15 40 15 46 15 51	15 50 15 56 16 2	16 I 16 7 16 I3	16 12 16 19 16 25	16 24 16 31 16 38	16 38 16 46 16 53	16 53 17 1 17 9	17 10 17 19 17 28	17 29 17 38 17 48	17 50 18 0 18 11	18 14 18 26 18 38
15 0 15 20 15 40	15 57 16 2 16 8	16 8 16 14 16 20	16 19 16 26 16 32	16 32 16 39 16 46	16 46 16 53 17 I	17 I 17 9 17 17	17 17 17 26 17 35	17 37 17 46 17 55	17 58 18 8 18 18	18 22 18 33 18 45	18 50 19 3 19 16
16 0 16 20 16 40	16 14 16 20 16 26	16 26 16 32 16 39	16 39 16 46 16 52	16 53 17 0	17 8 17 16 17 23	17 25 17 33 17 41	17 44 17 53 18 2	18 5 18 15 18 25	18 29 18 40 18 51	18 57 19 10 19 23	19 30 19 45 20 1
17 0 17 20 17 40	16 32 16 38 16 45	16 45 16 52 16 58	16 59 17 6 17 13	17 14 17 22 17 29	17 31 17 39 17 47	17 50 17 59 18 8	18 11 18 21 18 31	18 35 18 46 18 57	19 3 19 15 19 28	19 36 19 50 20 6	20 17 20 35 20 55
18 0 18 20 18 40	16 51 16 58		17 20 17 28 17 35	17 37 17 45 17 53	17 56 18 5 18 14	18 17 18 26 18 36	18 41 18 52 19 3	19 8 19 20 19 33	19 41 19 55 20 10	20 22 20 40 20 59	21 17 21 42 22 13
19 0 19 20 19 40	17 11 17 17 17 24	17 33	17 43 17 51 17 59	18 2 18 10 18 19	18 23 18 32 18 41	18 56	19 25	19 46 20 0 20 14	20 26 20 44 21 3	21 20 21 45 22 16	22 58
20 0 20 20 20 40	17 31 17 38 17 45	17 56	18 7 18 15 18 2 3	18 28 18 37 18 46	18 51 19 1 19 12	19 30	20 4	20 30 20 47 21 5	21 23 24 47 22 17		
21 0 21 20 21 40	17 52 18 6 18 8	18 20		18 56 19 6 19 16	19 34	20 8	20 50	21 50	23 I		
22 0 22 20 22 40	18 16 18 24 18 32	1 18 46	19 10		20 I	20 53	21 52	1			
23 0 23 20 23 27	18 4 18 4 18 5	9 19 13	19 41	20 14	20 50	5 21 54	1				

LATITUDE NORTH. Declination the Sun. 71° 72° 73° 74° 75° h. m. h. m. h. m. h. m. h. m. 8° 0′ 16 5 15 35 16 23 16 44 15 50 16 35 16 57 8 20 15 44 16 16 15 59 S 40 15 53 16 16 26 16 46 17 10 9 9 0 16 16 37 16 19 16 58 17 23 3 16 48 9 20 16 12 16 29 17 37 17 10 40 16 22 16 59 9 16 39 17 23 17 51 10 0 16 31 16 50 17 11 17 35 18 -5 16 41 IO 20 17 22 17 18 20 0 17 49 17 34 10 40 16 50 17 11 18 18 36 11 0 17 47 18 16 18 52 17 17 22 18 31 ΙI 20 17 11 17 34 17 59 19 ΙI 40 17 22 17 45 18 13 18 46 19 27 12 18 26 0 17 32 17 57 19 19 46 18 40 12 20 18 9 17 43 19 18 20 7 18 55 12 40 18 22 17 55 19 35 20 29 18 35 13 0 ıS 6 19 11 19 54 20 55 18 49 19 26 13 20 18 18 20 14 21 23 18 30 13 40 19 19 43 20 35 21 59 14 0 18 43 20 19 17 21 22 50 0 20 20 20 1.1 18 56 19 33 21 28 20 41 1.1 40 19 10 19 49 22 15 0 21 5 20 7 19 24 22 52 15 20 19 40 20 26 21 32 1.5 22 5 40 19 55 20 46 16 0 20 13 21 10 22 54 20 20 31 21 36 40 20 51 22 17 0 21 13 22 56 17 20 21 39 17 40 22 II 76° 77° 78° 79° 80° 8° 0' 18 16 17 9 17 39 19 5 20 15 17 55 8 20 17 23 1S 35 19 29 20 50 8 40 17 38 18 12 18 56 19 56 21 33 9 0 18 30 53 19 17 20 25 22 35 ı8 18 48 20 9 19 41 20 59 40 IS 25 8 9 19 20 6 21 40 18 41 10 0 19 28 20 31 22 39 18 59 10 20 19 50 21 6 40 19 18 20 15 21 46 11 0 19 38 20 41 22 43 TI 20 19 59 21 13 ΙI 40 20 23 21 50 12 0 20 49 22 46 12 20 21 19 21 55 12 40

DECLINATION OF THE SUN FOR THE YEAR 1899, AT GREEN-WICH APPARENT NOON.

WIC	H APPA	RENT N	OON.
Day of Month.	Jan.	Feb.	Mar.
1 4 7 10 13	-23° 0′ -22 44 22 22 21 57 21 28	-17° 4′ 16 12 15 16 14 19 13 19	7° 33′ 6 24 5 14 4 4 2 53
16 19 21 24 27 30	20 55 20 19 19 53 19 11 18 26 17 38	12 18 11 14 10 31 9 25 8 18	I 42 - 0 3I + 0 16 I 27 2 38 3 48
	Apr.	May.	June.
1 4 7 10 13	+ 4° 34′ 5 43 6 51 7 58 9 4	+15° 6′ 15 59 16 50 17 38 18 24	+22° 4' 22 27 22 46 23 I 23 I3
16 19 21 24 27 30	10 9 11 12 11 53 12 53 13 51 14 48	19 7 19 47 20 12 20 47 21 19 21 47	23 22 23 26 23 27 23 25 23 20 23 11
	July.	Aug.	Sept.
1 4 7 10 13	+23° 7′ 22 53 22 36 22 15 21 50 21 22	+ IS° 1′ 17 15 16 26 15 34 14 40	+ 8° 17′ 7 11 6 4 4 56 3 47
19 21 24 27 30	20 51 20 29 19 52 19 13 18 31	13 44 12 46 12 7 11 6 10 4 9 0	2 38 I 28 + 0 42 - 0 29 I 39 2 49
	Oct.	Nov.	Dec.
1 4 7 10	- 3° 12′ 4 22 5 31 6 40 7 48	—14° 27′ 15 24 16 18 17 10 18 0	-21° 50′ 22 16 22 38 22 56 23 10
16 19 21 24 27 30	8 55 10 0 10 43 11 47 12 48 13 49	18 46 19 29 19 56 20 35 21 9 21 40	23 20 23 26 23 27 23 26 23 20 23 10

DURATION OF ASTRONOMICAL TWILIGHT.

(Interval between sunrise or sunset and the time when the true position of the sun's center is 18° below the horizon.)

							_	_	_	_	_		_	=		=	=		_	_	_		_	_			=[
										NO	RT	н	AT	ıπ	JDE												
Date.	0 °	10	0 2	20°	2	5°	30°	3	2°	3	4°	3	6°	3	3°	4	0°	42	2°	44	0	46	5°	48	3°	50	o°
Jan. 1	h. m. I 14 I 14 I 13	1 1	5 1	18	I	21	I 20		28	1	29	T	31	T	22	Ť	36	I	30	I 4	.3	1	47	I	53 52	h. I I	59 57
Гев. I	I 12 I 11 I 10	I	12 I 12 I 11 I	15 14 13	I I	18 17 16	I 2: I 2: I 2:	2 I I I	24 23 22	I	26 25 24	I I I	28 27 26	I I	30 29 28	I I I	33 32 31	I I	36 34 33	I 3 I 3 I 3	39 37 36	I I I	43 41 40	I I	47 45 44	I I I	52 49 48
Mar. 1	I 00	I	10 1	13	I	16	I 2	9 I	22	I	24	I	26	I	29	Ι	31	I	34	I ,	37	Ι	4 I	I	45	I	
Apr. 1	I 00	I I	11 1	1 16	I	20	1 2 I 2	4 I	2'	7 1	29	I	32	I	36	I	39	I I	30 43		43 48	I	54	I 2	54 01	2	08
May 1	I I	3 I 3 I	14	1 10	I	24 26	1 3	2 1	1 3	5 1	39) 1	43	I	48	I	54	2	OI	2	10	2	20	2	35	2	35 58
June 1	II	5 I 5 I	17	I 2.	1 I	29	I 3	37	I 4	I	L 4:	5 1	50) 1	56	2	03	2	13	2	25	2	44	3	IÒ)	
July 1	II	4 I 3 I	15	I 2, I 2	3 I I I	20	I	32	I 3	6	I 3	9	I 4.	3 1	: 48	3 1	54	. 2	0	2	10	2	21	2	30	3	00
Aug. 1	II	2 I I I	13	II	6 1	20	I I	24	I 2	27	I 3	0	I 3	3	1 3	6 1	1 39	1	4.	3 I	48	1	54	1 2	0	1 2	2 00
Sept. 1	I	09 I	10	II	3	I I	3 I 7 I 5 I	20	I	22	I 2	24	I 2	6	I 2	9	1 3	í i	1 3	4 I	37	7	I 4	I	[4	5	1 50
Oct. 1	I I C	10 I	10	I I	13	I I	6 I 6 I	19 19 20	I I	2 I 2 I 2 2	I 2	23	I 2 I 2 I 2	25	I 2 I 2 I 2	8 8 8	I 3° I 3° I 3	0	I 3 I 3	3 I 3 I	36 36 30	5	I 3 I 3 I 4	9	I 4 I 4 I 4	3	I 48
Nov. 1	III	12 1	1 1 2	I	17	I 2	7 I 8 I 0 I	24	I	26	I	28	I ;	30	I 3	32	1 3	5	I 3	38 1	4	2	I 4	6	I 2	19	1 5
	ıı	14	I 14	1	18	I 2	21 I 22 I 22 I	25	I	27	I	29	I,	31	I 3	33	I 3	6	I d	10	I 4	4	I Z	17	I	52	I 5

DURATION OF CIVIL TWILIGHT.

(Interval between sunrise or sunset and the time when the true position of the sun's center is 6° below the horizon.)

[Minutes.]

D /	NORTH LATITUDE.														
Date.	O°	10°	20°	25°	30°	32°	34°	36°	38°	40°	42°	44°	46	48°	50°
Jan. 1	22	22	24	25 25	27 26	27 27	28 28	28	29 20	30	32 31	33	34	36	39 38
11 21	22	22	24	24	26	26	27	27	28	29	30	32	33	35 34	37
Feb. 1	22	22	23	24 23	25 25	26 26	27 26	27 27	27 27	28 28	20) 20	31 30	32 31	34 33	35 34
21	2 I	22	22	23	24	25	25	26	27	28	28	29	30	32	33
Mar. 1	2 I 2 I	22 2I	2 2 2 2	23 23	24 24	24 24	25 25	26 26	27 26	28 27	28 27	29 20	30 30	3 I 3 I	33 32
21	2 I	2 I	22	23	24	24	25	26	26	27	- 27	28	30	31	33
Apr. 1	2 I 2 I	2 I 2 2	22 22	23 23	24	25 25	25 26	26 26	27 27	28 28	28 28	29 29	30 31	32 32	33 34
2 I	22	22	22	23	25	25	26	27	28	28	29	30	32	34	35
May 1	22	22	23 23	24 24	25 26	26 27	27 28	28 29	28 29	29 30	30 31	32	33 35	35 36	36 39
21	22	22	24	25	27	28	28	29	30	31	33	35	36	38	41
June 1	22	22	24 24	25 26	27 28	28 28	28 29	29 30	31 31	3 ² 33	34	36 36	37 38	40 41	43 44
2 I	22	23	25	26	28	29	29	30	31	33	34	36	38	42	44
July 1	22	23	24 24	26 25	28 27	28 28	29	30 29	31 31	33 32	34 34	36 36	38 37	41 40	44 43
2 I	22	22	24	2.5	27	28	28	29	30	31	33	35	36	38	41
Aug. 1	22	22	23 23	24	26	27 26	28	29 28	28	20	30	33	35	36 35	39 36
2 I	22	22	22	23	25	25	26	28	28	28	29	30	32	34	35
Sept. 1	2 I 2 I	22 2I	22	23	24	25 25	26 25	26 26 26	27 27 26	28	28	29	30	32 31	34
21	21	21	22	23	24	24	25	26	26	27	27	29	30	31	32
Oct. 1	2 I 2 I	2 I 22	22	23	24 24 24	24	25 25 25	26 26	27 27	27 28 28	27 28 28	29	30	31 31 32	33
Nov. 1	2 I 2 2	22	22	23	25	²⁵	25	27	28	28	20	30	31	33	33
1 I I 2 I	22 22 22	22 22 22	23	24 24	25 26	26 26	27 27	28	28 28	29	30	31 32	32	33	35 37
Dec. 1	22	22	23	25	26	27	28	28	20	30	31	33	34	35	38
11 21	22 22 22	22 23	24 24 24	25 25 25	27 27	27 27	28 28	28	29	30	32	33	34	36 37	39

RELATIVE INTENSITY OF SOLAR RADIATION.

Mean intensity J for 24 hours of solar radiation on a horizontal surface at the top of the atmosphere and the solar constant A, in terms of the mean solar constant A₀.

		R	ELATI	VE M	EAN T	VERTI	CAL I	NTENS	SITY ($\left(\frac{J}{A_{\circ}}\right)$)·	
Date.	Longitude of the Sun.				LA'	ritudi	E NOR	тн.				$\frac{A}{A_{\circ}}$.
		0°	10°	20°	30°	40°	50°	60°	70°	80°	90°	
Jan. 1	0.99	0.303	0.265	0,220	0.169	0.117	0.066	0.018				1.0335
16	15.78	.307	.271	.229	.180	.129	.078	.028				1.0324
Feb. 1	31.54	.312	.282	.244	.200	.150	.100	.048	0.006			1.0288
15	45.34	.317	.293	.261	.223	.177	.118	.075	.027			1.0235
Mar. 1	59.14	.320	.303	.279	.245	.204	.158	.108	.056	0.013		1.0173
16	73.93	.321	.313	.296	.270	.236	• 195	.148	.097	.057		1.0090
<i>Apr</i> . 1	89.70	.317	.319	.312	.295	.269	.235	.195	.148	.101	0.082	0.9923
									252			
May 1	119.29	.303	.318	.330	.329	.320	.302	.278	.253	.255	.322	0.9841
June 1	149.82	.287	.315	.334	•345	•349	-345	.337	.344	.360	.366	0.9714
16	164.60	.283	.313	•334	.348	•354	-353	.348	.361	.378	.384	0.9679
July 1	179.39	.283	.312	.333	-347	.352	.351	.345	.356	-373	.379	0.9666
16	194.13	.287	.314	.332	.342	•345	.340	.329	.331	•347	.352	0.9674
Aug. 1	209.94	.294	.316	.330	-334	.330	.318	.300	.282	.295	.300	0.9709
16	224.73	.303	.318	.325	.322	.310	.291	.264	.234	.227	.231	0.9760
Sept. 1	240.50 255.29	.310	.318	.316	.305	.285	.256	.220	.180	.139	.043	0.9828
Oct. 1	270.07 284.86	.317	.308	.289	.261	.225	.183	.135	.084	.065		0.9995 1.0080
Nov. I	300.63	.312	.286	.251	.211	.164	.114	.063	.018			1.0164
16	315.42	.308	.276	.235	.190	.140	.089	.040				1.0235
Dec. 1	330.19	.304	.267	.224	.175	.124	.072	.024				1.0288
16	344.98	.302	.263	.218	.167	.115	.064	.016				1.0323
Year		0.305	0.301	0.289	0.268	0.241	0.209	0.173	0.144	0.133	0.126	
					<u> </u>	1				<u> </u>		l

TABLE 99.

RELATIVE AMOUNTS OF SOLAR RADIATION RECEIVED ON A

HORIZONTAL SURFACE DURING THE YEAR AT DIFFERENT LATITUDES.

Latitude.		AIMOSPHERIC	TRANSMISSION	COEFFICIENT.	1
(North.)	1.0	0.9	0.8	0.7	0.6
Equator.	439	374	316	262	213
10°	433	368	310	257	209
20°	416	350	293	242	195
30°	386	322	266	213	171
20° 30° 40°	347	284	231	185	144
50°	301	239	100	149	114
60°	240	101	148	113	84
60° 70° 80°	207	152	113	83	60
80°	192	134	94	64	43
90°	181	125	94 85	56	35

TABLE 100.

AIR MASS, M, CORRESPONDING TO DIFFERENT ZENITH DISTANCES OF THE SUN.

				SUN'S ZENITH DISTANCE.													
0.	1 '	2 °	3∘	4	5°	6°	7 °	8 °	9°								
AIR MASS.																	
1.00																	
I.02					I. 04												
1.06	1.07	1.08	1.00	I.00	1.10	1.11	I.I2	1.13	1.14								
1.15	1.17	1.18	1.19	I.20	I.22	1.23	1.25	1.27	1.28								
1.30	1.32	1.34	1.37	1.39	1.41	I.44	1.46	1.49	1.52								
1.55	1.59	1.62	1.66	1.70	I.74	1.78	1.83	1.88	1.04								
2.00	2.06	2.I2	2.19	2.27	2.36	2.45	2.55	2.65	2.77								
2.90	3.05	3.21	3.39	3 - 59	3.82	4.07	4.37	4.72	5.12								
5.60	6.18	6.88	7 . 77	8.90	10.30	12.44	15.36	19.79	26.96								
	1.02 1.06 1.15 1.30 1.55 2.00 2.90	1.02 1.06 1.07 1.15 1.30 1.32 1.55 1.59 2.00 2.06 2.90 3.05	1.02 1.06 1.07 1.15 1.17 1.18 1.30 1.32 1.34 1.55 1.59 1.62 2.00 2.06 2.12 2.00 3.05 3.21	1.02 1.06 1.07 1.08 1.09 1.15 1.17 1.18 1.19 1.30 1.32 1.34 1.37 1.55 1.59 1.62 1.66 2.00 2.06 2.12 2.19 2.00 3.05 3.21 3.39	1.00 1.02 1.06 1.07 1.18 1.19 1.20 1.30 1.32 1.34 1.37 1.39 1.55 1.59 1.62 1.66 1.70 2.00 2.06 2.12 2.19 2.27 2.00 3.05 3.21 3.39 3.59	1.00 1.02 1.06 1.07 1.15 1.17 1.32 1.34 1.37 1.39 1.41 1.55 1.59 1.62 1.66 1.70 1.74 2.00 2.06 2.12 2.19 2.00 3.05 3.21 3.39 3.59 3.82	1.00 1.02 1.06 1.07 1.15 1.17 1.32 1.34 1.37 1.39 1.41 1.44 1.55 1.59 1.62 1.66 1.70 1.74 1.78 2.00 2.06 2.12 2.19 2.27 2.36 2.45 2.90 3.05 3.21 3.39 3.59 3.82 4.07	1.00 1.02 1.06 1.07 1.15 1.17 1.32 1.34 1.37 1.39 1.41 1.44 1.55 1.59 1.62 1.66 1.70 1.74 1.78 1.83 2.00 2.06 2.12 2.19 2.27 2.36 2.45 2.55 2.90 3.05 3.21 3.39 3.59 3.82 4.07 4.37	1.00 1.02 1.06 1.07 1.08 1.00 1.00 1.10 1.11 1.12 1.13 1.15 1.17 1.18 1.19 1.20 1.22 1.23 1.25 1.27 1.30 1.32 1.34 1.37 1.39 1.41 1.44 1.46 1.49 1.55 1.59 1.62 1.66 1.70 1.74 1.78 1.83 1.88 2.00 2.06 2.12 2.19 2.27 2.36 2.45 2.55 2.65 2.00 3.05 3.21 3.30 3.59 3.82 4.07 4.37 4.72								

TABLE 101.

RELATIVE ILLUMINATION INTENSITIES.

Source of illumination.	Intensity.	Ratio to zenithal full moon.
Zenithal sun Sky at sunset Sky at end of civil twilight Zenithal full moon Quarter moon Starlight	Foot-candles. 9000.0 33.00 0.40 0.02 0.002 0.0008	465000.0 1650.0 20.0 1.0 0.1

MISCELLANEOUS TABLES.

WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

English measures—Temperature term	TABLE	102
Humidity term; auxiliary table	TABLE	103
Humidity and pressure terms, combined	Table	104
Metric measures—Temperature term	TABLE	105
Humidity term; auxiliary to table 107.	TABLE	100
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Atmospheric water-vapor lines in the visible spectrum	TABLE	108
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Energy distribution and atmospheric transmission of solar radiation	TABLE	111
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International Cloud Classification	TABLE	113
Beaufort Weather Notation	TABLE	114
International code of horizontal visibility	TABLE	115
List of meteorological stations	TABLE	116

WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Temperature term: $\delta_t = \frac{0.0012930}{1 + 0.002039~(t - 32^\circ)}$ Fahrenheit temperatures.

1 cubic centimeter of dry air at the temperature of 32°F. and pressure 760 mm., under the standard value of gravity, weighs 0.0012930 gram.

Tempera- ture	δ_t	$\text{Log } \delta_t$	Tempera- ture	δ_t	$\text{Log } \delta_t$	Tempera- ture	δ_t	$\text{Log }\delta_t$
F.	0.00	-10	F.	0.00	-10	F.	0.00	-10
_45°	15338	7.18577	30°	12983	7.11339	75°	11888	7.07512
-43	15155	.18056	31	12956	.11247	76	11866	.07430
-40 -25	14976	.17540	32	12930	.11160	77	11843	.07346
-35	14801	.17029	33	12904	.11073	78	11821	.07265
-30	14630	.16524		12877	.10981	79	11799	.07185
-25	0.00	.10524	34	0.00	.10901	19	0.00	.07103
_20	14463	7.16026	35	12851	7.10894	80	11777	7.07103
-18	14398	.15831	36	12825	.10806	81	11756	.07026
-16 -16	14333	.15634	37	12800	.10721	82	11734	.06946
-10 -14	14268	.15436	37 38	12774	.10633	83	11712	.06863
-12	14204	.15241	39	12748	.10544	84	11691	.06785
12	0.00		39	0.00	77.0944	1	0.00	,05
-10	14141	7.15048	40	12722	7.10456	85	11669	7.06703
— 8	14078	.14854	41	12697	.10370	86	11648	.06625
— 6	14016	.14663	42	12672	.10285	87	11626	.06543
- 4	13954	.14470	43	12646	.10195	88	11605	.06466
- 2	13893	.14279	44	12621	.10109	89	11584	.06387
~	0.00	1-1-1	1	0.00		1	0.00	
± 0	13832	7.14088	45	12596	7.10023	90	11563	7.06307
+ 1	13803	.13997	46	12571	.09937	91	11542	.06228
2	13773	.13903	47	12546	.09851	92	11521	.06149
3	13743	.13808	48	12522	.09767	93	11500	.06070
4	13713	.13713	49	12497	.09682	94	11479	.05992
II.	0.00	0, 0	1	0.00			0.00	
5	13683	7.13618	50	12472	7.09594	95	11458	7.05913
6	13654	.13527	15	12448	.09511	96	11438	.05835
	13625	.13434	52	12424	.09426	97	11417	.05755
7 8	13595	.13338	53	12399	.09338	98	11396	.05675
9	13566	.13245	54	12375	.09256	99	11376	.05600
	0.00			0.00		400	0.00	
10	13537	7.13152	55	12351	7.09171	100	11356	7.05523
II	13508	.13062	56	12327	.09087	101	11335	.05442
12	13480	.12970	57	12303	.09002	102	11315	.05367
13	13451	.12875	58	12279	.08916	103	11295	.05290
14	13423	.12785	59	12255	.08831	104	11275	.05213
45	0,00		CO.	0.00	0	105	0.00	
15	13394	7.12691	60	12232	7.08750	105	11254	7.05131
16	13366	.12600	61	12208	.08665	106	11235	.05058
17	13338	.12510	62	12185	.08583	107	11215	.04982
18	13310	.12419	63	12161	.08497	108	11195	.04902
19	13282	.12328	64	0.00	.08416	109	0.00	.04024
20	0.00	7.12235	65	12115	7.08334	110	11156	7.04752
21	13254	.12147	66	12092	.08251	112	11117	.04599
21 22	13227		67	12069	.08168	114	11078	.04399
23	13199	.12054	68	12009	.08085	114	11039	.04293
23	131/2	.11900	69	12023	.08003	811	11001	.04145
24	0.00	110/3	39	0.00			0.00	1-10
25	13117	7.11783	70	12000	7.07918	120	10963	7.03994
26	13090	.11694	71	11978	.07839	125	10869	.03619
	13063	.11604	72	11955	.07755	130	10777	.03250
27 28	13036	.11514	73	11933	.07675	135	10686	.02883
29	13010	.11428	74	11910	.07593	140	10597	.02518

WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Humidity term: Values of 0378 e.

Auxiliary to Table 104.

e = Vapor pressure in inches.

(See Tables 74 and 75.)

Temperature by normal hydrogen thermometer.

Dew- Point.	Vapor Pressure. (Ice.)	0.378 e	Dew- Point.	Vapor Pressure. (*)	0.378 e	Dew- Point,	Vapor Pressure. (Water.)	0.378 e	Dew- Point.	Vapor Pres- sure. (Water.)	0.378 e
F.	Inch.	Inch.	F.	Inch.	Inch.	F.	Inch.	Inch.	F.	Inches.	Inches.
-60°	0.0010	0.000	– 10°	0.0223	0.008	40°	0.2477	0.094	90°	1.423	0.538
59	.0011	.000	9	.0236	.009	41	.2575	.097	91	1.469	-555
58	1100.	.000	8	.0249	.009	42	.2677	.101	92	1.515	.573
57	.0012	.000	7	.0263	.010	43	.2782	.106	93	1.563	.591
56	.0013	.000	6	.0277	.010	44	.2891	.100	94	1.612	- 1
-55	0.0014	0.001	5	0.0292	0.011	45	0.3003	0.114	95	1.662	0.628
54	.0015	.001	4	.0308	.012	46	.3120	.118	96	1.714	.648
53	.0016	100.	3	.0325	.012	47	.3240	.122	97 98	1.767	.689
52	.0017	100.	2	.0343	.013	48	.3365	.127	99	1.878	.710
51	.0018	100,	I	.0361	.014	49	•3493	.132		1	
-50	0.0020	0.001	± 0	0.0381	0.014	50	0.3626	0.137	100	1.936	0.732
49	.0021	.001	+ 1	.0401	.015	51	.3763	.142	10I 102	2.055	·754
48	.0023	100.	2	.0423	.016	52	.3905	.147	103	2.055	.800
47	.0024	.001	3	.0445	.017	53	.4052		103	2.181	.824
46	.0026	100.	4	.0468	.018	54	.4203			2.246	0.849
-45	0.0028	0.001	+ 5	0.0493	0.019		0.4359	.171	106	2.314	.875
44	.0029	.001	6	.0519	.020		.4521			2.382	.900
43	.0031	.001	7 8	.0546	.021	0	.4859			2.453	.927
42	.0033	100.	1	.0574	.023		.5037			2.525	.954
41	.0036		9				0.5220		1	2.599	0.982
-40	0.0038		+ 10	0.0635	0.024		.5400			2.676	
39	.0040		11	.0667	.025		.5602			2.754	1.041
38	.0043		12	.0736			.580			2.833	
37	.0046		13	.0773	1		.601		1	2.915	
36	.0049			0.0812	1		0.6220			2.000	1.134
-35	0.0052		+ 15	.0852			.644	,		3.085	1 77
34	.0055		17	.0895			.6674			3.173	1.199
33	.0059		18	.0939		1 6	.690		118	3.264	
3 ² 31	.0066		10	.0985			.7150		119	3.356	1.269
-30	1		+20	0.1033	1		0.739	0.28	120	3.451	1.304
1	0.0070	-	21	.1084			.765		121	3.548	3 1.341
29	.0075	, [.1136			.791	9 .29		3.647	1.379
27	.0084		23	.1191	- 1		.819	1 .31	123	3.749	
26	,000	. -		.1248		7 74	.847	I .32	0 124	3.853	1
-25	0.000			0.1308	.	9 75	0.876	0 0.33		3.960	
24	.010	, ,		.1370		-	.905			4.06	
23	.010	١ .		.143.	-	4 77	.936	2 -35	4 127	4.180	
22	.011	'		.150	2 .05		.967				1 ///
21	.012			.157	3 .05		1.000	1		1	1
-20	0.012	7 0.00	+30	0.164			1.033				
19	.013			.172			1.067				
18	.014	3 .00	32	.180		8 82					· ^
17	.015	1 .00		.187						1	à {
16	.016	.00	34	.195	1			-			1
-15	0.016			0.203							
14	.017	00.	7 36	.211						1	1 /
13				.220	1 .						-
12	1	L	^	.229							1
11	.021		_ ~ ~ .								~
10 0.0223 0.008 40 0.2477 0.094 90 I.4234 0.538 I40 5.889 2.226											7

TABLE 104.

WEIGHT IN CRAMS OF ONE CUBIC CENTIMETER OF AIR.

Humidity and pressure terms combined: $\frac{\delta}{\delta_0} = \frac{h}{29.921} = \frac{B - 0.378e}{29.921}$.

B = Barometric pressure in inches; e = Vapor pressure in inches.

h.	h 29.921	Log h/29.921.	h.	<u>h</u> 29.291	Log h/29.921	h.	<u>h</u> 29.921	Log h/29.92I
Inch's. 10.0 10.1 10.2 10.3 10.4	0.3342 .3376 .3409 .3442 .3476	9.52402 .52835 .53262 .53686 .54106	Inches. 15.0 15.1 15.2 15.3 15.4	0.5013 .5047 .5080 .5113 .5147	- 10 9.70012 .70300 .70587 .70871 .71154	20.0 20.1 20.2 20.3 20.4	0.6684 .6718 .6751 .6784 .6818	9.82505 .82722 .82938 .83152 .83365
10.5 10.6 10.7 10.8 10.9	0.3509 •3543 •3576 •3609 •3643	9.54521 ·54933 ·55341 ·55745 ·56145	15.5 15.6 15.7 15.8 15.9	0.5180 ·5214 ·5247 ·5281 ·5314	9.71435 .71715 .71992 .72268 .72542	20.5 20.6 20.7 20.8 20.9	0.6851 .6885 .6918 .6952 .6985	9.83578 .83789 .83999 .84209
11.0	0.3676	9.56542	16.0	0.5347	9.72814	21.0	0.7018	9.84624
11.1	.3710	.56935	16.1	.5381	.73085	21.1	.7052	.84831
11.2	.3743	.57324	16.2	.5414	.73354	21.2	.7085	.85036
11.3	.3777	.57710	16.3	.5448	.73621	21.3	.7119	.85240
11.4	.3810	.58093	16.4	.5481	.73887	21.4	.7152	.85444
11.5	0.3843	9.58472	16.5	0.5515	9.74151	21.5	0.7186	9.85646
11.6	•3877	.58848	16.6	.5548	•74413	21.6	.7219	.85848
11.7	•3910	.59221	16.7	.5581	•74674	21.7	.7252	.86048
11.8	•3944	.59591	16.8	.5615	•74933	21.8	.7286	.86248
11.9	•3977	.59957	16.9	.5648	•75191	21.9	.7319	.86447
12.0	0.4011	9.60321	17.0	0.5682	9.75447	22.0	0.7353	9.86645
12.1	.4044	.60681	17.1	•5715	.75702	22.1	.7386	.86842
12.2	.4077	.61038	17.2	•5748	.75955	22.2	.7420	.87038
12.3	.4111	.61393	17.3	•5782	.76207	22.3	.7453	.87233
12.4	.4144	.61745	17.4	•5815	.76457	22.4	.7486	.87427
12.5	0.4178	9.62093	17.5	0.5849	9.76706	22.5	0.7520	9.87621
12.6	.4211	.62439	17.6	.5882	.76954	22.6	•7553	.87813
12.7	.4244	.62782	17.7	.5916	.77200	22.7	•7587	.88005
12.8	.4278	.63123	17.8	.5949	.77444	22.8	•7620	.88196
12.9	.4311	.63461	17.9	.5982	.77687	22.9	•7653	.88386
13.0	0.4345	9.63797	18.0	0.6016	9.77930	23.0	0.7687	9.88575
13.1	.4378	.64130	18.1	.6049	.78170	23.1	.7720	.88764
13.2	.4412	.64460	18.2	.6083	.78410	23.2	.7754	.88951
13.3	.4445	.64788	18.3	.6116	.78648	23.3	.7787	.89138
13.4	.4478	.65113	18.4	.6149	.78884	23.4	.7821	.89324
13.5	0.4512	9.65436	18.5	0.6183	9.79120	23.5	0.7854	9.89509
13.6	·4545	.65756	18.6	.6216	•79354	23.6	.7887	.89693
13.7	·4579	.66074	18.7	.6250	•79587	23.7	.7921	.89877
13.8	·4612	.66390	18.8	.6283	•79818	23.8	.7954	.90060
13.9	·4646	.66704	18.9	.6317	•80049	23.9	.7988	.90242
14.0	0.4679	9.67015	19.0	0.6350	9.80278	24.0	0.8021	9.90424
14.1	.4712	.67324	19.1	.6383	.80506	24.1	.8054	.90604
14.2	.4746	.67631	19.2	.6417	.80733	24.2	.8088	.90784
14.3	.4779	.67936	19.3	.6450	.80958	24.3	.8121	.90963
14.4	.4813	.68239	19.4	.6484	.81183	24.4	.8155	.91141
14.5	0.4846	9.68539	19.5	0.6517	9.81406	24.5	0.\$188	9.91319
14.6	.4879	.68837	19.6	.6551	.81628	24.6	.\$222	.91496
14.7	.4913	.69134	19.7	.6584	.81849	24.7	.\$255	.91672
14.8	.4946	.69429	19.8	.6617	.82069	24.8	.\$289	.91848
14.9	.4980	.69721	19.9	.6651	.82288	24.9	.8322	.92022

WEIGHT IN CRAMS OF ONE CUBIC CENTIMETER OF AIR.

Humidity and pressure terms combined: $\frac{\delta}{\delta_o} = \frac{h}{29.921} = \frac{B - 0.378 e}{29.921}$.

B = Barometric pressure in inches; e = Vapor pressure in inches.

h.	h 29.92I	Log -h_29.92I	h.	h 29.921	Log h 29.921	h.	h 29.921	Log h 29.921
Inches.		- 10	Inches.		– IO	Inches.		– 10
25.00 25.05	0.8355 .8372	9.92196	27.25 27.30	0.9107	9.95939	29.50 29.55	0.9859 .9876	9.99385 .99458
25.10	.8389	.92370	27.35	.9124	.96098	29.60	.9893	.99532
25.15 25.20	.8405 .8422	.92456	27.40	.9157	.96177 .96256	29.65 29.70	.9909 .9926	.99605 .99678
	10422	.92342	27.43	• 7 - 7 4	.90200		199-0	. 99070
25.25 25.30	0.8439 .8456	9.92628	27.50 27.55	0.9191 .920S	9.96336	29.75 29.80	0.9943 .9960	9.99751 .99824
25.35	.8472	.92800	27.60	.9224	.96493	29.85	.9976	.99897
25.40 25.45	.8489 .8506	.92886 .92971	27.65	.9241 .9258	.96572 .96650	29.90	.9993 1.0010	.99970 0.00042
		1929/1		.9230				
25.50 25.55	0.8522 .8539	9.93056	27.75 27.80	0.927.1	9.96728 .96807	30.00	1.0026 1.0043	.00115
25.60	.8556	.93226	27.85	.9308	.96885	30.10	1.0060	.00259
25.65	.8573	.93311	27.90	.9325	.96963	30.15	1.0076	.00331
25.70	.8589	.93396	27.95	.9341	.97040	30.20	1.0093	.00403
25.75	0.8606	9.93480	28.00	0.9358	9.97118	30.25	1.0110	0.00475
25.80 25.85	.8623 .8639	.93564	28.05 28.10	·9375 ·9391	.97195 .97 2 73	30.30	I.0I27 I.0I43	.00547
25.90	.8656	.93732	28.15	.9408	.97350	30.40	1.0160	.00690
25.95	.8673	.93816	28.20	•9425	.97427	30.45	1.0177	.00761
26.00	0.8690	9.93900	28.25	0.9441	9.97504	30.50	1.0193	0.00832
26.05 26.10	.8706 .8723	.93983 .94066	28.30 28.35	.9458 ·9475	.97581	30.55	1.0210 1.0227	.00903
26.15	.8740	.94149	28.40	.9492	-97734	30,65	1.0244	.01045
26.20	.8756	.94233	28.45	.9508	.97810	30.70	1.0260	.01116
26.25	0.8773	9.94315	28.50	0.9525	9.97887	30.75	1.0277	0.01187
26.30 26.35	.8790 .8806	.94398	28.55 28.60	.9542 .9558	.97963	30.80	1.0294	.01257
26.40	.8823	.94563	28.65	.9575	.98115	30.90	1.0327	.01398
26.45	.88.40	.94645	28.70	.9592	.98191	30.95	1.0344	.014 6 8
26.50	0.8857	9.94727	28.75	0.9609	9.98266	31.00	1.0361	0.01539
26.55 26.60	.8873 .8890	.94809	28.80 28.85	.9625 .9642	.98342	31.05	1.0377 1.0394	.01608
26.65	.8907	.94972	28.90	.9659	.98492	31.15	1.0411	.01748
26.70	.8924	.95054	28.95	.9675	.98567	31.20	1.0427	.01818
26.75	0.8940	9.95135	29.00	0.9692	9.98642	31.25	1.0444	0.01887
26.80 26.85	.8957 .8974	.95216	29.05 29.10	.9709	.98717	31.30	1.0461	.01957
26.90	.8990	.95378	29.15	.9742	.98866	31.40	1.0494	.02095
26.95	9007	.95458	29.20	•9759	.98941	31.45	1.0511	.02164
27.00	0.9024	9.95539	29.25	0.9776	9.99015	31.50	1.0528	0.02233
27.05	.9040	.95619	29.30	.9792	.99089	31.55	1.0544	.02302
27.15	.9074	.95779	29.40	.9826	.99237	31.65	1.0578	.02439
27.20	.9091	.95859	29.45	.9843	.99311	31.70	1.0594	.02508

WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Temperature term: $\delta_{t, 760} = \frac{0.0012930}{1 + 0.003670 t}$. Centigrade temperature.

