# SMITHSONIAN MISCELLANEOUS COLLECTIONS VOLUME 86 (WHOLE VOLUME) <br> SMITHSONIAN METEOROLOGICAL TABLES 

[based on guyot's meteorological and piysical tables]

$$
\begin{gathered}
\text { FIFTH REVISED EDITION } \\
\text { (Corrected to January, 193ı) }
\end{gathered}
$$


(Publication 3116)


CITY OF WASHINGTON
PUBLISHED BY THE SMITHSONIAN INSTITUTION

## SMITHSONIAN

## MISCELLANEOUS COLLECTIONS

VOL. 86

"EVERY MAN IS A VALUABLE MEMBER OF SOCIETY WHO, BY HIS OBSERVATIONS, RESEARCHES, AND EXPERIMENTS, PROCURES KNOWLEDGE FOR MEN"-SMITHSON
(Publication 3215)

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C. G. Abbot,<br>Secretary of the Smithsonian Institution.

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Smithsonian Meteorological Tables. Fifth Revised Edition. (Corrected to January, 193r.) 282 pages. I93I. (Publ. 3II6.) (Whole volume.)

SMITHSONIAN MISCELLANEOUS COLLECTIONS VOLUME 86 (WHOLE VOLUME)

## SMITHSONIAN

## METEOROLOGICAL TABLES

[BASED ON GUYO'T'S METEOROLOGICAL AND PHI'SICAL TABLES]
(Corrected to January, 193I)

(Publication 3116)

The I ord Paltimore J'ress
Paltimore, Md.
printed in the U.S.a.

## ADVERTISEMENT TO FIFTH REVISED EDITION.

The original edition of the Smithsonian Meteorological Tables was issued in 1893, and revised editions were published in 1896. 1897. 1907, and 1918. A fifth revised edition is here presented. which has been prepared under the direction of Charles F. Marvin, Chief of the U. S. Weather Bureau, assisted by Herbert H. Kimball, Senior Meteorologist of the same bureau. Officials of the U . S. Bureau of Standards have been consulted relative to the value of certain physical constants that enter into the calculation of the tables. All errata thus far detected in the earlier editions have been corrected.

The great development in the exploration of the free air to the height of the tropopause and even beyond calls for an extension of some tables to adapt them to the low temperatures and pressures experienced at these great heights, and also for a distinction between the symbols for the acceleration of gravity at the surface of the earth and in the free air. Also, the measurement of heights as " geopotentials" in " dynamic meters" calls for five new tables. The table of international meteorological symbols has been revised, and a table of " International code for horizontal visibility" has been added. Nuch of the work of extension of old tables and the computation of new ones has been done by the Aerological Division of the Weather Bureau.

The complete revision of the "List of meteorological stations," including an alphabetical arrangement by continents. countries, and stations, has been effected by Mr. W. W. Reed of the Climatological Division, U. S. Weather Bureau.

Charles G. Abbot, Secretary.

Smithsonian Institution, March 2I, 1931.

## ADVERTISEMENT TO FOURTH REVISED EDITION.

The original edition of the Smithsonian Meteorological Tables was issued in 1893, and revised editions were published in 1896, 1897, and 1907. A fourth revised edition is here presented, which has been prepared under the direction of Professor Charles F. Marvin, Chief of the U.S. Weather Bureau, assisted by Professor Herbert H. Kimball. They have had at their disposal numerous notes left by the late Professor Cleveland Abbe, and have consulted with officials of the U.S. Bureau of Standards and of other Government bureaus relative to the value of certain physical constants that have entered into the calculation of the tables.

All errata thus far detected in the earlier editions have here been corrected. New vapor pressure tables, derived from the latest experimental values by means of a modification of Van der Waals interpolation formula devised by Professor Marvin, have been introduced. The table of relative acceleration of gravity at different latitudes has been recomputed from a new equation based upon the latest investigations of the U.S. Coast and Geodetic Survey. These values have been employed in reducing barometric readings to the standard value of gravity adopted by the International Bureau of Weights and Measures, supplementing a table that has been introduced for directly reducing barometer readings from the value of gravity at the place of observation to its standard value.

The new values of vapor pressure and of gravity acceleration thus obtained, together with a recent and more accurate determination of the density of mercury, have called for an extensive revision of numerous other tables, and especially of those for the reduction of psychrometric observations, and the barometrical tables.

Among the new tables added are those for converting barometric inches and barometric millimeters into millibars, for determining heights from pressures expressed in dynamic units, tables of gradient winds, and tables giving the duration of astronomical and civil twilight, and the transmission percentages of radiation through moist air.

The tables of International Meteorological Symbols, of Cloud Classification, of the Beaufort Scale of Winds, of the Beaufort Weather Notation, and the List of Meteorological Stations, are among those extensively revised.

Tables for reducing barometric readings to sea level, and tables of logarithms of numbers, of natural sines and cosines, of tangents and cotangents, and for dividing by 28,29, and 3I, with a few others, have been omitted from this edition.

This reprint is from the electroplates that were employed in printing the Fourth Revised Edition, after making certain minor corrections. Charles D. Walcott,

## ADVERTISEMENT TO THIRD REVISED EDITION

The original edition of Smithsonian Meteorological Tables was issued in 1893, and revised editions were published in 1896 and 1897. A third revised edition is here presented, which has been prepared at the request of the late Professor Langley by the coöperation of Professors Alexander McAdie, Charles F. Marvin, and Cleveland Abbe.

All errata thus far detected have been corrected upon the plates, the Marvin vapor tensions over ice have been introduced, Professor F. H. Bigelow's System of Notation and Formulx has been added, the List of Meteorological Stations has been revised, and the International Meteorological Symbols, together with the Beaufort Notation, are given at the close of the volume.

R. Rathbun, Acting Secretary.

## Smithsonian Institution,

December, 1906.

## ADVERTISEMENT TO SECOND REVISED EDITION.

The edition of the Smithsonian Meteorological Tables issued in 1893 having become exhausted, a careful examination of the work has been made, at my request, by Mr. Alexander McAdie, of the United States Weather Bureau, and a revised edition was pullished in 1896, with corrections upon the plates and a few slight changes. The International Meteorological Symbols and an Index were also added.

The demand for the work has been so great that it becomes necessary to print a new edition of the revised work, which is here presented with corrections to date.
S. P. Langley, Secretary.

## Smithsonian Institution, Wasiington City, October 30, 1897.

## PREFACE TO EDITION OF 1893.

In comnection with the system of meteorological observations estab. lished by the Smithsonian Institution about 1850, a collection of meteorological tables was compiled by Dr. Arnold Guyot, at the request of Secretary Henry, and published in 1852 as a volume of the Miscellaneous Collections.

Five years later, in 1857, a second edition was published after sareful revision by the author, and the various series of tables were so enlarged as to extend the work from 212 to over 600 pages.

In 1859 a third edition was published, with further amendments.
Although designed primarily for the meteorological observers reporting to the Smithsonian Institution, the tables obtained a much wider circulation, and were extensively used by meteorologists and physicists in Europe and in the United States.

After twenty-five years of valuable service, the work was again revised by the author; and the fourth edition, containing over 700 pages, was published in 1884. Before finishing the last few tables, Dr. Guyot died, and the completion of the work was intrusted to his assistant, Prof. Whi. Libbey, Jr., who executed the duties of final editor.

In a few years the demand for the tables exlausted the edition, and thereupon it appeared desirable to recast entircly the work. After very careful consideration, $I$ decided to publish the new tables in three parts: Meteorological Tables, Geograpiical Tables, and Physical Tables, each representative of the latest knowledge in its field, and independent of the others; but the three forming a homogeneous series.

Although thus historically related to Dr. Guyot's Tables, the present work is so substantially changed with respect to material, arrangement, and presentation that it is not a fifth edition of the older tables, but essentially a new publication.

In its preparation the advantage of conformity with the recently issued International Meteorological Tables has been kept steadily in view, and so far as consistent with other decisions, the constants and methods there employed have been followed. The most important difference in constants is the relation of the yard to the metre. The value provisionally adopted by the Bureau of Weights and Measures of the United States Coast and Geodetic Survey,

$$
\text { I metre }=39.3700 \text { inches, }
$$

has been used here in the conversion-tables of metric and English linear measures, and in the transformation of all formulæ involving such conversions.

A large number of tables have been newly computed; those taken from the International Meteorological Tables and other official sources are credited in the introduction.

To Prof. Wm. Libbey, Jr., especial acknowledgments are due for a large amount of attention given to the present work. Prof. Libbey had already completed a revision, involving considerable recomputation, of the meteorological tables contained in the last edition of Guyot's Tables, when it was determined to adopt new values for many of the constants, and to have the present volume set with new type. This involved a large amount of new computation, which was placed under the direction of Mr. GEORGE E. Curtis, who has also written the text, and has carefully prepared the whole mannscript and carried it through the press. To Mr. Curtis's interest, and to his special experience as a meteorologist, the present volume is therefore largely due.

Prof. Libbey lias contributed Tables $38,39,55,56,61,74,77,89$, and 90 , and lias also read the proof-sheets of the entire work.

I desire to express my acknowledgments to Prof. Cleveland Abbe, for the manuscript of Tables $32,81,82,83,84,85,86$; to Mr. H. A. Hazen, for Tables 49, 50, 94, 95, 96, which have been taken from his Hand-book of Metcorological Tables; and also to the Superintendent of the United States Coast and Geodetic Survey, the Chief Signal Officer of the Army, and the Chief of the Weather Bureau, for much valuable counsel during the progress of the work.
S. P. LANGLEY,

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## INTRODUCTION.

## DESCRIPTION AND USE OF TABLES.

## THERMOMETRI.

The present standard for exact thermometry is the normal centigrade scale of the constant-volume hydrogen thermometer as defined by the International Bureau of Weights and Measures. The constant volume is one liter and the pressure at the freezing point is one meter of mercury reduced to freezing and standard gravity. The scale is completely defined by designating the temperature of melting ice, $0^{\circ}$, and of condensing steam, $100^{\circ}$, both under standard atmospheric pressure. All other thermometric scales that depend upon the physical properties of substances may by definition be made to coincide at the ice point and the boiling point with the normal scale as above defined, but they will diverge more or less from it and from each other at all other points. However, by international consent it is customary in most cases to refer other working scales to the hydrogen scale.

The absolute or thermodynamic scale. To obviate the difficulty which arises because thermometers of different type and substance inherently disagree except at the fixed points, Lord Kelvin proposed that temperatures be defined by reference to certain thermodynamic laws. This course furnishes a scale independent of the nature or properties of any particular substance. The resulting scale has been variously named the absolute, the thermodynamic, and, more recently, in honor of its author, the Kelvin scale. The temperature of melting ice by this scale on the centigrade basis is not as yet accurately known, but it is very nearly $273^{\circ} \cdot 13$, and that of the boiling point, $373^{\circ} \cdot \mathrm{I} 3$.

Many problems in physics and meteorology call for the use of the absolute scale; but it is not convenient, and in many cases not necessary, to adhere strictly to the true thermodynamic scale. In fact, the general requirements of science will very largely be met by the use of an approximate absolute scale which for the centigrade system is defined by the equation

$$
T=\left(273^{\circ}+t^{\circ} \mathrm{C} .\right)
$$

The observed quantity, $t^{\circ}$, may be referred to the normal hydrogen centigrade scale or be determined by any acceptable thermometric method.

This scale differs from the true Kelvin scale, first, because $273^{\circ}$ is not the exact value of the ice point on the Kelvin scale, second, because each observed value of $t^{\circ}$ other than $0^{\circ}$ or $100^{\circ}$ requires a particular correction to
convert it to the corresponding value on the Kelvin scale. These corrections will differ according to the kind of thermometer used in obtaining the value $t^{\circ}$, and while they are small for temperatures between $0^{\circ}$ and $100^{\circ}$ they are large at extreme temperatures and are important in all questions involving thermometric precision.

Since, however, the approximate absolute scale is sufficiently exact for nearly all purposes, and especially since it is most convenient in computations and in the publication of results, much confusion and uncertainty of terminology and meaning will be obviated if scientists will agree to give the approximate absolute scale a particular name of its own.

For the purpose of these tables the name Approximate Absolute will be employed, and in accordance therewith thermometric scales may be designated as follows:-

Scale. Ice point. Boiling point. Symbol.

| Centigrade | $0^{\circ}$ | $100^{\circ}$ | $C$. |
| :---: | :---: | :---: | :---: |
| Fahrenheit | 32 | 212 | $F$. or Fahr |
| Reaumur | 0 | 80 | $R$. |
| Thermodynamic <br> Absolute <br> Kelvin | $\left\{\begin{array}{l} 273.13 \mathrm{C} . \pm \\ 491.6 \mathrm{~F} . \pm \\ \text { (Names st } \\ \text { one ide } \end{array}\right.$ | $\begin{aligned} & 373.13 \text { C. } \pm \\ & 671.6 \quad F . \pm \\ & y \text { synonymous } \\ & \text { cale.) } \end{aligned}$ | $A$. or $K$ <br> strictly |
| Approximate Absolute | 273 | 373 | A.A. |

Table 1. Conversion of the Approximate Absolute thermometric scale to the Centigrade, Fahrenheit, and Reaumur scales.

The equivalent values of the four scales are given for every degree on the Approximate Absolute scale from $375^{\circ}$ to $0^{\circ}$.

By the help of the table of proportional parts preceding this table, it is also convenient for converting Fahrenheit to Centigrade and Reaumur, and Centigrade to Fahrenheit and Reaumur.

The formulæ expressing the relations between the different scales are also given, in which

$$
\begin{aligned}
A . A^{\circ} .^{\circ} & =\text { Temperature - Approximate Absolute Scale. } \\
C .^{\circ} & =\text { Temperature - Centigrade Scale. } \\
F .^{\circ} & =\text { Temperature - Fahrenheit Scale. } \\
R .^{\circ} & =\text { Temperature - Reaumur Scale. }
\end{aligned}
$$

## Examples:

To convert $285^{\circ} \cdot 5$ Approximate Absolute into Centigrade, Fahrenheit, and Reaumur.
From the table,

$$
285^{\circ} A \cdot A .=12^{\circ} \cdot C=53^{\circ} \cdot 6 F=9^{\circ} \cdot 6 R
$$

From the proportional parts, $\frac{0.5}{285.5 A . A}=\frac{0.5}{12.5 C}=\frac{0.9}{54.5 \mathrm{~F} .}=\frac{0.4}{10.0 R}$

To convert 16.9 Centigrade to Approximate Absolute, Fahrenheit, and Reaumur.
From the table, $\quad 166^{\circ} \mathrm{C}=289^{\circ} \mathrm{A} . \mathrm{A} .=60^{\circ} .8 \mathrm{~F} .=12^{\circ} .8 \mathrm{R}$.
From the proportional parts $-\frac{0.9}{16.9 \mathrm{C} .}=\frac{0.9}{289.9 \mathrm{~A} . \mathrm{A} .}=\frac{1.6}{62.4 \mathrm{~F} .}=\frac{0.7}{13.5 \mathrm{R} .}$
Or,

$$
\begin{aligned}
16^{\circ} .9 \times 2\left(\mathrm{I}-\frac{\mathrm{I}}{\mathrm{IO}}\right)+32 & =33.8 \\
& -3.4 \\
& -\frac{32.0}{62.4} \mathrm{~F}
\end{aligned}
$$

To convert $147^{\circ} 7$ Fahrenheit to Approximate Absolute, Centigrade, and Reaumur.
From the table,

$$
140^{\circ} . F=333^{\circ} \cdot A \cdot A .=60^{\circ} \quad C .=48^{\circ} \cdot R
$$

From the proportional parts $7.7=4.3=4.3=3.4$
$147.7 \mathrm{~F} .=337.3$ A.A $=64.3 \mathrm{C} .=5 \mathrm{I} .4 \mathrm{R}$.

Or, | $\frac{147.7-32.0}{2}\left(\mathrm{I}+\frac{\mathrm{I}}{\mathrm{IO}}+\frac{\mathrm{I}}{100}+\frac{\mathrm{I}}{1000}\right.$ etc. $)$ | $=57.85$ |
| ---: | :--- |
|  | +5.78 |
|  | $+\quad .58$ |
|  | $+\quad .06$ |
| 64.27 C. |  |

Fahrenheit may also be reduced to Approximate Absolute by obtaining its equivalent in Centigrade from Table 2 and adding 273 to the result.

To convert $18^{\circ} .3$ Reaumur to Approximate Absolute, Centigrade, and Fahrenheit.
From the table,

$$
16^{\circ} R .=293^{\circ} \cdot A \cdot A=20^{\circ} C=68^{\circ} \quad F .
$$

Frort the proportional parts, $\frac{2.3}{18.3}=\frac{2.9}{295.9} \mathrm{~A} . \mathrm{A} .=2.9=\frac{5.2}{22.9} \mathrm{C} .=\frac{73.2 \mathrm{~F}}{}$.
Or, $18.3 \times \frac{5}{4}=\frac{91.5}{4}=22.9 \mathrm{C}$., and $\left(18.3 \times \frac{9}{4}\right)+32=\frac{164.7}{4}+32=73.2 \mathrm{~F}$.
Table 2. Conversion of readings of the Fahrenheit thermometer to readings Centigrade.
The conversion of Fahrenheit temperatures to Centigrade temperatures is given for every tenth of a degree from $+130^{\circ} 9 F$. to $-120^{\circ} 9 \mathrm{~F}$. The side argument is the whole number of degrees Fahrenheit, and the top argument, tenths of a degree Fahrenheit; interpolation to hundredths of a degree, when desired, is readily effected mentally. The tabular values are given to hundredths of a degree Centigrade.

The formula for conversion is

$$
C^{\circ}=\frac{5}{9}\left(F^{\circ}-32^{\circ}\right)
$$

where $F^{\circ}$ is a given temperature Fahrenheit, and $C^{\circ}$ the corresponding temperature Centigrade.

## Example:

To convert 79.7 Fahrenheit to Centigrade.
The table gives directly $26^{\circ} .50 \mathrm{C}$.
For conversions of temperatures outside the limits of the table use Table 1.

Table 3. Conversion of readings of the Centigrade thermometer to readings Fahrenheit.

The conversion of Centigrade temperatures to Fahrenheit temperatures is given for every tenth of a degree Centigrade from $+60^{\circ} .9$ to $-90^{\circ} .9 \mathrm{C}$. The tabular values are expressed in hundredths of a degree Fahrenheit.

The formula for conversion is

$$
F^{\circ}=\frac{9}{5} C^{\circ}+32^{\circ}
$$

where $C^{\circ}$ is a given temperature Centigrade, and $F^{\circ}$ the corresponding temperature Fahrenheit.

For conversions of temperatures outside the limits of the table, use Table 1 or 4.

Table 4. Conversion of readings of the Centigrade thermometer near the boiling point to readings Fahrenheit.

This is an extension of Table 3 from 90.0 to $\mathbf{1 0 0 . 9}$ Centigrade.

## Example:

To convert $95^{\circ} \cdot 74$ Centigrade to Fahrenheit.
From the table,
By interpolation,

$$
\begin{aligned}
95^{\circ} \cdot 70 C & =204.26 F \\
\frac{0.04}{95.74} C & =\frac{0.07}{20+.33} F
\end{aligned}
$$

rable 5. Conversion of differences Fahrenheit to differences Centigrade.
The table gives for every tenth of a degree from $0^{\circ}$ to $20^{\circ} .9 \mathrm{~F}$. the corresponding lengths of the Centigrade scale.

Table 6. Conversion of differences Centigrade to differences Fahrenheit.
The table gives for every tenth of a degree from $0^{\circ}$ to $9^{\circ} \cdot 9 \mathrm{C}$. the corresponding lengths of the Fahrenheit scale.

## Example:

To find the equivalent difference in Fahrenheit degrees for a difference of 4.72 Centigrade.
From the table,
From the table by moving the decinal point for 0.2,


TABLES 7, 8.
Tables 7,8. Correction for the temperature of the emergent mercurial columin of thermometers.
When the temperature of the thermometer stem containing a portion of the mercury column is materially different from that of the bulb, a correction needs to be applied to the observed reading unless the instrument has been previously graduated for the condition of use. This correction frequently becomes necessary in physical experiments where the bulb only, or else the bulb with a portion of the stem, is immersed in a bath whose temperature is to be determined. In meteorological observations the correction may become appreciable in wet-bulb, dew-point, and solar-radiation thermometers, when the temperature of the bulb is considerably above or below the air temperature.

If $t^{\prime}$ be the average temperature of the emergent mercury column, $t$ the observed reading of the thermometer, $n$ the length of the mercury in the emergent stem in scale degrees, and a the apparent expansion of mercury in glass for $\mathrm{I}^{\circ}$, the correction is given by the expression

$$
a n\left(t-t^{\prime}\right) \text {, or }-a n\left(t^{\prime}-t\right)
$$

which latter may be the more convenient form when $t^{\prime}$ is greater than $t$.
The value of $a$ varies with the composition of the glass of which the thermometer stem is composed. For glass of unknown composition the best average value for centigrade temperatures appears to be 0.000 I 55 , while for stems of Jena $16^{111}$, or similar glasses, or Jena $59^{\text {III }}$, the values 0.00016 for the former and 0.000i 65 for the latter may be preferred. (Letter from U.S. Bureau of Standards dated January 5, 1918.)

The use of the formula given above presupposes that the mean temperature of the emergent column has been determined. This temperature may be approximately obtained in one of three ways. (I) By a "fadenthermometer" (Buckingham, Bulletin, Bureau of Standards, 8, 239, 191 I, Scientific Paper 170); (2) by exploring the temperature distribution along the stem and calculating the mean temperature; (3) by suspending along the side of, or attaching to the stem, a single thermometer. If properly placed this
thermometer will indicate the temperature of the emergent mercurial column to an accuracy sufficient for many purposes. Under conditions ordinarily met with in practice it is desirable to place the bulb of the auxiliary thermometer at some point below the middle of the emergent column.

It is to be noted that the correction sought is directly proportional to the value of $a$, and that this may vary for glass stems of different composition from 0.00015 to 0.000165 for Centigrade temperatures. For thermometers ordinarily used in meteorological work, however, 0.000155 appears to be a good average value for Centigrade temperatures ( 0.000086 for Fahrenheit temperatures), and the correction formulæ, therefore, are,

$$
\begin{aligned}
& T=t-0.000086 n\left(t^{\prime}-t\right) \text { Fahrenheit temperatures. } \\
& T=t-0.000 \mathrm{I} 55 n\left(t^{\prime}-t\right) \text { Centigrade temperatures. }
\end{aligned}
$$

In the above, $T=$ Corrected temperature.
$t=$ Observed temperature.
$t^{\prime}=$ Mean temperature of the glass stem and emergent mercury column.
$n=$ Length of mercury in the emergent stem in scale degrees.
When $t^{\prime}$ is $\left\{\begin{array}{l}\text { higher } \\ \text { lower }\end{array}\right\}$ than $t$ the numerical correction is to be $\left\{\begin{array}{l}\text { subtracted. } \\ \text { added. }\end{array}\right\}$
table 7 gives corrections computed to o.oi for Fahrenheit thermometers from the equation $C=-0.000086 n\left(t^{\prime}-t\right)$. The side argument, $n$, is given for $10^{\circ}$ intervals from $10^{\circ}$ to $130^{\circ}$; the top argument, $t^{\prime}-t$, for $10^{\circ}$ intervals from $10^{\circ}$ to $100^{\circ}$.

Table 8 gives corrections computed to o. Oi for Centigrade thermometers from the equation $C=-0.000155 n\left(t^{\prime}-t\right)$. The side argument, $n$, is given for $10^{\circ}$ intervals from $10^{\circ}$ to $100^{\circ}$; the top argument, $t^{\prime}-t$, for $10^{\circ}$ intervals from $\mathrm{IO}^{\circ}$ to $80^{\circ}$.

## Example:

The observed temperature of a black-bulb thermometer is $120^{\circ} \cdot 4 F_{\text {. }}$, the temperature of the glass stem is $55^{\circ} \cdot 2 F$., and the length of mercury in the emergent stem is $130^{\circ} \mathrm{F}$. To find the corrected temperature. With $n=130^{\circ} F$. and $t^{\prime}-t=-65^{\circ} F$., as arguments, Table 7 gives the correction $0^{\circ} .7 F^{\circ}$., which by the above rule is to be added to the observed temperature. The corrected temperature is therefore I2I.i $F$.

## CONVERSIONS INVOLVING LINEAR MEASURES.

The fundamental unit of length is the meter, the length of which is equal to the distance between the defining lines on the international prototype meter at the International Bureau of Weights and Measures (near Paris) when this standard is at the temperature of melting ice $\left(0^{\circ} \mathrm{C}\right)$. The relation
here adopted between the meter and the yard, the Englisn measure of length, is I meter $=39.3700$ inches, as legalized by Act of U.S. Congress, July 28, I866. This U.S. Standard of length must be distinguished from the British Imperial yard, comparisons of which with the international prototype meter give the relation I meter $=39.370$ II 3 inches. (See Smithsonian Physical Tables, 19ı6, p. 7, Table 3.)
table 9. Inches into millimeters.
TABLE 9.

$$
\text { I inch }=25 \cdot 40005 \text { millimeters. }
$$

The argument is given for every hundredth of an inch up to 32.00 inches, and the tabular values are given to hundredths of a millimeter. A table of proportional parts for thousandths of an inch is added on each page.

## Example:

To convert $2 \nmid .362$ inches to millimeters.
The table gives (p. 20).

$$
(24.36+.002) \text { inches }=(618.75+0.05) \mathrm{mm} .=618.80 \mathrm{~mm} .
$$

table 10. Millimeters into inches.
TABLE 10.
From o to 400 mm . the argument is given to every millimeter, with subsidiary interpolation tables for tenths and hundredths of a millimeter. The tabular values are given to four decimals. From 400 to 1000 mm ., covering the numerical values which are of frequent use in meteorology for the conversion of barometric readings from the metric to the English barometer, the argument is given for every tenth of a millimeter, and the tabular values to three decimals.

## Example:

To convert 143.34 mm . to inches.
The table gives

$$
(143+.3+.04) \mathrm{mm} .=(5.6299+0.0118+0.0016) \text { inches }=5.6433
$$ inches.

Tables 11, 12. Conversion of barometric readings into standard units of pressure.

The equation for the pressure in millibars, ${ }^{1} P_{m b}$, corresponding to the barometric height, $B$, is

$$
P_{m b}=B \frac{\Delta g_{0}}{\mathrm{IOOO}}
$$

where $\Delta$ is the densitv of mercury and $g_{0}$ is the standard value of gravity.

[^0]In order that pressures thus derived shall be expressed in C.G.S. units it is evident that the recognized standard values of the constants of the equation must be employed. It therefore becomes necessary to abandon the values for the density of mercury and for standard gravity heretofore employed, which had the sanction of the International Meteorological Committee, in favor of the more recently determined values that have been adopted by the International Bureau of Weights and Measures.

The value adopted for $\Delta$ is 13.5951 grams per cubic centimeter; ${ }^{1}$ and for $g_{0}, 980.655$ dynes. ${ }^{2}$

By the use of these constants in the above equation we obtain

$$
\begin{aligned}
& P_{m b}=\frac{1.333224}{} B \text { (millimeters), and } \\
& P_{m b}=\frac{1.333224}{0.03937} B=33.86395 B \text { (inches) }
\end{aligned}
$$

where $B$ is the height of the barometer in the units indicated, after reduc. tion to standard temperature and the standard value of gravity.
table 11. Barometric inches to millibars.
The argument is for 0.01 inch. From 0.00 to 2.49 inches the tabulated values are given to the nearest hundredth of a millibar, so that by removing the decimal one place to the right the value in millibars of every tenth inch from o.o to $2+.9$ inches may be obtained to the nearest tenth of a millibar. From 25.00 to 3 r. 99 inches the tabular values are given to the nearest tenth of a millibar.

The first part of the table may be used as a table of proportional parts for interpolation.
Ezample:
To convert 23.86 barometric inches into millibars of pressure.
From Table 11, 23.8 inches $=806.0$ millibars
.06 inch $=2.0$
23.86 inches $=\overline{808.0}$ millibars

Tabe 12. Barometric millimeters to millibars.
The argument is for each millimeter from 1 to 799, and the tabular values are given to the nearest tenth of a millibar.

This table may also be used to convert millibars into millimeters of mercury.

[^1]Example:
To convert 1003.5 millibars into millimeters of mercury. 1003.5 mb . $=(1002.6+0.9) \mathrm{mb} .=(752+0.68) \mathrm{mm} .=752.68 \mathrm{~mm}$.
table 13. Feet into meters.
TABLE 13.
From the adopted value of the meter, 39.3700 inches -
I English foot $=0.3048006$ meter.
Table 13 gives the value in meters and thousandths (or millimeters) for every foot from o to 99 feet; the value to hundredths of a meter (or centimeters) of every Io feet from 100 to 4090 feet; and the value to tenths of a meter of every io feet from 4000 to 9090 feet. In using the latter part, the first line of the table serves to interpolate for single feet.
Example:
To convert 47 feet 7 inches to meters. 47 feet 7 inches $=47.583$ feet.
The table gives
47 feet $=14.326$ meters.
By moving the decimal point
0.583 " $=0.178$ "
47.583 feet $=14.504$ meters.
table 14. Meters into feet.
TABLE 14.

```
I meter = 39.3700 inches = 3.280833 + feet.
```

From o to 509 meters the argument is given for every unit, and the tabular values to two decimals; from 500 to 5090 the argument is given to every 10 meters, and the tabular values to one decimal. The conversion for tenths of a meter is added for convenience of interpolation.
Ezample:
Convert 4327 meters to feet.
The table gives

$$
(+320+7) \text { meters }=(14173.2+23.0) \text { feet }=14196.2 \text { feet. }
$$

table 15. Miles into kilometers.
TABLE 15.

$$
\text { I mile }=1.609347 \text { kilometers. }
$$

The table extends from o to 1009 miles with argument to single miles, and from 1000 to 20000 miles for every 1000 miles. The tabular quantities are given to the nearest kilometer.
table 16. Kilometers into miles.
TABLE 16.

$$
\text { I kilometer }=0.621370 \text { mile. }
$$

The table extends to 1009 kilometers with argument to single kilometers, and from 1000 to 20000 kilometers for every 1000 kilometers. Tabular values are given to tenths of a mile.

## Example:

Convert 3957 kilometers into miles.
The table gives
$(3000+957)$ kilometers $=(1864.1+594.7)$ miles $=2458.8$ miles.

Table 17. Interconversion of nautical and statute miles.
The nautical mile as defined by the U.S. Coast and Geodetic Survey (Tables for a polyconic projection of maps. U.S. Coast and Geodetic Survey, Special Publication No. 5, page 4) is "A minute of arc of a great circle of a sphere whose surface equals that of the Clarke representative spheroid of $1866, "$ and the value given is 1853.25 meters, or 6080.20 feet.
table 18. Continental measures of length with their metric and English equivalents.

This table gives a miscellancous list of continental measures of length, alphabetically arranged, with the name of the country to which they belong and their metric and English equivalents.

CONVERSION OF MEASURES OF TIME AND ANGLE.
table 19. Arc into time.

$$
\mathrm{I}^{\circ}=4^{\mathrm{m}} ; \mathrm{I}^{\prime}=4^{\mathrm{s}} ; \mathrm{I}^{\prime \prime}=\frac{\mathrm{I}}{\mathrm{I}} \mathrm{~s}=0.067
$$

Example:
Change $124^{\circ} 15^{\prime} 24^{\prime \prime} 7$ into time.
From the table,

$$
\begin{array}{rlrl}
124^{\circ} & = & 8^{\mathrm{h}} & 16^{\mathrm{m}} \\
15^{\prime} & = & 0^{\mathrm{s}} \\
24^{\prime \prime} & = & & \mathrm{I} \\
0 & 0 \\
0^{\prime \prime} 7 & = & & 1.600 \\
& & & .047 \\
8^{\mathrm{h}} & 17^{\mathrm{m}} & 1.647
\end{array}
$$

table 20. Time into arc.

$$
\mathrm{I}^{\mathrm{h}}=\mathrm{I} 5^{\circ} ; \mathrm{I}^{\mathrm{m}}=15^{\prime} ; \mathrm{I}^{\mathrm{s}}=\mathrm{I} 5^{\prime \prime} .
$$

Example:
Change $8^{\mathrm{h}}$ I $7^{3 \mathrm{~m}} \mathrm{I}^{8} 647$ into arc.

| From the table, | $8^{\text {h }}$ | $=$ | $120^{\circ}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $17{ }^{\text {m }}$ | = | 4 | $15^{\prime}$ |  |
|  | $\mathrm{I}^{\text {s }}$ | $=$ |  |  | $15^{\prime \prime}$ |
|  | 0.64 | = |  |  | 9.60 |
| By moving the decimal point, | .007 | $=$ |  |  | 0. 10 |
|  |  |  | $124^{\circ}$ | $15^{\prime}$ | $24^{\prime \prime} 7$ |

tagle 21. Days into decimals of a year and angle.
The table gives for the beginning of each day the corresponding decimal of the year to five places. Thus, at the epoch represented by the beginning of the 15 th day, the decimal of the year that has elapsed since January i.O is computed from the fraction $\frac{14}{365.25}$. The corresponding value in angle obtained by multiplying this fraction by $360^{\circ}$, is given to the nearest minute.

Two additional columns serve to enter the table with the day of the month either of the common or the bissextile year as the argument, and may be used also for converting the day of the month to the day of the year, and vice versa.

## Example:

To find the number of days and the decimal of a year between February 12 and August 27 in a bissextile year.
Aug. 27: Day of year $=240$; decimal of a year $\quad=0.65+35$
Feb. 12: " " " = 43; " " $=\underline{0.11499}$
Interval in days $\quad=197$; interval in decimal of a year $=0.53936$
The decimal of the year corresponding to the interval 197 days may also be taken from the table by entering with the argument ig8.
table 22. Hours, minutes and seconds into decimals of a day.
TABLE 22.
The tabular values are given to six decimals.

## Example:

Convert $5^{\mathrm{h}} 24^{\mathrm{m}} 23^{\mathrm{s}} .4$ to the decimal of a day:

$$
\begin{array}{rlr}
5^{\mathrm{h}} & =0.208333 \\
24^{\mathrm{m}} & =0.016667 \\
23^{\mathrm{s}} & = & 266 \\
0.4 & = & \frac{5}{0.22527 \mathrm{I}}
\end{array}
$$

By interpolation, or by moving the decimal for $4^{\text {s }}$
table 23. Decimals of a day into hours, minutes and seconds.
TABLE 23
Example:
Convert 0.225271 to hours, minutes and seconds:

$$
\begin{aligned}
& 0.22 \text { day }=4^{\mathrm{h}} 48^{\mathrm{m}}+28^{\mathrm{m}} 4^{\mathrm{s}}=5^{\mathrm{h}} 16^{\mathrm{m}} 48^{\mathrm{s}} \\
& 0.005^{2} \text { day }=7^{\mathrm{m}} 12^{\mathrm{s}}+17^{\mathrm{s} .28}=72928 \\
& 0.00007 \mathrm{I} \text { day }=6.05+0.09=\frac{6.14}{5^{\mathrm{h}} 24^{\mathrm{m}} 23^{\mathrm{s}} \cdot 4}
\end{aligned}
$$

table 24. Minutes and seconds into decimals of an hour.
TABLE 24
The tabular values are given to six decimals.

## Example:

Convert $34^{\mathrm{m}} 28.7$ to decimals of an hour.

$$
\begin{array}{rrr}
34^{\mathrm{m}} & =\mathrm{o}^{\mathrm{h}} 566667 \\
28^{\mathrm{s}} & =7778 \\
0.7 & =\frac{194}{0.574639}
\end{array}
$$

## Table 25. Local mean time at apparent noon.

This table gives the local mean time ${ }^{1}$ that should be shown by a clock when the center of the sun crosses the meridian, on the ist, 8 th, I 6 th, and 24 th days of each month. The table is useful in correcting a clock by means of a sundial or noon mark.

## Example:

To find the correct local mean time when the sun crosses the meridian on December 15, i89I.
The table gives for December I6, I I ${ }^{\mathrm{h}} 56^{\mathrm{m}}$. By interpolating, it is seen that the change to December 15 would be only one-half minute; the correct clock time is therefore 4 minutes before 12 o'clock noon.
table 26. Sidereal time into mean solar time.
table 27. Mean solar time into sidereal time.
According to Newcomb, the length of the tropical year is 365.24220 mean solar days, ${ }^{2}$ whence
365.24220 solar days $=366.24220$ sidereal days.

Any interval of mean time may therefore be changed into sidereal time by increasing it by its $\frac{1}{365 \cdot 2+220}$ part, and any interval of sidereal time may be changed into mean time by diminishing it by its $\frac{1}{366.2+220}$ part.

Table 26 gives the quantities to be subtracted from the hours, minutes and seconds of a sidereal interval to obtain the corresponding mean time interval, and Table 27 gives the quantities to be added to the hours, minn!tes and seconds of a mean time interval to obtain the corresponding sidereal interval. The correction for seconds is sensibly the same for either a sidereal or a mean time interval and is therefore given but once, thus forming a part of each table.
Examples:
Change $14^{\mathrm{h}} 25^{\mathrm{m}} 36.2$ sidereal time into mean solar time.

| Given sidereal time |  | $14^{\text {h }}$ | $25^{\text {m }}$ | $36^{\text {s }}$. 2 |
| :---: | :---: | :---: | :---: | :---: |
| Correction for $14{ }^{\text {h }}$ | $=-2^{\mathrm{m}}$ I $7^{\text {s }}$.6I |  |  |  |
| $25^{\text {m }}$ | 4.10 |  |  |  |
| 36.2 | . IO |  |  |  |
|  | -2 2I.8I |  | -2 | 21.8 |
| Corresponding mean time | $=$ | 14 | 23 | 14.4 |

[^2]2. Change $13^{\mathrm{h}} 37^{\mathrm{m}} 22^{\mathrm{s}} .7$ mean solar time into sidereal time.

| Given mean time | = |  | $13^{\text {h }}$ |  | 22.7 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Correction for $13{ }^{\text {h }}$ | $=+2^{\mathrm{m}}$ | $8^{\text {s. }} 13$ |  |  |  |
| $37^{\text {m }}$ | $=+$ | 6.08 |  |  |  |
| $22^{\text {s. }} 7$ | + | 0.06 |  |  |  |
|  | $+2$ | 14.27 |  | +2 | 14.3 |
| Corresponding sidereal time | $=$ |  | 13 | 39 | 37.0 |

CONVERSION OF MEASURES OF WEIGHT.
TABLE 28.
Table 28. Conversion of avoirdupois pounds and ounces into kilograms.
The comparisons of July, I893, made by the International Bureau of Weights and Measures between the Imperial standard pound and the "kilogram prototype" resulted in the relation:

I pound avoirdupois $=453.5924277$ grams.
For the conversion of pounds, Table 28 gives the argument for every tenth of a pound up to 9.9 , and the tabular conversion values to ten-thousandths of a kilogram.

For the conversion of ounces, the argument is given for every tenth of an ounce up to 15.9 , and the tabular values to ten-thousandths of a kilogram.

Table 29. Conversion of kilograms into avoirdupois pounds and ounces.
From the above relation between the pound and the kilogram,

$$
\begin{aligned}
\text { I kilogram } & =2.204622 \text { avoirdupois pounds. } \\
& =35.274 \quad \text { avoirdupois ounces. }
\end{aligned}
$$

The table gives the value to thousandths of a pound of every tenth of a kilogram up to 9.9 ; the values of tenths of a kilogram in ounces to four decimals; and the values of hundredths of a kilogram in pounds and ounces to three and two decimals respectively.
table 30. Conversion of grains into grams.
TABLES 30, 31.
table 31. Conversion of grams into grains.
From the above relation between the pound and the kilogram,

$$
\begin{aligned}
& \text { I gram }=15.432356 \text { grains. } \\
& \text { I grain }=0.06479892 \text { gram } .
\end{aligned}
$$

Table 30 gives to ten-thousandths of a gram the value of every grain from I to 99 , and also the conversion of tenths and hundredths of a grain for convenience in interpolating.

Table 31 gives to hundredths of a grain the value of every tenth of a gram from O.I to 9.9 , and the value of every gram from 1 to 99 . The values of hundredths and thousandths of a gram are added as an aid to interpolation.

## WIND TABLES. CONVERSION OF VELOCITIES.

Table 32. Synoptic conversion of velocities.
This table, ${ }^{1}$ contained on a single page, converts miles per hour into meters per second, feet per second and kilometers per hour. The argument, miles per hour, is given for every half unit from o to 78 . Tabular values are given to one decimal. For the rapid interconversion of velocities, when extreme precision is not required, this table has proved of marked convenience and utility.
Table 33. Conversion of miles per hour into feet per second.
The argument is given for every unit up to I49 and the tabular values are given to one decimal.
Table 34. Conversion of feet per second into miles per hour.
The argument is given for every unit up to 199 and the tabular values are given to one decimal.
Table 35. Conversion of meters per second into miles per hour.
The argument is given for every tenth of a meter per second up to 60 meters per second, and the tabular values are given to one decimal.
Table 36. Conversion of miles per hour into meters per second.
The argument is given for every unit up to 149 , and the tabular values are given to two decimals.
Table 37. Conversion of meters per second into kilometers per hour.
The argument is given for every tenth of a meter per second up to 60 meters per second, and the tabular values are given to one decimal.
Table 38. Conversion of kilometers per hour into meters per second.
The argument is given for every unit up to 200, and the tabular values are given to two decimals.
Table 39. Scale of velocity equizalents of the so-called Beaufort scale of rivind.
The personal observation of the estimated force of the wind on an arbitrary scale is a method that belongs to the simplest meteorological records and is widely practiced. Although anemometers are used at meteorological observatories, the majority of observers are still dependent upon estimates based largely upon their own judgment, and so reliable can such estimates be made that for many purposes they abundantly answer the needs of meteorology as well as of climatology.

A great variety of such arbitrary scales have been adopted by different observers, but the one that has come into the most general use and received

[^3]the greatest definiteness of application is the duodecimal scale introduced into the British navy by Admiral Beaufort about iSoo.

Table 39 is taken from the Observer's Handbook of the Meteorological Office, London, edition of 1917, and the Marine Observer's Handbook of Meteorology, edition of 1930 . The velocity equivalents in meters per second and miles per hour are based on extensive observational data collected by Dr. G. C. Simpson and first published by the Meteorological Office in 1906. Several other sets of equivalents have been published in different countries. For a history of this subject see " Rept. Ioth Meeting International Meteorological Committee," Rome, 19I3, Appendix VII (London, 1914), and a paper by G. C. Simpson on "The velocity equivalents of the Beaufort scale," Professional Notes No. 44, Air Ministry, Meteorological Office, London, 1926.

Simpson points out that the Beaufort scale has been used by sailors for many generations to describe the effect of the air in motion on ships and their rigging, and upon the sea. With change in the rig of ships there still remains the effect of wind upon the surface of the sea, and to this has been added the effect upon objects on land.

Finally, it became desirable to interpret wind force on the Beaufort scale in terms of wind velocity as measured by the anemometer. For this purpose experiments with the anemometer both on land and on sea were made. The results showed considerable discrepancies in the velocity equivalents of winds indicated by different numbers on the Beaufort scale, but Simpson attributes these discrepancies to differences in anemometer exposures during the tests. For example, the Meteorological Office equivalents represent velocities measured by an anemometer not less than io meters above the ground level, while the Deutsche Seewarte equivalents represent velocities measured by anemometers as ordinarily exposed.

Simpson proposed a scale of equivalents about midway between those determined by the Meteorological Office and by the Seewarte, respectively, and this compromise scale was adopted by the Commission for Synoptic Weather Information of the International Meteorological Organization at its meeting in Zurich in 1926, with the proviso that the velocity equivalents correspond on land with the wind speed at a height of approximately 6 meters above a level surface. Since, however, the International Commission for Air Navigation has taken as the surface wind that measured at a height of 10 to I 5 meters above the ground, it has seemed best in these tables to continue to adhere to the British Meteorological Office equivalents, which are based on the equation $V=0.836 \sqrt{B^{3}}$, where $B$ is the Beaufort number representing the wind force, and $V$ is the velocity equivalent in meters per second.

The velocity equivalents adopted by the Commission for Synoptic Weather Information, referred to above, expressed in statute miles per hour, correspond very closely to the values in Table 39 expressed in nautical miles (knots) per hour.

In the Quarterly Journal of the Royal Mcteorological Socicty, volume xxx, No. 132, October, 1904, Prof. A. Lawrence Rotch has described an instrument for obtaining the true direction and velocity of the wind at sea aboard a moving vessel. If a line $A B$ represents the wind due to the motion of a steamer in an opposite direction, and $A C$ the direction of the wind relative to the vessel as shown by the drift of its smoke, then, by measuring the angle $D B A$ that the true wind makes with the vessel-which is easily done by watching the wave crests as they approach it-we obtain the third side, $B C$, of the triangle. This represents, in direction and also in length, on the scale used in setting off the speed of the ship, the true direction of the wind relative to the vessel and also its true velocity. The method fails when the wind direction coincides with the ship's course and becomes inaccurate when the angle between them is small.

## GRADIENT WINDS.

When the motions of the atmosphere attain a state of complete equilibrium of flow under definite systems of pressure gradients, the winds blow across the isobars at small angles of inclination depending upon the retarding effects of friction. At the surface of the earth friction is considerable and the angle across the isobars is often great. In the free air, however, the friction is small, and for some purposes may be disregarded entirely. Under an assumption of complete equilibrium of motion and frictionless flow the winds will blow exactly parallel to the isobars-that is, perpendicular to the gradient which produces and sustains the motion. Such winds are called gradient winds. The anomalous condition of flow of terrestrial winds perpendicular to the moving force is the result of the modifications of atmospheric motions due to the deflective influence of the earth's rotation, and to that other influence due to the inertia reaction of matter when it is constrained to move in a curved path, and commonly called centrifugal force. The equations for gradient wind motions have long been known to meteorologists from the work of Ferrel and others, and may be written in the following form:

For Cyclones

$$
\begin{equation*}
V=r\left[\sqrt{\omega^{2} \sin ^{2} \phi+\frac{\Delta P}{\rho r}}-\omega \sin \phi\right] \tag{I}
\end{equation*}
$$

For Anticyclones

$$
\begin{equation*}
V=r\left[\omega \sin \phi-\sqrt{\omega^{2} \sin ^{2} \phi-\frac{\Delta P}{\rho r}}\right] \tag{2}
\end{equation*}
$$

In C. G. S. Units, $V=$ velocity of the gradient wind in centimeters per second; $r=$ radius of curvature of isobars in centimeters; $\Delta P=$ pressure gradient in dynes per square centimeter per centimeter ; $\rho=$ density of air in grams per cubic centimeter ; $\omega=$ angular velocity of the earth's rotation
per second $=\frac{2 \pi}{86 I 64}$, and $\phi=$ latitude. In the Northern Hemisphere the winds gyrate counterclockwise in cyclones and clockwise in anticyclones. These gyrations are in the reversed direction each to each in the Southern Hemisphere.

In equation (2) the values of $V$ are imaginary for values of $\frac{\Delta P}{\rho r}$ greater than $\omega^{2} \sin ^{2} \phi$. The equality $\frac{\Delta P}{\rho r}=\omega^{2} \sin ^{2} \phi$, or $r=\frac{\Delta P}{\rho \omega^{2} \sin ^{2} \phi}$ defines and fixes an isobar with minimum curvature in anticyciones. Winds cannot flow parallel to the isobars within this critical isobar. For this isobar the gradient wind has its maximum value $V_{c}=\frac{\Delta P}{\rho \omega \sin \phi}$. For the same gradient and for an isobar with the same curvature in a cyclone the gradient velocity is $V_{l}=V_{c}(\sqrt{2}-\mathrm{I})=0.4 \mathrm{I} 4 V_{c}$.

When the isobars are parallel straight lines, a condition very often closely realized in nature, $r=\infty$ and the gradient winds have the value given by either (I) or (2) after squaring, namely,

$$
V_{r=\infty}=V_{s}=\frac{\Delta P}{2 \rho \omega \sin \phi}=\frac{1}{2} V_{c} .
$$

For practical units equation (I) becomes
Units of pressure.
$V=R\left[\begin{array}{lll}\sqrt{.0053173 \sin ^{2} \phi+\frac{\mathrm{I}}{\mathrm{IOR} \mathrm{\rho d}}}-.07292 \sin \phi \\ \sqrt{.0053173 \sin ^{2} \phi+\frac{.13333}{R \rho d}}-.07292 \sin \phi & \text { (I) (Millibars) } \\ \sqrt{.068914 \sin ^{2} \phi+\frac{\mathrm{I} .69+6}{R_{\rho} d}}-.26252 \sin \phi\end{array}\right]$ (II) (Millimeters)
$V=$ velocities in meters per second in (I) and (II) and in miles per hour in (III).
$R=$ radius of curvature of isobar (wind path) in kilometers in (I) and (II) and in miles in (III).

The gradient is to be deduced from isobars drawn for pressure intervals of I millibar in (I), I millimeter in (II) and $\frac{\mathrm{I}}{\mathrm{IO}}$ inch in (III); $d$, is the perpendicular distance between isobars (as above defined) in kilometers in (I) and (II), and in miles in (III). $\rho=$ density of air $=$ grams per cubic centimeter in all cases.

Also \begin{tabular}{c}

| Units of |
| :---: |
| pressure. | <br>

$V_{c}=\left[\begin{array}{ll}\frac{1.3713}{\rho d \sin \phi}(\text { IV }) \\
\frac{1.8284}{\rho d \sin \phi} & (\mathrm{~V}) \\
\frac{6.4552}{\rho d \sin \phi}(\mathrm{VI})\end{array}\right.$ and $R_{c}=\left[\begin{array}{ll}\frac{18.806}{\rho d \sin ^{2} \phi} & \text { (VII) (Millibars) } \\
\frac{25.073}{\rho d \sin ^{2} \phi} & \text { (VIII) (Millimeters) } \\
\frac{24.590}{\rho d \sin ^{2} \phi} & \text { (IX) (Inches) }\end{array}\right.$
\end{tabular}

Radius of critical curvature and velocities of gradient winds for frictionless motion in Highs and Lowus.
table 40. English Measures.
TABLES 40, 41.
table 41. Metric Measures.
These tables give the radius of curvature of the critical isobar in anticyclones, computed from the equation

$$
R_{c}=\frac{\Delta P}{\rho \omega^{2} \sin ^{2} \phi},
$$

the velocity of the wind on this isobar, computed from the equation

$$
V_{c}=\frac{\Delta P}{\rho \omega \sin \phi} ;
$$

the velocity of the wind on a straight isobar, computed from the equation

$$
V_{s}=\frac{\Delta P}{2 \rho \omega \sin \phi}=\frac{1}{2} V_{c} ; \text { and }
$$

the velocity of the wind in a cyclone having the same gradient as the anticyclone, and on an isobar having a radius of curvature equal to $R_{c}$, computed from the equation

$$
V_{1}=V_{c}(\sqrt{2}-1)=0.414 V_{c}
$$

Table ұо, English measures, gives values of $R_{c}$, in miles, and of $V_{c}$ High, $V_{s}$, and $V$ Low, in miles per hour. The side argument is the latitude for $10^{\circ}$, and at $5^{\circ}$ intervals from $20^{\circ}$ to $90^{\circ}$, inclusive. The top argument, $d$, is the perpendicular distance in miles between isobars drawn for pressure intervals of $\frac{\mathrm{I}}{\mathrm{IO}}$ inch. For values of $d$ one tenth as great as given in the heading of the table the values of $R_{c}, V_{c}$ High, $V_{s}$, and $V$ Low are increased tenfold.

Table 4I, metric measures, gives values of $R_{c}$ in kilometers, and of $V_{c}$ High, $V_{s}$, and V Low, in meters per second. The side argument is the same as in Table 40. The top argument, $d$, is the perpendicular distance in kilometers between isobars drawn for pressure intervals of I millimeter. For values of $d$ one tenth as great as given in the heading of the table the values of $R_{c}, V_{c}$ High, $V_{s}$, and $V$ Low are increased tenfold.

## TEMPERATURE TABLES.

## REDUCTION OF TEMPERATLRE TO SEA LEVEL.

Table 42. English Measures.
Table 43. Metric Measures.
These tables give for different altitudes and for different uniform rates of decrease of temperature with altitude, the amount in hundredths of a degree Fahrenheit and Centigrade, which must be added to observed temperatures in order to reduce them to sea level.

The rate of decrease of temperature with altitude varies from one region to another, and in the same region varies according to the season and the meteorological conditions; being in general greater in warm latitudes than in cold ones, greater in summer than in winter, and greater in areas of falling pressure than in areas of rising pressure. For continental plateau regions, the reduction often becomes fictitious or illusory. The use of the tables therefore requires experience and judgment in selecting the rate of decrease of temperature to be used. Much experimental work is now in progress with kites and balloons to determine average vertical gradients. It must be remembered that the tables here given are not tables giving the data as recently determined for various elevations.

The tables are given in order to facilitate the reduction of temperature either upward or downward in special insestigations, but the reduction is not ordinarily applied to meteorological observations.

The tables, 42 and 43, are computed for rates of temperature change ranging from $\mathrm{I}^{\circ}$ Fahrenheit in 200 feet to $I^{\circ}$ Fahrenheit in 900 feet, and from $I^{\circ}$ Centigrade in 100 meters to $I^{\circ}$ Centigrade in 500 meters; and for altitudes up to 5000 feet and 3000 meters respectively. Example, Table 42.

Observed temperature at an elevation of 2,500 feet, 52.5 F .

Reduction to sea level for an assumed decrease in temperature of $1^{\circ} \mathrm{F}$. for every 300 feet,
$\begin{array}{r}\circ \\ +\quad 8 \\ \hline\end{array}$
Temperature reduced to sea level,
$60^{\circ} 8 \mathrm{~F}$. Example, Table 43.

Observed temperature at an elevation of 500 meters, 12.5 C .

Reduction to sea level for an assumed decrease in temperature of $\mathrm{I}^{\circ} \mathrm{C}$. for every 200 meters,
Temperature reduced to sea level,

$$
\frac{+\quad 2!5}{15: 0} C
$$

## BAROMETRICAL TABLES.

## REDUCTION TO A STANDARD TEMPERATURE OF OBSERVATIONS MADE WITH MERCURIAL BAROMETERS HAVING BRASS SCALES.

The indicated height of the mercurial column in a barometer varies not only with changes of atmospheric pressure, but also with variations of the temperature of the mercury and of the scale. It is evident therefore that if
the height of the barometric column is to be a true relative measure of atmospheric pressure, the observed readings must be reduced to the values they would have if the mercury and scale were maintained at a constant standard temperature. This reduction is known as the reduction for temperature, and combines both the correction for the expansion of the mercury and that for the expansion of the scale, on the assumption that the attached thermometer gives the temperature both of the mercury and of the scale.

The freezing point is universally adopted as the standard temperature of the mercury, to which all readings are to be reduced. The temperature to which the scale is reduced is the normal or standard temperature of the adopted standard of length. For English scales, which depend upon the English yard, this is $62^{\circ}$ Fahrenheit. For metric scales, which depend upon the meter, it is $0^{\circ}$ Centigrade. As thus reduced, observations made with English and metric barometers become perfectly comparable when converted by the ordinary tables of linear conversion, viz: inches to millimeters and millimeters to inches (see Tables 9, Io), for these conversions refer to the meter at $0^{\circ}$ Centigrade and the English yard at $62^{\circ}$ Fahrenheit.

Prof. C. F. Marvin in the Monthly Weather Review for July, I898, has pointed out the necessity of caution in conversion of metric and English barometer readings:

## Example:

$$
\begin{array}{lc}
\text { Attached thermometer, } & 25^{\circ} .4 \mathrm{C} \\
\text { Barometer reading, } & 762.15 \mathrm{~mm} .
\end{array}
$$

If the temperature is converted to Fahrenheit $=77^{\circ} .7$ and the reading to 30.006 in ., the temperature correction according to table 44 would be -O.I33 inch and the reduced reading 29.873. This would be erroneous. The correct conversion is found by taking the correction corresponding to $25^{\circ}+\mathrm{C}$. and 762 mm ., i.e., -3.15 mm ., which gives a corrected reading of 759 mm ., and converted into inches gives 29.882 which is the correct result.

Professor Marvin further remarks that circumstances sometimes arise in which a Centigrade thermometer may be used to determine the temperature of an English barometer, or a Fahrenheit attached thermometer may be used with a metric scale. In all such cases the temperature must be brought into the same system of units as the observed scale reading before corrections can be applied, and the observed reading must then be corrected for temperature before any conversion can be made.

With aneroid barometers corrections for temperature and instrumental error must be determined for each instrument.

The general formula for reducing mercurial barometers with brass scales to the standard temperature is

$$
C=-B \frac{m(t-T)-l(t-\theta)}{\mathrm{I}+m(t-T)}
$$

in which $C=$ Correction for temperature.
$B=$ Observed height of the barometric column.
$t=$ Temperature of the attached thermometer.
$T=$ Standard temperature of the mercury.
$m=$ Coefficient of expansion of mercury.
$l=$ Coefficient of linear expansion of brass.
$\theta=$ Standard temperature of the scale.
The accepted determination of the coefficient of expansion of mercury is that given by Broch's reduction of Regnault's experiments, viz:

$$
m\left(\text { for } \mathrm{I}^{\circ} C .\right)=1 \mathrm{I}^{-9}\left(\mathrm{I} 8 \mathrm{I} 792+0.175 t+0.035 \mathrm{I} 16 t^{2}\right)
$$

As a sufficiently accurate approximation, the intermediate value

$$
m=0.00018 \mathrm{I} 8
$$

has been adopted uniformly for all temperatures in conformity with the usage of the International Meteorological Tables.

Various specimens of brass scales made of alloys of different composition show differences in their coefficients of expansion amounting to eight and sometimes ten per cent. of the total amount. The Smithsonian Tables prepared by Prof. Guyot were computed with the average value $l$ (for $\mathrm{I}^{\circ} C$.) $=0.0000 \mathrm{I} 88$; for the sake of uniformity with the International Meteorological Tables, the value

$$
l=0.0000184
$$

has been used in the present volume. For any individual scale, either value may easily be in error by four per cent.

A small portion of the tables has been independently computed, but the larger part of the values have been copied from the International Meteorological Tables, one inaccuracy having been found and corrected.

Table 44. Reduction of the barometer to standard temperature - English measures.

For the English barometer the formula for reducing observed readings to a standard temperature becomes

$$
C=-B \frac{m\left(t-32^{\circ}\right)-l\left(t-62^{\circ}\right)}{\mathrm{I}+m\left(t-32^{\circ}\right)}
$$

in which $B=$ Observed height of the barometer in English inches.
$t=$ Temperature of attached thermometer in degrees Fahrenheit.

$$
\begin{aligned}
m & =0.0001818 \times \frac{5}{9}=0.000101 \\
l & =0.0000184 \times \frac{5}{9}=0.0000102
\end{aligned}
$$

The combined reduction of the mercury to the freezing point and of the scale to $62^{\circ}$ Fahrenheit brings the point of no correction to approximately $28^{\circ} .5$ Fahrenheit. For temperatures above $28^{\circ} .5$ Fahrenheit, the correction is subtractive, and for temperatures below $28^{\circ} .5$ Fahrenheit, the correction is additive, as indicated by the signs ( + ) and ( - ) inserted throughout the table.

The table gives the corrections for every half degree Fahrenheit from $0^{\circ}$ to $100^{\circ}$. The limits of pressure are 19 and 31.6 inches, the corrections being computed for every half inch from 19 to 24 inches, and for every twotenths of an inch from 24 to 3 I .6 inches.

## Example :

Observed height of barometer $=29.143$
Attached thermometer, 54.5 F .
Reduction for temperature $=-0.068$
Barometric reading corrected for temperature $=29.075$
TABLE 45.
Table 45. Reduction of the barometer to standard temperature - Metric measures.

For the metric barometer the formula for reducing observed readings to the standard temperature, $o^{\circ} C$., becomes

$$
C=-B \frac{(m-l) t}{I+m t}
$$

in which $C$ and $B$ are expressed in millimeters and $t$ in Centigrade degrees.

$$
m=0.0001818 ; \quad l=0.0000184
$$

In the table, the limits adopted for the pressure are 440 and 795 millimeters, the intervals being io millimeters between 40 and 600 millimeters, and 5 millimeters between 600 and 795 millimeters.

The limits adopted for the temperature are $0^{\circ}$ and $+35^{\circ} .8$, the intervals being 0.5 and I.O from 440 to 560 millimeters, and $0^{\circ} .2$ from 560 to 795 millimeters.

For temperatures above $o^{\circ}$ Centigrade the correction is negative, and hence is to be subtracted from the observed readings.

For temperatures below $0^{\circ}$ Centigrade the correction is positive, and from $0^{\circ} \mathrm{C}$. down to $-20^{\circ} \mathrm{C}$. the numerical values thereof, for ordinary barometric work, do not materially differ from the values for the corresponding temperatures above $0^{\circ} \mathrm{C}$. Thus the correction for $-9^{\circ} \mathrm{C}$. is numerically the same as for $+9^{\circ} \mathrm{C}$. and is taken from the table. In physical work of extreme precision, the numerical values given for positive temperatures may be used for temperatures below $0^{\circ} C$. by applying to them the following corrections:

Corrections to be applied to the tabular values of Table 45 in order to use them when the temperature of the attached thermometer is below $0^{\circ}$ Centigrade.

| Temperature. | Pressure in millimeters. |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 450 | 500 | 550 | 600 | 650 | 700 | 750 | 800 |
| C. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $-\mathrm{I}^{\circ}$ | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| - 9 | .00 | . 00 | . 00 | . 00 | . 0 | . 00 | . 00 | . 00 |
| - 10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | +0.01 | +0.01 | to.01 |
| II | . 00 | . 00 | . 00 | . 00 | +0.01 | . OI | . OI | . 01 |
| 12 | . 0 | . 00 | . 00 | +0.01 | . Or | . 01 | . OI | . OI |
| 13 | . 00 | . 00 | +0.01 | . 01 | . OI | . 01 | . OI | . 01 |
| -14 | . 00 | +o.01 | . 01 | . Or | . Or | . 01 | . OI | . OI |
| - 15 | to.01 | toor | +0.01 | to.01 | to.or | +0.01 | +o.01 | +0.01 |
| 16 | . 01 | . 01 | . 01 | . 01 | . OI | . 01 | . 01 | . 01 |
| 17 | . 01 | - 01 | . 01 | . 01 | . OI | . 01 | . 01 | . 02 |
| 18 | . Or | . 01 | . 01 | . 01 | . 01 | . 01 | . OI | . 02 |
| $-19$ | . OI | .or | . 01 | . 01 | . OI | . OI | . 02 | . 02 |
| -20 | +0.01 | +0.01 | to.or | to.or | +o.01 | +0.02 | +0.02 | +0.02 |
| 21 | . 01 | . 01 | . OI | . 02 | . 02 | . 02 | . 02 | . 02 |
| 22 | . 01 | . 01 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 |
| 23 | .or | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 |
| -24 | . OI | . 02 | . 02 | . 02 | . 02 | . 02 | . 02 | . 03 |

Example:
Observed height of barometer, $763 \cdot 17^{\mathrm{mm}}:$ Temperature of the attached thermometer, $-12^{\circ} \mathrm{C}$.
Numerical value of the reduction for $+12^{\circ} \mathrm{C}$. $={ }^{1.50}$
Correction for temperature below o ${ }^{\circ} \mathrm{C}$.
$=+\underline{0.01}$
Reduction for $-12^{\circ} \mathrm{C}$.
$=+\quad \mathrm{I} .5 \mathrm{I}$
Observed height of barometer
$=763.17$
Barometer corrected for temperature
$=764.68$
Table 46. Reduction of the mercurial column in $\mathbf{U}$-shaped manometers with brass scales to standard temperature. English measures.

This is in reality an extension of Table 44 to the small differences in height of the mercurial columns as determined with a U -shaped manometer and is used especially in the calibration of instruments for upper-air investigations. Since the corrections are directly proportional to the observed height of the mercurial column, they have been obtained by multiplying corrections given in Table 44 by the appropriate decimal. They have been computed for each inch of pressure from I inch to 20 inches, inclusive, and for intervals of temperature of 2 degrees, from $0^{\circ}$ to $100^{\circ}$ Fahrenheit.

## Example:

Observed heights of the mercury in the manometer tubes (in.), +6.258 and -4.375 .
Difference in height of the two columns 10.633

Attached thermometer, $72^{\circ} .4 \mathrm{~F}$.
Correction for temperature

- .O42

Manometer reading corrected for temperature 10.591
For temperatures above $28^{\circ} 5$ Fahrenheit, the correction is subtractive, and for temperatures below 28.5 Fahrenheit, the correction is additive, as indicated by the signs $(+)$ and ( - ) inserted throughout the table.
table 47. Reduction of the mercurial columm in U -shaped manometers with brass scales to standard temperature. Metric measures.
This table is an extension of Table 45 to the small differences in height of the mercurial columns as determined with a U -shaped manometer. The values have been obtained from the corrections given in that table by the same process as those given in Table 46 were obtained from Table 44.

## Example:

Observed heights of the mercury in the manometer tubes (mm.), + 121.5 and -86.7.
Difference in height of the two columns
Attached thermometer, 18.4 C .
Correction for temperature
$-\quad 0.6$
Manometer reading corrected for temperature
207.6

For temperatures above $o^{\circ} \mathrm{C}$. the correction is negative, and hence is to be subtracted from the observed readings. For negative temperatures see the explanation of Table 45 .

## REDUCTION OF THE MERCURIAL BAROMETER TO STANDARD GRAVITY.

## Tables 48, 49, 50.

The mercurial barometer does not directly measure the atmospheric pressure. The latter is proportional to the weight of the mercurial column, and also to its height after certain corrections have been applied. Since the height of the barometric column is easily measured, by common consent the pressures are expressed in terms of this corrected height.

The observed height of the barometer changes with the temperature of the mercury as already shown, and also with the variations in the value of gravity, as well as with the pressure. Therefore, to obtain a height that shall be a true relative measure of the atmospheric pressure, the observed height of the mercurial column must not only be reduced to what its height would be if at a standard temperature, but also to what it would be at a standard value of gravity.

As stated on page xxii, the standard value of gravity adopted is 980.665 dynes. At the time of its adoption this value was assumed to apply for "latitude $45^{\circ}$ and sea-level" on the basis of the absolute determination of $g$ at the International Bureau by Defforges, 1887-1890 (Procés-Verbaux, Comité Inter. d. Poids et Mesures, I887, pp. 27-28, 86; i891, p. 135).

More recent determinations, ${ }^{1}$ based upon numerous measurements in all parts of the world, and assuming a certain ideal figure for the earth, give for the mean value of $g$ at latitude $45^{\circ}$ and sea level the value 980.621 dynes. This differs from the standard value by 0.044 dyne. Departures of this magnitude from the mean sea-level gravity of a given latitude are frequently encountered, and in some cases surpassed. They are attributed to topography and isostatic compensation, and to gravity anomalies. For example, according to Bowie, ${ }^{2}$ at Pikes Peak, Colo., the correction for topography and compensation is +0.187 dyne, while the gravity anomaly ${ }^{3}$ is +0.021 dyne, giving a total gravity departure of +0.208 dyne. Also, at Seattle, Wash., from the mean of measurements at two stations, the correction for topography and compensation is -0.019 dyne ${ }^{4}$ and the gravity anomaly is -0.093 dyne, ${ }^{5}$ giving a total gravity departure of -0.112 dyne. The gravity departure at Pikes Peak is sufficient to cause the barometer to read 0.004 inch or o. 10 mm . low, while the departure at Seattle is sufficient to cause the barometer to read 0.003 inch or 0.09 mm . high, as compared with what the readings would have been with gravity at normal intensity for the latitudes of the respective stations.

From the foregoing it is evident that the value of local gravity, $g_{l}$, at the observing station must be determined before the barometer reading can be accurately reduced to standard gravity. In many cases, and especially at sea, it is not practicable to measure $g_{2}$. In the United States its value may frequently be determined with sufficient accuracy in the following manner:
( i ) Compute $g_{\phi}$, mean gravity at sea level for the latitude of the station, from the equation ${ }^{6}$

$$
\begin{aligned}
g_{\phi} & =978.039\left(\mathrm{I}+0.005294 \sin ^{2} \phi-0.000007 \sin ^{2} 2 \phi\right), \\
& =980.621\left(\mathrm{I}-0.002640 \cos 2 \phi+0.000007 \cos ^{2} 2 \phi\right)
\end{aligned}
$$

(2) Correct $g_{\phi}$ for altitude by the equation ${ }^{7}$
$c($ dynes $)=-0.0003086 h$ (meters), or
$c($ dynes $)=-0.00009+h($ feet $)$,

[^4]where $h$ is the altitude of the station above sea level.
(3) Correct $g_{\phi}$ for gravity anomaly. ${ }^{1}$
(4) Finally, $g_{\phi}$ is to be corrected for topograply and isostatic compensation. ${ }^{2}$

## Example:

To determine the value of local gravity, $g_{1}$, at the Weather Bureaut Office, Atlanta, Ga., latitude $33^{\circ} 45^{\prime}$ N., longitude $84^{\circ} 23^{\prime}$ W., height of barometer above sea level, i2I 8 feet.
From Table 90, mean sea level gravity for latitude $33^{\circ} 45^{\prime} \quad=979.631$ dynes.
Correction for height of barometer
$(-0.00009+1218)=-0.114$ "
$\begin{array}{llll}\text { Correction for gravity anomaly, } & =-0.023 & " \\ \text { Correction for topography and compensation } & =+ & 0.014\end{array}$
Correction for topography and compensation
Local gravity at Weather Bureau Office, Atlanta,
Ga. $=979.508$ dynes.
Having determined $g_{l}$, the reduction of barometer readings to standard gravity is easily and accurately accomplished by multiplying by the ratio $g_{l} / g_{0}$, or by applying a correction to the barometer reading, otherwise corrected, derived from the expression $\frac{\left(g_{l}-g_{0}\right)}{g_{0}} B$. With $g_{l}<g_{0}$ the correction is to be subtracted; with $g_{l}>g_{0}$ the correction is to be added. In general, sufficient accuracy will be attained by computing the gravity correction for a station once for all from the equation $C=B_{n} \frac{\left(g_{1}-g_{0}\right)}{g_{0}}$, in which $B_{n}$ is the normal station barometer pressure, and $C$ is expressed in the same umits as $B_{n}$.

Table 48 gives corrections to reduce barometer readings to standard gravity. The top argument is the barometer reading. The side argument is the difference, $g_{l}-g_{0}$, for each tenth of a dyne up to 4.0 dynes. The relation is a linear function of both $g_{l}-g_{0}$ and $B$, and for barometer readings 10 or roo times greater than those given in the argument the correction may be obtained by removing the decimal point in the tabulated values one or two places, respectively, to the right. The correction obtained will be expressed in the same units as the barometer reading to be corrected.

## Example I.

The barometer reading corrected for temperature is 29.647 inches, and the local value of gravity is 978.08 . The difference, $g_{l}-g_{0},=-2.585$. From the table,
the correction for a barometer reading of 20 inches $=-0.0527 \mathrm{in}$. the correction for a barometer reading of 9 inches $=-0.0237 \mathrm{in}$. the correction for a barometer reading of 0.65 inches Correction for a barometer reading of 29.65 inches Corrected barometer reading $=29.647 \mathrm{in} .-0.078 \mathrm{in}$.
$=-0.0017 \mathrm{in}$.
$=-\overline{0.078} \mathrm{in}$.
$=29.569$ in.

[^5]
## Example 2.

The barometer reading reduced to $0^{\circ} C$ is 637.42 mm ., and the local value of gravity is 98I.5I. The difference, $g_{l}-g_{0}=+0.845$. From the table,
the correction for a barometer reading of 600 mm . the correction for a barometer reading of 30 mm . the correction for a barometer reading of 7 mm . Correction for a barometer reading of 637.4 mm . Corrected barometer reading $=637.42+0.55$
$=+0.517 \mathrm{~mm}$.
$=+0.026 \mathrm{~mm}$.
$=+\underline{0.006} \mathrm{~mm}$.
$=+0.55 \mathrm{~mm}$.
$=+637.97 \mathrm{~mm}$.

In the case of barometer readings made at sea, and also at some land stations, it is not practicable to determine local gravity with greater accuracy than it can be computed from the equations for variations with latitude and altitude given above. The reduction to standard gravity, accordingly, consists of two parts-a correction for altitude, and a correction from the computed sea-level gravity for the latitude of the station to standard gravity. The first part of the correction, or the correction for altitude, may be computed once for all from the expression $\mathrm{c}=-0.0003086 h B_{n}$ (metric measures), or $\mathrm{c}=-0.000094 h B_{n}$ (English measures), and is usually combined with the reduction of the barometer to sea level or to some other reference plane. The second part has heretofore consisted of a correction for the difference between the mean value of gravity for the latitude of the station and for latitude $45^{\circ}$; and, in accordance with the equation given above, it may be derived from the expression

$$
\left(-0.002640 \cos 2 \phi+0.000007 \cos ^{2} 2 \phi\right) B
$$

where $\phi$ is the latitude of the station, and $B$ is the barometer reading. The value of the ratio $\frac{g_{45} \cdot-g_{0}}{g_{0}}=\frac{980.62 \mathrm{I}-980.665}{980.665}=-0.000045$. Therefore, the expression for the gravity correction becomes

$$
\left(-0.00264 \cos 2 \phi+0.000007 \cos ^{2} 2 \phi-0.000045\right) B
$$

Table 49 (English measures) gives the corrections in thousandths of an inch for every degree of latitude and for each inch of barometric pressure from 19 to 30 inches, to reduce barometer readings to standard gravity, computed from the equation

$$
C=\left(-0.00264 \cos 2 \phi+0.000007 \cos ^{2} 2 \phi-0.000045\right) B
$$

Table 50 (metric measures) gives the same corrections in hundredths of a millimeter for each 20 millimeters barometric pressure from 520 to 780 millimeters.

## Example:

Barometric reading (corrected for temperature) at latitude
$63^{\circ} 55^{\prime}$,
Correction to standard gravity, Table 49,
Barometer reduced to standard gravity,
$=27.434$ inches
$=0.043$ inches
$=27.477$ inches

The adoption of this new value for standard gravity may require a slight correction to old barometric records in order to make the entire series of readings homogeneous. The amount of this correction will be the difference between the gravity correction computed by these new tables and by the old tables.

## Example:

Seattle, Wash., Lat. $47^{\circ} 38^{\prime}$ N., Long. $122^{\circ} 20^{\prime}$ W., height of barometer above sea level 125 feet, normal station barometer 29.89 inches.
$g_{\phi}$ (Table 90)
Correction for height ( $-0.000094 \times 125$ )
$=\quad 980.859$ dynes.
$=-\quad$ 012 "
$=-\quad .019 \quad$ "
$=-\frac{.093}{980.735}$ dynes.
Correction to reduce barometer readings to standard gravity, $980.735-980.665 B_{n}=+0.002$ inch. Old correction, +0.007 ; correction to old 980.665
records $=0.002 \mathrm{in} .-0.007 \mathrm{in} .=-0.005 \mathrm{in}$.
For correcting back records of readings at sea, or at any place where the value of local gravity cannot be determined, the correction is equal to the ratio $\frac{980.599-980.665}{980.665} B=-0.000067 B$. The corrections are as follows :

Barometer reading.
From 8 to 22 inches
From 23 to 32 inches
From 380 to 520 mm .
From 530 to 670 mm .
From 680 to 820 mm .

Correction.

- o.00I in.
-0.002 in.
-0.03 mm .
-0.04 mm .
-0.05 mm .


## REDUCTION OF BAROMETER READINGS TO SEA LEVEL.

Tables 5I to 63 inclusive, " Determinations of Heights by the Barometer," may be used for reducing barometric readings to sea level, provided the mean temperature and vapor pressure of the atmosphere between the observing station and sea level are known.

See "Example: (English Measures)," p. xlix.
Barometer at upper station corrected for temperature $=23.6 \mathrm{I} \mathrm{in}$.
Mean temperature of air column, $\theta, \quad=35^{\circ} \cdot \mathrm{F}$.
Latitude of station, $\phi$,
Altitude of station above mean sea level, $Z, \quad=6320 \mathrm{ft}$.
The equation for computing the altitude $Z$ is given on $p$. xlvii. This equation is simplified after justifiable approximations to the form (in English units)

$$
\begin{gathered}
62583.6\left(\log \frac{29.9}{B}-\log \frac{29.9}{B_{0}}\right)= \\
Z-Z\left[0.002039\left(\theta-50^{\circ}\right)+0.378 \frac{e}{b}+(\gamma+\eta)+\frac{Z+2 h_{0}}{R}\right]
\end{gathered}
$$

where the terms are as defined on Pp . xliv to xlvi, inclusive. Calling the terms in the bracket $(a),(b),(c)$ and $(d)$, respectively, to compute $B_{0}$ we have:
from Table 52 with $Z=6320$ feet and $\theta=35^{\circ} \circ \mathrm{F} ., \quad Z(a)=-194$
from Table $5+$ with $Z=6320$ feet and average humidity, $Z(b)=+16$
from Table 53 with $Z=6320$ feet and $\phi=44^{\circ} 16^{\prime}, \quad Z(c)=+16^{1}$
from Table 55 with $Z=6320$ feet and $h_{0}=0, \quad \underline{Z}(d)=+2$

$$
Z[(a)+(b)+(c)+(d)]=
$$

$=-160$.

Then since $Z=6320$ feet we have

$$
62583.6\left(\log \frac{29.9}{B}-\log \frac{29.9}{B_{0}}\right)=6320+160=6480 .
$$

From Table 5I for $B=23.6 \mathrm{I}$ in., we have

$$
\begin{aligned}
& 62583.6 \log \frac{29.9}{B}=6420, \text { hence } \\
& 62583.6 \log \frac{29.9}{B_{0}}=6420-6+80=-60
\end{aligned}
$$

Referring to Table 51 for the value of $B_{0}$ corresponding to this, we find $B_{0}=29.966 \mathrm{in}$.

See " Example: (Metric Measures)," p. lii.
Let, the barometric reading (reduced to $\mathrm{o}^{\circ} \mathrm{C}$.),
the mean temperature of the air column,
the mean vapor pressure of the air column,
the latitude,
the altitude of the station,

$$
\begin{aligned}
& B=655.7 \mathrm{~mm} ., \\
& \theta=12.3 \mathrm{C} ., \\
& e=9 \mathrm{mmm.} \\
& \phi=32^{\circ}, \\
& Z=1379 \text { meters. }
\end{aligned}
$$

The equation for computing $Z$ is simplified to the closely approximate form (from p. 1; for metric units)

$$
\begin{gathered}
18400\left(\log \frac{760}{B}-\log \frac{760}{B_{0}}\right)= \\
Z-Z\left[0.00367 \theta+0.378 \frac{e}{b}+(\gamma+\eta)+\frac{Z+2 h_{0}}{R}\right]
\end{gathered}
$$

where the terms are as defined on pp. xliv-xlvi.
Again calling the terms in the bracket $(a),(b),(c)$ and $(d)$, respectively, to compute $B_{0}$ we have:
from Table 59, with $Z=1379 \mathrm{~m}$. and $\theta=12^{\circ} \cdot 3 \mathrm{C} ., \quad Z(a)=62$
from Table 60, with $Z=1379 \mathrm{~m}$. and $e=9 \mathrm{~mm}$., $Z(b)=7$
from Table 62, with $Z=1379 \mathrm{~m}$. and $\phi=32^{\circ}, \quad Z(c)=5^{1}$
from Table 63 , with $Z=1379 \mathrm{~m}$. and $h_{0}=0$,
$\begin{array}{r}Z(d)=0 \\ \hline=7 t\end{array}$
Since $Z=1379 \mathrm{~m}$., we have

$$
18400\left(\log \frac{760}{B}-\log \frac{760}{B_{0}}\right)=1379-74=1305
$$

From Table 56 for $B=655.7 \mathrm{~mm}$., we have i $8400 \log \frac{760}{B}=$ II 79 , hence ェ $8400 \log \frac{760}{B_{0}}=$ ェ1 $79-$ I $305=-$ 126 .
Referring to Table 56 for the value of $B_{0}$ corresponding to this, we find $B_{0}=772.1 \mathrm{~mm}$.

There are no difficulties connected with the use of these tables to reduce barometric readings to sea level, but serious difficulties are often encountered in attempting to determine $\theta$ and $e$ from observations at the elevated station only (see pp. xxxiii and lxxii).

[^6]
## TABLES FOR DETERMINING HEIGHTS, AND CONVERSIONS

 INVOLVING GEOPOTENTIAL.
## THE HYPSOMETRIC FORMULA AND ITS CONSTANTS.

The fundamental formula for reducing the barometer to sea level and for determining heights by the barometer is the original formula of Laplace, amplified into the following form -
(I) $Z=K(\mathrm{I}+\alpha \theta)\left(\frac{\mathrm{I}}{\mathrm{I}-0.3788_{\bar{b}}^{e}}\right)\left(\mathrm{I}+\frac{g_{0}-g_{i}}{g_{0}}\right)\left(\mathrm{I}+\frac{h+h_{0}}{R}\right) \log \frac{p_{0}}{p}$,
or, where $g_{l}$, the value of local gravity is unknown,

$$
\begin{equation*}
Z=K(\mathrm{I}+a \theta)\left(\frac{\mathrm{I}}{\mathrm{I}-0.378_{\bar{b}}^{e}}\right)\left(\mathrm{I}+k \cos 2 \phi-k^{\prime} \cos ^{2} 2 \phi+\mathrm{C}\right)\left(\mathrm{I}+\frac{h+h_{0}}{R}\right) \log \frac{p_{0}}{p} \tag{2}
\end{equation*}
$$

in which $\quad h=$ Height of the upper station.
$h_{\circ}=$ Height of the lower station.
$Z=h-h_{0}$.
$p=$ Atmospheric pressure at the upper station.
$p_{0}=$ Atmospheric pressure at the lower station.
$R=$ Mean radius of the earth.
$\theta=$ Mean temperature of the air column between the altitudes $h$ and $h_{0}$.
$e=$ Mean pressure of aqueous vapor in the air column.
$b=$ Mean barometric pressure of the air column.
$\phi=$ Latitude of the stations.
$K=$ Barometric constant.
$a=$ Coefficient of the expansion of air.
$k$ and $k^{\prime}=$ Constants depending on the figure of the earth.

$$
\begin{aligned}
C & =\text { Constant }=\text { the ratio } \frac{g_{45^{\circ}}-g_{0}}{g_{0}} . \\
g_{0} & =\text { Standard value of gravity }=980.665 \text { dynes. } \\
g_{l} & =\text { Local value of gravity. }
\end{aligned}
$$

The pressures $p_{0}$ and $p$ are computed from the height of the column of mercury at the two stations; the ratio $\frac{B_{0}}{B}$ of the barometric heights may be substituted for the ratio $\frac{p_{0}}{p}$, if $B \circ$ and $B$ are reduced to the values that would be measured at the same temperature and under the same relative value of gravity.

The correction of the observed barometric heights for instrumental temperature is always separately made, but the correction for the variation of gravity with altitude is generally introduced into the formula itself.

If $B_{0}, B$ represent the barometric heights corrected for temperature only, we have the equation

$$
\frac{p_{0}}{p}=\frac{B_{0}}{B}\left(1+\mu \frac{Z}{R}\right),
$$

$\mu$ being a constant depending on the variation of gravity with altitude $\left(\frac{\mu}{R}=0.0000003\right)$, and

$$
\log \frac{p_{\circ}}{p}=\log \frac{B_{0}}{B}+\log \left(\mathrm{I}+\mu \frac{Z}{R}\right)
$$

Since $\frac{\mu Z}{R}$ is a very small fraction, we may write

$$
\text { Nap. } \log \left(1+\frac{\mu Z}{R}\right)=\frac{\mu Z}{R}, \text { and } \log \left(1+\frac{\mu Z}{R}\right)=\frac{\mu Z}{R} M
$$

$M$ being the modulus of common logarithms.
By substituting for $Z$ its approximate value $Z=K \log \frac{B_{0}}{B}$, we have

$$
\log \left(1+\frac{\mu Z}{R}\right)=\frac{\mu K}{R} M \log \frac{B_{0}}{B}
$$

With these substitutions the barometric formula becomes

$$
\begin{align*}
Z= & K(\mathrm{I}+a \theta)\left(\frac{\mathrm{I}}{\mathrm{I}-0.378_{b}^{\frac{e}{b}}}\right)\left(\mathrm{I}+\frac{g_{0}-g_{l}}{g_{0}}\right)\left(\mathrm{I}+\frac{h+h_{\mathrm{o}}}{R}\right) \times  \tag{I}\\
& \left(\mathrm{I}+\frac{\mu K}{R} M\right) \log \frac{B_{\circ}}{B}, \text { or }
\end{align*}
$$

(2) $Z=K(\mathrm{I}+\alpha \theta)\left(\frac{\mathrm{I}}{\mathrm{I}-0.3-8_{b}^{e}}\right)\left(\mathrm{I}+k \cos 2 \phi-k^{\prime} \cos ^{2} 2 \phi+C\right)\left(\mathrm{I}+\frac{h+h_{0}}{R}\right) \times$

$$
\left(\mathrm{I}+\frac{\mu K}{R} M\right) \log \frac{B_{0}}{B}
$$

As a further simplification we shall put

$$
\beta=0.378 \frac{e}{b}, \gamma=k \cos 2 \phi-k^{\prime} \cos ^{2} 2 \phi+C \text { and } \eta=\frac{\mu K}{R} M
$$

and write for the second form, (2), the formula --

$$
Z=K(\mathrm{I}+\alpha \theta)\left(\frac{\mathrm{I}}{\mathrm{I}-\beta}\right)(\mathrm{I}+\gamma)\left(\mathrm{I}+\frac{h+h_{0}}{R}\right)(\mathrm{I}+\eta) \log \frac{B_{0}}{B}
$$

Values of the constants. - The barometric constant $K$ is a complex quantity defined by the equation

$$
K=\frac{\Delta \times B_{n}}{\dot{\delta} \times M}
$$

$B_{n}$ is the normal barometric height of Laplace, 760 mm .
$\Delta$ is the density of mercury at the temperature of melting ice. The value adopted by the International Meteorological Committee, and which has been employed in previous editions of these tables is $\Delta=13.5956$. The
most probable value, taking into account the recently determined relation between the liter and the cubic decimeter, ${ }^{1}$ is as already stated, $\Delta=13.595 \mathrm{I}$ and this value is here adopted.
$\delta$ is the density of dry air at $0^{\circ} \mathrm{C}$ under the pressure of a column of mercury $B_{n}$ and under standard gravity. The value adopted by the International Bureau of Weights and Measures for air under the above conditions and free from $\mathrm{CO}_{2}$ is $\delta=0.0012928$ grams per cubic centimeter. ${ }^{2}$ This is in close agreement with the value ( $\delta=0.00129278$ ) used in previous editions of these tables. For air containing 4 parts in 10000 of $\mathrm{CO}_{2}$ it gives a density of o.00129307, and for air containing 3 parts in 10000 of $\mathrm{CO}_{2}$, the proportion adopted by Hann, ${ }^{3}$ it gives a density of 0.0012930I. Therefore, the value adopted for the density of air containing an average amount of $\mathrm{CO}_{2}$ is

$$
\delta=0.0012930
$$

$M$ (Modulus of common logarithms) $=0.4342945$. These numbers give for the value of the barometric constant

$$
K=18400 \text { meters. }
$$

For the remaining constants, the following values have been used:
$\alpha=0.00367$ for $I^{\circ}$ Centigrade. (International Bureau of Weights and Measures: Travaux et Mémoires, t. I, p. A. 54.)
$\gamma=k \cos 2 \phi-k^{\prime} \cos ^{2} 2 \phi+C=0.002640 \cos 2 \phi-0.000007 \cos ^{2} 2 \phi+$ 0.000045
$R=6367324$ meters. (A. R. Clarke: Geodesy, $8^{\circ}$, Oxford, i88o.)
$\eta=\frac{\mu K M}{R}=0.002396$. (Ferrel: Report Chief Signal Officer, 1885, pt. 2, pp. 17 and 393.)

TABLES 51, 52, 53, 54, 65 ,
THE DETERMINATION OF HEIGHTS BY THE BAROMETER.
Tables 51,52,53,54,55.

## English Measures.

Since a barometric determination of the height will rarely be made at a place where $g_{l}$ is known, the discussion which follows will be confined to the second form of the barometric formula developed in the preceding section (sce page xly). For convenience in computing heights it is arranged in the following form:

$$
Z=K\left(\log B_{\circ}-\log B\right)\left[\begin{array}{l}
(\mathrm{I}+\alpha \theta) \\
(\mathrm{I}+\beta) \\
\left(\mathrm{I}+k \cos 2 \phi-k^{\prime} \cos ^{2} 2 \phi+C\right)(\mathrm{I}+\eta) \\
\left(\mathrm{I}+\frac{Z+2 h_{\circ}}{R}\right)
\end{array}\right]
$$

[^7]in which $K\left(\log B_{\circ}-\log B\right)$ is an approximate value of $Z$ and the factors in the brackets are correction factors depending respectively on the air temperature, the humidity, the variation of gravity with latitude, the variation of gravity with altitude in its effect on the weight of mercury in the barometer, and the variation of gravity with altitude in its effect on the weight of the air. With the constants already given, the formula becomes in English measures:
\[

Z(feet)=60368^{1}\left(\log B_{0}-\log B\right)\left[$$
\begin{array}{l}
{\left[\mathrm{I}+0.002039\left(\theta-32^{\circ}\right)\right]} \\
(\mathrm{I}+\beta) \quad \\
\left(\mathrm{I}+0.00264 \mathrm{o} \cos 2 \phi-0.000007 \cos ^{2} 2 \phi\right. \\
+0.000045)(\mathrm{I}+0.00239) \\
\left(\mathrm{I}+\frac{Z+2 h_{\mathrm{o}}}{R}\right)
\end{array}
$$\right]
\]

In order to make the temperature correction as small as possible for average air temperatures, $50^{\circ} \mathrm{F}$. will be taken as the temperature at which the correction factor is zero. This is accomplished by the following transformation:

$$
1+0.002039\left(\theta-32^{\circ}\right)=\left[1+0.002039\left(\theta-50^{\circ}\right)\right]\left[1+0.0010195 \times 36^{\circ}\right] .
$$

The second factor of this expression combines with the constant, and gives $60368\left(\mathrm{I}+0.0010195 \times 36^{\circ}\right)=62583.6$.

The first approximate value of $Z$ is therefore

$$
62583.6\left(\log B_{0}-\log B\right) .
$$

In order further to increase the utility of the tables, we shall make a further substitution for $\log B_{\circ}-\log B$, and write

$$
62583.6\left(\log B_{0}-\log B\right)=62583.6\left(\log \frac{29.9}{B}-\log \frac{29.9}{B_{\circ}}\right) .
$$

Table 51 contains values of the expression

$$
62583.6 \log \frac{29.9}{B}
$$

for values of $B$ varying by intervals of 0.01 inch from 12.00 inches to 30.90 inches.

The first approximate value of $Z$ is then obtained by subtracting the tabular value corresponding to $B_{\circ}$ from the tabular value corresponding to $B$ ( $B$ and $B_{\circ}$ being the barometric readings observed and corrected for temperature at the upper and lower stations respectively).

Table 52 gives the temperature correction

$$
Z \times 0.002039\left(\theta-50^{\circ}\right)
$$

[^8]The side argument is the mean temperature of the air column ( $\theta$ ) given for intervals of $\mathrm{I}^{\circ}$ from $0^{\circ}$ to $100^{\circ} \mathrm{F}$. The top argument is the approximate difference of altitude $Z$ obtained from Table 5I.

For temperatures above $50^{\circ} \mathrm{F}$., the correction is to be added, and for temperatures below $50^{\circ} \mathrm{F}$., the correction is to be subtracted. It will be observed that the correction is a linear function of $Z$, and hence, for example, the value for $Z=1740$ is the sum of the corrections in the columns headed 1000,700 , and 40 .

In general, accurate altitudes cannot be obtained unless the temperature used is freed from diurnal variation.

Table 53 gives the correction for gravity, and for the effect of the variation of gravity with altitude on the weight of the mercury. When altitudes are determined with aneroid barometers the second factor does not enter the formula. In this case the effect of the latitude factor can be obtained by taking the difference between the tabular value for the given latitude and the tabular value for latitude $45^{\circ} 29^{\prime}$. The side argument is the latitude of the station given for intervals of $2^{\circ}$. The top argument is the approximate difference of height $Z$.

Table 54 gives the correction for the average humidity of the air at different temperatures. In evaluating the humidity factor as a function of the air temperature, the tables given by Prof. Ferrel have been adopted (Metcorological researches. Part iii. - Barometric hypsometry and reduction of the barometer to sea level. Report, U.S. Coast Survey, I88r. Appendix io.) These tables by interpolation, and by extrapolation below $o^{\circ} \mathrm{F}$., give the following values for $\beta$ :

For Fahrenheit temperatures,

| $\theta$ | $\beta$ | $\theta$ | $\beta$ | $\theta$ | $\beta$ | $\theta$ | $\beta$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. |  | F. |  | $F$. |  | F. |  |
| $-20^{\circ}$ | 0.00008 | $10^{\circ}$ | 0.00104 | $36^{\circ}$ | 0.00267 | $62^{\circ}$ | 0.00724 |
| - 16 | . 00020 | 12 | . 00111 | 38 | . 00293 | 64 | . 00762 |
| - 12 | . 00032 | 14 | .00118 | 40 | . 00322 | 66 | . 00801 |
| - 8 | . $000+4$ | 16 | .00126 | 42 | . 00353 | 68 | . 00839 |
|  |  | 18 | . 00134 | 44 | . 00386 | 70 | . 00877 |
| -6 | 0.00050 | 20 | . 00143 | 46 | . 0042 I | 72 | .00914 |
| - 4 | . 00056 | 22 | . 00153 | 48 | . 00458 |  |  |
| $-2$ | . 00062 | 24 | . 00163 | 50 | . 00496 | ${ }_{7} 6$ | 0.00990 |
|  | . 00068 | 26 | . 00174 | 52 | . 00534 | So | . 01065 |
| $+2$ | . 00075 | 28 | . 00187 | 54 | . 00572 | 84 | . OII4 1 |
|  | . 00082 | 30 | . 00203 | 56 | . 00610 | 88 | . 01217 |
| 6 | . 00089 | 32 | . 00222 | 58 | . 00648 | 92 | . O1293 |
| 8 | . 00006 | 34 | . 00243 | 60 | . 00686 | 96 | . 01369 |

This correction could have been incorporated with the temperature factor in Table 52, but it is given separately in order that the magnitude of the correction may be apparent, and in order that, when the actual hu-
midity is observed, the correction may be computed if desircd, by the expression

$$
Z\left(0.378 \frac{e}{b}\right)
$$

where $e$ is the mean pressure of vapor in the air column, and $b$ the mean barometric pressure.

The side argument is the mean temperature of the air column, varying by intervals of $2^{\circ}$ from $-20^{\circ} \mathrm{F}$. to $96^{\circ} \mathrm{F}$., except near the extremities of the table where the interval is $4^{\circ}$. The top argument is the approximate difference of altitude $Z$.

Table 55 gives the correction for the variation of gravity with altitude in its effect on the weight of the air. The side argument is the approximate difference of altitude $Z$, and the top argument is the elevation of the lower station $h_{0}$.

The corrections given by Tables 53, 54, and 55 are all additive.

## Example:

Let the barometric pressure observed, and corrected for temperature, at the upper and lower stations be, respectively, $B=23.61$ and $B_{\circ}=29.97$. Let the mean temperature of the air column be $35^{\circ}$ $F$., and the latitude $44^{\circ} 16^{\prime}$. To determine the difference of height.

| Table 51, argument 23.61, gives | Feet. 6420 |
| :---: | :---: |
| Table 51, " 29.97 , | 64 |
| Approximate difference of height ( $Z$ ) | $\overline{6484}$ |
| Table 52, with $Z=6484$ and $\theta=35^{\circ} \mathrm{F}$, gives | - 198 |
| Table 53, with $Z=6300$ and $\phi=44^{\circ}$, gives | + 16 |
| Table 54, with $Z=6300$ and $\theta=35^{\circ} \mathrm{F}$., gives |  |
| Table 55, with $Z=6300$ and $h_{\circ}=0$, gives |  |
| Final difference of height ( $Z$ ) | = 632 |

If in this example the barometric readings be observed with aneroid barometers, the correction to be obtained from Table 53 will be simply the portion due to the latitude factor, and this will be obtained by subtracting the tabular value for $45^{\circ} 29^{\prime}$ from that for $44^{\circ}$, the top argument being $Z=6300$. This gives $16-15=1$.

Tables 56, 57, 58, 59, 60, 61, 62, 63.

## Metric and Dynamic Measures.

The barometric formula developed on page xlvi is, in metric and dynamic units,
$Z$ (meters $)=18400\left(\log B_{0}-\log B\right)\left[\begin{array}{l}(1+0.00367 \text { ol } C) \\ \left(1+0.378 \frac{e}{b}\right) \\ \left(1+0.002640 \cos 2 \phi-0.000007 \cos ^{2} 2 \phi\right. \\ +0.000045)(1+0.00239) \\ \left(1+\frac{Z+2 h_{0}}{6367324}\right)\end{array}\right]$
The approximate value of $Z$ (the difference of height of the upper and lower station) is given by the factor $18400\left(\log B_{\circ}-\log B\right)$. This expression is computed by means of two entries of a table whose argument is the barometric pressure. In order that the two entries may result at once in an approximate value of the elevation of the upper and lower stations, a transformation is made, which gives the following identities:
I $8400\left(\log B_{\circ}-\log B\right)=\mathrm{I} 8400\left(\log \frac{760}{B}-\log \frac{760}{B_{\circ}}\right)$ - Metric measures, and $18400\left(\log B_{\circ}-\log B\right)=18,00\left(\log \frac{1013.3}{B}-\log \frac{1013.3}{B_{0}}\right)$-Dynamic measures.

Table 56 gives values of the expression $18400 \log \frac{760}{B}$ for values of $B$ varying by intervals of 1 mm . from 300 mm . to 779 mm . The first approximate value of $Z$ is then obtained by subtracting the tabular value corresponding to $B_{\circ}$ from the tabular value corresponding to $B$ ( $B$ and $B_{\circ}$ being the barometric readings observed and reduced to $0^{\circ} C$. at the upper and lower stations respectively). The first entry of Table 56 with the argument $B$ gives an approximate value of the elevation of the upper station above sea level, and the second entry with the argument $B$ ogives an approximate value of the elevation of the lower station.

Table 57 gives values of the expression $18400 \log \frac{1013.3}{b}$ for values of $B$ varying by intervals of 1 mb . from o mb. to 1049 mb . The approximate value of $Z$ is then obtained by subtracting the tabular value corresponding to $B_{0}$ from the tabular value corresponding to $B$ ( $B$ and $B_{0}$ being the barometric readings observed and reduced to $0^{\circ} C$. at the upper and lower stations respectively). The first entry of Table 57 with the argument $B$ gives an approximate value of the elevation of the upper station above sea level, and the second entry with the argument $B_{\circ}$ gives an approximate value of the elevation of the lower station.

Table 58 gives the temperature correction factor, $a=0.00367 \theta$, for each tenth of a degree centigrade, from $0^{\circ} \mathrm{C}$. to $50.9^{\circ} \mathrm{C}$. To find the correction corresponding to any mean temperature of the air column, $\theta$, multiply the approximate altitude as determined from Table 56 or 57 by the value of $a$ obtained from this table, and add the result if $\theta$ is above $0^{\circ} C$.; subtract, if below $\mathrm{O}^{\circ} \mathrm{C}$.

Attention is called to the fact that the formula is linear with respect to $\theta$, and hence that the correction, for example, for $59^{\circ} .8 \mathrm{C}$. equals the correction for $50^{\circ} .8$ plus the correction for $9^{\circ}$ or $.186+.033=.219$, and is to be added.

Table 59 is an amplification of Table 58 and gives the temperature correction $0.00367 \theta \times Z$.

The side argument is the approximate difference of elevation $Z$ and the top argument is the mean temperature of the air column. The values of $Z$ vary by intervals of 100 m . from 100 to 4000 meters and the temperature varies by intervals of $\mathrm{I}^{\circ}$ from $\mathrm{I}^{\circ} \mathrm{C}$. to $10^{\circ} \mathrm{C}$. with additional columns for $20^{\circ}, 30^{\circ}$, and $40^{\circ} \mathrm{C}$. This formula also is linear with respect to $\theta$, and hence the correction, for example, for $27^{\circ}$ equals the correction for $20^{\circ}$ plus the correction for $7^{\circ}$. When the table is used for temperatures below $0^{\circ} \mathrm{C}$. the tabular correction must be subtracted from, instead of added to, the approximate value of $Z$.

Table 60 (pp. 148 and i49) gives the correction for humidity resulting from the factor $0.378 \frac{e}{b} \times Z=\beta Z$.

Page 148 gives the value of $0.378 \frac{e}{b}$ multiplied by 10000 . The side argument is the mean pressure of aqueous vapor, $e$, which serves to represent the mean state of humidity of the air between the two stations. $e=\frac{1}{2}\left(e_{\mathrm{I}}+e_{\mathrm{O}}\right)$ ( $e_{\mathrm{I}}$ and $e_{\mathrm{O}}$ being the vapor pressures observed at the two stations) has been written at the head of the table, but the value to be assigned to $e$ is in reality left to the observer, independently of all hypothesis. The top argument is the mean barometric pressure $\frac{1}{2}\left(B+B_{0}\right)$.

The vapor pressure varies by millimeters from 1 to 40 , and the mean barometric pressure varies by intervals of 20 mm . from 500 mm . to 760 mm . The tabular values represent the humidity factor $\beta$, or $0.378 \frac{e}{b}$, multiplied by IOOOO.

Page 149 gives the correction for humidity, with $Z$ and $10000 \times 0.378 \frac{e}{b}$ (derived from page 148 ) as arguments.

The approximate difference of altitude is given by intervals of 100 meters from 100 to 4000 meters, with additional lines for 5000,6000 , and 7000 meters. The values of $10000 \beta$ vary by intervals of 25 from. 25 to 300 . The tabular values are given in tenths of meters to facilitate and increase the accuracy of interpolation.

Table 61. Humidity correction: Value of $\frac{1}{2}\left(\frac{0.378 \frac{e}{b}}{0.00367}\right)$. It has been found advantageous to express the humidity term, $\beta Z$, as a correction to the temperature term, a $\theta Z$.

Let $a \Delta \theta Z=\beta Z$; then,

$$
\Delta \theta=\frac{\beta}{a}=\frac{0.378 \frac{e}{b}}{0.00367}
$$

For convenience in computing, the tabulated values of $\Delta \theta$ are for $\frac{1}{2}\left(\frac{0.378^{\frac{e}{b}}}{0.00367}\right)$. The side and top arguments are air and vapor pressures, respectively, in mm. on p. 150 and in mb. on p. 151. Instead of computing $\Delta \theta$ from the mean of the values of $B$ and $e$ at the upper and lower stations it is computed for each station separately, and the sum of the two determinations is added to $\theta$.

Table 62 gives the correction for gravity, and for the effect of the variation of gravity with altitude on the weight of the mercurial column. When altitudes are determined with aneroid barometers the latter factor does not enter the formula. In this case the effect of the latitude factor can be obtained by subtracting the tabular value for latitude $45^{\circ} 29^{\prime}$ from the tabular value for the latitude in question.

The side argument is the approximate difference of elevation $Z$ varying by intervals of 100 meters from 100 to 4000 , and by 500 meters from 4000 to 7000 . The top argument is the latitude, varying by intervals of $5^{\circ}$ from $o^{\circ}$ to $75 .^{\circ}$

Table 63 gives the correction for the variation of gravity with altitude in its effect on the weight of the air.

The side argument is the same as in Table 62; the top argument is the height of the lower station, varying by intervals of 200 meters from o to 2000, with additional columns for 2500,3000 and 4000 meters.

The corrections given in Table 62 and Table 63 apply to the approximate heights computed from metric or dynamic measures by the use of Tables 56 to 61 , inclusive, and are additive.

## Example: (Metric Measures.)

Let the barometric reading (reduced to $0^{\circ} \mathrm{C}$.) at the upper station be 655.7 mm .; at the lower station, 772.4 mm . Let the mean temperature of the air column be $\theta=12^{\circ} .3 \mathrm{C}$., the mean vapor pressure $e=$ 9 mm . and the latitude $\phi=32^{\circ}$.
Table 56 , with argument 655.7 , gives 1179 meters.
Table 56, " " 772.4, " - $\mathbf{1 2 9}$
Approximate value of $Z=1308$
Table 59, with $Z=1308$ and $\theta=12.3 C$, gives 59
Table 60, with $e=9 \mathrm{~mm}$. and $Z=1370$, gives 7

Table 62, with $Z=1370$ and $\phi=32^{\circ}$, gives 5
Table 63 , with $Z=1370$ and $h_{0}=0$, gives
o
Corrected value of $Z \quad=\overline{1379}$ meters.

## Example: (Dynamic Measures.)

Let the barometer reading (reduced to $0^{\circ} \mathrm{C}$.) at the upper station be 448.6 mb .; at the lower station, 1000.3 mb . Let the vapor pres-
sure at the upper station be 2.4 mb .; at the lower station 7.3 mb . Let the mean temperature of the air column be $\theta=5^{\circ} 8 \mathrm{C}$. and the latitude $\phi=39^{\circ} 25^{\prime} \mathrm{N}$.
Table 57, with argument 448.6, gives 651 I meters.
Table 57, with argument 1000.3, gives ${ }^{1} \mathrm{O}_{4}$
Approximate value of $Z \quad \overline{6407}$ meters.
Table 6I, with arguments 449 and 2.4 gives $\Delta \theta=0.3$
Table 61, with arguments 1000 and 7.3 gives $\Delta \theta=0.4$
Table 58 , with $\theta=5^{\circ} 8+0^{\circ} .7=6{ }^{\circ} 5$, and $Z=6407$ gives $6.407 \times 0.024=$ I 54
Table 62 with $Z=656 \mathrm{I}$ and $\phi=39^{\circ} 25^{\prime}$, gives 19
Table 63 with $Z=6561$ and $h_{0}=0$, gives
Corrected value of $Z$ $=\overline{6587}$ meters.

## GEOPOTENTIAL: DYNAMIC HEIGHTS.

In accordance with the "Règlement " ${ }^{1}$ of the Commission Internationale de la Haute Atmosphère adopted at the meeting held in London in April, 1925, heights in all forms and publications of the International Commission are to be measured as " geopotentials " in " dynamic meters " above sea level.

The geopotential or gravity potential of a point is defined numerically as the value of the potential energy relative to sea level of a unit-mass situated at the point.

The application of geopotential as a measure of height becomes more evident when it is seen that surfaces of equal geopotential are identical with horizontal or level surfaces, and due to the geographical variation of gravity, they are not surfaces equally distant from sea level. In this regard it may be emphasized that energy is involved in displacing a mass of air from one position to another in which the potential energy of the mass is different, whereas the displacement of air may take place along horizontal or equigeopotential surfaces without the gain or expenditure of potential energy once the air is in a state of uniform motion. The latter statement, on the contrary, does not hold for surfaces of equal geometric height above sea level.

For the purposes of dynamical meteorology, in making comparisons of vertical positions, certain advantages are derived by defining the height of points above sea level in terms of geopotential. Heights measured in this way

[^9]are called " dynamic heights," after Prof. V. Bjerknes, ${ }^{1}$ and indicate relative potential energies of unit-mass. Thus, points of equal " dynamic height" lie in horizontal or geopotential surfaces.

The geopotential of a point, from the definition, is equal to the work done in lifting a unit-mass from sea level to the point, and is defined precisely by the expression:

$$
\begin{equation*}
\Gamma=-\int_{0}^{h} g d h \tag{I}
\end{equation*}
$$

where $\quad g=$ acceleration of gravity
and $\quad h=$ geometric height of the point above sea level.
The dimensions of geopotential in the absolute system are $l^{2} / t^{2}$. Following the proposal of Prof. Bjerknes, ${ }^{1}$ the unit of dynamic height is called the " dynamic meter" and has the magnitude $10 m^{2} / \mathrm{sec}^{2}$ where $g$ is measured in $m / \mathrm{sec}^{2}$, and $h$ in meters.

The unit is chosen with this magnitude for convenience, since a change in elevation of one meter geometric height produces a change in dynamic height of approximately 98 per cent of one "dynamic meter," $i . e .$, within the range of the majority of present atmospheric observations.

## CALCULATION OF DYNAMIC HEIGHTS.

Equation (I) may be solved by substituting in it Helmert's ${ }^{2}$ equation for the decrease of acceleration of gravity with height :

$$
\begin{equation*}
g=-\left(g_{\phi}-0.000003086 h\right) \tag{2}
\end{equation*}
$$

where
$g_{\phi}=$ acceleration of gravity below given point at sea level, in $m / \mathrm{sec}^{2}$.
$g=$ acceleration of gravity at point whose elevation is $h$ above sea level.
$h=$ geometric height in meters, above sea level.
The minus sign is used because gravity is directed downwards and heights are measured upwards positively.

Equation (I) becomes:

$$
\begin{equation*}
H_{d}=\frac{\mathrm{I}}{\mathrm{IO}} \int_{0}^{h}\left(g_{\phi}-0.000003086 h\right) d h \tag{3}
\end{equation*}
$$

where $H_{d}=$ dynamic height, in dynamic meters.

[^10]The factor $\frac{I}{I O}$ is substituted in eq. (I) to convert to units of dynamic height in dynamic meters ( $10 \mathrm{~m}^{2} / \mathrm{sec}^{2}$ ).

Integrating (3), we obtain

$$
\begin{equation*}
H_{d}=\frac{g_{\phi}}{10} h-\mathrm{I} .543 \times \mathrm{IO}^{-7} h^{2} \tag{4}
\end{equation*}
$$

For a first approximation, we may neglect the term in $h^{2}$ and take $g_{\phi}=9.8 \mathrm{~m} / \mathrm{sec}^{2}$,
whence
and (6)

$$
\begin{align*}
H_{d} & =0.98 h, \text { approximately }  \tag{5}\\
h & =\mathrm{I} .02 H_{d}, \text { approximately. }
\end{align*}
$$

Geometric heights ( $h$ ) may be expressed in terms of dynamic heights $\left(H_{d}\right)$ by a convenient approximate relationship.

Substituting (6) in the $h^{2}$ term of (4) we obtain

$$
\begin{equation*}
h=\frac{10}{g_{\phi}} H_{d}+\frac{1 \mathrm{O}}{g_{\phi}} \mathrm{I} \cdot 543(\mathrm{I} . \mathrm{O})^{2} \cdot \mathrm{IO}^{-\tau} \cdot H_{d}^{2} \tag{7}
\end{equation*}
$$

which is simplified for computation by taking 9.8062 as $g_{\phi}$ in the second term, this being the mean value at latitude $45^{\circ}$ and sea level.

Thus (7) becomes

$$
\begin{equation*}
h=\frac{10}{y_{\phi}} H_{d}+\mathrm{I} .63 j \times \mathrm{Io}^{-7} H_{d}^{2} \text { approximately. } \tag{8}
\end{equation*}
$$

We are indebted to Prof. V. Bjerknes and his collaborators for the above formulation, and for tables $6_{4}, 6_{5}, 6_{7}$ and 68 , which are copied directly from their " Dynamical Meteorology and Hydrography." ${ }^{1}$

## DESCRIPTION AND USE OF TABLES 64 TO 68 INCLUSIVE.

The purpose of these tables is to convert from geometric heights to dynamic heights and vice versa. Tables 64,65 , and 66 are used to convert geometric meters to dynamic meters. Tables 66,67 , and 68 are used to convert dynamic meters to geometric meters.

TABLE 64. Heights reduced from meters to dynamic meters, the acceleration of gravity at sea lcvel bcing 9.So.
This table, computed by means of equation (4) above, makes possible the reduction of geometric heights to dynamic heights, the acceleration of gravity at sea level being $9.80 \mathrm{~m} / \mathrm{sec}^{2}$. In this table the side argument is geometric height above sea level by intervals of 1000 m ., and the top argument is geometric height by intervals of 100 m . The proportionality table at the foot of the main table makes it possible to obtain dynamic heights corresponding to any integral number of geometric meters from o to 30,000 .

[^11]Table 65. Corrections to Table 64 for values of the acceleration of grazity at sea level different from 9.80.
This table is computed from a modification of equation (4) arranged to give the increments of dynamic height corresponding to changes in $g_{\phi}$ from $9.80 \mathrm{~m} / \mathrm{sec}^{2}$. This form is $H_{d}=\left(0.980 h_{l}-\mathrm{I} .5+3 \times \mathrm{IO}^{-7} h^{2}\right)+\frac{g_{\phi}-9.80}{\mathrm{IO}} h$ the latter factor being the increment.

Corrections obtained from this table are applied to values obtained from Table 64 for stations whose latitude is such that $g_{\phi}$ differs from $9.80 \mathrm{~m} / \mathrm{sec}^{2}$. The side argument here is geometric height by intervals of 1000 m . and the top argument is $g_{\phi}$, the acceleration of gravity at sea level. Interpolations must be made for geometric heights which are not in even km. and for values of $g_{\phi}$ which lie between the values given at the top.

Table 66. Normal value of the acceleration of gravity at sea level.
This table has been computed by means of the U. S. Coast and Geodetic Survey Formula

$$
g_{\phi}=9.80621\left(\mathrm{I}-0.002640 \cos 2 \phi+0.000007 \cos ^{2} 2 \phi\right)
$$

where
$g_{\phi}=$ normal value of acceleration of gravity in $m / \mathrm{sec}^{2}$ at latitude $\phi$ at sea level. and $\phi=$ latitude in degrees.
The side argument is latitude by intervals of $10^{\circ}$, and the top argument is latitude by unit degrees from o to 9 . Thus the value of $g_{\phi}$ may be obtained for every degree of latitude. For stations whose latitude cannot be expressed in whole degrees, interpolations may be made for fractional parts of degrees, or reference may be made to Table go.

Table 67. Heights reduced from dynamic meters to geometric meters, the accelcration of gravity being 9.So.
This table, computed by means of equation (8) converts dynamic heights to geometric heights, where $g_{\phi}=9.80 \mathrm{~m} / \mathrm{sec}^{2}$. The side argument is dynamic height by intervals of 1000 dynamic meters and the top argument is dynamic height by intervals of 100 dynamic meters. A proportionality table is added as in Table 64.

Table 68. Corrcctions to Table 67 for values of the acceleration of gravity at sea level different from 9.80.
This table is computed from a modification of equation (8). The modified form employed is

$$
\begin{equation*}
h=\left(\frac{10}{9.80} H_{d}+1.637 \times 10^{-7} H_{d}^{2}\right)+\frac{9.80-g_{\phi}}{0.98 g_{\phi}} H_{d} \tag{8a}
\end{equation*}
$$

Table 67 represents values obtained from the expression within the parentheses and Table 68 represents values computed from the latter factor, taking $0.98 g_{\phi}$ as equal to 9.60 for a close approximation of the denominator. This table thus gives increments of geometric height which are applied as corrections to values obtained from Table 67 for stations whose acceleration of gravity at sea level differs from 9.80 . The side argument is dynamic height by intervals of 1000 dynamic meters and the top argument is $g_{\phi}$, acceleration of gravity, by intervals of $0.01 \mathrm{~m} / \mathrm{sec} .^{2}$ Interpolations must be made for dynamic heights which are not in even thousands and for values of $g_{\phi}$ lying between those given at the top.

Table 69. Difference of height corresponding to a change of O.I inch in the barometer-English measures.

If we differentiate the barometric formula, page xlvii, we shall obtain, neglecting insensible quantities,

$$
d Z=-2628 \mathrm{I} \frac{d B}{B}\left(\mathrm{I}+0.002039\left(\theta-32^{\circ}\right)\right)(\mathrm{I}+\beta),
$$

in which $B$ represents the mean pressure of the air column $d Z$.
Putting $d B=0.1$ inch,

$$
d Z=-\frac{262 S . \mathrm{I}}{B}\left(\mathrm{I}+0.002039\left(\theta-32^{\circ}\right)\right)(\mathrm{I}+\beta)
$$

The second member, taken positively, expresses the height of a column of air in feet corresponding to a tenth of an inch in the barometer under standard gravity. Since the last factor $(I+\beta)$, as given on page xlviii, is a function of the temperature, the function has only two variables and admits of convenient tabulation

Table 69 , containing values of $d Z$ for short intervals of the arguments $B$ and $\theta$, has been taken from the Report of the U. S. Coast Survey, I88i, Appendix 10,-Barometric hypsometry and reduction of the barometer to sea level, by Wm. Ferrel. ${ }^{1}$

The temperature argument is given for every $5^{\circ}$ from $30^{\circ} \mathrm{F}$. to $85^{\circ} \mathrm{F}$., and the pressure argument for every 0.2 inch from 22.0 to 30.8 inches.

This table may be used in computing small differences of altitude, and, up to a thousand feet or more, very approximate results may be obtained.

[^12]Example:
Mean pressure at Augusta, October, I891, 29.94; temperature, $\quad 60^{\circ} .8 \mathrm{~F}$.
Mean pressure at Atlanta, October, I891, 28.97; temperature, $\quad 59^{\circ} 4$
Mean pressure of air column $\quad B=29.455 ; \quad \theta=60^{\circ} . \mathrm{I}$
Entering the table with 29.455 and $60^{\circ}$. as arguments, we take out 94.95 as the difference of elevation corresponding to a tenth of an inch difference of pressure. Multiplying this value by the number of tenths of inches difference in the observed pressures, viz. 97, we obtain the difference of elevation 921 feet.

TABLE 70.
Table 70. Difference of height corresponding to a change of one millimeter in the barometer - Metric measures.
This table has been computed by converting Table 69 into metric units. The temperature argument is given for every $2^{\circ}$ from $-2^{\circ} \mathrm{C}$. to $+36^{\circ} \mathrm{C}$.; the pressure argument is given for $10-\mathrm{mm}$. intervals from 760 to 560 mm .

TABLE 71.
Table 71. Babinet's formula for determining heights by the barometer.
Babinet's formula for computing differences of altitude ${ }^{1}$ represents the formula of Laplace quite accurately for differences of altitude up to 1000 meters, and within one per cent for much greater altitudes. As it has been quite widely disseminated among travelers and engineers, and is of convenient application, the formula is here given in English and metric measures. It might seem desirable to alter the figures given by Babinet so as to conform to the newer values of the barometrical constants now adopted; but this change would increase the resulting altitudes by less than one-half of one per cent without enhancing their reliability to a corresponding degree, on account of the outstanding uncertainty of the assumed mean temperature of the air.

The formula is, in English measures,

$$
Z(\text { feet })=52494\left[\mathrm{I}+\frac{t_{0}+t-64^{\circ}}{900}\right] \frac{B_{0}-B}{B_{0}+B}
$$

and in metric measures,

$$
Z \text { (meters })=\mathrm{I} 6000\left[\mathrm{I}+\frac{2\left(t_{\circ}+t\right)}{1000}\right] \frac{B_{\circ}-B}{B_{\circ}+B}
$$

in which $Z$ is the difference of elevation between a lower and an upper station at which the barometric pressures corrected for all sources of instrumental error are $B_{\circ}$ and $B$, and the observed air temperatures are $t_{0}$ and $t$, respectively.

For ready computation the formula is written

$$
Z=C \times \frac{B_{\circ}-B}{B_{\circ}+B},
$$

[^13]and the factor $C$, computed both in English and metric measures, has been kindly furnished by the late Prof. Cleveland Abbe. The argument is $\frac{1}{2}\left(t_{0}+t\right)$ given for every $5^{\circ}$ Fahrenheit between $10^{\circ}$ and $100^{\circ} F$., and for every $2^{\circ}$ Centigrade between - $10^{\circ}$ and $36^{\circ}$ Centigrade.

In using the table, it should be borne in mind that on account of the uncertainty in the assumed temperature, the last two figures in the value of $C$ are uncertain, and are here given only for the sake of convenience of interpolation. Consequently one should not attach to the resulting altitudes a greater degree of confidence than is warranted by the accuracy of the temperatures and the formula. The table shows that the numerical factor changes by about one per cent of its value for every change of five degrees Fahrenheit in the mean temperature of the stratum of air between the upper and lower stations; therefore the computed difference of altitude will have an uncertainty of one per cent if the assumed tempcrature of the air is in doubt by $5^{\circ} \mathrm{F}$. With these precautions the observer may properly estimate the reliability of his altitudes whether computed by Babinet's formula or by more elaborate tables.

## Example:

Let the barometric pressure observed and corrected for temperature at the upper and lower stations be, respectively, $B=635 \mathrm{~mm}$. and $B_{0}=730 \mathrm{~mm}$. Let the temperatures be, respectively, $t=15^{\circ} \mathrm{C}$., $t_{0}=20^{\circ} C$. To find the approximate difference of height.
With $\frac{1}{2}\left(t_{0}+t\right)=\frac{20^{\circ}+15^{\circ}}{2}=17^{\circ} .5 \mathrm{C}$., the table in metric measures gives

$$
C=17120 \text { meters. } \frac{B_{0}-B}{B_{0}+B}=\frac{95}{1365} .
$$

The approximate difference of height $=17120 \times \frac{95}{1365}=1191.5$ meters.

## THERMOMETRICAL MEASUREMENT OF HEIGHTS BY OESERVATION OF THE TEMPERATURE OF THE BOILING POINT OF WATER.

When water is heated in the open air, the elastic force of its vapor gradually increases, until it becomes equal to the incumbent weight of the atmosphere. Then, the pressure of the atmosphere being overcome, the steam escapes rapidly in large bubbles and the water boils. The temperature at which water boils in the open air thus depends upon the weight of the atmospheric column above it, and under a less barometric pressure the water will boil at a lower temperature than under a greater pressure. Now, as the weight of the atmosphere decreases with the elevation, it is obvious that, in ascending a mountain, the higher the station where an observation is made, the lower will be the temperature of the boiling point.

The difference of elevation between two places therefore can be de-
duced trom the temperature of boiling water observed at each station. It is only necessary to find the barometric pressures which correspond to those temperatures, and from these to compute the difference of height by the tables given herein for computing heights from barometric observations.

From the above, it may be seen that the heights determined by means of the temperature of boiling water are less reliable than those deduced from barometric observations. Both derive the difference of altitude from the difference of atmospheric pressure. But the temperature of boiling water is a less accurate measurement of the atmospheric pressure than is the height of the barometer. In the present state of thermometry it would hardly be safe, indeed, to rely, in the most favorable circumstances, upon quantities so small as hundredths of a degree, even when the thermometer has been constructed with the utmost care; moreover, the quality of the glass of the instrument, the form and substance of the vessel containing the water, the purity of the water itself, the position at which the bulb of the thermometer is placed, whether in the current of the steam or in the water, - all these circumstances cause no inconsiderable variations to take place in the indications of thermometers observed under the same atmospheric pressure. Owing to these various causes, an observation of the boiling point, differing by one-tenth of a degree from the true temperature, ought to be still admitted as a good one. Now, as the tables show, an error of one-tenth of a degree Centigrade in the temperature of boiling water would cause an error of 2 millimeters in the barometric pressure, or of from 70 to 80 feet in the final result, while with a good barometer the error of pressure will hardly ever exceed one-tenth of a milimeter, making a difference of 3 feet in altitude.

Notwithstanding these imperfections, the hypsometric thermometer is of the greatest utility to travellers and explorers in rough countries, on account of its being more conveniently transported and much less liable to accidents than the mercurial barometer. A suitable form for it, designed by Regnault (Annales de Chimie et de Physique, Tome xiv, p. 202), consists of an accurate thermometer with long degrees, subdivided into tenths. For observation the bulb is placed about 2 or 3 centimeters above the surface of the water, in the steam arising from distilled water in a cylindrical vessel, the water being made to boil by a spirit-lamp.

TABLES 72, 73
Barometric pressures at standard gravity corresponding to the temperature of boiling water.

Table 72. English Measures.
Table 73. Metric Measures.
Table 72 is copied directly from Table 75. The argument is the temperature of boiling water for every tenth of a degree from $185^{\circ}$ o to $214^{\circ} \cdot 9$ Fahrenheit. The tabular values are given to the nearest o.oor inch.

Table 73 is copied directly from Table 77. The argument is given for every tenth of a degree from $80^{\circ} .0$ to 100.9 C . The tabular values are given to the nearest 0.01 mm .

## HYGROMETRICAL TABLES.

## PRESSURE OF SATURATED AQUEOUS VAPOR.

In former editions of these tables the values of aqueous vapor pressures at temperatures between $-29^{\circ}$ and $100^{\circ} \mathrm{C}$. were based upon Broch's reduction of the classic observations of Regnault. (Travaux et Mémoires du Bureau international des Poids et Mesures, t. I, p. A 19-39). In these computations the same continuous mathematical function was employed to calculate the values of vapor pressure both above and below the point of change of state on freezing. This resulted in a systematic disagreement between observed and computed vapor pressures below the freezing point, and confirmed the inference from the laws of diffusion following from the kinetic theory of gases, namely, that the pressure of the vapor is different according as it is in contact with its liquid or its solid.

Seeking to remove the uncertainty of the values of vapor pressures at temperatures below freezing, Marvin (Annual Report Chief Signal Officer, 1891, Appendix No. io) made direct experimental determinations thereof, in the course of which the specimens of water were cooled to temperatures of from $-10^{\circ}$ to $-12^{\circ} \mathrm{C}$. while still retaining the liquid state, thus affording opportunity for measurements of vapor pressure over ice and over water at various temperatures below the freezing point. The results of these investigations, confirmed by similar independent studies by Juhlin, were printed in the third revised edition of these tables.

Since 1907, especially, several extended series ${ }^{1}$ of entirely new determinations, together covering the whole range of temperature from $-70^{\circ} \mathrm{C}$. to $+374^{\circ}$ C., have been made at the Physikalische-Technischen Reichsanstalt. Because of the elaborate instrumental means available and the extreme effort to eliminate all possible errors these results may be presumed to represent the most accurate series of experimental values of this important physical datum available to science.

Hitherto no satisfactory mathematical equation has been offered adequate to give computed values of vapor pressures with an order of precision comparable to the systematic self consistency of the observations

[^14]themselves. This is particularly the case with the more recent data over the whole range of temperature from $o^{\circ}$ to the critical temperature at about $374^{\circ}$ Centigrade. Two remedies have been utilized to overcome this difficulty. First, the employment of separate equations of interpolation adjusted to fit the observations accurately over a short range of temperature, $0^{\circ}$ to $100^{\circ}$ for example, as in the case of Broch's computations. (It has already been mentioned that theory requires the function for vapor pressures over ice to differ from the one for pressures over water, so that the values for ice offer no difficulty.) The second remedy sometimes employed consists in fitting any reasonably accurate equation as closely as possible to the observations. The differences between the observed and computed values are then charted and a smooth curve drawn by hand through the points thus located. This method has been employed notably by Henning ${ }^{1}$ and others, using an empirical equation proposed by Thiesen.

For the purpose of these tables Marvin has found it possible from among a multitude of equations to develop a modification of the theoretical equation of Van der Waals which fits the whole range of observations much better than any hitherto offered and with an order of precision quite comparable to the data itself. In fact, the equation serves to disclose inconsistencies in the observations, more particularly between $50^{\circ}$ and $80^{\circ} C$., which seem to suggest the need for further experimental determination of values possibly over the range between $0^{\circ}$ and $100^{\circ}$.

Although it is not difficult to show, as Cederberg ${ }^{2}$ has done, that the simple form of general theoretical equation for all vapors developed by Van der Waals is inadequate to represent experiments on water vapor with sufficient accuracy for practical rquirements, nevertheless a somewhat simple elaboration of its single constant suffices to remove this limitation in a very satisfactory manner.

The resulting equation is:
(1) $\log e=\log \pi-\left[A-b X+m X^{2}-n X^{3}+s Y^{4}\right] \frac{\theta-T}{T}$, where $X=\frac{T-453}{10}$.

The quantity within the square brackets in this equation replaces a single term of the Van der Waals equation which was regarded by him as a constant.

In Van der Waals's original equation $\pi$ and $\theta$ are respectively the critical pressure and temperature (absolute). In the present state of physical science, and from the very nature of the data, these quantities cannot be evaluated exactly. Moreover it is unnecessary to do so for the mere purpose of accurately fitting a mathematical curve to the observational data,

[^15]because the same result is attained by simply passing the curve through a point more accurately known and as near as may be to the critical point. This is equivalent to defining $\pi$ and $\theta$ by an "equation of condition." Another "equation of condition" fixes the pressure at the boiling point which by definition must be 760 mm . From the considerations given on page xv computations are greatly facilitated by taking all temperatures on the approximate absolute scale represented by $T=273 \times t^{\circ}$.

A careful preliminary analysis of the observational data in the vicinity of the critical temperature resulted in assigning values to $\theta$ and $\pi$ as follows :

$$
\theta=643^{\circ}, \log \cdot \pi=5.1959000
$$

It is emphasized here again that these data do not represent critical temperature conditions, but simply a convenient point on the pressure curve slightly below the critical temperature, the value of which is fixed with considerable accuracy by the observational data.

The value of the constant $A$ was fixed by the equation of condition, $e=760 \mathrm{~mm}$. when $T=373(X=-8)$. The remaining constants $(\mathrm{b}, \mathrm{m}, \mathrm{n}, \mathrm{s})$ are computed by the method of least squares. The results are as follows:

$$
\begin{aligned}
A & =3 \cdot 1443172 \\
b & =.00295944 \\
m & =.000+191398 \\
n & =.0000001829924 \\
s & =.00000008243516
\end{aligned}
$$

The number of significant figures in the constants is obviously greater than the accuracy of the data justifies, but is justified to facilitate computation and to secure accuracy in the interpolation of values which should themselves be as accurate as the data.

Observations of the pressure of aqueous vapor over ice have not been as numerous as those over water. Among the observations which have been used in recent times for the development of formulas to express the values of vapor pressures over ice there may be mentioned those of K. Scheel and W. Heuse ${ }^{1}$ at the Physikalisch-Technischen Reichsanstalt at Charlottenburg, those of W. Nernst ${ }^{2}$ at the Physikalisch-Chemischen Institut of the University of Berlin, and those of S. Weber ${ }^{3}$ at the Physical Laboratory of the Uni-

[^16]versity of Leiden. M. Thiesen, ${ }^{1}$ making use of the data of Scheel and Heuse, has developed a formula for vapor pressures over ice. This is given by the equation,
\[

$$
\begin{equation*}
\log _{10} e=\log _{10} e_{0}+9.632(\mathrm{I}-0.00035 t) \frac{t}{T} \tag{2}
\end{equation*}
$$

\]

where

$$
e_{0}=4.5785 \text { and } T=273+t,
$$

the vapor pressures, $e$, being in millimeters and temperatures, $t$, in degrees Centigrade.

For convenience in computing this equation, for metric units it may be written

$$
\begin{equation*}
\log _{10} e=0.66072+\left(\frac{9.632-0.0033712 t}{273+t}\right) t . \tag{3}
\end{equation*}
$$

For English units the equation becomes

$$
\begin{align*}
& \log _{10} e_{1}=\overline{\mathrm{I}} .255888+\left(\frac{9.69193-0.00187289 t_{1}}{459 \cdot 4+t_{1}}\right)\left(t_{1}-32\right)  \tag{4}\\
& e=\text { vapor pressure in millimeters. } \\
& e_{1}=\text { vapor pressure in inches. } \\
& t=\text { degrees Centigrade. } \\
& t_{1}=\text { degrees Fahrenheit. }
\end{align*}
$$

Although the Scheel and Heuse observations extended down to $-67^{\circ} 9 \mathrm{C}$., the pressure readings between $-60^{\circ} \mathrm{C}$. and that temperature were not very accurate, being discarded by Thiesen ${ }^{1}$ in obtaining the constants in equation (2).

Nernst has made determinations of vapor pressure down to at least $-50^{\circ} \mathrm{C}$., good agreement being found with Scheel and Heuse's measurements. By making use of accurate determinations of the heat of vaporization of ice at o. C., and attributing the deviations of water vapor from the gas laws to the existence of double water molecules ${ }^{2}$ Nernst with the collaboration of H. Levy has found for the vapor pressure over ice the formula

$$
\begin{equation*}
\log _{10} e=-\frac{2611.7}{T}+1.75 \log _{10} T-0.00210 T+6.5343, \tag{5}
\end{equation*}
$$

where $\quad e=$ vapor pressure in mm. of mercury and $\quad T=273.09+t$
$t=$ degrees Centigrade.
This formula has been checked by the accurate determinations of Weber the results of whose observations show good agreement with the values

[^17]calculated therefrom between the highest temperature at which he made observations, $-22.75^{\circ} \mathrm{C}$., and $-96^{\circ} \mathrm{C}$. Below the latter temperature the agreement does not appear so good. Comparisons between Weber's data and the values calculated by means of Thiesen's formula indicate that the latter formula most probably gives values which are slightly too high above $-40^{\circ} \mathrm{C}$., and slightly too low below that temperature.

Nernst ${ }^{1}$ has also developed a more complicated formula than (5), making use of Pollitzer's quantum-formula for the specific heat of ice. The agreement with Weber's data in this case is not quite as good on the whole as in the case of equation (5), and therefore it is not given here.

More recently, E. W. Washburn ${ }^{2}$ has developed a formula for the vapor pressure over ice, making use of Scheel and Heuse's, and Weber's observational data. Tables computed on the basis of this formula have been published in the Monthly Weather Review ${ }^{2}$ and in the International Critical Tables. ${ }^{3}$ Formula (5) gives slightly better agreement with the Weber data than does the last formula referred to. Further determinations are necessary to settle the question as to the most representative equation, especially within the range of temperatures between $0^{\circ} \mathrm{C}$. and $-20^{\circ} \mathrm{C}$. Some work has been done by Holborn, Scheel, and Henning ${ }^{4}$ to correct the values of Scheel and Heuse between $0^{\circ} \mathrm{C}$. and $-50^{\circ} \mathrm{C}$.

Table 76 has been computed by means of Thiesen's formula (3), from $0^{\circ} C$. to $-49^{\circ} .5 \mathrm{C}$. inclusive, and by means of Nernst's formula (5), from $-50^{\circ} \mathrm{C}$. to $-70^{\circ} \mathrm{C}$. inclusive.

The vapor pressures in the tables here given are expressed in standard manometric units.

TABLE 74.
Table 74. Pressure of aqueous vapor over ice. English measures.
The pressure, computed by equation (4) above, are given to 0.0000 I inch for each degree of temperature from $-60^{\circ}$ to $-15^{\circ}$, for each half degree from -I5 to $\pm 0^{\circ}$, and for each tenth of a degree from $\pm 0^{\circ} .0$ to $+32^{\circ}$.

TABLE 75.
Table 75. Pressure of aqueous vapor over water. English measures.
This table has been computed by converting Table 77 into English units. The temperature argument is given for every 0.1 from 32.0 to 214.9 $F$. The vapor pressures are to 0.0001 inch from 32.0 to $130^{\circ} .9 \mathrm{~F}$., and to 0.001 inch from 130.0 to $214^{\circ} 9 \mathrm{~F}$.

[^18]Table 76. Pressure of aqueous vapor over ice. Metric measures.
The pressures, given to the nearest 0.000 I mm., are computed by Nernst's Formula (5), above, for each degree of temperature from $-70^{\circ}$ to $-50^{\circ}$ inclusive, and by Thiesen's Formula (3), above, for each half degree from $-49^{\circ} .5$ to $-35^{\circ}$ inclusive, and each tenth of a degree from $-36^{\circ}$ o to $\pm 0.0$.

TABLE 77.
Table 77. Pressure of aqueous vapor over water. Metric measures.
The pressures, computed by equation (i) above, are given for each tenth of a degree to 0.001 mm . from $0^{\circ} .0$ to $59^{\circ} 9$, and to o.OI mm. from $50^{\circ}$. o to $100^{\circ} .9$. They are given for each degree to 0.1 mm . from $100^{\circ}$ to $189^{\circ}$, and in millimeters from $190^{\circ}$ to $374^{\circ}$.

TABLE 78
Table 78. Pressure of aqueous vapor over ice. Dynamic measures.
The pressures given in Table 78 , in millibars, have been obtained by multiplying the pressures given in Table 76, in millimeters, by I.333224, the value of one millimeter in millibars (see page xxii). The values are given for each tenth of a degree between $-70^{\circ} \mathrm{C}$. and $0^{\circ} \mathrm{C}$., inclusive. It may be noted as in the case of Table 76 that the values between temperatures $-50^{\circ} \mathrm{C}$. and $-70^{\circ} \mathrm{C}$. inclusive have been obtained by means of the Nernst Formula for the vapor pressure over ice (equation (5), p. lxiv), whereas the values between $-50^{\circ} \mathrm{C}$. and $0^{\circ} \mathrm{C}$. have been obtained by means of the Thiesen Formula (equation (3), p. lxiv). Over the range of temperatures between $-50^{\circ} \mathrm{C}$. and $-36^{\circ} \mathrm{C}$., the values for tenths of degrees have been obtained by linear interpolation between whole degrees and half degrees.

Table 79. Pressure of aqueous vapor over water. Dynamic measures.
Similarly, the vapor pressures in Table 79, in millibars, have been obtained by multiplying the pressures given in Table 77 by 1.333224 , and are given for each tenth of a degree between $0^{\circ} \mathrm{C}$. and $44^{\circ} \cdot{ }^{\circ} \mathrm{C}$., inclusive.

TABLES 80:81.
Table 80. Weight of a cubic foot of saturated aqueous vapor. English measures.
Table 81. Weight of a cubic meter of saturated aqueous vapor. Metric measures.
For many years it has been customary to assume that the specific gravity of water vapor relative to dry air is a constant whose theoretical value computed from the accurately known densities of its constituent gases is 0.622 I . Direct experimental determinations of the specific volume of dry saturated steam (as yet but few observations are available at moderate temperatures) show conclusively (I) that this theoretical specific gravity is true only for saturated vapor at very low temperatures or when the vapor is in a very attenuated state of partial saturation; (2) that at increasingly higher temperatures the specific gravity is increasingly greater than 0.6221 . These assertions are in accord with the values of weight per cubic foot of
water vapor tabulated by Marks \& Davis ${ }^{1}$ from the most recent determinations of the specific volume of water vapor. However, owing to the paucity of data, and its inaccuracy for the range of atmospheric temperatures and conditions, the values derived from densities given by Marks and Davis between $10^{\circ}$ and $50^{\circ}$ are probably too low and require revision. The basis on which this assertion is made is the generalization that the theoretical value 0.6221 is probably a minimum specific gravity towards which actual values asymptotically tend at low temperature and low relative humidity in the meteorological sense, or high super heats in the steam engincering sense. This generalization affords a very helpful "control" in harmonizing and combining experimental determinations of specific volume. It was thus employed in a recomputation, from the original experimental data on specific volumes, of the accompanying table of specific gravities, $d$, of saturated water vapor.

| $T .\left(C^{0}\right)$ | $d$ | $T .\left(C^{\circ}\right)$ | $d$ |
| :---: | :---: | :---: | :---: |
| -60 | 0.6226 | 60 | 0.6273 |
| 50 | 0.6227 | 70 | 0.6283 |
| 40 | 0.6229 | 80 | 0.6296 |
| 30 | 0.6230 | 90 | 0.6311 |
| 20 | 0.6232 | 100 | 0.6329 |
| -10 | 0.6235 | 110 | 0.6351 |
| $\pm 0$ | 0.6238 | 120 | 0.6377 |
| +10 | 0.6241 | 130 | 0.6408 |
| 20 | 0.6246 | 140 | 0.6446 |
| 30 | 0.6251 | 150 | 0.6491 |
| 40 | 0.6257 | 160 | 0.6545 |
| 50 | 0.6264 | 170 | 0.6609 |
|  |  | 180 | 0.6687 |

The weight of a cubic meter of saturated vapor is given by the expression

$$
W=\frac{d \cdot \delta}{1+a t} \cdot \frac{e}{760},
$$

$\delta$ is the weight of a cubic meter of dry air (free from carbonic acid) at temperature $0^{\circ} \mathrm{C}$., and pressure of 760 millimeters of mercury of standard density under standard gravity: $\delta=1.2928 \mathrm{~kg}$. (Bureau International des Poids et Mesures: Travaux et Mémoires, t. I, p. A 54.)
$d$ is the density of aqueous vapor relative to dry air: $d=0.622$ I.
While, as stated above, there is reason for believing that this value is too low, for atmospheric temperatures the error is less than one per cent. For practical work in meteorology and at moderate temperatures, it seems best to retain the theoretical value until the actual value has been determined

[^19]with greater accuracy. For all important calculations except those at low temperatures the values of $d$ in the Table on page lxvii should be employed.
$c$ is the pressure of saturated aqueous vapor at temperature $t$, taken from Tables 76 and 77.
$a$ is the coefficient of expansion of air for $C^{3}: a=0.003670$.
$t$ is the temperature in Centigrade degrees.
Whence we have
$$
W^{\prime}(\text { grams })={ }^{1} \mathrm{I} .05821 \times \frac{e}{1+0.003670 t} .
$$

Table 81 is computed from this formula and gives the weight of saturated vapor in grams in a cubic meter for dew-points from $-70^{\circ}$ to $+40^{\circ} 9 \mathrm{C}$., the intervals from $-35^{\circ}$ to $40^{\circ} 9 \mathrm{C}$., being 0.1 C . The tabular values are given to three decimals for temperatures above $-41^{\circ} \div$, and to four decimal places for temperatures below -41.5 .

The weight $W_{1}$ of a cubic foot of saturated vapor is obtained by converting the foregoing constants into English measures.

The weight of a cubic foot of dry air at temperature $32^{\circ} F$. and at a pressure of 760 mmn . or 29.921 inches is

We have therefore,

$$
\delta_{1}(\text { grains })=\frac{1292.78 \times 15.4 .323 .5}{(3.280833)^{3}}={ }^{2} 564.94 .
$$

$W_{1}$ (grains) $=\frac{\delta_{1} d}{29.92 \mathrm{I}} \times \frac{c_{1}}{1+a_{1}\left(t_{1}-32^{\circ}\right)}={ }^{3}$ I I. $7+59 \frac{c_{1}}{1+0.002039\left(t_{1}-32^{\circ}\right)}$
The temperature $t_{1}$ is expressed in degrees Fahrenheit; the vapor pressure $e_{1}$, expressed in inches, is obtained from Tables 74 and 75 .

Table 80 gives the weight of saturated aqueous vapor in grains per cubic foot for dew-points given to every degree from $-30^{\circ}$ to $+20^{\circ}$, to each half degree from $+20^{\circ}$ to $+70^{\circ}$, and for every $0^{\circ} 2$ from $70^{\circ}$. to $119^{\circ} 8 F$., the values being computed to the thousandth of a grain.

## REDUCTION OF OBSERVATIONS WITH THE PSYCHROMETER AND DETERMINATION OF RELATIVE HUMIDITY.

The psychrometric formula derived by Maxwell, Stefan, August, Regnault and others is, in its simplest form,

$$
e=e^{\prime}-\mathrm{AB}\left(t-t^{\prime}\right),
$$

in which $t=$ Air temperature.
$t^{\prime}=$ Temperature of the wet-bulb thermometer.
$e=$ Pressure of aqueous vapor in the air.
$e^{\prime}=$ Vapor pressure, saturated, at temperature $t^{\prime}$.
$B=$ Barometric pressure.
$A=\mathrm{A}$ quantity which, for the same instrument and for certain conditions, is a constant, or a function depending in a small measure on $t^{\prime}$.

[^20]All pressures are expressed in heights of mercurial column under standard gravity.

The important advance made since the time of Regnault consists in recognizing that the value of $A$ differs materially according to whether the wet-bulb is in quiet or moving air. This was experimentally demonstrated by the distinguished Italian physicist, Belli, in 1830 , and was well known to Espy, who always used a whirled psychrometer. The latter describes his practice as follows: "When experimenting to ascertain the dew-point by means of the wet-bulb, I always swung both thermometers moderately in the air, having first ascertained that a moderate movement produced the same depression as a rapid one."

The principles and methods of these two pioneers in accurate psychrometry have now come to be adopted in the standard practice of meteorologists, and psychrometric tables are adapted to the use of a whirled or ventilated instrument.

The factor $A$ depends in theory upon the size and shape of the thermometer buib, largeness of stem and velocity of ventilation, and different formulæ and tables would accordingly be required for different instruments. But by using a ventilating velocity of three meters or more per second, the differences in the results given by different instruments vanish, and the same tables can be adapted to any kind of a thermometer and to all changes of velocity above that which gives sensibly the greatest depression of the wet-bulb temperature; and with this arrangement there is no necessity to measure or estimate the velocity in each case further than to be certain that it does not fall below the assigned limit.

The formula and tables here given for obtaining the vapor pressure and dew-point from observations of the whirled or ventilated psychrometer are those deduced by Prof. Wm. Ferrel (Annual Report Chief Signal Officer, 1886, Appendix 24) from a discussion of a large number of observations.

Taking the psychrometric formula in metric units, pressures being expressed in millimeters and temperatures in centigrade degrees, Prof. Ferrel derived for $A$ the value

$$
A=0.000656\left(1+0.0019 t^{\prime}\right) .
$$

In this expression for $A$, the factor depending on $t^{\prime}$ arises from a similar term in the expression for the latent heat of water, and the theoretical value of the coefficient of $t^{\prime}$ is 0.00115 . Since it would require a very small change in the method of observing to cause the difference between the theoretical value and that obtained from the experiments, Prof. Ferrel adopted the theoretical coefficient 0.00115 and then recomputed the observations, obtaining therefrom the final value

$$
A=0.000660\left(1+0.001 \mathrm{I}_{5} t^{\prime}\right)
$$

With this value the psychrometric formula in metric measures becomes

$$
c=c^{\prime}-0.000660 B\left(t-t^{\prime}\right)\left(\mathrm{I}+0.001 \mathrm{I} 5 t^{\prime}\right) .
$$

Expressed in English measures, the formula is

$$
\begin{aligned}
e & =e^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left[1+0.0006+\left(t^{\prime}-32^{\circ}\right)\right] \\
& =e^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left(\mathrm{I}+\frac{t^{\prime}-32}{157 \mathrm{I}}\right)
\end{aligned}
$$

in which $\mathcal{e}=$ Vapor pressure in inches.
$e^{\prime}=$ Pressure of saturated aqueous vapor at temperature $t^{\prime}$.
$t=$ Temperature of the air in Fahrenheit degrees.
$t^{\prime}=$ Temperature of the wet-bulb thermometer in Fahrenheit degrees $B=$ Barometric pressure in inches.
Table 82. Reduction of Psychrometric Observations-English measures.

$$
\text { Values of } c=c^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left(1+\frac{t^{\prime}-32}{1571}\right)
$$

This table provides for computing the vapor pressure, $c$, from observations of ventilated wet- and dry-bulb Fahrenheit thermometers. From the vapor pressure thus computed the dew-point and relative humidity of the atmosphere may be obtained.

The tabular values of the vapor pressure, $e$, are computed for degree intervals of $t^{\prime}$ from $-20^{\circ}$ to $+110^{\circ} \mathrm{F}$. Below $+10^{\circ}$ the interval for $t-t^{\prime}$ is $0^{\circ} .2$, and above $10^{\circ}$ the interval is $I^{\circ}$.

Corrections for barometric pressure. The computation has been made for $B=30.0$ inches, but at the bottom, and usually, also, at the top of each page of the table is given a correction, $\Delta e \times \Delta B$, computed for $B=29.0$ inches or $\Delta B=\mathrm{I}$ inch. and for the value of $t^{\prime}$ indicated. The correction is a linear function of $\Delta B$. For atmospheric pressures less than 30.0 inches, it is to be added to the tabular values of $c$, while for atmospheric pressures greater than 30.0 inches it is to be subtracted.

The values of $e$ are given to 0.0001 inch for $t^{\prime}$ less than $10^{\circ}$, and to 0.001 inch for $t^{\prime}$ greater than $10^{\circ}$.

## Examples:

I. Given, $t=84^{\circ} .3 ; t^{\prime}=66^{\circ} 7$, and $B=30.00$ inches. With $t^{\prime}=66^{\circ} .7$ and $t-t^{\prime}=17^{\circ} \cdot 6$ as arguments, Table 82 gives for $e$ the value 0.462 inch. On page 182 , for $t-t^{\prime}=0.0$ it is seen that a vapor presure of 0.462 inch corresponds to a temperature $t^{\prime}=t=57^{\circ}$, which is the saturation, or dew-point temperature for the data given.
2. Given, $t=34^{\circ} .5 ; t^{\prime}=29^{\circ} .4 ; B=22.3$ inches. With $t^{\prime}=29^{\circ} .4$ and $t-t^{\prime}=5^{\circ} .1$ as arguments, Table 82 gives for $c$ the value o.Io4. $\Delta B=30.0-22.3=7.7$, and $\Delta e \times \Delta B=0.0018 \times 7.7=0.014$.
Correct value of $e$
$=0.118$ inch

For $t-t^{\prime}=0.0$ a vapor pressure of 0.118 inch corresponds to a temperature $t^{\prime}=t=23^{\circ}$ (see page 182), which is the saturation or dewpoint temperature for the data given.

## table 83. Relative humidity-Temperature Fahrenheit.

The table gives the vapor pressure corresponding to air temperatures from $-30^{\circ}$ to $+120^{\circ}$ at degree intervals (side argument) and for percentages of saturation at io per cent intervals (top argument). It is computed from the formula

$$
e=e_{s} \times \text { relative humidity }
$$

where $e_{s}$ is the saturation vapor pressure at the given air temperature. Below a temperature of $20^{\circ}$ the values of $c$ are given to o.0001 inch; above $20^{\circ}$ they are given to o.00I inch.

## Exampies:

I. In dew-point example 1 , above, the computed vapor pressure is 0.462 inch. Entering Table 83 with air temperature $84^{\circ} 3$ as side argument, we obtain vapor pressure
0.356 inch $\quad=$ relative humidity 30 and
0.462 inch -0.356 inch $=0.106$ inch $=\quad " \quad$ " $\frac{90}{10}=9$ therefore, vapor pressure 0.462 inch with $t=84^{\circ} 3 \mathrm{~F}$. = " " 39
2. In dew-point example 2, above, the computed vapor pressure is o.II8 inch. Entering Table 83 with air temperature $34^{\circ} 5$ as side argument, we obtain, vapor pressure
0.100 inch $\quad=$ relative humidity 50 and
0.118 inch-0.100 inch $=0.018$ inch = " " $\frac{90}{10}=9$ therefore, vapor pressure
O.II8 inch with $t=34 .{ }^{\circ} \mathrm{F}$. = " " 59
table 84. Reduction of Psychrometric Observations-Metric measures.

$$
\text { Values of } e=e^{\prime}-0.000660 B\left(t-t^{\prime}\right)\left(\mathrm{I}+0.001 \mathrm{I} 5 t^{\prime}\right)
$$

This table provides for computing the vapor pressure from observations of ventilated wet- and dry-bulb Centigrade thermometers. From the vapor pressure thus computed the dew-point and relative humidity of the atmosphere may be obtained.

The tabular values of the vapor pressure, $e$, are computed for degree intervals of $t^{\prime}$ from $-30^{\circ}$ to $+45^{\circ} \mathrm{C}$. Below $-5^{\circ}$. the interval for $t-t^{\prime}$ is $0^{\circ} \mathrm{I}$, and above $-5^{\circ} \mathrm{O}$ the interval is $\mathrm{I}^{\circ}$.

Corrections for barometric pressure. The computation has been made for $B=760 \mathrm{~mm}$. but on each page of the table is given a correction, $\Delta e \times \Delta B$, computed for $B=660$, or $\Delta P=100 \mathrm{~mm}$., and for the values of $t^{\prime}$ indicated. The correction is a linear function of $\Delta B$. For atmospheric pressures less than 760 mm . it is to be added to the tabular values of $c$, while for atmospheric pressures greater than 760 mm . it is to be subtracted. The values of $e$ are given to 0.001 mm . for $t^{\prime}$ less than -5.0 , and to 0.01 mm. for $t^{\prime}$ greater than $-5^{\circ}$. .

## Example:

Given, $t=10^{\circ} .4 C . ; t^{\prime}=8.3 C$, and $B=740 \mathrm{~mm}$. With $t^{\prime}=8^{\circ} .3$ and $t-t^{\prime}=2$. I as arguments, Table 84 gives for $e$ the value 7.15 mm .
$\Delta B=\frac{760-7+0}{100}=0.2 . \Delta e \times \Delta B=0.14 \times 0.2 \quad=0.03$.
Corrected value of $e$
$=7.18 \mathrm{~mm}$.
For $t-t^{\prime}=0$ a vapor pressure of 7.18 mm . corresponds to a temperature $t^{\prime}=t=6^{\circ} 3 \mathrm{C}$., which is the saturation, or dew-point temperature for the data given.

Table 85. Relative humidity-Temperature Centigrade.
This table gives the vapor pressure corresponding to air temperatures from $-45^{\circ} \mathrm{C}$. to $+55^{\circ} \mathrm{C}$. at degree intervals (side argument) and for percentage of saturation at ro per cent intervals (top argument). It is computed from the same formula as Table 83, namely,

$$
e=e_{s} \times \text { relative humidity }
$$

Below a temperature of $+5^{\circ}$. o the values of $e$ are given to 0.01 mm .; above $5^{\circ}$ o they are given to 0.1 mm .

## Example:

In the dew-point example given above, the computed vapor pressure is 7.18 mm. Entering Table $8_{5}$ with air temperature 10.4 as side argument, we obtain vapor pressure
$6.6 \mathrm{~mm} . \quad=$ relative humidity $\quad 70$
and

$$
7.18-6.6=0.58 \mathrm{~mm} . \quad=\quad " \quad \frac{60}{10}=6
$$

therefore, vapor pressure

$$
7.18 \mathrm{~mm} \text {. with } t=10.4 C=\quad " \quad=\quad=76
$$

TABLE 86.
table 86. Rate of decrease of vapor pressure weith altitude for mountain stations.
From hygrometric observations made at various mountain stations on the Himalayas, Mount Ararat, Teneriffe, and the Alps, Dr. J. Hann (Lehrbuch der Meteorologie Dritte Auflage, S. 230) has deduced the following empirical formula showing the average relation between the vapor
pressure $e_{0}$ at a lower station and $e$ the vapor pressure at another station at an altitude $h$ meters above it:

$$
\frac{e}{e_{0}}=10^{-\frac{h}{6300}} .
$$

This is of course an average relation for all times and places from which the actual rate of decrease of vapor pressure in any individual case may widely differ.

Table 86 gives the values of the ratio $\frac{e}{e_{0}}$ for values of $h$ from 200 to 6000 meters. An additional column gives the equivalent values of $h$ in feet.

REDUCTION OF SNOWFALL MEASUREMENT.
The determination of the water equivalent of snowfall has usually been made by one of two methods: (a) by dividing the depth of snow by an arbitrary factor ranging from 8 to 16 for snow of different degrees of compactness; (b) by melting the snow and measuring the depth of the resulting water. The first of these methods has always been recognized as incapable of giving reliable results, and the second, although much more accurate, is still open to objection. After extended experience in the trial of both these methods, it has been found that the most accurate and most convenient measurement is that of weighing the collected snow, and then converting the weight into depth in inches. The method is equally applicable whether the snow as it falls is caught in the gage, or a section of the fallen snow is taken by collecting it in an inverted gage.

Table 87. Depth of water corresponding to the weight of a cylindrical snow core, 2.655 inches in diameter.

This table is prepared for convenience in making surveys of the snow layer on the ground, particularly in the western mountain sections of the country. The weighing method is the only one found to be practicable. Present Weather Bureau practice is to take out a sample by means of a special tube, whose diameter, 2.655 inches, has been selected by reason of convenience in manipulation and simplicity in relation to the pound. Table 87 gives the depth of water in inches and hundredths corresponding to given weights. The argument is given in hundredths of a pound from o.or pound to 2.99 pounds.

Table 88. Depth of water corresponding to the weight of snow (or rain) collected in an 8 -inch gage.

The table gives the depth to hundredths of an inch, corresponding to the weight of snow or rain collected in a gage having a circular collecting mouth 8 inches in diameter - this being the standard size of gage used throughout the United States.

The argument is given in hundredths of a pound from o.or pound to 0.99 pound. When the weight of the collected snow or rain is one pound or more, the depth corresponding to even pounds may be obtained from the equivalent of one pound given in the heading of the table.

## Example:

The weight of the snow collected in a gage having a circular collecting mouth 8 inches in diameter is 3.48 pounds. Find the corresponding depth of water.
A weight of 3 lbs . corresponds to a depth of water of $0.5507 \times 3$, equals
1.65 in.

A weight of 0.48 lbs . corresponds to a depth of water of 0.26 A " " 3.48 " " " " 1.9 I in

Table 89. Quantity of rainfall corresponding to given depths.
TABLE 89.
This table gives for different depths of rainfail in inches over an acre the total quantity of water expressed in cubic inches, cubic feet, gallons, and tons. (See Henry, A. J. "Quantity of Rainfall corresponding to Given Depths." Monthly Weather Review, 1898, 26: fo8-09.)

## GEODETICAL TABLES.

Table 90. Value of apparent gravity on the earth at sea level. ${ }^{1}$
TABLE 90.
The value of apparent gravity on the earth at sea level is given for every twenty minutes of latitude from $5^{\circ}$ to $86^{\circ}$, and for degree intervals near the equator and the poles. It is computed to o.ool dyne from the equation ${ }^{2}$

$$
\begin{aligned}
g_{\phi} & =978.039\left(1+0.00529+\sin ^{2} \phi-0.000007 \sin ^{2} 2 \phi\right) \\
& =980.621\left(1-0.002640 \cos 2 \phi+0.000007 \cos ^{2} 2 \phi\right)
\end{aligned}
$$

in which $g_{\phi}$ is the value of the gravity at latitude $\phi$.
The second form of the equation is the more convenient for the computation.

TABLE 91.
Table 91. Relative acceleration of gravity at sea level at different latitudes.
The formula adopted for the variation with latitude of apparent gravity at sea level is that of the U.S. Coast and Geodetic Survey, given above.

The table gives the values of the ratio $\frac{g_{\phi}}{g_{45^{\circ}}}$ to six decimals for every $10^{\prime}$ of latitude from the equator to the pole.

[^21]
## LENGTH OF A DEGREE OF THE MERIDIAN AND OF ANY PARALLEL.

The dimensions of the earth used in computing lengths of the meridian and of parallels of latitude are those of Clarke's spheroid of $1866 .{ }^{1}$ This spheroid undoubtedly represents very closely the true size and shape of the earth, and is the one to which nearly all geodetic work in the United States is now referred.

The values of the constants are as follows:
$a$, semi-major axis $=20926062$ feet; $\log a=7.3206875$.
$b$, semi-minor axis $=20855121$ feet; $\log b=7.3192127$.

$$
e^{2}=\frac{a^{2}-b^{2}}{a^{2}}=0.00676866 ; \quad \log e^{2}=7.8305030-10 .
$$

With these values for the figure of the earth, the formula for computing any portion of a quadrant of the meridian is

Meridional distance in feet $=[5.5618284] \Delta \phi$ (in degrees),
-- [5.0269880] $\cos 2 \phi \sin \Delta \phi$,
$+[2.0528] \cos 4 \phi \sin 2 \Delta \phi$,
in which $2 \phi=\phi_{2}+\phi_{1}, \Delta \phi=\phi_{2}-\phi_{1} ; \phi_{1}, \phi_{2}=$ end latitudes of arc.
For the length of I degree, the formula becomes:
I degree of the meridian, in feet $=364609.9-1857.1 \cos 2 \phi+3.94 \cos 4 \phi$.
The length of the parallel is given by the equation
I degree of the parallel at latitude $\phi$, in feet $=$

$$
365538.48 \cos \phi-310.17 \cos 3 \phi+0.39 \cos 5 \phi .
$$

Table 92. Length of one degree of the meridian at different latitudes.
This gives for every degree of latitude the length of one degree of the meridian in statute miles to three decimals, in meters to one decimal, and in geographic miles to three decimals - the geographic mile being here defined to be one minute of arc on the equator. The values in meters are computed from the relation: I meter $=39.3700$ inches. The tabular values represent the length of an arc of one degree, the middle of which is situated at the corresponding latitude. For example, the length of an arc of one degree of the meridian, whose end latitudes are $29^{\circ} 30^{\prime}$ and $30^{\circ} 30^{\prime}$, is 68.879 statute miles.

Table 93. Length of one degree of the parallel at different latitudes.
This table is similar to Table 92.
${ }^{1}$ Comparisons of Standards of Length, made at the Ordnance Survey Office, Southampton, England, by Capt. A. R. Clarke, R. E., 1866.

Table 94. Duration of sumshine at different latitudes for different values of the sun's declination.


Let $Z$ be the zenith, and $N H$ the horizon of a place in the northern hemisphere.
$P$ the pole;
$Q E Q^{\prime}$ the celestial equator;
$R R^{\prime}$ the parallel described by the sun on any given day;
$S$ the position of the sun when its upper limb appears on the horizon;
$P N$ the latitude of the place, $\phi$.
$S T$ the sun's declination, $\delta$.
$P S$ the sun's poiar distance, $90^{\circ}-\delta$.
$Z S$ the sun's zenith distance, $z$.
$Z P S$ the hour angle of the sun from meridian, $t$.
$r$ the mean horizontal refraction $=34^{\prime}$ approximately .
$s$ the mean solar semi-diameter $=16^{\prime}$

$$
z=90^{\circ}+r+s=90^{\circ} 50^{\prime}
$$

In the spherical traingle $Z P S$, the hour angle $Z P S$ may be computed from the values of the three known sides by the formula

$$
\begin{gathered}
\sin \frac{1}{2} Z P S=\sqrt{\frac{\sin \frac{1}{2}(Z S+P Z-P S) \sin \frac{1}{2}(Z S+P S-P Z)}{\sin P Z \sin P S}} \\
\sin \frac{1}{2} t=\sqrt{\frac{\sin \frac{1}{2}(z+\delta-\phi) \sin \frac{1}{2}(z-\delta+\phi)}{\cos \phi \cos \delta}}
\end{gathered}
$$

The hour angle $t$, converted into mean solar time and multiplied by 2 is the duration of sunshine.

Table 94 has been computed for this volume by Prof. W'm. Libbey, Jr. It is a table of double entry with arguments $\delta$ and $\phi$. For north latitudes northerly declination is considered positive and southerly declination as negative. The table may be used for south latitudes by considering southerly declination as positive and northerly declination as negative.

The top argument is the latitude, given for every $5^{\circ}$ from $0^{\circ}$ to $40^{\circ}$, for every $2^{\circ}$ from $40^{\circ}$ to $60^{\circ}$, and for every degree from $60^{\circ}$ to $80^{\circ}$.

The side argument is the sun's declination for every $20^{\prime}$ from $S 23^{\circ} 27^{\prime}$ to $N 23^{\circ} 27^{\prime}$.

The duration of sunshine is given in hours and minutes.
To find the duration of sunshine for a given day at a place whose latitude is known, find the declination of the sun at mean noon for that day in the Nautical Almanac, and enter the table with the latitude and declination as arguments.

## Example:

To find the duration of sunshine, May 18,1892 , in latitude $49^{\circ} 30^{\prime}$ North.
From the Nautical Almanac, $\delta=19^{\circ} 43^{\prime} N$., at Greenwich apparent noon.
From the table, with $\delta=19^{\circ} 43^{\prime} N$. and $\phi=49^{\circ} 30^{\prime}$, the duration of sunshine is found to be $15^{h} 33^{m}$.
Table 95. Declination of the sun for the year I899, at Greenwevich apparent noon.
This table is an anxiliary to Table 94, and gives the declination of the sun for every third day of the year 1899 . These declinations may be used as approximate values for the corresponding dates of other years when the exact declination cannot readily be obtained. Thus, in the preceding example, the declination for May I8, 1892, may be taken as approximately the same as that for the same date in I899, viz. $19^{\circ} 34^{\prime}$.

## THE DURATION OF TWILIGHT.

A review of the literature ${ }^{1}$ indicates that from an early date astronomical twilight has been considered to end in the evening and begin in the morning when the true position of the sun's center is $18^{\circ}$ below the horizon. At this time stars of the sixth magnitude are visible near the zenith, and generally there is no trace on the horizon of the twilight glow.

It also appears that civil twilight ends in the evening and begins in the morning when the true position of the sun's center is $6^{\circ}$ below the horizon. At this time stars and planets of the first magnitude are just visible. In the evening the first purple light has just disappeared, and darkness compels the suspension of outdoor work unless artificial lighting is provided. In the morning the first purple light is beginning to be visible, and the illumination is sufficient for the resumption of outdoor occupations.

Some confusion has arisen in the computation of tables of the duration of both astronomical and civil twilight, due to the fact that in some instances the time of sunrise or sunset has been considered to be that instant when the center of the sun is on the true horizon; in others, when its center appears to be on the true horizon; and in still others when the upper limb of the sun appears to coincide with the true horizon. In the United States this latter is regarded as defining the time of sunrise and sunset.

In the tables here presented the duration of astronomical twilight is the interval between sunrise or sunset, according to this latter definition, and the instant the true position of the sun's center is $18^{\circ}$ below the horizon. Likewise, the duration of civil twilight is the interval from sunrise or sunset to the instant the true position of the sun's center is $6^{\circ}$ below the horizon.

[^22]The computations may be made from the equation

$$
\cos t=\frac{\sin a-\sin \phi \sin \delta}{\cos \phi \cos \delta}
$$

where $t$ is the sun's hour angle from the meridian, $a$ is the sun's altitude, considered minus below the horizon, $\delta$ is the solar declination, and $\phi$ is the latitude of the place of observation.

The solar declinations employed are those given in the American Ephemeris and Nautical Almanac, 1899, pp. 377-384, Solar Ephemeris for Washington.

The atmospheric refraction with the sun on the horizon has been assumed to be $34^{\prime}$, and 16 ' has been allowed for the sun's semi-diameter, so that at the instant of sunrise or sunset, as defined above, the true position of the sun's center is about $50^{\prime}$ below the horizon. The difference between this value of $t$ and its value with the sun $6^{\circ}$ and $18^{\circ}$ below the horizon gives, respectively, the duration of civil and astronomical twilight.

The computations have been simplified by the use of Ball's Altitude Tables, ${ }^{1}$ from which the value of $t$ has been determined for true altitudes of the sun of $-50^{\prime},-6^{\circ}$, and $-18^{\circ}$.

Table 96. Duration of astronomical twilight.
TABLE 96.
The duration of astronomical twilight is given to the nearest minute for the Ist, IIth, and 2 Ist day of each month for north latitudes, $0^{\circ}, 10^{\circ}$, $20^{\circ} ; 25^{\circ}$, and at $2^{\circ}$ intervals from $30^{\circ}$ to $50^{\circ}$, inclusive. The absence of data for latitude $50^{\circ}$ from June 1 to July in, inclusive, indicates that between these dates at this latitude astronomical twilight continues throughout the night.

Table 97. Duration of civil twilight.
TABLE 97.
The duration of civil twilight is given to the nearest minute for the Ist, 11 th and 2 Ist day of each month for north latitudes $0^{\circ}, 10^{\circ}, 20^{\circ}, 25^{\circ}$, and at $2^{\circ}$ intervals from $30^{\circ}$ to $50^{\circ}$, inclusive.

> RELATIVE INTENSITY OF SOLAR RADIATION AT DIFFERENT LATITUDES.

TABLE 98.
Table 98. Mean intensity for 24 hours of solar radiation on a horizontal surface at the top of the atmosphere.

This table is that of Prof. Wm. Ferrel, published in the Annual Report of the Chief Signal Officer, 1885, Part 2, p. 427, and computed from formulæ and constants given in Chapter II of the above publimation, pages 75 to 82 . It gives the mean intensity, $J$, for $2+$ hours of solar radiation received by a horizontal surface at the top of the atmosphere, in terms of the mean solar

[^23]constant $A_{\mathrm{o}}$, for each tenth parallel of latitude of the northern hemisphere, and for the first and sixteenth day of each month; also the values of the solar constant $A$ in terms of $A_{\circ}$, and the longitude of the sun for the given dates.

Table 99. Relative amounts of solar radiation received on a horizontal surface during the year at different latitudes.

The second column of this table is obtained from the last line of Table 98 by multiplying by 1440 , the number of minutes in $2+$ hours. It therefore gives the average daily amount of radiation that would be received from the sun on a horizontal surface at the surface of the earth if none were absorbed or scattered by the atmosphere, expressed in terms of the mean solar constant. The following columns give similar data, excert that the atmospheric transmission coefficient is assumed to be $0.9,0.8,0.7$ and o.6, respectively, and have been computed by utilizing Angot's work (Recherches théoretiques sur la distribution de la chaleur à la surface du globe, par M. Alfred Angot, Annales du Bureau Central Météorologique de France, Année 1883. v. I. B 121-B 169), which leads to practically the same values as Ferrel's when expressed in the same units.

The vertical argument of the table is for $10^{\circ}$ intervals of latitude from the equator to the north pole, inclusive.

Table 100. Air mass, m, corresponding to diffcrent renith distances of the sun.
For homogenous rays, the intensity of solar energy after passing through an air mass, $m$, is expressed by the equation $\mathrm{I}=\mathrm{I}_{0} a^{m}$, where $\mathrm{I}_{0}$ is the intensity before absorption, $a$ is the atmospheric transmission coefficient, or the proportion of the energy transmitted by unit air mass, and $m$ is the air mass passed through. If we take for unit air mass the atmospheric mass passed through by the rays when the sun is in the zenith, then for zenith distances of the sun less than $80^{\circ}$ the air mass is nearly proportional to the secant of the sun's zenith distance. In general, the secant gives air masses that are too high by an increasing amount as the zenith distance of the sun increases.

The equation by which air masses are sometimes computed is

$$
m=\frac{\text { atmospheric refraction }}{K \sin Z}
$$

where $Z$ is the sun's zenith distance and $K$ is a constant. The uncertain factor in this equation is the atmospheric refraction. Table 100 gives values of $m$ computed by Bemporad (Rend. Acc. Lincei., Roma, Ser. 5, V. 16, 2 Sem. 1907, pp. 66-71) from the above formula, using for $K$ the value $58^{\prime \prime} .36$. The argument is for each degree of $Z$ from $20^{\circ}$ to $89^{\circ}$, with values of $m$ added for $Z=0^{\circ}$, $10^{\circ}$, and $15^{\circ}$. The values of $m$ are given to two decinal places.

Table 101. Relative illumination intensities.
The table gives illumination intensities in foot-candles for zenithal sum, sky at sunset, sky at end of civil twilight, zenithal full moon, quarter moon, and starlight, and the ratio of these intensities to the illumination from the zenithal full moon. For the sources of the data see Kimball, Herbert H., " Duration and Intensity of Twilight," Monthly Weather Revicz, 1916, 44: 6I4-620.

## MISCELLANEOUS TABLES.

## WEIGHT IN GRAMS OF A CUBBC CENTIMETER OF AIR.

The following tables ( IO 2 to IO ) give the factors for computing the weight of a cubic centimeter of air at different temperatures, humidities and pressures.

$$
\delta=\frac{0.0012930}{\mathrm{I}+0.00367 t}\left(\frac{B-0.378 c}{760}\right)
$$

in which $\delta$ is the weight of a cubic centimeter of air expressed in grams, tunder the standard value of gravity ( $g=980.665$ )
$B$ is the atmospheric pressure in millimeters, under standard gravity ;
$c$ is the pressure of aqueous vapor in millimeters, under standard gravity ;
$t$ is the temperature in Centigrade degrees.
For dry atmospheric air (containing 0.0004 of its weight of carbonic acid) at a pressure of 760 mm . and temperature $0^{\circ} C$., the absolute density, or the weight of one cutbic centimeter, is 0.0012930 gram. See p. xlvi.

The weight of a cubic centimeter may also be written as follows:

$$
\delta=\frac{0.0012930}{1+0.002039\left(t-32^{\circ}\right)}\left(\frac{B-0.378 c}{29.92 \mathrm{I}}\right)
$$

where $\delta$ is defined as before, but $B$ and $c$ are expressed in inches and $t$ in Fahrenheit degrees. Thus by the use of tables based on these two formulæ, lines of equal atmospheric density may be drawn for the whole world, no matter whether the original observations are in English or metric measures.

## ENGLISH MEASURES.

TABLES 102, 103, 104.
Table 102. Temperature Term.
This table gives the values and logarithms of the expression

$$
\delta_{t, 29.921}=\frac{0.0012930}{\mathrm{I}+0.002039\left(t-32^{\circ}\right)}
$$

for values of $t$ extending from $-45^{\circ} \mathrm{F}$. to $+140^{\circ} \mathrm{F}$., the intervals between $0^{\circ} F$. and $110^{\circ} F$. being $I^{\circ}$.

The tabular values are given to five significant figures.

Table 103. Term for Iumidity; auxiliary to Table 102.
TABLE 104. Humidity and pressure term. $\frac{h}{29.92 \mathrm{I}}=\frac{B-0.378 e}{29.92 \mathrm{I}}$.
Table 103 gives values of $0.378 e$ to three decimal places as an aid to the use of Table rof. The argument is the dew-point given for every degree from $-60^{\circ} \mathrm{F}$. to $+140^{\circ} \mathrm{F}$. The second column gives the corresponding values of the vapor pressure $(e)$ derived from Tables 74 and 75 .

TABLE 104 gives values and logarithms of $\frac{h}{29.92 \mathrm{I}}=\frac{B-0.378 e}{29.92 \mathrm{I}}$ for values of $h$ extending from 10.0 to 3 I. 7 inches. The logarithms are given to five significant figures and the corresponding numbers to four decimals.

## Example:

The air temperature is $68^{\circ} \mathrm{F}$., the pressure is 29.36 inches and the dewpoint $5 \mathrm{I}^{\circ} \mathrm{F}$. Find the logarithm of the density.
Table IO2, for $t=68^{\circ} \mathrm{F}$., gives

$$
7.08085-10
$$

Table Io3, for dew-point $51^{\circ}$, gives $0.378 e=0.142$ inch,
Table IO4, for $h=B-0.378 e=29.36-0 . I_{4}=29.22$, gives

$$
9.98941 \text { - } 10
$$

Logarithm of density $=$

$$
\frac{30}{7.07056-10}
$$

## METRIC MEASURES.

TABLe 105. Temperature term.
This table gives values and logarithms of the expression

$$
\delta_{t,{ }_{760}}=\frac{0.0012930}{1+0.00367 t}
$$

for values of $t$ extending from $-34^{\circ} \mathrm{C}$. to $+69^{\circ} \mathrm{C}$. The tabular values are given to five significant figures.
Table 106. Term for humidity; auriliary to Table 107.
Table 107. Humidity and pressure terms. $\frac{h}{760}=\frac{B-0.378 e}{760}$.
Table io6 gives the values of $0.37^{8} e$ to hundredths of a millimeter for dew-points extending from $-50^{\circ} \mathrm{C}$. to $+60^{\circ} \mathrm{C}$. Above $-25^{\circ} \mathrm{C}$. the interval is one degree. The values of the vapor pressure, $e$, corresponding to these dew-points, given in the second column," are taken from tables 76 and 77.

Table 107 gives values and logarithms of $\frac{h}{760}=\frac{B-0.378 e}{760}$ for values of $h$ extending from 300 to 799 mm . The atmospheric pressure $B$ is the barometer reading corrected for gravity and $0.37^{8} e$ is the term for humidity obtained from Table io6. The logarithms are given to five significant figures and the corresponding numbers to four decimal places.

Table 108. Atmospheric acater-vapor lines in the visible spectrum.
Table io8, prepared by the Astrophysical Observatory at Washington, gives a summary of lines in St. John's (1928) revision of Rowland's "Preliminary Table of Solar Spectrum Wave Lengths," recorded as of atmospheric water vapor origin. There are more than 400 such lines in Rowland's table, but an abridgment is here made as follows:

Only lines of intensity " I " or greater are here separately given, but the total number and average intensity of the fainter lines lying between these are inserted. The scale of intensities is such that a line of intensity " I " is " just clearly visible" on Rowland's map; the $H$ and $K$ lines are of intensity, I,000; $D_{1}$ (the sodium line of greater wave length), 20; C., 40. "Lines more and more difficult to see " are distinguished by $0,-1,-2$, and -3 .

TABLE 109.
Table 109. Atmospheric water-vapor bands in the infra-red spectrum.
The values of Table 109 relate to the transmission of energy in the minima of various water-vapor bands, when there is 1 cm. of precipitable water in the path through the air. For other amounts of water-vapor, the depths of these minima may be taken as equal to $a^{\hat{o}}$, where $a$ is the coefficient taken from the third column of Table 109 and $\delta$ is the amount of precipitable water in cm . in the path. For average conditions in the transmission of radiation through the atmosphere, $\delta$ may be determined by the modification of Hann's formula $\delta=2.0 \varepsilon \mathrm{sec} . Z$, where $e$ is the vapor pressure in cms. as determined by wet and dry thermometers and $Z$ is the angle which the path makes with the vertical.

For the use of the transmissions observed in such bands for the inverse process of determining the amount of water-vapor in the atmosphere, see Fowle, Astrophysical Journal, 35, p. 149, 1912; 37, p. 359, 1913.

TABLE 110.
Table 110. Transmission percentages of radiation through moist air.
The values of Table ino will be of use when the transmission of energy through the atmosphere containing a known amount of water-vapor is under consideration. An approximate value for the energy transmitted may be had if the amount of energy from the source between the wavelengths of the first column is known and is multiplied by the corresponding transmission coefficients of the subsequent columms of the table. The table is compiled from Fowle, "Water-vapor Transparency," Smithsonian Miscellaneous Collections, 68, No. 8, 1917; see also, Fowle, "The Transparency of Aqueous Vapor," Astrophysical Journal, 42, p. 394, 1915.

TABLE 111.
TABLE 111. The spectral distribution of solar radiation and its transmission by the atmosphere.
The measured relative intensity of radiation at a given wave length depends not only upon the source, but also upon the prismatic dispersion.

Usually, a dispersion coefficient is used to reduce the intensities to what they would have been had the dispersion been the same at all wave lengths, but in Table ini it is that of the ultra-violet glass prism employed by the Astrophysical Observatory of the Smithsonian Institution in making Solar radiation measurements. Column I gives the deviation from $\omega_{1}$ in minutes of arc at which the energy was measured. Column 2 gives the corresponding wave length. Column 3 gives transmission coefficients, $a_{a \lambda}$, for pure dry air at 760 mm . pressure, with the sun in the zenith. They have been computed by means of Rayleigh's equation as modified by King. ${ }^{1}$ Fowle's ${ }^{2}$ values of $a_{v v \lambda}$, the transmission coefficient for that amount of atmospheric water vapor which if precipitated would produce a layer of water one centimeter thick, have been employed to compute the transmission of solar radiation through moist air. Column 5 gives what $\mathrm{Abbot}^{3}$ considers the most reliable value for the relative energy outside the atmosphere, $e_{0 \lambda}$, at the wave lengths corresponding to the deviations of Column I.

The data in the upper part of Columns 6,7 , and 8 have been computed by means of the factors shown in their respective headings. They give the energy distribution with the sun in the zenith and atmospleric pressure of 760 mm ., column 6 with no moisture present, and columns 7 and 8 with sufficient moisture to produce a layer of water 1.0 cm . and 2.0 cm . thick, respectively, if precipitated.

Fowle ${ }^{4}$ has shown that for average conditions the precipitable water in the atmosphere above a given place may be approximately determined from the equation $w=2.3 c$ 10 $\frac{-h}{22000}$, where $e$ is the surface water vapor pressure in centimeters and $l$ is the altitude of the place above sea level, in meters. The Aerological Division of the U. S. Weather Bureau is developing equations that more accurately express the relation between surface vapor pressure and the water-vapor content of the atmosphere, utilizing for this purpose its valuable accumulation of free-air data. It's results, which are approaching completion, will probably be published in the Monthly Weather Review during the current year.

Similarly, the data in the upper part of columns 9 and io have been computed for the sun at zenith distances 60 and 70.7 degrees, and the moisture content of the atmosphere equivalent to 1.0 cm ., and 3.0 cm ., of precipitable water, respectively.
${ }^{1}$ King, Louis Vessot. On the scattering and the absorption of light in gaseous media with applications to the intensity of sky radiation. Phil. Trans. Roy. Soc., London, A. 212, p. 375, 1919.
${ }^{2}$ Fowle, F. E. Water vapor transparency to low-temperature radiation. Smithsonian Misc. Coll., vol. 68, no. 8, 1917.
${ }^{3}$ Abbot, C. G., and others. The distribution of energy in the spectrum of the sun and stars. Smithsonian Misc. Coll., vol. 74, no. 7, 1923.
${ }^{4}$ Fowle, F. E. Atmospheric transparency for radiation. Monthly Weather Review, vol. 42, pp. 2-4, 1914.

These computations take account of the depletions of solar radiation by scattering only. We now proceed to compute the energy in the total solar spectrum after passing through dust-free air containing the amounts of atmospheric moisture specified, and with the sun at the distances from the zenith indicated.

The wave lengths given in column 2 do not cover the entire range of wave lengths included in the solar spectrum. It is therefore necessary to apply a correction to the measured energy so as to include the energy not


Figure i.
measured. Abbot's ${ }^{1}$ method of determining these corrections has been followed in computing the corrections for $\mathfrak{u}$. v. (ultra-violet) and i. r. (infrared) energy not measured, which are given in the lower part of Table inf. The absorption by water vapor in the great water vapor bands in the infrared (w. v. absorption) had been computed by the method developed by Fowle. ${ }^{2}$ Finally, Fowle has computed for this table the absorption by the permanent gases of the atmosphere.

The relative energy in different parts of the solar spectrum may now be determined by summing up the energies at different wave lengths, giving

[^24]double weight to those $10^{\prime}$ in deviation apart. It will be noted that the summation includes the following spectral bands, namely, below $0.346 \mu$, between $0.3+6$ and $0.405 \mu$, between 0.405 and $0.704 \mu$, and above $0.704 \mu$; or the short-wave ultra violet, the long-wave ultra violet, the visible radiation, and the infra-red radiation. The percentage of the energy included in each of these sections to the total energy is given, and the percentage of the total to the total before it enters the atmosphere, or the atmospheric transmission corresponding to the conditions as specified, is also given.

By means of computations such as are given in Table in ithe curves of Figure I, showing the depletion by scattering in passing through dry air, curve I, and through air containing different amounts of moisture, curves 2 to 8 , and the depletion by both scattering and absorption, curves $9-15$, have been constructed. The ordinates give atmospheric transmission ; the abscissas, air masses, $m$, corresponding to zenith distances of the sun $0^{\circ}, 60^{\circ}, 70.7^{\circ}$, and $75.7^{\circ}$. The values for $m$ less than I represent depletions at elevations above sea level.

For a more complete description of this figure see the Monthly Weather Review, $55: 167,1927$, and $56: 394,1928$, and $58: 43$. 1930 .

Abbot's correction for $u$. $v$. radiation below $0.3+6 \mu$, which is not measured, includes the radiation absorbed at these wave lengths by an average amount of atmospheric ozone, but does not take account of variations in the ozone content of the atmosphere. Fowle ${ }^{1}$ has shown that the absorption by ozone in the visible spectrum varies in amount with both time and place, and that it causes a depletion of solar radiation by about 0.2 to 0.4 per cent of the solar constant. This depletion has not been included in "Absorption by permanent gases," near the bottom of Table iI2. The values of atmospheric transmission in the last line of the table are therefore too high by from 0.2 to 0.4 per cent, more or less, depending upon the ozone absorption in the visible spectrum, and disregarding the possible error, probably small in amount, due to variations in the ozone absorption in the ultra-violet.

Example of the use of Figure 1. The atmospheric pressure is 76.0 cm ., the water vapor pressure 0.87 cm ., the zenith distance of the sun is $60^{\circ}$ ( $n=2.0$ ), and the elevation of the station is only slightly above sea level. The precipitable water $=2.3 \times 0.87 \times 10^{\frac{-h}{22000}}=2.0 \mathrm{~cm}$. From Figure I the transmission read from curve i I, for $m=2$, is 0.653 .
Table 112. International meteorological symbols.
The information under this heading has been compiled for the present edition by the librarian of the United States Weather Bureau, and represents current practice in the use of the symbols approved by the International Meteorological Organization. For further information on the sub-

[^25]ject of meteorological symbols, see Monthly Weather Review (Wash., D. C.), May, 1916, pp. 265-274.
table 113. International Cloud Classification.
In the " International Atlas of Clouds and of State of the Sky, Abridged edition for the use of Observers, Paris, 1930," the Commission of the International Meteorological Committee for the Study of Clouds has proposed a classification of clouds under Families A, B, C, and D, Forms a, b, and c, and Genera i to io inclusive. But since the definitions of most of these latter differ but little from those given in the International Cloud Atlas, ad edition, Paris. 1910, and since the new Atlas has not yet been generally accepted, the well known definitions of the older Atlas are adhered to in Table II3.
table 114. Beaufort zecather notation.
This table has been revised in the library of the United States Weather Bureau, and represents the current practice of American and British observers in the use of the Beaufort letters.
table 115. International code for horizontal visibility.
The code for horizontal visibility is used by a large number of Nations and was adopted by the International Commission for Air Navigation. Reference: Convention relating to the Regulation of Aerial Navigation dated October 13. 1919; corrected text of May 1929. The seat of the Commission and of its permanent Secretariat has been fixed at No. 20 Avenue Kléber, Paris.
Table 116. List of metcorological stations.
This list has been extensively revised, mainly by large additions for the continents of South America,' Asia, and Africa. It includes stations for which data appear in the " Réseau Mondial" of the British Metcorological Office for 1922 (published 1929), which were selected to represent, as far as available data permitted, the meteorology of all land areas of the globe, on the basis of two, or in some cases three, stations for each ten-degree square of latitude and longitude. Many additional stations are included for some countries, and especially for the United States.

No attempt has been made in this edition of the Smithsonian Tables to indicate the " order" of the several stations, according to the definitions adopted at the Viemna Congress of 1873: as, owing to the present widespread use of self-recording instruments, the old distinction between first and second order stations has lost much of its importance.

Several stations included in the list are no longer in operation. Data concerning the locations and altitudes of these stations are still valuable, in view of the frequent use made of their records in meteorological and climatological studies.

In general, the established English spellings of geographical names in foreign countries have been followed. Where no English name was established, native orthography has been followed.

## THERMOMETRICAL TABLES

Conversion of thermometric scales -
Approximate Absolute, Centigrade, Fahrenheit, and Reau- mur scales
Fahrenheit scale to Centigrade ..... Table 2
Centigrade scale to Fahrenheit ..... Table 3
Centigrade scale to Fahrenheit, near the boiling point of water ..... Table 4
Differences Fahrenheit to differences Centigrade ..... Table 5
Differences Centigrade to differences Fahrenheit ..... Table 6
Correction for the temperature of the emergent mercurial columnof thermómeters -
Correction for Fahrenheit thermometers ..... Table 7
Correction for Centigrade thermometers ..... Table 8

Table 1.
APPROXIMATE ABSOLUTE, CENTIGRADE, FAHRENHEIT, AND REAUMUR SCALES.

Conversion Formulæ for Approximate Absolute (A.A), Centigrade ( $C$ ), Fahrenheit $(F)$, and Reaumur ( $R$ ) Scales.

| $\begin{aligned} & A \cdot A=5 / 9(F-32)+273=C+273=5 / 4 R+273 \\ & C=5 / 9(F-32)=5 / 4 R=A . A-273=\frac{1}{2}(F-32)\left(\mathrm{I}+\frac{\mathrm{I}}{10}+\frac{\mathrm{I}}{100}+\frac{\mathrm{I}}{1000}+\right) \\ & F=9 / 5 C+32=9 / 4 R+32=9 / 5(A . A-273)+32=2 C\left(\mathrm{I}-\frac{\mathrm{I}}{10}\right)+32 \\ & R=4 / 9(F-32)=4 / 5 C=4 / 5(A . A-273) \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} F \\ C \\ A \cdot A \\ R \end{array}$ | ! | I.I |  | $6^{*}$ |  | 5 $2.77^{*}$ $2.22^{*}$ | 6 $3 \cdot 33^{*}$ $2.66 *$ | 7 $3.88 *$ $3.15 *$ |  |  |  |
| $\begin{array}{r} R \\ C \\ A \cdot A \\ F \end{array}$ | I. <br> 2. | 2.5 4.5 |  | $\begin{array}{ll} 5 & 5 \\ 5 & 9 \\ \text { k These } \end{array}$ | figu | $\begin{gathered} 5 \\ 6.25 \\ 1.25 \\ \text { es repeated } \end{gathered}$ | $\begin{gathered} 6 \\ 7.50 \\ \text { 13.50 } \\ \text { indefinitel } \end{gathered}$ | $\begin{gathered} 7 \\ 8.75 \\ 15.75 \\ y . \end{gathered}$ |  |  |  |
| A. A. | c. | $F$. | R. | A. A. | C. | $F$. | R. | A. A. | c. | $F$. | R. |
| $375^{\circ}$ | $102^{\circ}$ | 215.6 | $8{ }_{\text {I }}$. 6 | $350^{\circ}$ | $77^{\circ}$ | 1 $70^{\circ} .6$ | $6 \mathrm{I}^{\circ} .6$ | $325^{\circ}$ | $52^{\circ}$ | 125.6 | $41^{\circ} .6$ |
| 374 | IOI | 213.8 | 80.8 | 349 | 76 | 168.8 | 60.8 | 324 | 51 | 123.8 | 40.8 |
| 373 | 100 | 212.0 | So.o | 348 | 75 | 167.0 | 60.0 | 323 | 50 | 122.0 | 40.0 |
| 372 | 99 | 210.2 | 79.2 | 347 | 74 | 165.2 | 59.2 | 322 | 49 | 120.2 | 39.2 |
| 37 I | 98 | 208.4 | 78.4 | 346 | 73 | 163.4 | 58.4 | 321 | 48 | 118.4 | 38.4 |
| 370 | 97 | 206.6 | 77.6 | 345 | 72 | 16 1. 6 | 57.6 | 320 | 47 | 116.6 | 37.6 |
| 360 | 96 | 20.4 | 76.8 | 344 | 71 | r 59.8 | 56.8 | 319 | 46 | 114.8 | 36.8 |
| 368 | 95 | 203.0 | 76.0 | 343 | 70 | 158.0 | 56.0 | 318 | 45 | 113.0 | 36.0 |
| 367 | 94 | 201.2 | 75.2 | $34^{2}$ | 69 | 156.2 | 55.2 | 317 | 44 | III. 2 | 35.2 |
| 306 | 93 | 199.4 | $74 \cdot 4$ | 34 I | 68 | I 54.4 | 54.4 | 316 | 43 | 109.4 | 34.4 |
| 365 | 92 | 197.6 | 73.6 | 340 | 67 | 152.6 | 53.6 | 315 | 42 | 107.6 | 33.6 |
| 364 | 91 | 195.8 | 72.8 | 339 | 66 | 150.8 | 52.8 | 314 | 41 | 105.8 | 32.8 |
| 363 | 90 | 194.0 | 72.0 | 338 | 65 | 149.0 | 52.0 | 313 | 40 | 104.0 | 32.0 |
| 362 | 89 | 192.2 | 71.2 | 337 | 64 | 147.2 | 51.2 | 312 | 39 | 102.2 | 31.2 |
| 361 | 88 | 190.4 | 70.4 | 336 | 63 | 145.4 | 50.4 | 311 | 38 | 100.4 | 30.4 |
| 360 | 87 | I 88.6 | 60.6 | 335 | 62 | 143.6 | 49.6 | 310 | 37 | 98.6 | 29.6 |
| 359 | 86 | I'S6.8 | 68.8 | 334 | 61 | 14 I .8 | 48.8 | 309 | 36 | 96.8 | 28.8 |
| 358 | 85 | 185.0 | 68.0 | 333 | 60 | 140.0 | 48.0 | 308 | 35 | 95.0 | 28.0 |
| 357 | 84 | 183.2 | 67.2 | 332 | 59 | I 38.2 | 47.2 | 307 | 34 | 93.2 | 27.2 |
| 356 | 83 | 181.4 | 66.4 | 331 | 58 | I 36.4 | 46.4 | 306 | 33 | 91.4 | 26.4 |
| 355 | 82 | 179.6 | 65.6 | 330 | 57 | 134.6 | 45.6 | 305 | 32 | 80.6 | 25.6 |
| 354 | 8 I | 177.8 | 64.8 | 329 | 56 | I 32.8 | 44.8 | 304 | 31 | 87.8 | 24.8 |
| 353 | 80 | 176.0 | 64.0 | 328 | 55 | I 31.0 | 44.0 | 303 | 30 | 86.0 | 24.0 |
| $35^{2}$ | 79 | $17+.2$ | 63.2 | 327 | 54 | 129.2 | 43.2 | 302 | 29 | 84.2 | 23.2 |
| 351 | 78 | 172.4 | 62.4 | 326 | 53 | 127.4 | 42.4 | 301 | 28 | 82.4 | 22.4 |
| 350 | 77 | 170.6 | 6 r .6 | 325 | 52 | 125.6 | 41.6 | 300 | 27 | 80.6 | 21.6 |
| A. A. | c. | F. | R. | A. A. | C. | $F$. | R. | A.A. | c. | F. | R. |


| A.A. | C. | $F$. | R. | A. A. | C. | F. | R. | A. A. | C. | $F$. | R. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $300^{\circ}$ | $27^{\circ}$ | 80, 6 | 2 I $^{\circ} 6$ | $250^{\circ}$ | $-23^{\circ}$ | - 9.4 | -18.4 | $200^{\circ}$ | $-73^{\circ}$ | - 99.4 | $-58.4$ |
| 299 | 26 | 78.8 | 20.8 | 249 | 24 | 11.2 | 19.2 | 199 | 74 | 101.2 | 59.2 |
| 298 | 25 | 77.0 | 20.0 | 248 | 25 | ${ }^{1} 3.0$ | 20.0 | 198 | 75 | 103.0 | 60.0 |
| 297 | 24 | 75.2 | 19.2 | 247 | 26 | 14.8 | 20.8 | 197 | 76 | 10.4 | 60.8 |
| 296 | 23 | 73.4 | 18.4 | 246 | 27 | 16.6 | 21.6 | 196 | 77 | 106.6 | 6 ¢. 6 |
| 295 | 22 | 71.6 | 17.6 | 245 | $-28$ | $-18.4$ | -22.4 | 195 | $-78$ | -108.4 | -62.4 |
| 29.4 | 21 | 69.8 | 16.8 | 244 | 29 | 20.2 | 23.2 | 194 | 79 | 110.2 | 63.2 |
| 293 | 20 | 68.0 | 16.0 | 2.43 | 30 | 22.0 | 24.0 | 193 | 80 | I 12.0 | 64.0 |
| 292 | 19 | 66.2 | 15.2 | 242 | 31 | 23.8 | 24.8 | 192 | 81 | 113.8 | 64.8 |
| 291 | 18 | 64.4 | 14.4 | 241 | 32 | 25.6 | 25.6 | 191 | 82 | 115.6 | 65.6 |
| 290 | 17 | 62.6 | 13.6 | 240 | -33 | -27.4 | -26.4 | 190 | $-83$ | - 117.4 | -66.4 |
| 289 | 16 | 60.8 | 12.8 | 239 | 34 | 29.2 | 27.2 | 189 | 8 | 119.2 | 67.2 |
| 288 | 15 | 59.0 | 12 | 238 | 35 | 31.0 | 28.0 | 188 | 85 | 121.0 | 68.0 |
| 287 | 14 | 57.2 | II. 2 | 237 | 36 | 32.8 | 28.8 | 187 | 86 | 122.8 | 68.8 |
| 286 | 13 | 55.4 | 10.4 | 236 | 37 | 34.6 | 29.6 | I 86 | 87 | 124.6 | 69.6 |
| 285 | 12 | 53.6 | 9.6 | 235 | $-38$ | -36.4 | -30.4 | 185 | -88 | -126.4 | -70.4 |
| $28+$ | 11 | 51.8 | 8.8 | 234 | 39 | 38.2 | 31.2 | 184 | 89 | 128.2 | 71.2 |
| 283 | 10 | 50.0 | 8.0 | 233 | 40 | 40.0 | 32.0 | 183 | 90 | 130.0 | 72.0 |
| 282 | 8 | 48.2 | 7.2 | 232 | 41 | 41.8 | 32.8 | 182 | 91 | 131.8 | 72.8 |
| 281 | 8 | 46.4 | 6.4 | 231 | 42 | 43.6 | 33.6 | ISI | 92 | 133.6 | 73.6 |
| 280 | 7 | 44.6 | 5.6 | 230 | -43 | -45.4 | $-34.4$ | 180 | -93 | - 135.4 | -74.4 |
| 279 | 6 | 42.8 | 4.8 | 229 | 44 | 47.2 | 35.2 | 179 | 94 | 137.2 | 75.2 |
| 278 | 5 | 41.0 | 4.0 | 228 | 45 | 49.0 | 36.0 | 178 | 95 | 139.0 | 76.0 |
| 277 | 4 | 39.2 | 3.2 | 227 | 46 | 50.8 | 36.8 | 177 | 96 | 140.8 | 76.8 |
| 276 | 3 | 37.4 | 2.4 | 226 | 47 | 52.6 | 37.6 | 176 | 97 | 142.6 | 77.6 |
| 275 | + 2 | 35.6 | + 1.6 | 225 | -48 | -54.4 | -38.4 | 175 | -98 | - 144.4 | $-78.4$ |
| 274 | + I | 33.8 | + 0.8 | 22.4 | 49 | 56.2 | 39.2 | 174 | 99 | 146.2 | 79.2 |
| 273 | $\pm 0$ | 32.0 | $\pm 0.0$ | 223 | 50 | 58.0 | 40.0 | 173 | 100 | 148.0 | 80.0 |
| 272 | - | 30.2 | - 0.8 | 222 | 51 | 59.8 | 40.8 | 172 | 101 | 149.8 | 80.8 |
| 271 | - 2 | 28.4 | - 1.6 | 22 I | 52 | 61.6 | 41.6 | 171 | 102 | 151.6 | 8ı. 6 |
| 270 | $-3$ | 26.6 | - 2.4 | 220 | -53 | $-63.4$ | -42.4 | 170 | -103 | -153.4 | -82.4 |
| 269 | 4 | 24.8 | 3.2 | 219 | 54 | 65.2 | 43.2 | 169 | 104 | 155.2 | 83.2 |
| 268 | 5 | 23.0 | 4.0 | 218 | 55 | 67.0 | 44.0 | 168 | 105 | 157.0 | 84.0 |
| 267 | 6 | 21.2 | 4.8 | 217 | 56 | 68.8 | 44.8 | 167 | 106 | 158.8 | 84.8 |
| 266 | 7 | 19.4 | 5.6 | 216 | 57 | 70.6 | 45.6 | 166 | 107 | 160.6 | 85.6 |
| 265 | -8 | 17.6 | - 6.4 | 215 | -58 | -72.4 | -46.4 | 165 | -108 | -162.4 | -86.4 |
| 264 | 9 | 15.8 | 7.2 | 214 | 59 | 74.2 | 47.2 | 164 | 109 | 164.2 | 87.2 |
| 263 | 10 | 14.0 | 8.0 | 213 | 60 | 76.0 | 48.0 | 163 | 110 | 166.0 | 88.0 |
| 262 | II | 12.2 | 8.8 | 212 | 61 | 77.8 | 48.8 | 162 | III | 167.8 | 88.8 |
| 261 | I 2 | 10.4 | 9.6 | 2 II | 62 | 79.6 | 49.6 | 161 | II 2 | 169.6 | 89.6 |
| 260 | -13 | 8.6 | - 10.4 | 210 | -63 | -81.4 | -50.4 | 160 | -113 | -171.4 | -90.4 |
| 259 | 14 | 6.8 | II. 2 | 209 | 64 | 83.2 | 51.2 | 159 | 114 | 173.2 | 91.2 |
| 258 | 15 | 5.0 | 12.0 | 208 | 65 | 85.0 | 52.0 | 158 | 115 | 175.0 | 92.0 |
| 257 | 10 | 3.2 | 12.8 | 207 | 66 | 86.8 | 52.8 | 157 | 116 | 176.8 | 92.8 |
| 256 | 17 | + I. 4 | 13.6 | 206 | 67 | 88.6 | 53.6 | 156 | 117 | 178.6 | 93.6 |
| 255 | - 18 | -0.4 | - 14.4 | 205 | -68 | -90.4 | -54.4 | 155 | -118 | -180.4 | -94.4 |
| 254 | 19 | 2.2 | 15.2 | 204 | 69 | 92.2 | 55.2 | 154 | 119 | 182.2 | 95.2 |
| 253 | 20 | 4.0 | 16.0 | 203 | 70 | 94.0 | 56.0 | 153 | 120 | 184.0 | 96.0 |
| 252 | 21 | 5.8 | 16.8 | 202 | 71 | 95.8 | 56.8 | 152 | 121 | 185.8 | 96.8 |
| 251 | 22 | 7.6 | r 7.6 | 201 | 72 | 97.6 | 57.6 | 151 | 122 | 187.6 | 97.6 |
| 250 | $-23$ | -9.4 | -I8.4 | 200 | -73 | -99.4 | -58.4 | 150 | -123 | -189.4 | -98.4 |
| A. A. | C. | F. | R. | A. A. | C. | $F$. | R. | A.A. | C. | F. | R. |


| A. A. | C. | $F$. | R. | A. A. | C. | F. | R. | A. A. | C. | $F$. | R. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $150^{\circ}$ | $-123^{\circ}$ | -189.4 | - 98.4 | $100^{\circ}$ | $-173^{\circ}$ | -279.4 | -138.4 | $50^{\circ}$ | $-223^{\circ}$ | $-369.4$ | -178.4 |
| 149 | 124 | 191.2 | 99.2 | 99 | 174 | 28 I .2 | 139.2 | 49 | 224 | 371.2 | 179.2 |
| 148 | 125 | 193.0 | 100.0 | 98 | 175 | 283.0 | 140.0 | 48 | 225 | 373.0 | 180.0 |
| 147 | 126 | 19.4 .8 | 100.8 | 97 | 176 | 284.8 | 140.8 | 47 | 226 | 374.8 | I80.8 |
| 1.46 | 127 | 196.6 | 101. 6 | 96 | 177 | 286.6 | 141.6 | 46 | 227 | 376.6 | I81. 6 |
| 145 | -128 | -198.4 | -102.4 | 95 | $-178$ | $-288.4$ | -142.4 | 45 | -228 | -378.4 | -I82.4 |
| 144 | 129 | 200.2 | 103.2 | 94 | 179 | 290.2 | 143.2 | 44 | 229 | 380.2 | 183.2 |
| I43 | 130 | 202.0 | 104.0 | 93 | 180 | 292.0 | 144.0 | 43 | 230 | 382.0 | I84.0 |
| 142 | 131 | 203.8 | 104.8 | 92 | ISI | 293.8 | 144.8 | 42 | 231 | 383.8 | IS4.8 |
| 141 | 132 | 205.6 | 105.6 | 91 | 182 | 295.6 | 145.6 | 41 | 232 | 385.6 | 185.6 |
| 140 | -I33 | -207.4 | -106.4 | 90 | $-183$ | -297.4 | -146.4 | 40 | -233 | $-387 \cdot 4$ | -186.4 |
| 139 | 134 | 209.2 | 107.2 | 89 | 184 | 299.2 | 147.2 | 39 | 234 | 389.2 | 187.2 |
| 138 | 135 | 211.0 | 108.0 | 88 | 185 | 301.0 | I48.0 | 38 | 235 | 391.0 | 188.0 |
| 137 | 136 | 212.8 | 108.8 | 87 | I 86 | 302.8 | 148.8 | 37 | 236 | 392.8 | 188.8 |
| 136 | 137 | 214.6 | 109.6 | 86 | 187 | 304.6 | 149.6 | 36 | 237 | 394.6 | I 89.6 |
| 135 | $-\mathrm{I} 38$ | -216.4 | -IIO.4 | 85 | -188 | -306.4 | -150.4 | 35 | $-238$ | $-396.4$ | -190.4 |
| 134 | I 39 | 218.2 | 1.2 | ${ }_{8} 8_{4}$ | I89 | 308.2 | 151.2 | 34 | 239 | 398.2 | 191.2 |
| 133 | 140 | 220.0 | 112.0 | 83 | 190 | 310.0 | 152.0 | 33 | 240 | 400.0 | 192.0 |
| 132 | 141 | 221.8 | 112.8 | 82 | 191 | 31.8 | 152.8 | 32 | 241 | 401.8 | 192.8 |
| I3 I | 142 | 223.6 | 113.6 | 8 I | 192 | 313.6 | 153.6 | 31 | $24^{2}$ | 403.6 | 193.6 |
| 130 | -143 | -225.4 | -114.4 | 80 | -193 | $-315.4$ | -154.4 | 30 | -243 | -405.4 | -194.4 |
| I29 | 144 | 227.2 | 115.2 | 79 | $19+$ | 317.2 | 155.2 | 29 | 2.4 | 407.2 | 195.2 |
| 128 | 145 | 229.0 | 116.0 | 78 | 195 | 319.0 | 156.0 | 28 | 245 | 409.0 | 196.0 |
| 127 | 146 | 230.8 | I 16.8 | 77 | 196 | 320.8 | 156.8 | 27 | 246 | 410.8 | 196.8 |
| 126 | 147 | 232.6 | 117.6 | 76 | 197 | 322.6 | 157.6 | 26 | 247 | 412.6 | 197.6 |
| 125 | $-148$ | -234.4 | -118.4 | 75 | $-198$ | -324.4 | $-158.4$ | 25 | $-248$ | $-414.4$ | -198.4 |
| 124 | 149 | 236.2 | 119.2 | 74 | 199 | 326.2 | 159.2 | 24 | 249 | 416.2 | 199.2 |
| 123 | 150 | 238.0 | 120.0 | 73 | 200 | 328.0 | 160.0 | 23 | 250 | 4 IS .0 | 200.0 |
| 122 | 151 | 239.8 | 120.8 | 72 | 201 | 329.8 | 160.8 | 22 | 251 | 419.8 | 200.8 |
| 12 I | 152 | 241.6 | 121.6 | 71 | 202 | 331.6 | 161.6 | 2 I | 252 | 42 I .6 | 201.6 |
| 120 | - 153 | -243.4 | -122.4 | 70 | -203 | $-333.4$ | -162.4 | 20 | -253 | -423.4 | -202.4 |
| 119 | 154 | 245.2 | 123.2 | 69 | 204 | 335.2 | 163.2 | 19 | 254 | 425.2 | 203.2 |
| II8 | 155 | 247.0 | 124.0 | 68 | 205 | 337.0 | 164.0 | IS | 255 | 427.0 | 204.0 |
| 117 | 156 | 248.8 | 124.8 | 67 | 206 | 338.8 | 164.8 | 17 | 256 | 428.8 | 204.8 |
| I 16 | 157 | 250.6 | 125.6 | 66 | 207 | 340.6 | 165.6 | 16 | 257 | 430.6 | 205.6 |
| 115 | -158 | -252.4 | -126.4 | 65 | -208 | -342.4 | -166.4 | 15 | -258 | -432.4 | -206.4 |
| II4 | 159 | 254.2 | 127.2 | 64 | 209 | 3.4 .42 | 167.2 | 14 | 259 | 434.2 | 207.2 |
| II3 | 160 | 256.0 | 128.0 | 63 | 210 | 346.0 | 168.0 | 13 | 260 | 436.0 | 208.0 |
| II 2 | 161 | 257.8 | 128.8 | 62 | 211 | 347.8 | 168.8 | 12 | 261 | 437.8 | 208.8 |
| I II | 162 | 259.6 | 129.6 | 61 | 212 | 349.6 | 169.6 | II | 262 | 439.6 | 209.6 |
| 110 | -163 | -261.4 | -r30.4 | 60 | -213 | -351.4 | -170.4 | 10 | $-263$ | $-4.41 .4$ | -210.4 |
| 109 | 164 | 263.2 | 131.2 | 59 | 214 | 353.2 | 171.2 | 9 | 264 | 443.2 | 211.2 |
| 108 | 165 | 265.0 | 132.0 | 58 | 215 | 355.0 | 172.0 | 8 | 265 | 445.0 | 212.0 |
| 107 | 166 | 266.8 | 132.8 | 57 | 216 | 356.8 | 172.8 | 7 | 266 | 446.8 | 212.8 |
| 106 | 167 | 268.6 | 133.6 | 56 | 217 | 358.6 | 173.6 | 6 | 267 | 448.6 | 213.6 |
| 105 | -168 | -270.4 | -134.4 | 55 | $-218$ | $-360.4$ | -174.4 | 5 | -268 | -450.4 | -214.4 |
| 104 | 169 | 272.2 | 135.2 | 54 | 219 | 362.2 | 175.2 | 4 | 269 | 452.2 | 215.2 |
| 103 | 170 | 274.0 | 136.0 | 53 | 220 | 364.0 | 176.0 | 3 | 270 | 454.0 | 216.0 |
| 102 | 171 | 275.8 | 136.8 | 52 | 22 I | 365.8 | 176.8 | 2 | 271 | 455.8 | 216.8 |
| IOI | 172 | 277.6 | 137.6 | 51 | 222 | 367.6 | 177.6 | I | 272 | 457.6 | 217.6 |
| 100 | -173 | -279.4 | -I38.4 | 50 | -223 | $-369.4$ | -178.4 | 0 | -273 | -459.4 | $-218.4$ |
| A.A. | C. | $F$. | R. | A.A. | C. | F. | R. | A. A. | C. | $F$. | R. |

FAHRENHEIT SUALE TO CENTIGRADE.

| Fahren. heit. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | c. | c. | c. | c. | c. | c. | c. | c. | c. | c. |
| $+130^{\circ}$ | +54. ${ }^{\circ} 44$ | $+54.50$ | $+54.56$ | $+54.6 \mathrm{I}$ | $+54.67$ | $+54^{\circ} 72$ | $+54^{\circ} 78$ | $+54^{\circ} ._{3}$ | $+54.89$ | $+54.94$ |
| 129 | 53.89 | 53.94 | 54.00 | 54.06 | 54.11 | 54.17 | 54.22 | 54.28 | 54.33 | 54.39 |
| 128 | 53.33 | 53.39 | 53.44 | 53.50 | 53.56 | 53.61 | 53.67 | 53.72 | 53.78 | 53.83 |
| 127 | 52.78 | 52.83 | 52.89 | 52.94 | 53.00 | 53.06 | 53.1 I | 53.17 | 53.22 | 53.28 |
| 126 | 52.22 | 52.28 | 52.33 | 52.39 | 52.44 | 52.50 | 52.56 | 52.6 I | 52.67 | 52.72 |
| +125 | +51.67 | $+51.72$ | $+51.78$ | +51. $\mathrm{S}_{3}$ | +51.89 | +51.94 | +52.00 | +52.06 | +52.11 | +52.17 |
| 124 | 5 I.II | 51.17 | 51.22 | 51.28 | 51.33 | 5 I .39 | 51.44 | 51.50 | 51.56 | 51.61 |
| 123 | 50.56 | 50.61 | 50.67 | 50.72 | 50.78 | 50.83 | 50.89 | 50.94 | 51.00 | 51.06 |
| 122 | 50.00 | 50.06 | 50.11 | 50.17 | 50.22 | 50.28 | 50.33 | 50.39 | 50.44 | 50.50 |
| 121 | 49.44 | 49.50 | 49.56 | 49.6I | 49.67 | 49.72 | 49.78 | 49.83 | 49.89 | 49.94 |
| $+120$ | $+48.89$ | +43.94 | $+49.00$ | +49.06 | +49. 11 | +49.17 | +49.22 | +49.28 | $+49.33$ | +49.39 |
| 119 | 48.33 | 48.39 | 48.44 | 48.50 | 48.56 | 48.61 | 48.67 | 48.72 | 48.78 | 48.83 |
| 118 | 47.78 | 47.83 | 47.89 | 47.94 | 48.00 | 48.06 | 48. I I | 48.17 | 48.22 | 48.28 |
| 117 | 47.22 | 47.28 | 47.33 | 47.39 | 47.44 | 47.50 | 47.56 | 47.61 | 47.67 | 47.72 |
| I 16 | 46.67 | 46.72 | 46.78 | 46.83 | 46.89 | 46.94 | 47.00 | 47.06 | 47.11 | 47.17 |
| $+115$ | +46. 11 | +46.17 | $+46.22$ | $+46.28$ | $+46.33$ | +46.39 | $+46.44$ | $+46.50$ | +46.56 | +46.61 |
| II4 | 45.56 | 45.61 | 45.67 | 45.72 | 45.78 | 45.33 | 45.89 | 45.94 | 46.00 | 46.06 |
| 113 | 45.00 | 45. 06 | 45.11 | 45.17 | 45.22 | 45.28 | 45.33 | 45.39 | 45.44 | 45.50 |
| II2 | 44.44 | 44.50 | 44.56 | 44.61 | 44.67 | 44.72 | 44.78 | 44.33 | 44.89 | 44.94 |
| III | 43.89 | 43.94 | 44.00 | 44.06 | 44.11 | 44.17 | 44.22 | 44.28 | 44.33 | 44.39 |
| $+110$ | $+43.33$ | +43.39 | +43.44 | +43.50 | +43.56 | +43.6I | $+43.67$ | +43.72 | $+43.78$ | +43.83 |
| 109 | 42.75 | 42.83 | 42.89 | 42.94 | 43.00 | 43.06 | 43.1I | 43.17 | 43.22 | 43.28 |
| 108 | 42.22 | 42.28 | 42.33 | 42.39 | 42.44 | 42.50 | 42.56 | 42.61 | 42.67 | 42.72 |
| 107 | 41.67 | 41.72 | 41.78 | 41.83 | 41.89 | 41.94 | 42.00 | 42.06 | 42.11 | 42.17 |
| 106 | 41.1I | 41.17 | 41.22 | 41.28 | 41.33 | 41.39 | 4 I .44 | 41.50 | 41.56 | 41.61 |
| $\div 105$ | $+40.56$ | +40.6I | $+40.67$ | $+40.72$ | +40.78 | $+40.83$ | +40.89 | +40.94 | $+41.00$ | +41.06 |
| 104 | 40.00 | 40.06 | 40.11 | 40.17 | 40.22 | 40.28 | 40.33 | 40.39 | 40.44 | 40.50 |
| 103 | 39.44 | 39.50 | 39.56 | 39.61 | 39.67 | 39.72 | 39.78 | 39.83 | 39.89 | 39.94 |
| 102 | 38.89 | 38.94 | 39.00 | 39.06 | 39. I I | 39.17 | 39.22 | 39.28 | 39.33 | 39.39 |
| 101 | 38.33 | 38.39 | 38.44 | 38.50 | 38.56 | 38.61 | 38.67 | 38.72 | 38.78 | 38.83 |
| $+100$ | $+37.78$ | $+37.83$ | +37.89 | +37.94 | $+38.00$ | $+38.06$ | +38.11 | $+38.17$ | $+38.22$ | $+38.28$ |
| 99 | 37.22 | 37.28 | 37.33 | 37.39 | 37.44 | 37.50 | 37.56 | 37.61 | 37.67 | 37.72 |
| 98 | 36.67 | 36.72 | 36.78 | 36.83 | 36.89 | 36.94 | 37.00 | 37.06 | 37. I I | 37.17 |
| 97 | 36.11 35.56 | 36.17 | 36.22 35.67 | 36.28 | 36.33 | 36.39 | 36.44 | 36.50 | 36.56 | 36.61 |
| 96 | 35.56 | 35.61 | 35.67 | 35.72 | 35.78 | 35.83 | 35.89 | 35.94 | 36.00 | 36.06 |
| $+95$ | +35.00 | $+35.06$ | +35.11 | +35.17 | +35.22 | +35.28 | +35.33 | + 35.39 | $+35.44$ | +35.50 |
| 94 | 34.44 | 34.50 | 34.56 | 34.61 | 34.67 | 34.72 | 34.78 | 34.83 | 34.89 | 34.94 |
| 93 | 33.89 | 33.94 | 34.00 | 34.06 | 34.11 | 34.17 | 34.22 | 34.28 | 34.33 | 34.39 |
| 92 | 33.33 | 33.39 | 33.44 | 33.50 | 33.56 | 33.61 | 33.67 | 33.72 | 33.78 | 33.83 |
| 91 | 32.78 | 32.83 | 32.89 | 32.94 | 33.00 | 33.06 | 33.1 I | 33.17 | 33.22 | 33.28 |
| $+90$ | +32.22 | +32.28 | +32.33 | +32.39 | +32.44 | +32.50 | $+32.56$ | +32.61 | +32.67 | +32.72 |
| 89 | 31.67 | 31.72 | 31.78 | 31.83 | 31.89 | 31.94 | 32.00 | 32.06 | 32.11 | 32.17 |
| 88 | 31.11 | 31.17 | 31.22 | 31.28 | 31.33 | 31.39 | 31.44 | 31.50 | 31.56 | 3 S .61 |
| 87 86 | 30.56 | 30.61 | 30.67 | 30.72 | 30.78 | 30.83 | 30.89 | 30.94 | 31.00 | 31.06 |
| 86 | $30 . \mathrm{co}$ | 30.06 | 30.11 | 30.17 | 30.22 | 30.28 | 30.33 | 30.39 | 30.44 | 30.50 |
| $+85$ | +29.44 | $+29.50$ | +29.56 | +29.6I | +29.67 | +29.72 | +29.78 | +29.83 | +29.89 | +29.94 |
| 84 | 2889 | 28.94 | 29.00 | 29.06 | 29.11 | 29.17 | 29.22 | 29.28 | 29.33 | 29.39 |
| 83 | 28.33 | 28.39 | 28.44 | 28.50 | 28.56 | 28.61 | 28.67 | 28.72 | 28.78 | 28.83 |
| S2 | 27.78 27.22 | 27.83 | 27.89 | 27.94 | 28.00 | 28.06 | 28.11 | 28.17 | 28.22 | 28.28 |
| $+80$ | 27.22 +26.67 | 27.28 | 27.33 | 27.39 | 27.44 | 27.50 | 27.56 | 27.61 | 27.67 | 27.72 |
| +80 | +26.67 | +26.72 | +26.78 | +26.83 | +26.89 | +26.94 | +27.00 | +27.06 | +27.11 | +27.17 |
|  | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |

Smithsonian Tableg.
table 2.
FAHRENHEIT SCALE TO CENTIGRADE.

| Fahren. heit. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $+80^{\circ}$ | $\begin{gathered} c . \\ +26^{\circ} .67 \end{gathered}$ | $\begin{gathered} c . \\ +26^{\circ} \cdot 72 \end{gathered}$ | $\begin{gathered} \text { c. } \\ +26^{\circ} \cdot 78 \end{gathered}$ | $+26.83$ | $\begin{gathered} c . \\ +26: 89 \end{gathered}$ | $\begin{gathered} \text { C. } \\ +26.94 \end{gathered}$ | $\begin{array}{r} \text { c. } \\ +27.00 \end{array}$ | $\begin{gathered} c . \\ +27.06 \end{gathered}$ | $+27^{\circ} .11$ | $+27^{\circ} .17$ |
| 79 | 26.11 | 26.17 | 26.22 | 26.28 | 26.33 | 26.39 | 26.44 | 26.50 | 26.56 | 26.6 I |
| 78 | 25.56 | 25.6 I | 25.67 | 25.72 | 25.78 | 25.83 | 25.89 | 25.94 | 26.00 | 26.06 |
| 77 | 25.00 | 25.06 | 25. 11 | 25.17 | 25.22 | 25.28 | 25.33 | 25.39 | 25.44 | 25.50 |
| 76 | 24.44 | 24.50 | 24.56 | 24.6 I | 24.67 | 24.72 | 24.78 | 24.83 | 24.89 | 24.94 |
| +75 | +23.89 | +23.94 | +24.00 | $+24.06$ | $+24.11$ | $+24.17$ | +24.22 | +24.28 | $+24.33$ | $+24.39$ |
| 74 | 23.33 | 23.39 | 23.44 | 23.50 | 23.56 | 23.61 | 23.67 | 23.72 | 23.78 | 23.83 |
| 73 | 22.78 | 22.83 | 22.89 | 22.94 | 23.00 | 23.06 | 23.11 | 23.17 | 23.22 | 23.28 |
| 72 | 22.22 | 22.28 | 22.33 | 22.39 | 22.44 | 22.50 | 22.56 | 22.61 | 22.67 | 22.72 |
| 71 | 21.67 | 21.72 | 21.78 | 21.83 | 2 I .89 | 21.94 | 22.00 | 22.06 | 22.1 I | 22.i7 |
| +70 | +2I.II | +21.17 | +21.22 | +21.28 | +21.33 | +21.39 | +21.44 | $+21.50$ | +21.56 | +21.6I |
| 69 | 20.56 | 20.61 | 20.67 | 20.72 | 20.78 | 20.83 | 20.89 | 20.94 | 2 I . 00 | 21.06 |
| 68 | 20.00 | 20.06 | 20.11 | 20.17 | 20.22 | 20.28 | 20.33 | 20.39 | 20.44 | 20.50 |
| 67 | 19.44 | 19.50 | 19.56 | 19.61 | 19.67 | 19.72 | 19.78 | 19.83 | 19.39 | 19.94 |
| 66 | 18.89 | 18.94 | 19.00 | 19.06 | 19.11 | 19.17 | 19.22 | 19.28 | 19.33 | 19.39 |
| $+65$ | +18.33 | +18.39 | +18.44 | +18.50 | +18.56 | +18.6I | +18.67 | +18.72 | +18.78 | +18.83 |
| 64 | 17.78 | 17.83 | 17.89 | 17.94 | 18.00 | 18.06 | 18.11 | 18.17 | 18.22 | 18.28 |
| 63 | 17.22 | 17.28 | 17.33 | 17.39 | 17.44 | 17.50 | 17.56 | 17.61 | 17.67 | 17.72 |
| 62 | 16.67 | 16.72 | 16.78 | 16.83 | 16.89 | 16.94 | 17.00 | 17.06 | 17.11 | 17.17 |
| 61 | 16.11 | 16.17 | 16.22 | 16.28 | 16.33 | 16.39 | 16.44 | 16.50 | 16.56 | 16.61 |
| $+60$ | +15.56 | +15.61 | +15.67 | +15.72 | $+15.78$ | +15.83 | +15.89 | +15.94 | $+16.00$ | $+16.06$ |
| 59 | 15.00 | 15.06 | 15.11 | 15.17 | 15.22 | 15.28 | 15.33 | 15.39 | 15.44 | 15.50 |
| 58 | 14.44 | 14.50 | 14.56 | 14.61 | 14.67 | 14.72 | 14.78 | 14.33 | 14.89 | 14.94 |
| 57 | 13.89 | 13.94 | 14.00 | 14.06 | 14.11 | 14.17 | 14.22 | 14.28 | 14.33 | 14.39 |
| 56 | 13.33 | 13.39 | 13.44 | 13.50 | 13.56 | 13.61 | 13.67 | 13.72 | 13.78 | 13.83 |
| $+55$ | +12.78 | +12.83 | +12.89 | +12.94 | +13.00 | +13.06 | +13.11 | +13.17 | +13.22 | 广 13.28 |
| 54 | 12.22 | 12.28 | 12.33 | 12.39 | 12.44 | 12.50 | 12.56 | 12.61 | 12.67 | 12.72 |
| 53 | 11.67 | 11.72 | 11.78 | 11.83 | 11.89 | 11.94 | 12.00 | 12.06 | 12.11 | 12.17 |
| 52 | II. II | 11.17 | 11.22 | 11.28 | 11.33 | 11.39 | 11.44 | 11.50 | 11.56 | II. 61 |
| 51 | 10.56 | 10.61 | 10.67 | 10.72 | 10.78 | 10.83 | 10.89 | 10.94 | 11.00 | 11.06 |
| $+50$ | $+10.00$ | +10.06 | +10.11 | +10.17 | +10.22 | +10.28 | +10.33 | +10.39 | +10.44 | +10.50 |
| 49 | 9.44 | 9.50 | 9.56 | 9.61 | 9.67 | 9.72 | 9.78 | 9.83 | 9.89 | 9.94 |
| 48 | 8.89 | 8.94 | 9.00 | 9.06 | 9. 11 | 9.17 | 9.22 | 9.28 | 9.33 | 9.39 |
| 47 | 8.33 | 8.39 | 8.44 | 8.50 | 8.56 | 8.61 | 8.67 | 8.72 | 8.78 | 8.83 |
| 46 | 7.78 | 7.83 | 7.89 | 7.94 | 8.00 | 8.06 | 8.11 | S. 17 | S. 22 | 8. 28 |
| +45 | + 7.22 | + 7.28 | + 7.331 | + 7.39 | + 7.44 | $+7.50$ | + 7.56 | $+7.61$ | $+7.67$ | $+7.72$ |
| 44 | 6.67 | 6.72 | 6.78 | 6.83 | 6.89 | 6.94 | 7.00 | 7.06 | 7.11 | 7.17 |
| 43 | 6.11 | 6.17 | 6.22 | 6.28 | 6.33 | 6.39 | 6.44 | 6.50 | 6.56 | 6.61 |
| 42 | 5.56 | 5.61 | 5.67 | 5.72 | 5.78 | 5.83 | 5.89 | 5.94 | 6.00 | 6.06 |
| 41 | 5.00 | 5.06 | 5.11 | 5.17 | 5.22 | 5.28 | $5 \cdot 33$ | $5 \cdot 39$ | 5.44 | $5 \cdot 50$ |
| $+40$ | $+4.44$ | $+4.50$ | $+4.56$ | $+4.6 \mathrm{I}$ | $+4.67$ | $+4.72$ | $+4.78$ | $+4.83$ | $+4.89$ | $+4.94$ |
| 39 | 3.89 | 3.94 | 4.00 | 4.06 | 4.1 I | 4.17 | 4.22 | 4.28 | $4 \cdot 33$ | 4.39 |
| 38 | 3.33 | 3.39 | 3.44 | 3.50 | 3.56 | 3.61 | 3.67 | 3.72 | 3.78 | 3.83 |
| 37 | 2.78 | 2.83 | 2.89 | 2.94 | 3.00 | 3.06 | 3.11 | 3.17 | 3.22 | 3.28 |
| 36 | 2.22 | 2.28 | 2.33 | 2.39 | 2.44 | 2.50 | 2.56 | 2.61 | 2.67 | 2.72 |
| +35 | + 1.67 | $+1.72$ | + 1.78 | $+1.83$ | + 1.89 | + 1.94 | $+2.00$ | $+2.06$ | +2.11 | +2.17 |
| 34 | +1.11 | +1.17 | + 1.22 | +1.28 | +1.33 | + 1.39 | + 1.44 | + 1.50 | + 1.56 | + 1.61 |
| 33 | $+0.56$ | +0.6I | + 0.67 | +0.72 | + 0.78 | + 0.83 | + o. 89 | + 0.94 | + 1.00 | $+1.06$ |
| 32 | 0.00 | + 0.06 | + 0.11 | +0.17 | + 0.22 | + 0.2 S | $+0.33$ | +0.39 | $+0.44$ | $+0.50$ |
| 3 I | -0.56 | $-0.50$ | -0.44 | $-0.39$ | $-0.33$ | $-0.2 \mathrm{~S}$ | $-0.22$ | -0.17 | - 0.11 | $-0.06$ |
| $+30$ | - I.II | - 1.06 | - 1.00 | $-0.94$ | -0.89 | $-0.83$ | $-0.78$ | - 0.72 | $-0.67$ | - 0.6I |
|  | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |

FAHRENHEIT SCALE TO CENTIGRADE.

| Fahrenheit. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | c. | c. | c. | c. | c. | C. | C. | c. | c. | c. |
| $+30^{\circ}$ | - İ. ${ }^{\text {a }}$ I | - | - I | - | - | $-0.83$ | $-0.78$ | $-0.72$ | $-0.67$ | - 0.61 |
| 29 | 67 | 1.6I | 1.56 | 50 | . 44 | I. 39 | 33 | 2 S | . 22 | . 17 |
| 28 | 2.22 | 2.17 | 2.11 | 2.06 | 2.00 | 1.94 | 1.89 | 1.83 | 1.78 | . 72 |
| 27 | 2.78 | . 72 | 2.67 | 2.61 | 2.56 | 2.50 | 2.44 | 2.39 | 2.33 | 2.28 |
| 26 | 3.33 | 3.28 | 3.22 | 3.17 | 3.11 | 3.06 | 3.00 | 2.94 | 2.89 | 2.83 |
| $+25$ | - 3.89 | $-3.83$ | - 3 | - 3 | - 3 | - | $-3.56$ | $-3.50$ | $-3.44$ | 3.39 |
| 24 | 44 | 4.39 | 4.33 | 4.28 | 4.22 | 4.17 | 4.11 | 4.06 | 4.00 | 3.94 |
| 23 | 00 | 4.94 | 4.89 | 4.83 | 4.78 | 4.72 | 4.67 | 4.61 | 4.56 | . 50 |
| 22 |  | 50 | 5.44 | 5.39 | 5.33 | 5.28 | 5.22 | 5.17 | 5.11 | . 06 |
| 21 | I | 6.06 | 6.00 | $5 \cdot 94$ | 5.89 | 5.83 | 5.78 | 5.72 | 5.67 | .6I |
| +20 | - 6 | -6.61 | $-6.56$ | $-6.50$ | - 6.44 | - 6.39 | $-6.33$ | $-6.28$ | $-6.22$ | 6.17 |
| 19 | 7.22 | 17 | 7.11 | 7.06 | 7.00 | 6.94 | 6.89 | 6.83 | 6.78 | 6.72 |
| 18 | 7.78 | 72 | 7.67 | 7.61 | 7.56 | 7.50 | 7.44 | 7.39 | 7.33 | 7.28 |
| 17 | 33 | 8.28 | 8.22 | S. 17 | S. 11 | S. 06 | 8.00 | 7.94 | 7.89 | . 83 |
| 16 | 8.89 | 8.83 | S.78 | S. 72 | S. 67 | 8.61 | 8.56 | 8.50 | 8.44 | 8.39 |
| $+15$ | - 9 | - 9.39 | $-9.33$ | - 9 | - 9 | - 9.17 | - 9.11 | $-9.06$ | - 9.00 | $-8.94$ |
| 14 | 10 | 9.94 | 9.89 | 9.83 | 9.7 | 9.72 | 9.67 | 6I | 9.56 | 9.50 |
| 13 | 10 | 10.50 | 10.44 | 10.39 | 10.3 | 10.28 | 10.22 | 10.17 | 10.11 | 10.06 |
| 12 | II.II | II | 11 | 10.94 | 10.89 | 10.83 | 10.78 | 10.72 | 10.67 | I |
| II | 11.67 | I 1.6 | 11.5 | 11.50 | I 1.44 | 11.39 | 11.33 | 11.28 | 11.22 | 11.17 |
| $+10$ | --12.22 | -12 | -12.II | -12.06 | -I | -il. 94 | -11. $\mathrm{S}_{9}$ | $-11.83$ | -11.78 | -11.72 |
| 9 | 12 | 12. | 12.6 | 12 | 12.5 | 12 | 12.44 | 12.39 | 12.33 | 12.28 |
| 8 | 13 | 13.28 | 13.22 | 13 | 13.11 | 13.0 | 13.00 | 12.94 | 12.89 | 12.83 |
| 7 |  | 13.83 | 13.78 | 13.72 | 13.67 | 13.61 | 13.56 | 13.50 | 13.44 | 13.39 |
| 6 | 14.44 | 14.39 | 14.33 | 14.28 | 14.22 | 14.17 | 14.11 | 14.06 | 14.00 | 13.94 |
| + 5 | -I5 | --14 | -I | $-14.83$ | $-14.78$ | -I | -14.67 | -14.61 | $-14.56$ | -14.50 |
| 4 | 15 | 15. | 15.44 | 15.39 | 15.33 | 15.28 | 15.22 | 15.17 | 15.51 | 15.06 |
| 3 | 16.11 | 16.06 | 16.00 | 15.94 |  | ${ }^{1} 5.83$ | 15.78 | 15.72 | . 67 | 5.61 |
| 2 | 16.67 | 16.61 | 16.56 | 16.50 | 16.44 | 16.39 | 16.33 | 16.28 | 16.22 | 6.17 |
| , | 17.22 | 17.17 | 17.11 | 17.06 | 17.00 | 16.94 | 16.89 | 16.83 | 16.78 | 16.72 |
| + 0 | 17.78 | 17.72 | 17.67 | 17.61 | 17.56 | 17.50 | 17.44 | 17.39 | 17.33 | 17.28 |
| 0 | -I | $-17.83$ | - 17.89 | -17.94 | -18.00 | -18.06 | -IS. 1 | -IS. 17 | $-18.22$ | -18.28 |
| 1 | IS. 3 | 18.39 | 18.44 | 18.50 | 18.56 | I8.61 | 18.67 | 18.72 | 18.78 | 18.83 |
| 2 |  | 18.94 | 19.00 | 19.06 | 19. II | 19.17 | 19.22 | 19.28 | 19.33 | ${ }_{15} 89$ |
| 3 | 19.4 | 19.5 | 19.56 | 19.61 | 19.67 | 19.72 | 19.78 | 19.83 | 19.89 | $\underline{9.94}$ |
| 4 | 20.0 | 20.0 | 20.11 | 20.17 | 20.22 | 20.28 | 20.33 | 20.39 | 20.44 | 20.50 |
| $-5$ | -20 | -20. | -20. | -20. | -20 | -20.83 | -20.89 | -20 | -21.00 | -21.06 |
| 6 | 21.11 | 21.17 | 8 | 21. |  |  | 21. | 21.50 | 21.56 | 6I |
|  | 2 I .6 | 21.7 | 21.78 | 21.83 | 21.89 | 21.94 | 22.00 | 22.06 | 22.11 | 22.17 |
| 8 | 22.22 | 22.28 | 22.33 | 22.39 | 22.44 | 22.50 | 22.56 | 22.61 | 22.67 | 22.72 |
| 9 | 22.78 | 22.83 | 22.89 | 22.94 | 23.00 | 23.06 | 23. 11 | 23.17 | 23.22 | 23.28 |
| $-10$ |  | -23.39 | -23.44 |  | $-23.56$ | -23.61 | -23.67 | -23.72 | $-23.78$ | $-23.83$ |
| 11 | 23.8 | 23.94 | 24.00 | 24 | 24.11 | 24.17 | 24.22 | 24.28 | 24.33 | 24.39 |
| 12 | 24.4 | 24.50 | 24.56 |  | 24.67 | 24.72 | 24.7 | 24.83 | 24.89 | 24.94 |
| 13 | 25.00 | 25.06 | 25.11 | 25.17 | 25.22 | 25.28 | 25.33 | 25.39 | 25.44 | 25.50 |
| 14 | 25.5 | 25 | 25.67 | 25.72 | 25.78 | 25.83 | 25.89 | 25.94 | 26.00 | 26.06 |
| - 15 | -26.11 | -26.17 | -26.22 | $-26.28$ | -26.33 | $-26.39$ | -26.44 | -26.50 | $-26.56$ | -26.6I |
| 16 | 26.67 | 26.72 | 26.78 | 26.83 | 26.89 | 26.94 | 27.00 | 27.06 | 27.11 | 27.17 |
| 17 | 27.22 | 27.28 | 27.33 | 27.39 | 27.44 | 27.50 | 27.56 | 27.61 | 27.67 | 27.72 |
| 18 | 27.78 | 27.83 | 27.89 | 27.94 | 28.00 | 28.06 | 28.11 | 28.17 | 28.22 | 28.28 |
| 19 | 28.3 | 28.39 | 28.44 | 28.50 | 28.56 | 28 | 28.67 | 28.72 | 28.78 | 28.83 |
| -20 | -28.89 | -28.94 | -29.00 | -29.06 | -29.1 1 | $-29.17$ | -29.22 | $-29.28$ | -29.33 | -29.39 |
|  | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |

Table 2.
FAHRENHEIT SCALE TO CENTIGRADE.

| Fahren. heit. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | c. | c. | c. | c. | c. | c. | c. | c. | c. | c. |
| $-20^{\circ}$ | $-28.89$ | $-28.94$ | $-29.00$ | 29.06 | $-29.11$ | $-29^{\circ} 17$ | $-29^{\circ} 22$ | $-29^{\circ} .28$ | $-29.33$ | -29.39 |
| 21 | 29.44 | 29.50 | 29.56 | 29.61 | 29.67 | 29.72 | 29.78 | 29.83 | 29.89 | 29.94 |
| 22 | 30.00 | 30.06 | 30.11 | 30.17 | 30.22 | 33.28 | 30.33 | 30.39 | 30.44 | 30.50 |
| 23 | 30.56 | 30.61 | 30.67 | 30.72 | 30.78 | 30.83 | 30.89 | 30.94 | 31.00 | 31.06 |
| 24 | 3 I .11 | 31.17 | 31.22 | 31.28 | 31.33 | 31.39 | 31.44 | 31.50 | 31.56 | 31.6I |
| -25 | -31.67 | -31.72 | $-31.78$ | $-31.83$ | 31.89 | - 31.94 | -32.00 | -32.06 | -32.1I | -32.17 |
| 26 | 32.22 | 32.28 | 32.33 | 32.39 | 32.44 | 32.50 | 32.56 | 32.61 | 32.67 | 32.72 |
| 27 | 32.78 | 32.83 | 32.89 | 32.94 | 33.00 | 33.06 | 33.11 | 33.17 | 33.22 | 33.28 |
| 28 | 33.33 | 33.39 | 33.44 | 33.50 | 33.56 | 33.61 | 33.67 | 33.72 | 33.78 | 33.83 |
| 29 | 33.89 | 33.94 | 34.00 | 34.06 | 34.11 | 34.17 | 34.22 | 34.28 | 34.33 | 34.39 |
| -30 | -34.44 | -34.50 | $-34.56$ | -34.6I | $-34.67$ | $-34.72$ | $-34.78$ | $-34.83$ | -34.89 | -34.94 |
| 31 | 35.00 | 35.06 | 35.11 | 35.17 | 35.22 | 35.28 | 35.33 | $35 \cdot 39$ | 35.44 | 35.50 |
| 32 | 35.56 | 35.61 | 35.67 | 35.72 | 35.78 | 35.83 | 35.89 | 35.94 | 36.00 | 36.06 |
| 33 | 36.11 | 36.17 | 36.22 | 36.28 | 36.33 | 36.39 | 36.44 | 36.50 | 36.56 | 36.61 |
| 34 | 36.67 | 36.72 | 36.78 | 36.83 | 36.89 | 36.94 | 37.00 | 37.06 | 37.11 | 37.17 |
| -35 | -37.22 | $-37.28$ | $-37.33$ | -37.39 | -37.44 | -37.50 | -37.56 | $-37.61$ | $-37.67$ | $-37.72$ |
| 36 | 37.78 | 37.83 | 37.89 | 37.94 | 38.00 | 38.06 | 38.11 | 38.17 | 30.22 | 38.28 |
| 37 | 38.33 | 3 S .39 | 38.44 | 38.50 | 38.56 | 38.61 | $3^{8.67}$ | 38.72 | 38.78 | 38.83 |
| 38 | 38.89 | 38.94 | 39.00 | 39.06 | 39.1 I | 39.17 | 39.22 | 39.28 | 39.33 | 39.39 |
| 39 | 39.44 | 39.j0 | 39.56 | 39.61 | 39.67 | 39.72 | 39.78 | 39.83 | 39.89 | 39.94 |
| -40 | $-40.00$ | -40.06 | -40.11 | $-40.17$ | -40.22 | $-40.28$ | $-40.33$ | -40.39 | -40.44 | -40.50 |
| 41 | 40.56 | 40.61 | 40.67 | 40.72 | 40.78 | 40.83 | 40.89 | 40.94 | 41.00 | 41.06 |
| 42 | 41.11 | 41.17 | 41.22 | 41.28 | 41.33 | 41.39 | 41.44 | 41.50 | 41.56 | 41.61 |
| 43 | 41.67 | 41.72 | 41.78 | 41.83 | 4 I .39 | 41.94 | 42.00 | 42.06 | 42.11 | 42.17 |
| 44 | 42.22 | 42.28 | 42.33 | 42.39 | 42.44 | 42.50 | 42.56 | 42.61 | 42.67 | 42.72 |
| -45 | -42.78 | $-42.83$ | $-42.89$ | -42.94 | $-43.00$ | $-43.06$ | -43.11 | $-43.17$ | $-43.22$ | -43.29, |
| 46 | 43.33 | 43.39 | 43.44 | 43.50 | 43.56 | 43.61 | 43.67 | 43.72 | 43.78 | 43.83 |
| 47 | 43.89 | 43.94 | 44.00 | 44.06 | 44.1 I | 44.17 | 44.22 | 44.28 | 44.33 | 44.39 |
| 48 | 42.44 | 44.50 | $44.5^{5}$ | 44.61 | 44.67 | 44.72 | 44.78 | 44.83 | 44.89 | 44.94 |
| 49 | 45.00 | 45.06 | 45. I I | 45.17 | 45.22 | 45.2 S | $45 \cdot 33$ | $45 \cdot 39$ | 45.44 | 45.50 |
| $-50$ | -45.56 | -45.6I | $-45.67$ | -45.72 | $-45.78$ | $-45.83$ | $-45.89$ | -45.94 | $-46.00$ | $-46.06$ |
| 51 | 45.11 | 46.17 | 46.22 | 46.28 | 46.33 | 46.39 | 46.44 | 46.50 | 46.56 | 46.61 |
| 52 | 46.67 | 46.72 | 46.78 | 46.83 | 46.89 | 46.94 | 47.00 | 47.06 | 47.1 I | 47.17 |
| 53 | 47.22 | 47.28 | 47.33 | 47.39 | 47.44 | 47.50 | 47.56 | 47.61 | 47.67 | 47.72 |
| 54 | 47.78 | 47.83 | 47.89 | 47.94 | 48.00 | 48.06 | 48.11 | 48.17 | 48.22 | 48.28 |
| -55 | -48.33 | $-48.39$ | -48.44 | $-48.50$ | $-48.56$ | $-48.61$ | $-48.67$ | $-48.72$ | $-48.78$ | $-48.83$ |
| 56 | 48.89 | 48.94 | 49.00 | 49.06 | 49. 11 | 49.17 | 49.22 | 49.28 | 49.33 | 49.39 |
| 57 | 49.44 | 49.50 | 49.56 | 49.6I | 49.67 | 49.72 | 49.78 | 49.83 | 49.89 | 49.94 |
| 58 | 50.00 | 50.06 | 50.11 | 50.17 | 50.22 | 50.28 | 50.33 | 50.39 | 50.44 | 50.50 |
| 59 | 50.56 | 50.61 | 50.67 | 50.72 | 50.78 | 50.83 | 50.89 | 50.94 | 51.00 | 51.06 |
| -60 | -51.11 | -51.17 | -51.22 | $-51.28$ | $-51.33$ | -5I. 39 | -51.44 | $-51.50$ | $-51.56$ | -51.6I |
| $6 t$ | 51.67 | 51.72 | 51.78 | 51.83 | 51.89 | 51.94 | 52.00 | 52.06 | 52.11 | 52.17 |
| 62 | 52.22 | 52.28 | 52.33 | 52.39 | 52.44 | 52.50 | 52.56 | 52.61 | 52.67 | 52.72 |
| 63 | 52.78 | 52.83 | 52.89 | 52.94 | 53.00 | 53.06 | 53.11 | 53.17 | 53.22 | 53.28 |
| 64 | 53.33 | 53.39 | 53.44 | 53.50 | 53.56 | 53.61 | 53.67 | 53.72 | 53.78 | 53.83 |
| -65 | -53.39 | -53.94 | -54.00 | $-54.06$ | -54. 11 | $-54.17$ | $-54.22$ | $-54.28$ | $-54.33$ | -54.39 |
| 66 | 54.44 | 54.50 | 54.56 | 54.6 I | 54.67 | 54.72 | 54.78 | 54.83 | 54.89 | 54.94 |
| 67 | 55.00 | 55.06 | 55.1 I | 55.17 | 55.22 | 55.28 | 55.33 | 55.39 | 55.44 | 55.50 |
| 68 | 55.56 | 55.61 | 55.67 | 55.72 | 55.78 | 55.83 | 55.89 | 55.94 | 56.00 | 56.06 |
| 69 | 56.1 I | 56.17 | 56.22 | 56.28 | 56.33 | 56.39 | 56.44 | 56.50 | 56.56 | 56.61 |
| -70 | $-56.67$ | $-56.72$ | $-56.78$ | $-56.83$ | $-56.89$ | -56.94 | -57.00 | -57.06 | -57.11 | -57.17 |
|  | . 0 | . 1 | . 2 | .3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |

Smithsonian Tables.

FAHRENHEIT SCALE TO CENTIGRADE.

| Fahrenheit. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-56{ }^{\circ} 67$ | c. |  | c. | C. | $56^{\circ}$ | - $7^{\circ}$ | - $7^{\circ}$ O | . | C. |
| $-70^{\circ}$ | $-56.67$ | $-56.72$ | $-56.78$ | $-56^{\circ} .83$ | $-56^{\circ} \mathrm{B}$ 9 | $-56.94$ | -57.00 | -57.06 | $-57.11$ | $-57.17$ |
| 71 | 57.22 | 57.28 | 57.33 | 57.39 | 57.44 | 57.50 | 57.56 | 57.61 | 57.67 | 57.72 |
| 72 | 57.78 | 57.83 | 57.89 | 57.94 | 58.00 | 58.06 | 58.11 | 58.17 | 58.22 | 58.28 |
| 73 | 58.23 | 58.39 | 58.44 | 58.50 | 58.56 | 58.61 | 58.67 | 58.72 | 58.78 | 58.83 |
| 74 | 58.89 | 58.94 | 59.00 | 59.06 | 59.1 I | 59.17 | 59.22 | 59.28 | 59.33 | 59.39 |
| -75 | -59.44 | $-59.50$ | $-59.56$ | -59.6I | $-59.67$ | $-59.72$ | -59.78 | -59.83 | -59.89 | -59.94 |
| 76 | ¢0.0 | 60.06 | 60.11 | 60.17 | 60.22 | 60.28 | 60.33 | 60.39 | 60.44 | 60.50 |
| 77 | 60.56 | 60.61 | 60.67 | 60.72 | 60.78 | 60.83 | 60.89 | 60.94 | 61.00 | 61.06 |
| 78 | 6 I .1 I | 61.17 | 61.22 | $6 \pm .28$ | 6 r .33 | 61.39 | 61.44 | 61.50 | 61.56 | 61.6 I |
| 79 | 6 I .67 | 61.72 | 61.78 | 61.83 | 61.89 | 61.94 | 62.00 | 62.06 | 62.11 | 62.17 |
| -80 | -62.22 | $-62.28$ | $-62.33$ | $-62.39$ | -62.44 | -62.50 | $-62.56$ | -62.61 | -62.67 | -62.72 |
| 8 I | 62.78 | 62.83 | 62.89 | 62.94 | 63.00 | 63.06 | 63.11 | 63.17 | 63.22 | 63.28 |
| 82 | 63.33 | 6.3 .39 | 63.44 | 63.50 | 63.56 | 63.61 | 63.67 | 63.72 | 63.78 | 63.83 |
| 83 | 63.89 | 63.94 | 64.00 | 6.4 .06 | 64.1 I | 64.17 | 64.22 | 64.28 | 64.33 | 64.39 |
| 84 | 64.44 | 64.50 | 64.56 | 6.4 .61 | 64.67 | 64.72 | 64.78 | 64.83 | 64.89 | 64.94 |
| -85 | -65.00 | $-65.06$ | $-65.11$ | $-65.17$ | $-65.22$ | $-65.28$ | $-65.33$ | -65.39 | -65.44 | $-65.50$ |
| 86 | 65.56 | 65.61 | 65.67 | 65.72 | 65.78 | 65.83 | 65.89 | 65.94 | 66.00 | 66.06 |
| 87 | 66.11 | 66.17 | 66.22 | 66.28 | 66.33 | 66.39 | 66.44 | 66.50 | 66.56 | 66.6 r |
| 88 | 66.67 | 66.72 | 66.78 | 66.83 | 66.89 | 66.94 | 67.00 | 67.06 | 67.1 I | 67.17 |
| 89 | 67.22 | 67.28 | 67.33 | 67.39 | 67.44 | 67.50 | 67.56 | 67.61 | 67.67 | 67.72 |
| -90 | $-67.78$ | $-67.83$ | $-67.89$ | -67.94 | -68.00 | -68.06 | -68.11 | -68.17 | -68.22 | -68.28 |
| 91 | 68.33 | 68.39 | 68.44 | 68.50 | 68.56 | 68.61 | 68.67 | 68.72 | 68.78 | 68.83 |
| 92 | 68.89 | 68.94 | 69.00 | 69.06 | 69.11 | 69.17 | 69.22 | 69.28 | 69.33 | 69.39 |
| 93 | 69.44 | 69.50 | 69.56 | 69.61 | 69.67 | 69.72 | 69.78 | 69.83 | 69.89 | 69.94 |
| 94 | 70.00 | 70.06 | 70.11 | 70.17 | 70.22 | 70.28 | 70.33 | 70.39 | 70.44 | 70.50 |
| -95 | -70.56 | -70.61 | $-70.67$ | $-70.72$ | $-70.78$ | $-70.83$ | -70.89 | -70.94 | -71.00 | -71.06 |
| 96 | 71.11 | 71.17 | 71.22 | 71.28 | 71.33 | 71.39 | 71.44 | 71.50 | 71.56 | 7 I .61 |
| 97 | 71.67 | 71.72 | 71.78 | 71.83 | 7 I .89 | 71.94 | 72.00 | 72.06 | 72.11 | 72.17 |
| 98 | 72.22 | 72.28 | 72.33 | 72.39 | 72.44 | 72.50 | 72.56 | 72.61 | 72.67 | 72.72 |
| 99 | 72.78 | 72.83 | 72.89 | 72.94 | 73.00 | 73.06 | 73.11 | 73.17 | 73.22 | 73.28 |
| -100 | -73.33 | -73.39 | $-73.44$ | $-73.50$ | $-73.56$ | -73.61 | -73.67 | -73.72 | $-73.78$ | $-73.83$ |
| 101 | 73.89 | 73.94 | 74.00 | 74.06 | 74.11 | 74.17 | 74.22 | 74.28 | 74.33 | 74.39 |
| 102 | 74.44 | 74.50 | 74.56 | 74.6 | 74.67 | 74.72 | 74.78 | 74.83 | 74.89 | 74.94 |
| 103 | 75.00 | 75.06 | 75.11 | 75.17 | 75.22 | 75.28 | 75.33 | 75.39 | 75.44 | 75.50 |
| 104 | 75.56 | 75.61 | 75.67 | 75.72 | 75.78 | 75.83 | 75.89 | 75.94 | 76.00 | 76.06 |
| -105 | -76.11 | $-76.17$ | -.76.22 | $-76.28$ | $-76.33$ | $-76.39$ | $-76.44$ | -76.50 | $-76.56$ | -76.61 |
| 106 | 76.67 | 76.72 | 76.78 | 76.83 | 76.89 | 76.94 | 77.00 | 77.06 | 77.11 | 77.17 |
| 107 | 77.22 | 77.28 | 77.33 | 77.39 | 77.44 | 77.50 | 77.56 | 77.61 | 77.67 | 77.72 |
|  | 77.78 | 77.83 | 77.89 | 77.94 | 78.00 | 78.06 | 78.11 | 78.17 | 78.22 | 78.28 |
| 109 | 78.33 | 78.39 | 78.44 | 78.50 | 78.56 | 78.61 | 78.67 | 78.72 | 78.78 | 78.83 |
| -110 | -78.89 | -78.94 | -79.00 | -79.06 | -79.11 | -79.17 | -79.22 | -79.28 | -79.33 | -79.39 |
| III | 79.44 | 79.50 | 79.56 | 70.61 | 79.67 | 79.72 | 79.78 | 79.83 | 79.89 | 79.94 |
| 112 | 80.00 | 80.06 | 80.11 | 80.17 | 80.22 | 80.28 | 80.33 | 80.39 | 80.44 | 80.50 |
| 113 | 80.56 | 80.61 | 80.67 | 80.72 | 80.78 | 80.83 | 80.89 | 80.94 | 8 t .00 | 81.06 |
| 114 | 8 I .11 | 81.17 | 81.22 | 81.28 | 8 I .33 | 81.39 | 8 s .44 | 81.50 | 8т.56 | 8ı.6ı |
| -115 | -81. 67 | $-81.72$ | $-81.78$ | $-8 \mathrm{r} .83$ | $-81.89$ | -81.94 | -82.00 | $-82.06$ | -82.11 | -82.17 |
| 116 | 82.22 | 82.28 | 82.33 | 82.39 | 82.44 | 82.50 | 82.56 | 82.61 | 82.67 | 82.72 |
| 117 | 82.78 | 82.83 | 82.89 | 82.94 | 83.00 | 83.06 | 83.11 | 83.17 | 83.22 | 83.28 |
| 118 | 83.33 | 83.39 | 83.44 | 83.50 | 83.56 | 83.61 | 83.67 | 83.72 | 83.78 | 83.83 |
| 119 | 83.89 | 83.94 | 84.00 | S4.06 | 84.1 I | 84.17 | 84.22 | 84.28 | 84.33 | 84.39 |
| -120 | -84.44 | $-84.50$ | $-84.56$ | $-84.61$ | $-84.67$ | $-84.72$ | $-84.78$ | $-84.83$ | $-84.89$ | -84.94 |
|  | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | .7 | . 8 | . 9 |


| Centigrade. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $+60^{\circ}$ | $\begin{gathered} F \\ +140.00 \end{gathered}$ | $\begin{gathered} F \\ +140^{\circ} .18 \end{gathered}$ | $\begin{gathered} F . \\ +140 \cdot 36 \end{gathered}$ | $\begin{gathered} F . \\ +140.54 \end{gathered}$ | $\begin{array}{r} \text { F. } \\ +140.72 \end{array}$ | $\begin{gathered} F . \\ +140.90 \end{gathered}$ | $\begin{gathered} F . \\ +141.08 \end{gathered}$ | $\begin{gathered} F . \\ +141.26 \end{gathered}$ | $\begin{gathered} F \\ +141.44 \end{gathered}$ | $\begin{gathered} F . \\ +141.62 \end{gathered}$ |
| 59 | 138.20 | 138.38 | 138.56 | 138.74 | 138.92 | 139.10 | 139.28 | 139.46 | 139.64 | 139.82 |
| 58 | 136.40 | 136.58 | 136.76 | 136.94 | 137.12 | 137.30 | 137.48 | 137.66 | 137.84 | 138.02 |
| 57 | 13.4 .60 | 13.4 .78 | 134.96 | 135.14 | 135.32 | 135.50 | ${ }^{1} 35.68$ | 135.86 | 136.04 | 136.22 |
| 56 | 132.80 | I 32.98 | I 33.16 | 133.34 | 133.52 | 133.70 | 133.88 | 134.06 | 134.24 | 134.42 |
| $+55$ | +131.00 | +131.18 | +131.36 | +131.54 | +131.72 | +131.90 | +132.08 | +132.26 | +132.44 | +132.62 |
| 54 | 129.20 | 129.38 | 129.56 | 129.74 | 129.92 | 130.10 | 130.28 | 130.46 | 130.64 | ${ }^{1} 30.82$ |
| 53 | 127.40 | 127.58 | 127.76 | 127.94 | 128.12 | 128.30 | 128.48 | 128.66 | 128.84 | 129.02 |
| 52 | 125.60 | 125.78 | 125.96 | 126.14 | 126.32 | 126.50 | 126.68 | 126.86 | 127.04 | 127.22 |
| 51 | 123.80 | 123.98 | 124.16 | 124.34 | 124.52 | 12.4 .70 | I 24.88 | 125.06 | 125.24 | 125.42 |
| +50 | 122.00 | +122.18 | +122.36 | +122.54 | +122.72 | +122.90 | +123.08 | +123.26 | +123.44 | +123.62 |
| 49 | 120.20 | 120.38 | 120.56 | 120.74 | 120.92 | 121.10 | 121.28 | 121.46 | 121.64 | 121.82 |
| 48 | 118.40 | 118.58 | I18.76 | 118.94 | 119.12 | 119.30 | 119.48 | 119.66 | 119.84 | 120.02 |
| 47 | 116.60 | 116.78 | 116.96 | 117.14 | 117.32 | 117.50 | 117.68 | 117.86 | 118.04 | 118.22 |
| 46 | 114.80 | 114.98 | 115.16 | I15.34 | 115.52 | 115.70 | 115.88 | 116.06 | 116.24 | 116.42 |
| +45 | +113.00 | +113.18 | +113.36 | +113.54 | +113.72 | +113.90 | +114.08 | +114.26 | +114.44 | +114.62 |
| 44 | III. 20 | 111.38 | 111.56 | 111.74 | III.92 | II2.10 | 112.28 | 112.46 | 112.64 | 112.82 |
| 43 | 100.40 | 109.58 | 109.76 | 109.94 | 110.12 | 110.30 | 110.48 | 110.66 | 110.84 | 111.02 |
| 42 | 107.60 | 107.78 | 107.96 | 108.14 | 108.32 | 108.50 | 108.68 | 108.86 | 109.04 | 109.22 |
| 4 I | 105.80 | 105.98 | 106.16 | 106.34 | 106.52 | 106.70 | 106.88 | 107.06 | 107.24 | 107.42 |
| +40 | +104.00 | +104.18 | +104.36 | +104.54 | +104.72 | +104.90 | +105.08 | $+105.26$ | +105.44 | +105.62 |
| 39 | 102.20 | 102.38 | 102.56 | 102.74 | 102.92 | 103.10 | 103.28 | 103.46 | 103.64 | 103.82 |
| 38 | 100.40 | 100.58 | 100.76 | 100.94 | 101.12 | 101. 30 | 101.48 | 101.66 | 101.84 | 102.02 |
| 37 | 98.60 | 98.78 | 98.96 | 99.14 | 99.32 | 99.50 | 99.68 | 99.86 | 100.04 | 100.22 |
| 36 | 96.80 | 96.98 | 97.16 | 97.34 | 97.52 | 97.70 | 97.88 | 98.06 | 98.24 | 98.42 |
| +35 | + 95.00 | + 95.18 | 6 | + 95.54 | + 95.72 | 90 | $+96.08$ | + 96.26 | + 96.44 | $+96.62$ |
| 34 | 93.20 | 93.38 | 93.56 | 93.74 | 93.92 | 04.10 | 94.28 | 94.46 | 94.64 | 94.82 |
| 33 | 91.40 | 91.58 | 91.76 | 91.94 | 92.12 | 92.30 | 92.48 | 92.66 | 92.84 | 93.02 |
| 32 | 89.60 | 89.78 | S9.96 | 90.14 | 90.32 | 90.50 | 90.68 | 90.86 | 91.04 | 91.22 |
| 31 | 87.80 | 87.98 | 88.16 | 88.34 | 88.52 | 88.70 | 88.88 | 89.06 | 89.24 | 89.42 |
| $+30$ | + 86.00 | + 86.18 | + 86.36 | + 86.54 | + 86.72 | + 86.90 | + 87.08 | + 87.26 | + 87.44 | $+87.62$ |
| 29 | 84.20 | 84.38 | S4.56 | 84.74 | 8.4.92 | 85.10 | 85.28 | 85.46 | 85.64 | 85.82 |
| 28 | 82.40 | 82.58 | 82.76 | 82.94 | 83.12 | 83.30 | 83.48 | 83.66 | 83.84 | 84.02 |
| 27 | So. 60 | So. 78 | 80.96 | 8 I .14 | SI.32 | SI.50 | 81.68 | 81.86 | 82.04 | 82.22 |
| 26 | 78.80 | 78.98 | 79.16 | 79.34 | 79.52 | 79.70 | 79.88 | 80.06 | 80.24 | 80.42 |
| +25 | + 77.00 | + 77.18 | + 77.36 | + 77.54 | + 77.72 | + 77.90 | + 78.08 | + 78.26 | + 78.44 | $+78.62$ |
| 24 | 75.20 | 75.38 | 75.56 | 75.74 | 75.92 | 76.10 | 76.28 | 76.46 | 76.64 | 76.82 |
| 23 | 73.40 | 73.58 | 73.76 | 73.94 | 74.12 | 74.30 | 74.48 | 74.66 | 74.84 | 75.02 |
| 22 | 71.60 | 71.78 | 71.96 | 72.14 | 72.32 | 72.50 | 72.68 | 72.86 | 73.04 | 73.22 |
| 21 | 69.80 | 69.98 | 70.16 | 70.34 | 70.52 | 70.70 | 70.88 | 71.06 | 71.24 | 71.42 |
| +20 | + 68.00 | + 68.18 | + 68.36 | + 68.54 | + 68.72 | + 68.90 | $+69.08$ | $+69.26$ | + 69.44 | $+69.62$ |
| 19 | 66.20 | 66.38 | 66.56 | 66.74 | 66.92 | 67.10 | 67.28 | 67.46 | 67.64 | 67.82 |
| 18 | 64.40 | 6.4 .58 | 64.76 | 64.94 | 65.12 | 65.30 | 65.48 | 65.66 | 65.84 | 66.02 |
| 17 | 62.60 | 62.78 | - 62.96 | 63.14 | 63.32 | 63.50 | 63.68 | - 63.86 | 64.04 | -64.22 |
| 16 | 60.80 | 60.98 | 61.16 | 61.34 | 61.52 | 61.70 | 61.88 | 62.06 | 62.24 | 62.42 |
| $+15$ | + 59.00 | + 59.18 | + 59.36 | + 59.54 | + 59.72 | 59.90 | $+60.08$ | $+60.26$ | + 60.44 | $+60.62$ |
| 14 | 57.20 | 57.38 | 57.56 | 57.74 | 57.92 | 58.10 | 58.28 | - 58.46 | 58.64 | 58.82 |
| 13 | 55.40 | 55.58 | 55.76 | 55.94 | 56.12 | 56.30 | 56.48 | - 56.66 | 56.84 | 57.02 |
| 12 | 53.60 | 53.78 | - 53.96 | 54.14 | 54.32 | 54.50 | - 54.68 | - 54.86 | -55.04 | 55.22 |
| 11 | 51.80 | 51.98 | 52.16 | 52.34 | 52.52 | 52.70 | 52.88 | - 53.06 | 53.24 | 53.42 |
| $+10$ | + 50.00 | + 50.18 | + 50.36 | + 50.54 | + 50.72 | $+50.90$ | $+51.08$ | + 51.26 | + 51.44 | $+51.62$ |
|  |  | . 1 | . 2 | . 3 | . 4 | 5 | . 6 | .7 | . 8 | . 9 |

Smithsonian Tables.

GENTIGRADE SCALE TO FAHRENHEIT.

| Centigrade. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $+10^{\circ}$ | $+50^{\circ} .00$ | $+50^{\circ} .18$ | $+50^{\circ} .36$ | $+50^{\circ} .54$ | $\begin{gathered} F . \\ +50^{\circ} .72 \end{gathered}$ | $\begin{gathered} \text { F. } \\ +50.90 \end{gathered}$ | $\begin{gathered} F . \\ +51.08 \end{gathered}$ | $\begin{gathered} F . \\ +5 \mathrm{I} .26 \end{gathered}$ | $\begin{gathered} F . \\ +5 \mathrm{r} .44 \end{gathered}$ | $\begin{gathered} F_{0} \\ +5 I^{\circ} .62 \end{gathered}$ |
| + 9 | $+48.20$ | +48.38 | $+48.56$ | +48.74 | +48.92 | +49.10 | $+49.28$ | +49.46 | +49.64 | +49.82 |
| 8 | 46.40 | 46.58 | 46.76 | 46.94 | 47.12 | 47.30 | 47.48 | 47.66 | 47.84 | 48.02 |
| 7 | 44.60 | 44.78 | 44.96 | 45.14 | $45 \cdot 32$ | 45.50 | 45.68 | 45.86 | 46.04 | 46.22 |
| 6 | 42.80 | 42.98 | 43.16 | 43.34 | $43 \cdot 52$ | 43.70 | 43.88 | 44.06 | 44.24 | 44.42 |
| 5 | 41.00 | 41.18 | 41.36 | 41.54 | 41.72 | 41.90 | 42.08 | 42.26 | 42.44 | 42.62 |
| + 4 | $+39.20$ | $+39.38$ | +39.56 | +39.74 | $+39.92$ | +40.10 | $+40.28$ | $+40.46$ | +40.64 | +40.82 |
| 3 | 37.40 | 37.58 | 37.76 | 37.94 | 38.12 | 38.30 | 38.48 | 38.66 | 38.84 | 39.02 |
| 2 | 35.60 | 35.78 | 35.96 | 36.14 | 36.32 | 36.50 | 36.68 | 36.86 | 37.04 | 37.22 |
| 1 | 33.80 | 33.98 | 34.16 | $34 \cdot 34$ | 34.52 | 34.70 | 34.88 | 35.06 | 35.24 | 35.42 |
| + 0 | 32.00 | 32.18 | 32.36 | 32.54 | 32.72 | 32.90 | 33.08 | 33.26 | 33.44 | 33.62 |
| - 0 | +32.00 | $+31.82$ | +31.64 | $+31.46$ | +31.28 | +31.10 | +30.92 | +30.74 | +30.56 | 30.38 |
| I | 30.20 | 30.02 | 29.84 | 29.66 | 29.48 | 29.30 | 29.12 | 28.94 | 28.76 | 28.58 |
| 2 | 28.40 | 28.22 | 28.04 | 27.86 | 27.68 | 27.50 | 27.32 | 27.14 | 26.96 | 26.78 |
| 3 | 26.60 | 26.42 | 26.24 | 26.06 | 25.88 | 25.70 | 25.52 | 25.34 | 25.16 | 24.98 |
| 4 | 24.80 | 24.62 | 24.44 | 24.26 | 24.08 | 23.90 | 23.72 | 23.54 | 23.36 | 23.18 |
| - 5 | +23.00 | $+22.82$ | +22.6 | $+22.46$ | +22.28 | +22.10 | $+21.92$ | +21.74 | +21.56 | +21.38 |
| 6 | 21.2 | 21.02 | 20.84 | 20.66 | 20.48 | 20.30 | 20.12 | 4 | 19.76 | 9.58 |
| 7 | 19. | 19.22 | 19.04 | 18.86 | 18.68 | 18.50 | 18.32 | 18.14 | 17.96 | 17.78 |
| 8 | 17.60 | 17.42 | 17.24 | 17.06 | I6.88 | 16.70 | 16.52 | 16.34 | 16.16 | 5.98 |
| 9 | 15.80 | 15.62 | 15.44 | 15.26 | 15.08 | 14.90 | 14.72 | 14.54 | 14.36 | 14.18 |
| -10 | +14.00 | +13.82 | +13.6 | $+13.46$ | +13.28 | +13.10 | +12.92 | +12.74 | +12.56 | +12.38 |
| II | 12.20 | 12 | 11.84 | 11.66 | 11.48 | 11.30 | 11.12 | 10.94 | 10.76 | 10.58 |
| 12 | 10.40 | 10.22 | 10.04 | 9.86 | 9.68 | 9.50 | 9.32 | 9.14 | 8.96 | 8.78 |
| 13 | 8.60 | 8.42 | 8.24 | 8.06 | 7.88 | 7.70 | 7.52 | 7.34 | 7.16 | 6.98 |
| 14 | 6.80 | 6.62 | 6.44 | 6.26 | 6.08 | 5.90 | 5.72 | $5 \cdot 54$ | 5.36 | 5.18 |
| -15 | $+5.00$ | $+4.82$ | + 4.64 | $+4.46$ | $+4.28$ | + 4.10 | $+3.92$ | + 3.74 | $+3.56$ | $+3.38$ |
| 16 | $+3.20$ | $+3.02$ | + 2.84 | + 2.66 | + 2.48 | + 2.30 | + 2.12 | + 1.94 | + 1.76 | + 1.58 |
| 17 | + 1.40 | + 1.22 | + 1.04 | + 0.86 | $+0.68$ | $+0.50$ | $+0.32$ | + 0.14 | - 0.04 | - 0.22 |
| 18 | - | $-0.58$ | -0.76 | - | - 1.12 | - 1.30 | - 1.48 | - 1.66 | $-\quad 1.84$ | $-2.02$ |
| 19 | - 2 | - 2.38 | - 2.56 | - 2.74 | $-2.92$ | - 3.10 | $-3.28$ | - 3.46 | - 3.64 | $-3.82$ |
| -20 | - 4.00 | - 4.18 | - 4.36 | - 4.54 | $-4.72$ | - 4.90 | - 5.08 | $-5.26$ | - 5.44 | - 5.62 |
| 21 | 5.80 | 5.98 | 6.16 | 6.34 | 6.52 | 6.70 | 6.88 | 7.06 | 7.24 | 7.42 |
| 22 | 7.60 | 7.78 | 7.96 | 8.14 | S.32 | 8.50 | 8.68 | 8.86 | 9.04 | 9.22 |
| 23 | 9.40 | 9.58 | 9.76 | 9.94 | 10.12 | 10.30 | 10.48 | 10.66 | 10.84 | 11.02 |
| 24 | 11.20 | I 1.38 | 11.56 | 11.74 | 11.92 | 12.10 | 12.28 | 12.46 | 12.64 | 12.82 |
| -25 | -13.00 | -13.18 | - 13.36 | -13.54 | - 13.72 | -13.90 | -14.08 | -14.26 | -14.44 | -14.62 |
| 26 | 14.80 | 14.98 | 15.16 | 15.34 | 15.52 | 15.70 | 15.88 | 16.06 | 16.24 | 16.42 |
| 27 | 16.60 | 16.78 | 16.96 | 17.14 | 17.32 | 17.50 | 17.68 | 17.86 | 18.04 | 18.22 |
| 28 | 18.40 | 18.58 | 18.76 | 18.94 | 19.12 | 19.30 | 19.48 | 19.66 | 19.84 | 20.02 |
| 29 | 20.20 | 20.38 | 20.56 | 20.74 | 20.92 | 21.10 | 21.28 | 21.46 | 21.64 | 21.82 |
| -30 | -22.00 | -22.18 | -22.36 | -22.54 | -22.72 | -22.90 | $-23.08$ | $-23.26$ | -23.44 | $-23.62$ |
| 31 | 23.80 | 23.98 | 24.16 | 24.34 | 24.52 | 24.70 | 24.88 | 25.06 | 25.24 | 25.42 |
| 32 | 25.60 | 25.78 | 25.96 | 26.14 | 26.32 | 26.50 | 26.68 | 26.86 | 27.04 | 27.22 |
| 33 | 27.40 | 27.58 | 27.76 | 27.94 | 28. | 28.30 | 28.48 | 28.66 | 28.84 | 29.02 |
| 34 | 29.20 | 29.38 | 29.56 | 29.74 | 29.92 | 30.10 | 30.28 | 30.46 | 30.64 | 30.82 |
| -35 | -31.00 | -31.18 | -31.36 | -31.54 | $-31.72$ | -31.90 | $-32.08$ | $-32.26$ | -32.44 | $-32.62$ |
| 36 | 32.80 | 32.98 | 33.16 | 33.34 | 33.52 | 33.70 | 33.88 | 34.06 | 34.24 | 34.42 |
| 37 | 34.60 | 34.78 | 34.96 | 35.14 | $35 \cdot 32$ | 35.50 | 35.68 | 35.86 | 36.04 | 6.22 |
| 38 | 36.40 | 36.58 | 36.76 | 36.94 | 37.12 | 37.30 | 37.48 | 37.66 | 37.84 | 38.02 39.82 |
| 39 | 38.20 | 38.38 | 38.56 | 38.74 | 38.92 | 39.10 | 39.28 | 39.46 | 39.64 | 39.82 |
| -40 | -40.00 | -40.18 | $-40.36$ | $-40.54$ | $-40.72$ | -40.90 | $-41.08$ | -41.26 | -41.44 | -41. 62 |
|  | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |


| Centigrade. | . 0 | . 1 | . 2 | .3 | .4 | . 5 | . 6 | .7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F. | F. | F. | F. | F. | F. | F. | F, | F. | F. |
| $-40^{\circ}$ | - 40.00 | - 40.18 | $-40.36$ | $-40.54$ | - 40.72 | - 40.90 | - 41.08 | - 41.26 | $-4 \mathrm{I}^{\circ} .44$ | 41.62 |
| 4 I | 41.80 | 41.98 | 42.16 | 42.34 | 42.52 | 42.70 | 42.88 | 43.06 | 43.24 | 43.42 |
| 42 | 43.60 | 43.78 | 43.96 | 44.14 | 44.32 | 44.50 | 44.68 | 44.86 | 45.04 | 45.22 |
| 43 | 45.40 | 45.58 | 45.76 | 45.94 | 46.12 | 46.30 | 46.48 | 46.66 | 46.84 | 47.02 |
| 44 | 47.20 | 47.38 | $47 \cdot 56$ | 47.74 | 47.92 | 48.10 | 48.28 | 48.46 | 48.64 | 48.82 |
| - 45 | 49.00 | - 49.18 | - 40.36 | - 49.54 | 49.72 | 49.90 | - 50.08 | - 50.26 | - 50.44 | - 50.62 |
| 46 | 50.80 | 50.98 | 51.16 | 51.34 | 51.52 | 51.70 | 51.88 | 52.06 | 52.24 | 52.42 |
| 47 | 52.60 | 52.78 | 52.96 | 53.14 | 53.32 | 53.50 | 53.68 | 53.86 | 54.04 | 54.22 |
| 48 | 54.40 | 54.58 | 54.76 | 54.94 | 55.12 | $55 \cdot 30$ | 55.48 | 55.66 | 55.84 | 56.02 |
| 49 | .56.20 | 56.38 | 56.56 | 56.74 | 56.92 | 57.10 | 57.28 | 57.46 | 57.64 | 57.82 |
| - 50 | 58.00 | 58.18 | 58.36 | - 58.54 | 58.72 | 58.90 | 50.08 | 59.26 | - 59.44 | 59.62 |
| 51 | 59.80 | 59.98 | 60.16 | 60.34 | 60.52 | 60.70 | 60.98 | 61.06 | 61.24 | 61.42 |
| 52 | 61.60 | 61.78 | 61.96 | 62.14 | 62.32 | 62.50 | 62.68 | 62.86 | 63.04 | 63.22 |
| 53 | 63.40 | 63.58 | 63.76 | 63.94 | 64.12 | 64.30 | $6+.48$ | 64.66 | 64.84 | 65.02 |
| 54 | 65.20 | 65.38 | 65.56 | 65.74 | 65.92 | 66.10 | 66.28 | 66.46 | 66.64 | 66.82 |
| - 55 | 67.00 | -67.18 | - 67.36 | -67.54 | -67.72 | - 67.90 | - 68.08 | - 68.26 | - 68.44 | -68.62 |
| 56 | 68.80 | 68.98 | 69.16 | 69.34 | 69.52 | 69.70 | 69.88 | 70.06 | 70.24 | 70.42 |
| 57 | 70.60 | 70.78 | 70.96 | 71.14 | 71.32 | 71.50 | 71.68 | 71.86 | 72.04 | 72.22 |
| 58 | 72.40 | 72.58 | 72.76 | 72.94 | 73.12 | 73.30 | 73.48 | 73.66 | 73.84 | 74.02 |
| 59 | 74.20 | 74.38 | 74.56 | 74.74 | 74.92 | 75.10 | 75.28 | 75.46 | 75.64 | 75.82 |
| , -60 | 76.00 | $-76.18$ | - 76.36 | 76.54 | 76.72 | - 76.90- | - 77.08 | - 77.26 | - 77.44 | - 77.62 |
| 61 | 77.80 | 77.98 | 78.16 | 78.34 | 78.52 | 78.70 | 78.88 | 79.06 | 79.24 | 79.42 |
| 62 | 79.60 | 79.78 | 79.96 | 80.14 | 80.32 | 80.50 | 80.68 | 80.86 | SI.O4 | 81.22 |
| 63 | 8 I .40 | 8 I .58 | 81.76 | 81.94 | 82.12 | 82.30 | 82.48 | 82.66 | 82.84 | 83.02 |
| 64 | 83.20 | 83.38 | 83.56 | 83.74 | 83.92 | 84.10 | 84.28 | 84.46 | 84.64 | 84.82 |
| $-65$ | - 85.00 | -85.18 | $-85.36$ | - 85.54 | 85.72 | - 85.90 | - 86.08 | - 86.26 | - 86.44 | 86.62 |
| 66 | 86.80 | 86.98 | 87.16 | 87.34 | 87.52 | 87.70 | 87.88 | 88.06 | 88.24 | 88.42 |
| 67 | 88.60 | 88.78 | 88.96 | 89.14 | S9.32 | 89.50 | 89.68 | 89.86 | 90.04 | 90.22 |
| 68 | 90.40 | 90.58 | 90.76 | 90.94 | 91.12 | 91.30 | 91.48 | 91.66 | 91.84 | 92.02 |
| 69 | 92.20 | 92.38 | 92.56 | 92.74 | 92.92 | 93.10 | 93.28 | 93.46 | 93.64 | 93.82 |
| - 70 | 94.00 | - 94.18 | - 94.36 | - 94.54 | - 94.72 | - 94.90 | - 95.08 | - 95.26 | - 95.44 | - 95.62 |
| 71 | 95.80 | 95.98 | 96.16 | 96.34 | 96.52 | 96.70 | 96.88 | 97.06 | 97.24 | 97.42 |
| 72 | 97.60 | 97.78 | 97.96 | 98.14 | 98.32 | 98.50 | 98.68 | 98.86 | 99.04 | 99.22 |
| 73 | 99.40 | 99.58 | 99.76 | 99.94 | 100.12 | 100.30 | 100.48 | 100.66 | 100.84 | 101.02 |
| 74 | IOI. 20 | 101.38 | 101.56 | 101.74 | 101.92 | 102.10 | 102.28 | 102.46 | 102.64 | 102.82 |
| -75 | -103.00 | -103.18 | -103.36 | -103.54 | -103.72 | -103.90 | -104.08 | -104.26 | -104.44 | 10.4 .62 |
| 76 | 104.80 | 104.98 | 105.16 | 105.34 | 105.52 | 105.70 | 105.88 | 106.06 | 106.24 | 106.42 |
| 77 | 106.60 | 106.78 | 106.96 | 107.14 | 107.32 | 107.50 | 107.68 | 107.86 | 108.04 | 108.22 |
| 78 | 108.40 | 108.58 | 108.76 | 108.94 | 109.12 | 109.30 | 109.48 | 109.66 | 109.84 | 110.02 |
| 79 | 110.20 | 110.38 | 110.56 | 110.74 | 110.92 | 111.10 | III. 28 | III. 46 | III. 64 | 111.82 |
| $-80$ | \|-II2.00 | -112.18 | -II2.36 | -112.54 | -II2.72 | -II 2.90 | -113.08 | -113.26 | - 113.44 | -113.62 |
| 81 | 113.80 | 113.98 | II. 1.16 | II 1 + 34 | 114.52 | 114.70 | 114.88 | 115.06 | 115.24 | 115.42 |
| 82 | I 15.60 | 115.78 | 115.96 | 116.14 | 116.32 | 116.50 | 116.68 | 116.86 | 117.04 | 117.22 |
| 83 | I 17.40 | 117.58 | 117.76 | 117.94 | II8.I2 | 118.30 | 118.48 | 118.66 | 118.84 | 119.02 |
| 84 | I19.20 | 119.38 | I 19.56 | 119.74 | 119.92 | 120.10 | 120.28 | 120.46 | I 20.64 | 120.82 |
| -85 | -121.00 | -I21.18 | -121.36- | -121.54 | -121.72 | - 121.90 | -122.0S | - 122.26 | -I32.44 | -122.62 |
| 86 | 122.80 | 122.98 | 123.16 | 123.34 | 123.52 | 123.70 | 123.88 | 124.06 | 124.24 | 124.42 |
| 87 | 124.60 | 124.78 | 124.96 | 125.14 | 125.32 | 125.50 | 125.68 | 125.86 | 126.04 | 126.22 |
| 88 | I26.40 | 126.58 | 126.76 | 126.94 | 127.12 | 127.30 | 127.48 | 127.66 | 127.84 | 128.02 |
| 89 | I28.20 | 128.38 | 128.56 | 128.74 | 128.92 | 129.10 | I 29.28 | 129.46 | 129.64 | 129.82 |
| $-90$ | -130.00 | -130.18 | -130.36 | -130.54 | -130.72 | -130.90 | -131.08 | -131.26 | -131.44 | -131.62 |
|  | . 0 | .1 | . 2 | . 3 | .4 | . 5 | . 6 | .7 | . 8 | . 9 |

Table 4.
CENTIGRADE SCALE TO FAHRENHEIT - Near the Boiling Point.

| Centigrade. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $100^{\circ}$ | $\begin{gathered} \text { F. } \\ 212.00 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 212.18 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 212^{\circ} .36 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 212.54 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 212.72 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 212.90 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 213.08 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 213.26 \end{gathered}$ | $\begin{gathered} F . \\ 213 \circ 44 \end{gathered}$ | $\begin{gathered} F_{1} \\ 213: 62 \end{gathered}$ |
| 99 | 210.20 | 210.38 | 210.56 | 210.74 | 210.92 | 21.10 | 211.28 | 211.46 | 211.64 | 211.82 |
| 98 | 208.40 | 208.58 | 208.76 | 208.94 | 209.12 | 209.30 | 209.48 | 209.66 | 209.84 | 210.02 |
| 97 | 206.60 | 206.78 | 206.96 | 207.14 | 207.32 | 207.50 | 207.68 | 207.86 | 208.04 | 208.22 |
| 96 | 204.80 | 204.98 | 205.16 | 205.34 | 205.52 | 205.70 | 205.88 | 206.06 | 206.24 | 206.42 |
| 95 | 203.00 | 203.18 | 203.36 | 203.54 | 203.72 | 203.90 | 204.08 | 204.26 | 204.44 | 204.62 |
| 94 | 201.20 | 201.38 | 201.56 | 201.74 | 201.92 | 202.10 | 202.28 | 202.46 | 202.64 | 202.82 |
| 93 | 199.40 | 199.58 | 199.76 | 199.94 | 200. 12 | 200.30 | 200.48 | 200.66 | 200.84 | 201.02 |
| 92 | 197.60 | 197.78 | 197.96 | 198.14 | 198.32 | 198.50 | 198.68 | 198.86 | 199.04 | 199.22 |
| 91 | 195.80 | 195.98 | 196.16 | 196.34 | 196.52 | 196.70 | 196.88 | 197.06 | 197.24 | 197.42 |
| 90 | 194.00 | 194.18 | 194.36 | 194.54 | 194.72 | 194.90 | I95.08 | 195.26 | I95.44 | 195.62 |

TABLE 5.
DIFFERENCES FAHRENHEIT TO DIFFERENCES CENTIGRADE.

| Fahrenheit. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | $\begin{gathered} \text { c. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { c. } \\ 0.06 \end{gathered}$ | $\begin{gathered} \text { c. } \\ 0 . \mathrm{II}^{2} \end{gathered}$ | $\begin{gathered} c . \\ 0.17 \end{gathered}$ | $\begin{gathered} c . \\ 0.22 \end{gathered}$ | $\begin{gathered} \text { c. } \\ 0.28 \end{gathered}$ | $\begin{gathered} c . \\ 0.33 \end{gathered}$ | $\begin{gathered} \text { c. } \\ 0.39 \end{gathered}$ | $\begin{gathered} \text { c. } \\ 0.44 \end{gathered}$ | $\begin{gathered} \text { c. } \\ 0.50 \end{gathered}$ |
| 0 | 0.56 | 0.61 | 0.67 | 0.72 | 0.78 | 0.83 | 0.33 0.89 | 0.39 0.94 | I. 00 | I. 06 |
| 2 | I. 11 | I. 17 | I. 22 | I. 28 | 1.33 | I. 39 | I. 44 | I. 50 | I. 56 | I. 6 ? |
| 3 | I. 67 | 5.72 | 1.78 | I. 83 | 1.89 | I. 94 | 2.00 | 2.06 | 2.1 I | 2. 17 |
| 4 | 2.22 | 2.28 | 2.33 | 2.39 | 2.44 | 2.50 | 2.56 | 2.61 | 2.67 | 2.72 |
| 5 | 2.75 | 2.83 | 2.89 | 2.94 | 3.00 | 3.06 | 3. II | 3.17 | 3.22 | 3.28 |
| 6 | 3.33 | 3.39 | 3.44 | 3.50 | 3.56 | 3.61 | 3.67 | 3.72 | 3.78 | 3.83 |
| 7 | 3.89 | 3.94 | 4.00 | 4.06 | 4. II | 4.17 | 4.22 | 4.28 | 4.33 | 4.39 |
| 8 | 4.44 | 4.50 | 4.56 | 4.61 | 4.67 | 4.72 | 4.78 | 4.83 | 4.89 | 4.94 |
| 9 | 5.00 | 5.06 | 5. I I | 5.17 | 5.22 | 5.28 | 5.33 | 5.39 | 5.44 | 5.50 |
| 10 | 5.56 | 5.61 | 5.67 | 5.72 | 5.78 | 5.83 | 5.89 | 5.94 | 6.00 | 6.06 |
| I I | 6.11 | 6.17 | 6.22 | 6.28 | 6.33 | 6.39 | 6.44 | 6.50 | 6.56 | 6.61 |
| 12 | 6.67 | 6.72 | 6.78 | 6.83 | 6.89 | 6.94 | 7.00 | 7.06 | 7. I I | 7.17 |
| 13 | 7.22 | 7.28 | 7.33 | 7.39 | 7.44 | 7.50 | $7 \cdot 56$ | 7.61 | 7.67 | 7.72 |
| 14 | 7.78 | 7.83 | 7.89 | 7.94 | 8.00 | 8.06 | S.II | 8.17 | S. 22 | 8.28 |
| 15 | 8.33 | 8.39 | 8.44 | 8.50 | 8.56 | 8.6I | 8.67 | 8.72 | 8.78 | 8.83 |
| 16 | 8.89 | 8.94 | 9.00 | 9.06 | 9. I I | 9.17 | 9.22 | 9.28 | 9.33 | 9.39 |
| 17 | 9.44 | 9.50 | 9.56 | 9.61 | 9.67 | 9.72 | 9.78 | 9.83 | 9.89 | 9.94 |
| IS | 10.00 | 10.06 | 10. II | 10.17 | 10.22 | 10.28 | 10.33 | IO. 39 | 10.44 | 10.50 |
| 19 | 10.56 | 10.6I | 10.67 | 10.72 | 10.78 | 10.83 | Io. 89 | Io. 94 | 11.00 | I 1.06 |
| 20 | 11.11 | II 17 | 11.22 | II. 28 | II. 33 | 11.39 | I 1.44 | I I. 50 | I 1.56 | II.6I |

TABLE 6.
DIFFERENCES CENTIGRADE TO DIFFERENCES FAHRENHEIT.

| Centigrade. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | $\begin{gathered} \text { F. } \\ 0.00 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 0.18 \end{gathered}$ | $\begin{gathered} F . \\ 0.36 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 0.54 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 0_{0}^{0} .72 \end{gathered}$ | $\begin{gathered} \text { F. } \\ 0.90 \end{gathered}$ | $\begin{gathered} \text { F. } \\ \text { I.OS } \end{gathered}$ | $\begin{gathered} \text { F. } \\ \text { I. } 26 \end{gathered}$ | $\begin{gathered} \text { F. } \\ \text { I. } 44 \end{gathered}$ | $\begin{gathered} F . \\ 1.62 \end{gathered}$ |
| I | 1. So | I. 98 | 2.16 | 2.34 | 2.52 | 2.70 | 2.58 | 3.06 | 3.24 | 3.42 |
| 2 | 3.60 | 3.78 | 3.96 | 4.14 | 4.32 | 4.50 | 4.68 | 4.86 | 5.04 | 5.22 |
| 3 | 5.40 | 5.58 | 5.76 | 5.94 | 6.12 | 6.30 | 6.48 | 6.66 | 6.84 | 7.02 |
| 4 | 7.20 | $7 \cdot 38$ | 7.56 | 7.74 | 7.92 | 8.10 | 8.28 | 8.46 | 8.64 | 8.82 |
| 5 | 9.00 | 9.18 | 9.36 | 9.54 | 9.72 | 9.90 | 10.08 | 10.26 | 10.44 | 10.62 |
| 6 | 10.So | 10.98 | I1.16 | II 1.34 | II. 52 | 11.70 | II. SS | 12.06 | 12.24 | 12.42 |
| 7 | 12.60 | 12.78 | 12.96 | I3.14 | 13.32 | 13.50 | 13.68 | 13.86 | 14.04 | 14.22 |
| 8 | 14.40 | 14.58 | 14.76 | 14.94 | I5.12 | 15.30 | 15.48 | I 5.66 | 15.84 | 16.02 |
| 9 | 16.20 | 16.38 | 16.56 | 16.74 | 16.92 | 17.10 | 17.28 | 17.46 | 17.64 | 17.82 |

Smithsonian Tables.

CORRECTION FOR THE TEMPERATURE OF THE EMERGENT MERCURIAL COLUMN OF THERMOMETERS.
$T=t-0.000086 n\left(t^{\prime}-t\right)-$ Fahrenheit temperatures.
$T=t-0.000155 n\left(t^{\prime}-t\right)-$ Centigrade temperatures.
$T=$ Corrected temperature.
$t=$ Observed temperature.
$t^{\prime}=$ Mean temperature of the glass stem and emergent mercury column.
$n=$ Length of mercury in the emergent stem in scale degrees.
When $t^{\prime}$ is $\left\{\frac{\text { higher }}{\text { lower }}\right\}$ than $t$ the numerical correction is to be $\left\{\frac{\text { subtracted. }}{\text { added. }}\right\}$

Table 7.
CORRECTION FOR FAHRENHEIT THERMOMETERS.
Values of $0.000086 n\left(t^{\prime}-t\right)$

| $n$ | $t^{\prime}-t$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{\circ}$ | $20^{3}$ | $30^{\circ}$ | 40 | $50^{\circ}$ | $60^{\circ}$ | $70^{\circ}$ | $80^{\circ}$ | $90^{\circ}$ | $100^{\circ}$ |
| F. | F. | F. | F. | F. | F. | F. | F. |  | F. | F. |
| $10^{\circ}$ | O.OI | 0.02 | 0.03 | 0.03 | 0.04 | 0.05 |  | 0.07 | 0.08 | 0.09 |
| 20 | 0.02 | 0.03 | 0.05 | 0.07 | 0.09 | 0.10 | 0. 12 | 0.14 | 0.15 | 0.17 |
| 30 | 0.03 | 0.05 | 0.08 | 0.10 | 0.13 | 0.15 | 0.18 | 0.21 | 0.23 | 0.26 |
| 40 | 0.03 | 0.07 | 0.10 | 0.14 | 0.17 | 0.21 | 0.24 | 0.28 | 0.31 | 0.34 |
| 50 | 0.04 | 0.09 | 0.13 | 0.17 | 0.22 | 0.26 | 0.30 | 0.34 | 0.39 | 0.43 |
| 60 | 0.05 | 0.10 | 0.15 | 0.21 | 0.26 | 0.31 | 0.36 | 0.41 | 0.46 | 0.52 |
| 70 | 0.06 | 0.12 | 0.18 | 0.24 | 0.30 | 0.36 | 0.42 | 0.48 | 0.54 | 0.60 |
| 80 | 0.07 | 0.14 | 0.21 | 0.28 | 0.34 | 0.41 | 0.48 | 0.55 | 0.62 | 0.69 |
| 00 | 0.08 | 0.15 | 0.23 | 0.31 | 0.39 | 0.46 | 0.54 | 0.62 | 0.70 | 0.77 |
| 100 | 0.09 | 0.17 | 0.26 | 0.34 | 0.43 | 0.52 | 0.60 | 0.69 | 0.77 | 0.86 |
| 110 | 0.09 | 0.19 | 0.28 | 0.38 | 0.47 | 0.57 | 0.66 | 0.76 | 0.85 | 0.95 |
| 120 | 0.10 | 0.21 | 0.31 | 0.41 | 0.52 | 0.62 | 0.72 | 0.83 | 0.93 | 1.03 |
| 130 | 0.11 | 0.22 | 0.34 | 0.45 | 0.56 | 0.67 | 0.78 | 0.90 | 1.01 | 1.12 |

Table 8.
CORRECTION FOR CENTIGRADE THERMOMETERS.
Values of $0.000155 n\left(t^{\prime}-t\right)$

| $n$ | $t^{\prime}-1$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | $20^{\circ}$ | $30^{\circ}$ | 40 | 50 | 60 | 70 | $80^{\circ}$ |
| c. | ${ }_{0}$. | c. | c. | c. | c. | c. | c. | c. |
| 10 | 0.02 | 0.03 | 0.05 | 0.00 | 0.08 | 0.09 | O. 11 | 0.12 |
| 20 | 0.0.3 | 0.06 | 0.09 | 0.12 | 0.16 | 0.19 | 0.22 | 0.25 |
| 30 | 0.05 | 0.00 | 0.14 | 0.10 | 0.23 | 0.28 | 0.33 | 0.37 |
| 40 | 0.06 | 0.12 | 0.19 | 0.25 | 0.31 | 0.37 | 0.43 | 0.50 |
| 50 | 0.08 | 0.10 | 0.23 | 0.31 | 0.30 | 0.46 | 0.54 | 0.62 |
| 60 | 0.00 | 0.19 | 0.28 | 0.37 | 0.46 | 0.56 | 0.65 | 0.74 |
| 70 | O. 11 | 0.22 | 0.33 | 0.43 | 0.54 | 0.65 | 0.76 | 0.87 |
| 80 | 0.12 | 0.25 | 0.37 | 0.50 | 0.62 | 0.74 | 0.87 | 0.99 |
| 00 | -. 14 | 0.28 | 0.42 | 0.56 | 0.70 | 0.84 | 0.98 | 1.12 |
| 100 | O. I 6 | 0.31 | 0.46 | 0.62 | 0.78 | 0.93 | 1.08 | I. 24 |

## CONVERSIONS INVOLVING LINEAR MEASURES.

Inches into millimeters ..... Table 9
Millimeters into inches ..... Table 10
Barometric inches (mercury) into millibars ..... Table il
Barometric millimeters (mercury) into millibars ..... Table 12
Feet into meters ..... Table I3
Meters into feet ..... Table 14
Miles into kilometers ..... Table 15
Kilometers into miles ..... Table 16
Interconversion of nautical and statute miles ..... Table 17
Continental measures of length with their metric and EnglishequivalentsTable 18

INCHES INTO MILLIMETERS.
1 inch $=25.40005 \mathrm{~mm}$.

| Inches. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm | mm. | mm . | min. | mm. | mm, | mm . | mm. | mm. | mm. |
| 0.00 | 0.00 | 0.25 | 0.51 | 0.76 | . 02 | 1.27 | 1.52 | 1.78 | 2.03 | 2.29 |
| 0.10 | 2.54 | 2.79 | 3.05 | 3.30 | 3.56 | 3.81 | 4.06 | 4.32 | 4.57 | 4.83 |
| 0.20 | 5.08 | 5.33 | 5.59 | 5.84 | 6.10 | 6.35 | 6.60 | 6.86 | 7.11 | 7.37 |
| 0.30 | 7.62 | 7.87 | S.13 | 8.38 | S.64 | 8.89 | 9.14 | 9.40 | 9.65 | 9.91 |
| 0.40 | 10.16 | 10.41 | 10.67 | 10.92 | I1.18 | 11.43 | 11.68 | II. 94 | 12.19 | 12.45 |
| 0.50 | 12.70 | 12.95 | 13.21 | 13.46 | 13.72 | 13.97 | 14.22 | 14.48 | 14.73 | 14.99 |
| 0.60 | I5.24 | 15.49 | 15.75 | 16.00 | 16.26 | 16.51 | 16.76 | 17.02 | 17.27 | 17.53 |
| 0.70 | 17.78 | 18.03 | I8.29 | IS. 54 | 18.8o | 19.05 | 19.30 | 19.56 | 19.81 | 20.07 |
| 0.80 | 20.32 | 20.57 | 20.53 | 21.08 | 21.34 | 21.59 | 21.84 | 22.10 | 22.35 | 22.61 |
| 0.90 | 22.86 | 23.11 | 23.37 | 23.62 | 23.88 | 24.13 | 24.38 | 24.64 | 24.89 | 25.15 |
| 1.00 | 25.40 | 25.65 | 25.91 | 26.16 | 26.42 | 26.67 | 26.92 | 27.18 | 27.43 | 27.69 |
| 1.10 | 27.94 | 28.19 | 28.45 | 28.70 | 28.96 | 29.21 | 29.46 | 29.72 | 29.97 | 30.23 |
| 1.20 | 30.48 | 30.73 | 30.99 | 31.24 | 31.50 | 3 I .75 | 32.00 | 32.26 | 32.51 | 32.77 |
| 1.30 | 33.02 | 33.27 | 33.53 | 33.78 | 34.04 | 34.29 | 34.54 | 34.80 | 35.05 | 35.31 |
| I. 40 | 35.56 | 35.8I | 36.07 | 36.32 | 36.58 | 36.83 | 37.08 | 37.34 | 37.59 | 37.85 |
| 1.50 | 38.10 | 38.35 | 38.61 | 38.86 | 39.12 | 39.37 | 39.62 | 39.8S | 40.13 | 40.39 |
| 1.60 | 40.64 | 40.89 | 41.15 | 4 I .40 | 41.66 | 41.91 | 42.16 | 42.42 | 42.67 | 42.93 |
| 1.70 | 43.18 | 43.43 | 43.69 | 43.94 | 44.20 | 44.45 | 44.70 | 44.96 | 45.2 I | 45.47 |
| I.So | 45.72 | 45.97 | 46.23 | 46.48 | 46.74 | 46.99 | 47.24 | 47.50 | 47.75 | 48.01 |
| 1.90 | 48.26 | 48.51 | 48.77 | 49.02 | 49.28 | 49.53 | 49.78 | 50.04 | 50.29 | 50.55 |
| 2.00 | 50.So | 51.05 | 51.31 | 51.56 | 51.82 | 52.07 | 52.32 | 52.58 | 52.83 | 53.09 |
| 2.10 | 53.34 | 53.59 | 53.85 | 54.10 | 54.36 | 54.61 | 54.86 | 55.12 | 55.37 | 55.63 |
| 2.20 | 55.SS | 56.13 | 56.39 | 56.64 | 56.90 | 57.15 | 57.40 | 57.66 | 57.91 | 58.17 |
| 2.30 | 58.42 | 58.67 | 58.93 | 59.18 | 59.44 | 59.69 | 59.94 | 60.20 | 60.45 | 60.71 |
| 2.40 | 60.96 | 6 I .2 I | 61.47 | 61.72 | 6 I .98 | 62.23 | 62.48 | 62.74 | 62.99 | 63.25 |
| 2.50 | 63.50 | 63.75 | 64.01 | 64.26 | 64.52 | 64.77 | 65.02 | 65.28 | 65.53 | 65.79 |
| 2.60 | 66.04 | 66.29 | 66.55 | 66.80 | 67.06 | 67.31 | 67.56 | 67.82 | 68.07 | 68.33 |
| 2.70 | 65.58 | 68.83 | 69.09 | 69.34 | 69.60 | 69.85 | 70.10 | 70.36 | 70.61 | 70.87 |
| 2.80 | 71.12 | 71.37 | 71.63 | 71.88 | 72.14 | 72.39 | 72.64 | 72.90 | 73.15 | 73.41 |
| 2.90 | 73.66 | 73.91 | 74.17 | 74.42 | 74.68 | 74.93 | 75.18 | 75.44 | 75.69 | 75.95 |
| 3.00 | 76.20 | 76.45 | 76.71 | 76.96 | 77.22 | 77.47 | 77.72 | 77.98 | 78.23 | 78.49 |
| 3.10 | ${ }_{7} 8.74$ | 78.99 | 79.25 | 79.50 | 79.76 | So.OI | So. 26 | So. 52 | 80.77 | SI. 03 |
| 3.20 | S1. 28 | 81.53 | S1. 79 | S2.04 | S2.30 | S2.55 | S2.So | S3.06 | 83.31 | S3.57 |
| 3.30 | 83.82 | 84.07 | 84.33 | 84.59 | 84. $8_{4}$ | 85.09 | S5.34 | S5.60 | 85.85 | S6.I I |
| 3.40 | S6.36 | S6.6I | 86.87 | 87.12 | 87.38 | S7.63 | 87.88 | S8.14 | 88. 39 | S8.65 |
| 3.50 | 88.90 | S9.15 | S9.41 | S9.66 | S9.92 | 90.17 | 90.42 | 90.68 | 90.93 | 91.19 |
| 3.60 | 91.44 | 91.69 | 91.95 | 92.20 | 92.46 | 92.71 | 92.96 | 93.22 | 93.47 | 93.73 |
| 3.70 | 93.98 | 94.23 | 9.4 .49 | 94.74 | 95.00 | 95.25 | 95.50 | 95.76 | 96.01 | 96.27 |
| 3.80 | 96.52 | 96.77 | 97.03 | 97.28 | 97.54 | 97.79 | 98.04 | 98.30 | 98.55 | 98.81 |
| 3.90 | 99.06 | 99.31 | 99.57 | 99.82 | 100.08 | 100.33 | 100.58 | 100.84 | 101.09 | 101. 35 |
| 4.00 | 101.60 | IOI. 85 | 102.11 | 102.36 | 102.62 | 102.87 | 103.12 | 103.38 | 103.63 | 103. 99 |
| 4.10 | 104.14 | 104.39 | 104.65 | 104.90 | 105.16 | 105.41 | 105.66 | 105.92 | 106.17 | 106.43 |
| 4.20 | 106.68 | 106.93 | 107.19 | 107.44 | 107.70 | 107.95 | 108. 20 | 108.46 | 10S.71 | 108.97 |
| 4.30 | 109.22 | 109.47 | 109.73 | 109.98 | 110.24 | 110.49 | 110.74 | I I 1 . 00 | 111.25 | III.51 |
| 4.40 | III 1.76 | 112.01 | I 12.27 | 112.52 | 112.78 | 113.03 | 113.28 | II 3.54 | 113.79 | I 14.0.5 |
| 4.50 | 114.30 | 114.55 | 114.81 | 115.06 | II5.32 | 115.57 | 115.82 | I 16.08 | 116.33 | II6.59 |
| 4.60 | II6.84 | 117.09 | I17.35 | 117.60 | 117.86 | IIS.il | 118.36 | IIS.62 | 118.87 | 119.13 |
| 4.70 | II 9.38 | 119.63 | 119.89 | 120.14 | 120.40 | 120.65 | 120.90 | 121.16 | 121.4I | 121.67 |
| 4.80 | 121.92 | 122.17 | 122.43 | 122.68 | 122.94 | 123.19 | 123.44 | 123.70 | 123.95 | 124.2 I |
| 4.90 | 124.46 | 124.7 I | 124.97 | 125.22 | 125.48 | 125.73 | 125.98 | I26.24 | 126.49 | 126.75 |
| 5.00 | 127.00 | 127.25 | 127.51 | 127.76 | 128.02 | 128.27 | 128.52 | 128.78 | 129.03 | 129.29 |

$\begin{array}{lccccccccccc}\text { Proportional Parts. } & \text { Inch. } & 0.001 & 0.002 & 0.003 & 0.004 & 0.005 & 0.006 & 0.007 & 0.008 & 0.009 \\ & \text { mm. } & 0.025 & 0.051 & 0.076 & 0.102 & 0.127 & 0.152 & 0.178 & 0.203 & 0.229\end{array}$

Smithsonian Tableg.

I inch $=25.40005 \mathrm{~mm}$.


Table 9.
INCHES INTO MILLIMETERS.
1 inch $=\mathbf{2 5} .40005 \mathrm{~mm}$.

| Inches. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm | m | mn | mr | m | 111 m . | m | min. | mm. | mm. |
| 10.00 | 254.00 | 254.25 | 254.51 | 254.76 | 255.02 | 255.27 | 255.52 | 255.78 | 256.03 | 256.29 |
| . 10 | 256.54 | 256.79 | 257.05 | 257.30 | 257.56 | 257. ${ }^{\text {I }}$ | 25 S. 06 | 258.32 | 258.57 | 258.83 |
| 10.20 | 259.08 | 259.33 | 259.59 | 259.84 | 260. 10 | 260.35 | 260.60 | 260.86 | 261. II | 261.37 |
| 10.30 | 261.62 | 261.87 | 262. $\mathrm{I}_{3}$ | 262.38 | 262.64 | 262.89 | 263.14 | 263.40 | 263.65 | 263.91 |
| 10.40 | 264. 16 | $26+41$ | 264.63 | 264.92 | 265.18 | 265.43 | 265.68 | 265.94 | 266.19 | 266.45 |
| 10.50 | 266.70 | 266.95 | 267.21 | 267.46 | 267.72 | 267.97 | 268.22 | 268.48 | 268.73 | 268.99 |
| 10.60 | 269.24 | 269.49 | 269.75 | 270.00 | 270.26 | 270.51 | 270.76 | 271.02 | 271.27 | 271.53 |
| 10.70 | 271.78 | 272.03 | 272.29 | 272.54 | 272.80 | 273.05 | 273.30 | 273.56 | 273.81 | 274.07 |
| 10.So | 274.32 | 274.57 | 274.93 | 275.0S | 275.34 | 275.59 | 275.8.4 | 276. 10 | 276.35 | 276.61 |
| 10.90 | 276.86 | 277. I I | 277.37 | 277.62 | 277.88 | 278.13 | 278.38 | 278.64 | 278.89 | 279.15 |
| 11.00 | 279.40 | 279.65 | 279.91 | 280.16 | 280. 42 | 280. 67 | 280.92 | 28 I .18 | 281.43 | 281. 69 |
| I I.IG | 28.94 | 2S2.19 | 282.45 | 282.70 | 282.96 | 283.21 | 283.46 | 2S3.72 | 283.97 | 284.23 |
| 11.20 | 284.48 | 284.73 | 284.99 | 285.24 | 285.50 | $2 S 5.75$ | 286.00 | 286.26 | 286.51 | 286.77 |
| I 1.30 | 287.02 | 287.27 | 287.53 | 287.78 | 288.04 | 288.29 | 288.54 | 285.80 | 289.05 | 289.3I |
| 11.40 | 289.56 | 289.81 | 290.07 | 290.32 | 290.58 | 290.83 | 291.08 | 291.34 | 291.59 | 291.85 |
| 11.50 | 292.10 | 292.35 | 292.6I | 292.86 | 293.12 | 293.37 | 293.62 | 293.88 | 294. 13 | 294.39 |
| 11.60 | 294.64 | 294.89 | 295.15 | 295.40 | 295.66 | 295.91 | 296.16 | 296.42 | 296.67 | 296.93 |
| 11.70 | 297. IS | 297.43 | 297.69 | 297.94 | 298.20 | 298.45 | 298.70 | 298.96 | 299.21 | 299.47 |
| I 1. So | 299.72 | 299.97 | 300.23 | 300.48 | 300.74 | 300.99 | 301.24 | 301.50 | 301.75 | 302.01 |
| 11.90 | 302.26 | 302.5 I | 302.77 | 303.02 | 303.28 | 303.53 | 303.78 | 304.04 | 304.29 | 304.55 |
| 12.00 | 304.80 | 305.05 | 305.3I | 305.56 | 305.82 | 306.07 | 306.32 | 306.58 | 306.83 | 307.09 |
| 12.10 | 307.34 | 307.59 | 307.85 | 308. 10 | 308.36 | 308.61 | 308.86 | 309. 12 | 309.37 | 309.63 |
| 12.20 | 309.8S | 310.13 | 310.39 | 310.64 | 310.90 | 311.15 | 311.40 | 311.66 | 31.91 | 312.17 |
| 12.30 | 312.42 | 312.67 | 312.93 | 313.18 | 313.44 | 313.69 | 313.94 | 314.20 | 314.45 | 314.71 |
| 12.40 | 314.96 | 315.2 I | 315.47 | 315.72 | 315.98 | 316.23 | 316.48 | 316.74 | 316.99 | 317.25 |
| 12.50 | 317.50 | 317.75 | 3 IS . 1 | 318.26 | 318.52 | 318.77 | 319.02 | 319.28 | 319.53 | 319.79 |
| 12.60 | 320.04 | 320.29 | 320.55 | 320.80 | 321.06 | 321.31 | 32 I. 56 | 32 I .82 | 322.07 | 322.33 |
| 12.70 | 322.58 | 322.83 | 323.09 | 323.34 | 323.60 | 323.85 | 324. IO | 324.36 | 324.61 | 324.87 |
| 12.80 | 325. 12 | 325.37 | 325.63 | 325.88 | 326. I 4 | 326.39 | 326.64 | 326.90 | 327.15 | 327.41 |
| 12.90 | 327.66 | 327.91 | 328.17 | 328.42 | 328.68 | 328.93 | 329.18 | 329.44 | 329.69 | 329.95 |
| 13.00 | 330.20 | 330.45 | 330.71 | 330.96 | 331.22 | 331.47 | 331.72 | 331.98 | 332.23 | 332.49 |
| 13.10 | 332.74 | 332.99 | 333.25 | 333.50 | 333.76 | 334.01 | 334.26 | 334.52 | 334.77 | 335.03 |
| 13.20 | 335.28 | 335.53 | 335.79 | 336.04 | 336.30 | 336.55 | 336.80 | 337.06 | 337.31 | 337.57 |
| 13.30 | 337.82 | 338.07 | 338.33 | 338.58 | 338.84 | 339.09 | 339.34 | 339.60 | 339.85 | 340. II |
| 13.40 | 340.36 | 340.6I | 340. 87 | 34 I .12 | 341.38 | 341.63 | 341.88 | 342.14 | 342.39 | 342.65 |
| 13.50 | 342.90 | 343. I5 | 343.41 | 343.66 | 343.92 | 344. 7 | 344.42 | 344.68 | 344.93 | 345.19 |
| 13.60 | 345.44 | 345.69 | 345.95 | 346.20 | 346.46 | 346.71 | 346.96 | 347.22 | 347.47 | 347.73 |
| 13.70 | 347.98 | 3.48 .23 | 34 S .49 | 348.74 | 349.00 | 349.25 | 349.50 | 349.76 | 350.01 | 350.27 |
| 13.80 | 350.52 | 350.77 | 351.03 | 351.28 | 351.54 | 351.79 | 352.04 | 352.30 | $35^{2} .55$ | 352.8I |
| 13.90 | 353.06 | 353.3I | 353.57 | 353.82 | 354.0S | 354.33 | 354.58 | 354.84 | 355.09 | 355.35 |
| 14.00 | 355.60 | 355.85 | 356. II | 356.36 | 356.62 | 356.87 | 357.12 | 357.38 | 357.63 | 357.89 |
| 14.10 | 35 S. 14 | 358.39 | 358.65 | 358.90 | 359.16 | 359.41 | 359.66 | 359.92 | 360.17 | 360.43 |
| 14.20 | 360.68 | 360.93 | 361.19 | 361.44 | 361.70 | 361.95 | 362.20 | 362.46 | 362.71 | 362.97 |
| 14.30 | 363.22 | 363.47 | 363.73 | 363.98 | 364.24 | 364.49 | 364.74 | 365.00 | 365.25 | 365.5I |
| 14.40 | 365.76 | 366.01 | 366.27 | 366.52 | 366.78 | 367.03 | 367.28 | 367.54 | 367.79 | 368.05 |
| 14.50 | 368.30 | 368.55 | 368.8 I | 369.06 | 369.32 | 369.57 | 369.82 | 370.08 | 370.33 | 370.59 |
| 14.60 | 370.84 | 371.09 | 371.35 | 371.60 | 371.86 | 372.11 | 372.36 | 372.62 | 372.87 | 373.13 |
| 14.70 | 373.35 | 373.63 | 373.59 | 374.14 | 374.40 | 374.65 | 374.90 | 375.16 | 375.41 | 375.67 |
| 14.80 | 375.92 | 376. 17 | 376.43 | 376.68 | 376.94 | 377.19 | 377.44 | 377.70 | 377.95 | 378.21 |
| 14.90 | 378.46 | 378.71 | 378.97 | 379.22 | 379.48 | 379.73 | 379.98 | 380. 24 | 380.49 | 380. 75 |
| 15.00 | 381.00 | 381.25 | 381.51 | 3 SI. 76 | 382.02 | 382.27 | 382.52 | 382.78 | 383.03 | 383.29 |

$\begin{array}{llllllllllll}\text { Proportional Parts. Inch. } & 0.001 & 0.002 & 0.003 & 0.004 & 0.005 & 0.006 & 0.007 & 0.008 & 0.009\end{array}$ $\begin{array}{lllllllll}\mathrm{mm} & 0.025 & 0.05 \mathrm{I} & 0.076 & 0.102 & 0.127 & 0.152 & 0.178 & 0.203\end{array} 0.229$

1 inch $=25.40005 \mathrm{~mm}$.


Table 9.
INCHES INTO MILLIMETERS.
1 inch $=25.40005 \mathrm{~mm}$.

smitheonian Tableb.

1 inch $=25.40005 \mathrm{~mm}$.

| Inches. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm. | mm. | mm. | mm. | mm. | mmm. | mm. | mm. | . | mm. |
| 25.00 | 635.00 | 635.26 | 635.51 | 635.76 | 636.02 | 636.27 | 636.53 | 636.78 | 637.03 | 637.29 |
| 25.10 | 637.54 | 637.80 | 638.05 | 638.30 | 638.56 | 638.81 | 639.07 | 639.32 | 639.57 | 639.83 |
| 25.20 | 640.08 | 6.40 .34 | 640.59 | 640.84 | 6.41 .10 | 641.35 | 641.61 | 641.86 | 642.11 | 642.37 |
| 25.30 | 6.42 .62 | 642.88 | 643. 13 | $643 \cdot 38$ | 6.43 .64 | 643.59 | 644.15 | 644.40 | 644.65 | 644.91 |
| 25.40 | 645.16 | 645.42 | 645.67 | 645.92 | 6.46. IS | 646.43 | 6.46 .69 | 646.94 | 647.19 | 647.45 |
| 25.50 | 647.70 | 647.96 | 6.48 .21 | 648.46 | $6+8.72$ | 648.97 | 649.23 | 6.49 .45 | 649.73 | 649.99 |
| 25.60 | 650.24 | 650.50 | 650.75 | 651.00 | 65 I .26 | 651.51 | 65 I .77 | 65.02 | 654.27 | 652.53 |
| 25.70 | 652.78 | 653.04 | 653.29 | 653.54 | 653.80 | 654.05 | 654.31 | 654.56 | 654.8 I | 655.07 |
| 25.So | 655.32 | 655.58 | 655.83 | 656.08 | 656.34 | 656.59 | 656.85 | 657.10 | 657.35 | 657.61 |
| 25.90 | 657.86 | 65 S. 12 | 658.37 | $65 S .62$ | 65 S. SS | 659. I3 | 659.39 | 659.64 | 659.59 | 660.15 |
| 26.00 | 660.40 | 660.66 | 660.91 | 661.16 | 661.42 | 661.67 | 661.93; | 662.18 | 662.43 | 662.69 |
| 26.10 | 662.94 | 663.20 | 663.45 | 663.70 | 663.96 | 664.21 | 66.4 .47 | 664.72 | 664.97 | 665.23 |
| 26.20 | 665.48 | 665.74 | 665.99 | 666.24 | 666.50 | 666.75 | 667.01 | 667.26 | 667.51 | 667.77 |
| 26.30 | 668.02 | 668.28 | 665.53 | 665.78 | 669.04 | 669.29 | 669.55 | 669.So | 670.05 | 670.31 |
| 26.40 | 670.56 | 670.82 | 671.07 | 671.32 | 671.58 | 67 I .83 | 672.09 | 672.34 | 672.59 | 672.85 |
| 26.50 | 673.10 | 673.36 | 673.61 | 673.86 | 674.12 | 674.37 | 674.63 | 674.88 | 675.13 | 675.39 |
| 26.60 | 675.64 | 675.90 | 676.15 | 676.40 | 676.66 | 676.91 | 677.17 | 677.42 | 677.67 | 677.93 |
| 26.70 | 678.18 | 678.44 | 678.69 | 678.94 | 679.20 | 679.45 | 679.71 | 679.96 | 6So. 21 | 650.47 |
| 26.80 | 650.72 | 680.98 | 681.23 | 681.48 | 6 SI .74 | 68 I .99 | 682.25 | 682.50 | 682.75 | 683.01 |
| 26.90 | 683.26 | 683.52 | 683.77 | 684.02 | 684.28 | 684.53 | 684.79 | 685.04 | 655.29 | 685.55 |
| 27.00 | 685.80 | 686.06 | 686.3I | 686.56 | 686.82 | 687.07 | 687.33 | 687.58 | 687.83 | 688.09 |
| 27.10 | 685.34 | 688.60 | 688.85 | 6S9.10 | 689.36 | 6S9.61 | 689.87 | 690.12 | 690.37 | 690.63 |
| 27.20 | 690.85 | 691.14 | 691.39 | 691.64 | 691.90 | 692.15 | 692.41 | 692.66 | 692.91 | 693.17 |
| 27.30 | 693.42 | 693.68 | 693.93 | 694.18 | 694.44 | 69.4 .69 | 694.95 | 695.20 | 695.45 | 695.7 I |
| 27.40 | 695.96 | 696.22 | 696.47 | 696.72 | 696.98 | 697.23 | 697.49 | 697.74 | 697.99 | 698.25 |
| 27.50 | 698.50 | 698.76 | 699.01 | 699.26 | 699.52 | 699.77 | 700.03 | 700.28 | 700.53 | 700.79 |
| 27.60 | 701.04 | 701.30 | 701.55 | 701.80 | 702.06 | 702.31 | 702.57 | 702.82 | 703.07 | 703.33 |
| 27.70 | 703.58 | 703.84 | 704.09 | 704.34 | 70.60 | 704.85 | 705.11 | 705.36 | 705.61 | 705.87 |
| 27.80 | 706.12 | 706.35 | 706.63 | 706.88 | 707.14 | 707.39 | 707.65 | 707.90 | 708.15 | 708.41 |
| 27.90 | 708.66 | 708.92 | 709.17 | 709.42 | 709.68 | 709.93 | 710.19 | 710.44 | 710.69 | 710.95 |
| 28.00 | 711.20 | 711.46 | 711.71 | 711.96 | 712.22 | 712.47 | 712.73 | 712.98 | 713.23 | 713.49 |
| 2S.10 | 713.74 | 714.00 | 714.25 | 714.50 | 714.76 | 715.01 | 715.27 | 715.52 | 715.77 | 716.03 |
| 28.20 | 716.28 | 716.54 | 716.79 | 717.04 | 717.30 | 717.55 | 717.81 | 718.06 | 718.31 | 718.57 |
| 28.30 | 718.82 | 719.08 | 719.33 | 719.58 | 719.84 | 720.09 | 720.35 | 720.60 | 720.85 | 721.11 |
| 28.40 | 721.36 | 721.62 | 721.87 | 722.12 | 722.39 | 722.63 | 722.89 | 723.14 | 723.39 | 723.65 |
| 28.50 | 723.90 | 724.16 | 724.41 | 724.66 | 724.92 | 725.17 | 725.43 | 725.68 | 725.93 | 726. I9 |
| 28.60 | 726.44 | 726.70 | 726.95 | 727.20 | 727.46 | 727.71 | 727.97 | 728.22 | 728.47 | 728.73 |
| 28.70 | 728.98 | 729.24 | 729.49 | 729.74 | 730.00 | 730.25 | 730.51 | 730.76 | 731.01 | 731.27 |
| 2 2 .80 | 731.52 | 731.78 | 732.03 | 732.28 | 732.51 | 732.79 | 733.05 | 733.30 | 733.55 | 733.8I |
| 28.90 | 734.06 | 734.32 | 734.57 | 734.82 | 735.08 | 735.33 | 735.59 | 735.84 | 736.09 | 736.35 |
| 29.00 | 736.60 | 736.86 | 737.1 1 | 737.36 | 737.62 | 737.87 | 73S.13 | 73 S.38 | 738.63 | 738.89 |
| 29.10 | 739.14 | 739.40 | 739.65 | 739.90 | 740.16 | 740.41 | 740.67 | 740.92 | 741.17 | 741.43 |
| 29.20 | 74 I .68 | 741.94 | 742.19 | 742.44 | 742.70 | 742.95 | 743.21 | 743.46 | 743.71 | 743.97 |
| 29.30 | 744.22 | 744.48 | 744.73 | 744.98 | 745.24 | 745.49 | 745.75 | 746.00 | 746.25 | 746.51 |
| 29.40 | 746.76 | 747.02 | 747.27 | 747.52 | 747.78 | 748.03 | 748.29 | 748.54 | 748.79 | 749.05 |
| 29.50 | 749.30 | 749.56 | 749.8 I | 750.06 | 750.32 | 750.57 | 750.83 | 751.0S | 751.33 | 751.59 |
| 29.60 | 75 I .84 | 752.10 | 752.35 | 752.60 | 752.86 | 753.11 | 753.37 | 753.62 | 753.87 | 754.13 |
| 29.70 | 754.38 | 754.64 | 754.89 | 755. I4 | 755.40 | 755.65 | 755.91 | 756.16 | 756.41 | 756.67 |
| 29.80 | 756.92 | 757.18 | 757.43 | 757.68 | 757.94 | 75 S. 19 | 755.45 | 758.70 | 75S.95 | 759.21 |
| 29.90 | 759.46 | 759.72 | 759.97 | 760.22 | 760.48 | 760.73 | 760.99 | 761.24 | 761.49 | 761.75 |
| 30.00 | 762.00 | 762.26 | 762.51 | 762.76 | 763.02 | 763.27 | 763.53 | 763.78 | 764.03 | 764.29 |
| Proportional Parts |  | Inch. mm. | . 0.001 | 0.002 | 0.003 0. | $\begin{aligned} & 0.004 \\ & 0.102 \end{aligned}$ | $\begin{aligned} & 0.006 \\ & 0.152 \end{aligned}$ | $\begin{aligned} & 0.007 \\ & 0.178 \end{aligned}$ | 0.008 | $\begin{aligned} & 0.009 \\ & 0.229 \end{aligned}$ |
|  |  | 0.025 | 0.051 | 0.076 | 0.203 |  |  |  |  |

Table 9.
INCHES INTO MILLIMETERS.
1 inch $=25.40005 \mathrm{~mm}$.

| Inches. | . 00 | .01 | . 02 | . 03 | . 04 | 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm. | mm . | mm. | nm . | mm. | mm. | mmı. | тии. | mm. | mm. |
| 30.00 | 762.00 | 762.26 | 762.51 | 762.76 | 763.02 | 763.27 | 763.53 | 763.78 | 764.03 | 764.29 |
| 30.10 | 764.54 | 764.80 | 765.05 | 765.30 | 765.56 | 765.SI | 766.07 | 766.32 | 766.57 | 766.83 |
| 30.20 | 767.08 | 767.34 | 767.59 | 767.84 | 768. 10 | 768.35 | 768.6I | 768.86 | 769. I I | 769.37 |
| 30.30 | 769.62 | 769.88 | 770.13 | 770.38 | 770.64 | 770.89 | 771.15 | 771.40 | 771.65 | 771.91 |
| 30.40 | 772.16 | 772.42 | 772.67 | 772.92 | 773.1S | 773.43 | 773.69 | 773.94 | 774.19 | 774.45 |
| 30.50 | 77.4.70 | 774.96 | 775.2 I | 775.46 | 775.72 | 775.97 | 776.23 | 776.48 | 776.73 | 776.99 |
| 30.60 | 777.24 | 777.50 | 777.75 | 7ヶS.00 | 778.26 | 77 S .51 | 778.77 | 779.02 | 779.27 | 779.53 |
| 30.70 | 779.78 | 780.04 | 780.29 | 780.54 | 7 So .80 | 781.05 | ${ }_{7}^{781} .31$ | 781.56 | ${ }_{7 S 1}$ ISI | 782.07 |
| 30.80 | 782.32 | 782.58 | 782.83 | 783.08 | 783.34 | 783.59 | $7_{7} 8.85$ | 784.10 | 7S4.35 | 784.61 |
| 30.90 | 784.86 | 785.12 | 785.37 | 785.62 | 785.88 | 786.13 | 786.39 | 786.64 | 786.59 | 787.15 |
| 31.00 | 787.40 | 787.66 | 787.91 | 7SS.16 | 788.42 | 788.67 | 788.93 | 789.18 | 789.43 | 789.69 |
| 31.10 | 789.94 | 790.20 | 790.45 | 790.70 | 790.96 | 791.2I | 791.47 | 791.72 | 791.97 | 792.23 |
| 31.20 | 792.48 | 792.74 | 792.99 | 793.24 | 793.50 | 793.75 | 794.01 | 794.26 | 794.5 1 | 794.77 |
| 31.30 | 795.02 | 795.28 | 795.53 | 795.78 | 796.04 | 796.29 | 796.55 | 796.80 | 797.05 | 797.31 |
| 31.40 | 797.56 | 797.82 | 798.07 | 79 S. 32 | $79 \mathrm{~S} .5^{8}$ | 798.83 | 799.09 | 799.34 | 799.59 | 799.85 |
| 31.50 | Soo. Io | Soo. 36 | Soo. 61 | Soo. S6 | Soi. 12 | Soi. 37 | SoI. 63 | Soi. 88 | So2. 13 | So2. 39 |
| 31.60 | So2. 64 | So2.90 | So3. 15 | So3.40 | So3. 66 | So3.91 | So.4. 17 | So4.42 | So4. 67 | So4.93 |
| 31.70 | So5.IS | 805.44 | 805.69 | So5.94 | So6. 20 | So6.45 | So6.71 | So6.96 | So7.21 | So7. 47 |
| 31.80 | So7.72 | So7.9S | So8. 23 | SoS. 48 | SoS. 74 | SoS. 99 | 809. 25 | So9.50 | Sog. 75 | Sio.or |
| 31.90 | Sio. 26 | SIo. 52 | 810.77 | Sili. 02 | SII. 28 | 8II. 53 | 8ir. 79 | Si2.04 | SI2.29 | SI 2.55 |
| 32.00 | SI2.So |  |  |  |  |  |  |  |  |  |
| Proportional Parts |  | S. $\begin{aligned} & \text { Inch } \\ & \mathrm{mm} .\end{aligned}$ | 0.001 | 0.002 | 0.0030 | $4 \quad 0.005$ | 0.006 | 0.007 | $\begin{aligned} & 0.008 \\ & 0.203 \end{aligned}$ | $\begin{aligned} & 0.009 \\ & 0.229 \end{aligned}$ |
|  |  | 0.025 | 0.051 | 0.076 | $\begin{aligned} & 0.074 \\ & 0.102 \end{aligned}$ | $7 \quad 0.152$ | 0.178 |  |  |

Smithsonian Tableg

MILLIMETERS INTO INCHES.
$1 \mathrm{~mm} .=0.03937$ inch.

| Millimeters. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 0 | 0.0000 | 0.0394 | 0.0787 | 0.1181 | 0.1575 | 0.196S | 0.2362 | 0.2756 | 0.3150 | 0.3543 |
| 10 | 0.3937 | 0.4331 | 0.4724 | 0.5118 | 0.5512 | 0.5906 | 0.6299 | 0.6693 | 0.7087 | 0.7480 |
| 20 | 0.7874 | $0.326 S$ | 0.8661 | 0.9055 | 0.9449 | 0.9842 | 1.0236 | 1.0630 | 1.1024 | 1.1417 |
| 30 | I.ISII | I. 2205 | 1.2598 | 1.2992 | 1.3386 | 1.3780 | 1.4173 | 1.4567 | I. 4961 | I. 5354 |
| 40 | I. 5748 | 1.6142 | 1. 6535 | 1.6929 | 1.7323 | I.7716 | I. Sifo | 1.8504 | 1.8898 | I.929I |
| 50 | 1.9685 | 2.0079 | 2.0472 | 2.0866 | 2.1260 | 2.1654 | 2.2047 | 2.2441 | 2.2835 | 2.3228 |
| 60 | 2.3622 | 2.4016 | 2.4409 | 2.4803 | 2.5197 | 2.5590 | 2.5984 | 2.6378 | 2.6772 | 2.7165 |
| 70 | 2.7559 | 2.7953 | 2.8346 | 2.8740 | 2.9134 | 2.9528 | 2.992 I | 3.0315 | 3.0709 | 3.1102 |
| So | 3.1496 | 3.1890 | 3.2283 | 3.2677 | 3.3071 | 3.3464 | 3.3 S5S | 3.4252 | 3.4646 | 3.5039 |
| 90 | 3.5433 | 3.5828 | 3.6220 | 3.6614 | 3.7008 | 3.7402 | 3.7795 | 3.8189 | 3.8583 | 3.8976 |
| 100 | 3.9370 | 3.9764 | 4.0157 | 4.0551 | 4.0945 | 4.1338 | 4.1732 | 4.2126 | 4.2520 | 4.2913 |
| 110 | 4.3307 | 4.3701 | 4.4094 | 4.4488 | 4.4882 | 4.5276 | 4.5669 | 4.6063 | 4.6457 | 4.6850 |
| 120 | 4.7244 | 4.7638 | 4.8031 | 4.8425 | 4.88 I9 | 4.92 I2 | 4.9606 | 5.0000 | 5.0394 | 5.0787 |
| 130 | 5.1181 | 5.1575 | 5.1968 | 5.2362 | 5.2756 | 5.3150 | 5.3543 | 5.3937 | 5.433 I | 5.4724 |
| 140 | 5.5118 | 5.5512 | 5.5905 | 5.6299 | 5.6693 | 5.7086 | 5.7480 | 5.7874 | 5.8268 | 5.8661 |
| 150 | 5.9055 | 5.9449 | 5.9842 | 6.0236 | 6.0630 | 6.1024 | 6.1417 | 6.1811 | 6.2205 | 6.2598 |
| 160 | 6.2992 | 6.3386 | 6.3779 | 6.4173 | 6.4567 | 6.4960 | 6.5354 | 6.5748 | 6.6142 | 6.6535 |
| 170 | 6.6929 | 6.7323 | 6.7716 | 6.8110 | 6.8504 | 6.8898 | 6.9291 | 6.9685 | 7.0079 | 7.0472 |
| ISo | 7.0866 | 7.1260 | 7.1653 | 7.2047 | $7.244{ }^{1}$ | 7.2834 | 7.3228 | 7.3622 | 7.4016 | 7.4409 |
| 190 | 7.48 o 3 | 7.5197 | 7.5590 | 7.5984 | 7.6378 | 7.6772 | 7.7165 | 7.7559 | 7.7953 | 7.8346 |
| 200 | 7.8740 | 7.9134 | 7.9527 | 7.9921 | 8.0315 | S.0708 | 8.1102 | 8.1496 | 8.1890 | 8.2283 |
| 210 | 8.2677 | 8.3071 | S. 3464 | 8.3858 | 8.4252 | 8.4646 | 8.5039 | 8.5433 | 8.5827 | 8.6220 |
| 220 | 8.6614 | 8.7008 | 8.7401 | 8.7795 | 8.8189 | 8.8582 | 8.5976 | 8.9370 | 8.9764 | 9.0157 |
| 230 | 9.0551 | 9.0945 | 9.1338 | 9.1732 | 9.2126 | 9.2520 | 9.2913 | 9.3307 | 9.3701 | 9.4094 |
| 240 | 9.4488 | 9.4882 | 9.5275 | 9.5669 | 9.6063 | 9.6456 | 9.6850 | 9.7244 | 9.7638 | 9.8031 |
| 250 | 9.8425 | 9.8819 | 9.9212 | 9.9606 | 10.0000 | 10.0394 | 10.0787 | 10.118i | 10.1575 | 10.1968 |
| 260 | 10.2362 | 10.2756 | I0.3549 | 10.3543 | IO.3937 | 10.4330 | 10.4724 | 10.5118 | 10.5512 | 10.5905 |
| 270 | 10.6299 | 10.6693 | 10.7086 | 10.7480 | 10.7874 | 10.8268 | 10.8661 | 10.9055 | 10.9449 | 10.9842 |
| 280 | I 1.0236 | I I . 0630 | II.1023 | II.1417 | II.I8It | II 1.2204 | I 1.2598 | II. 2992 | I 1.3338 | I I 1.3779 |
| 290 | II. 4173 | II 4.4568 | II 14960 | I I. 5354 | I 1.5748 | I 1.6142 | I 1.6535 | I 1.6929 | 11.7323 | I 1.7716 |
| 300 | If.8110 | II. 8504 | II. 8897 | I 1.9291 | I I. 9685 | I2.0078 | 12.0472 | 12.0866 | 12.1260 | 12.1653 |
| 310 | 12.2047 | 12.244 I | 12.2834 | 12.3228 | I2.3622 | 12.4016 | I2.4409 | 12.4803 | 12.5197 | 12.5590 |
| 320 | 12.5984 | I2.637S | I2.6771 | 12.7165 | I2.7559 | I2.7952 | 12.8346 | 12.8740 | 12.9134 | 12.9527 |
| 330 | 12.992 I | 13.0315 | 13.0708 | 13.1102 | 13.1496 | I3.1890 | 13.2283 | I 3.2677 | 13.3071 | I3.3464 |
| $34{ }^{\circ}$ | 13.3858 | I 3.4252 | I3.4645 | I 3.5039 | I 3.5433 | I 3.5826 | 13.6220 | 13.6614 | 13.7008 | 13.7401 |
| 350 | I 3.7795 | 13.8189 | 13.8582 | 13.8976 | 13.9370 | I 3.9764 | I4.0157 | 14.0551 | 14.0945 | 14.1338 |
| 360 | I4.1732 | I4.2126 | I4.2519 | 14.2913 | 14.3307 | 14.3700 | 14.4094 | 14.4488 | 14.4882 | 14.5275 |
| 370 | I4.5669 | 14.6063 | 14.6456 | 146850 | 14.7244 | 14.7638 | 14.8031 | I4.8425 | I4.8819 | 14.9212 |
| 380 | I 4.9606 | 15.0000 | 15.0393 | 15.0787 | 15.1181 | I5.1574 | 15.1968 | 15.2362 | I5.2756 | 15.3149 |
| 390 | I 5.3543 | I5.3937 | 15.4330 | I 5.4724 | 15.5118 | 15.55 12 | I5.5905 | I 5.6299 | 15.6693 | 15.7086 |
| 400 | I 5.7480 | I5.7874 | 15.8267 | I 5.8661 | 15.9055 | I5.9448 | 15.9842 | 16.0236 | 16.0630 | 16.1023 |
|  | Tenths of a millimeter. |  |  |  |  | Hundredths of a millimeter. |  |  |  |  |
|  | mm. |  | mm . |  | Inch. <br> 0.0236 | min. <br> 0.01 | Inch. | $\mathrm{mm} .$ |  | Inch. 0.0024 |
|  | . 2 | 0.0039.0079 |  | 0.6 .7 | . $0 \times 76$ | . 02 | .0008 |  | . 07 | . 0028 |
|  | $\cdot 3$ | . 0118 |  | . 5 | . 0315 | . 03 | .0012 |  | . 08 | .no3r |
|  | . 4 | .0157.0197 |  | $\begin{array}{r} .9 \\ 1.0 \end{array}$ | . 0354 | . 04 | . 0016 |  | . 09 | .0035 |
|  | . 5 |  |  | . 0394 | . 05 | . 10 |  |  | . 0039 |

Smithbonian Tables.
rable 10.
MILLIMETERS INTO INCHES.
$1 \mathrm{~mm} .=0.03937$ inch.

| Millimeters | . 0 | .1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Iuches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 400 | 15.748 | 15.752 | 15.756 | 15.760 | 15.764 | 15.768 | 15.772 | 15.776 | 15.779 | $15.7 \mathrm{~S}_{3}$ |
| 401 | 15.787 | 15.791 | 15.795 | I5.799 | 15.803 | 15.807 | 15.81 I | I5.815 | 15.819 | ${ }^{1} 5.823$ |
| 402 | 15.827 | 15.831 | 15.835 | 15.839 | 15.842 | 15.846 | 15.550 | I 5.854 | 15.858 | 15.852 |
| 403 | 15.866 | 15.870 | 15.874 | 15.878 | 15.882 | I5.8S6 | 15.590 | 15.894 | I 5.898 | 15.902 |
| 404 | 15.905 | 15.909 | 15.913 | 15.917 | 15.921 | I5.925 | 15.929 | 15.933 | 15.937 | 15.94I |
| 405 | 15.9.45 | I 5.949 | 15.953 | I5.957 | 15.961 | 15.965 | 15.968 | 15.972 | I 5.976 | 15.980 |
| 406 | 15.984 | 15.988 | 15.992 | I 5.996 | 16.000 | 16.004 | $16.00 S$ | 16.012 | 16.016 | 16.020 |
| 407 | 16.024 | 16.028 | 16.031 | 16.035 | 16.039 | 16.043 | 16.047 | 16.051 | I6.055 | 16.059 |
| 408 | 16.063 | 16.067 | 16.07 I | 16.075 | 16.079 | 16.083 | 16.087 | 16.091 | 16.094 | 16.098 |
| 409 | 16.102 | 16.106 | 16.110 | 16.114 | 16.11S | I6. 122 | 16.126 | 16.130 | 16.134 | 16.13S |
| 410 | 16.142 | 16.146 | 16.150 | 16.154 | 16.157 | 16.16I | 16.165 | 16.169 | 16.173 | 16.177 |
| 4 II | 16.181 | 16.185 | 16.189 | 16.193 | 16.197 | 16.201 | I6.205 | 16.209 | 16.213 | 16.217 |
| 412 | 16.220 | 16.224 | 16.228 | 16.232 | 16.236 | 16.240 | 16.244 | 16.248 | 16.252 | 16.256 |
| 413 | 16.260 | 16.264 | 16.268 | 16.272 | 16.276 | 16.279 | 16.283 | 16.257 | 16.291 | 16.295 |
| 414 | 16.299 | 16.303 | 16.307 | 16.311 | 16.315 | 16.319 | 16.323 | 16.327 | 16.33 I | 16.335 |
| 415 | 16.339 | 16.342 | 16.346 | 16.350 | 16.354 | 16.358 | 16.362 | 16.366 | 16.370 | 16.374 |
| 416 | 16.378 | 16.382 | 16.386 | 16.390 | 16.394 | 16.398 | 16.402 | 16.405 | 16.409 | 16.413 |
| 417 | 16.417 | 16.42 I | 16.425 | 16.429 | 16.433 | 16.437 | 16.44 I | 16.445 | 16.449 | 16.453 |
| 418 | 16.457 | 16.461 | 16.465 | 16.468 | 16.472 | 16.476 | 16.480 | 16.484 | 16.458 | 16.492 |
| 419 | I6.496 | 16.500 | 16.504 | 16.508 | 16.512 | 16.516 | 16.520 | 16.524 | 16.528 | 16.53 I |
| 420 | I6.535 | 16.539 | 16.543 | 16.547 | 16.55I | 16.555 | 16.559 | 16.563 | 16.567 | 16.571 |
| 42 I | 16.575 | 16.579 | 16.583 | 16.587 | I6.591 | 16.594 | 16.598 | 16.602 | 16.606 | 16.610 |
| 422 | 16.614 | 16.61S | 16.622 | 16.626 | 16.630 | 16.634 | 16.638 | 16.642 | 16.646 | 16.650 |
| 423 | 16.654 | 16.657 | 16.661 | 16.665 | 16.669 | 16.673 | 16.677 | 16.68I | 16.685 | 16.689 |
| 424 | 16.693 | 16.697 | 16.701 | 16.705 | 16.709 | 16.713 | 16.717 | 16.720 | 16.724 | 16.728 |
| 425 | 16.732 | 16.736 | 16.740 | 16.744 | 16.748 | 16.752 | 16.756 | 16.760 | I6.764 | 16.768 |
| 426 | 16.772 | 16.776 | 16.779 | 16.783 | 16.787 | 16.791 | 16.795 | 16.799 | 16.503 | 16.807 |
| 427 | 16.811 | $16 . \mathrm{S}_{15}$ | 16.519 | 16.823 | 16.827 | 16.83 I | 16.835 | 16.839 | 16.842 | 16.846 |
| 428 | 16.550 | 16.854 | 16.858 | 16.862 | 16.866 | 16.870 | 16.874 | 16.578 | 16.882 | 16.856 |
| 429 | 16.590 | 16.89 .4 | 16.898 | 16.902 | 16.905 | 16.909 | 16.913 | 16.917 | 16.921 | 16.925 |
| 430 | 16.929 | 16.933 | 16.937 | 16.94 I | 16.945 | 16.949 | 16.953 | 16.957 | 16.961 | 16.965 |
| 431 | 16.968 | 16.972 | 16.976 | 16.980 | 16.954 | 16.958 | 16.992 | 16.996 | 17.000 | 17.004 |
| 432 | 17.00 S | 17.012 | 17.016 | 17.020 | 17.024 | 17.028 | 17.031 | 17.035 | 17.039 | 17.043 |
| 433 | 17.047 | 17.051 | 17.055 | 17.059 | 17.063 | 17.067 | 17.071 | 17.075 | 17.079 | 17.083 |
| 434 | 17.087 | 17.091 | 17.094 | 17.098 | 17.102 | 17.106 | 17.110 | 17.114 | 17.11S | 17.122 |
| 435 | 17.126 | 17.130 | 17.134 | 17.138 | 17.142 | 17.146 | 17.150 | 17.154 | 17.157 | 17.161 |
| 436 | 17.165 | 17.169 | 17.173 | \%7.177 | 17.151 | 17.185 | 17.189 | 17.193 | 17.197 | 17.201 |
| 437 | 17.205 | 17.209 | 17.213 | 17.217 | 17.220 | 17.224 | 17.228 | 17.232 | I 7.236. | 17.240 |
| 438 | 17.244 | 17.248 | 17.252 | 17.256 | 17.260 | 17.264 | 17.268 | 17.272 | 17.276 | 17.279 |
| 439 | 17.283 | 17.287 | 17.291 | 17.295 | 17.299 | 17.303 | 17.307 | 17.311 | 17.315 | 17.319 |
| 440 | 17.323 | 17.327 | I 7.33I | 17.335 | 17.339 | 17.342 | 17.346 | 17.350 | 17.354 | 17.358 |
| 441 | 17.362 | 17.366 | 17.370 | 17.374 | 17.378 | 17.382 | 17.356 | 17.390 | 17.394 | 17.398 |
| 442 | 17.402 | 17.405 | 17.409 | 17.413 | 17.417 | 17.42 I | 17.425 | 17.429 | 17.433 | 17.437 |
| 443 | 17.44 I | 17.445 | 17.449 | 17.453 | 17.457 | 17.461 | 17.465 | 17.468 | 17.472 | 17.476 |
| 444 | 17.450 | 17.484 | 17.488 | I7.492 | 17.496 | 17.500 | 17.504 | 17.50 S | 17.512 | 17.516 |
| 445 | 17.520 | 17.524 | 17.528 | 17.531 | 17.535 | 17.539 | 17.543 | 17.547 | I 7.55 I | 17.555 |
| 446 | 17.559 | 17.563 | 17.567 | 17.571 | 17.575 | 17.579 | 17.5 ${ }^{1} 3$ | 17.587 | 17.591 | 17.594 |
| 447 | 17.59 S | 17.602 | 17.606 | 17.610 | 17.614 | 17.618 | 17.622 | 17.626 | 17.630 | 17.634 |
| 448 | 17.6 .35 | 17.642 | 17.646 | 17.650 | 17.654 | 17.657 | 17.661 | 17.665 | 17.669 | 17.673 |
| 449 | 17.677 | 17.681 | 17.685 | 17.689 | 17.693 | 17.697 | 17.701 | 17.705 | 17.709 | 17.713 |
| 450 | I7.717 | 17.720 | 17.724 | 17.728 | 17.732 | 17.736 | 17.740 | 17.744 | 17.748 | 17.752 |