I cubic centimeter of dry air at the temperature of o°C. and pressure 760 mm., under the standard value of gravity, weighs 0.0012930 gram.

	t.	δ_t , 760	Log δ _{t, 760}	t.	$\delta_{t, 760}$	Log δ _{t, 760}	l t.	$\delta_{t, 760}$	Log δ _t , 760
	·.	-1, 700			1, 700		l		-18 -1, 700
	C.	0.00	-10	C	0.00	10	C.	0.00	-10
-	.34°	14774	7.16950	-4.5°	13147	7.11883	+18°.0	12129	7.08383
-	33	14712	.16768	-4.0	13123	.11804	18.5	12108	.08309
	-32	14651	.16587	-3.5	13098	.11720	19.0	12087	.08232
-	-31	14590	.16407	—3.0	13074	.11642	19.5	12066	.08156
	20	0.00	(-2.5	0.00		20.0	0.00	- 0000-
	-30	14529	7.16224	-2.0	13050	7.11562		12046	7.08085
	-29 -28	14470	.16047	-1.5	13026	.11481	20.5 21.0	12025	.08009
B 1		14410	.15691	-1.0	12978	.11321	21.5	11984	.07937
	-27 -26	14352 14294	.15515	-0.5	12970	.11321	22.0	11964	.07788
	-20	0.00	.13313	0.5	0.00			0.00	.07700
_	25	14236	7.15339	0.0	12930	7.11160	22.5	11944	7.07716
	-24	14179	.15166	+0.5	12906	.11079	23.0	11924	.07642
	-23	14122	.14990	1.0	12883	.11002	23.5	11903	.07566
	-22	14065	.14714	1.5	12859	.10921	24.0	11883	.07493
-	-21	14010	.14645	2.0	12836	.10844	24.5	11863	.07419
		0.00			0.00		05.0	0.00	
	-20.0	13955	7.14472	2.5	12812	7.10762	25.0	11843	7.07346
	-19.5	13927	.14386	3.0	12789	.10684	25.5	11823	.07273
	-19.0	13899	.14298	3.5	12766	.10607	26.0	11804	.07204
	-18.5	13872	.14215	4.0	12743	.10527	26.5	11784	.07131
-	-18.0	13844	.14126	4.5	0.00	.10450	27.0	0.00	.07056
	17.5	0.00	7.14044	5.0	12698	7.10372	27.5		7.06986
8	17.0	13790	.13956	5.5	12675	.10294	28.0	11745	.06912
	-16.5	13763	.13871	6.0	12651	.10294	28.5	11706	.06841
	-16.0	13737	.13790	6.5	12629	.10138	29.0	11686	.06767
	-15.5	13710	.13705	7.0	12606	.10058	29.5	11667	.06697
	- 0-0	0.00	-0, 0		0.00			0.00	,
-	15.0	13684	7.13621	7.5	12584	7.09982	30.0	11648	7.06625
	14.5	13657	.13536	8.0	12561	.09902	30.5	11628	.06550
	-14.0	13630	.13450	8.5	12539	.09828	31.0	11609	.06479
-	13.5	13604	.13368	9.0	12517	.09750	31.5	11590	.06408
	-13.0	13578	.13285	9.5	12494	.09670	32.0	11571	.06337
	12.5	0.00	7 12207	10.0	0.00	7.00504	32.5	0.00	7.06266
	-12.0	13552	7.13201	10.0	12472 12450	7.09594	33.0	11552	7.06266
	-12.0	13526 13500	.13117	11.0	12450	.09517	33.5	11514	.06123
	-11.0	13474	.12950	11.5	12406	.09363	34.0	11496	.06055
	-10.5	13448	.12866	12.0	12384	.09386	34.5	11477	.05984
		0.00			0.00			0.00	07-7
-	10.0	13423	7.12785	12.5	12363	7.09214	35.0	11458	7.05911
-	9.5	13397	.12701	13.0	12341	.09135	35.5	11440	.05843
-		13372	.12620	13.5	12320	.09061	36.0	11421	.05772
	- 8.5	13346	.12535	14.0	12298	.08983	36.5	11403	.05702
-	- 8.0	13321	.12454	14.5	12277	.08910	37.0	11384	.05629
_	- 7.5	0.00	7 1 2 2 7 2	15.0	0.00	7.08831	37.5	0.00	7.05562
		13296	7.12372	15.5	12255	.08757	38.0	11347	.05488
	- 6.5	132/1	.12292	16.0	12234	.08683	38.5	11347	.05419
	- 6.0	13221	.12126	16.5	12192	.08608	39.0	11311	.05352
l –		13196	.12044	17.0	12171	.08533	39.5	11293	.05282
	0.0	0.00	12-14		0.00	000		0.00	
-	- 5.0	13172	7.11966	17.5	12150	7.08458	40.0	11275	7.05213
				<u> </u>					

WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Temperature term. (Continued)

t. C. +40° 41	$\begin{array}{ c c c c }\hline \delta_{t, 760} \\ \hline 0.00 \\ \hline 11275 \\ 11239 \\ \hline \end{array}$	$ \begin{array}{c c} \text{Log } \delta_{t, 760} \\ \hline -10 \\ 7.05213 \\ .05074 \end{array} $	t. C. +50° 51	δ _t , 760 0.00 10925 10891	$ \begin{array}{c c} & \text{Log } \delta_{t, 760} \\ \hline & -10 \\ & 7.03842 \\ & .03707 \end{array} $	t. C. +60° 61	δ _t , 760 0.00 10597 10565	$ \begin{array}{c c} \text{Log } \delta_{t, 760} \\ \hline -10 \\ 7.02518 \\ .02388 \end{array} $
42 43 44 45 46	11203 11168 11132 0.00 11097 11063	.04933 .04798 .04657 7.04521 .04387	52 53 54 55 56	10858 10825 10792 0.00 10758 10726	.03576 .03443 .03309 7.03173 .03044	62 63 64 65 66	10534 10502 10471 0.00 10440 10409	.02258 .02128 .01999 7.01870 .01742
47 48 49	11028 10993 10959	.04251 .04112 .03977	57 58 59	10693 10661 10629	.02910 .02780 .02649	67 68 69	10378 10348 10317	.01611

TABLE 106.

Humidity term: Values of 0.378 e. Auxiliary to Table 107. e = Vapor pressure in mm. (See Tables 76 and 77).

		- vapor				ies /o and	117	
Dew- point	e Vapor Pressure (Ice)	0.378 <i>e</i>	Dew- point	e Vapor Pressure (Water)	0.378 <i>e</i>	Dew- point	e Vapor Pressure (Water)	0.378 <i>e</i>
C. -50° -45 -40 -35 -30	mm, 0.029 0.054 0.096 0.169 0.288	mm. 0.01 0.02 0.04 0.06 0.11	C. 0° 1 2 3	mm. 4.580 4.924 5.291 5.682 6.098	mm. 1.73 1.86 2.00 2.15 2.31	C. 30° 31 32 33 34	mm, 31.860 33.735 35.705 37.775 39.947	mm, 12.04 12.75 13.50 14.28 15.10
-25 24 23 22 21	0.480	0.18	5	6.541	2.47	35	42.227	15.96
	0.530	0.20	6	7.012	2.66	36	44.619	16.87
	0.585	0.22	7	7.513	2.84	37	47.127	17.81
	0.646	0.24	8	8.045	3.04	38	49.756	18.81
	0.712	0.27	9	8.610	3.25	39	52.510	19.85
-20	0.783	0.30	10	9.210	3.48	40	55.396	20.94
19	0.862	0.33	11	9.846	3.72	41	58.417	22.08
18	0.947	0.36	12	10.521	3.98	42	61.580	23.28
17	1.041	0.39	13	11.235	4.25	43	64.889	24.53
16	1.142	0.43	14	11.992	4.53	44	68.350	25.84
-15 14 13 12 11	1.252	0.47	15	12.794	4.84	45	71.968	27.20
	1.373	0.52	16	13.642	5.16	46	75.751	28.63
	1.503	0.57	17	14.539	5.50	47	79.703	30.13
	1.644	0.62	18	15.487	5.85	48	83.830	31.69
	1.798	0.68	19	16.489	6.23	49	88.140	33.32
-10	1.964	0.74	20	17.548	6.63	50	92.64	35.02
9	2.144	0.81	21	18.665	7.06	51	97.33	36.79
8	2.340	0.88	22	19.844	7.50	52	102.23	38.64
7	2.550	0.96	23	21.087	7.97	53	107.33	40.57
6	2.778	1.05	24	22.398	8.47	54	112.66	42.59
- 5	3.025	1.14	25	23.780	8.99	55	118.20	44.68
4	3.291	1.24	26	25.235	9.54	56	123.98	46.86
3	3.578	1.35	27	26.767	10.12	57	130.00	49.14
2	3.887	1.47	28	28.380	10.73	58	136.26	51.51
1	4.220	1.60	29	30.076	11.37	59	142.78	53.97
0	4.580	1.73	30	31.860	12.04	60	149.57	56.54

WEIGHT IN CRAMS OF ONE CUBIC CENTIMETER OF AIR.

Humidity and pressure terms combined : $\frac{\delta}{\delta_{\circ}} = \frac{\hbar}{760} = \frac{B - 0.378e}{760}$.

B = Barometric pressure in mm.; e = Vapor pressure in mm.

h.	<u>h</u> 760	Log h 760.	h.	<u>h</u> 760 ·	Log <u>h</u> 760	h.	h 760 °	Log h/760
mm.		- IO	mm.	(-	- 10	mm.		- 10
300	0.3947 ·3974	9.59631	400 401	0.5263	9.72125	450 451	0.5921 •5934	9.77240 .77336
304 306	.4000	.60206	402 403	.5289	.72341 .72449	452 453	.5947 .5961	·77432 ·77528
308	0.4079	9.61055	404 405	.5316 0.5329	.72557 9.72664	454 455	•5974 0.5987	.77624 9.77720
312 314	.4105	.61334 .61612	406 407	.5342 .5355	.72771	456 457	.6000 .6013	.77815
316 318	.4158 .4184	.61887 .62161	408 409	.5369 .5382	.72985 .73091	458 459	.6026 .6040	.78005 .78100
320 322	0.4211	9.62434 .62704	410 411	0.5395	9.73197	460 461	0.6053 .6066	9.78194 .78289
324 326	.4263	.62973	412	.5408	.73303 .73408	462 463	.6079	.78383
328	.4316	.63506	413	·5434 ·5447	.73514 .73619	464	.6105	.78570
330 332	0.434 2 .4368	9.63770 .64032	415 416	0.5461 •5474	9.73723 .73828	465 466	0.6118 .6132	9.78664 .78757
334 336	·4395 ·4421	.64293 .64552	417 418	.5487 .5500	.73932 .74036	467 468	.6145 .6158	.78850 .78943
338 340	·4447 0·4474	.64810 9.65066	419 420	·5513 0.5526	.74140	469 470	.6171 0.6184	.79036
342	.4500	.65321	421	.5540	9.74244 •74347	471	.6197	.79221
344 346 348	.4526 .4553 .4579	.65826	422 423 424	·5553 ·5566	.74450 .74553	472 473	.6224	.79313 .79405 .79496
350	0.4605	9.66325	425	·5579 0.5592	.74655 9.74758	474 475	0.6250	9.79588
352 354	.4632 .4658	.66573	426 427	.5605 .5618	.74860 .74961	476 477	.6263 .6276	.79679 .79770
356 358	.4684 .4711	.67064 .67307	428 429	.5632 .5645	.75063 .75164	478 479	.6289 .6303	.79861 .79952
360 362	0.4737 .4763	9.67549 .67790	430 431	0.5658 .5671	9.75265 .75366	480 481	0.6316	9.80043 .80133
364 366	.4789	.68029 .68267	432	.5684	.75467 .75567	482 483	.6342	.80223 .80313
368	.4842	.68503	434	.5711	.75668	484	.6368	.80403
370 372	0.4868 .4895	9.68739 .68973	435 436	0.5724 ·5737	9.75768 .75867	485 486	0.6382 .6395	9.80493 .80582
374 376	.4921 .4947	.69206 .69437	437 438	.575° .5763	.75967 .76066	487 488	.6408 .6421	.80672 .80761
378 380	·4974 o.5000	.69668 9.69897	439 440	.5776 0.5790	.76165 9.76264	489 490	.6434 o.6447	.80850 9.80938
382 384	.5026	.70125	44I 442	.5803	.76362 .76461	491 492	.6461 .6474	.81027
386 388	.5079	.70577 .70802	443 444	.5829	.76559 .76657	493 494	.6487	.81203 .81291
390	0.5132	9.71025	445	0.5855	9.76755	495	0.6513	9.81379
392 394	.5158 .5184	.71247 .71468	446	.5868 .5882	.76852 .76949	496 497	.6526	.81467
396 398	.5211 ·5237	.71688 .71907	448 449	.5895 .5908	.77046	498 499	.6553 .6566	.81642 .81729

SMITHSONIAN TABLES.

WEIGHT IN CRAMS OF ONE CUBIC CENTIMETER OF AIR.

Humidity and pressure terms combined : $\frac{\delta}{\delta_{\circ}} = \frac{h}{760} = \frac{B - 0.378e}{760}$.

B = Barometric pressure in mm.; e = Vapor pressure in mm.

h.	<u>ħ</u> .	Log h/760	h.	<u>h</u> 760·	Log h 760	h.	<u>h</u> 760 ·	Log h/760 ·
mm.		- Io	mm.		- 10	mm.		- 10
500	0.6579	9.81816	550	0.7237	9.85955	600	0.7895	9.89734
501	.6592	.81902	551	.7250	.86034 .86112	601 602	.7908	.89806
502 503	.6605 .6618	.81989	552 553	.7263 .7276	.86191	603	.7921 •7934	.89950
504	.6632	.82162	554	.7290	.86270	604	•7947	.90022
505	0.6645	9.82248	555	0.7303	9.86348	605	0.7961	9.90094
506	.6658	.82334	556	.7316	.86426	606	•7974	.90166
507 508	.6671 .6684	.82419 .82505	557 558	.7329 .7342	.86504 .86582	607 608	.7987 .8000	.90238
509	.6697	.82590	559	•7355	.86660	609	.8013	.90380
510	0.6711	9.82676	560	0.7368	9.86737	610	0.8026	9.90452
511	.6724	.82761 .82846	561 562	.7382	.86815 .86892	611	.8040 .8053	.90523
512 513	.6737 .6750	.82930	563	•7395 •7408	.86969	613	.8066	.90594
514	.6763	.83015	564	.7421	.87046	614	.8079	.90735
515	0.6776	9.83099	565	0.7434	9.87123	615	0.8092	9.90806
516	.6789 .6803	.83184	566 567	•7447	.87200	616	.8105	.90877
517 518	.6816	.83268 .83352	568	.7461	.87277 .87353	618	.8132	.90947
519	.6829	.83435	569	.7487	.87430	619	.8145	.91088
520	0.6842	9.83519	570	0.7500	9.87506	620	0.8158	9.91158
521	.6855 .6869	.83602 .83686	571	.7513 .7526	.87582 .87658	621	.8171 .8184	.91228
522 523	.6882	.83769	572 573	.7540	.87734	623	.8197	.91298
524	.6895	.83852	574	•7553	.87810	624	.8211	.91437
525	0.6908	9.83934	575	0.7566	9.87885	625	0.8224	9.91507
526 527	.6921 .6934	.84017	576 577	·7579 ·7592	.87961 .88036	626	.8237 .8250	.91576 .91645
528	.6947	.84182	578	.7605	.88111	628	.8263	.91715
529	.6961	.84264	579	.7618	.88186	629	.8276	.91784
530	0.6974	9.84346	580	0.7632	9.88261	630	0.8289	9.91853
531 532	.6987	.84428 .84510	581 582	.7645 .7658	.88336 .88411	631	.8303 .8316	.91922
533	.7013	.84591	583	.7671	.88486	633	.8329	.92059
534	.7026	.84673	584	.7684	.88560	634	.8342	.92128
535	0.7040	9.84754	585	0.7697	9.88634	635	0.8355	9.92196
536 537	.7053 .7066	.84835 .84916	586 587	.7711 .7724	.88708 .88782	636 637	.8368 .8382	.92264
538	.7079	.84997	588	.7737	.88856	638	.8395	.92401
539	.7092	.85078	589	.7750	.88930	639	.8408	.92469
540	0.7105	9.85158	590	0.7763	9.89004	640 641	0.8421	9.92537
541 542	.7118	.85238 .85318	591 592	.7776 .7789	.89077	642	.8434 .8447	.92672
543	.7145	.85399	593	.7803	.89224	643	.8461	.92740
544	.7158	.85478	594	.7816	.89297	644	.8474	.92807
545 546	0.7171	9.85558 .85638	595 596	0.78 2 9 . 7 842	9.89370 .89443	645 646	0.8487 .8500	9.92875
546 547	.7197	.85717	597	.7855	.89516	647	.8513	.92942
548	.7211	.85797	598	.7868	.89589	648	.8526	.93076
549	.7224	.85876	599	.7882	.89662	649	.8539	.93143

WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Humidity and pressure terms combined : $\frac{\delta}{\delta_0} = \frac{h}{760} = \frac{B - 0.378c}{760}$.

B = Barometric pressure in mm.; e = Vapor pressure in mm.

			1					
h.	<u>h</u> 760	Log h_ 760	h.	<u>h</u> 760	Log h/760	h.	760°	Log h/760
mm.		– 10	mm.		— 10	mm.		— IO
650	0.8553	9.93210	700	0.9211	9.96428	750	0.9868	9.99425
651 652	.8566 .8579	.93277	701 702	.9224 .9237	.96490 .96552	751 752	.9882 .9895	.99483
653	.8592	.93341	703	.9250	.96614	753	.9093	.99598
654	.8605	.93476	704	.9263	.96676	754	.9921	.99656
655	0.8618	9-93543	705	0.9276	9.96738	755	0.9934	9.99713
656	.S632	.93609	706	.9289	.96799	756	•9947	.99771
657 658	.8645 .8658	.93675 .93741	707 708	.9303 .9316	.96860 .96922	757 758	.9961 •9974	.99828 .99886
659	.8671	.93807	709	.9329	.96983	759	.9987	.99943
660	0.8684	9.93873	710	0.9342	9.97044	760	1.0000	0.00000
661	.8697	•93939	711	•9355	.97106	761	.0013	.00057
663	.8711 .8724	.94004	712 713	.9368 .9382	.97167	762 763	.0020	.00114
664	.8737	.94135	714	•9395	.97288	764	.0053	.00228
665	0.8750	9.94201	715	0.9408	9.97349	765	1.0066	0.00285
666	.8763	.94266	716	.9421	.97410	766	.0079	.00342
667 668	.8776 .8790	.94331	717 718	·9434 ·9447	.97470 .97531	767 768	.0092	.00398
669	.8803	.94461	719	.9461	•97592	769	.0118	.00511
670	0.8816	9.94526	720	0.9474	9.97652	770	1.0132	0.00568
671 672	.8829 .8842	.94591	72I 722	.9487	.97712	771	.0145 .0158	.00624
673	.8855	.94656 .94720	723	.9500 .9513	.97772 .97832	772 773	.0150	.00736
674	.8869	.94785	724	.9526	.97892	774	.0184	.00793
675 676	0.8882 .8895	9.94849	725	0.9539	9.97952 .98012	775 776	1.0197	0.00849
677	.8908	.94913	727	•9553 •9566	.98072	777	.0211	.00961
678	.8921	.95042	728	.9579	.98132	778	.0237	.01017
679	.8934	.95106	729	.9592	.98191	779	.0250	.01072
680 681	0.8947 .8960	9.95170	730 731	0.9605 .9618	9.98250	780 781	1.0263 .0276	0.01128
682	.8974	.95297	732	.9632	.98370	782	.0289	.01239
683 684	.8987	.95361	733	.9645	.98429	783	.0303	.01295
685	,9000	9.95488	734 735	.9658 0.9671	.98488	784 785	.0316	0.01350
686	0.9013 .9026	.9555I	736	.9684	9.98547 .98606	786	1.0329 .0342	.01461
687	.9039	.95614	737	.9697	.98665	787	.0355	.01516
688	.9053	.95677	738	.9711	.98724 .98783	788 789	.0368 .0382	.01571
690	0.9079	9.95804	739 740	0.9737	9.98842	790	1.0395	0.01681
691	.9092	.95866	741	.9750	.98900	791	.0408	.01736
692	.9105	.95929	742	.9763	.98959	792	.0421	.01791
693	.9118	.95992	743	.9776	.99018	793 794	.0434	.01846
695	0.9145	9.96117	745	0.9803	9.99134	795	1.0461	0.01955
696	.9158	.96180	746	.9816	.99192	796	.0474	.02010
697	.9171	.96242	747 748	.9829 .9842	.99251	797 798	.0487	.02064
699	.9197	.96366	749	.9855	.99367	799	.0513	.02173
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ATMOSPHERIC WATER-VAPOR LINES IN THE VISIBLE SPECTRUM.

	27				
Wave lengths	Num-	Inten-	Wave lengths	Num-	Inten-
	ber of	sity	in Ångströms	ber of	sity
in Ångströms	lines	Oit y	III Angstroms	lines	
5292.2	15	-2	5915.628		I
5861.6 -5869.8	7	2	5915.8 -5918.0	6	I
5870.653		I	5918.423		4
5871.2 -5875.6	8	—I	5919.0		-2
5876.126		1	5919.059		5
5877.3 -5879.2	4	—I	5919.647		7
5879.608		I	5920.2		i
5879.733		I	5920.564		Î
5880.5 -5880.7	2	0	5921.2 -5922.4		I
		I	5922.522		2
5880.935		0	5922.7 -5923.2		I
5881.1		1 - 1			
5881.872		I	5923.652		1
5882.0 -5883.0		0	5923.827		2
5883.908		5	5924.276		4
5884.2 -5885.6		1	5924.8	1	-2
5885.981		5	5925.007		2
5886.348		I	5926.6		2
5886.4 -5886.7	2	0	5928.296		2
5887.226		5	5928.8 -5931.0		2
5887.664		3	5932.097		5
5887.8	I	1	5932.788		2
5888.708		2	5933.0 -5940.0	14	2
5889.1	1	I	5940.427		I
5889.643		3	5940.9	I	-1
5889.888		2	5941.080		5
5890.2 -5890.7		0	5941.3		2
5891.186		I	5941.632		2
5891.5	1	0	5942.3		2
5891.665		4	5942.422		I
5892.401		3	5942.576		3
5893.1		0	5944-317		I
5893.513		I	5944-732		1
5894.4 -5896.4		-1	5945.2 -5945.3		
5896.498	3	Î	5945.652		1
5896.835		2	5946.010		3
5897.1 -5897.9		_ī	5946.7		-2
5898.173	4	4	5946.849	1	I
5898.4 -5898.8		-2	5947.070		2
5899.003		2	5947.4 -5949.0		-2
5899.923		2	5949.176	4	2
7099.923			5949.6 -5954.4		-1
5900.048		4 I	5954.956		I
5900.4 -5901.3		1 .	5955.8 -5956.3	4	2
5901.472	· · · · · ·	2	5957.884	4	I
5902.0		I	5958.246		1
5902.151			5961.4 -5966.3		1
5902.8		-2			I
5903.536			5966.670		1-1
5903.7 -5907.5		— I	5967.3	1	2
5907.858			5967.843	· · · · · ·	-2
5908.213			5968.1	I	2
5909.001		3	5968.280		— <u>I</u>
5909.5	I	I	5969.0 -5970.7		
5910.186			5971.341		I
5910.3 -5910.6	3	1-1	5975.114		I
5910.775			5976.5	I	1
5910.9 -5912.7		-2	5977.036		I
5913.000			5977.4 -6029.9		I
5914.218		6	6267.7 -6350.7		-2
5914.934			6463.5 -6479.5		-2
5915.438			6460.070		I
0, 0,40	1	1	(II) ' '		
					_

ATMOSPHERIC WATER-VAPOR LINES IN THE VISIBLE SPECTRUM.

Wave lengths in Ångströms	Num- ber of lines	Inten- sity	Wave lengths in Ångströms	Num- ber of lines	Inten- sity
in Ångströms 6480.3 -6483.1 6483.252 6483.5 -6490.7 6490.798 6492.9 -6493.3 6494.510 6495.864 6497.6 -6514.3 6514.737 6515.9 6516.527 6516.632 6517.1 -6519.2 6519.5 6521.9 -6523.7 6523.855 6523.855 6525.8 -6530.6 6532.369 6533.949 6534.6 -6542.3 6543.912 6545.8 -6547.7 6548.627 6552.636 653.8 -6558.2 6560.570 65671.0 6572.099 6573.5 6574.854	3 11 2 7 3 4 2 3 3 8 8 1 I	sity -3 I -3 I -1 I 2 -1 I 2 -2 I 3 I -3 I -2 I I -3 I -1 I -3 I -1 I -1 I -1 I -1 I	in Ångströms 6941.0. 6941.234 6942.163. 6942.387 6943.815. 6947.552 6947.6. 6948.997 6949.067 6950.77‡ 6953.586 6953.8 -6955.7 6956.416 6956.502 6059.467 6961.275 6964.564 6970.9 6977.487 6981.474 6984.9 6984.9 6986.592 6987.9 6989.001 6990.391 6990.391 6990.391 6993.535 6994.124 6998.7	lines I I I I I I I I I	sity -2 I 3 5 -I I I 1 -2 4 I 3 4 I 0 3 I 0 3 I 0 2 1 0 2 0 2
6929.3 6933.832. 6937.716. 6938.271. 6939.630. 6940.198.	I	-I 2 2 I 2 2 2	7005.1 -7009.9 7011.342 7016.452 7023.517 7027.0 7027.491	2 I	0 2 3 2 0 2

TABLE 109.

ATMOSPHERIC WATER-VAPOR BANDS IN THE INFRA-RED SPECTRUM.

Name of band	Wave- lengths	Transmission coefficient α	of numerous fir apparatus does i Wide bands o	f very great atm on are found in	he bolographic stinguish. ospheric water-
a		0.91 0.92	Name	Wave lengths	Absorption at Washington
ρ. σ. τ. Φ ₁ Φ ₂ Ιη Ψ.	0.933 0.945 0.974 1.119 1.134 1.172 1.331	0.90 0.63 0.69 0.91 0.54 0.60 0.92 0.74	ρστ Φ Ψ Ω Χ	μ μ 0.926-0.978 1.095-1.165 1.319-1.498 1.762-1.977 2.520-2.845	$\begin{array}{c} \text{0.3 to 0.5} \\ \text{0.5 to 0.8} \\ \text{0.7 to 1.0} \\ \text{0.9 to 1.0} \\ \text{1.0} \left\{ \begin{array}{c} \text{Partly} \\ \text{CO}_2 \end{array} \right\} \end{array}$
In Ψ Ψ ₁		0.36	See Vol. I, A Smithsonian Ins	nnuls Astrophysi	cal Observatory,

Rang Wave-le			PRECIPITABLE WATER IN CENTIMETERS.											
μ	μ	.001	.003	.006	.01	.03	.06	.10	.25	.50	1.0	2.0	6.0	10.0
0.75 t	0.1.0				100	99	99	98	97	95	93	90	83	78
1.0	1.25				99	99	98	97	95	92	89	85	74	69
1.25	1.5				96	92	84	80	66	57	51	44	31	28
1.5	2.0	,			98	97	94	88	79	73	70	66	60	57 :
2.	3.	96	92	87	84	77	70	64						
* 3.	4.	95	88	84	78	72	66	63						
4.	5· 6.	92	83 82	76	7 <i>I</i> 68	65 56	60	53	0.5					
5. 6.		95 85	54	75 50	31	24	51 8	47	35	2	0	0	0	
7.	7· 8.	94	84	76	68	57	46	4 35	3 16	10	2	0	0	0
8.	9.	100	100	100	99	98	96	94	6.5	10	-			
† 9.	10.	100	100	100	100	100	100	100	100	100	100	100		
10.	II.	100	100	100	100	100	100	100	100	100	100	100		
II.	12.	100	100	100	100	100	99	98	96	95	93	-		
I 2.	13.	100	100	100	100	99	99	97	86	82				
*13.	14.	100	100	100	99	97	94	90	80	60				
*14.	15.			96	93	80	75	50	15	0	0	0	0	0
*15.	16.					70	55	40	0	0	0	0	0	0
16.	17.						50	20	0	0	0	0	0	0
17.	18.						25	10	0	0	0	0	0	0
18.		0	0	0	0	0	0	0	0	0	0	0	0	0

^{*} These places require multiplication by the following factors to allow for losses in CO_2 gas. Under average sea-level outdoor conditions the CO_2 (partial pressure = 0.0003 atmos.) amounts to about 0.6 grams per cu.m. Paschen gives 3 times as much for indoor conditions.

 2μ to 3μ , for 2 grams in m^2 path (95); for 140 grams in m^2 path (93); 4 " 5, " " " (93); " (93); " (70);

4 5 , (93);
13 14 , slight allowance to be made;
14 15 , 80 grams in m² path reduces energy to zero;
15 16 , "

(70); more CO₂ no further effect;

0.65 for two air masses to allow for ozone absorption when the radiation comes from a celestial body.

F. Paschen gives (Annalen d. Physik. u. Chemie, 51, p. 14, 1804) the absorption of the radiation from a blackened strip at 500° C. by a layer 33 centimeters thick of water vapor at 100° C. and atmospheric pressure as follows:

Wave length	μ μ	μ μ	μ μ
	2.20-3.10	5.33-7.67	7.67-10 (?)
Percentage absorption	80	94	94-13

The following table, due to Rubens and Aschkinass (Annalen d. Physik u. Chemie, 64, p. 598, 1898), gives the absorption of radiation from a zircon burner by a layer 75 centimeters thick of water vapor saturated at 100° C. This amount of vapor is about equivalent to a layer of water 0.45 millimeter thick or to 1.5% of the water in a total vertical atmospheric column whose dewpoint at sea-level is 10° C. The region of spectrum examined includes most of the region of terrestrial radiation.

Wave length	μ 7.0	μ 8. o	μ μ 9.0~12.0	μ 12.4	μ 12.8	μ 13.4	μ 14.0
Percentage absorption	75	40	6	20	13	28	22
Wave length	μ 14.3	μ 15.0	μ 15.7	μ 16.0	μ 17.5	μ 18.3	μ 20. 0
Percentage absorption	43	35	65	52	88	80	100

TABLE 111.

ENERGY DISTRIBUTION AND ATMOSPHERIC TRANSMISSION OF SOLAR RADIATION.

						Ener	ution		
U. V. glass	Wave	Trans- mis-	Trans- mis-	U. V. glass	Dry air		Mois	t air	
devia- tion	lengths	sion	sion for	pris-			***********	Sun's	zenith
from		dry	water	matic energy	S	un in zenit	dista		
ω_1		air	vapor				60°.0	70°.7	
1	μ	$a_{a\lambda}$	$a_{x\lambda}$	$e_{0\lambda}$	$e_{0\lambda}a_{a\lambda}$	$e_{\theta\lambda}a_{a\lambda}a_{w\lambda}$	$e_{\theta\lambda}a_{a\lambda}a_{w\lambda}^2$	$e_{\theta\lambda}a_{a\lambda}^2a_{w\lambda}^2$	$e_{0\lambda}a_{w\lambda}^3a_{w\lambda}^9$
+230	.3504	0.556	0.926	127	71	65	61	34	II
220	.3600	.592	.934	150	89	84	78	46	17
210	.3709	.630	.940	179	113	106	100	63	26
200	.3838	.670	-945	191	128	121	114	76	34
190	-3974	.707	.949	246	174	165	156	111	54
180	.4127	.743	.953	396	294	280	267	198	105
170	.4307	.779	.957	452 506	352	337	323	252	144
160	.4516	.815	.961	596	486	467 582	448	365	224
150	•4753	.847 .876	.964 .968	713 808	604 708	582 685	561 663	475 581	311 406
140	.5026		-		810	786		689	
130	·5348 ·5742	.902 .926	.971 .974	897 1063	984	959	763 934	865	506 666
115	.5980	.937	.976	1177	1103	1077	1051	985	779
110	.6238	.947	.978	1248	1181	1155	1130	1070	866
105	.6530	.955	.980	1330	1271	1245	1220	1166	968
100	.6858	.963	.981	1420	1368	1342	1316	1268	1069
95	.7222	.970	.982	1441	1398	1373	1348	1308	1117
90	.7644	.976	.984	1442	1408	1385	1363	1330	1160
85	.8120	.981	.985	1431	1404	1383	1362	1337	1180
80	.8634	.985	.986	1410	1389	1370	1351	1331	1188
75	.9220	.989	.987	1374	1358	1341	1324	1308	1181
70	.9861	.991	.987	1321	1307	1290	1273	1265	1144
65	1.062	-994	.988	1242	1234	1219	1205	1197	1093
60	1.146	-995	.988	1084	1079	1066	1053	1048	959
55	1.225	.996	.988	956	952	941	930	926 802	848
50	1.302	-997	.988 .988	826	824 711	814 703	804 694	693	735 635
45	1.377 1.452	.998 .998	.988	713 629	628	620	613	612	561
40	1.528	.9985	.988	558	557	550	544	543	498
35	1.603	.9988	.988	504	503	497	491	491	450
25	1.670	.9990	.987	455	454	449	443	442	403
20	1.738	.9992	.987	412	412	406	401	401	365
+ 10	1.870	.9993	.987	320	320	316	312	311	284
± 0	2.000	.9995	.986	233	233	230	226	226	205
10	2.123	.9996	.985	150	150	148	146	145	131
20	2.242	-9997	.984	89	89	88	86	86	77
30	2.348	.9997	.983	74 68	74 68	73	72	72	63
- 40	2.442	.9998				67	66	66	58
	or u. v. n				435	346	264 1.0	0.5	0.0
Total	nt of tota .34640	II		3.1	1.3	1.2	1018	659	284
Per ce	nt of tota	μ		5.0	3.5	3.7	3.7	2.7	1.5
Total	.40570.	1 u		14462	12885	12501	12139	10874	8043
Per ce	nt of tota	il		40.2	39.2	43.4	44.3	43.7	42.3
Total.	.704-2.4.	12 μ		17855	17672	17432	17194	17030	15322
	or i. r. no			705	698	575	473	468	190
Cor. f	or w. v. a	bsorptic	on			3090	3665	4275	4814
	infra-red				18370	14917	14002	13223	10698
	ent of tota				56.0	51.7	51.1	53.1	56.2
	bed by pe			_	231	230	220	280	290
	spectrum				32608	28615	27203	24599 68 5	18743
Atmos	spheric tr	ansmiss	10n	100	90.8	79.7	75.8	68.5	52.2

The International Meteorological Symbols were adopted at the Vienna meteorological congress of 1873. A few additions and modifications have been made at subsequent international meteorological meetings. The forms of these symbols are more or less flexible. Those shown in the accompanying table are the forms which have generally been used in the United States. The principal variants found in the meteorological publications of the different countries are given in the Monthly Weather Review (Wash., D. C.), May, 1916, p. 268.

Exponents.—An exponent added to a symbol indicates the degree of intensity, ranging from ° weak (light, etc.) to ² strong (heavy, etc.). Thus, ◎°, light rain; ◎², heavy rain. German and French observers use the exponent ¹ to denote medium intensity, in accordance with the German and French versions of the report of the Vienna congress, and the German editions of the Codex. The English version of the above-mentioned report and the English edition of the Codex provide for the use of only two exponents, ° and ²; hence in English-speaking countries the omission of the exponent indicates medium intensity.

Time of occurrence.—When hours of occurrence are added to symbols, the abbreviation a is used for a.m., and p for p.m. Thus, \bigcirc 10a - 4p denotes "rain from 10 a.m. to 4 p. m." 12a = noon; 12p = midnight. The abbreviation n means "during night." Stations taking tri-daily observations may use a to mean between the first and second observation; p, between the second and third; and n, between the third and the first.

For further information concerning the International Symbols and other meteorological symbols, see "Meteorological Symbols," by C. Fitzhugh Talman, Monthly Weather Review (Wash., D. C.), May, 1916, pp. 265-274.

SMITHSONIAN TABLES.

INTERNATIONAL METEOROLOGICAL SYMBOLS.

Symbol.	Meaning.	Remarks.
	Rain.	nomains.
×	Snow.	
*	Rain and snow to-	
T	gether ("sleet"	
13	of British usage). Thunderstorm.	Thursday and lightning
T	Thunderstorm.	Thunder and lightning. Without lightning.
< .	Lightning.	Without thunder; "heat-lightning."
	Hail.*	
	Graupel.	Sometimes called "soft hail." French, <i>grésil</i> . Resembles little snow-pellets.
	Fog.	NT
	Ground fog. Wet fog.	Not exceeding the height of a man. One which wets exposed surfaces.
	Hoarfrost.	One which wets exposed surfaces.
	Dew.	
V	Rime.	A rough frost deposit from fog.
00	Glaze; Glazed frost.†	called "sleet."
1	Driving snow.	Ger., Schneegestöber; Fr., bourrasque de neige.
←	Ice-crystals.	Ice-needles sometimes seen floating or slowly falling in the air in clear, cold weather.
\boxtimes	Snow on ground.	Ground near station more than half covered. Wind of force 8–12, Beaufort scale. (Rept. Int. Met l
	Gale.	Comm., Berlin, 1910, English ed., p. 17.) Formerly
		used for "strong wind." A 3-barbed arrow is intro-
		duced in the 2d German ed. of the Int. Met'l Codex
		to denote "strong wind," but no authority is cited. According to the Observer's Handbook of the British
		Met'l Office "the number of barbs on the arrow may
		conveniently be made to represent the strongest wind
		force noted," but there is no international sanction for such variants.
	Sunshine.	In German edition of Int. Met'l Codex, but has never
		been definitely recognized by the international or-
		ganization. (See Rept. Int. Met'l Comm., South-
		port, 1903, Engl. ed., pp. 19 and 101.) Widely used in German and Austrian publications.
0	Solar halo.	
0	Solar corona.	
Ð	Lunar halo.	
9	Lunar corona. Rainbow	
	Aurora.	
	Zodiacal light.	
∞ 7	Haze.	Due to fine dust, or to the disturbance of atmospheric
		transparency by air-currents of different densities ("optical turbidity"), and not to water-drops. In
		practice, this is often difficult to distinguish from
		light fog (\equiv '), or "mist" of British observers.
		Prussian and Austrian observers underscore this symbol (\mathfrak{D}) to denote a definitely <i>smoky</i> atmosphere
		("Moorrauch").
\rightarrow	Mirage.	
Ó	Exceptional visibil-	
≡S≅	Sand storm or dust	
	storm.	
* Tr	ue hail which occurs chief	y with summer thunderstorms, should be distinguished from the

^{*} True hail, which occurs chiefly with summer thunderstorms, should be distinguished from the snowy pellets, like miniature snowballs, known as graupel, or soft hail (Δ): also from the small particles of clear ice, called slect by the U. S. Weather Bureau, for which there is no international symbol. On the history of the word sleet see Monthly Weather Review, May, 1916, pp. 381.886

† Glaze is the official term in the United States; glazed frost in Great Britain.

The International Conference of Meteorologists held at Munich in 1891 recommended the following classification of clouds, elaborated by Messrs. Abercromby and Hildebrandsson:

a. Detached clouds with rounded upper outlines (most frequent in dry weather).
 b. Clouds of great horizontal extent suggesting a layer or sheet (wet weather).

A. Upper Clouds, average altitude 9000m.

a. 1. Cirrus. b. 2. Cirro-stratus.

B. Intermediate Clouds, between 3000^m and 7000^m.

a. { 3. Cirro-cumulus. b. Alto-cumulus. 5. Alto-stratus.

C. Lower Clouds, below 2000m.

a. 6. Strato-cumulus. b. 7. Nimbus.

D. Clouds of diurnal ascending currents.

a. 8. Cumulus; top 1800^m; base 1400^m.
b. 9. Cumulo-nimbus; top 3000^m to 8000^m; base 1400^m.

E. High Fogs, under 1000m.

10. Stratus.

DEFINITIONS AND DESCRIPTIONS OF CLOUD FORMS.

- 1. Cirrus (Ci.). Detached clouds of delicate and fibrous appearance, often showing a featherlike structure, generally of a whitish color. Cirrus clouds take the most varied shapes, such as isolated tufts, thin filaments on a blue sky, threads spreading out in the form of feathers, curved filaments ending in tufts, sometimes called Cirrus uncinus, etc.; they are sometimes arranged in parallel belts which cross a portion of the sky in a great circle, and by an effect of perspective appear to converge towards a point on the horizon, or, if sufficiently extended, towards the opposite point also. (Ci.-St. and Ci.-Cu., etc., are also sometimes arranged in similar bands.)
- 2. Cirro-stratus (Ci.-St.). A thin, whilish sheet of clouds sometimes covering the sky completely and giving it only a milky appearance (it is then called Cirro-nebula), at other times presenting, more or less distinctly, a formation like a tangled web. This sheet often produces halos around the Sun and Moon.
- 3. Cirro-cumulus (Ci.-Cu.). Mackerel sky. Small globular masses or white flakes without shadows, or showing very slight shadows, arranged in groups and often in lines.
- 4. Alto-stratus (A.-St.). A thick sheet of a gray or bluish color, sometimes forming a compact mass of dark gray color and fibrous structure. At other times the sheet is thin, resembling thick Ci.-St., and through it the Sun or the Moon may be seen dimly gleaming as through ground glass. This form exhibits all changes peculiar to Ci.-St., but from measurements its average altitude is found to be about one half that of Ci.-St.
- 5. Alto-cumulus (A.-Cu.). Largish globular masses, white or grayish, partially shaded, arranged in groups or lines, and often so closely packed that their edges appear confused. The detached masses are generally larger and more compact (resembling St.-Cu.) at the center of the group, but the thickness of the layer varies. At times the masses spread themselves out and assume the appearance of small waves or thin slightly curved plates. At the margin they form into finer flakes (resembling Ci.-Cu.). They often spread themselves out in lines in one or two directions.
- 6. Strato-cumulus (St.-Cu.). Large globular masses or rolls of dark clouds often covering the whole sky, especially in winter. Generally St.-Cu. presents the appearance of a gray layer irregularly broken up into masses of which the edge is often formed of smaller masses, often of wavy appearance resembling A.-Cu. Sometimes this cloud-form presents the characteristic appearance of great rolls arranged in parallel lines and pressed close up against one another. In their centers these rolls are of a dark color. Blue sky may be seen through the intervening spaces which are of a much lighter color. (Roll-cumulus in England, Wulst-cumulus in Germany.) St.-Cu. clouds may be distinguished from Nb. by their globular or rolled appearance, and by the fact that they are not generally associated with rain.
- 7. Nimbus (Nb.), Rain Clouds. A thick layer of dark clouds, without shape and with ragged edges, from which steady rain or snow usually falls. Through the openings in these clouds an upper layer of Ci.-St. or A.-St. may be seen almost invariably. If a layer of Nb.

scparates up in a strong wind into shreds, or if small loose clouds are visible floating underneath a large Nb., the cloud may be described as Fracto-nimbus (Fr.-Nb.) ("Send" of sailors).