MILLIMETERS INTO INCHES.
$1 \mathrm{~mm} .=0.03937$ inch.

| Millimeters. | . 0 | . 1 | . 2 | . 3 | 4 | . 5 | 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 450 | 17.717 | 17.720 | I7.724 | 17.728 | 17.732 | 17.736 | 17.740 | 17.744 | 17.748 | I7.752 |
| 45 I | 17.756 | 17.760 | 17.764 | 17.768 | 17.772 | 17.776 | 17.779 | 17.783 | 17.787 | I7.791 |
| 452 | 17.795 | 17.799 | 17.803 | 17.807 | 17.8II | 17.815 | 17.819 | 17.823 | 17.827 | 17.83I |
| 453 | 17.835 | 17.839 | 17.842 | 17.846 | 17.850 | 17.854 | 17.858 | 17.862 | 17.866 | 17.870 |
| 454 | 17.874 | 17.878 | 17.882 | 17.886 | 17.890 | 17.894 | 17.898 | 17.902 | 17.905 | 17.909 |
| 455 | 17.913 | 17.917 | 17.921 | 17.925 | 17.929 | 17.933 | 17.937 | 17.941 | 17.945 | 17.949 |
| 456 | 17.953 | 17.957 | 17.961 | 17.965 | 17.968 | 17.972 | 17.976 | 17.980 | 17.984 | 17.988 |
| 457 | 17.992 | 17.996 | 18.000 | 18.004 | 18.008 | IS.OI 2 | 18.016 | 18.020 | 18.024 | 18.028 |
| 458 | I8.03I | 18.035 | 18.039 | 18.043 | 18.047 | 18.051 | 18.055 | 18.059 | 18.063 | 18.067 |
| 459 | 18.071 | 18.075 | 18.079 | 18.083 | 18.087 | I8.09I | I8.094 | 18.098 | IS. 102 | 18.106 |
| 460 | I8.110 | 18.114 | 18.118 | 18.122 | 18.126 | 18. 130 | 18. 134 | 18.138 | 18.142 | 18.146 |
| 461 | 18.150 | 18.154 | IS. 157 | 18.161 | IS. 165 | I8.169 | IS. 173 | IS. 177 | IS.18I | I8.185 |
| 462 | IS.IS9 | 18.193 | 18.197 | 18.201 | 18.205 | 18.209 | 18.213 | 18.216 | 18.220 | IS. 224 |
| 463 | 18.228 | 18.232 | 18.236 | 18.240 | 18.244 | I8.248 | 18.252 | 18.256 | I8.260 | I8.264 |
| 464 | 18.268 | 18.272 | 18.276 | 18.279 | 18.283 | 18.287 | 18.291 | I8.295 | I8. 299 | 18.303 |
| 455 | 18.307 | I8.3II | I8.315 | 18.319 | 18.323 | I8.327 | 18.33I | 18.335 | 18.339 | 18.342 |
| 466 | 18.346 | 18.350 | 18.354 | 18.358 | I8. 362 | IS. 366 | 18.370 | 18.374 | 18.378 | 18.382 |
| 467 | I8.386 | 18.390 | IS. 394 | 18.39 S | IS. 402 | 18.405 | I8.409 | 18.413 | 18.417 | 18.421 |
| 468 | 18.425 | 18.429 | 18.433 | IS.437 | I8.4.4I | 18.445 | I8.449 | 18.453 | 18.457 | IS.46I |
| 469 | IS.465 | 18.468 | 18.472 | 18.476 | I8.480 | 18.484 | 18.488 | 18.492 | I8.496 | 18.500 |
| 470 | I 8.504 | I 8.508 | 18.512 | 18.516 | 18.520 | I8.524 | 18.528 | IS.53I | 18.535 | I 8.539 |
| 471 | 18.543 | 18.547 | 18.551 | 18.555 | IS. 559 | I8.563 | 18.567 | 18.571 | 18.575 | 18.579 |
| 472 | I8.583 | 18.587 | 18.591 | 18.594 | I8.598 | 18.602 | 18.606 | 18.610 | 18.614 | 18.618 |
| 473 | 18.622 | 18.626 | 18.630 | I8.634 | IS.638 | 18.642 | 18.646 | 18.650 | 18.654 | 18.657 |
| 474 | 18.661 | 18.665 | 18.669 | IS.673 | 18.677 | I8.68I | 18.685 | 18.689 | 18.693 | 18.697 |
| 475 | 18.701 | 18.705 | 18.709 | 18.713 | 18.716 | 18.720 | IS. 724 | 18.728 | 18.732 | 18.736 |
| 476 | 18.740 | 18.744 | 18.748 | 18.752 | 18.756 | 18.760 | 18.764 | 18.768 | 18.772 | 18.776 |
| 477 | IS.779 | 18.783 | 18.787 | 18.791 | I8.795 | 18.799 | 18.803 | 18.807 | 18.81I | 18.815 |
| 478 | 18.819 | 18.823 | 18.827 | 18.83 I | 18.835 | 18.839 | 18.842 | I8.846 | 18.850 | 18.854 |
| 479 | I 8.858 | 18.862 | I8.866 | 18.870 | 18.874 | 18.878 | 18.882 | 18.886 | 18.890 | 18.894 |
| 480 | I 8.898 | 18.902 | I8.905 | 18.909 | 18.913 | 18.917 | 18.921 | 18.925 | I8.929 | 18.933 |
| 481 | 18.937 | 18.941 | I8.945 | 18.949 | IS. 953 | 18.957 | 18.961 | 18.965 | 18.968 | 18.972 |
| 482 | 18.976 | 18.980 | 18.984 | 18.988 | 18.992 | 18.996 | 19.000 | 19.004 | 19.008 | 19.012 |
| 483 | 19.016 | 19.020 | 19.024 | 19.028 | 19.03 I | 19.035 | 19.039 | 19.043 | 19.047 | 19.051 |
| 484 | 19.055 | 19.059 | 19.063 | 19.067 | 19.071 | 19.075 | 19.079 | 19.083 | 19.087 | 19.09I |
| 485 | 19.094 | 19.098 | 19.102 | 19.106 | 19.110 | 19.114 | 19.118 | 19. 122 | 19.126 | 19.130 |
| 486 | 19. I34 | 19.138 | 19.142 | 19.146 | 19.150 | 19.154 | 19.157 | 19.161 | 19.165 | 19.169 |
| 487 | 19.173 | 19.177 | 19.181 | 19.185 | 19.189 | 19.193 | 19. 197 | 19.201 | 19.205 | 19.209 |
| 488 | 19.213 | I9.216 | 19.220 | 19.224 | 19.228 | 19.232 | 19.236 | 19.240 | 19.244 | 19.248 |
| 489 | 19.252 | 19.256 | 19.260 | 19.264 | 19.268 | 19.272 | 19.276 | 19.279 | 19.283 | 19.287 |
| 490 | 19.291 | 19.295 | 19.299 | 19.303 | 19.307 | 19.3II | 19.315 | 19.319 | 19.323 | 19.327 |
| 491 | 19.331 | 19.335 | 19.339 | 19.342 | 19.346 | 19.350 | 19.354 | 19.358 | 19.362 | 19.366 |
| 492 | 19.370 | 19.374 | 19.378 | 19.382 | 19.386 | 19.390 | 19.394 | 19.398 | 19.402 | 19.405 |
| 493 | 19.409 | 19.413 | 19.417 | 19.421 | 19.425 | 19.429 | 19.433 | 19.437 | 19.441 | 19.445 |
| 494 | 19.449 | I9.453 | 19.457 | 19.46I | 19.465 | 19.468 | 19.472 | 19.476 | 19.480 | 19.484 |
| 495 | 19.488 | 19.492 | 19.496 | 19.500 | 19.504 | 19.508 | 19.512 | 19.516 | 19.520 | 19.524 |
| 496 | 19.528 | 19.531 | 19.535 | 19.539 | 19.543 | 19.547 | 19.55 I | 19.555 | 19.559 | 19.563 |
| 497 | 19.567 | 19.57 I | 19.575 | 19.579 | 19.583 | 19.587 | 19.591 | 19.594 | 19.598 | 19.602 |
| 498 | 19.606 | 19.610 | 19.614 | 19.618 | 19.622 | 19.626 | 19.630 | 19.634 | 19.638 | 19.642 |
| 499 | 19.646 | 19.650 | 19.654 | 19.657 | 19.661 | 19.665 | 19.669 | 19.673 | 19.677 | 19.68I |
| 500 | 19.685 | 19.689 | 19.693 | 19.697 | 19.701 | 19.705 | 19.709 | 19.713 | 19.716 | 19.720 |

Bmithgonian Tableg.
$1 \mathrm{~mm} .=0.03937$ inch.

| Milli- | 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 500 | 19.685 | 19.689 | 19.693 | 19.697 | 19.701 | 19.705 | 19.709 | 19.713 | 19.716 | 19.720 |
| 501 | 19.724 | 19.728 | 19.732 | 19.736 | 19.740 | 19.744 | 19.748 | 19.752 | 19.756 | 19.760 |
| 502 | 19.764 | 19.768 | 19.772 | 19.776 | 19.779 | 19.783 | 19.787 | 19.791 | 19.795 | 19.799 |
| 503 | 19.803 | 19.507 | 19.811 | 19.815 | 19.819 | 19.823 | 19.827 | 19.83 I | 19.835 | 19.839 |
| 504 | 19.842 | 19.846 | 19.850 | 19.854 | 19.858 | 19.862 | 19.866 | 19.870 | 19.874 | 19.878 |
| 505 | 19.882 | 19.886 | 19.890 | 19.894 | 19.898 | 19.902 | 19.905 | 19.909 | 19.913 | 19.917 |
| 506 | 19.92 I | 19.925 | 19.929 | 19.933 | 19.937 | 19.941 | 19.945 | 19.949 | 19.953 | 19.957 |
| 507 | 19.961 | 19.965 | 19.968 | 19.972 | 19.976 | 19.980 | 19.984 | 19.988 | 19.992 | 19.996 |
| 508 | 20.000 | 20.004 | 20.008 | 20.012 | 20.016 | 20.025 | 20.024 | 20.028 | 20.031 | 20.035 |
| 509 | 20.039 | 20.043 | 20.047 | 20.051 | 20.055 | 20.059 | 20.063 | 20.067 | 20.071 | 20.075 |
| 510 | 20.079 | 20.083 | 20.087 | 20.091 | 20.094 | 20.098 | 20.102 | 20.106 | 20.110 | 20.114 |
| 5 II | 20.11S | 20. 122 | 20.126 | 20.130 | 20.134 | 20.138 | 20.142 | 20.146 | 20.150 | 20.154 |
| 512 | 20.157 | 20.161 | 20.165 | 20.169 | 20.173 | 20.177 | 20.18I | 20.185 | 20.189 | 20.193 |
| 513 | 20.197 | 20.201 | 20.205 | 20.209 | 20.213 | 20.216 | 20.220 | 20.22 .4 | 20.22 S | 20.232 |
| 514 | 20.236 | 20.240 | 20.244 | 20.248 | 20.252 | 20.256 | 20.260 | 20.264 | 20.268 | 20.272 |
| 515 | 20.276 | 20.279 | 20.283 | 20.287 | 20.291 | 20.295 | 20.299 | 20.303 | 20.307 | 20.311 |
| 516 | 20.315 | 20.319 | 20.323 | 20.327 | 20.331 | 20.335 | 20.339 | 20.342 | 20.346 | 20.350 |
| 517 | 20.354 | 20.358 | 20362 | 20.366 | 20.370 | 20.374 | 20.37 S | 20.382 | 20.386 | 20.390 |
| 518 | 20.394 | 20.398 | 20.402 | 20.405 | 20.409 | 20.413 | 20.417 | 20.42 I | 20.425 | 20.429 |
| 519 | 20.433 | 20.437 | 20.441 | 20.445 | 20.449 | 20.453 | 20.457 | 20.46 I | 20.465 | 20.468 |
| 520 | 20.472 | 20.476 | 20.4So | 20.484 | 20.488 | 20.492 | 20.496 | 20.500 | 20.504 | 20.508 |
| 52 I | 20.512 | 20.516 | 20.520 | 20.524 | 20.528 | 20.531 | 20.535 | 20.539 | 20.543 | 20.547 |
| 522 | 20.55 I | 20.555 | 20.559 | 20.563 | 20.567 | 20.571 | 20.575 | 20.579 | 20.583 | 20.587 |
| 523 | 20.591 | 20.594 | 20.598 | 20.602 | 20.606 | 20.610 | 20.614 | 20.618 | 20.622 | 20.626 |
| 52.4 | 20.630 | 20.634 | 20.638 | 20.642 | 20.646 | 20.650 | 20.654 | 20.657 | 20.661 | 20.665 |
| 525 | 20.669 | 20.673 | 20.677 | 20.68I | 20.685 | 20.689 | 20.693 | 20.697 | 20.701 | 20.705 |
| 526 | 20.709 | 20.713 | 20.716 | 20.720 | 20.724 | 20.72 S | 20.732 | 20.736 | 20.740 | 20.744 |
| 527 | 20.748 | 20.752 | 20.756 | 20.760 | 20.764 | 20.768 | 20.772 | 20.776 | 20.779 | 20.783 |
| 528 | 20.787 | 20.791 | 20.795 | 20.799 | 20.803 | 20.807 | 20.811 | 20.815 | 20.819 | 20.823 |
| 529 | 20.827 | 20.831 | 20.835 | 20.839 | 20.842 | 20.846 | 20.850 | 20.854 | 20.858 | 20.862 |
| 530 | 20.866 | 20.870 | 20.874 | 20.878 | $20.8 S_{2}$ | 20.856 | 20.590 | 20.S94 | 20.898 | 20.902 |
| 531 | 20.905 | 20.909 | 20.913 | 20.917 | 20.92 I | 20.925 | 20.929 | 20.933 | 20.937 | 20.941 |
| 532 | 20.945 | 20.949 | 20.953 | 20.957 | 20.961 | 20.965 | 20.968 | 20.972 | 20.976 | 20.980 |
| 533 | 20.984 | 20.985 | 20.992 | 20.996 | 21.000 | 21.004 | 21.008 | 21.012 | 21.016 | 21.020 |
| 534 | 21.024 | 21.028 | 21.03 I | 21.035 | 21.039 | 21.043 | 21.047 | 21.051 | 21.055 | 21.059 |
| 535 | 21.063 | 21.067 | 21.071 | 21.075 | 21.079 | $2 \mathrm{I} .08_{3}$ | 21.087 | 21.091 | 21.094 | 21.098 |
| 536 | 21.102 | 21.106 | 21.110 | 21.114 | 21.118 | 21.122 | 21.126 | 21.130 | 21.134 | 21.138 |
| 5.37 | 21.142 | 21.146 | 21.150 | 21.154 | 21.157 | 21.16I | 21.165 | 21.169 | 21.173 | 21.177 |
| 538 | 2I.ISI | 21.185 | 21.189 | 21.193 | 21.197 | 21.201 | 21.205 | 21.209 | 21.213 | 21.216 |
| 539 | 21.220 | 21.224 | 21.22 S | 21.232 | 21.236 | 21.240 | 21.244 | 21.248 | 21.252 | 21.256 |
| 540 | 21.260 | 21.264 | 21.268 | 21.272 | 21.276 | 21.279 | 21.283 | 21.287 | 21.291 | 21.295 |
| 541 | 21.299 | 21.303 | 21.307 | 21.3II | 21.315 | 21.319 | 21.323 | 21.327 | 21.331 | 21.335 |
| 542 | 21.339 | 21.342 | 21.346 | 21.350 | 21.354 | 21.358 | 21.362 | 21.366 | 21.370 | 21.374 |
| 543 | $2 \mathrm{1.378}$ | 21.382 | 21.386 | 21.390 | 21.394 | 21.398 | 21.402 | 21.405 | 21.409 | 21.413 |
| 544 | 21.417 | 21.42 I | 21.425 | 21.429 | 21.433 | 21.437 | 21.44 I | 21.445 | 21.449 | 21.453 |
| 545 | 21.457 | 21.461 | 21.465 | 21.468 | 21.472 | 21.476 | 21.48o | 21.484 | 21.488 | 21. 492 |
| 546 | 21.496 | 21.500 | 21.504 | 21.508 | 21.512 | 21.516 | 21.520 | 21.524 | 21. 52 S | 21.53 I |
| 547 | 2 I .535 | 21.539 | 21.543 | 21.547 | 21.551 | 21.555 | 2 I .559 | 21.563 | 21.567 | 21.571 |
| $54{ }^{8}$ | 21.575 | 21.579 | 21.583 | 21.587 | 21.591 | 21.59 .4 | 21.598 | 21.602 | 21.606 | 21.610 |
| 549 | 21.614 | 21.618 | 21.622 | 21.626 | 21.630 | 21.634 | 21.638 | 21.642 | 21.646 | 21.650 |
| 550 | 21.654 | 21.657 | 21.661 | 21.665 | 21.66c | 21.673 | 21.677 | 21.681 | 21.685 | 21.689 |

MILLIMETERS INTO INCHES.
$\mathrm{I} \mathrm{mm} .=0.03937$ inch.

| Milli- | 0 | . 1 | . 2 | 3 | .4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. In | Inches. I | Iuches. In | Inches. In | Inches. In | Inches. I | Inches. In | Inches. I | Inches. In | Inches. |
| 550 | 21.6542 | 21.6572 | 21.6612 | 21.6652 | 21.6692 | 21.673 | 21.6772 | 21.681 | 21.685 | 21.689 |
| 551 | 21.6932 | 21.6972 | 21.701 | 21.7052 | 21.7092 | 21.713 | $21.716^{2}$ | 21.720 | 21.724 | 21.7 |
| 552 | 21.732 | 21.7362 | 21.7402 | 21.744 | 21.748 | 21.752 | 21.756 | 21.7 | 21 |  |
| 553 | 21.772 | 21.776 | 21.779 | 21.783 | 21.787 | 21.791 | 21.795 | 21.799 21.839 |  | I. 846 |
| 554 | 21. SII $^{2}$ | 21.815 | 21.819 | 21.823 | $21.827{ }^{2}$ | 21.831 | 21.035 | 21.839 |  | 6 |
| 555 | 21.850 | 21.854 | 21.858 | 21.862 | 21.866 | 21.870 | 21.874 | 21.878 | 21.882 | 21.886 |
| 556 | 21.890 | 21.8942 | 21.898 | 21.902 | 21.905 | 21.909 | 21.9132 | 21.917 | 21.921 | 21.925 |
| 557 | 21.9292 | 21.933 | 21.9372 | 21.941 | 21.945 | 21.949 | 21.953 | 21957 | 21.961 |  |
| 558 | 21.968 | 21.972 | 21.976 | 21.980 | 21.984 | 21.988 | 21.992 | 21.996 | 22.000 22.039 | 22.004 22.043 |
| 559 | 22.008 | 22.012 | 22.016 | 22.020 | 22.024 | 22.028 | 22.031 | 22.0 | 22. |  |
| 560 | 22.047 | 22.051 | 22.055 | 22.059 | 22.063 | 22.067 | 22.071 | 22.075 | 22.079 | 22.083 |
| 561 | 22.087 | 22.091 | 22.094 | 22.098 | 22.102 | 22. 106 | 22.110 | 22.114 | 22.118 |  |
| 562 | 22.126 | 22.130 | 22.134 | 22.138 | 22.142 | 22.146 | 22.150 | 22 |  | 22.201 |
| 563 | 22.165 | 22.169 | 22.173 | 22.177 22.216 | 22.151 22.220 | 22.155 22.224 | 22.228 | 22.232 | 22.236 | 22.240 |
| 564 | 22.205 | 22.209 | 2 |  |  |  |  |  |  |  |
| 565 | 22.244 | 22.248 | 22.252 | 22.256 | 22.260 | 22.264 | 22.268 | 22.272 | 22.276 | 22.279 22.319 |
| 566 | 22.283 | 22.287 | 22.291 | 22.295 | 22.299 | 22.303 22.342 | 22.3076 | 22.350 | 22.354 | 22.35 S |
| 567 | 22.323 | 22.327 | 22.331 22.370 | 22.335 22.374 | 22.378 | 22.3 S 2 | 22.386 | 22.390 | 22.394 | 22.398 |
| 569 | 22.402 | 22.405 | 22.409 | 22.413 | 22.417 | 22.42 I | 22.425 | 22.429 | 22.433 | 22.437 |
| 570 | 22.4.41 | 22.445 | 22.449 | 22.453 | 22.457 | 22.461 | 22.465 | 22.468 | 22.472 | 22.476 |
| 57 I | 22.480 | 22.484 | 22.488 | 22.492 | 22.496 | 22.500 | 22.504 | 22.508 | 22.512 | 22.516 |
| 572 | 22.520 | 22.52 .4 | 22.52 S | 22.531 | 22.535 | 22.539 | 22.543 | 22.547 | 22.551 | 22.555 |
| 573 | 22.559 | 22.563 | 22.567 | 22.571 | 22.575 | 22.579 | 22.553 | 22.587 |  | 22.634 |
| 574 | 22.598 | 22.602 | 22.606 | 22.610 | 22.614 | 22.615 | 22 |  |  | 22.634 |
| 575 | 22.638 | 22.642 | 22.646 | 22.650 | 22.653 | 22.657 | 22.661 | 22.665 | 22.669 | 22.673 |
| 576 | 22.677 | 22.681 | 22.685 | 22.689 | 22.693 | 22.697 | 22.701 | 22.705 | 22.709 | 22.713 22.752 |
| 577 | 22.716 | 22.720 | 22.724 | 22.728 | 22.732 | 22.736 | 22.740 | 22.744 22.783 | 22.787 | 22.791 22.791 |
| 578 | 22.756 | 22.760 | 22.764 | 22.768 22.807 | 22.772 22.811 | 22.776 22.815 | 22.779 22.819 | 22.7823 22.823 | 22.827 | 22.831 |
| 579 | 22.795 | 22.799 | 22.803 | 22 | 22.811 | 22.815 | 22.819 | 22.523 |  |  |
| 580 | 22.835 | 22.839 | 22.842 | 22.8.46 | 22.850 | 22.854 | 22.858 | 22.862 | 22.866 | 22.870 22.909 |
| 58 I | 22.874 | 22.878 | 22.882 | 22.886 | 22.890 | 22.894 | 22.898 | 22.902 22.941 | 22.905 22.945 | 22.909 22.949 |
| 582 | 22.913 | 22.917 | 22.921 | 22.925 | 22.929 | 22.933 | 22.937 | 22.941 22.980 | 22.924 | 22.988 |
| 583 | 22.953 | 22.957 | 22.961 | 22.965 23.004 | 22.968 | 22.972 23.012 | 22.976 23.016 | 23.020 | 23.024 | 23.028 |
| 584 | 22.992 | 22.996 | 23.000 | 23.004 | 23.008 | 23.012 |  |  |  |  |
| 585 | 23.031 | 23.035 | 23.039 | 23.043 | 23.047 | 23.051 | 23.055 | 23.059 23.098 | 23.063 23.102 | $\begin{aligned} & 23.007 \\ & 23.106 \end{aligned}$ |
| 586 | 23.071 | 23.075 | 23.079 | 23.083 | 23.087 | 23.091 23.130 | 23.094 23.134 | 23.098 23.138 | ( $\begin{aligned} & 23.102 \\ & 23142\end{aligned}$ | 23.146 |
| 58 | 23. 110 | 23.114 | 23.118 | 23.122 | 23.126 | 23.130 23.169 | 23.134 23.173 |  | 23.181 | 23.185 |
| 588 | 23.150 | 23. 153 | 23.157 | 23.161 | 23.165 | 23.169 23.209 | 23.173 23.213 | 23.216 | 23.220 | 23.224 |
| 589 | 23.189 | 23.193 | 23.197 | 23.201 | 23.205 | 23.209 |  |  |  | 23.264 |
| 590 | 23.228 | 23.232 | 23.236 | 23.240 | 23.244 | 23.248 23.28 | 23.252 23.291 | 23.256 23.295 | [12929 | 23.303 |
| 591 | 23.268 | 23.272 | 23.276 | 23.279 | 23.283 <br> 23.323 | 23.287 <br> 23.327 | 23.291 23.331 | 23.295 23.335 | -23.339 | 23.342 |
| 592 | 23.307 | 23.311 | 23.315 | 23.319 <br> 23 | (1) $\begin{aligned} & 23.323 \\ & 23.362\end{aligned}$ | 23.327 $23 \cdot 366$ 23.405 | 23.370 | 23.374 | $4 \quad 23.378$ | 23.382 |
| 593 | 23.346 | 23.350 | 23.354 | 23.358 <br> 23.398 | \|l|l $\begin{aligned} & 23.362 \\ & 23.402\end{aligned}$ | 23.366 23.405 | 23.409 | 23.413 |  23.417 | 23.421 |
| 594 | 23.386 | 23.390 | 23.394 | 23.39 | 23.402 |  |  | 23.453 | 323.457 | 23.461 |
| 595 | 23.425 | [123.429 | -23.433 | 23.437 | 23.441 <br> 23.480 | 13.445 <br> 23.484 | 23.449 23.488 | \|23.492 | 23.496 | 23.500 |
| 596 | 23.465 | 53.468 23.508 | 23.472 <br> 23.512 | 23.476 <br> 23.516 | 23.480 <br> 23.520 | 10 23.404 <br> 03.524  | $4{ }_{4}{ }^{23.528}$ | 23.53I | I 23.535 | \| 23.539 |
|  | 23.504 23.543 | 4 23.508 <br> 3 23.547 | 23.512 <br> 23.551 | 11 23.516 <br> 13.555  |  | 923.563 | - 23.567 | 23.571 | 123.575 | 523.579 |
| 599 | 23.583 | 3 23.587 | 23.591 | $1{ }^{1} 23.594$ | 423.598 | S 23.602 | 23.606 | 23.610 | 23.614 | 423.618 |
| 600 | 23.622 | 223.626 | 623.630 | - 23.634 | 423.638 | S 23.642 | 2 23.646 | 623.650 | O 23.653 | 323.657 |

$1 \mathrm{~mm} .=0.03937$ inch.

| Millimeters. | . 0 | . 1 | . 2 | . 3 | 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 600 | 23.622 | 23.626 | 23.630 | 23.634 | 23.638 | 23.642 | 23.646 | 23.650 | 23.653 | 23.657 |
| 601 | 23.661 | 23.665 | 23.669 | 23.673 | 23.677 | 23.681 | 23.685 | 23.689 | 23.693 | 23.697 |
| 602 | 23.701 | 23.705 | 23.709 | 23.713 | 23.716 | 23.720 | 23.724 | 23.728 | 23.732 | 23.736 |
| 603 | 23.740 | 23.714 | 23.748 | 23.752 | 23.756 | 23.760 | 23.764 | 23.768 | 23.772 | 23.776 |
| 604 | 23.779 | 23.753 | 23.787 | 23.791 | 23.795 | 23.799 | 23.503 | 23.507 | 23.811 | 23.815 |
| 605 | 23. S19 | 23. 2 23 | 23.827 | 23.831 | 23.835 | 23.839 | 23.842 | 23. 8.46 | 23.850 | 23.854 |
| 606 | 23.858 | 23.862 | 23.866 | 23.570 | 23.874 | 23.878 | $23.8 S_{2}$ | 23.886 | 23.890 | 23. 994 |
| 607 | 23.598 | 23.902 | 23.905 | 23.909 | 23.913 | 23.917 | 23.921 | 23.925 | 23.929 | 23.933 |
| 608 | 23.937 | 23.941 | 23.945 | 23.949 | 23.953 | 23.957 | 23.961 | 23.965 | 23.968 | 23.972 |
| 609 | 23.976 | 23.980 | 23.984 | 23.988 | 23.992 | 23.996 | 24.000 | 2.4 .004 | 24.008 | 24.012 |
| 610 | 24.016 | 24.020 | 24.024 | 24.028 | 24.031 | 24.035 | 24.039 | 24.043 | 2.4 .047 | 24.051 |
| 611 | 24.055 | 24.059 | 24.063 | 24.067 | 2.4.071 | 24.075 | 24.079 | 2.4 .083 | 24.087 | 24.091 |
| 612 | 2.4.094 | 24.098 | 24.102 | 24.106 | 24.110 | 24.114 | 24.118 | 24.122 | $2+126$ | 24.130 |
| 613 | 24.134 | 2.4.138 | 24. 142 | 24.146 | 24.150 | 24.153 | 24. 157 | 2.4.16I | 2.4. 165 | 24.169 |
| 614 | 24.173 | 24.177 | 24.18I | 24.185 | 24.189 | 2.4.193 | 24.197 | 24.201 | 24.205 | 24.209 |
| 615 | 24.213 | 2.4.216 | 24.220 | 24.224 | 24.228 | 2. 4.232 | 24.236 | 2.4 .240 | 24.244 | 24.248 |
| 616 | 24.252 | 24.256 | 24.260 | 2.4 .264 | 24.268 | 2.4 .272 | 24.276 | 24.279 | 24.253 | 24.287 |
| 617 | 24.291 | 24.295 | 2.4.299 | 24.303 | 24.307 | $2+3$ II | 24.315 | $2+319$ | 24.323 | 24.327 |
| 6 IS | 24.331 | 24.335 | 24.339 | 2.4.3.12 | 2.4.346 | 24.350 | 24.354 | 24.358 | 24.362 | 24.366 |
| 619 | 24.370 | 24.374 | 24.378 | 2.4 .382 | 2.4 .386 | $2+.390$ | 24.394 | $2+.398$ | 24.402 | 2.4 .405 |
| 620 | 24.409 | 2.4 .413 | 2.4 .417 | 2.4 .42 I | 24. 425 | 2.4 .429 | 24.433 | 24.437 | 24.441 | 24.445 |
| 621 | 24.449 | $2+453$ | $2+457$ | 2.4.461 | 24.465 | $2+.468$ | 24.472 | 24.476 | 24.480 | 24.484 |
| 622 | 24.488 | 24.492 | 2.4 .496 | 24.500 | 24.504 | 24.508 | 24.512 | 24.516 | 24.520 | 24.524 |
| 623 | 24.528 | $2+.531$ | $2+535$ | 24.539 | 2.4 .543 | 24.547 | 24.55 I | 24.555 | 2.4.559 | 24.563 |
| 62.4 | 24.567 | 24.571 | 2.4.575 | 24.579 | 2.4 .583 | 2.1.5S7 | 24.591 | 2.4.59.4 | 24.598 | 24.602 |
| 625 | 24.606 | 24.610 | 24.614 | 24.618 | 24.622 | 2. 4.626 | 24.630 | 2.4 .634 | 24.63 S | 24.642 |
| 626 | 24.646 | 24.650 | 24.653 | 2.4 .657 | $2+661$ | 24.665 | 24.669 | 2.4 .673 | 24.677 | 24.68 I |
| 627 | $2+.685$ | 2.4 .689 | 24.693 | 24.697 | 2.4.701 | 21.705 | 24.709 | 2.4 .713 | 24.716 | 24.720 |
| 62 S | 24.72 .4 | 24.725 | 24.732 | 24.736 | 2.4 .740 | 24.744 | 24.748 | 24.752 | 24.756 | 24.760 |
| 629 | 24.764 | 24.768 | 24.772 | 24.776 | 24.779 | 24.783 | 24.787 | 2.4.791 | 24.795 | 24.799 |
| 630 | $24 . \mathrm{So3}$ | 24.807 | 24.SII | 24.815 | 24.S19 | 24. $\mathrm{S}_{23}$ | 24.827 | 24.831 | 24.835 | 24.839 |
| 631 | 24.842 | 24.846 | 24.850 | 24.854 | 24.858 | 24.862 | 24.866 | 24.870 | 24.874 | 24.878 |
| 632 | 2.4.8S2 | 24.886 | 24.890 | 24.894 | 24.898 | 24.902 | 24.905 | 24.909 | 24.913 | 24.917 |
| 633 | 24.92 I | 24.925 | 24.929 | 24.933 | 24.937 | 24.941 | 24.945 | $2+.949$ | 24.953 | 24.957 |
| 634 | 24.961 | 24.965 | 24.965 | 24.972 | 24.976 | 24.950 | 24.984 | 24.988 | 24.992 | 24.996 |
| 635 | 25.000 | 25.004 | 25.008 | 25.012 | 25.016 | 25.020 | 25.024 | 25.028 | 25.031 | 25.035 |
| 636 | 25.039 | 25.043 | 25.047 | 25.051 | 25.055 | 25.059 | 25.063 | 25.067 | 25.071 | 25.075 |
| 637 | 25.079 | 25.083 | 25.087 | 25.091 | 25.094 | 25.098 | 25.102 | 25.106 | 25.110 | 25.114 |
| 638 | 25.118 | 25.122 | 25.126 | 25.130 | 25.134 | 25.138 | 25.142 | 25.146 | 25.150 | 25.153 |
| 639 | 25.157 | 25.161 | 25.165 | 25.169 | 25.173 | 25.177 | 25.18I | 25. IS5 | 25.189 | 25.193 |
| 640 | 25.197 | 25.201 | 25.205 | 25.209 | 25.213 | 25.216 | 25.220 | 25.224 | 25.22 S | 25.232 |
| 6.1 | 25.236 | 25.240 | 25.214 | 25.248 | 25.252 | 25.256 | 25.260 | 25.264 | 25.268 | 25.272 |
| 6.42 | 25.276 | 25.279 | 25.283 | 25.287 | 25.291 | 25.295 | 25.299 | 25.303 | 25.307 | 25.311 |
| 6.3 | 25.315 | 25.319 | 25.323 | 25.327 | 25.33 I | 25.335 | 25.339 | 25.342 | 25.346 | 25.350 |
| 6.44 | $25 \cdot 35$ t | $25 \cdot 358$ | 25.362 | 25.366 | 25.370 | 25.374 | 25.37 S | $25.3 \mathrm{~S}^{2}$ | 25.386 | 25.390 |
| 645 | 25.394 | 25.398 | 25.402 | 25.405 | 25.409 | 25.413 | 25.417 | 25.421 | 25.425 | 25.429 |
| 646 | 25.433 | 25.437 | 25.441 | 25.445 | 25.149 | 25.453 | 25.457 | 25.461 | 25.465 | 25.468 |
| 647 | 25.472 | 25.476 | 25.4So | 25.4 S 4 | 25.485 | 25.492 | 25.496 | 25.500 | 25.504 | 25.508 |
| 648 | 25.512 | 25.516 | 25.520 | 25.524 | 25.52 S | 25.531 | 25.535 | 25.539 | 25.543 | 25.547 |
| 649 | 25.551 | 25.555 | 25.559 | 25.563 | 25.567 | 25.57 I | 25.575 | 25.579 | $25.5{ }^{8} 3$ | 25.5S7 |
| 650 | 25.591 | 25.594 | 25.598 | 25.602 | 25.606 | 25.610 | 25.614 | 25.618 | 25.622 | 25.626 |

I mm. $=0.03937$ inch.

| Milli- meters. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inch |
| 650 | 25.591 | 25.594 | 25.598 | 25.602 | 25.606 | 25.610 | 25.614 | 25.61S | 25.622 | 25.626 |
| 651 | 25.630 | 25.634 | 25.638 | 25.642 | 25.646 | 25.650 | 25.653 | 25.657 | 25.661 | 25.665 |
| 652 | 25.669 | 25.673 | 25.677 | 25.68I | 25.685 | 25.689 | 25.693 | 25.697 | 25.701 | 25.705 |
| 653 | 25.709 | 25.713 | 25.716 | 25.720 | 25.724 | 25.728 | 25.732 | 25.736 | 25.740 | 25.744 |
| 654 | 25.748 | 25.752 | 25.756 | 25.760 | 25.764 | 25.768 | 25.772 | 25.776 | 25.779 | 25.783 |
| 655 | 25.787 | 25.79 I | 25.795 | 25.799 | 25.803 | 25.807 | 25.SII | 25.815 | 25.819 | 25.823 |
| 656 | 25.827 | 25.83 I | 25.835 | 25.839 | 25.842 | 25.846 | 25.850 | 25.854 | 25.858 | 25.862 |
| 657 | 25.866 | 25.870 | 25.874 | 25.878 | 25.882 | 25.856 | 25.890 | 25.894 | 25.898 | 25.902 |
| 658 | 25.905 | 25.909 | 25.913 | 25.917 | 25.921 | 25.925 | 25.929 | 25.933 | 25.937 | 25.94 I |
| 659 | 25.945 | 25.949 | 25.953 | 25.957 | 25.961 | 25.965 | 25.968 | 25.972 | 25.976 | 25.980 |
| 660 | 25.984 | 25.988 | 25.992 | 25.996 | 26.000 | 26.004 | 26.008 | 26.012 | 26.016 | 26.020 |
| 661 | 26.024 | 26.028 | 26.031 | 26.035 | 26.039 | 26.043 | 26.047 | 26.051 | 26.055 | 26.059 |
| 662 | 26.063 | 26.067 | 25.07 I | 26.075 | 25.079 | 26.053 | 26.087 | 26.090 | 26.094 | 26.098 |
| 663 | 26.102 | 26.106 | 26.110 | 26.1 14 | 26.1 IS | 26. 122 | 26. I26 | 26.130 | 26.134 | 26.138 |
| 664 | 26.142 | 26.146 | 26.150 | 26.153 | 26.157 | 26.161 | 26.165 | 26.169 | 26.173 | 26.177 |
| 665 | 26. ISI | 26.185 | 26.1S9 | 26. 193 |  | 26.201 | 26.205 | 26.209 | 26.213 | 26.216 |
| 666 | 26.220 | 26.22 .4 | 26.22 S | 26.232 | 26.236 | 26.240 | 26.244 | 26.245 | 26.252 | 26.256 |
| 667 | 26.260 | 26.26 .4 | 26.268 | 26.272 | 26.276 | 26.279 | 26.283 | 26.287 | 26.291 | 26.295 |
| 668 | 26.299 | 26.303 | 26.307 | 26.31 I | 26.315 | 26.319 | 26.323 | 26.327 | 26.331 | 26.335 |
| 669 | 26.339 | 26.3 .42 | 26.346 | 26.350 | 26.354 | 26.358 | 26.362 | 26.366 | 26.370 | 26.374 |
| 670 | 26.378 | 26.382 | 26.386 | 26.390 | $26.39+$ | 26.398 | 26.402 | 26.405 | 26.409 | 26.413 |
| 671 | 26.417 | 26.421 | 26.425 | 26.429 | 26.433 | 26.437 | 26.44 I | 26.445 | 26.449 | 26.453 |
| 672 | 26.457 | 26.46 I | 26.465 | 26.468 | 26.472 | 26.476 | 26.480 | 26.484 | 26.488 | 26.492 |
| 673 | 26.496 | 26.500 | 26.504 | 26.508 | 26.512 | 26.516 | 26.520 | 26.524 | 26.528 | 26.53 I |
| 674 | 26.535 | 26.539 | 26.543 | 26.547 | 26.55 I | 26.555 | 26.559 | 26.563 | 26.567 | 26.57 I |
| 675 | 26.575 | 26.579 | 26.583 | 26.587 | 26.590 | 26.59 .4 | 26.598 | 26.602 | 26.606 | 26.610 |
| 676 | 26.614 | 26.618 | 26.622 | 26.626 | 26.630 | 26.634 | 26.638 | 26.642 | 26.646 | 26.650 |
| 677 | 26.653 | 26.657 | 26.661 | 26.665 | 26.669 | 26.673 | 26.677 | 26.68 I | 26.685 | 26.689 |
| 678 | 26.693 | 26.697 | 26.701 | 26.705 | 26.709 | 26.713 | 26.716 | 26.720 | 26.724 | 26.72 S |
| 679 | 26.732 | 26.736 | 26.740 | 26.744 | 26.748 | 26.752 | 26.756 | 26.760 | 26.764 | 26.768 |
| 680 | 26.772 | 26.776 | 26.779 | 26.783 | 26.787 | 26.791 |  |  |  |  |
| 651 | 26.81 I | $26 . \mathrm{SI}_{5}$ | 26.819 | 26.823 | 26.827 | 26.83 I | 26.835 | 26.538 | 26.842 | 26.846 |
| 682 | 26.850 | 26.554 | 26.555 | 26.862 | 26.866 | 26.870 | 26.574 | 26.57S | 26.882 | 26.856 |
| 683 | 26.890 | 26.594 | 26.898 | 26.902 | 26.905 | 26.909 | 26.913 | 26.917 | 26.921 | 26.925 |
| 684 | 26.929 | 26.933 | 26.937 | 26.941 | 26.945 | 26.949 | 26.953 | 26.957 | 26.961 | 26.965 |
| 685 | 26.968 | 26.972 | 26.976 | 26.980 | 26.984 | 26.988 | 26.992 | 26.996 | 27.000 | 27.004 |
| 686 | 27.008 | 27.012 | 27.016 | 27.020 | 27.024 | 27.028 | 27.03 I | 27.035 | 27.039 | 27.043 |
| $65_{7}$ | 27.047 | 27.051 | 27.055 | 27.059 | 27.063 | 27.067 | 27.071 | 27.075 | 27.079 | 27.083 |
| 688 | 27.087 | 27.090 | 27.094 | 27.098 | 27.102 | 27.106 | 27.110 | 27.114 | 27.1IS | 27.122 |
| 689 | 27.126 | 27.130 | 27. I34 | 27.138 | 27.142 | 27.146 | 27.150 | 27.153 | 27.157 | 27.161 |
| 690 | 27.165 | 27.169 | 27.173 | 27.177 | 27.181 | 27.185 | 27.189 | 27.193 | 27.197 | 27.201 |
| 691 | 27.205 | 27.209 | 27.213 | 27.216 | 27.220 | 27.224 | 27.228 | 27.232 | 27.236 | 27.240 |
| 692 | 27.244 | 27.248 | 27.252 | 27.256 | 27.260 | 27.264 | 27.268 | 27.272 | 27.276 | 27.279 |
| 693 | 27.283 | 27.287 | 27.291 | $2 \% .295$ | 27.299 | 27.303 | 27.307 | 27.311 | 27.3 I5 | 27.319 |
| 694 | 27.323 | 27.327 | 27.331 | 27.335 | 27.339 | 27.342 | $27 \cdot 3.46$ | 27.350 | 27.354 | 27.358 |
| 695 | 27.362 | 27.366 | 27.370 | 27.374 | 27.378 | 27.382 | 27.386 | 27.390 | 27.394 | 27.398 |
| 696 | 27.402 | 27.405 | 27.409 | 27.413 | 27.417 | 27.421 | 27.425 | 27.429 | 27.433 | 27.437 |
| $697$ | 27.44 I | 27.445 | 27.449 | 27.453 | 27.457 | 27.46 I | 27.465 | 27.468 | 27.472 | 27.476 |
| $698$ | 27.450 | 27.484 | 27.488 | 27.492 | 27.496 | 27.500 | 27.504 | 27.508 | 27.512 | 27.516 |
| 699 | 27.520 | 27.524 | 27.52 S | 27.531 | 27.535 | 27.539 | 27.543 | 27.547 | 27.55I | 27.555 |
| 700 | 27.559 | 27.563 | 27.567 | 27.57 I | 27.575 | 27.579 | 27.583 | 27.587 | 27.590 | 27.594 |

smitysonian tables.

## MILLIMETERS INTO INCHES.

$1 \mathrm{~mm} .=0.03937$ inch.

| Millimeters. | . 0 | . 1 | . 2 | . 3 | 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 700 | 27.559 | 27.563 | 27.567 | 27.571 | 27.575 | 27.579 | 27.583 | 27.587 | 27.590 | 27.594 |
| 701 | 27.598 | 27.602 | 27.606 | 27.610 | 27.614 | 27.618 | 27.622 | 27.626 | 27.630 | 27.634 |
| 702 | 27.638 | 27.642 | 27.646 | 27.650 | 27.653 | 27.657 | 27.661 | 27.665 | 27.669 | 27.673 |
| 703 | 27.677 | 27.68I | 27.685 | 27.689 | 27.693 | 27.697 | 27.701 | 27.705 | 27.709 | 27.713 |
| 704 | 27.716 | 27.720 | 27.724 | 27.728 | 27.732 | 27.736 | 27.740 | 27.744 | 27.748 | 27.752 |
| 705 | 27.756 | 27.760 | 27.764 | 27.768 | 27.772 | 27.776 | 27.779 | 27.783 | 27.787 | 27.791 |
| 706 | 27.795 | 27.799 | 27.803 | 27.807 | 27.811 | 27.815 | 27.819 | 27.823 | 27.827 | 27.831 |
| 707 | 27.835 | 27.839 | 27.842 | 27.8.46 | 27.550 | 27.854 | 27.858 | 27.862 | 27.866 | 27.870 |
| 708 | 27.874 | 27.875 | 27.882 | 27.886 | 27.890 | 27.894 | 27.898 | 27.902 | 27.905 | 27.909 |
| 709 | 27.913 | 27.917 | 27.92 I | 27.925 | 27.929 | 27.933 | 27.937 | 27.941 | 27.945 | 27.949 |
| 710 | 27.953 | 27.957 | 27.961 | 27.965 | 27.968 | 27.972 | 27.976 | 27.980 | 27.984 | 27.988 |
| 711 | 27.992 | 27.996 | 28.000 | 29.004 | 28.008 | 28.012 | 28.016 | 28.020 | 28.024 | 2 S .02 S |
| 712 | 28.031 | 28.035 | 28.039 | 28.043 | 28.047 | 28.051 | 2 S. 055 | 23.059 | 28.063 | 28.067 |
| 713 | 28.071 | 28.075 | 28.079 | 28.083 | 28.087 | 28.090 | 28.094 | 28.098 | 28.102 | 28.106 |
| 714 | 28.110 | 28.114 | 28.1IS | 28.122 | 28.126 | 28.130 | 28.134 | 2S.138 | 2S. 142 | 28.146 |
| 715 | 28.150 | 2S. 153 | 2S. 157 | 28.16I | 28.165 | 28.169 | 28.173 | 28.177 | 28. 181 | 28.185 |
| 716 | 28.189 | 2S. 193 | 28.197 | 28.201 | 28.205 | 28.209 | $2 \mathrm{S.213}$ | 28.216 | 28.220 | 28.224 |
| 717 | 28.228 | 28.232 | 28.236 | 28.240 | 2 S .244 | 2 S .248 | 2 S. 252 | 28.256 | 28.260 | 28.264 |
| 718 | 28.268 | 28.272 | 28.276 | 28.279 | 28.283 | 28.287 | 28.291 | 28.295 | 28.299 | 28.303 |
| 719 | 28.307 | 28.3 II | $2 \mathrm{S.315}$ | 28.319 | 28.323 | 28.327 | 28.33 I | 28.335 | 28.339 | 28.342 |
| 720 | 28.346 | 28.350 | 28.354 | 28.358 | 28.362 | 28.366 | 28.370 | 28.374 | 28.378 | 2 S .382 |
| 721 | 28.386 | 28.390 | 28.394 | 28.398 | 2 S .402 | 28.405 | 28.409 | 28.413 | 28.417 | 2 S .42 I |
| 722 | 28.425 | 28.429 | 28.433 | 28.437 | 28.44 I | 28.445 | 28.449 | 28.453 | 2 S .457 | 28.461 |
| 723 | 28.465 | 28.468 | 2 S .472 | 28.476 | 2 S .480 | 28.484 | 28.488 | 2 S .492 | 28.496 | 28.500 |
| 724 | 28.504 | 28.508 | 28.512 | 28.516 | 28.520 | 28.524 | 28.528 | 28.531 | 28.535 | 28.539 |
| 725 | 28.543 | 28.547 | 28.551 | 28.555 | 28.559 | 28.563 | 28.567 | 28.571 | 28.575 | 28.579 |
| 726 | 2 S .583 | 28.587 | 28.590 | 28.594 | 28.598 | 28.602 | 28.606 | 28.610 | 28.614 | 28.618 |
| 727 | 28.622 | 28.626 | 2 S .630 | 28.634 | 28.638 | 28.642 | 28.6 .46 | 28.650 | 28.653 | 28.657 |
| 728 | 28.661 | 2 S .665 | 28.669 | 28.673 | 28.677 | 28.681 | 28.685 | 28.689 | 28.693 | 28.697 |
| 729 | 28.701 | 28.705 | 28.709 | 28.713 | 28.716 | 28.720 | 28.724 | 28.728 | 28.732 | 28.736 |
| 730 | 28.740 | 28.744 | 28.748 | 28.752 | 28.756 | 28.760 | 28.764 | 28.768 | 28.772 | 28.776 |
| 731 | 28.779 | 28.783 | 28.787 | 28.791 | 28.795 | 28.799 | $2 \mathrm{S}$. So3 | $28 . \mathrm{So7}$ | 28.8II | 28.815 |
| 732 | 28.819 | 28.823 | 28.827 | 28.831 | 28.835 | 28.839 | $2 \mathrm{S}. \mathrm{~S}_{4}$ | 28.846 | 28.850 | 28.854 |
| 733 | 28.858 | 28.862 | 28.866 | 28.870 | 28.874 | 28.878 | 28.882 | 2S.886 | 28.890 | 28.894 |
| 734 | 28.598 | 28.902 | 28.905 | 28.909 | 28.913 | 28.917 | 2 S .92 I | 28.925 | 28.929 | 28.933 |
| 735 | 28.937 | 28.94 I | 28.945 | 28.949 | 28.953 | 28.957 | 2S.96I | 28.965 | 28.968 | 2 S .972 |
| 736 | 28.976 | 28.980 | 28.984 | 28.988 | 28.992 | 28.996 | 29.000 | 29.004 | 29.008 | 29.012 |
| 737 | 29.016 | 29.020 | 29.024 | 29.028 | 29.03 I | 29.035 | 29.039 | 29.043 | 29.047 | 29.051 |
| 738 | 29.055 | 29.059 | 29.063 | 29.067 | 29.071 | 29.075 | 29.079 | 29.053 | 29.087 | 29.090 |
| 739 | 29.094 | 29.098 | 29.102 | 29. 106 | 29.1 IO | 29. I 14 | 29.118 | 29.122 | 29.126 | 29.130 |
| 740 | 29. 134 | 29.13S | 29.142 | 29.146 | 29.150 | 29.153 | 29.157 | 29.16I | 29.165 | 29.169 |
| 741 | 29.173 | 29.177 | 29.18I | 29.185 | 29.189 | 29.193 | 29.197 | 29.201 | 29.205 | 29.209 |
| 742 | 29.213 | 29.216 | 29.220 | 29.224 | 29.228 | 29.232 | 29.236 | 29.240 | 29.244 | 29.248 |
| 743 | 29.252 | 29.256 | 29.260 | 29.264 | 29.268 | 29.272 | 29.276 | 29.279 | 29.283 | 29.287 |
| 74.4 | 29.291 | 29.295 | 29.299 | 29.303 | 29.307 | 29.3 II | 29.315 | 29.319 | 29.323 | 29.327 |
| 745 | 29.331 | 29.335 | 29.339 | 29.342 | 29.346 | 29.350 | 29.354 | 29.358 | 29.362 | 29.366 |
| 746 | 29.370 | 29.374 | 29.378 | 29.382 | 29.386 | 29.390 | 29.394 | 29.398 | 29.402 | 29.405 |
| 747 | 29.409 | 29.413 | 29.417 | 29.421 | 29.425 | 29.429 | 29.433 | 29.437 | 29.44 I | 29.445 |
| 748 | 29.449 | 29.453 | 29.457 | 29.46 I | 29.465 | 29.468 | 29.472 | 29.476 | 29.480 | 29.484 |
| 749 | 29.458 | 29.492 | 29.496 | 29.500 | 29.504 | 29.508 | 29.512 | 29.516 | 29.520 | 29.524 |
| 750 | 29.528 | 29.53 I | 29.535 | 29.539 | 29.543 | 29.547 | 29.551 | 29.555 | 29.559 | 29.563 |

MILLIMETERS INTO INCHES.
$1 \mathrm{~mm} .=0.03937$ inch.

| Millimeters | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Iuches. | Inches. | Inches. | Inches. | Inches. |
| 750 | 29.52S | 29.53I | 29.535 | 29.539 | 29.543 | 29.547 | 29.55 I | 29.555 | 29.559 | 29.563 |
| 751 | 29.567 | 29.571 | 29.575 | 29.579 | 29.583 | 29.587 | 29.590 | 29.594 | 29.598 | 29.602 |
| 752 | 29.606 | 29.610 | 29.614 | 29.618 | 29.622 | 29.626 | 29.630 | 29.634 | 29.638 | 29.642 |
| 753 | 29.646 | 29.650 | 29.653 | 29.657 | 29.661 | 29.665 | 29.669 | 29.673 | 29.677 | 29.68I |
| 754 | 29.685 | 29.689 | 29.693 | 29.697 | 29.701 | 29.705 | 29.709 | 29.713 | 29.716 | 29.720 |
| 755 | 29.724 | 29.728 | 29.732 | 29.736 | 29.740 | 29.744 | 29.748 | 29.752 | 29.756 | 29.760 |
| 756 | 29.764 | 29.768 | 29.772 | 29.776 | 29.779 | 29.783 | 29.787 | 29.791 | 29.795 | 29.799 |
| 757 | 29.803 | 29.807 | 29.81 I | 29.815 | 29.819 | 29.823 | 29.827 | 29.831 | 29.835 | 29.839 |
| 758 | 29.842 | 29.846 | 29850 | 29.854 | 29.858 | 29.862 | 29.866 | 29.870 | 29.574 | 29.878 |
| 759 | 29.882 | 29.886 | 29. S90 | 29.594 | 29.898 | 29.902 | 29.905 | 29.909 | 29.913 | 29.917 |
| 760 | 29.92 I | 29.925 | 29.929 | 29.933 | 29.937 | 29.941 | 29.945 | 29.949 | 29.953 | 29.957 |
| 761 | 29.961 | 29.965 | 29.968 | 29.972 | 29.976 | 29.980 | 29.984 | 29.958 | 29.992 | 29.996 |
| 762 | 30.000 | 30.004 | 30.008 | 30.012 | 30.016 | 30.020 | 30.024 | 30.027 | 30.031 | 30.035 |
| 763 | 30.039 | 30.043 | 30.047 | 30.051 | 30.055 | 30.059 | 30.063 | 30.067 | 30.071 | 30.075 |
| 764 | 30.079 | 30.083 | 30.087 | 30.090 | 30.09.4 | 30.098 | 30.102 | 30. 106 | 30.110 | 30. 114 |
| 765 | 30. 118 | 30.122 | 30.126 | 30.130 | 30.134 | 30.138 | 30. 142 | 30. 146 | 30.150 | 30. 153 |
| 766 | 30. 157 | 30.161 | 30.165 | 30.169 | 30.173 | 30.177 | 30.18I | 30.185 | 30.159 | 30.193 |
| 767 | 30. 197 | 30.201 | 30.205 | 30.209 | 30.213 | 30.216 | 30.220 | 30.224 | 30.228 | 30.232 |
| 768 | 30.236 | 30.240 | 30.244 | 30.248 | 30.252 | 30.256 | 30.260 | 30.264 | 30.268 | 30.272 |
| 769 | 30.276 | 30.279 | 30.283 | 30.287 | 30.291 | 30.295 | 30.299 | 30.303 | 30.307 | 30.311 |
| 770 | 30.315 | 30.319 | 30.323 | 30.327 | 30.33I | 30.335 | 30.339 | 30.342 | 30.346 | 30.350 |
| 771 | 30.354 | 30.358 | 30.362 | 30.366 | 30.370 | 30.374 | 30.378 | 30.382 | 30.386 | 30.390 |
| 772 | 30.394 | 30.398 | 30.402 | 30.405 | 30.409 | 30.413 | 30.417 | 30.42 I | 30.425 | 30.429 |
| 773 | 30.433 | 30.437 | 30.441 | 30.445 | 30.449 | 30.453 | 30.457 | 30.461 | 30.465 | 30.468 |
| 774 | 30.472 | 30.476 | 30.4So | 30.484 | 30.488 | 30.492 | 30.496 | 30.500 | 30.504 | 30.508 |
| 775 | 30.512 | 30.516 | 30.520 | 30.524 | 30.528 | 30.53 I | 30.535 | 30.539 | 30.543 | 30.547 |
| 776 | 30.551 | 30.555 | 30.559 | 30.563 | 30.567 | 30.571 | 30.575 | 30.579 | 30.553 | 30.587 |
| 777 | 30.590 | 30.594 | 30.593 | 30.602 | 30.606 | 30.610 | 30.614 | 30.618 | 30.622 | 30.626 |
| 778 | 30.630 | 30.634 | 30.638 | 30.642 | 30.646 | 30.650 | 30.653 | 30.657 | 30.661 | 30.665 |
| 779 | 30.669 | 30.673 | 30.677 | 30.681 | 30.685 | 30.689 | 30.693 | 30.697 | 30.701 | 30.705 |
| 780 | 30.709 | 30.713 | 30.716 | 30.720 | 30.724 | 30.728 | 30.732 | 30.736 | 30.740 | 30.744 |
| 781 | 30.748 | 30.752 | 30.756 | 30.760 | 30.764 | 30.768 | 30.772 | 30.776 | 30.779 | 30.783 |
| 782 | 30.787 | 30.791 | 30.795 | 30.799 | 30.So3 | 30.807 | 30.8II | 30.815 | 30.819 | 30.823 |
| 783 | 30.827 | 30.83 I | 30.835 | 30.839 | 30.842 | 30.846 | 30.850 | 30.854 | 30.858 | 30.862 |
| 784 | 30.866 | 30.870 | 30.874 | 30.878 | 30.882 | 30.856 | 30.890 | 30. S94 | 30.898 | 30.902 |
| 785 | 30.905 | 30.909 | 30.913 | 30.917 | 30.92 I | 30.925 | 30.929 | 30.933 | 30.937 | 30.941 |
| 786 | 30.945 | 30.949 | 30.953 | 30.957 | 30.961 | 30.965 | 30.968 | 30.972 | 30.976 | 30.980 |
| 787 | 30.984 | 30.988 | 30.992 | 30.996 | 31.000 | 31.004 | 31.008 | 3 I .012 | 3 I .016 | 31.020 |
| 788 | 31.024 | 31.027 | 31.031 | 31.035 | 31.039 | 31.043 | 31.047 | 31.051 | 31.055 | 31.059 |
| 789 | 31.063 | 31.067 | 31.071 | 31.075 | 31.079 | 31.083 | 31.087 | 31.090 | 31.094 | 31.098 |
| 790 | 3 I .102 | 31. 106 | 3 I .110 | 31.114 | 31.118 | 31.122 | 31.126 | 31.130 | 31.134 | 3I.138 |
| 791 | 3 I .142 | 31.146 | 31.150 | 31.153 | 31.157 | 31.16I | 31.165 | 31.169 | 31.173 | 3 I .177 |
| 792 | 3 I .18 I | 3 I .185 | 31.189 | 31.193 | 31.197 | 31.201 | 31.205 | 31.209 | 31.213 | 31.216 |
| 793 | 31.220 | 31.224 | 31.228 | 31.232 | 31.236 | 31.240 | 31.244 | 31.248 | 31.252 | 31.256 |
| 794 | 31.260 | 31.264 | 31.268 | 31.272 | 31.276 | 31.279 | 31.283 | 31.287 | 31.291 | 31.295 |
| 795 | 31.299 | 31.303 | 31.307 | 3I.3II | 31.315 | 31.319 | 31.323 | 31.327 | 31.331 | 31.335 |
| 796 | 3 I .339 | 31.342 | 31.346 | 3 I .350 | 31.354 | 31.358 | 31.362 | 31.366 | 31.370 | 3 I .374 |
| 797 | 3 I .37 S | 3 I .382 | 3 I .380 | 31.390 | 3 I .394 | 31.398 | 3 I .402 | 31.405 | 31.409 | 3 I .413 |
| 798 | 31.417 | 3 I .42 I | 3 I .425 | 31.429 | 31.433 | 31.437 | 3 I .44 I | 3 I .445 | 3I. 449 | 3 I .453 |
| 799 | 31.457 | 31.461 | 31.465 | 31.468 | 31.472 | 31.476 | 31.4So | 3 I .484 | 31.488 | $3 \mathrm{I} .49^{2}$ |
| 800 | 31.496 | 31.500 | 31.504 | 31.508 | 31.512 | 31.516 | 31.520 | 31.524 | 31.527 | 31.53 I |

Smitheonian Tables.
$1 \mathrm{~mm} .=0.03937$ inch.

| Millimeters. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Iuches. | Inches. | Inches. | Inches. |
| 800 | 31.496 | 31.500 | 31.504 | 31.508 | 31.512 | 3I.516 | 31.520 | 31.524 | 31.527 | 31.531 |
| SoI | 31.535 | 31.539 | 31.543 | 31.547 | 31.55 I | 31.555 | 31.559 | 31.563 | 31.567 | 31.571 |
| So2 | 31.575 | 31.579 | 31.583 | 31.587 | 31.590 | 31.594 | 31.598 | 31.602 | 31.606 | 31.610 |
| $\mathrm{SO}_{3}$ | 31.614 | 31.6IS | 31.622 | 31.626 | 31.630 | 31.634 | 31.638 | 31.642 | 31.646 | 31.650 |
| SO. 4 | 31.653 | 31.657 | 3 I .66 I | 31.665 | 31.669 | 31.673 | 31.677 | 31.68 I | 31.685 | 31.689 |
| 805 | 31.693 | 31.697 | 31.701 | 31.705 | 31.709 | 31.713 | 31.716 | 31.730 | 31.724 | 31.728 |
| So6 | 31.732 | 31.736 | 31.740 | 31.744 | 31.748 | 31.752 | 31.756 | 31.760 | 31.764 | 31.768 |
| So7 | 31.772 | 31.776 | 31.779 | 31.783 | 31.757 | 31.791 | 31.795 | 31.799 | 31.803 | 31.807 |
| SoS | 3 I .SII | 3I.Si5 | 31.819 | 31.823 | 31.827 | 3 I. S3I | 31.835 | 31.839 | 3 I.S42 | 31.846 |
| So9 | $31 . S_{50}$ | 31.854 | 31.858 | 31.862 | 31.866 | 31.870 | 31.874 | 31.578 | 31.882 | 31.886 |
| 810 | 31.590 | 31.894 | 31.898 | 31.902 | 31.905 | 31.909 | 31.913 | 31.917 | 31.921 | 31.925 |
| SII | 31.929 | 31.933 | 31.937 | 31.94I | 31.945 | 31.949 | 31.953 | 31.957 | 31.961 | 31.965 |
| SI2 | 31.968 | 31.972 | 31.976 | 31.980 | 31.984 | 31.988 | 31.992 | 31.996 | 32.000 | 32.004 |
| SI 3 | 32.008 | 32.012 | 32.016 | 32.020 | 32.024 | 32.027 | 32.031 | 32.035 | 32.039 | 32.043 |
| SI4 | 32.047 | 32.05 I | 32.055 | 32.059 | 32.063 | 32.067 | 32.071 | 32.075 | 32.079 | 32.083 |
| 815 | 32.087 | 32.090 | 32.094 | 32.098 | 32.102 | 32.106 | 32.110 | 32.1I4 | 32.118 | 32.122 |
| Si6 | 32.126 | 32.130 | 32. 134 | 32.138 | 32.142 | 32.146 | 32.150 | 32.153 | 32.157 | 32.161 |
| SI7 | 32.165 | 32.169 | 32.173 | 32.177 | 32.1 I I | 32.185 | 32.189 | 32.193 | 32.197 | 32.201 |
| 818 | 32.205 | 32.209 | 32.213 | 32.216 | 32.220 | 32.22 .4 | 32.22 S | 32.232 | 32.236 | 32.240 |
| SI9 | 32.214 | 32.248 | 32.252 | 32.256 | 32.260 | 32.264 | 32.268 | 32.272 | 32.276 | 32.279 |
| 820 | 32.283 | 32.287 | 32.29 I | 32.295 | 32.299 | 32.303 | 32.307 | 32.311 | 32.315 | 32.319 |
| 821 | 32.323 | 32.327 | 32.33 I | 32.335 | 32.339 | 32.342 | 32.346 | 32.350 | 32.354 | 32.358 |
| S22 | 32.362 | 32.366 | 32.370 | 32.374 | 32.378 | 32.352 | 32.386 | 32.390 | 32.394 | 32.398 |
| 823 | 32.402 | 32.405 | 32.409 | 32.413 | 32.417 | 32.42 I | 32.425 | 32.429 | 32.433 | 32.437 |
| 82.4 | 32.44 I | 32.445 | 32.449 | 32.453 | 32.457 | 32.461 | 32.465 | 32.468 | 32.472 | 32.476 |
| 825 | 32.480 | 32.484 | 32.488 | 32.492 | 32.496 | 32.500 | 32.504 | 32.508 | 32.512 | 32.516 |
| 826 | 32.520 | 32.52 .4 | 32.527 | 32.53 I | 32.535 | 32.539 | 32.543 | 32.547 | 32.551 | 32.555 |
| S27 | 32.559 | 32.563 | 32.567 | 32.57 I | 32.575 | 32.579 | 32.583 | 32.587 | 32.590 | 32.594 |
| S2S | 32.598 | 32.602 | 32.606 | 32.610 | 32.614 | 32.6 IS | 32.622 | 32.626 | 32.630 | 32.634 |
| S29 | 32.638 | 32.6 .42 | 32.646 | 32.650 | 32.653 | 32.657 | 32.66 I | 32.665 | 32.669 | 32.673 |
| 830 | 32.677 | 32.68 I | 32.655 | 32.689 | 32.693 | 32.697 | 32.701 | 32.705 | 32.709 | 32.713 |
| 831 | 32.716 | 32.720 | 32.724 | 32.72 S | 32.732 | 32.736 | 32.740 | 32.744 | 32.748 | 32.752 |
| S32 | 32.756 | 32.760 | 32.76 .4 | 32.768 | 32.772 | 32.776 | 32.779 | 32.783 | 32.787 | 32.791 |
| S33 | 32.795 | 32.799 | $32 . \mathrm{So} 3$ | 32.807 | 32.SII | 32.815 | 32.819 | 32.823 | 32.827 | 32.831 |
| S34 | 32.835 | 32.839 | $32 . S_{42}$ | 32.846 | 32.850 | 32.854 | 32.858 | 32.862. | 32.866 | 32.870 |
| 835 | 32.874 | 32.878 | 32.882 | 32.886 | 32.890 | 32.894 | 32.898 | 32.902 | 32.905 | 32.909 |
| 836 | 32.913 | 32.917 | 32.92 I | 32.925 | 32.929 | 32.933 | 32.937 | 32.941 | 32.945 | 32.949 |
| 837 | 32.953 | 32.957 | 32.961 | 32.965 | 32.968 | 32.972 | 32.976 | 32.980 | 32.984 | 32.988 |
| 838 | 32.992 | 32.996 | 33.000 | 33.004 | 33.008 | 33.012 | 33.016 | 33.020 | 33.024 | 33.027 |
| S39 | 33.031 | 33.035 | 33.039 | 33.043 | 33.047 | 33.051 | 33.055 | 33.059 | 33.063 | 33.067 |
| 840 | 33.07 I | 33.075 | 33.079 | 33.083 | 33.087 | 33.090 | 33.094 | 33.098 | 33.102 | 33.106 |
| 841 | 33.110 | 33.114 | 33. IIS | 33.122 | 33.126 | 33.130 | 33.134 | 33.138 | 33.142 | 33.146 |
| 5.12 | 33.150 | 33.153 | 33. 157 | 33.161 | 33.165 | 33.169 | 33.173 | 33.177 | 33.1SI | 33.185 |
| 8.43 | 33.159 | 33.193 | 33.197 | 33.201 | 33.205 | 33.209 | 33.213 | 33.216 | 33.220 | 33.22 .4 |
| S44 | 33.228 | 33.232 | 33.236 | 33.240 | 33.244 | 33.248 | 33.252 | 33.256 | 33.260 | 33.264 |
| 845 | 33.268 | 33.272 | 33.276 | 33.279 | 33.283 | 33.287 | 33.291 | 33.295 | 33.299 | 33.303 |
| 846 | 33.307 | 33.311 | 33.315 | 33.319 | 33.323 | 33.327 | 33.331 | 33.335 | 33.339 | 33.342 |
| 847 | 33.346 | 33.350 | 33.354 | 33.358 | 33.362 | 33.366 | 33.370 | 33.374 | 33.378 | 33.382 |
| S48 | 33.386 | 33.390 | 33.394 | 33.398 | 33.402 | 33.405 | 33.409 | 33.413 | 33.417 | 33.421 |
| S49 | 33.425 | 33.429 | 33.433 | 33.437 | 33.441 | 33.445 | 33.449 | 33.453 | 33.457 | 33.461 |
| 850 | 33.464 | 33.468 | 33.472 | 33.476 | 33.4 So | 33.484 | 33.488 | 33.492 | 33.496 | $33 \cdot 500$ |

$1 \mathrm{~mm} .=0.03937$ inch.

| Millimeters. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inch | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 850 | 33.4 | 33.468 | 33.472 | 33.476 | 33.480 | 33.484 | 33.485 | 33.492 | 33.496 | 33.500 |
| S51 | 33.504 | 33.508 | 33.512 | 33.516 | 33.520 | 33.52.4 | 33.527 | 33.53 I | $33 \cdot 535$ | 33.539 |
| S52 | 33.543 | 33.547 | 33.551 | 33.555 | 33.559 | 33.563 | 33.567 | 33.57 I | 33.575 | 33.579 |
| S53 | 33.583 | 33.587 | 33.590 | 33.594 | 33.598 | 33.602 | 33.606 | 33.610 | 33.614 | 33.6IS |
| S54 | 33.622 | 33.626 | 33.630 | 33.634 | 33.638 | 33.642 | 33.646 | 33.650 | 33.653 | 33.657 |
| 855 | 33.661 | 33.665 | 33.669 | 33.673 | 33.677 | 33.681 | 33.685 | 33.689 | 33.693 | 33.697 |
| S56 | 33.701 | 33.705 | 33.709 | 33.713 | 33.716 | 33.720 | 33.724 | 33.728 | 33.732 | 33.736 |
| S57 | 33.740 | 33.744 | 33.748 | 33.752 | 33.756 | 33.760 | 33.764 | 33.768 | 33.772 | 33.776 |
| 858 | 33.779 | 33.783 | 33.787 | 33.791 | 33.795 | 33.799 | 33.803 | 33.807 | 33.8II | 33.8I5 |
| S59 | 33.819 | 33.823 | 33.827 | 33.831 | 33.835 | 33.839 | 33.842 | 33.8.46 | 33.850 | 33.854 |
| 860 | 33.558 | 33.862 | 33.866 | 33.570 | 33.574 | 33.8-5 | 33.882 | 33.886 | 33.890 | 33.894 |
| 861 | 33.898 | 33.902 | 33.905 | 33.909 | 33.913 | 33.917 | 33.92 I | 33.925 | 33.929 | 33.933 |
| 862 | 33.937 | 33.941 | 33.945 | 33.949 | 33.953 | 33.957 | 33.96 | 33.964 | 33.968 | 33.972 |
| 863 | 33.976 | 33.950 | 33.98. | 33.988 | 33.992 | 33.996 | 34.000 | 34.004 | 34.008 | 34.012 |
| S64 | 34.016 | 34.020 | 34.024 | 34.027 | 34.03 I | 34.035 | 34.039 | 34.043 | 34.047 | 34.051 |
| 865 | 34.055 | 34.059 | 34.063 | 34.067 | 34.071 | 34.075 | 34 | 34.083 | 34.087 | 34.090 |
| 866 | 34.094 | 34.098 | 34.102 | 34.106 | 34.1 10 | 34. I I 4 | 34.118 | 34.122 | 34.126 | 34.130 |
| 867 | 34.134 | 34.138 | 34.142 | 34.146 | 34.150 | 34.153 | 34.157 | 34.161 | 34.165 | 34.169 |
| 868 | 34.173 | 34.177 | 34.ISI | 34.185 | 34.189 | 34.193 | 34.197 | 34.201 | 34.205 | 34.209 |
| 869 | 34.213 | 34.216 | 34.220 | 34.224 | 34.228 | 34.232 | 34.236 | 34.240 | 34.244 | 34.248 |
| 870 | 34.252 | 34.256 | 34.260 | 34.26 .4 | 34.268 | 34.272 | 34.276 | 34.279 | 34.283 | 34.287 |
| S71 | 34.291 | 34.295 | 34.299 | 34.303 | 34.307 | 34.3 I | 34.315 | 34.319 | 34.323 | 34.327 |
| 872 | 34.33 I | 34.335 | 34.339 | 34.342 | 34.346 | 34.350 | $34 \cdot 354$ | 34.358 | 34.362 | 34.366 |
| 873 | 34.370 | 34.374 | 34.378 | 34.3 S2 | $3+\cdot 386$ | 34.390 | 34.39 .4 | 34.398 | 34.402 | 34.405 |
| 874 | 34.409 | 34.413 | 34.417 | 34.421 | 34.425 | 34.429 | 34.433 | 34.437 | 34.44 I | 34.445 |
| 875 | 34.449 | 34.453 | 34.457 | 34.46 I | 34.464 | 24.468 | 34.472 | 34.476 | 34.480 | 34.484 |
| 876 | 34.488 | 34.492 | 34.496 | 34.500 | 34.504 | 34.508 | 34.512 | 34.516 | 34.520 | $34 \cdot 524$ |
| 877 | 34.527 | 34.53I | 34.535 | 34.539 | 34.543 | 34.547 | $3+551$ | 34.555 | 34.559 | 34.563 |
| 878 | 34.567 | 34.57 I | 34.575 | 34.579 | 34.583 | 34.587 | 34.590 | 34.594 | 34.598 | 34.602 |
| S79 | 34.606 | 34.610 | 34.614 | 34.6I8 | 34.622 | 34.626 | 34.630 | 34.634 | 34.638 | 34.642 |
| 880 | 34.646 | 34.650 | 34.653 | 34.657 | 34.66I | 34.665 | 34.669 | 34.673 | 34.677 | 34.6SI |
| SSI | 34.685 | 34.689 | 34.693 | 34.697 | 34.701 | 34.705 | 34.709 | 34.713 | 34.716 | 34.720 |
| 882 | 34.72 .4 | 34.728 | $34.73^{2}$ | 34.736 | 34.740 | 34.744 | 34.74 S | 34.752 | 34.756 | 34.760 |
| 883 | 34.764 | 34.768 | 34.772 | 34.776 | 34.779 | 34.783 | 34.787 | 34.791 | 34.795 | 34.799 |
| SS. | $34 . \mathrm{So} 3$ | 34.807 | 34.8 I I | 34.815 | 34.819 | 34.823 | 34.827 | 34.83 I | 34.835 | 34.839 |
| 885 | 34. $8_{4} 42$ | 34.846 | 34.850 | 34.854 | 34.85 | 34.862 | 34.866 | 34.870 | 34.874 | 34.878 |
| 886 | 34.882 | 34.886 | 34.890 | 34.594 | 34.898 | 34.902 | 34.905 | 34.909 | 34.913 | 34.917 |
| 887 | 34.92 I | 34.925 | 34.929 | 34.933 | 34.937 | 34.94 .1 | 34.9.45 | 34.949 | 34.953 | 34.957 |
| SS8 | 34.96 I | 3.4 .964 | 3.4.968 | 34.972 | 34.976 | 34.9So | 34.984 | 34.9S8 | 34.992 | 34.996 |
| SS9 | 35.000 | 35.004 | 35.008 | 35.012 | 35.016 | 35.020 | 35.024 | 35.027 | 35.031 | 35.035 |
| 890 | 35.039 | 35.043 | 35.047 | 35.05 I | 35.055 | 35.059 | 35.063 | 35.067 | 35.071 | 35.075 |
| S91 | 35.079 | 35.083 | 35.087 | 35.090 | 35.094 | 35.098 | 35.102 | 35. 106 | 35.110 | 35.1 I4 |
| S92 | 35.1IS | 35. 122 | 35.126 | 35.130 | 35.134 | 35.138 | 35.142 | 35.146 | 35.150 | 35. I 53 |
| S93 | 35.157 | 35.16I | 35.165 | 35.169 | 35.173 | 35.177 | 35.18I | 35.185 | 35.189 | 35. 193 |
| 894 | 35.197 | 35.201 | 35.205 | 35.209 | 35.213 | 35.216 | 35.220 | 35.224 | 35.228 | 35.232 |
| 895 | 35.236 | 35.240 | 35.244 | 35.248 | 35.252 | 35.256 | 35.260 | 35.264 | 35.268 | 35.272 |
| S96 | 35.276 | 35.279 | 35.283 | 35.287 | 35.291 | 35.295 | 35.299 | 35.303 | 35.307 | 35.311 |
| S9 | 35.315 | 35-319 | 35.323 | 35.327 | 35.331 | 35.335 | 35.339 | 35.342 | 35.346 | 35.350 |
| S98 | 35.354 | $35 \cdot 35 \mathrm{~S}$ | $35 \cdot 362$ | 35.366 | 35.370 | 35.374 | 35.378 | 35.382 | 35.386 | 35.390 |
| S99 | 35.394 | 35-398 | 35.402 | 35.405 | 35.409 | 35.413 | 35.417 | 35.42I | 35.425 | 35.429 |
| 900 | 35.433 | 35.437 | 35.44I | 35.445 | 35.449 | 35.453 | 35.457 | 35.46 I | 35.464 | 35.468 |

Table 10.

## MILLIMETERS INTO INCHES.

I $\mathrm{mm} .=0.03937$ inch.

| Millimeters. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inclies. | Inches. | Iuches. | Iuches. | Inches. | Inches. | Inches. | Inches. |
| 900 | 35.433 | 35.437 | 35.44 I | 35.445 | 35.449 | 35.453 | 35.457 | 35.46I | 35.464 | 35.468 |
| 901 | 35.472 | 35.476 | 35.480 | 35.484 | 35.488 | 35.492 | 35.496 | 35.500 | 35.504 | 35.508 |
| 902 | 35.512 | 35.516 | 35.520 | 35.52.4 | 35.527 | 35.531 | 35.535 | 35.539 | 35.543 | 35.547 |
| 903 | 35.55 I | $35 \cdot 555$ | 35.559 | 35.563 | 35.567 | 35.57 I | 35.575 | 35.579 | 35.583 | 35.587 |
| 904 | 35.590 | 35.594 | 35.598 | 35.602 | 35.606 | 35.610 | 35.614 | 35.618 | 35.622 | 35.626 |
| 905 | 35.630 | 35.634 | 35.638 | 35.642 | 35.646 | 35.650 | 35.653 | 35.657 | 35.661 | 35.665 |
| 906 | 35.669 | 35.673 | 35.677 | 35.68I | 35.685 | 35.689 | 35.693 | 35.697 | 35.701 | 35.705 |
| 907 | 35.709 | 35.713 | 35.716 | 35.720 | 35.724 | 35.728 | 35.732 | 35.736 | 35.740 | 35.744 |
| 908 | 35.748 | 35.752 | 35.756 | 35.760 | 35.764 | 35.768 | 35.772 | 35.776 | 35.779 | 35.783 |
| 909 | 35.757 | 35.791 | 35.795 | 35.799 | 35.803 | 35. $\mathrm{So}^{7}$ | 35.8II | 35.815 | 35.819 | 35.823 |
| 910 | 35.827 | 35.831 | 35.835 | 35.839 | 35.842 | 35.8.46 | 35.850 | 35.854 | 35.858 | 35.862 |
| 911 | 35.866 | 35.870 | 35.874 | 35.878 | 35.882 | 35.886 | 35.890 | 35.894 | 35.898 | 35.902 |
| 912 | 35.905 | 35.909 | 35.913 | 35.917 | 35.92 I | 35.925 | 35.929 | 35.933 | 35.937 | 35.941 |
| 913 | 35.9.45 | 35.949 | 35.953 | 35.957 | 35.96 I | 35.964 | 35.968 | 35.972 | 35.976 | 35.980 |
| 914 | 35.984 | 35.988 | 35.992 | 35.996 | 36.000 | 36.004 | 36.008 | 36.012 | 36.016 | 36.020 |
| 915 | 36.024 | 36.027 | 36.03 I | 36.035 | 36.039 | 36.043 | 36.047 | 36.05 I | 36.055 | 36.059 |
| 916 | 36.063 | 36.067 | 36.071 | 36.075 | 36.079 | 36.083 | 36.087 | 36.090 | 36.094 | 36.098 |
| 917 | 36. IO2 | 36.106 | 36.110 | 36.114 | 36.1IS | 36.122 | 36.126 | 36.130 | 36.124 | 36.138 |
| 918 | 36. 142 | 36.146 | 36.150 | 36.153 | 36.157 | 36.161 | 36.165 | 36.169 | 30.173 | 36.177 |
| 919 | 36. IS I | 36.185 | 36.189 | 36.193 | 36.197 | 36.201 | 36.205 | 36.209 | 36.213 | 36.216 |
| 920 | 36.220 | 36.224 | 36.228 | 36.232 | 36.236 | 36.240 | 36.244 | 36.248 | 36.252 | 36.256 |
| 92 I | 36.260 | 36.264 | 36.268 | 36.272 | 36.276 | 36.279 | 36.283 | 36.287 | 36.291 | 36.295 |
| 922 | 36.299 | 36.303 | 36.307 | 36.31 I | 36.315 | 36.319 | 36.323 | 36.327 | 36.331 | 36.335 |
| 923 | 36.339 | 36.342 | 36.346 | 36.350 | 36.354 | 36.358 | 36.362 | 36.366 | 36.370 | 36.374 |
| 924 | 36.378 | 36.3 S2 | 36.386 | 36.390 | 36.39 .4 | 36.398 | 36.402 | 36.405 | 36.409 | 36.413 |
| 925 | 36.417 | 36.42 I | 36.425 | 36.429 | 36.433 | 36.437 | 36.44 I | 36.445 | 36.449 | 36.453 |
| 926 | 36.457 | 36.461 | 36.464 | 36.46 S | 36.472 | 36.476 | 36.480 | 36.484 | 36.488 | 36.492 |
| 927 | 36.496 | 36.500 | 36.50 .4 | 36.508 | . 36.512 | 36.516 | 36.520 | 36.524 | 36.527 | 36.53 I |
| 928 | 36.535 | 36.539 | 36.5.13 | 36.547 | 36.55 I | 36.555 | 36.559 | 36.563 | 36.567 | 36.571 |
| 929 | 36.575 | 36.579 | 36.583 | 36.587 | 36.590 | 36.59 .4 | 36.598 | 36.602 | 36.606 | 36.610 |
| 930 | 36.614 | 36.618 | 36.622 | 36.626 | 36.630 | 36.634 | 36.638 | 36.642 | 36.646 | 36.650 |
| 931 | 36.653 | 36.657 | 36.661 | 36.665 | 36.669 | 36.673 | 36.677 | 36.681 | 36.685 | 36.689 |
| 932 | 36.693 | 36.697 | 36.701 | 36.705 | 36.709 | 36.713 | 36.716 | 36.720 | 36.72 .4 | 36.72 S |
| 933 | 36.732 | 36.736 | 36.740 | 36.744 | 36.748 | 36.752 | 36.756 | 36.760 | 36.764 | 36.768 |
| 934 | 36.772 | 36.776 | 36.779 | 36.783 | 36.787 | 36.791 | 36.795 | 36.799 | 36.803 | 3 ¢. 807 |
| 935 | 36.SII | 36.815 | 36.819 | 36.823 | 36.827 | 36.83 I | 36.835 | 36.839 | 36.842 | 36.8.46 |
| 936 | 36.850 | 36.854 | 36.858 | 36.862 | 36.866 | 36.870 | 36.874 | 36.878 | 36.882 | 36.886 |
| 937 | 36.590 | 36.894 | 36.898 | 36.902 | 36.905 | 36.909 | 36.913 | 36.917 | 36.921 | 36.925 |
| 938 | 36.929 | 36.933 | 36.937 | 36.941 | 36.945 | 36.949 | 36.953 | 36.957 | 36.961 | 36.964 |
| 939 | 36.968 | 36.972 | 36.976 | 36.980 | 36.984 | 36.988 | 36.992 | 36.996 | 37.000 | 37.004 |
| 940 | 37.008 | 37.012 | 37.016 | 37.020 | 37.024 | 37.027 | 37.03I | 37.035 | 37.039 | 37.043 |
| 941 | 37.047 | 37.051 | 37.055 | 37.059 | 37.063 | 37.067 | 37.07 I | 37.075 | 37.079 | 37.083 |
| 9.42 | 37.087 | 37.090 | 37.09.4 | 37.098 | 37.102 | 37.106 | 37.110 | 37.114 | 37.118 | 37.122 |
| $9+3$ | 37.126 | 37.130 | 37.134 | 37.138 | 37.142 | 37.146 | 37.150 | 37.153 | 37.157 | 37.161 |
| 9.4 | 37.165 | 37.169 | 37.173 | 37.177 | 37.18I | 37.185 | 37.189 | 37.193 | 37.197 | 37.201 |
| 945 | 37.204 | 37.208 | 37.212 | 37.216 | 37.220 | 37.22 .4 | 37.228 | 37.232 | 37.236 | 37.240 |
| 9.46 | 37.244 | 37.248 | 37.252 | 37.256 | 37.260 | 37.264 | 37.268 | 37.272 | 37.276 | 37.279 |
| 947 | 37.283 | 37.287 | 37.291 | 37.295 | 37.299 | 37.303 | 37.307 | 37.311 | 37.315 | 37.319 |
| 948 | 37.323 | 37.327 | 37.331 | 37.335 | 37.339 | 37.342 | 37.346 | 37.350 | 37.354 | 37.35S |
| 949 | 37.362 | 37.366 | 37.370 | 37.374 | 37.378 | $37.3{ }^{\text {82 }}$ | 37.386 | 37.390 | 37.394 | 37.398 |
| 950 | 37.402 | 37.405 | 37.409 | 37.413 | 37.417 | 37.42 I | 37.425 | 37.429 | 37.433 | 37.437 |

$1 \mathrm{~mm} .=0.03937$ inch.

| Millimeters. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 950 | 37.402 | 37.405 | 37.409 | 37.413 | 37.417 | 37.42 I | 37.425 | 37.429 | 37.433 | 37.437 |
| 951 | 37.44 I | 37.445 | 37.449 | 37.453 | 37.457 | 37.461 | 37.464 | 37.468 | 37.472 | 37.476 |
| 952 | 37.48 O | 37.484 | 37.488 | 37.492 | 37.496 | 37.500 | 37.504 | 37.508 | 37.512 | 37.516 |
| 953 | 37.520 | 37.524 | 37.527 | 37.53 I | 37.535 | 37.539 | 37.543 | 37.547 | 37.55I | 37.555 |
| 954 | 37.559 | 37.563 | 37.567 | 37.571 | 37.575 | 37.579 | 37.583 | 37.587 | 37.590 | 37.594 |
| 955 | 37.598 | 37.602 | 37.606 | 37.610 | 37.614 | 37.618 | 37.622 | 37.626 | 37.630 | 37.634 |
| 956 | 37.638 | 37.642 | 37.646 | 37.650 | 37.653 | 37.657 | 37.661 | 37.665 | 37.669 | 37.673 |
| 957 | 37.677 | 37.681 | 37.685 | 37.689 | 37.693 | 37.697 | 37.701 | 37.705 | 37.709 | 37.713 |
| 958 | 37.716 | 37.720 | 37.724 | 37.728 | 37.732 | 37.736 | 37.740 | 37.744 | 37.74S | 37.752 |
| 959 | 37.756 | 37.760 | 37.764 | 37.768 | 37.772 | 37.776 | 37.779 | 37.783 | 37.787 | 37.791 |
| 960 | 37.795 | 37.799 | $37 . \mathrm{So} 3$ | 37.807 | 37.SII | 37.815 | 37.819 | 37.823 | 37.827 | 37.831 |
| 961 | 37.835 | 37.839 | 37.842 | 37.846 | 37.850 | 37.854 | 37.858 | 37.862 | 37.866 | 37.870 |
| 962 | 37.574 | 37.878 | 37.882 | 37.886 | 37.890 | 37.894 | 37.898 | 37.901 | 37.905 | 37.909 |
| 963 | 37.913 | 37.917 | 37.92 I | 37.925 | 37.929 | 37.933 | 37.937 | 37.941 | 37.945 | 37.949 |
| 964 | 37.953 | 37.957 | 37.961 | 37.964 | 37.968 | 37.972 | 37.976 | 37.980 | 37.984 | 37.98S |
| 965 |  | 37.996 | 38.000 | 38.004 | 38.008 | 38.012 | 38.016 | 3 S.020 | 38.024 | 38.027 |
| 966 | 38.03 | $3 \mathrm{S.035}$ | 38.039 | 38.043 | 38.047 | 38.051 | 3 3.055 | 3 3.059 | 38.063 | 38.067 |
| 967 | 38.071 | 38.075 | 38.079 | 38.083 | 38.087 | 38.090 | 38.094 | 38.098 | 38.102 | 38.106 |
| 968 | 38.110 | 3S.II4 | 38.118 | 38.122 | 38.126 | 38.130 | 3S. I34 | 38.138 | 3S. 142 | 38.146 |
| 969 | 38.150 | 3S. I 53 | 38. 157 | 38.16I | 38.165 | 38.169 | 38.173 | 38.177 | 3S.ISI | 38.185 |
| 970 | 38.189 | 38.193 | 38.197 | 3 3.201 | 38.205 | 38.209 | $3 \mathrm{S.213}$ | 38.216 | 38.220 | 38.224 |
| 971 | 38.228 | 38.232 | 38.236 | 3 S. 240 | 38.244 | 38.248 | 38.252 | 38.256 | 38.260 | 38.264 |
| 972 | 38.268 | 38.272 | 38.276 | 38.279 | 38.283 | 38.287 | 38.291 | 38.295 | 38.299 | 38.303 |
| 973 | 38.307 | 38.311 | 38.315 | 38.319 | 38.323 | 38.327 | 38.331 | 38.335 | 38.339 | $3^{S .} 3+2$ |
| 974 | 38.346 | 38.350 | 38.354 | 38.358 | 38.362 | 38.366 | 38.370 | 38.374 | 38.378 | 38.382 |
| 975 | 38.386 | 38.390 | 38.394 | 38.398 | 38.401 | 38.405 | 38.409 | 38.413 | 38.417 | 38.42 I |
| 976 | 3 S. 425 | 38.429 | 38.433 | 38.437 | 3 S .44 I | 38.445 | 38.449 | 38.453 | 38.457 | 38.461 |
| 977 | 38.464 | 38.468 | 38.472 | 38.476 | 38.480 | 38.484 | 38.488 | 3 S. 492 | 3 S. 496 | 38.500 |
| 978 | $3 \mathrm{S}$. | 3 S. 508 | 38.512 | 38.516 | 38.520 | 38.524 | 38.527 | 3 S. 531 | 38.535 | 38.539 |
| 979 | 38.543 | $3 \mathrm{S}$. | 38.55 I | 38.555 | 38.559 | 38.563 | 38.567 | 38.57 I | 38.575 | 38.579 |
| 980 | 38.583 | 38.587 | 38.590 | 38.594 | 38.598 | 38.602 | 38.606 | 38.610 | 38.614 | 38.618 |
| 981 | 38.622 | 38.626 | 38.630 | 38.634 | 38.638 | 38.642 | 38.646 | 38.650 | 38.653 | 38.657 |
| 982 | 38.661 | 38.665 | 38.669 | 38.673 | 38.677 | 38.68 I | 38.685 | 3 3.689 | 38.693 | 38.697 |
| 983 | 38.701 | 38.705 | 38.709 | 38.713 | 38.716 | 38.720 | 38.724 | 38.728 | 38.732 |  |
| 984 | 38.740 | 38.744 | 38.748 | 38.752 | 38.756 | 38.760 | 38.764 | 38.768 | 38.772 | 38.776 |
| 985 | 38.750 | 38.783 | 38.787 | 38.791 | 38.795 | 38.799 | 38.803 | 38.807 | 38.811 |  |
| 986 | 3 3. 19 | 38.823 | 38.827 | 38.831 | 38.835 | 38.839 | 38.842 | 38.846 | 38.850 | 38.854 |
| 987 | 3 S. 555 | 38.862 | 38.866 | 38.870 | 3 3. 874 | 38.875 | 3 S.SS2 | 38.886 | 38.890 | 38. 994 |
| 988 | 38.898 | 38.901 | 38.905 | 38.909 | 38.913 | 3 S.917 | 38.921 | 38.925 | 3 3.929 | 38.933 |
| 989 | 38.937 | $3 \mathrm{S.941}$ | $3^{88} .945$ | 38.949 | 3 S .953 | 3 S.957 | $3 \mathrm{S.961}$ | 38.964 | 38.968 | 38.972 |
| 990 | 38.976 | 38.9So | 38.984 | 38.988 | 38.992 | 38.996 | 39.000 | 39.004 | 39.008 | 39.012 |
| 991 | 39.016 | 39.020 | 39.024 | 39.027 | 39.031 | 39.035 | 39.039 | 39.043 | 39.047 | 39.051 |
| 992 | 39.055 | 39.059 | 39.063 | 39.067 | 39.071 | 39.075 | 39.079 | 39.083 | 39.087 | 39.090 |
| 99,3 | 39.094 | 39.098 | 39.102 | 39.106 | 39.110 | 39.114 | 39.118 | 39.122 | 39.126 | 39.130 |
| 994 | 39.134 | 39.138 | 39.142 | 39.146 | 39.150 | 39.153 | 39.157 | 39.161 | 39.165 | 39.169 |
| 995 | 39.173 | 39.177 | 39.18I | 39.185 | 39.189 | 39.193 | 39.197 | 39.201 | 39.205 |  |
| 996 | 39.213 | 39.216 | 39.220 | 39.224 | 39.228 | 39.232 | 39.236 | 39.240 | 39.244 | 39.248 |
| 997 | 39.252 | 39.256 | 39.260 | 39.264 | 39.268 | 39.272 | 39.276 | 39.279 | 39.283 | 39.287 |
| 998 | 39.291 | 39.295 | 39.299 | 39.303 | 39.307 | 39.311 | 39.315 | 39.319 | 39.323 | 39.327 |
| 999 | 39.331 | 39.335 | 39.339 | $39 \cdot 342$ | 39.346 | 39.350 | 39.354 | 39.358 | 39.362 | 39.366 |
| 1000 | 39.370 | 39.374 | 39.378 | 39.382 | 39.386 | 39.390 | 39.394 | 39.398 | 39.401 | 39.405 |

Table 11.
BAROMETRIC INCHES (MERCURY) INTO MILLIBARS.
I inch $=33.86395 \mathrm{mb}$.

| Inches | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mb. | mb. | mb. | mb . | mb. | nib. | mb . | mb. | mb . | mb. |
| 0.0 | 0.00 | 0.34 | 0.68 | . 02 | 1.35 | 1.69 | 2.03 | 2.37 | 2.71 | 3.05 |
| 0.1 | 3.39 | 3.73 | 4.06 | 4.40 | 4.74 | 5.08 | 5.43 | 5.76 | 6.10 | 6.43 |
| 0.2 | 6.77 | 7.11 | $7 \cdot 45$ | 7.79 | 8.13 | 8.47 | 8.80 | 9.14 | 9.48 | 9.82 |
| 0.3 | 10.16 | 10.50 | 10.84 | 11.18 | 11.51 | II. $\mathrm{S}_{5}$ | 12.19 | 12.53 | 12.87 | 13.21 |
| 0.4 | 13.55 | 13.88 | 14.22 | 14.56 | 14.90 | 15.24 | 15.58 | 15.92 | 16.25 | 16.59 |
| 0.5 | 16.93 | 17.27 | ${ }_{7} 7.61$ | 17.95 | 18.29 | 18.63 | 18.06 | 10.30 | 19.64 | 19.98 |
| 0.6 | 20.32 | 20.66 | 21.00 | 21.33 | 21.67 | 22.01 | 22.35 | 22.69 | 23.03 | 23.37 |
| 0.7 | 23.70 | 24.04 | 24.38 | $2+.72$ | 25.06 | 25.40 | 25.74 | 26.08 | 26.41 | 26.75 |
| 0.8 | 27.09 | 27.43 | 27.77 | $2 \mathrm{S.1} 1$ | 28.45 | 28.78 | 29.12 | 29.46 | 29.80 | 30.14 |
| 0.9 | 30.48 | 30.82 | 31.15 | 31.49 | 31.83 | 32.17 | 32.51 | 32.85 | 33.19 | 33.53 |
| 1.0 | 33.86 | 34.20 | 34.54 | 34.88 | 35.22 | 35.56 | 35.90 | 36.23 | 36.57 | 36.91 |
| I. 1 | 37.25 | 37.59 | 37.93 | 38.27 | 38.60 | 38.94 | 39.28 | 39.62 | 39.96 | 40.30 |
| 1. 2 | 40.64 | 40.98 | 41.31 | 41.65 | 41.99 | 42.33 | 42.67 | +3.01 | $43 \cdot 35$ | 43.68 |
| I. 3 | 44.02 | $44 \cdot 36$ | $4+70$ | 45.04 | 45.38 | 45.72 | 46.05 | 46.39 | 46.73 | 47.07 |
| 1.4 | 47.41 | 47.75 | 48.09 | 48.43 | 48.76 | 49.10 | $49 \cdot 44$ | 49.78 | 50.12 | 50.46 |
| 1.5 | 50.80 | 51.13 | 5 I .47 | 51.8I | 52.15 | 52.49 | 52.83 | 53.17 | 53.51 | 53.84 |
| 1.6 | 54.18 | 54.52 | 54.86 | 55.20 | 55.54 | 55.88 | 56.21 | 56.55 | 56.89 | 57.23 |
| 1.7 | 57.57 | 57.91 | 58.25 | 58.58 | 58.92 | 59.26 | 59.60 | 59.94 | 60.28 | 60.62 |
| 1. 8 | 60.96 | 61.29 | 61.63 | 61.97 | 62.31 | 62.65 | 62.99 | 63.33 | 03.66 | 64.00 |
| 1.9 | $64 \cdot 3+$ | 64.68 | 65.02 | 65.36 | 65.70 | 66.03 | 66.37 | 66.71 | 67.05 | 67.39 |
| 2.0 | 67.73 | 68.07 | 68.41 | 68.74 | 69.08 | 69.42 | 69.76 | 70.10 | 70.44 | 70.78 |
| 2.1 | 71.11 | 71.45 | 71.79 | 72.13 | 72.47 | 72.8 I | 73.15 | 73.48 | 73.82 | 74.16 |
| 2.2 | 74.50 | 74.84 | 75.18 | 75.52 | 75.86 | 76.19 | 76.53 | 76.87 | 77.21 | 77.55 |
| 2.3 | 77.89 | 78.23 | 78.56 | 78.90 | 79.24 | 79.58 | 79.92 | So. 26 | So. 60 | So. 93 |
| 2.4 | 81.27 | 81.61 | 81.95 | 82.29 | 82.63 | S2.97 | 83.31 | 83.64 | 83.98 | $8+32$ |
| 25.0 | 8.46 .6 | 846.9 | $8+7.3$ | 847.6 | 848.0 | 848.3 | S+8.6 | 8.49 .0 | $8+9.3$ | 849.6 |
| 25.1 | 850.0 | 850.3 | 850.7 | 851.0 | 851.3 | 851.7 | 852.0 | 852.4 | 852.7 | 853.0 |
| 25.2 | 853.4 | 853.7 | 854.0 | 854.4 | 854.7 | 855.1 | 855.4 | 855.7 | 856.1 | 856.4 |
| $25 \cdot 3$ | 856.8 | 857.1 | 857.4 | 857.8 | 858.1 | 858.5 | S58.8 | 859.1 | 859.5 | 859.8 |
| 25.4 | 860.1 | 860.5 | S60.8 | 861.2 | S61. 5 | 86 I .8 | 862.2 | 862.5 | 862.9 | 863.2 |
| 25.5 | 863.5 | 863.9 | 864.2 | 864.5 | 864.9 | 865.2 | 865.6 | 865.9 | 866.2 | 866.6 |
| 25.6 | 866.9 | 867.3 | 867.6 | 867.9 | 868.3 | 868.6 | 868.9 | 869.3 | 869.6 | 870.0 |
| 25.7 | 870.3 | 870.7 | 871.0 | 871.3 | 871.7 | 872.0 | 872.3 | 872.7 | 873.0 | 873.4 |
| 25.8 | 873.7 | S74.0 | 874.4 | S74.7 | 875.0 | $875 \cdot 4$ | 875.7 | 876.1 | 876.4 | 876.7 |
| 25.9 | 877.1 | $877 \cdot 4$ | 877.8 | S78.1 | 878.4 | 878.8 | 879.1 | 879.4 | 879.8 | 880.1 |
| 26.0 | 880.5 | 880.8 | 881.1 | 881.5 | S8ı. 8 | 88.2 | 882.5 | 882.8 | 883.2 | 883.5 |
| 26.1 | 883.8 | 884.2 | 88+5 | 884.9 | 885.2 | 885.5 | 885.9 | 886.2 | 886.6 | 880.9 |
| 26.2 | 887.2 | 887.6 | 887.9 | 888.3 | 888.6 | 888.9 | 889.3 | 889.6 | 889.9 | 890.3 |
| 26.3 | 890.6 | 891.0 | 891.3 | S91.6 | S92.0 | 892.3 | 80.7 | 893.0 | 893.3 | 893.7 |
| 26.4 | 894.0 | S94.3 | 89.4.7 | 895.0 | 895.4 | 895.7 | S96.0 | 896.4 | 896.7 | 897.I |
| 26.5 | 897.4 | S97.7 | 898.1 | 898.4 | S98.7 | S99.I | 899.4 | S99.8 | 900.1 | 900.4 |
| 26.6 | 900.8 | 901.1 | 901.5 | 901.8 | 902.1 | 902.5 | 902.5 | 903.2 | 903.5 | 903.8 |
| 26.7 | 904. 2 | 904.5 | 904.8 | 905.2 | 905.5 | 905.9 | 906.2 | 906.5 | 906.9 | 907.2 |
| 26.8 | 907.6 | 907.9 | 908.2 | 908.6 | 908.9 | 909.2 | 909.6 | 909.9 | 910.3 | 910.6 |
| 26.9 | 910.9 | 91.3 | 911.6 | 912.0 | 912.3 | 912.6 | 913.0 | 913.3 | 913.6 | 914.0 |
| 27.0 | 914.3 | 91.4.7 | 915.0 | 915.3 | 915.7 | 916.0 | 916.4 | 916.7 | 917.0 | 917.4 |
| 27.1 | 917.7 | 918.1 | 918.4 | 918.7 | 919.1 | 919.4 | 919.7 | 920.1 | 920.4 | 920.8 |
| 27.2 | 92 I .1 | 92 I .4 | 921.8 | 922.1 | 922.5 | 922.8 | 923.1 | 923.5 | 923.8 | 924.1 |
| 27.3 | 924.5 | 924.8 | 925.2 | 925.5 | 925.8 | 926.2 | 926.5 | 926.9 | 927.2 | 927.5 |
| 27.4 | 927.9 | 928.2 | 928.5 | 928.9 | 929.2 | 929.6 | 929.9 | 930.2 | 930.6 | 930.9 |

BAROMETRIC INCHES (MERCURY) INTO MILLIBARS.
I inch $=33.86395 \mathrm{mb}$.


Simithisonian tables.

Table 12.
BAROMETRIC MILLIMETERS (MERCURY) INTO MILLIBARS.
$1 \mathrm{~mm} .=1.33322387 \mathrm{mb}$.

| Millimeters. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mb. | mb . | mb. | mb. | mb. | mb. | mb. | mb. | mb. | mb. |
| 0 | $\bigcirc$ | 1.3 | 2.7 | 4.0 | $5 \cdot 3$ | 6.7 | 8.0 | 9.3 | 10.7 | 12.0 |
| 10 | 13.3 | 14.7 | 10.0 | 17.3 | 18.7 | 20.0 | 21.3 | 22.7 | 24.0 | 25.3 |
| 20 | 20.7 | 28.0 | 29.3 | 30.7 | 32.0 | $33 \cdot 3$ | 34.7 | 36.0 | 37.3 | 38.7 |
| 30 | 40.0 | 41.3 | 42.7 | +4.0 | $45 \cdot 3$ | 46.7 | 48.0 | 49.3 | 50.7 | 52.0 |
| 40 | 53.3 | 54.7 | 56.0 | 57.3 | 58.7 | 60.0 | 61.3 | 62.7 | 64.0 | 65.3 |
| 50 | 66.7 | 68.0 | 69.3 | 70.7 | 72.0 | 73.3 | 74.7 | 76.0 | 77.3 | 78.7 |
| 60 | 80.0 | 8 I .3 | 82.7 | 8.4 .0 | 85.3 | 86.7 | 88.0 | 89.3 | 90.7 | 92.0 |
| 70 | 93.3 | 94.7 | 96.0 | 97.3 | 98.7 | 100.0 | 101.3 | 102.7 | 104.0 | 105.3 |
| 80 | 106.7 | 108.0 | 109.3 | 110.7 | 112.0 | 113.3 | 114.7 | I 16.0 | 117.3 | 118.7 |
| 90 | 120.0 | 121.3 | 122.7 | 124.0 | 125.3 | 126.7 | I28.0 | I 29.3 | 130.7 | 132.0 |
| 100 | 133.3 | 134.7 | 136.0 | ${ }^{1} 37.3$ | 138.7 | 140.0 | 141.3 | 142.7 | 144.0 | 145.3 |
| 110 | 1+6.7 | 148.0 | 149.3 | 150.7 | 152.0 | 153.3 | 154.7 | I 56.0 | 157.3 | 158.7 |
| 120 | 160.0 | 161.3 | 162.7 | 164.0 | 165.3 | 166.7 | 168.0 | 169.3 | 170.7 | 172.0 |
| 130 | 173.3 | 174.7 | 176.0 | 177.3 | 178.7 | 180.0 | 181.3 | 182.7 | I84.0 | 185.3 |
| 140 | I 86.7 | 188.0 | 189.3 | 190.7 | 192.0 | 193.3 | 194.7 | 196.0 | 197.3 | 198.7 |
| 150 | 200.0 | 201.3 | 202.7 | 204.0 | 20.5 .3 | 206.6 | 208.0 | 209.3 | 210.6 | 212.0 |
| 160 | 213.3 | 214.6 | 216.0 | 217.3 | 218.6 | 220.0 | 221.3 | 222.6 | 224.0 | 225.3 |
| 170 | 220.6 | 228.0 | 229.3 | 230.6 | 232.0 | 233.3 | 234.6 | 236.0 | 237.3 | 238.6 |
| 180 | 240.0 | 2.41 .3 | 242.6 | 244.0 | 245.3 | 246.6 | 248.0 | 249.3 | 250.6 | 252.0 |
| 190 | 253.3 | 254.6 | 256.0 | 257.3 | 258.6 | 260.0 | 261.3 | 262.6 | 264.0 | 265.3 |
| 200 | 266.6 | 268.0 | 269.3 | 270.6 | 272.0 | 273.3 | 274.6 | ${ }_{27} 6.0$ | 277.3 | 278.6 |
| 210 | 280.0 | 281.3 | 282.6 | 284.0 | 285.3 | 286.6 | 288.0 | 289.3 | 290.6 | 292.0 |
| 220 | 293.3 | 294.6 | 296.0 | 297.3 | 208.6 | 300.0 | 301.3 | 302.6 | 304.0 | 305.3 |
| 230 | 306.6 | 308.0 | 309.3 | 310.6 | 312.0 | 313.3 | 314.6 | 316.0 | 317.3 | 318.6 |
| 240 | 320.0 | 321.3 | 322.6 | 324.0 | 325.3 | 326.6 | 328.0 | 329.3 | 330.6 | 332.0 |
| 250 | 333.3 | 334.6 | 336.0 | $337 \cdot 3$ | 338.6 | 340.0 | 341.3 | 342.6 | 344.0 |  |
| 260 | 346.6 | 348.0 | 349.3 | 350.6 | 352.0 | 353.3 | 354.6 | 356.0 | 357.3 | 358.6 |
| 270 | 360.0 | 361.3 | 362.6 | 364.0 | 365.3 | 366.6 | 368.0 | 369.3 | 370.6 | 372.0 |
| 280 | 373.3 | 374.6 | 376.0 | $377 \cdot 3$ | 378.6 | 380.0 | 381.3 | 382.6 | 384.0 | 385.3 |
| 290 | 386.6 | 388.0 | 389.3 | 390.6 | 392.0 | $393 \cdot 3$ | 394.6 | 396.0 | 397.3 | 398.6 |
| 300 | 400.0 | 401.3 | 402.6 | 404.0 | 405.3 | 406.6 | 408.0 | 409.3 | 410.6 | 412.0 |
| 310 | +13.3 | 414.6 | 416.0 | 417.3 | 418.6 | 420.0 | 42 I .3 | 422.6 | 424.0 | 425.3 |
| 320 | 426.6 | 428.0 | 429.3 | 430.6 | 432.0 | 433.3 | 434.6 | 436.0 | $437 \cdot 3$ | 438.6 |
| 330 | 440.0 | 441.3 | 442.6 | 444.0 | 445.3 | 446.6 | 448.0 | 449.3 | 450.6 | 452.0 |
| 340 | 45.3.3 | 454.6 | 456.0 | 457.3 | 458.6 | 460.0 | 461.3 | 462.6 | 464.0 | 465.3 |
| 350 | 466.6 | 468.0 | 469.3 | 470.6 | 472.0 | 473.3 | 474.6 | 476.0 | 477.3 | 478.6 |
| 360 | 480.0 | 481.3 | 482.6 | 484.0 | 485.3 | 486.6 | 488.0 | 489.3 | 490.6 | 492.0 |
| 370 | 493.3 | 494.6 | 496.0 | 497.3 | 498.6 | 500.0 | 501.3 | 502.6 | 50.4 .0 | 505.3 |
| 380 | 506.6 | 508.0 | 509.3 | 510.6 | 512.0 | 513.3 | 514.6 | 516.0 | 517.3 | 518.6 |
| 390 | 520.0 | 521.3 | 522.6 | 524.0 | 525.3 | 526.6 | 528.0 | 529.3 | 530.6 | 532.0 |
| 400 | $533 \cdot 3$ | 534.6 | 536.0 | 537.3 | 538.6 | 540.0 | 541.3 | 542.6 | 544.0 |  |
| 410 | 546.6 | 548.0 | 549.3 | 550.6 | 552.0 | 553.3 | 554.6 | 556.0 | 557.3 | 558.6 |
| 420 | 560.0 | 561.3 | 562.6 | 564.0 | 565.3 | 566.6 | 568.0 | 569.3 | 570.6 | 572.0 |
| 430 | 573.3 586.6 | 574.6 | 576.0 | 577.3 500.6 | 578.6 | 580.0 | 581.3 | 582.6 | 584.0 | 585.3 |
| 440 | 586.6 | 588.0 | 589.3 | 590.6 | 592.0 | 593.3 | 594.6 | 596.0 | 597.3 | 598.6 |

Smithsonian tables.

Table 12.
BAROMETRIC MILLIMETERS (MERCURY) INTO MILLIBARS.
$1 \mathrm{~mm} .=\mathrm{x} .33322387 \mathrm{mb}$.

| Millimeters. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mb. | mb. | mb . | mb. | mb. | mb. | mb. | mb . | mb. | mb. |
| 450 | 600.0 | 601.3 | 602.6 | 604.0 | 605.3 | 606.6 | 608.0 | 609.3 | 610.6 | 611.9 |
| 460 | 613.3 | 614.6 | 615.9 | 617.3 | 618.6 | 619.9 | 621.3 | 622.6 | 623.9 | 625.3 |
| 470 | 626.6 | 627.9 | 629.3 | 630.6 | 631.9 | 633.3 | 634.6 | 635.9 | 637.3 | 638.6 |
| 480 | 639.9 | 641.3 | 642.6 | 643.9 | 645.3 | 646.6 | 647.9 | 649.3 | 650.6 | 651.9 |
| 490 | $653 \cdot 3$ | 654.6 | 655.9 | 657.3 | 658.6 | 659.9 | 601.3 | 662.6 | 663.9 | $665 \cdot 3$ |
| 500 | 666.6 | 667.9 | 669.3 | 670.6 | 671.9 | 673.3 | 674.6 | 675.9 | 677.3 | 678.6 |
| 510 | 679.9 | 681.3 | 682.6 | 683.9 | 685.3 | 686.6 | 687.9 | 689.3 | 690.6 | 691.9 |
| 520 | 693.3 | 694.6 | 695.9 | $697 \cdot 3$ | 698.6 | 699.9 | 701.3 | 702.6 | 703.9 | 705.3 |
| 530 | 706.6 | 707.9 | 709.3 | 710.6 | 711.9 | 713.3 | 714.6 | 715.9 | 717.3 | 718.6 |
| 540 | 719.9 | 721.3 | 722.6 | 723.9 | $725 \cdot 3$ | 726.6 | 727.9 | 729.3 | 730.6 | 731.9 |
| 550 | 733.3 | 734.6 | 735.9 | 737.3 | 738.6 | 739.9 | 741.3 | 742.6 | 743.9 | $745 \cdot 3$ |
| 560 | 746.6 | 747.9 | 749.3 | 750.6 | 751.9 | 753.3 | 754.6 | 755.9 | 757.3 | 758.6 |
| 570 | 759.9 | 761.3 | 762.6 | 763.9 | 765.3 | 766.6 | 767.9 | 769.3 | 770.6 | 771.9 |
| 580 | 773.3 | 774.6 | 775.9 | 777.3 | 778.6 | 779.9 | 781.3 | 782.6 | 783.9 | 785.3 |
| 590 | 786.6 | 787.9 | 789.3 | 790.6 | 791.9 | $793 \cdot 3$ | 794.6 | 795.9 | $797 \cdot 3$ | 798.6 |
| 600 | 799.9 | 801.3 | 802.6 | 803.9 | 805.3 | 806.6 | 807.9 | 809.3 | 810.6 | 811.9 |
| 610 | 813.3 | 814.6 | 815.9 | 817.3 | 818.6 | 819.9 | 82 I .3 | 822.6 | 823.9 | 825.3 |
| 620 | 826.6 | 827.9 | 829.3 | 830.6 | 831.9 | 833.3 | 834.6 | 835.9 | 837.3 | 838.6 |
| 630 | 839.9 | 84 I .3 | 842.6 | 843.9 | $845 \cdot 3$ | 846.6 | 847.9 | 849.3 | 850.6 | 851.9 |
| 640 | 853.3 | 854.6 | 855.9 | 857.3 | 858.6 | 859.9 | 861.3 | 862.6 | 863.9 | 865.3 |
| 650 | 866.6 | 867.9 | 869.3 | 870.6 | 871.9 | 873.3 | 874.6 | 875.9 | 877.3 | 878.6 |
| 660 | 879.9 | 881.3 | 882.6 | 883.9 | 885.3 | 886.6 | 887.9 | 889.3 | 890.6 | 891.9 |
| 670 | 893.3 | 894.6 | 895.9 | 897.3 | 898.6 | 809.9 | 901.3 | 902.6 | 003.9 | 005.3 |
| 680 | 906.6 | 907.9 | 909.3 | 910.6 | 9II.9 | 913.3 | 914.6 | 915.9 | 917.3 | 918.6 |
| 690 | 919.9 | 921.3 | 922.6 | 923.9 | $925 \cdot 3$ | 926.6 | 927.9 | 929.3 | 930.6 | 931.9 |
| 700 | 933.3 | 934.6 | 935.9 | 937.3 | 938.6 | 939.9 | 941.3 | 942.6 | 943.9 | $045 \cdot 3$ |
| 710 | 946.6 | 947.9 | 949.3 | 950.6 | 951.9 | 953.3 | 954.6 | 955.9 | 957.3 | 958.6 |
| 720 | 959.9 | $96 \mathrm{t} \cdot 3$ | 962.6 | 963.9 | 905.3 | 966.6 | 967.9 | 969.3 | 970.6 | 971.9 |
| 730 | 973.3 | 974.6 | 975.9 | 977.3 | 978.6 | 979.9 | 981.3 | 982.6 | 983.9 | 985.3 |
| 740 | 986.6 | 987.9 | 989.3 | 990.6 | 991.9 | 993.3 | 994.6 | 995.9 | $997 \cdot 3$ | 998.6 |
| 750 | 999.9 | 1001.3 | 1002.6 | 100.3.9 | 1005.3 | 1006.6 | 1007.9 | 1009.3 | 1010.6 | 1011.9 |
| 760 | 1013.3 | 1014.6 | IO15.9 | 1017.2 | 1018.6 | IOI9.9 | 1021.2 | 1022.6 | 1023.9 | 1025.2 |
| 770 | 1026.6 | 1027.9 | 1029.2 | 1030.6 | 1031.9 | 1033.2 | 1034.6 | 1035.9 | 1037.2 | 1038.6 |
| 780 | 1039.9 | 1041.2 | 1042.6 | 1043.9 | 1045.2 | 1046.6 | 1047.9 | 1049.2 | 1050.6 | 1051.9 |
| 790 | 1053.2 | 1054.6 | 1055.9 | 1057.2 | 1058.6 | 1059.9 | 1061.2 | 1062.6 | 1063.9 | 1065.2 |

Smithsonian Tables.

1 foot $=03048006$ meter.

| Feet. | 0 | I | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | $\begin{gathered} \mathrm{m} . \\ \text { o.000 } \end{gathered}$ | m. $0.305$ | $\begin{aligned} & \mathrm{m} . \\ & 0.610 \end{aligned}$ | $\begin{gathered} 111 . \\ 0.914 \end{gathered}$ | m. $\text { I. } 219$ | m. $1.524$ | m. 1. 829 | $\begin{gathered} \mathrm{m} . \\ 2.134 \end{gathered}$ | $\mathrm{m} .$ $2.438$ | 11. |
| 10 | 3.045 | $3 \cdot 353$ | 3.658 | 3.962 | 4.267 | 4.572 | 4.877 | 5. IS2 | 5.486 | 5.791 |
| 20 | 6.096 | 6.401 | 6.706 | 7.010 | 7.315 | 7.620 | 7.925 | 8.230 | S. 534 | 8.839 |
| 30 | 9.14. | 9.449 | 9.754 | 10.058 | 10.363 | 10.668 | 10.973 | 11.278 | 11.582 | 11.887 |
| 40 | 12.192 | 12.497 | 12.SO2 | 13. 106 | 13.41 I | 13.716 | 14.02 I | 14.326 | 14.630 | 14.935 |
| 50 | I 5.240 | 15.545 | 15.550 | 16.154 | 16.459 | 16.764 | 17.069 | 17.374 | 17.678 | 17.983 |
| 60 | 18.288 | 18.593 | 18.898 | 19.202 | 19.507 | 19.812 | 20.117 | 20.422 | 20.726 | 21.03 I |
| 70 | 21.336 | 21.641 | 21.9.46 | 22.250 | 22.555 | 22.860 | 23.165 | 23.470 | 23.774 | 24.079 |
| So | 24.384 | 2.4.689 | 24.994 | 25.298 | 25.603 | 25.908 | 26.213 | 26.518 | 26.822 | 27.127 |
| 90 | 27.432 | 27.737 | 28.042 | 28.346 | 28.551 | 2 S .956 | 29.26I | 29.566 | 29.870 | 30.175 |
|  | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 |
| 100 | 30.48 | 33.53 | 36.58 | 39.62 | 42.67 | 45.72 | 48.77 | 51.82 | 54.86 | 57.91 |
| 200 | 60.96 | 6.4 .01 | 67.06 | 70.10 | 73.15 | 76.20 | 79.25 | 82.30 | S5.34 | S8. 39 |
| 300 | 91.44 | 94.49 | 97.54 | 100.58 | 103.63 | 106.68 | 109.73 | 112.78 | 115.82 | II 8.87 |
| 400 | 121.92 | 124.97 | 128.02 | 131.06 | 134.11 | 137.16 | 140.21 | 143.26 | 146.30 | 149.35 |
| 500 | 152.40 | 155.45 | 158.50 | 161.54 | 16.4 .59 | 167.64 | 170.69 | 173.74 | 176.78 | 179.83 |
| 600 | I S2. 88 | 185.93 | I88.98 | 192.02 | 195.07 | 198.12 | 201.17 | 204.22 | 207.26 | 210.31 |
| 700 | 213.36 | 216.41 | 219.46 | 222.50 | 225.55 | 228.60 | 231.65 | 234.70 | 237.74 | 240.79 |
| Soo | 243.84 | 246.89 | 249.94 | 252.98 | 256.03 | 259.08 | 262.13 | 265.18 | 268.22 | 271.27 |
| 900 | 274.32 | $277 \cdot 37$ | 280.42 | 283.46 | 286.51 | 289.56 | 292.61 | 295.66 | 298.70 | 301.75 |
| 1000 | 304.80 | 307.85 | 310.90 | 313.94 | 316.99 | 320.04 | 323.09 | 326.14 | 329.18 | 332.23 |
| 1100 | 335.28 | 338.33 | 341.38 | 344.42 | 347.47 | 350.52 | 353.57 | 356.62 | 359.67 | 362.71 |
| 1200 | 365.76 | 368. I $^{\text {I }}$ | 371.86 | 374.90 | 377.95 | 3 SI.00 | 384.05 | 387.10 | 390.14 | 393.19 |
| I 300 | 396.24 | 399.29 | 402.34 | 405.38 | 408.43 | 411.48 | 414.53 | 417.58 | 420.62 | 423.67 |
| 1400 | 426.72 | 429.77 | 432.82 | 435.86 | 438.91 | 441.96 | 445.01 | 448.06 | 451.10 | 454.15 |
| 1500 | 457.20 | 460.25 | 463.30 | 466.34 | 469.39 | 472.44 | 475.49 | 478.54 | 481.58 | 484.63 |
| 1600 | 487.68 | 490.73 | 493.78 | 496.82 | 499.87 | 502.92 | 505.97 | 509.02 | 512.07 | 515.11 |
| 1700 | 5 IS. 16 | 521.21 | 52.+. 26 | 527.3I | 530.35 | 533.40 | 536.45 | 539.50 | 542.55 | 545.59 |
| I Soo | 548.64 | 55 I .69 | 554.74 | 557.79 | 560.83 | 563.88 | 566.93 | 569.98 | 573.03 | 576.07 |
| 1900 | 579.12 | 582.17 | $5 \$ 5.22$ | 585.27 | 591.3I | 59+. 36 | 597.41 | 600.46 | 603.5 I | 606.55 |
| 2000 | 609.60 | 612.65 | 615.70 | 6IS. 75 | 621.79 | 62.4 .84 | 627.89 | 630.94 | 633.99 | 637.03 |
| 2100 | 640.08 | 643.13 | 646. IS | 649.23 | 652.27 | 655.32 | 658.37 | 66 I .42 | 66.4.47 | 667.51 |
| 2200 | 670.56 | 673.61 | 676.66 | 679.7 I | 682.75 | 685.80 | 688.55 | 691.90 | 694.95 | 697.99 |
| 2300 | 701.04 | 704.09 | 707.14 | 710.19 | 713.23 | 716.28 | 719.33 | 722.38 | 725.43 | 728.47 |
| 2400 | 731.52 | 734.57 | 737.62 | 740.67 | 743.71 | 746.76 | 749.81 | 752.86 | 755.91 | 758.95 |
| 2500 | 762.00 | 765.05 | 768.10 | 771.15 |  | 777.24 | 780.29 | 783.34 | 786.39 |  |
| 2600 | 792.48 | 795.53 | 798.58 | So1. 63 | SO4. 67 | 807.72 | SIO. 77 | SI3.82 | SI6.87 | S19.91 |
| 2700 | 822.96 | 826.01 | 829.06 | 832.11 | 835.15 | S3S. 20 | 841.25 | 844.30 | S47.35 | 850.39 |
| 2800 | 853.44 | S56.49 | S59.54 | 862.59 | 865.63 | 868.68 | 871.73 | S74.78 | S77.83 | S80. 87 |
| 2900 | S83.92 | S86.97 | S90.02 | S93.07 | S96.1 I | 899.16 | 902.21 | 905.26 | 908.31 | 911. 35 |
| 3000 | 914.40 | 917.45 | 920.50 | 923.55 | 926.59 | 929.64 | 932.69 | $935.74$ | 938.79 | $9+1.83$ |
| 3100 | 944.SS | 947.93 | 950.98 | 954.03 | 957.07 | 960. 12 | 963.17 | 966.22 | 969.27 | 972.31 |
| 3200 | 975.36 | 978.41 | 98 c .16 | 9S.4.5 1 | 987.55 | 990.60 | . 993.65 | 996.70 | 999.75 | 1002.79 |
| 3300 | 1005.84 | 1008.89 | IOII.94 | 1014.99 | 1018.03 | 1021.08 | 1024.13 | 1027.18 | 1030.23 | 1033.27 |
| 3400 | 1036.32 | 1039.37 | 1042.42 | 10.45 .47 | 1048.51 | 1051.56 | 1054.6I | 1057.66 | 1060.71 | 1063.75 |
| 3500 | 1066.80 | 1069.85 | I672.90 | 1075.95 | 1078.99 | 1082.04 | Io85.09 | 1088. 14 | 1091.19 | 1094.23 |
| 3600 | 1097.28 | 1100.33 | 1103.38 | 1106.43 | 1109.47 | II I 2.52 | 1115.57 | I I I 8.62 | I121.67 | 1124.71 |
| 3700 3800 | I 127.76 I I 58.24 | 1130.81 | 1133.86 | 1136.91 | 1139.95 | 1143.00 | 11.46 .05 | II 149.10 | II 52.15 | II 55.19 |
| 3800 3900 | II 58.24 | 1161.29 | 1164.34 | 1107.39 | 1170.43 | 1173.48 | I 1766.53 | II79.58 | 1182.63 | 1185.67 |
| 3900 | I IS8.72 | 1191.77 | 119.4 .82 | 1197.87 | 1200.91 | 1203.96 | 1207.(11 | 1210.06 | 1213.1I | 1216.15 |
| 4000 | 1219.20 | 1222.25 | 1225.30 | 1228.35 | 1231.39 | 1234.4.t | 1237.49 | I 240.54 | 12.43 .59 | 1246.63 |

FEET INTO METERS.
1 foot $=0.3048006$ meter.

| Feet. | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | m. | m. | m . | m. | m | 11. | m. | m. | m . | m. |
| 4000 | 1219.2 | 1222.3 | 1225.3 | I22S. 3 | 1231.4 | 1234.4 | 1237.5 | 1240.5 | I 243.6 | 12,46.6 |
| 4100 | 1249.7 | 1252.7 | 1255.8 | 125S.S | I26I.9 | 1264.9 | I268.0 | 1271.0 | 1274.1 | 1277. I |
| 4200 | I2SO. 2 | 1283.2 | 12S6.3 | I2S9.3 | 1292.4 | I 295.4 | 1298.5 | I301.5 | I304. 5 | I307.6 |
| 4300 | I310.6 | 1313.7 | I316.7 | 1319.8 | 1322.8 | 1325.9 | 1328.9 | 1332.0 | 1335.0 | 1338. 1 |
| 4400 | I34I. I | I 344.2 | I 347.2 | I 350.3 | I 353.3 | I 356.4 | 1359.4 | I362.5 | I 365.5 | 1368.6 |
| 4500 | 1371.6 | 1374.7 | 1 377.7 | 1380.7 | 1383.8 | I386.S | 1389.9 | I 392.0 | 1396.0 | I 399.0 |
| 4600 | 1402. 1 | 1405.1 | 1408.2 | 1411.2 | 1414.3 | 1417.3 | 1420.4 | 1423.4 | 1426.5 | 1429.5 |
| 4700 | 1432.6 | 1435.6 | I43S.7 | 1441.7 | I444.8 | I 447.8 | 1450.9 | I453.9 | 1456.9 | 1460.0 |
| 4800 | 1463.0 | 1466. I | 1469. I | I472.2 | 1475.2 | I 478.3 | 1481.3 | 1484.4 | 1487.4 | I490. 5 |
| 4900 | 1493.5 | 1496.6 | 1499.6 | I502.7 | I 505.7 | I 508.8 | I5II.S | 1514.9 | 1517.9 | 152 1. 0 |
| 5000 | I524.0 | 1527.1 | 1530.1 | 1533. 1 | 1536.2 | I539.2 | I 542.3 | I545.3 | I 5.48 .4 | 1551.4 |
| 5100 | I554.5 | I557.5 | 1560.6 | 1563.6 | I566.7 | I 569.7 | 1572.8 | I $575 . \mathrm{S}$ | I578.9 | I5SI. 9 |
| 5200 | I585.0 | 1588.0 | I591.I | I594. I | 1597.2 | 1600.2 | 1603.3 | 1606.3 | 1609.3 | 16I2.4 |
| 5300 | 1615.4 | 1618.5 | 1621.5. | I624.6 | 1627.6 | 1630.7 | 1633.7 | $1636 . S$ | I639.8 | 1642.9 |
| 5400 | 1645.9 | 16.49.0 | 1652.0 | 1655. I | 1658. I | 1661.2 | 1664.2 | 1667.3 | 1670.3 | 1673.4 |
| 5500 | 1676.4 | Iо́79.5 | I682.5 | 1685.5 | I688.6 | I691.6 | 1694.7 | 1697.7 | 1700.8 | 1703.8 |
| 5600 | I706.9 | 1709.9 | 1713.0 | 1716.0 | 1719.1 | 1722.1 | I725.2 | 1728.2 | 1731.3 | 1734.3 |
| 5700 | 1737.4 | 1740.4 | 1743.5 | 1746.5 | 1749.6 | 1752.6 | I755.7 | 1758.7 | 1761.7 | 1764.8 |
| 5800 | I767.8 | 1770.9 | I773.9 | 1777.0 | 1780.0 | I7S3. | I786. I | 1789.2 | 1792.2 | 1795.3 |
| 5900 | I798.3 | ISOI. 4 | ISO4.4 | ISO7.5 | 1810.5 | ISI3.6 | 1816.6 | 1519.7 | I822.7 | I 825.8 |
| 6000 | I828.8 | 1831.9 | 1834.9 | 1837.9 | 1841.0 | IS44.0 | I 847.1 | 1850. 1 | I 853.2 | IS56.2 |
| 6100 | IS59.3 | IS62.3 | IS65.4 | I 868.4 | 1871.5 | IS74.5 | IS77.6 | I880. 6 | IS83.7 | 1886.7 |
| 6200 | I889.8 | I892.8 | I895.9 | IS98.9 | 1902.0 | I905.0 | I908. I | I9II.I | I914.I | 1917.2 |
| 6300 | 1920.2 | 1923.3 | 1926.3 | 1929.4 | 1932.4 | 1935.5 | 1938.5 | 1941.6 | I944.6 | 1947.7 |
| 6.400 | 1950.7 | 1953.8 | I956.8 | 1959.9 | 1962.9 | 1966.0 | 1969.0 | 1972. I | 1975. I | 1978.2 |
| 6500 | I98I. 2 | I984.3 | 1987.3 | 1990.3 | 1993.4 | I996.4 | 1999.5 | 2002.5 | 2005.6 | 2008.6 |
| 6600 | 2011.7 | 2014.7 | 2017.8 | 2020.8 | 2023.9 | 2026.9 | 2030.0 | 2033.0 | 2036. I | 2039. I |
| 6700 | 2042.2 | 2045.2 | 204S.3 | 2051.3 | 2054.4 | 2057.4 | 2060.5 | 2063.5 | 2066.5 | 2069.6 |
| 6800 | 2072.6 | 2075.7 | 2078.7 | 2081. 8 | 2084.8 | 2087.9 | 2090.9 | 2094.0 | 2097.0 | 2100.1 |
| 6900 | 2103.1 | 2106.2 | 2109.2 | 2 I12.3 | 2115.3 | 2118.4 | 2 I 21.4 | 2124.5 | $2127 \cdot 5$ | 2130.6 |
| 7000 | 2133.6 | 2136.7 | 2139.7 | 2 I42.7 | 2145.8 | 2148.8 | 2 I5 I. 9 | 2154.9 | 2158.0 | 216 I .0 |
| 7100 | 2164.1 | 2167.1 | 2170.2 | 2173.2 | 2176.3 | 2179.3 | 2182.4 | 2185.4 | 2188.5 | 2 I91. 5 |
| 7200 | 2194.6 | 2197.6 | 2200.7 | 2203.7 | 2206.8 | 2209.8 | 2212.9 | 2215.9 | 2218.9 | 2222.0 |
| 7300 | 2225.0 | 2228. 1 | 2231.I | 2234.2 | 2237.2 | 2240.3 | 2243.3 | 2246.4 | 2249.4 | 2252.5 |
| 7400 | 2255.5 | 2258.6 | 2261.6 | 2264.7 | 2267.7 | 2270.8 | 2273.8 | 2276.9 | 2279.9 | 2283.0 |
| 7500 | 2286.0 | 2289. 1 | 2292.I | 2295. I | 2298.2 | 2301.2 | 2304.3 | 2307.3 | 2310.4 | 2313.4 |
| 7600 | 2316.5 | 2319.5 | 2322.6 | 2325.6 | 2328.7 | 2331.7 | 2334.8 | 2337.8 | 2340.9 | 2343.9 |
| 7700 | 2347.0 | 2350.0 | 2353. 1 | 2356. I | 2359.2 | 2362.2 | 2365.3 | 2368.3 | 2371.3 | 2374.4 |
| 7800 | 2377.4 | 23 So. 5 | 2383.5 | 2386.6 | 2389.6 | 2392.7 | 2395.7 | 2398.8 | 2401.8 | 2404.9 |
| 7900 | 2407.9 | 2411.0 | 2414.0 | 2417.1 | 2420. I | 2423.2 | 2426.2 | 2429.3 | 2432.3 | 2435.4 |
| 8000 | 2438.4 | 2441.5 | 2444.5 | 2447.5 | 2450.6 | 2453.6 | 2.456 .7 | 2459.7 | 2462.8 | 2465.8 |
| 8100 | 2.468 .9 | 2471.9 | 2.475 .0 | 2478.0 | 24SI. I | 2484. I | 2487.2 | 2.490 .2 | 2493.3 | 2496.3 |
| S200 | 2499.4 | 2502.4 | 2505.5 | 2508.5 | 2511.6 | 2514.6 | 2517.7 | 2520.7 | 2523.7 | 2526.8 |
| 8300 | 2529.8 | 2532.9 | 2535.9 | 2539.0 | 2542.0 | 2545. I | 254S.I | 2551.2 | 2554.2 | 2557.3 |
| S400 | 2560.3 | 2563.4 | 2566.4 | 2569.5 | 2572.5 | 2575.6 | 2578.6 | 25 SI .7 | 2584.7 | 2587.8 |
| 8500 | 2590.8 | 2593.9 | 2596.9 | 2599.9 | 2603.0 | 2606.0 | 2609. 1 | 2612.1 | 2615.2 | 2618.2 |
| 8600 | 262 I. 3 | 2624.3 | 2627.4 | 2630.4 | 2633.5 | 2636.5 | 2639.6 | 26.42 .6 | 2645.7 | 2648.7 |
| S700 | 2651.8 | 2654.8 | 2657.9 | 2660.9 | 2664.0 | 2667.0 | 2670. I | 2673.1 | 2676.1 | 2679.2 |
| SSOO | 2682.2 | 2685.3 | 2688.3 | 2691.4 | 2694.4 | 2697.5 | 2700.5 | 2703.6 | 2706.6 | 2709.7 |
| 8900 | 2712.7 | 2715.8 | 2718.8 | 2721.9 | 2724.9 | 2728.0 | 2731.0 | 2734.1 | 2737. 1 | 2740.2 |
| 9000 | 2743.2 | 2746.3 | 2749.3 | 2752.3 | 2755.4 | 2758.4 | 2761.5 | 2764.5 | 2767.6 | 2770.6 |

Table 14.
METERS INTO FEET.
I meter $=39.3700$ inches $=3.280833$ feet.

| Meters. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| 0 | 0.00 | 3.28 | 6.56 | 9.84 | 13.12 | 16.40 | 19.68 | 22.97 | 26.25 | 29.53 |
| 10 | 32.81 | 36.09 | 39.37 | 42.65 | 45.93 | 49.21 | 52.49 | 55.77 | 59.05 | 62.34 |
| 20 | 65.62 | 68.90 | 72.18 | 75.46 | 78.74 | S2.02 | S5.30. | S8.58 | 91. 86 | 95.14 |
| 30 | 98.42 | 101.71 | 104.99 | 108.27 | II I. 55 | 114.83 | IIS.II | 121.39 | 124.67 | 127.95 |
| 40 | I 31.23 | I34.5 | 137.79 | 141.08 | 144.36 | 147.64 | 150.92 | 154.20 | 157.48 | 160.76 |
| 50 | 164.04 | 167.32 | 170.60 | 173.88 | 177.16 | ISo. 45 | 183.73 | 187.01 | 190.29 | 193.57 |
| 60 | 196.85 | 200.13 | 203.41 | 206.69 | 209.97 | 213.25 | 216.53 | 219.82 | 223.10 | 226.38 |
| 70 | 229.66 | 232.94 | 236.22 | 239.50 | 2.42 .78 | 246.06 | 249.34 | 252.62 | 255.90 | 259.19 |
| So | 262.47 | 265.75 | 269.03 | 272.31 | 275.59 | 278.87 | 282.15 | 285.43 | 288.71 | 291.99 |
| 90 | 295.27 | 298.56 | 301.84 | 305.12 | 308.40 | 311.68 | 314.96 | 318.24 | 32 I .52 | 324.80 |
| 100 | 328.08 | 331.36 | 334.64 | 337.93 | $3+1.21$ | 344.49 | 347.77 | 351.05 | 354.33 | 357.61 |
| 110 | 360.89 | 364.17 | 367.45 | 370.73 | 374.01 | 377.30 | 3 So. 58 | 383.86 | 357.14 | 390.42 |
| 120 | 393.70 | 396.98 | 400.26 | 403.54 | 406.82 | 410.10 | 413.38 | 416.67 | 419.95 | 423.23 |
| 130 | 426.51 | 429.79 | 433.07 | 436.35 | 439.63 | 442.91 | 446.19 | 449.47 | 452.75 | 456.04 |
| 140 | 459.32 | 462.60 | 465.85 | 469.16 | 472.44 | 475.72 | 479.00 | 482.28 | 485.56 | 488.84 |
| 150 | 492.12 | 495.41 | 498.69 | 501.97 | 505.25 | 508.53 | 5II.SI | 515.09 | 518.37 | 521.65 |
| 160 | 524.93 | 528.21 | 531.49 | 534.78 | 538.06 | 541.34 | 54.62 | 547.90 | 551.18 | 554.46 |
| 170 | 557.74 | 561.02 | 564.30 | 567.58 | 570.86 | 574.15 | 577.43 | 580.71 | 583.99 | 587.27 |
| I So | 590.55 | 593.83 | 597.II | 600.39 | 603.67 | 606.95 | 610.23 | 613.52 | 616.80 | 620.08 |
| 190 | 623.36 | 626.64 | 629.92 | 633.20 | 636.48 | 639.76 | 643.04 | 646.32 | 649.60 | 652.89 |
| 200 | 656.17 | 659.45 | 662.73 | 666.01 | 669.29 | 672.57 | 675.85 | 679.13 | 682.41 | 685.69 |
| 210 | 688.97 | 692.26 | 695.54 | 698.82 | 702.10 | 705.38 | 708.66 | 711.94 | 715.22 | 718.50 |
| 220 | 721.78 | 725.06 | 728.34 | 731.63 | 734.91 | 738.19 | 741.47 | 744.75 | 748.03 | 751.3 J |
| 230 | 754.59 | 757.87 | $76 \pm .15$ | 764.43 | 767.71 | 771.00 | 774.28 | 777.56 | 780.84 | 784.12 |
| 240 | 787.40 | 790.68 | 793.96 | 797.24 | Soo. 52 | So3.So | So7.08 | Sio. 37 | 813.65 | SI6.93 |
| 250 | S20.2 1 |  | S26.77 | S30.05 | S33.33 | S36.6I | S39.89 | S43.17 | S46.45 | 849.74 |
| 260 | S53.02 | S56.30 | 859.5S | 862.56 | 866.14 | S69.42 | 872.70 | 875.98 | S79.26 | S82.54 |
| 270 | S85.82 | S89.11 | S92.39 | S95.67 | S9S.95 | 902.23 | 905.51 | 908.79 | $9^{1} 2.07$ | 915.35 |
| 2 So | 918.63 | 921.91 | 925.19 | $92 \mathrm{S.4S}$ | 931.76 | 935.04 | 938.32 | 941.60 | 944.58 | 948.16 |
| 290 | 951.44 | 954.72 | 958.00 | 96 I .28 | 96.4.56 | 967.85 | 971.13 | 974.41 | 977.69 | 980.97 |
| 300 | 9S4. 25 | 987.53 | 990.81 | 994.09 | 997.37 | 1000.65 | 1003.93 | 1007.22 | 1010.50 | 1013.78 |
| 310 | 1017.06 | 1020.34 | 1023.62 | 1026.90 | 1030.18 | 1033.46 | 1036.74 | 1040.02 | 1043.30 | 1046.59 |
| 320 | 1049.87 | 1053.15 | 1056.43 | 1059.71 | 1062.99 | 1066.27 | 1069.55 | 1072.83 | 1076.11 | 1079.39 |
| 330 | IoS2.67 | 1085.96 | 1089.24 | 1092.52 | 1095.80 | 1099.08 | I IO2.36 | 1105.64 | I 109.92 | I I 12.20 |
| 340 | 1115.48 | 1118.76 | II 22.04 | I 125.33 | I I28.6I | 1131.89 | I 135.17 | 1138.45 | 1141.73 | I 1 45.01 |
| 350 | 1148.29 | 1151.57 | 1154.85 | 1158.13 | II 61.41 | 1164.70 | 1167.98 | II7 7.26 | I 174.54 | 1177.82 |
| 360 | 1181.10 | 1184.38 | II 87.66 | I 190.94 | 1194.22 | 1197.50 | 1200.78 | 1204.07 | 1207.35 | 1210.63 |
| 370 | 1213.91 | 1217.19 | 1220.47 | 1223.75 | 1227.03 | 1230.31 | 1233.59 | 1236.87 | I240.15 | I 243.44 |
| 380 | 1246.72 | 1250.00 | 1253.28 | 1256.56 | 1259.S4 | 1263.12 | I266.40 | 1269.68 | 1272.96 | 1276.24 |
| 390 | 1279.52 | 1282.81 | 1286.09 | 1289.37 | 1292.65 | 1295.93 | 1299.21 | I 302.49 | 1305.77 | 1309.05 |
| 400 | 1312.33 | 1315.61 | I318.S9 | 1322.18 | 1325.46 | 1328.74 | 1332.02 | 1335.30 | 1338.58 | I 341.86 |
| 410 | 1345.14 | 1348.42 | 1351.70 | 1354.98 | 1358.26 | 1361.55 | 1364.83 | I368.1 I | I371.39 | 1374.67 |
| 420 | 1377.95 | 1381.23 | I 3 S4.51 | 1387.79 | I 391.07 | ${ }^{1} 394.35$ | 1397.63 | I 400.92 | 1404.20 | 1407.48 |
| 430 | 1410.76 | 1414.04 | 1417.32 | 1420.60 | 1423.88 | I 427.16 | 1430.44 | 1433.72 | 1437.00 | 1440.29 |
| 440 | [443.57 | I446.85 | 1450.13 | 1453.41 | I456.69 | I 459.97 | 1463.25 | I 466.53 | I469.81 | 1473.09 |
| 450 | 1476.37 | 1479.66 | 1482.94 | 1486.22 | I4S9.50 | 1492.78 | 1496.06 | I 499.34 | 1502.62 | 1505.90 |
| 460 | I509.18 | 1512.46 | 1515.74 | 1519.03 | I522.31 | 1525.59 | 1528.87 | I532.15 | 1535.43 | 1538.71 |
| 470 | I 541 I .99 | I545.27 | I 548.55 | 1551.83 | I555. I I | ${ }^{1} 558.40$ | 1561.68 | I564.96 | 1568.24 | 1571.52 |
| 4 So | [574.80 | 1578.08 | I5SI. 36 | 1584.64 | 1587.92 | 1591.20 | 1594.48 | 1597.77 | 1601.05 | 1604.33 |
| $49^{\circ}$ | 1607.61 | 1610.89 | 1614.17 | 1617.45 | 1620.73 | 162.4.01 | 1627.29 | 1630.57 | 1633.85 | 1637.14 |
| 500 | 16.40.42 | 1643.70 | 1646.98 | 1650.26 | 1653.54 | 1656.82 | 1660.10 | 1663.38 | 1660.66 | 1669.94 |

METERS INTO FEET.
I meter $=39.3700$ inches $=3280833$ feet.


Table 15.
MILES INTO KILOMETERS.
I mile $=1.609347$ kilometers.

| Miles. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | km . | km . | km . | 上m. | km . | km . | km . | km . | km . | km |
| 0 | 0 | 2 | 3 | 5 | 6 | 8 | 10 | II | 13 | 14 |
| 10 | 16 | IS | 19 | 21 | 23 | 24 | 26 | 27 | 29 | 31 |
| 20 | 32 | 34 | 35 | 37 | 39 | 40 | 42 | 43 | 45 | 47 |
| 30 | 48 | 50 | 5 I | 53 | 55 | 56 | 58 | 60 | 61 | 63 |
| 40 | 64 | 66 | 68 | 69 | 71 | 72 | 74 | 76 | 77 | 79 |
| 50 | So | S2 | 84 | S5 | 87 | S9 | 90 | 92 | 93 | 95 |
| 60 | 97 | 98 | 100 | IOI | 103 | 105 | 106 | 108 | 109 | 111 |
| 70 | I 13 | 114 | 116 | II7 | II9 | 121 | 122 | 124 | 126 | 127 |
| So | 129 | 130 | 132 | 134 | 135 | 137 | 13 S | 140 | 142 | 143 |
| 90 | 145 | 146 | 148 | 150 | 151 | 153 | 154 | 156 | 158 | 159 |
| 100 | 161 | 163 | 164 | 166 | 167 | 169 | 171 | 172 | 174 | 175 |
| 1 Io | 177 | 179 | 180 | 182 | $\mathrm{IS}_{3}$ | 185 | 187 | ISS | 190 | 192 |
| 120 | 193 | 195 | 196 | 198 | 200 | 201 | 203 | 204 | 206 | 208 |
| 130 | 209 | 2 II | 212 | 214 | 216 | 217 | 219 | 220 | 222 | 224 |
| 140 | 225 | 227 | 229 | 230 | 232 | 233 | 235 | 237 | 23 S | 240 |
| 150 | 241 | 243 | 245 | 246 | 248 | 249 | 251 | 253 | 254 | 256 |
| 160 | 257 | 259 | 261 | 262 | 26.4 | 266 | 267 | 269 | 270 | 272 |
| 170 | 274 | 275 | 277 | 278 | 2 So | 2 S 2 | $2 S_{3}$ | 2 S 5 | 286 | 2 SS |
| ISo | 290 | 291 | 293 | 295 | 296 | 298 | 299 | 301 | 303 | 304 |
| 190 | 306 | 307 | 309 | 311 | 312 | 314 | 315 | 317 | 319 | 320 |
| 200 | 322 | 323 | 325 | 327 | 328 | 330 | 332 | 333 | 335 | 336 |
| 210 | 338 | 340 | 341 | 343 | 344 | 346 | 348 | 349 | 351 | 352 |
| 220 | 354 | 356 | 357 | 359 | 360 | 362 | 364 | 365 | 367 | 369 |
| 230 | 370 | 372 | 373 | 375 | 377 | 378 | 380 | 381 | 383 | 385 |
| 240 | 386 | 388 | 389 | 391 | 393 | 394 | 396 | 398 | 399 | 401 |
| 250 | 402 | 404 | 406 | 407 | 409 | 410 | 412 | 414 | 415 | 417 |
| 260 | 418 | 420 | 422 | 423 | 425 | 426 | 428 | 430 | 431 | 433 |
| 270 | 435 | 436 | 438 | 439 | 44 I | 443 | 444 | 446 | 447 | 449 |
| 280 | 45 I | 452 | 454 | 455 | 457 | 459 | 460 | 462 | 463 | 465 |
| 290 | 467 | 468 | 470 | 472 | 473 | 475 | 476 | 478 | 480 | 481 |
| 300 | 483 | 484 | 486 | 488 | 489 | 491 | $49^{2}$ | 494 | 496 | 497 |
| 310 | 499 | 501 | 502 | 504 | 505 | 507 | 509 | 510 | 512 | 5 I 3 |
| 320 | 515 | 517 | 518 | 520 | 52 I | 523 | 525 | 526 | 528 | 529 |
| 330 | 531 | 533 | 534 | 536 | 538 | 539 | 54 I | 542 | 544 | 546 |
| 340 | 547 | 549 | 550 | 552 | 554 | 555 | 557 | 558 | 560 | 562 |
| 350 | 563 | 565 | 566 | 568 | 570 | 571 | 573 | 575 | 576 | 578 |
| 360 | 579 | 581 | 583 | 584 | 5 56 | 587 | 589 | 591 | 592 | 594 |
| 370 | 595 | 597 | 599 | 600 | 602 | 604 | 605 | 607 | 608 | 610 |
| 380 | 6 I 2 | 613 | 6 I 5 | 616 | 618 | 620 | 62 I | 623 | 624 | 626 |
| 390 | 628 | 629 | 631 | 632 | 634 | 636 | 637 | 639 | 64 I | 642 |
| 400 | 644 | 645 | 647 | 649 | 650 | 652 | 653 | 655 | 657 | 658 |
| 410 | 660 | 661 | 663 | 665 | 666 | 668 | 669 | 67 I | 673 | 674 |
| 420 | 676 | 678 | 679 | 681 | 682 | -684 | 656 | 687 | 689 | 690 |
| 430 | 692 | 694 | 695 | 697 | 698 | 700 | 702 | 703 | 705 | 706 |
| 440 | 708 | 710 | 711 | 713 | 715 | 716 | 718 | 719 | 721 | 723 |
| 450 | 724 | 726 | 727 | 729 | 731 | 732 | 734 | 735 | 737 | 739 |
| 460 | 740 | 742 | 744 | 745 | 747 | 748 | 750 | 752 | 753 | 755 |
| 470 | 756 | 758 | 760 | 761 | 763 | 764 | 766 | 768 | 769 | 771 |
| 480 | 772 | 774 | 776 | 778 | 779 | 781 | ${ }_{7} 82$ | ${ }_{7} 84$ | 785 | 787 |
| 490 | 789 | 790 | 792 | 793 | 795 | 797 | 798 | Soo | 801 | 803 |
| 500 | So5 | So6 | So8 | So9 | SII | SI3 | SI4 | Si6 | SIS | 819 |
| 510 | 82 I | 822 | S24 | S26 | S27 | S29 | S30 | 832 | S34 | S35 |
| 520 | 837 | 838 | 840 | S42 | 843 | 845 | 847 | 848 | S50 | 851 |
| 530 | 853 | 855 | 856 | S58 | S59 | 861 | 863 | S64 | 866 | 867 |
| 540 | S69 | 871 | 572 | 874 | 875 | 877 | 879 | 880 | 882 | S84 |
| 550 | SS5 | 887 | 888 | S90 | S92 | S93 | S95 | S96 | S98 | 900 |


| Miles. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | km . | km. | km . | km . | km . | km . | km. | km. | km . | km. |
| 550 | 885 | 887 | 8SS | 890 | 892 | S93 | S95 | S96 | S9S | 900 |
| 560 | 901 | 903 | 904 | 906 | 908 | 909 | 911 | 912 | 914 | 916 |
| 570 | 917 | 919 | 921 | 922 | 924 | 925 | 927 | 929 | 930 | 932 |
| 580 | 933 | 935 | 937 | 938 | 940 | 941 | 943 | 945 | 946 | 948 |
| 590 | 950 | 951 | 953 | 954 | 956 | 958 | 959 | 961 | 962 | 964 |
| 600 | 966 | 967 | 969 | 970 | 972 | 974 | 975 | 977 | 978 | 9So |
| 610 | 982 | 983 | 955 | 987 | 988 | 990 | 991 | 993 | 995 | 996 |
| 620 | 998 | 999 | 1001 | 1003 | 1004 | 1006 | 1007 | 1009 | IOII | 1012 |
| 630 | 1014 | 1015 | 1017 | 1019 | 1020 | 1022 | 1024 | 1025 | 1027 | 1028 |
| 640 | 1030 | 1032 | 1033 | 1035 | 1036 | 1038 | 1040 | 1041 | 1043 | 1044 |
| 650 | 1046 | 1048 | 1049 | 1051 | 1053 | 1054 | 1056 | 1057 | 1059 | 1061 |
| 660 | 1062 | 1064 | 1065 | 1067 | 1069 | 1070 | 1072 | 1073 | 1075 | 1077 |
| 670 | 1078 | 1080 | 1081 | 1083 | Io85 | IoS6 | IoS8 | 1090 | 1091 | 1093 |
| 680 | 1094 | 1096 | IogS | 1099 | I 1101 | I IO2 | 1104 | 1106 | 1107 | 1109 |
| 690 | IIIO | III 2 | III4 | I II5 | III7 | IIIS | 1120 | I 122 | 1123 | 1125 |
| 700 | 1127 | 1128 | 1130 | II3I | 1133 | I 135 | 1136 | 1138 | 1139 | 1141 |
| 710 | 1143 | 1144 | II46 | 1147 | I 149 | 1151 | 1152 | II54 | I 156 | 1157 |
| 720 | I 159 | 1160 | 1162 | 1164 | 1165 | 1167 | 1168 | II70 | 1172 | 1173 |
| 730 | II 75 | 1176 | 1178 | IISo | IISI | 1183 | 1184 | I IS6 | I ISS | 1189 |
| 740 | 1191 | 1193 | II94 | 1196 | I 197 | 1199 | 1201 | 1202 | 1204 | 1205 |
| 750 | 1207 | 1209 | 1210 | 1212 | 1213 | 1215 | 1217 | 1218 | 1220 | 1221 |
| 760 | 1223 | 1225 | 1226 | 1228 | 1230 | 1231 | 1233 | 1234 | 1236 | 1238 |
| 770 | 1239 | 1241 | 1242 | I 244 | 1246 | 1247 | 1249 | 1250 | 1252 | 1254 |
| 780 | 1255 | 1257 | 1259 | 1260 | 1262 | 1263 | 1265 | 1267 | 1268 | 1270 |
| 790 | 1271 | 1273 | 1275 | 1276 | 1278 | 1279 | 12 SI | 1283 | 1284 | 1286 |
| 800 | 1287 | 1289 | 1291 | 1292 | 1294 | 1296 | 1297 | 1299 | 1300 | 1302 |
| 810 | 1304 | 1305 | 1307 | 1308 | 1310 | 1312 | 1313 | I315 | ${ }^{1} 316$ | 1318 |
| 820 | 1320 | 1321 | 1323 | I 324 | 1326 | 1328 | I329 | 1331 | 1333 | 1334 |
| 830 | 1336 | 1337 | 1339 | 1341 | 1342 | I 344 | ${ }^{1} 345$ | 1347 | 1349 | 1350 |
| 840 | 1352 | I 353 | 1355 | 1357 | 1358 | I360 | I362 | 1363 | 1365 | 1366 |
| 850 | 1368 | 1370 | 1371 | 1373 | I374 | 1376 | 1378 | 1379 | I3SI | 1382 |
| 860 | 1384 | ${ }_{1} 386$ | 1387 | 1389 | I 390 | I 392 | 1394 | 1395 | I 397 | 1399 |
| 870 | 1400 | 1402 | 1403 | 1405 | 1407 | 1408 | 1410 | 1411 | 1413 | 1415 |
| 88o | 1416 | 1418 | 1419 | 1421 | 1423 | I424 | 1426 | 1427 | 1429 | 1431 |
| 890 | 1432 | 1434 | 1436 | 1437 | 1439 | 1440 | 1442 | 1444 | 1445 | 1447 |
| 900 | 1448 | 1450 | 1452 | 1453 | 1455 | 1456 | 1458 | 1460 | 1461 | 1463 |
| 910 | 1464 | 1466 | 1468 | 1469 | 1471 | 1473 | 1474 | 1476 | 1477 | 1479 |
| 920 | 1481 | 1482 | 1484 | 1485 | 1487 | 1489 | 1490 | 1492 | 1493 | 1495 |
| 930 | 1497 | 1498 | 1500 | 1502 | 1503 | 1505 | 1506 | 1508 | 1510 | 1511 |
| 940 | 1513 | I5I4 | 1516 | ${ }_{1518}$ | 1519 | 1521 | ${ }^{1} 522$ | ${ }^{1} 524$ | 1526 | 1527 |
| 950 | 1529 | 1530 | 1532 | I534 | 1535 | 1537 | 1539 | I540 | 1542 | 1543 |
| 960 | I 545 | I547 | ${ }^{1} 548$ | I 550 | 155 | 1553 | 1555 | ${ }^{1} 556$ | 155 S | 1559 |
| 970 | 1561 | 1563 | I564 | 1566 | 1567 | 1569 | 1571 | 1572 | 1574 | ${ }^{1} 576$ |
| 980 | I 577 | 1579 | 1580 | 1582 | 1.55 | 1585 | 1587 | 1588 | 1590 | 1592 |
| 990 | I 593 | ${ }^{1} 595$ | 1596 | 1598 | 1600 | 1601 | 1603 | 1605 | 1606 | 1608 |
| 1000 | 1609 | 161I | 1613 | 1614 | 1616 | 16ヶ7 | 1619 | 1621 | I622 | 1624 |
|  | Miles. | km . |  |  |  | iles. | km . | Miles. | km . |  |
|  | 1000 | 1609 |  |  |  | 000 | 17703 | 16000 | 25750 |  |
|  | 2000 | 3219 |  |  |  | 000 | 19312 | 17000 | 27359 |  |
|  | 3000 | 4828 |  |  |  | 000 | 20922 | 18000 | 28968 |  |
|  | 4000 | 6437 |  |  |  | 000 | 22531 | 19000 | 30578 |  |
|  | 5000 | So47 | 100 |  |  | 000 | 24140 | 20000 | 32187 |  |

Table 16.
KILOMETERS INTO MILES.
I kilometer $=0.621370 \mathrm{mile}$.

| Kilometers. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Miles. | Miles. | Miles. | Miles. | Miles. | Miles. | Miles. | Miles. | Miles. | Miles. |
| 0 | 0.0 | 0.6 | 1.2 | 1.9 | 2.5 | 3.1 | $3 \cdot 7$ | $4 \cdot 3$ | 5.0 | 5.6 |
| 10 | 6.2 | 6.8 | 7.5 | 8.1 | 8.7 | 9.3 | 9.9 | 10.6 | II. 2 | I 1.8 |
| 20 | I2.4 | 13.0 | 13.7 | 14.3 | 14.9 | 15.5 | 16.2 | 16.8 | 17.4 | IS.0 |
| 30 | 18.6 | 19.3 | 19.9 | 20.5 | 21.1 | 21.7 | 22.4 | 23.0 | 23.6 | 24.2 |
| 40 | 24.9 | 25.5 | 26. 1 | 26.7 | 27.3 | 28.0 | 28.6 | 29.2 | 29.8 | 30.4 |
| 50 | 3 I. I | 31.7 | 32.3 | 32.9 | 33.6 | 34.2 | 34.8 | 35.4 | 36.0 | 36.7 |
| 60 | 37.3 | 37.9 | 38.5 | 39.1 | 39.8 | 40.4 | 41.0 | 4 I .6 | 42.3 | 42.9 |
| 70 | 43.5 | 44.1 | 44.7 | 45.4 | 46.0 | 46.6 | 47.2 | 47.8 | 48.5 | 49. I |
| So | 49.7 | 50.3 | 51.0 | 51.6 | 52.2 | 52.8 | 53.4 | 54.1 | 54.7 | $55 \cdot 3$ |
| 90 | 55.9 | 56.5 | 57.2 | 57.8 | 58.4 | 59.0 | 59.7 | 60.3 | 60.9 | 61.5 |
| 100 | 62.1 | 62.8 | 63.4 | 64.0 | 64.6 | 65.2 | 65.9 | 66.5 | 67.1 | 67.7 |
| 110 | 68.4 | 69.0 | 69.6 | 70.2 | 70.8 | 71.5 | 72.1 | 72.7 | 73.3 | 73.9 |
| 120 | 74.6 | 75.2 | 75.8 | 76.4 | 77.0 | 77.7 | 78.3 | 78.9 | 79.5 | 80.2 |
| 130 | So. 8 | 8 SI .4 | 82.0 | S2.6 | 83.3 | 83.9 | 84.5 | 85. 1 | 85.7 | 86.4 |
| 140 | 87.0 | 87.6 | 88.2 | 88.9 | S9.5 | 90. I | 90.7 | 91.3 | 92.0 | 92.6 |
| 150 | 93.2 | 93.8 | 94.4 | 95. I | 95.7 | 96.3 | 96.9 | 97.6 | 98.2 | 98.8 |
| 160 | 99.4 | 100.0 | 100.7 | 101.3 | 101.9 | 102.5 | 103.I | 103.8 | 104.4 | 105.0 |
| 170 | 105.6 | 106.3 | 106.9 | 107.5 | 108. I | 108.7 | 109.4 | I 10.0 | 110.6 | III. 2 |
| ISo | III. 8 | 112.5 | II3.I | II3.7 | II4.3 | 115.0 | 115.6 | 116.2 | 116.8 | 117.4 |
| 190 | 118.1 | 118.7 | 119.3 | 119.9 | 120.5 | 121.2 | 121.8 | 122.4 | 123.0 | 123.7 |
| 200 | 124.3 | 124.9 | 125.5 | 126. I | 126.8 | I27.4 | 128.0 | 128.6 | 129.2 | 129.9 |
| 210 | 130.5 | 131.r | 131.7 | 132.4 | 133.0 | 133.6 | 134.2 | 134.8 | 135.5 | 136. 1 |
| 220 | 136.7 | 137.3 | I 37.9 | I 38.6 | I 39.2 | I 39.8 | 140.4 | I41.1 | 141.7 | 142.3 |
| 230 | I 42.9 | 143.5 | I44.2 | I 44.8 | 145.4 | I46.0 | 146.6 | I 47.3 | 147.9 | 148.5 |
| 240 | 149.1 | 149.8 | I50.4 | I51.0 | ${ }^{1} 51.6$ | I52.2 | I 52.9 | ${ }^{1} 53.5$ | 154. I | 154.7 |
| 250 | 155.3 | 156.0 | 156.6 | 157.2 | 157.8 | 158.4 | 159.1 | 159.7 | 160.3 | 160.9 |
| 260 | 161.6 | 162.2 | 162.8 | 163.4 | 164.0 | 164.7 | 165.3 | 165.9 | 166.5 | 167.1 |
| 270 | 167.8 | 168.4 | 169.0 | 169.6 | 170.3 | 170.9 | 171.5 | 172.1 | 172.7 | 173.4 |
| 280 | 174.0 | 174.6 | 175.2 | 175.8 | 176.5 | 177.1 | 177.7 | 178.3 | 179.0 | 179.6 |
| 290 | ISo. 2 | 180.8 | I81.4 | IS2. I | 182.7 | 183.3 | 183.9 | I 84.5 | 185.2 | 185.8 |
| 300 | 186.4 | 187.0 | 187.7 | I88.3 | I88.9 | 189.5 | 190. I | 190.8 | 191.4 | 192.0 |
| 310 | 192.6 | 193.2 | 193.9 | 194.5 | 195.I | 195.7 | 196.4 | 197.0 | 197.6 | 198.2 |
| 320 | 198.8 | 199.5 | 200. I | 200.7 | 201.3 | 201.9 | 202.6 | 203.2 | 203.8 | 204.4 |
| 330 | 205. I | 205.7 | 206.3 | 206.9 | 207.5 | 208.2 | 203.8 | 209.4 | 210.0 | 210.6 |
| 340 | 211.3 | 211.9 | 212.5 | 213.1 | 213.8 | 214.4 | 215.0 | 215.6 | 216.2 | 216.9 |
| 350 | 217.5 | 218.1 | 218.7 | 219.3 | 220.0 | 220.6 | 221.2 | 221.8 | 222.5 | 223. I |
| 360 | 223.7 | 224.3 | 224.9 | 225.6 | 226.2 | 226.8 | 227.4 | 228.0 | 228.7 | 229.3 |
| 370 | 229.9 | 230.5 | 23 I .1 | 231.8 | 232.4 | 233.0 | 233.6 | 234.3 | 234.9 | 235.5 |
| 380 | 236.1 | 236.7 | 237.4 | 238.0 | 238.6 | 239.2 | 239.8 | 240.5 | 241.1 | 241.7 |
| 390 | 242.3 | 243.0 | 243.6 | 244.2 | 244.8 | $245 \cdot 4$ | 246.1 | 2.46 .7 | 247.3 | 247.9 |
| 400 | 248.5 | 249.2 | 249.8 | 250.4 | 251.0 | 251.7 | 252.3 | 252.9 | 253.5 | 254.1 |
| 410 | 254.8 | 255.4 | 256.0 | 256.6 | 257.2 | 257.9 | 258.5 | 259. I | 259.7 | 260.4 |
| 420 | 261.0 | 261.6 | 262.2 | 262.8 | 263.5 | 264. I | 264.7 | 265.3 | 265.9 | 266.6 |
| 430 | 267.2 | 267.8 | 268.4 | 269. I | 269.7 | 270.3 | 270.9 | 271.5 | 272.2 | 272.8 |
| 440 | 273.4 | 274.0 | 254.6 | 275.3 | 275.9 | 276.5 | 277.1 | 277.8 | 278.4 | 279.0 |
| 450 | 279.6 | 280.2 | 280.9 | 281.5 | 282. I | 282.7 | 283.3 | 284.0 | 284.6 | 285.2 |
| 460 | 285.8 | 286.5 | 287. 1 | 287.7 | 288.3 | 288.9 | -289.6 | 290.2 | 290.8 | 291.4 |
| 470 | 292.0 | 292.7 | 293.3 | 293.9 | 294.5 | 295.2 | 295.8 | 296.4 | 297.0 | 297.6 |
| 480 | 298.3 | 298.9 | 299.5 | 300. 1 | 300.7 | 301.4 | 302.0 | 302.6 | 303.2 | 303.8 |
| 490 | 304.5 | 305. I | 305.7 | 306.3 | 307.0 | 307.6 | 308.2 | 308.8 | 309.4 | 310.1 |
| 500 | 310.7 | 311.3 | 311.9 | 312.5 | 313.2 | 313.8 | 314.4 | $3^{15} 5.0$ | 315.7 | 316.3 |
| 510 | 316.9 | 317.5 | 318.1 | 318.8 | 319.4 | 320.0 | 320.6 | 321.2 | 321.9 | 322.5 |
| 520 | 323. 1 | 323.7 | 324.4 | 325.0 | 325.6 | 326.2 | 326.8 | 327.5 | 328.1 | 328.7 |
| 530 | 329.3 | 329.9 | 330.6 | 33 I .2 | 33 I .8 | 332.4 | 333. 1 | 333.7 | 334.3 | 334.9 |
| 540 | 335.5 | 336.2 | 336.8 | 337.4 | 338.0 | 338.6 | 339.3 | 339.9 | 340.5 | 34 I .1 |

KILOMETERS INTO MILES.

| Kilometers. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 550 | Miles.341.8 | Miles. | Miles. | Miles.343.6 | $\begin{aligned} & \text { Miles. } \\ & 344.2 \end{aligned}$ | Miles.344.9 | $\begin{aligned} & \text { Miles. } \\ & 345.5 \end{aligned}$ | $\begin{aligned} & \text { Miles. } \\ & 346.1 \end{aligned}$ | $\begin{aligned} & \text { Mile } \text {. } \\ & 346.7 \end{aligned}$ | Miles.$347 \cdot 3$ |
|  |  | Miles. 342.4 | Miles. |  |  |  |  |  |  |  |
| 560 | 348.0 | 348.6 | 349.2 | 349.8 | 350.5 | 35 I. I | 351.7 | 352.3 | 352.9 | 353.6 |
| 570 | 354.2360.4 | 354.8 | 35.4 | 356.0 | 356.7 | 357.3 | 357.9 | 358.5 | 359.2 | 359.8 |
| 5 So |  | 361.0 | 36 I. 6 | 362.3 | 362.9 | 363.5 | 364.1 | 364.7 | 365.4 | 366.0 |
| 590 | $\begin{aligned} & 360.4 \\ & 366.6 \end{aligned}$ | 367.2 | 367.9 | 368.5 | 369. 1 | 369.7 | 370.3 | 371.0 | 371.6 | 372.2 |
| 600 | 372.8 | 373.4 | 374. I | 374.7 | $375 \cdot 3$ | 375.9 | 376.6 | 377.2 | 377.8 | 378.4 |
| 610 | 379.0 | 379.7 | 3 30. 3 | 3 30. 9 | 381.5 | 382.1 | 382.8 | 383.4 | 384.0 | 3S4.6 |
| 620 | 385.2 | 385.9 | 386.5 | 387. I | 387.7 | 3 SS. 4 | 389.0 | 389.6 | 390.2 | 390.8 |
| 630 | $\begin{aligned} & 391.5 \\ & 397.7 \end{aligned}$ | 392. 1 | 392.7 | 393.3 | 393.9 | 394.6 | 395.2 | 395.8 | 396.4 | 397. I |
| 640 |  | 398.3 | 398.9 | 399.5 | 400.2 | 400.8 | 401.4 | 402.0 | 402.6 | 403.3 |
| 650 | 403.9 | 404.5 | 405. 1 | 405.8 | 406.4 | 407.0 | 407.6 | 408.2 | 408.9 | 409.5 |
| 660 | 410.1 | 410.7 | 411.3 | 412.0 | 412.6 | 413.2 | 413.8 | 414.5 | 415.1 | 415.7 |
| 670 | 416.3422.5 | 416.9 | 417.6 | 418.2 | 418.8 | 419.4 | 420.0 | 420.7 | 421.3 | 421.9 |
| 680 |  | 423.2 | 423.8 | 424.4 | 425.0 | 425.6 | 426.3 | 426.9 | 427.5 | 42S. I |
| 690 | 428.7 | 429.4 | 430.0 | 430.6 | 431.2 | 431.9 | 432.5 | 433. 1 | 433.7 | 434.3 |
| 700 | 435.0 | 435.6 | 436.2 | 436.8 | 437.4 | 438. 1 | 438.7 | $439 \cdot 3$ | 439.9 | 440.6 |
| 710 | 44 I .2 | 441.8 | 442.4 | 443.0 | 443.7 | 444.3 | 444.9 | 445.5 | 446. I | 446.8 |
| 720 | 447.4453.6 | 448.0 | 448.6 | 449.3 | 449.9 | 450.5 | 451. I | 451.7 | 452.4 | 453.0 |
| 730 |  | 454.2 | 454.8 | 455.5 | 456. I | 456.7 | $457 \cdot 3$ | 457.9 | 458.6 | 459.2 |
| 740 | $\begin{aligned} & 453.6 \\ & 459.8 \end{aligned}$ | 460.4 | 461. I | 461.7 | 462.3 | 462.9 | 463.5 | 464.2 | 464.8 | 465.4 |
| 750 | 466.0 | 466.6 | 467.3 | 467.9 | 468.5 | 469. I | 469.8 | 470.4 | 471.0 | 471.6 |
| 760 | 472.2 | 472.9 | $473 \cdot 5$ | 474. I | 474.7 | 475.3 | 476.0 | 476.6 | 477.2 | 477.8 |
| 770 | $\begin{aligned} & 47 S .5 \\ & 48.4 .7 \end{aligned}$ | 479.1 | 479.7 | 480.3 | 480.9 | 48 I .6 | 482.2 | 482.8 | 483.4 | 484.0 |
| 780 |  | 485.3 | 485.9 | 486.5 | 487.2 | 487.8 | 488.4 | 489.0 | 489.6 | 490.3 |
| 790 | 490.9 | 491.5 | 492. I | 492.7 | 493.4 | 494.0 | 494.6 | 495.2 | 495.9 | 496.5 |
| 800 | 497. I | 497.7 | 49 S .3 | 499.0 | 499.6 | 500.2 | 500.8 | 501.4 | 502. I | 502.7 |
| Sio | 503.3 | 503.9 | 504.6 | 505.2 | 505.8 | 506.4 | 507.0 | 507.7 | 508.3 | 508.9 |
| 820 | $\begin{aligned} & 509.5 \\ & 515.7 \end{aligned}$ | 510.1 | 510.8 | 511.4 | 512.0 | 512.6 | 513.3 | 513.9 | 514.5 | 515. I |
| 830 |  | 516.4 | 517.0 | 517.6 | 518.2 | 518.8 | 519.5 | 520.1 | 520.7 | 521.3 |
| 840 | $\begin{aligned} & 515.7 \\ & 522.0 \end{aligned}$ | 522.6 | 523.2 | 523.8 | 524.4 | 525. I | 525.7 | 526.3 | 526.9 | 527.5 |
| 850 | 528.2 | 528.8 | 529.4 | 530.0 | 530.6 | 531.3 | 531.9 | 532.5 | 533. I | 533.8 |
| 860 | 534.4 | 535.0 | 535.6 | 536.2 | 536.9 | 537.5 | 538. 1 | 538.7 | 539.3 | 540.0 |
| 870 | 540.6546.8 | 541.2 | 541.8 | 542.5 | 543. I | 543.7 | 544.3 | 544.9 | 545.6 | 546.2 |
| 880 |  | 547.4 | 548.0 | 548.7 | 549.3 | 549.9 | 550.5 | 55 I .2 | 55 I .8 | 552.4 |
| 890 | 553.0 | 553.6 | 554.3 | 554.9 | 555.5 | 556. I | 556.7 | 557.4 | 558.0 | 558.6 |
| 900 | 559.2 | 559.9 | 560.5 | 561. I | 561.7 | 562.3 | 563.0 | 563.6 | 564.2 | 564.8 |
| 910 | 565.4 | 566. I | 566.7 | 567.3 | 567.9 | 568.6 | 569.2 | 569.8 | 570.4 | 571.0 |
| 920 | $\begin{aligned} & 571.7 \\ & 577.9 \end{aligned}$ | 572.3 | 572.9 | 573.5 | 574. I | 574.8 | 575.4 | 576.0 | 576.6 | 577.3 |
| 930 |  | 578.5 | 579.1 | 579.7 | 580.4 | 5 SI.O | 5 SI .6 | 582.2 | 582.8 | 583.5 |
| 940 | $\begin{aligned} & 577.9 \\ & 584 . \mathrm{I} \end{aligned}$ | 584.7 | 585.3 | 586.0 | 586.6 | 587.2 | 587.8 | 588.4 | 589.1 | 589.7 |
| 950 | 590.3 <br> 596.5 <br> 602.7 <br> 608.9 <br> 615.2 <br> 621.4 | 590.9 <br> 597. I <br> 603.4 <br> 609.6 <br> 615.8 <br> 622.0 | 591.5 597.8 604.0 610.2 616.4 622.6 | 592.2 <br> 598.4 <br> 604.6 <br> 610.8 <br> 617.0 <br> 623.2 | 592.8 <br> 599.0 <br> 605.2 <br> 611.4 <br> 617.6 <br> 623.9 | $\begin{aligned} & 593.4 \\ & 599.6 \\ & 605.8 \\ & 612.0 \\ & 618.3 \\ & 624.5 \end{aligned}$ | 594.0 <br> 600.2 <br> 606.5 <br> 612.7 <br> 618.9 <br> 625.1 | 594.7 600.9 607.1 613.3 619.5 625.7 | 595.3 601.5 607.7 613.9 620. 1 626.3 | $\begin{aligned} & 595.9 \\ & 602.1 \\ & 608.3 \\ & 614.5 \\ & 620.7 \\ & 627.0 \end{aligned}$ |
| 960 |  |  |  |  |  |  |  |  |  |  |
| 970 |  |  |  |  |  |  |  |  |  |  |
| 980 |  |  |  |  |  |  |  |  |  |  |
| 990 |  |  |  |  |  |  |  |  |  |  |
| 1000 |  |  |  |  |  |  |  |  |  |  |
|  | km. Miles. <br> $\mathbf{l 0 0 0}$ 621.4 <br> $\mathbf{2 0 0 0}$ 1242.7 <br> 3000 1864.1 <br> 4000 2485.5 <br> 5000 3106.8 |  | 5m Mil | Miles. |  | km. | Miles. | $\mathrm{km} \text {. }$ | Miles. |  |
|  |  |  | 600 |  |  | 0006 |  | $16000$ | 9941.9 |  |
|  |  |  |  | 0 |  | 7 | 56.4 | 17000 | 10563.3 |  |
|  |  |  | 800 | 0497 |  | 000 S | 77.8 | 18000 | I 1184.7 |  |
|  |  |  | 900 | 0559 |  | 000 | 99.2 | 19000 | 11806.0 |  |
|  |  |  | 1000 | 0 621 |  | 000 | 20.5 | 20000 | 12427.4 |  |

Table 17.
INTERCONVERSION OF NAUTICAL AND STATUTE MILES.
I nautical mile* $=6080.20$ feet.

| Nautical Miles. | Statute Miles. | Statute Miles. | Nautical Miles. |
| :---: | :---: | :---: | :---: |
| 1 | 1.1516 | 1 | 0.8684 |
| 2 | 2.3031 | 1.7368 |  |
| 3 | 3.4547 | 2.6052 |  |
| 4 | 4.6062 | 3 | 3.4736 |
| 5 | 5.7578 | 4 | 4.3420 |
| 6 | 6.9093 | 5 | 5.2104 |
| 7 | 8.0609 | 6 | 6.9787 |
| 8 | 9.2124 | 7 | 7.8155 |
| 9 | 10.3640 | 9 |  |

* As defined by the United States Coast Survey.