8. Cumulus (Cu.), Wool pack Clouds.—Thick clouds of which the upper surface is dome-shaped and exhibits protuberances while the base is horizontal. These clouds appear to be formed by a diurnal ascensional movement which is almost always noticeable. When the cloud is opposite the Sun, the surfaces facing the observer have a greater brilliance than the margins of the protuberances. When the light falls aslant, as is usually the case, these clouds throw deep shadows; when, on the contrary, the clouds are on the same side of the observer as the Sun, they appear dark with bright edges.

True cumulus has well defined upper and lower limits, but in strong winds a broken cloud resembling Cumulus is often seen in which the detached portions undergo continual change. This form may be distinguished by the name Fracto-

cumulus (Fr.-Cu.).

o. Cumulo-nimbus (Cu.-Nb.), The Thunder-Cloud; Shower-Cloud.—Heavy masses of cloud rising in the form of mountains, turrets or anvils, generally surmounted by a sheet or screen of fibrous appearance (false Cirrus) and having at its base a mass of cloud similar to nimbus. From the base local showers of rain or snow (occasionally of hail or soft hail) usually fall. Sometimes the upper edges assume the compact form of cumulus, and form massive peaks round which delicate "false Cirrus" floats. At other times the edges themselves separate into a fringe of filaments similar to Cirrus clouds. This last form is particularly common in spring

The front of thunder-clouds of wide extent frequently presents the form of a large

arc spread over a portion of a uniformly brighter sky.

10. Stratus (St.) .- A uniform layer of cloud resembling a fog but not restina on the ground. When this sheet is broken up into irregular shreds in a wind, or by the summits of mountains, it may be distinguished by the name Fracto-stratus (Fr.-St.).

During summer all low clouds tend to assume forms resembling Cumulus, and may be described accordingly as Stratus cumuliformis, Nimbus cumuliformis, etc. The term Mammato-cumulus is applied to a cloud having a mammillated lower

surface, occurring especially in connection with severe local storms.

The ovoid form, with sharp edges, assumed by certain clouds, particularly during the occurrence of sirocco, mistral or foehn, is indicated by the adjective lenticularis. e.g., Cumulus lenticularis (Cu. lent.), Stratus lenticularis (St. lent.). Such clouds frequently show irridescence.

For pictures of typical cloud forms see

Clarke, George A. Clouds. London, 1920. Great Britain, Meteorological office. Cloud forms according to the international elassification. 2d ed. London, 1921.

Humphreys, William J. Fogs and clouds. Baltimore. 1926.

International meteorological committee. International cloud-atlas. 2d ed. Paris. 1910. [Abridged edition for use of observers. 1930.]

U. S. Weather bureau. Cloud forms according to the international system of classification. 2d ed. Washington. 1928.

BEAUFORT WEATHER NOTATION.

Especially intended for the use of mariners, but sometimes used at land stations. The original notation was devised in 1805 by Admiral Sir F. Beaufort; it has since been slightly altered and amplified by British and American meteorologists. The following symbols are used by the marine observers of the U. S. Weather Bureau:

```
Upper Atmosphere:
  b.-Blue sky.
  c.-Cloudy sky.
  o.-Overcast sky.
Lower Atmosphere:
  v.—Visibility (exceptionally clear).
  z.—Haze.
 m.—Mist.
  f.-Fog.
Precipitation:
  d.—Drizzling.
  p.—Passing showers.
  r.—Rain.
  s.-Snow.
  h.-Hail.
Electric phenomena:
   1.—Lightning.
  t.—Thunder.
Wind:
  q.—Squally.
The British Meteorological Office also uses the following:
  e.-Wet air without rain.
  g.—Gloom.
  u.—Ugly or threatening appearance of the weather.
  w.—Dew.
  tl.—Thunderstorm.
KQ.—Line squall.
 rs.—Sleet (rain and snow together).
 fe.-Wet fog.
  y.—Dry air (less than 60% relative humidity).
  x.—Hoarfrost.
```

According to instructions to the marine meteorological observers of the U. S. Weather Bureau, the underscoring of a letter denotes great intensity and double underscoring very great intensity.

The following instructions appear in the Meteorological Observer's Handbook of the British Meteorological Office (1926 edition):

"Capital letters are used to indicate occasions when the phenomenon to be noted is of unusual intensity. At the other end of the scale, occasions of slight intensity are distinguished by adding a small suffix o. Thus,

```
R.—Heavy rain.
r.—Moderate.
r<sub>o</sub>.—Slight rain.
```

and similarly with other phenomena.

"Continuity is indicated by repeating the letter; thus,

```
RR.—Continuous heavy rain. rr.—Continuous moderate rain.
```

"The prefix 'i' is used to indicate 'occasional' or 'intermittent'; thus,

```
if.—Occasional fog. ir..—Intermittent slight rain."
```

INTERNATIONAL CODE FOR HORIZONTAL VISIBILITY.

```
Code
figure.

Objects.

O = not visible at 50 meters (55 yards).

1 = not visible at 500 meters (220 yards).

2 = not visible at 500 meters (550 yards).

3 = not visible at 1,000 meters (1,100 yards).

4 = not visible at 2,000 meters (2½ miles).

5 = not visible at 4,000 meters (2½ miles).

6 = not visible at 20,000 meters (12½ miles).

7 = not visible at 20,000 meters (31 miles).

8 = not visible at 50,000 meters (31 miles).

9 = visible at 50,000 meters or more.
```

SMITHSONIAN TABLES.

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NORTH AMERICA.	Latitude	Longitude from Greenwich	Heigh	ıt
ALASKA				
A 11 - 1 - 1 - 1 - 1	66° 34′ N.	152° 44′ W.	Feet 1000	m.
Allakaket* *Barrow	7I 23	152° 44′ W. 156 17	23	305 7
*Dillingham	59 0	158 28	80	24
*Dutch Harbor	53 55	166 30	50	15
*Eagle Fairbanks	64 46 64 51	141 12 147 52	834 500	254 152
Fort Yukon	66 34	145 18	417	127
Holy Cross	62 12	159 50	50	15
Juneau	58 18	134 24	203	62
Ketchikan	55 20 61 29	131 37 142 57	75 2003	23 610
*Kodiak	57 48	152 22	155	47
McKinley Park	63 44	148 55	2015	614
Nome *St. Paul Island	64 30	165 24 170 10	22 40	7 12
Shishmaref	57 15 66 13	170 10 166 0	12	4
*Sitka	57 3	135 19	65	20
Skagway	59 27	135 19	30	9
Tanana *Valdez	65 10 61 7	152 6 146 16	220 400	67 122
Yakutat	59 33	139 44	5	2
CANADA	3.7	***		
Athabasca	54 43 N.		1550 2240	472 683
Banff	59 35 51 10	133 38 115 34	4521	1378
*Barkerville	53 2	121 35	4180	1274
Battleford	52 41	108 20	1592	485
Bella Coola *Belle Isle	52 40 51 53	126 54 55 53	150 426	46 130
*Berens River	52 18	97 23	710	216
*Calgary	51 2	114 2	3428	1045
*Carcross Charlottetown	61 11 46 14	134 34 63 10	2171 38	662 12
Chatham.	47 3	65 29	28	9
Chesterfield Inlet	63 45	91 50	48	15
Cochrane	49 2	81 0	930	283
Craig Harbor* *Dawson	76 20 64 4	80 50	1062	3 324
Doucet	48 13	76 37	1236	377
Edmonton	53 33	113 30	2158	658
Father Point	48 31 49 43	68 10 54 17	20 30	6
Fond du Lac	59 20	107 24	690	210
Fort Chimo	58 10	68 10	50	15
*Fort Chipewyan	58 52	01 111	714 6	218
Fort Churchill* *Fort George	58 51 53 50	94 II 79 5	320	98
*Fort Good Hope	66 25	128 53	214	65
Fort McPherson	67 26	134 57	150	46
Fort Norman	64 57 54 28	125 0 124 12	266 2280	81 695
Fort St. John	56 15	124 12	1462	446
*Fort Simpson	61 52	121 35	423	129
Fort Vermilion	58 27	116 3	950	290

	->-0					
CANADA	Lat	itude	fr	gitude om enwich	He	ght
(Continued)					Feet	m
	44°60 58869 50062 5149 53363 500550 4556 500655 500655 4572 48847 57753 44775 484775 4946 5046443	39' N. 51 12 30 41 17 50 23 0 49 35 1 15 15 30 14 33 8 3 30 19 43 27 35 20 10 18 30 48 13 57 17 34 27 20 10 40 52	63° 115 62 139 120 92 70 116 71 101 135 100 97 73 73 80 61 60 97 75 85 66 80 89 92 105 130 103 71 132 60 66 52 63 81 107 60 79 89	36' W. 20 21 15 29 12 40 8 2 155 51 37 50 555 35 41 48 10 21 44 44 45 10 24 46	Feet 88 529 49 15 1262 1140 52 5670 860 1900 2144 1690 1255 187 30 13 20 720 294 620 635 13 644 30 12 49 1450 170 2115 296 215 296 25 119 125 30 857 2392 48 379 1128	m. 27 161 15 5 385 347 16 1728 262 579 653 515 383 57 9 4 6 219 90 189 194 4 196 9 4 15 442 52 645 90 8 36 38 9 261 729 15 116 344
Vancouver. *Victoria. White River. *Winnipeg.	53 49 48 48 49	17 24 35 53	123 123 85 97	5 19 16 7	136 230 1244 760	41 70 379 232
CANAL ZONE	49	33	97	/	700	232
Balboa Heights	8 9 9	58 N. 21 3	79 79 79	33 W. 55 39	118 36 404	36 11 123

	Latitude	Longitude from Greenwich	Height
*Belize Corinto Greytown Guatemala Managua Puerto Barrios Puerto Castilla San Jose *San Salvador.	17° 29′ N. 12 28 10 55 14 37 12 10 15 43 16 0 9 56 13 42	88° 14′ W. 87 12 83 43 90 31 86 15 88 45 86 2 84 7 89 12	Feet m. 17 5 4855 1480 135 41 3760 1146 2155 657
GREENLAND *Angmagsalik. *Godthaab. *Inglefield Bay. *Ivigtut. *Jakobshavn. Julianehaab. Mygbugten. Scoresby Sound.	65 36 N. 64 10 77 27 61 12 69 13 60 43 73 30 70 29	37 34 W. 51 44 66 40 48 10 51 2 46 3 21 30 21 58	95 66 29 20 82 25 31 233 71 13 4 56 17
ICELAND *Akureyri. *Grimsey Grimsstad. Modrudal. Papey. *Stykkisholm. *Vestmanno.	65 40 N. 66 33 65 36 65 19 64 36 65 5 63 24	18 5 W. 18 1 16 12 15 55 14 13 22 46 20 17	13 4 22 1263 385 1575 480 92 28 82 25 433 132
MEXICO Acapulco Altar Campeche Casas Grandes. *Chihuahua Choix. *Colima Culiacan Durango. Frontera. Guadalajara Guanajuato Guaymas Hermosillo Huetamo. *La Paz Las Vigas. *Leon Lerdo Mazatlan *Merida Monclova. *Monterrey *Morelia	16 50 N. 30 43 19 51 30 25 28 38 26 50 19 12 24 48 24 1 18 32 20 41 21 1 27 55 29 8 18 34 24 10 19 40 21 7 25 30 23 11 20 58 26 54 25 40 19 42	99 56 W. 111 43 90 32 107 55 106 4 108 18 103 45 107 24 104 40 92 39 103 20 101 15 110 53 110 50 100 53 110 21 97 7 101 41 103 32 106 25 89 38 101 25 100 18 101 7	10 3 1299 396 82 25 4774 1455 4669 1423 1017 310 1670 509 174 53 6188 1886 7 2 5105 1556 6683 2037 13 4 716 218 1401 427 39 12 8140 2481 5935 1809 3740 1140 256 78 72 22 1978 603 1732 528 6309 1923

			-	
MEXICO	Latitude	Longitude from Greenwich	Heigh	t
(Continued)			Feet	m.
Motozintla Oaxaca. Pachuca. Panuco Parral. Payo Obispo. Progreso. Puerto Mexico *Salina Cruz. San Luis Potosi. *Tacubaya (Mexico City). Tampico. Tapachula. Teapa. Tehuacan. Tenosique. Tepic. Tuxtla Gutierrez. Valladolid. Vera Cruz. Victoria. Zacatecas.	15° 22′ N. 17	92° 14′ W. 96 42 98 45 105 58 105 58 105 40 88 20 89 40 94 24 95 12 100 58 99 11 97 51 92 16 92 57 97 23 91 26 104 53 93 6 88 13 96 8 99 8 102 34	4774 5128 7989 2625 5420 13 46 46 48 6158 7575 59 551 148 5420 197 3025 1759 72 52 1040 8570	1455 1563 2435 800 1652 4 14 14 14 2309 18 168 45 1652 60 922 536 22 16 317 2612
*Abilene. *Abilene. Albany. Alpena. Amarillo. Anniston. Apalachicola. Asheville. Atlanta. Atlantic City. Augusta. Austin. Baker. Baltimore. Bentonville. Binghamton. Birmingham. *Bismarck. Block Island. Boise. Boston. Brownsville. Buffalo. Burlington Cairo. Canton Cape Henry. Charles City. *Charleston. Charlotte. Charlotte. Charlotte.	32 23 N. 42 39 45 5 35 13 33 39 29 45 35 36 33 45 39 22 33 28 30 16 44 46 39 17 36 22 46 47 41 10 43 37 44 10 43 37 44 221 36 2 26 0 42 53 44 36 56 43 4 36 56 43 47 35 13 35 4	99 40 W. 73 45 83 30 101 50 85 50 84 58 82 32 84 23 74 25 81 54 97 44 117 50 76 37 94 12 75 55 86 50 100 38 71 36 116 13 71 4 95 49 97 26 78 53 73 12 89 10 75 10 76 0 92 38 79 56 80 51	1738 97 609 3676 741 36 2253 1173 52 182 605 3471 123 1303 871 700 1674 26 2739 125 765 57 767 403 358 448 18 1015 48 779 762	530 30 186 1120 226 11 687 358 16 55 184 1058 37 397 265 213 510 8 835 38 233 17 234 123 109 137 55 309 15 237 237 232

UNITED STATES	Latitude	Longitude from Greenwich	Heigh	t
*Cheyenne *Chicago. Cincinnati. Cleveland. Columbia, Mo. Columbia, S. C. Columbus. Concord. Concordia. Corpus Christi. Dallas. Davenport. Dayton. Del Rio. *Denver. Des Moines. Detroit. Devils Lake. Dodge City. Dubuque. Due West. *Duluth. Eastport. Elkins. Ellendale. El Paso. Erie. Escanaba. Eureka. Evansville. Flagstaff. Fort Smith. Fort Wayne. Fort Worth. Fresno. *Galveston. Grand Haven. Grand Haven. Grand Junction. Grand Rapids. Green Bay. Greenville. Groesbeck. Hannibal. Harrisburg. Hattford. Hatteras. Havre. *Helena. Houghton. Houston Huron. Independence. Indianapolis. Iola. Ithaca.	41 35 42 20 48 7 37 45 42 30 34 21 46 47 44 54 38 53 45 59 31 47 42 7 45 48 40 48 37 58 35 12 36 42 29 18 43 4 39 4 40 48 37 58 38 45 59 31 47 42 7 45 48 40 48 37 58 41 5 36 42 29 18 41 46 31 30 32 43 36 42 29 18 41 42 58 42 39 43 42 50 31 30 32 43 33 45 50 31 30 31 30 31 30 32 43 33 45 50 31 50 37 55 38 48 34 48 39 46 37 55	104° 48′ W. 87 35 84 31 81 42 92 20 81 3 83 0 71 32 97 41 97 25 96 47 90 38 84 10 100 53 105 0 93 37 83 3 98 52 100 0 44 82 22 92 6 66 59 79 49 98 34 106 30 80 5 87 5 124 11 87 33 111 37 94 24 85 10 97 15 119 49 94 50 86 14 108 34 85 40 88 0 82 24 96 28 91 20 76 52 72 40 75 40 109 40 112 4 88 34 95 24 96 12 97 15 119 49 94 50 86 14 108 34 87 33 111 37 94 24 88 0 89 22 92 40 75 40 109 40 112 4 88 34 95 24 96 12 97 25 76 29	Feet 6088 673 627 762 784 351 822 289 1392 20 512 606 899 944 5292 861 730 1478 2509 700 711 1133 76 1947 1457 3778 714 612 62 431 6907 457 856 670 327 54 632 4602 707 617 1039 461 534 374 159 11 2505 4110 668 138 1306 3957 822 984 836	m. 1856 205 191 232 239 107 251 88 424 6 156 185 274 288 1613 262 222 450 765 213 217 345 23 593 444 1152 218 187 19 131 2105 139 261 204 100 16 193 1403 215 188 317 141 163 1144 48 3 764 1253 204 42 398 1206 251 300 255

UNITED STATES	Latitude	Longitude from Greenwich	Heig	ht
(Continued)			Feet	m.
Jacksonville Kalispell Kansas City Keokuk *Key West Knoxville La Crosse Lander. Lansing Lewiston Lexington Lincoln Little Rock Los Angeles Louisville Ludington Lynchburg Macon Marquette Memphis Meridian Miami Miles City Milwaukee Minneapolis *Mobile *Modena Montgomery Moorhead Nantucket *Nashville New Haven *New Orleans New York Norfolk North Head *North Platte Oklahoma City Omaha Oswego Palestine Parkersburg Pensacola Peoria Philadelphia Phoenix Pierre Pittsburgh Pocatello Port Angeles Port Arthur Port Huron	30° 20′ N. 48 10 39 5 40 22 24 33 35 56 43 49 44 250 42 44 46 25 38 2 40 49 34 45 33 57 37 25 32 50 43 35 46 34 35 57 37 25 32 25 48 46 25 41 17 36 10 41 18 29 57 40 43 37 48 32 23 41 17 36 10 41 18 29 57 40 43 31 45	81° 39′ W. 114 25 94 37 91 26 81 48 83 58 91 15 108 45 84 26 117 2 84 33 96 45 92 16 118 15 85 45 86 27 79 9 83 38 89 23 87 24 90 3 88 40 80 12 105 49 87 54 93 18 88 2 113 54 86 18 96 44 70 6 86 47 72 56 90 4 74 0 76 17 72 41 124 4 100 45 97 33 95 56 76 35 95 40 81 36 87 13 89 36 75 9 112 0 100 21 80 0 112 29 1123 6 93 55 82 26 70 15	Feet 43 2973 963 614 22 995 714 5372 878 757 989 1189 357 338 525 637 681 370 974 734 339 375 25 2371 681 918 57 5473 223 940 12 546 106 53 314 91 876 211 2821 1214 1105 335 510 637 56 609 114 1108 1572 842 4477 29 34 638 103	m. 13 906 294 187 7 303 218 1637 268 231 301 362 109 103 160 194 208 113 297 224 122 114 8 723 208 280 17 1668 68 286 4 166 32 16 96 28 267 64 860 370 337 102 155 194 17 186 35 338 479 257 1365 9 10 194 31

I I				
UNITED STATES	Latitude	Longitude from Greenwich	Heigl	nt
(Continued)			Foot	m
*Portland, Ore Providence Providence Pueblo Raleigh Rapid City Reading Red Bluff Reno Richmond Rochester Roseburg Roswell Royal Center Sacramento St. Joseph *St. Louis St. Paul *Salt Lake City San Antonio *San Diego Sandusky Sandusky Sandy Hook *San Francisco San Jose *Santa Fe Sault Ste Marie Savannah Scranton Seattle Sheridan Shreveport Sioux City Spokane Springfield, Ill Springfield, Mo Syracuse Tacoma Tatoosh Island Tatylor Terre Haute Thomasville Tonopah Topeka	45° 32′ N. 41° 50 38° 18 35° 45° 44° 20 40° 10 39° 32° 37° 32° 43° 43° 43° 43° 43° 43° 43° 43° 44° 53° 38° 35° 39° 49° 38° 38° 44° 48° 37° 20° 35° 41° 46° 30° 32° 43° 41° 25° 40° 28° 37° 48° 37° 20° 35° 41° 46° 30° 32° 5° 41° 24° 47° 38° 44° 48° 37° 20° 35° 41° 46° 30° 32° 5° 41° 24° 48° 33° 31° 22° 47° 40° 39° 48° 43° 48° 32° 20° 42° 29° 43° 48° 33° 35° 33° 33° 35° 33° 33° 33° 33° 33° 33° 33° 33° 33° 33° 33°	from Greenwich 122° 41' W. 71 25 104 36 78 37 103 12 75 58 122 15 119 49 77 27 77 42 123 20 104 27 86 29 121 30 94 51 90 12 93 3 111 54 98 28 117 10 82 40 74 1 122 26 121 54 105 57 84 21 81 5 75 42 122 20 106 57 93 40 96 24 117 25 89 39 93 18 76 10 122 23 88 27 124 44 97 20 87 24 88 58 83 34 117 4 95 41	Feet 153 160 4685 376 3259 325 332 4532 144 523 510 3566 736 69 967 568 837 4360 693 87 629 22 155 141 7013 614 65 805 125 3790 249 1135 1929 636 1324 597 194 35 597 194 35 586 583 575 273 628 6090 987	m. 47 49 1428 115 993 99 101 1381 44 159 155 1087 224 21 295 173 255 1329 211 27 192 7 47 43 2138 187 20 245 38 1155 76 346 588 194 404 182 59 11 26 178 83 191 1856 301 58
Trenton. Valentine. Vicksburg. Walla Walla *Washington Wichita Williston. Wilmington. Winnemucca. Wytheville. Yankton. Yellowstone Park Vuma.	40 14 42 50 32 22 46 2 38 54 37 41 48 9 34 14 40 58 36 56 42 54 44 58 32 45	74 45 100 32 90 53 118 20 77 3 97 20 103 35 77 57 117 43 81 5 97 28 110 42 114 36	190 2598 247 991 112 1358 1878 78 4344 2304 1233 6241 141	58 792 75 302 34 414 572 24 1324 702 376 1902 43

	. (London, 19	- 5.7		
	Latitude	Longitude from Greenwich	Heigl	ht
WEST INDIES			Feet	m
Basseterre, St. Kitts. *Bridgetown, Barbados. Camaguey, Cuba. Castleton Gardens, Jamaica. Cayey, Porto Rico. Christiansted, Virgin Is. Cienfuegos, Cuba. Fort de France, Martinique. Grand Turk, Bahama Is. *Havana (Belén). Hill Gardens, Jamaica. Kingston, Jamaica. Mooretown, Jamaica. *Nassau, Bahama Is. *Negril Point, Jamaica. Pinar del Rio, Cuba. *Port au Prince, Haiti. Port of Spain, Triniclad. Puerto Plata, Dominican Rep. *Richmond Hill, Grenada Roseau, Dominica. San Juan, Porto Rico. Santiago de Cuba. Santo Domingo, Dominican Rep. Stony Hill, Jamaica. Swan Island. Willemstad, Curaçao.	17° 20′ N. 13 6 21 19 18 12 18 6 17 45 22 9 14 36 21 21 23 8 18 8 18 1 18 6 25 5 18 15 22 24 18 33 10 39 19 49 12 31 15 17 18 29 20 1 18 28 18 28 18 5 17 24 12 6	62° 44′ W. 59 37 77 55 76 49 66 12 62 42 80 27 61 2 71 7 82 21 76 45 76 48 76 27 77 21 78 24 83 44 72 20 61 31 70 43 61 45 66 7 75 52 69 53 76 48 83 17 68 56	30 30 344 496 1350 25 98 25 11 79 4900 24 600 12 33 180 121 40 27 509 25 82 118 57 1400 35 75	m. 9 9 105 151 411 8 30 8 3 24 1494 7 183 4 10 555 37 12 8 155 8 25 36 17 427 111 23
SOUTH AMERICA ARGENTINA *Año Nuevo. Azul. *Bahia Blanca *Buenos Aires *Catamarca Ceres. Choele Choel Chos Malal. Colonia 16 de Octubre. Concordia. *Cordoba Corrientes. General Acha. *Goya. Junin. La Quiaca. Mar del Plata. *Puerto Madryn Rivadavia. *Salta. San Juan. San Luis. *Santa Cruz. Santa Fe. Staten Island Tucuman. Ushuaia.	54° 39′ S. 36° 45 38° 45 38° 45 34° 36° 28° 27 29° 55 39° 17 37° 22 42° 12 45° 30° 31° 23 31° 25 27° 27 37° 22 29° 9 34° 36° 22° 10° 37° 59 42° 49 24° 12 24° 46° 31° 32° 33° 18° 52° 22° 31° 40° 54° 43° 56° 50° 54° 50° 54° 50°	64° 8′ W. 59 52 62 15 58 22 65 47 61 58 65 38 69 50 71 8 69 0 58 2 64 12 58 49 64 36 59 15 60 52 65 31 57 6 64 58 62 56 65 28 68 42 66 19 68 15 60 42 63 47 65 11 68 20	164 446 82 82 1673 285 456 2648 1827 899 79 1388 177 715 86 259 11358 82 50 682 3865 2178 2323 39 85 128 1467 26	50 136 25 25 510 87 139 807 557 274 24 423 54 218 26 79 3462 25 14 208 1178 664 708 12 26 39 447 8

	Latitude	Longitude from Greenwich	Heig	nt
BOLIVIA			Feet	m.
La Paz*Sucre	16° 30′ S.	68° 9′ W. 65 16	11909 9344	3630 2848
BRAZIL Alto Itatiaya	22 25 S.	44 50 W.	7152	2180
*Aracaju *Bahia (Ondina)	10 55 13 0	37 3 38 31	20 I54	6 47
*Barra do Corda Belem (Para)	5 30 1 27	45 16 48 29	266 43	81
*Bello HorizonteBoa Vista	19 55	43 55	2936	895
Brotas	22 i6 S.	48 4	2067	630
*CaetiteCoary	14 3 4 22	42 37 63 3	2943	897
*Corumba *Curityba	18 59 25 25	57 39 49 17	509 2979	155 908
*Cuyaba *Fernando_Noronha	15 36 3 50	56 6 32 25	541 348	165 106
Floriano PeixotoFonte Boa	9 I 2 35	67 26 66 I		
FormosaFortaleza (Porongaba)	15 32 3 46	47 18 38 32	2992 85	912 26
Goyaz*Manaos	15 55 3 8	50 8 60 I	1706 144	520 44
Morro do Chapeo Passo Fundo	11 33 28 16	41 14 52 24	3543 2326	1080 709
Pesquira Pirapora	8 24 17 21	36 46 44 57	2221 1549	677 472
*Porto Alegre Porto Nacional	30 I 10 39	51 13 48 20	36 778	1 I 237
Porto Velho*Quixeramobim	8 47	63 55	407	124
Recife (Pernambuco)	8 4	39 15 34 5 ²	679 98	207 30
Remate de Males	4 2I 32 2	70 24 52 6	10	3
*Rio de Janeiro	22 54 6 43	43 10 69 57	200	61
S. Gabriel S. Luiz (Maranhao)	0 8 2 32	67 3	279 66	85 20
São Paulo*Taperinha	23 33 2 30	46 38 54 20	2690 66	820 20
Theophilo Ottoni	17 50 22 27	41 26 42 55	1001 3120	305 951
Tres Lagoas	20 47 19 41	51 42 47 56	1148 2493	350 760
Uruguayana	29 45	57 5	243	74
CHILE Antofagasta	23 39 S.	70 25 W.	308	94
Arica Bahia Felix	18 28 52 58	70 20 74 4	16 49	5
Cabo Raper	46 50	73 56	131	40
*Concepcion (P. Tumbes) *Coquimbo (P. Tortuga)	36 37	73 6	394 89	120
Coquinibo (1. Tortuga)	29 56	71 27	09	27

Areteorological Office for 1922. (London, 1929.)							
CHILI	La	titude	f	ngitude rom enwich	Heig	ght	
(Continued) El Teniente. *Evanjelistas. *Iquique. *Juan Fernandez. Lonquimay. Melinka. Potrerillos. Puerto Montt. *Punta Arenas. *Punta Dungeness. *Santiago. Talca. Temuco. Valdivia. *Valparaiso (P. Angeles).	34° 52° 20° 33° 38° 43° 26° 41° 53° 52° 33° 35° 38° 39° 33° 33° 33° 33° 33° 33° 33° 33° 33	6' S. 24 12 37 26 54 30 28 10 24 27 26 45 48 1	70° 75 70 78 71 73 69 72 70 68 70 71 72 73 71	38' W. 6 11 50 14 46 27 57 54 26 42 40 38 14 38	Feet 7001 180 30 1132 3182 16 9350 328 92 16 1706 322 361 30 135	m. 2134 55 9 345 970 5 2850 100 28 5 520 98 110 9 41	
COLOMBIA Andagoya. *Bogota. Bucaramanga. Buenaventura. Pasto. Popayan.	5 4 6 3 1	4 N. 36 52 53 13 26	76 74 73 77 77 76	55 W. 5 34 10 28 36	250 8677 3340 8510 5709	76 26,5 1018 2594 1740	
ECUADOR Ambato Banos Guayaquil Quito	I I 2 0	15 S. 24 12 14	78 78 79 78	37 W. 24 51 30	8419 5906 40 9239	2566 1800 12 2816	
GUIANA *Cayenne. Dadanawa. *Georgetown *Paramaribo. Placer R'Awa.	4 2 6 5 3	56 N. 48 50 49 36	52 59 58 55 54	21 W. 26 12 9	20 6 I2	6 2 	
PARAGUAY *Asuncion. Mision Inglesa Puerto Bertoni.	25 23 25	21 S. 23 40	57 58 54	37 W. 23 35	305 361 515	93 110 157	
PERU *Arequipa. Cerro de Pasco. Cuzco. El Misti. Lima. Piura	16 10 13 16 12	22 S. 46 31 16 3	71 76 72 71 77 80	33 W. 6 3 30 3 40	7874 14272 11319 19200 512 164	2400 4350 3450 5852 156 50	
URUGUAY Durazno*Montevideo	33 34	19 S. 52	56 58	33 W. 32	299 95	91 29	

	Latitude	Longitude from Greenwich	Height
VENEZUELA			Feet m.
Calabozo *Caracas *Ciudad Bolivar El Peru Maracaibo *Merida	8° 56′ N. 10 30 8 9 7 19 10 38 8 36	67° 26′ W. 66 55 63 33 61 49 71 36 71 9	328 100 3419 1042 125 38 723 220 26 8 5384 1641
EUROPE ALBANIA Durazzo	41 19 N.	19 28 E.	23 7
AUSTRIA Bad-Gastein Graz. Innsbruck. Linz. Obir. Sonnblick. *Vienna.	47 7 N. 47 4 47 16 48 18 46 30 47 3 48 15	13 8 E. 15 28 11 24 14 16 14 29 12 57 16 22	3356 1023 1211 369 1909 582 997 304 6706 2044 10190 3106 666 203
BELGIUM *Brussels (Uccle)	50 48 N.	4 22 E.	328 100
*Aberdeen Belfast Ben Nevis Ben Nevis Birr Castle Birmingham Blacksod Point Cardiff Deerness Dublin Edinburgh Glasgow *Green wich Hull Kew *Lerwick Liverpool (Bidston) London (Westminster) Malin Head Norwich Plymouth Southampton Stornoway Tynemouth *Valencia Waterford	57 10 N. 54 35 56 48 53 6 52 28 54 6 51 28 58 56 53 21 55 55 55 53 51 28 53 45 51 28 53 24 51 30 55 23 51 30 55 23 51 30 55 23 51 30 55 23 51 30 55 21 50 55 58 51 50 55 58 11 55 0 51 56 52 16	2 6 W. 5 56 5 0 7 55 1 56 10 4 3 10 2 45 6 16 3 11 4 18 0 0 0 16 0 19 1 8 3 4 0 8 7 24 1 17 E. 4 8 W. 1 24 6 22 1 27 10 15 7 7	46 61 19 4405 1343 175 53 535 535 163 330 101 202 62 160 49 12 4 227 69 180 55 149 45 112 4 18 5 112 34 188 57 27 8 208 63 93 93 28 116 35 64 20 51 16 96 29 30 9 20 6
BULGARIA Burgas Philippopolis. Pleven. Rilski Monastir. *Sofia.	42 29 N. 42 9 43 31 42 8 42 42	27 29 E. 24 45 24 32 23 21 23 20	16 5 525 160 105 32 3855 1175 1804 550

Meteorological Office for 1922. (London, 1929.)							
	La	Latitude		fı	gitude rom enwich	Heig	rht
CZECHO-SLOVAKIA						Feet	
Brünn. C. Budejovice. Cheb. Kosice. Prague.	49° 48 50 48 50	58 4 44 5	N.	16° 14 12 21 14	35' E. 27 26 15 25	820 1283 1585 689 663	m. 250 391 483 210 202
DENMARK							
*Copenhagen. Fanö. Sand (Faroe Islands). Tvingstrup. Vestervig.	55 55 61 55 56	41 27 52 53 47	N.	8 6 9 8	33 E. 24 49 55 19	43 20 7 217 62	13 6 2 66 19
ESTHONIA *Dorpat (Tartu)	58 59	23 26	N.	26 24	43 E. 45	243 16	74 5
FINLAND *Helsingfors	60 68 64 62 67 61 61	12 57 13 55 22 42 30 5	N·	24 26 27 27 26 30 23 21	55 E. 49 46 40 39 41 46 37	157 502 479 761 591 62 325 30	48 153 146 233 180 19 99
FRANCE							
Aurillac Bordeaux. Brest. Charleville Chateaureaux. Cherbourg. Dijon. Dunkerque. Gap. Havre Lyon. *Marseille. Mont Blanc (Des Bosses) Mont Ventoux. Nancy. *Nantes. Nice (observatory). *Paris (Parc St. Maur). Pic du Midi. Puy de Dome. Rennes. Toulouse.	44 44 48 49 46 47 51 44 49 45 44 48 47 43 44 48 42 45 48 43	56 50 23 46 49 39 19 2 34 29 41 18 59 10 42 15 43 44 48 56 46 7	N.	2 0 4 4 1 1 5 2 6 0 4 5 6 6 1 7 2 0 2 1 1	26 E. 42 W. 30 43 E. 41 38 W. 2 E. 22 5 6 47 23 51 17 11 34 W. 18 E. 30 8 8 58 41 W. 27 E.	2247 243 210 476 512 59 781 52 2425 102 981 246 14301 6234 718 121 1138 164 9380 4813 105 636	685 74 64 145 156 18 238 16 739 75 4359 1900 219 37 347 50 2859 1467 32 194
GERMANY Berlin Bremen	5 ² 53	31 5	N.	13	22 E. 47	184 52	56 16

GERMANY	Latitude	Longitude from Greenwich	Heigh	t
(Continued) Breslau. Brocken. Cassel. Cologne. Dresden. Flensburg. Frankfort on the Main. Freiburg. *Hamburg. Königsberg Koslin. Leipzig. Munich. Münster. Nuremberg. Osterode. *Potsdam. Schneekoppe. Stettin. Stuttgart. Trier Zugspitze.	51° 7′ N. 51 48 51 20 50 56 51 4 54 47 50 7 47 59 53 33 54 43 54 12 51 20 48 9 51 58 49 27 53 42 52 23 50 44 53 26 48 47 49 25 47 25	17° 5' E. 10 37 9 31 6 57 13 44 9 27 8 39 7 51 9 58 20 30 16 11 12 23 11 34 7 37 11 3 19 58 13 4 15 44 14 34 9 10 6 39 10 59	Feet 397 3785 659 184 361 52 394 912 131 75 151 404 1726 210 1020 367 279 5282 85 883 486 9718	m. 121 1153 201 56 110 16 120 278 40 23 46 123 526 64 311 112 85 1610 26 269 148 2962
GREECE Adrianople. *Athens. Corfu. Mitylene. Naxos. Patras. Salonika. Tripolitza.	4I 40 N. 37 58 39 37 39 6 37 6 38 I5 40 34 37 3I	26 38 E. 23 43 19 57 26 34 25 23 21 45 22 59 22 23	279 351 108 131 13 134 230 2182	85 107 33 40 4 41 70 665
HUNGARY *Budapest Debreczen Nagy-Kanizsa Szeged	47 31 N 47 23 46 28 46 15	. 19 1 E. 21 38 17 0 20 9	426 423 535 312	130 129 163 95
ITALY Avellino Bari Belluno Bologna Catanzaro Chieti Fiume Florence Genoa Lecce Livorno Milan Naples Perugia	40 55 N 41 8 46 9 44 30 38 55 42 21 45 20 43 46 44 25 40 21 43 33 45 28 40 52 43 7	. 14 48 E. 16 52 12 23 11 18 16 36 14 10 14 24 11 15 8 56 18 10 10 18 9 9 14 18 12 21	1214 39 1325 180 1312 1119 79 164 69 256 10 482 489 1617	370 12 404 555 400 341 24 50 21 78 3 147 149

ITALY	Lat	itude		fr	gitud om enwic		Heig	ht
(Continued) *Rome (U. C. M.)	41°	53′ 1	V.	12°	29'	E.	Feet 167	m. 51
Trento. Trieste. Turin. Venice.	46 45 45 45	4 39 4 26		11 13 7 12	17 46 41 20		1024 26 906 82	312 8 276 25
JUGOSLAVIA								
Banjaluka. Belgrade Bjelašnica. Kupres. Laibach. Maribor. Monastir. Ragusa Sarajevo Sebenico. Vranje.	44 44 43 44 46 46 41 42 43 43 42	46 1 48 42 0 3 34 1 38 52 43 33	V	17 20 18 17 14 15 21 18 18 15 21	12 27 15 17 30 39 23 7 26 54 54	E.	535 453 6781 3904 1004 886 2034 59 2090 16	163 138 2067 1190 306 270 620 18 637 5
LATVIA		,				Б		
Libau Riga	56 56	31 I 57	N.	21 24	6	E.	20 43	6
LITHUANIA Kaunas	54	55 1	N.	23	56	E.	282	86
MEDITERRANEAN ISLANDS								
Ajaccio (Corsica). Cagliari (Sardinia). Candia (Crete). Messina (Sicily). *Nicosia (Cyprus). Palermo (Sicily). *Palma (Mallorca) Sassari (Sardinia). Syracuse (Sicily).	41 39 35 38 35 38 39 40 37 35	55 1 12 19 12 9 7 34 33 3 53	N.	8 9 25 15 33 13 2 8 15	44 5 9 31 22 19 39 33 13 30	E.	52 240 108 164 522 233 75 735 75 185	16 73 33 50 159 71 23 224 23 56
NETHERLANDS								
Amsterdam. *De Bilt. Groningen. Rotterdam.	52 52 53 51	23 1 6 13 54	N.	4 5 6 4	55 11 33 29	E.	7 10 7 13	2 3 2 4
NORWAY Aasberg*Alesund	60 62	28	N.	8 6	26 10	Е.	2982 20	909 6
Alten. *Bergen. *Bodö. Brönö. Dovre. Ingoy. Mandal.	69 60 67 65 62 71 58	58 24 17 28 5 4		23 5 14 12 9 24 7	15 19 26 12 7 6 27		33 144 56 16 2113 26	10 44 17 5 644 8