Table 18.

## CONTINENTAL MEASURES OF LENGTH WITH THEIR METRIC AND ENGLISH EQUIVALENTS.

The asterisk (*) indicates that the measure is obsolete or seldom used.

| Measure. | Metric Equivalent. | English Equivalent. |
| :---: | :---: | :---: |
| El (Netherlands) . . . . . . . . . . . . . . . . | 1 meter. | 3.2808 feet. |
| Fathom, Swedish $=6$ feet . . . . . . . . . | 1.7814 | 5.8445 " |
| Foot, Austrian* | 0.31608 " | 1.0370 " |
| old French* | 0.32484 " | I.0657 " |
| Russian | 0.30 .480 " | 1 " |
| Rheinlandisch or Rhenish (Prussia*, Dennuark, Norway*). | 0.313S5 " | 1. 0297 " |
| Swedish* | 0.2969 " | 0.974 I |
| Spanislı* $=1 / 3$ vara | 0.2786 " | 0.9140 " |
| *Klafter, Wiener (Vienna) . . . . . . . . . . . | 1.896.48 " | 6.2221 " |
| * Line, old French $=\frac{1}{144}$ foot | 0.22558 cm . | 0.0888 iuch. |
| Mile, Austrian post* $=24000$ feet . . . . . . | 7.58594 I. 852 | 4.714 statute miles. <br> I. 1508 " " |
| Swedish $=36000$ feet | 10.69 " | 6.642 " |
| Norwegian $=36000$ feet | II.2986 " | 7.02 " |
| Netherlands (mijl). | I " | 0.6214 " " |
| Prussian (law of 1868) | 7.500 | 4.660 " " |
| Danish | 7.5324 | 4.6804 |
| Palm, Netherlands | O.I meter. | 0.3281 feet. |
| * Rode, Danish | 3.7662 , " | 12.356 " |
| *Ruthe, Prussian, Norwegian | 3.7662 | 12.356 " |
| Sagene (Russian) | 2.1336 | 7 |
| \#'Toise, old French $=6$ feet | I. 9490 | 6.3943 " |
| *Vara, Spanish | 0.8359 " | 2.7424 " |
| Mexican | 0.8380 | 2.7493 |
| Werst, or versta (Russian) $=500$ sashjene . | 1. 0668 km . | 3.500 " |

## CONVERSION OF MEASURES OF TIME AND ANGLE.

Arc into time ..... Table ig
Time into arc ..... Table 20
Days into decimals of a year and angle ..... Table 21
Hours, minutes and seconds into decimals of a day ..... Table 22
Decimals of a day into hours, minutes and seconds ..... Table 23
Minutes and seconds into decimals of an hour ..... Table $2+$
Local mean time at apparent noon ..... Table 25
Sidereal time into mean solar time ..... Table 26
Mean solar time into sidereal time ..... Table 27

ARC INTO TIME.

| - | h. m. | - | h. m. | - | h. m. | - | h m. | - | h. m. | - | h. m. | , | m. s. | 11 | s. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | $\bigcirc$ | 60 | 40 | 120 | 8 o | 180 | 120 | 240 | 16 - | 300 | 200 | 0 | $\bigcirc 0$ | 0 | 0.000 |
| 1 | - 4 | 6 I | 44 | 121 | S 4 | 18 I | 124 | 241 | 164 | 301 | 204 | I | O 4 | 1 | 0.067 |
| 2 | - S | 62 | 48 | 12 | S 8 | I82 | 128 | 242 | 16 S | 302 | 20 S | 2 | - S | 2 | 0.133 |
| 3 | O 12 | 63 | 412 | 123 | 812 | 183 | 1212 | 243 | 1612 | 303 | 2012 | 3 | O 12 | 3 | 0.200 |
| 4 | - 16 | 64 | 416 | 124 | 816 | IS4 | 1216 | 244 | 1616 | 304 | 2016 | 4 | - 16 | 4 | 0. 267 |
| 5 | - 20 | 65 | 420 | 125 | 820 | 185 | 1220 | 245 | 1620 | 305 | 2020 | 5 | O 20 | 5 | 0.333 |
| 6 | O 24 | 66 | 424 | 126 | 824 | IS6 | 1224 | 246 | 1624 | 306 | 2024 | 6 | - 24 | 6 | 0.400 |
| 7 | - 28 | 67 | 428 | 127 | 828 | IS7 | 1228 | 247 | 1628 | 307 | 2028 | 7 | - 28 | 7 | 0.467 |
| S | - 32 | 68 | 432 | 128 | 832 | ISS | 1232 | 2.48 | 1632 | 308 | 2032 | 8 | - 32 | 8 | 0.533 |
| 9 | - 36 | 69 | 4.36 | 12 | 836 | 189 | 1236 | 2.49 | 1636 | 309 | 2036 | 9 | 036 | 9 | 0.600 |
| 10 | - 40 | 70 | 440 | 130 | 840 | 190 | 1240 | 250 | 1640 | 310 | 2040 | 10 | - 40 | 10 | 0.667 |
| 11 | O 44 | 71 | 444 | 131 | 844 | 191 | 1244 | 25 I | 1644 | 311 | 2044 | 11 | - 44 | II | 0.733 |
| 12 | O 48 | 72 | 443 | 132 | S 48 | 192 | 1248 | 252 | 1648 | 312 | 2048 | 12 | - $45^{5}$ | 2 | o. 800 |
| 13 | O 52 | 73 | 452 | I33 | S 52 | 193 | 1252 | 253 | 1652 | 313 | 2052 | 13 | - 52 | 13 | 0. 867 |
| 14 | - 56 | 74 | 456 | 1.34 | S 56 | 194 | 1256 | 254 | I6 56 | 314 | 2056 | 14 | - 56 | 14 | 0.933 |
| 15 | I 0 | 75 | 5 O | 135 | 9 o | 195 | 130 | 255 | 170 | 315 | 210 | 15 | 10 | 15 | 1.000 |
| 16 | I 4 | 76 | 5 | 136 | 94 | 196 | 134 | 256 | 174 | 316 | 214 | 16 | 14 | 16 | 1.067 |
| 17 | 18 | 77 | 5 S | 137 | 98 | 197 | 138 | 257 | 178 | 317 | 218 | 17 | 1 | 17 | I. 133 |
| IS | 112 | 78 | 512 | 138 | 912 | 198 | 1312 | 25 S | 1712 | 318 | 2 I 12 | 18 | 112 | IS | 1.200 |
| 19 | 116 | 79 | 516 | 139 | 916 | 199 | 1316 | 259 | 1716 | 319 | 21 16 | 19 | 116 | 9 | 1.267 |
| 20 | 120 | 80 | 520 | 140 | 920 | 200 | 1320 | 260 | 1720 | 320 | 21 20 | 20 | I 20 | 20 | 1.333 |
| 21 | I 24 | Sil | 524 | 41 | 924 | 201 | 1324 | 261 | 1724 | 32 I | 21 24 | 2 I | I 24 | 21 | 1.400 |
| 22 | 128 | S2 | 528 | I 42 | 928 | 202 | 1328 | 62 | 1728 | 322 | 21 28 | 22 | I 28 | 22 | I. 467 |
| 23 | I 32 | $\mathrm{S}_{3}$ | 532 | 143 | 932 | 203 | 1332 | 263 | 1732 | 323 | 2132 | 23 | 132 | 23 | 1.533 |
| 24 | I 36 | S | 536 | I 44 | 936 | 204 | 1336 | 264 | 1736 | 324 | 2136 | 24 | I 36 | 24 | I. 600 |
| 25 | I 40 | 85 | 540 | 145 | 940 | 205 | 1340 | 265 | 1740 | 325 | 2140 | 25 | I 40 | 25 | I. 667 |
| 26 | 144 | S6 | 544 | 146 | 944 | 206 | 1344 | 266 | 1744 | 326 | 2144 | 26 | I 44 | 26 | 1.733 |
| 27 | 148 | 87 | 548 | 147 | 948 | 207 | 1348 | 267 | 1748 | 327 | 2148 | 27 | I 48 | 27 | I. Soo |
| 28 | 152 | SS | 552 | 148 | 952 | 208 | 1352 | 268 | 1752 | 328 | 2152 | 2 S | I 52 | 28 | 1.867 |
| 29 | I 56 | 80 | 5.56 | 149 | 956 | 209 | I3 56 | 269 | 1756 | 329 | 2156 | 29 | I 56 | 29 | 1.933 |
| 30 | 20 | 90 | 6 | 150 | 10 | 210 | 140 | 270 | $18 \quad 0$ | 330 | 22 | 30 | 2 | 30 | 2.000 |
| 31 | 24 | 91 | 6 | 51 |  | 211 | I4 4 | 271 | I8 | 331 | 22 | 31 |  | 31 | 2.067 |
| 32 | 2 S | 92 | 68 | 152 | 108 | 2 I | 148 | 272 | I8 8 | 332 | 22 | 32 | 2 | 32 | 2. I 33 |
| 33 | 212 | 93 | 612 | 153 | IO I2 | 213 | 1412 | 273 | IS 12 | 333 | 22 I2 | 33 | 212 | 33 | 2.200 |
| 34 | 216 | 94 | 616 | 154 | Io 16 | 214 | 1416 | 274 | I8 16 | 33 | 22 I6 | 34 | 216 | 34 | 2.267 |
| 35 | 220 | 95 | 620 | 155 | IO 20 | 215 | I4 20 | 275 | IS 20 | 335 | 2220 | 35 | 220 | 35 | 2.333 |
| 36 | 224 | 96 | 624 | 156 | IO 24 | 216 | 1424 | 276 | IS 2.4 | 336 | 2224 | 36 | 224 | 36 | 2.400 |
| 37 | 228 | 97 | 628 | 157 | 102 S | 217 | 1428 | 277 | IS 28 | 337 | 2228 | 37 | 228 | 37 | 2.467 |
| 38 | 232 | 98 | 632 | 158 | IO 32 | 218 | 1432 | 278 | IS 32 | 338 | 2232 | 38 | 232 | 38 | 2.533 |
| 39 | 236 | 99 | 636 | 159 | 1036 | 219 | 1436 | 279 | IS 36 | 339 | 2236 | 39 | 236 | 39 | 2.600 |
| 40 | 240 | 100 | 640 | 160 | 1040 | 220 | 1440 | 280 | 1840 | 340 | 2240 | 40 | 240 | 40 | 2.667 |
| 41 | 244 | IOI | 644 | 161 | 1044 | 221 | 1444 | 281 | IS 44 | 34 I | 2244 | 41 | 2.44 | 41 | 2.733 |
| 42 | 248 | 2 | 648 | 162 | 1048 | 22 | 1448 | 282 | I8 48 | 342 | 2248 | 42 | 248 | 42 | 2.800 |
| 43 | 252 | 103 | 652 | 163 | 1052 | 223 | 1452 | 283 | I8 52 | 343 | 2252 | 43 | 252 | 43 | 2.867 |
| 44 | 256 | 104 | 656 | 164 | 10 56 | 224 | I4 56 | 284 | IS 56 | 344 | 2256 | 44 | 256 | 44 | 2.933 |
| 45 | 30 | 105 | 7 o | 165 | II 0 | 225 | 150 | 285 | 19 O | 345 | 230 | 45 | 30 | 45 | 3.000 |
| 46 | 3 | 10 | 74 | 166 | II 4 | 226 | 154 | 286 | I9 4 | 346 | 234 | 46 | 3 | 46 | 3.067 |
| 47 | 38 | 107 | 78 | 167 | II 8 | 227 | 15 S | 287 | 198 | 347 | 238 | 47 | 3 S | 47 | 3.133 |
| 48 | 312 | 10 | 712 | 168 | II 12 | 228 | 1512 | 285 | 1912 | 348 | 2312 | 48 | 312 | 48 | 3.200 |
| 49 | 316 | 109 | 716 | 169 | II 16 | 229 | 1516 | 289 | 1916 | 3.4 | 2.316 | 49 | 316 | 49 | 3.267 |
| 50 | 320 | 110 | 720 | 170 | 1120 | 230 | 1520 | 290 | 1920 | 350 | 2320 | 50 | 320 | 50 | 3.33,3 |
| 51 | 324 | II I | 724 | 171 | II 24 | 231 | 1524 | 291 | 1924 | 351 | 2324 | 51 | 324 | 51 | 3.400 |
| 52 | 328 | 112 | 728 | 172 | II 28 | 232 | 1528 | 292 | 1928 | 352 | 2328 | 52 | 328 | 52 | 3.467 |
| 53 | 332 | 113 | 732 | 173 | II 32 | 233 | 1532 | 293 | I9 32 | 353 | 2332 | 53 | 332 | 53 | 3.533 |
| 54 | 336 | 114 | 736 | 174 | II 36 | 234 | 1536 | 294 | 1936 | 354 | 2336 | 54 | $33^{6}$ | 54 | 3.600 |
| 55 | 340 | 115 | 740 | 175 | II 40 | 235 | 1540 | 295 | 1940 | 355 | 2340 | 55 | 340 | 55 | 3.667 |
| 56 | 344 | 116 | 744 | 176 | II 44 | 236 | 1544 | 296 | 1944 | 356 | 2344 | 56 | 344 | 56 | 3.733 |
| 57 | 345 | 117 | 748 | 177 | II 48 | 237 | I5 48 | 297 | 1948 | 357 | 2348 | 57 | 348 | 57 | 3.800 |
| 58 | 352 | IIS | 752 | 178 | II 52 | 238 | I5 52 | 298 | 1952 | 35 S | 2352 | 58 | 352 | 58 | 3.867 |
| 59 | 356 | I19 | 756 | 179 | II 56 | 239 | 1556 | 299 | 1956 | 35\% | 고 56 | 59 | 356 | 59 | - 3.933 |
| 60 | 4 O | 120 | 80 | 180 | 120 | 240 | 16 O | 300 | 20 O | 360 | 240 | 60 | 4 ○ | 60 | 4.000 |

emitheonian Tableg.

## TIME INTO ARC.

| Hours into Arc. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time. | Arc. | Time. | Arc. | Time. | Arc. | Time. | Arc. | Time. | Arc. | Time. | Arc. |
| hrs. | - | hrs. | - | hrs. | - | hrs. | - | hts. | - | hrs. | - |
| 1 | 15 | 5 | 75 | 9 | ${ }^{1} 35$ | 13 | 195 | 17 | 255 | 21 | 315 |
| 2 | 30 | 6 | 90 | 10 | 150 | 14 | 210 | 18 | 270 | 22 | 330 |
| 3 | 45 | 7 | 105 | 11 | 165 | 15 | 225 | 19 | 285 | 23 | 345 |
| 4 | 60 | 8 | 120 | 12 | ISo | 16 | 2.40 | 20 | 300 | 24 | 360 |

Minutes of Time into Arc.

| m. | - | , | m. |  | , | m. |  | , | s. | , | // | s |  | / | s. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  | 15 | 21 |  | 15 | 41 | 10 | 15 | 1 | o | 15 | 21 |  | 15 | 41 |  |  |
| 2 | $\bigcirc$ | 30 | 22 |  | 30 | 42 | 103 | 30 | 2 | - | 30 | 22 |  | 30 | 42 |  | 30 |
| 3 | - | 45 | 23 | 5 | 45 | 43 |  | 45 | 3 | - | 45 | 23 | 5 | 45 | 43 |  | 45 |
| 4 | I | - | 2. | 6 | - | 44 |  | - | 4 | I | - | 24 | 6 | 0 | 44 | 1 | 0 |
| 5 | I | 15 | 25 | 6 | 15 | 45 | 11 | 15 | 5 | I | 15 | 25 | 6 | 15 | 45 |  | 15 |
| 6 | I | 30 | 26 | 6 | 30 | 46 |  | 30 | 6 | 1 | 30 | 26 | 6 | 30 | 46 |  | 30 |
| 7 | 1 | 45 | 27 | 6 | 45 | 47 | II | 45 | 7 | 1 | 45 | 27 | 6 | 45 | 47 |  | 45 |
| 8 | 2 | - | 28 | 7 | o | 48 |  | $\bigcirc$ | 8 | 2 | - | 28 | 7 | o | 48 | 12 | 0 |
| 9 | 2 | 15 | 29 | 7 | 15 | 49 | 12 | 15 | 9 | 2 | 15 | 29 | 7 | 15 | 49 | 12 | 15 |
| 10 | 2 | 30 | 30 | 7 | 30 | 50 | 12 | 30 | 0 | 2 | 30 | 30 | 7 | 30 | 50 | 12 | 30 |
| 11 | 2 | 45 | 31 | 7 | 45 | 5 I | 12 | 45 | 11 | 2 | 45 | 31 | 7 | 45 | 5 I | 12 | 45 |
| 12 | 3 | - | 32 | 8 | - | 52 | 13 | 0 | 12 | 3 | o | 32 | S | - | 52 | 13 | O |
| 13 | 3 | I5 | 33 | S | 15 | 53 |  | 15 | 13 | 3 | 15 | 33 | 8 | 15 | 53 | 13 | 15 |
| 14 | 3 | 30 | 34 | S | 30 | 54 | 13 | 30 | 14 | 3 | 30 | 34 | 8 | 30 | 54 | 13 | 30 |
| 15 | 3 | 45 | 35 | 8 | 45 | 55 | 13 | 45 | 15 | 3 | 45 | 35 | 8 | 45 | 55 | 13 | 45 |
| 16 | 4 | - | 36 | 9 | 0 | 56 | 14 | 0 | 16 | 4 | - | 36 | 9 |  | 56 | 14 | 0 |
| 17 | 4 | I5 | 37 | 9 | 15 | 57 |  | I5 | 17 | 4 | 15 | 37 |  | 15 | 57 | 14 | 15 |
| 18 | 4 | 30 | 38 | 9 | 30 | 58 |  | 30 | IS | 4 | 30 | 38 |  |  | 58 | 14 | 30 |
| 19 | 4 | 45 | 39 | 9 | 45 | 59 |  | 45 | 19 | 4 | 45 | 39 | 9 | 45 | 59 | 14 | 45 |
| 20 | 5 | O | 40 | 10 | O | 60 | 15 | 0 | 20 | 5 | 0 | 40 | 10 | $\bigcirc$ | 60 | 15 |  |

Hundredths of a Second of Time into Arc.

| Hundredths of a Second of time | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| s. 0.00 | ó.00 | O. 15 | 0.10 | 0. 0.45 | 0.60 | O. 75 | 0. 0.90 | I'.05 | Í. 20 | I. 1.35 |
| . 10 | 1.50 | 1.65 | 1.80 | 1.95 | 2. 10 | 0.25 | 2.40 | 2.55 | 2.70 | 2.85 |
| . 20 | 3.00 | 3.15 | 3.30 | 3.45 | 3.60 | 3.75 | 3.90 | 4.05 | 4.20 | 4.35 |
| . 30 | 4.50 | 4.65 | 4.80 | 4.95 | 5.10 | 5.25 | 5.40 | 5.55 | 5.70 | 5.85 |
| . 40 | 6.00 | 6.15 | 6.30 | 6.45 | 6.60 | 6.75 | 6.90 | 7.05 | 7.20 | $7 \cdot 35$ |
| 0.50 | 7.50 | 7.65 | 7.50 | 7.95 | 8.10 | 8.25 | 8.40 | 8.55 | 8.70 | 8.85 |
| . 60 | 9.00 | 9.15 | 9.30 | 9.45 | 9.60 | 9.75 | 9.90 | 10.05 | 10.20 | 10.35 |
| . 70 | 10.50 | 10.65 | 10.80 | 10.95 | 11.10 | 11.25 | 11.40 | 11.55 | 11.70 | 11.85 |
| .So | 12.00 | 12.15 | 12.30 | 12.45 | 12.60 | I2.75 | 12.90 | 13.05 | 13.20 | 13.35 |
| . 90 | I 3.50 | 13.65 | 13.80 | 13.95 | 14. 10 | 14.25 | 14.40 | I 4.55 | 14.70 | 14.85 |

Table 21.

DAYS INTO DECIMALS OF A YEAR AND ANGLE.

| $\begin{gathered} \text { Day } \\ \text { of } \\ \text { Year. } \end{gathered}$ | $\begin{aligned} & \text { Decimal } \\ & \text { of } \\ & \text { a Year. } \end{aligned}$ | Angle. | Day of | Month. | $\begin{gathered} \text { Day } \\ \text { of } \\ \text { Year. } \end{gathered}$ | Decimal of a Year. | Angle. | Day of Month. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Common Year. | Bissextile Year. |  |  |  | $\begin{aligned} & \text { Common } \\ & \text { Year. } \end{aligned}$ | Bissextile Year. |
| 1 | 0.00000 | $0^{\circ} 0^{\prime}$ | Jan. I | Jan. 1 | 51 | 0.13689 | $49^{\circ} 17^{\prime}$ | Feb. 20 | Feb. 20 |
| 2 | . 00274 | - 59 |  | 2 | 52 | . 13963 | 5016 | 2 I | 2 I |
| 3 | . 00548 | 158 | 3 | 3 | 53 | . 14237 | 51 I5 | 22 | 22 |
| 4 | .00S2I | 257 | 4 | 4 | 54 | . 145 II | 5214 | 23 | 23 |
| 5 | 0.01095 | 357 | 5 | 5 | 55 | 0. 14784 | 5313 | 24 | 24 |
| 6 | . 01369 | 456 | 6 | 6 | 56 | . 15058 | 54 13 | 25 | 25 |
| 7 | . 01643 | 555 | 7 | 7 | 57 | - 15332 | 5512 | 26 | 26 |
| 8 | . 01916 | 654 | 8 | S | 58 | . 15606 | 56 II | 27 | 27 |
| 9 | .02190 | 753 | 9 | 9 | 59 | . 15880 | 57 IO | 2 S | 2 S |
| 10 | 0.02464 | 852 | 10 | 10 | 60 | 0.16153 | $58 \quad 9$ | Mar. I | 29 |
| 1 I | . 02738 | 9 5I | II | II | 61 | . 16427 | 598 | 2 | Mar. 1 |
| 12 | . 03011 | 1051 | 12 | 12 | 62 | . 16701 | 607 | 3 | 2 |
| 13 | . 03285 | II 50 | I3 | 13 | 63 | . 16975 | 617 | 4 | 3 |
| 14 | . 03559 | 1249 | 14 | 14 | 6. | . 17248 | 626 | 5 | 4 |
| 15 | 0.03833 | I3 48 | 15 | 15 | 65 | O. 17522 | 635 | 6 | 5 |
| 16 | .04107 | 1447 | 16 | 16 | 66 | . 17796 | 644 | 7 | 6 |
| 17 | .04381 | I5 46 | 17 | 17 | 67 | . 18070 | 653 | 8 | 7 |
| 18 | . 04654 | 1645 | 18 | 18 | 65 | . IS344 | 662 | 9 | 8 |
| 19 | . 04928 | 1744 | 19 | 19 | 69 | .18617 | 67 I | 10 | 9 |
| 20 | 0.05202 | I8 44 | 20 | 20 | 70 | 0.18891 | 68 - | II | 10 |
| 2 I | . 05476 | 1943 | 21 | 21 | 71 | . 19165 | 69 - | 12 | 11 |
| 22 | . 05749 | 2042 | 22 | 22 | 72 | . 19439 | 6959 | 13 | 12 |
| 23 | . 06023 | 2141 | 23 | 23 | 73 | . 19713 | $70 \quad 58$ | 14 | 13 |
| 24 | . 06297 | 2240 | 24 | 24 | 74 | . 19986 | 7157 | 15 | 14 |
| 25 | 0.06571 | 2339 | 25 | 25 | 75 | 0.20260 | 7256 | 16 | 15 |
| 26 | . 06845 | 24 3S | 26 | 26 | 76 | . 20534 | 7355 | 17 | 16 |
| 27 | . 07 II8 | 2538 | 27 | 27 | 77 | . 20SoS | 7454 | IS | 17 |
| 28 | . 07.392 | 2637 | 28 | 28 | 78 | . 2108 I | 7554 | 19 | 18 |
| 29 | . 07666 | 2736 | 29 | 29 | 79 | . 21355 | 7653 | 20 | 19 |
| 30 | 0.07940 | 2835 | 30 | 30 | 80 | 0.21629 | 7\% 52 | 2 I | 20 |
| 31 | .082I 4 | 2934 | Feb ${ }^{31}$ | - 3 I | SI | . 21903 | - 5 | 22 | 2 I |
| 32 | . 08487 | $30 \quad 33$ | Feb. I | Feb. 1 | 82 | . 22177 | 7950 | 23 | 22 |
| 33 | .08761 | 3132 | 2 | 2 | S3 | . 22450 | So 49 | 24 | 23 |
| 34 | . 09035 | 3232 | 3 | 3 | 84 | . 22724 | 8 I 4 S | 25 | 24 |
| 35 | 0.09309 | 33 3I | 4 | 4 | 85 | 0.22998 | S2 48 | 26 | 25 |
| 36 | . 09582 | 3430 | 5 | 5 | S6 | . 23272 | 8347 | 27 | 26 |
| 37 | . 09585 | $35 \quad 29$ | 6 | 6 | S7 | . 23546 | 8446 | 28 | 27 |
| 3 S | .10130 | $\begin{array}{ll}36 & 28\end{array}$ | 7 | 7 | 88 | .23SI9 | S5 45 | 29 | 28 |
| 39 | . 10404 | 3727 | 8 | 8 | 89 | . 2.4093 | 8644 | 30 | 29 |
| 40 | 0. 10678 | 3826 | 9 | 9 | 90 | 0.2.4367 | 8743 | 31 | 30 |
| 41 | . IO95I | 3926 | 10 | 10 | 91 | :24641 | SS 42 | Apr. 1 | 31 |
| 42 | . II 225 | 4025 | II | I I | 92 | . 24914 | 8942 | 2 | Apr. 1 |
| 43 | . II 499 | 4124 | 12 | 12 | 93 | .25ISS | 9041 | 3 | 2 |
| 44 | . I I 773 | 4223 | 13 | 13 | 94 | . 25462 | 9140 | 4 | 3 |
| 45 | O. 12047 | 4322 | 14 | 14 | 95 | 0.25736 | 9239 | 5 | 4 |
| 46 | . 12320 | 44 21 | 15 | 15 | 96 | . 26010 | 9338 | 6 | 5 |
| 47 | . 12594 | $45 \quad 20$ | 16 | 16 | 97 | . 26283 | 9437 | 7 | 6 |
| 48 | . 12868 | 46 I9 | 17 | 17 | 98 | . 26557 | 9536 | 8 | 7 |
| 49 | . 13142 | 47 I9 | 18 | 18 | 99 | . 26831 | 9635 | 9 | 8 |
| 50 | 0.13415 | 48 I8 | 19 | 19 | 100 | 0.27105 | 9735 | 10 | 9 |

DAYS INTO DECIMALS OF A YEAR AND ANGLE.

| $\begin{gathered} \text { Day } \\ \text { of } \\ \text { Year. } \end{gathered}$ | $\begin{aligned} & \text { Decimal } \\ & \text { of } \\ & \text { a Year. } \end{aligned}$ | Angle. | Day of Month. |  | $\begin{gathered} \text { Day } \\ \text { of } \\ \text { Year. } \end{gathered}$ | Decimal of a Year. | Angle. | Day of Month. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \text { Common } \\ & \text { Year. } \end{aligned}$ | Bissextile Year. |  |  |  | Common Year. | Bissextile Year. |
| 101 | 0.27379 | $98^{\circ} 34^{\prime}$ | Apr. II | Apr. 10 | 151 | 0.41068 | $147^{\circ} 51^{\prime}$ | May 3I | May 30 |
| 102 | . 27652 | 9933 | 12 | 11 | 152 | . 41342 | 14850 | fune 1 | 3 I |
| 103 | . 27926 | 100 32 | I3 | 12 | 153 | .41615 | 14949 |  | June 1 |
| 104 | . 28200 | IOI 3I | 14 | 13 | 154 | .41889 | 15048 | 3 | 2 |
| 105 | 0.28474 | 10230 | 15 | 14 | 155 | 0.42163 | 15147 | 4 | 3 |
| 106 | . 28747 | 10329 | 16 | 15 | I56 | . 42437 | 15246 | 5 | 4 |
| 107 | . 29021 | 10429 | 17 | 16 | 157 | . 42710 | 15345 | 6 | 5 |
| 108 | . 29295 | 10528 | 18 | 17 | 158 | . 42984 | 15445 | 7 | 6 |
| 109 | . 29569 | 10627 | 19 | 18 | 159 | .4325 | I 5544 | 8 | 7 |
| 110 | 0.29843 | 10726 | 20 | 19 | 160 | 0.43532 | 15643 | 9 | 8 |
| III | . 30116 | 10825 | 21 | 20 | 161 | .43806 | 15742 | 10 | 9 |
| 112 | . 30390 | 10924 | 22 | 21 | 162 | . 44079 | 15841 | 11 | 10 |
| 113 | . 30664 | IIO 23 | 23 | 22 | 163 | . 44353 | 15940 | 12 | 11 |
| II4 | . 30938 | III 23 | 24 | 23 | 164 | . 44627 | 16039 | 13 | 12 |
| 115 | 0.31211 | 11222 | 25 | 24 | 165 | 0.44901 | 16 I 39 | 14 | 13 |
| 116 | . 31485 | 11321 | 26 | 25 | 166 | . 45175 | 16238 | 15 | 14 |
| 117 | . 31759 | 11420 | 27 | 26 | 167 | . 45448 | 16337 | 16 | 15 |
| 118 | . 32033 | 11519 | 28 | 27 | 168 | . 45722 | 16436 | 17 | 16 |
| 119 | . 32307 | 116 IS | 29 | 28 | 169 | . 45996 | 16535 | 18 | 17 |
| 120 | 0.32580 | 11717 | 30 | 29 | 170 | 0.46270 | 16634 | 19 | 18 |
| 121 | . 32854 | 11817 | May I | 30 | 175 | . 46543 | 16733 | 20 | 19 |
| 122 | . 33128 | 11916 | 2 | May I | 172 | . 46817 | 16833 | 2 I | 20 |
| 123 | . 33402 | 12015 | 3 | 2 | 173 | .47091 | 16932 | 22 | 2 I |
| 124 | . 3.3676 | 12114 | 4 | 3 | 174 | . 47365 | 17031 | 23 | 22 |
| 125 | 0.33949 | 122 I3 | 5 | 4 | 175 | 0.47639 | 17130 | 24 | 23 |
| 126 | . 34223 | 12312 | 6 | 5 | 176 | . 47912 | 17229 | 25 | 24 |
| 127 | - 34497 | 124 II | 7 | 6 | 177 | . 48186 | 17328 | 26 | 25 |
| 128 | -34771 | 12510 | 8 | 7 | 178 | . 48460 | 17427 | 27 | 26 |
| 129 | . 35044 | 12610 | 9 | 8 | 179 | . 48734 | $175 \quad 26$ | 28 | 27 |
| 130 | 0.353 I 8 | $127 \quad 9$ | 10 | 9 | 180 | 0.49008 | 17626 | 29 | 28 |
| 131 | . 35592 | 128 S | 11 | 10 | 181 | . 4928 I | 17725 | $]^{30}$ | 29 |
| 132 | . 35866 | 1297 | 12 | II | 182 | . 49555 | 17824 | July I | $3^{30}$ |
| 133 | . 36140 | 1306 | 13 | 12 | 183 | . 49829 | 17923 | 2 | July 1 |
| 134 | . 36413 | I3I 5 | 14 | 13 | 184 | . 50103 | ISo 22 | 3 | 2 |
| 135 | 0. 36687 | I32 4 | 15 | 14 | 185 | 0.50376 | 18121 | 4 | 3 |
| 136 | . 36961 | 1334 | 16 | 15 | 186 | . 50650 | 18220 | 5 | 4 |
| 137 | . 37235 | 1343 | 17 | 16 | 187 | . 50924 | 18320 | 6 | 5 |
| 138 | -37509 | 1352 | 18 | 17 | IS8 | .51198 | 18419 | 7 | 6 |
| 139 | . 37782 | 136 I | 19 | 18 | IS9 | . 51472 | 185 I8 | 8 | 7 |
| 140 | 0.3 So56 | 137 o | 20 | 19 | 190 | 0.51745 | 18617 | 9 | 8 |
| 141 | . 38330 | 13759 | 21 | 20 | 191 | . 52019 | 18716 | 10 | 9 |
| 142 | . 38604 | 13858 | 22 | 21 | 192 | . 52293 | 18815 | II | 10 |
| 143 | -38877 | I 3958 | 23 | 22 | 193 | . 52567 | I89 14 | 12 | 11 |
| 144 | .3915I | 1.40 .57 | 24 | 23 | 194 | . 5284 I | 19014 | 13 | 12 |
| 145 | 0.39425 | 14156 | 25 | 2.4 | 195 | 0.53 II4 | 19113 | 14 | 13 |
| 146 | . 39699 | 14255 | 26 | 25 | 196 | . 53388 | 19212 | 15 | 14 |
| 147 | - 39973 | 14354 | 27 | 26 | 197 | . 53662 | 193 II | 16 | 15 |
| 148 | . 40246 | 14453 | 28 | 27 | 198 | . 53936 | 19410 | 17 | 16 |
| 149 | . 40520 | 14552 | 29 | 28 | 199 | . 54209 | 1959 | 18 | 17 |
| 150 | 0.40794 | 14651 | 30 | 29 | 200 | 0.54483 | 196 8 | 19 | 18 |

Table 21.

DAYS INTO DECIMALS OF A YEAR AND ANGLE.

| $\begin{aligned} & \text { Day } \\ & \text { of } \\ & \text { Year. } \end{aligned}$ | $\begin{aligned} & \text { Decimal } \\ & \text { of } \\ & \text { a Year. } \end{aligned}$ | Angle. | Day of Month. |  | $\begin{aligned} & \text { Day } \\ & \text { of } \\ & \text { Year. } \end{aligned}$ | Decimal of a Year. | Angle. | Day of Month. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Common Year. | Bissextile Year. |  |  |  | Common Year. | Bissextile Year. |
| 201 | 0.54757 | $197^{\circ} \mathrm{S}^{\prime}$ | July 20 | July 19 | 251 | 0.68446 | $246^{\circ} 24^{\prime}$ | Sept. S | Sept. 7 |
| 202 | . 55031 | 1987 | 21 | 20 | 252 | . 68720 | 24724 | 9 | 8 |
| 203 | . 55305 | 1996 | 22 | 21 | 253 | . 68994 | 24 S 23 | 10 | 9 |
| 20.4 | . 55578 | 2005 | 23 | 22 | 254 | . 69268 | 24922 | I I | 10 |
| 205 | 0. $55 \mathrm{~S}_{52}$ | 2014 | 24 | 23 | 255 | 0.69541 | 25021 | 12 | II |
| 206 | . 56126 | 2023 | 25 | 24 | 256 | . 69815 | 25120 | 13 | 12 |
| 207 | . 56400 | 2032 | 26 | 25 | 257 | . 70089 | 25219 | 14 | 13 |
| 208 | . 56674 | 204 I | 27 | 26 | 258 | .70363 | 253 IS | 15 | 14 |
| 209 | . 56947 | 205 I | 28 | 27 | 259 | .70637 | 254 I7 | 16 | 15 |
| 210 | 0.5722 I | 206 o | 29 | 28 | 260 | 0.70910 | 255 I7 | 17 | 16 |
| 211 | . 57495 | 20659 | 30 | 29 | 261 | .71184 | 25616 | 18 | 17 |
| 212 | . 57769 | 2075 S | 3 I | 30 | 262 | . 71458 | 257 I 5 | 19 | 18 |
| 213 | -5SO42 | 20857 | Aug. I | 3 I | 263 | . 71732 | 25 S 14 | 20 | 19 |
| 214 | .58316 | 20956 | 2 | Aug. 1 | 264 | . 72005 | 259 I 3 | 21 | 20 |
| 215 | 0.58590 | 21055 | 3 | 2 | 265 | 0.72279 | 26012 | 22 | 21 |
| 216 | . 58864 | 21155 | 4 | 3 | 266 | . 72553 | 261 II | 23 | 22 |
| 217 | .59138 | 21254 | 5 | 4 | 267 | . 72827 | 262 II | 24 | 23 |
| 215 | . 5941 I | 21353 | 6 | 5 | 268 | .73101 | 263 Io | 25 | 24 |
| 219 | .59685 | 21452 | 7 | 6 | 269 | . 73374 | 2649 | 26 | 25 |
| 220 | 0.59959 | 215 51 | 8 | 7 | 270 | 0.73648 | 265 S | 27 | 26 |
| 22 I | . 60233 | 21650 | 9 | 8 | 27 I | . 73922 | 266 | 2.8 | 27 |
| 222 | . 60507 | 21749 | 10 | 9 | 272 | .74196 | 2676 | 29 | 28 |
| 223 | .60780 | 21849 | 11 | 10 | 273 | . 74470 | 2685 | 30 | 29 |
| 22.4 | .61054 | 2194 S | 12 | 11 | 274 | .74743 | 2695 | Cct. I | 30 |
| 225 | 0.6132S | 22047 | 13 | 12 | 275 | 0.75017 | 2704 | 2 | Oct. I |
| 226 | . 61602 | 22146 | 14 | 13 | 276 | . 75291 | 271 | 3 | 2 |
| 227 | .61875 | 22245 | 15 | 14 | 277 | . 75565 | 2722 | 4 | 3 |
| 228 | . 62149 | 22344 | 16 | 15 | 278 | .75838 | 273 I | 5 | 4 |
| 229 | . 62423 | 22.43 | 17 | 16 | 279 | .76112 | 274 o | 6 | 5 |
| 230 | 0.62697 | 22543 | 18 | 17 | 280 | 0.76386 | 27459 | 7 | 6 |
| 231 | . 62971 | 22642 | 19 | 18 | 2 SI | . 76660 | 27559 | 8 | 7 |
| 232 | . 63244 | 22741 | 20 | 19 | 2 S 2 | . 76934 | 27658 | 9 | 8 |
| 233 | . 63515 | 22 S 40 | 21 | 20 | 283 | . 77207 | 27757 | 10 | 9 |
| 234 | . 63792 | 22939 | 22 | 21 | 2 S 4 | .774SI | 27S 56 | II | 10 |
| 235 | 0.64066 | 2303 S | 23 | 22 | 285 | 0.77755 | 27955 | 12 | 11 |
| 236 | . 64339 | 23137 | 24 | 23 | 286 | .7S029 | 2 So 54 | 13 | 12 |
| 237 | .64613 | 23236 | 25 | 24 | 287 | . 78303 | 28153 | 14 | 13 |
| 238 | .64887 | 23336 | 26 | 25 | 288 | .75576 | 2 S 252 | 15 | 14 |
| 239 | .6516I | 23435 | 27 | 26 | 289 | .78850 | 28352 | 16 | 15 |
| 240 | 0.65435 | 23534 | 28 | 27 | 290 | 0.79124 | 28451 | 17 | 16 |
| 241 | . 6570 O | 23633 | 29 | 28 | 291 | . 79398 | 28550 | 18 | 17 |
| 2.42 | .65982 | 23732 | 30 | 29 | 292 | .79671 | 28649 | 19 | 18 |
| 243 | . 66256 | 23831 | Scti ${ }^{31}$ | 30 | 293 | . 79945 | 28748 | 20 | 19 |
| 244 | . 66530 | 23930 | Sept. I | 3 I | 294 | . $\mathrm{So2} 19$ | 28847 | 21 | 20 |
| 245 | 0.66804 | 24030 | 2 | Sept. I | 295 | 0.80493 | 28946 | 22 | 21 |
| 246 | . 67077 | 24129 | 3 | 2 | 296 | . 80767 | 29046 | 23 | 22 |
| 2.47 | . 67351 | 24228 | 4 | 3 | 297 | . SiO40 | 29145 | 24 | 23 |
| 2.48 | . 67625 | 24327 | 5 | 4 | 298 | . Si3IT | 29244 | 25 | 24 |
| 2.49 | .67S99 | 24426 | 6 | 5 | 299 | .Si5SS | 29343 | 26 | 25 |
| 250 | 0.68172 | 24525 | 7 | 6 | 300 | 0.SiS62 | 29442 | 27 | 26 |

DAYS INTO DECIMALS OF A YEAR AND ANGLE.

| $\begin{gathered} \text { Day } \\ \text { of } \\ \text { Year. } \end{gathered}$ | $\begin{aligned} & \text { Decimal } \\ & \text { of } \\ & \text { a Year. } \end{aligned}$ | Angle. | Day of | Month. | $\begin{aligned} & \text { Day } \\ & \text { of } \\ & \text { Year. } \end{aligned}$ | Decimal of a Year. | Angl | Day of Monih. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Common Year | Bissextile Year. |  |  |  |  | Common Year. | Bissextile Year. |
| 301 | 0.82136 | $295{ }^{\circ} 4 \mathrm{I}^{\prime}$ | Oct. 28 | Oct. 27 | 351 | 0.95825 | $344{ }^{\circ}$ |  | Dec. 17 | Dec. :6 |
| 302 | . 82409 | 29640 | 29 |  | 352 | . 96099 |  |  | 18 | 17 |
| 303 | . 82683 | 29740 | 30 | 29 | 353 | . 96372 |  |  | 19 | 18 |
| 304 | . 82957 | 29839 | 3 I | 30 | 354 | . 96646 |  |  | 20 | 19 |
| 305 | 0. 8323 I | 29938 | Nov. I | 3I | 355 | 0.96920 |  |  | 21 | 20 |
| 306 | . 53504 | 30037 | 2 | Nov. I | 356 | . 97194 | 349 |  | 22 | 21 |
| 307 | . 83778 | 30136 | 3 | 2 | 357 | . 97467 |  |  | 23 | 22 |
| 308 | . 84052 | 30235 | 4 | 3 | 358 | .97741 |  |  | 24 | 23 |
| 309 | . 84326 | 30334 | 5 | 4 | 359 | .98oI 5 | 352 |  | 25 | 2.4 |
| 310 | 0.84600 | 30434 | 6 | 5 | 360 | 0.98289 |  |  | 26 | 25 |
| 311 | . 44873 | 30533 | 7 | 6 | 36 I | . 98563 |  |  | 27 | 26 |
| 312 | . 55147 | 30632 | S | 7 | 362 | .9S836 |  |  | 2 S | 27 |
| 313 | . $5_{5421}$ | 30731 | 9 | 8 | 363 | -99110 |  |  | 29 | 2 S |
| 314 | . 55695 | 30830 | 10 | 9 | 364 | . 99384 |  |  | 30 | 29 |
| 315 | 0.85969 | 30929 | 11 | 10 | 365 | 0.99658 |  |  | 31 | 30 |
| 316 | . 56242 | 31028 | 12 | 11 | 366 | . 99932 | 359 |  |  | 31 |
| 317 | . 86516 | 31127 | 13 | 12 |  |  |  |  |  |  |
| 318 | . 86790 | 31227 | 14 | 13 |  |  |  |  |  |  |
| 319 | . 87064 | 31326 | 15 | 14 | Conv | ersion for | ours. | Conv | version for | Minutes. |
| 320 | 0.S7337 | 31425 | 16 | 15 |  |  |  |  |  |  |
| 321 | . 87611 | $\begin{array}{ll}315 & 24\end{array}$ | 17 | 16 | Hrs. | Dec. of Year. | Angle. | Min. | Dec. of Year. | Ang'e. |
| 322 | .87885 | $\begin{array}{llll}316 & 23\end{array}$ | IS | 17 |  |  |  |  |  |  |
| 323 | . SSI $^{\text {S }} 5$ | 3 I 722 | 19 | IS |  |  |  |  |  |  |
| 324 | . 88433 | 3 IS 21 | 20 | 19 | 1 | 0.0001 I | 2.5 | 1 | 0.00000 | 0.04 |
| 325 | $0 . S 8706$ | 319 2I | 21 | 20 | 2 | 23 | 4.9 | 2 | - | . 08 |
| 326 | . 88980 | 32020 | 22 | 2 I | 3 | 34 | 7.4 | 3 ' | , | . 12 |
| 327 | . S 9254 | 32119 | 23 | 22 | 4 | 46 | $9 \cdot 9$ | 4 | I | . 16 |
| 328 | . S 952 S | 322 I8 | 24 | 23 |  |  |  |  |  |  |
| 329 | . S 9 So 2 | 32317 | 25 | 24 | 6 | 0.00057 68 | 12.3 | 6 | 0.00001 | 0.21 .25 |
| 330 | 0.90075 | 32416 | 26 | 25 | 7 | So | 17.2 | 7 | I | . 29 |
| 331 | . 90349 | 32515 | 27 | 26 | 8 | 9 I | 19.7 | 8 | 2 | . 33 |
| 332 | . 90623 | 32615 | 28 | 27 | 9 | 103 | 22.2 | 9 | 2 | . 37 |
| 333 | . 90897 | 32714 | 29 | 2 S |  |  |  |  |  |  |
| 334 | .91170 | 32813 | 30 | 29 | 10 | 0.00114 | 24.6 | 10 | 0.00002 | 0.41 |
|  |  |  |  |  | II | 126 | 27.1 | 20 | 4 | . $\mathrm{S}_{2}$ |
| 335 | 0.91444 | 32912 | Dec. I |  | 12 | 137 | 29.6 | 30 | 6 | 1.23 |
| 336 | .91718 | 33011 | 2 | Dec. 1 | 13 | 148 | 32.0 | 40 | 8 | 1.64 |
| 337 | .91992 | 33110 | 3 | 2 | 14 | 160 | 34.5 | 50 | 10 | 2.05 |
| 338 | . 92266 | 3329 | 4 | 3 |  |  |  |  |  |  |
| 339 | . 92539 | 3339 | 5 | 4 | 15 | 0.0017 I | 37.0 | 60 | 0.00011 | 2.46 |
| 340 | 0.92813 |  | 6 |  | 16 | 183 | 39.4 |  |  |  |
| 34 I | . 93087 | 3357 | 7 | 6 | 17 | 194 | 41.9 |  |  |  |
| 342 | . 93361 | 3366 | S | 7 | IS | 205 | 44.4 |  |  |  |
| 343 | . 93634 | 3375 | 9 | 8 | 19 | 217 | 46.5 |  |  |  |
| 344 | . 93908 | 33 S 4 | Io | 9 | 20 | 0.00228 | 49.3 |  |  |  |
| 345 | 0.94182 |  | II | IO | 21 | 240 | 51.7 |  |  |  |
| 346 | . 944456 | $\begin{array}{ll}340 & \\ 34\end{array}$ | 12 | 11 | 22 | 251 | 54.2 |  |  |  |
| 347 | . 94730 | 3412 | 13 | 12 | 23 | 262 | 56.7 |  |  |  |
| 348 | . 95003 | 342 I | 14 | 13 | 24 | 274 | 59.1 |  |  |  |
| 349 | . 95277 | 343 o | 15 | 14 |  |  |  |  |  |  |
| 350 | 0.9555 I | 34359 | 16 | 15 |  |  |  |  |  |  |

Table 22.
HOURS, MINUTES AND SECONDS INTO DECIMALS OF A DAY.

| Hours. | Day. | Min. | Day. | Min. | Day. | Sec. | Day. | Sec. | Day. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.041667 | 1 | 0.000694 | 31 | 0.021 528 | 1 | 0.000012 | 31 | 0.000359 |
| 2 | .083 333 | 2 | .ool 3 S9 | 32 | . 022222 | 2 | . 000023 | 32 | . 000370 |
| 3 | . 125000 | 3 | . 002083 | 33 | . 022917 | 3 | . 000035 | 33 | . 000382 |
| 4 | . 166667 | 4 | . 002778 | 34 | .02361 I | 4 | . 000046 | 34 | . 000394 |
| 5 | 0.208333 | 5 | 0.003472 | 35 | 0.024305 | 5 | 0.000058 | 35 | 0.000405 |
| 6 | . 250000 | 6 | . 004167 | 36 | . 025000 | 6 | . 000069 | 36 | . 000417 |
| 7 | . 291667 | 7 | .00.4 86I | 37 | . 025694 | 7 | . 0000 osi | 37 | .oon 428 |
| 8 | . 333333 | 8 | . 005556 | 38 | . 026389 | S | .000 093 | 38 | .000440 |
| 9 | . 375000 | 9 | . 006250 | 39 | . 027 o83 | 9 | . 000104 | 39 | . 00045 I |
| 10 | 0.416667 | 10 | 0.006944 | 40 | 0.027778 | 10 | 0.000116 | 40 | 0.000463 |
| 1 I | . 458333 | 11 | . 007639 | 41 | .028 472 | 1 I | .000 127 | 4 I | . 000475 |
| 12 | . 500000 | 12 | .008 333 | 42 | . 029167 | 12 | .000 I39 | 42 | . 000486 |
| 13 | . 541667 | 13 | . 009028 | 43 | . 029861 | 13 | .000 I 50 | 43 | . 000498 |
| 14 | .583333 | 14 | . 009722 | 44 | . 030556 | 14 | .000 I62 | 44 | .000509 |
| 15 | 0.625000 | 15 | 0.010417 | 45 | 0.031250 | 15 | 0.000174 | 45 | 0.000521 |
| 16 | . 666667 | 16 | .OII II I | 46 | .031 944 | 16 | . 000185 | 46 | . 000532 |
| 17 | . 708333 | 17 | . OII 806 | 47 | . 032639 | 17 | .000 197 | 47 | . 000544 |
| 18 | . 750000 | 18 | . 012500 | 48 | . 033333 | 18 | . 000208 | 48 | . 000556 |
| 19 | .791 667 | 19 | .OI3 I9.4 | 49 | . 034028 | 19 | . 000220 | 49 | . 000567 |
| 20 | 0.833333 | 20 | 0.013889 | 50 | 0.034722 | 20 | 0.000231 | 50 | 0.000579 |
| 21 | . 875000 | 21 | .OI4 $5^{83}$ | 5 I | . 035417 | 21 | . 000243 | 5 I | . 000590 |
| 22 | .916667 | 22 | . 015278 | 52 | .036 11 I | 22 | . 000255 | 52 | . 000602 |
| 23 | .958333 | 23 | .O15 972 | 53 | . 036806 | 23 | . 000266 | 53 | .000 6I3 |
| 24 | 1.000000 | 24 | .016667 | 5.4 | . 037500 | 2.4 | .000 278 | 54 | .000 625 |
|  |  | 25 | 0.017361 | 55 | 0.038194 | 25 | 0.000289 | 55 | 0.000637 |
|  |  | 26 | .oIS 056 | 56 | .038 889 | 26 | . 000301 | 56 | . 000648 |
|  |  | 27 | . 018750 | 57 | . 039583 | 27 | .000 3 I 3 | 57 | . 000660 |
|  |  | 2 S | . 019444 | 58 | . 040278 | 28 | .000 324 | 58 | . 000671 |
|  |  | 29 | . 020139 | 59 | . 040972 | 29 | . 000336 | 59 | .000683 |
|  |  | 30 | 0.020833 | 60 | 0.04 I 667 | 30 | 0.000347 | 60 | . 000694 |

table 23.
DECIMALS OF A DAY INTO HOURS, MINUTES AND SECONDS.

| Hundredths of a Day. |  |  |  | Ten Thousandths of a Day. |  |  | Millionths of a Day. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| d. |  | m. | s. | d. | min | sec. | d. | sec. |
| 0.01 |  |  |  | 0.0001 |  | S. 64 | 0.000001 | 0.09 |
| . 02 |  |  |  | 2 |  | 17.28 | 2 | O. 17 |
| . 03 |  |  |  | 3 |  | 25.92 | 3 | 0.26 |
| . 04 |  |  |  | 4 |  | 34.56 | 4 | 0.35 |
| 0.05 | 1 | 12 | - | 0.0005 |  | 4.3 .20 | 0.000005 | 0.43 |
| . 06 |  | 26 |  |  |  | 5 I .84 | 6 | 0.52 |
| . 07 | 1 | 40 |  | 7 | I | 0.48 | 7 | 0.60 |
| . 08 |  |  |  | 8 | I | 9.12 | S | 0. 69 |
| . 09 |  | 9 |  | 9 | I | 17.76 | 9 | 0.78 |
| 0.10 | 2 | 24 | - | 0.0010 | 1 | 26.40 | 0.000010 | 0. 86 |
| . 20 |  | 48 | 0 | 20 | 2 | 52.80 | 20 | 1.73 |
| . 30 |  | 12 | - | 30 | 4 | 19.20 | 30 | 2.59 |
| . 40 | 9 | 36 | - | 40 | 5 | 45.60 | 40 | 3.46 |
| 0.50 |  | O | - | 0.0050 | 7 | 12.00 | 0.000050 |  |
| . 60 |  | 24 | $\bigcirc$ | 60 |  | 38.40 | 60 | 5.18 |
| . 70 |  | 48 |  | 70 |  | 4.80 | 70 | 6.05 |
| . 80 |  | 12 | $\bigcirc$ | So |  | 3 I .20 | So | 6.91 |
| .90 |  | 36 | 0 | 90 | I2 | 57.60 | 90 | $7 \cdot 78$ |

MINUTES AND SECONDS INTO DECIMALS OF AN HOUR.

| Min. | Decimals of an hour. | Min. | Decimals of an hour. | Sec. | Decimals of an hour. | Sec. | Decimals of an hour. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | 0.016667 | 31 | 0.516667 | 1 | 0.000278 | 31 | 0.0086 II |
| 2 | . 033333 | 32 | . 533333 | 2 | . 000556 | 32 | . 008 859 |
| 3 | . 050000 | 33 | . 550000 | 3 | . $000 \mathrm{~S}_{3}$ | 33 | . 009167 |
| 4 | . 066667 | 34 | . 566667 | 4 | . O O1 II I | 34 | .009 444 |
| 5 | o.oS3 333 | 35 | 0.583 333 | 5 | 0.001389 | 35 | 0.009722 |
| 6 | . 100000 | 36 | . 600000 | 6 | .001 667 | 36 | . 010000 |
| 7 | .II6667 | 37 | . 616667 | 7 | .001 944 | 37 | . 010278 |
| 8 | . 133333 | 3 S | . 633333 | S | . 002222 | 3 S | .OIO 556 |
| 9 | . 150000 | 39 | .650000 | 9 | . 002500 | 39 | . 010 S33 |
| 10 | o.I66667 | 40 | 0.666667 | 10 | 0.002778 | 40 | O.OII III |
| II | . 183.333 | 4 I | . 683333 | II | . 003056 | 41 | .OII 389 |
| 12 | . 200000 | 42 | . 700000 | 12 | . 003333 | 42 | .OII 667 |
| 13 | . 216667 | 43 | .716667 | 13 | .003611 | 43 | .OII 944 |
| 14 | . 233333 | 44 | .733333 | 14 | . 003 SS9 | 44 | . 012222 |
| 15 | 0.250000 | 45 | 0.750000 | 15 | 0.004167 | 45 | 0.012500 |
| 16 | . 266667 | 46 | . 766667 | 16 | . 004444 | 46 | . 01277 S |
| 17 | .2S3 333 | 47 | . 783333 | 17 | . 004722 | 47 | . 013056 |
| 18 | . 300000 | 48 | . Soo 000 | 18 | . 005000 | 48 | . 013333 |
| 19 | . 316667 | 49 | .S16667 | 19 | . 005278 | 49 | .013611 |
| 20 | 0.333333 | 50 | $0 . S 33333$ | 20 | 0.005556 | 50 | 0.013 S89 |
| 21 | . 350000 | 51 | . 550000 | 21 | . 005833 | 51 | .014 167 |
| 22 | . 366667 | 52 | . 666667 | 22 | . 006111 | 52 | .OI4 444 |
| 23 | . 383333 | 53 | .SS3 333 | 23 | . 006389 | 53 | .OI4 722 |
| 24 | . 400000 | 54 | . 900000 | 24 | . 006667 | 54 | . 015000 |
| 25 | 0.416667 | 55 | 0.916667 | 25 | 0.006944 | 55 | 0.015 278 |
| 26 | . 433333 | 56 | . 933333 | 26 | . 007222 | 56 | .OI 5.556 |
| 27 | . 450000 | 57 | . 950000 | 27 | . 007500 | 57 | . 015833 |
| 28 | . 466667 | 58 | . 966667 | 28 | . 007778 | 58 | .or6 11 I |
| 29 | . 4 S3 333 | 59 | .9S3 333 | 29 | . 008056 | 59 | .016 359 |
| 30 | 0.500000 | 60 | 1.000000 | 30 | 0.008333 | 60 | 0.016 667 |

Table 25.
LOCAL MEAN TIME AT APPARENT NOON.

| Day of Month. | JAN. | FEB. | MAR. | APR. | MAY. | JUNE. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 8 16 24 | $\begin{array}{lr}\text { h. } & \text { mi. } \\ \text { I2 } & 4 \\ \text { I2 } & 7 \\ \text { I2 } & 10 \\ \text { I2 } & 12\end{array}$ | $\begin{array}{ll}\text { h. } & \text { m. } \\ \text { 12 } & 14 \\ 12 & 14 \\ 12 & 14 \\ 12 & 13\end{array}$ | h. m. <br> I2 I2 <br> I2 II <br> I2 9 <br> I2 6 | h. m. <br> I2 4 <br> I2 2 <br> I2 0 <br> II 58 | $\begin{array}{cc} \text { h. } & \text { m. } \\ \text { II } & 57 \\ \text { II } & 56 \\ \text { II } & 56 \\ \text { II } & 57 \end{array}$ | $\begin{array}{lr} \text { h. } & \text { m. } \\ \text { II } & 58 \\ \text { II } & 59 \\ \text { I2 } & 0 \\ \text { I2 } & 2 \end{array}$ |
|  | JULY. | AUG. | SEPT. | OCT. | NOV. | D. ${ }^{\text {a }}$ C. |
| 1 8 16 24 | h. m. <br> $\begin{array}{ll}\text { I2 } & 4 \\ \text { I2 } & 5 \\ \text { I2 } & 6 \\ \text { I2 } & 6\end{array}$ | $\begin{array}{rr}\mathrm{h} . & \mathrm{m} \\ \mathrm{I} 2 & 6 \\ \mathrm{I} 2 & 5 \\ 12 & 4 \\ \mathrm{I} 2 & 2\end{array}$ | h. m. <br> I2 0 <br> II 58 <br> II 55 <br> II 52 | $\begin{array}{ll} \text { h. } & \text { m. } \\ \text { II } & 50 \\ \text { II } & 48 \\ \text { II } & 46 \\ \text { II } & 44 \end{array}$ | h. m. <br> II 44 <br> II 44 <br> II 45 <br> II 47 | h. m. <br> II 49 <br> II 52 <br> II 56 <br> I2 0 |

Smithoonian Tables.

Table 26.
SIDEREAL TIME INTO MEAN SOLAR TIME.

The tabular values are to be subtracted from a sidereal time interval.

| Hrs. | $\begin{aligned} & \text { Reduction } \\ & \text { to } \\ & \text { Mean Time. } \end{aligned}$ | Min. |  | Min. |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $h$. | m. s. | m. | s. | m. | s. |
| 1 | - 9.83 | 1 | o. 16 | 31 | 5.08 |
| 2 | - 19.66 | 2 | o. 33 | 32 | 5.24 |
| 3 | - 29.49 | 3 | 0. 49 | 33 | 5.41 |
| 4 | - 39.32 | 4 | 0.66 | 34 | 5.57 |
| 5 | - 49.15 | 5 | 0. 82 | 35 | 5.73 |
| 6 | - 58.98 | 6 | 0.98 | 36 | 5.90 |
| 7 | 18.81 | 7 | I. 15 | 37 | 6.06 |
| 8 | I 18.64 | 8 | 1.31 | 35 | 6.23 |
| 9 | I 28.47 | 9 | 1.47 | 39 | 6.39 |
| 10 | 138.30 | 10 | 1.64 | 40 | 6.55 |
| 11 | I 48.13 | II | 1.80 | 41 | 6.72 |
| 12 | I 57.95 | 12 | 1.97 | 42 | 6.88 |
| 13 | 27.78 | 13 | 2.13 | 43 | 7.04 |
| 14 | 2 I7.6I | 14 | 2.29 | 44 | 7.21 |
| 15 | 227.44 | 15 | 2.46 | 45 | 7.37 |
| 16 | 237.27 | 16 | 2.62 | 46 | 7.54 |
| 17 | 2 47.10 | 17 | 2.79 | 47 | 7.70 |
| 18 | 256.93 | 18 | 2.95 | 48 | 7.86 |
| 19 | $3 \quad 6.76$ | I9 | 3.11 | 49 | S. 03 |
| 20 | 316.59 | 20 | 3.28 | 50 | S. 19 |
| 21 | 326.42 | 21 | 3.44 | 51 | 8.36 |
| 22 | 3 36.25 | 22 | 3.60 | 52 | 8.52 |
| 23 | 3 46.08 | 23 | 3.77 | 53 | S.68 |
| 24 | 3 55.9I | 24 | 3.93 | 54 | 8.85 |
|  |  | 25 | 4. 10 | 55 | 9.01 |
|  |  | 26 | 4.26 | 56 | 9.17 |
|  |  | 27 | 4.42 | 57 | 9.34 |
|  |  | 28 | 4.59 | 58 | 9.50 |
|  |  | 29 | 4.75 | 59 | 9.67 |
|  |  | 30 | 4.91 | 60 | 9.83 |

Table 27.
MEAN SOLAR TIME INTO SIDEREAL TIME.

The tabular values are to be added to a mean solar time interval.

| Hrs. | Reduction to Sidereal Time. | Min. | Reduc. tion to Sidereal Time. | Min. | Reducton to Siderea Time. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $h$. | m. s. | m. | s. | m. | s. |
| I | - 9.86 | 1 | 0.16 | 31 | 5.09 |
| 2 | - 19.71 | 2 | 0.33 | 32 | 5.26 |
| 3 | - 29.57 | 3 | 0.49 | 33 | 5.42 |
| 4 | - 39.43 | 4 | 0. 66 | 34 | 5.59 |
| 5 | - 49.28 | 5 | 0.82 | 35 | 5.75 |
| 6 | - 59.14 | 6 | 0.99 | 36 | 5.91 |
| 7 | 19.00 | 7 | 1.15 | 37 | 6.08 |
| 8 | I IS. 85 | 8 | 1.31 | 38 | 6.24 |
| 9 | 128.71 | 9 | I. 48 | 39 | 6.41 |
| 10 | I 38.56 | 10 | 1.64 | 40 | 6.57 |
| II | I 48.42 | 11 | 1.81 | 4 I | 6.74 |
| 12 | I 58.28 | 12 | 1.97 | 42 | 6.90 |
| 13 | 28.13 | 13 | 2. 14 | 43 | 7.06 |
| 1.4 | $2 \quad 17.99$ | 14 | 2.30 | 44 | 7.23 |
| 15 | $2 \quad 27.85$ | 15 | 2.46 | 45 | 7.39 |
| 16 | 237.70 | 16 | 2.63 | 46 | 7.56 |
| 17 | 247.56 | 17 | 2.79 | 47 | 7.72 |
| 18 | 257.42 | IS | 2.96 | 48 | 7.89 |
| 19 | $3 \quad 7.27$ | 19 | 3.12 | 49 | 8.05 |
| 20 | $3 \quad 17.13$ | 20 | 3.29 | 50 | 8.21 |
| 21 | $3 \quad 26.99$ | 21 | 3.45 | 51 | 8.38 |
| 22 | 3 3 | 22 | .3.61 | 52 | 8.54 |
| 23 | 3 46.70 | 23 | 3.78 | 53 | 8.71 |
| 24 | 356.56 | 24 | 3.94 | 54 | 8.87 |
|  |  | 25 | 4. I I | 55 | 9.04 |
|  |  | 26 | 4.27 | 56 | 9.20 |
|  |  | 27 | 4.4 | 57 | 9.36 |
|  |  | 28 | 4.60 | 58 | 9.53 |
|  |  | 29 | 4.76 | 59 | 9.69 |
|  |  | 30 | 4.93 | 60 | 9.86 |

## Reduction for Seconds-sidereal or mean solar.

The tabular values are to be $\left\{\begin{array}{l}\text { subtracted from a sidereal } \\
\text { added to a mean solar }\end{array}\right\}$ time interval.

| Sidereal or Mean Time | 0 | I | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| s. | s. | s. | S. | s. | s. | s. | s. | s. | s. | s. |
| 0 | 0.00 | 0.00 | 0.01 | 0.01 | 0.OI | O.OI | 0.02 | 0.02 | 0.02 | 0.02 |
| 10 | . 03 | . 03 | . 03 | . 04 | . 04 | . 04 | . 04 | . 05 | . 05 | . 05 |
| 20 | . 05 | . 06 | . 06 | . 06 | . 07 | . 07 | . 07 | . 07 | . 08 | . 08 |
| 30 | . 08 | . 08 | . 09 | . 09 | . 09 | . 10 | . 10 | . 10 | . 10 | . II |
| 40 | .II | .II | . 11 | . 12 | . 12 | . 12 | . 13 | .13 | . 13 | . 13 |
| 50 | 0.14 | 0.14 | 0.14 | 0.15 ${ }^{*}$ | 0.15 | 0.15 | 0.15 | 0.16 | 0.16 | 0.16 |

Smithbonian Tableg.

## CONVERSION OF MEASURES OF WEIGHT.

Conversion of avoirdupois pounds and ounces into kilograms . TABLE 28 Conversion of kilograms into avoirdupois pounds and ounces . Table 29 Conversion of grains into grams . . . . . . . . . Table 30 Conversion of grams into grains . . . . . . . . . . . Table 3I

Table 28.

## AVOIRDUPOIS POUNDS AND OUNCES INTO KILOGRAMS.

I avoirdupois pound $=0.4535924$ kilogram.
I avoirdupois ounce $=0.0283495$ kilogram.

| Pounds. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | kg. | kg . | kg. | kg . | kg. | kg. | kg. | kg . | kg. | kg. |
| 0 | 0.0000 | 0.0454 | 0.0907 | 0.1361 | O. 1814 | 0.2268 | 0.2722 | 0.3175 | 0.3629 | $0.40{ }^{2} 2$ |
| 1 | 0.4536 | 0.4990 | 0.5443 | 0.5897 | 0.6350 | 0.6804 | 0.7257 | 0.7711 | 0.8165 | 0.8618 |
| 2 | 0.9072 | 0.9525 | 0.9979 | 1. 0433 | 1.0886 | I. 1340 | I.1793 | 1.2247 | 1.2701 | 1.3154 |
| 3 | 1.3608 | 1.406I | 1.4515 | 1.4969 | 1.5422 | 1.5876 | 1.6329 | 1.6783 | 1.7237 | 1.7690 |
| 4 | 1.8144 | I. 8597 | 1.905I | 1.9504 | 1.9958 | 2.0412 | 2.0565 | 2.1319 | 2. 1772 | 2.2226 |
| 5 | 2.2680 | 2.3133 | 2.3587 | 2.4040 | 2.4494 | 2.4948 | 2.5401 | 2.5855 | 2.6308 | 2.6762 |
| 6 | 2.7216 | 2.7669 | 2.8123 | 2.8576 | 2.9030 | 2.9484 | 2.9937 | 3.0391 | 3.0844 | 3.1298 |
| 7 | 3.175I | 3.2205 | 3.2659 | 3.3112 | 3.3566 | 3.4019 | 3.4473 | 3.4927 | 3.53 So | 3.5834 |
| 8 | 3.6287 | 3.6741 | 3.7195 | 3.7648 | 3.8102 | 3. S $_{555}$ | 3.9009 | 3.9463 | 3.9916 | 4.0370 |
| 9 | 4.0823 | 4.1277 | 4.1731 | 4.2184 | 4.2638 | 4.3091 | $4 \cdot 3545$ | 4.399 S | 4.4452 | 4.4906 |
| Ounces. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
|  | kg . | $\mathrm{kg} \text {. }$ | kg. | kg. | kg. | kg . | kg. | kg. | kg. | kg. |
| 0 | 0.0000 | 0.0028 | 0.0057 | 0.0085 | 0.0113 | 0.0142 | 0.0170 | o.oI98 | 0.0227 | 0.0255 |
| I | . 0283 | . 0312 | . 0340 | . 0369 | . 0397 | . 0425 | . 0454 | . 0482 | . 0510 | . 0539 |
| 2 | . 0567 | . 0595 | . 0624 | . 0652 | .06So | . 0709 | . 0737 | . 0765 | .0794 | .0S22 |
| 3 | . 0850 | .0879 | . 0907 | . 0936 | .0964 | . 0992 | . 102 I | . 1049 | . 1077 | . 1106 |
| 4 | . 1134 | . 1162 | . 1191 | . 1219 | . 1247 | . 1276 | . 1304 | . 1332 | . 1361 | . 13 S9 |
| 5 | 0.1417 | 0.1446 | 0. 1474 | 0.1503 | 0.153I | O. 1559 | 0.1588 | 0.1616 | 0.1644 | 0.1673 |
| 6 | .1701 | . 1729 | .1758 | . 1786 | . 1814 | .1843 | .1871 | . 1899 | . 1928 | . 1956 |
| 7 | . 1984 | .2013 | . 2041 | . 2070 | . 2098 | . 2126 | . 2155 | . 2183 | .2211 | . 2240 |
| 8 | . 2268 | .2296 | . 2325 | . 2353 | . 23 SI | .2410 | . 243 S | . 2466 | . 2495 | . 2523 |
| 9 | . 2551 | . 2580 | . 2608 | . 2637 | . 2665 | . 2693 | . 2722 | . 2750 | . 2778 | . 2807 |
| 10 | 0.2835 | 0.2863 | 0.2892 | 0.2920 | 0.2948 | 0.2977 | 0.3005 | 0.3033 | 0.3062 | 0.3090 |
| II | . 3118 | . 3147 | . 3175 | . 3203 | .3232 | . 3260 | . 3289 | . 3317 | - 3345 | . 3374 |
| 12 | . 3402 | . 3430 | . 3459 | . 3487 | . 3515 | . 3544 | . 3572 | . 3600 | . 3629 | . 3657 |
| 13 | . 3685 | . 3714 | -3742 | . 3770 | . 3799 | .3827 | . 3856 | -3884 | . 3912 | - 3941 |
| 14 | . 3969 | - 3997 | . 4026 | . 4054 | . 4082 | .4III | . 4139 | .4167 | .4196 | . 4224 |
| 15 | .4252 | .428I | . 4309 | . 4337 | .4366 | . 4394 | .4423 | .445 I | . 4479 | . 4508 |

Smithsonian Tables.

Table 29.
KILOGRAMS INTO AVOIRDUPOIS POUNDS AND OUNCES.
I kilogram $=2.204622$ avoirdupois pounds.


Table 30.

## GRAINS INTO GRAMS.

I grain $=0.06479892$ gram.


Smitheonian tableg.

GRAMS INTO GRAINS.
I gram $=15.432356$ grains.


## WIND TAbles.

Synoptic conversion of velocities ..... Table 32
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## SYNOPTIC CONVERSION OF VELOCITIES.

Miles per hour into meters per second, feet per second and kilometers per hour.

| $\begin{aligned} & \text { Miles } \\ & \text { per } \end{aligned}$ hour. | Meters per second | Feet per second. | Kilometers per hour. | Miles per hour. | $\begin{aligned} & \text { Meters } \\ & \text { per } \end{aligned}$ second. |  | Kilometers per hour. | Miles per hour. | Meters per second. | Feet per second | Kilometers per hour. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 | 0.0 | 0.0 | 0.0 | 26.0 | 11.6 | 3 S.I | 41.8 | 52.0 | 23.2 | 76.3 | 83.7 |
| 0.5 | 0.2 | 0.7 | $0 . S$ | 26.5 | 11.8 | 38.9 | 42.6 | 52.5 | 23.5 | 77.0 | 84.5 |
| 1.0 | 0.4 | I. 5 | 1.6 | 27.0 | 12.1 | 39.6 | 43.5 | 53.0 | 23.7 | 77.7 | 85.3 |
| I. 5 | 0.7 | 2.2 | 2.4 | 27.5 | 12.3 | 40.3 | 44.3 | 53.5 | 23.9 | 78.5 | S6.1 |
| 2.0 | 0.9 | 2.9 | 3.2 | 28.0 | 12.5 | 4 I .1 | 45.1 | 54.0 | 24.1 | 79.2 | S6.9 |
| 2.5 | I.I | 3.7 | 4.0 | 28.5 | 12.7 | 41.8 | 45.9 | 54.5 | 24.4 | 79.9 | 87.7 |
| 3.0 | I. 3 | 4.4 | 4.8 | 29.0 | 13.0 | 42.5 | 46.7 | 55.0 | 24.6 | 80.7 | 88.5 |
| 3.5 | 1.6 | 5.1 | 5.6 | 29.5 | 13.2 | $43 \cdot 3$ | 47.5 | 55.5 | 24.8 | 81.4 | 89.3 |
| 4.0 | I.S | 5.9 | 6.4 | 30.0 | 13.4 | 44.0 | 48.3 | 56.0 | 25.0 | 82.I | 90.1 |
| 4.5 | 2.0 | 6.6 | 7.2 | 30.5 | 13.6 | 44.7 | 49.1 | 56.5 | 25.3 | S2.9 | 90.9 |
| 5.0 | 2.2 | 7.3 | 8.0 | 31.0 | I3.9 | 45.5 | 49.9 | 57.0 | 25.5 | S3.6 | 91.7 |
| 5.5 | 2.5 | S.I | 8.9 | 31.5 | I4.I | 46.2 | 50.7 | 57.5 | 25.7 | S. 4.3 | 92.5 |
| 6.0 | 2.7 | S.8 | 9.7 | 32.0 | 14.3 | 46.9 | 51.5 | 58.0 | 25.9 | S5.1 | 93.3 |
| 6.5 | 2.9 | 9.5 | 10.5 | 32.5 | I4.5 | 47.7 | 52.3 | 58.5 | 26.2 | S5. 8 | 94.I |
| 7.0 | 3.1 | 10.3 | 11.3 | 33.0 | 14.8 | 48.4 | 53.1 | 59.0 | 26.4 | S6.5 | 95.0 |
| $7 \cdot 5$ | 3.4 | I 1.0 | 12.1 | 33.5 | 15.0 | 49.1 | 53.9 | 59.5 | 26.6 | 87.3 | 95.8 |
| 8.0 | 3.6 | 11.7 | 12.9 | 34.0 | 15.2 | 49.9 | 54.7 | 60.0 | 26.8 | SS.O | 96.6 |
| 8.5 | 3.8 | 12.5 | 13.7 | 34.5 | 15.4 | 50.6 | 55.5 | 60.5 | 27.0 | 88.7 | 97.4 |
| 9.0 | 4.0 | 13.2 | 14.5 | 35.0 | 15.6 | 51.3 | 56.3 | 61.0 | $27 \cdot 3$ | S9.5 | 98.2 |
| 9.5 | 4.2 | 13.9 | 15.3 | 35.5 | 15.9 | 52.1 | 57.1 | 61.5 | 27.5 | 90.2 | 99.0 |
| 10.0 | $4 \cdot 5$ | 14.7 | 16.1 | 36.0 | 16.1 | 52.8 | 57.9 | 62.0 | 27.7 | 90.9 | 99.8 |
| 10.5 | 4.7 | I5.4 | 16.9 | 36.5 | 16.3 | 53.5 | 5 S .7 | 62.5 | 27.9 | 91.7 | 100.6 |
| II.O | 4.9 | 16.I | 17.7 | 37.0 | 16.5 | 54.3 | 59.5 | 63.0 | 28.2 | 92.4 | IOI. 4 |
| 11.5 | 5.1 | 16.9 | 18.5 | 37.5 | 16.8 | 55.0 | 60.4 | 63.5 | 28.4 | 93.I | 102.2 |
| 12.0 | 5.4 | 17.6 | 19.3 | 38.0 | 17.0 | 55.7 | 61.2 | 64.0 | 28.6 | 93.9 | 103.0 |
| 12.5 | 5.6 | 18.3 | 20.1 | 38.5 | 17.2 | 56.5 | 62.0 | 64.5 | $2 \mathrm{S}$. 8 | 94.6 | 103.8 |
| 13.0 | 5.8 | 19.1 | 20.9 | 39.0 | 17.4 | 57.2 | 62.8 | 65.0 | 29.1 | 95.3 | 104.6 |
| 13.5 | 6.0 | 19.8 | 21.7 | 39.5 | 17.7 | 57.9 | 63.6 | 65.5 | 29.3 | 96.1 | 105.4 |
| 14.0 | 6.3 | 20.5 | 22.5 | 40.0 | 17.9 | 58.7 | 64.4 | 66.0 | 29.5 | 96.8 | 106.2 |
| 14.5 | 6.5 | 21.3 | 23.3 | 40.5 | 18.1 | 59.4 | 65.2 | 66.5 | 29.7 | 97.5 | 107.0 |
| 15.0 | 6.7 | 22.0 | 24.1 | 41.0 | I8.3 | 60.1 | 66.0 | 67.0 | 30.0 | 98.3 | 107.8 |
| 15.5 | 6.9 | 22.7 | 24.9 | 41.5 | IS.6 | 60.9 | 66.8 | 67.5 | 30.2 | 99.0 | 108.6 |
| 16.0 | 7.2 | 23.5 | 25.7 | 42.0 | 18.8 | 61.6 | 67.6 | 68.0 | 30.4 | 99.7 | 109.4 |
| 16.5 | 7.4 | 24.2 | 26.6 | 42.5 | 19.0 | 62.3 | 65.4 | 68.5 | 30.6 | 100.5 | 110.2 |
| 17.0 | 7.6 | 24.9 | 27.4 | 43.0 | 19.2 | 63.1 | 69.2 | 69.0 | 30.8 | 101.2 | 111.0 |
| 17.5 | 7.8 | 25.7 | 28.2 | 43.5 | 19.4 | 63.8 | 70.0 | 69.5 | 31.1 | IOI. 9 | I I 1.8 |
| 18.0 | S.O | 26.4 | 29.0 | 44.0 | 19.7 | 64.5 | 70.8 | 70.0 | 31.3 | 102.7 | I 12.7 |
| 18.5 | S. 3 | 27.1 | 29.8 | 44.5 | 19.9 | 65.3 | 71.6 | 70.5 | 31.5 | 103.4 | I 13.5 |
| 19.0 | S. 5 | 27.9 | 30.6 | 45.0 | 20.1 | 66.0 | 72.4 | 71.0 | 31.7 | 104.1 | 114.3 |
| 19.5 | 8.7 | 28.6 | 3 I .4 | 45.5 | 20.3 | 66.7 | 73.2 | 71.5 | 32.0 | 104.9 | II5.I |
| 20.0 | 8.9 | 29.3 | 32.2 | 46.0 | 20.6 | 67.5 | 74.0 | 72.0 | 32.2 | 105.6 | 115.9 |
| 20.5 | 9.2 | 30.1 | 33.0 | 46.5 | 20.8 | 68.2 | 74.8 | 72.5 | 32.4 | 106.3 | 116.7 |
| 21.0 | 9.4 | 30.8 | 33.8 | 47.0 | 21.0 | 68.9 | 75.6 | 73.0 | 32.6 | 107.1 | I 17.5 |
| 2 I .5 | 9.6 | 31.5 | 34.6 | 47.5 | 21.2 | 69.7 | 76.4 | 73.5 | 32.9 | 107.8 | I I8.3 |
| 22.0 | 9.8 | 32.3 | 35.4 | 48.0 | 21.5 | 70.4 | 77.2 | 74.0 | 33.1 | 108.5 | I 19.I |
| 22.5 | 10.1 | 33.0 | 36.2 | 48.5 | 21.7 | 71.1 | 78.1 | 74.5 | 33.3 | 109.3 | I19.9 |
| 23.0 | 10.3 | 33.7 | 37.0 | 49.0 | 21.9 | 71.9 | 78.9 | 75.0 | 33.5 | 110.0 | 120.7 |
| 23.5 | 10.5 | 34.5 | 37.8 | 49.5 | 22.1 | 72.6 | 79.7 | 75.5 | 33.5 | I 10.7 | I2 1.5 |
| 24.0 | 10.7 | 35.2 | 38.6 | 50.0 | 22.4 | 73.3 | So. 5 | 76.0 | 34.0 | 111.5 | 122.3 |
| 2.4 .5 | 11.0 | 35.9 | 39.4 | 50.5 | 22.6 | 74.1 | SI. 3 | 76.5 | 34.2 | 112.2 | 123.1 |
| 25.0 | 11.2 | 36.7 | 40.2 | 51.0 | 22.8 | 74.8 | S2.I | 77.0 | 34.4 | II 2.9 | 123.9 |
| 25.5 | 11.4 | 37.4 | 41.0 | 5 I .5 | 23.0 | 75.5 | S2.9 | 77.5 | 34.6 | 113.7 | 124.7 |
| 26.0 | II. 6 | $3 \mathrm{S.1}$ | 41.8 | 52.0 | 23.2 | 76.3 | S3.7 | 78.0 | 34.9 | 114.4 | I 25.5 |

## MILES PER HOUR INTO FEET PER SECOND.

I mile per hour $=\frac{44}{30}$ feet per second.

| Miles per hour. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Feet per sec. | Feet per sec. | Feet per | Feet per sec. | Feet per sec | Feet per | Feet per | Feet per | Feet per | Feet per |
| 0 | 0.0 | I. 5 | 2.9 | 4.4 | 5.9 | 7.3 | 8.8 | 10.3 | 11.7 | 2 |
| 10 | 14.7 | 16.1 | 17.6 | 19.1 | 20.5 | 22.0 | 23.5 | 24.9 | 26.4 | 27.9 |
| 20 | 29.3 | 30.8 | 32.3 | 33.7 | 35.2 | 36.7 | 3 S. I | 39.6 | 4I. I | 42.5 |
| 30 | 44.0 | 45.5 | 46.9 | 48.4 | 49.9 | $5 \mathrm{I} \cdot 3$ | 52.8 | 54.3 | 55.7 | 57.2 |
| 40 | 58.7 | 60.1 | 61.6 | 63.1 | 64.5 | 66.0 | 67.5 | 68.9 | 70.4 | 7 I .9 |
| 50 | 73.3 | 74.8 | 76.3 | 77.7 | 79.2 | 80.7 | 82.I | 83.6 | S5.1 | S6.5 |
| 60 | 88.0 | S9.5 | 90.9 | 92.4 | 93.9 | 95.3 | 96.8 | 98.3 | 99.7 | IOI. 2 |
| 70 | 102.7 | 104. I | 105.6 | 107. 1 | 108. 5 | 110.0 | III. 5 | I12.9 | 114.4 | 115.9 |
| So | 117.3 | IIS.S | 120.3 | 121.7 | 123.2 | 124.7 | 126.1 | 127.6 | 129.1 | 130.5 |
| 90 | 132.0 | 133.5 | 134.9 | I36.4 | I 37.9 | 139.3 | 140.8 | 142.3 | 143.7 | I45.2 |
| 100 | 146.7 | 148. 1 | 149.6 | 151.1 | 152.5 | I54.0 | I 55.5 | 156.9 | I5S.4 | 159.9 |
| 110 | 161.3 | 162.8 | 16.4.3 | 165.7 | 167.2 | 168.7 | 170. 1 | 171.6 | 173.1 | 174.5 |
| 120 | 176.0 | 177.5 | 178.9 | ISo. 4 | 181.9 | 183.3 | 184.8 | IS6.3 | 187.7 | IS9.2 |
| 130 | 190.7 | 192.I | 193.6 | 195.1 | 196.5 | 198.0 | 199.5 | 200.9 | 202.4 | 203.9 |
| 140 | 205.3 | 206.8 | 208.3 | 209.7 | 211.2 | 212.7 | 214. 1 | 215.6 | 217.1 | 218.5 |

Table 34.

## FEET PER SECOND INTO MILES PER HOUR.

1 foot per second $=\frac{30}{44}$ miles per hour.

| Feet per sec. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Mites per hr. | Miles per hr. | Miles per hr. |
| 0 | 0.0 | 0.7 | I. 4 | 2.0 | 2.7 | 3.4 | 4.1 | 4.8 | $5 \cdot 5$ | 6.1 |
| 10 | 6.8 | $7 \cdot 5$ | 8.2 | 8.9 | 9.5 | 10.2 | 10.9 | I 1.6 | 12.3 | 13.0 |
| 20 | 13.6 | 14.3 | 15.0 | 15.7 | 16.4 | 17.0 | 17.7 | 18.4 | 19.1 | 19.8 |
| 30 | 20.5 | 2 I . 1 | 21.8 | 22.5 | 23.2 | 23.9 | 24.5 | 25.2 | 25.9 | 26.6 |
| 40 | 27.3 | 28.0 | 28.6 | 29.3 | 30.0 | 30.7 | 31.4 | 32.0 | 32.7 | 33.4 |
| 50 | 34. I | 34.8 | 35.5 | 36.1 | 36.8 | 37.5 | 38.2 | 38.9 | 39.5 | $4{ }^{\circ} 2$ |
| 60 | 40.9 | 41.6 | 42.3 | 43.0 | 43.6 | 44.3 | 45.0 | 45.7 | 46.4 | 47.0 |
| 70 | 47.7 | 48.4 | 49. I | 49.8 | 50.5 | 5 I .1 | 51.8 | 52.5 | 53.2 | 53.9 |
| 80 | 54.5 | 55.2 | 55.9 | 56.6 | $57 \cdot 3$ | 58.0 | 58.6 | 59.3 | 60.0 | 60.7 |
| 90 | 61.4 | 62.0 | 62.7 | 63.4 | 64.1 | 64.8 | 65.5 | 66.1 | 66.8 | 67.5 |
| 100 | 68.2 | 65.9 | 69.5 | 70.2 | 70.9 | 71.6 | 72.3 | 73.0 | 73.6 | 74.3 |
| 110 | 75.0 | 75.7 | 76.4 | 77.0 | 77.7 | 78.4 | 79.1 | 79.8 | 8.5 | SI. 1 |
| 120 | Si. 8 | 82.5 | 83.2 | 83.9 | 84.5 | 85.2 | S5.9 | S6.6 | 87.3 | SS.0 |
| 130 | 88.6 | 89.3 | 90.0 | 90.7 | 91.4 | 92.0 | 92.7 | 93.4 | 94.1 | 94.8 |
| 140 | 95.5 | 96.1 | 96.8 | 97.5 | 98.2 | 98.9 | 99.5 | 100.2 | 100.9 | IOI. 6 |
| 150 | 102.3 | 103.0 | 103.6 | 104.3 | 105.0 | 105.7 | 106.4 | 107.0 | 107.7 | Io8.4 |
| 160 | 109. I | 109.8 | 110.5 | III. I | III. 8 | II2.5 | 113.2 | 113.9 | 114.5 | I 15.2 |
| 170 | II 5.9 | 116.6 | II7.3 | IIS.O | I18.6 | 119.3 | 120.0 | 120.7 | 121.4 | 120.0 |
| ISo | I22.7 | 123.4 | I24. 1 | 124.8 | 125.5 | I26.I | 126.8 | 127.5 | $12 \mathrm{S}$. | 128.9 |
| 190 | 129.5 | 130.2 | I30.9 | 131.6 | 132.3 | 133.0 | I 33.6 | 134.3 | I 35.0 | I 35.7 |

Gmithsonian Tableb.

## METERS PER SECOND INTO MILES PER HOUR.

I meter per second $=2.236932$ miles per hour.

| Meters per second. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Miles per hr. | Miles per lir. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. |
| 0 | 0.0 | 0.2 | 0.4 | 0.7 | 0.9 | I. I | 1.3 | 1.6 | 1.8 | 2.0 |
| I | 2.2 | 2.5 | 2.7 | 2.9 | 3. 1 | 3.4 | 3.6 | 3.8 | 4.0 | 4.3 |
| 2 | $4 \cdot 5$ | 4.7 | 4.9 | 5. I | 5.4 | 5.6 | 5.8 | 6.0 | 6.3 | 6.5 |
| 3 | 6.7 | 6.9 | 7.2 | 7.4 | 7.6 | 7.8 | 8.1 | 8.3 | S. 5 | 8.7 |
| 4 | S. 9 | 9.2 | 9.4 | 9.6 | 9.8 | 10.1 | 10.3 | 10.5 | 10.7 | II.O |
| 5 | 11.2 | ${ }^{1} \mathrm{I} .4$ | II. 6 | 11.9 | 12.1 | 12.3 | 12.5 | 12.8 | 13.0 | 13.2 |
| 6 | 13.4 | 13.6 | 13.9 | 14. I | 14.3 | 14.5 | 14.8 | 15.0 | 15.2 | 15.4 |
| 7 | 15.7 | 15.9 | 16.1 | 16.3 | 16.6 | 16.8 | 17.0 | 17.2 | 17.4 | 17.7 |
| 8 | 17.9 | 18.1 | 18.3 | 18.6 | 18.8 | 19.0 | 19.2 | 19.5 | 19.7 | 19.9 |
| 9 | 20.1 | 20.4 | 20.6 | 20.8 | 21.0 | 2 I .3 | 21.5 | 2 I .7 | 21.9 | 22. I |
| 10 | 22.4 | 22.6 | 22.8 | 23.0 | 23.3 | 23.5 | 23.7 | 23.9 | 24.2 | 24.4 |
| II | 24.6 | 2.4 .8 | 25. I | 25.3 | 25.5 | 25.7 | 25.9 | 26.2 | 26.4 | 26.6 |
| 12 | 26.8 | 27. I | 27.3 | 27.5 | 27.7 | 28.0 | 28.2 | 2 S .4 | 28.6 | 28.9 |
| 13 | 29. I | 29.3 | 29.5 | 29.8 | 30.0 | 30.2 | 30.4 | 30.6 | 30.9 | 31.1 |
| 14 | 31.3 | 31.5 | 31.8 | 32.0 | 32.2 | 32.4 | 32.7 | 32.9 | 33. 1 | 33.3 |
| 15 | 33.6 | 33.8 | 34.0 | 34.2 | 34.4 | 34.7 | 34.9 | 35. I | 35.3 | 35.6 |
| 16 | 35.8 | 36.0 | 36.2 | 36.5 | 36.7 | 36.9 | 37.1 | 37.4 | 37.6 | 37.8 |
| 17 | 38.0 | 38.3 | 3 3.5 | 38.7 | 38.9 | 39.1 | 39.4 | 39.6 | 39.8 | 40.0 |
| IS | 40.3 | 40.5 | 40.7 | 40.9 | 41.2 | 41.4 | 41.6 | 41.8 | 42.1 | 42.3 |
| 19 | 42.5 | 42.7 | 43.0 | 43.2 | 43.4 | 43.6 | 43.8 | 44.1 | $4+3$ | 44.5 |
| 20 | 44.7 | 45.0 | 45.2 | 45.4 | 45.6 | $45 \cdot 9$ | 46.1 | 46.3 | 46.5 | 46.8 |
| 2 I | 47.0 | 47.2 | 47.4 | 47.6 | 47.9 | 48.1 | 4 S .3 | 48.5 | 48.8 | 49.0 |
| 22 | 49.2 | 49.4 | 49.7 | 49.9 | 50.1 | 50.3 | 50.6 | 50.8 | 51.0 | 51.2 |
| 23 | 51.5 | 51.7 | 51.9 | 52.1 | 52.3 | 52.6 | 52.8 | 53.0 | 53.2 | 53.5 |
| 24 | 53.7 | 53.9 | 54.1 | 54.4 | 54.6 | 54.8 | 55.0 | 55.3 | 55.5 | 55.7 |
| 25 | 55.9 | 56.1 | 56.4 | 56.6 | 56.8 | 57.0 | 57.3 | 57.5 | 57.7 | 57.9 |
| 26 | 58.2 | 5 S. 4 | 58.6 | 58.8 | 59.1 | 59.3 | 59.5 | 59.7 | 60.0 | 60.2 |
| 27 | 60.4 | 60.6 | 60.8 | 6 I .1 | 6 I .3 | 61.5 | 6 I .7 | 62.0 | 62.2 | 62.4 |
| 28 | 62.6 | 62.9 | 63.1 | 63.3 | 63.5 | 63.8 | 64.0 | 64.2 | 64.4 | 64.6 |
| 29 | 64.9 | 65.1 | 65.3 | 65.5 | 65.8 | 66.0 | 66.2 | 66.4 | 66.7 | 66.9 |
| 30 | 67.1 | 67.3 | 67.6 | 67.8 | 68.0 | 68.2 | 68.5 | 68.7 | 68.9 | 69.1 |
| 31 | 69.3 | 69.6 | 69.8 | 70.0 | 70.2 | 70.5 | 70.7 | 70.9 | 71.1 | 71.4 |
| 32 | 71.6 | 71.8 | 72.0 | 72.3 | 72.5 | 72.7 | 72.9 | 73. 1 | 73.4 | 73.6 |
| 33 | 73.8 | 74.0 | 74.3 | 74.5 | 74.7 | 74.9 | 75.2 | 75.4 | 75.6 | 75.8 |
| 34 | 76.1 | 76.3 | 76.5 | 76.7 | 77.0 | 77.2 | 77.4 | 77.6 | 77.8 | 78.1 |
| 35 | 78.3 | 78.5 | 78.7 | 79.0 | 79.2 | 79.4 | 79.6 | 79.9 | So. I | So. 3 |
| 36 | So. 5 | So. 8 | Si.o | SI. 2 | SI. 4 | SI. 6 | SI. 9 | S2.I | S2.3 | S2.5 |
| 37 | 82.8 | 83.0 | 83.2 | 83.4 | 83.7 | 84.0 | S4. I | S4.3 | S4.6 | S4.8 |
| 38 | 85.0 | S5.2 | S5.5 | 85.7 | S5.9 | S6. I | 86.3 | S6.6 | S6.8 | S7.0 |
| 39 | 87.2 | S7.5 | 87.7 | 87.9 | S8. I | 88.4 | S8. 6 | S8.8 | S9.0 | S9.3 |
| 40 | S9.5 | 89.7 | S9.9 | 90.2 | 90.4 | 90.6 | 90.8 | 91.0 | 91.3 | 91.5 |
| 41 | 91.7 | 91.9 | 92.2 | 92.4 | 92.6 | 92.8 | 93. I | 93.3 | 93.5 | 93.7 |
| 42 | 94.0 | 94.2 | 94.4 | 94.6 | 94.8 | 95.1 | 95.3 | 95.5 | 95.7 | 96.0 |
| 43 | 96.2 | 96.4 | 96.6 | 96.9 | 97.1 | 97.3 | 97.5 | 97.8 | 98.0 | 98.2 |
| 44 | 98.4 | 98.7 | 98.9 | 99. I | 99.3 | 99.5 | 99.8 | 100.0 | 100.2 | 100.4 |


| Meters per second. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. | Miles per hr. |
| 45 | 100.7 | 100.9 | IOI. I | IOI. 3 | 101.6 | IOI. 8 | 102.0 | 102.2 | 102.5 | 102.7 |
| 46 | IO2.9 | 103.1 | 103.3 | 103.6 | 103.8 | 104.0 | 104.2 | 104.5 | 104.7 | 104. 9 |
| 47 | 105. I | 105.4 | 105.6 | 105.8 | 106.0 | 106.3 | 106.5 | 106.7 | 106.9 | 107.2 |
| 48 | 107.4 | 107.6 | 107.8 | 108.0 | 108.3 | IoS. 5 | 108.7 | 108.9 | 109.2 | 109.4 |
| 49 | 109.6 | 109.8 | IIO. I | 110.3 | I 10.5 | 110.7 | III. 0 | II I. 2 | II II. 4 | III. 6 |
| 50 | III.S | II2.I | II 2.3 | II2.5 | 112.7 | II3.0 | II3.2 | II3.4 | II3.6 | II3.9 |
| 51 | I 14.1 | 114.3 | I 14.5 | I 14.8 | II 5.0 | II 5.2 | II5.4 | 115.7 | II5.9 | 116. 1 |
| 52 | I 16.3 | 116.6 | II6.8 | 117.0 | 117.2 | II7.4 | 117.7 | II7.9 | IIS.I | IIS.3 |
| 53 | IIS.6 | II8.8 | 119.0 | II9.2 | I 19.5 | 119.7 | 119.9 | 120. 1 | 120.4 | 120.6 |
| 54 | 120.8 | 121.0 | 121.3 | 121.5 | 121.7 | 121.9 | 122.1 | 122.4 | 122.6 | 122.8 |
| 55 | 123.0 | 123.3 | 123.5 | 123.7 | 123.9 | 12.4 .2 | 124.4 | 124.6 | I24.8 | I25. I |
| 56 | 125.3 | 125.5 | 125.7 | 126.0 | 126.2 | I26.4 | 126.6 | 126.8 | 127.1 | 127.3 |
| 57 | 127.5 | 127.8 | I28.0 | I28.2 | I28.4 | 128.6 | 128.9 | 129. I | 129.3 | 129.5 |
| 58 | 129.7 | 130.0 | 130.2 | I 30.4 | 130.7 | 130.9 | I3I. 1 | 131.3 | 131.6 | 131.8 |
| 59 | I 32.0 | 132.2 | I 32.5 | 132.7 | I32.9 | I33. I | 133.3 | I 33.6 | I 33.8 | 134.0 |

table 36.

## MILES PER HOUR INTO METERS PER SECOND.

I mile per hour $=0.4470409$ meters per second.

| Miles per hour. | 0 | I | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | meters per sec. | meters per sec. | meters per sec. | meters <br> per sec. | meters <br> per sec. | meters <br> per sec. | meters per sec. | meters per sec. | meters per sec. | meters per sec. |
| 0 | 0.00 | 0.45 | o. 89 | 1.34 | I. 79 | 2.24 | 2.68 | 3.13 | 3.58 | 4.02 |
| 10 | 4.47 | 4.92 | $5 \cdot 36$ | 5.81 | 6.26 | 6.71 | 7.15 | 7.60 | 8.05 | 8.49 |
| 20 | 8.94 | 9.39 | 9.83 | 10.28 | 10.73 | II. I8 | 11.62 | 12.07 | 12.52 | 12.96 |
| 30 | 13.41 | 13.86 | 14.31 | 14.75 | 15.20 | 15.65 | 16.09 | 16.54 | 16.99 | 17.43 |
| 40 | I7.88 | 18.33 | 18.78 | 19.22 | 19.67 | 20.12 | 20.56 | 21.01 | 21.46 | 21.90 |
| 50 | 22.35 | 22.80 | 23.25 | 23.69 | 24. I4 | 24.59 | 25.03 | 25.48 | 25.93 | 26.37 |
| 60 | 26.82 | 27.27 | 27.72 | 28.16 | 28.61 | 29.06 | 29.50 | 29.95 | 30.40 | 30.85 |
| 70 | 31.29 | 31.74 | 32.19 | 32.63 | 33.08 | 33.53 | 33.98 | 34.42 | 34.87 | 35.32 |
| 80 | 35.76 | 36.21 | 36.66 | 37.10 | 37.55 | 3 S .00 | 38.44 | 38.89 | 39.34 | 39.79 |
| 90 | 40.23 | 40.68 | 4 I . I 3 | 4 I .57 | 42.02 | 42.47 | 42.92 | $43 \cdot 36$ | 43.81 | 44.26 |
| 100 | 44.70 | 45. 15 | 45.60 | 46.04 | 46.49 | 46.94 | 47.39 | 47.83 | 48.28 | 48.73 |
| 110 | 49.17 | 49.62 | 50.07 | 50.51 | 50.96 | 5 I .41 | 51.86 | 52.30 | 52.75 | 53.20 |
| 120 | 53.64 | 54.09 | 54.54 | 54.98 | 55.43 | 55.88 | 56.33 | 56.77 | 57.22 | 57.67 |
| 130 | 58.12 | 58.56 | 59.01 | 59.46 | 59.90 | 60.35 | 60.80 | 61.24 | 61.69 | 62. 14 |
| 140 | 62.59 | 63.03 | 63.48 | 63.93 | 64.37 | 64.82 | 65.27 | 65.72 | 66.16 | 66.61 |

Smithsonian Tables.

Table 37.
METERS PER SECOND INTO KILOMETERS PER HOUR.
I meter per second $=3.6$ kilometers per hour.

| Meters per second. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { kim. } \\ & \text { per hr. } \end{aligned}$ | $\underset{\text { per hr. }}{\text { kin. }}$ | $\begin{aligned} & \mathrm{km} . \\ & \text { per } \mathrm{hr} . \end{aligned}$ | $\begin{gathered} \text { kni. } \\ \text { per hr. } \end{gathered}$ | $\begin{aligned} & \text { km. } \\ & \text { per hr. } \end{aligned}$ | $\begin{gathered} \text { knı. } \\ \text { per hr. } \end{gathered}$ | $\underset{\text { km. }}{\text { per hr. }}$ | $\underset{\text { per } \mathrm{kr} .}{\mathrm{km.}}$ | $\begin{gathered} \text { km. } \\ \text { per hr. } \end{gathered}$ | $\operatorname{km.}_{\text {per hr. }}$ |
| 0 | 0.0 | 0. 4 | 0.7 | I. I | 1.4 | I.S | 2.2 | 2.5 | 2.9 | 3.2 |
| I | 3.6 | 4.0 | $4 \cdot 3$ | 4.7 | 5.0 | 5.4 | 5.8 | 6.1 | 6.5 | 6.8 |
| 2 | 7.2 | 7.6 | 7.9 | S. 3 | S.6 | 9.0 | 9.4 | 9.7 | 10.1 | 10.4 |
| 3 | 10.8 | 11.2 | 11.5 | 11.9 | 12.2 | 12.6 | 13.0 | 13.3 | 13.7 | 14.0 |
| 4 | 14.4 | 14.8 | 15.1 | 15.5 | 15.8 | 16.2 | 16.6 | 16.9 | 17.3 | 17.6 |
| 5 | IS.O | 18.4 | 18.7 | 19. 1 | 19.4 | 19.8 | 20.2 | 20.5 | 20.9 | 21.2 |
| 6 | 21.6 | 22.0 | 22.3 | 22.7 | 23.0 | 23.4 | 23.8 | 24.1 | 24.5 | 24.5 |
| 7 | 25.2 | 25.6 | 25.9 | 26.3 | 26.6 | 27.0 | 27.4 | 27.7 | 2 S . 1 | 28.4 |
| 8 | 28.8 | 29.2 | 29.5 | 29.9 | 30.2 | 30.6 | 31.0 | 31.3 | 31.7 | 32.0 |
| 9 | 32.4 | 32.8 | 33. 1 | 33.5 | 33.8 | 34.2 | 34.6 | 34.9 | $35 \cdot 3$ | 35.6 |
| 10 | 36.0 | 36.4 | 36.7 | 37. I | 37.4 | 37.8 | 38.2 | 38.5 | 38.9 | 39.2 |
| 11 | 39.6 | 40.0 | 40.3 | 40.7 | 41.0 | 41.4 | 41.8 | 42. I | 42.5 | 42.8 |
| 12 | 43.2 | 43.6 | 43.9 | 44.3 | 44.6 | 45.0 | 45.4 | 45.7 | 46.1 | 46.4 |
| 13 | 46.8 | 47.2 | 47.5 | 47.9 | 48.2 | 48.6 | 49.0 | 49.3 | 49.7 | 50.0 |
| 14 | 50.4 | 50.8 | 5 I .1 | 51.5 | 51.8 | 52.2 | 52.6 | 52.9 | 53.3 | 53.6 |
| 15 | 54.0 | 54.4 | 54.7 | 55. I | 55.4 | 55.8 | 56.2 | 56.5 | 56.9 | 57.2 |
| 16 | 57.6 | 58.0 | 58.3 | 58.7 | 59.0 | 59.4 | 59.8 | 60.1 | 60.5 | 60.8 |
| 17 | 6 I .2 | 61.6 | 61.9 | 62.3 | 62.6 | 63.0 | 63.4 | 63.7 | 64.1 | 64.4 |
| 18 | 64.8 | 65.2 | 65.5 | 65.9 | 66.2 | 66.6 | 67.0 | 67.3 | 67.7 | 68.0 |
| 19 | 68.4 | 68.8 | 69.1 | 69.5 | 69.8 | 70.2 | 70.6 | 70.9 | 71.3 | 71.6 |
| 20 | 72.0 | 72.4 | 72.7 | 73.1 | 73.4 | 73.8 | 74.2 | 74.5 | 74.9 | 75.2 |
| 21 | 75.6 | 76.0 | 76.3 | 76.7 | 77.0 | 77.4 | 77.8 | 78.1 | 78.5 | 78.8 |
| 22 | 79.2 | 79.6 | 79.9 | So. 3 | 80.6 | Si.o | SI. 4 | SI. 7 | S2. 1 | S2.4 |
| 23 | S2.8 | S3.2 | 83.5 | 83.9 | S4.2 | S+. 6 | S5.0 | S5.3 | S5.7 | 86.0 |
| 24 | S6.4 | S6.8 | 87.1 | S7.5 | S7.8 | 88.2 | SS. 6 | 88.9 | 89.3 | S9.6 |
| 25 | 90.0 | 90.4 | 90.7 | 91.I | 91.4 | 91.8 | 92.2 | 92.5 | 92.9 | 93.2 |
| 26 | 93.6 | 94.0 | 94.3 | 94.7 | 95.0 | 95.4 | 95.8 | 96. I | 96.5 | 96.8 |
| 27 | 97.2 | 97.6 | 97.9 | 98.3 | 98.6 | 99.0 | 99.4 | 99.7 | 100. I | 100.4 |
| 28 | 100.8 | 101.2 | 101.5 | 101.9 | 102.2 | 102.6 | 103.0 | 103.3 | 103.7 | 10.4 .0 |
| 29 | 104.4 | 104. 8 | 105. I | 105.5 | 105.8 | 106.2 | 106.6 | 106.9 | 107.3 | 107.6 |
| 30 | 108.0 | 108.4 | 108.7 | 109. 1 | 109.4 | 109.8 | 110.2 | 110.5 | 110.9 | III. 2 |
| 3 I | III. 6 | 112.0 | I12.3 | I 12.7 | 113.0 | II 3.4 | $113 . \mathrm{S}$ | II4. 1 | I 14.5 | 114.8 |
| 32 | II 5.2 | 115.6 | 115.9 | II6.3 | I 16.6 | II7.0 | 117.4 | 117.7 | IIS. I | IIS. 4 |
| 33 | I I 8.8 | 119.2 | 119.5 | 119.9 | 120.2 | 120.6 | 121.0 | 121.3 | 121.7 | 122.0 |
| 34 | 122.4 | 122.8 | I23.1 | 123.5 | 123.8 | 124.2 | 124.6 | 124.9 | 125.3 | 125.6 |
| 35 | 126.0 | 126.4 | 126.7 | 127.1 | 127.4 | 127.8 | 12 S .2 | 12S. 5 | $12 \mathrm{S.9}$ | 129.2 |
| 36 | 129.6 | 130.0 | 130.3 | 130.7 | 131.0 | 131.4 | 131.8 | 132. I | I 32.5 | 132.8 |
| 37 | 133.2 | 133.6 | 133.9 | I 34.3 | 134.6 | 135.0 | I 35.4 | 135.7 | 136. 1 | 136.4 |
| 38 | ${ }^{1} 36.8$ | ${ }^{1} 37.2$ | I 37.5 | 137.9 | 138.2 | 138.6 | 139.0 | 139.3 | 139.7 | 140.0 |
| 39 | I. 40.4 | 140.8 | I41. I | 141.5 | 141.8 | 142.2 | 142.6 | 142.9 | 143.3 | 143.6 |
| 40 | 144.0 | 144.4 | 144.7 | 145.1 | 145.4 | 145.8 | 146.2 | 146.5 | 146.9 | 147.2 |
| 41 | 147.6 | 148.0 | 148.3 | 148.7 | 149.0 | 149.4 | I 49.8 | 150.1 | 150.5 | I50.S |
| 42 | ${ }^{1} 51.2$ | 151.6 | 151.9 | 152.3 | 152.6 | I53.0 | 153.4 | 153.7 | I54. I | I 54.4 |
| 43 | 154.8 | ${ }^{1} 55.2$ | I55.5 | 155.9 | 156.2 | ${ }^{1} 56.6$ | 157.0 | 157.3 | 157.7 | 158.0 |
| 44 | 158.4 | 158.8 | 159.1 | 159.5 | 159.8 | 160.2 | 160.6 | 160.9 | 161.3 | Iól. 6 |

Table 37.
METERS PER SECOND INTO KILOMETERS PER HOUR.

| Meters per second. | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | km . per hr. | $\underset{\text { per } \mathrm{km} .}{\mathrm{km} .}$ | $\begin{aligned} & \text { km. } \\ & \text { per } \mathrm{hr} . \end{aligned}$ | $\begin{aligned} & \text { km. } \\ & \text { per } \mathrm{hr} . \end{aligned}$ | $\begin{aligned} & \text { km. } \\ & \text { per hr. } \end{aligned}$ | $\begin{gathered} \mathrm{km} . \\ \text { per } \mathrm{hr} . \end{gathered}$ | km. per hr. | $\begin{aligned} & \mathrm{km} . \\ & \text { per } \mathrm{hr} . \end{aligned}$ | $\begin{aligned} & \mathrm{km} . \\ & \text { per } \mathrm{hr} . \end{aligned}$ | $\underset{\text { per hr. }}{\text { km. }}$ |
| 45 | 162.0 | 162.4 | 162.7 | 163.1 | 163.4 | 163.8 | 16.4 | 164.5 | 164.9 | 165.2 |
| 46 | 165.6 | 166.0 | 166.3 | 166.7 | 167.0 | 167.4 | 167.8 | 168. 1 | 168.5 | 165.8 |
| 47 | 169.2 | 169.6 | 169.9 | 170.3 | 170.6 | 171.0 | 171.4 | 171.7 | 172.1 | 172.4 |
| 4 S | 172.8 | 173.2 | 173.5 | 173.9 | 174.2 | 174.6 | 175.0 | 175.3 | 175.7 | 176.0 |
| 49 | 176.4 | 176.8 | 177.1 | 177.5 | 177.8 | 17S.2 | 178.6 | 178.9 | 179.3 | 179.6 |
| 50 | I 80.0 | 180.4 | 180. 7 | 181. I | 181.4 | 181. 8 | 182.2 | 182.5 | 182.9 | 183.2 |
| 51 | 183.6 | 184.0 | IS4.3 | 184.7 | I85.0 | 185.4 | IS5.8 | 186. 1 | I86.5 | 186.8 |
| 52 | 187.2 | 187.6 | I87.9 | ISS. 3 | IS8.6 | 189.0 | 189.4 | I 89.7 | 190. 1 | 190.4 |
| 53 | 190.8 | 191.2 | 191.5 | 191.9 | 192.2 | 192.6 | 193.0 | 193.3 | 193.7 | 194.0 |
| 54 | 194.4 | 194.8 | 195. I | 195.5 | 195.8 | 196.2 | 196.6 | 196.9 | 197.3 | 197.6 |
| 55 | 198.0 | 198.4 | 198.7 | 199. I | 199.4 | 199.8 | 200.2 | 200.5 | 200.9 | 201.2 |
| 56 | 201.6 | 202.0 | 202.3 | 202.7 | 203.0 | 203.4 | 203.8 | 204. 1 | 204.5 | 204.8 |
| 57 | 205.2 | 205.6 | 205.9 | 206.3 | 206.6 | 207.0 | 207.4 | 207.7 | 20S. I | 208.4 |
| 58 | 208.8 | 209.2 | 209.5 | 209.9 | 210.2 | 210.6 | 211.0 | 211.3 | 211.7 | 212.0 |
| 59 | 212.4 | 212.8 | 213.1 | 213.5 | 213.8 | 214.2 | 214.6 | 214.9 | 215.3 | 215.6 |

Table 38.
KILOMETERS PER HOUR INTO METERS PER SECOND.
I kilometer per hour $=\frac{10}{36}$ meters per second.

| Kilcmeters per hour. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | meters per sec. | meters per sec. | meters per sec. | meters per sec. | meters per sec. | meters per sec. | meters per sec. | meters per sec. | meters per sec. | meters per sec. |
| 0 | 0.00 | 0.28 | 0.56 | 0.83 | I.II | I. 39 | 1.67 | 1.94 | 2.22 | 2.50 |
| 10 | 2.78 | 3.06 | $3 \cdot 33$ | 3.61 | 3.89 | 4.17 | 4.44 | 4.72 | 5.00 | 5.28 |
| 20 | 5.56 | 5.83 | 6.11 | 6.39 | 6.67 | 6.94 | 7.22 | 7.50 | 7.78 | 8.06 |
| 30 | S. 33 | 8.61 | S. 99 | 9.17 | 9.44 | 9.72 | 10.00 | 10.28 | 10.56 | 10.83 |
| 40 | II. I I | I 1.39 | II. 67 | II. 9.4 | 12.22 | 12.50 | 12.78 | 13.06 | 13.33 | 13.61 |
| 50 | 13.89 | 14.17 | 14.44 | 14.72 | 15.00 | 15.28 | 15.56 | 15.83 | 16. 11 | 16.39 |
| 60 | 16.67 | 16.94 | 17.22 | 17.50 | 17.78 | 18.06 | 18.33 | 18.61 | 18.89 | 19.17 |
| 70 | 19.44 | 19.72 | 20.00 | 20.28 | 20.56 | 20.83 | 21.11 | 2 I .39 | 21.67 | 21.94 |
| So | 22.22 | 22.50 | 22.78 | 23.06 | 23.33 | 23.61 | 23.89 | 24. 17 | 24.44 | 24.72 |
| 90 | 25.00 | 25.28 | 25.56 | 25.83 | 26. 11 | 26.39 | 26.67 | 26.94 | 27.22 | 27.50 |
| 100 | 27.78 | 28.06 | 28.33 | 28.61 | 28.89 | 29.17 | 29.44 | 29.72 | 30.00 | 30.28 |
| 110 | 30.56 | 30.83 | 3 I .11 | 31.39 | 31.67 | 31.94 | 32.22 | 32.50 | 32.78 | 33.06 |
| 120 | 33.33 | 33.61 | 33.89 | 34.17 | 34.44 | 34.72 | 35.00 | 35.28 | 35.56 | 35.83 |
| 130 | 36. 11 | 36.39 | 36.67 | 36.94 | 37.22 | 37.50 | 37.78 | 38.06 | 38.33 | 38.61 |
| 140 | 38.89 | 39.17 | 39.44 | 39.72 | 40.00 | 40.28 | 40.56 | 40.83 | 41.11 | 4 I .39 |
| 150 | 41.67 | 41.94 | 42.22 | 42.50 | 42.78 | 43.06 | 43.33 | 43.61 | 43.89 | 44. 17 |
| 160 | 44.44 | 44.72 | 45.00 | 45.28 | 45.56 | 45.83 | 46.11 | 46.39 | 46.67 | 46.94 |
| 170 | 47.22 | 47.50 | 47.78 | 48.06 | 48.33 | 48.61 | 48.89 | 49.17 | 49.44 | 49.72 |
| ISo | 50.00 | 50.28 | 50.56 | 50.83 | 51. II | 51.39 | 51.67 | 5.94 | 52.22 | 52.50 |
| 190 | 52.78 | 53.06 | 53.33 | 53.61 | 53.89 | 54.17 | 54.44 | $5+72$ | 55.00 | 55.28 |

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Table 39.

## SCALE OF VELOCITY EQUIVALENTS OF THE SO-CALLED BEAUFORT SCALE OF WIND.

| Beaufort Number, International | Beaufort description of wind, International | Deep Sea Criterion. 1874, International |  | Specification for use on land | Limits of velocity |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Miles per hour | Meters per sec. |
|  |  |  |  | Nautical (knots) |  | Statute |
| 0 | Calm | Just sufficient to give steerage way. ${ }^{1}$ |  |  | Calm, smoke rises vertically. | $\begin{aligned} & \text { Less } \\ & \text { than } 1 \end{aligned}$ | $\begin{aligned} & \text { Less } \\ & \text { than } 1 \end{aligned}$ | $\begin{aligned} & \text { Less than } \\ & 0.4 \end{aligned}$ |
| 1 | Light air |  |  | Direction of wind shown by smoke drift, but not by wind vanes. | 1 to 3 | 1 to 3 | 0.4 to 1.5 |
| 2 | Light breeze | That in which a well-conditioned man-ofwar, with all sail set, and clean full, would go in smooth water from- | $1 \text { to } 2 \text { knots }$ |  | Wind feit on face: leaves rustle; ordinary vane moved by wind. <br> Leaves and small twigs in constant motion; wind extends light flag. <br> Raises dust and loose paper: small branches are moved. | 4 to 6 | 4 to 7 | 1.6 to 3.3 |
| 3 | $\begin{aligned} & \text { Gentle } \\ & \text { breeze } \end{aligned}$ |  | \| 3 to 4 knots | 7 to 10 |  | 8 to 12 | 3.4 to 5.4 |
| 4 | Moderate breeze |  | 5 to 6 knots | 11 to 16 |  | 13 to 18 | 5.5 to 7.9 |
| 5 | $\begin{aligned} & \text { Fresh } \\ & \text { breeze } \end{aligned}$ | That to which she could just carry in chase, full and by- | $\left\{\begin{array}{l}\text { Royals. \&c } \\ \text { Top gallant } \\ \text { sails. }\end{array}\right.$ | Small trees in leaf begin to sway; crested wavelets form on inland waters. <br> Large branches in motion; whestling heard in telegraph wires; umbrellas used with difficulty. | 17 to 21 | 19 to 24 | 8.0 to 10.7 |
| 6 | Strong brceze |  |  |  | 22 to 27 | 25 to 31 | 10.8 to 13.8 |
| 7 | Moderate gale | That to which she could just carry in chase, full and by- | $\left\{\begin{array}{c}\text { Tonsails, } \\ \text { jnb, \&c. } \\ \\ \text { Reefed up- } \\ \text { per top- } \\ \text { sails and } \\ \text { courses } \\ \text { Lower top- } \\ \text { sails and } \\ \text { courses. }\end{array}\right.$ | Whole trees in motion; inconvenience felt when walking against wind. | 28 to 33 | 32 to 38 | 13.9 to 17.1 |
| 8 | $\begin{gathered} \text { Fresh } \\ \text { gale } \end{gathered}$ |  |  | Breaks twigs off trees; generally impedes progress. | 34 to 40 | 39 to 46 | 17.2 to 20.7 |
| 9 | Strong gale |  |  | Slight structural damage occurs (chimney pots and slate removed). | 41 to 47 | 47 to 54 | 20.8 to 24.4 |
| 10 | Whole gale | That with which she could scarcely bear lower maintopsail and recfed foresail. |  | Seldom experienced inland; trees uprooted; considerable structural damage occurs. | 48 to 55 | 55 to 63 | 24.5 to 28.4 |
| 11 | Storm | That which would reduce her to storm stay-sails. |  | Very rarely experienced, accompanied by wide-spread damage. | 56 to 65 | 64 to 75 | 28.5 to 33.5 |
| 12 | $\begin{aligned} & \text { Hurri- } \\ & \text { cane } \end{aligned}$ | That which no canvas could withstand. |  |  | Above 65 | Above 75 | Above 33.5 |

${ }^{1}$ A full-rigged ship of 1874 .
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Table 40.

## RADIUS OF CRITICAL CURVATURE AND VELOCITIES OF GRADIENT WINDS FOR FRICTIONLESS MOTION IN HIGHS AND LOWS.

## Evglish Measures.

$R_{c}=$ radius of critical curvature in miles. $V_{c}$ High $=$ maximum speed in miles per hour on isobar of critical curvature. $V_{s}=$ speed along straight line isobars $=0.5 V_{c} . \quad V$ Low $=$ speed in Low along isobar of curvature $R_{c} . V$ Low $=0.4142 V_{c}$.
The table is computed for a density of the air, $\rho=.0010$, which represents the conditions in the free air at an elevation of, roughly, one mile. Values for any other density can be readily found by dividing each or any of the tabulated values by the ratio of the densities, as, for example, for surface conditions divide by $1.2=\frac{.0010}{.0012}$ and so on

| $\begin{aligned} & \text { Lati- } \\ & \text { tude: } \\ & \phi \end{aligned}$ | $d$ (miles) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 125 | 150 | 175 | 200 | 250 | 300 | 400 | 500 | 600 | 800 |
| $10^{\circ}$ | $R_{c}$ | 8160 | 6530 | 5440 | 4660 | 4080 | 3260 | 2720 | 2040 | 1630 | 1360 | 1020 |
|  | $V_{c}$ High | 372 | 298 | 248 | 212 | 186 | 149 | 124 | 93.0 | 74.4 | 62.0 | 46.5 |
|  |  | 186 | 149 | 124 | 106 | 93.0 | 74.4 | 62.0 | 46.5 | 37.2 | 31.0 | 23.2 |
|  | $V$ Low | I 54 | 123 | 103 | 88.0 | 77.0 | 61.6 | 51.3 | 38.5 | 30.8 | 25.7 | 19.2 |
| 20 | $R_{c}$ | 2100 | 1680 | 1400 | 1200 | 1050 | S41 | 701 | 526 | 420 | 350 | 263 |
|  | $V_{c} \mathrm{High}$ | 189 | 151 | 126 | 108 | 94.4 | 75.5 | 62.9 | 47.2 | 37.8 | 31.5 | 23.6 |
|  | $V^{\prime}$ s | 94. 4 | 75.5 | 62.9 | 54.0 | 47.2 | 37.8 | 3 I .4 | 23.6 | 18.9 | 15.8 | 11.8 |
|  | $V$ Low | 78.2 | 62.5 | 52.1 | 44.7 | 39. I | 31.3 | 26. I | 19.6 | 15.7 | 13.0 | 9.8 |
| 25 |  | 1380 | 1100 | 918 | 787 | 688 | 551 | 459 | $3+4$ | 275 | 230 | 172 |
|  | $V_{c}^{c}$ High | 153 | 122 | 102 | 87.3 | 76.4 | 61.1 | 50.9 | $3^{8 .} 2$ | 30.6 | 25.5 | 19. I |
|  | $V$ s | 76.4 | 61.1 | 50.9 | 43.6 | 38.2 | 30.6 | 25.4 | 19. I | 15.3 | 12.8 | 9.5 |
|  | $V$ Low | 63.3 | 50.6 | 42.2 | 36.2 | 31.6 | 25.3 | 2I. I | 15.8 | 12.7 | 10.6 | 7.9 |
| 30 |  | 984 | 787 | 656 | 562 | . 492 | 393 | 328 | 2.46 | 197 | 164 | 123 |
|  | $V_{c} \mathrm{High}$ | 129 | 103 | 86. I | 73.8 | 64.5 | 51.6 | 43.0 | 32.3 | 25.8 | 2 I .5 | 16. I |
|  | $V$ s | 64.5 | 51.6 | 43.0 | 36.9 | 32.2 | 25.8 | 21.5 | 16. 2 | 12.9 | 10.8 | 8.1 |
|  | $V$ Low | 53.5 | 42.8 | 35.7 | 30.6 | 26.7 | 21. 4 | 178 | 13.4 | 10.7 | 8.9 | 6.7 |
| 35 |  | 747 | 598 | 498 | 427 | 374 | 299 | 249 | 187 | 150 | 125 | 93.4 |
|  | $V_{c}$ High | 112 | 90.0 | 75.0 | 64.3 | 56.3 | 45.0 | 37.5 | 28. I | 22.5 | 18.8 | 14. I |
|  | $V$ s | 56.3 | 45.0 | 37.5 | 32.2 | 28.2 | 22.5 | 18.8 | 14.0 | 11.2 | 9.4 | 7.0 |
|  | $V$ Low | 46.6 | 37.3 | 31. I | 26.6 | 23.3 | 18.6 | I 5.5 | II. 6 | 9.3 | 7.8 | 5.8 |
| 40 |  | 595 | 476 | 397 | 340 | 298 | 238 | 198 | 149 | 119 | 99.2 | 74.4 |
|  | $V_{c}^{c} \mathrm{High}$ | 100 | 80.3 | 66.9 | 57.4 | 50.2 | 40.2 | 33.5 | 25.1 | 20. 1 | 16.7 | 12.6 |
|  | $V$ s | 50.2 | 40.2 | 33.4 | 28.7 | 25. 1 | 20.1 | 16.8 | 12.6 | 10.0 | 8.4 | 6.3 |
|  | $V$ Low | 41.6 | 33.3 | 27.7 | 23.8 | 20.8 | 16.7 | 13.9 | 10.4 | 8.3 | 6.9 | 5. 2 |
| 45 |  | 492 | 393 | 328 | 28 I | 246 | 197 | 164 | 123 | 98.4 | 82.0 | 61. 5 |
|  | $V_{c}$ High | 91.3 | 73.0 | 60.9 | 52.2 | 45.6 | 36.5 | 30.4 | 22.8 | 18.3 | 15.2 | 11. 4 |
|  | $V^{\prime}$ s | 45.6 | 36.5 | 30.4 | 26. I | 22.8 | 18.2 | 15.2 | II. 4 | 9.2 | 7.6 | $5 \cdot 7$ |
|  | $V$ Low | 37.8 | 30.2 | 25.2 | 21.6 | 18.9 | 15. I | 12.6 | 9.4 | 7.6 | 6.3 | 4.7 |
| 50 |  | 419 | 335 | 279 | 240 | 210 | 168 | 140 | 105 | 83.8 | 69.9 | 52.4 |
|  | $V_{c}{ }_{c}$ High | 84.3 | 67.4 | 56.2 | 48.2 | 42.1 | 33.7 | 28. I | 21. I | 16.9 | 14.0 | 10. 5 |
|  | $V^{\text {s }}$ | 42.1 | 33.7 | 28. I | 24. I | 21.0 | 16.8 | 14.0 | 10.6 | 8.4 | 7.0 | $5 \cdot 3$ |
|  | $V$ Low | 34.9 | 27.9 | 23.3 | 20.0 | 17.4 | 14.0 | 11.6 | 8.7 | 7.0 | 5.8 | $4 \cdot 4$ |
| 55 | $R_{c}$ | 366 | 293 | 244 | 209 | 183 | 147 | 122 | 91.6 | 73.3 | 61.1 | 45.8 |
|  | $V_{c}^{c}$ High | 78.8 | 63.0 | 52.5 | 45.0 | 39.4 | 31.5 | 26.3 | 19.7 | 15.8 | 13.1 | 9.8 |
|  | $V_{s}$ | 39.4 | 31.5 | 26.2 | 22.5 | 19.7 | 15.8 | 13.2 | 9.8 | 7.9 | 6.6 | 4.9 |
|  | $V$ Low | 32.6 | 26. I | 21.7 | 18. 6 | 16.3 | 13.0 | 10.9 | 8.2 | 6.5 | 5.4 | 4.1 |
| 60 | $R_{c}$ | 328 | 262 | 219 | 187 | 16. | 131 | 109 | 82.0 | 65.6 | 54.7 | 41.0 |
|  | $V \mathrm{Cligh}$ | 74.5 | 59.6 | 49.7 | 42.6 |  | 29.8 | 24.8 | 18.6 | 14.9 | 12.4 | 9.3 |
|  | $V \mathrm{~s}$ | 37.3 | 29.8 | 24.8 | 21.3 | 18.6 | 14.9 | 12.4 | 9.3 | $7 \cdot 4$ | 6.2 | $4 \cdot 7$ |
|  | $V$ Low | 30.9 | 24.7 | 20.6 | 17.6 | 15.5 | 12.3 | 10. 3 | $7 \cdot 7$ | 6.2 | 5. I | 3.9 |
| 65 |  | 299 | 240 | 200 | 171 | 150 | 120 | 99.8 | 74.8 | 59.9 | 49.9 | 37.4 |
|  | $V_{c}^{c}$ High | 71.2 | 57.0 | 47.5 | 40.7 | 35.6 | 28.5 | 23.7 | 17.8 | 14.2 | II. 9 | 8.9 |
|  |  | 35.6 | 28.5 | 23.8 | 20.4 | 17.8 | 14.2 | II. 8 | 8.9 | 7.1 | 6.0 | $4 \cdot 4$ |
|  | $V$ Low | 29.5 | 23.6 | 19.7 | 16. 9 | 14.7 | II. 8 | 9.8 | 7.4 | 5.9 | 4.9 | 3.7 |

Table 40.
radius of critical Gurvature and velocities of gradient WINDS FOR FRICTIONLESS MOTION IN HIGHS AND LOWS.

English Measures.

| $\begin{aligned} & \text { Lati- } \\ & \text { tude: } \\ & \text { De } \end{aligned}$ | $d$ (miles) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 125 | 150 | 175 | 200 | 250 | 300 | 400 | 500 | 600 | 800 |
| $70^{\circ}$ |  | 278 | 223 | 86 | 159 | 139 | 111 | 92.8 | 69.6 | 55.7 | 46.4 | $3+.8$ |
|  | $V_{c}{ }_{c}$ High | 68.7 | 55.0 | 45.8 | 39.3 | $3+3$ | 27.5 | 22.9 | 17.2 | 13.7 | 11.4 | 8.6 |
|  | $V_{s}$ | 34.3 | 27.5 | 22.9 | 10.6 | 17.2 | 13.8 | 11.4 | 8.6 | 6.8 | 5.7 | 4.3 |
|  | $V$ Low | 28.5 | 22.8 | 19.0 | 16.3 | 14.2 | 11.4 | 9. 5 | 7.1 | 5.7 | 4.7 | 3.6 |
| 75 |  | 264 | 211 | 176 | 151 | 132 | 105 | 87.9 | 65.9 | 52.7 | 43.9 | 33.0 |
|  | $V_{c}^{c}$ High | 66.8 | 53.5 | +4. 6 | 38.2 | 33.4 | 26.7 | 22.3 | 16.7 | 13.4 | 11. 1 | 8.4 |
|  | $V_{V}{ }^{\text {s }}$ Low | 33.4 27.7 | 26.8 22.2 | 22.3 18.5 | 19. 15 15.8 | 10.7 13.8 | 13.4 11.1 | 11.2 9.2 | 8.4 0.0 | 6.7 5.0 | 5.6 4.6 | 4.2 3.5 |
| 80 |  |  |  | 169 |  |  | 101 | St. 5 | 63.4 |  |  |  |
|  | $V_{c}$ High | 65.5 | 52.4 | 43.7 | 37.5 | 32.8 | 20.2 | 21.8 | 16.4 | 13.1 | 10.9 | 8. 2 |
|  |  | 32.8 | 26.2 | 21.8 | 18.8 | 16.4 | 13. | 10.0 | 8.2 | 6.6 | 5.4 | +. 1 |
|  | $V$ Low | 27. 1 | 21.7 | 18.1 | 15.5 | 13.6 | 10.9 | 9.0 | 6.8 | 5.4 | $+5$ | 3.4 |
| 85 |  |  | 108 | 165 | 142 | 124 | 09.1 | S2.6 | 82.0 | 49.6 | 41.3 | 31.0 |
|  | $V_{c}$ High | 648 | 51.8 | 43.2 | 37.0 | 32.4 | 25.9 | 21.6 | 16.2 | 13.0 | 10.8 | S. I |
|  |  | 32.4 | 25.9 | 22.6 | 18.5 | 16. 2 | 13.0 | 10.8 | S. I | 0.5 | 5.4 | +. 0 |
|  | $V$ Low | 26.8 | 21.5 | 17.9 | 15.3 | 13.4 | 10.7 | 9 | 0.7 | 5.4 | 4.5 | 3.4 |
| 90 |  | 246 | 197 | 164 | 140 | 123 | 08.4 | 82.0 | 61.5 | 49.2 | 41.0 | 30.7 |
|  | $V_{c}^{c}$ High | 64.6 | 51.6 | +3.0 | 36.9 | 32.3 | 25.8 | 21.5 | 16.1 | 12.0 | 10.8 | S. I |
|  | $V_{V}{ }^{\text {s }}$ Low | 32.3 26.8 | 25.8 | 21.5 | 18.4 | 16.2 | 12.9 | 10.8 | 8.0 | 6.4 | 5.4 | 4.0 |
|  | V Low | 20.8 | 21.4 | 17.5 | 15.3 | 13.4 | 10.7 | 8.9 | 6.7 | $5 \cdot 3$ | + 5 | $3 \cdot 3$ |

## Table 41.

radius of critical curvature and velocities of gradient WINDS FOR FRICTIONLESS MOTION IN HIGHS AND LOWS.

## Metric Measures.

$R_{c}=$ radius of critical curvature in kilometers. $\quad V_{c} H i g h=$ maximum speed in meters per second on isobar of critical curvature. $V_{s}=$ speed along straight line isobars $=0.5 V_{c} . V$ Low $=$ speed in Low along isobar of curvature $R_{c} . V$ Low $=0.4142 \mathrm{~V}$.

The remarks in heading of Table 40 relative to the density of the air apply equally to Table 4 I .

| Lati- <br> tude: <br> - | $d$ (kilometers) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 125 | 150 | 175 | 200 | 250 | 300 | 400 | 500 | 600 | 800 |
| $10^{\circ}$ | $R_{c}$ | 8330 | 6660 | 5550 | 4760 | 4160 | 3330 | 2780 | 20So | 1670 | 1390 | 10.40 |
|  | $V_{c}$ High | 105 | 84.3 | 70.2 | 60.2 | 52.7 | 42.1 | 35.1 | 26.3 | 21.1 | 17.6 | 13.2 |
|  | $V$ s | 52.7 | 42.2 | 35. I | 30. I | 26.4 | 21.0 | 17.6 | 13.2 | 106 | 8.8 | 6.6 |
|  | $V$ Low | $43 \cdot 5$ | 34.9 | 29.1 | 24.9 | 21.8 | 17.4 | 14.5 | 10.9 | 8.7 | $7 \cdot 3$ | $5 \cdot 5$ |
| 20 | $R_{c}$ | 2140 | 1710 | r430 | 1220 | 1070 | 857 | 714 | 536 | 429 | 357 | 268 |
|  | $V_{c}$ High | 53.5 | 42.8 | 35.6 | 30.5 | 26.7 | 21.4 | 17.8 | 13.4 | 10.7 | 8.9 | 6.7 |
|  | $V_{s}$ | 26.7 | 21.4 | 17.8 | 15.2 | 13.4 | 10. 7 | 8.9 | 6.7 | 5.4 | 4.4 | 3.4 |
|  | $V$ Low | 22.2 | 17.7 | 14.7 | 12.6 | 11. I | S. 9 | $7 \cdot 4$ | 5.6 | 4.4 | 3.7 | 2.8 |
| 25 | $R_{c}$ | . 1400 | 1120 |  | 802 | 702 | 562 | 468 | 351 | 281 | 234 | 175 |
|  | $V{ }_{c} \mathrm{High}$ | 43.3 | 34.6 | 28.8 | 24.7 | 21.6 | 17.3 | 14.4 | 10.8 | 8.7 | 7.2 | 5.4 |
|  | $V{ }^{\text {s }}$ | 21.6 | 17.3 | 14.4 | 12.4 | 10.8 | 8.6 | 7.2 | 5.4 | 4.4 | 3.6 | 2. 7 |
|  | $V$ Low | 17.9 | 14.3 | 11.9 | 10.2 | 8.9 | 7.2 | 6.0 | $4 \cdot 5$ | 3.6 | 3.0 | 2.2 |
| 30 | $R_{C}$ | 1003 | 802 | 669 | 573 | 501 | 401 | 334 | 251 | 201 | 167 | 125 |
|  | $V_{c}$ High | 36.6 | 29.3 | 24.4 | 20.9 | 18.3 | 14.6 | 12.2 | 9.1 | $7 \cdot 3$ | 6.1 | 4.6 |
|  | $V_{s}$ | 18.3 | 14.6 | 12.2 | 10.4 | 9.2 | $7 \cdot 3$ | 6.1 | 4.6 | 3.6 | 3.0 | 2.3 |
|  | \\|V L Low | 15.2 | 12. I | 10. I | 8.7 | 7.6 | 6.0 | 5. I | 3.8 | 3.0 | 2.5 | 1.9 |

Smithsonian Tables.

Table 41. RADIUS OF CRITICAL CURVATURE AND VELOCITIES OF GRADIENT WINDS FOR FRICTIONLESS MOTION IN HIGHS AND LOWS.

Metric Measures.

| Latitude: | $d$ (kilometers) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 100 | 125 | 150 | 175 | 200 | 250 | 300 | 400 | 500 | 600 | 800 |
| $35^{\circ}$ | $R_{c}$ | 762 | 610 | 508 | 435 | 381 | 305 | 254 | 191 | 152 | 127 | 95.3 |
|  | $V_{c}$ High | 31.9 | 25.5 | 21.3 | 18.2 | I5.9 | 12.8 | 10.6 | 8.0 | 6.4 | $5 \cdot 3$ | 4.0 |
|  | $V_{s}$ | 15.9 | 12.8 | 10.6 | 9. I | 8.0 | 6.4 | $5 \cdot 3$ | 4.0 | 3.2 | 2.6 | 2.0 |
|  | $V$ Low | 13.2 | 10.6 | 8. 8 | $7 \cdot 5$ | 6.6 | $5 \cdot 3$ | 4.4 | $3 \cdot 3$ | 2.7 | 2.2 | 1. 7 |
| 40 | $R_{c}$ | 607 | 485 | 405 | 347 | 303 | ${ }^{2} 43$ | 202 | 152 | 12 I | 101 | 75.8 |
|  | $V_{c}$ High | 28.4 | 22.8 | 19.0 | 16.3 | 14.2 | 11.4 | $9 \cdot 5$ | 7.1 | 5.7 | 4.7 | 75.8 3.6 |
|  | $V_{s}$ | 14.2 | II. 4 | 9.5 | 8. 2 | 7.1 | 5.7 | 4.8 | 3.6 | 2.8 | 2.4 | I. 8 |
|  | 1 Low |  | 9.4 | 7.9 | 6.8 | $5 \cdot 9$ | 4.7 | $3 \cdot 9$ | 2.9 | 2.4 | I. 9 | I. 5 |
| 45 | $R_{c}$ | 501 | 401 | 334 | 287 | 251 | 201 | 167 | 125 | 100 | 83.6 | 62.7 |
|  | $V_{c}$ c High | 25.9 | 20.7 | 17.2 | 14.8 | 12.9 | 10.3 | 8.6 | 6.5 | 5.2 | $4 \cdot 3$ | 3.2 |
|  | $V_{s}$ | 12.9 | 10.4 | 8.6 | 7.4 | 6.4 | 5.2 | 4.3 | 3.2 | 2.6 | 2. 2 | I. 6 |
|  | $V$ Low | 10. 7 | 8.6 | 7.1 | 6.1 | $5 \cdot 3$ | $4 \cdot 3$ | 3.6 | 2. 7 | 2.2 | I. 8 | I. 3 |
| 50 | $R_{c}$ | 427 | $34^{2}$ | 285 | 244 | 214 | 171 | 142 | 107 | 85.5 | 71.2 | 53.4 |
|  | $V_{c}$ c High | 23.9 | 10.1 | 15.9 | 13.6 | II. 9 | 9.5 | 8.0 | 6.0 | 4.8 | 4.0 | 3.0 |
|  | $V^{\text {s }}$ | II. 9 | 9.6 | 8.0 | 6.8 | 6.0 | 4.8 | 4.0 | 3.0 | 2.4 | 2.0 | I. 5 |
|  | $V$ Low | 9.9 | $7 \cdot 9$ | 6.6 | 5.6 | 4.9 | 3.9 | $3 \cdot 3$ | 2.5 | 2.0 | 1.7 | I. 2 |
| 55 | $R_{c}$ | 374 | 299 | 249 | 213 | 187 | 149 | 125 | 93.4 | 74.7 | 62.3 |  |
|  | $V_{c}$ High | 22.3 | 17.9 | $1+9$ | 12.8 | 11. 2 | 8.9 | $7 \cdot 7$ | 5.6 | 4.5 | 3.7 | 2.8 |
|  | $V_{V}{ }^{\text {s }}$ | II. 2 | 9.0 | 7.4 | 6.4 | 5.6 | 4.4 | 3.7 | 2.8 | 2.2 | 1.8 | I. 4 |
|  | 1 Low | 9.2 | 7.4 | 6.2 | $5 \cdot 3$ | 4.6 | 3.7 | 3.1 | 2.3 | 1.9 | I. 5 | I. 2 |
| 60 | $R_{c}$ | 334 | 267 | 223 | 191 | 167 | 134 | 111 | 83.6 | 66.9 | 55.7 | 41.8 |
|  | $V_{c}$ High | 21.1 | 16.9 | 14. 1 | 12. 1 | 10.6 | 8.4 | 7.0 | 5.3 | 4.2 | 3.5 | 2.6 |
|  | $V_{s}$ | 10. 6 | 8.4 | 7.0 | 6.0 | $5 \cdot 3$ | 4.2 | $3 \cdot 5$ | 2.6 | 2.1 | 1.8 | I. 3 |
|  | $V$ Low | 8. 7 | 7.0 | 5.8 | 5.0 | $4 \cdot 4$ | $3 \cdot 5$ | 2.9 | 2.2 | I. 7 | I. 4 | I. I |
| 65 | $R_{c}$ | 305 | 244 | 20.4 | 174 | 153 |  | 102 | 76.3 | 61.0 | 50.9 | 38.2 |
|  | $V_{C} \text { High }$ | 20. 2 | 16. 1 | 13.4 | II. 5 | 10. 1 | 8.1 | 6.7 | 5.0 | 4.0 | 3.4 | 2.5 |
|  | $V^{s}$ s Low | 10. I | 8.0 | 6.7 | 5.8 | 5.0 | 4.0 | 3.4 | 2. 5 | 2.0 | I. 7 | I. 2 |
|  | $V$ Low | S. 4 | 6.7 | 5.6 | 4.8 | 4.2 | $3 \cdot 4$ | 2.8 | 2. I | I. 7 | 1.4 | I. 0 |
| 70 | $R_{c}$ | 284 | 227 | 189 | 162 | 142 |  |  | 71.0 | 56.8 | 47.3 | 35.5 |
|  | $V_{c}$ High | 19. 5 | 15.6 | 13.0 | II. I | 9.7 | 7.8 | -6. 5 | $+9$ | 3.9 | 3.2 | 2.4 |
|  | $V^{\text {s }}$ Low | 9. 7 | 7.8 | 6.5 | 5.6 | 4.8 | 3.9 | 3.2 | 2.4 | 2.0 | I. 6 | 1.2 |
|  | $V$ Low | 8. I | 6.5 | $5 \cdot 4$ | 4.6 | 4.0 | 3.2 | 2.7 | 2.0 | 1. 6 | I. 3 | 1. 0 |
| 75 | $R_{c}$ | 269 | 215 | 179 | 154 | 134 |  |  | 67.2 | $53 \cdot 7$ | 44.8 | 33.6 |
|  | $V_{c}$ High | 18.9 | 15. I | I2. 6 | 10.8 | 9.5 | 7.6 | 6.3 | 4.7 | 3.8 | 3.2 | 2.4 |
|  | $V_{s}$ | $9.5$ | 7.6 | 6.3 | $5 \cdot 4$ | 4.8 | 3.8 | 3.2 | 2.4 | I. 9 | I. 6 | I. 2 |
|  | $V$ Low | 7.8 | 6.3 | 5.2 | 4.5 | 3.9 | 3.1 | 2.6 | 1.9 | I. 6 | I. 3 | I. 0 |
| 80 | $R_{c}$ |  | 207 | 172 | 148 | 129 | 103 | 86.2 | 64.6 | 51.7 | 43.1 | 32.3 |
|  | $V$ c High | 18.6 | 14.9 | 12.4 | 10. 6 | 9.3 | 7.4 | 6.2 | 4.6 | 3.7 | 3. I | 2.3 |
|  |  | 9.3 | 7.4 | 6.2 | 53 | 4.6 | 3.7 | 3.1 | 2.3 | I. 8 | I. 6 | I. 2 |
|  | $V$ Low | $7 \cdot 7$ | 6.2 | 5. I | 4.4 | $3 \cdot 9$ | 3.1 | 2.6 | I. 9 | I. 5 | I. 3 | I. 0 |
| 85 | $R_{c}$ | 25.3 | 202 | 168 | 144 | 126 | 101 | 84. 2 | 63.2 | 50.5 | 42.1 | 31.6 |
|  | $V_{c}$ High | 18.4 | 14.7 | I 2.2 | 10. 5 | 9.2 | $7 \cdot 3$ | 6.1 | 4.6 | 3.7 | 3.1 | 2.3 |
|  | $V^{s}$ Low | 9.2 | 7.4 | 6.1 | 5.2 | 4.6 | 3.6 | 3.0 | 2.3 | 1.8 | I. 6 | I. 2 |
|  | $V$ Low | 7.6 | 6.1 | 5. I | 4.3 | 3.8 | 3.0 | 2. 5 | I. 9 | 1. 5 | 1.3 | I. 0 |
| 90 |  | 251 | 201 | 167 | 143 | 125 | 100 | 83.6 | 62.7 | 50. I | 41.8 | 3 I. 3 |
|  | $V_{c}$ High | 18.3 | 14. 6 | 12.2 | 10.4 | 9.1 | 7.3 | 6.1 | 4.6 | 3.7 | 3.0 | 2.3 |
|  | $V^{\text {s }}$ Low | 9.1 | $7 \cdot 3$ | 6.1 | 5.2 | 4.6 | 3.6 | 3.0 | 2.3 | 1.8 | I. 5 | I. 2 |
|  | $V$ Low | 7.6 | 6.0 | 5. I | $4 \cdot 3$ | 3.8 | 3.0 | 2.5 | 1.9 | I. 5 | I. 2 | 1.0 |

## REDUCTION OF TEMPERATURE TO SEA LEVEL.

English measures
Table 42
Metric measures . . . . . . . . . . . . . . . . Table 43

REDUCTION OF TEMPERATURE TO SEA LEVEL.
ENGLISH MEASURES.

| Rate of decrease $\qquad$ |  | DIF | FERE | NCES | BETW | EEN | $\mathrm{A}^{\prime}$ | EA | $\begin{aligned} & \mathrm{RA}^{\prime} \\ & \mathrm{EV} \end{aligned}$ | URE | T AN | AL |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ALTITUdE in feet. |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 | 1000 | 2000 | 3000 | 4000 | 5000 |
| Feet. | F. | $\bigcirc$ | ${ }^{\circ}$ | $2^{\circ}$ |  |  |  | F. | F. | F. | F. | F. | F. | F. |
| 200 | 0.50 | I.oo | 1.50 | 2.00 | 2.50 | 3.00 | $3 \cdot 50$ | $4.00$ | $4^{\circ} \cdot 50$ | $5.00$ | $10.00$ | $15^{\circ} .00$ | $20.00$ | $25.00$ |
| 205 | 0.49 | 0.98 | 1.46 | I. 95 | 2.44 | 2.93 | 3.41 | 3.90 | $4 \cdot 39$ | 4.88 | 9.76 | 14.63 | 19.51 | 24.39 |
| 210 | 0.48 | 0.95 | I. 43 | I. 90 | 2.38 | 2.86 | 3.33 | 3.8 I | 4.29 | 4.76 | 9.52 | 14.29 | 19.05 | 23.81 |
| 215 | 0.47 | 0.93 | I. 40 | I. 56 | 2.33 | 2.79 | 3.26 | 3.72 | 4.19 | 4.65 | 9.30 | 13.95 | 18.60 | 23.26 |
| 220 | 0.45 | 0.91 | 1.36 | 1.82 | 2.27 | 2.73 | 3.18 | 3.64 | 4.09 | 4.55 | 9.09 | 13.63 | 18.18 | 22.72 |
| 230 | 0.43 | 0.87 | 1.30 | 1.74 | 2.17 | 2.61 | 3.04 | 3.48 | 3.91 | 4.35 | 8.70 | 13.04 | 17.39 | 21.74 |
| 2.40 | 0.42 | 0.83 | 1.25 | 1. 67 | 2.08 | 2.50 | 2.92 | 3.33 | 3.75 | 4.17 | 8.33 | 12.50 | 16.67 | 20.83 |
| 250 | 0.40 | 0.80 | 1.20 | 1. 60 | 2.00 | 2.40 | 2.80 | 3.20 | 3.60 | 4.00 | 8.00 | 12.00 | 16.00 | 20.00 |
| 260 | 0.38 | 0.77 | I. 15 | 1.54 | 1.92 | 2.31 | 2.69 | 3.08 | 3.46 | 3.85 | 7.69 | II 1.54 | ${ }^{1} 5.38$ | 19.23 |
| 270 | 0.37 | 0.74 | I. II | 1.48 | I. 85 | 2.22 | 2.59 | 2.96 | 3.33 | 3.70 | 7.41 | II.II | 14.81 | 18.52 |
| 280 | 0.36 | 0.71 | 1.07 | I. 43 | 1.79 | 2. 14 | 2.50 | 2.86 | 3.21 | $3 \cdot 57$ | 7.14 | 10.71 | 14.29 | 17.86 |
| 290 | 0.34 | 0.69 | 1.03 | 1. 38 | 1.73 | 2.07 | 2.41 | 2.76 | 3.10 | 3.45 | 6.90 | 10.34 | 13.79 | 17.24 |
| 300 | 0.33 | 0.67 | 1.00 | I. 33 | 1.67 | 2.00 | 2.33 | 2.67 | 3.00 | 3.33 | 6.67 | 10.00 | 13.33 | 16.67 |
| 310 | 0.32 | 0.65 | 0.97 | 1.29 | 1.61 | 1.94 | 2.26 | 2.58 | 2.90 | 3.23 | 6.45 | 9.68 | 12.90 | 16.13 |
| 320 | 0.31 | 0.62 | 0.94 | I. 25 | 1.56 | 1.87 | 2.19 | 2.50 | 2.81 | 3.12 | 6.25 | 9.37 | 12.50 | 15.62 |
| 340 | 0.29 | 0.59 | 0.88 | 1. 18 | 1.47 | 1.7 | 2.06 | 2.35 | 2.65 | 2.94 | 5.88 | 8.82 | 11.76 | 14.71 |
| 36 | 0.28 | 0.5 | 0.83 | I. II | I. 39 | 1.67 | I. 94 | 2.22 | 2.50 | 2.78 | 5.56 | 8.33 | I1. II | 13.89 |
| 3 So | 0.26 | 0.53 | 0.79 | I. 05 | 1.32 | 1. 58 | I. 84 | 2. 10 | 2.37 | 2.63 | 5.26 | 7.89 | 10.53 | 13.16 |
| 400 | 0.25 | 0.50 | 0.75 | I. 00 | 1.25 | 1.50 | I. 75 | 2.00 | 2.25 | 2.50 | 5.00 | 7.50 | 10.00 | 12.50 |
| 420 | 0.24 | 0.48 | 0.71 | 0.95 | I. 19 | 1.43 | 1. 67 | I. 90 | 2.14 | 2.38 | 4.76 | 7.14 | 9.52 | II.90 |
| 440 | 0.23 | 0.45 | 0.68 | 0.91 | I. I4 | I. 36 | 1.59 | 1. 82 | 2.05 | 2.27 | 4.55 | 6.82 | 9.09 | II 1.36 |
| 460 | 0.22 | 0.43 | 0.65 | 0.87 | 1.09 | 1.30 | 1.52 | I. 74 | I. 96 | 2.17 | $4 \cdot 35$ | 6.52 | 8.70 | 10.87 |
| 480 | 0.21 | 0.42 | 0.62 | 0.83 | 1.04 | I. 25 | 1.46 | I. 67 | 1.87 | 2.08 | 4.17 | 6.25 | 8.33 | 10.42 |
| 500 | 0.20 | 0.40 | 0.60 | o. 80 | 1.00 | 1.20 | I. 40 | 1.60 | 1.80 | 2.00 | 4.00 | 6.00 | 8.00 | 10.00 |
| 520 | O. 19 | 0.38 | 0.58 | 0.77 | 0.96 | I. 15 | 1.35 | I. 54 | 1.73 | 1.92 | 3.85 | 5.77 | 7.69 | 9.62 |
| 540 | 0.19 | 0.37 | 0.56 | 0.74 | 0.93 | I. II | 1.35 | I. 48 | 1. 67 | I. 85 | 3.70 | 5.56 | 7.41 | 26 |
| 560 | 0. 18 | 0.36 | 0.54 | 0.71 | 0.89 | 1.07 | 1.25 | 1.43 | 1.61 | 1.79 | 3.57 | $5 \cdot 36$ | 7.14 | 8.93 |
| 5 So | 0.17 | 0.34 | 0.52 | 0.69 | 0.86 | I. 03 | 1.21 | 1.38 | 1.55 | 1.72 | 3.45 | 5.17 | 6.90 | 8.62 |
| 600 | 0.17 | 0.33 | 0.50 | 0.67 | 0. 83 | 1.00 | I. 17 | I. 33 | I. 50 | 1.67 | 3.33 | 5.00 | 6.67 | 8.33 |
| 620 | O. 16 | 0.32 | 0.48 | 0.65 | 0.8I | 0.97 | I. 13 | I. 29 | I. 45 | 1.6I | 3.23 | 4.84 | 6.45 | 8.06 |
| 650 | O. 15 | 0.31 | 0.46 | 0.62 | 0.77 | 0.92 | J.08 | 1.23 | 1.38 | I. 54 | 3.08 | 4.62 | 6.15 | 7.69 |
| 700 | 0.14 | 0.29 | 0.43 | 0.57 | 0.71 | 0.86 | 1.00 | I. 14 | 1.29 | I. 43 | 2.86 | 4.29 | 5.71 | 7.14 |
| 750 | 0. 13 | 0.27 | 0.40 | 0.53 | 0.67 | 0.80 | 0.93 | 1.07 | 1.20 | I. 33 | 2.67 | 4.00 | 5.33 | 6.67 |
| 00 | 0.12 | 0.25 | 0.37 | 0.50 | 0.62 | 0.75 | 0.87 | 1.00 | I. 12 | I. 25 | 2.50 | 3.75 | 5.00 | 6.25 |
| 850 | 0.12 | 0.24 | 0.35 | 0.47 | 0.59 | 0.71 | 0.82 | 0.94 | 1.06 | 1. 18 | 2.35 | 3.53 | 4.71 | 5.88 |
| 900 | O. I I | 0.22 | 0.33 | 0.44 | 0.56 | 0.67 | 0.78 | 0.89 | 1.00 | I. II | 2.22 | 3.33 | 4.44 | $5 \cdot 56$ |

Tabular values are to be added to the observed temperature to obtain the temperature at sea level.

REDUCTION OF TEMPERATURE TO SEA LEVEL. METRIC MEASURES.

| Rate of decrease of temperature. $i^{\circ} \mathrm{C}$. forevery | DIFFERENCES |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ALTITUDE IN METERS. |  |  |  |  |  |  |  |  |  |  |  |
|  | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 | 1000 | 2000 | 3000 |
| $\begin{array}{r} \mathrm{m} \\ 100 \end{array}$ | $\begin{gathered} \text { c. } \\ \text { I.Oo } \end{gathered}$ | $\begin{aligned} & \text { c. } \\ & 2.00 \end{aligned}$ | $\begin{gathered} \text { c. } \\ 3.00 \end{gathered}$ | $\begin{gathered} c . \\ 4: 00 \end{gathered}$ | c. 5.00 | $\begin{gathered} c . \\ 6: 00 \end{gathered}$ | $\begin{gathered} \text { c. } \\ 7.00 \end{gathered}$ | c. $8.00$ | C. | c. |  |  |
| 102 | 0.98 | 1.96 | 2.94 | 92 | 4.90 | 5.88 | 6.86 | 7.84 | 8.82 | 9.80 | 19.61 |  |
| 104 | 0.96 | 1.92 | 2.88 | 3.85 | 4.81 | 5.77 | 6.73 | 7.69 | 8.65 | 9.62 | 19.23 | 28.85 |
| 106 | 0.94 | 1. 89 | 2.83 | 3.77 | 4.72 | 5.6 ¢́ | 6.60 | $7 \cdot 55$ | 8. 49 | 9.43 | 18.87 | 28.30 |
| Io8 | 0.93 | 1.85 | 2.78 | 3.70 | 4.63 | 5.56 | 6.48 | 7.41 | S. 33 | 9.26 | 18.52 | 27.78 |
| 110 | 0.91 | 1.82 | 2.73 | 3.64 | 4.55 | 5.45 | 6.36 | 7.27 | 8.18 | 9.09 | I8.18 | 27.27 |
| II5 | 0.87 | 1.74 | 2.61 | 3.48 | 4.35 | 5.22 | 6.09 | 6.96 | 7.83 | 8.70 | 17.39 | 26.09 |
| 120 | 0.83 | 1.67 | 2.50 | 3.33 | 4. 17 | 5.00 | 5.83 | 6.67 | 7.50 | 8.33 | 16.67 | 25.00 |
| 125 | 0.8o | 1.60 | 2.40 | 3.20 | 4.00 | 4.80 | 5.60 | 6.40 | 7.20 | 8.00 | 16.00 | 24.00 |
| 130 | 0.77 | 1.54 | 2.31 | 3.08 | 3.85 | 4.62 | 5.38 | 6.15 | 6.92 | 7.69 | 15.38 | 23.08 |
| 135 | 0.74 | 1.48 | 2.22 | 2.96 | 3.70 | 4.44 | 5.19 | 5.93 | 6.66 | 7.41 | 14.8I | 22.22 |
| 140 | 0.71 | 1.43 | 2.14 | 2.86 | 3.57 | 4.29 | 5.00 | 5.7 I | 6.43 | 7.14 | 14.29 | 21.43 |
| 145 | 0.69 | 1.38 | 2.07 | 2.76 | 3.45 | 4. 14 | 4.83 | $5 \cdot 52$ | 6.21 | 6.90 | 13.79 | 20.69 |
| 150 | 0.67 | 1.33 | 2.00 | 2.67 | 3.33 | 4.00 | 4.67 | $5 \cdot 33$ | 6.00 | 6.67 | 13.33 | 20.00 |
| ${ }^{1} 55$ | 0.65 | 1.29 | 1.94 | 2.58 | 3.23 | 3.87 | $4 \cdot 52$ | 5.16 | 5.8 I | 6.45 | 12.90 | 19.35 |
| 160 | 0.62 | I. 25 | 1.87 | 2.50 | 3.12 | $3 \cdot 75$ | $4 \cdot 37$ | 5.00 | 5.62 | 6.25 | 12.50 | 18.75 |
| 170 | 0.59 | I. I8 | 1.76 | 2.35 | 2.94 | 3.53 | 4. 12 | 4.70 | 5.29 | 5.88 | 11.76 | 17.65 |
| I 80 | 0.56 | I.II | 1.67 | 2.22 | 2.78 | 3.33 | 3.89 | 4.44 | 5.00 | 5.56 | II. I I | 16.67 |
| 190 | 0.53 | 1.05 | 1.58 | 2.10 | 2.63 | 3.16 | 3.68 | 4.2 I | 4.74 | 5.26 | 10.53 | I 5.79 |
| 200 | 0.50 | 1.00 | I. 50 | 2.00 | 2.50 | 3.00 | 3.50 | 4.00 | 4.50 | 5.00 | 10.00 | I 5.00 |
| 210 | 0.48 | 0.95 | I. 43 | 1.90 | 2.38 | 2.86 | $3 \cdot 33$ | 3.8 I | 4.29 | 4.76 | 9.52 | 14.29 |
| 220 | 0.45 | 0.91 | 1. 36 | 1.82 | 2.27 | 2.73 | 3.18 | 3.64 | 4.09 | 4.55 | 9.09 | 13.64 |
| 230 | 0.43 | 0.87 | I. 30 | 1.74 | 2.17 | 2.61 | 3.04 | 3.48 | 3.91 | 4.35 | 8.70 | 13.04 |
| 2.40 | 0.42 | 0.83 | 1.25 | 1.67 | 2.08 | 2.50 | 2.92 | 3.33 | 3.75 | 4.17 | 8.33 | 12.50 |
| 250 | 0.40 | 0.80 | I. 20 | 1.60 | 2.00 | 2.40 | 2.80 | 3.20 | 3.60 | 4.00 | 8.00 | 12.00 |
| 260 | 0.38 | 0.77 | I. 15 | 1.54 | 1.92 | 2.31 | 2.69 | 3.08 | 3.46 | 3.85 | 7.69 | I I 5.54 |
| 270 | 0.37 | 0.74 | I.II | 1.48 | 1.85 | 2.22 | 2.59 | 2.96 | 3.33 | 3.70 | 7.41 | II. II |
| 280 | 0.36 | 0.71 | 1.07 | 1.43 | 1.79 | 2.14 | 2.50 | 2.86 | 3.21 | 3.57 | 7.14 | 10.71 |
| 290 | 0.34 | 0.69 | 1.03 | 1.38 | 1.72 | 2.07 | 2.41 | 2.76 | 3.10 | 3.45 | 6.90 | 10.34 |
| 300 | 0.33 | 0.67 | 1.00 | 1.33 | 1.67 | 2.00 | 2.33 | 2.67 | 3.00 | 3.33 | 6.67 | 10.00 |
| 320 | 0.31 | 0.62 | 0.94 | 1.25 | 1.56 | r. 87 | 2. 19 | 2.50 | 2.81 | 3.12 | 6.25 | 9.37 |
| 340 | 0.29 | 0.59 | 0.88 | I. 18 | 1.47 | 1. 76 | 2.06 | 2.35 | 2.65 | 2.94 | 5.88 | 8.82 |
| 360 | 0.28 | 0.56 | 0. 83 | I.II | 1.39 | 1.67 | 1.94 | 2.22 | 2.50 | 2.78 | 5.56 | 8.33 |
| 3 So | 0.26 | 0.53 | 0.79 | 1.05 | I. 32 | I. 58 | I. 84 | 2.10 | 2.37 | 2.63 | 5.26 | 7.89 |
| 400 | 0.25 | 0.50 | 0.75 | 1.00 | 1.25 | I. 50 | 1.75 | 2.00 | 2.25 | 2.50 | 5.00 | 7.50 |
| 420 | 0.24 | 0.48 | 0.71 | 0.95 | I. 19 | I. 43 | 1.67 | I. 90 | 2.14 | 2.38 | 4.76 | 7.14 |
| 440 | 0.23 | 0.45 | 0.68 | 0.91 | I. 14 | I. 36 | I. 59 | 1.82 | 2.05 | 2.27 | 4.55 | 6.82 |
| 460 | 0.22 | 0.43 | 0.65 | 0.87 | 1.09 | 1.30 | I. 52 | 1.74 | 1.96 | 2.17 | 4.35 | 6.52 |
| 480 | 0.21 | 0.42 | 0.62 | 0.83 | 1.04 | I. 25 | I. 46 | 1. 67 | 1.87 | 2.08 | 4.17 | 6.25 |
| 500 | 0.20 | 0.40 | 0.60 | 0. 80 | 1.00 | I. 20 | 1. 40 | 1.60 | I. 80 | 2.00 | 4.00 | 6.00 |

Tabular values are to be added to the observed temperature to obtain
the temperature at sea level.

## REDUCTION OF BAROMETER READINGS TO STANDARD UNITS

Reduction of the barometer to standard temperature-Table 44
Metric measures ..... Table 45
Reduction of the mercurial column to standard temperature. (For U-shaped manometers with hrass scales.)
English measures ..... Table 46
Metric measures ..... Table 47
Reduction of the mercurial barometer to standard gravity.
Direct reduction from local to standard gravity ..... Table 48
Reduction through variation with latitude-
English measures ..... Table 49
Metric measures ..... Table 50

Table 44.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Ther. mometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 19.0 | 19.5 | 20.0 | 20.5 | 21.0 | 21.5 | 22.0 | 22.5 | 23.0 | 23.5 |
| $\begin{array}{r} \text { F. } \\ 0.0 \end{array}$ | $\begin{gathered} \text { Inch. } \\ \text { +o.050 } \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.05 \mathrm{I} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.052 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.053 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.055 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.056 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.057 \end{gathered}$ | $\begin{gathered} \text { Inclı. } \\ +0.059 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.060 \end{gathered}$ | $\begin{array}{r} \text { Inch. } \\ +0.061 \end{array}$ |
| $+0.5$ | +0.049 | +0.050 | +0.05I | +0.053 | +0.054 | +0.055 | +0.056 | +0.058 | +0.059 | $+0.060$ |
| 1.0 | . 048 | . 049 | . 050 | . 052 | . 053 | . 054 | . 055 | . 057 | . 058 | . 059 |
| 1.5 | . 047 | . 048 | . 049 | .05I | . 052 | . 053 | . 054 | . 056 | . 057 | . 058 |
| 2.0 | . 046 | . 047 | . 049 | . 050 | .05I | .0,52 | . 053 | . 055 | . 056 | . 057 |
| 2.5 | . 045 | . 046 | . 048 | . 049 | . 050 | .05I | . 052 | . 054 | . 055 | . 056 |
| 3.0 | +0.044 | +0.046 | +0.047 | +0.048 | +0.049 | +0.050 | +0.05I | +0.053 | +0.054 | +0.055 |
| 3.5 | . 043 | . 045 | . 046 | . 047 | . 048 | . 049 | . 050 | .05I | . 053 | . 054 |
| 4.0 | . 043 | . 044 | . 045 | . 046 | . 047 | . 048 | . 049 | . 050 | . 052 | . 053 |
| 4.5 | . 042 | . 043 | . 044 | .045 | . 046 | . 047 | . 048 | . 049 | .05I | . 052 |
| 5.0 | .04I | . 042 | . 043 | . 044 | . 045 | . 046 | . 047 | .048 | . 049 | .05I |
| 5.5 | +0.040 | +0.04I | $+0.042$ | +0.043 | +0.044 | $+0.045$ | +0.046 | +0.047 | +0.048 | +0.049 |
| 6.0 | . 039 | . 040 | . 041 | . 042 | . 043 | . 044 | . 045 | . 046 | . 047 | . 0.48 |
| 6.5 | . 038 | . 039 | . 040 | .04I | . 042 | . 043 | . 0.44 | . 045 | . 046 | . 047 |
| 7.0 | . 037 | . 038 | . 039 | . 040 | . 041 | . 042 | . 043 | . 044 | . 045 | . 046 |
| 7.5 | . 037 | . 038 | .038 | . 039 | . 040 | .04I | . 042 | . 043 | . 044 | . 045 |
| 8.0 | +0.036 | +0.037 | $+0.038$ | +0.038 | +0.039 | +0.040 | +0.04I | +0.042 | +0.043 | +0.044 |
| 8.5 | . 035 | . 036 | . 037 | . 038 | . 038 | . 039 | . 040 | . 041 | . 042 | . 043 |
| 9.0 | . 034 | . 035 | . 036 | . 037 | . 038 | . 038 | . 039 | . 040 | . 041 | . 042 |
| 9.5 | . 033 | . 034 | . 035 | . 036 | . 037 | . 037 | . 038 | . 039 | . 040 | .04I |
| 10.0 | . 032 | . 033 | . 034 | . 035 | . 036 | . 036 | . 037 | . 038 | . 039 | . 040 |
| 10.5 | +0.031 | $+0.032$ | +0.033 | +0.034 | +0.035 | +0.035 | +0.036 | $+0.037$ | +0.038 | +0.039 |
| 11.0 | . 030 | . 031 | . 032 | . 033 | . 034 | . 034 | . 035 | . 036 | . 037 | . 038 |
| 11.5 | . 030 | . 030 | . 031 | . 032 | . 033 | . 034 | . 034 | . 035 | . 036 | . 037 |
| 12.0 | . 029 | . 030 | . 030 | .03I | . 032 | . 033 | . 033 | . 034 | . 035 | . 036 |
| 12.5 | . 028 | . 029 | . 029 | . 030 | . 031 | . 032 | . 032 | .033 | . 034 | .c34 |
| 13.0 | +0.027 | $+0.028$ | +0.028 | +0.029 | +0.030 | +0.03I | +0.03I | +0.032 | +0.033 | +0.033 |
| 13.5 | . 026 | . 027 | . 028 | . 028 | . 029 | . 030 | . 030 | .03I | . 032 | . 032 |
| 14.0 | . 025 | . 026 | . 027 | . 027 | . 028 | . 029 | . 029 | . 030 | . 031 | .03I |
| 14.5 | . 024 | . 025 | . 026 | . 026 | . 027 | . 028 | . 028 | . 029 | . 030 | . 030 |
| 15.0 | . 024 | . 024 | . 025 | . 025 | . 026 | . 027 | . 027 | . 028 | . 029 | . 029 |
| 15.5 | +0.023 | +0.023 | +0.024 | $+0.024$ | +0.025 | +0.026 | +0.026 | +0.027 | $+0.027$ | +0.028 |
| 16.0 | . 022 | . 023 | . 023 | . 024 | . 024 | . 025 | . 025 | . 026 | . 226 | . 027 |
| 16.5 | . 021 | . 022 | . 022 | . 023 | . 023 | . 024 | . 024 | . 025 | . 025 | . 026 |
| 17.0 | . 020 | . 021 | . 021 | . 022 | . 022 | . 023 | . 023 | .02.4 | . 024 | . 025 |
| 17.5 | . 019 | . 020 | . 020 | . 02 I | . 021 | . 022 | . 022 | . 023 | . 023 | . 024 |
| 18.0 | +0.018 | +0.019 | +0.019 | +0.020 | $+0.020$ | $+0.021$ | +0.02I | +0.022 | +0.022 | $+0.023$ |
| 18.5 | . 017 | . 018 | . 018 | . 019 | . 019 | . 020 | . 020 | . 021 | . 021 | . 022 |
| 19.0 | . 017 | . 017 | . 018 | . 018 | . 018 | . 019 | . 019 | . 020 | . 020 | . 02 I |
| 19.5 | . 016 | . 016 | . 017 | . 017 | . 017 | . 118 | .oi8 | . 019 | . 019 | . 020 |
| 20.0 | . 15 | . 015 | .or6 | .or6 | . 016 | . 017 | . 017 | . 118 | . 018 | . 018 |
| 20.5 | +0.014 | +0.014 | +0.015 | +0.015 | +0.016 | +0.016 | +0.016 | +0.017 | +0.017 | +0.017 |
| 21.0 | . 013 | . 014 | . O 4 | . 014 | . 015 | . 015 | . 015 | . 016 | . 016 | . 016 |
| 21.5 | . OI 2 | . 013 | . 013 | .OI3 | .oI4 | . 014 | .OI4 | . 015 | . 015 | . 015 |
| 22.0 | . OII | . 012 | . OI 2 | . 012 | .OI3 | . 013 | . 13 | . 014 | .OI4 | . 014 |
| 22.5 | .OII | . OII | . 01 II | .OII | . 012 | .OI2 | . 012 | . 013 | . OI 3 | . 1213 |
| 23.0 | +0.010 | +0.010 | +0.010 | +0.010 | +0.011 | +0.011 | +0.011 | +0.012 | +0.012 | +0.012 |
| 23.5 | . 009 | . 009 | . 009 | . 010 | . 010 | . 010 | . 010 | . 011 | . OI I | . OII |
| 24.0 | . 008 | . 008 | . 008 | . 009 | . 009 | . 009 | . 009 | . 010 | . 010 | . 010 |
| 24.5 | . 007 | . 007 | . 008 | .008 | .008 | . 008 | . 008 | . 009 | . 009 | . 009 |
| 25.0 | . 006 | . 006 | . 007 | . 007 | . 007 | . 007 | . 007 | . 008 | . 008 | . 008 |

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Ther- | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| heit. | 19.0 | 19.5 | 20.0 | 20.5 | 21.0 | 21.5 | 22.0 | 22.5 | 23.0 | 23.5 |
| $\begin{array}{r} \text { F. } \\ 25: 5 \end{array}$ | $\begin{gathered} \text { Inch. } \\ +0.005 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.006 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ + \text { + } .006 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.006 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ \text {--0.006 } \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.006 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ + \text { o.006 } \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.006 \end{gathered}$ | $\begin{array}{r} \text { Inch. } \\ +0.007 \end{array}$ | Inch. <br> $-0.007$ |
| 26.0 | . 005 | . 005 | . 005 | . 005 | . 005 | .005 | . 005 | . 005 | . 005 | . 006 |
| 26.5 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 005 |
| 27.0 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 |
| 27.5 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 |
| 28.0 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +o.0nt | +0.001 | +0.001 | +0.001 | +0.001 |
| 28.5 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.0 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 |
| 29.5 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 |
| 30.0 | . 002 | . 002 | . 002 | . 003 | .003 | . 003 | . 003 | . 003 | . 003 | . 003 |
| 30.5 | -0.003 | -0.003 | -0.003 | $-0.003$ | -0.004 | -0.004 | -0.004 | -0.004 | -0.00. 4 | $-0.034$ |
| 31.0 | . 004 | . 004 | . 004 | . 004 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 |
| 31.5 | . 005 | . 005 | . 005 | . 005 | .005 | . 006 | . 006 | . 006 | . 006 | . 006 |
| 32.0 | . 006 | . 006 | . 006 | . 006 | . 006 | . 007 | . 007 | . 007 | . 007 | . 007 |
| 32.5 | . 007 | . 007 | . 007 | . 007 | . 007 | . 008 | . 008 | . 008 | . 008 | . 008 |
| 33.0 | -0.008 | -0.008 | -0.008 | -0.008 | -0.008 | -0.009 | -0.009 | -0.009 | -0.009 | -0.009 |
| 33.5 | . 008 | . 009 | . 009 | . 009 | .009 | . 010 | . 010 | . 010 | . O IO | . 010 |
| 34.0 | .009 | . 010 | . OIO | . OIO | . 010 | . OIO | . OII | . OI 1 | . OII | . 011 |
| 34.5 | . 010 | . 010 | . OI I | . OI I | . 011 | . OII | .OI 2 | . 012 | .OI 2 | . 013 |
| 35.0 | . OII | . OII | .OI2 | .OI 2 | . 012 | .OI2 | . OI 3 | . O 3 | .OI3 | . 014 |
| 35.5 | -O.OI 2 | -0.012 | -0.012 | -0.013 | -0.013 | -0.013 | -0.014 | -0.014 | -0.014 | -0.015 |
| 36.0 | . 013 | . 013 | . OI 3 | .or 4 | . 114 | . 014 | . 015 | . 015 | . 015 | . 016 |
| 36.5 | . 014 | . 014 | .or4 | . 15 | .oI5 | . 15 | . 016 | . 016 | . 016 | . 017 |
| 37.0 | .or4 | . OI 5 | .oI 5 | . 016 | . 016 | . 16 | . 017 | . 017 | . 017 | .oi8 |
| 37.5 | .O15 | . 016 | .or6 | . 017 | .017 | . OI 7 | . or 8 | . 018 | .oI9 | . 019 |
| 38.0 | -0.016 | $-0.017$ | -0.017 | -0.017 | -0.018 | -0.018 | -0.019 | -0.019 | $-0.020$ | -0.020 |
| 38.5 | . 017 | . 017 | . 018 | . 018 | . 019 | .oI9 | . 020 | . O 2 O | . O 21 | . O 2 I |
| 39.0 | .oI8 | . 018 | .OI9 | . 019 | . 020 | . 020 | . O 2 I , | . 221 | . 022 | . 022 |
| 39.5 | . 019 | . 019 | . 020 | . 020 | . 02 I | . O 2 I | . 022 | . 022 | . 023 | . 023 |
| 40.0 | . 020 | . 020 | . 021 | . 021 | . 022 | . 022 | . 023 | . 023 | . 02.4 | . 024 |
| 40.5 | -0.020 | -0.021 | -0.022 | -0.022 | -0.023 | -0.023 | -0.024 | -0.024 | -0.025 | -0.025 |
| 41.0 | . 02 I | . 022 | . 022 | . 023 | . 024 | . 024 | . 025 | . 025 | . 026 | . 026 |
| 41.5 | . 022 | . 023 | . 023 | . 024 | . 025 | . 025 | . 026 | . 026 | . 027 | . 027 |
| 42.0 | . 023 | . 024 | . 024 | . 025 | . 025 | . 026 | . 027 | . 027 | . 028 | . 029 |
| 42.5 | . 024 | . 025 | . 025 | . 026 | . 026 | . 027 | . 028 | . 028 | . 029 | . 030 |
| 43.0 | -0.025 | -0.025 | -0.026 | -0.027 | -0.027 | -0.028 | $-0.029$ | -0.029 | -0.030 | -0.031 |
| 43.5 | . 026 | . 026 | . 027 | . 028 | . 028 | . 029 | . 030 | . 030 | . 03 I | . 032 |
| 44.0 | . 026 | . 027 | . 028 | . 029 | . 029 | . 030 | . 03 t | . O I | . 032 | . 033 |
| 44.5 | . 027 | . 028 | . 029 | .030 | .030 | .03I | .032 | . 032 | . 033 | . 034 |
| 45.0 | . 028 | . 029 | . 030 | . 030 | . 031 | . 032 | . 033 | . 033 | . 034 | . 035 |
| 45.5 | -0.029 | -0.030 | -0.03I | -0.031 | -0.032 | -0.033 | -0.034 | -0.034 | -0.035 | -0.036 |
| 46.0 | . 030 | . 03 I | .03I | . 032 | . 033 | .034 | . 035 | . 035 | . 036 | . 037 |
| 46.5 | .03I | . 032 | . 032 | . 033 | . 034 | . 035 | . 036 | . 036 | . 037 | .038 |
| 47.0 | . 032 | . 032 | . 033 | . 034 | . 035 | .036 | . 037 | . 037 | .03S | . 039 |
| 47.5 | . 033 | . 033 | . 034 | . 035 | . 036 | . 037 | .038 | .038 | . 039 | . 040 |
| 48.0 | -0.033 | -0.034 | -0.035 | -0.036 | -0.037 | -0.038 | -0.039 | -0.0.40 | -0.040 | -0.041 |
| 48.5 | . 034 | . 035 | . 036 | . 037 | .038 | . 039 | . 040 | . 041 | . 041 | . 042 |
| 49.0 | . 035 | . 036 | . 037 | . 038 | . 039 | . 040 | . 041 | . 042 | . 042 | . 043 |
| 49.5 | .036 | . 037 | . 038 | . 039 | . 040 | . 0.41 | . 042 | . 043 | . 044 | . 044 |
| 50.0 | . 037 | .038 | . 039 | . 040 | .041 | . 042 | . 043 | . 044 | 0. 45 | . 046 |

Table 44.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES

| Attached Thermometer Fahrenheit. | HEIGHT OF THE, BAROMETER IN INCIESS. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 19.0 | 19.5 | 20.0 | 20.5 | 21.0 | 21.5 | 22.0 | 22.5 | 23.0 | 23.5 |
| $\stackrel{F}{\text { F. }}$ | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch | Iuch. |
| 50.5 | -0.038 | -0.039 | -0.040 | -0.0.41 | -0.042 | -0.043 | -0.044 | -0.045 | -0.0.46 | -0.047 |
| 51.0 | . 039 | . 040 | . 041 | . 042 | . 043 | .044 | . 045 | . 046 | 0.47 | . 048 |
| 51.5 | . 039 | . 040 | . 0.41 | . 0.42 | . 044 | . 045 | . 046 | . 047 | . 048 | . 0.49 |
| 52.0 | .040 | .04I | . 042 | . 043 | . 044 | . 046 | . 047 | . 048 | . 049 | . 050 |
| 52.5 | . 041 | . 042 | . 0.43 | . 044 | . 045 | . 047 | .048 | . 049 | . 050 | . 051 |
| 53.0 | -0.042 | -0.043 | -0.044 | -0.045 | -0.046 | -0.047 | -0.049 | -0.050 | -0.05 I | $-0.052$ |
| 53.5 | . 043 | . 044 | . 045 | . 046 | . 047 | . 048 | . 050 | . 051 | . 052 | . 053 |
| 54.0 | . 044 | . 045 | . 046 | . 047 | . 048 | . 049 | . 051 | . 052 | . 053 | . 054 |
| 54.5 | .0.45 | . 046 | . 047 | . 048 | . 049 | . 050 | . 052 | . 053 | . 054 | . 055 |
| 55.0 | . 045 | . 047 | .048 | . 049 | . 050 | . 051 | . 053 | . 054 | . 055 | . 056 |
| 55.5 | -0.046 | -0.047 | -0.049 | -0.050 | -0.05 I | $-0.052$ | -0.054 | -0.055 | -0.056 | -0.057 |
| 56.0 | . 047 | . 048 | . 050 | . 051 | . 052 | . 053 | . 055 | . 056 | . 057 | . 058 |
| 56.5 | . 048 | . 049 | . 050 | . 052 | . 053 | . 054 | . 056 | . 057 | . 058 | . 059 |
| 57.0 | . 049 | . 050 | . 051 | . 053 | . 054 | . 055 | . 057 | . 058 | . 059 | .060 |
| 57.5 | . 050 | . 051 | . 052 | . 054 | . 055 | . 056 | .058 | . 059 | . 060 | .06I |
| 58.0 | -0.05I | -0.052 | $-0.053$ | -0.055 | -0.056 | -0.057 | -0.059 | -0.060 | -0.06I | -0.063 |
| 58.5 | .05I | . 053 | . 054 | . 055 | . 057 | .05' | . 060 | . 061 | . 062 | . 064 |
| 59.0 | . 052 | . 054 | . 055 | . 056 | . 058 | . 059 | . 061 | . 062 | . 063 | . 065 |
| 59.5 | . 053 | . 055 | . 056 | . 057 | . 059 | . 060 | .06I | . 063 | . 064 | . 066 |
| 60.0 | .054 | . 055 | . 057 | .058 | . 060 | .06I | . 062 | . 064 | . 065 | . 067 |
| 60.5 | -0.055 | -0.056 | -0.058 | -0.059 | -0.06I | -0.062 | $-0.063$ | -0.065 | -0.066 | -0.068 |
| 61.0 | . 056 | . 057 | . 059 | . 060 | . 062 | . 063 | . 064 | . 066 | . 067 | . 069 |
| 61.5 | . 057 | .058 | . 060 | .06I | . 062 | . 064 | .065 | . 067 | . 068 | . 070 |
| 62.0 | . 057 | . 059 | . 060 | . 062 | . 063 | . 065 | . 066 | . 068 | .069 | . 071 |
| 62.5 | .058 | . 060 | .06I | . 063 | . 064 | . 066 | . 067 | . 069 | .07I | . 072 |
| 63.0 | -0.059 | -0.06I | -0.062 | -0.064 | $-0.065$ | -0.067 | -0.068 | -0.070 | -0.072 | -0.073 |
| 63.5 | . 060 | . 062 | . 063 | . 065 | . 066 | 0.68 | . 069 | . 071 | . 073 | .074 |
| 64.0 | . 061 | . 062 | . 064 | . 066 | . 067 | . 069 | . 070 | . 072 | . 074 | . 075 |
| 64.5 | . 062 | . 063 | . 065 | . 067 | . 068 | . 070 | .071 | . 073 | . 075 | . 076 |
| 65.0 | . 063 | .064 | . 066 | . 067 | . 069 | . 071 | . 072 | . 074 | . 076 | . 077 |
| 65.5 | -0.063 | -0.065 | $-0.067$ | -0.068 | -0.070 | -0.072 | -0.073 | -0.075 | -0.077 | -0.078 |
| 66.0 | . 064 | . 066 | . 068 | . 069 | . 071 | . 073 | . 074 | . 076 | .078 | . 079 |
| 66.5 | . 065 | . 067 | . 069 | . 070 | . 072 | . 074 | . 075 | . 077 | . 079 | .08I |
| 67.0 | . 066 | . 068 | . 069 | .071 | . 073 | . 075 | . 076 | . 078 | . 080 | .082 |
| 67.5 | . 067 | . 069 | . 070 | . 072 | . 074 | . 076 | . 077 | . 079 | .08I | .083 |
| 68.0 | -0.068 | -0.069 | -0.071 | -0.073 | -0.075 | -0.077 | -0.078 | -0.08o | -0.082 | $-0.084$ |
| 68.5 | . 069 | . 070 | . 072 | . 074 | . 076 | . 078 | . 079 | .08I | .083 | .oS5 |
| 69.0 | .069 | . 071 | . 073 | . 075 | . 077 | . 079 | .080 | . 082 | . 084 | .086 |
| 69.5 | .070 | . 072 | . 074 | . 076 | . 078 | . 079 | .08I | . 083 | . 085 | .087 |
| 70.0 | . 071 | . 073 | . 075 | . 077 | . 079 | .oso | .082 | . 084 | . 086 | . 088 |
| 70.5 | -0.072 | -0.074 | $-0.076$ | -0.078 | -0.080 | -0.08I | $-0.083$ | $-0.085$ | $-0.087$ | -0.089 |
| 71.0 | . 073 | . 075 | . 077 | . 079 | . 080 | .082 | . 084 | .086 | . 088 | . 090 |
| 71.5 | . 074 | . 076 | . 078 | . 079 | . OS I | .083 | .085 | . 087 | .o89 | .09I |
| 72.0 | . 075 | . 076 | . 078 | . 080 | . 082 | .084 | . 086 | . 088 | . 090 | . 092 |
| 72.5 | . 075 | . 077 | . 079 | .OSI | .o83 | .085 | .087 | . 089 | .09I | . 093 |
| 73.0 | -0.076 | $-0.078$ | -0.080 | -0.082 | $-\mathrm{o.OS} 4$ | -0.086 | -0.088 | -0.090 | -0.092 | -0.094 |
| 73.5 | . 077 | .079 | .OSI | . 083 | .085 | . 087 | .089 | . 091 | . 093 | . 095 |
| 74.0 | . 078 | . OSO | .082 | .084 | . 086 | . 088 | . 090 | . 092 | . 09.4 | .096 |
| 74.5 | .079 | .08I | .083 | .o85 | .087 | .089 | .09I | . 093 | . 095 | . 097 |
| 75.0 | .oSo | .082 | .084 | . 086 | .os8 | . 090 | . 092 | . 094 | . 096 | . 099 |

Table 44.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.


## Table 44.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Ther- | HEIGITT OF T |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fahrenheit. | 24.0 | 24.2 | 24.4 | 24.6 | 24.8 | 25.0 | 25.2 | 25.4 | 25.6 | 25.8 |
| $\begin{gathered} \text { F. } \\ 0^{\circ} .0 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.063 \end{gathered}$ | $\begin{array}{r} \text { Inch. } \\ +0.063 \end{array}$ | $\begin{gathered} \text { Inch. } \\ +0.064 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.064 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.065 \end{gathered}$ | $\begin{array}{r} \text { Inch. } \\ +0.065 \end{array}$ | $\begin{gathered} \text { Inch. } \\ +0.066 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ \div 0.066 \end{gathered}$ | $\begin{array}{r} \text { Inch. } \\ +0.067 \end{array}$ | $\begin{gathered} \text { Inch. } \\ +0.067 \end{gathered}$ |
| +0.5 | to.061 | +0.062 | +0.063 | +0.063 | +0.064 | +0.064 | +0.005 | $+0.065$ | +0.066 | +0.066 |
| 1.0 | . 060 | .06I | I .06I | . 062 | . 062 | .063 | . 063 | . 064 | . 064 | . 065 |
| 1.5 | . 059 | . 060 | .060 | .06I | .06I | .062 | . 062 | .063 | . 063 | .064 |
| 2.0 | . 058 | . 059 | . 059 | . 060 | . 060 | .06I | .06I | .062 | .062 | . 063 |
| 2.5 | . 057 | . 058 | . 058 | . 059 | . 059 | . 059 | . 060 | .060 | .06I | .06I |
| 3.0 | +0.056 | +0.056 | +0.057 | +0.057 | +0.058 | +0.05S | +0.059 | +0.059 | +0.060 | +0.060 |
| $3 \cdot 5$ | . 055 | . 055 | . 056 | . 056 | . 057 | .057 | . 058 | . 058 | . 059 | . 059 |
| 4.0 | . 054 | . 054 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 | . 057 | . 058 |
| 4.5 | . 053 | . 053 | . 054 | . 054 | . 054 | .055 | . 055 | . 056 | . 056 | . 057 |
| 5.0 | .052 | . 052 | .052 | . 053 | .053 | . 054 | . 054 | . 055 | . 055 | . 056 |
| 5.5 | +0.05I | +0.05I | +0.05I | $+0.052$ | +0.052 | +0.053 | +0.053 | +0.053 | +0.054 | +0.054 |
| 6.0 | . 049 | . 050 | . 050 | . 051 | . 051 | . 052 | . 052 | . 052 | . 053 | . 053 |
| 6.5 | .048 | . 049 | . 049 | . 050 | . 050 | . 050 | .051 | . 051 | . 052 | . 052 |
| 7.0 | . 047 | . 048 | . 048 | . 048 | . 049 | . 049 | . 050 | . 050 | . 050 | . 05 I |
| 7.5 | .046 | . 047 | . 047 | .0 .47 | .048 | .048 | . 048 | . 049 | . 049 | . 050 |
| 8.0 | +0.045 | +0.045 | $+0.046$ | +0.0.46 | +0.047 | +0.047 | +0.047 | +0.048 | +0.048 | +0.048 |
| 8.5 | . 044 | . 044 | . 045 | . 045 | . 045 | . 046 | . 046 | . 047 | . 0.47 | . 047 |
| 9.0 | . 043 | . 043 | . 044 | . 044 | . 044 | .045 | . 045 | . 045 | . 046 | .046 |
| 9.5 | .042 | . 042 | . 042 | . 0.43 | . 043 | . 044 | . 044 | . 044 | . 0.45 | . 045 |
| 10.0 | .041 | .04I | .041 | . 0.42 | . 042 | . 042 | . 043 | . 043 | . 043 | . 044 |
| 10.5 | +0.040 | +0.040 | $+0.040$ | +0.041 | +0.04I | +0.04I | +0.042 | +0.0.42 | +.0.042 | +0.043 |
| I 1.0 | . 039 | . 039 | . 039 | . 039 | . 040 | . 040 | . 040 | .04I | . 041 | . 041 |
| II. 5 | . 037 | .038 | . 038 | .038 | . 039 | . 039 | . 039 | . 040 | . 040 | . 040 |
| 12.0 | . 036 | .037 | . 037 | .037 | . 038 | .038 | . 038 | . 038 | .039 | . 039 |
| 12.5 | .035 | .036 | .036 | .036 | . 036 | .037 | . 037 | . 037 | . 038 | .038 |
| 13.0 | +0.034 | +0.034 | $+0.035$ | +0.035 | +0.035 | $+0.036$ | +0.036 | $+0.036$ | $+0.036$ | +0.037 |
| I 3.5 | . 033 | . 033 | . 034 | . 034 | . 034 | .034 | . 035 | . 035 | . 035 | . 036 |
| 14.0 | . 032 | .O32 | . 032 | . 033 | . 033 | . 033 | . 034 | . 034 | . 034 | . 034 |
| 14.5 | .O3I | .O3I | . 031 | . 032 | . 032 | . 032 | . 032 | . 033 | . 033 | . 033 |
| I 5.0 | . 030 | .030 | .030 | .030 | .03I | .O3I | . O 3 I | . 031 | . 032 | . 032 |
| 15.5 | +0.029 | $+0.029$ | $+0.029$ | $+0.029$ | +0.030 | $+0.030$ | +0.030 | +0.030 | +0.03I | $+0.031$ |
| I6.0 | .028 | .028 | . 028 | .028 | . 028 | . 029 | . 029 | . 029 | . 029 | . 030 |
| 16.5 | . 026 | . 027 | . 027 | .027 | . 027 | . 028 | . 028 | . 028 | . 028 | . 023 |
| I7.0 | . 025 | . 026 | . 026 | .026 | . 026 | . 026 | . 027 | . 027 | . 027 | .027 |
| I7.5 | . 024 | . 024 | . 025 | .025 | . 025 | . 025 | . 026 | . 026 | . 026 | . 026 |
| 18.0 | +0.023 | +0.023 | +0.024 | +0.024 | +0.024 | +0.024 | +0.024 | +0.025 | +0.025 | $+0.025$ |
| 18.5 | . 022 | . 022 | . 022 | .023 | . 023 | . 023 | . 023 | . 023 | . 024 | . 024 |
| 19.0 | . O 2 I | . 021 | . 021 | . 022 | . 022 | . 022 | .022 | . 022 | . 022 | . 023 |
| 19.5 | . 020 | . 020 | . 020 | . 022 | . O 2 I | . 021 | . 021 | . 021 | . 02 I | . O 2 I |
| 20.0 | . 019 | . 019 | .OI9 | .OI9 | . OI9 | . 020 | . 020 | . O 20 | . 020 | . 020 |
| 20.5 | t-0.018 | +0.018 | +O.OIS | +0.018 | +0.018 | $+0.018$ | +0.019 | +0.019 | to.019 | +0.019 |
| 21.0 | .OI7 | . 017 | . O17 | . 017 | . OI7 | .OI7 | . O17 | . 18 | . 018 | . OIS |
| 2 I .5 | . 016 | .OI6 | . 016 | .016 | . 016 | .OI6 | . O16 | .OI6 | .O17 | .OI 7 |
| 22.0 | . 014 | .OIE | . 015 | . 015 | .OI5 | .OI5 | . 015 | . OI5 | .015 | . 016 |
| 22.5 | .OI3 | .OI3 | .OI4 | . 014 | .OI4 | .OI4 | . OI4 | . OI4 | .OI4 | . 014 |
| 23.0 | +0.012 | +0.012 | +0.012 | +0.013 | +0.013 | +0.013 | +0.013 | +0.013 | +0.013 | +0.013 |
| 23.5 | . OII | .OII | . OII | .OII | . OI 2 | . OI 2 | .OI2 | .OI2 | .OI2 | . OI2 |
| 24.0 | . 010 | . O1O | . 010 | . 010 | . 010 | . OII | . OII | .OII | .OII | .OII |
| 24.5 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . OC9 | . 010 | . 010 | . 010 |
| 25.0 | . 008 | . 008 | .008 | . 008 | . 008 | . 008 | . or 8 | . 008 | . 008 | . 009 |

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 24.0 | 24.2 | 24.4 | 24.6 | 24.8 | 25.0 | 25.2 | 25.4 | 25.6 | 25.8 |
| $\begin{gathered} \text { F. } \\ 25.5 \end{gathered}$ | Inch. +0.007 | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | Inch. +0.007 | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | Inch. +0.007 | Inch. $+0.007$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | Inch. $+0.007$ | Inch. | Inch. |
| 26.0 | +0.007 .006 | +0.007 .006 | +0.007 .006 | +0.007 .006 | +0.007 .006 | +0.007 .006 | +0.007 .006 | +0.007 .006 | 0.007 .006 | 0.007 .006 |
| 26.5 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 |
| 27.0 | . 004 | .004 | .004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 |
| 27.5 | . 002 | . 002 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 |
| 28.0 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.00I | +0.001 | +0.001 |
| 28.5 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.0 | 0.001 | 0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 |
| 29.5 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 |
| 30.0 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 |
| 30.5 | -0.004 | -0.004 | -0.004 | 0.004 | 0.004 | 0.004 | 0.004 | -0.004 | 0.004 | -0.004 |
| 31.0 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 006 | . 006 |
| 31.5 | . 006 | . 006 | . 006 | . 006 | . 006 | . 007 | . 007 | . 007 | . 007 | . 007 |
| 32.0 | . 007 | . 007 | . 007 | .008 | . 008 | . 008 | . 008 | . 008 | .008 | . 008 |
| 32.5 | . 008 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 |
| 33.0 | 0.010 | 0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 | -0.010 |
| 33.5 | . 111 | . OII | . 011 | . 011 | . 01 I | . 011 | . 011 | . OI 1 | . OI | . OI 1 |
| 34.0 | . 012 | . OL 2 | . 012 | . 012 | .OI2 | .OI2 | . 012 | . 012 | . 012 | . 013 |
| 34.5 | .013 | . 013 | . 013 | . 013 | . 013 | . 13 | . 013 | . 014 | . 014 | . 014 |
| 35.0 | . 014 | . 014 | . 014 | . 014 | .OI4 | . 014 | . 015 | . 015 | . O 5 | . 015 |
| 35.5 | -0.015 | -0.015 | -0.015 | -0.015 | -0.015 | -0.016 | -0.016 | -0.016 | -0.016 | -0.016 |
| 36.0 | . 016 | . 016 | . 016 | . 016 | . 017 | . 017 | . 017 | . 017 | . 017 | . 017 |
| 36.5 | . 017 | . 017 | . 017 | . 018 | . 018 | . 018 | . 018 | . 018 | . 018 | .or8 |
| 37.0 | . 018 | . OI 8 | . 019 | .O19 | . 019 | . 019 | .O19 | .019 | . 019 | .019 |
| 37.5 | . 019 | . 019 | . 020 | . 020 | . 020 | . 020 | . 020 | . 020 | . 02 I | . 021 |
| 38.0 | 0.020 | -0.021 | -0.02 J | -0.021 | -0.021 | -0.021 | -0.021 | -0.022 | -0.022 | -0.022 |
| 38.5 | I | . 022 | 22 | . 022 | . 022 | . 022 | . 023 | . 023 | . 023 | . 023 |
| 39.0 | . 023 | . 023 | . 023 | . 023 | . 023 | . 024 | . 024 | . 024 | . 024 | . 024 |
| 39.5 | . 024 | . 024 | . 024 | . 024 | . 024 | . 025 | . 025 | . 025 | . 025 | . 025 |
| 40.0 | . 025 | . 025 | . 025 | . 025 | . 026 | . 026 | . 026 | . 026 | . 026 | . 027 |
| 40.5 | -0.026 | -0.026 | -0.026 | -0.026 | -0.027 | -0.027 | -0.027 | -0.027 | -0.028 | -0.028 |
| 41.0 | . 027 | . 027 | . 027 | . 028 | . 028 | . 028 | . 028 | . 029 | . 029 | . 029 |
| 41.5 | . 028 | . 028 | . 028 | . 029 | . 029 | . 029 | . 029 | . 030 | . 030 | . 030 |
| 42.0 | . 029 | . 029 | . 030 | . 030 | . 030 | . 030 | .03I | . 031 | . 031 | . 031 |
| 42.5 | . 030 | . 030 | . 031 | . 031 | . 031 | .03I | . 032 | . 032 | . 032 | . 032 |
| 43.0 | -0.031 | -0.032 | -0.032 | -0.032 | -0.032 | -0.033 | -0.033 | -0.033 | -0.033 | -0.034 |
| 43.5 | . 032 | . 033 | . 033 | . 033 | . 033 | . 034 | . 034 | . 034 | . 035 | . 035 |
| 44.0 | . 033 | . 034 | . 034 | . 034 | . 035 | . 035 | . 035 | . 035 | . 036 | . 036 |
| 44.5 | . 035 | . 035 | . 035 | . 035 | . 036 | . 036 | . 036 | . 037 | . 037 | . 037 |
| 45.0 | . 036 | . 036 | . 036 | . 037 | . 037 | . 037 | . 037 | . 038 | .038 | . 038 |
| 45.5 | -0.037 | -0.037 | -0.037 | -0.038 | -0.038 | -0.038 | -0.039 | -0.039 | -0.039 | -0.039 |
| 46.0 | . 038 | . 038 | . 038 | . 039 | . 039 | . 039 | . 040 | . 040 | . 040 | . 041 |
| 46.5 | . 039 | . 039 | . 040 | . 040 | . 040 | .04I | . 041 | .041 | . 041 | . 042 |
| 47.0 | . 040 | . 040 | . 041 | .04I | .04I | . 042 | . 042 | . 042 | . 043 | . 043 |
| 47.5 | .04I | . 041 | . 042 | . 042 | . 042 | . 043 | . 043 | . 043 | . 044 | . 044 |
| 48.0 | -0.042 | -0.042 | -0.043 | -0.043 | -0.044 | -0.044 | -0.044 | -0.045 | -0.045 | -0.045 |
| 48.5 | . 043 | . 044 | . 044 | . 044 | . 045 | . 045 | . 045 | . 046 | . 046 | . 046 |
| 49.0 | . 044 | . 045 | . 045 | . 045 | . 046 | . 046 | . 047 | . 047 | . 047 | . 048 |
| 49.5 | . 045 | . 046 | . 046 | . 047 | . 047 | . 047 | . 048 | . 048 | . 048 | . 049 |
| 50.0 | . 046 | . 047 | . 047 | . 048 | . 048 | .048 | . 049 | . 049 | . 050 | . 050 |

Table 44.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Ther- | HEIGIIT OF THI: BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fahren- heit. | 24.0 | 24.2 | 24.4 | 24.6 | 24.8 | 25.0 | 25.2 | 25.4 | 25.6 | 25.8 |
| F. | Inch. | Inch. | Iuch. | Inch. | Inch. | Iuch. | Inch. | Inch. | Inch. | Inch. |
| 50.5 | -0.048 | -0.0.48 | -0.0.48 | -0.049 | -0.0.49 | -0.050 | -0.050 | -0.050 | -0.05I | 0.051 |
| 51.0 | . 049 | . 049 | . 049 | . 050 | . 050 | . 051 | . 05 I | . 051 | . 052 | . 052 |
| 51.5 | . 050 | . 050 | .05I | .051 | . 051 | . 052 | . 052 | . 053 | . 053 | . 053 |
| 52.0 | .051 | . 051 | . 052 | . 052 | . 053 | . 053 | . 053 | . 054 | . 054 | . 055 |
| 52.5 | .052 | . 052 | . 053 | . 053 | . 054 | . 054 | . 055 | . 055 | . 055 | . 056 |
| 53.0 | -0.053 | -0.053 | -0.054 | -0.054 | -0.055 | -0.055 | -0.056 | $-0.056$ | -0.057 | -0.057 |
| 53.5 | . 054 | . 055 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 | . 058 | . 058 |
| 54.0 | .055 | . 056 | .056 | .057 | .057 | . 057 | . 058 | .058 | . 059 | . 059 |
| 54.5 | . 056 | . 057 | . 057 | .058 | . 058 | . 059 | . 059 | . 060 | . 060 | . 060 |
| 55.0 | . 057 | . 058 | .058 | . 059 | . 059 | . 060 | . 060 | . 061 | .06I | . 062 |
| 55.5 | -0.05 ${ }^{\text {S }}$ | -0.059 | -0.059 | -0.060 | -0.060 | -0.061 | -0.061 | -0.062 | -0.062 | -0.063 |
| 56.0 | . 060 | . 060 | . 060 | . 061 | . 061 | . 062 | . 062 | . 063 | . 063 | . 064 |
| 56.5 | .06I | . 061 | . 062 | . 062 | . 063 | .063 | . 064 | . 064 | . 065 | . 065 |
| 57.0 | . 062 | . 062 | .063 | .063 | . 064 | . 064 | . 065 | . 065 | . 066 | . 066 |
| 57.5 | . 063 | . 063 | . 064 | . 06.4 | . 065 | . 065 | . 066 | . 066 | . 067 | .067 |
| 58.0 | -0.064 | -0.064 | -0.065 | -0.065 | -0.066 | -0.066 | -0.067 | -0.068 | -0.06S | -0.069 |
| 58.5 | . 065 | . 065 | . 066 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | .070 |
| 59.0 | . 066 | . 067 | . 067 | . 068 | .06S | .069 | . 069 | . 070 | . 070 | . 071 |
| 59.5 | .067 | . 068 | . 068 | . 069 | . 069 | . 070 | . 070 | . 071 | .072 | . 072 |
| 60.0 | .06S | . 069 | . 069 | . 070 | .070 | . 071 | . 072 | . 072 | . 073 | . 073 |
| 60.5 | -0.069 | -0.070 | -0.070 | -0.071 | -0.072 | -0.072 | -0.073 | -0.073 | -0.074 | -0.074 |
| 61.0 | . 070 | . 071 | .072 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 076 |
| 61.5 | . 071 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 076 | .076 | . 077 |
| 62.0 | . 073 | . 073 | .074 | .074 | . 075 | . 076 | . 076 | . 077 | . 077 | . 078 |
| 62.5 | . 074 | . 074 | . 075 | . 075 | . 076 | . 077 | . 077 | . 078 | . 078 | .079 |
| 63.0 | -0.075 | -0.075 | -0.076 | -0.077 | -0.077 | -0.078 | -0.078 | -0.079 | -0.080 | -0.080 |
| 63.5 | . 076 | . 076 | . 077 | . 078 | . 078 | . 079 | .oSo | . 080 | . OS I | .o8I |
| 64.0 | . 077 | . 077 | . 078 | . 079 | . 079 | . 080 | . oS I | . 08 I | . 082 | .082 |
| 64.5 | .078 | . 079 | . 079 | . 0 So | . 08.1 | . OSI | . OS 2 | .082 | .083 | .084 |
| 65.0 | . 079 | . 080 | .080 | . 081 | . 082 | .082 | .o83 | .08.4 | .084 | . 085 |
| 65.5 | -0.080 | -0.081 | -0.08I | -0.082 | -0.083 | -0.083 | -0.084 | -0.085 | -0.085 | -0.086 |
| 66.0 | . 08 I | .OS2 | . 083 | .o83 | .084 | . 085 | . 085 | . 080 | . 087 | .087 |
| 66.5 | .082 | .os3 | .084 | .084 | .o85 | .os6 | . 086 | . 087 | . 088 | .o8S |
| 67.0 | . 083 | .os4 | .o85 | . 085 | . 086 | . 087 | . 087 | . 088 | .089 | .090 |
| 67.5 | .08. 4 | .o85 | .086 | .087 | . 087 | . 088 | . 089 | .os9 | . 090 | . 091 |
| 68.0 | -0.085 | -0.086 | $-0.087$ | -0.088 | -0.088 | -0.089 | -0.090 | -0.090 | -0.091 | -0.092 |
| 68.5 | . 087 | .oS7 | . 088 | . 089 | . 089 | . 090 | . 091 | . 092 | . 092 | . 093 |
| 69.0 | . 088 | .os8 | .os9 | . 090 | . 091 | . 091 | . 092 | . 093 | . 093 | . 094 |
| 69.5 | .089 | .089 | . 090 | . 091 | . 092 | . 092 | . 093 | . 09.4 | . 095 | . 095 |
| 70.0 | . 090 | .091 | .09I | . 092 | . 093 | . 09.4 | . 094 | . 095 | . 096 | . 097 |
| 70.5 | -0.091 | -0.092 | -0.092 | $-0.093$ | -0.094 | -0.095 | -0.095 | -0.096 | -0.097 | -0.098 |
| 71.0 | . 092 | . 093 | . 09.4 | . 094 | . 095 | . 096 | . 097 | . 097 | .098 | . 099 |
| 71.5 | . 093 | . 094 | . 095 | . 095 | .096 | . 097 | . 098 | .098 | . 099 | . 100 |
| 72.0 | . 094 | . 095 | .096 | . 096 | .097 | . 098 | . 099 | . 100 | . ICo) | . IOI |
| 72.5 | . 095 | .096 | . 097 | . 098 | .09' | . 099 | . 100 | . 101 | . 102 | . 102 |
| 73.0 |  |  | -0.098 | -0.099 | -0. 100 | -0. 100 | -O. IOI | -0. 102 | --0. 103 | -0.104 |
| 73.5 | . 097 | .098 | . 099 | . 100 | . IOi | . IOI | . 102 | . 103 | .104 | . 105 |
| 74.0 | . 098 | . 099 | . 100 | . IOI | . 102 | . 103 | .103 | . 104 | . 105 | . 106 |
| 74.5 | . 100 | . 100 | . IOI | . 102 | . 103 | . 10.4 | . 105 | . 105 | . 106 | . 107 |
| 75.0 | . 101 | . 101 | . 102 | . 103 | . 104 | . 105 | . 106 | . 106 | . 107 | . 108 |

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Ther- | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FahrenFahre heit. | 24.0 | 24.2 | 24.4 | 24.6 | 24.8 | 25.0 | 25.2 | 25.4 | 25.6 | 25.8 |
| $\begin{array}{r} \text { F. } \\ 75^{\circ} .5 \end{array}$ | $\begin{gathered} \text { Inch. } \\ -\mathrm{O} .102 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ -\mathrm{O} .103 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ -\mathrm{O} . \mathrm{IO} 3 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ -\mathrm{O} . \mathrm{IO}_{4} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ -0.105 \end{gathered}$ | $\begin{gathered} \text { Iuch. } \\ -\mathrm{O} .106 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ -0.107 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ -\mathrm{O} . \mathrm{IoS} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ -\mathrm{O} .10 \mathrm{~S} \end{gathered}$ | Inch. <br> -0. 109 |
| 76.0 | . 103 | . 104 | . 104 | . 105 | . 106 | . 107 | . 108 | . 109 | . 110 | . 10 |
| 76.5 | . 104 | . 105 | . 106 | . 106 | .107 | . 108 | . 109 | . 1 Io | . 11 I | . 112 |
| 77.0 | . 105 | . 106 | . 107 | . 108 | . 108 | . 109 | . 110 | . II I | . 112 | . 113 |
| 77.5 | . 106 | . 107 | . IOS | . 109 | . 110 | . 110 | . III | . 112 | . 113 | . 114 |
| 78.0 | $-\mathrm{O} .107$ | -0. 108 | -0.109 | -0.110 | -O. 11 I | -0.112 | -0.112 | -0.113 | -0.114 | -O. 115 |
| 7 S .5 | . 108 | . 109 | . 110 | . 111 | . 12 | . 113 | . 114 | . II 4 | . 115 | . 116 |
| 79.0 | . 109 | . 110 | . 111 | . 112 | . 113 | . 114 | . 115 | . 116 | . 117 | . 117 |
| 79.5 | . 110 | III | . 112 | . 113 | . 114 | . II5 | . 116 | . 117 | . 118 | . 119 |
| 80.0 | . I I I | . 112 | .113 | . 114 | . 115 | . 116 | . 117 | . 118 | . 19 | . 120 |
| 80.5 | -0.112 | -0. 113 | -0.114 | -0.115 | -0.116 | -0.117 | -0.118 | -0.119 | -0.120 | -0.12I |
| 81.0 | . 114 | . 115 | . 115 | . 116 | . 117 | . 118 | . 119 | . 120 | . 12 I | . 122 |
| 8 I .5 | . 115 | . 116 | . 117 | . 118 | . 118 | . 19 | . 120 | . 121 | . 122 | . 123 |
| 82.0 | . 116 | . 117 | . 118 | . 119 | . 120 | . 12 I | . 122 | . 122 | . 123 | . 124 |
| 82.5 | . 117 | . 118 | -119 | . 120 | . 121 | . 122 | . 123 | . 124 | . 125 | . 126 |
| 83.0 | -O.IIS | -0. 119 | -O. 120 | -0.121 | -0.122 | -0.123 | -0. 124 | -0.125 | -0. 126 | -0.127 |
| S3.5 | . 119 | . 120 | . 121 | . 122 | . 123 | . 124 | . 125 | . 126 | . 127 | . 128 |
| 84.0 | . 120 | . 12 I | . 122 | . 123 | . 124 | . 125 | . 126 | . 127 | . 128 | - 129 |
| S.4.5 | . 121 | . 122 | . 123 | . 124 | . 125 | . 126 | . 127 | . 128 | . 129 | . 30 |
| 85.0 | . 122 | . 123 | . 124 | . 125 | . 126 | . 127 | 128 | . 129 | . 130 | . 131 |
| 85.5 | -0.123 | -O. I 24 | -O. 125 | -0.126 | -0. 127 | -0.128 | -0.129 | -O. 130 | -0.13I | -0.133 |
| S6.0 | . 124 | . 125 | . 126 | . 127 | . 128 | . 30 | . 31 | . 132 | . 133 | . 134 |
| S6.5 | . 125 | . 126 | . 128 | . 129 | . 130 | . 313 | . 132 | . 133 | - 134 | . 135 |
| 87.0 | . 126 | . 128 | . 129 | . 130 | . 131 | . 132 | . 133 | . 134 | . 135 | . 136 |
| S7.5 | . 128 | . 129 | . 130 | . 31 | . 32 | . 133 | . 34 | . 135 | . 136 | . 37 |
| 88.0 | -0.129 | -0.130 | -0.131 | -0.132 | -0. 133 | -0.134 | -0. 135 | -0. 136 | -0.137 | -0.138 |
| SS. 5 | . 130 | . 131 | . 132 | . 133 | . 134 | . 135 | . 36 | . 137 | . 138 | . 39 |
| 89.0 | .131 | . 132 | . 133 | . 134 | . 335 | . 136 | . 137 | . 138 | . 140 | . 141 |
| 89.5 | .132 | . 133 | . 134 | . 135 | . 136 | . 137 | .138 | . 140 | . 141 | . 142 |
| 90.0 | . 133 | . 134 | . 135 | . 136 | . 137 | . 138 | . 140 | . 141 | . 142 | . 143 |
| 90.5 | -0.134 | -O. I 35 | -0. 136 | -0. I37 | -01.39 | -0.140 | -0.141 | -0.142 | -0.143 | -0.144 |
| 91.0 | . 135 | . 136 | . 137 | . 138 | . 140 | . 141 | . 142 | .143 | . 144 | . 145 |
| 91.5 | . 136 | . 137 | . 138 | . 140 | . 141 | . 142 | . 143 | . 144 | . 145 | . 146 |
| 92.0 | . 137 | .138 | . 140 | . 141 | . 142 | . 143 | . 144 | . 145 | . 146 | . 148 |
| 92.5 | . 138 | . 139 | . 141 | . 142 | . 143 | . 144 | . 145 | . 146 | . 148 | . 149 |
| 93.0 | -O. 139 | -0.141 | -0.142 | -0.143 | -0.144 | -0.145 | -0.146 | -0.148 | -0. 149 | -0. 150 |
| 93.5 | . 140 | . 142 | . I43 | . 144 | . 145 | . 146 | . 148 | . 149 | . 150 | . 51 |
| 94.0 | . 142 | . 143 | . 144 | . 145 | . 146 | .147 | . 149 | . 150 | .151 | . 55 |
| 94.5 | . 143 | . 144 | . 145 | . 146 | . I 47 | . 149 | . 150 | .151 | . 152 | . 153 |
| 95.0 | . 144 | . 145 | . 146 | . 147 | . 149 | . 150 | . 151 | . 152 | . 153 | . 154 |
| 95.5 | -0.145 | -0.146 |  | -0.148 | -0.150 | -0.15 ${ }^{1}$ | -0. 152 | -0.153 | -0. 154 | -o. 156 |
| 96.0 | . 146 | . 147 | . 148 | . 550 | . 151 | . 152 | . 153 | . 154 | . 156 | . 157 |
| 96.5 | .147 | . 148 | . 149 | . 151 | - 152 | . 53 | -154 | . 156 | . 157 | . 158 |
| 97.0 | .148 | .149 | . 150 | . 152 | . 153 | . 154 | . 155 | . 157 | . 158 | 159 -160 |
| 97.5 | . 149 | .150 | . 152 | . 153 | . 154 | . 155 | . 157 | . 15 | . 159 | . 160 |
| 98.0 | -0.150 | -0.15 I | -0. 153 | -0.154 | -0.155 | -0.156 | -0.158 | -0.159 | -0.160 | $-\mathrm{O} .16 \mathrm{I}$ |
| 98.5 | . 515 | . 153 | . 154 | . 155 | . 156 | . 158 | - 159 | . 160 | . 161 | . 163 |
| 99.0 | . 152 | . 554 | . 155 | . 156 | . 157 | . 159 | . 160 | . 161 | . 162 | 164 .165 |
| 99.5 | . 553 | . 155 | . 156 | 157 .158 | 159 .160 | .160 .161 | .161 .162 | .162 .163 | .164 .165 | .165 .166 |
| 100.0 | . 154 | . 156 | . 157 | . 158 | . 160 | . 161 | . 162 | .163 | . 165 | . 166 |

Table 44.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Thermometer Fahrenheil. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 26.0 | 26.2 | 26.4 | 26.6 | 26.8 | 27.0 | 27.2 | 27.4 | 27.6 | 27.8 |
| $\begin{gathered} F . \\ 0.0 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ \text { +0.068 } \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.068 \end{gathered}$ | $\begin{gathered} \text { Iuch. } \\ +0.069 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +-0.069 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.070 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.070 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.07 \mathrm{I} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.07 \mathrm{I} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.072 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.072 \end{gathered}$ |
| +0.5 | +0.067 | +0.067 | +0.068 | +-0.068 | +0.069 | +0.069 | $+0.070$ | +0.070 | +0.071 | +0.071 |
| I. 0 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 070 |
| 1.5 | . 064 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 | . 069 |
| 2.0 | . 063 | . 064 | . 064 | . 065 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 |
| 2.5 | . 062 | . 062 | . 063 | . 063 | . 064 | . 064 | . 065 | . 065 | . 066 | . 066 |
| 3.0 | +0.061 | +0.06I | +0.062 | +0.062 | +0.063 | $+0.063$ | +0.063 | +0.064 | +0.064 | +0.065 |
| 3.5 | . 059 | . 060 | . 060 | .061 | .06I | . 062 | . 062 | . 063 | . 063 | . 064 |
| 4.0 | . 058 | . 059 | . 059 | . 060 | . 060 | .06I | .06I | .06I | . 062 | . 062 |
| 4.5 | . 057 | . 058 | . 058 | . 058 | . 059 | . 059 | . 060 | .060 | .06I | .06I |
| 5.0 | . 056 | . 056 | . 057 | . 057 | . 058 | . 058 | . 059 | . 059 | . 059 | . 060 |
| 5.5 | +0.055 | +0.055 | +0.056 | $+0.056$ | +0.056 | +0.057 | +0.057 | +0.058 | +0.058 | +0.059 |
| 6.0 | . 054 | . 054 | . 054 | . 055 | . 055 | .056 | . 056 | . 056 | . 057 | . 057 |
| 6.5 | .052 | . 053 | . 053 | . 054 | . 054 | . 054 | . 055 | . 055 | . 056 | . 056 |
| 7.0 | .05I | . 052 | . 052 | . 052 | . 053 | . 053 | . 054 | . 054 | . 054 | . 055 |
| 7.5 | . 050 | . 050 | . 051 | . 051 | .052 | . 052 | .052 | . 053 | . 053 | . 053 |
| 8.0 | +0.049 | +0.049 | $+0.050$ | +0.050 | +0.050 | +0.051 | +0.05I | +0.05I | +0.052 | +0.052 |
| 8.5 | . 048 | . 048 | . 048 | . 049 | . 049 | . 049 | . 050 | . 050 | . 05 I | . 051 |
| 9.0 | . 046 | . 047 | . 047 | . 048 | . 048 | . 048 | . 049 | . 049 | . 049 | . 050 |
| 9.5 | . 045 | . 046 | . 046 | . 046 | . 047 | . 047 | . 047 | . 048 | . 048 | . 048 |
| 10.0 | . 044 | . 044 | . 045 | . 045 | . 045 | . 0.46 | . 046 | . 046 | . 047 | . 047 |
| 10.5 | +0.043 | +0.043 | +0.044 | +0.044 | +0.044 | +0.0.45 | +0.045 | +0.045 | +0.046 | +0.046 |
| 11.0 | . 042 | . 042 | . 042 | . 043 | . 043 | . 043 | . 044 | . 0.44 | . 044 | . 045 |
| II. 5 | .04I | .04I | .041 | .041 | . 042 | . 042 | . 042 | . 043 | . 043 | . 043 |
| 12.0 | . 039 | . 040 | . 040 | . 040 | . 041 | . 041 | . 041 | .041 | . 042 | . 042 |
| 12.5 | .038 | .038 | . 039 | . 039 | . 039 | . 040 | . 040 | . 040 | . 040 | . 041 |
| 13.0 | +0.037 | +0.037 | +0.038 | +0.038 | +0.038 | +0.038 | +0.039 | +0.039 | +0.039 | +0.040 |
| 13.5 | .036 | . 036 | . 036 | . 037 | . 037 | . 037 | . 037 | . 038 | . 038 | . 038 |
| 14.0 | . 035 | . 035 | . 035 | . 035 | . 036 | . 036 | . 036 | . 036 | . 937 | . 037 |
| 14.5 | . 033 | . 034 | . 034 | . 034 | . 034 | . 035 | . 035 | . 035 | . 035 | . 036 |
| 15.0 | . 032 | . 032 | . 033 | . 033 | . 033 | . 033 | . 034 | . 034 | . 034 | . 034 |
| 15.5 | +0.031 | +0.031 | +0.032 | +0.032 | +0.032 | +0.032 | +0.032 | +0.033 | +0.033 | +0.033 |
| 16.0 | . 030 | .030 | . 030 | . 031 | .03I | .031 | . 031 | .031 | . 032 | . 032 |
| 16.5 | . 029 | . 029 | . 029 | . 029 | . 030 | . 030 | . 030 | . 030 | . 030 | . 031 |
| 17.0 | . 027 | . 028 | . 028 | . 028 | . 028 | . 029 | . 029 | . 029 | . 029 | . 029 |
| 17.5 | . 026 | . 027 | . 027 | . 027 | . 027 | . 027 | . 028 | . 028 | . 02 S | . 028 |
| 18.0 | +0.025 | +0.025 | $+0.026$ | +0.026 | $+0.026$ | +0.026 | $+0.026$ | +0.026 | +0.027 | $+0.027$ |
| 18.5 | . 024 | . 024 | . 024 | . 024 | . 025 | . 025 | . 025 | . 025 | . 025 | . 026 |
| 19.0 | . 023 | . 023 | . 023 | . 023 | . 023 | . 024 | . 024 | . 024 | . 024 | . 024 |
| 19.5 | . 022 | . 022 | . 022 | . 022 | . 022 | . 022 | . 023 | . 023 | . 023 | . 023 |
| 20.0 | . 020 | . 021 | . O 2 I | . 02 I | .021 | . 02 I | . 02 I | . 02 I | . 022 | . 022 |
| 20.5 | +u.019 | +0.019 | $+0.020$ | +0.020 | +0.020 | +0.020 | +0.020 | +0.020 | +0.020 | +0.02I |
| 21.0 | . OI 8 | . 018 | . OI 8 | . 018 | . 019 | . 019 | . 019 | . 019 | . 019 | . 019 |
| 21.5 | . 017 | . 017 | . 017 | . 017 | . 017 | . 017 | . 018 | . 018 | .ors | .or8 |
| 22.0 | . 016 | .016 | . 016 | . 016 | .or6 | . 016 | .oi6 | . 017 | . 017 | . 017 |
| 22.5 | . 014 | . 015 | . OI 5 | . 1215 | . 015 | . 015 | . 015 | . 015 | . OI 5 | . O 5 |
| 23.0 | +0.013 | +0.013 | +0.014 | +o.014 | +0.014 | +0.014 | +0.014 | +0.014 | +0.014 | +0.014 |
| 23.5 | . 012 | . 012 | . OL 2 | . Or 2 | . OL 2 | . 013 | . 013 | . 013 | . 013 | . O 3 |
| 24.0 | .OII | . 1.1 I | . OII | . OII | . OII | . OII | . OII | . OI 2 | . O 2 | . 12 |
| 24.5 | . 010 | . 010 | . OI | . 010 | .010 | . 010 | . OI | . OIO | . OIO | . 110 |
| 25.0 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 |

TAble 44.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 26.0 | 26.2 | 26.4 | 26.6 | 26.8 | 27.0 | 27.2 | 27.4 | 27.6 | 27.8 |
| $\begin{gathered} \text { F. } \\ 25^{\circ} .5 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.007 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.00 \mathrm{~S} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ + \text { o.00S } \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +\mathrm{o.00S} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.00 \mathrm{~S} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ \text { fo.00S } \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ + \text { o.00S } \end{gathered}$ |
| 26.0 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 007 | . 007 | . 007 |
| 26.5 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 |
| 27.0 | .004 | . 004 | .004 | . 004 | . 004 | . 004 | . 004 | .00.4 | . 004 | . 004 |
| 27.5 | .003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | .003 | . 003 | . 003 |
| 28.0 | +.0.001 | +0.001 | +0.002 | $+0.002$ | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 |
| 28.5 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 29.0 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 |
| 29.5 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 |
| 30.0 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 |
| 30.5 | 0.004 | -0.004 | -0.004 | -0 005 | -0.005 | -0.005 | -0.005 | 0.005 | -0.005 | 0.005 |
| 31.0 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 | . 006 |
| 31.5 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 |
| 32.0 | . 008 | . 008 | . 008 | . 008 | .008 | . 008 | . 008 | . 008 | . 008 | . 009 |
| 32.5 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 010 | . 010 | . OIO | . OIO |
| 33.0 | -0.010 | -0.010 | -0.010 | -0.011 | -0.011 | $\rightarrow 0.01$ I | -0.011 | -0.01 I | -0.011 | -0.01 1 |
| 33.5 | .OII | . 012 | . OI 2 | . 012 | . 012 | . 012 | . 012 | . 012 | . OI 2 | . 012 |
| 34.0 | .OI3 | . 013 | .OI3 | . 013 | .OI3 | .OI3 | . OI 3 | . Or 3 | . OI 3 | . OI 4 |
| 34.5 | . 014 | . 014 | . 014 | .OI4 | . 014 | . 014 | . 014 | .or 5 | .OI5 | . 015 |
| 35.0 | . 015 | . 015 | . OI 5 | . 015 | . 015 | . 016 | . 016 | . 016 | . 016 | . 016 |
| 35.5 | -0.016 | -0.016 | -0.016 | -0.017 | -0.017 | -0.017 | -0.017 | -0.017 | -0.017 | -0.017 |
| 36.0 | . 017 | . 018 | . 018 | . 018 | . 018 | . 018 | . 018 | . 018 | . 018 | . 019 |
| 36.5 | . 019 | . 019 | . 019 | . 19 | . 019 | . 019 | . 019 | . 020 | . 020 | . 020 |
| 37.0 | . 020 | . 020 | . 020 | . 020 | . 020 | . 02 I | . 021 | . O 2 I | . 021 | . 021 |
| 37.5 | . 02 I | . $\mathrm{O2I}$ | . $\mathrm{O2}$ I | . O 2 I | . 022 | . 022 | . 022 | . 022 | . 022 | . 022 |
| 38.0 | -0.022 | -0.022 | -0.022 | -0.023 | -0.023 | -0.023 | -0.023 | -0.023 | -0.023 | -0.024 |
| 38.5 | . 023 | . 023 | . 024 | . 024 | . 024 | . 024 | . 024 | . 025 | . 025 | . 025 |
| 39.0 | . 024 | . 025 | . 025 | . 025 | . 025 | . 025 | . 026 | . 026 | . 026 | . 026 |
| 39.5 | . 026 | . 026 | . 026 | . 026 | . 026 | . 027 | . 027 | . 027 | . 027 | . 027 |
| 40.0 | . 027 | .027 | . 027 | . 027 | . 028 | . 028 | . 028 | . 028 | . 028 | . 029 |
| 40.5 | 0.028 | -0.028 | -0.028 | -0.029 | -0.029 | -0.029 | -0.029 | -0.030 | -0.030 | -0.030 |
| 41.0 | . 029 | . 029 | . 030 | . 030 | . 030 | . 030 | . 031 | . 031 | . 031 | . 031 |
| 41.5 | . 030 | .03I | . 031 | . 031 | . 031 | . 032 | . 032 | . 032 | . 032 | . 032 |
| 42.0 | . 032 | . 032 | . 032 | .032 | . 033 | . 033 | . 033 | . 033 | . 033 | . 034 |
| 42.5 | . 033 | . 033 | . 033 | . 033 | . 034 | . 034 | . 034 | . 034 | . 035 | . 035 |
| 43.0 | -0.034 | -0.034 |  | -0.035 | -0.035 | -0.035 | -0.035 | -0.036 | -0.036 | -0.036 |
| 43.5 | . 035 | . 035 | .036 | . 036 | . 036 | . 036 | . 037 | . 037 | . 037 | . 037 |
| 44.0 | . 036 | . 037 | . 037 | . 037 | . 037 | . 038 | . 038 | . 038 | . 038 | . 039 |
| 44.5 | . 037 | . 038 | . 038 | . 038 | 039 | . 039 | . 039 | . 039 | . 040 | . 040 |
| 45.0 | . 039 | . 039 | . 039 | . 039 | . 040 | . 040 | . 040 | . 0.41 | . 041 | . 041 |
| 45.5 | -0,040 | -0.040 | -0.040 | -0.04I | -0.04I | -0.04I | -0.042 | -0.042 | -0.042 | -0.043 |
| 46.0 | . 041 | . 041 | . 042 | . 042 | . 042 | . 043 | . 043 | . 043 | . 043 | . 0.44 |
| 46.5 | . 042 | . 042 | . 043 | . 043 | . 043 | . 044 | . 044 | . 044 | . 045 | . 045 |
| 47.0 | . 043 | . 044 | . 044 | . 044 | . 045 | . 045 | . 045 | . 046 | . 046 | . 046 |
| 47.5 | . 045 | . 0.45 | . 045 | . 0.46 | . 046 | .046 | . 047 | . 047 | . 047 | . 048 |
| 48.0 | -0.046 | -0.046 | -0.046 | -0.047 | -0.047 | -0.047 | -0.048 | -0.048 | -0.048 | -0.049 |
| 48.5 | . 047 | . 047 | . 048 | . 048 | . 048 | . 049 | . 0.49 | . 049 | . 050 | . 050 |
| 49.0 | . 048 | . 048 | . 049 | . 049 | . 049 | . 050 | . 050 | . 051 | . 051 | .05I |
| 49.5 | . 049 | . 050 | . 050 | . 050 | .051 | . 051 | .05I | . 052 | . 052 | . 053 |
| 50.0 | . 050 | .05I | . 051 | . 052 | . 052 | . 052 | . 053 | . 053 | . 053 | . 054 |

Table 44.
REDUC'TION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached Ther- | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fahren ${ }^{\text {F }}$ heit. | 26.0 | 26.2 | 26.4 | 26.6 | 26.8 | 27.0 | 27.2 | 27.4 | 27.6 | 27.8 |
| F. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| 50.5 | -0.052 | -0.052 | -0.052 | -0.053 | -0.053 | -0.054 | -0.054 | -0.054 | -0.055 | -0.055 |
| 51.0 | . 053 | . 053 | . 054 | .054 | . 054 | . 055 | . 055 | . 056 | . 056 | . 056 |
| 51.5 | . 054 | . 054 | . 055 | . 055 | . 056 | . 056 | . 056 | . 057 | . 057 | . 058 |
| 52.0 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 | .05S | .058 | . 058 | . 059 |
| 52.5 | . 056 | . 057 | . 057 | .05S | .058 | . 058 | . 059 | . 059 | . 060 | . 060 |
| 53.0 | -0.057 | -0.058 | -0.058 | -0.059 | -0.059 | -0.060 | -0.060 | $-0.061$ | -0.061 | $-0.061$ |
| 53.5 | . 059 | . 059 | . 059 | .060 | . 060 | .06I | . 061 | . 062 | . 062 | . 063 |
| 54.0 | . 060 | . 060 | .06I | . 061 | . 062 | . 062 | . 063 | . 063 | . 063 | . 064 |
| 54.5 | . 061 | . 061 | . 062 | . 062 | . 063 | . 063 | .064 | . 064 | . 065 | . 065 |
| 55.0 | . 062 | . 063 | . 063 | . 064 | . 064 | . 064 | . 065 | . 065 | . 066 | . 066 |
| 55.5 | -0.063 | -0.064 | -0.064 | -0.065 | -0.065 | -0.066 | -0.066 | -0.067 | -0.067 | -0.068 |
| 56.0 | . 064 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 | . 069 |
| 56.5 | . 066 | . 066 | .067 | . 067 | .068 | . 068 | . 069 | .069 | . 070 | . 070 |
| 57.0 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 070 | . 070 | . 071 | .071 |
| 57.5 | . 068 | . 069 | . 069 | . 070 | .070 | . 071 | . 07 I | . 072 | . 072 | . 073 |
| 58.0 | -0.069 | -0.070 | -0.070 | -0.071 | -0.071 | -0.072 | -0.072 | -0.073 | -0.073 | -0.074 |
| 58.5 | . 070 | . 071 | . 071 | . 072 | . 072 | . 073 | .074 | . 074 | . 075 | . 075 |
| 59.0 | . 072 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 075 | .076 | .076 |
| 59.5 | . 073 | . 073 | . 074 | . 074 | . 075 | . 075 | .076 | .077 | . 077 | .078 |
| 60.0 | . 074 | . 074 | . 075 | . 076 | .076 | . 077 | . 077 | .078 | .078 | . 079 |
| 60.5 | -0.075 | -0.076 | -0.076 | -0.077 | -0.077 | $-0.078$ | -0.078 | -0.079 | -0.080 | -0.08o |
| 61.0 | . 076 | . 077 | .0.7 | . 078 | . 079 | .079 | .oSo | .OSo | .08I | .081 |
| 6 I .5 | . 077 | . 078 | . 079 | . 079 | . 0.50 | .080 | .oSI | .082 | .082 | .083 |
| 62.0 | . 079 | . 079 | .080 | .oSo | . 081 | .082 | .os2 | .083 | .083 | .o84 |
| 62.5 | .080 | .oso | .08I | .082 | .082 | . 083 | .083 | .084 | . 085 | . 085 |
| 63.0 | -0.081 | -0.082 | -0.082 | -0.083 | -0.083 | -0.084 | -0.085 | $-0.085$ | -0.086 | -0.086 |
| 63.5 | . 082 | . 083 | .083 | .os 4 | . 085 | . 085 | .os6 | . 086 | . 087 | . 088 |
| 64.0 | . 083 | . 084 | .085 | . 085 | .086 | .086 | .o87 | .088 | . 088 | .089 |
| 64.5 | .084 | .oS5 | .086 | . 086 | .087 | . 088 | . 088 | . 089 | .090 | . 090 |
| 65.0 | .086 | . 086 | . 087 | . 088 | . 088 | .089 | . 090 | . 090 | .09I | . 092 |
| 65.5 | -0.087 | -0.087 | 0.088 | -0.089 | -0.089 | -0.090 | -0.091 | -0.091 | -0.092 | -0.093 |
| 66.0 | . 088 | .089 | .089 | . 090 | .09I | .091 | . 092 | . 093 | . 093 | . 094 |
| 66.5 | .089 | . 090 | . 090 | .09I | . 092 | . 093 | . 093 | . 094 | . 095 | . 095 |
| 67.0 | .090 | . 091 | . 092 | . 092 | . 093 | .094 | .09.4 | . 095 | . 090 | . 097 |
| 67.5 | . 092 | . 092 | . 093 | . 094 | . 094 | .095 | . 096 | . 096 | . 097 | . 098 |
| 68.0 | -0.093 | -0.093 | -0.094 | -0.095 | -0.095 | $-0.096$ | -0.097 | -0.098 | -0.09 | -0.099 |
| 68.5 | . 094 | . 095 | . 095 | . 096 | . 097 | . 097 | .098 | . 099 | . 100 | . 100 |
| 69.0 | . 095 | .096 | . 096 | . 097 | .098 | . 099 | . 099 | . 100 | . 101 | . 102 |
| 69.5 | . 096 | . 097 | .098 | .098 | . 099 | . 100 | . 101 | . 101 | . 102 | . 103 |
| 70.0 | . 097 | . 098 | . 099 | . 100 | .100 | . 101 | . 102 | . 103 | . 103 | . 104 |
| 70.5 | -0.09S | -0.099 | -0.100 | -0.101 | -O.101 | -0.102 | -0.103 | -0.104 | -0.105 | -0.105 |
| 71.0 | . 100 | . 100 | . 101 | . 102 | . 103 | . 103 | . 104 | . 105 | . 106 | . 107 |
| 71.5 | . IOI | . 102 | . 102 | . 103 | . 104 | . 105 | . 105 | . 106 | . 107 | . 108 |
| 72.0 | . 102 | .103 | .104 | .104 | .105 | .106 | .107 | .107 | .108 | .109 |
| 72.5 | . 103 | . 104 | . 105 | . 106 | . 106 | .107 | . 108 | .109 | .109 | . 110 |
| 73.0 | -0.104 | -0.105 | -0.106 | -0.107 | -0.108 | -0.10S | -0.109 | -0.110 | -0.111 | -0.112 |
| 73.5 | . 105 | . 106 | . 107 | . 108 | . 109 | . 110 | . 110 | . 111 | . 112 | .113 |
| 74.0 | .107 | . 107 | .108 | .109 | . 110 | . III | . I12 | . 112 | . 113 | . II4 |
| 74.5 | . 108 | . 109 | .109 | . 110 | . II I | . 112 | .II3 | . 114 | 114 | . 115 |
| 75.0 | . 109 | . 110 | . 111 | . 112 | . 112 | . 113 | .II4 | . II5 | 116 | . 117 |

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Ther- | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fahren- heit. | 26.0 | 26.2 | 26.4 | 26.6 | 26.8 | 27.0 | 27.2 | 27.4 | 27.6 | 27.8 |
| F. | Inch. | Inch. | ach. | . | Inch. | Inc | nch. | nch. | Iuch. | Inch. |
| 75.5 | -0.110 | -O. III | -0.112 | -0.113 | -0.114 | -0.114 | -0.115 | -0.116 | -0.117 | -0.11S |
| 76.0 | . 111 | . 112 | . II3 | . 114 | . 115 | . 116 | . 116 | . 117 | . 118 | .119 |
| 76.5 | . II3 | . 113 | . 114 | . 115 | . 116 | . 117 | . 118 | . 119 | . 119 | . 120 |
| 77.0 | . 114 | . II | . 115 | . 116 | . 117 | . 118 | . 119 | . 120 | . 121 | . 122 |
| 77.5 | . 115 | . 116 | . 117 | . 117 | . IIS | . 119 | . 120 | . 121 | . 122 | . 123 |
| 78.0 | -O.116 | -0. 117 | -0.118 | -0.119 | -0.120 | -0.120 | -0.121 | -0.122 | -0.123 | -0. 124 |
| 78.5 | . 117 | . 118 | . 119 | . 120 | . 121 | . 122 | . 123 | . 123 | . 124 | . 125 |
| 79.0 | . IIS | . 119 | . 120 | . 121 | . 122 | .123 | . 124 | . 125 | . 126 | . 127 |
| 79.5 | . 120 | . 120 | . 121 | . 122 | . 123 | . 124 | . 125 | . 126 | . 127 | . 128 |
| 8.0 | . 12 I | . 122 | . 123 | . 123 | . 124 | . 125 | . 126 | . 127 | . 128 | . 129 |
| 80.5 | -0.122 | -0.123 | -0.124 | -0.125 | -0.126 | -0.127 | -0.127 | -0.128 | -0.129 | $\rightarrow 0.130$ |
| Si.o | . 123 | . 124 | . 125 | . 126 | . 127 | . 128 | . 129 | . 130 | . 131 | . 132 |
| 81.5 | . 124 | . 125 | . 126 | . 127 | . 128 | . 129 | . 130 | . 131 | . 32 | . 133 |
| S2.0 | . 125 | . 126 | . 127 | . 128 | . 129 | . 130 | . 131 | . 132 | . 133 | . 134 |
| 82.5 | . 127 | . 128 | . 12 S | . 129 | . 130 | . 13 I | . 132 | . 133 | . 134 | . 135 |
| 83.0 | -0.128 | -0.129 | -0.130 | -0.13I | -0.132 | -0.133 | -0.134 | -0.135 | -0. I36 | -0.137 |
| 83.5 | . 129 | . 130 | . 331 | . 132 | . 133 | . 134 | . 135 | . 136 | . 137 | . 138 |
| 84.0 | . 130 | .131 | . 132 | . 133 | - 134 | . 135 | . 136 | . 137 | . 138 | . 139 |
| 84.5 | . 13 I | . 132 | . 133 | . 134 | . 135 | . 136 | . 137 | .138 | . 139 | . 140 |
| S5.0 | . 132 | . 133 | . 134 | . 135 | . 136 | . 137 | . 138 | . 139 | . 141 | . 142 |
| 85.5 | -0.134 | -0. I35 | -0.136 | -0.137 | -0.13 3 | -0.139 | -0.140 | -0.141 | -0.142 | -0. 143 |
| 86.0 | . 135 | .136 | . 137 | . 138 | . 139 | . 140 | . 141 | . 142 | . 143 | . I44 |
| 86.5 | . 136 | . 137 | . 138 | . 139 | .140 | . 141 | . I42 | . 143 | . 144 | . 145 |
| 87.0 | . 137 | .13S | . 139 | . 140 | . 141 | . 142 | . 143 | . 144 | . 145 | . 147 |
| 87.5 | .138 | . 139 | . 140 | . 141 | . 142 | . 144 | . 145 | . 146 | . 147 | . 148 |
| 88.0 | -O.I39 | -0.140 | -0.142 | -0.143 | -0.144 | -0.145 | -0.146 | -0.147 | -0.14S | -0. 149 |
| 88.5 | . 141 | . 142 | . 143 | . 144 | . 145 | . 146 | . 147 | . 148 | . 149 | . 150 |
| 89.0 | . 142 | . 143 | . 144 | . 145 | . 146 | . 147 | . 148 | . 149 | . 150 | . 152 |
| S9.5 | .143 | . 144 | . 1.45 | . 146 | . 147 | . 148 | . 149 | . 151 | . 152 | . 153 |
| 90.0 | . 144 | . 145 | . 146 | . 147 | . 148 | . 150 | .151 | . 152 | . 153 | . 154 |
| 90.5 | -0.145 | -0.146 | -0. 147 | -0.149 | -0.150 | -0.151 | -0.152 | -0.153 | -0.154 | -0.155 |
| 91.0 | .146 | . 147 | . 149 | . 150 | . 151 | . 152 | . 153 | . 154 | -155 | . 157 |
| 91.5 | . 148 | . 149 | . 150 | . 151 | . 152 | . 153 | . 154 | . 155 | . 157 | . 158 |
| 92.0 | . 149 | . 150 | . 151 | . 152 | . 153 | . 154 | . 156 | . 157 | .158 | . 159 |
| 92.5 | . 150 | . 151 | . 152 | . 153 | . 154 | . 156 | . 157 | . 158 | - 159 | . 160 |
| 93.0 | -0.15I | -0.152 | -0.153 | -0.155 | -0.156 | -0.157 | -0.158 | -0.159 | -0.160 | -0.16I |
| 93.5 | . 152 | . 153 | . 155 | . 156 | . 157 | .15S | . 159 | . 160 | . 162 | .163 |
| 94.0 | . 153 | . 155 | . 156 | . 157 | . 158 | . 159 | . 160 | .162 | . 163 | . 164 |
| 94.5 | . 155 | . 156 | . 157 | . 158 | . 159 | . 160 | .162 | . 163 | . 164 | . 165 |
| 95.0 | . 156 | . 157 | . 158 | . 159 | . 160 | . 162 | . 163 | . 164 | . 165 | . 166 |
| 95.5 | -0.157 | -0.158 | -0.159 | -0.160 | -0.162 | $-0.163$ | -0.164 | -0.165 | -0.167 | -0.168 |
| 96.0 | . 158 | . 159 | . 160 | . 162 | .163 | . 164 | . 165 | . 167 | . 168 | . 169 |
| 96.5 | . 159 | . 160 | . 162 | .163 | .164 | .165 | . 167 | . 168 | . 169 | . 170 |
| 97.0 | .160 | . 162 | . 163 | . 164 | .165 | .167 | . 168 | . 169 | . 170 | . 171 |
| 97.5 | .162 | . 163 | . 164 | . 165 | . 166 | . 168 | . 169 | . 170 | . 171 | . 173 |
| 98.0 | -0.163 | -0.164 | -0.165 | -0.166 | -0.168 | -0.169 | -0.170 | -0.171 | -0.173 | -0.174 |
| 98.5 | . 164 | . 165 | . 166 | . 168 | .169 | . 170 | . 171 | . 173 | . 174 | . 175 |
| 99.0 | . 165 | . 166 | . 168 | . 169 | .170 | . 171 | . 173 | . 174 | . 175 | . 176 |
| 99.5 | . 166 | . 167 | . 169 | . 170 | .171 | . 173 | . 174 | . 175 | . 176 | . 178 |
| 100.0 | . 167 | . 169 | . 170 | . 171 | . 172 | . 174 | . 175 | . 176 | . 178 | . 179 |

## Table 44.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Ther- | HT OF THE BAROMETER IN |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fahren- heit. | 28.0 | 28.2 | 28.4 | 28.6 | 28.8 | 29.0 | 29.2 | 29.4 | 29.6 | 29.8 |
| $\begin{gathered} F . \\ 0.0 \end{gathered}$ | $\left\|\begin{array}{c} \text { 1uch. } \\ +0.073 \end{array}\right\|$ | $\begin{gathered} \text { Inch. } \\ +0.074 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.074 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.075 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.075 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.076 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.076 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +\mathrm{o} .077 \end{gathered}$ | $\begin{gathered} \text { lnch. } \\ +\mathrm{O} .077 \end{gathered}$ | $\begin{array}{r} \text { Inch. } \\ +0.078 \end{array}$ |
| +0.5 | +0.072 | +0.072 | +0.073 | +0.073 | +0.074 | +0.074 | +0.075 | +0.075 | $+0.076$ | +0.076 |
| 1.0 | . 070 | . 07 l | .071 | . 072 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 |
| r. 5 | . 069 | . 070 | . 070 | . 071 | . 07 I | .072 | .072 | . 073 | . 073 | . 074 |
| 2.0 | . 068 | . 068 | . 069 | . 069 | .070 | .070 | . 071 | . 071 | . 072 | . 072 |
| 2.5 | .067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 069 | . 070 | . 070 | . 071 |
| 3.0 | +0.065 | +0.066 | +0.066 | +0.067 | +0.067 | +0.068 | -0.068 | +0.069 | +0.069 | +0.070 |
| 3.5 | . 064 | . 065 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 |
| 4.0 | . 063 | . 063 | . 064 | .064 | . 065 | . 065 | . 065 | . 066 | . 066 | . 067 |
| 4.5 | . 062 | . 062 | . 062 | . 063 | . 063 | . 064 | .064 | . 065 | . 065 | . 065 |
| 5.0 | . 060 | . 061 | . 061 | . 062 | . 062 | . 062 | . 063 | . 063 | .064 | .064 |
| 5.5 | +0.059 | +0.059 | +0.060 | +0.060 | +0.061 | +0.06r | +0.062 | +0.062 | +0.062 | +0.063 |
| 6.0 | .05s | .05S | . 059 | . 059 | . 059 | . 060 | . 060 | . 061 | . 061 | .061 |
| 6.5 | . 056 | . 057 | . 057 | . 058 | . 058 | . 058 | . 059 | . 059 | . 060 | . 060 |
| 7.0 | . 055 | . 056 | .056 | .056 | .057 | . 057 | . 057 | .05S | . 058 | . 059 |
| 7.5 | . 054 | . 054 | . 055 | . 055 | . 055 | .056 | .056 | . 057 | . 057 | . 0.57 |
| 8.0 | +0.053 | +0.053 | +0.053 | +0.054 | +0.054 | +0.054 | +0.055 | +0.055 | +0.056 | +0.056 |
| 8.5 | . 051 | . 052 | . 052 | . 052 | . 053 | . 053 | . 053 | . 054 | . 054 | . 055 |
| 9.0 | . 050 | . 050 | . 051 | . 051 | .05I | . 052 | . 052 | . 053 | . 053 | . 053 |
| 9.5 | . 049 | . 049 | . 049 | . 050 | . 050 | . 050 | . 051 | .05 I | . 052 | . 052 |
| 10.0 | .047 | .048 | . 048 | . 0.48 | . 049 | . 049 | . 050 | . 050 | . 050 | . 051 |
| 10.5 | +0.046 | +0.047 | +0.047 | +0.047 | +0.048 | +0.0.48 | +0.048 | +0.049 | +0.049 | +0.049 |
| 11.0 | .045 | . 045 | . 046 | . 046 | .046 | . 047 | . 047 | . 047 | . 047 | .048 |
| I 1.5 | .04.4 | . 044 | . 044 | . 045 | . 045 | . 045 | .046 | . 046 | . 0.46 | .046 |
| 12.0 | .042 | . 0.43 | . 043 | . 043 | . 044 | . 044 | . 044 | . 044 | . 045 | . 045 |
| 12.5 | .0.41 | . 04 r | . 042 | . 0.42 | . 0.42 | . 043 | . 043 | . 043 | . 043 | . 044 |
| 13.0 | +0.0.40 | +0.040 | +0.040 | +0.041 | +0.041 | +0.041 | +0.042 | +0.042 | $+0.042$ | +0.042 |
| 13.5 | . 039 | . 039 | . 039 | . 039 | . 040 | . 040 | . 0.40 | . 040 | . 0.41 | . 041 |
| 14.0 | . 037 | . 038 | .038 | .038 | . 038 | . 039 | . 039 | .039 | . 039 | . 040 |
| 14.5 | . 036 | . 036 | . 037 | . 037 | . 037 | . 037 | . 038 | .038 | . 038 | .038 |
| 15.0 | . 035 | . 035 | . 035 | . 035 | . 036 | . 036 | . 036 | . 036 | . 037 | . 037 |
| 15.5 | +0.033 | +0.034 | +0.034 | +0.034 | +0.034 | +0.035 | +0.035 | +0.035 | +0.035 | $+0.036$ |
| 16.0 | .032 | . 032 | . 033 | . 033 | . 033 | . 033 | . 034 | . 034 | . 034 | . 034 |
| 16.5 | .031 | . 031 | . 031 | . 032 | . 032 | .032 | . 032 | . 032 | . 033 | . 033 |
| 17.0 | . 030 | . 030 | . 030 | . 030 | . 030 | .031 | . 031 | . 031 | .03I | .032 |
| 17.5 | . 028 | . 029 | . 029 | . 029 | . 029 | . 029 | . 030 | . 030 | . 030 | . 030 |
| 18.0 | +0.027 | +0.027 | +0.027 | +0.028 | +0.028 | +0.028 | +0.028 | +0.028 | +0.029 | +0.029 |
| 18.5 | . 026 | .026 | . 025 | . 026 | . 027 | . 027 | . 027 | . 027 | . 027 | . 027 |
| 19.0 | . 025 | . 025 | . 025 | . 025 | . 025 | . 025 | . 026 | . 026 | . 026 | . 026 |
| 19.5 | . 023 | . 023 | . 02.4 | . 024 | . 024 | .024 | . 024 | . 024 | . 025 | . 025 |
| 20.0 | . 022 | . 022 | . 022 | . 022 | . 023 | . 023 | . 023 | . 023 | . 023 | . 023 |
| 20.5 | +0.02 I | +0.02I | +0.02 I | +0.02I | +0.02I | +0.02I | +0.022 | +0.022 | +0.022 | +0.022 |
| 21.0 | .oi9 | . 020 | . 020 | . 020 | . 020 | . 020 | . 020 | . 020 | . 022 I | . 021 |
| 21.5 | . 018 | . 018 | . 018 | .OI9 | . 019 | . 019 | .or9 | . 019 | .or9 | .or9 |
| 22.0 | .017 | .017 | .017 | .017 | . 017 | .017 | . 018 | . 018 | .OIS | .ois |
| 22.5 | . 016 | .016 | .016 | .016 | . 016 | . 016 | .or6 | . 16 | . 016 | .or 7 |
| 23.0 | +0.014 | +0.014 | +0.015 | +0.015 | +0.015 | +0.015 | +0.015 | +0.015 | +0.015 | +0.015 |
| 23.5 | .OI3 | .013 | . 013 | .013 | .013 | .014 | . 014 | . 014 | . OI 4 | . 014 |
| 24.0 | .012 | .012 | .OI2 | . 012 | .012 | .012 | .012 | . 012 | . 012 | .or3 |
| 24.5 | . 011 | . 011 | . 011 | . 011 | . 011 | . 111 | . 011 | .OII | . 011 | . OI |
| 25.0 | . 009 | . 069 | . 009 | . 009 | .009 | . 010 | . 010 | . 010 | . 010 | . 010 |

Table 44.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. ENGLISH MEASURES.

| Attached Thermometer Fahren. heit. | d HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 28.0 | 28.2 | 28.4 | 28.6 | 28.8 | 29.0 | 29.2 | 29.4 | 29.6 | 29.8 |
| F. | Inch. | Inch. | Inch. | Inch. |  |  | Inch. | Inch. | Inch. |  |
| 25.5 | +o.00S | +0.008 | +0.008 | +0.008 | +o.00S | +0.008 | +0.008 | +0.008 | +0.008 | $\begin{aligned} & \text { luch. } \\ & +0.008 \end{aligned}$ |
| 26.0 | . 007 | . 007 | . 007 | . 007 | . 007 | - .007 | . 007 | . 007 | 1.008 <br> .007 | . .007 |
| 26.5 | . 005 | .005 | . 005 | . 006 | . 006 | 6 . 006 | . .006 | . 006 | - .006 | . 006 |
| 27.0 | .004 | .004 | . 004 | . 004 | . 004 | . 004 | 4 . 004 | . 00.4 | . 004 | . 004 |
| 27.5 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . .003 | . 003 | .003 | .003 |
| 28.0 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 |  |  |  |
| 28.5 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | +0.002 0.000 | +0.002 0.000 | $\begin{array}{r} +0.002 \\ 0.000 \end{array}$ |
| 29.0 | -0.001 | -0.001 | -0.001 | -0.001 | -0.00I | -0.001 | -0.001 | -0.000 | - $\begin{array}{r}0.000 \\ -0.001\end{array}$ | $\begin{array}{r} 0.000 \\ -0.001 \end{array}$ |
| 29.5 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | .002 | . 002 | . 0.002 |
| 30.0 | . 003 | .004 | . 004 | . 004 | . 004 | .004 | .004 | . 004 | .004 | .002 |
| 30.5 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 |  |  |  |  |
| 31.0 | . 006 | . 006 | . 006 | . 006 | .006 | . 006 | -0.005 | -0.005 | -0.005 .006 | $\begin{array}{r} -0.005 \\ .006 \end{array}$ |
| 31.5 | .007 | . 007 | . 007 | . 007 | . 008 | .008 | . 008 | . 008 | . 008 | .008 |
| 32.0 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 |
| 32.5 | .oio | .oio | . 010 | . OIO | . 010 | . 010 | . O O | . 10 | . 010 | .oro |
| 33.0 | -0.01 1 | -0.011 | -0.01 I | -O.OI I | -O.OI I | -0.012 | -0.012 | -0.012 | -0.012 | -0.012 |
| 33.5 | . 012 | . 012 | . 013 | . 013 | . 013 | .OI3 | .OI3 | . 013 | . 013 |  |
| 34.0 | .OI4 | .oI4 | . 014 | .OI4 | .oI4 | . 014 | .OI4 | .OI4 | .OI 4 | .OI5 |
| 34.5 | . 015 | . 015 | .or 5 | .or 5 | . 015 | . 015 | . 016 | .or 6 | .oi6 | . 016 |
| 35.0 | .oi6 | .oi6 | . 016 | .or 7 | . 017 | . 017 | . 017 | . 17 | . 017 | . 017 |
| 35.5 | -0.017 | -0.018 | -0.018 | -0.ois | -0.018 | -0.018 | -0.018 |  | -o.ors |  |
| 36.0 | . 179 | . 019 | . 019 | .OI 9 | . 019 | .019 | -0.018 | -0.018 | -0.018 | -0.019 .020 |
| 36.5 | . 020 | . O 2 O | . 020 | . 020 | . 02 I | . 02 I | . 02 I | . O 2 I | I | . 021 |
| 37.0 | . 02 I | . O 2 I | . 022 | . 022 | . 022 | . 022 | 22 | . 02 | . 022 | . 023 |
| 37.5 | . 023 | . 023 | . 023 | .023 | . 023 | . 023 | . 024 | . 024 | . 024 | . 024 |
| 38.0 | -0.024 | -0.02. 4 | -0.024 | -0.024 | -0.024 | -0.025 | -0.025 |  |  |  |
| 38.5 | . 025 | . 025 | . 025 | . 026 | . 026 | . 026 | -0.025 | -0.025 | -0.025 | -0.025 |
| 39.0 | .026 | . 027 | . 027 | . 027 | . 027 | . 027 | . 027 | . 028 | .028 | . 028 |
| 39.5 | . 028 | . 028 | . 028 | . 028 | . 028 | . 029 | . 029 | . 029 | .029 | . 029 |
| 40.0 | . 029 | . 029 | . 029 | . 030 | . 030 | . 030 | . 030 | .030 | .03I | . 03 I |
| 40.5 | -0.030 | -0.030 | -0.031 | -0.03I | -0.03 I | -0.031 | -0.03I | -0.032 | -0.032 | -0.032 |
| 41.0 | . O I | . 032 | . 032 | . 032 | .032 | . 033 | -. 033 | . 033 | .033 | . 033 |
| 41.5 | . 033 | . 033 | . 033 | . 033 | . 034 | . 034 | .034 | .034 | . 035 | . 035 |
| 42.0 | . 034 | . 034 | .034 | . 035 | . 035 | . 035 | . 035 | .036 | .036 | .036 |
| 42.5 | . 035 | . 035 | . 036 | .036 | . 036 | . 036 | . 037 | . 037 | . 037 | . 037 |
| 43.0 | -0.036 | -0.037 |  | -0.037 | $-0.038$ | -0.038 | -0.038 |  |  |  |
| 43.5 | . 038 | . 038 | .03 ${ }^{\text {S }}$ | . 039 | . 039 | . 039 | .039 | -0.038 | $\begin{array}{r} -0.039 \\ .040 \end{array}$ | -0.039 .040 |
| 44.0 | . 039 | . 039 | . 040 | . 0.40 | . 040 | . 040 | . 041 | . 041 | . 041 | . 042 |
| 44.5 | . 040 | .041 | . 041 | .041 | . 041 | . 042 | . 042 | . 042 | . 043 | . 043 |
| 45.0 | . 042 | . 042 | . 042 | . 0.42 | . 043 | . 043 | . 043 | . 0.44 | . 044 | . 044 |
| 45.5 | -0.043 | -0.043 | -0.043 | -0.044 |  |  |  | -0.045 | -0.045 | -0.046 |
| 46.0 | . 044 | . 044 | . 045 | . 045 | . 045 | . 046 | . 046 | . 046 | -0.047 | -0.046 |
| 46.5 | . 045 | .046 | . 046 | . 046 | . 047 | . 047 | . 047 | . 048 | . 0.48 | . 048 |
| 47.0 | .047 | . 047 | . 047 | . 048 | .048 | . 048 | . 049 | . 049 | . 049 | .050 |
| 47.5 | .048 | . 048 | . 049 | . 049 | . 0.49 | . 050 | . 050 | . 050 | . 05 I | . 051 |
| 48.0 | -0.049 | -0.050 - | -0.050 | -0.050 | -0.05 I | -0.05I - | -0.05I | -0.052 | -0.052 | -0.052 |
| 48.5 | . 050 | . 051 | . 051 | . 052 | . 052 | .052 | . 053 | . 053 | . 053 | . 054 |
| 49.0 | . 052 | . 052 | . 052 | . 053 | . 053 | . 054 | . 054 | . 054 | . 055 | . 055 |
| 49.5 | . 053 | . 053 | . 054 | . 054 | . 054 | . 055 | . 055 | . 056 | . 056 | .056 |
| 50.0 | . 054 | . 055 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 | . 057 | . 058 |

Table 44.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 28.0 | 28.2 | 28.4 | 28.6 | 28.8 | 29.0 | 29.2 | 29.4 | 29.6 | 29.8 |
| F. 50.5 | Inch. o.055 | Inch. $-0.056$ | Inch. | Inch. | Inch. | Inch. | $\begin{gathered} \text { Inch. } \\ -0.058 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ -0.05 S \end{gathered}$ | Inch. $-0.059$ | Inch. |
| 51.0 | . 057 | . 057 | . 058 | . 058 | . 058 | . 059 | . 059 | .060 | . 060 | . 060 |
| 51.5 | . 058 | . 058 | . 059 | . 059 | . 060 | . 060 | . 061 | .06I | .06I | .062 |
| 52.0 | . 059 | . 060 | . 060 | .06I | .06I | .06I | . 062 | . 062 | .063 | . 063 |
| 52.5 | .06I | .06I | .06I | . 062 | . 062 | . 063 | . 063 | . 064 | . 064 | . 064 |
| 53.0 | 0.062 | -0.062 | -0.063 | -0.063 | -0.064 | -0.064 | -0.064 | $-0.065$ | -0.065 | -0.066 |
| 53.5 | . 063 | . 064 | . 064 | . 064 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 |
| 54.0 | . 064 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 | . 068 |
| 54.5 | . 066 | . 066 | . 067 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 070 |
| 55.0 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 070 | . 070 | .07I | . 071 |
| 55.5 | -0.068 | -0.069 | -0.069 | -0.070 | -0.070 | -0.071 | -0.071 | -0.072 | -0.072 | -0.073 |
| 56.0 | . 069 | . 070 | . 070 | . 071 | . 071 | . 072 | . 072 | . 073 | . 073 | . 074 |
| 56.5 | .071 | .071 | . 072 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 075 |
| 57.0 | . 072 | . 072 | . 073 | . 073 | . 074 | . 075 | . 075 | . 076 | . 076 | . 077 |
| 57.5 | . 073 | . 074 | . 074 | . 075 | . 075 | . 076 | . 076 | . 077 | . 077 | . 078 |
| 58.0 | -0.074 | -0.075 | -0.076 | -0.076 | -0.077 | -0.077 | -0.078 | -0.078 | -0.079 | -0.079 |
| 58.5 | . 076 | . 076 | . 077 | . 077 | . 078 | . 078 | . 079 | .08o | .080 | .c8I |
| 59.0 | . 077 | .078 | . 078 | . 079 | . 079 | .080 | .080 | .081 | .081 | . 082 |
| 59.5 | .078 | . 079 | . 079 | . 080 | .08I | .081 | .082 | . 082 | .083 | . 083 |
| 60.0 | .0So | .08o | .08I | .08I | . 082 | . 082 | . 083 | . 084 | .084 | . 085 |
| 60.5 | -0.08I | -0.08I | -0.082 | -0.083 | -0.083 | -0.084 | -0.084 | -0.085 | -0.085 | -0.086 |
| 61.0 | . 082 | . 088 | . 083 | . 084 | . 084 | . 085 | . 086 | . 086 | . 087 | . 087 |
| 61. 5 | .o83 | .oS4 | . 085 | .085 | . 086 | .086 | . 087 | . 087 | . 088 | . 089 |
| 62.0 | .o85 | .oS5 | .086 | .086 | . 087 | . 088 | . 088 | .089 | .089 | . 090 |
| 62.5 | .086 | . 086 | .087 | . 088 | . 088 | .089 | . 090 | . 090 | .091 | .091 |
| 63.0 | -0.087 | -0.08S | -0.088 | -0.089 | -0.090 | -0.090 | -0.091 | -0.091 | -0.092 | -0.093 |
| 63.5 | .088 | .oS9 | . 090 | . 090 | .09I | . 092 | . 092 | . 093 | . 093 | . 094 |
| 64.0 | . 090 | .090 | . 091 | . 092 | . 092 | . 093 | . 093 | . 094 | . 095 | . 095 |
| 64.5 | . 091 | . 092 | . 092 | . 093 | . 093 | . 094 | . 095 | . 095 | . 096 | . 097 |
| 65.0 | . 092 | . 093 | . 093 | . 094 | . 095 | . 095 | . 096 | . 097 | . 097 | . 098 |
| 65.5 | 0.093 | -0.094 | -0.095 | -0.095 | -0.096 | -0.097 | -0.097 | -0.098 | -0.099 | -0.099 |
| 66.0 | . 095 | . 095 | . 096 | . 097 | . 097 | . 098 | . 099 | . 099 | .100 | . 101 |
| 66.5 | . 096 | . 097 | . 097 | .098 | . 099 | . 099 | . 100 | . 101 | . 101 | . 102 |
| 67.0 | . 097 | . 098 | . 099 | . 099 | . 100 | . 101 | . 101 | . 102 | .103 | . 103 |
| 67.5 | . 098 | . 099 | . 100 | . 101 | . IOI | . 102 | . 103 | . 103 | . 104 | .105 |
| 68.0 | -0.100 | -0.100 | -0.101 | -0.102 | -0.103 | -0.103 | -0.104 | -0.105 | -0.105 | -0.106 |
| 68.5 | . IOI | . 102 | . 102 | . 103 | . 104 | .105 | . 105 | . 106 | . 107 | . 107 |
| 69.0 | . 102 | .103 | . 104 | . 104 | .105 | . 106 | . 107 | .107 | . 108 | . 109 |
| 69.5 | . 104 | . 104 | . 105 | . 106 | . 106 | . 107 | . 108 | . 109 | . 109 | . 110 |
| 70.0 | . 105 | . 106 | . 106 | . 107 | . 108 | . 109 | . 109 | . 110 | . III | . 112 |
| 70.5 | -0.106 | -0.107 | -0.108 | -0.108 | -0.109 | -O. 110 | -O.III | -0.111 | -0.112 | -0.113 |
| 71.0 | . 107 | . 108 | . 109 | . 110 | . 110 | . III | . 112 | . 113 | .II3 | .II4 |
| 71.5 | .109 | . 109 | . 110 | . III | . 112 | . 112 | . 113 | .114 | .II5 | .116 |
| 72.0 | . 110 | . 111 | . 111 | . 112 | . 113 | .114 | . 115 | . 115 | .II6 | .II7 |
| 72.5 | . 111 | . 112 | . 13 3 | . II3 | . 114 | . 115 | . 116 | . 117 | . 117 | . 118 |
| 73.0 | -0.112 | -0.113 | -0. I I4 | -0. II 5 | -0. 116 | -0.116 | -0.117 | -0.118 | -0.119 | -0.120 |
| 73.5 | . 114 | . 114 | . 115 | . 116 | . 117 | . 118 | . 118 | . 119 | . 120 | . 121 |
| 74.0 | . 115 | . 116 | . 117 | . 117 | . 118 | .119 | . 120 | . 121 | . 121 | . 122 |
| 74.5 | . 116 | . 117 | . 118 | . 119 | . 119 | . 120 | . 121 | . 122 | . 123 | . 124 |
| 75.0 | . 117 | . I 18 | . 119 | . 120 | .121 | . 122 | . 122 | .123 | . 124 | . 125 |

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Ther- | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fahren- | 28.0 | 28.2 | 28.4 | 286 | 288 | 29.0 | 29.2 | 29.4 | 29.6 | 29.8 |
| F. 75.5 | Inch. <br> O. II9 | $\begin{gathered} \text { Inch. } \\ -0.119 \end{gathered}$ | $\begin{aligned} & \text { Inch. } \\ & -\mathrm{O} .120 \end{aligned}$ | $\begin{gathered} \text { Inch. } \\ - \text { O. I } 2 \text { I } \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ -0.122 \end{gathered}$ | Inch. | Inch. | Iuch. <br> -0. 125 | Inch. <br> O. 125 | Iuch. -0. 126 |
| 76.0 | . 120 | . 121 | 22 | . 122 | . 123 | . 124 | . 125 | . 126 |  | I28 |
| 76.5 | . 121 | . 122 | . 123 | . 124 | . 125 | . 125 | . 126 | . 127 | 128 | 129 |
| 77.0 | . 122 | . 123 | . 124 | . 125 | . 126 | . 127 | . 128 | . 129 | . 129 | . 130 |
| 77.5 | . 124 | . 125 | . 125 | . 126 | . 127 | . 128 | . 129 | . 130 | . 31 | . 132 |
| 78.0 | -0.125 | -0.126 | -0. 127 | -0.128 | -0.129 | -0.129 | -0.130 | -0.131 | -0.132 | -0.133 |
| 78.5 | . 126 | . 127 | . 128 | . 129 | . 130 | . 13 I | . 132 | . 133 | . 133 | . 134 |
| 79.0 | . 127 | . 128 | . 129 | . 130 | I3I | .132 | . 133 | . 134 | . 135 | . 136 |
| 79.5 | . 129 | . 130 | . 131 | . 311 | . 132 | . 133 | . 134 | . 135 | . 136 | .137 |
| So.o | . 130 | . 31 | . 132 | . 133 | . 134 | . 135 | . 136 | . 136 | . 137 | .138 |
| 80.5 | -0.131 | -0.132 | -0.133 | -0.134 | -0.135 | -0.136 | -0.137 | -0.138 | -0.139 | -0.140 |
| SI. 0 | .132 | . 133 | . 134 | . 135 | . 136 | . 137 | . 138 | . 139 | . 140 | . 141 |
| 81. 5 | . 134 | . 135 | .136 | . 137 | .I38 | . 139 | . 139 | . 140 | . 141 | . 142 |
| 82.0 | . I35 | . 136 | .137 | . 138 | . I39 | .140 | . 141 | . 142 | . 143 | . 144 |
| 82.5 | . 136 | . 137 | . 138 | . 139 | . 140 | . 141 | . 142 | . 143 | . 144 | . 145 |
| 83.0 | -0.138 | -0. I39 | -0.139 | -0.140 | -0.141 | -0.142 | -0.143 | -0.144 | -0.145 | -0.146 |
| 83.5 | . 139 | . 140 | .141 | . 142 | . I43 | . 144 | . 145 | .I46 | . 147 | . 148 |
| 84.0 | . 140 | . 141 | . 142 | . 143 | . 144 | . 145 | . 146 | . 147 | . 148 | . 149 |
| 84.5 | . 141 | . 142 | . 143 | . 144 | . 145 | . 146 | .147 | . 148 | . 149 | . 150 |
| 85.0 | . 143 | . 144 | . 145 | . 146 | . 147 | . 148 | . 149 | . 150 | . 151 | . 52 |
| 85.5 | -0.144 | -0. 145 | -0.146 | -0.147 | -0.148 | -0.149 | -0.150 | -0.151 | -0.152 | -0. 153 |
| S6.0 | . 145 | . 146 | . 147 | . 148 | . 149 | . 150 | . 151 | . 152 | . 153 | . 154 |
| 86.5 | . 146 | . 147 | .148 | . 149 | . 151 | . 152 | . 153 | . 154 | . 155 | . 156 |
| 87.0 | . 148 | . 149 | . 150 | . 151 | . 152 | . 153 | . 54 | . 155 | . 156 | . 157 |
| 87.5 | . 149 | . 150 | . 151 | . 152 | . 153 | . 154 | . 155 | . 156 | . 157 | . 155 |
| 88.0 | -0.150 | -0.151 | -0.152 | -0.153 | -0. 154 | -0.155 | -0.157 | -0.158 | -0.159 | $\rightarrow 0.160$ |
| 83.5 | . 515 | . 152 | . 154 | . 155 | .156 | . 157 | .158 | . 159 | . 160 | . 161 |
| 89.0 | . 153 | . 154 | . 155 | . 156 | . 157 | .158 | . 159 | . 160 | . 161 | . 162 |
| 89.5 | . 154 | . 155 | . 156 | . 157 | . 158 | . 159 | .160 | . 162 | .163 | . 164 |
| 90.0 | . 155 | . 156 | . 157 | . 158 | . 160 | .16I | . 162 | .163 | .164 | . 165 |
| 90.5 | -0.156 | -0.157 | -0.159 | -0.160 | -0.16I | -0.162 | $-0.163$ | -0.164 | -0.165 | -0.166 |
| 91.0 | . 158 | . 159 | . 160 | .161 | . 162 | . 163 | . 164 | . 166 | . 167 | . 168 |
| 91.5 | . 159 | . 160 | . 161 | . 162 | . 163 | . 165 | .166 | . 167 | . 168 | . 169 |
| 92.0 | . 160 | .161 | . 162 | . 164 | . 165 | . 166 | . 167 | . 168 | . 169 | . 170 |
| 92.5 | .16I | .163 | . 164 | . 165 | . 166 | .167 | . 168 | . 169 | . 171 | . 172 |
| 93.0 | -0.163 | -0. 164 | -0.165 | -0.166 | -0.167 | -0.168 | -0.170 | -0.171 | -0.172 | -0.173 |
| 93.5 | .164 | . 165 | . 166 | .167 | . 169 | . 170 | .171 | . 172 | . 173 | . 174 |
| 94.0 | .165 | . 166 | . 165 | . 169 | . 170 | . 171 | . 172 | . 173 | . 175 | . 176 |
| 94.5 | .166 | . 168 | . 169 | . 170 | .171 | . 172 | . 174 | . 175 | . 176 | . 177 |
| 95.0 | . 168 | .169 | . 170 | . 171 | . 172 | . 174 | . 175 | . 176 | . 177 | .178 |
| 95.5 | -0.169 | -0.170 | -0.171 | -0.173 | -0.174 | -0.175 | -0.176 | -0.177 | -0.179 | -0.180 |
| 96.0 | . 170 | . 171 | . 173 | . 174 | . 175 | . 176 | . 177 | . 179 | . 180 | . ISI |
| 96.5 | . 171 | .173 | . 174 | . 175 | . 176 | . 178 | -179 | .180 | . 18 I | . I 82 |
| 97.0 | .173 | . 174 | . 175 | .176 | . 178 | . 179 | . ISo | . 181 | .183 | . 184 |
| 97.5 | -174 | . 175 | . 176 | . 178 | . 179 | . ISo | . $\mathrm{S}_{1}$ | . 183 | . 184 | . 185 |
| 98.0 | -0.175 | -0.176 | -0.178 | -0.179 | -0.180 | -0.18I | -0.183 | -0.184 | -0.185 | -0.186 |
| 98.5 | .176 | . 178 | . 179 | . 180 | . 181 | . 183 | . IS 4 | . 185 | . 187 | . 188 |
| 99.0 | . 178 | . 179 | .180 | . 182 | . 183 | .IS4 | .185 | . 187 | . 188 | . 189 |
| 99.5 | .179 | . 180 | . 182 | . 183 | .184 | . 185 | .187 | . 188 | . 189 | . 190 |
| 100.0 | .180 | . 182 | . 183 | . 184 | . 185 | .187 | . 188 | . 159 | .191 | . 192 |

Table 44.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE ENGLISH MEASURES.

| Attached Thermometer Fahrenheit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 29.8 | 30.0 | 30.2 | 30.4 | 30.6 | 30.8 | 31.0 | 31.2 | 31.4 | 31.6 |
| $\begin{gathered} \text { F. } \\ 0.0 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.0-5 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.078 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.079 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.079 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ \text { +o.oSo } \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +\mathrm{o} .08 \mathrm{ol} \end{gathered}$ | $\left\lvert\, \begin{gathered} \text { Inch. } \\ +0.08 \mathrm{I} \end{gathered}\right.$ | $\begin{gathered} \text { Inch. } \\ +\mathrm{o.0SI} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.0 S 2 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.082 \end{gathered}$ |
| 0.5 | +0.076 | $+0.077$ | +0.077 | +0.078 | +0.078 | +0.079 | +0.079 | +0.0So | +0.08o | +0.081 |
| 1.0 | . 075 | . 076 | . 076 | . 077 | . 077 | . 078 | . 078 | . 079 | .079 | .oSo |
| 1.5 | . 074 | . 074 | . 075 | . 075 | .076 | . 076 | . 077 | . 077 | .078 | .07S |
| 2.0 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 075 | . 076 | .076 | . 077 |
| 2.5 | .071 | . 07 I | . 072 | . 072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 075 |
| 3.0 | +0.070 | +0.070 | +0.070 | +0.071 | +0.071 | +0.072 | +0.072 | +0.073 | +0.073 | +0.074 |
| 3.5 | . 068 | . 069 | . 069 | . 070 | .070 | . 070 | . 07 I | . 07 I | . 072 | . 072 |
| 4.0 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 070 | . 070 | . 070 | .071 |
| 4.5 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 | . 069 | . 069 | . 069 |
| 5.0 | . 064 | . 065 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 | . 068 | . 068 |
| 5.5 | +0.063 | +0.063 | +0.064 | +0.064 | +0.064 | +0.065 | +0.065 | +0.066 | +0.066 | +0.067 |
| 6.0 | .06I | . 062 | . 062 | .063 | . 063 | . 063 | . 064 | . 064 | . 065 | . 065 |
| 6.5 | . 060 | . 060 | . 061 | .06I | . 062 | . 062 | . 062 | . 063 | .063 | . 064 |
| 7.0 | . 059 | . 059 | . 059 | . 060 | . 060 | .06I | .06I | .06I | . 062 | . 062 |
| 7.5 | . 057 | . 058 | . 058 | .058 | .059 | . 059 | . 060 | . 060 | . 060 | . 061 |
| 8.0 | +0.056 | +0.056 | +0.057 | $+0.057$ | $+0.057$ | +0.058 | +0.058 | +0.059 | +0.059 | +0.059 |
| 8.5 | . 055 | . 055 | . 055 | . 056 | . 056 | . 056 | . 057 | . 057 | . 058 | . 058 |
| 9.0 | . 053 | . 054 | . 054 | . 054 | . 055 | . 055 | . 055 | . 056 | .056 | . 056 |
| 9.5 | .052 | . 052 | . 053 | . 053 | . 053 | . 054 | . 054 | . 054 | . 055 | . 055 |
| 10.0 | . 051 | . 051 | .05I | .052 | . 052 | .052 | . 053 | . 053 | . 053 | . 054 |
| 10.5 | +0.049 | +0.049 | +0.050 | +0.050 | +0.050 | +0.051 | +0.051 | +0.051 | +0.052 | $+0.052$ |
| II. 0 | . 048 | . 048 | . 048 | . 049 | . 049 | . 049 | . 050 | . 050 | . 050 | . 051 |
| II. 5 | . 046 | . 047 | . 047 | . 047 | . 048 | . 048 | .048 | . 049 | . 049 | . 049 |
| 12.0 | . 045 | . 045 | . 046 | . 046 | . 046 | . 047 | . 047 | . 047 | .048 | . 048 |
| 12.5 | . 044 | . 044 | . 044 | . 045 | . 045 | . 045 | . 045 | . 046 | .046 | .046 |
| 13.0 | +0.042 | +0.043 | $\div 0.043$ | +0.043 | +0.0.44 | +0.044 | +0.044 | +0.044 | +0.045 | +0.045 |
| 13.5 | . 041 | .04I | . 042 | .042 | . 042 | . 042 | . 043 | . 043 | . 043 | . 043 |
| 14.0 | . 040 | . 040 | . 040 | . 040 | .04I | .04I | .041 | . 042 | .042 | . 042 |
| 14.5 | . 033 | . 039 | . 039 | . 039 | . 039 | . 040 | .040 | . 040 | .040 | .04I |
| 15.0 | .037 | .037 | . 037 | .03S | . 038 | .038 | .038 | . 039 | .039 | . 039 |
| 15.5 | +0.036 | +0.036 | +0.036 | +0.036 | +0.037 | +0.037 | +0.037 | $+0.037$ | +0.037 | +0.038 |
| 16.0 | . 034 | . 034 | . 035 | . 035 | . 035 | . 035 | .036 | . 036 | .036 | . 036 |
| 16.5 | . 033 | . 033 | . 033 | . 034 | . 034 | . 034 | . 034 | . 034 | . 035 | .035 |
| 17.0 | . 032 | . 032 | . 032 | . 032 | . 032 | . 033 | . 033 | . 033 | . 033 | . 033 |
| 17.5 | . 030 | . 030 | . 031 | . 031 | . 03 I | . 03 I | .031 | . 032 | . 032 | .032 |
| 18.0 | +0.029 | +0.029 | $+0.029$ | +0.029 | +0.030 | +0.030 | +0.030 | +0.030 | +0.030 | +0.03I |
| 18.5 | . 027 | . 028 | . 028 | . 02 S | . 028 | . 028 | . 029 | . 029 | . 029 | . 029 |
| 19.0 | . 026 | . 026 | . 026 | . 027 | . 027 | . 027 | . 027 | . 027 | . 027 | . 028 |
| 19.5 | . 025 | . 025 | . 025 | . 025 | . 025 | . 026 | . 026 | . 026 | . 026 | . 026 |
| 20.0 | . 023 | . 02.4 | . 024 | . 024 | . 024 | . 024 | . 024 | . 024 | . 025 | . 025 |
| 20.5 | +0.022 | +0.022 | $+0.022$ | +0.022 | +0.023 | $+0.023$ | +0.023 | $+0.023$ | $+0.023$ | +0.023 |
| 21.0 | . 021 | . 021 | . 021 | . 021 | . 02 I | . 02 I | . 022 | . 022 | . 022 | . 022 |
| 21.5 | .019 | .OI9 | . 020 | . 020 | . 020 | . 020 | . 020 | . 020 | . 020 | . 020 |
| 22.0 | . 018 | .or8 | .or8 | .oı8 | . 018 | .OI9 | . 019 | . 019 | .OI9 | .ol9 |
| 22.5 | . 017 | . 017 | . 017 | .017 | . 017 | . 017 | .017 | . 017 | . 017 | . 018 |
| 23.0 | +0.015 | +o.015 | +0.015 | +0.016 | +0.016 | +0.016 | +0.016 | +0.016 | +0.016 | +0.016 |
| 23.5 | . 014 | .OI4 | . 014 | .OI4 | .OI4 | . 014 | . 014 | . OI 5 | . 015 | . 015 |
| 24.0 | . 013 | .OI3 | . 013 | . 013 | .OI 3 | . OI 3 | . 013 | . 013 | .oI3 | .OI3 |
| 24.5 | . OI 1 | .OII | .OII | . 011 | .oII | . OI 2 | . 012 | . 012 | . O 2 | . 012 |
| 25.0 | . 010 | . 010 | . 010 | . OIO | .oro | .oio | . O O | . O O | o. 10 | . 10 |

Table 44.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Ther- | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ahren heit. | 29.8 | 30.0 | 30.2 | 30.4 | 30.6 | 30.8 | 31.0 | 31.2 | 31.4 | 31.6 |
| F. | Inch. |  |  |  |  |  |  |  | Inch. | nch. |
| 25.5 | +0.008 | +0.009 | +0.009 | +0.009 | +0.009 | $+0.009$ | +0.009 | +0.009 | +0.009 | +0.009 |
| 26.0 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 008 | - 0.008 |
| 26.5 | . 006 | . 006 | . 006 | . 006 | . .006 | . .006 | . 006 | . 006 | . 006 | -.006 |
| 27.0 | . 004 | 4 .004 | . 004 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 | . 005 |
| 27.5 | . 003 | . 003 | . 003 | . 003 | . 003 | .003 | . 003 | . 003 | . 003 | . 003 |
| 28.0 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | +0.002 | to.002 |
| 28.5 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | +0.002 0.000 |
| 29.0 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | -0.001 | - $\begin{array}{r}\text { 0.000 } \\ -0.001\end{array}$ |
| 29.5 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 | . 002 |
| 30.0 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 | . 004 |
| 30.5 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 | -0.005 |
| 31.0 | . 006 | . 006 | . 006 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 | . 007 |
| 31.5 | . 008 | . 008 | . 008 | . 008 | . 008 | . 008 | .008 | . 008 | . 008 | . 008 |
| 32.0 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 009 | . 010 | . 010 | . 010 |
| 32.5 | . 010 | .OII | . 011 | . OI I | . OI I | . 017 | . 011 | . OII | .OII | . OI 1 |
| 33.0 | -0.012 | -0.012 | -0.012 | -0.012 | -0.012 | -0.012 | -0.012 | -0.012 | -0.012 | -0.013 |
| 33.5 | . 013 | . 013 | . 013 | . 013 | . 014 | . 014 | .OI4 | . OI 4 | . 014 | . 014 |
| 34.0 | . 015 | . 015 | . OI 5 | . 015 | . 015 | . 015 | . 015 | . 015 | . 015 | . OI 5 |
| 34.5 | . 016 | . 016 | . 016 | . 016 | . 016 | . 016 | . 017 | . 017 | . 017 | . 1017 |
| 35.0 | . 017 | .017 | . 017 | . 018 | . 018 | . OI 8 | . 018 | .ors | . 018 | . 018 |
| 35.5 | 0.019 | -0.019 | -0.019 | -0.019 | -0.019 | -0.019 | -0.019 | -0.019 | -0.020 | -0.020 |
| 36.0 | . 020 | . 020 | . 020 | . 020 | . 020 | . 021 | .02I | . 02 I | . 021 | . 021 |
| 36.5 | . 021 | . 021 | . 022 | . 022 | . 022 | . 022 | . 022 | . 022 | . 022 | . 023 |
| 37.0 | . 023 | . 023 | . 023 | . 023 | . 023 | . 023 | . 024 | . 024 | . 024 | . 024 |
| 37.5 | . 024 | . 024 | . 024 | . 024 | . 025 | . 025 | . 025 | . 025 | . 025 | . 025 |
| 38.0 | -0.025 | -0.026 | -0.026 | -0.026 | -0.026 | -0.026 | -0.026 | -0.027 | -0.027 | -0.027 |
| 38.5 | . . 027 | . 027 | . 027 | . 027 | . 027 | . 028 | . 028 | . 028 | . 028 | . 028 |
| 39.0 | . 028 | . 028 | . 028 | . 029 | . 029 | . 029 | . 029 | . 029 | . 030 | . 030 |
| 39.5 | . 029 | . 030 | . 030 | .030 | . 030 | .030 | .03I | .03I | . 031 | . 031 |
| 40.0 | .03I | . 03 I | . 031 | . 03 I | . 032 | . 032 | . 032 | .032 | . 032 | . 033 |
| 40.5 | -0.032 | -0.032 | -0.033 | -0.033 | -0.033 | -0.033 | -0.033 | -0.034 | -0.034 | -0.034 |
| 41.0 | . 033 | . 034 | . 034 | . 034 | . 034 | . 035 | . 035 | . 035 | . 035 | . 035 |
| 41.5 | .035 | . 035 | . 035 | . 035 | . 036 | . 036 | .036 | .036 | . 037 | . 037 |
| 42.0 | . 036 | . 036 | . 037 | . 037 | . 037 | . 037 | . 038 | . 038 | . 038 | . 038 |
| 42.5 | . 037 | . 038 | . 038 | . 038 | . 038 | . 039 | . 039 | . 039 | . 040 | . 040 |
| 43.0 | -0.039 | -0.039 | -0.039 | -0.040 | -0.040 | -0.040 | -0.040 | -0.04I | -0.04I | -0.04I |
| 43.5 | . 040 | . 040 | .041 | . 041 | .04I | . 042 | . 042 | . 042 | . 042 | . 043 |
| 44.0 | . 042 | . 042 | . 042 | . 042 | . 043 | . 043 | . 043 | . 043 | . 044 | . 044 |
| 44.5 | . 043 | . 043 | . 043 | . 044 | . 044 | . 044 | . 045 | . 045 | .045 | . 045 |
| 45.0 | . 044 | . 045 | . 045 | . 045 | . 045 | . 046 | . 046 | . 046 | . 047 | . 047 |
| 45.5 | -0.046 | -0.046 | -0.046 | -0.047 | -0.047 | -0.047 | -0.047 | -0.048 | -0.048 | --0.048 |
| 46.0 | . 047 | . 047 | . 048 | . 048 | . 048 | . 049 | . 049 | . 049 | . 049 | . 050 |
| 46.5 | . 048 | . 049 | . 049 | . 049 | .050 | .050 | . 050 | .05I | .051 | . 051 |
| 47.0 | . 050 | . 050 | . 050 | .051 | .051 | . 051 | . 052 | . 052 | . 052 | . 053 |
| 47.5 | . 051 | .051 | .052 | .052 | .052 | . 053 | . 053 | . 053 | . 054 | . 054 |
| 48.0 | -0.052 | -0.053 | -0.053 | -0.053 | -0.054 |  |  |  | -0.055 | -0.055 |
| 48.5 | . 054 | . 054 | . 054 | . 055 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 |
| 49.0 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 | . 057 | . 058 | . 058 | . 053 |
| 49.5 | . 056 | . 057 | . 057 | . 058 | .058 | . 058 | . 059 | . 059 | . 059 | . 060 |
| 50.0 | . 058 | . 058 | . 058 | . 059 | . 059 | . 060 | . 060 | . 060 | .06I | .061 |

Table 44.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
ENGLISH MEASURES.

| Attached Ther- | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fahren- heit. | 29.8 | 30.0 | 30.2 | 30.4 | 30.6 | 30.8 | 31.0 | 31.2 | 31.4 | 31.6 |
| F. | Inch. | Iuch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| 50.5 | 0.059 | -0.059 | -0.060 | -0.060 | -0.061 | -0.06I | -0.06I | -0.062 | -0.062 | -0.063 |
| 51.0 | . 060 | . 061 | . 061 | . 062 | . 062 | . 062 | . 063 | . 063 | . 06.4 | . 064 |
| 51.5 | . 062 | .062 | .063 | . 063 | .063 | .064 | .064 | . 065 | . 065 | . 065 |
| 52.0 | . 063 | . 064 | . 064 | .064 | . 065 | . 065 | . 066 | . 066 | . 066 | . 067 |
| 52.5 | . 064 | . 065 | . 065 | . 066 | . 066 | . 067 | . 067 | . 067 | . 068 | . 068 |
| 53.0 | -0.066 | -0.066 | -0.067 | -0.067 | -0.068 | -0.06S | -0.068 | -0.069 | -0.069 | -0.070 |
| 5.3 .5 | . 067 | . 068 | . 065 | . 069 | . 069 | . 069 | . 070 | . 070 | . 071 | . 071 |
| 54.0 | . 068 | . 069 | . 069 | . 070 | . 070 | .07I | . 071 | .072 | . 072 | . 073 |
| 54.5 | .070 | . 070 | .07I | . 071 | . 072 | . 072 | . 073 | . 073 | . 074 | . 074 |
| 55.0 | .07 5 | . 072 | .072 | . 073 | . 073 | . 074 | . 074 | . 075 | . 075 | . 075 |
| 55.5 | -0.073 | -0.073 | -0.074 | -0.074 | -0.074 | -0.075 | -0.075 | -0.076 | -0.076 | -0.077 |
| 56.0 | . 074 | . 074 | . 075 | . 075 | . 076 | . 076 | . 077 | . 077 | . 078 | . 078 |
| 56.5 | . 075 | . 076 | .076 | . 077 | .077 | .07S | .078 | . 079 | . 079 | .080 |
| 57.0 | .077 | . 077 | .078 | . 078 | . 079 | . 079 | .oSo | .OSO | .08I | .08I |
| 57.5 | .078 | . 078 | . 079 | . 079 | .0So | .OSI | .08I | .082 | . 082 | .083 |
| 58.0 | -0.079 | -0.0So | -0.080 | -0.08I | -0.08I | -0.082 | $-0.082$ | $-0.083$ | -0.084 | -0.084 |
| 58.5 | .OSI | . OSI | .0S2 | . 082 | . 083 | .os3 | .084 | .084 | . 0 S5 | . 085 |
| 59.0 | .082 | .083 | .083 | .084 | .084 | . 085 | .0S5 | . 086 | . 086 | . 087 |
| 59.5 | $.08_{3}$ | .os4 | .084 | .085 | . 086 | .086 | .087 | .087 | .OSS | .088 |
| 60.0 | . 085 | .oS5 | . 086 | .os6 | . 087 | . 087 | .oSS | .os9 | .os9 | .090 |
| 60.5 | 0.086 | -0.0S7 | -0.087 | -0.08S | -0.08S | -0.089 | -0.089 | -0.090 | -0.091 | -0.091 |
| 61.0 | .087 | .oSS | .089 | .oS9 | . 090 | . 090 | .09I | .091 | . 092 | . 093 |
| 61.5 | .oS9 | .oS9 | .090 | . 090 | .09I | . 092 | . 092 | . 093 | . 093 | . 094 |
| 62.0 | . 090 | .09I | .091 | . 092 | . 092 | . 093 | . 094 | . 094 | . 095 | . 095 |
| 62.5 | .091 | . 092 | . 093 | . 093 | . 094 | . 094 | . 095 | . 096 | . 096 | . 097 |
| 63.0 | -0.093 | -0.093 | -0.094 | -0.095 | -0.095 | -0.096 | -0.096 | -0.097 | -0.09S | -0.09S |
| 63.5 | . 094 | . 095 | . 095 | . 096 | . 097 | . 097 | .098 | .09S | . 099 | . 100 |
| 64.0 | . 095 | . 096 | . 097 | . 097 | .098 | . 099 | . 099 | .100 | . 101 | . IOI |
| 64.5 | . 097 | . 097 | .098 | . 099 | .099 | . 100 | . 101 | . IO | . 102 | . 103 |
| 65.0 | .ogS | . 099 | . 099 | . 100 | . IOI | . IOI | . 102 | . 103 | . 103 | . 104 |
| 65.5 | -0.099 | -0. 100 | -0.101 | -O.IOI | -0.102 | -0.103 | -0.103 | -0.104 | -0.105 | -0.105 |
| 66.0 | . IOI | . IOI | . 102 | . 103 | .103 | . 104 | . 105 | . 106 | . 106 | . 107 |
| 66.5 | . 102 | . 103 | . 103 | . 104 | .105 | .106 | . 106 | . 107 | . 108 | . 108 |
| 67.0 | . 103 | . 104 | . 105 | . 106 | .106 | . 107 | . ioS | . 108 | . 109 | . 110 |
| 67.5 | . 105 | . 106 | . 106 | . 107 | . 108 | . 108 | . 109 | . 110 | . 110 | . II I |
| 68.0 | -0.106 | $-0.107$ | -0.108 | -0.108 | -0.109 | -0.110 | -0.110 | -O. III | -0.112 | -0.113 |
| 6 S .5 | . 107 | . IOS | . 109 | . 110 | . 110 | . III | . 112 | . 113 | .113 | . II4 |
| 69.0 | . 109 | . 110 | . 110 | . 111 | . 112 | . 112 | . 113 | . 114 | . 115 | . 115 |
| 69.5 | . 110 | . III | . 112 | . 112 | . 113 | . II4 | . 115 | . 115 | .116 | . 117 |
| 70.0 | . 112 | . 112 | . 113 | . 114 | . 115 | . 115 | .116 | .117 | . 117 | .IIS |
| 70.5 | -0.113 | -0.114 | -0.114 | -0.115 | -0.116 | -0.117 | -0.117 | -0. IIS | -0.119 | -0.120 |
| 71.0 | . 114 | . II 5 | . 116 | . 116 | . 117 | . IIS | . 119 | . 120 | . 120 | .12I |
| 71.5 | . 116 | . 116 | .117 | . 118 | . 119 | . 19 | . 120 | . 121 | . 122 | . 123 |
| 72.0 | . 117 | . 118 | . 118 | . 119 | .120 | . 121 | . 122 | . 122 | .123 | . 124 |
| 72.5 | . 118 | . 119 | . 120 | . 121 | . 121 | . 122 | .123 | . 124 | .125 | .125 |
| 73.0 | -0.120 | -0.120 | -0.121 | -0.122 | -0.123 | -0.124 | -0.124 | -0.125 | -0.126 | -0.127 |
| 73.5 | . 121 | . 122 | . 123 | . 123 | .124 | . 125 | . 126 | . 127 | . 127 | . 12 S |
| 74.0 | . 122 | . 123 | . 124 | . 125 | . 126 | . 126 | . 127 | . 128 | . 129 | .130 |
| 74.5 75.0 | .124 .125 | 124 .126 | . 125 | . 126 | .127 .128 | . 128 | . 129 | . 129 | . 130 | .13I |
| 75.0 | . 125 | . 126 | . 127 | . 127 | . 128 | . 129 | . 130 | . 131 | . 132 | .132 |

## REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

 ENGLISH MEASURES.| Attached Thermometer Fahren. heit. | HEIGHT OF THE BAROMETER IN INCHES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 29.8 | 30.0 | 30.2 | 30.4 | 30.6 | 30.8 | 31.0 | 31.2 | 31.4 | 31.6 |
| F. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. | Inch. |
| 75.5 | -0.126 | -0.127 | -0.128 | -0.129 | -0.130 | -0.131 | -0.131 | -0.132 | -0. 133 | -0.134 |
| 76.0 | . 128 | . 128 | . 129 | . 130 | . 311 | .132 | . 133 | . 134 | . 134 | . 135 |
| 76.5 | . 129 | . 130 | . 131 | . 132 | . 132 | . 133 | . 134 | . 135 | . 136 | . 137 |
| 77.0 | . 130 | .13I | .132 | . 133 | . 134 | . 135 | . 136 | . 136 | . I37 | . 138 |
| 77.5 | . 132 | . 133 | . 133 | . I34 | . 135 | . 136 | . 137 | . 138 | . I 39 | . 140 |
| 78.0 | -0.133 | -0.134 | -0.135 | -0.136 | -0.137 | -0.137 | -0.138 | -0.139 | -0.140 | -0.141 |
| 78.5 | . 134 | . 135 | . 136 | . 137 | . 138 | . 139 | . 140 | . 141 | . 142 | . 142 |
| 79.0 | . 136 | . 137 | . 137 | . 138 | . 139 | . 140 | . I4I | . 142 | . 143 | . 144 |
| 79.5 | . 137 | . 138 | - I39 | . 140 | . 141 | . 142 | . 143 | . 143 | . 144 | . 145 |
| 80.0 | . 138 | . 139 | . 140 | . 141 | . 142 | . 143 | . 144 | . 145 | . 146 | . 147 |
| 80.5 | -0.140 | -0.14I | -0.142 | -0.142 | -0.143 | -0.144 | -0.145 | -0.146 | -0.147 | -0.148 |
| 81.0 | . 141 | . 142 | . 143 | . 144 | . 145 | . 146 | . 147 | . 148 | . 149 | . 150 |
| 81.5 | . 142 | . 143 | . 144 | . 145 | . 146 | . 147 | . 148 | . 149 | . 150 | . 151 |
| 82.0 | . 144 | . 145 | . 146 | . 147 | .148 | . 149 | . 149 | . 150 | .15I | . 152 |
| 82.5 | . 145 | . 146 | . 147 | . 148 | . 149 | . 150 | . 151 | . 152 | . 53 | . 154 |
| 83.0 | -0.146 | -0.147 | -0.148 | -0.149 | -0.150 | -0.151 | -0.152 | -0.153 | -0.154 | -0.155 |
| 83.5 | . 148 | . 149 | . 150 | . 151 | . 152 | . 153 | . 154 | . 155 | . 156 | . 157 |
| 84.0 | . 149 | . 150 | . 515 | . 152 | . 153 | . 154 | . 155 | . 156 | . 157 | . 158 |
| 84.5 | . 150 | . 151 | . 152 | . 153 | . 154 | . 155 | . 156 | . 157 | . 158 | . 159 |
| 85.0 | . 152 | . 153 | . 154 | . 155 | . 156 | . 157 | . 158 | . 159 | . 160 | . 161 |
| 85.5 | -0.153 | -0.154 | -0.155 | -0.156 | -0.157 | -0.158 | -0.159 | -0.160 | -0.16I | -0.162 |
| 86.0 | . 154 | . 155 | . 156 | . 158 | . 159 | . 160 | .16I | . 162 | . 163 | . 164 |
| 86.5 | . 156 | . 157 | . 158 | . 159 | . 160 | .16I | .16.2 | .163 | . 164 | . 165 |
| 87.0 | . 157 | . 158 | . 159 | . 160 | . 161 | . 162 | . 163 | . 164 | . 166 | .167 |
| 87.5 | . 158 | . 159 | .161 | . 162 | . 163 | . 164 | . 165 | . 166 | . 167 | . 168 |
| 88.0 | -0.160 | -0.161 | -0.162 | -0.163 | -0.164 | -0.165 | -0.166 | -0.167 | -0.168 | -0.169 |
| 88.5 | . 161 | . 162 | . 163 | . 164 | . 165 | . 166 | . 168 | . 169 | . 170 | .171 |
| 89.0 | . 162 | . 164 | . 165 | . 166 | . 167 | . 168 | . 169 | . 170 | . 171 | .172 |
| 89.5 | . 164 | . 165 | . 166 | . 167 | . 168 | .169 | . 170 | . 171 | . 173 | . 174 |
| 90.0 | .165 | . 166 | . 167 | . 168 | . 170 | .171 | . 172 | . 173 | . 174 | . 175 |
| 90.5 | -0.166 | -0.168 | -0.169 | -0.170 | -0.171 | -0.172 | -0.173 | -0.174 | -0.175 | $-0.176$ |
| 91.0 | . 168 | . 169 | . 170 | . 171 | . 172 | . 173 | . 175 | . 176 | . 177 | . 178 |
| 91.5 | . 169 | .170 | .171 | . 173 | . 174 | . 175 | . 176 | . 177 | . 178 | . 179 |
| 92.0 | . 170 | . 172 | .173 | . 174 | . 175 | . 176 | .177 | . 178 | . 180 | .181 |
| 92.5 | . 172 | . 173 | . 174 | . 175 | . 176 | . 178 | . 179 | . 180 | .181 | .182 |
| 93.0 | -0.173 | -0.174 | -0.175 | -0.177 | -0.178 | -0.179 | -0.180 | -0.18I | -0.182 | -0.184 |
| 93.5 | . 174 | . 176 | . 177 | . 178 | . 179 | . I8o | . 181 | .183 | . 184 | -. 185 |
| 94.0 | . 176 | . 177 | .178 | . 179 | . ISo | . 182 | . 183 | . 184 | . 185 | . I86 |
| 94.5 | . 177 | .178 | .179 | . 181 | . 182 | . 183 | . IS4 | . 185 | . 187 | . 188 |
| 95.0 | . 178 | . 180 | .181 | . 182 | . 183 | . 184 | . 186 | . 187 | . 188 | . 189 |
| 95.5 | -0.180 | -0.18I | $-0.182$ | -0.183 | -0.185 | -0.186 | -0.187 | -0.188 | -0 189 | -0.191 |
| 96.0 | . 181 | . 182 | . 184 | . 185 | . 186 | . 187 | . 188 | . 190 | . 191 | . 192 |
| 96.5 | . 182 | . 184 | . 185 | . 186 | . 187 | . 189 | . 190 | .191 | . 192 | . 193 |
| 97.0 | . IS4 | . 185 | . 186 | .187 | . 189 | . 190 | . 191 | . 192 | . 194 | . 195 |
| 97.5 | . 185 | . 186 | . 188 | . 189 | . 190 | .191 | . 193 | . 194 | . 195 | . 196 |
| 98.0 | -0.186 | -0.188 | -0.189 | -0.190 | -0.191 | -0.193 | -0.194 | -0.195 | -0.196 | -0.198 |
| 98.5 | . 188 | . 189 | . 190 | . 192 | . 193 | . 194 | . 195 | . 197 | . 198 | . 199 |
| 99.0 | . 189 | . 190 | . 192 | . 193 | . 194 | . 195 | . 197 | . 198 | . 199 | . 201 |
| 99.5 | . 190 | . 192 | . 193 | . 194 | . 196 | . 197 | . 198 | . 199 | . 201 | . 202 |
| 100.0 | . 192 | . 193 | . 194 | . 196 | . 197 | . 198 | . 200 | . 201 | . 202 | . 203 |

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE METRIC MEASURES.
for temperatures above $0^{\circ}$ centigrade, the correction to be subtracted.

| Attached Thermometer Centigrade. | height of the barometer in millimeters. |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 440 | 450 | 460 | 470 | 480 | 490 | 500 | 510 | 520 | 530 | 540 | 550 | 560 |
| c. | mm. | mm. | mm . | mm. | mm . | mm . | mm . | mm. | mm. | mm. | mm. | mm. | mm . |
| 0.0 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.5 | . 04 | . 04 | . 04 | . 04 | . 04 | . 04 | . 04 | . 0.4 | . 04 | . 04 | . 04 | . 04 | . 05 |
| 1.0 | . 07 | . 07 | . 08 | . 08 | . 08 | . 08 | .o8 | . 08 | . 08 | . 09 | . 09 | . 09 | . 09 |
| 1.5 | . 11 | . II | . 1 I | . 12 | . 12 | . 12 | . 12 | . 12 | . 13 | . 13 | . 13 | . 13 | . 14 |
| 2.0 | . 14 | . 15 | . 15 | . 15 | . 16 | . 16 | . 16 | . 17 | . 17 | . 17 | . 18 | . 18 | . 18 |
| 2.5 | 0.18 | 0.18 | O. 19 | 0. 19 | 0. 20 | 0.20 | 0.20 | 0. 21 | 0.2I | 0.22 | 0.22 | 0.22 | 0.23 |
| 3.0 | . 22 | . 22 | . 23 | . 23 | . 24 | . 24 | . 24 | . 25 | . 25 | . 26 | . 26 | . 27 | . 27 |
| 3.5 | . 25 | . 26 | . 26 | . 27 | . 27 | . 28 | . 29 | . 29 | . 30 | . 30 | . 31 | . 31 | . 32 |
| 4.0 | . 29 | . 29 | . 30 | . 31 | . 31 | . 32 | . 33 | . 33 | . 34 | . 35 | . 35 | . 36 | . 37 |
| 4.5 | . 32 | . 33 | - 34 | - 35 | . 35 | . 36 | . 37 | . 37 | . 38 | . 39 | . 40 | . 40 | . 4 I |
| 5.0 | 0.36 | 0.37 | 0.38 | 0.38 | 0.39 | 0.40 | 0.41 | 0.42 | 0.42 | 10.43 | 0.44 | 0.45 | 0.46 |
| 5.5 | . 40 | . 40 | . 41 | . 42 | . 43 | . 44 | . 45 | . 46 | . 47 | . 48 | 48 | . 49 | . 50 |
| 6.0 | . 43 | . 41 | . 45 | . 46 | . 47 | . 48 | . 49 | . 50 | . 51 | . 52 | . 53 | . 54 | . 55 |
| 6.5 | . 47 | .48 | . 49 | . 50 | . 5 I | . 52 | . 53 | . 54 | . 55 | . 56 | . 57 | . 58 | . 59 |
| 7.0 | . 50 | . 51 | . 53 | . 54 | . 55 | . 56 | . 57 | . 58 | . 59 | .61 | . 62 | . 63 | . 64 |
| 7.5 | 0.54 | 0.55 | 0.56 | 0.58 | 0.59 | 0.60 | 0.6I | 0.62 | 0.64 | 0.65 | 0. 66 | 0.67 | 0.69 |
| 8 o | . 57 | . 59 | . 60 | . 61 | . 63 | . 64 | . 65 | . 67 | . 68 | . 69 | . 70 | . 72 | . 73 |
| 8.5 | .61 | . 62 | . 64 | . 65 | .67 | . 68 | . 69 | . 71 | . 72 | . 73 | . 75 | . 76 | . 78 |
| 9.0 | . 65 | . 66 | . 68 | . 69 | . 70 | . 72 | . 73 | . 75 | .76 | . 78 | .79 | . 81 | . 82 |
| 9.5 | . 68 | .70 | . 71 | . 73 | . 74 | .76 | .77 | . 79 | . 81 | . 82 | . 84 | . 85 | . 87 |
| 10.0 | 0.72 | 0.73 | 0. 75 | 0.77 | 0.78 | 0.80 | 0.82 | 0. 83 | 0. 85 | 0.86 | 0.88 | 0.90 | 0.91 |
| 10.5 | . 75 | . 77 | . 79 | . 80 | . 82 | . 84 | . 86 | . 87 | . 89 | .91 | . 92 | . 94 | . 96 |
| II. 0 | . 79 | . 81 | . 83 | . ¢ $_{4}$ | . 86 | . 88 | . 90 | . 91 | . 93 | . 95 | . 97 | . 99 | 1.00 |
| I 1.5 | . 83 | . 84 | . 86 | . 88 | .90 | . 92 | . 94 | . 96 | . 98 | . 99 | 1.01 | 1.03 | 1.05 |
| 12.0 | . 86 | . 88 | . 90 | . 92 | . 94 | .96 | . 98 | 1.00 | 1.02 | 1.04 | I. 06 | 1.08 | I. IO |
| 13.0 | - 93 | 0.95 | 0.97 | 1.00 | 1.02 | 1.04 | 1. 06 | 1.0S | 1. 10 | 1.12 | I. 14 | I. 17 | I. 19 |
| 14.0 | 1.00 | 1.03 | 1.05 | 1. 07 | I. 10 | I. 12 | I. 14 | I. 16 | 1.19 | 1.21 | I. 23 | 1. 25 | 1. 28 |
| 15.0 | 1.08 | 110 | 1.12 | I.I5 | 1.17 | I. 20 | 1.22 | 1.25 | 1.27 | 1.30 | 1.32 | 1.34 | I. 37 |
| 16.0 | 1. I5 | 1.17 | I. 20 | 1.23 | I. 25 | 1. 28 | 1.30 | 1.33 | 1. 36 | I. 38 | I.4I | I. 43 | I. 46 |
| 17.0 | 1.22 | 1.25 | 1.27 | 1.30 | 1.33 | 1. 36 | 1.38 | 1.41 | 1. 44 | 1.47 | 1.50 | 1.52 | 1.55 |
| 18.0 | 1.29 | 1.32 | 1.35 | 1.38 | I. 41 | 1.44 | 1.47 | 1.50 | 1.52 | I. 55 | 1.58 | 1.61 | 1. 64 |
| 19.0 | 1.36 | 1.39 | 1.42 | 1.45 | I. 49 | 1.52 | I. 55 | 1.58 | I.6I | I. 64 | 1.67 | 1.70 | 1.73 |
| 20.0 | 1.43 | 1.47 | 1.50 | 1.53 | 1.56 | 1. 60 | 1.63 | I. 66 | I. 69 | 1.73 | I. 76 | 1.79 | 1.82 |
| 2 I .0 | 1.50 | I. 54 | I. 57 | 1.61 | 1.64 | 1.67 | 1.71 | 1.74 | I. 78 | 1.81 | 1.85 | 1.88 | I.91 |
| 22.0 | I. 58 | 1.6I | 1.65 | 1.68 | 1.72 | 1.75 | I. 79 | 1. 83 | I. 86 | I. 90 | 1.93 | 1.97 | 2.01 |
| 23.0 | 1.65 | 1.68 | 1. 72 | 1.76 | 1.80 | 1.83 | 1.87 | 191 | 1.95 | 1.98 | 2.02 | 2.06 | 2. 10 |
| 24.0 | 1.72 | 1.76 | 1. 30 | I. 84 | 1.87 | 1.91 | 1.95 | 1.99 | 2.03 | 2.07 | 2. II | 2.15 | 2.19 |
| 25.0 | 1.79 | J. 83 | I. 87 | I.91 | I. 95 | 1.99 | 2.03 | 2.07 | 2. II | 2.16 | 2.20 | 2.24 | 2.28 |
| 26.0 | 1.86 | 1.90 | I. 95 | I. 99 | 2.03 | 2.07 | 2.11 | 2. I6 | 2.20 | 2.24 | 2.28 | 2.33 | 2.37 |
| 27.0 | I. 93 | 1.98 | 2.02 | 2.06 | 2. II | 2. I5 | 2.20 | 2.24 | 2.28 | 2.33 | 2.37 | 2.41 | 2.46 |
| 28.0 | 2.00 | 2.05 | 2.09 | 2.14 | 2. 18 | 2.23 | 2.28 | 2.32 | 2.37 | 2.41 | 2.46 | 2.50 | 2.55 |
| 29.0 | 2.07 | 2. 12 | 2.17 | 2.22 | 2.26 | 2.31 | 2.36 | 2.40 | 2.45 | 2.50 | 2.55 | 2.59 | 2.64 |
| 30.0 | 2.15 | 2.19 | 2.24 | 2.29 | 2.34 | 2.39 | 2.44 | 2.49 | : 5. 4 | 2.58 | 2.63 | 2.68 | 2.73 |
| 31.0 | 2.22 | 2.27 | 2.32 | 2.37 | 2.42 | 2.47 | 2.52 | 2.57 | 2.02 | 2.57 | 2.72 | 2.77 | 2.82 |
| 32.0 | 2.29 | 2.34 | 2.39 | 2.44 | 2.50 | 2.55 | 2.60 | 2.65 | 2.70 | 2.76 | 2.81 | 286 | 2.91 |
| 33.0 | 2.36 | 2.41 | 247 |  | 2.57 | 2.63 | 2.68 | 2.73 | 2.79 | 2.84 | 2.89 | 2.95 | 3.00 |
| 34.0 | 2.43 | 2.48 | 2.54 | 2.60 | 2.65 | 2.71 | 2.76 | 2.82 | 2.87 | 2.93 | 2.98 | 3.04 | 3.09 |
| 35.0 | 2.50 | 2.55 | 2.61 | 2.67 | 2.73 | 2.78 | 2.84 | 2.90 | 2.96 | 3.01 | 3.07 | 3.13 | 3.18 |

Table 45.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, the CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 560 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 570 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | $0 \% 0$ | 0:2 | 0.4 | 0.6 | 0.8 | 0.0 | 0:2 | 0.4 | 0.6 | 0.8 |
| c. | mm . | mm . | mm. | mm . | mm . | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.05 | 0.07 | 0.00 | 0.02 | 0.04 | 0.06 | 0.07 |
| I | . 09 | . II | . I3 | . 15 | . 16 | . 09 | . II | . I3 | . 15 | . 17 |
| 2 | . 18 | . 20 | . 22 | . 24 | . 26 | . 19 | . 20 | . 22 | . 24 | . 26 |
| 3 | . 27 | . 29 | . 31 | . 33 | . 35 | . 28 | . 30 | $\cdot 32$ | . 34 | . 35 |
| 4 | $\cdot 37$ | . 3 S | . 40 | . 42 | . 44 | . 37 | . 39 | .4I | .43 | . 45 |
| 5 | 0.46 | 0.48 | 0.49 | 0.51 | 0.53 | 0.47 | 0.48 | 0.50 | 0. 52 | 0.54 |
| 6 | . 55 | . 57 | . 5 S | . 60 | . 62 | . 56 | . 5 S | . 60 | . 61 | . 63 |
| 7 | . 64 | . 66 | . 68 | . 69 | . 71 | .65 | . 67 | . 69 | . 71 | . 73 |
| 8 | . 73 | .75 | .77 | . 79 | .So | .74 | .76 | . 78 | . So | . 82 |
| 9 | . S 2 | . 84 | . 86 | . 58 | . 90 | . 84 | . 86 | . 87 | . 89 | . 91 |
| 10 | 0.91 | 0.93 | 0.95 | 0.97 | 0.99 | 0.93 | 0.95 | 0.97 | 0.99 | I. 00 |
| II | 1.00 | 1.02 | I. 0.4 | 1.06 | I. 08 | 1.02 | I. 0.4 | 1.06 | 1.08 | I. 10 |
| 12 | I. 10 | I. II | I. I3 | 1.15 | I. 17 | I. 12 | I. 13 | I. 15 | I. 17 | I. 19 |
| I3 | I. 19 | 1.20 | I. 22 | I. 24 | I. 26 | I. 21 | 1.23 | 1.25 | 1.26 | 1.28 |
| 14 | 1. 28 | 1.30 | I. 3 I | 1.33 | I. 35 | 1.30 | I. 32 | I. 34 | I. 36 | 1.37 |
| 15 | 1.37 | 1.39 | 1.41 | I. 42 | I. 44 | I. 39 | I. 4 I | 1.43 | I. 45 | I. 47 |
| 16 | I. 46 | 1.48 | 1.50 | I. 51 | I. 53 | 1.49 | I. 50 | 1.52 | 1.54 | I. 56 |
| 17 | I. 55 | 1.57 | 1.59 | I.6I | 1.62 | 1. 58 | I. 60 | 1.62 | 1.63 | I. 65 |
| IS | 1.64 | 1.66 | 1.68 | 1.70 | 1.71 | I. 67 | I. 69 | 1.71 | 1.73 | 1.75 |
| 19 | 1.73 | I. 75 | 1.77 | I. 79 | 1.81 | 1. 76 | 1.78 | I. So | I. 82 | 1.84 |
| 20 | I. $\mathrm{S}_{2}$ | J. $\mathrm{S}_{4}$ | I. 66 | I. SS | 1.90 | I. 86 | I. 87 | I. 99 | I.91 | I. 93 |
| 2 I | 1.91 | 1.93 | 1.95 | 1.97 | 1.99 | I. 95 | 1.97 | 1.99 | 2.00 | 2.02 |
| 22 | 2.01 | 2.02 | 2.04 | 2.06 | 2.08 | 2.04 | 2.06 | 2.0 S | 2.10 | 2.1 I |
| 23 | 2.10 | 2.11 | 2.13 | 2.15 | 2.17 | 2.13 | 2.15 | 2.17 | 2.19 | 2.21 |
| 24 | 2.19 | 2.20 | 2.22 | 2.24 | 2.26 | 2.23 | 2.24 | 2.26 | 2.28 | 2.30 |
| 25 | 2.28 | 2.30 | 2.3 I | 2.33 | 2.35 | 2.32 | 2.34 | 2.35 | 2.37 | 2.39 |
| 26 | 2.37 | 2.39 | 2.40 | 2.42 | 2.44 | 2.41 | 2.43 | 2.45 | 247 | 2.48 |
| 27 | 2.46 | 2.48 | 2.49 | 2.51 | 2.53 | 2.50 | 2.52 | 2.54 | 2.56 | 2.58 |
| 28 | 2.55 | 2.57 | 2.59 | 2.60 | 2.62 | 2.59 | 2.61 | 2.63 | 2.65 | 2.67 |
| 29 | 2.64 | 2.66 | 2.68 | 2.69 | 2.71 | 2.69 | 2.71 | 2.72 | 2.74 | 2.76 |
| 30 | 2.73 | 2.75 | 2.77 | 2.78 | $2 . \mathrm{So}$ | 2.78 | $2 . \mathrm{So}$ | $2 . \mathrm{S} 2$ | 2.83 | 2.85 |
| 31 | 2.82 | 2.84 | 2. S 6 | 2.87 | $2 . \mathrm{S} 9$ | 2.87 | 2.89 | 2.91 | 2.93 | 2.94 |
| 32 | 2.91 | 2.93 | 2.95 | 2.97 | 2.98 | 2.96 | 2.98 | 3.00 | 3.02 | 3.04 |
| 33 | 3.00 | 3.02 | 3.04 | 3.06 | 3.07 | 3.06 | 3.07 | 3.09 | 3.11 | 3.13 |
| 34 | 3.09 | 3.11 | 3.13 | 3.15 | 3.16 | 3.15 | 3.17 | 3.15 | 3.20 | 3.22 |
| 35 | 3.18 | 3.20 | 3.22 | 3.24 | 3.25 | 3.24 | 3.26 | 3.28 | 3.29 | 3.31 |

Table 45.

## REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

 METRIC MEASURES.FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 580 mm . |  |  |  |  | HEIGIIT OF THE BAROMETER 590 mm. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| C. | mmı. | mmı. | mm . | mm. | mm. | mım. | mm. | mm . | mm. | mm . |
| $0{ }^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 |
| 1 | . 09 | . II | . 13 | . 15 | . 17 | . 10 | . 12 | . 13 | . 15 | . 17 |
| 2 | . 19 | . 21 | . 23 | . 25 | . 27 | . 19 | .21 | . 23 | .25 | . 27 |
| 3 | . 28 | . 30 | $\cdot 32$ | . 34 | . 36 | . 29 | . 31 | . 33 | . 35 | . 37 |
| 4 | $\cdot 3^{8}$ | . 40 | . 42 | . 44 | . 45 | - 39 | . 40 | . 42 | . 44 | . 46 |
| 5 | 0.47 | 0.49 | 0.51 | 0.53 | 0.55 | 0.48 | 0.50 | 0.52 | 0.54 | 0.56 |
| 6 | . 57 | . 59 | .6I | . 62 | . 64 | . 58 | . 60 | . 62 | . 64 | . 65 |
| 7 | . 66 | . 68 | .70 | . 72 | . 74 | . 67 | . 69 | . 7 SI | . 73 | . 75 |
| 8 | .76 | .78 | . 79 | . 81 | . 83 | . 77 | . 79 | . 81 | .83 | . 85 |
| 9 | .85 | . 87 | .89 | . 91 | . 93 | .87 | . 89 | . 90 | .92 | . 94 |
| 10 | 0.95 | 0.96 | 0.98 | 1.00 | I. 02 | 0.96 | 0.98 | 1.00 | 1.02 | 1. 04 |
| II | 1.04 | 1.06 | 1.08 | 1.10 | I. 12 | 1.06 | 1.08 | I. 10 | 1.12 | I. 14 |
| 12 | I. 13 | I. 15 | I. 17 | I. 19 | I. 21 | I. 15 | 1.17 | 1. 19 | I. 21 | 1. 23 |
| 13 | I. 23 | 1.25 | 1.27 | 1.29 | 1.30 | 1.25 | 1.27 | 1.29 | 1.31 | 1.33 |
| 14 | 1.32 | 1. 34 | 1. 36 | 1.38 | I. 40 | I. 35 | 1.37 | 1.38 | 1. 40 | I. 42 |
| 15 | 1.42 | 1. 44 | I. 46 | 1.47 | I. 49 | 1. 44 | 1.46 | 1.48 | 1.50 | 1.52 |
| 16 | I. 51 | 1. 53 | 1.55 | 1.57 | I. 59 | 1.54 | I. 56 | 1.58 | 1.60 | 1.61 |
| 17 | 1.6I | 1.62 | I. 64 | I. 66 | 1.68 | I. 63 | I. 65 | 1.67 | 1.69 | 1.71 |
| 18 | 1.70 | 1.72 | 1.74 | 1. 76 | 1. 78 | I. 73 | 1.75 | 1.77 | I. 79 | I. $\mathrm{SI}^{\text {I }}$ |
| 19 | 1.79 | I. 81 | 1.83 | I. 85 | 1.87 | I. 83 | I. 84 | 1. 86 | 1. 88 | 1.90 |
| 20 | I. 89 | 1.91 | 1.93 | 1.95 | 1.96 | I. 92 | 1.94 | 1.96 | 1.98 | 2.00 |
| 21 | 1.98 | 2.00 | 2.02 | 2.04 | 2.06 | 2.02 | 2.04 | 2.06 | 2.07 | 2.09 |
| 22 | 2.08 | 2.10 | 2.11 | 2.13 | 2.15 | 2. II | 2.13 | 2. 15 | 2.17 | 2.19 |
| 23 | 2.17 | 2.19 | 2.21 | 2.23 | 2.25 | 2.21 | 2.23 | 2.25 | 2.27 | 2.25 |
| 24 | 2.26 | 2.28 | 2.30 | 2.32 | 2.34 | 2.30 | 2.32 | 2.34 | 2.36 | 2.38 |
| 25 | 2.36 | 2.38 | 2.40 | 2.41 | 2.43 | 2.40 | 2.42 | 2.44 | 2.46 | 2.48 |
| 26 | 2.45 | 2.47 | 2.49 | 2.51 | 2.53 | 2.49 | 2.51 | 2.53 | 2.55 | 2.57 |
| 27 | 2.55 | 2.57 | 2.58 | 2.60 | 2.62 | 2.59 | 2.61 | 2.63 | 2.65 | 2.67 |
| 28 | 2.64 | 2.66 | 2.68 | 2.70 | 2.72 | 2.69 | 2.70 | 2.72 | 2.74 | 2.76 |
| 29 | 2.73 | 2.75 | 2.77 | 2.79 | 2.81 | 2.78 | 2. So | 2.82 | 2.84 | 2.86 |
| 30 | 2.83 | 2.85 |  | 2.95 | 2.90 | 2.88 | 2.90 | 2.91 | 2.93 | 2.95 |
| 31 | 2.92 | 2.94 | 2.96 | 2.98 | 3.00 | 2.97 | 2.99 | 3.01 | 3.03 | 3.05 |
| 32 | 3.02 | 3.03 | 3.05 | 3.07 | 3.09 | 3.07 | 3.09 | 3.11 | 3.12 | 3.14 |
| 33 | 3.11 | 3.13 | 3.15 | 3.16 | 3.18 | 3.16 | 3.18 | 3.20 | 3.22 | 3.24 |
| 34 | 3.20 | 3.22 | 3.24 | 3.26 | 3.28 | 3.26 | 3.28 | 3.30 | 3.3 I | 3.33 |
| 35 | 3.30 | 3.31 | 3.33 | 3.35 | 3.37 | 3.35 | 3.37 | 3.39 | 3.41 | 3.43 |

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Table 45.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
METRIC MEASURES.
FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | heigiit of the barometer 600 mm . |  |  |  |  | HEIGHT OF TIIE BAROMETER 605 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Ther. mometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | 11 mm . | 11111. | 11112. | 1113. | mm. | 1111. | 1111. | 11112. | mm. |
| $0{ }^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.0S |
| I | . 10 | . 12 | . 14 | . 16 | . 18 | . 10 | . 12 | . 14 | . 16 | . 18 |
| 2 | . 20 | . 22 | . 24 | . 25 | . 27 | . 20 | .22 | . 24 | . 26 | . 28 |
| 3 | . 29 | . 31 | .33 | . 35 | . 37 | - 30 | .32 | . 34 | .36 | .38 |
| 4 | . 39 | . 41 | . 43 | . 45 | . 47 | .40 | .4I | . 43 | . 45 | .47 |
| 5 | 0.49 | 0.51 | 0.53 | 0.55 | 0.57 | 0.49 | 0.51 | 0.53 | 0.55 | 0.57 |
| 6 | . 59 | . 61 | . 63 | . 65 | . 67 | . 59 | . 61 | . 63 | . 65 | . 67 |
| 7 | . 69 | . 70 | . 72 | . 74 | . 76 | . 69 | . 71 | . 73 | . 75 | . 77 |
| 8 | .78 | . So | . 82 | . 84 | . 86 | . 79 | . SI | . $3_{3}$ | . 85 | . 87 |
| 9 | . 88 | .90 | .92 | . 94 | .96 | .89 | .91 | . 93 | . 95 | . 97 |
| 10 | 0.98 | 1.00 | I. O 2 | 1.04 | 1.06 | 0.99 | 1.01 | 1.03 | 1.05 | 1.07 |
| 11 | 1.0S | I. 10 | I. 12 | I. 13 | I. 15 | 1.09 | 1. 10 | 1.12 | 1.14 | 1.16 |
| 12 | 1.17 | I. 19 | I. 21 | 1.23 | I. 25 | I. 18 | 1.20 | I. 22 | I. 24 | I. 26 |
| 13 | 1.27 | 1.29 | 1.3I | I. 33 | I. 35 | 1.28 | 1.30 | 1. 32 | I. 34 | I. 36 |
| 14 | 1.37 | I. 39 | I. 41 | I. 43 | I. 45 | 1.38 | 1.40 | I. 42 | I. 44 | 1. 46 |
| 15 | I. 47 | 1. 49 | 1.51 | I. 53 | I. 54 | 1.48 | 1.50 | I. 52 | I. 54 | 1.56 |
| 16 | I. 56 | 1.58 | 1.60 | 1.62 | 1.64 | 1.58 | 1.60 | 1.62 | I. 64 | I. 66 |
| 17 | 1.66 | 1.68 | 1.70 | 1.72 | 1.74 | I. 68 | 1.70 | 1.71 | 1.73 | 1.75 |
| 18 | 1.76 | 1.78 | I. So | 1. 82 | I. 84 | 1.77 | 1.79 | I. SI | $1 . S_{3}$ | I. 85 |
| 19 | I. 86 | 1.88 | 1.90 | 1.91 | 1.93 | I. 87 | 1. 89 | 1.91 | 1.93 | 1.95 |
| 20 | 1.95 | 1.97 | I. 99 | 2.01 | 2.03 | 1.97 | 1.99 | 2.01 | 2.03 | 2.05 |
| 21 | 2.05 | 2.07 | 2.09 | 2.11 | 2.13 | 2.07 | 2.09 | 2.11 | 2. I 3 | 2.15 |
| 22 | 2.15 | 2. 17 | 2.19 | 2.21 | 2.23 | 2.17 | 2. 19 | 2.21 | 2.23 | 2.24 |
| 23 | 2.25 | 2.26 | 2.28 | 2.30 | 2.32 | 2.26 | 2.28 | 2.30 | 2.32 | 2.34 |
| 24 | 2.34 | 2.36 | 2.38 | 2.40 | 2.42 | 2.36 | 2.35 | 2.40 | 2.42 | 2.44 |
| 25 | 2.44 | 2.46 | 2.48 | 2.50 | 2.52 | 2.46 | 2.48 | 2.50 | 2.52 | 2.54 |
| 26 | 2.54 | 2.56 | 2.58 | 2.60 | 2.61 | 2.56 | 2.58 | 2.60 | 2.62 | 2.64 |
| 27 | 2.63 | 2.65 | 2.67 | 2.69 | 2.71 | 2.66 | 2.68 | 2.70 | 2.71 | 2.73 |
| 28 | 2.73 | 2.75 | 2.77 | 2.79 | 2.81 | 2.75 | 2.77 | 2.79 | 2.81 | 2.83 |
| 29 | 2.83 | 2.85 | 2.87 | 2.89 | 2.91 | 2.95 | 2.87 | 2.89 | 2.91 | 2.93 |
| 30 | 2.93 | 2.94 | 2.96 | 2.98 | 3.00 | 2.95 | 2.97 | 2.99 | 3.01 | 3.03 |
| 3 I | 3.02 | 3.04 | 3.06 | 3.08 | 3.10 | 3.05 | 3.07 | 3.09 | 3.11 | 3.13 |
| 32 | 3.12 | 3.14 | 3.16 | 3.1S | 3.20 | 3.15 | 3.16 | 3.18 | 3.20 | 3.22 |
| 33 | 3.22 | 3.24 | 3.25 | 3.27 | 3.29 | 3.24 | 3.26 | 3.28 | 3.30 | 3.32 |
| 34 | 3.31 | 3.33 | 3.35 | 3.37 | 3.39 | 3.34 | 3.36 | 3.38 | 3.40 | 3.42 |
| 35 | 3.41 | 3.43 | 3.45 | 3.47 | 3.49 | 3.44 | 3.46 | 3.48 | 3.50 | 3.52 |

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Table 45.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | IIEIGIIT OF TIIE BAROMETER 610 mm . |  |  |  |  | HEIGIIT OF TIIE BAROMETER 615 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0:8 |
| c. | mm . | mm . | mm. | mm. | mm. | mm . | mm . | mm . | nım. | mm . |
| $0{ }^{\circ}$ | 0.00 | 0.02 | 0.0.4 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 |
| 1 | . 10 | . 12 | . 14 | . 16 | . 18 | . 10 | . 12 | . 14 | . 16 | . 18 |
| 2 | . 20 | . 22 | . 24 | . 26 | . 28 | . 20 | . 22 | . 24 | . 26 | . 28 |
| 3 | . 30 | . 32 | . 34 | . 36 | . 38 | . 30 | $\cdot 32$ | - 34 | . 36 | . 38 |
| 4 | . 40 | .42 | . 44 | .46 | . 48 | . 40 | .42 | . 44 | .46 | . 48 |
| 5 | 0.50 | 0.52 | 0.54 | 0.56 | 0.58 | 0.50 | 0.52 | 0.54 | 0.56 | 0.58 |
| 6 | . 60 | . 62 | . 64 | . 66 | . 68 | . 60 | . 62 | . 64 | . 66 | . 68 |
| 7 | . 70 | .72 | .74 | . 76 | .78 | .70 | .72 | . 74 | .76 | .78 |
| 8 | . 80 | . 82 | . 8.4 | . 86 | . 88 | . 80 | . 82 | . 84 | . 86 | . 88 |
| 9 | .90 | .92 | . 94 | .96 | .98 | . 90 | .92 | . 94 | .96 | . 98 |
| 10 | 0.99 | I. OI | 1.03 | 1.05 | 1.07 | 1.00 | I. 02 | 1. 04 | 1.06 | 1.08 |
| I I | 1.09 | I. II | I. 13 | I. 15 | 1.17 | 1. 10 | 1. 12 | I. 14 | 1.16 | 1.18 |
| 12 | I. 19 | 1.21 | 1.23 | 1.25 | 1.27 | 1.20 | I. 22 | 1.2.4 | I. 26 | I. 28 |
| 13 | 1. 29 | 1.31 | 1.33 | 1.35 | 1.37 | 1.30 | I. 32 | I. 34 | I. 36 | I. 38 |
| 14 | I. 39 | 1.4I | 1.43 | 1.45 | 1.47 | 1.40 | I. 42 | 1.44 | I. 46 | I. 48 |
| 15 | 1.49 | I. 51 | 1.53 | I. 55 | 1.57 | 1.50 | 1.52 | I. 54 | I. 56 | 1. 58 |
| 16 | 1.59 | 1.61 | 1.63 | 1.65 | 1. 67 | 1. 60 | 1.62 | 1.64 | 1.66 | 1.68 |
| 17 | 1.69 | 1.71 | 1.73 | 1.75 | 1. 77 | 1. 70 | 1.72 | 1.74 | 1. 76 | 1. 78 |
| 18 | 1.79 | I. SI | 1.83 | 1.85 | 1.87 | 1.80 | 1.82 | I. 84 | 1.86 | I. 88 |
| 19 | I. 89 | 1.91 | 1.93 | 1.95 | 1.97 | I. 90 | 1.92 | 1.94 | 1.96 | 1.98 |
| 20 | 1.99 | 2.01 | 2.03 | 2.05 | 2.07 | 2.00 | 2.02 | 2.04 | 2.06 | 2.08 |
| 2 I | 2.09 | 2. IO | 2.12 | 2.14 | 2. 16 | 2.10 | 2.12 | 2. 14 | 2.16 | 2.18 |
| 22 | 2.18 | 2.20 | 2.22 | 2.24 | 2.26 | 2.20 | 2.22 | 2.24 | 2.26 | 2.28 |
| 23 | 2.28 | 2.30 | 2.32 | 2.34 | 2.36 | 2.30 | 2.32 | 2.34 | 2.36 | 2.38 |
| 24 | 2.38 | 2.40 | 2.42 | 2.44 | 2.46 | 2.40 | 2.42 | 2.44 | 2.46 | 2.48 |
| 25 | 2.48 | 2.50 | 2.52 | 2.54 | 2.56 | 2.50 | 2.52 | 2.54 | 2.56 | 2.58 |
| 26 | 2.58 | 2.60 | 2.62 | 2.64 | 2.66 | 2.60 | 2.62 | 2.64 | 2.66 | 2.68 |
| 27 | 2.68 | 2.70 | 2.72 | 2.74 | 2.76 | 2.70 | 2.72 | 2.74 | 2.76 | 2.78 |
| 28 | 2.78 | 2.So | 2.82 | 2.84 | 2.86 | 2.80 | 2.82 | 2.84 | 2.86 | 2.88 |
| 29 | 2.88 | 2.90 | 2.91 | 2.93 | 2.95 | 2.90 | 2.92 | 2.94 | 2.96 | 2.98 |
| 30 | 2.97 | 2.99 | 3.01 | 3.03 | 3.05 | 3.00 | 3.02 | 3.04 | 3.06 | 3.08 |
| 31 | 3.07 | 3.09 | 3.11 | 3.13 | 3.15 | 3.10 | 3.12 | 3.14 | 3.16 | 3.18 |
| 32 | 3.17 | 3.19 | 3.21 | 3.23 | 3.25 | 3.20 | 3.22 | 3.24 | 3.26 | 3.23 |
| 33 | 3.27 | 3.29 | $3 \cdot 31$ | 3.33 | 3.35 | 3.30 | $3 \cdot 32$ | $3 \cdot 34$ | 3.36 | 3.35 |
| 34 | 3.37 | 3.39 | 3.41 | 3.43 | 3.45 | 3.40 | 3.42 | 3.44 | 3.46 | 3.48 |
| 35 | 3.47 | 3.49 | 3.51 | 3.53 | 3.55 | 3.49 | 3.51 | 3.53 | 3.55 | $3 \cdot 57$ |

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table 45.
REDUCIION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTEO.

|  | heigirt of the barometer 620 mm . |  |  |  |  | height of the barometen 625 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.3 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm . | mm . | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 |
| I | . 10 | . 12 | . 14 | . 16 | . 18 | . 10 | . 12 | . 14 | . 16 | . 18 |
| 2 | . 20 | . 22 | . 24 | . 26 | . 28 | . 20 | . 22 | . 24 | . 27 | . 29 |
| 3 | . 30 | . 32 | - 34 | . 36 | - 38 | . 31 | . 33 | . 35 | .37 | . 39 |
| 4 | .40 | . 43 | . 45 | . 47 | . 49 | . 41 | . 43 | . 45 | .47 | . 49 |
| 5 | 0.51 | 0.53 | 0.55 | 0.57 | 0.59 | 0.51 | 0.53 | 0.55 | 0.57 | 0.59 |
| 6 | . 61 | . 63 | . 65 | . 67 | . 69 | . 61 | . 63 | . 65 | . 67 | . 69 |
| 7 | . 71 | . 73 | . 75 | . 77 | .79 | . 71 | . 73 | . 75 | . 78 | . 80 |
| 8 | . 81 | . 83 | . 85 | . 87 | . 89 | . 82 | . $8_{4}$ | . 86 | . 88 | . 90 |
| 9 | . 91 | . 93 | . 95 | . 97 | . 99 | .92 | . 94 | .96 | . 98 | 1.00 |
| 10 | I.OI | 1.03 | 1.05 | 1.07 | 1.09 | 1.02 | I. 04 | 1.06 | 1.08 | 1.10 |
| II | I. I I | I. 13 | I. 15 | 1.17 | I. 19 | I. 12 | 1.14 | 1.16 | I. 18 | 1.20 |
| 12 | I. 21 | 1.23 | 1.25 | 1.27 | I. 29 | I. 22 | 1.24 | 1.26 | 1.28 | 1.30 |
| I 3 | I. 31 | 1.33 | I. 35 | 1.37 | I. 39 | I. 32 | 1.34 | I. 37 | 1. 39 | 1.41 |
| 14 | I. 41 | 1.43 | 1.46 | 1.48 | 1.50 | I. 43 | 1.45 | I. 47 | 1.49 | 1. 51 |
| 15 | 1.52 | 1.54 | 1.56 | 1.58 | 1. 60 | 1.53 | I. 55 | I. 57 | 1.59 | 1.61 |
| 16 | 1.62 | 1.64 | 1.66 | 1.68 | 1.70 | 1.63 | 1. 65 | 1.67 | 1.69 | 1.71 |
| 17 | 1.72 | 1.74 | 1.76 | 1.78 | I. 80 | 1.73 | I. 75 | 1.77 | 1.79 | 1.81 |
| IS | 1.82 | 1.84 | 1.86 | I. 88 | 1.90 | I. 83 | 1.85 | 1.87 | 1.89 | 1.91 |
| 19 | 1.92 | 1.94 | 1.96 | 1.98 | 2.00 | 1.93 | 1.95 | 1.97 | 1.99 | 2.01 |
| 20 | 2.02 | 2.04 | 2.06 | 2.08 | 2. IO | 2.04 | 2.06 | 2.08 | 2.10 | 2.12 |
| 21 | 2. 12 | 2.14 | 2.16 | 2.18 | 2.20 | 2.14 | 2. 16 | 2.18 | 2.20 | 2.22 |
| 22 | 2.22 | 2.24 | 2.26 | 2.28 | 2.30 | 2.24 | 2.26 | 2.28 | 2.30 | 2.32 |
| 23 | 2.32 | 2.34 | 2.35 | 2.38 | 2.40 | 2.34 | 2.36 | 2.38 | 2.40 | 2.42 |
| 24 | 2.42 | 2.44 | 2.46 | 2.48 | 2.50 | 2.44 | 2.46 | 2.48 | 2.50 | 2.52 |
| 25 | 2.52 | 2.54 | 2.56 | 2.58 | 2.60 | 2.54 | 2.56 | 2.58 | 2.60 | 2.62 |
| 26 | 2.62 | 2.64 | 2.66 | 2.68 | 2.70 | 2.64 | 2.66 | 2.68 | 2.70 | 2.72 |
| 27 | 2.72 | 2.74 | 2.76 | 2.78 | 2.So | 2.74 | 2.76 | 2.78 | 2.80 | 2.82 |
| 28 | 2.82 | 2.84 | 2.86 | 2.88 | 2.90 | 2.55 | 2.87 | 2.89 | 2.91 | 2.93 |
| 29 | 2.92 | 2.94 | 2.96 | 2.98 | 3.00 | 2.95 | 2.97 | 2.99 | 3.01 | 3.03 |
| 30 | 3.02 | 3.04 | 3.06 | 3.08 | 3.10 | 3.05 | 3.07 | 3.09 | 3.11 | 3. 13 |
| 31 | 3.12 | 3.14 | 3.16 | 3.18 | 3.20 | 3.15 | 3.17 | 3.19 | 3.21 | 3.23 |
| 32 | 3.22 | 3.24 | 3.26 | 3.28 | 3.30 | 3.25 | 3.27 | 3.29 | 3.31 | 3.33 |
| 33 | 3.32 | 3.34 | 3.36 | 3.38 | 3.40 | $3 \cdot 35$ | $3 \cdot 37$ | 3.39 | 3.4 I | 3.43 |
| 34 | 3.42 | 3.44 | 3.46 | 3.48 | 3.50 | 3.45 | 3.47 | 3.49 | 3.51 | 3.53 |
| 35 | 3.52 | $3 \cdot 54$ | 3.56 | 3.58 | 3.60 | 3.55 | 3.57 | $3 \cdot 59$ | 3.6 r | 3.63 |

Smithsonian Tableb.