NORWAY	Latitude		fr	gitude om nwich	Heig	ht
(Continued)					Feet	m.
*MehavnOsloTromso*Trondhjem*Vardo	69 3 63 2	1' N. 5 9 6 2	27° 10 18 10 31	47' E. 43 57 25 8	33 82 374 194 46	10 25 114 59 14
POLAND Bialystok Cracow. Lemberg. Nowyport (Neufahrwasser) Posen. Sarny. Vilna. *Warsaw.	49 5 54 2 52 2 51 2 54 4	8 N. 4 30 24 25 22 41 3	23 19 24 18 16 26 25 21	o E. 58 1 40 56 34 15 3	463 725 1093 36 299 518 446 295	141 221 333 11 91 158 136 90
PORTUGAL Coimbra Lagos *Lisbon Montalegre Oporto Serra da Estrella	37 38 4 41 4	2 N. 6 3 9 9	8 8 9 7 8 7	25 W. 38 9 45 34 33	459 43 312 3369 328 4547	140 13 95 1027 100 1386
RUMANIA Baia Mare. Braila. Brasov. *Bucharest. Cernauti. Cluj. Constanta. Craiova Iasi. Sinaia. Sulina. Timisoara.	45 1 45 3 44 2 48 1 46 4 44 1 47 1 45 2 45	88 N. 66 89 55 76 61 90 91 91	23 27 25 26 25 23 28 23 27 25 29 21	35 E. 58 36 6 26 35 39 48 29 34 40 17	741 39 1870 269 738 1191 13 361 328 2822 7 299	226 12 570 82 225 363 4 110 100 860 2 91
SPAIN Albacete. Badajos. Barcelona. Burgos. Cadiz. Ciudad Real. Coruña. Granada. *Madrid. Malaga. Murcia. Oviedo. Pamplona Salamanca. San Sebastian.	41 2 42 2 36 3 8 5 43 2 37 1 40 2 36 4 37 5 43 4 42 4	0 N. 54 23 32 59 23 11 24 43 59 23 49 58	1 6 2 3 6 3 8 3 3 4 1 5 1 5 1	51 W. 58 10 E. 42 W. 18 56 23 36 41 25 8 49 40 40 59	2251 640 138 2822 33 2060 82 2260 2188 131 197 800 1519 2661 75	686 195 42 860 10 628 25 689 667 40 60 244 463 811 23

SPAIN		Latitude		gitude rom enwich	Heig	rht
(Continued)					Feet	
Seville Soria. Teruel. Tortosa. Valencia. Zaragoza.	37° 41 40 40 39 41	23' N. 40 21 49 28 39	5° 2 1 0 0	59′ W. 29 7 30 E. 23 W. 53		m. 30 1058 919 50 18 237
SWEDEN				_		
Abisko. Göteborg. *Haparanda. Harnosand Jönköping. Kalmar. Karlstad. Stensele. Stockholm. Storlien Sveg. *Uppsala.	68 57 65 62 57 56 59 65 63 62 59	21 N. 42 50 38 47 40 23 4 21 19 2 51	18 11 24 17 14 16 13 17 18 12 14	49 E. 58 9 57 10 22 30 10 4 6 19 38	1273 52 30 30 322 33 174 1076 144 1975 1191 79	388 16 9 9 98 10 53 328 44 602 363 24
SWITZERLAND						
Basel. Bern. Chaumont. Davos Platz. Geneva. Lugano. Pilatus Kulm Säntis. *Zurich.	47 46 47 46 46 46 46 47 47	33 N. 57 1 48 12 0 59 15 23	7 7 6 9 6 8 8 9	35 E. 26 59 49 9 57 16 20 33	909 1877 3697 5121 1329 906 6785 8202 1617	277 572 1127 1561 405 276 2068 2500 493
TURKEY						
Istanbul (Constantinople)	41	2 N.	28	47 E.	423	129
UNION OF SOVIET SOCIALIST REPUBLICS Alexandrovsk. *Archangel. *Astrakhan. Baku, Transcaucasia. Batum, Transcaucasia. Bezenchuk. Divnoe. Dnepropetrovsk, Ukraine. Erivan, Transcaucasia. Gandzha, Transcaucasia. Genichesk, Ukraine. Kandalaksha Kanin Nos. Kargopol. *Kazan Kem. *Kharkov, Ukraine.	69 64 46 40 41 52 45 48 40 41 46 67 68 61 55 64 50	12 N. 34 21 21 39 59 51 27 10 40 11 8 39 47 57 0	33 40 48 49 41 49 43 35 44 46 34 32 43 38 49 34 36	28 E. 33 2 50 38 29 21 4 30 21 50 26 18 57 8 39 14	105 20 —66 30 11 154 230 276 3253 1450 11 49 158 262 33 459	32 6 —20 9 3 47 70 84 992 442 3 15 48 80 10

UNION OF SOVIET SOCIALIST REPUBLICS	Latitude	Longitude from Greenwich	Height	
Kharlovka *Kiev, Ukraine Kislovodsk Krasnodar *Leningrad *Lenkoran, Transcaucasia Lugansk, Ukraine *Moscow Nizhnii Novgorod *Novorossiisk *Odessa, Ukraine Okseno *Orenburg Padani Penza Petrovsk Petrun Rostov on the Don *Saratov Sevastopol, Ukraine Stalingrad Sura *Tiflis, Transcaucasia Troitskoe Pechorskoe Ufa Uman, Ukraine Ust Sisolsk *Ust Tsylma Vasilevitchi Velikie Luki Velikie Luki Velikii Ustyug Vishnii Volochek Vitebsk, White Russia Vologda Voronezh Vyatka Zhizdra ASIA	46 26 67 35 51 45 63 15 53 11 42 59 66 28 47 12 51 32 44 37 54 47 48 42 63 35 41 43 62 42 53 44 43 65 26 66 28 67 35 40 46 57 35 56 21 60 46 57 35 57 35	37° 22′ E. 30 30 42 42 38 59 36 54 30 16 48 51 39 20 44 16 27 33 37 49 30 46 52 11 555 6 33 15 45 1 47 30 60 35 39 41 46 2 33 32 32 4 44 31 45 38 44 48 56 13 55 56 30 13 50 51 52 10 29 48 30 31 46 18 34 34 30 11 44 41 39 50 39 13 49 40 34 44	600 2718 134 23 28 —66 210 49 656 2548 1540 122 141 359 416 734 25 21 430 82 822 213 207 1327 338 631 708 403 264 439 354 228 534 4426 2263 458 523 590	112 183 228 411 7 9 200 644 1150 667 665 337 43 631 225 227 224 80 123 124 125 126 123 126 127 128 130 140 150 160 160 160 160 160 160 160 16
AFGHANISTAN Kabul*Seistan	. 01	N. 69 9 E 61 50		760 610
ARABIA *Aden Bahrein Koweit Muscat.	. 26 I5 . 29 20	N. 45 3 E 50 30 48 0 58 35	. 94 18 3 20	27 5 1 6

Meteorological Office for 1922. (London, 1929.)								
	Latitude	Longitude from Greenwich	Heig	ht				
CHINA			Feet	m.				
*Amoy Batang Changsha Chefoo Chengku Chengtu Chungking Foochow Fukow Hangchow *Hankow *Hongkong Ichang Kiukiang Kiukiang Kiungchow Kweilin Kweiyang Lungchow Nanking Ningyuenfu Pakhoi Peiping (Peking) Samshui (Canton) *Shanghai (Zikawei) Silung Silung Siwantse Sunchow Szengenfu Taiyuanfu Tatungfu *Tengueh *Tientsin	24° 27′ N. 30° I 28° 12 37° 33 30° 38 29° 34 25° 59 34° 9 30° 11 30° 355 22° 18 30° 42 25° 58 29° 45 20° I 25° 19 26° 18 22° 22 32° 5 27° 555 21° 59 39° 54 23° 6 31° 12 24° 27 40° 58 23° 17 23° 22 37° 53 36° 19 40° 7 24° 45°	99 3 112 47 121 22 107 20 104 2 106 31 119 27 114 30 120 12 114 17 114 10 111 16 114 46 116 8 110 16 110 22 106 40 106 45 118 49 102 18 109 7 116 30 112 53 121 26 105 30 115 18 109 59 108 2 112 29 115 12 113 13 98 14	13 6562 197 10 2000 1700 755 66 33 118 105 1699 66 33 3527 52 16 361 33 23 3828 3051 4690 5357	4 2000 60 3 610 518 230 20 10 36 32 518 20 10 1075 16 10 7 116 930 116 117 118 119 				
Tsingtao.	39 9 36 4	117 11	16 253	5 77				
WenchowYunnanfu	28 1	120 40	10	3				
	25 2	102 41	0211	1893				
EASTERN TURKESTAN Kashgar	39 30 N.	75 53 E.	4255	1297				
	39 30 N.	75 53 E.	4255	1297				
FRENCH INDO-CHINA Battambang Cape Padaran Honba Kampot Laokay Luang Prabang *Nhatrang Phnom Penh Phongsaly *Phu Lien *Saigon Savannakhet Stungtreng Tourane (Tientcha) Vien-tiane Vinh.	13 5 N. 11 35 12 5 10 37 22 30 19 50 12 15 11 32 21 41 20 48 10 47 16 31 13 28 16 8 17 59 18 38	103 10 E. 109 8 108 45 104 11 103 57 102 4 109 12 104 52 104 52 106 38 106 42 104 42 105 59 108 18 102 33 105 39	581 4869 305 1050 13 43 4619 381 36 426 509 	177 1484 93 320 4 13 1408 116 11 130 1555 6				

	Latitude	Longitude from Greenwich	Heigl	nt
INDIA Ahmadabad. *Akyab. *Allahabad. *Bangalore *Bombay. *Calcutta *Cherrapunji Chittagong. *Cochin. *Colombo, Ceylon. Cuttack. Dalbandin, Baluchistan. *Darjeeling. Delhi. Dera Ismail Khan. Fort Sandeman, Baluchistan. Gangtok, Sikkim *Gauhati. Gilgit. Hyderabad, Deccan. Hyderabad, Sind. Indore. *Jacobabad. *Jaipur. Jhansi. Kalat, Baluchistan. *Karachi. Katmandu, Nepal. *Kodaikanal *Lahore. Lashio. *Leh. Lucknow. *Madras. *Mandalay Mergui. Mukteswar Myitkyina. Mysore *Nagpur Negapatam. *Nuwara Elija, Ceylon. Panjgur, Baluchistan. Pasni, Baluchistan. *Rangoon. Sambalpur Sibsagar *Simla Srinagar. *Trincomali, Ceylon.	23° 2′ N. 20 11 25 25 12 59 18 54 23 36 25 15 22 21 9 58 6 54 20 48 28 57 27 3 28 39 31 51 31 21 27 20 26 8 35 56 17 20 25 23 22 44 28 17 26 56 25 27 29 1 24 53 27 43 10 14 31 34 22 55 34 10 26 55 13 4 21 59 12 27 29 19 25 34 110 46 6 59 26 57 25 14 20 42 34 2 18 31 30 13 16 43 21 28 26 59 31 6 31 7 33 6	72° 38′ E. 92° 56 81° 51 77° 38 72° 49 88° 23 91° 42 90° 53 76° 27 79° 53 85° 54 64° 30° 88 41 74° 21 78° 30° 68 24 75° 50° 68 29 75° 52 78° 37 66° 57 85° 21 77° 28 80° 59 75° 52 78° 37 66° 57 85° 21 77° 42 80° 59 75° 50° 77 42 80° 59 80° 14 96° 0 98° 35 79° 38 97° 16 64° 22 79° 53 80° 46 64° 27 79° 53 80° 46 64° 28 63° 30° 83 10° 71° 37 73° 55 66° 13 84° 11 94° 41 77° 8 74° 51	Feet 163 20 309 3021 37 20 4309 87 9 24 80 2772 7432 718 590 4614 5760 196 4890 1719 96 1821 186 1431 824 6630 13 4388 7688 702 2820 11503 368 22 250 66 7592 463 2518 1017 31 6188 3177 10 179 1113 1846 5502 18 486 332 7232 5204	m. 50 6 94 921 11 6 1314 26 3 7 24 845 2265 219 180 1406 1756 60 1490 524 29 555 57 436 251 2021 4 1337 2343 214 860 3506 112 7 76 20 2314 141 767 310 9 1886 968 3 55 339 563 1677 5 148 101 2204 1586

Meteorological Office for 1922. (London, 1929.)						
	La	Latitude		ngitude rom enwich	Height	
IRAQ (MESOPOTAMIA)					Feet	
*Bagdad Basra Mosul JAPAN	33° 30 36	21' N. 25 22	44° 47 43	28' E. 50 14	106 10 869	m. 32 3 265
Hakodate Hiroshima Ibukasan.	41 34 35	47 N. 23 25	140 132 136	43 E. 27 24	13 10 4514	4 3 1376
Kanazawa. Kobe. *Kyoto. Matumoto. *Miyako. Miyazaki.	36 34 35 36 39 31	32 41 1 14 38 55	136 135 135 137 141 131	39 11 44 59 59 26	92 190 141 1909 98 26	28 58 43 582 30 8
*Nagasaki. *Naha. Naze *Nemuro. Niigata	32 26 28 43 37	44 13 23 20 55	129 127 129 145 139	52 41 30 35 3	436 26 13 89 85	133 8 4 27 26
Onahama Otiai, Sakhalin. Sakai. Sapporo *Syana, Kurile Islands.	36 47 35 43 45	56 20 33 4 14	140 142 133 141 147	54 47 14 21 53	20 89 10 56 128	6 27 3 17 39
*Taihoku, Taiwan. Tainan, Taiwan. *Tokyo. Tukubasan.	25 23 35 36	2 0 41 13	121 120 139 140	31 13 46 6	30 46 20 2854	9 14 6 870
KOREA (CHOSEN) Gensan. Husan	39 35	11 N.	127	26 E.	118 39	36 12
*Jinsen (Chemulpo). Mokpo Ryuganpo. Tyukotin.	37 34 39 41	29 47 56 47	126 126 124 126	37 20 22 53	226 92 20 1030	69 28 6 314
*Yuki MALAY PENINSULA	42	40	130	24	210	64
Kuala Lumpur. Malacca. *Penang Rhododendron Hill. *Singapore.	3 2 5 4 1	9 N. 14 34 28 18	101 102 100 101 103	41 E. 14 20 23 51	320 23 16 5120 36	98 7 5 1561
MANCHURIA			0	3-	3,0	
Changchun Dairen. Harbin Khailar *Mukden. Tsitsihar.	43 38 45 49 41 47	55 N. 54 46 14 48 10	125 121 126 119 123 123	18 E. 38 50 43 23 49	709 315 482 2028 144 499	216 96 147 618 44 152
MONGOLIA						
Chabernoor Sungshutsuitze	40 41	31 N. 23	111 120	42 E. 57	2854 328	870 100

	La	Latitude Longitude from Greenwich			Heig	yht		
PALESTINE							Feet	m.
Haifa Jericho. Jerusalem Kasr Hadschla. Tiberias.	32° 31 31 31 32	48° 51° 47° 50° 47°	N.	34° 35 35 35 35 35	59' E. 27 13 30 32		33 820 2487 1083 -653	10 250 758 —330 —199
PERSIA								
*Bushire Ispahan. *Jask. Kerman. Kermanshah. *Meshed. *Tehran.	28 32 25 30 34 36 35	59 38 44 30 18 16 41	N.	50 51 57 57 47 59 51	53 E 36 47 0 4 35 25		14 5817 13 4934 3104 4002	4 1773 4 1504 946 1220
SIAM					**			
Bandon. Bangkok. Bang Nara. Chantaboun. Chiengmai Chiengrai. Konken. Korat. Nakon Sawan. Nan. Pitsanoulok.	9 13 6 12 18 19 16 14 15 18	3 43 25 35 45 55 28 57 41 46 48	N.	95 100 101 102 98 99 102 102 100 100	20 E. 25 51 5 53 51 39 4 2 44 7		9 1003 105 48	306 306 32
SYRIA								
*Beirut. Deir-es-Zor Ksara Muslimie. Palmyre.	33 35 33 36 34	45 18 49 22 34	N.	35 40 35 37 38	28 E. 2 35 2 3		659 3028 1483 1325	34 201 923 452 404
ТІВЕТ								
Gartok Gyantse Pharijong	31 28 27	45 55 39	N.	80 89 89	20 E. 33 14	1	5100 3110 4400	4602 3996 4389
TURKEY					0 15			-0
Adana. Angora. Diarbekr. Erzerum Sinope. Smyrna.	36 39 40 39 42 38	58 58 25 55 1 27	N.	35 32 37 41 35 27	18 E. 48 50 17 19		125 2825 2346 6345 59 115	38 861 715 1934 18 35
UNION OF SOVIET								
SOCIALIST REPUBLICS *Akmolinsk Aktiubinsk *Alma Ata Anadyr	51 50 43 64	12 17 16 45	N.	71 57 76 177	23 E. 15 53 33	1	731 2760 74	353 223 841 23

Meteorological O		(20114011) 19	29.7	
UNION OF SOVIET SOCIALIST REPUBLICS	Latitude	Longitude from Greenwich	Heig	ht
Askabad. Ayan. Barguzin. *Barnaul. *Beresov. Bering Island. *Blagovyeschensk. Bodaibo. Bokhara Bratskii Ostrog Bulun. *Cherdyn. Cherdyn. Cherniaeva. Chimbai. *Chita. *Dickson. Ekimchan. Elgjai. *Fort Alexandrovsk. Guriev. *Irkutsk. Kazache. Kharborovsk. Khatanga. *Kirensk. Kizil Orda. Kolpashevo. Koziravskaia. *Krasnoyarsk. Kurgan. Markovo. *Minusinsk. Mogocha. Morre Salle. Muraviev Amurski Nagornii Priisk Naiakhan. *Nikolaievsk on the Amur Nizhne Kolymsk. Novi Port. *Obdorsk. Ola. Olekminsk. *Omsk. *Perm. *Petropavlovsk. Russkoe Uste Sagastyr. Semipalatinsk. Sovetskaia Gavan Sredne Kolymsk *Surgut. *Sverdlovsk (Ekaterinburg)	37° 57′ N. 56° 28° 53° 27° 56° 53° 20° 63° 56° 55° 12° 50° 16° 57° 56° 39° 43° 56° 44° 70° 45° 60° 24° 42° 56° 52° 2° 47° 42° 56° 52° 2° 47° 42° 56° 53° 46° 44° 31° 47° 7° 52° 17° 70° 45° 48° 28° 71° 32° 57° 47° 44° 51° 58° 18° 55° 55° 64° 45° 53° 44° 44° 51° 58° 18° 55° 55° 64° 45° 55° 55° 64° 45° 55° 55° 64° 45° 55° 55° 64° 45° 55° 55° 64° 45° 55° 55° 64° 45° 55° 55° 64° 45° 55° 55° 64° 45° 55° 55° 64° 45° 55° 55° 64° 45° 55° 55° 64° 45° 55° 55° 64° 45° 55° 55° 66° 66° 70° 71° 73° 73° 73° 73° 73° 73° 73° 73° 73° 73	58° 23′ E. 138 17 109 38 83 47 65 4 165 59 127 30 114 13 64 33 101 50 127 47 156 31 126 0 59 46 113 30 80 23 132 58 116 56 50 16 51 55 104 20 135 58 135 3 102 9 108 7 65 27 82 55 159 38 52 59 92 51 65 19 170 50 91 41 119 47 66 48 133 38 125 0 91 41 119 47 66 48 133 38 125 0 91 41 119 47 66 48 133 38 125 0 91 41 119 47 66 48 133 38 125 0 91 41 119 47 66 48 133 38 125 0 91 41 119 47 66 48 133 38 125 0 91 41 119 47 66 48 133 38 125 0 91 41 119 47 66 48 133 38 125 0 91 41 119 47 66 35 149 43 160 59 72 57 66 35 143 17 151 13 120 26 73 23 56 15 158 39 149 26 126 35 149 26 126 35 149 26 127 151 50 158 39 149 26 126 35 158 39 149 26 127 154 50 73 24 160 38	Feet 716 33 161 519 131 17 467 729 66 685 693 2254 75 1558 443 —77 —70 1531 46 181 230 935 426 256 —19 518 252 66 965 2038 46 220 95 69 16 16 502 352 535 444 20 16 502 352 535 444 20 16 776 76 76 99 131 922	m. 218 10 49 158 40 5 142 20 209 211 687 23 475 135 —23 475 135 —21 467 14 555 70 285 130 78 —6 158 77 20 294 621 14 67 29 21 5 5 5 5 5 5 153 107 163 13 6 5 237 17 30 40 281