Table 45.

## REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE. THE CORRECTION IS TO BE SUBTRACTED

|  | HEIGHT OF THE BAROMETER 630 mm . |  |  |  |  | height of tile baroneter 635 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm. | min. | mm. | mm . | mm . | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 |
| 1 | . 10 | . 12 | . 14 | . 16 | . 19 | . 10 | . 12 | . 15 | .17 | . 19 |
| 2 | . 21 | . 23 | . 25 | . 27 | . 29 | . 21 | . 23 | . 25 | . 27 | . 29 |
| 3 | . 31 | . 33 | . 35 | . 37 | . 39 | . 31 | . 33 | . 35 | . 37 | . 39 |
| 4 | . 41 | . 43 | . 45 | . 47 | . 49 | . 41 | . 44 | . 46 | .48 | . 50 |
| 5 | 0.51 | 0.53 | 0.56 | 0.58 | 0.60 | 0. 52 | 0. 54 | 0.56 | 0.58 | 0.60 |
| 6 | . 62 | . 64 | . 66 | . 68 | . 70 | . 62 | . 64 | . 66 | . 68 | . 70 |
| 7 | .72 | .74 | . 76 | . 78 | . 80 | . 73 | .75 | .77 | . 79 | . 81 |
| 8 | . 82 | . 84 | . 86 | . 88 | . 90 | . 83 | . 85 | . 87 | . 89 | .91 |
| 9 | .92 | . 95 | . 97 | . 99 | I.OI | . 93 | . 95 | . 97 | . 99 | 1.02 |
| 10 | 1.03 | I. 05 | 1.07 | 1.09 | I.II | 1.04 | 1.06 | 1.08 | I. 10 | I. 12 |
| I I | I. 13 | I. 15 | 1.17 | 1. 19 | 1.21 | 1.14 | I. 16 | I. 18 | 1.20 | 1.22 |
| 12 | 1.23 | I. 25 | 1.27 | 1.29 | 1.31 | 1.24 | I. 26 | 1.28 | 1.30 | 1.33 |
| 13 | I. 34 | I. 36 | 1.38 | 1.40 | 1.42 | 1.35 | I. 37 | 1.39 | 1.41 | 1.43 |
| 14 | I. 44 | 1. 46 | I. 48 | 1. 50 | 1.52 | I. 45 | I. 47 | 1.49 | I. 51 | I. 53 |
| 15 | I. 54 | I. 56 | I. 58 | 1.60 | 1.62 | 1.55 | I. 57 | 1.59 | I.6I | 1.63 |
| 16 | 1.64 | 1.66 | 1.68 | 1.70 | 1.72 | 1.66 | 1.68 | 1.70 | 1.72 | 1.74 |
| 17 | 1. 74 | 1. 77 | 1.79 | I. 81 | 1.83 | 1. 76 | 1.78 | I. So | I. 82 | 1.84 |
| 18 | 1.85 | 1.87 | I. 89 | 1.91 | 1.93 | I. 86 | 1.83 | 1.90 | 1.92 | 1.94 |
| 19 | I. 95 | 1.97 | 1.99 | 2.01 | 2.03 | 1. 96 | 1.99 | 2.01 | 2.03 | 2.05 |
| 20 | 2.05 | 2.07 | 2.09 | 2.11 | 2.13 | 2.07 | 2.09 | 2.11 | 2.13 | 2.15 |
| 2 I | 2.15 | 2.17 | 2.19 | 2.21 | 2.24 | 2.17 | 2.19 | 2.21 | 2.23 | 2.25 |
| 22 | 2.26 | 2.28 | 2.30 | 2.32 | 2.34 | 2.27 | 2.29 | 2.31 | 2.34 | 2.36 |
| 23 | 2.36 | 2.38 | 2.40 | 2.42 | 2.44 | 2.38 | 2.40 | 2.42 | 2.44 | 2.46 |
| 24 | 2.46 | 2.48 | 2.50 | 2.52 | 2.54 | 2.48 | 2.50 | 2.52 | 2.54 | 2.56 |
| 25 | 2.56 | 2.58 | 2.60 | 2.62 | 2.64 | 2.58 | 2.60 | 2.62 | 2.64 | 2.66 |
| 26 | 2.66 | 2.68 | 2.70 | 2.73 | 2.75 | 2.69 | 2.71 | 2.73 | 2.75 | 2.77 |
| 27 | 2.75 | 2.79 | 2.81 | 2.83 | 2.85 | 2.79 | 2.81 | 2.83 | 2.85 | 2.87 |
| 2 S | 2.87 | 2.89 | 2.91 | 2.93 | 2.95 | 2.89 | 2.91 | 2.93 | 2.95 | 2.97 |
| 29 | 2.97 | 2.99 | 3.01 | 3.03 | 3.05 | 2.99 | 3.01 | 3.03 | 3.05 | 3.08 |
| 30 | 3.07 | 3.09 | 3. II | 3. 13 | 3. 15 | 3.10 | 3. 12 | 3.14 | 3.16 | 3.18 |
| 31 | 3.17 | 3.19 | 3.21 | 3.23 | 3.25 | 3.20 | 3.22 | 3.24 | 3.26 | 3.25 |
| 32 | 3.28 | 3.30 | 3.32 | 3.34 | 3.36 | 3.30 | 3.32 | 3.34 | $3 \cdot 36$ | 3.38 |
| 33 | 3.38 | 3.40 | 3.42 | 3.44 | 3.46 | 3.40 | 3.42 | 3.44 | 3.47 | 3.49 |
| 34 | 3.48 | 3.50 | 3.52 | 3.54 | 3.56 | 3.51 | 3.53 | 3.55 | 3.57 | 3.59 |
| 35 | 3.58 | 3.60 | 3.62 | 3.64 | 3.66 | 3.6 I | 3.63 | 3.65 | 3.67 | 3.69 |

for temperatures above $0^{\circ}$ Centigrade, the correction is to be subtracted.

|  | IIEIGIIT OF THE BAROMETER 640 mm. |  |  |  |  | HEIGIT OF THE BAROMETER 645 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | $0 \% 2$ | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm . | mm. | mm. | mm. | mm. | mm. | mm. | mm . | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 |
| 1 | . 10 | . 13 | . 15 | . 17 | . 19 | . 11 | . 13 | . 15 | .17 | . 19 |
| 2 | . 21 | . 23 | .25 | . 27 | . 29 | . 21 | . 23 | . 25 | . 27 | . 29 |
| 3 | . 31 | . 33 | . 36 | . 38 | . 40 | - 32 | - 34 | . 36 | . 38 | . 40 |
| 4 | . 42 | . 44 | .46 | . 48 | . 50 | .42 | . 44 | .46 | .48 | . 51 |
| 5 | 0.52 | 0.54 | 0.56 | 0.59 | 0.6I | 0.53 | 0. 55 | 0.57 | 0.59 | 0.61 |
| 6 | . 63 | . 65 | . 67 | . 69 | .71 | . 63 | . 65 | . 67 | . 69 | . 72 |
| 7 | .73 | . 75 | . 77 | . 79 | .8I | . 74 | .76 | . 78 | . So | . 82 |
| 8 | . 84 | . 86 | . 88 | . 90 | . 92 | . 84 | . 86 | . 88 | . 90 | . 93 |
| 9 | . 94 | .96 | .98 | 1.00 | 1.02 | . 95 | . 97 | . 99 | I.OI | 1.03 |
| 10 | 1.04 | 1.06 | 1.09 | 1.11 | I. 13 | 1.05 | 1.07 | 1.09 | I. 12 | I. 14 |
| 11 | I. 15 | I. 17 | 1.19 | I. 21 | 1.23 | 1. 16 | I. 18 | 1.20 | 1.22 | 1.24 |
| 12 | 1.25 | 1.27 | I. 29 | 1.31 | I. 34 | 1.26 | I. 28 | I. 30 | 1.32 | I. 35 |
| 13 | 1.36 | 1.38 | 1.40 | I. 42 | 1.44 | 1.37 | I. 39 | I. 41 | 1.43 | 1.45 |
| 14 | 1.46 | 1.48 | I. 50 | 1.52 | 1.54 | 1.47 | I. 49 | I. 51 | 1.53 | I. 56 |
| 15 | 1.56 | 1. 59 | 1.61 | 1. 63 | 1. 65 | I. 58 | I. 60 | I. 62 | I. 64 | 1.66 |
| 16 | 1.67 | 1.69 | 1.71 | 1.73 | 1.75 | 1.68 | 1.70 | 1.72 | 1.74 | 1.77 |
| 17 | 1.77 | 1.79 | 1.81 | 1.83 | 1.86 | 1.79 | 1.81 | I. $\mathrm{S}_{3}$ | I. 85 | I. 87 |
| 18 | 1.88 | 1.90 | 1.92 | 1.94 | 1.96 | 1. 89 | 1.91 | 1.93 | 1.95 | I. 97 |
| 19 | 1.98 | 2.00 | 2.02 | 2.04 | 2.06 | 2.00 | 2.02 | 2.04 | 2.06 | 2.08 |
| 20 | 2.08 | 2.10 | 2.13 | 2. 15 | 2. 17 | 2.10 | 2.12 | 2. I4 | 2.16 | 2.18 |
| 21 | 2.19 | 2.21 | 2.23 | 2.25 | 2.27 | 2.20 | 2.23 | 2.25 | 2.27 | 2.29 |
| 22 | 2.29 | 2.31 | 2.33 | 2.35 | 2.37 | 2.31 | 2.33 | 2.35 | 2.37 | 2.39 |
| 23 | 2.40 | 2.42 | 2.44 | 2.46 | 2.48 | 2.41 | 2.43 | 2.46 | 2.48 | 2.50 |
| 24 | 2.50 | 2.52 | 2.54 | 2.56 | 2.58 | 2.52 | 2.54 | 2.56 | 2.58 | 2.60 |
| 25 | 2.60 | 2.62 | 2.64 | 2.66 | 2.69 | 2.62 | 2.64 | 2.66 | 2.69 | 2.71 |
| 26 | 2.71 | 2.73 | 2.75 | 2.77 | 2.79 | 2.73 | 2.75 | 2.77 | 2.79 | 2.81 |
| 27 | 2.81 | 2.83 | 2.85 | 2.87 | 2.89 | 2.83 | 2.85 | 2.87 | 2.89 | 2.92 |
| 28 | 2.91 | 2.93 | 2.95 | 2.98 | 3.00 | 2.94 | 2.96 | 2.98 | 3.00 | 3.02 |
| 29 | 3.02 | 3.04 | 3.06 | 3.08 | 3.10 | 3.04 | 3.06 | 3.08 | 3.10 | 3.12 |
| 30 | 3.12 | 3.14 | 3.16 | 3.18 | 3.20 | 3.14 | 3.17 | 3.19 | 3.21 | 3.23 |
| 31 | 3.22 | 3.24 | 3.27 | 3.29 | $3 \cdot 3 \mathrm{I}$ | 3.25 | 3.27 | 3.29 | $3 \cdot 31$ | 3.33 |
| 32 | 3.33 | $3 \cdot 35$ | 3.37 | 3.39 | 3.41 | 3.35 | 3.37 | 3.39 | 3.42 | 3.44 |
| 33 | 3.43 | 3.45 | 3.47 | 3.49 | 3.51 | 3.46 | 3.48 | 3.50 | 3.52 | 3.54 |
| 34 | 3.53 | 3.55 | 3.58 | 360 | 3.62 | 3.56 | 3.58 | 3.60 | 3.62 | 3.64 |
| 35 | 3.64 | 3.66 | 3.68 | 3.70 | 3.72 | 3.67 | 3.69 | 3.71 | 3.73 | 3.75 |

Smithionian Tables.

Table 45.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | heigilt of the barometfr 650 mm . |  |  |  |  | helchit of the barometer 655 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0:0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0\% 6 | 0.8 |
| c. | minl. | mm. | mm. | mm. | mm. | mm . | mm. | mm. | mm. | 11 m . |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.08 | 0.00 | 0.02 | 0.04 | 0.06 | 0.09 |
| I | . 11 | . 13 | . 15 | . 17 | . 19 | . I I | . 13 | . 15 | . 17 | . 19 |
| 2 | . 21 | . 23 | . 25 | . 28 | . 30 | . 21 | . 24 | . 26 | . 2 S | .30 |
| 3 | . 32 | . 34 | . 36 | . 38 | . 40 | .32 | . 34 | . 36 | . 39 | . 41 |
| 4 | .42 | . 45 | . 47 | .49 | . 51 | . 43 | . 45 | . 47 | . 49 | . 51 |
| 5 | 0.53 | 0.55 | 0.57 | 0.59 | 0.62 | 0.53 | 0.56 | 0.58 | 0.60 | 0.62 |
| 6 | . 64 | . 66 | . 68 | . 70 | . 72 | . 64 | . 66 | . 68 | . 71 | . 73 |
| 7 | . 74 | .76 | .78 | .8I | . 83 | . 75 | . 77 | . 79 | . 81 | . 83 |
| 8 | . 85 | . 87 | . 89 | .91 | . 93 | . 55 | . 88 | . 90 | . 92 | . 94 |
| 9 | . 95 | .98 | 1.00 | 1.02 | I. 04 | .96 | . 98 | 1.00 | 1.03 | 1.05 |
| 10 | 1. 06 | 1.08 | I. 10 | I. 12 | 1.14 | 1.07 | 1.09 | I. II | I. 13 | 1.15 |
| 11 | I. 17 | 1.19 | 1.21 | 1.23 | 1. 25 | 1.17 | 1.20 | 1.22 | 1.24 | 1.26 |
| 12 | I. 27 | 1.29 | 1.31 | I. 34 | 1. 36 | 1.28 | 1.30 | I. 32 | 1.35 | 1.37 |
| 13 | I. 38 | 1.40 | 1.42 | I. 44 | 1.46 | I. 39 | I. 41 | I. 43 | I. 45 | 1.47 |
| 14 | I. 48 | I. 50 | I. 53 | 1. 55 | I. 57 | I. 49 | I. 52 | I. 54 | 1.56 | I. 58 |
| 15 | I. 59 | I.6I | 1. 63 | 1. 65 | 1.67 | I. 60 | I. 62 | 1.64 | 1. 66 | 1. 69 |
| 16 | I. 69 | 1.72 | 1.74 | 1.76 | 1.75 | 1.71 | 1.73 | 1.75 | 1.77 | 1.79 |
| 17 | I. 80 | 1.82 | 1.84 | I. 86 | 1. 88 | I. $\mathrm{SI}_{1}$ | I. $\mathrm{S}_{4}$ | 1.86 | 1.88 | 1.90 |
| 18 | 1.91 | I. 93 | 1.95 | 1.97 | I. 99 | 1.92 | 1.94 | 1.96 | I. 98 | 2.01 |
| 19 | 2.01 | 2.03 | 2.05 | 2.07 | 2.10 | 2.03 | 2.05 | 2.07 | 2.09 | 2.11 |
| 20 | 2.12 | 2.14 | 2.16 | 2.18 | 2.20 | 2.13 | 2.15 | 2.18 | 2.20 | 2.22 |
| 21 | 2.22 | 2.24 | 2.26 | 2.29 | 2.31 | 2.24 | 2.26 | 2.28 | 2.30 | 2.32 |
| 22 | 2.33 | 2.35 | 2.37 | 2.39 | 2.41 | 2.35 | 2.37 | 2.39 | 2.41 | 2.43 |
| 23 | 2.43 | 2.45 | 2.47 | 2.50 | 2.52 | 2.45 | 2.47 | 2.49 | 2.52 | 2.54 |
| 24 | 2.54 | 2.56 | 2.58 | 2.60 | 2.62 | 2.56 | 2.58 | 2.60 | 2.62 | 2.64 |
| 25 | 2.64 | 2.66 | 2.69 | 2.71 | 2.73 | 2.66 | 2.68 | 2.71 | 2.73 | 2.75 |
| 26 | 2.75 | 2.77 | 2.79 | 2.81 | 2.83 | 2.77 | 2.79 | 2.81 | 2.83 | 2.55 |
| 27 | 2.85 | 2.87 | 2.90 | 2.92 | 2.94 | 2.58 | 2.90 | 2.92 | 2.94 | 2.96 |
| 28 | 2.96 | 2.98 | 3.00 | 3.02 | 3.04 | 2.98 | 3.00 | 3.02 | 3.05 | 3.07 |
| 29 | 3.06 | 3.08 | 3.11 | 3.13 | 3.15 | 3.09 | 3.11 | 3.13 | 3.15 | 3.17 |
| 30 | 3.17 | 3.19 | 3.21 | 3.23 | 3.25 | 3.19 | 3.21 | 3.24 | 3.26 | 3.28 |
| 31 | 3.27 | $3 \cdot 30$ | 3.32 | 3.34 | $3 \cdot 36$ | $3 \cdot 30$ | $3 \cdot 32$ | 3.34 | $3 \cdot 36$ | $3 \cdot 38$ |
| 32 | $3 \cdot 38$ | 3.40 | 3.42 | 3.44 | 3.46 | 3.41 | $3 \cdot 43$ | 3.45 | 3.47 | 3.49 |
| 33 | 3.48 | 3.51 | 3.53 | 3.55 | 3.57 | 3.51 | 3.53 | 3.55 | 3.57 | 3.60 |
| 34 | 3.59 | 3.61 | 3.63 | 3.65 | 3.67 | 3.62 | 3.64 | 3.66 | 3.68 | 3.70 |
| 35 | 3.69 | 3.71 | 3.74 | 3.76 | 3.78 | 3.72 | 3.74 | 3.76 | 3.79 | 3.81 |

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Table 45.
REDUUTION OF THE BAROMETER TO STANDARD TEMPERATURE.
METRIC MEASURES.
FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | neIGHT OF THE BAROMETER 660 mm . |  |  |  |  | height of the barometer 665 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0. 4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | 1 mm . | mm. | 1mm. | mm. | mm. | mm. | nm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.06 | 0.09 | 0.00 | 0.02 | 0.04 | 0.07 | 0.09 |
| I | . II | . 13 | . 15 | . 17 | . 19 | . 11 | . 13 | . 15 | .17 | . 20 |
| 2 | . 22 | . 24 | . 26 | . 28 | . 30 | . 22 | . 24 | . 26 | . 28 | . 30 |
| 3 | - 32 | . 34 | .37 | . 39 | . 41 | . 33 | . 35 | . 37 | . 39 | . 41 |
| 4 | . 43 | . 45 | . 47 | . 50 | . 52 | . 43 | . 46 | .48 | . 50 | . 52 |
| 5 | 0.54 | 0.56 | 0.58 | 0.60 | 0.62 | 0.54 | 0.56 | 0.59 | 0.61 | 0.63 |
| 6 | . 65 | . 67 | . 69 | . 71 | . 73 | . 65 | . 67 | . 69 | . 72 | . 74 |
| 7 | . 75 | . 78 | . 80 | . 82 | . 84 | . 76 | . 78 | . 80 | . 82 | . 85 |
| 8 | . 86 | . 88 | . 90 | . 93 | . 95 | . 87 | . 89 | . 91 | . 93 | . 95 |
| 9 | . 97 | . 99 | I. OI | I. 03 | 1.05 | .98 | 1.00 | 1.02 | 1.04 | 1.06 |
| 10 | 1.08 | I. 10 | I. 12 | I. 14 | 1.16 | 1.08 | I. 11 | I. 13 | 1.15 | 1.17 |
| II | I. 18 | I. 21 | 1.23 | 1.25 | 1.27 | I. 19 | 1.21 | 1.24 | I. 26 | 1. 28 |
| 12 | 1.29 | 1.31 | I. 33 | 1. 36 | 1. 38 | 1.30 | I. 32 | I. 34 | 1.37 | 1.39 |
| 13 | 1.40 | 1.42 | I. 44 | 1.46 | 1.48 | 1.41 | 1. 43 | I. 45 | 1.47 | I. 50 |
| 14 | 1.51 | I. 53 | L. 55 | 1.57 | 1. 59 | I. 52 | 1. 54 | I. 56 | 1.58 | 1.60 |
| 15 | 1.6 1 | 1.63 | 1. 66 | 1.68 | 1.70 | 1.63 | 1.65 | 1.67 | 1.69 | 1.71 |
| 16 | 1.72 | 1.74 | 1.76 | 1.78 | I. 81 | 1.73 | I. 76 | 1.78 | I. So | 1.82 |
| 17 | $1 . \mathrm{S}_{3}$ | 1.85 | 1.87 | 1.89 | 1.91 | 1. 84 | 1.86 | 1.88 | 1.91 | 1.93 |
| 18 | 1.93 | 1.96 | 1.98 | 2.00 | 2.02 | 1.95 | 1.97 | 1.99 | 2.01 | 2.04 |
| 19 | 2.04 | 2.06 | 2.08 | 2.11 | 2.13 | 2.06 | 2.08 | 2.10 | 2.12 | 2.14 |
| 20 | 2.15 | 2.17 | 2. 19 | 2.2 I | 2.23 | 2.17 | 2.19 | 2.21 | 2.23 | 2.25 |
| 21 | 2.26 | 2.28 | 2.30 | 2.32 | 2.34 | 2.27 | 2.29 | 2.32 | 2.34 | 2.36 |
| 22 | 2.36 | 2.38 | 2.41 | 2.43 | 2.45 | 2.38 | 2.40 | 2.42 | 2.45 | 2.47 |
| 23 | 2.47 | 2.49 | 2.51 | 2.53 | 2.56 | 2.49 | 2.51 | 2.53 | 2.55 | 2.57 |
| 24 | 2.58 | 2.60 | 2.62 | 2.64 | 2.66 | 2.60 | 2.62 | 2.64 | 2.66 | 2.68 |
| 25 | 2.68 | 2.71 | 2.73 | 2.75 | 2.77 | 2.70 | 2.73 | 2.75 | 2.77 | 2.79 |
| 26 | 2.79 | 2.81 | 2.83 | 2.85 | 2.88 | 2.81 | 2.83 | 2.85 | 2.88 | 2.90 |
| 27 | 2.90 | 2.92 | 2.94 | 2.96 | 2.98 | 2.92 | 2.94 | 2.96 | 2.98 | 3.01 |
| 28 | 3.00 | 3.03 | 3.05 | 3.07 | 3.09 | 3.03 | 3.05 | 3.07 | 3.09 | 3.11 |
| 29 | 3.11 | 3.13 | 3.15 | 3.18 | 3.20 | 3.13 | 3.16 | 3.18 | 3.20 | 3.22 |
| 30 | 3.22 | 3.24 | 3.26 | 3.28 | 3.30 | 3.24 | 3.26 | 3.29 | 3.31 | 3.33 |
| 31 | 3.32 | 3.35 | 3.37 | 3.39 | 3.41 | $3 \cdot 35$ | $3 \cdot 37$ | 3.39 | 3.41 | 3.44 |
| 32 | 3.43 | 3.45 | 3.47 | 3.49 | 3.52 | 3.46 | 3.48 | 3.50 | 3.52 | 3.54 |
| 33 | 3.54 | 356 | 3.58 | 3.60 | 3.62 | 3.56 | 3.59 | 3.61 | 3.63 | 3.65 |
| 34 | 3.64 | 3.67 | 3.69 | 3.71 | 3.73 | 3.67 | 3.69 | 3.71 | 3.74 | 3.76 |
| 35 | 3.75 | 3.77 | 3.79 | 3.81 | 3.84 | 3.78 | 3.80 | 3.82 | 3.84 | 3.86 |

Bmithsonian tableg.

Table 45.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE METRIC MEASURES.
for temperatures above $0^{\circ}$ centigrade, the correction is to be subtracted.

|  | HEIGIT OF THE B.AROMETER$670 \mathrm{~mm} .$ |  |  |  |  | HEIGHT OF THE BAROMETER 675 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | 111 ml . | 1 mm . | mm. | mm . | mm. | mm. | mm . | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.07 | 0.09 | 0.00 | 0.02 | 0.04 | 0.07 | 0.09 |
| I | . II | . 13 | . 15 | . 18 | . 20 | . I I | . 13 | . 15 | . 18 | . 20 |
| 2 | . 22 | . 24 | . 26 | . 28 | -31 | . 22 | . 24 | . 26 | . 29 | -3I |
| 3 | . 33 | . 35 | . 37 | - 39 | . 42 | . 33 | . 35 | . 37 | . 40 | . 42 |
| 4 | . 44 | . 46 | .48 | . 50 | . 53 | . 44 | .46 | . 48 | . 51 | . 53 |
| 5 | 0.55 | 0.57 | 0.59 | 0.61 | 0.63 | 0.55 | 0.57 | 0.60 | 0.62 | 0.64 |
| 6 | . 66 | . 68 | . 70 | . 72 | . 74 | . 66 | . 68 | . 71 | . 73 | . 75 |
| 7 | . 77 | . 79 | .SI | . 83 | . 85 | . 77 | . 79 | . 82 | . 84 | . 86 |
| 8 | . 87 | .90 | . 92 | . 94 | . 96 | . 88 | . 90 | . 93 | . 95 | . 97 |
| 9 | .98 | I.OI | 1. 03 | 1.05 | 1.07 | . 99 | I.OI | 1.04 | 1.06 | 1.08 |
| 10 | 1.09 | I. II | 1.14 | 1. 16 | I. 18 | 1.10 | I. 12 | 1.14 | I. 17 | I. 19 |
| 11 | 1.20 | 1.22 | I. 25 | 1.27 | I. 29 | I. 21 | I. 23 | 1.25 | I. 28 | 1.30 |
| 12 | 1. 31 | 1.33 | 1.35 | 1.38 | I. 40 | 1.32 | I. 34 | I. 36 | I. 39 | 1.41 |
| 13 | 1.42 | 1.44 | I. 46 | I. 49 | 1.51 | I. 43 | I. 45 | I. 47 | I. 50 | 1.52 |
| 14 | I. 53 | I. 55 | I. 57 | 1.59 | 1.62 | I. 54 | 1. 56 | 1.58 | 1.6I | 1.63 |
| 15 | 1. 64 | 1. 66 | 1. 68 | 1.70 | I. 72 | 1.65 | 1.67 | 1.69 | 1.72 | I. 74 |
| 16 | 1.75 | 1.77 | 1.79 | 1.81 | 1.83 | 1.76 | 1.78 | 1.80 | 1.83 | I. 85 |
| 17 | 1.86 | 1.88 | 1.90 | 1.92 | 1.94 | 1.87 | 1.89 | 1.91 | 1.94 | 1.96 |
| 18 | 1.96 | 1.99 | 2.01 | 2.03 | 2.05 | 1.98 | 2.00 | 2.02 | 2.04 | 2.07 |
| 19 | 2.07 | 2.09 | 2.12 | 2.14 | 2.16 | 2.09 | 2. II | 2.13 | 2.15 | 2.18 |
| 20 | 2. IS | 2.20 | 2.23 | 2.25 | 2.27 | 2.20 | 2.22 | 2.24 | 2.26 | 2.29 |
| 21 | 2.29 | 2.31 | 2.33 | 2.36 | 2.38 | 2.31 | 2.33 | 2.35 | 2.37 | 2.39 |
| 22 | 2.40 | 2.42 | 2.44 | 2.46 | 2.49 | 2.42 | 2.44 | 2.46 | 2.48 | 2.50 |
| 23 | 2.51 | 2.53 | 2.55 | 2.57 | 2.59 | 2.53 | 2.55 | 2.57 | 2.59 | 2.61 |
| 24 | 2.62 | 2.64 | 2.66 | 2.68 | 2.70 | 2.64 | 2.66 | 2.68 | 2.70 | 2.72 |
| 25 | 2.72 | 2.75 | 2.77 | 2.79 | 2.81 | 2.74 | 2.77 | 2.79 | $2 . S 1$ | 2.83 |
| 26 | 2.83 | 2.85 | 2.88 | 2.90 | 2.92 | 2.85 | 2.88 | 2.90 | 2.92 | 2.94 |
| 27 | 2.94 | 2.96 | 2.98 | 3.01 | 3.03 | 2.96 | 2.99 | 3.01 | 3.03 | 3.05 |
| 28 | 3.05 | 3.07 | 3.09 | 3.11 | 3.14 | 3.07 | 3.09 | 3.12 | 3.14 | 3.16 |
| 29 | 3.16 | 3.IS | 3.20 | 3.22 | 3.24 | 3.18 | 3.20 | 3.23 | 3.25 | 3.27 |
| 30 | 3.27 | 3.29 | 3.3: | 3.33 | 3.35 | 3.29 | 3.31 | 3.33 | 3.36 | $3 \cdot 38$ |
| 3 I | $3 \cdot 37$ | 3.40 | 3.42 | 3.44 | 3.46 | 3.40 | 3.42 | 3.44 | 3.47 | 3.49 |
| 33 | 3.48 | 3.50 | 3.53 | 3.55 | 3.57 | 3.51 | 3.53 | 3.55 | 3.57 | 3.60 |
| 33 | 3.59 | 3.61 | 3.63 | 3.66 | 3.68 | 3.62 | 3.64 | 3.66 | 3.68 | 3.71 |
| 34 | 3.70 | 3.72 | 3.74 | 3.76 | 3.79 | 3.73 | 3.75 | 3.77 | 3.79 | 3.81 |
| 35 | 3.8 I | 3.83 | 3.85 | 3.87 | 3.89 | 3.84 | 3.86 | 3.88 | 3.90 | 3.92 |

Table 45.

## REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

METRIC MEASURES.
FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF THE BAROMETER 680 mm . |  |  |  |  | heigiit of the barometer 685 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mim. | mm . | mm. | mm. | mm. | mm . | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.04 | 0.07 | 0.09 | 0.00 | 0.02 | 0.04 | 0.07 | 0.09 |
| I | . 11 | . 13 | . 16 | . 18 | . 20 | . I I | . 13 | . 16 | . 18 | . 20 |
| 2 | . 22 | . 24 | . 27 | . 29 | . 31 | . 22 | . 25 | . 27 | . 29 | . 31 |
| 3 | .33 | . 36 | - $3^{8}$ | . 40 | . 42 | - 34 | . 36 | . 38 | . 40 | . 43 |
| 4 | . 44 | . 47 | . 49 | . 51 | . 53 | . 45 | . 47 | . 49 | . 51 | . 54 |
| 5 | 0.56 | 0.58 | 0.60 | 0.62 | 0.64 | 0.56 | 0.58 | 0.60 | 0.63 | 0.65 |
| 6 | . 67 | . 69 | . 71 | . 73 | . 75 | . 67 | . 69 | . 72 | . 74 | . 76 |
| 7 | .78 | . So | . 82 | . 84 | . 87 | .78 | . 80 | . 83 | . 35 | . 87 |
| 8 | . 59 | .91 | . 93 | . 95 | . 98 | . 89 | . 92 | . 94 | . 96 | . 98 |
| 9 | I. 00 | 1.02 | I. 04 | I. 06 | I. 09 | I.OI | 1.03 | 1.05 | 1.07 | 1.09 |
| 10 | I. I I | I. I3 | I. I5 | 1.18 | 1.20 | I. 12 | I. 14 | I. 16 | I. 18 | 1.21 |
| II | 1.22 | 1.24 | I. 26 | 1.29 | 1.31 | 1.23 | I. 25 | 1.27 | I. 30 | I. 32 |
| 12 | 1.33 | 1.35 | I. 37 | 1.40 | 1.42 | 1.34 | 1.36 | 1.38 | I. 41 | I. 43 |
| 13 | I. 44 | 1.46 | I. 49 | I. 51 | I. 53 | I. 45 | 1.47 | 1. 50 | I. 52 | I. 54 |
| 14 | I. 55 | 1.57 | 1.60 | 1.62 | I. 64 | 1.56 | 1.59 | I.6I | 1.63 | I. 65 |
| 15 | 1. 66 | 1.68 | 1.71 | 1.73 | 1.75 | 1.67 | 1.70 | 1.72 | 1.74 | 1. 76 |
| 16 | 1.77 | 1.79 | 1.82 | I. 84 | I. 86 | 1.79 | 1.81 | I. 83 | I. 85 | I. 87 |
| 17 | 1.88 | 1.91 | 1.93 | I. 95 | 1.97 | 1.90 | 1.92 | I. 94 | I. 96 | I. 99 |
| IS | 1.99 | 2.02 | 2.04 | 2.06 | 2.08 | 2.01 | 2.03 | 2.05 | 2.07 | 2. 10 |
| 19 | 2.10 | 2.13 | 2.15 | 2.17 | 2.19 | 2.12 | 2.14 | 2.16 | 2.19 | 2.21 |
| 20 | 2.21 | 2.24 | 2.26 | 2.28 | 2.30 | 2.23 | 2.25 | 2.27 | 2.30 | 2.32 |
| 21 | 2.32 | 2.35 | 2.37 | 2.39 | 2.41 | 2.34 | 2.36 | 2.39 | 2.41 | 2.43 |
| 22 | 2.43 | 2.46 | 2.48 | 2.50 | 2.52 | 2.45 | 2.47 | 2.50 | 2.52 | 2.54 |
| 23 | 2.54 | 2.57 | 2.59 | 2.61 | 2.63 | 2.56 | 2.59 | 2.61 | 2.63 | 2.65 |
| 24 | 2.66 | 2.68 | 2.70 | 2.72 | 2.74 | 2.67 | 2.70 | 2.72 | 2.74 | 2.76 |
| 25 | 2.77 | 2.79 | 2.81 | 2.83 | 2.95 | 2.79 | 2.81 | 2.83 | 2.85 | 2.87 |
| 26 | 2.88 | 2.90 | 2.92 | 2.94 | 2.96 | 2.90 | 2.92 | 2.94 | 2.96 | 2.99 |
| 27 | 2.99 | 3.01 | 3.03 | 3.05 | 3.07 | 3.01 | 3.03 | 3.05 | 3.07 | 3.10 |
| 28 | 3.10 | 3.12 | 3.14 | 3.16 | 3.18 | 3.12 | 3.14 | 3.16 | 3.18 | 3.21 |
| 29 | 3.21 | 3.23 | 3.25 | 3.27 | 3.29 | 3.23 | 3.25 | 3.27 | 3.30 | 3.32 |
| 30 | 3.32 | $3 \cdot 34$ | $3 \cdot 36$ | 3.38 | 3.40 | 3.34 | 3.36 | 3.38 | 3.41 | 3.43 |
| 31 | 3.43 | 3.45 | 3.47 | 3.49 | 3.51 | 3.45 | 3.47 | 3.49 | 3.52 | 3.54 |
| 32 | 3.54 | 3.56 | 3.58 | 3.60 | 3.62 | 3.56 | 3.58 | 3.61 | 3.63 | 3.65 |
| 33 | 3.64 | 3.67 | 3.69 | 3.71 | 3.73 | 3.67 | 3.69 | 3.72 | 3.74 3 | 3.76 |
| 34 | 3.75 | 3.78 | 3.80 | 3.82 | 3.84 | 3.78 | 3.50 | 3.83 | 3.85 | 3.87 |
| 35 | 3.86 | 3.89 | 3.91 | 3.93 | 3.95 | 3.89 | 3.91 | 3.94 | 3.96 | 3.98 |

Table 45.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.
fOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, the CORRECTION IS TO BE SUBTRACIED.

|  | heIGIIT OF TIIE B MROMETEL: 690 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 695 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached <br> Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm. | mm. | mm. | mm . | mm. | mm . | mm. | mm. | mm . |
| $0{ }^{5}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 |
| 1 | . I I | . 14 | . 16 | . 18 | . 20 | . 11 | . 14 | . 16 | . 18 | . 20 |
| 2 | . 23 | .25 | .27 | .29 | . 32 | .23 | .25 | . 27 | - 30 | . 32 |
| 3 | - 34 | . 36 | .38 | . 41 | . 43 | . 34 | . 36 | . 39 | . 41 | . 43 |
| 4 | . 45 | . 47 | . 50 | . 52 | . 54 | . 45 | . 48 | . 50 | .52 | . 54 |
| 5 | 0.56 | 0.59 | 0.61 | 0.63 | 0.65 | 0.57 | 0.59 | 0.61 | 0.64 | 0.66 |
| 6 | . 68 | . 70 | . 72 | . 74 | . 77 | . 68 | . 70 | .73 | . 75 | . 77 |
| 7 | . 79 | . 81 | . 83 | . 86 | . 88 | . 79 | . 82 | . 84 | . 86 | . 88 |
| 8 | . 90 | . 92 | . 95 | . 97 | . 99 | .91 | . 93 | . 95 | . 98 | 1.00 |
| 9 | I.OI | 1.04 | 1.06 | 1.08 | 1.10 | 1.02 | 1. 04 | I. 07 | 1.09 | I. II |
| 10 | I. 13 | 1.15 | 1.17 | 1.19 | 1.22 | I. 13 | 1. 16 | I. 18 | 1.20 | 1.22 |
| II | 1.24 | 1.26 | 1. 28 | 1.3I | 1.33 | 1.25 | 1.27 | 1.29 | 1.3I | I. 34 |
| 12 | I. 35 | 1.37 | 1.39 | 1.42 | 1.44 | 1.36 | 1.38 | 1.41 | 1.43 | 1.45 |
| 13 | 1.46 | 1.48 | 1.51 | 1.53 | I. 55 | 1.47 | I. 50 | I. 52 | 1.54 | I. 56 |
| 14 | 1.57 | 1.60 | 1.62 | 1.64 | 1.66 | I. 59 | 1.61 | 1.63 | 1.65 | 1.68 |
| 15 | 1.69 | 1.71 | 1.73 | 1.75 | 1.78 | 1.70 | 1.72 | 1.74 | 1.77 | 1.79 |
| 16 | 1.80 | 1.82 | 1. 84 | 1.87 | 1. 89 | 1.81 | 1. $\mathrm{S}_{3}$ | 1.86 | 1. 88 | 1.90 |
| 17 | 1.91 | 1.93 | 1.96 | 1.98 | 2.00 | 1.92 | 1.95 | 1.97 | 1.99 | 2.01 |
| 18 | 2.02 | 2.05 | 2.07 | 2.09 | 2.11 | 2.04 | 2.06 | 2.08 | 2.11 | 2.13 |
| 19 | 2. 13 | 2.16 | 2.18 | 2.20 | 2.22 | 2.15 | 2.17 | 2.20 | 2.22 | 2.24 |
| 20 | 2.25 | 2.27 | 2.29 | 2.31 | 2.34 | 2.26 | 2.29 | 2.31 | 2.33 | 2.35 |
| 21 | 2.36 | 2.38 | 2.40 | 2.43 | 2.45 | 2.38 | 2.40 | 2.42 | 2.44 | 2.47 |
| 22 | 2.47 | 2.49 | 2.52 | 2.54 | 2.56 | 2.49 | 2.51 | 2.53 | 2.56 | 2.58 |
| 23 | 2.58 | 2.60 | 2.63 | 2.65 | 2.67 | 2.60 | 2.62 | 2.65 | 2.67 | 2.69 |
| 24 | 2.69 | 2.72 | 2.74 | 2.76 | 2.78 | 2.71 | 2.74 | 2.76 | 2.78 | 2.80 |
| 25 | 2.81 | 2.83 | 2.85 | 287 | 2.90 | 2.83 | 2.85 | 2.87 | 2.89 | 2.92 |
| 26 | 2.92 | 2.94 | 2.96 | 2.99 | 3.01 | 2.94 | 2.96 | 2.98 | 3.01 | 3.03 |
| 27 | 3.03 | 3.05 | 3.07 | 3.10 | 3.12 | 3.05 | 3.07 | 3.10 | 3.12 | 3.14 |
| 28 | 3.14 | 3.16 | 3.19 | 3.21 | 3.23 | 3.16 | 3.19 | 3.21 | 3.23 | 3.25 |
| 29 | 3.25 | 3.27 | $3 \cdot 30$ | 3.32 | 3.34 | 3.28 | 3.30 | $3 \cdot 32$ | 3.34 | $3 \cdot 37$ |
| 30 | 3.36 | $3 \cdot 39$ | 3.41 | 3.43 | 3.45 | 3.39 | 3.41 | 3.43 | 3.46 | 3.48 |
| 31 | 3.48 | 3.50 | 3.52 | 3.54 | 3.56 | 3.50 | 3.52 | 3.55 | 3.57 | 3.59 |
| 32 | 3.59 | 3.61 | 3.63 | 3.65 | 3.68 | 3.61 | 3.64 | 3.66 | 3.68 | 3.70 |
| $33$ | 3.70 | 3.72 | 3.74 | 3.77 | 3.79 | 3.73 | 3.75 | 3.77 | 3.79 | 3.8! |
| 34 | 3.8 I | 3.83 | 3.85 | 3.88 | 3.90 | 3.84 | 3.86 | 3.88 | 3.90 | 3.93 |
| 35 | 3.92 | 3.94 | 3.97 | 3.99 | 4.01 | 3.95 | 3.97 | 3.99 | 4.02 | 4.04 |

Gmithsonian Tables.
hevuction of the barometer to standard temperature METRIC MEASURES
for temperatures above $0^{\circ}$ centigrade, the correction is to be subtracted.

|  | HEIGHT OF THE BAROMETER 700 mm . |  |  |  |  | IIEIGHT OF THE BAROMETEL 705 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0\%6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm . | mm . | mm . | mm . | mm. | mm. | mm. | mm. | mm. | mm. |
| $0{ }^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 |
| 1 | . 11 | . 14 | . 16 | . 18 | . 21 | . 12 | . 14 | . 16 | . 18 | . 2 I |
| 2 | . 23 | . 25 | . 27 | . 30 | . 32 | . 23 | . 25 | . 28 | .30 | . 32 |
| 3 | . 34 | . 37 | . 39 | . 41 | . 43 | . 35 | . 37 | . 39 | . 41 | . 44 |
| 4 | .46 | . 48 | . 50 | . 53 | . 55 | . 46 | . 48 | . 51 | .53 | . 55 |
| 5 | 0.57 | 0.59 | 0.62 | 0. 64 | 0. 66 | 0.58 | 0.60 | 0.62 | 0.64 | 0.67 |
| 6 | . 69 | . 71 | .73 | .75 | . 78 | . 69 | .71 | . 74 | . 76 | . 78 |
| 7 | . So | . 82 | .85 | . 87 | . 89 | . 81 | .83 | . 85 | . 87 | . 90 |
| 8 | . 91 | . 94 | . 96 | . 98 | 1.00 | . 92 | . 94 | . 97 | . 99 | I. 1.1 |
| 9 | 1. 03 | 1. 05 | 1.07 | 1. 10 | 1.12 | 1.04 | 1.06 | I. 08 | 1.10 | 1. 13 |
| 10 | 1.14 | I. 16 | 1.19 | 1.21 | 1.23 | 1. 15 | 1.17 | 1.20 | 1.22 | 1.24 |
| 11 | 1.26 | 1.28 | 1.30 | 1.32 | 1.35 | 1.26 | 1.29 | 1.31 | 1.33 | 1.36 |
| 12 | 1.37 | I. 39 | I. 42 | 1.44 | 1.46 | 1.38 | 1.40 | I. 43 | 1.45 | 1.47 |
| 13 | 1.48 | 1.51 | I. 53 | 1.55 | 1.57 | 1.49 | I. 52 | I. 54 | I. 56 | 1.59 |
| 14 | 1. 60 | 1.62 | I. 64 | 1.67 | 1.69 | 1.6I | 1. 63 | I. 65 | 1.68 | 1.70 |
| 15 | 1.71 | 1.73 | 1.76 | 1.78 | 1.80 | 1.72 | 1.75 | 1.77 | 1.79 | 1.81 |
| 16 | 1.82 | 1. 85 | 1.87 | 1. 89 | 1. 92 | 1.84 | I. 86 | I. 88 | 1.91 | 1.93 |
| 17 | I. 94 | 1.96 | 1.98 | 2.01 | 2.03 | 1.95 | 1.98 | 2.00 | 2.02 | 2.04 |
| 18 | 2.05 | 2.07 | 2. 10 | 2.12 | 2.14 | 2.07 | 2.09 | 2.11 | 2.14 | 2.16 |
| 19 | 2.17 | 2.19 | 2.21 | 2.23 | 2.26 | 2.18 | 2.20 | 2.23 | 2.25 | 2.27 |
| 20 | 2.28 | 2.30 | 2.32 | 2.35 | 2.37 | 2.30 | 2.32 | 2.34 | 2.36 | 2.39 |
| 21 | 2.39 | 2.42 | 2.44 | 2.46 | 2.48 | 2.41 | 2.43 | 2.46 | 2.48 | 2.50 |
| 22 | 2.51 | 2.53 | 2.55 | 2.57 | 2.60 | 2.52 | 2.55 | 2.57 | 2.59 | 2.62 |
| 23 | 2.62 | 2.64 | 2.67 | 2.69 | 2.71 | 2.64 | 2.66 | 2.68 | 2.71 | 2.73 |
| 24 | 2.73 | 2.76 | 2.78 | 2.80 | 2.82 | 2.75 | 2.78 | 2.80 | 2.82 | 2.84 |
| 25 | 2.85 | 2.8\% | 2.89 | 2.91 | 2.94 | 2.87 | 2.89 | 2.91 | 2.94 | 2.96 |
| 26 | 2.96 | 2.98 | 3.01 | 3.03 | 3.05 | 2.98 | 3.00 | 3.03 | 3.05 | 3.07 |
| 27 | 3.07 | 3.10 | 3.12 | 3.14 | 3.16 | 3.10 | 3.12 | 3.14 | 3.16 | 3.19 |
| 28 | 3.19 | 3.21 | 3.23 | 3.25 | 3.28 | 3.21 | 3.23 | 3.25 | 3.28 | 3.30 |
| 29 | 3.30 | 332 | 3.34 | 3.37 | 3.39 | 3.32 | 3.35 | 3.37 | 3.39 | 3.41 |
| 30 | 3.41 | 3.44 | 3.46 | 3.48 | 3.50 | 3.44 | 3.46 | 3.48 | 3.51 | 3.53 |
| 31 | 3.53 | 3.55 | 3.57 | 3.59 | 3.62 | 3.55 | 3.57 | 3.60 | 3.62 | 3.64 |
| 32 | 3.64 | 3.66 | 3.68 | 3.7 I | 3.73 | 3.66 | 3.69 | 3.71 | 3.73 | 3.76 |
| 33 | 3.75 | 3.77 | 3.80 | 3.82 | 3.84 | 3.78 | 3.80 | 3.82 | 3.85 | 3.87 |
| 34 | 3.87 | 3.89 | 3.91 | 3.93 | 3.96 | 3.89 | 3.92 | 3.94 | 3.96 | 3.98 |
| 35 | 3.98 | 4.00 | 4.02 | 4.05 | 4.07 | 4.01 | 4.03 | 4.05 | 4.07 | 4.10 |

[^26]Table 45.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.
for temperatures above $0^{\circ}$ centigrade, the correction is to be subtracteo.

|  | height of the barometer 710 mm . |  |  |  |  | HEIGHT OF TIIE BAROMETER 715 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached <br> Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0:8 | $0: 0$ | 0.2 | 0\%.4 | 0.6 | 0.8 |
| c. | min. | mm . | mm. | mm. | mm . | mm. | mm. | mm . | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 |
|  | . 12 | . 14 | . 16 | . 19 | . 21 | . 12 | . 14 | . 16 | . 19 | . 21 |
| 2 | . 23 | . 26 | . 28 | .30 | $\cdot 32$ | .23 | . 26 | . 28 | - 30 | . 33 |
| 3 | . 35 | - 37 | - 39 | . 42 | . 44 | $\cdot 35$ | - 37 | . 40 | . 42 | . 44 |
| 4 | . 46 | . 49 | . 51 | . 53 | . 56 | . 47 | . 49 | . 51 | . 54 | . 56 |
| 5 | 0.58 | 0.60 | 0.63 | 0.65 | 0.67 | 0.58 | 0.6I | 0.63 | 0.65 | 0.68 |
| 6 | . 70 | . 72 | . 74 | . 76 | . 79 | . 70 | . 72 | . 75 | . 77 | . 79 |
| 7 | .SI | . 83 | . 86 | . 88 | . 90 | . 82 | . 84 | . 86 | . 99 | . 91 |
| 8 | . 93 | . 95 | . 97 | 1.00 | 1.02 | . 93 | .96 | . 98 | 1.00 | 1.03 |
| 9 | 1.04 | 1.07 | 1.09 | I. 11 | I. 13 | 1.05 | 1.07 | I. 10 | I. 12 | 1.14 |
| 10 | 1.16 | I. 18 | 1.20 | 1.23 | 1.25 | 1.17 | 1. 19 | I. 21 | 1. 24 | 1.26 |
| 11 | 1.27 | 1.30 | 1.32 | I. 34 | 1.37 | 1.28 | 1.3I | 1.33 | 1. 35 | 1.38 |
| 12 | 1.39 | I. 41 | 1.44 | 1.46 | I. 48 | 1.40 | 1.42 | 1.45 | 1.47 | 1.49 |
| 13 | 1.50 | 1.53 | 1. 55 | I. 57 | 1.60 | 1.52 | 1.54 | 1.56 | 1.58 | 1.61 |
| 14 | 1.62 | I. 64 | 1.67 | 1.69 | 1.71 | 1.63 | I. 65 | 1. 68 | 1.70 | 1.72 |
| 15 | 1. 74 | 1.76 | 1.78 | 1.80 | 1. 83 | 1.75 | 1.77 | 1.79 | 1.82 | I. $\mathrm{S}_{4}$ |
| 16 | 1.85 | 1.87 | 1.90 | 1.92 | 1.94 | 1.86 | 1.89 | 1.91 | 1.93 | 1.96 |
| 17 | 1.97 | 1.99 | 2.01 | 2.04 | 2.06 | 1.98 | 2.00 | 2.03 | 2.05 | 2.07 |
| 18 | 2.08 | 2.10 | 2.13 | 2.15 | 2.17 | 2.10 | 2.12 | 2.14 | 2.17 | 2.19 |
| 19 | 2.20 | 2.22 | 2.24 | 2.27 | 2.29 | 2.21 | 2.24 | 2.26 | 2.28 | 2.30 |
| 20 | 2.31 | 2.33 | 2.36 | 2.38 | 2.40 | 2.33 | 2.35 | 2.37 | 2.40 | 2.42 |
| 21 | 2.43 | 2.45 | 2.47 | 2.50 | 2.52 | 2.44 | 2.47 | 2.49 | 2.51 | 2.54 |
| 22 | 2.54 | 2.57 | 2.59 | 2.61 | 2.63 | 2.56 | 2.58 | 2.61 | 2.63 | 2.65 |
| 23 | 2.66 | 2.68 | 2.70 | 2.73 | 2.75 | 2.68 | 2.70 | 2.72 | 2.75 | 2.77 |
| 24 | 2.77 | 2.80 | 2.82 | 2.84 | 2.86 | 2.79 | 2.81 | 2.84 | 2.86 | 2.88 |
| 25 | 2.89 | 2.91 | 2.93 | 2.96 | 2.98 | 2.91 | 2.93 | 2.95 | 2.98 | 3.00 |
| 26 | 3.00 | 3.03 | 3.05 | 3.07 | 3.09 | 3.02 | 3.05 | 3.07 | 3.09 | 3.12 |
| 27 | 3.12 | 3.14 | 3.16 | 3.19 | 3.21 | 3.14 | 3.16 | 3.19 | 3.21 | 3.23 |
| 28 | 3.23 | 3.25 | 3.28 | 3.30 | 3.32 | 3.25 | 3.28 | 3.30 | 3.32 | 3.35 |
| 29 | 3.35 | 3.37 | 3.39 | 3.42 | 3.44 | $3 \cdot 37$ | 3.39 | 3.42 | 3.44 | 3.46 |
| 30 | 3.46 | 3.48 | 3.51 | 3.53 | 3.55 | 3.49 | 3.51 | 3.53 | 3.56 | 3.58 |
| 31 | 3.58 | 3.60 | 3.62 | 3.65 | 3.67 | 3.60 | 3.62 | 3.65 | 3.67 | 3.69 |
| 32 | 3.69 | 3.71 | 3.74 | 3.76 | 3.78 | 3.72 | 3.74 | 3.76 | 3.79 | 3.81 |
| 33 | 3.81 | 3.83 | 3.85 | 3.87 | 3.90 | 3.83 | 3.86 | 3.88 | 3.90 | 3.92 |
| 34 | 3.92 | 3.94 | 3.97 | 3.99 | 4.01 | 3.95 | 3.97 | 3.99 | 4.02 | 4.04 |
| 35 | 4.03 | 4.06 | 4.08 | 4.10 | 4.13 | 4.06 | 4.09 | 4. II | 4.13 | 4.16 |

Smitheonian Tableg.

REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | IEIGHT OF TIIE BAROMETER 720 mm . |  |  |  |  | heigirt of tile barometer 725 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| 0 | mm. | mm. | mm. | mm . | mm. | mm. | mm . | mm. | mm. | mm. |
| $0{ }^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 | 0.00 | 0.02 | 0.05 | 0.07 | 0.09 |
| 1 | 12 | . 14 | . 16 | . 19 | . 21 | . 12 | . I 4 | . 17 | . 19 | . 21 |
| 2 | . 2.4 | . 26 | . 28 | . 31 | . 33 | . 24 | . 26 | . 28 | . 3 I | . 33 |
| 3 | . 35 | . 38 | . 40 | . 42 | . 45 | . 36 | . 38 | . 40 | . 43 | . 45 |
| 4 | . 47 | . 49 | . 52 | . 54 | . 56 | . 47 | . 50 | . 52 | . 54 | . 57 |
| 5 | 0.59 | 0.61 | 0.63 | 0.66 | 0.68 | 0.59 | 0.62 | 0.64 | 0.66 | 0.69 |
| 6 | . 71 | . 73 | . 75 | . 78 | . 80 | . 71 | . 73 | .64 .76 | . 78 | . So |
| 7 | . 82 | . 85 | . 87 | . 89 | . 92 | . $8_{3}$ | . 85 | . 88 | . 90 | . 92 |
| 8 | . 94 | . 96 | . 99 | I. 01 | 1.03 | . 95 | . 97 | . 99 | 1.02 | 1.04 |
| 9 | 1. 06 | 1.08 | I. IO | I. I 3 | I. 15 | 1.06 | I. 09 | I. II | I. 14 | I. 16 |
| 10 | I. 17 | 1.20 | 1.22 | 1.24 | 1.27 | I. IS | I. 21 | I. 23 | 1.25 | 1.28 |
| II | I. 29 | 1.31 | I. 34 | 1. 36 | I. 39 | 1.30 | I. 32 | I. 35 | 1.37 | I. 39 |
| 12 | 1. 41 | I. 43 | I. 46 | I. 48 | 1. 50 | I. 42 | I. 44 | I. 47 | I. 49 | I. 51 |
| 13 | I. 53 | I. 55 | I. 57 | 1. 60 | 1. 62 | I. 54 | I. 56 | 1.58 | I. 61 | 1. 63 |
| 14 | I. 64 | 1.67 | 1.69 | 1.71 | 1. 74 | 1.65 | 1.68 | I. 70 | I. 73 | I. 75 |
| 15 | 1. 76 | 1.78 | 1.81 | 1. 83 | I. 55 | 1.77 | 1.80 | I. 82 | 1. 84 | 1.87 |
| 16 | I. 88 | 1.90 | 1.92 | 1.95 | I. 97 | I. 89 | I.91 | I. 94 | I. 96 | I. 98 |
| 17 | 1.99 | 2.02 | 2.04 | 2.06 | 2.09 | 2.01 | 2.03 | 2.05 | 2.08 | 2.10 |
| 18 | 2. I I | 2. 13 | 2.16 | 2. IS | 2.20 | 2.13 | 2.15 | 2.17 | 2.20 | 2.22 |
| 19 | 2.23 | 2.25 | 2.27 | 2.30 | 2.32 | 2.24 | 2.27 | 2.29 | 2.31 | 2.34 |
| 20 | 2.34 | 2.37 | 2.39 | 2.41 | 2.44 | 2.36 | 2.38 | 2.41 | 2.43 | 2.45 |
| 21 | 2.46 | 2.48 | 2.51 | 2.53 | 2.55 | 2.48 | 2.50 | 2.53 | 2.45 2.5 | 2.45 2.57 |
| 22 | 2.58 | 2.60 | 2.62 | 2.65 | 2.67 | 2.60 | 2.62 | 2.64 | 2.67 | 2.69 |
| 23 | 2.69 | 2.72 | 2.74 | 2.76 | 2.79 | 2.71 | 2.74 | 2.76 | 2.78 | 2.81 |
| 24 | 2.81 | 2.83 | 2.86 | 2.88 | 2.90 | 2.83 | 2.85 | 2.88 | 2.90 | 2.92 |
| 25 | 2.93 | 2.95 | 2.97 | 3.00 | 3.02 | 2.95 | 2.97 | 3.00 | 3.02 |  |
| 26 | 3.04 | 3.07 | 3.09 | 3.11 | 3.14 | 3.07 | 3.09 | 3.11 | 3.14 | 3.16 |
| 27 | 3.16 | 3.18 | 3.21 | 3.23 | 3.25 | 3.18 | 3.21 | 3.23 | 3.25 | 3.28 |
| 28 | 3.28 | 3.30 | 3.32 | 3.35 | 3.37 | 3.30 | 3.32 | 3.35 | 3.37 | 3.39 |
| 29 | 3.39 | 3.42 | 3.44 | 3.46 | 3.49 | 3.42 | 3.44 | 3.46 | 3.49 | 3.51 |
| 30 | 3.51 | 3.53 | 3.56 | 3.58 | 3.60 | 3.53 | 3.56 | 3.58 | 3.50 | 3.63 |
| 3 I | 3.63 | 3.65 | 3.67 | 3.70 | 3.72 | 3.65 | 3.68 | 3.70 | 3.72 | 3.75 |
| 32 | 3.74 | 3.77 | 3.79 | 3.81 | 3.84 | 3.77 | 3.79 | 3.82 | 3.84 | 3.86 |
| 33 | 3.86 | 3.88 | 3.91 | 3.93 | 3.95 | 3.89 | 3.91 | 3.93 | 3.96 | 3.98 |
| 24 | 3.98 | 4.00 | 4.02 | 4.05 | 4.07 | 4.00 | 4.03 | 4.05 | 4.07 | 4.10 |
| 35 | 4.09 | 4. II | 4. I4 | 4.16 | 4. I8 | 4. 12 | 4. 14 | 4.17 | 4.19 | 4.2 I |

Emitmgonian Tableg.

Table 45.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.
for temperatures above $0^{\circ}$ centigrade. the correction is to be subtracteo.

|  | heigirt of tile barometer 730 mm . |  |  |  |  | HIEIGIIT OF THE BAROMETER 735 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer | $0 \%$ | 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm . | mm . | mm . | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0. 10 | 0.00 | 0.02 | 0.05 | 0.07 | O. 10 |
| I | . 12 | . 14 | .17 | . 19 | . 21 | . 12 | . 14 | . 17 | . 19 | . 22 |
| 2 | . 24 | . 26 | . 29 | . 3 I | . 33 | . 24 | . 26 | . 29 | . 31 | . 34 |
| 3 | . 36 | . 38 | . 41 | . 43 | . 45 | . 36 | . 38 | . 41 | . 43 | . 46 |
| 4 | .48 | . 50 | . 52 | . 55 | . 57 | .48 | . 50 | . 53 | . 55 | . 58 |
| 5 | 0.60 | 0.62 | 0.64 | 0.67 | 0.69 | 0.60 | 0.62 | 0.65 | 0.67 | 0.70 |
| 6 | . 7 I | . 74 | . 76 | . 79 | . 81 | .72 | . 74 | . 77 | . 79 | . 82 |
| 7 | . 83 | . 86 | . 88 | .91 | . 93 | . 84 | . 86 | . 89 | .91 | . 94 |
| 8 | . 95 | . 98 | 1.00 | 1.02 | 1.05 | . 96 | .98 | I.OI | 1.03 | 1.06 |
| 9 | 1.07 | I. 10 | I. 12 | I. 14 | I. 17 | 1.08 | I. 10 | I. 13 | 1. 15 | I. 17 |
| 10 | I. 19 | I. 21 | 1.24 | 1.26 | 1.29 | 1.20 | 1. 22 | I. 25 | 1.27 | 1.29 |
| I I | 1.31 | 1.33 | 1. 36 | 1.38 | I. 40 | 1.32 | I. 34 | I. 37 | I. 39 | 1.41 |
| 12 | 1.43 | 1.45 | 1. 48 | I. 50 | I. 52 | I. 44 | I. 46 | I. 49 | I. 51 | 1.53 |
| 13 | 1. 55 | I. 57 | I. 59 | 1. 62 | 1.64 | I. 56 | 1. 58 | I.6I | 1.63 | 1.65 |
| 14 | I. 67 | I. 69 | 1.71 | 1. 74 | 1. 76 | I. 68 | 1.70 | 1.72 | I. 75 | 1.77 |
| 15 | 1.78 | 1.8I | 1.83 | 1. 86 | I. 88 | I. So | 1.82 | 1.84 | I. 87 | 1. 89 |
| 16 | 1.90 | 1.93 | I. 95 | 1.97 | 2.00 | 1.92 | 1.94 | 1.96 | I. 99 | 2.01 |
| 17 | 2.02 | 2.05 | 2.07 | 2.09 | 2.12 | 2.04 | 2.06 | 2.08 | 2.11 | 2. 13 |
| 18 | 2. 14 | 2. 16 | 2. 19 | 2.2 I | 2.23 | 2. 15 | 2. IS | 2.20 | 2.23 | 2.25 |
| 19 | 2.26 | 2.28 | 2.31 | 2.33 | 2.35 | 2.27 | 2.30 | 2.32 | 2.35 | 2.37 |
| 20 | 2.38 | 2.40 | 2.42 | 2.45 | 2.47 | 2.39 | 2.42 | 2.44 | 2.46 | 2.49 |
| 21 | 2.50 | 2.52 | 2.54 | 2.57 | 2.59 | 2.51 | 2.54 | 2.56 | 2.58 | 2.61 |
| 22 | 2.61 | 2.64 | 2.66 | 2.68 | 2.71 | 2.63 | 2.66 | 2.68 | 2.70 | 2.73 |
| 23 | 2.73 | 2.76 | 2.78 | 2.80 | 2.83 | 2.75 | 2.77 | 2.80 | 2.82 | 2.95 |
| 24 | 2.85 | 2.87 | 2.90 | 2.92 | 2.94 | 2.87 | 2.89 | 2.92 | 2.94 | 2.97 |
| 25 | 2.97 | 2.99 | 3.02 | 3.04 | 3.06 | 2.99 | 3.01 | 3.04 | 3.06 | 3.08 |
| 26 | 3.09 | 3.11 | 3.13 | 3.16 | 3.18 | 3.11 | 3.13 | 3.16 | 3.18 | 3.20 |
| 27 | 3.20 | 3.23 | 3.25 | 3.28 | 3.30 | 3.23 | 3.25 | 3.27 | 3.30 | 3.32 |
| 28 | 3.32 | 3.35 | 3.37 | 3.39 | 3.42 | 3.35 | 3.37 | 3.39 | 3.42 | 3.44 |
| 29 | 3.44 | 3.46 | 3.49 | 3.5 I | 3.54 | 3.46 | 3.49 | $3 \cdot 51$ | 3.54 | 3.56 |
| 30 | 3.56 | 3.58 | 3.61 | 3.63 | 3.65 | 3.58 | 3.61 | 3.63 | 3.65 | 3.68 |
| 3 I | 3.68 | 3.70 | 3.72 | 3.75 | 3.77 | 3.70 | 3.73 | 3.75 | 3.77 | 3.80 |
| 32 | 3.79 | 3.82 | 3.84 | 3.87 | 3.89 | 3.82 | 3.84 | 3.87 | 3.89 | 3.92 |
| 33 | 3.91 | 3.94 | 3.96 | 3.98 | 4.01 | 3.94 | 3.96 | 3.99 | 4.01 | 4.03 |
| 34 | 4.03 | 4.05 | 4.08 | 4.10 | 4.12 | 4.06 | 4.08 | 4. II | 4.13 | 4.15 |
| 35 | 4. 15 | 4.17 | 4.20 | 4.22 | 4.24 | 4. IS | 4.20 | 4.22 | 4.25 | 4.27 |

## REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.

METRIC MEASURES.
for temperatures above $0^{\circ}$ Centigrade, the correction is to be subtracted.

|  | height of tile barometer 740 mm . |  |  |  |  | HEIGIIT OF TIIE BAROMETER 745 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer | $0: 0$ | 0.2 | 0.4 | 0.6 | 0.8 | $0 \%$ | 0.2 | 0.4 | 0.6 | $0 \% 8$ |
| c. | mm. | mm. | mm. | mm . | mm . | mm. | mm. | mm . | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0.10 | 0.00 | 0.02 | 0.05 | 0.07 | 0.10 |
| I | . 12 | . 15 | . 17 | . 19 | . 22 | . 12 | . 15 | .17 | . 19 | . 22 |
| 2 | . 24 | . 27 | . 29 | . 31 | . 34 | . 24 | . 27 | .29 | .32 | . 34 |
| 3 | . 36 | - 39 | . 41 | . 44 | . 46 | - 37 | . 39 | . 41 | . 44 | . 46 |
| 4 | .48 | . 51 | . 53 | . 56 | . 58 | . 49 | .51 | . 54 | . 56 | . 58 |
| 5 | 0.60 | 0.63 | o. 65 | 0.68 | 0.70 | 0.61 | 0.63 | 0.66 | 0.68 | 0.71 |
| 6 | . 72 | . 75 | . 77 | . So | . 82 | .73 | . 75 | . 78 | . 80 | . 83 |
| 7 | . 85 | . 87 | . 89 | . 92 | . 94 | . 85 | . 85 | . 90 | . 92 | . 95 |
| 8 | . 97 | . 99 | I. OI | 1. 04 | 1.06 | . 97 | 1.00 | I. 02 | 1.05 | 1.07 |
| 9 | I. 09 | I. II | I. 13 | 1. 16 | I. 18 | 1. 09 | 1. 12 | I. 14 | 1. 17 | 1.19 |
| 10 | 1.21 | 1.23 | I. 26 | 1.28 | 1.30 | 1.22 | 1.24 | I. 26 | I. 29 | 1.31 |
| I I | 1.33 | I. 35 | I. 38 | 1.40 | I. 42 | I. 34 | 1. 36 | 1. 38 | I. 41 | 1.43 |
| 12 | I. 45 | 1.47 | 1.50 | I. 52 | 1.54 | 1. 46 | 1.48 | 1.51 | I. 53 | 1.55 |
| 13 | I. 57 | I. 59 | 1.62 | 1. 64 | 1.66 | I. 58 | 1. 60 | I. 63 | I. 65 | 1.68 |
| 14 | I. 69 | 1.71 | 1.74 | 1. 76 | 1.78 | 1.70 | 1.72 | 1. 75 | 1.77 | 1.80 |
| 15 | I. Sr | 1.83 | 1. 86 | 1. 88 | 1.90 | 1.82 | I. 85 | I. 87 | I. 89 | 1.92 |
| 16 | 1.93 | 1.95 | 1.98 | 2.00 | 2.03 | 1.94 | 1.97 | 1.99 | 2.01 | 2.04 |
| 17 | 2.05 | 2.07 | 2.10 | 2.12 | 2.15 | 2.06 | 2.09 | 2.1 I | 2. I4 | 2. 16 |
| 18 | 2.17 | 2.19 | 2.22 | 2.24 | 2.27 | 2.18 | 2.21 | 2.23 | 2.26 | 2.28 |
| I9 | 2.29 | 2.31 | 2.34 | 2.36 | 2.39 | 2.31 | 2.33 | 2.35 | 2.38 | 2.40 |
| 20 | 2.41 | 2.43 | 2.46 | 2.48 | 2.51 | 2.43 | 2.45 | 2.47 | 2.50 | 2.52 |
| 21 | 2.53 | 2.55 | 2.58 | 2.60 | 2.63 | 2.55 | 2.57 | 2.59 | 2.62 | 2.64 |
| 22 | 2.65 | 2.67 | 2.70 | 2.72 | 2.75 | 2.67 | 2.69 | 2.72 | 2.74 | 2.76 |
| 23 | 2.77 | 2.79 | 2.82 | 2.84 | 2.87 | 2.79 | 2.81 | 2.84 | 2.56 | 2.88 |
| 2.4 | 2.89 | 2.91 | 2.94 | 2.96 | 2.99 | 2.91 | 2.93 | 2.96 | 2.98 | 3.01 |
| 25 | 3.01 | 3.03 | 3.06 | 3.08 | 3.11 | 3.03 | 3.05 | 3.08 | 3.10 | 3.13 |
| 26 | 3.13 | 3.15 | 3.18 | 3.20 | 3.22 | 3.15 | 3.17 | 3.20 | 3.22 | 3.25 |
| 27 | 2. 25 | 3.27 | 3.30 | 3.32 | $3 \cdot 34$ | 3.27 | 3.29 | 3.32 | 3.34 | 3.37 |
| 28 | 3.37 | 3.39 | 3.42 | 3.44 | 3.46 | 3.39 | 3.42 | 3.44 | 3.46 | 3.49 |
| 29 | $3 \cdot 49$ | 3.51 | 3.54 | 3.56 | 3.58 | 3.5I | 3.54 | 3.56 | 3.58 | 3.61 |
| 30 | 3.61 | 3.63 | 3.66 | 3.68 | 3.70 | 3.63 | 3.66 | 3.68 | 3.70 | 3.73 |
| 31 | 3.73 | 3.75 | 3.78 | 3.80 | 3.82 | 3.75 | 3.78 | 3. So | 3.82 | 3.85 |
| 32 | 3.55 | 3.87 | 3.89 | 3.92 | 3.94 | 3.87 | 3.90 | 3.92 | 3.95 | 3.97 |
| 33 | 3.97 | 3.99 | 4.01 | 4.04 | 4.06 | 3.99 | 4.02 | 4 | 4.07 | 4.09 |
| 34 | 4.09 | 4.1 I | 4.13 | 4.16 | 4.18 | 4.11 | 4.14 | 4.16 | 4.19 | 4.21 |
| 35 | 4.2 I | 4.23 | 4.25 | 4.28 | 4.30 | 4.23 | 4.26 | 4.28 | $4.3{ }^{1}$ | 4.33 |

Smithaonian Tables.

Table 45.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE.
METRIC MEASURES.
FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, the CORRECTION IS TO BE SUBTRACTED.

|  | IIEIGHT OF TIIE BAROMETER 750 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 755 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Ther-mom-ter. | $0 \%$ | 0 0.2 | 0.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | $0 \% 6$ | 0.8 |
| c. | milu. | min. | 1 mm . | mm. | mm . | mm. | mm. | min. | nim. | mm. |
| $0{ }^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | O. 10 | 0.00 | 0.02 | 0.05 | 0.07 | O. 10 |
| I | . 12 | . 15 | . 17 | . 20 | . 22 | . 12 | . 15 | . 17 | . 20 | . 22 |
| 2 | . 25 | . 27 | . 29 | . 32 | . 34 | . 25 | . 27 | .30 | . 32 | . 35 |
| 3 | . 37 | . 39 | . 42 | . 44 | . 47 | . 37 | - 39 | . 42 | . 44 | . 47 |
| 4 | . 49 | . 51 | . 54 | .56 | . 59 | . 49 | . 52 | . 54 | . 57 | . 59 |
| 5 | 0.61 | 0.64 | 0.66 | 0.69 | 0.71 | 0.62 | 0. 64 | 0.67 | 0.69 | 0.71 |
| 6 | . 73 | . 76 | . 78 | . $\mathrm{SI}^{\text {I }}$ | . 83 | .74 | . 76 | . 79 | . SI | . 84 |
| 7 | . 86 | . 88 | .91 | . 93 | . 95 | . 86 | . 89 | . 91 | . 94 | . 96 |
| 8 | .98 | 1.00 | 1.03 | 1.05 | 1. 08 | . 99 | I.OI | 1.03 | 1.06 | 1.08 |
| 9 | 1. 10 | I. 13 | I. 15 | I. 17 | I. 20 | I. II | I. I3 | 1. 16 | I. IS | I. 2 I |
| 10 | 1.22 | 1.25 | 1.27 | I. 30 | 1.32 | 1.23 | 1.26 | 1.28 | 1.31 | 1.33 |
| II | 1. 35 | 1.37 | I. 39 | 1.42 | I. 44 | 1. 35 | I. 38 | 1.40 | 1.43 | 1.45 |
| 12 | 1.47 | I. 49 | 1.52 | I. 54 | I. 56 | I. 48 | 1.50 | 1.53 | I. 55 | 1.58 |
| 13 | I. 59 | 1.61 | 1. 64 | 1. 66 | I. 69 | I. 60 | 1.62 | 1.65 | 1.67 | 1.70 |
| 14 | 1.71 | 1.74 | 1. 76 | 1.78 | I. 81 | 1.72 | 1.75 | 1.77 | 1. 80 | 1.82 |
| 15 | 1.83 | I. 86 | 1. 88 | I.91 | I. 93 | 1. 85 | 1.87 | 1.89 | I. 92 | 1.94 |
| 16 | 1.96 | 1.98 | 2.00 | 2.03 | 2.05 | 1.97 | 1.99 | 2.02 | 2.04 | 2.07 |
| 17 | 2.08 | 2.10 | 2.13 | 2.15 | 2.17 | 2.09 | 2.12 | 2.14 | 2.16 | 2.19 |
| I 8 | 2.20 | 2.22 | 2.25 | 2.27 | 2.30 | 2.21 | 2.24 | 2.26 | 2.29 | 2.3 I |
| 19 | 2.32 | 2.34 | 2.37 | 2.39 | 2.42 | 2.34 | 2.36 | 2.38 | 2.41 | 2.43 |
| 20 | 2.44 | 2.47 | 2.49 | 2.52 | 2.54 | 2.46 | 2.48 | 2.51 | 2.53 | 2.56 |
| 2 I | 2.56 | 2.59 | 2.61 | 2.64 | 2.66 | 2.58 | 2.61 | 2.63 | 2.65 | 2.68 |
| 22 | 2.69 | 2.71 | 2.73 | 2.76 | 2.78 | 2.70 | 2.73 | 2.75 | 2.78 | 2.80 |
| 23 | 2.81 | 2.83 | 2.86 | 2.88 | 2.90 | 2.83 | 2.85 | 2.87 | 2.90 | 2.92 |
| 24 | 2.93 | 2.95 | 2.98 | 3.00 | 3.03 | 2.95 | 2.97 | 3.00 | 3.02 | 3.05 |
| 25 | 3.05 | 3.07 | 3.10 | 3.12 | 3.15 | 3.07 | 3.09 | 3.12 | 3.14 | 3.17 |
| 26 | 3. 17 | 3.20 | 3.22 | 3.24 | 3.27 | 3.19 | 3.22 | 3.24 | 3.27 | 3.29 |
| 27 | 3.29 | 3.32 | $3 \cdot 34$ | 3.37 | $3 \cdot 39$ | $3 \cdot 31$ | 3.34 | 3.36 | 3.39 | 3.41 |
| 2 S | 3.41 | 3.44 | 3.46 | 3.49 | 3.51 | 3.44 | 3.46 | 3.49 | 3.51 | 3.53 |
| 29 | 3.54 | 3.56 | 3.58 | 3.61 | 3.63 | 3.56 | 3.58 | 3.61 | 3.63 | 3.66 |
| 30 | 3.66 | 3.68 | 3.71 | 3.73 | 3.75 | 3.68 | 3.71 | 3.73 | 3.75 | 3.78 |
| 31 | 3.78 | 3.80 | 3.83 | 3.85 | 3.87 | 3.80 | 3.83 | 3.55 | 3.88 | 3.90 |
| 32 | 3.90 | 3.92 | 3.95 | 3.97 | 4.00 | 3.92 | 3.95 | 3.97 | 4.00 | 4.02 |
| 33 | 4.02 | 4.04 | 4.07 | 4.09 | 4. 12 | 4.05 | 4.07 | 4.10 | 4.12 | 4. 14 |
| 34 | 4. 14 | 4. 17 | 4.19 | 4.21 | 4.24 | 4.17 | 4.19 | 4.22 | 4.24 | 4.27 |
| 35 | - 4.26 | 4.29 | 4.31 | 4.33 | 4.36 | 4.29 | 4.31 | 4.34 | 4.36 | $4 \cdot 39$ |

Smithsonian Tobles.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | HEIGHT OF TIIE BAROMETER 760 mm . |  |  |  |  | heIght of tile barometer 765 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Ther. mometer. | 0.0 | 0.2 | 0\%.4 | 0.6 | 0.8 | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.02 | 0.05 | 0.07 | 0. 10 | 0.00 | 0.03 | 0.05 | 0.07 | 0. 10 |
| I | . 12 | . 15 | . 17 | . 20 | . 22 | . 13 | . 15 | . 17 | . 20 | . 22 |
| 2 | . 25 | . 27 | . 30 | .32 | - 35 | . 25 | . 27 | . 30 | .32 | . 35 |
| 3 | . 37 | . 40 | .42 | . 45 | . 47 | . 37 | . 40 | . 42 | . 45 | . 47 |
| 4 | . 50 | . 52 | . 55 | . 57 | . 60 | . 50 | . 52 | . 55 | . 57 | . 60 |
| 5 | 0.62 | 0.65 | 0. 67 | 0.69 | 0.72 | 0.62 | 0.65 | 0.67 | 0.70 | 0.72 |
| 6 | . 74 | . 77 | . 79 | . 82 | . 84 | . 75 | . 77 | . 80 | . 82 | . 85 |
| 7 | . 87 | . 89 | . 92 | . 94 | . 97 | . 87 | . 90 | . 92 | . 95 | . 97 |
| 8 | . 99 | I. 02 | I. 04 | 1.07 | 1.09 | 1.00 | 1.02 | 1.05 | 1.07 | I. IO |
| 9 | I. 12 | 1.14 | I. 17 | I. 19 | 1.2I | 1.12 | 1.15 | I. 17 | 1.20 | 1.22 |
| 10 | I. 24 | 1. 26 | 1.29 | 1.31 | 1.34 | 1.25 | 1.27 | 1.30 | 1.32 | 1.35 |
| 11 | 1. 36 | I. 39 | 1.41 | I. 44 | I. 46 | I. 37 | 1.40 | 1.42 | 1.45 | 1.47 |
| 12 | 1. 49 | I. 51 | I. 54 | 1.56 | I. 59 | 1.50 | 1.52 | I. 55 | 1.57 | 1.60 |
| I3 | 1.6I | I. 64 | 1.66 | 1.68 | 1.71 | 1.62 | 1.65 | 1.67 | 1.70 | 1.72 |
| 14 | 1.73 | 1.76 | 1.78 | I. SI | 1.83 | 1.75 | 1.77 | 1. 80 | I. 82 | 1. 85 |
| 15 | 1.86 | 1.88 | I.91 | 1.93 | 1.96 | 1.87 | 1.89 | 1.92 | 1.94 | 1.97 |
| 16 | 1.98 | 2.01 | 2.03 | 2.06 | 2.08 | 1.99 | 2.02 | 2.04 | 2.07 | 2.09 |
| 17 | 2.10 | 2.13 | 2.15 | 2.18 | 2.20 | 2.12 | 2.14 | 2.17 | 2.19 | 2.22 |
| 18 | 2.23 | 2.25 | 2.28 | 2.30 | 2.33 | 2.24 | 2.27 | 2.29 | 2.32 | 2.34 |
| 19 | 2.35 | 2.38 | 2.40 | 2.43 | 2.45 | 2.37 | 2.39 | 2.42 | 2.44 | 2.47 |
| 20 | 2.47 | 2.50 | 2.52 | 2.55 | 2.57 | 2.49 | 2.52 | 2.54 | 2.57 | 2.59 |
| 21 | 2.60 | 2.62 | 2.65 | 2.67 | 2.70 | 2.62 | 2.64 | 2.66 | 2.69 | 2.71 |
| 22 | 2.72 | 2.75 | 2.77 | 2.80 | 2.82 | 2.74 | 2.76 | 2.79 | 2.81 | 2.84 |
| 23 | 2.84 | 2.87 | 2.89 | 2.92 | 2.94 | 2.86 | 2.89 | 2.91 | 2.94 | 2.96 |
| 24 | 2.97 | 2.99 | 3.02 | 3.04 | 3.07 | 2.99 | 3.01 | 3.04 | 3.06 | 3.09 |
| 25 | 3.09 | 3.12 | 3. 14 | 3.16 | 3.19 | 3.11 | 3. 14 | 3.16 | 3.19 | 3.21 |
| 26 | 3.21 | 3.24 | 3.26 | 3.29 | $3 \cdot 31$ | 3.23 | 3.26 | 3.28 | $3 \cdot 3 \mathrm{I}$ | 3.33 |
| 27 | 3.34 | 3.36 | 3.39 | 3.41 | 3.43 | 3.36 | 3.38 | 3.41 | 343 | $3 \cdot 46$ |
| 28 | 3.46 | 3.48 | 3.51 | 3.53 | 3.56 | 3.48 | 3.51 | 3.53 | 3.56 | 3.58 |
| 29 | 3.58 | 3.6 I | 3.63 | 3.66 | 3.68 | 3.61 | 3.63 | 3.66 | 3.68 | 3.70 |
| 30 | 3.71 | 3.73 |  | 3.78 | 3.So | 3.73 | 3.75 | 3.78 | 3.80 | 3.83 |
| 31 | 3.83 | 3.85 | 3.88 | 3.90 | 3.93 | 3.85 | 3.88 | 3.90 | 3.93 | 3.95 |
| 32 | 3.95 | 3.98 | 4.00 | 4.02 | 4.05 | 3.98 | 4.00 | 4.03 | 4.05 | 4.08 |
| 33 | 4.07 | 4. IO | 4.12 | 4. 15 | 4. 17 | 4. 10 | 4.13 | 4.15 | 4. 17 | 4.20 |
| 34 | 4.20 | 4.22 | 4.25 | 4.27 | 4.29 | 4.22 | 4.25 | 4.27 | 4.30 | 4.32 |
| 35 | 4.32 | 4.34 | 4.37 | 4.39 | 4.42 | $4 \cdot 35$ | 4.37 | 4.40 | 4.42 | 4.45 |

## Emithionian Tables.

Table 45.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | height of tile barometer. 770 mm . |  |  |  |  | HEIGHT OF THE BAROMETER 775 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | $0 \%$ | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | mm. | mm. | mm. | mm . | mm. | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.03 | 0.05 | 0.08 | 0. 10 | 0.00 | 0.03 | 0.05 | 0.08 | 0. 10 |
| I | . 13 | . 15 | . 18 | . 20 | . 23 | . 13 | . 15 | . 18 | . 20 | . 23 |
| 2 | . 25 | . 28 | - 30 | -33 | . 35 | . 25 | . 28 | . 30 | -33 | . 35 |
| 3 | . 38 | . 40 | . 43 | . 45 | . 48 | . 38 | . 40 | . 43 | . 46 | . 48 |
| 4 | . 50 | . 53 | . 55 | . 58 | . 60 | . 51 | . 53 | . 56 | .58 | .6I |
| 5 | 0.63 | 0.65 | 0.68 | 0.70 | 0.73 | 0.63 | 0.66 | 0.68 | 0.71 | 0.73 |
| 6 | . 75 | . 78 | . 80 | . 83 | . 85 | . 76 | .78 | . 81 | . 83 | . 86 |
| 7 | . 88 | . 90 | . 93 | . 95 | . 98 | . 89 | .91 | . 94 | . 96 | . 99 |
| 8 | I.OI | 1.03 | 1.06 | 1.08 | I. II | I.OI | 1.04 | 1.06 | 1.09 | I. II |
| 9 | I. 13 | 1.16 | I. 18 | 1.21 | 1.23 | I. 14 | I. 16 | 1. 19 | 1.21 | 1.24 |
| 10 | 1. 26 | 1.28 | 1.31 | I. 33 | 1. 36 | I. 26 | 1.29 | 1.31 | 1.34 | I. 36 |
| II | I. 38 | 1.41 | 1.43 | I. 46 | 1.48 | I. 39 | I. 42 | 1.44 | 1.47 | 1.49 |
| 12 | 1.51 | 1. 53 | 1.56 | 1.58 | 1.6I | 1.52 | 1.54 | 1. 57 | I. 59 | 1.62 |
| 13 | 1.63 | 1.66 | 1.68 | 1.71 | 1.73 | 1.64 | 1.67 | 1.69 | 1.72 | 1.74 |
| 14 | 1.76 | 1.78 | 1.81 | 1.83 | I. 86 | 1.77 | 1.79 | 1.82 | 1.84 | 1.87 |
| 15 | 1.88 | 1.91 | 1.93 | 1.96 | 1.98 | I. 89 | 1.92 | I. 94 | I. 97 | 2.00 |
| 16 | 2.01 | 2.03 | 2.06 | 2.08 | 2.11 | 2.02 | 2.05 | 2.07 | 2.10 | 2.12 |
| 17 | 2.13 | 2.16 | 2.18 | 2.21 | 2.23 | 2. 15 | 2.17 | 2.20 | 2.22 | 2.25 |
| IS | 2.26 | 2.28 | 2.31 | 2.33 | 2.36 | 2.27 | 2.30 | 2.32 | 2.35 | 2.37 |
| 19 | 2.38 | 2.41 | 2.43 | 2.46 | 2.48 | 2.40 | 2.42 | 2.45 | 2.47 | 2.50 |
| 20 | 2.51 | 2.53 | 2.56 | 2.58 | 2.61 | 2.52 | 2.55 | 2.57 | 2.60 | 2.62 |
| 21 | 2.63 | 2.66 | 2.68 | 2.71 | 2.73 | 2.65 | 2.67 | 2.70 | 2.72 | 2.75 |
| 22 | 2.76 | 2.78 | 2.81 | 2.83 | 2.86 | 2.77 | 2.80 | 2.83 | 2.85 | 2.88 |
| 23 | 2.88 | 2.91 | 2.93 | 2.96 | 2.98 | 2.90 | 2.93 | 2.95 | 2.98 | 3.00 |
| 2.4 | 3.01 | 3.03 | 3.06 | 3.08 | 3.11 | 3.03 | 3.05 | 3.08 | 3.10 | 3. 13 |
| 25 | 3.13 | 3.16 | 3.18 | 3.21 | 3.23 | 3.15 | 3.18 | 3.20 | 3.23 |  |
| 26 | 3.26 | 3.28 | 3.31 | 3.33 | 3.36 | 3.28 | 3.30 | 3.33 | 3.35 | 3.38 |
| 27 | $3 \cdot 38$ | 3.41 | 3.43 | 3.46 | 3.48 | 3.40 | 3.43 | 3.45 | 3.48 | 3.50 |
| 28 | 3.51 | 3.53 | 3.56 | 3.58 | 3.60 | 3.53 | 3.55 | 3.58 | 3.60 | 3.63 |
| 29 | 3.63 | 3.65 | 3.68 | 3.70 | 3.73 | 3.65 | 3.68 | 3.70 | 3.73 | 3.75 |
| 30 | 3.75 | 3.78 | 3.80 | 3.83 | 3.85 | 3.78 | 3.80 | 3.83 | 3.85 | 3.88 |
| 31 | 3.58 | 3.90 | 3.93 | 3.95 | 3.98 | 3.90 | 3.93 | 3.95 | 3.98 | 4.00 |
| 32 | 4.00 | 4.03 | 4.05 | 4.08 | 4.10 | 4.03 | 4.05 | 4.08 | 4.10 | 4.13 |
| 33 | 4.13 | 4.15 | 4.18 | 4.20 | 4.23 | 4.15 | 4.18 | 4.20 | 4.23 | 4.25 |
| 34 | 4.25 | 4.28 | 4.30 | 4.33 | 4.35 | 4.28 | 4.30 | 4.33 | 4.35 | 4.3 S |
| 35 | $4 \cdot 38$ | 4.40 | 4.43 | 4.45 | 4.48 | 4.40 | 4.43 | 4.45 | 4.48 | 4.50 |

Emithsonian Tables.

Table 45.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE. METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, THE CORRECTION IS TO BE SUBTRACTED.

|  | himint uf the banometer 780 mm . |  |  |  |  | HEICHT OF TIIE BAROMETER 785 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Ther. mometer. | 0.0 | 0.2 | 0.4 | 0.6 | 0.8 | $0 \%$ | 0.2 | 0.4 | 0\%6 | 0.8 |
| c. | mm. | mm. | mm. | mm. | mm. | mm. | mm . | mm. | mm. | mm. |
| $0^{\circ}$ | 0.00 | 0.03 | 0.05 | 0.08 | 0. 10 | 0.00 | 0.03 | 0.05 | 0.08 | -. 10 |
| 1 | . 13 | . 15 | I8 | . 20 | . 23 | . 13 | . 15 | . 18 | . 21 | . 23 |
| 2 | .25 | . 28 | . 31 | . 33 | . 36 | . 26 | . 28 | . 31 | . 33 | .36 |
| 3 | . 38 | . 41 | . 43 | . 46 | . 48 | . 38 | . 41 | . 44 | . 46 | . 49 |
| 4 | . 51 | . 53 | . 56 | . 59 | .6I | . 51 | . 54 | . 56 | . 59 | . 62 |
| 5 | 0.64 | 0.66 | 0.69 | 0.71 | 0. 74 | 0.64 | 0.67 | 0.69 | 0.72 | 0.74 |
| 6 | . 76 | . 79 | . SI | . 84 | . 87 | . 77 | . 79 | . 82 | . 85 | . 87 |
| 7 | . 89 | . 92 | . 94 | . 97 | . 99 | . 90 | .92 | . 95 | . 97 | 1.00 |
| 8 | 1.02 | 1.04 | 1.07 | 1.09 | 1.12 | 1.02 | 1.05 | 1.08 | I. 10 | I. 13 |
| 9 | 1.15 | 1.17 | 1.20 | 1.22 | I. 25 | I. 15 | I. 18 | 1.20 | I. 23 | 1.25 |
| 10 | 1.27 | 1.30 | 1.32 | 1.35 | 1.37 | 1.28 | 1.31 | I. 33 | 1.36 | 1. 38 |
| 11 | 1.40 | I. 42 | 1. 45 | I. 48 | I. 50 | I. 41 | 1.43 | I. 46 | 1. 48 | 1.51 |
| 12 | I. 53 | 1. 55 | I. 58 | 1. 60 | 1.63 | 1.54 | 1. 56 | 1.59 | I. 61 | I. 64 |
| 13 | 1.65 | I. 68 | 1.70 | 1.73 | I. 75 | 1.66 | I. 69 | 1.71 | 1.74 | 1.77 |
| 14 | 1.78 | 1. 81 | 1. 83 | 1.86 | I. 88 | 1.79 | 1.82 | I. 84 | 1.87 | I. S 9 |
| 15 | 1.91 | 1.93 | 1.96 | 1.98 | 2.01 | 1.92 | 1.94 | 1.97 | 2.00 | 2.02 |
| 16 | 2.03 | 2.06 | 2.08 | 2.11 | 2.13 | 2.05 | 2.07 | 2.10 | 2.12 | 2.15 |
| 17 | 2.16 | 2.19 | 2.21 | 2.24 | 2.26 | 2.17 | 2.20 | 2.22 | 2.25 | 2.28 |
| IS | 2.29 | 2.31 | 2.34 | 2.36 | 2.39 | 2.30 | 2.33 | 2.35 | 2.38 | 2.40 |
| 19 | 2.41 | 2.44 | 2.46 | 2.49 | 2.51 | 2.43 | 2.45 | 2.48 | 2.51 | 2.53 |
| 20 | 2.54 | 2.57 | 2.59 | 2.62 | 2.64 | 2.56 | 2.58 | 2.61 | 2.63 | 2.66 |
| 21 | 2.67 | 2.69 | 2.72 | 2.74 | 2.77 | 2.68 | 2.71 | 2.73 | 2.76 | 2.79 |
| 22 | 2.79 | 2.82 | 2.84 | 2.87 | 2.89 | 2.81 | 2.84 | 2.86 | 2.89 | 2.91 |
| 23 | 2.92 | 2.94 | 2.97 | 3.00 | 3.02 | 2.94 | 2.96 | 2.99 | 3.01 | 3.04 |
| 24 | 3.05 | 3.07 | 3.10 | 3.12 | 3.15 | 3.07 | 3.09 | 3.12 | 3.14 | 3.17 |
| 25 | 3.17 | 3.20 | 3.22 | 3.25 | 3.27 | 3.19 | 3.22 | 3.24 | 3.27 | 3.29 |
| 26 | 3.30 | $3 \cdot 32$ | 3.35 | $3 \cdot 37$ | 3.40 | 3.32 | $3 \cdot 34$ | 3.37 | 3.40 | 3.42 |
| 27 | 3.42 | 3.45 | 3.47 | 3.50 | 3.53 | 3.45 | $3 \cdot 47$ | 3.50 | 3.52 | 3.55 |
| 28 | 3.55 | 3.58 | 3.60 | 3.63 | 3.65 | 3.57 | 3.60 | 3.62 | 3.65 | 3.57 3.67 |
| 29 | 3.68 | 3.70 | 3.73 | 3.75 | 3.78 | 3.70 | 3.73 | 3.75 | 3.75 | 3.80 |
| 30 | 3.80 | 3.83 | 3.85 | 3.85 | 3.90 | 3.83 | 3.85 | 3.85 | 3.90 | 3.93 |
| 31 | 3.93 | 3.95 | 3.98 | 4.00 | 4.03 | 3.95 | 3.98 | 4.00 | 4.03 | 4.06 |
| 32 | 4.05 | 4.08 | 4. I I | 4. I3 | 4.16 | 4.08 | 4. I I | 4. 13 | 4.16 | 4.18 |
| 33 | 4. IS | 4.21 | 4.23 | 4.26 | 4.28 | 4.21 | 4.23 | 4.26 | 4.28 | 4.31 |
| 34 | 4.31 | 4.33 | 4.36 | 4.38 | 4.41 | 4.33 | 4.36 | 4.39 | 4.41 | 4.44 |
| 35 | 4.43 | 4.46 | 4.48 | 4.51 | 4.53 | 4.46 | 4.49 | 4.51 | 4.54 | 4.56 |

Smithion an Tables.
table 45.
REDUCTION OF THE BAROMETER TO STANDARD TEMPERATURE METRIC MEASURES.

FOR TEMPERATURES ABOVE $0^{\circ}$ CENTIGRADE, the CORRECTION IS TO BE SUBTRACTED.

|  | heIgit of tile barometer 790 mm . |  |  |  |  | heigilt of tile barometer 795 mm . |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Attached Thermometer. | 0.0 | 0.2 | 0\%4 | $0 \% 6$ | 0.8 | $0 \%$ | 0.2 | 0.4 | 0.6 | 0.8 |
| c. | minl. | mm. | mim. | mm. | mm . | mm. | mm. | mm. | mı. | mm. |
| $0^{\circ}$ | 0.00 | 0.03 | 0.05 | 0.08 | O. 10 | 0.00 | 0.03 | 0.05 | 0.08 | 0. 10 |
| I | . 13 | . 15 | . 18 | . 21 | . 23 | . 13 | . 16 | . 18 | . 21 | . 23 |
| 2 | . 26 | . 28 | . 3 I | . 34 | - 36 | . 26 | . 29 | -3I | . 34 | . 36 |
| 3 | . 39 | . 41 | - 44 | . 46 | -49 | - 39 | . 42 | . 44 | . 47 | . 49 |
| 4 | . 52 | . 54 | . 57 | . 59 | . 62 | . 52 | . 55 | . 57 | . 60 | . 62 |
| 5 | 0.64 | 0.67 | 0.70 | 0.72 | 0.75 | 0.65 | 0.67 | 0.70 | 0.73 | 0.75 |
| 6 | . 77 | . 50 | . 83 | . 85 | . 88 | .78 | . 80 | . 83 | . 86 | . 88 |
| 7 | . 90 | . 93 | . 95 | . 98 | I. OI | . 91 | . 93 | . 96 | . 99 | I. OI |
| 8 | 1.03 | I. 06 | 1.08 | I. I I | I. 13 | 1.04 | 1.06 | 1.09 | I. 12 | I. 14 |
| 9 | I. 16 | I. 19 | I. 21 | I. 24 | 1.26 | I. 17 | 1. 19 | 1.22 | 1.24 | I. 27 |
| 10 | I. 29 | I. 31 | I. 3.4 | 1. 37 | I. 39 | 1.30 | 1.32 | I. 35 | I. 37 | 1.40 |
| II | 1.42 | I. 44 | I. 47 | I. 49 | I. 52 | I. 43 | 1.45 | I. 48 | 1.50 | I. 53 |
| 12 | I. 55 | 1.57 | 1.60 | 1.62 | 1. 65 | I. 56 | 1. 58 | 1.6I | 1. 63 | I. 66 |
| 13 | 1.67 | 1.70 | 1.73 | 1. 75 | 1. 78 | 1. 68 | 1.71 | I. 74 | 1.76 | I. 79 |
| 14 | I. So | I. $\mathrm{S}_{3}$ | 1. 85 | I. 58 | I.91 | I. 81 | 1.84 | 1.87 | 1.89 | 1.92 |
| 15 | 1.93 | 1.96 | 1.98 | 2.01 | 2.03 | I. 94 | 1.97 | 1.99 | 2.02 | 2.05 |
| 16 | 2.06 | 2.09 | 2.11 | 2.14 | 2.16 | 2.07 | 2.10 | 2.12 | 2.15 | 2.18 |
| 17 | 2.19 | 2.21 | 2.24 | 2.26 | 2.29 | 2.20 | 2.23 | 2.25 | 2.28 | 2.30 |
| IS | 2.32 | 2.34 | 2.37 | 2.39 | 2.42 | 2.33 | 2.36 | 2.38 | 2.41 | 2.43 |
| 19 | 2.44 | 2.47 | 2.50 | 2.52 | 2.55 | 2.46 | 2.49 | 2.51 | 2.54 | 2.56 |
| 20 | 2.57 | 2.60 | 2.62 | 2.65 | 2.67 | 2.59 | 2.61 | 2.64 | 2.67 | 2.69 |
| 21 | 2.70 | 2.73 | 2.75 | 2.78 | 2.50 | 2.72 | 2.74 | 2.77 | 2.79 | 2.82 |
| 22 | $2 . S_{3}$ | 2.85 | 2.88 | 2.91 | 2.93 | 2.85 | 2.87 | 2.90 | 2.92 | 2.95 |
| 23 | 2.96 | 2.98 | 3.01 | 3.03 | 3.06 | 2.98 | 3.00 | 3.03 | 3.05 | 3.08 |
| 24 | 3.08 | 3.11 | 3.14 | 3.16 | 3.19 | 3.10 | 3.13 | 3.16 | 3.18 | 3.21 |
| 25 | 3.21 | 3.24 | 3.26 | 3.29 | $3 \cdot 31$ | 3.23 | 3.26 | 3.28 | 3.31 | 3.34 |
| 26 | 3.34 | $3 \cdot 37$ | $3 \cdot 39$ | 3.42 | 3.44 | $3 \cdot 36$ | 3.39 | 3.41 | 3.44 | 3.46 |
| 27 | 3.47 | 3.49 | 3.52 | 3.54 | 3.57 | 3.49 | $3 \cdot 52$ | 3.54 | 3.57 | 3.59 |
| 28 | 3.60 | 3.62 | 3.65 | 3.67 | 3.70 | 3.62 | 3.64 | 3.67 | 3.70 | 3.72 |
| 29 | 3.72 | 3.75 | 3.77 | 3.80 | 3.83 | 3.75 | 3.77 | 3.80 | 3.82 | 3.85 |
| 30 | 3.85 | 3.88 | 3.90 | 3.93 | 3.95 | 3.88 | 3.90 | 3.93 | 3.95 | 3.98 |
| 31 | 3.98 | 4.00 | 4.03 | 4.06 | 4.08 | 4.00 | 4.03 | 4.06 | 4.08 | 4. II |
| 32 | 4. I I | 4.13 | 4.16 | 4. IS | 4.21 | 4.13 | 4.16 | 4. IS | 4.21 | 4.24 |
| 33 | 4.23 | 4.26 | 4.29 | $4 \cdot 31$ | 4.34 | 4.26 | 4.29 | 4.31 | $4 \cdot 34$ | $4 \cdot 36$ |
| 34 | $4 \cdot 36$ | 4.39 | 4.41 | 4.44 | 4.46 | 4.39 | 4.42 | 4.44 | 4.47 | 4.49 |
| 35 | 4.49 | 4.51 | 4.54 | 4.57 | 4.59 | 4.52 | 4.54 | 4.57 | 4.59 | 4.62 |

## ENGLISH MEASURES

Table reconstructed from Table 44 to adapt it to U-shaped manometers with brass scales.

|  | Difference in height of the two columns, i. e., the algebraic difference of their readings, in inches. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
| F 0 0 2 | $\begin{gathered} \text { Inch. } \\ +0.003 \\ +0.002 \end{gathered}$ | $\begin{aligned} & \text { Inch. } \\ & +0.005 \end{aligned}$ | $\begin{gathered} \text { Inch. } \\ +0.008 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.010 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.013 \end{gathered}$ | $\begin{aligned} & \text { Inch. } \\ & +0.016 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & +0.018 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & +0.02 \mathrm{I} \end{aligned}$ | $\begin{gathered} \text { Inch. } \\ +0.023 \end{gathered}$ | $\begin{array}{r} \text { Inch. } \\ +0.026 \end{array}$ |
| 4 | +0.002 .002 |  | +0.007 .007 | +0.010 | +0.012 | +0.015 | +0.017 | +0.019 | $+0.022$ | +0.024 |
| 6 | . 002 | .004 | . 006 | . 008 | . 010 | .013 | .016 | . 018 | 0.20 | 0.22 |
| 8 | . 002 | . 004 | . 006 | . 008 | . 009 | . OI 1 | .OI 3 | . 017 | . 019 | 21 |
| 10 | . 002 | . 003 | . 005 | . 007 | . 008 | . 10 | . 1212 | . 014 | . 015 | .019 .017 |
| 12 | +0.002 | +0.003 | +0.005 | +0.006 | +0.008 | +0.009 | +0.011 | +0.012 | +0.014 | +o.015 |
| 14 | . 0001 | . 003 | .004 | . 005 | . 007 | . 008 | . 009 | . 011 | . 012 | +0.015 .013 |
| 18 | .001 | . 002 | . 003 | . 005 | . 006 | . 007 | . 008 | . 009 | . 010 | . O 12 |
| 20 | . 001 | . 002 | .02 | .004 | . 005 | . 006 | . 007 | . 008 | . 009 | 10 |
| 22 |  |  |  |  |  |  |  |  | . 007 | . 008 |
| 24 | 000 | . 001 | , I | +0.002 | +0.003 | +0.004 | +0.004 | +0.005 | 0.005 | +0.006 |
| 26 | . 000 | .001 | . 00 I | O22 | .002 | . 002 | . 003 | . 003 | .004 | . 004 |
| 28 | . 000 | 00 | oo | . 000 | .001 | . 000 | . 002 | . 002 | . 002 | . 003 |
| 30 | . 000 | . 000 | . 000 | -.001 | -.001 | -.000 | -.000 | .001 | .001 | .001 -.001 |
| 32 | 0.000 | OI | 0.001 | .00I | 0.002 | . 002 | 0.002 | -0.003 |  |  |
| 34 | -.001 | . 001 | . 002 | . 002 | . 003 | . 003 | .004 | .004 | .003 .005 | -0.003 |
| 36 | . 001 | . 001 | . 002 | . 003 | . 003 | . 004 | . 005 | . 005 | .006 | $\begin{aligned} & .005 \\ & .007 \end{aligned}$ |
| 38 | .00I | . 002 | . 003 | . 003 | .004 | . 005 | . 006 | .007 | . 0 | . 008 |
| 40 | . 001 | . 002 | . 003 | . 004 | . 005 | .006 | .007 | . 008 | . 009 | . 010 |
| 42 | 0.001 | 02 | 4 | 005 | . 006 | . 007 |  |  |  |  |
| 44 | OOI | .003 | .004 | 006 | . 007 | . 008 | . 010 | . 0 | 012 | -0.012 |
| 46 | . 002 | .003 | . 005 | . 006 | . 008 | . 009 | . 011 | . 013 | . 012 | .014 |
| 48 | . 002 | .004 | . 005 | . 007 | . 009 | . 017 | . 012 | .OI4 | . 016 | . 018 |
| 50 | . 002 | .004 | . 006 | . 008 | . 010 | . OL 2 | . 014 | . 016 | . 018 | . 019 |
| 52 | 0.002 | O4 | 06 | . 008 | 0.011 | 0.013 | .015 | 0.017 | 0.019 |  |
| 54 | 02 | . 005 | . 007 | .009 | . 01 I | . 014 | . 016 | .oi 8 | .021 | . 023 |
| 56 | . 002 | . 005 | . 007 | . 010 | . 012 | . 015 | . 017 | . 020 | . 02 | . 025 |
| 58 | . 003 | . 005 | . 008 | .OI I | .OI3 | . 016 | . 019 | . 022 I | . 024 | . 027 |
| 60 | . 003 | . 006 | . 008 | . 011 | .OI4 | . 017 | . 020 | . 023 | . 025 | . 028 |
| 62 | -0.003 | 0.006 | 0.009 | 0.012 | 0.015 | 0.018 | 0.021 | 0.024 | 0.027 | 0.030 |
| 64 | .003 | .006 | . 010 | . 013 | .016 | . 1219 | . 022 | . 026 | . 029 | . 032 |
| 66 | .003 | .007 | . 010 | .014 | . 017 | . 020 | . 022 | . 027 | .03I | . 034 |
| 68 | . 004 | .007 | . 01 I | .014 | . 018 | . 02 I | . 025 | . 028 | .032 | . 036 |
| 70 | . 004 | . 007 | . OII | . 015 | . 019 | . 022 | . 026 | . 030 | . 034 | . 037 |
| 72 | 0.004 | . 008 | $0.012$ | -0.016 | $-0.020$ | 0.024 | -0.027 | -0.031 | 0.035 | -0.039 |
| 74 | .004 | .008 | . 012 | .016 | . 020 | . 025 | . 029 | . 033 | . 037 | .041 |
| 76 | . 004 | . 009 | .013 | . 017 | . 021 | . 026 | . 030 | . 034 | . 038 | . 043 |
| 78 80 | . 004 | . 009 | . 013 | . 018 | . 022 | .027 | .03I | . 036 | . 040 | . 045 |
| 80 | . 005 | . 009 | . 014 | . 019 | . 023 | . 028 | . 032 | . 037 | .042 | . 0.46 |
| 82 | -0.005 | 0.010 | 0.014 | -0.019 | 0.024 | 0.029 | -0.034 | 0.039 | 0.043 | -0.048 |
| 84 | . 005 | . 010 | . 015 | . 020 | . 025 | . 030 | . 035 | . 040 | . 045 | . 050 |
| 86 | . 005 | .010 | . 016 | . 021 | . 026 | . 03 I | . 036 | . 042 | . 047 | . 052 |
| 88 | . 005 | . 011 | . 016 | . 021 | . 027 | . 032 | . 037 | . 043 | . 048 | . 053 |
| 90 | . 006 | .OII | . 017 | . 022 | . 028 | . 033 | . 039 | . 044 | . 050 | . 055 |
| 92 | 0.006 | O.OI I | 0.017 | -0.023 | -0.029 | 0.034 | 0.040 | 0.046 | -0.052 | -0.057 |
| 94 | . 006 | .OI2 | . 018 | . 024 | . 030 | . 035 | . 04 I | . 047 | .053 | . 059 |
| 96 | . 006 | . 012 | . 118 | .024 | . 030 | . 036 | . 043 | . 049 | . 055 | .06I |
| 98 | . 006 | . 013 | .019 | . 025 | .031 | . 038 | . 044 | . 050 | .056 | . 063 |
| 100 | . 006 | . 013 | . 019 | . 026 | . 032 | . 039 | . 045 | .052 | .058 | . 064 |

Table 46.
REDUCTION OF THE MERCURIAL COLUMN TO STANDARD TEMPERATURE.
ENGLISH MEASURES
Table reconstructed from Table 44 to adapt it to $U$-shaped manometers with brass scales.

|  | Difference in height of the two columns, i. E., the algebraic difference of their readings, in inches. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| $\mathrm{F} .$ | $\begin{aligned} & \text { Inch. } \\ & +0.029 \end{aligned}$ | $\begin{gathered} \text { Inch. } \\ +0.03 \mathrm{I} \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.034 \end{gathered}$ | $\begin{aligned} & \text { Inch. } \\ & +0.037 \end{aligned}$ | $\begin{gathered} \text { Inch. } \\ +0.039 \end{gathered}$ | $\begin{gathered} \text { Inch. } \\ +0.042 \end{gathered}$ | $\begin{aligned} & \text { Inch. } \\ & +0.044 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & +0.047 \end{aligned}$ | $\begin{gathered} \text { Inch. } \\ +0.050 \end{gathered}$ | $\begin{aligned} & \text { Inch. } \\ & +0.052 \end{aligned}$ |
| 2 | +0.027 | +0.029 | +0.03I | +0.034 | $+0.036$ | +0.039 | +0.041 | +0.044 | +0.046 | +0.049 |
| 4 | . 025 | . 027 | .029 | . 031 | .033 | . 036 | . 038 | . 0.40 | . 043 | . 045 |
| 6 | .023 | . 025 | . 027 | . 029 | . 031 | . 033 | . 035 | . 037 | . 039 | .04I |
| 8 | . 021 | .023 | . 025 | . 026 | . 028 | . 030 | .032 | . 034 | . 036 | . 038 |
| 10 | .OI9 | . 020 | . 022 | . 024 | .025 | .027 | . 029 | . 03 I | . 032 | . 034 |
| 12 | +0.017 | +0.018 | +0.020 | +0.021 | +0.023 | +0.024 | $+0.026$ | +0.027 | +0.029 | $+0.030$ |
| 14 | .OI 5 | .OI6 | .OI7 | .018 | . 020 | . 021 | .023 | . 024 | . 025 | . 027 |
| 16 | .OI 3 | .OI4 | .OI 5 | .016 | . 017 | .OI9 | . 020 | . 02 I | .022 | . 023 |
| 18 | . 017 | . 012 | .OI 3 | .OI4 | .015 | .016 | .016 | .OI7 | . 018 | . 019 |
| 20 | .009 | . 009 | . OIO | . OI I | . 012 | .OI3 | .OI 3 | .OI4 | . 015 | .016 |
| 22 | +0.007 | +0.007 | +0.008 | +0.008 | $+0.009$ | +0.010 | +0.010 | +0.01I | +0.011 | $+0.012$ |
| 24 | .005 | . 005 | . 006 | . 006 | . 006 | . 007 | .007 | . 008 | . 008 | . 008 |
| 26 | .003 | .003 | .003 | . 004 | .004 | . 004 | . 004 | . 004 | . 005 | . 005 |
| 28 | . 001 | .001 | . OOI | . 001 | . OOI | . 001 | . 001 | . OOI | . 001 | . 001 |
| 30 | -0.001 | -0.002 | 0.002 | $-0.002$ | $-0.002$ | -0.002 | -0.002 | $-0.002$ | $-0.002$ | -0.002 |
| 32 | -0.003 | -0.004 | -0.004 | -0.004 | 0.005 | 0.005 | 0.005 | $-0.006$ | -0.006 | -0.006 |
| 34 | .005 | . 006 | . 007 | . 007 | . 008 | . 008 | . 008 | . 009 | . 009 | . 010 |
| 36 | . 007 | . 008 | .009 | . 009 | . 010 | . 011 | . 011 | .OI 2 | .013 | .OI3 |
| 38 | .009 | .010 | .OII | .012 | . 013 | . 014 | . 014 | .015 | .016 | .017 |
| 40 | . OII | .012 | .OI 3 | .015 | . 016 | . 017 | . 018 | . 019 | . 020 | . 021 |
| 42 | -0.013 | -0.015 | -0.016 | -0.017 | O.OI 8 | -0.020 | 0.02 I | -0.022 | -0.023 | -0.024 |
| 44 | .O15 | . 017 | .OI 8 | .OI9 | . 021 | . 022 | . 024 | . 025 | . 026 | . 028 |
| 46 | .OI 7 | . 019 | .020 | . 022 | .024 | . 025 | .027 | . 028 | . 030 | . 031 |
| 48 | .019 | . 021 | . 023 | . 025 | .026 | . 028 | . 030 | .032 | .033 | . 035 |
| 50 | . 02 I | .023 | .025 | .027 | . 029 | . 03 I | .033 | . 035 | .037 | . 039 |
| 52 | -0.023 | $-0.025$ | $-0.027$ | $-0.030$ | $-0.032$ | $-0.034$ | -0.036 | -0.038 | -0.040 | $-0.042$ |
| 54 | . 025 | . 028 | . 030 | . 032 | . 034 | . 037 | . 039 | .04I | . 044 | .046 |
| 56 | . 027 | . 030 | .032 | . 035 | . 037 | .040 | .042 | .045 | .047 | . 050 |
| 58 | . 029 | . 032 | . 035 | .037 | .040 | . 043 | .045 | .048 | .051 | .053 |
| 60 | . 031 | .034 | .037 | .040 | .042 | .045 | .048 | .05I | .054 | .057 |
| 62 | -0.033 | $-0.036$ | -0.039 | -0.0.42 | -0.045 | -0.048 | -0.05I | -0.054 | -0.057 | -0.060 |
| 64 | . 035 | . 038 | .042 | . 045 | .048 | .051 | . 054 | . 058 | .06I | .064 |
| 66 | . 037 | .04I | .044 | .048 | .05I | .054 | .057 | .06I | .064 | . 068 |
| 68 | . 039 | . 043 | .046 | .050 | .053 | .057 | .06I | .064 | . 068 | . 071 |
| 70 | .04 I | .045 | .049 | .052 | .056 | . 060 | .064 | .067 | . 071 | . 075 |
| 72 | -0.043 | -0.047 | -0.05 I | -0.055 | $-0.059$ | -0.063 | $-0.067$ | -0.071 | -0.075 | -0.078 |
| 74 | .045 | . 049 | . 053 | . 057 | . 061 | . 065 | . 070 | .074 | . 078 | . 082 |
| 76 | .047 | .051 | .056 | . 060 | .064 | . 068 | .073 | .077 | .08I | . 086 |
| 78 | .049 | .054 | .058 | . 062 | .067 | .071 | .076 | .080 | .085 | . 089 |
| 80 | .05I | .056 | .060 | .065 | . 070 | .074 | .079 | .084 | . 088 | .093 |
| 2 | -0.053 | -0.058 | -0.063 | -0.067 | -0.072 | $-0.077$ | -0.082 | $-0.087$ | -0.092 | $-0.096$ |
| 84 | . 055 | . 060 | .065 | . 070 | .075 | . 080 | . 085 | . 090 | .095 | . 100 |
| 86 | . 057 | . 062 | .067 | . 073 | .078 | .083 | . 088 | . 093 | . 098 | . 104 |
| 88 | .059 | .064 | .070 | .075 | .080 | . 086 | .09I | . 096 | .102 | . 107 |
| 90 | .06I | . 066 | .072 | .078 | .083 | . 089 | .094 | .100 | . 105 | . I 11 |
| 92 | -0.063 | -0.069 | $-0.074$ | -0.080 | -0.086 | 0.092 | -0.097 | -0.103 | -0.109 | -O.II 4 |
| 94 | . 065 | . 071 | .077 | . 083 | . 089 | . 095 | .100 | .106 | . I12 | . 118 |
| 96 | .067 | . 073 | . 079 | . 085 | . 091 | .097 | . 103 | . 109 | .I I 5 | . 122 |
| 98 | .069 | . 075 | .08I | . 088 | .094 | . 100 | . 106 | . I 13 | . 119 | . 125 |
| 100 | . 071 | . 077 | .084 | .090 | . 097 | . 103 | . 109 | . 116 | . 122, | . 129 |

REDUCTION OF THE MERCURIAL COLUMN TO STANDARD TEMPERATURE. METRIC MEASURES
Table reconstructed from Table 45 to adapt it to U-shaped manometers with brass scales. For temperatures above $0^{\circ} \mathrm{C}$., the correction is to be subtracted; for temperatures below, added.

| Attached thermometer | Difference in height of the two columins, i. e., the algebraic difference of their readings (mm.). |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 20 | 40 | 60 | 80 | 100 | 120 | 140 | 160 | 180 | 200 | 220 | 240 |
| C. | mm . | mm . | mm. | mm . | mm . | mm . | mm . | min. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| I | . 0 | . 0 | . 0 | . 0 | . 0 | . 0 | . 0 | . 0 | . 0 | . 0 | . 0 | . 0 |
| 2 | . 0 | . 0 | . 0 | . 0 | . 0 | . 0 | . 0 | . 1 | . 1 | . 1 | . I | . 1 |
| 3 | . 0 | . 0 | . 0 | . 0 | . 0 | . 1 | . 1 | . 1 | . 1 | . 1 | . 1 | . I |
| 4 | . 0 | . 0 | . 0 | . 1 | . 1 | . I | . 1 | . 1 | . 1 | . I | . I | . 2 |
| 5 | 0.0 | 0.0 | 0.0 | O.I | O.I | 0.1 | O. I | O.I | O.I | 0.2 | 0.2 | 0.2 |
| 6 | . 0 | . 0 | .I | . 1 | . 1 | . 1 | . 1 | . 2 | . 2 | . 2 | . 2 | . 2 |
| 7 | . 0 | . 0 | . 1 | . I | . 1 | . 1 | . 2 | . 2 | . 2 | . 2 | . 3 | . 3 |
| 8 | . 0 | . 1 | . I | . 1 | . I | . 2 | . 2 | . 2 | . 2 | . 3 | . 3 | . 3 |
| 9 | . 0 | . 1 | . 1 | . 1 | . 1 | . 2 | . 2 | . 2 | . 3 | . 3 | - 3 | . 4 |
| 10 | 0.0 | 0.1 | 0.1 | O.I | 0.2 | 0.2 | 0.2 | 0.3 | 0.3 | 0.3 | 0.4 | 0.4 |
| 11 | . 0 | . 1 | . I | . 1 | . 2 | . 2 | . 3 | . 3 | . 3 | . 4 | . 4 | . 4 |
| 12 | . 0 | . 1 | . 1 | . 2 | . 2 | . 2 | . 3 | . 3 | . 4 | . 4 | . 4 | . 5 |
| 13 | . 0 | . 1 | . I | . 2 | . 2 | -3 | -3 | . 3 | . 4 | . 4 | . 5 | . 5 |
| 14 | . 0 | . 1 | . 1 | .2 | . 2 | . 3 | . 3 | . 4 | .4 | . 5 | . 5 | . 5 |
| 15 | 0.0 | 0.1 | 0.1 | 0.2 | 0.2 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 | 0.5 |  |
| 16 | . 1 | . 1 | . 2 | . 2 | . 3 | . 3 | . 4 | . 4 | . 5 | . 5 | . 6 | . 6 |
| 17 | . I | . 1 | . 2 | . 2 | - 3 | - 3 | . 4 | . 4 | . 5 | . 6 | . 6 | . 7 |
| 18 | . 1 | . 1 | . 2 | . 2 | . 3 | . 4 | . 4 | . 5 | . 5 | . 6 | . 6 | .7 |
| 19 | . 1 | . 1 | .2 | .2 | $\cdot 3$ | . 4 | . 4 | . 5 | . 6 | . 6 | . 7 | . 7 |
| 20 | O. I | 0.1 | 0.2 | 0.3 | 0.3 | 0.4 | 0.5 | 0.5 | 0.6 | 0.7 | 0.7 | 0.8 |
| 21 | . 1 | . I | . 2 | . 3 | . 3 | . 4 | . 5 | . 5 | . 6 | . 7 | . 8 | . 8 |
| 22 | . 1 | . I | . 2 | . 3 | . 4 | . 4 | . 5 | . 6 | . 6 | . 7 | . 8 | . 9 |
| 23 | . 1 | . I | . 2 | . 3 | . 4 | . 4 | . 5 | . 6 | .7 | . 7 | . 8 | . 9 |
| 24 | . 1 | . 2 | . 2 | $\cdot 3$ | . 4 | . 5 | . 5 | . 6 | . 7 | . 8 | . 9 | . 9 |
| 25 | O.I | 0.2 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.7 | 0.8 | 0.9 | 1.0 |
| 26 | . 1 | . 2 | . 3 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 8 | . 9 | 1.0 |
| 27 | . I | .2 | $\cdot 3$ | . 4 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 | I. 0 | I. I |
| 28 | . I | . 2 | . 3 | . 4 | . 5 | . 5 | . 6 | . 7 | . 8 | . 9 | I. 0 | I.I |
| 29 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | .7 | . 8 | . 8 | . 9 | 1.0 | I.I |
| 30 | O.I | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1.0 | I.I | 1.2 |
| 31 | . I | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 | 1.0 | I.I | 1.2 |
| 32 | . 1 | . 2 | . 3 | .4 | . 5 | . 6 | . 7 | . 8 | . 9 | 1.0 | I.I | I. 2 |
| 33 | . 1 | .2 | $\cdot 3$ | .4 | . 5 | . 6 | . 8 | . 9 | 1.0 | I. I | I. 2 | 1.3 |
| 34 | . I | . 2 | $\cdot 3$ | .4 | . 6 | .7 | . 8 | . 9 | 1.0 | I. I | 1.2 | 1.3 |

Smithsonian Tables

Table 47.
REDUCTION OF THE MERCURIAL COLUMN TO STANDARD TEMPERATURE.

## METRIC MEASURES

Table reconstructed from Table 45 to adapt it to $U$-shaped manometers with brass scales.
For temperatures above $0^{\circ} \mathrm{C}$., the correction is to be subtracted; for temperatures below, added.

|  | Difference in height of the two columns, i. e., the algebraic DIFFERENCE OF THEIR READINGS (MM.). |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 260 | 280 | 300 | 320 | 340 | 360 | 380 | 400 | 420 | 440 | 460 | 480 | 500 |
| C. | mm. | mm . | mm. | mm. | mm . | mm . | mm . | mm . | mm. | mm. | mm. | mm. | mm . |
| $0^{\circ}$ | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| I | . 0 | . 0 | . 0 | . I | . I | . I | . I | . I | . 1 | . I | . I | . I | . I |
| 2 | . I | . I | . I | . I | . I | . I | . I | . I | . 1 | . I | . 2 | . 2 | . 2 |
| 3 | . I | . I | . I | . 2 | . 2 | . 2 | . 2 | . 2 | . 2 | . 2 | . 2 | . 2 | . 2 |
| 4 | . 2 | . 2 | . 2 | . 2 | . 2 | . 2 | . 2 | . 3 | . 3 | . 3 | . 3 | . 3 | .3 |
| 5 | 0.2 | 0.2 | 0.2 | 0.3 | . 03 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 |
| 6 | . 3 | . 3 | . 3 | . 3 | . 3 | . 4 | . 4 | . 4 | . 4 | . 4 | . 5 | . 5 | . 5 |
| 7 | . 3 | - 3 | . 3 | . 4 | . 4 | . 4 | . 4 | . 5 | . 5 | . 5 | . 5 | . 5 | . 6 |
| 8 | . 3 | . 4 | . 4 | . 4 | . 4 | . 5 | . 5 | . 5 | . 5 | . 6 | . 6 | . 6 | .7 |
| 9 | . 4 | .4 | . 4 | . 5 | . 5 | . 5 | . 6 | . 6 | . 6 | .6 | .7 | . 7 | .7 |
| 10 | 0.4 | 0.5 | 0.5 | 0.5 | 0.6 | 0.6 | 0.6 | 0.7 | 0.7 | 0.7 | 0.8 | 0.8 | 0.8 |
| I I | . 5 | . 5 | . 5 | . 6 | . 6 | . 6 | . 7 | . 7 | . 8 | . 8 | . 8 | . 9 | . 9 |
| 12 | . 5 | . 5 | . 6 | .6 | .7 | .7 | .7 | . 8 | . 8 | .9 | .9 | . 9 | I. 0 |
| 13 | . 5 | . 6 | . 6 | . 7 | . 7 | . 8 | . 8 | . 8 | . 9 | . 9 | I . 0 | 1.0 | I. I |
| 14 | .6 | . 6 | .7 | .7 | . 8 | . 8 | .9 | .9 | I. 0 | 1.0 | 1.0 | I. I | I. I |
| 15 | 0.6 | 0.7 | 0.7 | 0.8 | 0.8 | 0.9 | 0.9 | I. 0 | I. 0 | I.I | I. I | 1.2 | 1.2 |
| 16 | .7 | . 7 | . 8 | . 8 | .9 | . 9 | 1.0 | I . 0 | I. I | I. I | I. 2 | I. 2 | I. 3 |
| 17 | . 7 | . 8 | . 8 | . 9 | .9 | I. 0 | I. I | I. I | I. 2 | I. 2 | I. 3 | 1.3 | I. 4 |
| 18 | . 8 | . 8 | .9 | . 9 | I. 0 | I. I | I. I | 1.2 | I. 2 | I. 3 | I. 3 | 1.4 | I. 5 |
| 19 | . 8 | .9 | .9 | 1.0 | I. I | I. I | I. 2 | 1.2 | I. 3 | I. 4 | I. 4 | I. 5 | I. 5 |
| 20 | 0.8 | 0.9 | 1.0 | I. 0 | I.I | 1.2 | 1.2 | 1.3 | I. 4 | 1.4 | 1.5 | I. 6 | I. 6 |
| 21 | . 9 | 1.0 | I. 0 | I. I | I. 2 | 1.2 | I. 3 | 1.4 | 1.4 | 1.5 | 1.6 | I. 6 | I. 7 |
| 22 | . 9 | 1.0 | I. I | I. I | 1.2 | I. 3 | 1.4 | I. 4 | 1.5 | 1.6 | 1.6 | 1.7 | I. 8 |
| 23 | 1.0 | 1.0 | I. I | I. 2 | I. 3 | I. 3 | I. 4 | 1.5 | 1.6 | 1.6 | 1.7 | 1.8 | 1.9 |
| 24 | I . 0 | I. I | 1.2 | I. 2 | I. 3 | 1.4 | 1.5 | I. 6 | I. 6 | 1.7 | I. 8 | 1.9 | 1.9 |
| 25 | I. I | I. I | 1.2 | 1.3 | 1.4 | 1.5 | I. 5 | I. 6 | 1.7 | 1.8 | 1.9 | 2.0 | 2.0 |
| 26 | I. I | 1.2 | 1.3 | 1.4 | 1.4 | 1.5 | I. 6 | I. 7 | I. 8 | 1.9 | 1.9 | 2.0 | 2.1 |
| 27 | I. I | I. 2 | I. 3 | 1.4 | 1.5 | 1.6 | 1.7 | 1.8 | I. 8 | 1.9 | 2.0 | 2.1 | 2.2 |
| 28 | 1.2 | 1.3 | I. 4 | 1.5 | I. 5 | I. 6 | 1.7 | I. 8 | 1.9 | 2.0 | 2.1 | 2.2 | 2.3 |
| 29 | 1.2 | I. 3 | I. 4 | I. 5 | 1.6 | 1.7 | 1.8 | 1.9 | 2.0 | 2.1 | 2.2 | 2.3 | 2.4 |
| 30 | I. 3 | I. 4 | I. 5 | I. 6 | 1.7 | I. 8 | 1.9 | 2.0 | 2.0 | 2.1 | 2.2 | 2.3 | 2.4 |
| 3 I | I. 3 | I. 4 | I. 5 | 1.6 | 1.7 | 1.8 | 1.9 | 2.0 | 2.1 | 2.2 | 2.3 | 2.4 | 2.5 |
| 32 | I. 4 | I. 5 | I. 6 | I. 7 | I. 8 | 1.9 | 2.0 | 2.1 | 2.2 | 2.3 | 2.4 | 2.5 | 2.6 |
| 33 | 1.4 | I. 5 | I. 6 | 1.7 | I. 8 | 1.9 | 2.0 | 2.1 | 2.2 | 2.4 | 2.5 | 2.6 | 2.7 |
| 34 | I. 4 | I. 5 | I. 7 | I. 8 | I. 9 | 2.0 | 2.1 | 2.2 | 2.3 | 2.4 | 2.5 | 2.6 | 2.8 |

Smithsonian Tables GRAVITY.

$$
C=\frac{\left(g_{t}-g_{0}\right)}{g_{0}} B
$$

(WITH $\mathrm{g}_{2}<\mathrm{g}_{0}$ THE CORRECTION IS TO BE SUBTRACTED ; WITH $\mathrm{g}_{l}>\mathrm{g}_{0}$ IT IS TO BE ADDED.)

| $g_{l}-g_{0}$ | BAROMETER READING $B$. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1.0 | 2.0 | 3.0 | 4.0 | 5.0 | 6.0 | 7.0 | 8.0 | 9.0 | 10.0 |
| Dynes. |  |  |  |  |  |  |  |  |  |  |
| 0.1 | 0.00010 | 0.00020 | 0.00031 | $0.000+1$ | 0.00051 | 0.00061 | 0.00071 | 0.00082 | 0.00092 | 0.00102 |
| 0.2 | 00020 | 00041 | 00061 | 00082 | 00102 | 00122 | 00143 | 00163 | 00184 | 00204 |
| 0.3 | 00031 | 00061 | 00092 | O122 | 00153 | 00184 | 00214 | 00245 | 00275 | 00306 |
| 0.4 | 00041 | 00082 | 00122 | 00163 | 0020.4 | 00245 | 00286 | 00326 | 00367 | 00408 |
| 0.5 | 0005 I | 00102 | -0153 | 00204 | 00255 | 00306 | 00357 | 00408 | 00459 | 00510 |
| 0.6 | 0.00061 | 0.00122 | 0.0018 .4 | 0.00245 | 0.00306 | 0.00367 | 0.00428 | $0.00+89$ | 0.00551 | 0.00612 |
| 0.7 | 00071 | OOI43 | 00214 | 00286 | 00357 | 00428 | 00500 | 00571 | 006.42 | 00714 |
| 0.8 | 00082 | 00163 | 00245 | 00326 | 00408 | OO+49 | 00571 | 00653 | 00734 | 00816 |
| 0.9 | 00092 | oor84 | 00275 | 00367 | 00.459 | 00551 | 00642 | 00734 | 00826 | 00918 |
| 1.0 | 00102 | 00204 | 00306 | 00408 | 00510 | 00612 | 00714 | 008ı6 | 00918 | O1020 |
| 1.1 | 0.00112 | 0.00224 | 0.00337 | 0.00449 | 0.00561 | 0.00673 | 0.00785 | 0.00897 | 0.01010 | 0.01122 |
| I. 2 | 00122 | 00245 | 00367 | 00489 | 00612 | $0073+$ | 00857 | 00979 | OIIOI | OI 224 |
| I. 3 | 00133 | 00265 | 00398 | 00530 | 00663 | 00795 | 00928 | 01061 | OI 193 | O1326 |
| 1.4 | $\infty 143$ | 00286 | 00428 | 00571 | 00714 | 00857 | 00999 | OII4 ${ }^{2}$ | 01285 | 01428 |
| 1.5 | 00153 | 00306 | 00.459 | 0061 2 | 00765 | OO918 | 01071 | 01224 | -1377 | O1530 |
| 1.6 | 0.00163 | 0.00326 | 0.00489 | 0.00653 | 0.00816 | 0.00979 | 0.01142 | 0.01305 | 0.01468 | 0.01632 |
| 1.7 | 00173 | 00347 | 00520 | 00693 | 00867 | 01040 | 01213 | OI 387 | 01560 | O1734 |
| 1.8 | 00184 | 00367 | -055 I | 00734 | 00918 | OIIII | -1285 | OI468 | 01652 | 01835 |
| I. 9 | $\infty \times 19$ | 00387 | 0058 I | 00775 | 00969 | O1162 | OI 356 | OI550 | OI 744 | O1937 |
| 2.0 | 00204 | 00.408 | 00612 | 00816 | 01020 | O1224 | 01428 | 01632 | Or835 | 02039 |
| 2.1 | 0.00214 | 0.00428 | 0.00642 | $0.008_{57}$ | 0.01071 | 0.01285 | 0.01499 | 0.01713 | 0.01927 | 0.02141 |
| 2.2 | 00224 | 00449 | 00673 | 00897 | Ori 22 | Or 346 | or 570 | 01795 | 02019 | 02243 |
| 2.3 | 00235 | 00469 | 00704 | 00938 | OII 73 | 01407 | 01642 | 01876 | O2III | 02345 |
| 2.4 | 00245 | 00489 | 00734 | 00979 | O1224 | 01468 | -1713 | -1958 | 02203 | 02447 |
| 2.5 | 00255 | 00510 | 00765 | O1020 | O1275 | OI530 | 01783 | 02039 | 02294 | 02549 |
| 2.6 | 0.00265 | 0.00530 | 0.00795 | 0.01061 | 0.01326 | 0.01591 | 0.01856 | 0.02121 | 0.02386 | 0.02651 |
| 2.7 | 00275 | 00551 | 00826 | OIIOI | 01377 | -1652 | 01927 | 02203 | 02478 | 02753 |
| 2.8 | 00286 | 00571 | 00857 | OII $\mathrm{q}^{2}$ | OI428 | 01713 | -1999 | 02284 | 02570 | 02855 |
| 2.9 | 00296 | 00591 | 00887 | Ori83 | 01479 | 01774 | 02070 | 02366 | 02661 | 02958 |
| 3.0 | 00306 | 00612 | 00918 | OI2 2.4 | O1530 | 01835 | $02 \mathrm{I}+\mathrm{I}$ | 02447 | 02753 | 03059 |
| 3.1 | 0.00316 | 0.00632 | 0.00048 | 0.01264 | 0.01581 | 0.01897 | 0.02213 | 0.02529 | 0.02845 | 0.03161 |
| 3.2 | 00326 | 00653 | 00079 | 01305 | 01632 | 01958 | 02284 | 02610 | 02937 | 03263 |
| $3 \cdot 3$ | 00337 | 00673 | -1010 | OI3.46 | 01683 | 02019 | 02356 | 02692 | 03029 | 03365 |
| 3.4 | © 0347 | 00693 | 010.40 | -1387 | 01734 | 02080 | 02427 | 02774 | 03120 | 03467 |
| 3.5 | 00357 | 00714 | 01071 | OT 428 | 01785 | 02141 | 02498 | 02855 | 03212 | $\bigcirc 3569$ |
| 3.6 | 0.00367 | 0.00734 | 0.01101 | 0.01468 | 0.01835 | 0.02203 | 0.02570 | 0.02937 | 0.03304 | 0.03671 |
| 3.7 | 00377 | 00755 | OII32 | -1500 | -1886 | 02264 | 02641 | 03018 | 03396 | $\bigcirc 3773$ |
| 3.8 | 00387 | 00775 | OII62 | -1550 | 01937 | 02325 | 02712 | 03100 | 03487 | 03875 |
| 3.9 | 00398 | 00795 | -1193 | 01591 | -1988 | 02386 | 02784 | 03182 | 03579 | 03977 |
| 4.0 | 00408 | 00816 | 01224 | 01632 | 02039 | 02447 | 02855 | 03263 | 03671 | 04079 |

[^27]Table 49.
REDUCTION OF THE BAROMETER TO STANDARD GRAVITY.
ENGLISH MEASURES.
FROM LATITUOE $0^{\circ}$ TO $45^{\circ}$, THE CORRECTION IS TO BE SUBTRACTEO.


EMITHSONIAN TABLES.

FROM LATITUDE $46^{\circ}$ TO $90^{\circ}$ THE CORREGTION IS TO BE AODED.

| Lati tude. | HEIGHT OF THE BIROMETFR TN INCHES. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 |
| $45^{\circ}$ | $\begin{aligned} & \text { Inch. } \\ & -0.001 \end{aligned}$ | $\begin{gathered} \text { Inch. } \\ -0.00 \mathrm{I} \end{gathered}$ | Inch. -0.001 | $\begin{gathered} \text { Inch. } \\ -0.001 \end{gathered}$ | $\begin{aligned} & \text { Inch. } \\ & -0.001 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & -0.001 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & -0.001 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & -0.00 \mathrm{I} \end{aligned}$ | $\begin{gathered} \text { Inch. } \\ -0.001 \end{gathered}$ | $\begin{aligned} & \text { Inch. } \\ & -0.001 \end{aligned}$ | $\begin{aligned} & \text { Inch. } \\ & -0.001 \end{aligned}$ | Inch. $-0.001$ |
| 46 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 | +0.001 |
| 47 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 |
| 48 | 0.004 | 0.005 | 0.005 | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.007 | 0.007 |
| 49 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 | 0.008 | 0.009 | 0.009 | 0.000 | 0.010 |
| 50 | 0.008 | 0.008 | 0.009 | 0.000 | 0.010 | 0.010 | 0.010 | 0.011 | 0.011 | 0.012 | 0.012 | 0.012 |
| 51 | +0.010 | +0.010 | +0.01 1 | +0.01 I | +0.012 | +0.012 | +0.013 | +0.013 | +0.014 | +0.014 | +0.015 | 15 |
| 52 | 0.01 I | 0.012 | 0.012 | 0.013 | 0.014 | 0.014 | 0.015 | 0.015 | 0.016 | 0.016 | 0.017 | 0.018 |
| 53 | 0.013 | 0.014 | 0.014 | 0.015 | 0.016 | 0.016 | 0.017 | 0.018 | 0.018 | 0.010 | 0.020 | 0.020 |
| 54 | 0.015 | 0.015 | 0.016 | 0.017 | 0.018 | 0.019 | 0.019 | 0.020 | 0.021 | 0.022 | 0.022 | 0.023 |
| 55 | 0.016 | 0.017 | 0.018 | 0.019 | 0.020 | 0.02 I | 0.021 | 0.022 | 0.023 | 0.024 | 0.025 | 0.026 |
| 56 | +0.018 | +0.019 | $+0.020$ | +0.021 | +0.022 | +0.023 | +0.024 | +0.024 | 0.026 | +0.026 | +0.027 | 2 S |
| - | 0.020 | 0.021 | 0.022 | 0.023 | 0.024 | 0.025 | 0.026 | 0.027 | 0.028 | 0.029 | 0.030 | 0.031 |
| 58 | 0.021 | 0.022 | 0.023 | 0.025 | 0.026 | 0.027 | 0.028 | 0.029 | 0.030 | 0.031 | 0.032 | 0.033 |
| 59 | 0.023 | 0.024 | 0.025 | 0.026 | 0.028 | 0.020 | 0.030 | 0.031 | 0.032 | 0.033 | 0.035 | 0.036 |
| 60 | $0.02+$ | 0.026 | 0.027 | 0.028 | 0.029 | 0.031 | 0.032 | 0.033 | 0.0 .34 | 0.036 | 0.037 | 0.038 |
| 61 | +0.026 | +0.027 | +0.028 | +0.030 | +0.031 | +0.0.33 | +0.034 | -0.035 | +0.037 | +0.038 | +0.0.39 | +0.041 |
| 62 | 0.027 | 0.029 | 0.030 | 0.032 | 0.033 | 0.034 | 0.036 | 0.037 | 0.039 | 0.010 | 0.0.1? | 0.043 |
| 63 | 0.029 | 0.030 | 0.032 | 0.033 | 0.035 | 0.036 | 0.038 | 0.030 | 0.041 | 0.042 | 0.044 | 0.045 |
| 64 | 0.030 | 0.032 | 0.033 | 0.035 | 0.036 | 0.038 | 0.040 | 0.041 | 0.043 | 0.0 .44 | 0.046 | 0.047 |
| 65 | 0.031 | 0.033 | 0.035 | 0.036 | 0.038 | 0.040 | 0.041 | 0.04 .3 | 0.045 | 0.046 | 0.048 | 0.050 |
| 66 | +0.033 | +0.034 | +0.036 | +0.038 | +0.040 | +0.0.4 1 | +0.043 | +0.045 | $+0.047$ | +0.0.4 | 0.05 | 0.052 |
| 67 | 0.034 | 0.036 | 0.038 | 0.039 | 0.041 | $0.0+3$ | 0.045 | 0.047 | 0.048 | 0.050 | 0.052 | 0.054 |
| 68 | 0.035 | 0.037 | 0.039 | 0.071 | 0.043 | 0.045 | 0.046 | 0.048 | 0.050 | 0.052 | 0.054 | 0.056 |
| 69 | 0.036 | 0.038 | 0.040 | 0.042 | 0.044 | 0.046 | 0.048 | 0.050 | 0.052 | 0.054 | 0.056 | 0.058 |
| 70 | 0.038 | 0.040 | 0.042 | 0.044 | 0.046 | 0.048 | 0.050 | 0.052 | 0.053 | 0.055 | 0.057 | 0.059 |
| 71 | +0.039 | +0.0.11 | $+0.043$ | +0.045 | +0.047 | +0.049 | +0.051 | +0.053 | +0.055 | +0.057 | +0.059 | +0.061 |
| 72 | 0.040 | 0.042 | 0.047 | 0.046 | 0.048 | 0.050 | 0.052 | 0.054 | 0.057 | 0.059 | 0.061 | 0.063 |
| 73 | 0.041 | 0.043 | 0.045 | 0.047 | 0.049 | 0.052 | 0.054 | 0.056 | 0.058 | 0.060 | 0.062 | 0.064 |
| 74 | 0.042 | 0.044 | 0.046 | 0.048 | 0.051 | 0.053 | 0.055 | 0.057 | 0.059 | 0.062 | 0.064 | 0.066 |
| 75 | 0.043 | 0.045 | 0.047 | 0.049 | 0.052 | 0.054 | 0.056 | 0.058 | 0.061 | 0.063 | 0.065 | 0.067 |
| 76 | +0.0.4. | +0.0.46 | +0.0.48 | +0.050 | +0.053 | +0.055 | +0.057 | +0.060 | +0.062 | +0.064 | +0.066 | +0.069 |
| 77 | 0.044 | 0.047 | 0.049 | 0.051 | 0.054 | 0.056 | 0.058 | 0.061 | 0.063 | 0.065 | 0.068 | 0.070 |
| 78 | 0.045 | 0.047 | 0.050 | 0.052 | 0.055 | 0.057 | 0.059 | 0.062 | 0.064 | 0.066 | 0.069 | 0.07 I |
| 79 | 0.046 | 0.048 | 0.051 | 0.053 | 0.055 | 0.058 | 0.060 | 0.063 | 0.065 | 0.067 | 0.070 | 0.072 |
| 80 | 0.046 | 0.049 | 0.051 | 0.054 | 0.056 | 0.059 | 0.061 | 0.063 | 0.066 | 0.068 | 0.071 | 0.073 |
| 81 | +0.047 | +0.049 | +0.052 | +0.05 4 | +0.057 | +0.059 | +0.062 | +0.064 | $+0.067$ | +0.060 | +0.072 | +0.074 |
| 82 | 0.047 | 0.050 | 0.052 | 0.055 | 0.057 | 0.060 | 0.062 | 0.065 | 0.067 | 0.070 | 0.072 | 0.075 |
| 83 | 0.048 | 0.050 | 0.053 | 0.056 | 0.058 | 0.061 | 0.063 | 0.066 | 0.068 | 0.071 | 0.073 | 0.076 |
| 84 | 0.048 | 0.051 | 0.053 | 0.056 | 0.059 | 0.061 | 0.064 | 0.066 | 0.069 | 0.071 | 0.074 | 0.076 |
| 85 | 0.049 | 0.05 I | 0.054 | 0.056 | 0.059 | 0.061 | 0.064 | 0.067 | 0.069 | 0.072 | 0.074 | 0.077 |
| 90 | +0.0.40 | +0.052 | +0.055 | +0.057 | +0.060 | $+0.062$ | +0.065 | +0.068 | +0.070 | +0.073 | +0.075 | $+0.078$ |

## Table 50. <br> REDUCTION OF THE BAROMETER TO STANDARD GRAVITY. <br> METRIC MEASURES.

FROM LATITUDE $0^{\circ}$ TO $45^{\circ}$, THE CORRECTION IS TO BE SUBTRACTED.

| Latitude. | HEIGHT OF THE BAROMETER IN MILLIMETERS. |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 520 | 540 | 560 | 580 | 600 | 620 | 640 | 660 | 680 | 700 | 720 | 740 | 760 | 780 |
|  | mm. | mm. | mm. | m. |  |  | m. | mm. |  |  | mm. |  | m. | mm. |
| $0^{\circ}$ | -1.39 | -1.45 | -1.50 | -1.55 | -1.61 | -1.66 | -1.71 | -1.77 | -1.82 | $-1.87$ | -1.93 | - 1.98 | -2.04 | -2.09 |
| 5 | -1.37 | -1. $4^{2}$ | -1.48 | $-1.53$ | -1.58 | -1.64 | -1. 69 | -1.74 | -1.79 | -1. 85 | -1.90 | -I.95 | -2.00 | -2.06 |
| 6 | 1.36 | 1.42 | 1.47 | 1.52 | 1.57 | 1.63 | 1.68 | 1.73 | 1.78 | 1.83 | I. 89 | I. 94 | 1.99 | 2.04 |
| 7 | I. 35 | 1.40 | 1.46 | I. 51 | 1.56 | 1.61 | I. 66 | 1.72 | 1.77 | 1.82 | 1.87 | . 1.92 | 1.98 | 2.03 |
| 8 | 1.34 | 1.39 | 1.44 | 1.49 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 | 1.85 | 1.91 | 1.96 | 2.01 |
| 9 | 1.33 | I. 38 | 1.43 | 1.48 | I. 53 | 1.58 | 1.63 | I. 68 | 1.73 | 1.78 | I. 84 | I. 89 | I. 94 | 1.99 |
| 10 | -1.31 | -1.36 | -1.4 1 | -1. 46 | -1.51 | -1.56 | -1.61 | -1.66 | -1.71 | -1.76 | -1.81 | -1.86 | -1.92 | -1.97 |
| 11 | 1.29 | 1.34 | 1.39 | 1.44 | 1.49 | I. 54 | 1.59 | 1.64 | 1.69 | 1.74 | 1.79 | 1.84 | 1.89 | 1.94 |
| 12 | 1.27 | 1. 32 | 1.37 | 1.42 | 1.47 | 1.52 | 1.57 | 1.62 | I. 67 | 1.72 | 1.76 | 1.8: | 1.86 | 1.91 |
| 13 | 1.25 | 1.30 | 1.35 | 1.40 | 1.45 | 1.50 | I. 54 | I. 59 | I. 64 | 1.69 | 1.74 | 1.78 | 1.83 | 1.88 |
| 14 | 1.23 | I. 28 | I. 33 | 1. 38 | 1.42 | 1.47 | 1.52 | 1.56 | I. 61 | I. 66 | 1.71 | 1.75 | 1.80 | 1.85 |
| 15 | -1.2I | -I. 26 | - I. 30 | -1.35 | - 1.40 | -1.44 | -1.49 | -1.54 | -1.58 | -1. 63 | -1.67 | $-1.72$ | -1.77 | $-\mathrm{I} .8 \mathrm{I}$ |
| 16 | I. 19 | I. 23 | 1.28 | 1.32 | 1.37 | 1.41 | 1.46 | 1.50 | 1.55 | 1.60 | 1.64 | 1.69 | 1.73 | 1.78 |
| 17 | I. 16 | 1.20 | 1.25 | 1.29 | I. 34 | 1.38 | 1.43 | 1.47 | 1.52 | I. 56 | 1.60 | 1.65 | 1.69 | 1.74 |
| 18 | I. 13 | I. 18 | 1.22 | I. 26 | I. 31 | I. 35 | 1.39 | 1.44 | I. 48 | 1.52 | 1.57 | 1.61 | 1.65 | 1.70 |
| 19 | I. 10 | I. 15 | 1.19 | 1.23 | I. 27 | 1.32 | I. 36 | 1.40 | 1.44 | 1.48 | 1.53 | 1.57 | I. 61 | 1. 65 |
| 20 | -1.07 | -I.II | -1.16 | -1.20 | -1.24 | -1.28 | -1.32 | -1.36 | -1.40 | -1.44 | -1.49 | -1.53 | -1.57 | -1.61 |
| 2 I | 04 | 1.08 | 1.12 | 1.16 | 1.20 | 1.24 | 1.28 | 1.32 | 1.36 | 1.40 | I. 44 | 1.48 | 1.52 | 1. 56 |
| 22 | 1.01 | 1.05 | 1.09 | 1.13 | I. 16 | 1.20 | 1.24 | 1.28 | 1.32 | I. 36 | 1.40 | 1.44 | 1.48 | I. 51 |
| 23 | 0.98 | I. OI | 1.05 | 1.09 | I. 13 | 1.16 | 1.20 | I. 24 | 1.28 | 1.31 | 1.35 | I. 39 | 1.43 | 1.46 |
| 24 | 0.94 | 0.98 | 1.OI | 1.05 | 1.08 | I. 12 | 1.16 | I.19 | 1.23 | 1.27 | 1.30 | 1.34 | 1.37 | 1.41 |
| 25 | -0.90 | -0.94 | -0.97 | -1.01 | -1.04 | -1.08 | - I. 11 | -1.15 | -I.18 | -1.22 | -1.25 | -I. 29 | -1.32 | -1.36 |
| 26 | 0.87 | 0.90 | 0.93 | 0.97 | 1.00 | 1.03 | 1.07 | 1.10 | 1.13 | 1.17 | 1.20 | 1.23 | 1.27 | 1.30 |
| 27 | 0.83 | 0.86 | 0.89 | 0.92 | 0.96 | 0.99 | 1.02 | 1.05 | 1.08 | I. 12 | 1.15 | 1.18 | 1.21 | 1.24 |
| 28 | 0.79 | 0.82 | 0.85 | 0.88 | 0.91 | 0.94 | 0.97 | 1.00 | 1.03 | 1.06 | 1.09 | 1.12 | I. 15 | 1.18 |
| 29 | 0.75 | 0.78 | 0.81 | 0.84 | 0.86 | 0.89 | 0.92 | 0.95 | 0.98 | I.OI | 1.04 | 1.07 | 1.10 | 1.12 |
| 30 | -0.71 | -0.74 | -0.76 | -0.79 | -0.82 | -0.85 | -0.87 | -0.90 | -0.93 | -0.95 | -0.98 | -1.01 | -1.04 | -1.06 |
| 31 | 0.67 | 0.69 | 0.72 | 0.74 | 0.77 | 0.80 | 0.82 | 0.85 | 0.87 | 0.90 | 0.92 | 0.95 | 0.98 | 1.00 |
| 32 | 0.62 | 0.65 | 0.67 | 0.70 | 0.72 | 0.74 | 0.77 | 0.79 | 0.82 | 0.84 | 0.86 | 0.89 | 0.91 | 0.94 |
| 33 | 0.58 | 0.60 | 0.63 | 0.65 | 0.67 | 0.69 | 0.72 | 0.74 | 0.76 | 0.78 | 0.80 | 0.83 | 0.85 | 0.87 |
| 34 | 0.54 | 0.56 | 0.58 | 0.60 | 0.62 | 0.64 | 0.66 | 0.68 | 0.70 | 0.72 | 0.74 | 0.76 | 0.79 | 0.81 |
| 35 | -0.49 | -0.51 | -0.53 | -0.55 | -0.57 | -0.59 | -0.61 | -0.63 | -0.64 | -0.66 | -0.68 | -0.70 | $-0.72$ | -0.74 |
| 36 | 0.45 | 0.46 | 0.48 | 0.50 | 0.52 | 0.53 | 0.55 | 0.57 | 0.58 | 0.60 | 0.62 | 0.64 | 0.65 | 0.67 |
| 37 | 0.40 | 0.42 | 0.43 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.54 | 0.56 | 0.57 | 0.59 | 0.60 |
| 38 | 0.36 | 0.37 | 0.38 | 0.40 | 0.41 | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 |
| 39 | 0.31 | 0.32 | 0.33 | 0.34 | 40.36 | 0.37 | 0.38 | 0.39 | 0.40 | 0.42 | 0.43 | 0.44 | 0.45 | 0.46 |
| 40 | -0.26 | -0.27 | -0.28 | -0.29 | -0.30 | -0.31 | -0.32 | -0.33 | -0.34 | $-0.35$ | -0.36 | -0.37 | -0.38 | -0.39 |
| 4 I | 0.21 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.30 | 0.31 | 0.32 |
| 42 | 0.17 | 0.17 | 0.18 | 0.19 | 0.19 | 0.20 | 0.21 | 0.21 | 0.22 | 0.22 | 0.23 | 0.24 | 0.24 | 0.25 |
| 43 | 0.12 | 0.12 | 2.13 | 0.13 | 3 0.14 | 0.14 | 0.15 | 0.15 | 0.16 | 0.16 | 0.16 | 0.17 | 0.17 | 0.18 |
| 44 | 0.07 | 0.07 | 0.08 | 8 | 0.08 | 0.08 | 0.09 | 0.09 | 0.09 | 0.10 | - | 0.10 | 0.1 | 0.11 |
| 45 | -0.02 | -0.02 | -0.03 | -0.03 | --0.03 | -0.03 | -0.03 | -0.0.3 | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | -0.04 |

Smithsonian tables.

FROM LATITUDE $46^{\circ}$ TO $90^{\circ}$, THE CORRECTION IS TO BE ADOEO.

| Lati- <br> tude. | HEIGIT OF THE BAROMETER IN MILLIMETERS. |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 520 | 540 | 560 | 580 | 600 | 620 | 640 | 660 | 680 | 700 | 720 | 740 | 760 | 780 |
|  | mm. | mm. | mm. | mm. | m. | m. | n. | mm. | . | mm. | mm. | m. | mm. | mm. |
| 45 | -0.02 | -0.02 | -0.03 | -0.03 | $-0.03$ | $-0.03$ | -0.03 | -0.03 | -0.03 | -0.03 | -0.03 | 0.03 | -0.03 | -0.04 |
| 46 | 1-0.02 | +0.03 | +0.03 | +0.03 | +0.03 | +0.03 | +0.03 | +0.03 | +0.03 | +0.03 | $+0.03$ | +0.03 | +0.04 | +0.04 |
| 47 | 0.07 | 0.08 | 0.08 | 0.08 | 0.08 | 0.09 | 0.09 | 0.09 | 0.09 | 0.10 | 0.10 | 0.10 | -. 10 | 0.11 |
| 48 | 0.12 | 0.12 | 0.13 | O. 13 | O. 14 | 0.14 | 0.15 | 0.15 | 0.16 | 0.16 | 0.17 | 0.17 | 0.18 | 0.18 |
| 49 | 0.17 | 0.17 | O.I8 | O. IO | O.19 | 0.20 | 0.21 | 0.21 | 0.22 | 0.23 | 0.23 | 0.24 | 0.25 | 0.25 |
| 50 | 0.22 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 | 0.3 I | 0.31 | 0.32 |
| 51 | to. 26 | +0.27 | +0.28 | +0.29 | +0.30 | +0.31 | +0.32 | +0.33 | +0.34 | +0.35 | +0.36 | +0.37 | +0.38 | +0.39 |
| 52 | 0.31 | 0.32 | 0.33 | 0.34 | 0.36 | 0.37 | 0.38 | 0.39 | 0.40 , | , 0.42 | 0.43 | 0.44 | 0.45 | 0.46 |
| 53 | 0.36 | 0.37 | 0.38 | 0.40 | 0.41 | 0.42 | 0.44 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.53 |
| 54 | 0.40 | 0.42 | 0.43 | 0.45 | 0.46 | 0.48 | 0.49 | 0.51 | 0.52 | 0.54 | 0.56 | 0.57 | 0.59 | 0.60 |
| 55 | 0.45 | 0.46 | 0.48 | 0.50 | 0.52 | 0.53 | 0.55 | 0.57 | 0.58 | 0.60 | 0.62 | 0.64 | 0.65 | 0.67 |
| 56 | 0.49 | +0.51 | +0.53 | +0.55 | +0.57 | $+0.59$ | +0.60 | +0.62 | +0.64 | +0.66 | +0.68 | 0.70 | +0.72 | +0.74 |
| 57 | 0.54 | 0.56 | 0.58 | 0.60 | 0.62 | 0.64 | 0.66 | 0.68 | 0.70 | 0.72 | $0.74{ }^{\prime}$ | 0.76 | 0.78 | 0.80 |
| 58 | 0.58 | 0.60 | 0.62 | 0.65 | 0.67 | 0.69 | 0.71 | 0.74 | 0.76 | 0.78 | 0.80 | 0.82 | 0.85 | 0.87 |
| 59 | 0.62 | 0.65 | 0.67 | 0.69 | 0.72 | 0.74 | 0.77 | 0.79 | 0.81 | 0.84 | 0.86 | 0.89 | 0.91 | 0.93 |
| 60 | 0.66 | 0.69 | 0.72 | 0.74 | 0.77 | 0.79 | 0.82 | 0.84 | 0.87 | 0.89 | 0.92 | 0.94 | 0.97 | 1.00 |
| 61 | +0.71 | +0.73 | +0.76 | +0.79 | $+0.81$ | +0.84 | $+0.87$ | +0.89 | +0.92 | +0.95 | +0.08 | 1.00 | $+1.03$ | +1.06 |
| 62 | 0.74 | 0.77 | 0.80 | 0.83 | 0.85 | 0.88 | 0.91 | 0.94 | 0.97 | 1.00 | I. $\mathrm{O}_{2}$ | 1.05 | 1.08 | I. I I |
| 63 | 0.78 | 0.8 I | 0.85 | 0.88 , | 0.91 | 0.94 | 0.07 | 1.00 | 1.03 | 1.06 | 1.09 | I.12 | I. I5 | 1.18 |
| 64 | 0.82 | 0.85 | 0.89 | 0.92 | 0.95 | 0.08 | 1.01 | 1.04 | 1.08 | I. I I | I. 14 | 1.17 | 1.20 | 1.23 |
| 65 | 0.86 | 0.89 | 0.93 | 0.96 | 0.99 | 1.03 | 1.06 | 1.09 | I. I3 | 1.10 | I. 19 | 1.22 | I. 26 | I. 29 |
| 66 | +0.90 | +0.93 | +0.97 | +1.00 | +1.04 | +1.07 | + I. 10 | +1.14 | +1.17 | +1.21 | +1.2. | 1.28 | +1.3I | +1.35 |
| 67 | 0.93 | 0.97 | 1.00 | 1.04 | 1.08 | I.II | 1.15 | I.IS | 1.22 | 1.25 | 1. 29 | 1.33 | I. 36 | 1.40 |
| 68 | 0.97 | 1.00 | 1.04 | 1.08 | I. 11 | 1.15 | 1.19 | I. 23 | I. 26 | 1.30 | I. 34 | 1.37 | 1.41 | 1.45 |
| 69 | 1.00 | 1.04 | 1.08 | I.II | I.I5 | 1.19 | 1. 23 | 1.27 | 1.31 | I. 34 | 1.38 | 1.42 | 1.46 | 1.50 |
| 70 | 1.03 | 1.07 | I. II | 1.15 | 1.19 | 1.23 | 1.27 | I. 3 I | I. 35 | I. 39 | 1.43 | 1.47 | 1.51 | I. 55 |
| 71 | +1.06 | +1.10 | +I.I4 | + I. 18 | +1.22 | +1.26 | +1.3I | +1.35 | +1.39 | +1.43 | +1.47 | 1.51 | +1.55 | +1.59 |
| 72 | 1.09 | I. 13 | I. I 7 | 1.22 | 1.26 | 1.30 | 1.34 | I. 38 | I. 42 | 1.47 | I. 51 | 1.55 | 1.59 | 1.63 |
| 73 | I. I 2 | I. 16 | 1.20 | 1.25 | 1.29 | 1.33 | I. 37 | 1.42 | 1.46 | 1.50 | I. 55 | 1. 59 | 1.63 | 1.67 |
| 74 | 1.14 | 1. 19 | 1.23 | 1. 28 | I. 32 | I. 36 | 1.41 | 1.45 | 1.50 | I. 54 | 1.58 | 1.63 | 1.67 | 1.72 |
| 75 | 1.17 | I. 2 I | 1. 20 | 30 | I. 35 | 1. 39 | 1.44 | 1.48 | 1.53 | 1.57 | 1.62 | 1. 66 | 1.71 | 1.75 |
| 76 | +1.19 | +1.24 | +1.28 | +1.33 | +1.37 | +1.42 | +1.47 | +1.51 | +1.56 | $+1.60$ | $+1.65$ | +1.70 | +1.74 | +1.79 |
| 77 | I. 21 | I. 26 | I. 31 | 1.35 | 1.40 | 1.45 | 1.49 | 1.54 | I. 59 | 1.63 | 1.68 | I. 73 | 1.77 | 1.82 |
| 78 | 1.23 | 1. 28 | I. 33 | 1.38 | 1.42 | 1.47 | I. 52 | I. 57 | 1.61 | 1. 66 | 1.71 | 1.70 | 1.80 | I. 85 |
| 79 | 1.25 | I. 30 | I. 35 | 1.40 | I. 45 | 1.49 | I. 54 | I. 59 | I. 64 | 1.69 | 1.73 | 1.78 | 1.83 | 1.88 |
| 80 | 1.27 | 1. 32 | I. 37 | 1.42 | . 147 | I. 51 | 1. 56 | 1.61 | 1. 66 | I. 71 | 1.76 | I. 8 I | 1.86 | 1.90 |
| 8 | +1.29 | +1.33 | +1.38 | +1.43 | $+1.48$ | +1.53 | +1.58 | +1.63 | +1.68 | +1.73 | 1.78 | +1.83 | I. SS | +1.93 |
| 82 | 1.30 | 1.35 | 1.40 | 1.45 | 1.50 | I. 55 | 1.60 | 1.65 | 1.70 | 1.75 | I. 80 | 1.85 | 1.90 | 1.95 |
| 83 | I. 3 I | I. 36 | 1.41 | 1.46 | I. 5 I | 1. 56 | 1.61 | 1.67 | 1.72 | 1.77 | I. 82 | 1.87 | 1.92 | 1.97 |
| 84 | I. 32 | 1.37 | 1.42 | 1.48 | I. 53 | I. 58 | 1.63 | 1.68 | 1.73 | 1.78 | 1.83 | 1.88 | 1.93 | I. 08 |
| 85 | I. 33 | 1.38 | 1. 43 | I. 49 | I. 54 | 1.59 | 1. 64 | 1.69 | I. 74 | 1.79 | 1.84 | 1.90 | 1.95 | 2.00 |
| 90 | +1.35 | +1.41 | $+1.46$ | +1.5I | $+1.56$ | +1.61 | $+1.67$ | +1.72 | +1.77 | $+1.82$ | 1.87 | 1.93 | +1.98 | $+2.03$ |

SMITHSONIAN TABLES.

TABLES FOR DETERMINING HEIGHTS, AND CONVERSIONS INVOLVING
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DETERMINATION OF HEIGHTS BY THE BAROMETER.
ENGLISH MEASURES.
Values of $60368[1+0.0010195 \times 36] \log \frac{29.90}{B}$.

| Barometric Pressure. B. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inches. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| 12.00 | 24814 | 24791 | 24769 | 24746 | 24723 | 24701 | 24678 | 24656 | 24633 | 24611 |
| 12.10 | 24588 | 24566 | 24543 | 2452 I | 24499 | 24476 | 24454 | 2443 I | 24409 | 24387 |
| 12.20 | 24365 | 24342 | 24320 | 24298 | 24276 | 24253 | 24231 | 24209 | 24187 | 24165 |
| 12.30 | 24143 | 24121 | 24098 | 24076 | 24054 | 24032 | 24010 | 23988 | 23966 | 23944 |
| 12.40 | 23923 | 23901 | 23879 | 23857 | 23835 | 23813 | 23791 | 23770 | 23748 | 23726 |
| 12.50 | 23704 | 23682 | 23661 | 23639 | 23617 | 23596 | 23574 | 23552 | 23531 | 23509 |
| 12.6 | 2348 | 23466 | 23445 | 23423 | 23402 | 23380 | 23359 | 23337 | 23316 | 23294 |
| 12.70 | 2327 | 23251 | 23230 | 23209 | 23187 | 23166 | 23145 | 23123 | 23102 | 23081 |
| 12.80 | 23060 | 23038 | 23017 | 22996 | 22975 | 22954 | 22933 | 22911 | 22890 | 22869 |
| 12.90 | 22848 | 22827 | 22806 | 22785 | 22764 | 22743 | 22722 | 22701 | 22680 | 22659 |
| 13.00 | 22638 | 22617 | 22596 | 22576 | 22555 | 2253 | 2251 | 22492 | 22471 | 22451 |
| 13.10 | 22430 | 22409 | 22388 | 22368 | 22347 | 22326 | 22306 | 22285 | 22264 | 22244 |
| 13.20 | 22223 | 22203 | 22182 | 22162 | 22141 | 22121 | 2210 | 22080 | 22059 | 22039 |
| 13.30 | 22018 | 21998 | 21977 | 2195 | 21937 | 2191 | 2,Sy6 | 21876 | 21855 | 21835 |
| 13.40 | 21815 | 21794 | ${ }^{21} 774$ | 21754 | 21734 | 21713 | 21693 | 21673 | 21653 | 21633 |
| 13.50 | 21612 | 21592 | 21572 | 21552 | 21532 | 21512 | 21492 | 21472 | 21452 | 21432 |
| 13.60 | 21412 | 21392 | 21372 | 21352 | 21332 | 21312 | 21292 | 21272 | 21252 | 21233 |
| 13.70 13 | 21213 | 21193 | 21173 | 2153 | 21134 | 21114 | 21094 | 21074 | 21054 | 21035 |
| 13.80 | 21015 | 20995 | 20976 | 20956 | 20936 | 20917 | 20897 | 20878 | 20858 | 20838 |
| 13.90 | 20819 | 20799 | 20780 | 20760 | 20741 | 20721 | 20702 | 2068 | 20663 | 20643 |
| 14.00 | 20624 | 20605 | 20585 | 20566 | 20546 | 20527 | 20508 | 20488 | 20469 | 20450 |
| 14.10 | 20431 | 2041 I | 20392 | 20373 | 20354 | 20334 | 20315 | 20296 | 20277 | 20258 |
| 14.20 | 20238 | 20219 | 20200 | 20181 | 20162 | 20143 | 20124 | 20105 | 20086 | 20067 |
| 14.30 | 20048 | 20029 | 20010 | 19991 | 19972 | 19953 | 19934 | 19915 | 19896 | 19877 |
| 14.40 | 19858 | 19839 | 19821 | 19802 | 19783 | 19764 | 19745 | 19727 | 19708 | 19689 |
| 14.50 | 19670 | 19651 | 19633 | 19614 | 19595 | 195 | 19558 | 195 | 1952I | 02 |
| 14.60 | 19483 | 19465 | 19446 | 19428 | 19409 | 19390 | 19372 | 19353 | 19335 | 19316 |
| 14.70 | 19298 | 19279 | 19261 | 19242 | 19224 | 19206 | 19187 | 19169 | 19150 | 19132 |
| 14.80 | 19114 | 19095 | 19077 | 19059 | 19040 | 19022 | 19004 | 18985 | 18967 | 18949 |
| 14.90 | 18931 | 18912 | 18894 | 18876 | 18858 | 18840 | 1882 | 18803 | -585 | 18767 |
| 15.00 | 18749 | 18731 | 18713 | 18694 | 18676 | IS658 | 18640 | 18622 | 18604 | 18586 |
| 15.10 | 18568 | 18550 | 18532 | 15514 | 18496 | 18478 | 18460 | 18442 | 18425 | 18407 |
| 15.20 | 18359 | 18371 | 18353 | I8335 | 18317 | 18300 | 18282 | 18264 | 18246 | 18228 |
| 15.30 | 18211 | 18193 | 18175 | 18157 | 18140 | 18122 | 18104 | 18086 | 18069 | I8051 |
| 15.40 | I 8033 | ISOI | 17998 | 17981 | 17963 | 17945 | 17928 | 1791 | 178 | 875 |
| 15.50 | 17858 | 17840 | 17823 | 17805 | 17788 | 1777 | 1775 | 1773 | 17718 | 00 |
| 15.60 | 17683 | 17665 | 17648 | 17631 | 17613 | 17596 | 17578 | 17561 | 17544 | 17526 |
| 15.70 | 17509 | 17492 | 17474 | 17457 | 17440 | 17423 | 17405 | 17388 | 17371 | 17354 |
| 15.80 | 17337 | 17319 | 17302 | 17285 | 17268 | 17251 | 17234 | 17215 | 17199 | 17182 |
| 15.90 | 17165 | 17148 | 17131 | 17114 | 17097 | 17080 | 17063 | 17046 | 17029 | 17012 |
| 16.00 | 16995 | 16978 | 16961 | 16944 | 16927 | 16910 | 16893 | 16876 | 16859 | 16842 |
| 16.10 | 16825 | 16808 | 16792 | 16775 | 16758 | 16741 | 16724 | 16707 | 16691 | 16674 |
| 16.20 | 16657 | 16640 | 16623 | 16607 | 16590 | 16573 | 16557 | 16540 | 16523 | 16506 |
| 16.30 | 16490 | 16473 | 16456 | 16440 | 16423 | 16406 | 16390 | 16373 | 16357 | 16340 |
| 16.40 | 16324 | 16307 | 16290 | 16274 | 16257 | 16241 | 16224 | 16208 | 16191 | 16175 |
| 16.50 | 16158 | 16142 | 16125 | 16109 | 16092 | 16076 | 16060 | 16043 | 16027 | 16010 |
| 16.60 | 15994 | 15978 | 15961 | 15945 | 15929 | 15912 | 15896 | 15880 | 15863 | 15847 |
| 16.70 | 15831 | 15815 | 15798 | 15782 | 15766 | 15750 | 15733 | 15717 | 15701 | 15685 |
| 16.80 | 15669 | 15652 | 15636 | 15620 | 15604 | 15588 | 15572 | ${ }^{1} 5556$ | 15539 | ${ }^{1} 5523$ |
| 16.90 | 15507 | 15491 | 15475 | 15459 | 443 | 15427 | 154II | 15395 | 15379 | ${ }^{5} 5363$ |
| 17.00 | 15347 | 15331 | 15315 | 15299 | 15283 | 15267 | 1525I | 15235 | 15219 | 15203 |

Table 51.
DETERMINATION OF HEIGHTS BY THE BAFIOMETER.
ENGLISH MEASURES.
Values of $60368[1+0.0010195 \times 36] \log \frac{29.90}{B}$

| Barometric P-essure B. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inches. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| 17.00 | 15347 | 15331 | 15315 | 15299 | 15283 | 15267 | 15251 | 15235 | 15219 | 15203 |
| 17.10 | 15187 | 15172 | I5156 | 15140 | 15124 | 15108 | 15092 | 15076 | 15061 | 15045 |
| 17.20 | I5029 | 15013 | 14997 | 14982 | 14966 | 14950 | 14934 | 14919 | 14903 | 14887 |
| 17.30 | 14871 | 14856 | 14840 | 14824 | 14809 | 14793 | 14777 | 14762 | 14746 | 14730 |
| 17.40 | 14715 | 14699 | 14684 | 14668 | 14652 | 14637 | 1462 I | 14606 | 14590 | 14575 |
| 17.50 | 14559 | 14544 | I 4528 | 14512 | 14497 | I4481 | 14466 | 14451 | 14435 | 14420 |
| 17.60 | 14404 | 14389 | 14373 | 14358 | 14342 | 14327 | 14312 | 14296 | 14281 | 14266 |
| 17.70 | 14250 | 14235 | 14219 | 14204 | 14189 | 14173 | 14158 | 14143 | 14128 | 14112 |
| 17.80 | 14097 | 14082 | 14067 | 14051 | 14036 | 14021 | 14006 | 13990 | I 3975 | 13960 |
| 17.90 | I 3945 | 13930 | I 3914 | 13899 | 13884 | 13869 | 1.3854 | 13839 | 13 S24 | 13808 |
| 18.00 | I 3793 | 13778 | 13763 | 13748 | 13733 | 13718 | 13703 | I3688 | 13673 | I 3658 |
| 18.10 | I 3643 | 13628 | 13613 | 13598 | ${ }^{1} 3583$ | 13568 | I 3553 | 13538 | 13523 | 13508 |
| 18.20 | 12493 | 13478 | 13463 | I 3448 | I 3433 | 13418 | ${ }^{1} 3404$ | 13389 | 13374 | ${ }^{1} 3359$ |
| 18.30 | I3j14 | 13329 | 13314 | 13300 | 13285 | 13270 | 13255 | 13240 | I 3226 | I32II |
| IS.40 | 13196 | 13181 | 13166 | I 3152 | 13137 | I3122 | 13107 | 13093 | 13078 | 13063 |
| 18.50 | I 3049 | 13034 | 13019 | 13005 | 12990 | 12975 | 12961 | 12946 | 12931 | 12917 |
| 18.60 | 12902 | 12888 | 12873 | 12 S 58 | 12844 | 12829 | 12SI5 | 12800 | 12785 | 12771 |
| 18.70 | 12756 | 12742 | 12727 | 12713 | 12695 | 126S4 | 12669 | 12655 | 12640 | 12626 |
| 18.80 | '2611 | 12597 | $125 \mathrm{~S}_{3}$ | 12568 | 12554 | 12539 | 12525 | 12510 | 12496 | 12482 |
| 18.90 | 1.2467 | 12453 | 12438 | 12424 | 12410 | 12395 | 12381 | 12367 | 12352 | 12338 |
| 19.00 | 12324 | 12310 | 12295 | 12281 | 12267 | 12252 | 12238 | 12224 | 12210 | 12195 |
| 19.10 | 1218I | 12167 | I2 153 | 12138 | 12124 | 12110 | 12096 | 12082 | 12068 | 12053 |
| 19.20 | 12039 | 12025 | I2OII | 11997 | 11983 | 11969 | 11954 | 119.40 | 11926 | 11912 |
| 19.30 | I 1898 | 11884 | IIS70 | II856 | II842 | IIS28 | 11814 | I I Soo | 11786 | 11772 |
| 19.40 | 11758 | 11744 | 11730 | 11716 | 11702 | I 1688 | 11674 | 11660 | 11646 | 11632 |
| 19.50 | II618 | 11604 | II590 | 11576 | 11562 | 11548 | II534 | I 1520 | 11507 | I 1493 |
| 19.60 | I I479 | I 1465 | 11451 | 11437 | 11423 | 11410 | I 1396 | 11382 | II368 | I I 354 |
| 19.70 | I 1340 | I 1327 | 11313 | 11299 | 11285 | 11272 | I 1258 | II 244 | 11230 | I1217 |
| 19.80 | I 1203 | IIIS9 | III75 | III 62 | III48 | III 134 | III2 1 | 11107 | 11093 | I IOSO |
| 19.90 | 11066 | 11052 | 11039 | IIO25 | IIOII | 10998 | 10984 | 10970 | 10957 | 10943 |
| 20.00 | 10930 | 10916 | 10903 | 108S9 | 10 S75 | 10S62 | 10S48 | 10835 | 10821 | 10SoS |
| 20.10 | 10794 | 107SI | 10767 | 10754 | 10740 | 10727 | 10713 | 10700 | 10686 | 10673 |
| 20.20 | 10659 | 10646 | 10632 | 10619 | 10605 | 10592 | 10579 | 10565 | 10552 | 10538 |
| 20.30 | IO525 | 10512 | 10498 | I24S5 | 10472 | 10458 | 10445 | 10431 | 10418 | 10.405 |
| 20.40 | 10391 | 10378 | 10365 | 10352 | 10338 | 10325 | 10312 | 10298 | 10285 | 10272 |
| 20.50 | 10259 | 10245 | 10232 | 10219 | 10206 | 10192 | IOI79 | 10166 | 10153 | 10139 |
| 20.60 | IOI26 | 10113 | 10100 | 10087 | 10074 | 10060 | 10047 | 10034 | 10021 | 10008 |
| 20.70 | 9995 | 9982 | 9968 | 9955 | 99.42 | 9929 | 9916 | 9903 | 9890 | 9 977 |
| 20.So | 9864 | 9851 | 9838 | 9825 | 9812 | 9799 | 9786 | 9772 | 9759 | 9746 |
| 20.90 | 9733 | 9720 | 9707 | 9694 | 968 I | 9668 | 9655 | 96.42 | 9629 | 9617 |
| 21.00 | 9604 | 9591 | 9578 | 9565 | 9552 | 9539 | 9526 | 9513 | 9500 | 9487 |
| 21.10 | 9474 | 9462 | 9449 | 9436 | 9423 | 9410 | 9397 | $93{ }^{\text {S }} 4$ | 9372 | 9359 |
| 21.20 | 9346 | 9333 | 9320 | 9307 | 9295 | 9282 | 9269 | 9256 | 9244 | 9231 |
| 21.30 | 9218 | 9205 | 9193 | 9180 | 9167 | 9154 | 9142 | 9129 | 9116 | 9103 |
| 21.40 | 909I | 9078 | 9065 | 9053 | 9040 | 9027 | 9015 | 9002 | $89 \mathrm{S9}$ | 8977 |
| 21.50 | 8964 | 8951 | 8939 | S926 | 8913 | 8901 | 8888 | 8876 | 8863 | S850 |
| 21.60 | 8838 | 8825 | 8813 | 8800 | 8788 | S775 | S762 | 8750 | 8737 | 8725 |
| 21.70 | 8712 | 8700 | 8687 | 8675 | S662 | 8650 | 8637 | 8625 | 8612 | 8600 |
| 21.80 | 8587 | 8575 | 8562 | 8550 | $\mathrm{S}_{53} 8$ | S525 | S513 | 8500 | 8488 | S475 |
| 21.90 | 8463 | 845 I | 8.438 | S426 | S413 | 8401 | $\mathrm{S}_{3} \mathrm{~S}_{9}$ | 8376 | 8364 | 8352 |
| 22.00 | 8339 | 8.327 | S314 | 8302 | S290 | 8277 | 8265 | 8253 | 8240 | 8228 |

## DETERMINATION OF HEIGHTS BY THE BAROMETER.

ENGLISH MEASURES.
Values of $60368[1+0.0010195 \times 36] \log \frac{29.90}{B}$.

| Barometric Pressure. B. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inches. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| 22.00 | 8339 | 8327 | 8354 | 8302 | 8290 | 8277 | 8265 | 8253 | 8240 | 8228 |
| 22.10 | S216 | 8204 | 8191 | Si79 | 8167 | 8r54 | 8142 | SI30 | Sil 8 | 8 I 5 |
| 22.20 | So93 | So8 1 | So69 | 8056 | So44 | 8032 | 8020 | Soo8 | 7995 | 7983 |
| 22.30 | 7971 | 7959 | 7947 | 7935 | 7922 | 7910 | 7898 | 7886 | 7874 | 7862 |
| 22.40 | 7849 | 7837 | 7825 | 7313 | 7801 | 7789 | 7777 | 7765 | 7753 | 7740 |
| 22.50 | 7728 | 7716 | 7704 | 7692 | 7680 | 7668 | 7656 | 7644 | 7632 | 7620 |
| 22.60 | 7608 | 7596 | 7584 | 7572 | 7560 | 7548 | 7536 | 7524 | 7512 | 7500 |
| 22.70 | 7488 | 7476 | 7464 | 7452 | 7440 | 7428 | 7416 | 7404 | 7392 | 7380 |
| 22.80 | 7368 | 7356 | 7345 | 7333 | 7321 | 7309 | 7297 | 7285 | 7273 | 7261 |
| 22.90 | 7249 | 7238 | 7226 | 7214 | 7202 | 7190 | 7178 | 7166 | 7155 | 7143 |
| 23.00 | 7131 | 7119 | 7107 | 7096 | 7084 | 7072 | 7060 | 7048 | 7037 | 7025 |
| 23.10 | 7013 | 7001 | 6990 | 6978 | 6966 | 6954 | 6943 | 6931 | 6919 | 6907 |
| 23.20 | 6896 | 6884 | 6572 | 6861 | 6849 | 6837 | 6825 | 6814 | 6802 | 6790 |
| 23.30 | 6779 | 6767 | 6755 | 6744 | 6732 | 6721 | 6709 | 6697 | 6686 | 6674 |
| 23.40 | 6662 | 665 I | 6639 | 6628 | 6616 | 6604 | 6593 | 6581 | 6570 | 6558 |
| 23.50 | 6546 | 6535 | 6523 | 6512 | 6500 | 6489 | 6477 | 6466 | 6454 | 6443 |
| 23.60 | 6431 | 6420 | 6408 | 6397 | 6385 | 6374 | 6362 | 6351 | 6339 | 6328 |
| 23.70 | 6316 | 6305 | 6293 | 6282 | 6270 | 6259 | 6247 | 6236 | 6225 | 6213 |
| 23.80 | 6202 | 6190 | 6179 | 6167 | 6156 | 6145 | 6133 | 6122 | 6110 | 6099 |
| 23.90 | 6088 | 6076 | 6065 | 6054 | 6042 | 6031 | 6020 | 6008 | 5997 | 5986 |
| 24.00 | 5974 | 5963 | 5952 | 5940 | 5929 | 5918 | 5906 | 5895 | 5884 | 5872 |
| 24.10 | 5861 | 5850 | 5839 | 5827 | 5816 | 5805 | 5794 | 5782 | 5771 | 5760 |
| 24.20 | 5749 | 5737 | 5726 | 5715 | 5704 | 5693 | 5681 | 5670 | 5659 | 5648 |
| 24.30 | 5637 | 5625 | 5614 | 5603 | 5592 | 558 I | 5570 | 5558 | 5547 | 5536 |
| 24.40 | 5525 | 5514 | 5503 | 5492 | 5480 | 5469 | 5458 | 5447 | 5436 | 5425 |
| 24.50 | 5414 | 5403 | 5392 | 5381 | 5369 | 5358 | 5347 | 5336 | 5325 | 5314 |
| 24.60 | 5303 | 5292 | 5281 | 5270 | 5259 | 5248 | 5237 | 5226 | 5215 | 5204 |
| 24.70 | 5193 | 5182 | 5171 | 5160 | 5149 | 5138 | 5127 | 5116 | 5105 | 5094 |
| 24.80 | $50{ }^{5}$ | 5072 | 5061 | 5050 | 5039 | 5028 | 5017 | 5006 | 4995 | 4985 |
| 24.90 | 4974 | 4963 | 4952 | 494 I | 4930 | 4919 | 4908 | 4897 | 4886 | 4876 |
| 25.00 | 4865 | 4854 | 4843 | 4832 | 4821 | 4810 | 4800 | 4789 | 4778 | 4767 |
| 25.10 | 4756 | 4745 | 4735 | 4724 | 4713 | 4702 | 4691 | 4681 | 4670 | 4659 |
| 25.20 | 4648 | 4637 | 4627 | 4616 | 4605 | 4594 | 4584 | 4573 | 4562 | 455 I |
| 25.30 | 4540 | 4530 | 4519 | 4508 | 4498 | 4487 | 4476 | 4465 | 4455 | 4444 |
| 25.40 | 4433 | - 4423 | 4412 | 4401 | 4391 | 4380 | 4369 | 4358 | 4348 | 4337 |
| 25.50 | 4326 | 4316 | 4305 | 4295 | 4284 | 4273 | 4263 | 4252 | 4241 | 423 I |
| 25.60 | 4220 | 4209 | 4199 | 4188 | 4178 | 4167 | 4156 | 4146 | 4135 | 4125 |
| 25.70 | 4114 | 4104 | 4093 | 4082 | 4072 | 4061 | 4051 | 4040 | 4030 | 4019 |
| 25.80 | 4009 | 3998 | 3988 | 3977 | 3966 | 3956 | 3945 | 3935 | 3924 | 3914 |
| 25.90 | 3903 | 3893 | 3882 | 3872 | 3861 | 3851 | 3841 | 3830 | 3820 | 3809 |
| 26.00 | 3799 | 3788 | 3778 | 3767 | 3757 | 3746 | 3736 | 3726 | 3715 | 3705 |
| 26.10 | 3694 | 3684 | 3674 | 3663 | 3653 | 3642 | 3632 | 3622 | 3611 | 3601 |
| 26.20 | 3590 | 3580 | 3570 | 3559 | 3549 | 3539 | 3528 | 3518 | 3508 | 3497 |
| 26.30 | 3487 | 3477 | 3466 | 3456 | 3446 | 3435 | 3425 | 3415 | 3404 | 3394 |
| 26.40 | 3384 | 3373 | 3363 | 3353 | 3343 | 3332 | 3322 | 3312 | 3301 | 3291 |
| 26.50 | 3281 | 3270 | 3260 | 3250 | 3240 | 3230 | 3219 | 3209 | 3199 | 3189 |

Table 51.

## DETERMINATION OF HEIGHTS BY THE BAROMETER.

ENGLISH MEASURES.
Values of $60368[1+0.0010195 \times 36] \log \frac{29.90}{B}$.

| Barometric Pressure. B. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Luches. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| 26.50 | 32 II | 3270 | 3260 | 3250 | 3240 | 3230 | 3219 | 3209 | 3199 | 3 I 89 |
| 26.60 | 3179 | 3168 | 3158 | 3148 | 3138 | 3128 | 3117 | 3107 | 3097 | 3087 |
| 26.70 | 3077 | 3066 | 3056 | 3046 | 3036 | 3026 | 3016 | 3005 | 2995 | 2985 |
| 26.80 | 2975 | 2965 | 2955 | 2945 | 2934 | 292.4 | 2914 | 2904 | 2894 | 2884 |
| 26.90 | 2874 | 2864 | 2854 | 2843 | 2833 | 2823 | 2 SI 3 | $2 \mathrm{So3}$ | 2793 | 2783 |
| 27.00 | 2773 | 2763 | 2753 | 2743 | 2733 | 2723 | 2713 | 2703 | 2692 | 2682 |
| 27.10 | 2672 | 2662 | 2652 | 2642 | 2632 | 2622 | 2612 | 2602 | 2592 | 2582 |
| 27.20 | 2572 | 2562 | 2552 | 2542 | 2532 | 2522 | 2512 | 2502 | 2493 | 2483 |
| 27.30 | 2473 | 2463 | 2453 | 2443 | 2433 | 2423 | 2413 | 2403 | 2393 | 2353 |
| 27.40 | 2373 | 2363 | 2353 | 2343 | 2334 | 2324 | 2314 | 2304 | 229. | 2284 |
| 27.50 | 2274 | 2264 | 2254 | 2245 | 2235 | 2225 | 2215 | 2205 | 2195 | 2185 |
| 27.60 | 2176 | 2166 | 2156 | 2146 | 2136 | 2126 | 2116 | 2107 | 2097, | -ก87 |
| 27.70 | 2077 | 2067 | 2058 | 2048 | 2038 | 2028 | 2018 | 2009 | 1999 | 1989 |
| 27.80 | 1979 | 1970 | 1960 | 1950 | 1940 | 1930 | 1921 | I91I | 1901 | 1891 |
| 27.90 | 1882 | 1872 | IS62 | I852 | 1843 | 1833 | 1823 | I814 | 1804 | 1794 |
| 28.00 | 1784 | 1775 | 1765 | I755 | 1746 | 1736 | 1726 | 1717 | 1707 | 1697 |
| 28.10 | 1688 | 1678 | 1668 | 1659 | 1649 | 1639 | 1630 | 1620 | 1610 | 1601 |
| 28.20 | 1591 | I 581 | 1572 | 1562 | 1552 | I 543 | I 533 | 1524 | 1514 | 1504 |
| 28.30 | 1495 | 1485 | 1476 | 1466 | 1456 | 1447 | 1437 | 1428 | 1418 | 1408 |
| 28.40 | I 399 | 1389 | 1380 | 1370 | I361 | I 351 | 1342 | 1332 | 1322 | 1313 |
| 28.50 | 1303 | 1294 | 1284 | 1275 | 1265 | 1256 | 1246 | 1237 | 1227 | 1218 |
| 28.60 | 1208 | I 199 | IIS9 | 1180 | 1170 | 1161 | 1151 | 1142 | II32 | 1123 |
| 28.70 | III 3 | 1104 | 1094 | 1085 | 1075 | 1066 | 1057 | 1047 | 1038 | 1028 |
| 2 2.30 | 1019 | 1009 | 1000 | 990 | 98 I | 972 | 962 | 953 | 943 | 934 |
| 28.90 | 925 | 915 | 906 | 896 | SS7 | 878 | \$68 | 859 | 849 | 840 |
| 29.00 | 831 | 821 | SI2 | 803 | 793 | 784 | 775 | 765 | 756 | 746 |
| 29.10 | 737 | 728 | 718 | 709 | 700 | 690 | 681 | 672 | 663 | 653 |
| 29.20 | 644 | 635 | 625 | 616 | 607 | 597 | 588 | 579 | 570 | 560 |
| 29.30 | 551 | 542 | 532 | 523 | 514 | 505 | 495 | 486 | 477 | 468 |
| 29.40 | 458 | 449 | 440 | 43 I | 421 | 412 | 403 | 394 | 3 S 4 | 375 |
| 29.50 | 366 | 357 | 348 | 338 | 329 | 320 | 311 | 302 | 292 | 283 |
| 29.60 | 274 | 265 | 256 | 247 | 237 | 228 | 219 | 210 | 201 | 192 |
| 29.70 | 182 | 173 | 164 | 155 | 146 | 137 | 128 | 118 | 109 | 100 |
| 29.80 | +91 | + 82 | + 73 | + 64 | + 55 | + 45 | + 36 | + 27 | + I8 | + 9 |
| 29.90 | - | - 9 | - 18 | - 27 | $-36$ | - 45 | $-55$ | - 64 | $-73$ | $-82$ |
| 30.00 | - 9I | - 100 | - 109 | $-118$ | - 127 | - 136 | - I45 | - I54 | $-163$ | - I72 |
| 30.10 | -181 | - 190 | - I99 | - 208 | $-217$ | - 226 | -235 | -244 | - 253 | $-262$ |
| 30.20 | -271 | - 280 | -289 | - 298 | $-307$ | $-316$ | $-325$ | -334 | -343 | $-352$ |
| 30.30 | -36I | $-370$ | -379 | $-388$ | - 397 | -406 | -415 | -424 | -433 | -442 |
| 30.40 | -45I | $-460$ | -469 | $-47 \mathrm{~S}$ | $-486$ | -495 | $-504$ | -513 | $-522$ | $-531$ |
| 30.50 | - 540 | - 549 | $-558$ | $-567$ | -576 | $-585$ | - 593 | $-602$ | -6II | $-620$ |
| 30.60 | -629 | -63S | -647 | -656 | -665 | -673 | -682 | -691 | - 700 | -709 |
| 30.70 | $-718$ | -727 | -735 | -744 | $-753$ | -762 | - 771 | -780 | - 788 | -797 |
| 30.80 | -806 | -SI5 | -S24 | $-833$ | -84I | $-850$ | $-859$ | - 868 | - S77 | -885 |

DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.
Term for Temperature : $0.002039\left(\theta-50^{\circ}\right) \mathrm{z}$.


| Mean Temperature. $\theta$. |  | APPROXIMATE DIFFERENCE OF HEIGHT OBTAINED FROM TAble 61. |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 20 | 40 | 60 | 80 | '100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 |
| F. |  | Feet. | Feet. | Feet. | Feet. | Feet. | $\overline{\text { Feet. }}$ | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| $49^{\circ}$ | $51^{\circ}$ | 0 | 0 | 0 | o | 0 | o | 1 | 1 | 1 | 1 | 1 | 2 | 2 |
| 48 | 52 | - | - | 0 | $\bigcirc$ | - | I | 1 | 2 | 2 | 2 | 3 | 3 | 4 |
| 47 | 53 | $\bigcirc$ | 0 | 0 | o | I | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 6 |
| 46 | 54 | $\bigcirc$ | 0 | o | 1 | 1 | 2 | 2 | 3 | 4 | 5 | 6 | 7 | 7 |
| 45 | 55 | $\bigcirc$ | $\bigcirc$ | 1 | 1 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 44 | 56 | $\bigcirc$ | $\bigcirc$ | 1 | 1 | 1 | 2 | 4 | 5 | 6 | 7 | 9 | 10 | 11 |
| 43 | 57 | $\bigcirc$ | 1 | 1 | I | 1 | 3 | 4 | 6 | 7 | 9 | 10 | II | 13 |
| 42 | 58 | $\bigcirc$ | 1 | 1 | I | 2 | 3 | 5 | 7 | 8 | 10 | 11 | 13 | 15 |
| 4 I | 59 | $\bigcirc$ | 1 | 1 | 1 | 2 | 4 | 6 | 7 | 9 | II | 13 | 15 | 17 |
| 40 | 60 | O | 1 | 1 | 2 | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 |
| 39 | 61 | $\bigcirc$ | 1 | 1 | 2 | 2 | 4 | 7 | 9 | II | 13 | 16 | 18 | 20 |
| 38 | 62 | - | I | 1 | 2 | 2 | 5 | 7 | 10 | 12 | 15 | 17 | 20 | 22 |
| 37 | 63 | I | I | 2 | 2 | 3 | 5 | 8 | II | 13 | 16 | 19 | 21 | 24 |
| 36 | 64 | 1 | I | 2 | 2 | 3 | 6 | 9 | II | 14 | 17 | 20 | 23 | 26 |
| 35 | 65 | 1 | 1 | 2 | 2 | 3 | 6 | 9 | 12 | 15 | 18 | 2 I | 24 | 28 |
| 34 | 66 | I | 1 | 2 | 3 | 3 | 7 | 10 | 13 | 16 | 20 | 23 | 26 | 29 |
| 33 | 67 | I | 1 | 2 | 3 | 3 | 7 | 10 | 14 | 17 | 21 | 24 | 28 | 31 |
| 32 | 68 | I | 1 | 2 | 3 | 4 | 7 | 11 | 15 | 18 | 22 | 26 | 29 | 33 |
| 3 I | 69 | 1 | 2 | 2 | 3 | 4 | 8 | 12 | 15 | 19 | 23 | 27 | 31 | 35 |
| 30 | 70 | 1 | 2 | 2 | 3 | 4 | 8 | 12 | 16 | 20 | 24 | 29 | 33 | 37 |
| 29 | 71 | 1 | 2 | 3 | 3 | 4 | 9 | 13 | 17 | 21 | 26 | 30 | 34 | 39 |
| 28 | 72 | I | 2 | 3 | 4 | 4 | 9 | 13 | 18 | 22 | 27 | 31 | 36 | 40 |
| 27 | 73 | I | 2 | 3 | 4 | 5 | 9 | 14 | 19 | 23 | 28 | 33 | 38 | 42 |
| 26 | 74 | I | 2 | 3 | 4 | 5 | 10 | 15 | 20 | 24 | 29 | 34 | 39 | 44 |
| 25 | 75 | I | 2 | 3 | 4 | 5 | 10 | 15 | 20 | 25 | 31 | 36 | 4 I | 46 |
| 24 | 76 | 1 | 2 | 3 | 4 | 5 | 11 | 16 | 21 | 27 | 32 | 37 | 42 | 48 |
| 23 | 77 | 1 | 2 | 3 | 4 | 6 | 11 | 17 | 22 | 28 | 33 | 39 | 44 | 50 |
| 22 | 78 | I | 2 | 3 | 5 | 6 | 11 | 17 | 23 | 29 | 34 | 40 | 46 | 51 |
| 21 | 79 | 1 | 2 | 4 | 5 | 6 | 12 | 18 | 24 | 30 | 35 | 41 | 47 | 53 |
| 20 | 80 | I | 2 | 4 | 5 | 6 | 12 | 18 | 24 | 3 I | 37 | 43 | 49 | 55 |
| 19 | SI | 1 | 3 | 4 | 5 | 6 | 13 | 19 | 25 | 32 | 38 | 44 | 51 | 57 |
| 18 | 82 | 1 | 3 | 4 | 5 | 7 | 13 | 20 | 26 | 33 | 39 | 46 | 52 | 59 |
| 17 | $\mathrm{S}_{3}$ | 1 | 3 | 4 | 5 | 7 | 13 | 20 | 27 | 34 | 40 | 47 | 54 | 61 |
| 16 | S4 | 1 | 3 | 4 | 6 | 7 | 14 | 21 | 28 | 35 | 42 | 49 | 55 | 62 |
| 15 | 85 | 1 | 3 | 4 | 6 | 7 | 14 | 2 I | 29 | 36 | 43 | 50 | 57 |  |
| 14 | 86 | 1 | 3 | 4 | 6 | 7 | 15 | 22 | 29 | 37 | 44 | 51 | 59 | 66 |
| 13 | 87 | 2 | 3 | 5 | 6 | 8 | 15 | 23 | 30 | 38 | 45 | 53 | 60 | 68 |
| 12 | SS | 2 | 3 | 5 | 6 | S | 15 | 23 | 31 | 39 | 46 | 54 | 62 | 70 |
| 11 | 89 | 2 | 3 | 5 | 6 | 8 | 16 | 24 | 32 | 40 | 48 | 56 | 64 | 72 |
| 10 | 90 | 2 | 3 | 5 | 7 | 8 | 16 | 24 | 33 | 41 | 49 | 57 | 65 | 73 |
| 9 | 91 | 2 | 3 | 5 | 7 | S | 17 | 25 | 33 | 42 | 50 | 59 | 67 | 75 |
| 8 | 92 | 2 | 3 | 5 | 7 | 9 | 17 | 26 | 34 | 43 | 5 I | 60 | 69 | 77 |
|  | 93 | 2 | 4 | 5 | 7 | 9 | 18 | 26 | 35 | 44 | 53 | 61 | 70 | 79 |
| 6 | 9.4 | 2 | 4 | 5 | 7 | 9 | IS | 27 | 36 | 45 | 54 | 63 | 72 | SI |
| 5 | 95 | 2 | 4 | 6 | 7 | 9 | 18 | 28 | 37 | 46 | 55 | 64 | 73 | 83 |
| 4 | 96 | 2 | 4 | 6 | 8 | 9 | 19 | 28 | 38 | 47 | 56 | 66 | 75 | 84 |
| 3 | 97 | 2 | 4 | 6 | S | 10 | 19 | 29 | 38 | 48 | 57 | 67 | 77 | 86 |
| 2 | 98 | $?$ | 4 | 6 | 8 | 10 | 20 | 29 | 39 | 49 | 59 | 69 | 78 | 88 |
| 1 | 99 | 2 | 4 | 6 | S | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 |
| 0 | 100 | 2 | 4 | 6 | 8 | 10 | 20 | 3 I | 4 I | 5 I | 61 | 71 | 82 | 92 |

## Table 52.

DETERMINATION OF HEIGHTS BY THE BAROMETER. ENGLISH MEASURES.
Term for Temperature : $0.002039\left(\theta-50^{\circ}\right) \mathrm{z}$.
For temperatures $\left\{\begin{array}{l}\text { above } 50^{\circ} \mathrm{F} . \\ \text { below } 50^{\circ} \mathrm{F} .\end{array}\right\}$ the values are to be $\left\{\begin{array}{l}\text { added. } \\ \text { subtrac }\end{array}\right.$ below $50^{\circ} \mathrm{F}$. the values are to be $\{$ subtracted.

| Mean Temperature. $\theta$. |  | APPROXIMATE DIFFERENCE OF |  |  |  |  | HEIGH | T OBTAINED |  | FROM | TABL | 51. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1000 | 2000 | 3000 | 4000 | 5000 | 6000 | 7000 | 8000 | 9000 | 10000 | 20000 |
| $\begin{gathered} F . \\ 49^{\circ} \end{gathered}$ | F. $51^{\circ}$ | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| $49^{\circ}$ | $51^{\circ}$ | 2 | 4 | $6$ | S | 10 | 12 | 14 | 16 | 18 | 20 | 4 I |
| 48 | 52 | 4 | 8 | 12 | 16 | 20 | 2.4 | 29 | 33 | 37 | 4 I | S2 |
| 47 | 53 | 6 | 12 | 18 | 24 | 31 | 37 | 43 | 49 | 55 | 61 | 122 |
| 46 | 54 | S | 16 | 24 | 33 | 4 I | 49 | 57 | 65 | 73 | S2 | 163 |
| 45 | 55 | 10 | 20 | 31 | 4 I | 51 | 61 | 71 | 82 | 92 | 102 | 204 |
| 44 | 56 | 12 | 24 | 37 | 49 | 61 | 73 | S6 | 98 | 110 | 122 | 245 |
| 43 | 57 | 14 | 29 | 43 | 57 | 71 | 86 | 100 | 114 | 128 | 143 | 285 |
| 42 | 5 S | 16 | 33 | 49 | 65 | S2 | 98 | 114 | 130 | 147 | 163 | 326 |
| 41 | 59 | IS | 37 | 55 | 73 | 92 | 110 | 128 | 147 | 165 | I 84 | 367 |
| 40 | 60 | 20 | 4 I | 61 | 82 | 102 | 122 | 143 | 163 | I8.4 | 204 | 408 |
| 39 | 61 | 22 | 45 | 67 | 90 | I 12 | 135 | I57 | 179 | 202 | 224 | 449 |
| 38 | 62 | 24 | 49 | 73 | 98 | 122 | 147 | 171 | 196 | 220 | 245 | 489 |
| 37 | 63 | 27 | 53 | So | 106 | ${ }^{1} 33$ | I 59 | 186 | 212 | 239 | 265 | 530 |
| 36 | 64 | 29 | 57 | 86 | 114 | 143 | 17 I | 200 | 228 | 257 | 285 | 57 I |
| 35 | 65 | 31 | 61 | 92 | 122 | 153 | I84 | 214 | 245 | 275 | 306 | 612 |
| 34 | 66 | 33 | 65 | 98 | 130 | 163 | 196 | 228 | 261 | 294 | 326 | 652 |
| 33 | 67 | 35 | 69 | 104 | I39 | 173 | 208 | 2.43 | 277 | 312 | 347 | 693 |
| 32 | 68 | 37 | 73 | 110 | 147 | I84 | 220 | 257 | 294 | 330 | 367 | 734 |
| 31 | 69 | 39 | 77 | 116 | ${ }^{1} 55$ | 19.4 | 232 | 27 I | 310 | 349 | 387 | 775 |
| 30 | 70 | 41 | 82 | 122 | 163 | 204 | 245 | 285 | 326 | 367 | 408 | 816 |
| 29 | 71 | 43 | 86 | 128 | 171 | 214 | 257 | 300 | 343 | $3{ }^{3} 5$ | 428 | 856 |
| 28 | 72 | 45 | 90 | 135 | 179 | 224 | 269 | 314 | 359 | 404 | 449 | S97 |
| 27 | 7.3 | 47 | 94 | 141 | I88 | 234 | 281 | 328 | 375 | 422 | 469 | 938 |
| 26 | 74 | 49 | 98 | 147 | 196 | 245 | 294 | 343 | 391 | 440 | 489 | 979 |
| 25 | 75 | 5 I | IO2 | 153 | 204 | 255 | 306 | 357 | 408 | 459 | 510 | 1020 |
| 24 | 76 | 53 | 106 | 159 | 212 | 265 | 318 | 371 | 424 | 477 | 530 | 1060 |
| 23 | 77 | 55 | 110 | 165 | 220 | 275 | 330 | 385 | 440 | 495 | 551 | IIOI |
| 22 | 78 | 57 | 114 | 171 | 228 | 285 | 343 | 400 | 457 | 514 | 571 | 1142 |
| 21 | 79 | 59 | 118 | 177 | 236 | 296 | 355 | 4 I 4 | 473 | 532 | 591 | I 183 |
| 20 | 80 | 61 | 122 | 184 | 245 | 306 | 367 | 428 | 489 | 55 I | 612 | 1223 |
| 19 | 81 | 63 | 126 | 190 | 253 | 316 | 379 | 442 | 506 | 569 | 632 | 1264 |
| IS | 82 | 65 | 130 | 196 | 261 | 326 | 391 | 457 | 522 | 587 | 652 | 1305 |
| 17 | 83 | 67 | 135 | 202 | 269 | 336 | 404 | 471 | 538 | 606 | 673 | I 346 |
| 16 | 84 | 69 | I39 | 208 | 277 | 347 | 416 | 485 | 555 | 624 | 693 | I3S7 |
| 15 | 85 | 71 | 143 | 214 | 285 | 357 | 428 | 500 | 571 | 642 | 714 | 1427 |
| 14 | 86 | 73 | 147 | 220 | 294 | 367 | 440 | 514 | 557 | 661 | 734 | I 468 |
| 13 | 87 | 75 | 15 I | 226 | 302 | 377 | 453 | 528 | 604 | 679 | 754 | I 509 |
| 12 | 88 | 77 | I55 | 232 | 310 | 387 | 465 | 542 | 620 | 697 | 775 | 1550 |
| II | 89 | So | I59 | 239 | 318 | 398 | 477 | 557 | 636 | 716 | 795 | ${ }^{1} 590$ |
| 10 | 90 | 82 | 163 | 245 | 326 | 408 | 489 | 57 I | 652 | 734 | Si6 | 1631 |
|  | 91 | S4 | 167 | 251 | 334 | 418 | 502 | 585 | 669 | 752 | 836 | 1672 |
| 8 | 92 | 86 | 171 | 257 | 343 | 428 | 514 | 599 | 685 | 771 | 856 | 1713 |
| 7 | 93 | S8 | 175 | 263 | 35 I | 438 | 526 | 614 | 701 | 789 | S77 | 1754 |
| 6 | 94 | 90 | 179 | 269 | 359 | 449 | 538 | 628 | 718 | S07 | S97 | 1794 |
| 5 | 95 | 92 | 184 | 275 | 367 | 459 | 551 | 642 | 734 | 826 | 918 | 1835 |
| 4 | 96 | 94 | IS8 | 2 SI | 375 | 469 | 563 | 657 | 750 | S44 | 938 | I876 |
| 3 | 97 | 96 | 192 | 287 | 383 | 479 | 575 | 671 | 767 | 862 | 958 | 1917 |
| 2 | 98 | 98 | 196 | 294 | 391 | 489 | 587 | 685 | 783 | 88I | 979 | 1957 |
| 1 | 99 | 100 | 200 | 300 | 400 | 500 | 599 | 699 | 799 | 899 | 999 | 1998 |
| 0 | 100 | 102 | 204 | 306 | 408 | 510 | 612 | 714 | 8I6 | 918 | 1020 | 2039 | ENGLISH MEASURES.

Correction for Gravity and Weight of Mercury: $z\left(0.002640 \cos 2 \phi-0.000007 \cos ^{2} 2 \phi+0.00244\right)$.

| Latitude. <br> $\phi$ | APPROXIMATE |  |  | DIFFERENCE O |  | HEIGH | T OBTAINED |  | FROM | tables | 51-52. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 500 | 1000 | 1500 | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 | 5500 |
|  | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |  |  |  |  |
| $0^{\circ}$ | +3 | $+5$ | +8 | +10 | +13 | +15 | +i8 | $\begin{array}{r} \text { reet. } \\ +20 \end{array}$ | $\begin{array}{r} \text { reet. } \\ +\quad 23 \end{array}$ | $\begin{array}{r} \text { Feet. } \\ +25 \end{array}$ | $\begin{aligned} & \text { Feet. } \\ & +28 \end{aligned}$ |
| 2 | 3 | 5 | 8 | 10 | 13 | 15 | 18 | 20 | 23 2 | +25 | +28 |
| 4 | 3 | 5 | 8 | 10 | 13 | 15 | 18 | 20 | 23 | 25 | 28 |
| 8 | 3 | 5 | 8 | 10 | 13 | 15 | 18 | 20 | 23 | 25 | 28 |
| 8 | 2 | 5 | 7 | 10 | 12 | 15 | 17 | 20 | 22 | 25 | 27 |
| 10 | +2 | $+5$ | +7 | +10 | +12 | +15 | $+17$ | +20 | $+22$ | +25 |  |
| 12 | , | 5 | 7 | 10 | 12 | 15 | 17 | 19 | - 22 | +25 24 | +27 +27 |
| 14 | 2 | 5 | 7 | 10 | 12 | 14 | 17 | 19 | 21 | 24 24 | 27 26 |
| 16 | 2 | 5 | 7 | 9 | 12 | 14 | 16 | 19 | 2 I | 23 | 26 |
| 18 | 2 | 5 | 7 | 9 | 11 | 14 | 16 | 18 | 2 I | 23 | 25 |
| 20 | +2 | +4 | +7 | $+9$ | +II | +13 | +16 | +18 | +20 | $+22$ |  |
| 22 |  | 4 | 6 | 9 | 1 I | 13 | 15 | + 7 | 19 +10 | $\begin{array}{r}+22 \\ \hline 22\end{array}$ | +24 +24 |
| 24 | 2 | 4 | 6 | 8 | 10 | 13 | 15 | 17 | 19 | 21 |  |
| 26 | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 | 23 22 |
| 28 | 2 | 4 | 6 | S | 10 | 12 | 14 | 16 | 18 | 20 | 21 |
| 30 | $+2$ | +4 | $+6$ | +8 | +9 | +1I | +13 | +15 | $+17$ | +19 | +2I |
| 32 | 2 | 4 | 5 | 7 | 9 | 11 | 13 | 14 | 16 | 18 | 20 |
| 34 | 2 | 3 | 5 | 7 | 9 | 10 | 12 | 14 | 15 | 17 | 19 |
| 36 | 2 | 3 | 5 | 6 | 8 | 10 | II | 13 | 15 | 10 | 18 |
| 38 | 2 | 3 | 5 | 6 | 8 | 9 | 11 | 12 | 14 | 15 | 17 |
| 40 | $+1$ | $+3$ | +4 | $+6$ | $+7$ | + 9 | $+10$ | +12 | +13 | $+14$ | +16 |
| 42 | I | 3 | 4 | 5 | 7 | 8 | 9 | 11 | 12 | 13 | 15 |
| 44 | I | 3 | 4 | 5 | 6 | S | 9 | 10 | II | 13 | 14 |
| 45 | +1 | +2 | +4 | + 5 | $+6$ | $+7$ | $+9$ | +10 | + 11 | $+12$ | +13 |
| 46 | +1 | +2 | +4 | $+5$ | +6 | $+7$ | $+8$ | + 9 | +11 | +12 |  |
| 48 | 1 | , | 3 | 4 | 5 | 6 | 8 | 9 | 10 | 11 | 12 |
| 50 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | II |
| 52 | +1 | +2 | $+3$ | + 4 | + 4 | $+5$ | + 6 | $+7$ | $+8$ |  | +10 |
| 54 | I | 2 |  | 3 | 4 | 5 | 6 | 6 | 7 | 8 | 9 |
| 56 | 1 | I | 2 | 3 | 4 | 4 | 5 | 6 | 7 | 7 | 8 |
| 58 | I | 1 | 2 | 3 | 3 | 4 | 4 | 5 | 6 | 6 | 7 |
| 60 | I | I | 2 | 2 | 3 | 3 | 4 | 4 | 5 | 6 | 6 |
| 62 | $\bigcirc$ | +1 |  | + 2 | + 2 |  |  |  |  |  |  |
| 64 | $\bigcirc$ | 1 | + | 2 | 2 | + | 3 3 | 4 4 | + 3 3 | 5 4 | 5 4 |
| 66 | $\bigcirc$ | I | I | I | 2 | 2 |  | 3 | 3 | 3 | 3 |
| 68 | $\bigcirc$ | 1 | I | I | 1 | 2 | 2 | 2 | 2 | 3 | 3 |
| 70 | - | $\bigcirc$ | I | 1 | I | 1 | 1 | 2 | 2 | 2 | 2 |
| 72 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | + I | + I | + 1 | + I | + I | + I | + I |
| 74 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | I | 1 | I | 1 | I | 1 |
| 76 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |
| 78 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - | $\bigcirc$ | - | $\bigcirc$ | $\bigcirc$ |
| 80 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |

Smithsonian tables.

ENGLISH MEASURES.
Correction for Gravity and Weight of Mercury : $z\left(0.002640 \cos 2 \phi-0.000007 \cos ^{2} 2 \phi+0.00244\right)$.

| Latitude. $\phi$ | APPROXIMATE DIFFERENCE OF HEIGIT OBTALNED FROM TABLES 51-52. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6000 | 7000 | 8000 | 9000 | 10000 | 11000 | 12000 | 13000 | 14000 | 15000 | 20000 |
|  | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| $0^{\circ}$ | $+30$ | +35 | +4I | +46 | +5I | +56 | +6I | $+66$ | +71 | +76 | +ior |
| 2 | 30 | 35 | 40 | 46 | 51 | 56 | 61 | 66 | 71 | 76 | 101 |
| 4 | 30 | 35 | 40 | 45 | 50 | 55 | 61 | 66 | 71 | 76 | 101 |
| 6 | 30 | 35 | 40 | 45 | 50 | 55 | 61 | 66 | 71 | 76 | 100 |
| 8 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 99 |
| 10 | +29 | +34 | +39 | +44 | +49 | +54 | +59 | +64 | $+69$ | +74 | +98 |
| 12 | 29 | 34 | 39 | 44 | 48 | 53 | 58 | 63 | 68 | 73 | 97 |
| 14 | 29 | 33 | 38 | 43 | 48 | 52 | 57 | 62 | 67 | 71 | 95 |
| 16 | 28 | 33 | 37 | 42 | 47 | 51 | 56 | 61 | 65 | 70 | 93 |
| 18 | 27 | 32 | 37 | 41 | 46 | 50 | 55 | 59 | 64 | 68 | 91 |
| 20 | +27 | $+31$ | $+36$ | $+40$ | +45 | +49 | +53 | $+58$ | +62 | $+67$ | $+89$ |
| 22 | 26 | 30 | 35 | 39 | 43 | 48 | 52 | 56 | 61 | 65 | 87 |
| 24 | 25 | 29 | 34 | 38 | 42 | 46 | 50 | 55 | 59 | 63 | 84 |
| 26 | 24 | 28 | 32 | 37 | 41 | 45 | 49 | 53 | 57 | 61 | 81 |
| 28 | 23 | 27 | 31 | 35 | 39 | 43 | 47 | 51 | 55 | 59 | 78 |
| 30 | +23 | +26 | $+30$ | +34 | $+38$ | +41 | +45 | +49 | +53 | $+56$ | + 75 |
| 32 | 22 | 25 | 29 | 32 | 36 | 40 | 43 | 47 | 50 | 54 | 72 |
| 34 | 21 | 2.4 | 27 | 31 | 34 | 38 | 41 | 44 | 48 | 51 | 68 |
| 36 | 20 | 23 | 26 | 20 | 32 | 36 | 39 | 42 | 46 | 49 | 65 |
| 38 | 18 | 22 | 25 | 28 | 31 | 34 | 37 | 40 | 43 | 46 | 61 |
| 40 | +17 | +20 | +23 | +26 | $+20$ | $+32$ | +35 | +38 | +41 | +43 | + 57 |
| 42 | 16 | 19 | 22 | 24 | 27 | 30 | 33 | 35 | $3^{8}$ | 41 | 54 |
| 44 | 15 | 18 | 20 | 23 | 25 | 28 | 30 | 33 | 35 | 38 | 50 |
| 45 | + $\mathrm{I}_{5}$ | $+17$ | +19 | +22 | +24 | +27 | +29 | $+32$ | +34 | $+37$ | + 49 |
| 46 | +14 | $+16$ | +19 | +2I | +23 | +26 | $+28$ | $+30$ | +33 | +35 | $+46$ |
| 48 | 13 | 15 | 17 | 19 | 22 | 24 | 26 | 28 | 30 | 32 | 43 |
| 50 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 40 |
| 52 | + 11 | +13 | + 1.4 | +16 | +18 | +20 | +22 | +23 | +25 | $+27$ | $+36$ |
| 54 | 10 | 11 | 13 | 15 | 16 | IS | 19 | 21 | 23 | 24 | 32 |
| 56 | 9 | 10 | 12 | 13 | 14 | 16 | 17 | 19 | 20 | 22 | 29 |
| 58 |  | 9 | 10 | 11 | 13 | 1.4 | 15 | 17 | 18 | 19 | 26 |
| 60 | 7 | S | 9 | 10 | 11 | 12 | 13 | 14 | 16 | 17 | 22 |
| 62 | + 6 | + 7 | +8 | $+9$ | +10 | +11 | +II | +12 | +13 | +14 | + 19 |
| 64 |  | 6 | 6 |  | 8 | 9 | 10 | 10 | 11 | 12 |  |
| 66 | 4 | 5 | 5 | 6 | 7 | 7 | 8 | 9 | 9 | 10 | 13 |
| 68 | 3 | 4 | + | 5 | 5 | 6 | 6 | 7 | 7 | 8 | 11 |
| 70 | 2 | 3 | 3 | 4 | 4 | 4 | 5 | 5 | 6 | 6 | 8 |
| 72 | + 2 | '+2 | $+2$ | $+3$ | $+3$ |  |  |  |  |  |  |
| 74 76 | $\begin{array}{r}+ \\ + \\ + \\ + \\ \hline\end{array}$ | +1 $+\quad 1$ | + 2 +1 | +2 $+\quad 1$ | $+\quad 2$ $+\quad 1$ |  |  |  |  |  |  |
| 78 |  | 0 | $\bigcirc$ | $\bigcirc$ | - |  |  |  |  |  |  |
| 80 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - I |  |  |  |  |  |  |

Smithsonian Tables.

Table 54.
DETERMINATION OF HEIGHTS BY THE BAROMETER.
ENGLISH MEASURES.
Correction for an Average Degree of Humidity.

| Mean Temperature. | APPROXIMATE DLFFERENCE OF HEIGHT OBTAINED FROM TABLES 51-52 |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 500 | 1000 | 2000 | 3000 | 4000 | 5000 | 6000 | 7000 | 8000 | 9000 | 10000 | 20000 |
| F. $\begin{array}{r}\text { F. } \\ -20^{\circ} \\ -16 \\ -12\end{array}$ | Feet. | Feet. 0 0 0 0 | Feet. 0 0 + I | Feet. 0 +1 1 | Feet. 0 +1 I | Feet. 0 +1 2 | Feet. 0 +1 2 | Feet. +I I 2 | Feet. +I 2 3 | Feet. +1 2 3 | Feet. +1 2 3 | Feet. +2 4 6 |
| $-8$ | $\bigcirc$ | - | I | I | 2 | 2 | 3 | 3 | 4 | 4 | 4 | 9 |
| - 6 | - | $\bigcirc$ | I | I | 2 | 2 | 3 | 3 | 4 | 4 | 5 | 10 |
| - 4 | - | + I | I | 2 | 2 | 3 | 3 | 4 | 4 | 5 | 6 | II |
| - 2 | 0 | I | I | 2 | 2 | 3 | 4 | 4 | 5 | 6 | 6 | 12 |
| 0 | 0 | I | I | 2 | 3 | 3 | 4 | 5 | 5 | 6 | 7 | 14 |
| + 2 | o | I | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 | 7 | 15 |
|  | - | I | 2 | 2 | 3 | 4 | 5 | 6 | 7 | 7 | 8 | 16 |
| 6 | o | I | 2 | 3 | 4 | 4 | 5 | 6 | 7 | 8 | 9 | 18 |
| 8 | - | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 19 |
| 10 | + I | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 21 |
| 12 | 1 | I | 2 | 3 | 4 | 6 | 7 | 8 | 9 | 10 | I I | 22 |
| 14 | I | I | 2 | 4 | 5 | 6 | 7 | S | 9 | II | 12 | 24 |
| 16 | 1 | I | 3 | 4 | 5 | 6 | 8 | 9 | 10 | II | 13 | 25 |
| 18 | 1 | I | 3 | 4 | 5 | 7 | 8 | 9 | II | 12 | 13 | 27 |
| 20 | I | 1 | 3 | 4 | 6 | 7 | 9 | 10 | II | 13 | 14 | 29 |
| 22 | I | 2 | 3 | 5 | 6 | 8 | 9 | II | 12 | 14 | 15 | 3 I |
| 24 | I | 2 | 3 | 5 | 7 | 8 | Io | II | 13 | 15 | 16 | 33 |
| 26 | I | 2 | 3 | 5 | 7 | 9 | Io | 12 | 14 | 16 | 17 | 35 |
| 28 | 1 | 2 | 4 | 6 | 7 | 9 | I I | 13 | 15 | 17 | 19 | 37 |
| 30 | I | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | I 8 | 20 | 4 I |
| 32 | I | 2 | 4 | 7 | 9 | II | 13 | 16 | 18 | 20 | 22 | 44 |
| 34 | 1 | 2 | 5 | 7 | 10 | 12 | 15 | 17 | 19 | 22 | 24 | 49 |
| 36 | I | 3 | 5 | 8 | I I | 13 | 16 | 19 | 2 I | 24 | 27 | 53 |
| 38 | I | 3 | 6 | 9 | 12 | 15 | IS | 21 | 23 | 26 | 29 | 59 |
| 40 | 2 | 3 | 6 | 10 | 13 | 16 | 19 | 23 | 26 | 29 | 32 | 64 |
| 42 | 2 | 4 | 7 | II | 14 | 18 | 21 | 25 | 28 | 32 | 35 | 71 |
| 44 | 2 | 4 | 8 | 12 | 15 | 19 | 23 | 27 | 31 | 35 | 39 | 77 |
| 46 | 2 | 4 | 8 | 13 | 17 | 21 | 25 | 29 | 34 | 3 S | 42 | 84 |
| 48 | 2 | 5 | 9 | 14 | 18 | 23 | 27 | 32 | 37 | 41 | 46 | 92 |
| 50 | 2 | 5 | 10 | I5 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 99 |
| 52 | 3 | 5 | II | 16 | 21 | 27 | 32 | 37 | 43 | 48 | 53 | 107 |
| 54 | 3 | 6 | II | 17 | 23 | 29 | 34 | 40 | 46 | 51 | 57 | II4 |
| 56 | 3 | 6 | 12 | 18 | 24 | 30 | 37 | 43 | 49 | 55 | 61 | 122 |
| 58 | 3 | 6 | 13 | 19 | 26 | 32 | 39 | 45 | 52 | 58 | 65 | 130 |
| 60 | 3 | 7 | 14 | 21 | 27 | 34 | 41 | 48 | 55 | 62 | 69 | 137 |
| 62 | 4 | 7 | 14 | 22 | 29 | 36 | 43 | 5 I | 58 | 65 | 72 | 145 |
| 64 | 4 | 8 | 15 | 23 | 30 | 38 | 46 | 53 | 61 | 69 | 76 | 152 |
| 66 | 4 | 8 | 16 | 24 | 32 | 40 | 48 | 56 | 64 | 72 | So | I60 |
| 68 | 4 | 8 | 17 | 25 | 34 | 42 | 50 | 59 | 67 | 76 | S4 | 168 |
| 70 | 4 | 9 | 18 | 26 | 35 | 44 | 53 | 61 | 70 | 79 | S8 | 175 |
| 72 | 5 | 9 | IS | 27 | 37 | 46 | 55 | 64 | 73 | S2 | 91 | 183 |
| 76 | 5 | 10 | 20 | 30 | 40 | 49 | 59 | 69 | 79 | 89 | 99 | 198 |
| So | 5 | II | 21 | 32 | 43 | 53 | 64 | 75 | 85 | 96 | 106 | 213 |
| 84 | 6 | II | 23 | 34 | 46 | 57 | 68 | So | 91 | 103 | 114 | 228 |
| SS | 6 | 12 | 24 | 37 | 49 | 61 | 73 | 85 | 97 | 110 | 122 | 243 |
| 92 | 6 | 13 | 26 | 39 | 52 | 65 | 78 | 91 | IO3 | I 16 | 129 | 259 |
| 96 | 7 | 14 | 27 | 4 I | 55 | 68 | 82 | 96 | 110 | 123 | 137 | 274 |

Table 55.
DETERMINATION OF HEIGHTS BY THE BAROMETER.
ENGLISH MEASURES.
Correction for the Variation of Gravity with Altitude : $\frac{z\left(z+2 h_{0}\right)}{R}$.

| Approximate diffe, ence of height. Z. | HEIGHT OF LOWER STATION IN FEET ( $h_{0}$ ) . |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 1000 | 2000 | 3000 | 4000 | 5000 | 6000 | 7000 | 8000 | 9000 | 10000 | 12000 |
| Fee'. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| 500 | - | - | - | - | - | - | o | o | o | 0 | 0 | + I |
| 1000 | $\bigcirc$ | - | O | 0 | - | + I | + I | + I | + I | + I | +1 | I |
| 1500 | o | o | o | + I | + I | 1 | 1 | 1 | 1 | I | 2 | 2 |
| 2000 | - | - | +1 | I | I | 1 | I | 2 | 2 | 2 | 2 | 2 |
| 2500 | $\bigcirc$ | + I | 1 | I | 1 | 1 | 2 | 2 | 2 | 2 | 3 | 3 |
| 3000 | - | 1 | I | 1 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 4 |
| 3500 | + I | 1 | I | 2 | 2 | 2 | 3 | 3 | 3 | 4 | 4 | 5 |
| 4000 | 1 | 1 | 2 | 2 | 2 | 3 | 3 | 3 | 4 | 4 | 5 | 5 |
| 4500 | 1 | I | 2 | 2 | 3 | 3 | 4 | 4 | 4 | 5 | 5 | 6 |
| 5000 | I | 2 | 2 | 3 | 3 | 4 | 4 | 5 | 5 | 6 | 6 | 7 |
| 5500 | 1 | 2 | 3 | 3 | 4 | 4 | 5 | 5 | 6 | 6 | 7 | 8 |
| 6000 | 2 | 2 | 3 | 3 | 4 | 5 | 5 | 6 | 6 | 7 | 7 | 9 |
| 6500 | 2 | 3 | 3 | 4 | 5 | 5 | 6 | 6 | 7 | S | S | 9 |
| 7000 | 2 | 3 | 4 | 4 | 5 | 6 | 6 | 7 | 8 | 8 | 9 | 10 |
| 7500 | 3 | 3 | 4 | 5 | 6 | 6 | 7 | S | 8 | 9 | 10 | II |
| Sooo | 3 | 4 | 5 | 5 | 6 | 7 | S | 8 | 9 | 10 | II | 12 |
| 8500 | 3 | 4 | 5 | 6 | 7 | S | S | 9 | 10 | II | 12 | 13 |
| 9000 | 4 | 5 | 6 | 6 | 7 | 8 | 9 | 10 | II | 12 | 12 | 14 |
| 9500 | 4 | 5 | 6 | 7 | S | 9 | 10 | I I | 12 | 13 | 13 | 15 |
| 10000 | 5 | 6 | 7 | S | 9 | 10 | 11 | 11 | 12 | 13 | If | 16 |
| 11000 | 6 | 7 | S | 9 | 10 | I I | 12 | 13 | 14 | 15 | 16 | 15 |
| 12000 | 7 | S | 9 | 10 | II | 13 | 14 | 15 | 16 | 17 | IS | 2 I |
| 13000 | S | 9 | II | 12 | 13 | 14 | 16 | 17 | IS | 19 | 21 | 23 |
| 14000 | 9 | 11 | 12 | 13 | 15 | 16 | 17 | 19 | 20 | 2 I | 23 | 25 |
| 15000 | 1 I | 12 | 14 | I5 | 17 | 18 | 19 | 2 I | 22 | 24 | 25 | 28 |
| 16000 | 12 | 14 | 15 | 17 | IS | 20 | 21 | 23 | 25 | 26 | 28 | 3 I |
| 17000 | 14 | 15 | 17 | 19 | 20 | 22 | 2.4 | 25 | 27 | 28 | 30 |  |
| I Sooo | 16 | 17 | 19 | 21 | 22 | 2.4 | 26 | 28 | 30 | 3 I |  |  |
| 19000 | 17 | 19 | 21 | 23 | 25 | 26 | 2 S | 30 | 32 |  |  |  |
| 20000 | 19 | 21 | 23 | 25 | 27 | 29 | 31 |  |  |  |  |  |

## DETERMINATION OF HEIGHTS BY THE BAROMETER. METRIC MEASURES.

Values of $18400 \log \frac{760}{B}$.

| Barometric Pressure. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm . | m. | m. | m. | m. | m. | m. | m. | m. | . | 1 m. |
| 300 | 7428 | 7401 | 7375 | 7348 | 7322 | 7296 | 7270 | 7244 | 72 IS | 19. |
| 310 | 7166 | 7140 | 7115 | $7 \mathrm{OS9}$ | 7064 | 7038 | 7013 | 6987 | 6962 | 6937 |
| 320 | 6912 | 6887 | 6862 | 6838 | 6813 | 6-59 | 6764 | 6740 | 6715 | 6691 |
| 330 | 6666 | 6642 | 6618 | 6594 | 6570 | 6546 | 6522 | 6498 | 6475 | 6451 |
| 340 | 6428 | 6405 | 63 SI | 6358 | 6334 | 6311 | 6288 | 6265 | 6242 | 6219 |
| 350 | 6196 | 6173 | 6151 | 6128 | 6106 | 6083 | 6061 | 6038 | 6016 |  |
| 360 | 5971 | 5949 | 5927 | 5905 | 5883 | 5861 | 5839 | ${ }_{5} \mathrm{~S}_{7}$ | 5795 | 5993 5773 |
| 370 350 | 5752 | 5730 | 5709 | 5687 | 5666 | 5644 | 5623 | 5602 | 558 I | 5560 |
| 350 | 5539 | 5518 | 5497 | 5476 | 5455 | 5434 | 5414 | 5393 | 5373 | 5352 |
| 390 | 5332 | 53 II | 5291 | 5270 | 5250 | 5229 | 5209 | 5189 | 5169 | 5I49 |
| 400 | 5129 | 5109 | 5089 | 5069 | 5049 | 5029 | 5010 | 4990 | 4971 |  |
| 410 420 | 4932 4739 | 4912 | 4893 | 4873 | 4854 | 4834 | $4 \mathrm{SI}_{5}$ | 4796 | 4977 | 4951 4758 |
| 420 | 4739 | 4720 | 4701 | 4682 | 4663 | 46.44 | 4625 | 4606 | 45 SS | 4569 |
| 430 | 4551 | 4532 | 4514 | 4495 | 4477 | 4458 | 4440 | 4422 | 4404 | 4386 |
| 440 | 4368 | 4350 | 4332 | 4314 | 4296 | 4278 | 4260 | 4242 | 4224 | 4206 |
| 450 | 4188 | 4170 | 4152 | 4134 | 4117 | 4099 | 4082 | 4064 | 4047 | 4029 |
| 460 | 4 OI 2 | 3994 | 3977 | 3959 | 3942 | 3925 | 3908 | 3891 | 3874 | 3857 |
| 470 | 3840 3672 | 3823 | 3806 | 3789 | 3772 | 3755 | 3738 | 3721 | 3705 | 3688 |
| 490 | 3672 3507 | 3655 | 3639 | 3622 | 3606 | 3589 | 3573 | 3556 | 3540 | 3523 |
| 490 | 3507 | 3490 | 3474 | 3458 | 3442 | 3426 | 3410 | 3394 | 3378 | 3362 |
| 500 | 3346 | 3330 | 3314 | 3298 | 3282 | 3266 | 3250 | 3235 | 3219 |  |
| 510 520 | 3188 | 3172 3017 | 3157 | 3141 | 3126 | 3110 | 3095 | 3235 | 3064 | 3203 3048 |
| 520 530 | 3033 2880 | 3017 | 3002 | 2986 | 2971 | 2955 | 2940 | 2925 | 2910 | 2895 |
| 530 | 2880 | 2865 | 2850 | 2835 | 2820 | 2 SO 5 | 2790 | 2775 | 2760 | 2745 |
| 540 | 2731 | 2716 | 2701 | 2687 | 2672 | 2657 | 2643 | 2628 | 2613 | 2599 |
| 550 | 2584 | 2570 | 2555 | 2541 | 2526 | 2512 | 2497 | 2.483 | 2468 | 2454 |
| 560 | 2440 | 2426 | 2411 | 2397 | 2383 | 2369 | 2355 | 234 I | 2327 | 2313 |
| 570 | 2299 | 2285 | 2271 | 2257 | 2243 | 2229 | 2215 | 2201 | 2 ISS | 2174 |
| 580 590 | 2160 | 2146 | 2133 | 2119 | 2105 | 2092 | 2078 | 2064 | 2051 | 2037 |
| 590 | 2023 | 2010 | 1996 | 1983 | 1969 | 1956 | 1942 | 1929 | 1915 | 1902 |
| 600 | I889 | 1875 | I862 | I $\mathrm{S}_{4} 8$ | 1835 | 1822 | 1809 | 1796 | 1783 | 1770 |
| 610 | 1757 | 1744 | 1731 | 1718 | 1705 | 1692 | 1679 | 1666 | 1653 | 1640 |
| 620 | 1627 | 1614 | 1601 | 1588 | 1576 | 1563 | 1550 | 1537 | 1525 | ${ }^{1} 1212$ |
| 630 640 | 1499 | 1486 | 1474 | 1461 | 1448 | 1436 | 1423 | 1411 | I 398 | 1386 |
| 640 | 1373 | 1361 | 1348 | I 336 | 1323 | - I3II | 1298 | 1286 | 1273 | I 261 |
| 650 | 1249 | 1236 | 1224 | 1212 | 1199 | 1187 | I 175 | 1163 |  |  |
| 660 670 | 1127 | III5 | 1103 | 1091 | 1079 | 1067 | 1055 | 1043 | 1151 | 1139 1019 |
| 670 680 | 1007 889 | 995 | 983 | 971 | 960 | 948 | 936 | 924 | 913 | 901 |
| 680 690 | SS9 772 | 877 761 | 866 | 854 | 842 | 831 | 819 | 807 | 796 | 784 |
| 690 | 772 | 761 | 749 | 738 | 726 | 715 | 703 | 692 | 680 | 669 |
| 700 | 657 | 646 | 635 | 623 | 612 | 601 | 589 | 578 | 567 | 555 |
| 710 | 544 | 533 | 52 I | 510 | 499 | 487 | 476 | 465 | 454 | 443 |
| 720 | 432 | 42 I | 410 | 399 | 3 SS | 377 | 366 | 355 | 344 | 333 |
| 730 | 322 | 3 II | 300 | 2 S 9 | 278 | 267 | 256 | 245 | 234 | 224 |
| 740 | 213 | 202 | 192 | 181 | 170 | 160 | 149 | 138 | 128 | 117 |
| $750+$ | + 106 | + 95 | $+85$ | + 74 | + 64 | $+53$ |  | + 32 | + 22 | + II |
| 760 | 0 | - 10 | - 21 | - 31 | - 42 | - 52 | + 63 | + 73 | - 83 | - 94 |
| 770 | - 104 | - II5 | - 125 | - I 36 | -146 | $-156$ | $-166$ | -177 | $-\mathrm{IS} 7$ | -197 |

[^28]Table 57.
DETERMINATION OF HEIGHTS BY THE BAROMETER. DYNAMIC MEASURES.
Values of $18400 \log \frac{1013.3}{B}$

| Barometric Pressure | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mb . | m. | m. | m. | m. | m. | m. | m. | m. | m, | m. |
| 0 | $\infty$ | 55306 | 49767 | 46527 | 44228 | 42445 | 40988 | 39756 | 38689 | 37748 |
| 10 | 36906 | 36144 | 35448 | 34809 | 34217 | 33666 | 33150 | 32665 | 32209 | 31777 |
| 20 | 31367 | 30977 | 30605 | 30250 | 29910 | 29584 | 29270 | 2 S 969 | 28678 | 28397 |
| 30 | 28127 | 27865 | 27611 | 27365 | 27126 | 20895 | 26670 | 26451 | 26238 | 26031 |
| 40 | 25828 | 25630 | 25438 | 25250 | 25066 | 24887 | 24711 | 24539 | 24371 | 24206 |
| 50 | 24043 | 23886 | 23731 | 23579 | 23430 | 23283 | 23139 | 22998 | 22859 | 22722 |
| 60 | 22588 | 22456 | 22326 | 22198 | 22072 | 21948 | 21827 | 21706 | 21587 | 21471 |
| 70 | 21356 | 21242 | 21131 | 21021 | 20912 | 20805 | 20699 | 20594 | 20491 | 20389 |
| So | 20289 | 20189 | 20092 | 19995 | 19899 | 19804 | 1971 I | 19618 | 19527 | 19437 |
| 90 | 19348 | 19259 | 19172 | 19086 | 19000 | 18916 | 18832 | 18749 | 18667 | 18586 |
| 100 | 18506 | 18426 | 18347 | 18269 | 18192 | 18116 | 18040 | 17965 | 17891 | 17817 |
| 110 | 17744 | 17672 | 17600 | 17529 | 17459 | 17389 | 17320 | I725I | 17183 | 17115 |
| 120 | 17049 | 16982 | 16917 | 16851 | 16787 | 16722 | 16659 | 16596 | 16533 | 16471 |
| 130 | 16409 | 16348 | 16287 | 16227 | 16167 | 16108 | 16048 | ${ }^{1} 5990$ | 15932 | 15874 |
| 140 | 15817 | 15760 | 15703 | 15647 | 15592 | 15536 | 15482 | I 5427 | 15373 | 15319 |
| 150 | 15266 | 15212 | 15160 | 15107 | 15055 | 15004 | 14952 | 14901 | 14850 | 14800 |
| 160 | 14750 | 14700 | 14650 | 14601 | 14553 | 14504 | 14456 | 14408 | 14360 | 14312 |
| 170 | 14265 | 14218 | 14172 | 14125 | 14079 | 14034 | I 3988 | 13943 | 13898 | 13853 |
| 180 | 13800 | 13764 | 13720 | 13677 | 13633 | 13590 | 13547 | 1350.4 | 13461 | 13419 |
| r90 | 13377 | 13335 | 13293 | 13251 | 13210 | 13169 | 13128 | 13087 | 13047 | 13007 |
| 200 | 12967 | 12927 | 12887 | 12848 | $12 \mathrm{So8}$ | 12769 | 12730 | :2692 | 12653 | 12615 |
| 210 | 12577 | 12539 | 12501 | 12463 | 12426 | 12389 | 12352 | 12315 | 12278 | 12242 |
| 220 | 12205 | 12169 | 12133 | 12097 | I 2061 | 12026 | 11990 | 11955 | 11920 | 11885 |
| 230 | 11850 | IISI5 | 11781 | I 1746 | 11712 | 11678 | 11644 | 11610 | 11577 | 11543 |
| 240 | 11510 | 11476 | 11443 | 11410 | 11378 | 11345 | 11312 | 11280 | 11248 | 11216 |
| 250 | 11184 | III $5^{2}$ | 11120 | 11088 | 11057 | 11025 | 10994 | 10963 | 10932 | 10901 |
| 260 | 10870 | 10839 | 10809 | 10778 | 10748 | 10718 | 10688 | 10658 | 10628 | 10598 |
| 270 | 10569 | 10539 | 10510 | 10480 | 10451 | 10422 | 10393 | 10364 | 10335 | 10307 |
| 280 | 10278 | 10249 | 10221 | 10193 | 10165 | 10137 | 10108 | 100SI | 10053 | 10025 |
| 290 | 9997 | 9970 | 9943 | 9915 | 9888 | 9861 | 9834 | $9 \mathrm{So7}$ | 9780 | 9753 |
| 300 | 9727 | 9700 | 9674 | 9647 | 9621 | 9594 | 9568 | 9542 | 9516 | 9490 |
| 310 | 9465 | 9439 | 9413 | 9388 | 9362 | 9337 | 9311 | 9286 | 9261 | 9236 |
| 320 | 9211 | 9186 | 9161 | 9136 | 9111 | 9087 | 9062 | 9038 | 9014 | 8989 |
| 330 | S965 | 8941 | 8917 | 8893 | 8869 | 8845 | 882 I | 8797 | 8773 | 8750 |
| 340 | 8726 | 8703 | 8679 | 8656 | 8633 | 8610 | 8587 | 8564 | 8541 | 8518 |
| 350 | 8495 | 8472 | 8449 | 8427 | 8404 | 83 SI | S359 | 8336 | 8314 | 8292 |
| 360 | 8270 | 8247 | 8225 | 8203 | 8181 | 8159 | 8138 | 8116 | 8094 | 8073 |
| 370 | 8051 | 8029 | 8008 | 7986 | 7965 | 7943 | 7922 | 7901 | 7880 | 7859 |
| 380 | 7838 | 7817 | 7796 | 7775 | 7754 | 7733 | 7712 | 7692 | 7671 | 7651 |
| 390 | 7630 | 7610 | 7589 | 7569 | 7548 | 7528 | 7508 | 7488 | 7468 | 7448 |
| 400 | 7428 | 7408 | 7388 | 7368 | 7348 | 7328 | 7309 | 7289 | 7269 | 7250 |
| 410 | 7230 | 7211 | 7191 | 7172 | 7153 | 7133 | 7114 | 7095 | 7076 | 7057 |
| 420 | 7038 | 7019 | 7000 | 6981 | 6962 | 6943 | 6924 | 6906 | 6887 | 6868 |
| 430 | 6850 | 6831 | 6813 | 6794 | 6776 | 6757 | 6739 | 6721 | 6703 | 6684 |
| 440 | 6666 | 6648 | 6630 | 6612 | 6594 | 6576 | 6558 | 6540 | 6522 | 6504 |
| 450 | 6487 | 6469 | 6451 | 6433 | 6416 | 6398 | 6381 | 6363 | 6346 | 6328 |
| 460 | 6311 | 6294 | 6276 | 6259 | 6242 | 6225 | 6207 | 6190 | 6173 | 6156 |
| 470 | 6139 | 6122 | 6105 | 6088 | 6071 | 6055 | 6038 | 6021 | 6004 | 5987 |
| 480 | 5071 | 5954 | 5937 | 5921 | 5004 | 5888 | 5871 | 5855 | 5839 | 5822 |
| 490 | 5806 | 5790 | 5773 | 5757 | 5741 | 5725 | 5709 | 5693 | 5677 | 5661 |

Table 57.
DETERMINATION OF HEIGHTS BY THE BAROMETER. DYNAMIC MEASURES.

Values of $18400 \log \frac{1013.3}{B}$

| Barometric Pressure | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mb. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. |
| 500 | 5645 | 5629 | 5613 | 5597 | 5581 | 5565 | 55.49 | 5533 | 5518 | 5502 |
| 510 | 5486 | 5471 | 5455 | 5439 | 5424 | 5408 | 5393 | 5377 | 5362 | 5346 |
| 520 | 5331 | 5316 | 5300 | 5285 | 5270 | 5255 | 5239 | 5224 | 5209 | 5194 |
| 530 | 5179 | 5164 | 5149 | 5134 | 5119 | 5104 | 5089 | 5074 | 5059 | 5044 |
| 540 | 5030 | 5015 | 5000 | 4985 | 4971 | 4950 | 4941 | 4927 | 4912 | 4898 |
| 550 | 4883 | 4868 | 4854 | 4839 | 4825 | 4811 | 4796 | 4782 | 4768 | 4753 |
| 560 | 4739 | 4725 | 4710 | 4696 | 4682 | 4668 | 4654 | 4640 | 4626 | 4612 |
| 570 | 4598 | 4583 | 4569 | 4556 | 4542 | 4528 | 4514 | 4500 | 4486 | 4472 |
| 580 | 4459 | 4445 | 4431 | 4417 | 4404 | 4390 | 4376 | 4363 | 4349 | 4335 |
| 590 | 4322 | 4308 | 4295 | 4281 | 4268 | 4254 | 42.41 | 4228 | 4214 | 4201 |
| 600 | 4188 | 4174 | 4161 | 4148 | 4134 | 4121 | 4108 | 4095 | 4082 | 4069 |
| 610 | 4056 | 4042 | 4029 | 4016 | +003 | 3990 | 3977 | 3964 | 3951 | 3939 |
| 620 | 3926 | 3913 | 3900 | 3887 | 3874 | 3861 | 3849 | 3836 | 3823 | 3810 |
| 630 | 3798 | 3785 | 3772 | 3760 | 3747 | 3735 | 3722 | 3709 | 3697 | 3684 |
| 640 | 3672 | 3659 | 3647 | 3635 | 3622 | 3610 | 3597 | 3585 | 3573 | 3560 |
| 650 | 3548 | 3536 | 3523 | 351 I | 3499 | 3487 | 3475 | 3462 | 3450 | 3438 |
| 660 | 3426 | 3414 | 3402 | 3390 | 3378 | 3366 | 3354 | 3342 | 3330 | 3318 |
| 670 | 3306 | 3294 | 3282 | 3270 | 3258 | 3246 | 3235 | 3223 | 3211 | 3199 |
| 680 | 3187 | 3176 | 3164 | 3152 | 3141 | 3129 | 3117 | 3106 | 3094 | 3082 |
| 690 | 3071 | 3059 | 3048 | 3036 | 3025 | 3013 | 3002 | 2990 | 2979 | 2967 |
| 700 | 2956 | 2944 | 2933 | 2922 | 2910 | 2899 | 2888 | 2876 | 2865 | 2854 |
| 710 | 2842 | 2831 | 2820 | 2809 | 2798 | 2786 | 2775 | 2764 | 2753 | 2742 |
| 720 | 2731 | 2720 | 2708 | 2697 | 2686 | 2675 | 2664 | 2653 | 2642 | 2631 |
| 730 | 2621 | 2609 | 2599 | 2588 | 2577 | 2566 | 2555 | 2544 | 2533 | 2523 |
| 740 | 2512 | 2501 | 2490 | 2479 | 2469 | 2458 | 2447 | 2437 | 2426 | 2415 |
| 750 | 2405 | 2394 | 2383 | 2373 | 2362 | 2351 | 2341 | 2330 | 2320 | 2309 |
| 760 | 2299 | 2288 | 2278 | 2267 | 2257 | 22.46 | 2236 | 2225 | 2215 | 2205 |
| 770 | 219.4 | 2184 | 2173 | 2163 | 2153 | 2142 | 2132 | 2122 | 2112 | 2101 |
| 780 | 2091 | 2081 | 2071 | 2060 | 2050 | 2040 | 2030 | 2020 | 2009 | 1999 |
| 790 | 1989 | 1979 | 1969 | 1959 | 1949 | 1939 | 1929 | 1919 | 1909 | 1899 |
| 800 | 1889 | 1879 | 1869 | 1859 | 1849 | 1839 | 1829 | 18 I9 | 1809 | 1799 |
| 810 | 1789 | 1780 | 1770 | 1760 | 1750 | 1740 | 1731 | 1721 | 1711 | 1701 |
| 820 | 1692 | 1682 | 1672 | 1662 | 1653 | 1643 | 1633 | 1623 | 1614 | 1604 |
| 830 | 1595 | 1585 | 1575 | 1566 | 1556 | 1547 | 1537 | 1527 | 1518 | 1508 |
| 840 | 1499 | 1489 | 1480 | 1470 | 1461 | 1451 | 1442 | 1433 | 1423 | 1414 |
| 850 | 1404 | 1395 | 1386 | 1376 | 1367 | 1357 | 1348 | 1339 | 1329 | 1320 |
| 860 | 1311 | 1302 | 1292 | 1283 | 1274 | 1264 | 1255 | 1246 | 1237 | 1228 |
| 870 | 1218 | 1209 | 1200 | 1191 | 1182 | 1173 | 1164 | 1154 | 1145 | 1136 |
| 880 | 1127 | 1118 | 1109 | 1100 | 1091 | 1082 | 1073 | 1064 | 1055 | 1046 |
| 890 | 1037 | 1028 | 1019 | 1010 | 1001 | 992 | 983 | 974 | 965 | 956 |
| 900 | 948 | 939 | 930 | 92 I | 912 | 903 | S94 | 886 | 877 | 868 |
| 910 | 859 | 850 | 842 | 833 | 824 | 815 | 807 | 798 | 789 | 781 |
| 920 | 772 | 763 | 755 | 746 | 737 | 729 | 720 | 711 | 703 | 694 |
| 930 | 686 | 677 | 668 | 660 | 651 | 643 | 634 | 626 | 617 | 608 |
| 940 | 600 | 592 | 583 | 575 | 566 | $55^{8}$ | 549 | 54 I | 532 | 524 |
| 950 | 516 | 507 | 499 | 490 | 482 | 474 | 465 | 457 | 448 | 440 |
| 960 | 432 | 424 | 415 | 407 | 399 | 390 | 382 | 374 | 365 | 357 |
| 970 | 349 | 34 I | 332 | 324 | 316 | 308 | 300 | 292 | 283 | 275 |
| 980 | 267 | 259 | 251 | 243 | 234 | 226 | 218 | 210 | 202 | 194 |
| 990 | 186 | 178 | 170 | 162 | 154 | 146 | 138 | 130 | 122 | 114 |
| 1000 | 106 | 98 | 90 | 82 | 74 | 66 | 58 | 50 | 42 | 34 |
| 1010 | 26 | 18 | 10 | 2 | - 6 | - 13 | - 21 | - 29 | - 37 | - 45 |
| 1020 | - 53 | -61 | - 68 | $-76$ | - 84 | - 92 | $-100$ | $-107$ | - 115 | -123 |
| 1030 | -131 | -138 | -146 | - I54 | -162 | $-169$ | -177 | $-185$ | -192 | $-200$ |
| 1040 | -208 | $-215$ | $-223$ | $-231$ | $-238$ | -246 | -254 | -261 | -269 | -277 |

Table 58.
DETERMINATION OF HEIGHTS BY THE BAROMETER.
METRIC MEASURES.
Temperature correction factor, $a=.00367 \theta$.
Multiply approximate altitudes, determined from table 56 or 57 . by values of a corresponding to mean temperature, $\theta$, of air column. Add, if $\theta$ is above $0^{\circ} \mathrm{C}$; subtract, if below $\circ^{\circ} \mathrm{C}$.

| Mean Temp. $\theta$ | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{C}$. | a. | a. | a. | a. | a. | $a$. | $a$. | $a$. | $a$. | $a$. |
| 0 | 0.000 | 0.000 | 0.001 | 0.001 | 0.001 | 0.002 | 0.002 | 0.003 | 0.003 | 0.003 |
| 1 | . 004 | .004 | . 004 | . 005 | . 005 | . 006 | . 006 | . 006 | . 007 | . 007 |
| 2 | . 007 | . 008 | . 008 | . 008 | . 009 | . 009 | . 010 | . 010 | . 010 | . 011 |
| 3 | . 011 | . 011 | . 012 | . 012 | . 012 | . 013 | . 013 | . 014 | . 014 | . 014 |
| 4 | . 015 | .015 | .015 | . 016 | . 016 | . 017 | . 017 | . 017 | . 018 | . 018 |
| 5 | . 018 | . 019 | .or9 | . 19 | . 020 | . 020 | . 221 | . 021 | . 021 | . 022 |
| 6 | . 022 | . 022 | . 023 | . 023 | . 023 | . 024 | . 024 | . 025 | . 025 | . 025 |
| 7 | . 026 | . 026 | . 026 | . 027 | . 027 | . 028 | . 028 | . 028 | . 029 | . 029 |
| 8 | . 029 | . 030 | . 030 | . 030 | . 031 | . 031 | .032 | . 032 | . 032 | . 033 |
| 9 | . 033 | . 033 | .0,34 | . 034 | . 034 | . 035 | . 035 | . 036 | .036 | . 036 |
| 10 | . 037 | . 037 | . 037 | . 038 | . 038 | . 039 | . 039 | . 039 | . 040 | . 040 |
| 11 | . 040 | . 041 | . 041 | . $0+1$ | . 042 | . 042 | . 043 | . 043 | . 043 | . 044 |
| 12 | . 044 | . 044 | . 045 | . 045 | . 046 | . 046 | . 046 | . 047 | . 047 | . 047 |
| 13 | . 048 | . 0.48 | . 048 | . 049 | . 049 | . 050 | . 050 | . 050 | . 051 | . 051 |
| 14 | .051 | .052 | . 052 | . 352 | . 053 | . 053 | . 054 | . 054 | . 054 | . 055 |
| 15 | . 055 | . 055 | . 056 | . 056 | . 057 | . 057 | . 057 | . 058 | .058 | .058 |
| 16 | . 059 | . 059 | . 059 | . 060 | . 060 | . 061 | . 061 | . 061 | . 062 | . 062 |
| 17 | . 062 | . 063 | . 063 | .063 | . 064 | . 064 | . 065 | . 065 | . 065 | . 066 |
| 18 | . 066 | . 066 | . 067 | .067 | . 068 | . 068 | . 068 | . 069 | . 069 | . 069 |
| 19 | . 070 | . 070 | . 070 | . 071 | . 071 | . 072 | . 072 | . 072 | . 073 | . 073 |
| 20 | . 073 | . 074 | . 074 | . 075 | . 075 | . 075 | . 076 | .076 | . 076 | . 077 |
| 2 I | . 077 | . 077 | . 078 | . 078 | . 079 | . 079 | . 079 | . 080 | . 080 | . 080 |
| 22 | . 081 | . 081 | . 081 | .082 | . 082 | . 083 | . 083 | . 083 | . 084 | . 084 |
| 23 | . 08.8 | . 085 | . 085 | . 086 | . 086 | . 086 | . 087 | . 087 | . 087 | . 088 |
| 24 | . 088 | . 088 | . 089 | .089 | . 090 | . 090 | . 090 | .091 | .09I | .091 |
| 25 | . 092 | . 092 | . 002 | . 093 | . 093 | . 094 |  |  |  | . 095 |
| 26 | . 095 | . 096 | . 096 | . 097 | . 097 | . 097 | . 098 | . 098 | . 098 | . 099 |
| 27 | . 099 | . 099 | . 100 | . 100 | . 101 | . 101 | . 101 | . 102 | . 102 | . 102 |
| 28 | . 103 | .103 | . 103 | . 104 | . 104 | . 105 | . 105 | . 105 | . 106 | . 106 |
| 29 | . 106 | .107 | . 107 | . 108 | . 108 | . 108 | .109 | . 109 | .109 | . 110 |
| 30 | . 110 | . 110 | . 111 | . 111 | . 112 | . 112 | . 112 | . 113 | . 113 | . 113 |
| 31 | . 114 | . 114 | . 115 | . 115 | . 115 | . 116 | . 116 | . 116 | . 117 | . 117 |
| 32 | .117 | . 118 | . 118 | .119 | . 119 | . 119 | .120 | . 120 | . 120 | . 121 |
| 33 | . 121 | . 121 | . 122 | . 122 | .123 | . 123 | . 123 | . 124 | .124 | . 124 |
| 34 | . 125 | . 125 | . 126 | . 126 | . 126 | . 127 | . 127 | . 127 | . 128 | . 128 |
| 35 | . 128 | . 129 | . 129 | . 130 | .130 | . 130 | . 131 | . 131 | . 131 | . 132 |
| 36 | . 132 | . 132 | . 133 | . 133 | . 134 | . 134 | . 34 | . 135 | . 135 | . 135 |
| 37 | . 136 | . 136 | .137 | . 137 | . 137 | . 138 | . 38 | .'38 | . 139 | . 139 |
| 38 | . 139 | . 140 | .140 | .141 | .141 | . 141 | .142 | . 142 | .142 | . 143 |
| 39 | . 143 | . $1+3$ | . 144 | . $14+$ | . 145 | . 145 | . 145 | . 146 | .146 | . 146 |
| 40 | . 147 | . 147 | . 148 | . 148 | .148 | . 149 | . 149 | . 149 | . 150 | . 150 |
| 41 | . 150 | . 151 | .151 | . 152 | . 152 | . 152 | . 153 | . 153 | . 153 | . 154 |
| 42 | . 154 | . 155 | . 155 | . 155 | . 150 | . 156 | .156 | . 157 | . 157 | . 157 |
| 43 | . 158 | . 158 | . 159 | . 159 | . 159 | . 160 | . 160 | . 160 | . 161 | . 161 |
| 44 | . 161 | . 162 | . 162 | . 163 | .163 | . 163 | . 164 | . 164 | . 164 | . 165 |
| 45 | . 165 | . 166 | . 166 | . 166 | .167 | .167 | .167 | . 168 | . 168 | . 168 |
| 46 | . 169 | . 169 | .170 | . 170 | . 170 | . 171 | . 171 | . 171 | . 172 | . 172 |
| 47 | . 172 | . 173 | .173 | . 174 |  | . 174 | . 175 | . 175 | . 175 | . 176 |
| 48 | . 176 | .177 | .177 | .177 | . 178 | .178 | .178 | . 179 | . 179 | .179 |
| 49 | . 180 | . 180 | .181 | .181 | .181 | . 182 | . 182 | . 182 | . 183 | .183 |
| 50 | . 184 | .184 | .184 | . 185 | .185 | .185 | . 186 | . 186 | . 186 | . 187 |

## DETERMINATION OF HEIGHTS BY THE BAROMETER.

METRIC MEASURES.
Term for Temperature: $0.00367 \theta \times z$.
For temperatures $\left\{\begin{array}{l}\text { above } o^{\circ} \mathrm{C} . \\ \text { below } 0^{\circ} \mathrm{C} .\end{array}\right\}$ the values are to be $\left\{\begin{array}{l}\text { added. } \\ \text { subtracted. }\end{array}\right.$

| Approximate difference of height. 2. | MEAN TEMPERATURE OF AIR COLUMN IN CENTIGRADE DEGREES $(\theta)$. |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $1{ }^{\circ}$ | $2^{\circ}$ | $3^{\circ}$ | $4^{\circ}$ | $5^{\circ}$ | $6^{\circ}$ | $7^{\circ}$ | $8^{\circ}$ | $9^{\circ}$ | $10^{\circ}$ | $20^{\circ}$ | $30^{\circ}$ | $40^{\circ}$ |
| m. | m. | m. | m. | m. | m . | m. | m. | m. | m. | m. | m. | m. | m. |
| 100 | 0 | 1 | 1 | 1 | 2 | 2 | 3 | 3 | 3 | 4 | 7 | 11 | 15 |
| 200 | I | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 | 7 | 15 | 22 | 29 |
| 300 | 1 | 2 | 3 | 4 | 6 | 7 | 8 | 9 | 10 | 1 I | 22 | 33 | 44 |
| 400 | I | 3 | 4 | 6 | 7 | 9 | 10 | 12 | 13 | 15 | 29 | 44 | 59 |
| 500 | 2 | 4 | 6 | 7 | 9 | II | 13 | 15 | 17 | 18 | 37 | 55 | 73 |
| 600 | 2 | 4 | 7 | 9 | II | 13 | 15 | 18 | 20 | 22 | 44 | 66 | S8 |
| 700 | 3 | 5 | 8 | 10 | 13 | 15 | 18 | 21 | 23 | 26 | 51 | 77 | 103 |
| 800 | 3 | 6 | 9 | 12 | 15 | I8 | 21 | 23 | 26 | 29 | 59 | 88 | 117 |
| 900 | 3 | 7 | 10 | 13 | 17 | 20 | 23 | 26 | 30 | 33 | 66 | 99 | 132 |
| 1000 | 4 | 7 | 11 | 15 | 18 | 22 | 26 | 29 | 33 | 37 | 73 | 110 | 147 |
| 1100 | 4 | 8 | 12 | 16 | 20 | 24 | 28 | 32 | 36 | 40 | 81 | 121 | 161 |
| I 200 | 4 | 9 | 13 | 18 | 22 | 26 | 31 | 35 | 40 | 44 | 85 | 132 | 176 |
| 1300 | 5 | 10 | 14 | 19 | 24 | 29 | 33 | 38 | 43 | 48 | 95 | 143 | 191 |
| 1400 | 5 | 10 | 15 | 21 | 26 | 3 I | 36 | 41 | 46 | 51 | 103 | 154 | 206 |
| 1500 | 6 | II | 17 | 22 | 28 | 33 | 39 | 44 | 50 | 55 | 110 | 165 | 220 |
| 1600 | 6 | 12 | 18 | 23 | 29 | 35 | 41 | 47 | 53 | 59 | 117 | 176 | 235 |
| 1700 | 6 | 12 | 19 | 25 | 31 | 37 | 44 | 50 | 56 | 62 | 125 | 187 | 250 |
| I 800 | 7 | 13 | 20 | 26 | 33 | 40 | 46 | 53 | 59 | 66 | 132 | 198 | 264 |
| 1900 | 7 | 14 | 21 | 28 | 35 | 42 | 49 | 56 | 63 | 70 | 139 | 209 | 279 |
| 2000 | 7 | I5 | 22 | 29 | 37 | 44 | 51 | 59 | 66 | 73 | 147 | 220 | 294 |
| 2100 | S | 15 | 23 | 3 I | 39 | 46 | 54 | 62 | 69 | 77 | 154 | 231 | 308 |
| 2200 | 8 | 16 | 24 | 32 | 40 | 48 | 57 | 65 | 73 | 81 | 161 | 242 | 323 |
| 2300 | S | 17 | 25 | 34 | 42 | 51 | 59 | 68 | 76 | 84 | 169 | 253 | 33 S |
| 2400 | 9 | 18 | 26 | 35 | 44 | 53 | 62 | 70 | 79 | 88 | 176 | 264 | 352 |
| 2500 | 9 | 18 | 28 | 37 | 46 | 55 | 64 | 73 | 83 | 92 | 184 | 275 | 367 |
| 2600 | 10 | 19 | 29 | 38 | 48 | 57 | 67 | 76 | 86 | 95 | 191 | 286 | 382 |
| 2700 | 10 | 20 | 30 | 40 | 50 | 59 | 69 | 79 | 89 | 99 | 198 | 297 | 396 |
| 2800 | 10 | 21 | 31 | 41 | 51 | 62 | 72 | 82 | 92 | 103 | 206 | 308 | 411 |
| 2900 | I I | 21 | 32 | 43 | 53 | 64 | 75 | 85 | 96 | 106 | 213 | 319 | 426 |
| 3000 | II | 22 | 33 | 44 | 55 | 66 | 77 | 88 | 99 | 110 | 220 | 330 | 440 |
| 3100 | II | 23 | 34 | 46 | 57 | 68 | 80 | 91 | 102 | 114 | 228 | 341 | 455 |
| 3200 | 12 | 23 | 35 | 47 | 59 | 70 | S2 | 94 | 106 | 117 | 235 | 352 | 470 |
| 3300 | 12 | 24 | 36 | 48 | 61 | 73 | 85 | 97 | 109 | 121 | 242 | 363 | 484 |
| 3400 | 12 | 25 | 37 | 50 | 62 | 75 | 87 | 100 | 112 | 125 | 250 | 374 | 499 |
| 3500 | 13 | 26 | 39 | 5 I | 64 | 77 | 90 | 103 | 116 | 128 | 257 | 385 | 514 |
| 3600 | 13 | 26 | 40 | 53 | 66 | 79 | 92 | 106 | 119 | 132 | 264 | 396 | 528 |
| 3700 | 14 | 27 | 41 | 54 | 68 | 8 I | 95 | 109 | 122 | 136 | 272 | 407 | 543 |
| 3800 | 14 | 28 | 42 | 56 | 70 | 84 | 98 | 112 | 126 | 139 | 279 | 418 | 558 |
| 3900 | 14 | 29 | 43 | 57 | 72 | S6 | 100 | II5 | 129 | 143 | 286 | 429 | 573 |
| 4000 | 15 | 29 | 44 | 59 | 73 | 88 | 103 | 117 | 132 | 147 | 294 | 440 | 587 |
| 5000 | 18 | 37 | 55 | 73 | 92 | 110 | 128 | 147 | 165 | 183 | 367 | 551 | 734 |
| 6000 | 22 | 44 | 66 | 88 | 110 | 132 | 154 | 176 | 198 | 220 | 440 | 661 | 831 |
| 7000 | 26 | 5 I | 77 | 103 | 128 | 154 | 180 | 206 | 231 | 257 | 514 | 771 | 1028 |

©mithionian Tables.

Table 60.
DETERMINATION OF HEIGHTS BY THE BAROMETER. METRIC MEASURES.
Correction for Humidity: Values of $10000 \beta$.

$$
\beta=0.378_{\bar{b}}^{e}=0.378^{e_{1}+e_{0}} \underset{B+B_{0}}{ } .
$$



## DETERMINATION OF HEIGHTS BY THE BAROMETER.

 METRIC MEASURES.Correction for Humidity: $10000 \beta \times z$.
Top argument: Values of $10000 \beta$ obtained from page 148
Side argument: Approximate difference of height (z).

| Approximate Difference of Height. $z$. | $10000 \beta$. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 25 | 50 | 75 | 100 | 125 | 150 | 175 | 200 | 225 | 250 | 275 | 300 |
| m. | m. | m. | m. | m . | $\mathrm{m}^{\text {. }}$ | m . | mu. | mu. | m. | m | m. | m. |
| 100 | 0.3 | 0.5 | 0.8 | 1.0 | 1.3 | 1.5 | 1.8 | 2.0 | 2.3 | 2.5 | 2.8 | 3.0 |
| 200 | 0.5 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | $3 \cdot 5$ | 4.0 | $4 \cdot 5$ | 5.0 | 5.5 | 6.0 |
| 300 | 0.8 | 1.5 | 2.3 | 3.0 | 3.8 | 4.5 | $5 \cdot 3$ | 6.0 | 6.8 | 7.5 | 8.3 | 9.0 |
| 400 | I. 0 | 2.0 | 3.0 | 4.0 | 5.0 | 6.0 | 7.0 | 8.0 | 9.0 | 10.0 | 11.0 | 12.0 |
| 500 | 1.3 | 2.5 | 3.8 | 5.0 | 6.3 | $7 \cdot 5$ | 8.8 | 10.0 | 11.3 | 12.5 | 13.8 | 15.0 |
| 600 | I. 5 | 3.0 | $4 \cdot 5$ | 6.0 | 7.5 | 9.0 | 10.5 | 12.0 | 13.5 | 15.0 | 16.5 | 18.0 |
| 700 | 1.8 | 3.5 | $5 \cdot 3$ | 7.0 | 8.8 | 10.5 | 12.3 | 14.0 | 15.8 | 17.5 | 19.3 | 21.0 |
| Soo | 2.0 | 4.0 | 6.0 | 8.0 | 10.0 | 12.0 | 14.0 | 16.0 | 18.0 | 20.0 | 22.0 | 24.0 |
| 900 | 2.3 | $4 \cdot 5$ | 6.8 | 9.0 | I 1.3 | 13.5 | 15.8 | 18.0 | 20.3 | 22.5 | 24.8 | 27.0 |
| 1000 | 2.5 | 5.0 | 7.5 | 10.0 | 12.5 | 15.0 | 17.5 | 20.0 | 22.5 | 25.0 | 27.5 | 30.0 |
| I 100 | 2.8 | 5.5 | 8.3 | II. 0 | 13.8 | 16.5 | 19.3 | 22.0 | 24.8 | 27.5 | 30.3 | 33.0 |
| 1200 | 3.0 | 6.0 | 9.0 | 12.0 | 15.0 | 18.0 | 21.0 | 24.0 | 27.0 | 30.0 | 33.0 | 36.0 |
| 1300 | 3.3 | 6.5 | 9.8 | 13.0 | 16.3 | 19.5 | 22.8 | 26.0 | 29.3 | 32.5 | 35.8 | 39.0 |
| 1400 | $3 \cdot 5$ | 7.0 | IG. 5 | 14.0 | 17.5 | 21.0 | 24.5 | 28.0 | 31.5 | 35.0 | 38.5 | 42.0 |
| 1500 | 3.8 | 7.5 | 11.3 | 15.0 | I8.8 | 22.5 | 26.3 | 30.0 | 33.8 | 37.5 | $4 \mathrm{I} \cdot 3$ | 45.0 |
| 1600 | 4.0 | 8.0 | 12.0 | 16.0 | 20.0 | 24.0 | 28.0 | 32.0 | 36.0 | 40.0 | 44.0 | 48.0 |
| 1700 | $4 \cdot 3$ | 8.5 | 12.8 | 17.0 | 21.3 | 25.5 | 29.8 | 34.0 | 38.3 | 42.5 | 46.8 | 51.0 |
| ISoo | 4.5 | 9.0 | 13.5 | 18.0 | 22.5 | 27.0 | 31.5 | 36.0 | 40.5 | 45.0 | 49.5 | 54.0 |
| 1900 | 4.8 | 9.5 | 14.3 | 19.0 | 23.8 | 28.5 | $33 \cdot 3$ | 38.0 | 42.8 | 47.5 | 52.3 | 57.0 |
| 2000 | 5.0 | 10.0 | 15.0 | 20.0 | 25.0 | 30.0 | 35.0 | 40.0 | 45.0 | 50.0 | 55.0 | 60.0 |
| 2100 | $5 \cdot 3$ | 10.5 | 15.8 | 21.0 | 26.3 | 31.5 | 36.8 | 42.0 | 47.3 | 52.5 | 57.8 | 63.0 |
| 2200 | 5.5 | II.O | 16.5 | 22.0 | 27.5 | 33.0 | 38.5 | 44.0 | 49.5 | 55.0 | 60.5 | 66.0 |
| 2300 | 5.8 | 1 I .5 | 17.3 | 23.0 | 28.8 | 34.5 | 40.3 | 46.0 | 51.8 | 57.5 | 63.3 | 69.0 |
| 2400 | 6.0 | 12.0 | 18.0 | 24.0 | 30.0 | 36.0 | 42.0 | 48.0 | 54.0 | 60.0 | 66.0 | 72.0 |
| 2500 | 6.3 | 12.5 | 18.8 | 25.0 | 31.3 | 37.5 | 43.8 | 50.0 | 56.3 | 62.5 | 68.8 | 75.0 |
| 2600 | 6.5 | 13.0 | 19.5 | 26.0 | 32.5 | 39.0 | 45.5 | 52.0 | 58.5 | 65.0 | 71.5 | 78.0 |
| 2700 | 6.5 | 13.5 | 20.3 | 27.0 | 33.8 | 40.5 | 47.3 | 54.0 | 60.8 | 67.5 | $74 \cdot 3$ | 81.0 |
| 2800 | 7.0 | 14.0 | 21.0 | 28.0 | 35.0 | 42.0 | 49.0 | 56.0 | 63.0 | 70.0 | 77.0 | 84.0 |
| 2900 | 7.3 | 14.5 | 21.8 | 29.0 | 36.3 | 43.5 | 50.8 | 58.0 | 65.3 | 72.5 | 79.8 | 87.0 |
| 3000 | 7.5 | 15.0 | 22.5 | 30.0 | 37.5 | 45.0 | 52.5 | 60.0 | 67.5 | 75.0 | 82.5 | 90.0 |
| 3100 | 7.8 | 15.5 | 23.3 | 31.0 | 38.8 | 46.5 | 54.3 | 62.0 | 69.8 | 77.5 | 85.3 | 93.0 |
| 3200 | 8.0 | 16.0 | 24.0 | 32.0 | 40.0 | 48.0 | 56.0 | 64.0 | 72.0 | 80.0 | 88.0 | 96.0 |
| 3300 | 8.3 | 16.5 | 24.8 | 33.0 | 41.3 | 49.5 | 57.8 | 66.0 | 74.3 | 82.5 | 90.8 | 99.0 |
| 3400 | 8.5 | 17.0 | 25.5 | 34.0 | 42.5 | 51.0 | 59.5 | 68.0 | 76.5 | 85.0 | 93.5 | 102.0 |
| 3500 | 8.8 | 17.5 | 26.3 | 35.0 | 43.8 | 52.5 | 61.3 | 70.0 | 78.8 | 87.5 | 96.3 | 105.0 |
| 3600 | 9.0 | 18.0 | 27.0 | 36.0 | 45.0 | 54.0 | 63.0 | 72.0 | 81.0 | 90.0 | 99.0 | 108.0 |
| 3700 | $9 \cdot 3$ | 18.5 | 27.8 | 37.0 | 46.3 | 55.5 | 64.8 | 74.0 | S3.3 | 92.5 | 101.8 | II 1.0 |
| 3800 | 9.5 | 19.0 | 28.5 | 38.0 | 47.5 | 57.0 | 66.5 | 76.0 | 85.5 | 95.0 | 104.5 | 114.0 |
| 3900 | 9.8 | 19.5 | 29.3 | 39.0 | 48.8 | 58.5 | 68.3 | 78.0 | 87.8 | 97.5 | 107.3 | 117.0 |
| 4000 | 10.0 | 20.0 | 30.0 | 40.0 | 50.0 | 60.0 | 70.0 | So.o | 90.0 | 100.0 | 110.0 | 120.0 |
| 5000 | 12.5 | 25.0 | 37.5 | 50.0 | 62.5 | 75.0 | 87.5 | 100.0 | 112.5 | 125.0 | 137.5 | 150.0 |
| 6000 | 15.0 | 30.0 | 45.0 | 60.0 | 75.0 | 90.0 | 105.0 | 1200 | 135.0 | 150.0 | 165.0 | 180.0 |
| 7000 | 17.5 | 35.0 | 52.5 | 70.0 | 87.5 | 105.0 | 122.5 | 140.0 | 157.5 | 175.0 | 192.5 | 210.0 |

METRIC MEASURES.
Correction for Humidity: Values of $\frac{1}{2}\left(\frac{0.378_{\bar{b}}^{e}}{0.00367}\right)$
Top argument : Values of $e$.
Side argument : Values of $b$. Auxiliary to Table 58.

| Air Pressure. | VAPOR PRESSURE mm. |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.5 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 20 | 30 |
| mm. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$ | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. |
| 780 | 0.0 | O. I | O. 1 | 0.2 | 0.3 | 0.3 | 0.4 | 0.5 | 0.5 | 0.6 | 0.7 | 1.3 | 2.0 |
| 760 | . 0 | . 1 | . 1 | . 2 | . 3 | . 3 | . 4 | . 5 | . 5 | . 6 | . 7 | 1.4 | 2.0 |
| 740 | . 0 | . 1 | . I | . 2 | . 3 | . 4 | . 4 | -5 | . 6 | . 6 | .7 | 1.4 | 2.1 |
| 720 | . 0 | . 1 | . I | . 2 | . 3 | 4 | 4 | . 5 | . 6 | . 6 | .7 | 1.4 | 2.1 |
| 700 | . 0 | . 1 | . 2 | . 2 | $\cdot 3$ | . 4 | 4 | . 5 | . 6 | . 7 | . 7 | 1.5 | 2.2 |
| 680 | . 0 | . 1 | . 2 | . 2 | . 3 | . 4 | 4 | . 5 | . 6 | . 7 | . 8 | 1.5 |  |
| 660 | . 0 | . 1 | . 2 | . 2 | . 3 | . 4 | .5 | . 5 | . 6 | .7 | . 8 | 1.6 |  |
| 640 | . 0 | . 1 | . 2 | . 2 | . 3 | . 4 | . 5 | . 6 | . 0 | .7 | . 8 | 1. 6 |  |
| 020 | . 0 | . 1 | . 2 | . 2 | $\cdot 3$ | . 4 | . 5 | . 6 | . 7 | . 8 | . 8 | 1.7 |  |
| 600 | . 0 | . 1 | . 2 | $\cdot 3$ | . 3 | . 4 | . 5 | . 6 | .7 | . 8 | .9 | 1.7 |  |
| 580 | . 0 | . 1 | . 2 | -3 | 4 | . 4 | . 5 | . 6 | .7 | . 8 | .9 |  |  |
| 560 | . 0 | . 1 | . 2 | . 3 | 4 | . 5 | . 6 | . | .7 | . 8 | . 9 |  |  |
| 540 | . 0 | . 1 | . 2 | - 3 | .4 | .5 | . 6 | .7 | . 8 | . 9 | 1.0 |  |  |
| 520 | . 0 | . 1 | . 2 | -3 | 4 | . 5 | . 6 | .7 | . 8 | . 9 |  |  |  |
| 500 | . 0 | . 1 | . 2 | -3 | 4 | . 5 | . 6 | .7 | . 8 | . 9 |  |  |  |
| 480 | . 1 | . 1 | . 2 | -3 | 4 | . 5 | . 6 | . 8 |  |  |  |  |  |
| 460 | . 1 | . 1 | . 2 | - 3 | . 4 | . 6 | .7 | . 8 |  |  |  |  |  |
| $44^{\circ}$ | . I | . 1 | . 2 | . 4 | . 5 | . 6 | .7 |  |  |  |  |  |  |
| 420 | . 1 | . 1 | . 2 | . 4 | . 5 | . 6 | .7 |  |  |  |  |  |  |
| 400 | . 1 | . 1 | $\cdot 3$ | . 4 | . 5 | . 6 |  |  |  |  |  |  |  |
| 380 | . 1 | . 1 | . 3 | 4 | 5 |  |  |  |  |  |  |  |  |
| 360 | . 1 | . 1 | $\cdot 3$ | . 4 | . 6 |  |  |  |  |  |  |  |  |
| 340 | . 1 | . 2 | . 3 | . 4 |  |  |  |  |  |  |  |  |  |
| 320 | . 1 | . 2 | -3 | . 5 |  |  |  |  |  |  |  |  |  |
| 300 | . I | . 2 | $\cdot 3$ |  |  |  |  |  |  |  |  |  |  |
| 280 | . 1 | . 2 | . 4 |  |  |  |  |  |  |  |  |  |  |
| 260 | . 1 | . 2 | . 4 |  |  |  |  |  |  |  |  |  |  |
| 1240 | . 1 | . 2 | . 4 |  |  |  |  |  |  |  |  |  |  |
| 220 | . 1 | . 2 |  |  |  |  |  |  |  |  |  |  |  |
| 200 | . 1 | $\cdot 3$ |  |  |  |  |  |  |  |  |  |  |  |
| 180 | . 1 | $\cdot 3$ |  |  |  |  |  |  |  |  |  |  |  |
| 160 | . 2 | . 3 |  |  |  |  |  |  |  |  |  |  |  |
| I40 | . 2 | . 4 |  |  |  |  |  |  |  |  |  |  |  |
| 120 | . 2 | . 4 |  |  |  |  |  |  |  |  |  |  |  |
| 100 | . 3 | . 5 |  |  |  |  |  |  |  |  |  |  |  |
| 80 | -3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 60 | .4 |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | . 6 |  |  |  |  |  |  |  |  |  |  |  |  |
| 20 | I. 3 |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | 2.6 |  |  |  |  |  |  |  |  |  |  |  |  |

Smithsoniay Tables.

Correction for Humidity: Values of $\frac{1}{2}\left(\frac{0.378 \frac{e}{b}}{0.00367}\right)$
Top argument: Values of $e$.
Side argument : Values of $b$. Auxiliary to Table 58.

| Air Pressure. | VAPOR PRESSURE mb. |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.5 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 20 | 30 | 40 |
| mb. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. |  |  | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. |
| 1080 | 0.0 | 0.0 | 0.1 | 0.1 | 0.2 | 0.2 | 0.3 | 0.3 | 0.4 | 0.4 | 0.5 | 1.0 | I. 4 | 1.9 |
| 1060 | . 0 | . 0 | . I | . 1 | . 2 | . 2 | . 3 | . 3 | - 4 | . 4 | . 5 | 1.0 | 1.4 I. 5 | 1.9 |
| 1040 | . 0 | . 0 | . I | . 1 | . 2 | . 2 | . 3 | . 3 | - 4 | . 4 | . 5 | 1.0 | I. 5 |  |
| 1020 | . 0 | . 1 | . 1 | . 2 | . 2 | . 3 | . 3 | 4 | - 4 | . 5 | . 5 | 1.0 | 1.5 | 2.0 2.0 |
| 1000 | . 0 | .i | . 1 | . 2 | . 2 | $\cdot 3$ | . 3 | . 4 | - + | . 5 | .5 | I. 1 | 1.5 | 2.0 2.1 |
| 980 | . 0 | . 1 | . 1 | . 2 | . 2 | -3 |  |  |  |  |  |  |  |  |
| 960 | . 0 | . 1 | . I | . 2 | . 2 | . 3 | . 3 | .4 .4 | 4 .4 | . 5 | . 5 | I. I |  | 2.1 |
| 9.9 | . 0 | . 1 | . I | . 2 | . 2 | . 3 | . 3 | . + | . 4 | . 5 | . 5 | 1.1 | 1.6 | 2.1 |
| 920 | . 0 | . 1 | . I | . 2 | . 2 | . 3 | . 3 |  |  | $\cdot .5$ | . 6 | I.I | 1.6 | 2.2 |
| 900 | . 0 | . 1 | . 1 | . 2 | . 2 | . 3 | . 3 | .4 | $\stackrel{7}{7}$ | . 5 | . 6 | I.I | 1.7 | 2.2 |
| 880 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | . 0 | . 1 | . 1 | . 2 | . 2 | -3 | . 4 | . 4 | . 5 | . 5 | . 6 | 1.2 |  |  |
| 860 | . 0 | . 1 | . I | . 2 | . 2 | . 3 | . 4 | . 4 | . 5 | . 5 | . 6 | 1.2 | 1. 8 | 2.3 2.4 |
| 840 | . 0 | . 1 | . I | . 2 | . 2 | . 3 | . 4 | . 4 | . 5 | . 6 | . 6 | I. 2 | I. 8 |  |
| 820 | . 0 | I | . I | . 2 | $\cdot 3$ | -3 | - 7 | . 4 | . 5 | . 6 | . 6 | 1.3 | 1.9 |  |
| 800 | . 0 | . 1 | . 1 | . 2 | $\cdot 3$ | -3 | - 4 | . 5 | . 5 | . 6 | . 6 | I. 3 | I. 0 |  |
| 780 | . 0 | . I | . I | . 2 | $\cdot 3$ |  |  |  |  |  |  |  |  |  |
| 760 | . 0 | . 1 | . 1 | . 2 | . 3 | . 3 | $\stackrel{+}{4}$ | $\cdot 5$ .5 | . 5 | . 6 |  | 1.3 1.4 | 2.0 |  |
| 740 | . 0 | . I | . I | . 2 | . 3 | . 3 | 4 | . 5 | .6 | . 6 | . 7 | 1.4 1.4 |  |  |
| 720 | . 0 | . 1 | . I | . 2 | -3 | . 4 | - + | . 5 | . 6 | . 6 | . 7 | 1.4 |  |  |
| 700 | . 0 | . 1 | . 1 | . 2 | . 3 | . 4 | . 4 | . 5 | . 6 | .7 | .7 | 1.4 |  |  |
| 680 | . 0 | . 1 | . 2 | . 2 | $\cdot 3$ | $\cdot 4$ | . 5 | . 5 | . 6 |  |  |  |  |  |
| 660 | . 0 | . 1 | .2 | . 2 | . 3 | 4 | .5 | . 5 | . 6 | .7 | . 8 |  |  |  |
| 640 | . 0 | . 1 | . 2 | . 2 | . 3 | .4 | . 5 | . 6 | . 6 | . 7 | . 8 |  |  |  |
| 620 | . 0 | . 1 | . 2 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 7 |  |  |  |  |
| 600 | . 0 | . 1 | .2 | -3 | . 3 | 4 | . 5 | . 6 | . 7 | . 8 |  |  |  |  |
| 580 | . 0 | . I | . 2 | . 3 | + | . 4 | . 5 | . 6 | . 7 | . 8 |  |  |  |  |
| 560 | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 6 | . 7 |  |  |  |  |  |
| 540 | . 0 | . 1 | . 2 | . 3 | 4 | . 5 | . 6 | . 7 | . 8 |  |  |  |  |  |
| 520 | . 0 | . 1 | . 2 | . 3 | - 4 | . 5 | . 0 | .7 | . 8 |  |  |  |  |  |
| 500 | . I | . 1 | . 2 | . 3 | - 4 | . 5 | . 6 | .7 |  |  |  |  |  |  |
| 480 | . 1 | . 1 | . 2 | -3 | $\cdot 4$ | . 5 | . 6 | . 8 |  |  |  | VAPO | PRES | URE |
| 460 | . 1 | . 1 | . 2 | . 3 | . 4 | . 6 | . 7 | . 8 |  |  | Pres- |  |  |  |
| 440 | . 1 | . 1 | . 2 | . 4 | - 5 | . 6 | . 7 |  |  |  | sure. |  |  |  |
| 420 | . 1 | . 1 | . 2 | $\cdots$ | . 5 | . 6 | .7 |  |  |  |  | 0.5 | 1 | 2 |
| 400 | . 1 | . 1 | . 3 | 4 | . 5 |  | . 8 |  |  |  |  |  |  |  |
| 380 | . 1 | . I |  |  |  |  |  |  |  |  |  | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. | ${ }^{\circ} \mathrm{C}$. |
| 360 | . 1 | . I | . 3 | 4 . | . 6 | . 7 |  |  |  |  |  | . 1 | $\cdot 3$ | . 6 |
| 340 | . 1 | . 2 | . 3 | . 5 | . 6 | . 8 |  |  |  |  | 160 | $\cdot 2$ | - 3 | . 6 |
| 320 | . 1 | . 2 | . 3 | . 5 | . 6 |  |  |  |  |  | 120 | . 2 | .4 .4 |  |
| 300 | . 1 | .2 | $\cdot 3$ | . 5 | . 7 |  |  |  |  |  | 100 |  | . 5 |  |
| 280 | . 1 | . 2 | $\cdot 4$ | . 6 | . 7 |  |  |  |  |  |  |  |  |  |
| 260 | . I | . 2 |  | . 6 |  |  |  |  |  |  | 60 | .3 .4 |  |  |
| 240 | . I | . 2 | $\cdot 7$ | . 0 |  |  |  |  |  |  | 40 | . 6 |  |  |
| 220 | . 1 | . 2 |  | . 7 |  |  |  |  |  |  | 20 | I. 3 |  |  |
| 200 | . 1 | -3 | . 5 |  |  |  |  |  |  |  | 10 | 2.6 |  |  |

Table 62.
DETERMINATION OF HEIGHTS BY THE BAROMETER.
METRIC MEASURES.
Correction for Gravity and Weight of Mercury : $z\left(0.002640 \cos 2 \phi-0.000007 \cos ^{2} 2 \phi+0.00244\right)$.

| Approximate difference of Height. Z. | Latitude ( $\phi$ ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0^{\circ}$ | $5^{\circ}$ | $10^{\circ}$ | $15^{\circ}$ | $20^{\circ}$ | $25^{\circ}$ | $30^{\circ}$ | $35^{\circ}$ | $40^{\circ}$ | $45^{\circ}$ | $50^{\circ}$ | $55^{\circ}$ | $60^{\circ}$ | $65^{\circ}$ | $70^{\circ}$ | $75^{\circ}$ |
| Meters. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. | m. |
| 100 | I | 1 | - | - | $\bigcirc$ | - | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |
| 200 | 1 | 1 | 1 | 1 | I | 1 | I | I | I | - | - | - | 0 | - | - | $\bigcirc$ |
| 300 | 2 | 2 | 1 | 1 | I | 1 | 1 | 1 | 1 | 1 | 1 | $\bigcirc$ | - | - | - | $\bigcirc$ |
| 400 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | I | 1 | I | I | I | $\bigcirc$ | - | - | $\bigcirc$ |
| 500 | 3 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 1 | I | 1 | 1 | 1 | $\bigcirc$ | - | $\bigcirc$ |
| 600 | 3 | 3 | 3 | 3 | 3 | 2 | 2 | 2 | 2 | 1 | 1 | 1 | 1 | $\bigcirc$ | - | $\bigcirc$ |
| 700 | 4 | 4 | 3 | 3 | 3 | 3 | 3 | 2 | 2 | 2 | 1 | 1 | 1 | 1 | - | $\bigcirc$ |
| 800 | 4 | 4 | 4 | 4 | 4 | 3 | 3 | 3 | 2. | 2 | 2 | I | 1 | 1 | - | - |
| 900 | 5 | 5 | 4 | 4 | 4 | 4 | 3 | 3 | 3 | 2 | 2 | I | 1 | I | - | $\bigcirc$ |
| 1000 | 5 | 5 | 5 | 5 | 4 | 4 | 4 | 3 | 3 | 2 | 2 | 2 | 1 | 1 | $\bigcirc$ | - |
| 1100 | 6 | 6 | 5 | 5 | 5 | 5 | 4 | 4 | 3 | 3 | 2 | 2 | 1 | 1 | $\bigcirc$ | $\bigcirc$ |
| 1200 | 6 | 6 | 6 | 6 | 5 | 5 | 5 | 4 | 3 | 3 | 2 | 2 | I | 1 | $\bigcirc$ | - |
| 1300 | 7 | 7 | 6 | 6 | 6 | 5 | 5 | 4 | 4 | 3 | 3 | 2 | 1 | 1 | 1 | $\bigcirc$ |
| 1400 | 7 | 7 | 7 | 7 | 6 | 6 | 5 | 5 | 4 | 3 | 3 | 2 | 2 | I | I | $\bigcirc$ |
| 1500 | 8 | 8 | 7 | 7 | 7 | 6 | 6 | 5 | 4 | 4 | 3 | 2 | 2 | 1 | 1 | $\bigcirc$ |
| 1600 | 8 | 8 | 8 | 8 | 7 | 7 | 6 | 5 | 5 | 4 | 3 | 2 | 2 | 1 | I | - |
| 1700 | 9 | 9 | 8 | 8 | 8 | 7 | 6 | 6 | 5 | 4 | 3 | 3 | 2 | I | I | $\bigcirc$ |
| 1800 | 9 | 9 | 9 | 8 | 8 | 7 | 7 | 6 | 5 | 4 | 4 | 3 | 2 | 1 | I | $\bigcirc$ |
| 1900 | 10 | 10 | 9 | 9 | 8 | 8 | 7 | 6 | 5 | 5 | 4 | 3 | 2 | I | I | $\bigcirc$ |
| 2000 | 10 | 10 | 10 | 9 | 9 | 8 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 1 | $\bigcirc$ |
| 2100 | II | 11 | 10 | 10 | 9 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 2 | 1 | $\bigcirc$ |
| 2200 | I I | II | II | 10 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 2 | 1 | $\bigcirc$ |
| 2300 | 12 | 12 | 11 | II | 10 | 9 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | $\bigcirc$ |
| 2.400 | 12 | I 2 | 12 | II | II | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 0 | 1 | $\bigcirc$ |
| 2500 | 13 | 13 | 12 | 12 | II | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | $\bigcirc$ |
| 2600 | 13 | 13 | İ3 | 12 | 12 | 11 | 10 | 9 | 8 | 6 | 5 | 4 | 3 | 2 | 1 | $\bigcirc$ |
| 2700 | 1.4 | 14 | 13 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 5 | 4 | 3 | 2 | 1 | $\bigcirc$ |
| 2800 | I4 | 14 | 14 | 13 | 12 | 12 | I I | 9 | 8 | 7 | 6 | 4 | 3 | 2 | 1 | $\bigcirc$ |
| 2900 | 15 | 15 | 14 | 14 | 13 | 12 | I I | 10 | 8 | 7 | 6 | 4 | 3 | 2 | 1 | $\bigcirc$ |
| 3000 | 15 | 15 | 15 | 14 | 13 | 12 | I I | 10 | 9 | 7 | 6 | 5 | 3 | 2 | 1 | $\bigcirc$ |
| 3100 | 16 | 16 | 15 | 15 | 14 | 13 | 12 | 10 | 9 | 8 | 6 | 5 | 3 | 2 | 1 | $\bigcirc$ |
| 3200 | 16 | 16 | 16 | 15 | 14 | 13 | 12 | 11 | 9 | 8 | 6 | 5 | 4 | 2 | 1 | - |
| 3300 | 17 | 17 | 16 | 16 | 15 | 14 | 12 | 11 | 10 | 8 | 7 | 5 | 4 | 2 | 1 | $\bigcirc$ |
| 3400 | 17 | 17 | 17 | 16 | 15 | 14 | 13 | I I | 10 | 8 | 7 | 5 | 4 | 2 | I | $\bigcirc$ |
| 3500 | 18 | 18 | 17 | 17 | 16 | 14 | 13 | 12 | 10 | 9 | 7 | 5 | 4 | 3 | 1 | 1 |
| 3600 | 18 | 18 | 18 | 17 | 16 | 15 | 14 | 12 | 10 | 9 | 7 | 5 | 4 | 3 | 1 | 1 |
| 3700 | 19 | 19 | 18 | 17 | 16 | 15 | 14 | 12 | 11 | 9 | 7 | 6 | 4 | 3 | 2 | 1 |
| 3800 | 19 | 19 | 19 | 18 | 17 | 16 | 14 | 13 | II | 9 | 8 | 6 | 4 | 3 | 2 |  |
| 3900 | 20 | 20 | 19 | 18 | 17 | 16 | 15 | 13 | II | 9 | 8 | 6 | 4 | 3 | 2 | I |
| 4000 | 20 | 20 | 20 | 19 | 18 | 17 | 15 | 13 | 12 | 10 | 8 | 6 | 4 | 3 | 2 | 1 |
| 4500 | 23 | 23 | 22 | 21 | 20 | 19 | 17 | 15 | 13 | II | 9 | 7 | 5 | 3 | 2 | 1 |
| 5000 | 25 | 25 | 25 | 24 | 22 | 21 | 19 | 17 | 1.4 | 12 | 10 | 8 | 6 | 4 | 2 | 1 |
| 5500 | 28 | 28 | 27 | 26 | 24 | 23 | 21 | 18 | 16 | 13 | 11 | 8 | 6 | 4 | 2 | 1 |
| 6000 | 30 | 30 | 29 | 28 | 27 | 25 | 23 | 20 | 17 | 15 | 12 | 9 | 7 | 4 | 2 | 1 |
| 6500 | 33 | 33 | 32 | 31 | 29 | 27 | 24 | 22 | 19 | 16 | 13 | 10 | 7 | 5 | 3 | 1 |
| 7000 | 35 | 35 | 34 | 33 | 31 | 29 | 26 | 23 | 20 | 17 | 14 | II | 8 | 5 | 3 | 1 |

Table 63.
DETERMINATION OF HEIGHTS BY THE BAROMETER.
METRIC MEASURES.
Correction for the variation of gravity with altitude: $\frac{z\left(z+2 h_{0}\right)}{R}$

| Approximate difference of height. Z. | height of lower station in meters ( $h_{0}$ ) . |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 200 | 400 | 600 | 800 | 1000 | 1200 | 1400 | 1600 | 1800 | 2000 | 2500 | 3000 | 4000 |
| meters | m . | m. | m. | m. | m. | m. | m. | m. | m . | m. | m . | m. | m. | m. |
| 200 | 0 | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - | $\bigcirc$ | o | 0 | O | 0 | - | $\bigcirc$ | 0 |
| 300 | 0 | o | o | - | o | - | 0 | - | $\bigcirc$ | - | 0 | O | 0 | 0 |
| 400 | 0 | o | - | $\bigcirc$ | - | o | $\bigcirc$ | - | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | - | $\bigcirc$ | I |
| 500 | 0 | 0 | $\bigcirc$ | 0 | $\bigcirc$ | o | o | o | o | o | o | o | 1 | 1 |
| 600 | o | 0 | - | - | $\bigcirc$ | - | 0 | - | 0 | O | 0 | I | I | I |
| 700 | 0 | - | - | - | $\bigcirc$ | 0 | 0 | - | $\bigcirc$ | $\bigcirc$ | I | I | 1 | 1 |
| 800 | 0 | - | $\bigcirc$ | - | $\bigcirc$ | $\bigcirc$ | - | - | 1 | I | I | I | I | I |
| 900 | 0 | 0 | - | - | - | - | o | I | I | 1 | I | I | I | 1 |
| 1000 | - | o | 0 | o | 0 | O | 1 | I | 1 | 1 | I | I | 1 | 1 |
| 1100 | - | - | 0 | - | - | 1 | I | 1 | I | I | I | 1 | I | 2 |
| I 200 | 0 | - | o | - | I | 1 | I | I | I | I | I | I | I | 2 |
| 1300 | o | - | - | I | I | 1 | I | I | I | 1 | I | I | 1 | 2 |
| 1400 | o | 0 | - | I | I | 1 | I | 1 | 1 | I | I | I | 2 | 2 |
| 1500 | 0 | o | I | I | I | I | I | 1 | I | I | I | 2 | 2 | 2 |
| 1600 | $\bigcirc$ | I | I | I | I | I | 1 | 1 | I | I | 1 | 2 | 2 | 2 |
| 1700 | - | 1 | I | I | 1 | 1 | I | I | 1 | I | 2 | 2 | 2 | 3 |
| 1800 | 1 | I | I | I | I | I | I | I | 1 | 2 | 2 | 2 | 2 | 3 |
| 1900 | I | I | 1 | I | I | 1 | I | I | 2 | 2 | 2 | 2 | 2 | 3 |
| 2000 | I | I | I | I | I | *I | I | 2 | 2 | 2 | 2 | 2 | 3 | 3 |
| 2100 | I | 1 | I | 1 | 1 | I | I | 2 | 2 | 2 | 2 | 2 | 3 | 3 |
| 2200 | I | I | I | I | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 4 |
| 2300 | I | I | I | I | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 4 |
| 2400 | I | I | I | I | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 4 |
| 2500 | 1 | 1 | I | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 4 |
| 2600 | 1 | I | I | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 4 | 4 |
| 2700 | 1 | 1 | I | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 4 | 5 |
| 2800 | 1 | 1 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 4 | 5 |
| 2900 | I | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 4 | 4 | 5 |
| 3000 | I | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 5 |
| 3100 | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 5 |
| 3200 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 5 | 6 |
| 3300 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 5 | 6 |
| 3400 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 5 | 6 |
| 3500 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 5 | 5 | 6 |
| 3600 | 2 | 2 | 2 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 5 | 5 | 7 |
| 3700 | 2 | 2 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 4 | 5 | 6 | 7 |
| 3 Soo | 2 | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 5 | 5 | 6 | 7 |
| 3900 | 2 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 5 | 5 | 5 | 6 | 7 |
| 4000 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 5 | 5 | 5 | 6 | 6 | 8 |
| 4500 | 3 | 3 | 4 | 4 | 4 | 5 | 5 | 5 | 5 | 6 | 6 | 7 | 7 | 9 |
| 5000 | 4 | 4 | 5 | 5 | 5 | 5 | 6 | 6 | 6 | 7 | 7 | 8 | 9 | 10 |
| 5500 | 5 | 5 | 5 | 6 | 6 | 6 | 7 | 7 | 8 | 8 | 8 | 9 | 10 | 12 |
| 6000 | 6 | 6 | 6 | 7 | 7 | 8 | 8 | S | 9 | 9 | 9 | 10 | 1 I | 13 |
| 6500 | 7 | 7 | 7 | 8 | 8 | 9 | 9 | 9 | 10 | 10 | I I | 12 | 13 | 15 |
| 7000 | S | S | 9 | 9 | 9 | 10 | 10 | II | II | 12 | 12 | 13 | 14 | 16 |

Table 64.
HEIGHTS REDUCED FROM METERS TO DYNAMIC METERS, THE
ACCELERATION OF GRAVITY AT SEA LEVEL BEING 9.80 .

| $\begin{aligned} & \text { Height } \\ & \text { (meters) } \end{aligned}$ | 0 | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 29000 | 28290 | 28387 | 28484 | 28582 | 28679 | 28776 | 28873 | 28970 | 29067 | 29164 |
| 28000 | 27319 | 27416 | 27513 | 27610 | 27708 | 27805 | 27902 | 27999 | 28096 | 28193 |
| 27000 | 26347 | 26445 | 26542 | 26639 | 26736 | 26833 | 26930 | 27028 | 27125 | 27222 |
| 26000 | 25376 | 25473 | 25570 | 25667 | 25764 | 25862 | 25959 | 26056 | 26153 | 26250 |
| 25000 | 24404 | 24501 | 24598 | 24695 | 24792 | 24890 | 24987 | 25084 | 25181 | 25279 |
| 24000 | 23431 | 23528 | 23626 | 23723 | 23820 | 23917 | 24015 | 24112 | 24209 | 24306 |
| 23000 | 22458 | 22556 | 22653 | 22750 | 22847 | 22945 | 23042 | 23139 | 23237 | 23334 |
| 22000 | 21485 | 21583 | 21680 | 21777 | 21875 | 21972 | 22069 | 22166 | 22264 | 22361 |
| 21000 | 20512 | 20609 | 20707 | 20804 | 20901 | 20999 | 21096 | 21193 | 21291 | 21388 |
| 20000 | 19538 | 19636 | 19733 | 19830 | 19928 | 20025 | 20122 | 20220 | 20317 | 20415 |
| 19000 | I 8564 | 18662 | I 8759 | 18856 | I 8954 | 19051 | 19149 | 19246 | 19344 | I944I |
| 18000 | 17590 | 17687 | 17785 | 17882 | 17980 | 18077 | 18175 | 18272 | 18369 | 18467 |
| 17000 | 16615 | 16713 | 16810 | 16908 | 17005 | 17103 | 17200 | 17298 | 17395 | 17493 |
| 16000 | I 5640 | 15738 | 15835 | 15933 | 16030 | 16128 | 16225 | 16323 | 16420 | 16518 |
| 15000 | 14665 | 14763 | 14860 | 14958 | I 5055 | I 5153 | 15250 | I $534{ }^{8}$ | I 5446 | I 5543 |
| I 4000 | 13690 | 13787 | 13885 | 13982 | 14080 | 14178 | 14275 | 14373 | 14470 | 14568 |
| 13000 | 12714 | I28II | 12909 | 13007 | 13104 | 13202 | 13299 | 13397 | I 3495 | I 3592 |
| 12000 | 11738 | 11835 | 11933 | 12031 | 12128 | 12226 | 12323 | 1242 I | I2519 | 12616 |
| 11000 | 10761 | 10859 | 10957 | 11054 | III 52 | I 1250 | I 1347 | I I 445 | I 1543 | II640 |
| 10000 | 9785 | 9882 | 9980 | 10078 | 10175 | 10273 | 1037 I | 10468 | 10566 | 10664 |
| 9000 | 8807 | 8905 | 9003 | 9101 | 9198 | 9296 | 9394 | 9492 | 9589 | 9687 |
| 8000 | 7830 | 7928 | 8026 | 8123 | 822 I | 8319 | 8417 | 8514 | 8612 | 8710 |
| 7000 | 6852 | 6950 | 7048 | 7146 | 7244 | $73+1$ | 7439 | 7537 | 7635 | 7732 |
| 6000 | 5874 | 5972 | 6070 | 6168 | 6266 | 6363 | 6461 | 6559 | 6657 | 6755 |
| 5000 | 4896 | 4994 | 5092 | 5190 | 5287 | 5385 | 5483 | 558 I | 5679 | 5777 |
| 4000 | 3918 | 4015 | 4113 | 42 II | 4309 | 4407 | 4505 | 4603 | 4700 | 4798 |
| 3000 | 2939 | 3037 | 3134 | 3232 | 3330 | 3428 | 3526 | 3624 | 3722 | 3820 |
| 2000 | 1959 | 2057 | 2155 | 2253 | 2351 | 2449 | 2547 | 2645 | 2743 | 2841 |
| 1000 | 980 | 1078 | 1176 | 1274 | I 372 | 1470 | I 568 | 1666 | 1763 | I 861 |
| 0 | 0 | 98 | 196 | 294 | 392 | 490 | 588 | 686 | 784 | 882 |
|  | 0 | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 |

Proportionality Table.

| Meters | $\mathbf{0}$ | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ |
| :---: | ---: | ---: | ---: | ---: | ---: | :---: | :---: | :---: | :---: | :---: |
| 90 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 |
| 80 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 |
| 70 | 69 | 70 | 71 | 72 | 73 | 74 | 74 | 75 | 76 | 77 |
| 60 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 |
| 50 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 |
| 40 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 |
| 30 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 |
| 20 | 20 | 21 | 22 | 23 | 24 | 24 | 25 | 26 | 27 | 28 |
| 10 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| 0 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|  | $\mathbf{0}$ | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | 5 | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ |

Smithsonian Tables

Table 65.
CORRECTIONS TO TABLE 64 FOR VALUES OF THE ACCELERATION OF GRAVITY AT SEA LEVEL DIFFERENT FROM 9.80.

| $\begin{aligned} & \text { Height } \\ & \text { (meters) } \end{aligned}$ | Acceleration of grayity at sea level. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 9.76 | 9.77 | 9.78 | 9.79 | 9.80 | 9.81 | 9.82 | 9.83 | 9.84 |
| 29000 | -116 | $-87$ | $-58$ | -29 | 0 | 29 | 58 | 87 | 116 |
| 28000 | -112 | -84 | $-56$ | -28 | O | 28 | 56 | 84 | 112 |
| 27000 | -108 | -81 | -54 | -27 | - | 27 | 54 | 8 I | 108 |
| 26000 | $-104$ | -78 | -52 | -26 | o | 26 | 52 | 78 | 104 |
| 25000 | $-100$ | -75 | -50 | -25 | 0 | 25 | 50 | 75 | 100 |
| 24000 | - 96 | -72 | -48 | -24 | o | 24 | 48 | 72 | 96 |
| 23000 | -92 | -69 | -46 | -23 | O | 23 | 46 | 69 | 92 |
| 22000 | - 88 | -66 | -44 | -22 | o | 22 | 44 | 66 | 88 |
| 21000 | - 84 | -63 | -42 | -2I | O | 21 | 42 | 63 | 84 |
| 20000 | - 80 | -60 | -40 | -20 | O | 20 | 40 | 60 | 80 |
| 19000 | - 76 | -57 | -38 | -19 | 0 | 19 | 38 | 57 | 76 |
| 18000 | - 72 | -54 | -36 | -18 | - | 18 | 36 | 54 | 72 |
| 17000 | -68 | -51 | -34 | -17 | o | 17 | 34 | 5 I | 68 |
| 16000 | - 64 | -48 | -32 | -16 | o | 16 | 32 | 48 | 64 |
| 15000 | -60 | -45 | -30 | -15 | 0 | 15 | 30 | 45 | 60 |
| 14000 | - 56 | -42 | -28 | -I4 | o | 14 | 28 | 42 | 56 |
| 13000 |  | -39 | -26 | -13 | o | 13 | 26 | 39 | 52 |
| 12000 | - $4^{8}$ | -36 | -24 | -I2 | - | 12 | 24 | 36 | 48 |
| 11000 | - 44 | -33 | -22 | - 11 | o | 11 | 22 | 33 | 44 |
| 10000 | - $4^{0}$ | $-30$ | $-20$ | - 10 | o | 10 | 20 | 30 | 40 |
|  |  | -27 | -18 |  | 0 |  | 18 | 27 | 36 |
| 8000 | - 32 | -24 | -16 | -8 | 0 | 8 | 16 | 24 | 32 |
| 7000 | - 28 | -21 | -I4 | $-7$ | - | 7 | 14 | 21 | 28 |
| 6000 | - 24 | -I8 | -I2 | - 6 | o | 6 | 12 | 18 | 24 |
| 5000 | - 20 | -15 | $-\mathrm{IO}$ | - 5 | o | 5 | 10 | 15 | 20 |
| 4000 | - 16 | -12 | -8 | - 4 | 0 | 4 | 8 | 12 | 16 |
| 3000 | - 12 | - 9 | - 6 | -3 | 0 | 3 | 6 | 9 | 12 |
| 2000 | - 8 | - 6 | - 4 | - 2 | o | 2 | 4 | 6 | 8 |
| 1000 | - 4 | - 3 | - 2 | - I | o | 1 | 2 | 3 | 4 |
| - | 0 | 0 | 0 | o | o | o | 0 | 0 | $\bigcirc$ |
|  | 9.76 | 9.77 | 9.78 | 9.79 | 9.80 | 9.81 | 9.82 | 9.83 | 9.84 |

Table 66.
NORMAL VALUE OF THE ACCELERATION OF GRAVITY AT SEA LEVEL, $\mathbf{G}_{\phi}, \mathbf{M} / \mathbf{S E C} .^{2}$

| Latitude | $0{ }^{\circ}$ | $1{ }^{\circ}$ | $2^{\circ}$ | $3^{\circ}$ | $4^{\circ}$ | $5^{\circ}$ | $6^{\circ}$ | $7^{\circ}$ | $8^{\circ}$ | $9^{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $80^{\circ}$ | 9.8306 | . 8309 | 9.8312 | 9.8314 | 9.8316 | 9.8318 | 9.8319 | 9.8320 | 9.832 I | 9.8322 |
| $70^{\circ}$ | 9.8261 | 9.8266 | 9.8272 | 9.8277 | 9.8282 | 9.8287 | 9.8291 | 9.8295 | 9.8299 | 9.8303 |
| $60^{\circ}$ | 9.8192 | 9.8200 | 9.8207 | 9.8214 | 9.8222 | 9.8229 | 9.8236 | 9.8242 | 9.8249 | 9.8255 |
| $50^{\circ}$ | 9.8107 | 9.8116 | 9.8125 | 9.8134 | $9.81{ }^{4} 2$ | 9.8151 | 9.8159 | 9.8168 | 9.8176 | 9.8184 |
| $40^{\circ}$ | 9.8017 | 9.8026 | 9.8035 | 9.8044 | 9.8053 | 9.8062 | 9.8071 | 9.8080 | 9.8089 | 9.8098 |
| $30^{\circ}$ | 9.7933 | 9.7941 | 9.7949 | 9.7957 | 9.7965 | 9.7974 | 9.7982 | 9.7991 | 9.8000 | 9.8008 |
| $20^{\circ}$ | 9.7864 | 9.7870 | 9.7876 | 9.7883 | 9.7889 | 9.7896 | 9.7903 | 9.7910 | 9.7918 | 9.7925 |
| $10^{\circ}$ | 9.7819 | 9.7823 | 9.78 | 7830 | 9.7834 | 9.7838 | 9.7843 | 9.7848 | 9.7853 | 9.7858 |
| $0^{\circ}$ | 9.7804 | 9.780 | 9.780 | 9.7805 | 9.7806 | 9.7808 | 9.7810 | 9.7812 | 9.7814 |  |

$S_{\phi}$ at $90^{\circ}=0.8322$

Table 67.

## HEIGHTS REDUCED FROM DYNAMIC METERS TO GEOMETRIC METERS, THE ACCELERATION OF GRAVITY AT SEA LEVEL BEING 9.80.

| Height (dynamic meters) | 0 | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 29000 | 29729 | 29832 | 29935 | 30038 | 30141 | 30244 | 30347 | 30451 | 30554 | 30657 |
| 28000 | 28700 | 28803 | 28906 | 29009 | 29112 | 29215 | 29318 | 29420 | 29523 | 29626 |
| 27000 | 27670 | 27773 | 27876 | 27979 | 28082 | 28185 | 28288 | 28391 | 28494 | 28597 |
| 26000 | 26641 | 26744 | 26847 | 26950 | 27053 | 27156 | 27259 | 27362 | 27464 | 27567 |
| 25000 | 25612 | 25715 | 25818 | 25921 | 26024 | 26127 | 26230 | 26333 | 26435 | 26538 |
| 24000 | 24584 | 24687 | 24790 | 24893 | 24995 | 25098 | 25201 | 25304 | 25407 | 25510 |
| 23000 | 23556 | 23659 | 23762 | 23864 | 23967 | 24070 | $2+173$ | 24276 | 24378 | 24481 |
| 22000 | 22528 | 22631 | 22734 | 22836 | 22939 | 23042 | 23145 | 23248 | 23350 | 23453 |
| 21000 | 21501 | 21603 | 21706 | 21809 | 21912 | 22014 | 22117 | 22220 | 22323 | 22425 |
| 20000 | 20474 | 20576 | 20679 | 20782 | 20884 | 20987 | 21090 | 21193 | 21295 | 21398 |
| 19000 | 19447 | 19549 | 19652 | 19755 | 19858 | 19960 | 20063 | 20166 | 20268 | 20371 |
| 18000 | 18420 | I 8523 | 18626 | 18728 | 18831 | 18934 | 19036 | 19139 | 19242 | 19344 |
| 17000 | 17394 | 17497 | 17599 | 17702 | 17805 | 17907 | 18010 | 18112 | 18215 | 18318 |
| 16000 | 16368 | 16471 | 16574 | 16676 | 16779 | 16881 | 16984 | 17086 | 17189 | 17292 |
| 15000 | I 5343 | I 5445 | 15548 | 15651 | 15753 | 15856 | 15958 | 16061 | 16163 | 16266 |
| 14000 | $1+318$ | 14420 | 14523 | 14625 | 14728 | 14830 | 14933 | 15035 | 15138 | 15240 |
| 13000 | 13293 | 13395 | 13498 | 13600 | 13703 | 13805 | 13908 | 14010 | 14113 | 14215 |
| 12000 | 12268 | 12371 | 12473 | 12576 | 12678 | 12781 | 12883 | 12986 | 13088 | 13190 |
| 11000 | 11244 | 11347 | I I 449 | II 552 | 11654 | I 1756 | 11859 | 11961 | 12064 | 12166 |
| 10000 | 10220 | 10323 | 10425 | 10528 | 10630 | 10732 | 10835 | 10937 | 11040 | 11142 |
| 9000 | 9197 | 9299 | 9402 | 9504 | 9606 | 9709 | 9811 | 9913 | 10016 | 10118 |
| 8000 | 8174 | 8276 | 8378 | 848 I | 8583 | 8685 | 8788 | 8890 | 8992 | 9095 |
| 7000 | 7151 | 7253 | 7355 | 7458 | 7560 | 7662 | 7765 | 7867 | 7969 | 8071 |
| 6000 | 6128 | 6231 | 6333 | 6435 | 6537 | 6640 | 6742 | 6844 | 6946 | 7049 |
| 5000 | 5106 | 5208 | 53 II | 5413 | 5515 | 5617 | 5719 | 5822 | 5924 | 6026 |
| 4000 | 4084 | 4186 | 4289 | 4391 | 4493 | 4595 | 4697 | 4800 | 4902 | 5004 |
| 3000 | 3063 | 3165 | 3267 | 3369 | 3471 | 3573 | 3676 | 3778 | 3880 | 3982 |
| 2000 | 2042 | 2144 | 2246 | 2348 | 2450 | 2552 | 2654 | 2756 | 2858 | 2961 |
| 1000 | IO2I | 1123 | 1225 | 1327 | 1429 | 1531 | 1633 | 1735 | 1837 | 1939 |
| 0 | 0 | 102 | 204 | 306 | 408 | 510 | 612 | 714 | 816 | 919 |
|  | 0 | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 |

Proportionality Table.

| Meters | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 90 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 | IOI |
| 80 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 |
| 70 | 71 | 72 | 73 | 74 | 76 | 77 | 78 | 79 | 80 | 81 |
| 60 | 6 I | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 |
| 50 | 5 I | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 |
| 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 |
| 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 |
| 20 | 20 | 21 | 22 | 23 | 24 | 26 | 27 | 28 | 29 | 30 |
| 10 | 10 | II | 12 | 13 | I 4 | 15 | 16 | 17 | 18 | 19 |
| 0 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

Smithsonian Tables GRAVITY AT SEA LEVEL DIFFERENT FROM 9.80.

| Height (dynamic meters) | Acceleration of gravity at sea level. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 9.76 | 9.77 | 9.78 | 9.79 | 9.80 | 9.81 | 9.82 | 9.83 | 9.84 |
| 29000 | 121 | 91 | 60 | - 30 | 0 | -30 | -60 | -9I | -I2I |
| 28000 | 117 | 88 | 58 | 29 | 0 | -29 | -58 | -88 | -117 |
| 27000 | 113 | 8. | 56 | 28 | 0 | -28 | -56 | -84 | -II3 |
| 26000 | 108 | 81 | 54 | 27 | o | -27 | -54 | -81 | -108 |
| 25000 | 104 | 78 | 52 | 26 | 0 | -26 | -52 | $-78$ | -104 |
| 24000 | 100 | 75 | 50 | 25 | 0 | -25 | -50 | -75 | -100 |
| 23000 | 96 | 72 | 48 | 24 | 0 | -24 | -48 | -72 | - 96 |
| 22000 | 92 | 69 | 46 | 23 | o | -23 | -46 | -69 | -92 |
| 21000 | 87 | 66 | 44 | 22 | 0 | -22 | -44 | -66 | - 87 |
| 20000 | 83 | 62 | 42 | 21 | 0 | -2I | -42 | -62 | -83 |
| 19000 | 79 | 59 | 40 | 20 | 0 | -20 | -40 | -59 | - 79 |
| 18000 | 75 | 56 | 37 | 19 | 0 | -19 | -37 | -56 | - 75 |
| 17000 | 71 | 53 | 35 | 18 | 0 | -18 | -35 | -53 | - 71 |
| 16000 | 67 | 50 | 33 | 17 | 0 | -17 | -33 | $-50$ | -67 |
| 15000 | 62 | 47 | 31 | 16 | o | -16 | -3I | $-47$ | - 62 |
| 14000 | 58 | 44 | 29 | 15 | 0 | -I5 | -29 | -44 | - 58 |
| 13000 | 54 | 4 I | 27 | 14 | 0 | -14 | -27 | -4I | - 54 |
| 12000 | 50 | 37 | 25 | 13 | 0 | -13 | -25 | -37 | - 50 |
| 11000 | 46 | 34 | 23 | 11 | o | -II | $-23$ | -34 | - 46 |
| 10000 | 42 | 3 I | 21 | 10 | o | -10 | -21 | -31 | - 42 |
| 9000 | 37 | 28 | 19 | 9 | 0 | -9 | -19 | -28 | - 37 |
| 8000 | 33 | 25 | 17 | 8 | o | - 8 | -17 | -25 | - 33 |
| 7000 | 29 | 22 | 15 | 7 | o | - 7 | -15 | -22 | - 29 |
| 6000 | 25 | 19 | 12 | 6 | o | - 6 | -I2 | -19 | - 25 |
| 5000 | 2 I | 16 | 10 | 5 | 0 | - 5 | -10 | -16 | -2I |
| 4000 | 17 | 12 | 8 | 4 | 0 | - 4 | - 8 | -12 | - I7 |
| 3000 | 13 | 9 | 6 | 3 | 0 | -3 | - 6 | -9 | - 13 |
| 12000 | 8 4 | 6 3 | 4 | 2 | o | 1 -1 | - 4 | -6 | - 8 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 9.76 | 9.77 | 9.78 | 9.79 | 9.80 | 9.81 | 9.82 | 9.83 | 9.84 |

Examples to tables 67 and 68.

| 1 | 2 | 3 | 4 | 5 |
| ---: | ---: | ---: | ---: | ---: |
| 1614 | 1633 | 14 | +2 | 1649 |
| 2804 | 2858 | 4 | +3 | 2865 |
| 4704 | 4800 | 4 | +6 | 4810 |
| 12140 | 12371 | $4 I$ | +16 | 12428 |

Column

1. Heights above sea level given in dynamic meters.
2. Values of table 67 for the dynamic heights, $1600,2800,4700,12100$.
3. Values of proportionality table for dynamic heights $14,4,4,40$.
4. Corrections from table 68 for $g=9.7873$ at sea level and for the heights of column 1.
5. Sum of numbers in columns 2,3 and 4 , giving the geometrical heights corresponding to the dynamic heights of column 1 .

Examples to tables 64 and 65 .

| 1 | 2 | 3 | 4 | 5 |
| ---: | ---: | ---: | ---: | ---: |
| 1649 | I 568 | 48 | -2 | 1614 |
| 2865 | 2743 | 64 | -3 | 2804 |
| 4810 | 4700 | 10 | -6 | 4704 |
| 12428 | 12128 | 27 | -15 | I2I40 |

Column

1. Heights above sea level given in meters.
2. Values of table 64 for the heights 1600,2800 , 4800, 12400.
3. Values of proportionality table for the heights 49, 65, 10, 28.
4. Corrections from table 65 for $g=9.7873$ at sea level and for the heights of column 1.
5. Sum of numbers in columns 2,3 and 4 , giving the dynamic heights corresponding to the geometrical heights of column 1.

Table 69.
DIFFERENCE OF HEIGHT CORRESPONDING TO A CHANGE OF 0.1 INCH IN THE BAROMETER.

ENGLISH MEASURES.

| Barometric Pressure. | MEAN TEMPERATURE OF THE AIR IN FAHRENHEIT DEGREES. |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $30^{\circ}$ | $35^{\circ}$ | $40^{\circ}$ | $45^{\circ}$ | $50^{\circ}$ | $55^{\circ}$ | $60^{\circ}$ | $65^{\circ}$ | $70^{\circ}$ | $75^{\circ}$ | $80^{\circ}$ | $85^{\circ}$ |
| Inche | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. | Feet. |
| 22.0 | 119.2 | 120.5 | 121.8 | 123. 1 | 124.4 | 125.8 | I27.1 | 128.5 | 129.8 | 131.2 | 132.5 | 133.9 |
| . 2 | IIS.2 | 119.4 | 120.7 | 122.0 | 123.3 | 124.7 | I26.0 | 127.3 | 128.7 | 130.0 | I3 1.3 | 132.7 |
| .4 | 117.1 | 118.3 | 119.6 | 120.9 | 122.2 | 123.6 | 124.9 | 126.2 | 127.5 | I28.8 | I30.2 | 131.5 |
| . 6 | II6.I | 117.3 | 118.6 | 119.8 | I2I.I | I22.5 | 123.8 | 125. I | J26.4 | 127.7 | 129.0 | I30. 3 |
| . 8 | 115.0 | 116.3 | 117.5 | I 18.8 | 120.1 | 121.4 | 122.7 | 124.0 | 125.3 | I26.6 | 127.9 | I29.2 |
| 23.0 | I14.0 | 115.3 | 116.5 | 117.8 | 119.0 | I20.3 | 121. 6 | 122.9 | 124.2 | 125.5 | 126.8 | I2S. I |
| . 2 | II3.1 | 114.3 | I15.5 | 116.8 | 118.0 | 119.3 | 120.6 | 121.8 | 123.1 | 124.4 | 125.7 | 127.0 |
| . 4 | II2.I | 113.3 | II4.5 | 115.8 | 117.0 | I I8.3 | I 19.5 | I 20.8 | 122.1 | 123.3 | 124.6 | 125.9 |
| . 6 | III.I | II2.3 | II3.5 | 114.8 | 116.0 | 117.3 | 118.5 | 119.8 | 121.0 | 122.3 | 123.5 | 124.8 |
| . 8 | IIO. 2 | III.4 | I I 2.6 | 113.8 | II5. I | 116.3 | 117.5 | I 8.8 | 120.0 | 121.3 | 122.5 | 123.8 |
| 24.0 | 109.3 | 110.5 | 111.7 | 112.9 | II4. 1 | 115.3 | 116.5 | 117.8 | 119.0 | 120.2 | 121.5 | 122.7 |
| . 2 | IoS. 4 | 109.5 | I 10.7 | III. 9 | II3.I | II 4.4 | 115.6 | 116.8 | 118.0 | II9.2 | 120.5 | 121.7 |
| . 4 | 107.5 | 108.6 | 109.8 | III.O | II2.2 | 113.4 | I 14.6 | I 15.9 | 117.1 | I18.3 | 119.5 | 120.7 |
| . 6 | 106.6 | 107.8 | 108.9 | IIO. I | IIII. 3 | I 12.5 | 113.7 | I I 4.9 | II6. I | 117.3 | 118.5 | 119.7 |
| . 8 | 105.8 | 106.9 | 108. 1 | 109. 2 | 110.4 | III. 6 | II 2.8 | 114.0 | II 5.2 | 116.4 | 117.6 | i18.8 |
| 25.0 | 104.9 | 106.0 | 107.2 | 108. 3 | 109.5 | 110.7 | III. 9 | II3.1 | 114.2 | 115.4 | 116.6 | 117.8 |
| . 2 | 104. I | 105.2 | 106.3 | 107. 5 | 108.7 | 109.8 | III.O | II 2.2 | 113.3 | 114.5 | I 15.7 | 116.9 |
| . 4 | 103.3 | 10.4 .4 | 105.5 | 106.6 | 107.8 | 109.0 | IIO.I | III. 3 | II 2.4 | II 3.6 | 114.8 | 116.0 |
| . 6 | 102.5 | 103.6 | 104.7 | 105.8 | 107.0 | IOS. I | 109.3 | I 10.4 | III. 6 | 112.7 | 113.9 | 115.1 |
| . 8 | IOI. 7 | 102.8 | 103.9 | 105.0 | 106. I | 107.3 | 108.4 | tog. 6 | 110.7 | 111.9 | II3.0 | II 4.2 |
| 26.0 | 100.9 | 102.0 | 103. I | 104.2 | 105.3 | 106.4 | 107.6 | 108.7 | 109.9 | III.O | 112.I | 113.3 |
| . 2 | 100. I | IOI. 2 | 102.3 | 103.4 | 104.5 | 105.6 | 106.8 | 107.9 | 109.0 | IIO. I | III. 3 | I 12.4 |
| . 4 | 99.4 | 100.4 | 101. 5 | 102.6 | 103.7 | 10.4 .8 | 106.0 | 107. 1 | 10S. 2 | 109.3 | 110.4 | I I 1.6 |
| . 6 | 98.6 | 99.7 | 100.7 | IOI. 8 | IO2.9 | 104.0 | 105.2 | 106.3 | 107.4 | 108. 5 | 109. 6 | 110.7 |
| . 8 | 97.9 | 98.9 | 100.0 | IOI, I | 102.2 | 103.3 | 104.4 | 105.5 | 106.6 | 107.7 | 108.8 | 109.9 |
| 27.0 | 97. 1 | 98.2 | 99.2 | 100.3 | 101.4 | 102.5 | 103.6 | 104.7 | 105.8 | 106.9 | IOS.O | 109. I |
| . 2 | 96.4 | 97.5 | 98.5 | 99.6 | 100.7 | IoI. 8 | 102.8 | 103.9 | 105.0 | 106. I | 107.2 | 10S. 3 |
| . 4 | 95.7 | 96.8 | $97 . \mathrm{S}$ | 98.9 | 99.9 | 101.0 | 102. I | 103.2 | 104.2 | 105.3 | 106.4 | 107.5 |
| . 6 | 95.0 | 96.1 | 97.1 | 98.1 | 99.2 | 100.3 | IOI. 3 | 102.4 | 103.5 | 104.6 | 105.6 | 106. 7 |
| . 8 | 94.3 | 95.4 | 96.4 | 97.4 | 98.5 | 99.6 | 100.6 | 101.7 | 102.7 | 103.8 | 104.9 | 105.9 |
| 28.0 | 93.7 | 94.7 | $95 \cdot 7$ | 96.7 | 97.8 | 9 9.8 | 99.9 | IOI. 0 | 102.0 | 103. 1 | 104.1 | 105.2 |
| . 2 | 93.0 | 94.0 | 95.0 | 96.1 | 97. I | 9S. I | 99.2 | 100.2 | 101.3 | 102.3 | 103.4 | 104.4 |
| -4 | 92.4 | 93.4 | 94.4 | 95.4 | 96.4 | 97.5 | 98.5 | 99.5 | 100. 6 | IOI. 6 | 102.7 | 103.7 |
| . 6 | 91.7 | 92.7 | 93.7 | 94.7 | 95.7 | 96.8 | 97.8 | 98.8 | 99.9 | 100.9 | IOL. 9 | 103.0 |
| . 8 | 9 I .1 | 92.1 | 93.I | 94. I | 95. I | 96.1 | 97. I | 98.2 | 99.2 | 100. 2 | IOI. 2 | 102.3 |
| 29.0 | 90.4 | 91.4 | 92.4 | 93.4 | 94.4 | 95.4 | 96.5 | 97.5 | 98.5 | 99.5 | 100.5 | IOI. 6 |
| . 2 | S9. 8 | 90.8 | 91.8 | 92.8 | 93.8 | 94.8 | 95.8 | 96.8 | 97.8 | 98.8 | 99.9 | I00. 9 |
| . 4 | S9.2 | 90.2 | 9 I .1 | 92.1 | 93. I | 94.1 | 95.1 | 96.1 | 97. I | 98.2 | 99.2 | 100.2 |
| . 6 | 88.6 | S9.6 | 90.5 | 91.5 | 92.5 | 93.5 | 94.5 | 95.5 | 96.5 | 97.5 | 98.5 |  |
| . 8 | 88.0 | S9.0 | 89.9 | 90.9 | 91.9 | 92.9 | 93.9 | 94.9 | 95.8 | 96.8 | 97.8 | 98.8 |
| 30.0 | 87.4 | 88.4 | 89.3 | 90.3 | 91.3 | 92.3 | 93.2 | 94.2 | 95.2 | 96.2 | 97.2 | 98.2 |
| . 2 | S6. ${ }^{\text {S }}$ | 87.8 | S5. 7 | S9.7 | 90.7 | 91.7 | 92.6 | 93.6 | 94.6 | 95.6 | 96.5 | 97.5 |
| - 4 | 86.3 | 87.2 | 88.2 | 89.1 | 90.1 | 9 I .1 | 92.0 | 93.0 | 94.0 | 94.9 | 95.9 | 96.9 |
| . 8 | 85.7 | 86.7 | 87.6 | 88.5 | S9.5 | 90.5 | 91.4 | 92.4 | 93.3 | 94.3 | 95.3 | 96.2 |
| . 8 | S5.2 | S6. I | 87.0 | 88.0 | SS. 9 | S9.9 | 90.8 | 91.8 | 92.7 | 93.7 | 94.7 | 95.6 |

Table 70.
DIFFERENCE OF HEIGHT CORRESPONDING TO A CHANGE OF 1 MILLIMETER IN THE BAROMETER.

METRIC MEASURES.

| Barometric Pressure. | MEAN TEMPERATURE OF THE AIR IN CENTIGRADE DEGREES. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-2^{\circ}$ | $0^{\circ}$ | $2^{\circ}$ | $4^{\circ}$ | $6^{\circ}$ | $8^{\circ}$ | $10^{\circ}$ | $12^{\circ}$ | $14^{\circ}$ | $16^{\circ}$ |
| $\begin{aligned} & \mathrm{mm} . \\ & 760 \end{aligned}$ | $\begin{array}{\|c} \text { Meters. } \\ 10.48 \end{array}$ | $\begin{gathered} \text { Meters. } \\ 10.57 \end{gathered}$ | Meters. 10.65 | $\begin{array}{\|c\|} \hline \text { Meters. } \\ 10.73 \end{array}$ | Meters. IO.SI | Meters. $\text { Io. } 89$ | Meters. $10.9 \mathrm{~S}$ | Meters. <br> II. 06 | $\begin{gathered} \text { Meters. } \\ \text { II. I5 } \end{gathered}$ | $\begin{gathered} \text { Meters. } \\ \text { I } 1.23 \end{gathered}$ |
| 750 | 10.62 | 10.71 | 10.79 | 10.87 | 10.95 | II. 04 | 11.13 | II. 2 I | II. 30 | II. 38 |
| 740 | 10.77 | 10.85 | 10.93 | 1 I .02 | II. 10 | II. 19 | II. 28 | II 1. 36 | 11.45 | II. 54 |
| 730 | 10.91 | 11.00 | 11.08 | 11.17 | II. 26 | II. 35 | 11.43 | II. 52 | 11.61 | 11.70 |
| 720 | 11.06 | II. 15 | 11.24 | 11.32 | 11.42 | II. 51 | II 1.59 | I 1.68 | I 1.77 | I 1.86 |
| 710 | I 1.22 | 11.31 | I 1.40 | II 1.48 | II. 58 | 11.67 | 11.75 | II. $\mathrm{S}_{5}$ | II 1.94 | 12.03 |
| 700 | II. 3 S | 11.47 | 11.56 | 11.65 | II. 74 | I 1.83 | II. 92 | 12.02 | 12.11 | 12.20 |
| 690 | I I. 55 | 11.63 | 11.72 | 11.82 | 11.91 | 12.00 | 12.09 | 12.19 | 12.28 | 12.38 |
| 680 | 11.72 | II. So | $11 . \mathrm{S} 9$ | 11.99 | 12.08 | 12.18 | 12.27 | 12.37 | 12.46 | 12.56 |
| 670 | II. 89 | 11.98 | 12.07 | 12.17 | 12.26 | 12.36 | 12.46 | 12.55 | 12.65 | 12.75 |
| 660 | 12.07 | 12.16 | 12.26 | 12.35 | 12.45 | I2.55 | 12.65 | 12.74 | 12.84 | 12.94 |
| 650 | 12.26 | 12.35 | 12.45 | 12.54 | 12.64 | 12.74 | 12.84 | 12.94 | 13.04 | 13.14 |
| 640 | I 2.45 | 12.55 | 12.64 | 12.74 | 12.84 | 12.94 | 13.04 | I3.14 | 13.24 | 13.35 |
| 630 | 12.65 | 12.75 | 12.84 | 12.94 | 13.04 | I3.15 | 13.25 | 13.35 | 13.45 | 13.56 |
| 620 | 12.85 | 12.96 | 13.05 | 13.15 | ${ }^{1} 3.25$ | 13.36 | 13.46 | I 3.57 | 13.67 | 13.78 |
| 610 | 13.06 | 13.17 | 13.27 | 13.37 | 13.47 | ${ }^{1} 3.58$ | ${ }^{1} 3.68$ | 13.79 | 13.89 | 14.01 |
| 600 | 13.28 | 13.39 | 13.49 | 13.59 | 13.70 | 13.80 | I3.91 | 14.02 | 14.13 | 14.24 |
| 590 | I 3.51 | 13.62 | 13.72 | 13.82 | 13.93 | 14.03 | I4. 15 | 14.26 | 14.37 | 14.48 |
| 5 So | 13.74 | 13.85 | ${ }^{1} 3.96$ | 14.06 | 14.17 | 14.28 | 14.39 | 14.51 | 14.62 | 14.73 |
| 570 | 13.98 | 14.09 | 14.20 | 14.31 | 14.42 | 14.53 | 14.64 | 14.76 | 14.88 | 14.99 |
| 560 | 14.23 | 14.34 | 14.45 | I. 4.57 | 14.68 | I4.79 | 14.90 | 15.02 | I5.14 | I 5.25 |
| Barom $n$ tric Pressure. | MEAN TEMPERATURE OF THE AIR IN CENTIGRADE DEGREES. |  |  |  |  |  |  |  |  |  |
|  | $18^{\circ}$ | $20^{\circ}$ | $22^{\circ}$ | $24^{\circ}$ | $26^{\circ}$ | $28^{\circ}$ | $30^{\circ}$ | $32^{\circ}$ | $34^{\circ}$ | $36^{\circ}$ |
| $\begin{aligned} & \mathrm{mm} . \\ & 760 \end{aligned}$ | Meters. $\text { II. } 32$ | $\begin{gathered} \hline \text { Meters. } \\ \text { II. } 4 \mathrm{I} \end{gathered}$ | Meters. $\text { II } 49$ | Meters. $11.58$ | $\begin{gathered} \text { Meters. } \\ \text { I I. } 66 \end{gathered}$ | $\begin{gathered} \hline \text { Meters. } \\ \text { II. } 75 \end{gathered}$ | Meters. $\text { II. } 84$ | Meters. $11.92$ | $\begin{array}{\|c\|} \hline \text { Meters. } \\ \text { I2.0I } \end{array}$ | Meters. $\text { 12. } 10$ |
| 750 | II. 47 | II. 56 | 11.64 | II. 73 | II. $\mathrm{S}_{2}$ | 11.91 | 12.00 | 12.08 | 12.17 | 12.26 |
| 740 | 11.63 | II. 72 | 11.80 | 11.89 | II.98 | 12.07 | 12.16 | 12.24 | 12.33 | 12.42 |
| 730 | II. 79 | II .88 | 11.96 | 12.05 | 12.15 | 12.23 | 12.32 | 12.41 | 12.50 | 12.59 |
| 720 | 11.95 | 12.04 | 12.13 | 12.22 | 12.32 | 12.40 | 12.49 | 12.58 | 12.68 | 12.77 |
| 710 | I2.12 | 12.21 | 12.30 | 12.39 | 12.49 | 12.58 | 12.67 | 12.76 | I2. 86 | 12.95 |
| 700 | 12.29 | 12.39 | 12.48 | 12.57 | 12.67 | 12.76 | 12.85 | 12.94 | 13.04 | 13.13 |
| 690 | 12.47 | 12.57 | 12.66 | 12.75 | 12.85 | 12.94 | 13.04 | 13.13 | 13.23 | 13.32 |
| 6So | 12.66 | 12.75 | 12.85 | 12.94 | 13.04 | I3.13 | 13.23 | 13.32 | 13.42 | 13.52 |
| 670 | 12.85 | 12.94 | 13.04 | 13.14 | 13.23 | ${ }^{1} 3.33$ | 13.43 | 13.52 | 13.62 | I 3.72 |
| 660 | 13.04 | 13.14 | 13.24 | 13.34 | 13.43 | 13.53 | 13.63 | 13.73 | 13.83 | 13.93 |
| 650 | I 3.24 | I3.34 | 13.44 | 13.54 | 13.64 | 13.74 | 13.84 | 13.94 | 1.4 .04 | 14.15 |
| 640 | 13.45 | 13.55 | 13.65 | 13.75 | 13.85 | 13.96 | 14.06 | 14.15 | 14.26 | 14.37 |
| 630 | 13.66 | 13.76 | 13.87 | 13.97 | 14.07 | 14.18 | 14.28 | 14.38 | 14.49 | 14.60 |
| 620 | 13.85 | 13.98 | 14.09 | 14.20 | 14.30 | 14.41 | 14.51 | 14.62 | 14.72 | 14.83 |
| 610 | 14.11 | 14.2 I | 14.32 | 14.43 | 14.54 | 14.64 | 14.75 | 14.86 | 14.96 | 15.07 |
| 600 | 14.35 | 14.45 | 14.56 | 14.67 | 14.78 | 14.89 | ${ }^{1} 5.00$ | ${ }^{15} 511$ | 15.21 | 15.32 |
| 590 | 14.59 | 14.70 | 14.81 | 14.92 | 15.03 | 15.14 | 15.25 | 15.36 | 15.47 | 15.59 |
| 580 | 14.84 | 14.95 | 15.07 | 15.17 | 15.29 | 15.40 | ${ }^{15} 5.52$ | 15.63 | 15.74 | 15.86 |
| 570 | 15.10 | 15.21 | 15.33 | 15.44 | 15.56 | 15.67 | 15.79 | 15.91 | 16.02 | 16.14 |
| 560 | 15.37 | 15.48 | 15.60 | 15.72 | 15.84 | 15.95 | 16.07 | 16.19 | 16.30 | 16.42 |

Table 71.

## DETERMINATION OF HEIGHTS BY THE BAROMETER.

## Formula of Babinet.

$$
z=C \frac{B_{0}-B}{B_{0}+B}
$$

$C($ in feet $)=52494\left[1+\frac{t_{0}+t-64}{900}\right]-$ English Measures.
$C$ (in metres) $=16000\left[1+\frac{2\left(t_{0}+t\right)}{1000}\right]$-Metric Measures.
In which $Z=$ Difference of height of two stations in feet or metres.
$B_{0}, B=$ Barometric readings at the lower and upper stations respectively, corrected for all sources of instrumental error.
$t_{0}, t=$ Air temperatures at the lower and upper stations respectively.
Values of $C$.
ENGLISH MEASURES.

| $1 / 2\left(t_{0}+\mathbf{t}\right)$. | $\log C$. | c. |
| :---: | :---: | :---: |
| F. |  | Feet. |
| $10^{\circ}$ | 4.69834 | 4992 S |
| 15 | . 70339 | 50511 |
| 20 | .70837 | 51094 |
| 25 | .71330 | 51677 |
| 30 | .71518 | 52261 |
| 35 | 4.72300 | 52844 |
| 40 | . 72777 | 53428 |
| 45 | . 73248 | 5401 I |
| 50 | . 73715 | 54595 |
| 55 | .74177 | 55178 |
| 60 | 4.74633 | 55761 |
| 65 | . $750 \mathrm{~S}_{5}$ | 56344 |
| 70 | . 75532 | 56927 |
| 75 | . 75975 | 5751 I |
| So | .76413 | 5So94 |
| 85 | 4.76847 | 5S677 |
| 90 | . 77276 | 59260 |
| 95 | .77702 | 59844 |
| 100 | .78123 | 60427 |


| $1 / 2\left(t_{0}+\mathbf{t}\right)$. | $\log C$. | c. |
| :---: | :---: | :---: |
| c. |  | Metres. |
| $-10^{\circ}$ | 4.IS639 | 15360 |
| -8 | . 19000 | 15488 |
| -6 | . 19357 | 15616 |
| -4 | . 19712 | 15744 |
| -2 | . 20063 | 15872 |
| 0 | 4.20412 | 16000 |
| $+2$ | . 20758 | 16128 |
| 4 | . 211 IOI | 16256 |
| 6 | . 21442 | 16384 |
| S | . 21780 | 16512 |
| 10 | 4.22II5 | 16640 |
| 12 | . 224.48 | 16768 |
| 14 | . 22778 | 16896 |
| 16 | .23106 | 17024 |
| 18 | . $23+3 \mathrm{I}$ | 17152 |
| 20 | 4.23754 | 17280 |
| 22 | . 2.4075 | 17408 |
| 24 | . 24393 | ${ }^{17536}$ |
| 26 | .24709 | 17664 |
| 28 | . 25022 | 17792 |
| 30 | 4.25334 | 17920 |
| 32 | . 25643 | $1 \mathrm{SO}_{48}$ |
| 34 | . 25950 | ${ }_{18176}$ |
| 36 | . 26255 | $1 \mathrm{~S}_{3} 04$ |

8mithbonian Tables.