UNION OF SOVIET SOCIALIST REPUBLICS	Latitude	Longitude from Greenwich	Heigh	t
(Continued) *Tashkent. *Tobolsk. *Tomsk. Turgai. Turkestan. *Turukhansk. Uralsk. Ust Maiskoe Ust Yeniseisk Verkhne Inbatskoe Verkhne Tamborskoe. *Verkhoiansk. *Viluisk. *Vladivostok. *Yakutsk. *Yeniseisk. Zaisan.	41° 20′ N. 58 12 56 30 49 38 43 18 65 55 51 15 60 25 69 38 63 7 50 40 67 33 63 45 43 7 62 1 58 27 47 28	69° 18′ E. 68 14 84 54 63 27 68 17 87 37 51 17 134 29 84 22 88 1 137 20 133 34 121 35 131 55 139 43 92 10 84 51	Feet 355 398 427 279 131 112 581 79 98 328 95 358 254 2139	m. 108 121 131 85 40 34 177 24 30 100 29 109 77 652
MALAY ARCHIPELAGO EAST INDIES *Amboina. Balikpapan. Bandoeng. *Batavia. Buitenzorg. *Dobo. Finschhafen. Hollandia. Kalisat. *Kupang. Konstantinhafen. Macasser. *Manokwari. *Medan. *Menado. *Padang. Pangerango. *Pasuruan. *Pontianak. *Port Moresby. *Samarai. *Sandakan. Tosari.	3 42 S. 1 15 6 54 6 11 6 35 9 43 5 14 6 33 2 32 8 2 10 16 5 29 5 5 0 52 3 35 N. 1 30 0 56 S. 6 44 7 38 0 1 9 29 10 37 5 50 S.	124 50 100 22 107 2 112 55 109 20 147 9 150 40	13 16 2395 26 787 26 16 3609 148 7 62 82 30 23 9908 16 10 130 49 105 5692	4 5 730 8 240 8 5 1100 45 2 19 25 9 7 3020 5 3 39 15 32 1735
PHILIPPINE ISLANDS Aparri. Baguio. Dagupan. Davao. Iloilo. *Iwahig. Legaspi. *Manila. *Surigao. Tacloban. *Tagbilaran. Zamboanga.	16 25 16 3 7 I 10 42 9 44 13 9 14 35 9 48 11 15 9 38	121 38 E. 120 35 120 20 125 35 122 34 118 38 123 45 120 59 125 29 125 0 123 51 122 5	13 4961 16 10 20 43 13 46 20 10 69	4 1512 5 3 6 13 4 14 6 3 21 3

meteorological office for 1922.						
AFRICA	La	titude	f	ngitude rom enwich	Hei	ght
AFRICA					70	
Adis Abeba. Gambela. Harrar.	9° 8 9	2' N. 15 , 42	38° 34 42	45' E. 35 30	Feet 8005 1345 6089	m. 2440 410 1856
ALGERIA						
Adrar. *Algiers (Bouzareah) Algiers (Hotel de Ville) Biskra. *Colomb Bechar. Constantine. El Golea. Fort National Geryville. In Salah. La Calle. Laghouat. Oran. Ourgla. Sidi-bel-Abbès. Tamanrasset Tebessa. Touggourt.	27 36 36 31 36 30 36 33 27 36 33 35 31 35 22 35	28 N. 48 37 51 38 22 33 38 41 17 54 48 42 55 12 36 25 6	3 3 5 2 6 3 4 1 2 8 2 0 5 8 6	5 W. 2 E. 4 4 4 13 W. 37 42 12 0 27 26 53 39 16 E. 38 W. 26 E. 7 4	459 1129 125 410 2523 2165 1293 3091 4331 984 33 2464 174 515 1562 4350 2831 226	140 344 38 125 769 660 394 942 1320 300 10 751 53 157 476 1380 863 69
ANGLO-EGYPTIAN SUDAN *El Fasher. *El Obeid. Gallabat. *Khartoum. *Malakal. Merowe. **Mongalla. *Port Sudan. Wadi Halfa. *Wau.	13 13 12 15 9 18 5 19 21	32 N. 11 48 37 35 29 11 37 55 42	25 30 36 32 31 31 31 37 31 28	18 E. 14 10 33 37 50 47 13 19 3	2395 1867 2500 1280 1293 837 1470 20 413	730 569 762 390 394 255 448 6 126 440
ANGOLA *Loanda. Lobito. Luimbale. Malanje. *Mossamedes Omupanda São Salvador	8 12 11 9 15 17 6	49 S. 19 50 30 12 8 20	13 13 15 16 12 15	13 E. 36 0 9 54 47	167 59 5413 3776 39 3445 1844	51 18 1650 1100 12 1050 562
BECHUANALAND Palapye Road Tsau	22 20	33 S.	27 22	10 E. 30	3011	918
BELGIAN CONGO Avakubi. Banana. Barumbu. Bolobo.	I 6 I 2	20 N. o S. 20 N. II S.	27 12 23 16	35 E. 27 30 17	1968 7 1083	600 2 330

Note.—Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

BELGIAN CONGO	Latitude	Longitude from Greenwich	Height
(Continued) Eala *Elisabethville Lula Mahagi Nyangwe Usumbura	11° 39′ S. 2 53	18° 21' E. 27 28 20 25 31 1 26 14 29 20	Feet m. 1181 360 4055 1236 2789 850 1900 579 2625 800
CAMEROONS Duala Ebolowa. Jaunde. Molundu.	4 3 N. 2 55 3 3 ² 2 2	9 41 E. 11 10 11 32 15 13	26 8 2100 640 2395 730 1181 360
EGYPT *Alexandria *Aswan. Cairo (Ezbekiya). Dakhla Oasis. *Helwan. Port Said. *Siwa. Suez. *Tor.	31 12 N. 24 2 30 3 25 29 29 52 31 16 29 12 29 56 28 14	29 53 E. 32 53 31 15 29 0 31 20 32 19 25 29 32 33 33 37	105 328 100 66 20 328 100 381 116 13 4 -75 -23 10 3 7
ERITREA Asmara	15 21 N. 15 37	38 56 E. 39 27	7782 2372 64 20
FRENCH EQUATORIAL AFRICA *Brazzaville Libreville Loango. Ste. Croix	4 17 S. 0 23 N. 4 39 S. 1 44	15 16 E. 9 26 11 48 10 21	951 290 115 35 164 50 640 195
FRENCH WEST AFRICA Bobo Dioulasso. Dakar. Grand Bassam, Ivory Coast. Kaedi. Kayes. Kissidougou *Konakry. Koroko. Lome, Dahomey. Porto Novo, Dahomey. St. Louis. Sansane Mangu, Dahomey. Sedhiou. *Segu-Sikoro. Sokode, Dahomey. *Timbuktu. Toumodi, Ivory Coast. Waghadugu.	11 10 N. 14 40 5 12 16 9 14 26 9 11 9 31 9 27 6 7 6 28 16 2 10 21 12 42 13 26 8 58 16 46 6 33 12 22	4 19 W. 17 25 3 45 13 30 11 26 10 6 13 43 5 7 1 13 E. 2 41 16 30 W. 0 30 E. 15 33 W. 6 18 1 10 E. 3 2 W. 5 1 1 34	1476

SMITHSONIAN TABLES

	Lat	itude	fr	gitude om enwich	Height	
GAMBIA		and the second s			Feet	m.
Bathurst *McCarthy Island	13°	27' N. 32	16° 14	34′ W. 46	7 16	2 5
GOLD COAST COLONY *Accra Axim Coomassie Tamale	5 4 6 9	33 N. 42 41 23	0 2 I 0	12 W. 14 37 52	60 20 900 600	18 6 274 183
KENYA COLONY Fort Hall. Kisumu. *Lamu. Limoru. Masongoleni. Mombasa. Moyale. *Nairobi.	0 0 2 1 2 4 3 1	43 S. 6 16 7 28 4 31 N. 18 S.	37 34 40 36 37 39 39 36	10 E. 45 50 39 59 42 5	4410 3880 10 7300 50 5450	1344 1183 3 2225 15
LIBERIA Monrovia (Schieffen)	6	11 N.	10	33 W.	25	8
LIBYA Azizia Bengazi Cirene. Misda Tobruk Tripoli	3 ² 3 ² 3 ² 3 ¹ 3 ² 3 ²	32 N. 6 49 39 3 54	13 20 21 13 23 13	1 E. 4 51 1 59	518 82 2067 1345 151 59	158 25 630 410 46 18
MADAGASCAR Antsirane Farafangana Mandritsara Marovoay Morondava *Tamatave *Tananarivo	12 22 15 16 20 18 18	25 S. 53 44 3 15 9	49 47 48 46 44 49 47	20 E. 56 50 42 18 26 33	89 33 945 148 13 4531	27 10 288 45 4 1381
MOROCCO Casablanca. Fes. Marrakech. *Melilla Mogador Oudja. Rabat. Safi. Tangier.	33 34 31 35 31 34 34 32 35	37 N. 0 38 17 29 39 0 18	7 4 7 3 9 1 6 8 5	34 W. 53 59 0 46 54 20 50 52	131 1365 1509 26 36 1821 210 230 148	40 416 460 8 11 555 64 70 45
NIGERIA Calabar Debundja. Forcados.	4 4 5	58 N. 5 23	8 8 5	19 E. 59 26	157 30 4	48 9 1

NIGERIA	Latitude	Longitude from Greenwich	Height	
*Kaduna (Continued) *Kaduna *Lagos Lakoja *Maiduguri *Sokoto *Yola	10° 34′ N. 6 27 7 48 11 47 13 2 9 12	7° 24' E. 3 24 6 44 13 11 5 15 12 30	Feet 2088 6 320 1186 1160 850	m. 637 2 96 361 354 259
NORTHERN RHODESIA Feira Fort Jameson Livingstone Mongu Ndola	15 38 S. 13 45 17 51 15 20 12 55	30 18 E. 32 53 25 51 23 11 28 35	3000 3330	314 1103 914 1015 1262
NYASALAND Fort Johnston Nkata *Zomba	14 31 S. 11 37 15 22	35 14 E. 34 18 35 18	1263 1400 2948	385 427 899
PORTUGUESE EAST AFRICA Beira. Inhambane. *Lourenço Marques. Macequece. Malema Mozambique (Mossouril). Quelimane.	19 50 S. 23 53 25 58 18 56 14 58 14 57 17 53	34 51 E. 35 24 32 36 32 52 37 22 40 40 36 53	30 10 194 2306 2132 49 20	9 3 59 703 650 15 6
PORTUGUESE GUINEA Bolama	11 34 N	. 15 28 W.	16	5
RIO DE ORO Cape Juby	27 57 N	. 12 56 W.		
SIERRA LEONE Daru*Freetown Kaballa	8 o N 8 30 9 34	. 10 53 W. 13 14 11 31	224	68
SOMALILAND *Berbera Giumbo Jibouti Lugh Mogadiscio	0 14 S 11 35 N 3 45	. 42 37	30 98 20 633 59	9 30 6 193 18
SOUTHERN RHODESIA *Bulawayo Gwaai. *Gwelo. Juliasdale. Mt. Selinda. *Salisbury. Tuli. Umtali.	19 30 19 28 18 22 20 28 17 48 21 54	. 28 36 E. 27 45 29 45 32 40 32 41 31 5 29 12 32 41	4440 3620 4650 6670 3520 4865 1754 3670	1353 1103 1417 1850 1073 1483 535 1119

	Latitud	łe	fr	gitude om enwich	Heig	ht
SOUTH WEST AFRICA					174	
Bethany Franzfontein. Gibeon Grootfontein. Luderitz Bay Mt. Brukkaros Swakopmund Warmbad. *Windhuk	26° 30 20 11 25 8 19 33 26 39 25 52 22 41 28 27 22 34	' S.	17° 15 17 18 15 17 18 15	10' E. 46 7 10 48 31 44 5	Feet 3067 3773 3777 5020 13 5202 26 2362 5463	m. 935 1150 1130 1530 4 1586 8 720 1665
TANGANYIKA TERRITORY Bismarckburg. Dar es Salaam. Kondoa Irangi. Lindi. Mahenge. Mwanza. New Langenburg. Tabora. Tandala. Tanga. Ujiji.	8 28 6 49 4 55 10 0 8 41 2 31 9 16 5 1 9 23 5 4 4 55	S.	31 39 35 39 36 32 33 32 34 39 29	8 E. 18 57 44 3 54 38 49 14 7	2658 26 4626 26 3363 3740 5085 4058 6729 92 2690	810 8 1410 8 1025 1140 1550 1237 2051 28 820
TUNIS Bizerte. Dehibat. Metlaoui. Sfax. *Tunis.	37 17 32 3 34 22 34 44 36 48	N.	9 10 8 10	52 E. 43 24 45	33 1066 735 23 105	10 325 224 7 32
UGANDA						
*Entebbe Fort Portal Kitgum Mbale Mbarara	0 4 0 40 3 20 1 6 0 37		32 30 32 34 30	28 E. 17 53 11 39	3850 5300 3000 4000 4800	1173 1615 914 1219 1463
UNION OF SOUTH AFRICA Aliwal North Barberton Beaufort West Bloemfontein *Cape Town Clanwilliam *Durban *East London Graaf Reinet Grahamstown Hlabisa *Johannesburg Kenhart Kimberley Kokstad Komati Poort	30 42 25 47 32 21 29 7 33 56 32 10 29 52 33 1 32 16 33 18 28 8 26 11 29 21 28 44 30 33 25 26	S.	26 31 22 26 18 18 31 27 24 26 31 28 21 24 29 31	40 E. 3 36 13 29 55 3 54 32 32 52 3 9 46 26 56	4330 2885 2850 4518 40 245 20 150 2430 1700 800 5750 2704 4042 4280 620	1320 879 869 1377 12 75 6 46 741 518 244 1753 824 1232 1304 189

Meteorological O	ince for 1922.	(2011217, 7)		
	Latitude	Longitude from Greenwich	Height	
UNION OF SOUTH AFRICA (Continued) Kuruman Lindley. Mafeking. Mossel Bay Newcastle. Ookiep Pietermaritzburg Pietersburg. Port Elizabeth Port Nolloth Pretoria.	34 II 27 45 29 36 29 35 23 54 33 58 29 I4	23° 37′ E. 27 55 25 39 22 9 29 56 17 52 30 32 29 28 25 37 28 12 28 12	Feet 4500 5000 4194 100 3890 3036 2272 4270 176 25 4350	m. 1372 1524 1278 30 1186 925 692 1302 54 8 1326
AUSTRALASIA AUSTRALIA *Adelaide. *Alice Springs. Armidale. Bendigo. *Boulia. *Bourke. *Brisbane. Broken Hill Burketown. Canberra. Cape Leeuwin Carnarvon. Charlotte Waters. Chartertowers. Condon. Cooktown. *Coolgardie. *Daly Waters. *Darwin. *Derby. Dubbo. Esperance. *Georgetown Geraldton. *Halls Creek. Hav. Herberton *Hobart. Isisford. *Katanning. Kiandra. *Launceston *Laverton. *Mein. *Melbourne *Mitchell. *Nullagine. Oatlands. Omeo.	30 32 36 46 22 55 30 13 27 28 31 57 17 46 35 15 34 52 24 54 25 56 20 3 20 0 15 29 30 57 16 16 12 28 33 50 18 22 18 33 50 18 22 17 23 17 9 34 30 17 23 42 53 24 15 33 42 35 52 41 27 228 40 13 13 37 49 26 32 21 53	133 37 151 38 144 17 139 38 145 58 153 2 141 28 139 34 149 15 115 8 113 39 134 55 146 16 119 21 145 14 121 10 133 23 130 51 123 40 148 35 121 55 143 32 144 36 127 46 145 55 144 36 127 46 145 55 144 24 117 35 148 32 147 10 122 23 147 10 122 23 147 10 122 23 147 52 147 52 147 52 147 52 147 52 147 52 147 52 147 52 147 52 147 24	140 1926 3333 758 479 364 137 1000 27 (2000) 163 15 645 1019 35 17 1388 692 98 52 863 14 302 13 1227 55 305 2890 177 -650 1017 4640 33 1529 400 115 1102 1266 1400 2108	43 587 1016 231 146 111 42 305 8 (610) 50 5 197 311 11 5 423 211 30 16 263 4 92 4 374 17 93 881 54 198 310 144 198 310 144 144 154 164 174 185 186 186 187 187 187 187 187 187 187 187

AUSTRALIA	Latitude	Longitude from Greenwich	Height
(Continued) *Onslow Peak Hill *Perth Port Augusta *Rockhampton Springs Stanthorpe *Streaky Bay *Sydney Tennants Creek *Thargomindah Thursday Island Toowoomba Wentworth Wilcannia *William Creek	21° 43′ S. 25° 38 31° 57 32° 29 23° 24 42° 53 28° 36° 32° 48° 33° 52° 19° 32° 27° 58° 10° 36° 27° 34° 34° 8° 31° 31° 28° 55°	114° 57′ E. 118 47 115 50 137 46 150 30 149 19 151 59 134 13 151 12 134 11 143 43 142 14 151 57 141 58 143 23 136 21	Feet m. 13 4 1929 588 197 60 18 5 36 11 2495 760 2656 810 43 13 138 42 1075 328 404 123 17 5 1921 586 144 44 246 75 249 76
Wiluna Wyndham Yalgoo NEW ZEALAND *Auckland *Christchurch	26 37 15 27 28 23 36 50 S. 43 32	120 21 128 7 116 43 174 50 E. 172 39	1700 518 23 7 1044 318 152 46 25 8
*Dunedin. Hokitika. *Invercargill. Rotorua. Taihape. Wellington. ATLANTIC OCEAN, N.	45 52 42 42 46 25 38 9 39 40 41 16	170 31 170 49 168 21 176 15 175 49 174 46	300 12 4 12 4 932 284 2157 10 3
Angra, Azores Is. *Bermuda (Prospect). *Funchal, Madeira I. *Horta, Azores Is. *Izana, Canary Is. *La Laguna, Canary Is. *Ponta Delgada, Azores Is. *Santa Cruz, Azores Is. Santa Cruz, Canary Is. *Santiago, C. Verde Is. *St. Vincent, C. Verde Is.	38 19 N 32 18 32 37 38 32 28 19 28 28 37 44 39 27 28 41 14 54 16 54	. 27 I4 W. 64 46 16 54 28 38 16 30 16 20 25 40 3I 8 17 46 23 3I 25 4	135 41 151 46 82 25 213 65 7766 2367 1795 547 72 22 92 28 39 12 112 34 36 11
ATLANTIC OCEAN, S. *Cape Pembroke, Falkland Is. *Grytviken, South Georgia. *St. Helena	54 13	57 42 W. 36 33 5 40	70 21 13 4 1900 579
INDIAN OCEAN *Christmas Island *Cocos Island Madagascar (see Africa)	10 25 S. 12 5	105 43 E. 96 53	20 6 16 5
*Mauritius *Minicoy *Port Blair *Seychelles *Zanzibar	20 6 8 17 N 11 40 4 37 S. 6 10	92 40	180 55 7 2 59 18 16 5 72 22

Note.—Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

	Latitude		Longitude from Greenwich		Height	
PACIFIC OCEAN, N. *Bonin Islands *Fanning Island *Guam Hilo, Hawaii Holualoa, Hawaii *Honolulu Humuula, Hawaii *Midway Island Ujelang Island Volcano House, Hawaii *Yap PACIFIC OCEAN, S.	27° 3 13 19 19 21 19 28 9 19	5' N. 54 24 44 38 19 43 15 42 26 29	142° 159 144 155 155 157 155 177 161 155 138	11' E. 23 W. 38 E. 3 W. 55 52 26 22 2 E. 16 W. 8 E.	Feet 13 16 66 40 1450 39 6685 20 30 3984 118	m. 4 5 20 12 442 12 2038 6 9 1214 36
*Apia, Samoan Is. *Avarua, Cook Is. Easter Island. Herbertshöhe, Bismarck Arch. *Juan Fernandez Is. *Lord Howe Island. Noumea, New Caledonia. *Ocean Island. Papeete, Tahiti. *Suva, Fiji Is. *Tulagi, Solomon Is.	13 21 27 4 33 31 29 22 0 17 18	48 S. 12 10 20 27 20 4 16 52 32 8 5	171 159 109 152 78 159 167 166 169 149 178	46 W. 47 26 17 E. 50 W. 0 E. 59 27 35 34 W. 26 E. 8	16 20 98 200 1132 16 49 30 177 20 59	5 6 30 61 345 5 15 9 54 6 18
ARCTIC REGION (See also Alaska, Canada, Greenland and Iceland under North America) *Bear Island Fort Conger. *Green Harbor *Jan Mayen. Lyakhorsi Island. Matotchkin Shar Refuge Harbor *Vaigach Island Wrangell Island	74 81 78 70 73 73 77 70 70	28 N. 44 2 59 5 16 32 24 55	19 64 14 8 142 56 72 58 178	17 E. 45 W. 15 E. 18 W. 20 E. 24 73 W. 48 E. 3 W.	125 13 75 36	38 4 23
ANTARCTIC REGION Discovery, McMurdo Sound *Laurie Island Little America Port Charcot Snow Hill	77 60 78 65 64	51 S. 44 36 3 22	166 44 163 63 57	45 E. 39 W. 35 26 0	75 30	23 9

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