Table 72.
BAROMETRIC PRESSURES CORRESPONDING TO THE TEMPERATURE OF THE BOILING POINT OF WATER.

ENGLISH MEASURES.

| $\begin{gathered} \text { Tempera- } \\ \text { ture. } \\ \hline \end{gathered}$ | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| $185^{\circ}$ | 17.075 | 17.112 | 17.150 | 17.187 | 17.224 | 17.262 | 17.300 | 17.337 | 17.375 | 17.413 |
| 186 | 17.450 | 17.488 | 17.526 | 17.564 | 17.602 | 17.641 | 17.679 | 17.717 | 17.756 | 17.794 |
| 187 | 17.832 | 17.871 | 17.910 | 17.948 | 17.987 | 18.026 | 18.065 | IS.104 | 18.143 | 18.182 |
| 188 | 18.221 | 18.261 | 18.300 | 18.340 | 18.379 | 18.419 | 18.458 | 18.498 | 18.538 | 18.578 |
| 189 | 18.618 | 18.658 | 18.698 | 18.738 | 18.778 | 18.818 | 18.859 | 18.899 | 18.940 | 18.980 |
| 190 | 19.02 I | 19.062 | 19.102 | 19.143 | 19.184 | 19.225 | 19.266 | 19.308 | 19.349 | 19.390 |
| 191 | 19.431 | 19.473 | 19.514 | 19.556 | 19.598 | 19.639 | 19.681 | 19.723 | 19.765 | 19.807 |
| 192 | 19.849 | 19.892 | 19.934 | 19.976 | 20.019 | 20.061 | 20.104 | 20.146 | 20.189 | 20.232 |
| 193 | 20.275 | 20.318 | 20.361 | 20.404 | 20.447 | 20.490 | 20.533 | 20.577 | 20.620 | 20.664 |
| 194 | 20.707 | 20.751 | 20.795 | 20.839 | 20.883 | 20.927 | 20.971 | 21.015 | 21.059 | 21.103 |
| 195 | 21.148 | 21.192 | 21.237 | 21.282 | 21.326 | 21.371 | 21.416 | 21.461 | 21.506 | 21.551 |
| 196 | 21.597 | 21.642 | 21.687 | 21.733 | 21.778 | 21.824 | 21.870 | 21.915 | 21.961 | 22.007 |
| 197 | 22.053 | 22.099 | 22.145 | 22.192 | 22.238 | 22.284 | 22.33 I | 22.377 | 22.424 | 22.471 |
| 198 | 22.517 | 22.564 | 22.611 | 22.658 | 22.706 | 22.753 | 22.800 | 22.847 | 22.895 | 22.942 |
| 199 | 22.990 | 23.038 | 23.085 | 23.133 | 23.181 | 23.229 | 23.277 | 23.325 | 23.374 | 23.422 |
| 200 | 23.470 | 23.519 | 23.568 | 23.616 | 23.665 | 23.714 | 23.763 | 23.812 | 23.861 | 23.910 |
| 201 | 23.959 | 24.009 | 24.058 | 24.108 | 24.157 | 24.207 | 24.257 | 24.307 | 24.357 | 24.407 |
| 20 | 24.457 | 24.507 | 24.557 | 24.608 | 24.658 | 24.709 | 24.759 | 24.810 | 24.861 | 24.912 |
| 203 | 24.963 | 25.014 | 25.065 | 25.116 | 25.168 | 25.219 | 25.27 I | 25.322 | 25.374 | 25.426 |
| 204 | 25.478 | 25.530 | 25.582 | 25.634 | 25.686 | 25.738 | 25.791 | 25.843 | 25.896 | 25.948 |
| 205 | 26.001 | 26.054 | 26.107 | 26.160 | 26.213 | 26.266 | 26.319 | 26.373 | 26.426 | 26.480 |
| 206 | 26.534 | 26.587 | 26.641 | 26.695 | 26.749 | 26.803 | 26.857 | 26.912 | 26.966 | 27.021 |
| 207 | 27.075 | 27.130 | 27.184 | 27.239 | 27.294 | 27.349 | 27.404 | 27.460 | 27.515 | 27.570 |
| 208 | 27.626 | 27.681 | 27.737 | 27.793 | 27.848 | 27.904 | 27.960 | 28.016 | 28.073 | 28.129 |
| 209 | 28.185 | 28.242 | 28.298 | 28.355 | 28.412 | 28.469 | 28.526 | 28.583 | 28.640 | 28.697 |
| 210 | 28.754 | 28.812 | 28.869 | 28.927 | 28.985 | 29.042 | 29.100 | 29.158 | 29.216 | 29.275 |
| 211 | 29.333 | 29.391 | 29.450 | 29.508 | 29.567 | 29.626 | 29.685 | 29.744 | 29.803 | 29.862 |
| 212 | 29.92 I | 29.981 | 30.040 | 30.100 | 30.159 | 30.219 | 30.279 | 30.339 | 30.399 | 30.459 |
| 213 | 30.519 | 30.580 | 30.640 | 30.701 | 30.761 | 30.822 | 30.883 | 30.944 | 31.005 | 31.066 |
| 214 | 31.127 | 31.199 | 31.250 | 31.311 | 31.373 | 31.435 | 31.497 | 31.559 | 31.621 | 31.683 |

METRIC MEASURES.
Table 73.

| Tempera- ture. | . 0 | . 1 | . 2 | .3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $80^{\circ}$ | 355.40 | 356.84 | 358.28 | 359.73 | 361.19 | 362.65 | 364.1 I | 365.58 | 367.06 | 368.54 |
| 81 | 370.03 | 371.52 | 373.01 | 374.51 | 376.02 | 377.53 | 379.05 | 380.57 | 382.09 | 383.62 |
| 82 | 385.16 | 386.70 | 388.25 | 389.80 | 391.36 | 392.92 | 394.49 | 396.06 | 397.64 | 399.22 |
| 83 | 400.8 I | 402.40 | 404.00 | 405.6I | 407.22 | 408.83 | $4^{10.45}$ | 412.08 | 413.71 | 415.35 |
| 84 | 416.99 | 418.64 | 420.29 | 421.95 | 423.61 | 425.28 | 426.95 | 428.64 | 430.32 | 432.01 |
| 85 | 433.71 | 435.41 | 437.12 | 438.83 | 440.55 | 442.28 | 444.01 | 445.75 | 447.49 | 449.24 |
| 86 | 450.99 | 452.75 | 454.51 | 456.28 | 458.06 | 459.84 | 461.63 | 463.42 | 465.22 | 467.03 |
| 87 | 468.84 | 470.66 | 472.48 | 474.31 | 476.14 | 477.99 | 479.83 | 481.68 | 483.54 | 485.41 |
| 88 | 487.28 | 489.16 | 491.04 | 492.93 | 494.82 | 496.72 | 498.63 | 500.54 | 502.46 | 504.39 |
| 89 | 506.32 | 508.26 | 510.20 | 512.15 | 514.11 | 516.07 | 518.04 | 520.01 | 521.99 | 523.98 |
| 90 | 525.97 | 527.97 | 529.98 | 531.99 | 534.01 | 536.04 | 538.07 | 540.11 | 542.15 | 544.21 |
| 91 | 546.26 | 548.33 | 550.40 | 552.48 | 554.56 | 556.65 | 558.75 | 560.85 | 562.96 | 565.08 |
| 92 | 567.20 | 569.33 | 571.47 | 573.61 | 575.76 | 577.92 | 580.08 | 582.25 | 584.43 | 586.6 x |
| 93 | 588.80 | 591.00 | 593.20 | 595.4 I | 597.63 | 599.86 | 602.09 | 604.33 | 606.57 | 608.82 |
| 94 | 611.08 | 613.35 | 615.62 | 617.90 | 620.19 | 622.48 | 624.79 | 627.09 | 629.41 | 631.73 |
| 95 | 634.06 | 636.40 | 638.74 | 641.09 | 643.45 | 645.82 | 648.19 | 650.57 | 652.96 | 655.35 |
| 96 | 657.75 | 660.16 | 662.58 | 665.00 | 667.43 | 669.87 | 672.32 | 674.77 | 677.23 | 679.70 |
| 97 | 682.18 | 684.66 | 687.15 | 689.65 | 692.15 | 694.67 | 697.19 | 699.71 | 702.25 | 704.79 |
| 98 | 707.35 | 709.90 | 712.47 | 715.04 | 717.63 | 720.22 | 722.8 I | 725.42 | 728.03 | 730.65 |
| 99 | 733.28 | 735.92 | 738.56 | 741.21 | 743.87 | 746.54 | 749.22 | 751.90 | 754.59 | 757.29 |
| 100 | 760.00 | 762.72 | 765.44 | 768.17 | 770.91 | 773.66 | 776.42 | 779.18 | 781.95 | 784.73 |

## HYGROMETRICAL TABLES.

Pressure of aqueous vapor over ice—English measures . . . Table 74
Pressure of aqueous vapor over water-English measures . . Table 75
Pressure of aqueous vapor over ice—Metric measures . . . Table 76
Pressure of aqueous rapor over water-Metric measures . . Table 77
Pressure of aqueous vapor over ice-Dynamic measures . . Table 78
Pressure of aqueous rapor over water-Dynamic measures . . Table 79
Weight of a cubic foot of saturated vapor-English measures . Table So
Weight of a cubic meter of saturated vapor-Metric measures . Table 8I

Table 74.
PRESSURE OF AQUEOUS VAPOR OVER ICE.
ENGLISH MEASURES.

| Temperature. | Vapor Pressure. | Tempera ture. | Vapor Pressure. | Tempera- <br> e. ture. | Vapor Pressure. | Tempera ture. | Vapor Pressure. |  | Temperature. | Vapor Pressure. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inches. | $F$ $-45^{\circ}$ | Inches. | . $\begin{gathered}\text { F. } \\ -30^{\circ}\end{gathered}$ | Inches. |  | Inches. |  | ${ }^{\text {F. }} 5^{\circ}$ | inches. |
|  | 0.00099 |  | 0. 00275 |  | 0.0070 |  |  |  | $7{ }^{\circ}$ | 0. 02556 |
| 59 | . 00107 | 7 |  | $4{ }^{-29}$ | . 0074 | 14.5 |  | I 738 | 7.0 | 02626 |
| 58 | OOI 14 | 43 | . 00313 | $13-28$ | . 0079 | 514.0 |  | 1787 | 6.5 | . 02698 |
| 57 | . 00123 | 3 | . 00334 | 34 | . 0084 | 413.5 |  | 1838 | 6.0 | . 02771 |
| 56 | . 00131 | I 41 | . 00356 | 26 | . 0089 | $6 \quad 13.0$ |  | 90 | $5 \cdot 5$ | . 02847 |
| -55 | . 00141 | I -40 | . 00379 | $79-25$ | . 000 | $1-12.5$ |  | 43 - | -50 | . 02924 |
| 54 | . 00151 | 1 19 | . 00404 | 424 | . 0100 | 12.0 |  | 1998 | 4. 5 | . 03003 |
| 53 | . 00161 | $1{ }^{8}$ | . 00431 | 123 | - or Io6 | 9 II. 5 |  | 2054 | 4.0 | . 03084 |
| 52 | . 00173 | 3 37 | . 00458 | 8 22 | . OII 13 | 33 I1.0 |  | 2111 | 3.5 | . 03168 |
| 51 | . 00185 | 5 - 36 | . 00488 | 8 | . 0120 | 10.5 |  | 170 | 3.0 | . 03253 |
| -50 | . 00198 | $8-35$ | . 00519 | $19-20$ | . O 12 | $22-10.0$ |  | 230 - | -2.5 | . 03340 |
| 49 | . 00211 | 134 | . 00552 | 52 19 | . 0134 | 47 -9.5 |  | 292 | 2.0 | . 03429 |
| 48 | . 00226 | 633 | . 00588 | 18 | . 014 | 6 9.0 |  | 356 | I. 5 | . 03520 |
| 47 | . 00241 | 132 | . 00625 | 25 17 | . 01510 | 108.5 |  | 421 | - | . 03614 |
| 46 | . 00258 | 8 31 | . 00664 | - 16 |  | 8.0 | . 02487 |  | 0.5 | . 03710 |
| Temperat. | . 0 | . 1 | 2 | . 3 | .4 | .5 | . 6 | . 7 | . 8 | . 9 |
| F. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | nches. | nches. | . Inches. | Inches. |
| 0 | 0.038090 | 0.03829 | 0.038490 | 0.03869 | 0.03890 | 0.039100 | 0. 03930 | 0.03951 | 10.03971 | 10.03992 |
| 1 | . 04013 | . 04034 | . 04055 | . 04076 | . 04097 | . 04118 | . 04140 | . 04161 | 1.04183 | 3.04204 |
| 2 | . 04226 | . 04248 | . 04270 | . 04292 | . 04314 | . 04337 | . 04359 | . 04382 | 2 . 04404 | +.04427 |
| 3 | . 04450 | . 04473 | . 04496 | . 04519 | . 04543 | . 04566 | . 04590 | . 0.4613 | 3.04637 | 7.04661 |
| 4 | . 04685 | .04709 | . 04733 | . 04758 | . 04782 | .04807 | . 0.4831 | . 0.4856 | 6 . 04881 | I . 04906 |
| 5 | . 04931 | . 04956 | . 04982 | . 05007 | . 05033 | . 05058 | .05084 | . 05110 | -. 05136 | 6.05102 |
| 6 | . 05189 | . 05215 | 05242 | . 05269 | . 05296 | . 05322 | . 05350 | . 05377 | 7 . 05404 | 4.05431 |
| 7 | . 05459 | . 05487 | . 05514 | . 05.542 | . 05570 | . 05598 | . 05627 | . 05655 | 5.05684 | 4.05712 |
| 8 | . 05741 | . 05770 | . 05799 | . 05828 | . 05858 | . 05887 | . 05917 | . 05947 | 7.05977 | 7.06007 |
| 9 | . 06037 | . 06067 | . 06098 | . 06128 | . 06159 | . 06190 | . 06221 | . 06252 | 2.06283 | 3.06315 |
| 10 | . 06346 | . 06378 | . 06410 | . 06442 | . 06474 | . 06507 | . 06539 | 06572 | 2.06605 | 5.06638 |
| 11 | . 06670 | . 06703 | . 06737 | . 06770 | . 06804 | . 06838 | . 06872 | . 06906 | 6.06940 | -. 06975 |
| 12 | . 07009 | . 07044 | . 07079 | . 07114 | . 07149 | . 07184 | . 07220 | . 07256 | 6.07292 | 2.07328 |
| 13 | . 07363 | . 07399 | . 07436 | . 07472 | . 07509 | . 07546 | . 07583 | . 07621 | 1.07658 | 8, .07696 |
| 14 | . 07733 | . 07771 | . 07809 | . 07848 | . 07886 | . 07925 | . 07964 | . 08003 | 3 . 08042 | $2 . .08082$ |
| 15 | . O8I 21 | .08161 | . 08201 | . 08241 | .08281 | . 08321 | . 08362 | . 08402 | 2.08443 | 3.08484 |
| 16 | . 08525 | . 08566 | . 08608 | . 08650 | . 08602 | .08734 | . 08777 | . 08SI9 | 9.08862 | 2.08905 |
| 17 | . 08948 | . 08991 | . 09035 | . 09079 | . 00123 | . 09167 | . 09211 | . 09255 | 55.09300 | -. 09345 |
| 18 | . 09390 | . 09435 | . 09481 | . 09520 | . 00572 | . 09618 | . 00664 | . 09711 | I . 09757 | 7 . ogSo4 |
| 19 | . 09851 | . 00898 | . 09046 | . 09994 | . 10042 | . 10090 | . 10138 | 10186 | $66 \cdot 10235$ | 5 . 10284 |
| 20 | . 10333 | . 10383 | . 10432 | . 10482 | 10532 | . 10582 | . 10633 | . 10683 | 3.10734 | $4 \cdot 10785$ |
| 21 | . 10836 | 10888 | . 10940 | . 10992 | . 11044 | . 11096 | . 11149 | . 11202 | 2 . 11255 | 5.11308 |
| 22 | . 11361 | . 11415 | . 11469 | . 11523 | . 11578 | . 11632 | . 11687 | . 11742 | 22.11798 | 8 . 11853 |
| 23 | . 11909 | . 11965 | . 12022 | . 12078 | . 12135 | . 12192 | . 12250 | . 12307 | 7 . 12365 | 5.12423 |
| 24 | . 12481 | . 12540 | . 12598 | . 12657 | . 12717 | . 12776 | . 12836 | . 12896 | 6 . 12956 | 6.13017 |
| 25 | . 13077 | . 13138 | . 13200 | . 13261 | . 13323 | . 13385 | . 13447 | . 13510 | 10.13573 | 3.13636 |
| 26 | . 13699 | . 13763 | . 13827 | . 13891 | . 13956 | . 14021 | . 14086 | . 14151 | 11.14216 | 6 . 14282 |
| 27 | . 14348 | . 14415 | . 14481 | . 14548 | . 14616 | . 14683 | . 14751 | . 14819 | 19.14887 | 7.14956 |
| 28 | . 15024 | . 15093 | . 15163 | . 15233 | . 15303 | . 15374 | . 15444 | . 15515 | 5 . 15586 | 6.15658 |
| 29 | . 15729 | . 15801 | . 15874 | I 5947 | . 16020 | . 16093 | . 16167 | . 16241 | 1 . 16315 | 5.16389 |
| 30 | . 16463 | . 16538 | . 16614 | . 16600 | . 16766 | . 16842 | . 16919 | . 16996 | 6 . 17073 | 3.17150 |
| 31 | . 17228 | . 17306 | . 17386 | 17466 | . 17546 | . 17626 | . 17707 | . 17788 | - I7869 | 9.17950 |
| 32 | . 18032 |  |  |  |  |  |  |  |  |  |

Smithsonian Tables.

ENGLISH MEASURES.

| Temperature. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |  |
| $32^{\circ}$ | 0.1803 | 0.1810 | 0.1818 | 0.1825 | $0.1833$ | $0.1840$ | $0.1847$ | $0.1855$ | $0.1862$ | $0.1870$ |
| 33 | .1877 | . 1885 | .1893 | . 1900 | . 1908 | .1915 | . 1923 | .1931 | . 1939 | . 1946 |
| 34 | . 1954 | . 1962 | . 1970 | . 1978 | . 1986 | .1994 | . 2002 | . 2010 | . 2018 | . 2026 |
| 35 | . 2034 | . 2042 | . 2050 | . 2059 | . 2067 | . 2075 | . 2083 | . 2091 | . 2100 | . 2108 |
| 36 | . 2117 | . 2125 | . 2133 | . 2142 | . 2150 | . 2159 | . 2168 | . 2176 | . 2185 | . 2193 |
| 37 | . 2202 | . 2211 | . 2220 | . 2228 | . 2237 | . 2246 | . 2255 | . 2264 | . 2273 | . 2282 |
| 38 | . 2291 | . 2300 | . 2309 | . 2318 | . 2327 | . 2336 | . 2345 | . 2355 | . 2364 | . 2373 |
| 39 | .2382 | . 2392 | . 2401 | . 2410 | .2420 | . 2429 | . 2439 | . 2448 | . 2458 | . 2467 |
| 40 | . 2477 | .2487 | . 2496 | . 2506 | .2516 | . 2526 | . 2536 | . 2545 | . 2555 | . 2565 |
| 41 | . 2575 | .2585 | . 2595 | . 2606 | . 2616 | . 2626 | . 2636 | . 2646 | . 2656 | . 2667 |
| 42 | . 2677 | . 2687 | . 2698 | . 2708 | . 2719 | . 2729 | . 27.40 | . 2750 | . 2761 | . 2771 |
| 43 | . 2782 | . 2793 | . 2804 | .2814 | . 2825 | . 2836 | . 2847 | . 2858 | . 2869 | . 2880 |
| 44 | .2891 | . 2902 | . 2913 | .2924 | . 2935 | . 2946 | . 2958 | . 2969 | . 2981 | . 2992 |
| 45 | . 3003 | . 3014 | . 3026 | . 3037 | . 3049 | .3061 | . 3073 | - 3084 | . 3096 | . 3108 |
| 46 | . 3120 | . 3132 | . 3144 | . 3156 | . 3167 | . 3179 | . 3191 | . 3203 | . 3216 | . 3228 |
| 47 | . 3240 | . 3252 | . 3265 | - 3277 | -3289 | . 3301 | . 3314 | . 3326 | . 3339 | . 3352 |
| 48 | . 3365 | . 3377 | - 3390 | - 3402 | .3415 | . 3428 | . 3441 | . 3454 | . 3467 | . 3480 |
| 49 | - 3493 | . 3506 | . 3519 | . 3532 | . 3546 | . 3559 | . 3572 | . 3585 | . 3599 | . 3612 |
| 50 | . 3626 | . 3639 | .3653 | . 3666 | . 3680 | -3694 | - 3708 | -3722 | . 3736 | . 3749 |
| 51 | .3763 | - 3777 | -3791 | .3805 | . 3820 | . 3834 | . 3848 | . 3862 | .3876 | . 3890 |
| 52 | . 3905 | .3919 | . 3934 | - 3948 | . 3963 | -3978 | - 3993 | . 4007 | . 4022 | . 4037 |
| 53 | . 4052 | . 4067 | . 4082 | .4097 | -4112 | .4127 | . 4142 | .4157 | .4172 | . 4187 |
| 54 | . 4203 | . 4218 | . 4234 | .4249 | .4265 | . 4280 | . 4296 | .4312 | . 4328 | . 4343 |
| 55 | . 4359 | . 4375 | . 4391 | . 4407 | . 4423 | . 4439 | . 4455 | . 447 I | . 4488 | . 4504 |
| 56 | . 452 I | . 4537 | . 4554 | . 4570 | . 4587 | . 4603 | . 4620 | . 4637 | . 465.4 | . 4670 |
| 57 | . 4687 | . 4704 | . 4721 | . 4738 | . 4755 | . 4772 | . 4790 | . 4807 | . 4824 | . 48.11 |
| 58 | . 4859 | . 4876 | . 4894 | . 4912 | . 4930 | . 4947 | . 4965 | . 4983 | . 5001 | . 5019 |
| 59 | . 5037 | . 5055 | . 5073 | .5091 | . 5110 | . 5128 | . 5146 | . 5164 | . 5183 | . 5201 |
| 60 | . 5220 | . 5239 | . 5258 | . 5276 | - 5295 | . 5314 | . 5333 | . 5352 | -5371 | . 5390 |
| 61 | . 5409 | . 5428 | . 5448 | . 5467 | . 5486 | . 5505 | . 5525 | . 5545 | . 5565 | . 5584 |
| 62 | . 5604 | . 5624 | . 56.44 | .5663 | . 5683 | . 5703 | . 5724 | . 5744 | . 5764 | . 5784 |
| 63 | . 5805 | . 5825 | . 58.46 | . 5866 | . 5887 | . 5908 | . 5929 | . 5950 | . 5971 | . 5992 |
| 64 | . 6013 | . 6034 | . 6055 | . 6076 | . 6097 | .6118 | . 6140 | .6161 | . 6183 | . 620.4 |
| 65 | . 6226 | . 6248 | . 6270 | . 6292 | . 6314 | .6336 | . 6358 | . 6380 | . 6402 | . 6424 |
| 66 | . 6447 | . 6469 | . 6492 | . 6514 | . 6537 | . 6559 | .6582 | . 6605 | . 6628 | . 6651 |
| 67 | . 6674 | . 6697 | . 6721 | . 6744 | . 6767 | . 6790 | . 6814 | .6837 | . 6861 | . 6885 |
| 68 | . 6909 | . 6932 | . 6956 | . 6980 | . 7004 | . 7028 | . 7053 | . 7077 | . 7101 | . 7125 |
| 69 | . 7150 | . 7174 | .7199 | . 7224 | . 7249 | . 7274 | . 7299 | .7324 | . 7348 | . 7373 |
| 70 | . 7399 | . 7424 | . 7449 | . 7474 | . 7500 | . 7526 | .7552 | . 7577 | . 7603 | . 7629 |
| 71 | . 7655 | .7681 | . 7707 | . 7733 | . 7760 | . 7786 | . 7813 | . 7839 | . 7866 | . 7892 |
| 72 | . 7919 | . 7946 | . 7973 | . 8000 | . 8027 | . 8054 | . 8081 | . 8108 | .8136 | . 8163 |
| 73 | .8191 | . 8219 | . 8247 | . 8274 | . 8302 | . 8330 | . 8358 | . 8386 | . 8414 | . 8442 |
| 74 | . 8471 | . 8499 | . 8528 | . 8556 | .8585 | .8614 | . 8643 | . 8672 | .8701 | . 8730 |
| 75 | . 8760 | . 8789 | .88ı8 | . 8847 | . 8877 | . 8007 | . 8937 | . 8966 | . 8996 | . 9026 |
| 76 | . 9056 | . 9086 | .9117 | .9147 | . 9178 | . 9208 | . 9239 | . 9269 | . 9300 | . 9331 |
| 77 | . 9362 | . 9393 | .9424 | . 9455 | . 9487 | .9518 | . 9550 | . 9581 | . 9613 | .9645 |
| 78 | . 9677 | . 9709 | . 9741 | . 9773 | . 9805 | .9837 | . 9870 | . 9902 | . 9935 | . 9968 |
| 79 | 1.0001. | 1.0033 | 1.0066 | 1.0099 | 1.0133 | 1.0166 | 1.0199 | 1.0232 | 1.0266 | 1.0300 |
| 80 | 1.0334 | 1.0367 | 1.0401 | 1.0435 | 1.0470 | 1.0504 | 1.0538 | 1.0572 | 1.0607 | 1.064 1 |

Table 75.
PRESSURE OF AQUEOUS VAPOR OVER WATER.
ENGLISH MEASURES.

| Temperature. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| $80^{\circ}$ | 1.0334 | 1.0367 | 1.0401 | 1.0435 | 1.0470 | 1.0504 | 1.0538 | 1.0572 | 1.0607 | 1.0641 |
| 81 | 1.0676 | 1.0711 | 1.0746 | 1.0781 | 1.0816 | 1.0851 | 1.0887 | 1.0022 | 1.0958 | 1.0993 |
| 82 | 1.1029 | 1.1065 | 1.1ioi | 1.1137 | 1.1173 | 1.1209 | 1.1246 | 1.1282 | I.1319 | 1.1355 |
| 83 | 1.1392 | 1.1429 | 1.1466 | 1.1503 | 1.1540 | 1.1577 | 1.165 | 1.1652 | 1.1690 | 1.1727 |
| 84 | 1.1765 | 1.1803 | I.IS4I | 1.1879 | 1.1917 | 1.1955 | 1.1994 | 1. 2032 | 1.2071 | 1.2110 |
| 85 | 1.2149 | 1.2188 | 1.2227 | 1. 2266 | 1.2305 | 1.2344 | 1.2384 | I. 2423 | 1.2463 | 1.2503 |
| 86 | 1.2543 | 1.2583 | I. 2623 | I. 2663 | 1.2704 | 1.2744 | 1.2785 | 1. 2826 | 1.2867 | 1.2908 |
| 87 | I. 2949 | 1. 2990 | 1.3031 | 1.3072 | 1.3114 | I. 3155 | 1.3197 | I. 3239 | 1.3281 | 1.3323 |
| 88 | 1.3365 | 1.3407 | I. 3450 | 1. 3492 | 1.3535 | 1.3578 | 1.3621 | I. 3664 | 1.3707 | 1.3750 |
| 89 | I. 3794 | 1.3837 | 1.3881 | 1.3925 | I. 3969 | 1.4013 | 1.4057 | I. 410 I | 1.4146 | 1.4190 |
| 90 | 1.4234 | 1.4279 | I. 4324 | 1. 4360 | 1.44 I 4 | I. 4459 | 1.4505 | I. 4550 | 1.4596 | 1.4642 |
| 91 | 1.4688 | 1.4734 | 1.4780 | 1. 4826 | 1.4872 | 1.4918 | I. 4965 | 1.5012 | 1.5059 | 1.5106 |
| 92 | 1.5153 | 1. 5200 | I. 5247 | I. 5294 | I. 5342 | 1.5390 | 1.5438 | I. 5486 | 1. 5534 | 1.5582 |
| 93 | I. 5630 | 1.5678 | 1.5727 | 1.5776 | 1.5825 | 1.5874 | 1.5923 | 1.5972 | 1.6022 | 1.6071 |
| 94 | 1.612I | 1.6171 | 1.6221 | 1.6271 | 1.632 I | 1.6371 | 1. 6422 | 1.6472 | 1.6523 | 1. 6574 |
| 95 | 1. 6625 | 1.6676 | 1.6728 | 1.6779 | 1.683I | 1.6882 | 1.6934 | I. 6986 | 1.7038 | 1.7090 |
| 96 | 1.7143 | 1.7195 | 1.7248 | 1.7301 | 1.7354 | 1.7407 | 1. 7460 | 1.7513 | 1.7567 | 1.7620 |
| 97 | 1.7674 | 1. 7728 | 1.7782 | 1. 7836 | 1.7891 | 1.7945 | I. 8000 | I. 8055 | 1.SIIO | 1. 81.65 |
| 98 | 1.8220 | 1.8275 | 1.8331 | 1.8386 | 1.8442 | 1.8498 | I. 8554 | 1.8610 | 1. 8667 | 1.8723 |
| 99 | 1.8780 | 1.8837 | 1.8894 | 1.8951 | 1.9008 | 1.9065 | 1.9123 | 1.9ISI | 1.9239 | 1.9297 |
| 100 | 1.9355 | 1.9413 | 1.9472 | 1.9530 | 1.9589 | 1.9648 | 1.9707 | 1.9766 | 1.9826 | 1.9885 |
| 101 | 1.9945 | 2.0005 | 2.0065 | 2.0125 | 2.0185 | 2.0245 | 2.0306 | 2.0367 | 2.0428 | 2.0489 |
| 102 | 2.0550 | 2.0611 | 2.0673 | 2.0735 | 2.0797 | 2.0859 | 2.0921 | 2.0083 | 2.10 .46 | 2.1108 |
| 103 | 2.1171 | 2.1234 | 2.1298 | 2.1361 | 2.1425 | 2.1488 | 2.1552 | 2.1616 | 2.1680 | 2.1744 |
| 104 | 2.1809 | 2.1874 | 2.1939 | 2.2004 | 2.2069 | 2.2134 | 2.2200 | 2.2265 | 2.2331 | 2.2397 |
| 105 | 2.2463 | 2.2529 | 2.2596 | 2.2663 | 2.2730 | 2.2797 | 2.2864 | 2.2931 | 2.2999 | 2.3067 |
| 106 | 2.3135 | 2.3203 | 2.3271 | 2.3339 | 2.3408 | 2.3477 | 2.3546 | 2.3615 | 2.3684 | 2.3753 |
| 107 | 2.3823 | 2.3893 | 2.3963 | 2.4033 | 2.4103 | 2.4173 | 2.4244 | 2.4315 | 2.4386 | 2.4457 |
| 108 | 2.4529 | 2.4600 | 2.4672 | 2.4744 | 2.4816 | 2.4888 | 2.4961 | 2.5033 | 2.5106 | 2.5179 |
| 109 | 2.5252 | 2.5325 | 2.5399 | 2.5473 | 2.5547 | 2.562 I | 2.5695 | 2.5770 | 2.5845 | 2.5919 |
| 110 | 2.5994 | 2.6069 | 2.6145 | 2.6220 | 2.6296 | 2.6372 | 2.6448 | 2.6524 | 2.6601 | 2.6678 |
| III | 2.6755 | 2.6832 | 2.6909 | 2.6986 | 2.7064 | 2.7142 | 2.7220 | 2.7298 | 2.7377 | 2.7456 |
| I | 2.7535 | 2.7614 | 2.7693 | 2.7772 | 2.7852 | 2.7932 | 2.8012 | 2.8002 | 2.8173 | 2.8253 |
| II3 | 2.8334 | 2.8415 | 2.8496 | 2.8577 | 2.8659 | 2.8741 | 2.8823 | 2.8905 | 2.8988 | 2.9070 |
| II4 | 2.9153 | 2.9236 | 2.9320 | 2.9403 | 2.9487 | 2.957 I | 2.9655 | 2.9739 | 2.9823 | 2.9908 |
| 115 | 2.9993 | 3.0078 | 3.0163 | 3.0248 | 3.0334 | 3.0420 | 3.0506 | 3.0592 | 3.0679 | 3.0766 |
| 116 | 3.0853 | 3.0940 | 3.1027 | 3.1115 | 3.1203 | 3.1291 | 3.1379 | 3.1467 | 3.1556 | 3.1645 |
| 117 | 3.1734 | 3.1823 | 3.1913 | 3.2003 | 3.2093 | 3.2183 | 3.2273 | 3.2364 | 3.2455 | 3.2546 |
| 118 | 3.2637 | 3.2728 | 3.2820 | 3.2912 | 3.300.4 | 3.3096 | 3.3189 | $3 \cdot 3282$ | 3.3375 | 3.3468 |
| 119 | 3.3562 | $3 \cdot 3655$ | 3.3749 | $3 \cdot 3843$ | 3.3938 | 3.4032 | 3.4127 | 3.4222 | 3.4318 | 3.4413 |
| 120 | 3.4509 | 3.4605 | 3.4701 | 3.4797 | 3.489 .4 | 3.499 I | 3.5088 | 3.5185 | 3.5283 | 3.5381 |
| 121 | 3.5479 | 3.5577 | 3.5676 | 3.5774 | 3.5873 | 3.5972 | 3.6072 | 3.6172 | 3.6272 | 3.6372 |
| 122 | 3.6472 | 3.6573 | 3.6674 | 3.6775 | 3.6876 | 3.6977 | 3.7079 | 3.7181 | 3.7284 | 3.7386 |
| 123 | 3.7489 | 3.7592 | 3.7695 | 3.7799 | 3.7903 | 3.8007 | 3.8111 | 3.8215 | 3.8320 | 3.8425 |
| 124 | 3.8530 | 3.8636 | 3.8742 | 3.8848 | 3.8954 | 3.9060 | 3.9107 | 3.9274 | 3.938 I | 3.9488 |
| 125 | 3.9596 | 3.9704 | 3.9813 | 3.9921 | 4.0030 | 4.0139 | 4.0248 | 4.0357 | 4.0467 | 4.0577 |
| 126 | 4.0687 | 4.0797 | 4.0908 | 4.1019 | 4.1131 | 4.1242 | 4.1354 | 4.1466 | 4.1578 | 4.1690 |
| 127 | 4.1803 | 4.1916 | 4.2030 | 4.2143 | 4.2256 | 4.2370 | 4.2485 | 4.2599 | 4.2714 | 4.2829 |
| 128 | 4.2945 | 4.3061 | 4.3177 | $4 \cdot 3293$ | 4.3410 | 4.3527 | 4.3645 | 4.3702 | 4.3880 | 4.3998 |
| 129 | 4.4116 | 4.4235 | 4.4354 | 4.4473 | 4.4592 | 4.47 II | 4.483 I | 4.4951 | 4.5072 | 4.5192 |
| 130 | 4.5313 | $4 \cdot 5434$ | 4.5555 | 4.5677 | 4.5798 | 4.592 I | 4.6043 | 4.6166 | 4.6289 | 4.6412 |

## PRESSURE OF AQUEOUS VAPOR OVER WATER.

ENGLISH MEASURES.

| Temperature. | . 0 | . 1 | . 2 | . 3 | . 4 | .5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| $130^{\circ}$ | 4.53 I | $4 \cdot 5+3$ | 4.556 | 4.568 | 4.580 | 4.592 | 4.604 | 4.617 | 4.629 | 4.641 |
| 131 | 4.654 | 4.666 | 4.678 | 4.691 | 4.703 | 4.716 | 4.728 | 4.741 | 4.754 | 4.766 |
| 132 | 4.779 | 4.792 | 4.80 .4 | 4.817 | 4.830 | 4.843 | 4.855 | 4.868 | 4.88 I | 4.894 |
| 133 | 4.907 | 4.920 | 4.933 | 4.946 | 4.959 | 4.972 | 4.985 | 4.998 | 5.012 | 5.025 |
| 134 | 5.038 | 5.05 I | 5.065 | 5.078 | 5.091 | 5.105 | 5.118 | 5.132 | 5.145 | 5.158 |
| 135 | 5.172 | 5.186 | 5.190 | 5.213 | 5.226 | 5.240 | 5.254 | 5.268 | 5.28 I | 5.295 |
| 136 | 5.309 | $5 \cdot 323$ | 5.337 | $5 \cdot 35 \mathrm{I}$ | 5.365 | 5.379 | 5.392 | 5.407 | 5.42 I | 5.435 |
| 137 | 5.449 | 5.463 | 5.477 | 5.492 | $5 \cdot 506$ | $5 \cdot 520$ | 5.535 | 5.549 | 5.563 | 5.578 |
| 138 | 5.592 | 5.607 | 5.621 | 5.636 | 5.650 | 5.665 | 5.680 | 5.694 | 5.709 | 5.724 |
| 139 | $5 \cdot 739$ | 5.754 | 5.768 | $5 \cdot 783$ | $5 \cdot 798$ | 5.813 | 5.828 | 5.843 | 5.858 | 5.873 |
| 140 | 5.889 | 5.904 | 5.919 | 5.934 | 5.949 | 5.965 | 5.980 | 5.995 | 6.011 | 6.026 |
| 141 | 6.041 | 6.057 | 6.072 | 6.088 | 6.104 | 6.119 | 6.135 | 6.151 | 6.166 | 6.182 |
| 142 | 6.198 | 6.214 | 6.229 | 6.245 | 6.261 | 6.277 | 6.293 | 6.309 | 6.325 | 6.34 r |
| 143 | 6.358 | 6.374 | 6.390 | 6.406 | 6.422 | 6.439 | 6.455 | 6.472 | 6.488 | 6.504 |
| 144 | 6.52 I | 6.537 | 6.554 | 6.571 | 6.587 | 6.604 | 6.621 | 6.637 | 6.654 | 6.671 |
| 145 | 6.688 | 6.705 | 6.722 | 6.739 | 6.756 | 6.773 | 6.790 | 6.807 | 6.824 | 6.841 |
| 146 | 6.858 | 6.876 | 6.803 | 6.910 | 6.928 | 6.945 | 6.962 | 6.980 | 6.997 | 7.015 |
| 147 | 7.032 | 7.050 | 7.068 | 7.085 | 7.103 | 7.121 | 7.139 | 7.156 | 7.174 | 7.192 |
| 148 | 7.210 | 7.228 | 7.246 | 7.264 | 7.282 | 7.300 | 7.319 | $7 \cdot 337$ | $7 \cdot 355$ | 7.374 |
| 149 | 7.392 | 7.410 | $7 \cdot 429$ | 7.447 | $7 \cdot 466$ | $7 \cdot 484$ | $7 \cdot 503$ | $7 \cdot 52 \mathrm{I}$ | 7.540 | 7.559 |
| 150 | 7.577 | 7.596 | 7.615 | 7.634 | 7.653 | 7.672 | 7.691 | 7.710 | 7.729 | 7.748 |
| 151 | 7.767 | 7.786 | 7.805 | 7.824 | 7.844 | 7.863 | 7.882 | 7.902 | 7.921 | 7.941 |
| 152 | 7.960 | 7.980 | 8.000 | 8.019 | 8.039 | 8.059 | 8.078 | 8.098 | 8.118 | 8.138 |
| 153 | 8.158 | 8.178 | 8.108 | 8.218 | 8.238 | 8.258 | 8.278 | 8.298 | 8.319 | 8.339 |
| I 54 | 8.360 | 8.380 | 8.400 | 8.42 I | 8.441 | 8.462 | 8.482 | 8.503 | 8.524 | 8.545 |
| 155 | 8.565 | 8.586 | 8.607 | 8.628 | 8.649 | 8.670 | 8.69 I | 8.712 | 8.733 | 8.754 |
| 156 | S. 776 | 8.797 | 8.818 | 8.839 | 8.861 | 8.882 | 8.904 | 8.025 | 8.947 | 8.968 |
| 157 | 8.990 | 9.012 | 9.034 | 9.055 | 9.077 | 9.099 | 9.121 | 9.143 | 9.165 | 9.187 |
| 158 | 9.209 | 9.231 | 9.253 | 9.276 | 9.298 | 9.320 | 9.342 | 9.365 | 9.387 | 9.410 |
| 159 | 9.432 | 9.455 | 9.478 | 9.500 | 9.523 | 9.546 | 9.569 | 9.592 | 9.615 | 9.638 |
| 160 | 9.661 | 9.684 | 9.707 | 9.730 | 9.753 | 9.776 | 9.799 | 9.823 | 9.846 | 9.870 |
| 161 | 9.893 | 9.916 | 9.940 | 9.964 | 9.987 | 10.011 | 10.035 | 10.059 | 10.082 | 10.106 |
| 162 | 10. 130 | 10.154 | 10.178 | 10.203 | 10.227 | 10.251 | 10.275 | 10.299 | 10.324 | 10.348 |
| r63 | 10.373 | 10.397 | 10.422 | 10.446 | 10.471 | 10.495 | 10.520 | 10.545 | 10.570 | 10.595 |
| 164 | 10.620 | 10.645 | 10.670 | 10.695 | 10.720 | 10.745 | 10.770 | 10.795 | 10.821 | 10.846 |
| 165 | 10.872 | 10.897 | 10.922 | 10.948 | 10.974 | 10.999 | 11.025 | 11.051 | 11.077 | II.102 |
| 166 | I1.128 | 11.154 | 11.180 | 11.206 | 11.232 | 11.258 | II. 284 | 11.311 | 11.337 | 11.363 |
| 167 | 11.390 | 11.417 | II. 444 | 11.470 | Ir. 497 | 11.523 | 11.550 | 11.577 | 11.604 | 11.631 |
| 168 | 11.658 | 11.685 | 11.712 | 11.739 | 11.766 | 11.793 | II.82I | 11.848 | I 1.875 | 11.903 |
| 169 | 11.930 | 11.957 | 11.985 | 12.013 | 12.040 | 12.068 | 12.096 | 12.124 | 12.152 | 12.180 |
| 170 | 12.208 | 12.236 | 12.264 | 12.292 | 12.320 | 12.349 | 12.377 | 12.406 | 12.434 | 12.463 |
| 171 | 12.49 I | 12.520 | 12.548 | 12.577 | 12.606 | 12.635 | 12.664 | 12.693 | 12.722 | 12.75 I |
| 172 | 12.780 | 12.809 | 12.838 | 12.868 | I 2.897 | 12.927 | 12.956 | 12.986 | 13.015 | 13.045 |
| 173 | 13.074 | 13.104 | 13.134 | 13.164 | 13.194 | 13.224 | 13.254 | 13.284 | I3.314 | 13.344 |
| 174 | 13.374 | 13.405 | 13.435 | 13.465 | 1 3.496 | 13.527 | 13.557 | 13.588 | 13.619 | 13.649 |
| 175 | 13.680 | 13.711 | 13.742 | 13.773 | 13.804 | 13.835 | 13.867 | 13.898 | 13.929 | 13.96I |
| 176 | 13.992 | 14.024 | 14.055 | 14.087 | 14.118 | 14.150 | 14.182 | 1.4.214 | 14.246 | 14.278 |
| 177 | 14.310 | 14.342 | 14.374 | 14.406 | 14.438 | 14.47 I | 14.503 | 1.4.536 | 14.568 | 14.601 |
| 178 | 14.633 | 14.666 | 14.699 | 14.731 | 14.764 | 14.797 | 14.830 | 14.864 | 14.897 | 14.930 |
| 179 | 14.963 | 14.996 | 15.030 | 15.063 | 15.097 | 15.130 | 15.164 | 15.197 | 15.231 | 15.265 |
| 180 | 15.299 | 15.333 | 15.367 | 15.401 | 15.435 | 15.469 | 15.504 | 15.538 | 15.572 | 15.607 |

Table 75.
PRESSURE OF AQUEOUS VAPOR OVER WATER.
ENGLISH MEASURES.

| Temperature. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | .7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| $180^{\circ}$ | 15.299 | 15.333 | 15.367 | I5.401 | 15.435 | 15.469 | 15.504 | 15.538 | 15.572 | 15.607 |
| 181 | 15.641 | 15.676 | 15.710 | 15.745 | 15.780 | 15.815 | 15.850 | 15.885 | 15.920 | 15.955 |
| 182 | 15.990 | 16.025 | 16.060 | 16.096 | 16.131 | 16.167 | 16.202 | 16.238 | 16.274 | 16.309 |
| 183 | 16.345 | 16.381 | 16.417 | 16.453 | 16.489 | 16.525 | 16.561 | 16.598 | 16.634 | 16.670 |
| 184 | 16.707 | 16.743 | 16.780 | 16.817 | I6.853 | 16.890 | 16.927 | 16.964 | 17.001 | 17.038 |
| 185 | 17.075 | 17.112 | 17.150 | 17.187 | I7.224 | 17.262 | 17.300 | 17.337 | 17.375 | 17.413 |
| 186 | 17.450 | 17.488 | 17.526 | 17.564 | 17.602 | 17.641 | 17.679 | 17.717 | 17.756 | 17.794 |
| 187 | 17.832 | 17.87 I | 17.910 | 17.9.48 | 17.087 | 18.026 | 18.065 | 18.104 | 18.143 | 18.182 |
| 188 | 18.221 | 18.261 | 18.300 | 18.340 | 18.379 | 18.419 | 18.458 | 18.498 | 18.538 | 18.578 |
| 189 | 18.618 | 18.658 | 18.698 | 18.738 | 18.778 | 18.818 | 18.859 | 18.899 | 18.940 | 18.980 |
| 190 | 19.021 | 19.062 | 19.102 | 19.143 | 19.184 | 19.225 | 19.266 | 19.308 | 19.349 | 19.390 |
| 191 | 19.431 | 19.473 | 19.514 | 19.556 | 10.598 | 19.639 | 19.681 | 19.723 | 19.765 | 19.807 |
| 192 | 19.849 | 19.892 | 19.934 | 19.976 | 20.019 | 20.061 | 20.104 | 20.146 | 20.189 | 20.232 |
| 193 | 20.275 | 20.318 | 20.361 | 20.404 | 20.447 | 20.490 | 20.533 | 20.577 | 20.620 | 20.664 |
| 194 | 20.707 | 20.751 | 20.795 | 20.839 | 20.883 | 20.927 | 20.97 I | 21.015 | 21.059 | 21.103 |
| 195 | 21.148 | 21.102 | 21.237 | 21.282 | 21.326 | 21.371 | 21.416 | 21.461 | 21.506 | 21.551 |
| 196 | 21.597 | 21.642 | 21.687 | 21.733 | 21.778 | 21.824 | 21.870 | 21.915 | 21.961 | 22.007 |
| 197 | 22.053 | 22.099 | 22.145 | 22.192 | 22.238 | 22.284 | 22.331 | 22.377 | 22.424 | 22.471 |
| 198 | 22.517 | 22.504 | 22.611 | 22.658 | 22.706 | 22.753 | 22.800 | 22.847 | 22.895 | 22.942 |
| 199 | 22.990 | 23.038 | 23.085 | 23.133 | 23.181 | 23.229 | 23.277 | 23.325 | 23.374 | 23.422 |
| 200 | 23.470 | 23.519 | 23.568 | 23.616 | 23.665 | 23.714 | 23.763 | 23.812 | 23.861 | 23.910 |
| 201 | 23.959 | 24.009 | 24.058 | 24.108 | 24.157 | 24.207 | 2.4 .257 | 24.307 | 24.357 | 24.407 |
| 202 | 24.457 | 24.507 | 24.557 | 24.608 | 24.658 | 24.709 | 24.759 | 24.810 | 24.861 | 24.912 |
| 203 | 24.963 | 25.014 | 25.065 | 25.116 | 25.168 | 25.219 | 25.27 I | 25.322 | 25.374 | 25.426 |
| 20.4 | 25.478 | 25.530 | 25.582 | 25.634 | 25.686 | 25.738 | 25.791 | 25.843 | 25.896 | 25.948 |
| 205 | 26.001 | 26.054 | 26.107 | 26.160 | 26.213 | 26.266 | 26.319 | 26.373 | 26.426 | 26.480 |
| 206 | 26.534 | 26.587 | 26.641 | 26.695 | 26.749 | 26.803 | 26.857 | 26.912 | 26.966 | 27.021 |
| 207 | 27.075 | 27.130 | 27.184 | 27.239 | 27.294 | 27.349 | 27.404 | 27.460 | 27.515 | 27.570 |
| 208 | 27.626 | 27.681 | 27.737 | 27.793 | 27.848 | 27.904 | 27.960 | 28.016 | 28.073 | 28.129 |
| 209 | 28.185 | 28.242 | 28.298 | 28.355 | 28.412 | 28.469 | 28.526 | 28.583 | 28.640 | 28.697 |
| 210 | 28.754 | 28.812 | 28.869 | 28.927 | 28.985 | 29.042 | 29.100 | 29.158 | 29.216 | 29.275 |
| 211 | 29.333 | 29.391 | 20.450 | 29.508 | 29.567 | 29.626 | 29.685 | 29.744 | 29.803 | 29.862 |
| 212 | 29.92 I | 29.981 | 30.040 | 30.100 | 30.159 | 30.219 | 30.279 | 30.339 | 30.399 | 30.459 |
| 213 | 30.519 | 30.580 | 30.640 | 30.701 | 30.761 | 30.822 | 30.883 | 30.944 | 31.005 | 31.066 |
| 214 | 31.127 | 31.189. | 31.250 | 31.3 II | 31.373 | 31.435 | 31.497 | 31.559 | 31.621 | 31.683 |

Smithsonian Tables.

PRESSURE OF AQUEOUS VAPOR OVER ICE.
METRIC MEASURES


Table 77.
PRESSURE OF AQUEOUS VAPOR OVER WATER.
METRIC MEASURES.

| $\begin{aligned} & \text { Tem- } \\ & \text { pera- } \\ & \text { ture. } \end{aligned}$ | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $0^{\circ}$ | $4 \cdot 580$ | 4.614 | 4.647 | 4.68 I | 4.715 | 4.750 | 4.784 | 4.819 | 4.854 | 4.889 |
| 1 | 4.924 | 4.960 | 4.996 | 5.032 | 5.068 | 5.105 | 5.142 | 5.179 | 5.216 | 5.254 |
| 2 | 5.291 | $5 \cdot 329$ | 5.368 | 5.406 | 5.445 | 5.484 | 5.523 | 5.562 | 5.602 | 5.642 |
| 3 | 5.682 | 5.723 | 5.763 | 5.804 | 5.846 | 5.887 | 5.929 | 5.971 | 6.013 | 6.056 |
| 4 | 6.098 | 6.141 | 6.185 | 6.228 | 6.272 | 6.316 | 6.361 | 6.406 | 6.450 | 6.496 |
| 5 | 6.541 | 6.587 | 6.633 | 6.680 | 6.726 | 6.773 | 6.820 | 6.868 | 6.916 | 6.964 |
| 6 | 7.012 | 7.061 | 7.110 | 7.159 | 7.209 | 7.259 | 7.300 | 7.360 | 7.410 | 7.462 |
| 7 | 7.513 | 7.565 | 7.617 | 7.669 | 7.722 | 7.775 | 7.828 | 7.882 | 7.036 | 7.99 I |
| 8 | 8.045 | 8.100 | 8.156 | 8.211 | 8.267 | S. 324 | 8.380 | S.437 | 8.494 | 8.552 |
| 9 | 8.610 | S.669 | 8.727 | 8.786 | 8.846 | 8.906 | 8.966 | 9.026 | 9.087 | 9.148 |
| 10 | 9.210 | 9.272 | 9.334 | 9.397 | 9.460 | 9.523 | 9.587 | 9.651 | 0.716 | 0.78 x |
| I I | 9.846 | 9.912 | 9.978 | 10.044 | 10.111 | 10.178 | 10.246 | 10.314 | 10.382 | 10.45 I |
| 12 | 10.52 I | 10.590 | 10.660 | 10.731 | 10.801 | 10.873 | 10.044 | 11.016 | 11.080 | 11.162 |
| 13 | 11.235 | 11.309 | 11.383 | 11.458 | II. 533 | 11.608 | I1.684 | 11.761 | 11.837 | 11.915 |
| 14 | 11.992 | 12.070 | 12.149 | 12.228 | I 2.307 | 12.387 | 12.468 | 12.549 | 12.630 | 12.712 |
| 15 | 12.794 | 12.877 | 12.960 | 13.043 | I3.127 | 13.212 | 13.297 | 13.383 | 13.460 | 13.555 |
| 15 | 13.642 | 13.729 | 13.817 | 13.906 | 13.995 | 14.084 | 14.174 | 14.265 | 14.356 | 14.447 |
| 17 | 14.539 | 14.632 | 14.725 | 14.818 | 14.912 | 15.007 | 15.102 | 15.197 | 15.203 | 15.390 |
| 18 | 15.487 | 15.585 | 15.683 | 15.782 | 15.882 | 15.981 | 16.082 | 16.183 | 16.285 | 16.387 |
| 19 | 16.489 | 16.593 | 16.696 | 16.801 | 16.906 | 17.011 | 17.117 | 17.224 | 17.331 | 17.439 |
| 20 | 17.548 | 17.657 | 17.766 | 17.877 | 17.987 | 18.009 | 18.211 | 18.323 | 18.437 | 18.551 |
| 21 | 18.665 | 18.780 | 18.896 | 19.012 | 19.129 | 19.247 | 10.365 | 19.484 | 19.603 | 19.723 |
| 22 | 19.844 | 19.965 | 20.087 | 20.210 | 20.333 | 20.457 | 20.582 | 20.707 | 20.833 | 20.960 |
| 23 | 21.087 | 21.215 | 21.344 | 21.473 | 21.604 | 21.734 | 21.866 | 21.998 | 22.131 | 22.264 |
| 24 | 22.398 | 22.533 | 22.669 | 22.805 | 22.942 | 23.080 | 23.219 | 23.358 | 23.498 | 23.638 |
| 25 | 23.780 | 23.022 | 24.065 | 24.209 | 24.353 | 24.498 | ${ }_{24}{ }^{4} 644$ | 24.791 | 24.938 | 25.086 |
| 26 | 25.235 | 25.385 | 25.535 | 25.687 | 25.839 | 25.901 | 26.145 | 26.299 | 26.455 | 26.610 |
| 27 | 26.767 | 26.925 | 27.083 | 27.242 | 27.402 | 27.563 | 27.725 | 27.887 | 28.051 | 28.215 |
| 28 | 28.380 | 28.546 | 28.712 | 28.880 | 29.048 | 29.217 | 29.387 | 29.558 | 29.730 | 29.903 |
| 29 | 30.076 | 30.25 I | 30.426 | 30.602 | 30.779 | 30.957 | 31.136 | 31.315 | 31.496 | 31.678 |
| 30 | 31.860 | 32.043 | 32.228 | 32.413 | 32.599 | 32.786 | 32.074 | 33.163 | 33.353 | 33.543 |
| 31 | 33.735 | 33.928 | 34.121 | 34.316 | 34.512 | 34.708 | 34.906 | 35.104 | 35.303 | 35.504 |
| 32 | 35.705 | 35.008 | 36.111 | 36.315 | 36.52 I | 36.727 | 36.035 | 37.143 | 37.353 | 37.563 |
| 33 | 37.775 | 37.987 | 38.201 | 38.415 | 38.631 | 38.848 | 30.065 | 39.284 | 39.504 | 39.725 |
| 34 | 39.947 | 40.170 | 40.394 | 40.619 | 40.846 | 41.073 | 41.302 | 41.531 | 41.762 | 41.994 |
| 35 | 42.227 | 42.46 I | +2.696 | 42.932 | 43.170 | 43.408 | 43.648 | 43.889 | 44.131 | 44.374 |
| 36 | 44.619 | 44.804 | 45.111 | $45 \cdot 358$ | 45.608 | 45.858 | 46.109 | 46.362 | 46.615 | 46.870 |
| 37 | 47.127 | 47.384 | 47.643 | 47.902 | 48.163 | 48.426 | 48.689 | 48.054 | 49.220 | 49.487 |
| 38 | 49.756 | 50.025 | 50.296 | 50.560 | 50.842 | 51.117 | 51.393 | 51.670 | 51.949 | 52.229 |
| 39 | 52.510 | 52.793 | 53.077 | 53.362 | 53.649 | 53.937 | 54.226 | 54.516 | 54.808 | 55.101 |
| 40 | $55 \cdot 396$ | 55.692 | 55.989 | 56.288 | 56.588 | 56.889 | 57.102 | 57.496 | 57.802 | 58.109 |
| 41 | 58.417 | 58.727 | 59.038 | 59.351 | 50.665 | 59.9 ${ }^{\text {I }}$ I | 60.298 | 00.616 | 60.036 | 61.257 |
| 42 | 61.580 | 61.004 | 62.230 | 62.557 | 62.886 | 63.216 | 63.547 | 63.880 | 64.215 | 64.551 |
| 43 | 64.889 | 65.228 | 65.560 | 65.911 | 66.255 | 66.600 | 66.947 | 67.295 | 67.645 | 67.997 |
| 44 | 68.350 | 68.704 | 69.06 I | 69.419 | 69.778 | 70.139 | 70.502 | 70.866 | 71.232 | 71.599 |
| 45 | 71.968 | 72.339 | 72.712 | 73.086 | 73.461 | 73.839 | 74.218 | 74.598 | 74.981 | 75.365 |
| 46 | 75.751 | 76.138 | 76.527 | 76.918 | 77.311 | 77.705 | 78.101 | 78.499 | 78.808 | 79.300 |
| 47 | 79.703 | 80.107 | 80.514 | 80.922 | 81.332 | 81.744 | 82.158 | 82.573 | 82.990 | 83.409 |
| 48 | 83.830 | 84.253 88.58 | 84.677 | 85.104 | 85.532 | 85.962 | 86.304 | 86.828 | 87.263 | 87.701 |
| 49 | SS.140 | 88.581 | 80.024 | S0.470 | 89.916 | 90.365 | 90.816 | 91.269 | 91.723 | 92.180 |
| 50 | 92.639 | 93.099 | 93.562 | 94.026 | 94.492 | 94.961 | 95.431 | 95.903 | 96.378 | 96.854 |

METRIC MEASURES.

| Temture. | . 0 | . 1 | . 2 | . 3 | . 4 | .5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $50^{\circ}$ | 92.64 | 93.10 | $93 \cdot 56$ | 94.03 . | 94.49 | 94.96 | 95.43 | 95.90 | 96.38 | 96.85 |
| 51 | 97.33 | 97.81 | 98.30 | 98.78 | 99.27 | 99.76 | 100.25 | 100.74 | IOI. 23 | 101.73 |
| 52 | 102.23 | 102.73 | 103.23 | 103.74 | 104.25 | 104.75 | 105.27 | 105.78 | 106.30 | 106.81 |
| 53 | 107.33 | 107.86 | 108.38 | 108.91 | 109.44 | 109.97 | 110.50 | 111.04 | 111.57 | 112.11 |
| 54 | I 12.66 | 113.20 | 113.75 | 114.30 | 114.85 | 115.40 | 115.96 | 116.51 | 117.07 | 117.64 |
| 55 | 118.20 | 118.77 | 119.34 | 119.91 | 120.49 | 121.06 | 121.64 | 122.22 | 122.81 | 123.39 |
| 56 | 123.98 | 124.57 | 125.16 | 125.76 | 126.36 | 126.96 | 127.56 | 128.17 | 128.77 | 129.38 |
| 57 | 130.00 | 130.61 | 131.23 | 131.85 | 132.47 | 133.10 | 133.73 | 1 34.36 | 134.99 | 135.62 |
| 58 | 136.26 | 136.90 | 137.54 | I38.19 | 138.84 | 139.49 | 140.14 | 140.80 | 141.46 | 142.12 |
| 59 | 142.78 | 143.45 | 144.12 | 144.79 | 145.46 | 146.14 | 146.82 | I 47.50 | 148.19 | 148.88 |
| 60 | 149.57 | 150.26 | 150.95 | 151.65 | 152.35 | 153.06 | 153.77 | I 54.48 | 155.19 | I55.90 |
| 61 | 156.62 | 157.34 | 158.07 | 158.79 | 159.52 | 160.26 | 160.99 | 161.73 | 162.47 | 163.21 |
| 62 | 163.96 | 164.71 | 165.46 | 166.22 | 166.98 | 167.74 | 168.50 | 169.27 | 170.04 | 170.81 |
| 63 | 171.59 | 172.37 | 173.15 | 173.93 | 174.72 | 175.51 | 176.31 | 177.10 | 177.91 | 178.71 |
| 64 | 179.52 | 180.32 | 181.14 | 181.95 | 182.77 | 183.59 | 18.42 | 185.25 | 186.08 | 186.91 |
| 65 | 187.75 | 188.59 | 189.44 | 190.28 | 191.13 | 191.99 | 192.85 | 193.71 | 19.4 .57 | 195.44 |
| 66 | 196.31 | 197.18 | 198.06 | 198.94 | 199.82 | 200.71 | 201.60 | 202.49 | 203.39 | 204.29 |
| 67 | 205.19 | 206.10 | 207.01 | 207.92 | 208.84 | 209.76 | 210.68 | 211.61 | 212.54 | 213.47 |
| 68 | $214.4{ }^{1}$ | 215.35 | 216.30 | 217.24 | 218.20 | 219.15 | 220.11 | 221.07 | 222.04 | 223.01 |
| 69 | 223.98 | 224.96 | 225.94 | 226.92 | 227.91 | 228.90 | 229.89 | 230.89 | 231.89 | 232.90 |
| 70 | 233.91 | 234.92 | 235.94 | 236.96 | 237.98 | 239.01 | 240.04 | 241.08 | 242.12 | 243.16 |
| 71 | 244.21 | 245.26 | 246.31 | 247.37 | 248.43 | 249.50 | 250.57 | 251.64 | 252.72 | 253.80 |
| 72 | 254.88 | 255.97 | 257.07 | 258.16 | 259.27 | 260.37 | 261.48 | 262.59 | 263.71 | $26+83$ |
| 73 | 265.96 | 267.08 | 268.22 | 269.35 | 270.50 | 271.64 | 272.79 | 273.94 | 275.10 | 276.26 |
| 74 | 277.43 | 278.60 | 279.77 | 280.95 | 282.13 | 283.32 | 284.5 1 | 285.71 | 286.90 | 288.11 |
| 75 | 289.32 | 290.53 | 291.74 | 292.97 | 294.19 | 295.42 | 296.65 | 297.89 | 299.13 | 300.38 |
| 76 | 301.63 | 302.89 | 304.15 | 305.4 I | 306.68 | 307.95 | 309.23 | 310.51 | 311.80 | 313.09 |
| 77 | 314.38 | 315.68 | 316.99 | 318.30 | 319.61 | 320.93 | 322.25 | 323.58 | 324.91 | 326.25 |
| 78 | 327.59 | 328.93 | 330.28 | 331.64 | 333.00 | 334.36 | 335.73 | 337.10 | $3384^{88}$ | 339.86 |
| 79 | 341.25 | 342.65 | 344.04 | $3+5.44$ | 346.85 | 348.26 | 349.68 | 351.10 | 352.53 | 3.33 .96 |
| 80 | 355.40 | 356.84 | 358.28 | 359.73 | 361.19 | 362.65 | 364.11 | 365.58 | 367.06 | 368.54 |
| 81 | 370.03 | 371.52 | 373.01 | 374.51 | 376.02 | 377.53 | 379.05 | 380.57 | 382.09 | 383.62 |
| 82 | 385.16 | 386.70 | 388.25 | 389.80 | 391.36 | 392.92 | 394.49 | 396.06 | 397.64 | 399.22 |
| 83 | 400.81 | 402.40 | +04.00 | 405.61 | 407.22 | 408.83 | 410.45 | 412.08 | 413.71 | 415.35 |
| 84 | 416.99 | 418.64 | 420.29 | 421.95 | 423.61 | 425.28 | 426.95 | 428.64 | 430.32 | 432.01 |
| 85 | 433.71 | $435 \cdot 41$ | 437.12 | 438.83 | 440.55 | 442.28 | 444.01 | 445.75 | 447.49 | 449.24 |
| 86 | 450.99 | 452.75 | 454.51 | 456.28 | 458.06 | 459.84 | $46 \pm .63$ | 463.42 | 465.22 | 467.03 |
| 87 | 468.84 | 470.66 | 472.48 | 474.31 | 476.14 | 477.99 | 479.83 | 481.68 | 483.54 | 485.41 |
| 88 | 487.28 | 489.16 | 491.04 | 492.93 | 494.82 | 496.72 | 498.63 | 500.54 | 502.46 | 504.39 |
| 89 | 506.32 | 508.26 | 510.20 | 512.15 | 514.11 | 516.07 | 518.04 | 520.01 | 521.99 | 523.98 |
| 90 | 525.97 | 527.97 | 529.98 | 531.99 | 534.01 | 536.04 | 538.07 | 540.11 | 542.15 | 544.21 |
| 91 | 546.26 | 548.33 | 550.40 | 552.48 | 554.56 | 556.65 | 558.75 | 560.85 | 562.96 | 565.08 |
| 92 | 567.20 | 569.33 | 571.47 | 573.61 | 575.76 | 577.92 | 580.08 | 582.25 | 58.4.43 | 586.61 |
| 93 | 588.80 | 591.00 | 593.20 | 595.41 | 597.63 | 599.86 | 602.09 | 604.33 | 606.57 | 608.82 |
| 94 | 611.08 | 613.35 | 615.62 | 617.90 | 620.19 | 622.48 | 624.79 | 627.09 | 629.41 | 631.73 |
| 95 | 634.06 | 636.40 | 638.74 | 641.09 | 643.45 | 645.82 | 648.19 | 650.57 | 652.96 | $655 \cdot 35$ |
| 96 | 657.75 | 660.16 | 662.58 | 665.00 | 667.43 | 669.87 | 672.32 | 674.77 | 677.23 | 679.70 |
| 97 | 682.18 | 684.66 | 687.15 | 689.65 | 692.15 | 694.67 | 697.19 | 699.71 | 702.25 | 704.79 |
| 98 | 707.35 | 709.90 | 712.47 | 715.04 | 717.63 | 720.22 | 722.81 | 725.42 | 728.03 | 730.65 |
| 99 | 733.28 | 735.92 | 738.56 | 741.21 | 743.87 | 746.54 | 749.22 | 751.90 | 754.59 | 757.29 |
| 100 | 760.00 | 762.72 | 765.44 | 768.17 | 770.91 | 773.66 | 776.42 | 779.18 | 781.95 | 784.73 |

TABLE 77.
PRESSURE OF AQUEOUS VAPOR OVER WATER.
METRIC MEASURES.

| Temperature | $0^{\circ}$ | $1{ }^{\circ}$ | $2^{\circ}$ | $3^{\circ}$ | $4^{\circ}$ | $5^{\circ}$ | $6^{\circ}$ | $7^{\circ}$ | 8 | $9^{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6. | mm. | mm. | mm. | mm. | mm. | m | mm. | mm. | mm. |  |
| $100^{\circ}$ | 760.0 | 787.5 | 815.9 | 845.0 | 875. I | 906.0 | 937.8 | 970.5 | 1004. 2 | 1038.8 |
| 110 | 1074.4 | IIII.O | 1148.6 | 1187.2 | 1226.9 | 1267.7 | 1309.6 | 1352.6 | 1396.8 | I $4+2$. 1 |
| 120 | 1488.7 | 1536.4 | 1585.4 | 1635.7 | 1687.3 | 1740.2 | $179+4$ | 1850.0 | 1907.0 | 1965.4 |
| 130 | 2025.2 | 2086.5 | 2149.3 | 2213.7 | 2279.6 | 2347.0 | 2416.1 | 2486.8 | 2559.2 | 2633.2 |
| I 40 | 2709.0 | 2786.5 | 2865.8 | 2947.0 | 3029.9 | 3114.7 | 3201.4 | 3290. I | 3380.7 | $3+73 \cdot 3$ |
| $150^{\circ}$ | 3507.9 | 3664.6 | 3703.3 | 3864.2 | 3967.2 | 4072.4 | 4179.8 | 4289.5 | 4701.5 | 4515.7 |
| I60 | 4632.4 | 4751.4 | 4872.8 | 4996.7 | 5123.1 | 5252.0 | 5383.4 | 5517.5 | 5654.2 | 5793. 5 |
| 170 | 5935.6 | 6080.4 | 6228.0 | 6378.4 | 6531.7 | 6687.8 | 6846.9 | 7009.0 | 7174.0 | 7342.1 |
| 180 | 7513.3 | 7687.7 | 7865.2 | $80+5 \cdot 9$ | 8229.8 | 8417.0 | 8607.6 | 8801.5 | 8998.9 | 9199.6 |
| $190^{\circ}$ | 9404 | 9612 | 9823 | 10038 | 10257 | 10479 | 10705 | 10935 | 11169 | 11407 |
| 200 | 11648 | 11894 | 12143 | 12397 | 12654 | 12916 | 13182 | 13452 | 13727 | 1,4006 |
| 210 | 14289 | 14577 | 14869 | 15165 | 15467 | 15772 | 16083 | 16398 | 16718 | 17043 |
| 220 | 17372 | 17707 | 18046 | 18391 | 18740 | 19095 | 19454 | 19819 | 20190 | 20565 |
| $230^{\circ}$ | 20946 | 21332 | 21724 | 22121 | 22524 | 22932 | 23347 | 23766 | 24192 | 24623 |
| 240 | 25001 | 25504 | 25953 | 26408 | 26870 | 27337 | 27811 | 28291 | 28778 | 29270 |
| 250 | 29770 | 30275 | 30787 | 31306 | 31832 | 32364 | 32903 | $33+49$ | 34002 | 34562 |
| 260 | 35128 | 35702 | 36283 | 36872 | $37+67$ | 38070 | 38680 | 39298 | 39923 | 40556 |
| 270 | 41197 | 41845 | 42501 | 43165 | 43836 | 44516 | 45204 | 45899 | 46603 | 473 I6 |
| $280^{\circ}$ | 48036 | 48765 | 49503 | 50248 | 51003 | 51766 | 52538 | 53318 | 54108 | 54906 |
| 290 | 55714 | 56530 | 57356 | 58191 | 59035 | 59888 | 60751 | 61624 | 62506 | 63.308 |
| 300 | 64299 | 65211 | 66132 | 67063 | 68005 | 68956 | 69918 | 70890 | 71872 | 72865 |
| 310 | 73869 | 74883 | 75907 | 76043 | 77990 | 79047 | Soli6 | 81195 | 82286 | 83389 |
| 320 | 84503 | 85628 | 86765 | 87913 | 89074 | 90246 | 91430 | 92626 | 93835 | 95056 |
| $330^{\circ}$ | c6280 | 97534 | 98703 | 100060 | 101350 | 102640 | 103950 | 105280 | 106610 | 107960 |
| 340 | 109320 | 110700 | 112090 | 113490 | II 4910 | I 16340 | 117780 | I 19240 | 120720 | 122210 |
| 350 | 123710 | 125220 | 126760 | 128310 | 129870 | 131440 | 133030 | I 34640 | 136270 | 137000 |
| 360 | 130560 | $1+1230$ | 142020 | I+4620 | $14634^{\circ}$ | 148070 | 149820 | I5 I 590 | 153380 | 155180 |
| 370 | 157000 | 158840 | 160690 | 162560 | 164450 |  |  |  |  |  |

SMITHSONIAN TABLES.

PRESSURE OF AQUEOUS VAPOR OVER ICE.
DYNAMIC MEASURES

| Temp. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mb | mb. | mb. | mb. | mb. | mb. | mb. | mb. | m | mb |
| $-70^{\circ}$ | 0.0026 | 0.0025 | 0.0025 | 0.0025 | 0.0024 | 0.0024 | 0.0024 | 0.0023 | 0.0023 | 0.0023 |
| -69 | 0.0030 | 0.0029 | 0.0029 | 0.0029 | 0.0028 | 0.0028 | 0.0027 | 0.0027 | 0.0027 | 0.0026 |
| -68 | 0.0035 | 0.0034 | 0.0034 | 0.0033 | 0.0033 | 0.0032 | 0.0032 | 0.0031 | 0.0031 | 0.0030 |
| -67 | 0.0040 | 0.0040 | 0.0039 | 0.0038 | 0.0038 | 0.0037 | 0.0037 | 0.0036 | 0.0036 | 0.0035 |
| -66 | 0.00 .46 | 0.0046 | 0.0045 | 0.0044 | 0.0044 | $0.00+3$ | 0.0043 | 0.0042 | 0.0041 | 0.0041 |
| -65 | 0.0054 | 0.0053 | 0.0052 | 0.0051 | 0.0051 | 0.0050 | 0.0049 | 0.0048 | 0.00 .48 | 0.0047 |
| -64 | 0.0062 | 0.0061 | 0.0060 | 0.0059 | 0.0058 | 0.0057 | 0.0057 | 0.0056 | 0.0055 | 0.0054 |
| -63 | 0.0071 | 0.0070 | 0.0069 | 0.0068 | 0.0067 | 0.0066 | 0.0065 | $0.006+$ | 0.0063 | 0.0063 |
| -62 | 0.0082 | 0.0080 | 0.0079 | 0.0078 | 0.0077 | 0.0076 | 0.0075 | $0.007+$ | 0.0073 | 0.0072 |
| -6I | 0.0094 | 0.0092 | 0.0091 | 0.0090 | 0.0089 | 0.0087 | 0.0086 | 0.0085 | $0.008+$ | 0.0083 |
| -60 | 0.011 | 0.011 | 0.010 | . 010 | . 010 | 0.010 | 0.0099 | 0.0097 | 0.0096 | 0.0095 |
| -59 | 0.012 | 0.012 | 0.012 | 0.012 | 0.012 | 0.011 | 0.011 | 0.01 I | 0.011 | 0.01 I |
| $-58$ | 0.014 | 0.014 | 0.014 | 0.013 | 0.013 | 0.013 | 0.013 | 0.013 | 0.013 | 0.012 |
| -57 | 0.016 | 0.016 | 0.016 | 0.015 | 0.015 | 0.015 | 0.015 | 0.015 | 0.014 | 0.014 |
| -56 | 0.018 | 0.018 | 0.018 | 0.018 | 0.017 | 0.017 | 0.017 | 0.017 | 0.016 | 0.016 |
| --55 | 0.02 I | 0.021 | 0.020 | 0.020 | 0.020 | 0.020 | 0.019 | 0.019 | 0.019 | 0.019 |
| -54 | 0.024 | 0.023 | 0.023 | 0.023 | 0.022 | 0.022 | 0.022 | 0.022 | 0.021 | 0.021 |
| -53 | 0.027 | 0.027 | 0.026 | 0.026 | 0.026 | 0.025 | 0.025 | 0.025 | 0.024 | 0.024 |
| $-52$ | 0.031 | 0.030 | 0.030 | 0.029 | 0.029 | 0.029 | 0.028 | 0.028 | 0.028 | 0.027 |
| $-51$ | 0.035 | 0.03t | 0.034 | 0.033 | 0.033 | 0.033 | 0.032 | 0.032 | 0.031 | 0.03 I |
| -50 | 0.039 | 0.039 | 0.038 | 0.038 | 0.037 | 0.037 | 0.036 | 0.036 | 0.036 | 0.035 |
| -49 | 0.044 | 0.043 | 0.043 | 0.042 | 0.0 .42 | 0.041 | 0.041 | 0.040 | 0.040 | 0.039 |
| -48 | 0.050 | 0.049 | 0.049 | 0.048 | 0.047 | 0.047 | 0.046 | 0.046 | 0.045 | 0.044 |
| -47 | 0.056 | 0.055 | 0.055 | 0.054 | 0.053 | 0.053 | 0.052 | 0.052 | 0.051 | 0.050 |
| $-46$ | 0.063 | 0.063 | 0.062 | 0.061 | 0.060 | 0.060 | 0.059 | 0.058 | 0.058 | 0.057 |
| -45 | 0.072 | 0.07 I | 0.070 | 0.069 | 0.068 | 0.067 | 0.067 | 0.066 | 0.065 | 0.064 |
| -44 | 0.081 | 0.080 | 0.079 | 0.078 | 0.077 | 0.076 | 0.075 | 0.074 | 0.073 | 0.072 |
| -43 | 0.09 I | 0.090 | 0.089 | 0.088 | 0.087 | 0.086 | 0.085 | 0.084 | 0.083 | 0.082 |
| $-42$ | 0.102 | O.IO1 | 0.100 | 0.098 | 0.097 | 0.096 | 0.095 | 0.094 | 0.093 | 0.092 |
| -4I | 0.115 | 0.113 | 0.112 | O. 11 I | 0.109 | 0.108 | 0.107 | 0.106 | 0.104 | 0.103 |
| -40 | 0.129 | 0.127 | 0.126 | 0. 124 | 0.123 | 0.121 | 0.120 | O.II9 | O. 117 | 0.116 |
| -39 | $0.1+4$ | 0.142 | $0.1+1$ | 0.139 | 0.138 | 0.136 | 0.134 | 0.133 | 0.132 | 0.130 |
| -38 | 0.161 | 0.159 | 0.158 | 0.156 | 0.154 | $0.15{ }^{2}$ | 0.151 | 0. 149 | 0.147 | 0.146 |
| -37 | 0.180 | 0.178 | 0.1 76 | 0.174 | 0.172 | 0.171 | 0.169 | 0.167 | 0.165 | 0.163 |
| $-36$ | 0.201 | 0.199 | 0.197 | 0.195 | 0.193 | 0.191 | -. 189 | 0.186 | 0.184 | 0.182 |

Smithsonian Tables

Table 78.
PRESSURE OF AQUEOUS VAPOR OVER ICE.
DYNAMIC MEASURES

| Temp. | . 0 | . 1 | . 2 | .3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C. | mb. | mb . | mb . | mb . | mb . | mb . | mb . | mb. | mb. | mb . |
| $-35^{\circ}$ | 0.225 | 0.222 | 0.220 | 0.218 | 0.215 | 0.213 | 0.21 I | 0.208 | 0.206 | 0.204 |
| -34 | 0.251 | 0.248 | 0.245 | 0.243 | 0.240 | 0.237 | 0.235 | 0.232 | 0.230 | 0.227 |
| -33 | 0.279 | 0.276 | 0.273 | 0.270 | 0.267 | 0.265 | 0.262 | 0.259 | 0.256 | 0.253 |
| -32 | 0.311 | 0.307 | 0.304 | 0.301 | 0.298 | 0.295 | 0.291 | 0.288 | 0.285 | 0.282 |
| $-31$ | 0.345 | 0.342 | 0.338 | 0.335 | 0.33I | 0.328 | 0.324 | 0.32 I | 0.317 | 0.314 |
| $-30$ | 0.384 | 0.380 | 0.376 | 0.372 | 0.368 | 0.364 | 0.360 | 0.357 | 0.353 | 0.349 |
| -29 | 0.426 | 0.42 I | 0.417 | 0.413 | 0.408 | 0.404 | 0.400 | 0.396 | 0.392 | 0.388 |
| -28 | 0.472 | 0.467 | 0.462 | 0.458 | 0.453 | 0.448 | 0.444 | 0.439 | 0.435 | 0.430 |
| -27 | 0.523 | 0.518 | 0.512 | 0.507 | 0.502 | 0.497 | 0.492 | 0.487 | 0.482 | 0.477 |
| -26 | 0.579 | 0.573 | 0.567 | 0.561 | 0.556 | 0.550 | 0.545 | 0.539 | 0.534 | 0.528 |
| $-25$ | 0.640 | 0.634 | 0.627 | 0.621 | 0.615 | 0.609 | 0.602 | 0.596 | 0.590 | 0.585 |
| -24 | 0.707 | 0.700 | 0.693 | 0.686 | 0.679 | 0.673 | 0.666 | 0.659 | 0.653 | 0.646 |
| $-23$ | 0.780 | 0.773 | 0.765 | 0.758 | 0.750 | 0.743 | 0.736 | 0.728 | 0.72 I | 0.714 |
| -22 | 0.861 | 0.852 | 0.844 | 0.836 | 0.828 | 0.820 | 0.812 | 0.804 | 0.796 | 0.788 |
| $-21$ | 0.949 | 0.939 | 0.930 | 0.92 I | 0.912 | 0.904 | 0.895 | 0.886 | 0.878 | 0.869 |
| --20 | 1.04 | 1.03 | 1.02 | I. OI | 1.00 | 1.00 | 0.986 | 0.976 | 0.967 | 0.958 |
| -19 | 1.15 | I. 14 | I. 13 | 1.12 | I. II | 1.10 | 1.09 | 1.07 | 1.06 | 1.05 |
| -18 | I. 26 | 1.25 | 1.24 | 1.23 | I. 22 | 1.20 | I. 19 | 1.18 | 1.17 | 1.16 |
| $-17$ | I. 39 | 1.37 | I. 36 | I. 35 | I. 34 | I. 32 | 1. 31 | I. 30 | 1.29 | 1.27 |
| -16 | I. 52 | I. 51 | I. 49 | I. 48 | I. 47 | I. 45 | 1.44 | I. 43 | I. 41 | 1.40 |
| -15 | I. 67 | I. 65 | 1.64 | 1. 62 | 1.6I | 1. 59 | I. 58 | 1. 57 | 1.55 | I. 54 |
| -14 | 1.83 | I. 81 | I. 80 | I. 78 | 1.76 | 1.75 | 1.73 | I. 72 | 1.70 | 1.69 |
| -13 | 2.00 | 1.99 | 1.97 | 1.95 | 1.93 | 1.92 | 1.90 | 1.88 | I. 86 | 1.85 |
| -12 | 2.19 | 2.17 | 2.15 | 2.13 | 2.12 | 2.10 | 2.08 | 2.06 | 2.04 | 2.02 |
| -II | 2.40 | 2.38 | 2.35 | 2.33 | 2.31 | 2.29 | 2.27 | 2.25 | 2.23 | 2.21 |
| $-10$ | 2.62 | 2.60 | 2.57 | 2.55 | 2.53 | 2.51 | 2.48 | 2.46 | 2.44 | 2.42 |
| -9 -8 | 2.86 | 2.83 | 2.81 | 2.78 | 2.76 | 2.74 | 2.71 | 2.69 | 2.67 | 2.64 |
| -8 | 3.12 | 3.09 | 3.07 | 3.04 | 3.01 | 2.99 | 2.96 | 2.93 | 2.91 | 2.88 |
| -7 | 3.40 | 3.37 | 3.34 | $3 \cdot 3$ I | 3.29 | 3.26 | 3.23 | 3.20 | 3.17 | 3.15 |
| -6 | 3.70 | 3.67 | 3.64 | 3.6I | 3.58 | 3.55 | $3 \cdot 52$ | 3.49 | 3.46 | 3.43 |
| - 5 | 4.03 | 4.00 | 3.97 | 3.93 | 3.90 | 3.87 | 3.83 | 3.80 | 3.77 | 3.74 |
| - 4 | 4.39 | 4.35 | 4.31 | 4.28 | 4.24 | 4.21 | 4.17 | 4.14 | 4.10 | 4.07 |
| - 3 | 4.77 | 4.73 | 4.69 | 4.65 | 4.61 | 4.58 | 4.54 | 4.50 | 4.46 | 4.42 |
| - 2 | 5.18 | 5.14 | 5.10 | 5.06 | 5.OI | 4.97 | 4.93 | 4.89 | 4.85 | 4.81 |
| - I | 5.63 | $5 \cdot 58$ | $5 \cdot 53$ | 5.49 | 5.44 | 5.40 | $5 \cdot 36$ | 5.3I | 5.27 | 5.23 |
| -0 | 6.11 | 6.06 | 6.01 | 5.96 | 5.91 | 5.86 | 5.81 | 5.77 | $5 \cdot 72$ | 5.67 |

Smithsonian Tables

Table 79.
PRESSURE OF AQUEOUS VAPOR OVER WATER.
DYNAMIC MEASURES

| Temp. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| c. | mb . | mb . | mb . | mb . | mb . |  |  |  | mb . | mb . |
| $0^{\circ}$ | 6.11 | 6.15 | 6.20 | 6.24 | 6.29 | 6.33 | 6.38 | 6.42 | 6.47 | 6.52 |
| 1 | 6.56 | 6.61 | 6.66 | 6.71 | 6.76 | 6.81 | 6.86 | 6.90 | 6.95 | 7.00 |
| 2 | 7.05 | 7.10 | 7.16 | 7.21 | 7.26 | 7.31 | 7.36 | 7.42 | 7.47 | 7.52 |
| 3 | 7.58 | 7.63 | 7.68 | 7.74 | 7.79 | 7.85 | 7.90 | 7.96 | 8.02 | 8.07 |
| 4 | 8.13 | 8.19 | 8.25 | 8.30 | 8.36 | 8.42 | 8.48 | 8.54 | 8.60 | 8.66 |
| 5 | 8.72 | 8.78 | 8.84 | 8.91 | 8.97 | 9.03 | 9.09 | 9.16 | 9.22 | 9.28 |
| 6 | 9.35 | 9.41 | 9.48 | 9.54 | 9.61 | 9.68 | 9.74 | 9.81 | 9.88 | 9.95 |
| 7 | 10.02 | 10.09 | 10.16 | 10.22 | 10.30 | 10.37 | 10.44 | 10.51 | 10.58 | 10.65 |
| 8 | 10.73 | 10.80 | 10.87 | 10.95 | 11.02 | 11.10 | II 117 | 11.25 | 11.32 | 11.40 |
| 9 | 11.48 | 11.56 | 11.64 | 11.71 | 11.79 | 11.87 | I 1.95 | 12.03 | 12.12 | 12.20 |
| 10 | 12.28 | 12.36 | 12.44 | 12.53 | 12.61 | 12.70 | 12.78 | 12.87 | 12.95 | 13.04 |
| 11 | 13.13 | 13.21 | 13.30 | 13.39 | 13.48 | 13.57 | 13.66 | 13.75 | 13.84 | 13.93 |
| 12 | 14.03 | 14.12 | 14.21 | 14.31 | 14.40 | 14.50 | 14.59 | 14.69 | 14.78 | I 4.88 |
| 13 | 14.98 | 15.08 | 15.18 | 15.28 | 15.38 | 15.48 | I 5.58 | 15.68 | 15.78 | 15.89 |
| 14 | 15.99 | 16.09 | 16.20 | 16.30 | 16.41 | 16.51 | 16.62 | 16.73 | 16.84 | 16.95 |
| 15 | 17.06 | 17.17 | 17.28 | 17.39 | 17.50 | 17.61 | 17.73 | 17.84 | 17.96 | 18.07 |
| 16 | 18.19 | 18.30 | 18.42 | 18.54 | 18.66 | 18.78 | 18.90 | 19.02 | 19.14 | 19.26 |
| 17 | 19.38 | 19.51 | 19.63 | 19.76 | 19.88 | 20.01 | 20.13 | 20.26 | 20.39 | 20.52 |
| 18 | 20.65 | 20.78 | 20.91 | 2 I .04 | 21.17 | 21.31 | 21.44 | 21.58 | 21.71 | 21.85 |
| 19 | 21.98 | 22.12 | 22.26 | 22.40 | 22.54 | 22.68 | 22.82 | 22.96 | 23.11 | 23.25 |
| 20 | 23.40 | 23.54 | 23.69 | 23.83 | 23.98 | 24.13 | 24.28 | 24.43 | 2.4 .58 | 24.73 |
| 21 | 24.88 | 25.04 | 25.19 | 25.35 | 25.50 | 25.66 | 25.82 | 25.98 | 26.14 | 26.30 |
| 22 | 26.46 | 26.62 | 26.78 | 26.94 | 27.11 | 27.27 | 27.44 | 27.61 | 27.78 | 27.94 |
| 23 | 28.11 | 28.28 | 28.46 | 28.63 | 28.80 | 28.98 | 29.15 | 29.33 | 29.51 | 29.68 |
| 24 | 29.86 | 30.04 | 30.22 | 30.40 | 30.59 | 30.77 | 30.96 | 31.14 | 31.33 | 3 I .5 I |
| 25 | 31.70 | 31.89 | 32.08 | 32.28 | 32.47 | 32.66 | 32.86 | 33.05 | 33.25 | 33.45 |
| 26 | 33.64 | 33.84 | $3+.04$ | $3+.25$ | 34.45 | 34.65 | 34.86 | 35.06 | 35.27 | 35.48 |
| 27 | 35.69 | 35.90 | 36.11 | 36.32 | 36.53 | 36.75 | 36.96 | 37.18 | 37.40 | 37.62 |
| 28 | 37.84 | 38.06 | 38.28 | 38.50 | 38.73 | 38.95 | 39.18 | 39.41 | 39.64 | 39.87 |
| 29 | 40.10 | 40.33 | 40.56 | 40.80 | 41.04 | 41.27 | 41.51 | 41.75 | 41.99 | 42.23 |
| 30 | 42.48 | 42.72 | 42.97 | 43.21 | $43 \cdot 46$ | 43.71 | 43.96 | 44.21 | 44.47 | 44.72 |
| 31 | 44.98 | 45.23 | 45.49 | 45.75 | 46.01 | 46.27 | 46.54 | 46.80 | 47.07 | 47.33 |
| 32 | 47.60 | 47.87 | 48.14 | 48.42 | 48.69 | 48.97 | 49.24 | 49.52 | 49.80 | 50.08 |
| 33 | 50.36 | 50.65 | 50.93 | 51.22 | 51.50 | 51.79 | 52.08 | 52.37 | 52.67 | 52.96 |
| 34 | 53.26 | 53.56 | 53.85 | 54.15 | 54.46 | 54.76 | 55.06 | 55.37 | 55.68 | 55.99 |
| 35 | 56.30 | 56.61 | 56.92 | 57.24 | 57.56 | 57.87 | 58.19 | 58.51 | 58.84 | 59.16 |
| 36 | 59.49 | 59.81 | 60.14 | 60.47 | 60.81 | 61.14 | 61.47 | 61.81 | 62.15 | 62.49 |
| 37 | 62.83 | 63.17 | 63.52 | 63.86 | $6+.21$ | $6+56$ | 64.91 | 65.27 | 65.62 | 65.98 |
| 38 | 66.34 | 66.69 | 67.06 | $67 \cdot 4^{2}$ | 67.78 | 68.15 | 68.52 | 68.89 | 69.26 | 69.63 |
| 39 | 70.01 | 70.38 | 70.76 | 71.14 | 71.53 | 71.91 | 72.30 | 72.68 | 73.07 | $73 \cdot 4^{6}$ |
| 40 | 73.86 | 74.25 | 74.65 | 75.04 | $75 \cdot 44$ | 75.85 | 76.25 | 76.66 | 77.06 | 77.47 |
| 41 | 77.88 | 78.30 | 78.71 | 79.13 | 79.55 | 79.97 | 80.39 | 80.81 | 81.24 | 81.67 |
| 42 | 82.10 | 82.53 | 82.97 | 83.40 | 83.84 | 84.28 | 84.72 | 85.17 | 85.61 | 86.06 |
| 43 | 86.51 | 86.96 | 87.42 | 87.87 | 88.33 | 88.79 | 89.26 | 89.72 | 90.19 | 90.66 |
| 44 | 91.13 | 91.60 | 92.07 | 92.55 | 93.03 | 93.51 | 93.99 | $94 \cdot 48$ | 94.97 | 95.46 |

Smithsonian Tables

Table 80.
WEIGHT OF A CUBIC FOOT OF SATURATED VAPOR.
ENGLISH MEASURES.

| Temperature. |  | Temperature. | . 0 | . 5 | Temperaature. | . 0 | . 2 | . 4 | . 6 | . 8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Grains | F. | Grains | Grains | F. | Grains | Grains | Grains | Grains | Grains |
| $-30^{\circ}$ | 0.095 | $+20^{\circ}$ | 1.244 | 1.273 | $+70^{\circ}$ | 8.066 | 8.117 | 8.170 | 8.223 | 8.276 |
| 29 | 0.100 | 21 | 1.301 | 1.332 | 71 | 8.329 | 8.383 | 8.437 | 8.491 | 8.546 |
| 28 | 0.106 | 22 | 1. 362 | I. 393 | 72 | 8.600 | 8.656 | 8.711 | 8.766 | 8.823 |
| 27 | 0.112 | 23 | 1.425 | 1. 457 | 73 | 8.879 | 8.936 | 8.992 | 9.050 | 9.107 |
| 26 | 0.119 | 24 | 1.490 | 1.524 | 74 | 9.165 | 9.223 | 9.281 | 9.34 I | 9.400 |
| -25 | 0. 126 | $+25$ | I. 558 | 1.593 | $+75$ | 9.460 | 0.519 | 9.579 | 9.640 | 9.700 |
| 24 | 0.134 | 26 | 1.629 | 1.666 | 76 | 9.761 | 9.823 | 9.885 | 9.947 | 10.009 |
| 23 | $0.14{ }^{1}$ | 27 | 1.703 | 1.741 | 77 | 10.072 | 10.135 | 10.199 | 10.263 | 10.327 |
| 22 | 0.150 | 28 | 1.779 | 1.819 | 78 | 10.392 | 10.457 | 10.521 | 10.587 | 10.653 |
| 21 | 0.158 | 29 | 1. 859 | 1.900 | 79 | 10.720 | 10.785 | 10.853 | 10.92 I | 10.987 |
| -20 | 0.167 | $+30$ | 1.942 | 1.984 | $+80$ | 11.056 | II.124 | 11.193 | 11.262 | 11.331 |
| 19 | 0.176 | 31 | 2.028 | 2.072 | 81 | 11.401 | 11.471 | $11.54{ }^{2}$ | 11.613 | 11.685 |
| 18 | 0.187 | 32 | 2.118 | 2.159 | 82 | I 1.756 | 11. 828 | I 1.900 | 11.974 | 12.047 |
| 17 | 0.197 | 33 | 2.200 | 2.242 | 83 | I2.12 I | 12.195 | 12.269 | 12.344 | 12.419 |
| 16 | 0.208 | 34 | 2.286 | 2.330 | 84 | 12.494 | 12.570 | I 2.646 | 12.723 | 12.800 |
| -15 | 0.220 | +35 | 2.375 | 2.420 | $+85$ | 12.878 | 12.956 | 13.034 | 13.113 | $13.19{ }^{2}$ |
| 14 | 0.232 | 36 | 2.466 | 2.513 | 86 | 13.272 | 13.351 | 13.432 | 13.512 | 13.594 |
| 13 | 0.244 | 37 | 2.560 | 2.609 | 87 | 13.676 | 13.758 | 13.840 | 13.923 | 14.006 |
| 12 | 0.258 | 38 | 2.658 | 2.708 | 88 | 14.090 | 14.174 | 14.258 | 14.344 | 14.429 |
| I I | 0.272 | 39 | 2.759 | 2.810 | 89 | 14.515 | 14.601 | 14.689 | 14.776 | 14.864 |
| -10 | 0.286 | $+40$ | 2.863 | 2.916 | $+90$ | 14.951 | 15.040 | 15.129 | 15.219 | 15.309 |
| 9 | 0.302 | 41 | 2.970 | 3.026 | 91 | 15.400 | 15.490 | 15.581 | 15.673 | 15.766 |
| 8 | 0.318 | 42 | 3.082 | 3.138 | 92 | 15.858 | 15.95 I | 16.045 | 16.139 | 16.234 |
| 7 | 0.335 | 43 | 3.196 | 3.254 | 93 | 16.328 | 16.423 | 16.520 | 16.616 | 16.713 |
| 6 | 0.353 | 44 | 3.315 | 3.374 | 94 | 16.810 | 16.909 | 17.007 | 17.106 | 17.205 |
| - 5 | 0.37 I | $+45$ | 3.436 | 3.499 | $+95$ | 17.305 | 17.406 | 17.506 | 17.607 | 17.709 |
| 4 | 0.301 | 46 | 3.563 | 3.627 | 96 | 17.812 | 17.914 | 18.018 | 18.121 | 18.226 |
| 3 | 0.411 | 47 | 3.693 | 3.759 | 97 | 18.330 | 18.436 | 18.542 | 18.648 | 18.755 |
| , | 0.433 | 48 | 3.828 | 3.895 | 98 | 18.863 | 18.971 | 19.079 | 19.188 | 19.298 |
| I | 0.455 | 49 | 3.965 | 4.036 | 99 | 19.407 | 19.518 | 19.629 | 19.74 I | 19.853 |
| $\pm 0$ | 0.479 | +50 | 4.108 | 4.181 | $+100$ | 19.966 | 20.079 | 20.193 | 20.307 | 20.422 |
| + 1 | 0.503 | 51 | 4.255 | 4.331 | 101 | 20.538 | 20.654 | 20.770 | 20.887 | 21.005 |
| 2 | 0.529 | 52 | 4.407 | 4.485 | 102 | 21.123 | 21.242 | 21.362 | 21.481 | 21.602 |
| 3 | 0.556 | 53 | 4.564 | 4.644 | 103 | 21.723 | 21.845 | 21.967 | 22.090 | 22.213 |
| 4 | 0.584 | 54 | 4.725 | 4.807 | 104 | 22.337 | 22.462 | 22.588 | 22.714 | 22.839 |
| 5 | 0.613 | $+55$ | 4.891 | 4.976 | +105 | 22.966 | 23.095 | 23.223 | 23.35 I | 23.481 |
| 6 | 0.644 | 56 | 5.062 | 5.149 | 106 | 23.611 | 23.742 | 23.873 | 24.005 | 24.138 |
| 8 | 0.676 | 57 | 5.238 | $5 \cdot 328$ | 107 | 24.271 | 24.405 | 2.4.539 | 2.4 .673 | 24.809 |
| 8 | 0.709 | 58 | 5.420 | $5 \cdot 513$ | 108 | 24.946 | 25.082 | 25.220 | 25.358 | 25.497 |
| 9 | 0.744 | 59 | 5.607 | 5.703 | 109 | 25.636 | 25.776 | 25.917 | 26.058 | 26.201 |
| 10 | 0.780 | $+60$ | 5.800 | 5.899 | + 110 | 26.343 | 25.486 | 26.630 | 26.775 | 26.920 |
| 1 I | 0.818 | 61 | 5.999 | 6.099 | III | 27.066 | 27.213 | 27.360 | 27.508 | 27.657 |
| 12 | 0.858 | 62 | 6.203 | 6.306 | II 2 | 27.807 | 27.956 | 28.107 | 28.259 | 28.411 |
| 13 | 0.900 | 63 | 6.413 | 6.521 | 113 | 28.563 | 28.717 | 28.87 I | 29.026 | 29.181 |
| 14 | 0.943 | 64 | 6.630 | 6.740 | II 4 | 29.338 | 29.495 | 29.653 | 29.812 | 29.970 |
| 15 | 0.988 | $+65$ | 6.852 | 6.966 | $+115$ | 30.130 | 30.291 | 30.452 | 30.614 | 30.777 |
| 16 | 1.035 | 66 | 7.082 | 7.198 | 116 | 30.940 | 31.104 | 31.270 | 31.435 | 31.601 |
| 17 | 1.084 | 67 | 7.317 | 7.437 | 117 | 31.768 | 31.937 | 32.106 | 32.274 | 32.445 |
| 18 | 1.135 | 68 | 7.560 | 7.683 | 118 | 32.616 | 32.787 | 32.960 | 33.133 | 33.307 |
| $+10$ | 1.189 | +69 | 7.809 | 7.937 | +119 | 33.482 | 33.657 | 33.834 | 34.010 | 34.189 |

WEIGHT OF A CUBIC METER OF SATURATED VAPOR OVER ICE.
METRIC MEASURES


Table 81.
WEIGHT OF A CUBIC METER OF SATURATED VAPOR OVER WATER.
METRIC MEASURES

| Temp. | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C. | grams | grams | grams | grams | grams | grams | grams | grams | grams | grams |
| $+0^{\circ}$ | 4.847 | 4.88 I | 4.914 | $4 \cdot 948$ | 4.982 | 5.017 | 5.05 I | 5.086 | 5.121 | 5.157 |
|  | 5.192 | 5.228 | 5.264 | $5 \cdot 300$ | $5 \cdot 336$ | $5 \cdot 373$ | 5.410 | 5.447 | 5.483 | $5 \cdot 52 \mathrm{I}$ |
| 2 | $5 \cdot 559$ | $5 \cdot 596$ | 5.634 | 5.673 | 5.71 I | 5.750 | 5.789 | 5.828 | 5.868 | 5.908 |
| 3 | $5 \cdot 947$ | 5.988 | 6.028 | 6.068 | 6.110 | 6.151 | 6.192 | 6.234 | 6.275 | 6.318 |
| 4 | 6.360 | 6.402 | 6.445 | 6.488 | 6.532 | 6.575 | 6.619 | 6.664 | 6.708 | 6.753 |
| $+5$ | 6.797 | 6.842 | 6.888 | 6.934 | 6.979 | 7.025 | 7.072 | 7.119 | 7.166 | 7.213 |
|  | 7.261 | 7.309 | 7.357 | $7 \cdot 405$ | $7 \cdot 453$ | $7 \cdot 502$ | $7 \cdot 552$ | 7.601 | 7.651 | 7.701 |
| 7 | 7.751 | 7.802 | 7.853 | 7.904 | 7.956 | 8.007 | 8.059 | 8.112 | 8.164 | 8.217 |
| 8 | 8.27 I | 8.324 | 8.378 | 8.432 | 8.487 | 8.542 | 8.597 | 8.652 | 8.708 | 8.764 |
| 9 | 8.82 I | 8.877 | 8.934 | 8.99 I | 9.049 | 9.106 | 9.165 | 9.223 | 9.282 | $9 \cdot 341$ |
| $+10$ | 9.40 I | 9.46 I | $9 \cdot 52 \mathrm{I}$ | 9.582 | 9.643 | 9.704 | 9.765 | 9.827 | 9.889 | 9.952 |
| 11 | 10.015 | 10.078 | 10.142 | 10.205 | 10.270 | 10.334 | 10.400 | 10.465 | 10.530 | 10.597 |
| 12 | 10.664 | 10.730 | 10.797 | 10.865 | 10.932 | I 1.00I | I 1.069 | II. 138 | I 1.208 | I 1.278 |
| 13 | II. 348 | II.418 | I 1. 489 | 11.561 | 11.632 | 11.704 | 11.777 | 11.850 | 11.922 | I 1.997 |
| 14 | 12.070 | 12.144 | 12.219 | 12.295 | 12.370 | 12.446 | 12.523 | 12.600 | 12.677 | 12.754 |
| $+15$ | 12.832 | 12.911 | 12.990 | 13.068 | 13.148 | 13.229 | 13.309 | 13.390 | 13.472 | 13.553 |
| 16 | 13.635 | 13.718 | 13.801 | I 3.885 | 13.969 | 14.053 | 14.139 | 14.224 | 14.309 | 14.395 |
| 17 | 14.482 | 14.569 | 14.657 | 14.744 | 14.833 | 14.922 | 15.01 I | 15.101 | 15.19 I | I 5.282 |
| 18 | 15.373 | 15.465 | I 5.557 | 15.650 | 15.743 | 15.836 | 15.931 | 16.025 | 16.12I | 16.216 |
| 19 | 16.31 I | 16.409 | 16.505 | 16.603 | 16.701 | 16.799 | 16.898 | 16.998 | 17.097 | I 7.198 |
| $+20$ | 17.300 | 17.401 | 17.503 | 17.606 | 17.708 | 17.812 | 17.917 | 18.021 | 18.126 | 18.232 |
| 21 | 18.338 | 18.445 | 18.553 | 18.660 | 18.768 | I 8.878 | 18.987 | 19.097 | 19.207 | 19.319 |
| 22 | 19.430 | 19.542 | 19.655 | 19.769 | 19.882 | 19.996 | 20.112 | 20.227 | 20.343 | 20.461 |
| 23 | 20.578 | 20.695 | 20.814 | 20.933 | 21.053 | 21.173 | 21.295 | 21.416 | 21.538 | 21.660 |
| 24 | 21.783 | 21.907 | 22.032 | 22.157 | 22.282 | 22.409 | 22.536 | 22.663 | 22.791 | 22.920 |
| $+25$ | 23.049 | 23.179 | 23.310 | 23.442 | 23.573 | 23.706 | 23.839 | 23.973 | 24.107 | 24.242 |
| 26 | 24.378 | 24.514 | 24.651 | 24.790 | 24.929 | 25.066 | 25.206 | 25.346 | 25.488 | 25.629 |
| 27 | 25.771 | 25.915 | 26.058 | 26.203 | 26.348 | 26.494 | 26.641 | 26.787 | 26.936 | 27.084 |
| 28 | 27.234 | 27.384 | 27.534 | 27.686 | 27.837 | 27.990 | 28.143 | 28.298 | 28.453 | 28.609 |
| 29 | 28.765 | 28.923 | 29.08I | 29.239 | 29.399 | 29.559 | 29.720 | 29.881 | 30.044 | 30.207 |
| $+30$ | 30.37 I | 30.535 | 30.701 | 30.867 | 31.034 | 31.202 | 31.37 I | 31.540 | 31.710 | 31.880 |
| 31 | 32.052 | 32.225 | 32.398 | 32.572 | 32.747 | 32.923 | 33.100 | 33.277 | 33.454 | 33.633 |
| 32 | 33.812 | 33.993 | 34.175 | 34.356 | $3+540$ | 34.723 | 34.909 | 35.094 | 35.280 | 35.467 |
| 33 | 35.656 | 35.844 | 36.034 | 36.224 | 36.416 | 36.609 | 36.801 | 36.995 | 37.190 | 37.386 |
| 34 | 37.583 | 37.780 | 37.979 | 38.178 | 38.378 | 38.579 | 38.782 | 38.984 | 39.187 | 39.395 |
| $+35$ | 39.599 | 39.805 | 40.013 | 40.22 I | 40.430 | 40.640 | 40.851 | 41.064 | 41.277 | 41.491 |
| 36 | 41.706 | 41.921 | 42.139 | 42.356 | 42.575 | 42.795 | 43.015 | 43.237 | 43.459 | 43.683 |
| 37 | 43.908 | 44.134 | 44.360 | 44.587 | 44.815 | 45.046 | 45.277 | 45.507 | 45.740 | 45.973 |
| 38 | 46.208 | 46.443 | 46.680 | 46.918 | 47.156 | 47.396 | 47.636 | 47.878 | 48.121 | 48.365 |
| 39 | 48.609 | 48.855 | 49.103 | 49.350 | 49.600 | 49.850 | 50.101 | 50.353 | 50.606 | 50.861 |
| $+40$ | 5.117 7 | 51.373 | 51.63I | 51.890 | 52.150 | 52.410 | 52.673 | 52.936 | 53.200 | 53.466 |

[^29]
## HYGROMETRICAL TABLES.

Reduction of psychrometric observations - English measures.
Values of $e=e^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left(1+\frac{t^{\prime}-32}{1571}\right)$. Table 82
Relative humidity - Temperature Fahrenheit . . . Table 83
Reduction of psychrometric observations - Metric Measures.
Values of $e=e^{\prime}-0.000660 B\left(t-t^{\prime}\right)\left(\mathrm{I}+0.00115 t^{\prime}\right)$. Table 84
Relative humidity - Temperature Centigrade . . . . Table $8_{5}$
Rate of decrease of vapor pressure with altitude . . . . . Table 86
Reduction of snowfall measurements.
Depth of water corresponding to the weight of a cylindrical snow core 2.655 inches in diameter

Table 87
Depth of water corresponding to the weight of snow (or rain) collected in an 8 -inch gage .

Table 88
Quantity of rainfall corresponding to given depths . . . Table 89

Table 82.

## REDUCTION OF PSYCHROMETRIC OBSERVATIONS. <br> ENGLISH MEASURES.

Values of $e=e^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left(\mathrm{I}+\frac{t^{\prime}-32}{157 \mathrm{I}}\right)$
Pressure of Saturated Aqueous Vapor, $\varepsilon$.

| Temperature. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { F. } \\ -60^{\circ} \end{gathered}$ | Inches. .0010 | Inches. | Inches. | Inches. | Inches | Inches. | Inches. | Inches. | Inches. | Inches. |
| 50 | 20 | . 0018 | . 0017 | .0016 | . 0015 | .0014 | .0013 | .OOI 2 | .OOII | . 0011 |
| 40 | 38 | 36 | 33 | 31 | 29 | 28 | 26 | 24 | 23 | 21 |
| 30 | 71 | 66 | 62 | 59 | 55 | 52 | 49 | 46 | 43 | 40 |
| 20 | . 0127 | . 0120 | . 0113 | . 0107 | . 1010 | . 0095 | . 0090 | . 0084 | . 0080 | . 0075 |

$e=e^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left(\mathrm{I}+\frac{t^{\prime}-32}{157 \mathrm{I}}\right)$
$B=30.0$ inches

| $t^{\prime}$ | $1-t^{\prime}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | . 0 | . 2 | . 4 | . 6 | . 8 | 1.0 | 1.2 | 1.4 | 1.6 | 1.8 |
|  | Inches. | Inches. | Inches. | Inches. | Inches, | Inches, | Inches. | Inches. | Inches. | Inches. |
| $-20^{\circ}$ | . 0127 | . 0106 | . 0085 | . 0063 | .0042 | . 0021 |  |  |  |  |
| 19 | 135 | 113 | 92 | 71 | 49 | 28 | . 0007 |  |  |  |
| 18 | 143 | 12 I | . 0100 | 79 | 57 | 36 | . 0015 |  |  |  |
| 17 | 15 I | 130 | 108 | 87 | 66 | 44 | 23 | . 0002 |  |  |
| 10 | 160 | 138 | 117 | 96 | 74 | 53 | 32 | . 0010 |  |  |
| 15 | 169 | 148 | 126 | . 0105 | 84 | 62 | 41 | 19 |  |  |
| 14 | 179 | 157 | 136 | 115 | 93 | 72 | 50 | 20 | . 0008 |  |
| 13 | 189 | 168 | 146 | 125 | . 0103 | 82 | 61 | 39 | . 0018 |  |
| 12 | 200 | 178 | 157 | 136 | 114 | 93 | 7 I | 50 | 29 | . 0007 |
| II | 211 | 190 | 168 | 147 | 125 | . 0104 | 83 | 61 | 40 | .0018 |
| 10 | 223 | 202 | 180 | r 59 | 137 | 116 | 94 | 73 | 52 | 30 |
| 9 | 236 | 214 | 193 | 171 | 150 | 128 | . 0107 | 85 | 64 | 43 |
| 8 | 249 | 227 | 206 | 184 | 163 | 141 | 120 | 98 | 77 | 56 |
| 7 | 263 | 241 | 220 | 198 | 177 | I55 | 134 | . 0112 | 91 | 69 |
| 6 | 277 | 256 | 234 | 213 | 191 | 170 | 148 | 127 | . 0105 | 84 |
| 5 | 292 | 271 | 249 | 228 | 206 | 185 | 163 | 142 | 120 | . 0099 |
| 4 | 308 | 287 | 265 | 244 | 222 | 201 | 179 | 158 | 136 | . 0115 |
| 3 | 325 | 304 | 282 | 261 | 239 | 218 | 196 | 175 | ${ }^{1} 53$ | 132 |
| 2 | 343 | 321 | 300 | 278 | 257 | 235 | 214 | 192 | 171 | 149 |
| - I | 361 | 340 | 318 | 297 | 275 | 254 | 232 | 210 | 189 | 167 |
| $\pm 0$ | 381 | 350 | 338 | 316 | 294 | 273 | 251 | 230 | 208 | 187 |
| + 1 | 401 | 380 | 358 | 337 | 315 | 293 | 272 | 250 | 229 | 207 |
| 2 | 423 | 401 | 379 | 358 | 336 | 315 | 293 | 271 | 250 | 228 |
| 3 | 445 | 423 | 402 | 380 | 359 | 337 | 315 | 294 | 272 | 250 |
| 4 | 468 | 447 | 425 | 40.4 | 382 | 360 | 339 | 317 | 295 | 274 |
| 5 | 493 | 47 I | 450 | 428 | 407 | 385 | 363 | 342 | 320 | 298 |
| 6 | 519 | 497 | 476 | 454 | 432 | 411 | 389 | 367 | 346 | 324 |
| 7 | 546 | 524 | 503 | 481 | 459 | 438 | 416 | 394 | 373 | 351 |
| 8 | 574 | 552 | 531 | 509 | 487 | 466 | 444 | 422 | 401 | 379 |
| 9 | 604 | 582 | 560 | 539 | 517 | 495 | 474 | 452 | 430 | 408 |
| 10 | . 0635 | .0613 | . 0591 | . 0569 | .0548 | . 0526 | . 0504 | .0483 | . 0461 | . 0439 |
| $\left.\begin{array}{r} -20 \\ +10 \end{array}\right\}$ | $\Delta e \times \Delta B$ | +.000 I | +.0001 | +.0002 | +.0003 | +.0004 | +.0004 | +.0005 | +.0006 | +.0007 |

Smithsonian tables.

## REDUCTION OF PSYCHROMETRIC OBSERVATIONS.

 ENGLISH MEASURES.Values of $e=e^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left(\mathrm{I}+\frac{t^{\prime}-32}{157 \mathrm{I}}\right)$
$B=30.0$ inches


Table 82.
REDUCTION OF PSYCHROMETRIC OBSERVATIONS. ENGLISH MEASURES.
Values of $c=e^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left(\mathrm{I}+\frac{t^{\prime}}{15^{\prime} \mathrm{I}} 32\right)$
$B=30.0$ inches

| $i^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 1.0 | 2.0 | 3.0 | 4.0 | 5.0 | 6.0 | 7.0 | 8.0 | 9.0 |
| $\begin{aligned} & \text { F } \\ & 10^{\circ} \end{aligned}$ | $\begin{gathered} \text { Inches. } \\ \Delta e \times \Delta B \end{gathered}$ | $\begin{array}{r} \text { Inches. } \\ +.0004 \end{array}$ | $\begin{array}{r} \text { Inches. } \\ +.0007 \end{array}$ | $\begin{aligned} & \text { Inches. } \\ & +.00 \text { I } \end{aligned}$ | $\begin{array}{r} \text { Inches. } \\ +.0014 \end{array}$ | $\begin{array}{r} \text { Inches. } \\ +.0018 \end{array}$ | $\begin{aligned} & \text { Inches. } \\ & +.0022 \end{aligned}$ | $\begin{array}{r} \text { Inches. } \\ +.0025 \end{array}$ | $\begin{array}{r} \text { Inches. } \\ +.0029 \end{array}$ | $\begin{array}{r} \text { Inches. } \\ +.0033 \end{array}$ |
| $10^{\circ}$ | 0.063 | 0.053 | 0.042 | 0.031 | 0.020 | 0.009 |  |  |  |  |
| II | 67 | 56 | 45 | 34 | 23 | . 012 | 0.002 |  |  |  |
| 12 | 70 | 59 | 48 | .37 | 27 | 16 | 5 |  |  |  |
| 13 | 74 | 63 | 52 | 41 | 30 | 19 | 8 |  |  |  |
| 14 | 77 | 66 | 56 | 45 | 34 | 23 | . OI 2 | 0.001 |  |  |
| 15 | 8 I | 70 | 59 | 49 | 38 | 27 | 16 | 5 |  |  |
| 16 | 85 | 74 | 63 | 53 | 42 | 31 | 20 | 9 |  |  |
| 17 | 89 | 79 | 68 | 57 | 46 | 35 | 24 | .013 | 0.002 |  |
| 18 | 94 | 83 | 72 | 61 | 50 | 30 | 28 | 18 | 7 |  |
| 19 | . 099 | 88 | 77 | 66 | 55 | 4.4 | 33 | 22 | 11 | 0.000 |
| 20 | . 103 | 92 | 81 | 71 | 60 | 49 | 38 | 27 | 16 | . 005 |
| 2 I | . 108 | 97 | 86 | 76 | 65 | 54 | 43 | 32 | 21 | . 010 |
| 22 | .II4 | . 103 | 92 | 81 | 70 | 59 | 48 | 37 | 26 | 15 |
| 23 | .119 | . 108 | 97 | 86 | 75 | 64 | 53 | 42 | 32 | 21 |
| 24 | . 125 | . I 14 | .103 | 92 | 8 I | 70 | 59 | 48 | 37 | 26 |
| 25 | .131 | . 120 | . 109 | 98 | 87 | 76 | 65 | 54 | 43 | 32 |
| 26 | .137 | . 126 | . 115 | . 104 | 93 | 82 | 71 | 60 | 49 | 38 |
| 27 | .143 | . 133 | . 122 | . 111 | . 100 | 89 | 78 | 67 | 56 | 45 |
| 28 | . 150 | . 139 | . 128 | . 117 | . 106 | 95 | 84 | 73 | 62 | 51 |
| 29 | . 157 | .146 | . 135 | . 124 | . II3 | .102 | 91 | 80 | 69 | 58 |
| 30 | . 165 | . 154 | .143 | .132 | . 121 | . 110 | 99 | 88 | 77 | 66 |
| 31 | . 772 | .161 | . 150 | . 139 | . 128 | . 117 | . 106 | 95 | 84 | 73 |
| 32 | .180 | .169 | . 158 | . 147 | . 136 | . 125 | . 114 | . 103 | 92 | 81 |
| 33 | . 188 | .177 | . 166 | .155 | . 144 | . 133 | . 122 | . 111 | . 100 | 89 |
| 34 | .195 | . 184 | .173 | . 162 | . 151 | . 140 | . 129 | . 118 | . 107 | 96 |
| 35 | . 203 | . 192 | .18I | . 170 | . 159 | . 148 | . I37 | . 126 | .115 | . 104 |
| 36 | . 212 | . 201 | . 190 | . 179 | . 168 | . 157 | . 145 | .134 | . 123 | . 112 |
| 37 | . 220 | . 209 | .198 | . 187 | . 176 | .165 | . 154 | . 143 | . 132 | .121 |
| 38 | . 229 | . 218 | . 207 | . 196 | . 185 | . 174 | .163 | . 152 | .141 | .130 |
| 39 | . 238 | . 227 | . 216 | . 205 | . 194 | . 183 | . 172 | .161 | . 150 | . 139 |
| 40 | . 248 | . 237 | . 226 | . 215 | . 203 | . 192 | .181 | .170 | . 159 | .148 |
| 41 | . 258 | . 246 | . 235 | . 224 | . 213 | . 202 | . 191 | .180 | .169 | . 158 |
| 42 | . 268 | . 257 | . 246 | . 234 | . 223 | . 212 | . 201 | . 190 | . 179 | . 168 |
| 43 | . 278 | . 267 | . 256 | . 245 | .234 | .223 | . 212 | . 201 | . 190 | .178 |
| 44 | . 289 | . 278 | . 267 | . 256 | . 245 | . 234 | . 223 | . 211 | . 200 | .189 |
| 45 | . 300 | . 289 | . 278 | .267 | . 256 | . 245 | . 234 | . 223 | . 2 I 1 | . 200 |
| 46 | . 312 | -301 | . 290 | . 279 | . 268 | . 256 | . 245 | . 234 | .223 | . 212 |
| 47 | . 324 | . 313 | . 302 | . 291 | . 280 | . 268 | .257 | . 246 | . 235 | . 224 |
| 48 | . 336 | . 325 | . 314 | .303 | . 292 | . 281 | .270 | . 259 | .248 | .236 |
| 49 | .349 | . 338 | .327 | . 316 | . 305 | . 294 | .283 | .271 | . 260 | . 249 |
| 50 | .363 | .351 | . 340 | . 329 | . 318 | . 307 | . 296 | .285 | . 274 |  |
| 5 I | .376 | . 365 | . 354 | . 343 | . 332 | . 32 I | . 309 | . 298 | . 287 | . 276 |
| 52 | .390 | -379 | . 368 | . 357 | . 346 | . 335 | . 324 | . 312 | . 301 | . 290 |
| 53 | .405 | . 394 | .383 | . 372 | .361 | - 349 | . 338 | .327 | .316 | . 305 |
| 54 | .420 | . 409 | . 398 | $\cdot 387$ | . 376 | . 364 | -353 | . 342 | . 33 I | . 320 |
| 55 | .436 | . 425 | . 414 | . 402 | . 391 | . 380 | .369 | . 358 | -347 | -335 |
| 56 | . 452 | .441 | . 430 | . 419 | . 407 | . 396 | .385 | . 374 | . 363 | . 352 |
| 57 | . 469 | . 458 | . 446 | . 435 | . 424 | . 413 | . 402 | -390 | . 379 | . 368 |
| 58 | .486 | . 475 | . 464 | . 452 | . 441 | . 430 | . 419 | . 408 | -396 | . 385 |
| 59 | . 504 | . 493 | .48I | . 470 | . 459 | . 448 | . 437 | . 425 | . 414 | . 403 |
| 60 | 0.522 | 0.511 | 0.500 | 0.488 | 0.477 | 0.466 | 0.455 | 0.444 | 0.432 | 0.42 I |
| 60 | $\Delta c \times \Delta B$ | +.0004 | $+.0007$ | +.0011 | +.0015 | +.0019 | +.0022 | +.0026 | +.0030 | +.0034 |

table 82.
REDUCTION OF PSYCHROMETRIC OBSERVATIONS.
ENGLISH MEASURES.
Values of $e=e^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left(\mathrm{I}+\frac{t^{\prime}-32}{\mathrm{I}_{57} \mathrm{I}}\right)$
$B=30.00$

| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| F. $30^{\circ} \Delta e \times \Delta B$ | $\begin{aligned} & \text { Inches. } \\ & \text { +.00.3 } \end{aligned}$ | $\begin{aligned} & \text { Inches. } \\ & +.0040 \end{aligned}$ | $\begin{aligned} & \text { Inches. } \\ & +.0044 \end{aligned}$ | $\begin{aligned} & \text { Inches. } \\ & +.0048 \end{aligned}$ | $\begin{aligned} & \text { Inches. } \\ & +.005 \mathrm{I} \end{aligned}$ | $\begin{array}{\|l\|} \hline \text { Inches. } \\ +.0055 \end{array}$ | $\begin{aligned} & \text { Inches. } \\ & +. .0050 \end{aligned}$ | Inches. $+.0062$ | $\begin{aligned} & \text { Inches. } \\ & +.0066 \end{aligned}$ | $\begin{aligned} & \text { Inches. } \\ & +.0070 \end{aligned}$ |
| $22^{\circ}$ | 0.004 |  |  |  |  |  |  |  |  |  |
| 23 24 | .010 15 |  |  |  |  |  |  |  |  |  |
| 25 | 21 | 0.010 |  |  |  |  |  |  |  |  |
| 26 | 27 | 16 | 0.005 |  |  |  |  |  |  |  |
| 27 | 34 | 23 | . 112 | 0.001 |  |  |  |  |  |  |
| 28 29 | 40 | 29 36 | 18 25 | . $r_{4}^{7}$ | 0.003 |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| 30 | 55 | 44 | 3.3 | 22 | . 111 | 0.000 |  |  |  |  |
| 31 | 62 | 51 | 40 | 29 | 18 | . 007 |  |  |  |  |
| 32 | 70 | 59 | 48 | 37 | 26 | . 015 | 0.004 |  |  |  |
| 33 34 | 78 85 | 67 74 | 55 63 | 44 52 | 33 41 | 22 30 | 11 | 0.000 .008 |  |  |
| 34 |  |  | 63 | 52 |  |  |  | . 008 |  |  |
| 35 | 93 | 82 | 71 | 60 | 49 | 38 | 27 | . 016 | 0.005 |  |
| 36 | . 101 | 90 | 79 | 68 | 57 | 46 | 35 | 24 | . 013 | 0.002 |
| 37 | . 110 | 99 | 88 | 77 | 66 | 55 | 43 | 32 | 2 I |  |
| 38 | . 119 | . 108 | 06 | 85 | 74 | 63 | 52 | 41 | 30 | 19 28 |
| 39 | . 128 | . 117 | . 105 | 94 | 83 | 72 | 61 | 50 | 39 |  |
| 40 | . 137 | . 126 | .II5 | . 104 | 93 | 82 | 71 | 60 | 49 | 37 |
| 41 | . 147 | . 136 | . 125 | . 114 | . 103 | 91 | 80 | 69 | 58 | 47 |
| 42 | . 157 | . 146 | . 135 | .124 | .113 | . 101 | 90 | 79 | 68 | 57 |
| 43 | . 167 | .156 | . 145 | .134 | . 123 | . 112 | . 101 | 90 | 79 89 | 68 -8 |
| 44 | .178 | .167 | .156 | .145 | . 134 | . 123 | . 112 | . 100 | 89 | 78 |
| 45 | . 189 | . 178 | . 167 | . 156 | . 145 | . 134 | . 123 | . 112 | . 100 | 89 |
| 46 | . 201 | . 190 | . 179 | . 168 | . 156 | . 145 | . 134 | . 123 | . 112 | .101 |
| 47 | . 213 | . 202 | . 191 | . 180 | . 168 | . 157 | . 46 | . 135 | . 124 | .113 |
| 48 | .225 | . 214 | . 203 | . 192 | . 181 | .170 +182 | .159 .171 | .147 .160 | .136 .149 | .125 .138 |
| 49 | . 238 | . 227 | . 216 | . 205 | . 193 | . 182 | . 171 | . 160 | . 149 |  |
| 50 | . 251 | . 240 | . 229 | . 218 | . 207 | . 196 | .184 | . 173 | .162 | .151 |
| 51 | . 265 | . 254 | . 243 | . 231 | . 220 | . 209 | . 198 | . 187 | .176 | . 165 |
| 52 | . 279 | . 268 | . 257 | . 246 | . 234 | . 223 | . 212 | . 201 | . 100 | .179 |
| 53 | . 294 | . 282 | . 271 | . 260 | . 249 | .238 | . 227 | . 216 | . 204 | . 193 |
| 54 | . 309 | . 297 | . 286 | . 275 | . 264 | . 253 | .242 | .231 | . 219 | . 208 |
| 55 | . 324 | -313 | . 302 | .291 | . 280 | . 268 | . 257 | . 246 | . 235 | . 224 |
| 56 | - 340 | -329 | . 318 | . 307 | . 296 | . 285 | . 273 | . 262 | . 251 | . 2.40 |
| 57 | - 357 | . 346 | . 334 | . 323 | -312 | . 301 | . 290 | .279 .206 | . 267 | . 256 |
| 58 59 | .374 .392 | .363 .381 | .352 .369 | .340 .358 | .329 .347 | .318 .336 | .307 .325 | .296 .313 | .284 .302 | .273 .291 |
| 59 | -392 |  |  |  |  |  |  |  |  |  |
| 60 | 0.410 | 0.399 | 0.388 | 0.376 | 0.365 | 0.354 | 0.343 | 0.331 | 0.320 | 0.309 |
| $60 \Delta e \times \Delta B$ | +.0037 | +.0041 | +.0045 | +. 0049 | +.0052 | +.0056 | +.0060 | +.0064 | +.0067 | +.0071 |

## ENGLISH MEASURES.

Values of $e=e^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left(1+\frac{t^{\prime}-32}{157 \mathrm{I}}\right)$
$B=30.00$

| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 |
| F. | inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| $40^{\circ} \Delta \mathrm{e} \times \Delta B$ | +.0074 | +.0077 | +.008 I | +. 0085 | +.0089 | +.0092 | +.0096 | +.0100 | $+.0103$ | +.0107 |
| $38^{\circ}$ | 0.008 |  |  |  |  |  |  |  |  |  |
| 39 | . 017 | 0.006 |  |  |  |  |  |  |  |  |
| 40 | 26 | . 015 | 0.004 |  |  |  |  |  |  |  |
| 41 | 36 | 25 | . 014 | 0.003 |  |  |  |  |  |  |
| 42 | 46 | 35 | 24 | . 013 | 0.002 |  |  |  |  |  |
| 43 | 56 | 45 | 34 | 23 | . 012 | 0.001 |  |  |  |  |
| 44 | 67 | 56 | 45 | 34 | 23 | . 012 | 0.001 |  |  |  |
| 45 | 78 | 67 | 56 | 45 | 34 | 23 | . Ol 2 | 0.001 |  |  |
| 46 | 90 | 79 | 68 | 57 | 45 | 34 | 23 | . 012 | 0.001 |  |
| 47 | .102 | 91 | 79 | 68 | 57 | 46 | 35 | 24 | 13 | 0.002 |
| 48 | . 114 | . 103 | 92 | SI | 70 | 58 | 47 | 36 | 25 | . 014 |
| 49 | . 127 | . 110 | . 104 | 93 | 82 | 71 | 60 | 49 | 38 | 27 |
| 50 | . 140 | . 129 | . 118 | . 106 | 95 | $8_{4}$ | 73 | 62 | 51 | 40 |
| 51 | . 153 | . 142 | .131 | . 120 | .109 | 08 | 87 | 75 | 64 | 53 |
| 52 | . 167 | . 156 | . 145 | . 134 | . 123 | . 112 | . I O | 89 | 78 | 67 |
| 53 | . 182 | . 77 | . 160 | . 149 | . 137 | . 126 | . 115 | . 104 | 93 | 82 |
| 54 | . 197 | . 186 | . 775 | . 164 | . 152 | . 141 | . 130 | . 119 | . 108 | 97 |
| 55 | . 212 | . 201 | . 190 | . 179 | . 168 | . 157 | .145 | . 134 | . 123 | . 112 |
| 56 | . 229 | . 218 | . 206 | . 195 | . 184 | . 173 | . 162 | . 150 | . 139 | . 128 |
| 57 | . 245 | . 234 | . 223 | . 211 | . 200 | . 189 | . 178 | . 167 | . 156 | . 144 |
| 58 | . 262 | . 251 | . 240 | . 228 | . 217 | . 206 | . 195 | . 184 | . 173 | .161 |
| 59 | . 280 | . 269 | . 257 | . 246 | . 235 | . 224 | . 213 | . 201 | . 190 | . 179 |
| 60 | 0.298 | 0.287 | 0.275 | 0.264 | 0.253 | 0.242 | 0.231 | 0.219 | 0.208 | 0.197 |
| $60 \Delta e \times \Delta B$ | +.0075 | +.0078 | +.0082 | +.0086 | +.0090 | $+.0093$ | $+.0097$ | +.O101 | +.0105 | +.0108 |
| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |
|  | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 |
|  | Inches. |  | Inches. | Incties. | Inches. | Inches. |  | Inches. | Inches. | Inches. |
| $50^{\circ} \Delta e \times \Delta B$ | +.0111 | $+.0115$ | $+.0119$ | $+.0122$ | $+.0126$ | $+.0130$ | $+.0134$ | $+.0137$ | +.0141 | +.0145 |
| $48^{\circ}$ | 0.003 |  |  |  |  |  |  |  |  |  |
| 49 | . 015 | . 004 |  |  |  |  |  |  |  |  |
| 50 | 29 | . 017 | 0.006 |  |  |  |  |  |  |  |
| 51 | 42 | 31 | . 020 | 0.009 |  |  |  |  |  |  |
| 52 | 56 | 45 | 34 | . 023 | 0.011 | 0.000 |  |  |  |  |
| 53 | 70 | 59 | 48 | 37 | 26 | . 015 | 0.004 |  |  |  |
| 54 | 85 | 74 | 63 | 52 | 41 | 30 | . 018 | 0.007 |  |  |
| 55 | .IOI | 90 | 78 | 67 | 56 | 45 | 34 | . 023 | 0.011 | 0.000 |
| 56 | .117 | . 106 | 95 | 83 | 72 | 61 | 50 | 39 | 28 | . 016 |
| 57 | . 133 | . 122 | . 111 | . 100 | 88 | 77 | 66 | 55 | 44 | 32 |
| 58 | . 150 | . 139 | . 128 | .117 | . 105 | 94 | 83 | 72 | 6 I | 49 |
| 59 | . 168 | . 157 | . 145 | . 134 | .123 | . 112 | . IOI | 89 | 78 | 67 |
| 60 | 0.186 | 0.175 | 0.163 | 0.152 | 0.141 | 0.130 | 0.119 | 0.107 | 0.096 | 0.085 |
| $60 \Delta c \times \Delta B$ | +.01 12 | +.0116 | +.0120 | +.O1 23 | +.0127 | +.0131 | +.0134 | +.0138 | +.0142 | +.0146 |
| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |
|  | 40 | 41 | 42 | 43 | 44 | 45 | 46 |  |  |  |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |  |  |  |
| $56^{\circ}$ | 0.005 |  |  |  |  |  |  |  |  |  |
| 57 58 | . 021 | 0.010 |  |  |  |  |  |  |  |  |
|  |  |  |  | 0.005 .022 |  |  |  |  |  |  |
| 59 60 |  |  |  |  | 0.011 0.029 | 0.000 0.018 |  |  |  |  |
| $60 \Delta c \times \Delta B$ | +.0149 | +.0153 | +.0157 | +.0161 | +.0164 | +.0168 | +.0172 |  |  |  |

Values of $e=e^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left(\mathrm{I}+\frac{t^{\prime}-32}{157 \mathrm{I}}\right)$
$B=30.00$

| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 1.0 | 2.0 | 3.0 | 4.0 | 5.0 | 6.0 | 7.0 | 8.0 | 9.0 | 10.0 |
| F. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| $60^{\circ}$ | $\Delta e \times \Delta B$ | +.0004 | +.0007 | +.001 1 | +.0015 | +.0019 | +. 0022 | +.0026 | +.0030 | +.0034 | +.0037 |
| $60^{\circ}$ | 0.522 | 0.511 | 0.500 | 0.488 | 0.477 | 0.466 | 0.455 | 0.444 | 0.432 | 0.42 I | 0.410 |
| 61 | . 541 | . 530 | . 518 | . 507 | . 496 | . 485 | . 474 | . .462 | . +51 | . 440 | . 429 |
| 62 | . 560 | . 549 | . 538 | . 527 | .516 | . 504 | . 493 | . 482 | . 471 | - 459 | . 448 |
| 63 | - 580 | 569 | . 558 | . 547 | . 536 | . 524 | . 513 | . 502 | . 491 | . 479 | . 468 |
| 64 | . 601 | . 590 | . 579 | . 568 | . 556 | . 545 | . 534 | . 523 | . 511 | . 500 | . 489 |
| 65 | . 623 | .6I I | . 600 | . 589 | . 578 | . 566 | . 555 | . 544 | . 533 | . 521 | . 510 |
| 66 | . 645 | . 633 | . 622 | . 611 | . 600 | . 588 | . 577 | . 566 | . 555 | . 543 | . 532 |
| 67 | . 667 | . 656 | . 645 | . 634 | . 622 | . 611 | . 600 | . 589 | . 577 | . 566 | . 555 |
| 68 | . 691 | . 680 | . 668 | . 657 | . 646 | . 635 | . 623 | . 612 | . 601 | . 590 | . 578 |
| 69 | . 715 | .704 | . 692 | . 68 I | . 670 | . 659 | . 647 | . 636 | . 625 | . 614 | . 602 |
| 70 | . 740 | . 729 | . 717 | . 706 | . 695 | . 684 | . 672 | . 66 I | . 650 | . 638 | . 627 |
| 71 | . 766 | .754 | -743 | . 732 | . 720 | . 709 | . 698 | . 687 | . 675 | . 664 | . 653 |
| 72 | .792 | .781 | .769 | . 758 | . 747 | . 735 | . 724 | . 713 | . 702 | . 690 | . 679 |
| 73 | . 819 | . 808 | . 797 | . 785 | . 774 | . 763 | . 751 | . 740 | . 729 | . 717 | . 706 |
| 74 | . 847 | . 836 | . 824 | . 813 | . 802 | .791 | . 779 | .768 | .757 | . 745 | . 734 |
| 75 | . 876 | . 865 | . 853 | . 842 | . 831 | . 819 | . $\mathrm{So8}$ | .797 | . 7 Sb | . 774 | . 763 |
| 76 | . 906 | . 894 | . 883 | . 872 | . 860 | . 849 | . 838 | . 826 | . $\mathrm{II}_{5}$ | . 804 | . 792 |
| 77 | . 936 | . 925 | . 914 | . 902 | . 891 | . 880 | . 868 | . 857 | . 846 | . 834 | . 823 |
| 78 | .968 | . 956 | . 945 | . 934 | . 922 | .91 1 | . 900 | . 888 | . 877 | . 866 | . 854 |
| 79 | 1.000 | . 989 | . 977 | . 966 | . 955 | . 943 | . 932 | . 921 | . 909 | . 898 | . 887 |
| 80 | 1.033 | 1.022 | I.OII | . 999 | . 988 | . 977 | . 965 | .954 | . $9+3$ | .93I | . 920 |
| 81 | . 068 | . 056 | . 045 | 1.034 | 1.022 | 1.OII | . 999 | . 988 | . 977 | . 965 | . 954 |
| 82 | . 103 | . 092 | . 080 | . 069 | . 057 | . 046 | 1.035 | 1.023 | 1.012 | 1.001 | . 989 |
| 83 | . 139 | . 128 | . 116 | . 105 | . 094 | . 082 | . 071 | . 060 | . 048 | . 037 | 1.026 |
| 84 | . 176 | . 165 | . 154 | . $1+2$ | . 31 | . 120 | . 108 | . 097 | . 086 | . 074 | . 063 |
| 85 | 1.215 | I. 204 | 1.192 | 1.181 | 1.J69 | 1.158 | 1.147 | 1.135 | 1.124 | I.II 2 | 1.101 |
| 86 | . 254 | .243 | . 232 | . 220 | . 209 | . 197 | . 186 | . 175 | .163 | . 152 | . 140 |
| 87 | . 295 | . $2 \mathrm{~S}_{4}$ | . 272 | . 261 | . 249 | . 238 | . 227 | . 215 | . 204 | . 192 | . 181 |
| 88 | . 336 | . 325 | . 314 | . 302 | . 291 | . 279 | . 268 | . 257 | .245 | . 234 | . 222 |
| 89 | . 379 | . 368 | . 357 | -345 | . 334 | . 322 | . 311 | . 300 | . 288 | . 277 | . 265 |
| 90 | 1.423 | 1.412 | I. 401 | 1.389 | 1.378 | I. 366 | 1.355 | I. 343 | 1.332 | 1.321 | 1.309 |
| 91 | . 469 | . 457 | . 446 | 435 | . 423 | . 412 | . 400 | . 389 | . 377 | . 366 | . 355 |
| 92 | -515 | . 504 | . 492 | . 481 | . 470 | . 458 | . 447 | . 435 | - +24 | . +12 | . 401 |
| 93 | .563 | . 552 | - 540 | . 529 | . 517 | . 506 | . 494 | . 483 | -471 | . 460 | . 449 |
| 94 | . 612 | . 601 | .589 | . 578 | . 566 | . 555 | - 543 | . 532 | . 52 I | . 509 | . 498 |
| 95 | 1. 662 | 1.651 | 1.640 | 1.628 | 1. 617 | 1.605 | 1. 594 | 1. 582 | I. 57 I | I. 559 | I. 548 |
| 96 | . 714 | . 703 | . 691 | .680 | . 668 | . 657 | . 646 | . 634 | . 623 | . 611 | . 600 |
| 97 | . 767 | . 756 | . 744 | . 733 | . 722 | . 710 | . 699 | . 687 | .776 | . 064 | . 653 |
| 98 | . 822 | . 811 | . 799 | . 788 | . 776 | . 765 | . 753 | .742 | . 730 | . 719 | . 707 |
| 99 | . 878 | . 867 | . 855 | . 844 | .832 | . 82 I | . 809 | . 798 | .786 | . 775 | . 763 |
| 100 | 1.936 | 1.924 | 1.913 | 1.901 | 1.890 | 1.878 | 1.867 | 1.855 | 1.844 | 1.832 | 1.82 I |
| 101 | . 994 | . 983 | . 972 | . 960 | . 949 | . 937 | . 926 | . 914 | . 903 | . 891 | . 880 |
| 102 | 2.055 | 2.043 | 2.032 | 2.020 | 2.009 | . 997 | . 986 | . 974 | . 963 | .95I | . 940 |
| 103 | .117 | . 106 | . 094 | . 083 | . 071 | 2.060 | 2.048 | 2.037 | 2.025 | 2.014 | 2.002 |
| 104 | . 181 | .169 | . 158 | . 46 | . 135 | .123 | .112 | . 100 | . 089 | . 077 | . 066 |
| 105 | 2.240 | 2.235 | 2.223 | 2.212 | 2.200 | 2.189 | 2.177 | 2.166 | 2.154 | 2.143 | 2. 13 I |
| 106 | . 314 | . 302 | . 290 | . 279 | . 267 | . 256 | . 244 | . 233 | . 221 | . 210 | . 198 |
| 107 | .382 | .371 | . 359 | -348 | . 336 | . 325 | -313 | . 302 | . 290 | . 278 | . 267 |
| 108 | . 453 | 441 | . 430 | .418 | . 407 | -395 | -384 | . 372 | . 361 | -340 | . 337 |
| 109 | . 525 | . 514 | .502 | 491 | 479 | .467 | - 456 | -44 | $\cdot 433$ | . 421 | . 410 |
| 110 | 2.599 | 2.588 | 2.576 | 2.565 | 2.553 | 2.542 | 2.530 | 2.519 | 2.507 | 2.495 | 2.484 |
| 110 | $\Delta c \times \Delta B$ | +.0004 | +.0008 | +.0012 | +.015 | +.0019 | +.0023 | +.0027 | +.003 1 | +.0035 | +.0039 |

Table 82.
REDUCTION OF PSYCHROMETRIC OBSERVATIONS. ENGLISH MEASURES.

$$
\begin{gathered}
\text { Values of } e=e^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left(\mathrm{I}+\frac{t^{\prime}-32}{\mathrm{I}_{57 \mathrm{I}}}\right) \\
B=30.00
\end{gathered}
$$

| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| F. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| $60^{\circ}$ | $\Delta e \times \Delta B$ | +.004 I | +.0045 | +.0049 | $+.0052$ | +.0056 | +.0060 | $+.0063$ | $+.0067$ | +.0071 | +.0075 |
| $60^{\circ}$ | 0.522 | 0.399 | 0.388 | 0.376 | 0.305 | 0.354 | 0.343 | 0.331 | 0.320 | 0.309 | 0.298 |
| 61 | . 54 I | 0.418 | . 406 | . 395 | . 384 | . 373 | . 361 | . 350 | . 339 | . 328 | . 317 |
| 62 | . 560 | . 437 | . 426 | . 415 | . 403 | . $39^{2}$ | . 381 | . 370 | -358 | . 347 | . 336 |
| 63 | . 580 | . 457 | . 446 | . 435 | . 423 | . 412 | . 401 | . 390 | . 378 | . 367 | . 356 |
| 64 | . 601 | . 478 | . 466 | . 455 | . 444 | . 433 | . 422 | . 410 | -399 | . 388 | . 377 |
| 65 | . 623 | . 499 | . 488 | . 476 | . 465 | . 454 | . 443 | . 43 I | . 420 | . 409 | - 398 |
| 66 | . 645 | . 52 I | . 510 | . 498 | . 487 | . 476 | . 465 | . 453 | . 442 | . 431 | . 420 |
| 67 | .667 | . 544 | . 532 | . 52 I | . 510 | . 499 | . 487 | . 476 | . 465 | . 454 | . 442 |
| 68 | . 691 | . 567 | . 556 | . 544 | . 533 | . 522 | . 511 | . 499 | . 488 | . 477 | . 466 |
| 69 | . 715 | . 591 | . 580 | . 568 | . 557 | . 546 | . 535 | .523 | . 512 | . 501 | . 490 |
| 70 | . 740 | . 616 | . 605 | - 593 | . 582 | . 57 I | -559 | . 548 | . 537 | . 526 | .514 |
| 71 | .766 | . 641 | . 630 | . 619 | . 608 | . 596 | . 585 | . 574 | . 562 | . 551 | . 540 |
| 72 | .792 | . 668 | .656 | . 645 | . 634 | . 623 | .61 1 | . 600 | .589 | . 577 | . 566 |
| 73 | . 819 | . 695 | . 684 | . 672 | . 661 | . 650 | . 638 | . 627 | . 616 | . 604 | . 593 |
| 74 | . 847 | . 723 | . 711 | . 700 | . 689 | . 678 | . 666 | . 655 | . 644 | .632 | . 62 I |
| 75 | . 876 | . 752 | . 740 | . 729 | . 718 | . 706 | . 695 | . 684 | . 672 | . 661 | . 650 |
| 76 | . 906 | . 781 | . 770 | .758 | . 747 | . 736 | . 725 | . 713 | . 702 | . 69 I | . 679 |
| 77 | . 936 | . 812 | . 800 | . 789 | . 778 | . 766 | . 755 | . 744 | . 732 | . 721 | . 710 |
| 78 | . 968 | . 843 | . 832 | . 820 | . 809 | . 798 | . 786 | . 775 | .764 | . 752 | . 741 |
| 79 | 1.000 | . 875 | . 864 | . 853 | . 841 | . 830 | . 819 | . 807 | . 796 | .785 | . 773 |
| 80 | 1.033 | . 909 | . 897 | . 886 | . 875 | . 863 | . 852 | . 841 I | . 829 | . 818 | . 806 |
| 81 | . 068 | . 943 | . 931 | . 920 | . 909 | . 897 | . 886 | . 875 | . 863 | . 852 | . 841 |
| 82 | . 103 | . 978 | . 967 | . 955 | . 944 | . 932 | . 921 | . 910 | . 898 | . 887 | . 876 |
| 83 | . 139 | 1.014 | 1.003 | .991 | . 980 | .969 | . 957 | . 946 | . 935 | . 923 | .912 |
| 84 | . 176 | . 051 | . 0.40 | 1.029 | 1.017 | 1.006 | . 995 | .983 | . 972 | . 960 | . 949 |
| 85 | 1.215 | 1.090 | 1.078 | 1.067 | 1.056 | I. 044 | I. 033 | 1.021 | 1.010 | . 999 | . 987 |
| 86 | . 254 | . 129 | . 118 | . 106 | . 095 | . 083 | . 072 | .061 | . 049 | 1.038 | 1.027 |
| 87 | . 295 | . 170 | . 158 | . 147 | . 135 | . 124 | . 113 | . 101 | . 090 | . 078 | . 067 |
| 88 | . 336 | . 211 | . 200 | . 188 | . 177 | . 165 | . 154 | . 143 | . 13 I | . 120 | . 108 |
| 89 | . 379 | . 254 | . 242 | . 231 | . 220 | . 208 | . 197 | . 185 | . 174 | . 163 | . 151 |
| 90 | 1.423 | 1. 298 | 1.286 | 1.275 | 1. 264 | 1.252 | 1.241 | 1.229 | 1.218 | 1.206 | 1.195 |
| 91 | . 469 | . 343 | . 332 | . 320 | . 309 | . 297 | . 286 | . 275 | . 263 | . 252 | . 240 |
| 92 | . 515 | . 390 | . 378 | . 367 | . 355 | . 344 | . 332 | . 32 I | . 310 | . 298 | . 287 |
| 93 | .563 | . 437 | . 426 | . 414 | . 403 | . 391 | -380 | -369 | -357 | -346 | -334 |
| 94 | .6ı 2 | . 486 | . 475 | . 463 | -452 | . 440 | . 429 | . 418 | . 406 | -395 | . 383 |
| 95 | 1.662 | I. 537 | 1.525 | 1.514 | 1.502 | 1.491 | 1.479 | 1.468 | 1.456 | I. 445 | 1.433 |
| 96 | . 714 | . 588 | . 577 | . 565 | - 554 | -542 | . 53 I | . 520 | . 508 | . 497 | . 485 |
| 97 | . 767 | . 641 | . 630 | . 618 | . 607 | . 595 | . 584 | . 572 | . 561 | . 550 | . 538 |
| 98 | . 822 | . 696 | . 684 | . 673 | . 661 | . 650 | . 638 | . 627 | . 615 | . 604 | . 593 |
| 90 | . 878 | . 752 | . 740 | . 729 | .717 | . 706 | . 694 | . 683 | . 67 I | . 660 | . 648 |
| 100 | 1.936 | 1.809 | 1.798 | 1.786 | 1.775 | 1.763 | 1.752 | 1.740 | 1. 729 | 1.717 | 1.706 |
| 101 | . 99.4 | . 868 | . 857 | . 845 | . 834 | . 822 | .8II | . 799 | . 788 | . 776 | .765 |
| 102 | 2.055 | . 928 | . 917 | . 905 | . 894 | . 882 | .871 | . 859 | . 848 | . 836 | . 825 |
| 103 | . 117 | .991 | . 979 | . 968 | . 956 | . 944 | . 933 | .921 | . 910 | . 898 | . 887 |
| 104 | . 18 I | 2.054 | 2.043 | 2.031 | 2.020 | 2.008 | . 997 | . 985 | . 974 | . 962 | .95I |
| 105 | 2.246 | 2.120 | 2.108 | 2.097 | 2.085 | 2.073 | 2.062 | 2.050 | 2.039 | 2.027 | 2.016 |
| 106 | . 314 | . 187 | . 775 | . 164 | . 152 | . 141 | . 129 | . 118 | . 106 | . 094 | . 083 |
| 107 | . 382 | . 255 | . 244 | . 232 | . 221 | . 209 | . 198 | . 186 | . 175 | .163 | . 152 |
| 108 | . 453 | - 326 | . 314 | . 302 | . 291 | .280 | . 268 | . 257 | . 245 | . 234 | . 222 |
| 109 | . 525 | -398 | -387 | . 375 | .364 | . 352 | . 340 | . 329 | .317 | . 306 | . 294 |
| 110 | 2.599 | 2.472 | 2.461 | 2.449 | 2.438 | 2.426 | 2.414 | 2.403 | 2.391 | 2.380 | 2.368 |
| 110 | $\Delta{ }_{P} \times \Delta B$ | +.0042 | +.0046 | +.0050 | +.0054 | +.0058 | +.0062 | +.0065 | +.0069 | +.0073 | +.0077 |

## ENGLISH MEASURES.

Values of $e=e^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left(\mathrm{I}+\frac{t^{\prime}-32}{1571}\right)$
$B=30.00$

$$
B=30.00
$$

|  | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 |
| F. | Inches. | Inches. | Inches. | Inches. | !nches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| $60^{\circ}$ | $\Delta e \times \Delta B$ | +.0078 | +.co82 | +.0086 | +.009 C | +. 0093 | +.0097 | +. | +.0105 | +. 0108 | +.OI 12 |
| $60^{\circ}$ | 0.522 | 0.287 | 0.275 | 0. 264 | 0.253 | 0.242 | 0.231 | 0.219 | 0.208 | -.197 | 0.186 |
| 61 | . 54 I | 0.305 | . 294 | . 283 | . 272 | . 261 | . 249 | . 238 | . 227 | . 216 | . 205 |
| 62 | . 560 | . 325 | . 314 | - 302 | . 291 | . 280 | . 269 | . 257 | . 246 | . 235 | . 224 |
| 63 | . 580 | . 345 | . 334 | . 322 | . 311 | . 300 | . 289 | . 277 | . 266 | . 255 | . 244 |
| 64 | . 601 | . 365 | . 354 | - 343 | . 332 | . 320 | . 309 | . 298 | . 287 | .276 | . 264 |
| 65 | . 623 | . 387 | -375 | . 364 | -353 | -342 | -330 | -319 | . 308 | . 297 | . 285 |
| 66 | . 645 | -408 | - 397 | -386 | - 375 | . 363 | . 352 | . 341 | . 330 | . 319 | . 307 |
| 67 | . 667 | . 431 | . 420 | . 409 | -397 | -386 | - 375 | . 364 | . 352 | . 341 | . 330 |
| 68 | . 691 | . 454 | . 443 | . 432 | . 421 | . 409 | -398 | . 387 | . 376 | . 364 | . 353 |
| 69 | . 715 | . 478 | . 467 | . 456 | . 445 | . 433 | . 422 | . 4 I | - 399 | . 388 | . 377 |
| 70 | . 740 | . 503 | . 492 | . 48 I | . 469 | . 458 | . 447 | . 435 | . 424 | . 413 | . 402 |
| 71 | . 766 | . 529 | . 517 | . 506 | . 495 | .483 | . 472 | . 461 | . 450 | . 438 | . 427 |
| 72 | . 792 | . 555 | . 544 | . 532 | . 521 | . 510 | . 498 | .487 | . 476 | . 464 | . 453 |
| 73 | . 819 | .582 | . 571 | - 559 | -548 | . 537 | . 525 | . 514 | . 503 | .491 | . 480 |
| 74 | . 847 | . 610 | . 598 | .587 | . 576 | . 564 | . 553 | . 542 | 531 | . 519 | . 508 |
| 75 | . 876 | . 638 | . 627 | . 616 | . 605 | . 593 | $.5^{82}$ | . 571 | -559 | . 548 | . 537 |
| 76 | . 906 | . 668 | . 657 | . 645 | . 634 | . 623 | .61 | . 600 | . 589 | . 577 | . 566 |
| 77 | . 936 | . 698 | . 687 | . 676 | . 664 | . 653 | . 642 | . 630 | . 619 | . 608 | . 596 |
| 78 | . 968 | . 730 | . 718 | . 707 | . 696 | . 684 | . 673 | . 662 | . 650 | . 639 | . 628 |
| 79 | 1.000 | .762 | .751 | . 739 | . 728 | . 717 | . 705 | . 694 | . 683 | . 671 | . 660 |
| 80 | 1.033 | . 795 | .784 | . 772 | .761 | . 750 | . 738 | . 727 | . 716 | . 704 | . 693 |
| 81 | . 068 | . 829 | . 818 | . 806 | . 795 | . 784 | . 772 | . 761 | . 750 | . 738 | . 727 |
| 82 | . 103 | . 864 | . 853 | . 842 | . 830 | . 819 | . 808 | . 796 | . 785 | . 773 | . 762 |
| 83 | . 39 | . 900 | . 889 | . 878 | . 866 | . 855 | . 844 | . 832 | .821 | . 810 | . 798 |
| 84 | . 176 | . 938 | . 926 | . 915 | . 904 | . 892 | . 881 | . 869 | . 858 | . 847 | . 835 |
| 85 | I. 215 | . 976 | . 965 | . 953 | . 942 | . 930 | . 919 | . 908 | . 896 | . 885 | . 873 |
| 86 | . 254 | I. 015 | I. 004 | . 992 | . 98 I | . 970 | . 958 | . 947 | . 935 | . 92.4 | . 913 |
| 87 | . 295 | . 056 | . 044 | 1.033 | 1.021 | 1.010 | . 999 | .987 | . 976 | . 964 | . 953 |
| 88 | . 336 | . 097 | . 086 | . 074 | . 063 | . 051 | 1.040 | 1.029 | 1.017 | 1. 006 | . 994 |
| 89 | . 379 | . 140 | . 128 | . 117 | . 106 | . 094 | . 083 | . 071 | . 060 | . 649 | 1.037 |
| 90 | 1.423 | I. 184 | 1.172 | I. 161 | 1.149 | I.I38 | 1.127 | I.II 5 | I. 104 | 1.092 | 1.081 |
| 91 | . 469 | . 229 | . 217 | . 206 | . 195 | . 183 | . 172 | . 160 | . 149 | . 138 | . 126 |
| 92 | . 515 | . 275 | . 264 | . 252 | . 241 | . 230 | . 218 | . 207 | . 195 | . 184 | . 172 |
| 93 | . 563 | . 323 | . 311 | . 300 | . 288 | . 277 | . 266 | . 254 | . 243 | . 231 | . 220 |
| 94 | . 612 | . 372 | . 360 | - 349 | . 337 | . 326 | . 315 | . 303 | .292 | . 280 | . 269 |
| 95 | 1.662 | 1.422 | 1.41 I | 1.399 | I. 388 | 1. 376 | 1.365 | I. 353 | 1.342 | 1.330 | I.319 |
| 96 | . 714 | 474 | . 462 | -451 | . 439 | . 428 | . 416 | . 405 | . 393 | . 382 | . 371 |
| 97 | . 767 | . 527 | . 515 | . 504 | . 492 | . 481 | . 469 | . 458 | -446 | . 435 | . 423 |
| 98 | . 822 | . 581 | . 570 | . 558 | . 547 | . 535 | . 524 | . 512 | . 501 | . 489 | . 478 |
| 99 | . 878 | . 637 | . 625 | . 614 | . 602 | . 591 | . 580 | . 568 | . 557 | . 54.5 | . 534 |
| 100 | 1.936 | 1. 694 | 1.683 | 1.671 | 1.660 | 1. 648 | 1.637 | 1.625 | 1.614 | 1.602 | 1.591 |
| 101 | . 994 | . 753 | . 742 | . 730 | . 719 | . 707 | . 696 | . 684 | . 673 | . 661 | . 650 |
| 102 | 2.055 | . 813 | . 802 | . 790 | . 779 | .767 | . 756 | . 744 | . 733 | . 721 | . 710 |
| 103 | . 117 | . 875 | . 864 | . 852 | .84I | . 829 | . 818 | . 806 | . 795 | . 783 | . 772 |
| 104 | .181 | . 939 | . 928 | .916 | . 905 | . 893 | . 882 | . 870 | . 858 | . 847 | . 835 |
| 105 | 2.246 | 2.004 | I. 993 | 1.981 | 1.970 | 1.958 | 1.947 | 1.935 | I. 924 | I.912 | 1.901 |
| 106 | . 314 | . 071 | 2.060 | 2.048 | 2.037 | 2.025 | 2.OI 4 | 2.002 | . 991 | . 979 | . 968 |
| 107 108 | .382 .453 | . 140 | . 129 | -117 | . 105 | . 094 | . 082 | . 071 | 2.059 | 2.048 | 2.036 |
| 108 | . 453 | . 211 | . 199 | . 187 | . 776 | . 164 | . 153 | . 141 | . 130 | . 118 | . 107 |
| 109 | - 525 | . 283 | . 271 | . 260 | . 248 | . 236 | . 225 | . 213 | . 202 | . 190 | . 179 |
| 110 | 2.599 | 2.357 | 2.345 | 2.334 | 2.322 | 2.310 | 2.299 | 2.287 | 2.276 | 2.264 | 2.253 |
| 110 | $\Delta c \times \Delta B$ | +.co8I | +.0085 | +.co89 | +.0092 | +.0006 | +. 0100 | +.0104 | +.0108 | +.0112 | +.0116 |

Table 82.
REDUCTION OF PSYCHROMETRIC OBSERVATIONS. ENGLISH MEASURES.
Values of $e=e^{\prime}-0.000367 B\left(t-t^{\prime}\right)\left(\mathrm{I}+\frac{t^{\prime}-32}{157 \mathrm{I}}\right)$
$B=30.00$

| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 |
| F. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| $60^{\circ}$ | $\Delta e \times \Delta B$ | +.01 16 | +.01 20 | +.CI 2.3 | +.012\% | +.0131 | +.0134 | +.0138 | +.0142 | +.0146 | +.0149 |
| $60^{\circ}$ | 0.522 | 0.175 | 0.163 | O. 152 | 0.141 | -. 130 | 0.119 | 0.107 | 0.096 | 0.085 | 0.074 |
| 61 | .54I | . 193 | . 182 | . 17 I | .16c | . 148 | . 137 | . 126 | . 115 | . 104 | . 092 |
| 62 | . 560 | . 213 | . 201 | . 190 | . 779 | . 168 | . 156 | . 145 | . 134 | . 123 | . 112 |
| 63 | . 580 | . 232 | . 221 | . 210 | . 199 | . 188 | .176 | . 165 | . 154 | . 143 | . 311 |
| 64 | .601 | . 253 | . 242 | . 231 | . 219 | . 208 | . 197 | . 186 | . 174 | . 163 | . 152 |
| 65 | . 623 | . 274 | . 263 | . 252 | . 240 | . 229 | . 218 | . 207 | . 195 | . 18.4 | . 173 |
| 66 | . 645 | . 296 | . 285 | . 274 | . 262 | . 251 | . 240 | . 229 | . 217 | . 206 | . 195 |
| 67 | . 667 | . 318 | . 307 | . 296 | . 285 | . 273 | . 262 | .251 | . 240 | . 228 | . 217 |
| 68 | .691 | . 342 | . 330 | . 319 | . 308 | . 297 | . 285 | . 274 | .263 | .252 | . 240 |
| 69 | . 715 | . 366 | . 354 | - 343 | . 332 | . 32 I | . 309 | . 298 | .287 | . 275 | . 264 |
| 70 | -740 | . 390 | -379 | . 368 | -357 | -345 | . 334 | -323 | .311 | -300 | . 289 |
| 71 | . 766 | . 416 | . 404 | . 393 | . 382 | . 371 | . 359 | . 348 | . 337 | . 325 | . 314 |
| 72 | . 792 | . 442 | . 431 | .419 | . 408 | . 397 | .385 | . 374 | . 363 | . 352 | -340 |
| 73 | . 819 | . 469 | . 458 | . 446 | . 435 | . 424 | . 412 | . 401 | . 390 | . 379 | . 367 |
| 74 | . 847 | . 496 | . 485 | . 474 | . 463 | .45I | . 440 | . 429 | . 418 | . 406 | . 395 |
| 75 | . 876 | . 525 | . 514 | . 503 | . 491 | .480 | . 469 | . 457 | . 446 | . 435 | . 424 |
| 76 | . 906 | . 555 | . 543 | . 532 | . 521 | . 509 | . 498 | . 487 | . 476 | . 464 | . 453 |
| 77 | . 936 | . 585 | . 574 | . 562 | .551 | -540 | . 529 | . 517 | . 506 | . 495 | . 483 |
| 78 | . 968 | . 616 | . 605 | . 594 | . 582 | . 571 | . 56 c | -548 | -537 | . 526 | . 514 |
| 79 | 1.000 | . 649 | . 637 | . 626 | . 615 | . 603 | . 592 | .581 | . 569 | - 558 | - 547 |
| 80 | 1.0.33 | . 682 | . 670 | . 659 | . 648 | . 636 | . 625 | . 614 | . 602 | . 591 | . 580 |
| 81 | . 068 | . 716 | . 704 | . 693 | . 682 | . 678 | . 659 | . 648 | . 636 | . 625 | . 613 |
| 82 | . 103 | . 751 | . 739 | . 728 | . 717 | .705 | . 694 | .683 | . 67 I | 660 | . 648 |
| 83 | . 139 | . 787 | . 775 | . 764 | . 753 | .741 | . 730 | . 719 | . 707 | . 696 | . 685 |
| 84 | . 176 | . 824 | . 813 | . 801 | . 790 | .778 | . 767 | . 756 | . 744 | . 733 | . 722 |
| 85 | I. 215 | . 862 | . 851 | . 839 | . 828 | . 817 | . 805 | . 794 | .782 | . 771 | . 760 |
| 86 | . 254 | .901 | . 890 | . 878 | . 867 | . 856 | . 844 | . 833 | . 822 | . 810 | . 799 |
| 87 | . 295 | . 942 | . 930 | .919 | . 907 | . 896 | .885 | . 873 | . 862 | . 850 | . 839 |
| 88 | . 336 | .983 | . 972 | . 960 | . 949 | . 937 | . 926 | .915 | .903 | . 892 | . 880 |
| 89 | . 379 | 1.026 | 1.014 | 1.003 | .991 | .980 | .969 | . 957 | . 946 | . 934 | . 923 |
| 90 | 1.423 | 1.069 | 1.058 | 1.047 | 1.035 | 1.024 | 1.012 | 1.001 | . 990 | . 978 | 967 |
| 91 | . 469 | . 115 | .103 | . 092 | .08c | . 069 | . 058 | . 046 | 1.035 | 1.023 | 1.012 |
| 92 | . 515 | . 161 | . 150 | . 138 | . 127 | . 115 | . 104 | . 092 | .081 | . 070 | . 058 |
| 93 | . 563 | . 208 | . 197 | . 186 | . 174 | .163 | . 51 | . 140 | . 128 | . 117 | . 105 |
| 94 | . 612 | . 257 | . 2.46 | . 234 | . 223 | . 212 | . 200 | . 189 | .177 | .166 | . 154 |
| 95 | 1.662 | 1.308 | 1. 296 | 1. 285 | 1. 273 | 1. 262 | 1. 250 | 1. 239 | 1.227 | 1.216 | 1. 204 |
| 96 | . 714 | . 359 | . 348 | . 3.36 | . 325 | . 313 | . 302 | . 290 | . 279 | : 267 | . 256 |
| 97 | . 767 | . 412 | . 401 | -389 | . 378 | -366 | . 355 | . 343 | .332 | . 320 | - 309 |
| 98 | . 822 | . 466 | . 455 | . 443 | . 432 | . 420 | . 409 | - 398 | - 386 | . 375 | . 363 |
| 99 | . 878 | . 522 | . 511 | . 499 | . 488 | .476 | . 465 | . 453 | . 442 | . 430 | . 419 |
| 100 | I. 936 | 1.579 | 1. 568 | 1. 556 | 1.545 | 1.533 | 1. 522 | 1. 510 | 1. 499 | 1. 488 | 1. 476 |
| 101 | . 994 | . 638 | . 627 | . 615 | . 604 | . 592 | . 581 | .509 | . 558 | . 546 | . 535 |
| 102 | 2.055 | . 698 | . 687 | . 675 | . 664 | . 652 | . 64 I | . 629 | . 618 | . 606 | . 595 |
| 103 | . 117 | . 760 | . 749 | . 737 | . 726 | . 714 | .703 | . 691 | . 680 | . 668 | . 657 |
| 10.4 | . 181 | . 824 | . 812 | . Sor | .789 | . 778 | .766 | . 755 | . 743 | . 732 | . 720 |
| 105 | 2.246 | 1.889 | 1. 878 | 1.866 | 1. $8_{55}$ | 1.843 | I. $8_{32}$ | 1.820 | 1.808 | 1. 797 | 1. 785 |
| 106 | . 314 | . 956 | . 945 | . 933 | . 922 | . 910 | . So 8 | . 887 | . 875 | . 864 | . 852 |
| 107 | . 382 | 2.025 | 2.613 | 2.002 | . 990 | . 979 | .907 | . 955 | . 944 | . 932 | . 921 |
| 108 | . 453 | . 005 | . 084 | . 072 | 2.060 | 2.049 | 2.037 | 2.026 | 2.014 | 2.003 | . 991 |
| 100 | 2.525 | 2.167 | 2.156 | 2.144 | 2.133 | 2.121 | 2.1C0 | 2.098 | 2.086 | 2.075 | 2.063 |
| 110 | $\Delta_{c} \times \Delta B$ | +.0119 | +.0123 | +.012 | +.C13I | +.c135 | -.0130 | +.014.3 | +.0146 | +.0150 | +. 0154 |

## REDUCTION OF PSYCHROMETRIC OBSERVATIONS. ENGLISH MEASURES.

| Values of $e=e^{\prime}-0.000367 B$$B=30.00$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |  |
|  | 0.0 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 |
| F. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches | nches. | Inches. | Inches. | Inches. | Inches. |
| $60^{\circ}$ | $\Delta e \times \Delta B$ | +.0153 | +.c1 57 | +.0161 | +.0164 | +.0168 | +. 0172 | +.0176 | +. 0179 | +.0183 | +.0187 |
| $60^{\circ}$ | 0.522 | 0.063 | 0.051 | 0.040 | 0.629 | 0.018 | 0.007 |  |  |  |  |
| 61 | . 54 I | .08I | .070 | . 059 | . 048 | . 036 | . 025 | 0.014 | 0.003 |  |  |
| 62 | . 560 | . 100 | .089 | . 078 | . 067 | . 055 | . 044 | . 033 | . 022 | 0.011 |  |
| 63 | . 580 | . 120 | . 100 | .c98 | . 087 | . 075 | . 064 | . 053 | . 042 | . 030 | 0.019 |
| 64 | . 601 | .14 I | . 29 | . 118 | . 107 | . 096 | . 085 | . 073 | .c62 | . 051 | . 040 |
| 65 | . 623 | . 162 | . 150 | . 139 | . 128 | . 117 | .105 | .c94 | .083 | . 072 | . 061 |
| 66 | . 645 | . 184 | . 172 | . 161 | . 150 | . 139 | . 127 | . 116 | . 105 | . 094 | . 082 |
| 67 | . 667 | . 206 | . 195 | .183 | . 172 | . 161 | . 150 | . 138 | . 127 | . 116 | . 105 |
| 68 | . 69 I | . 229 | . 218 | . 207 | . 195 | . 184 | . 173 | .162 | . 150 | . 139 | . 128 |
| 69 | . 715 | . 253 | . 242 | . 230 | $\therefore 219$ | . 208 | . 197 | . 185 | . 174 | .163 | . 152 |
| 70 | . 740 | .278 | . 266 | . 255 | . 244 | .232 | . 221 | . 210 | . 199 | .187 | . 176 |
| 71 | . 766 | . 303 | . 292 | . 280 | . 269 | . 258 | . 246 | . 235 | . 224 | . 213 | . 201 |
| 72 | . 792 | . 329 | -318 | . 306 | . 295 | . 284 | . 273 | . 261 | . 250 | . 239 | . 227 |
| 73 | . 819 | . 356 | -345 | . 333 | -322 | . 311 | . 299 | . 288 | . 277 | . 266 | . 254 |
| 74 | . 847 | . 384 | .372 | . 361 | . 350 | .338 | .327 | .316 | .304 | . 293 | 282 |
| 75 | . 876 | . 412 | . 401 | . 390 | . 378 | . 367 | .356 | -344 | - 333 | . 322 | . 310 |
| 76 | .9c6 | . 442 | . 430 | . 419 | . 408 | - 396 | -385 | . 374 | . 362 | . 35 I | . 340 |
| 77 | . 936 | . 472 | . 461 | . 449 | .438 | . 427 | . 415 | . 404 | - 393 | -381 | . 370 |
| 78 | . 968 | . 503 | . 492 | . 480 | . 469 | . 458 | . 446 | . 435 | . 424 | .412 | . 401 |
| 79 | 1.000 | . 535 | . 524 | . 513 | . 501 | . 490 | . 478 | . 467 | . 456 | - 444 | . 433 |
| 80 | 1.033 | . 568 | . 557 | . 546 | . 534 | . 523 | . 511 | . 500 | . 489 | 477 | . 466 |
| 81 | . 068 | . 602 | . 591 | . 579 | . 568 | . 557 | . 545 | . 534 | . 523 | . 511 | . 500 |
| 82 | . 103 | . 637 | . 626 | . 614 | . 603 | . 592 | . 580 | . 569 | . 558 | . 546 | . 535 |
| 83 | . 139 | . 673 | . 662 | . 650 | . 639 | . 628 | . 616 | . 605 | . 594 | .582 | . 571 |
| 84 | .176 | . 710 | . 699 | . 687 | . 676 | . 665 | . 653 | .642 | . 63 I | . 619 | . 608 |
| 85 | 1.215 | .748 | . 737 | . 725 | . 714 | . 703 | . 69 I | . 680 | . 669 | . 657 | .646 |
| 86 | . 254 | .787 | . 776 | .765 | . 753 | . 742 | . 730 | . 719 | . 708 | . 696 | . 685 |
| 87 | . 295 | . 828 | . 816 | . 805 | . 793 | .782 | . 771 | . 759 | . 748 | . 737 | . 725 |
| 88 | . 336 | . 869 | . 858 | . 846 | . 835 | . 823 | . 812 | . 801 | . 789 | . 778 | . 766 |
| 89 | . 379 | .912 | . 900 | . 889 | . 877 | . 866 | . 855 | . 843 | .832 | . 820 | . 809 |
| 90 | 1.423 | . 955 | . 944 | . 932 | . 921 | .910 | . 898 | .887 | . 875 | . 864 | . 853 |
| 91 | . 469 | 1.000 | . 989 | . 978 | . 966 | . 955 | . 94.3 | . 932 | . 920 | . 909 | . 898 |
| 92 | . 515 | . 047 | 1.035 | 1.024 | 1.012 | 1.001 | . 989 | . 978 | . 967 | . 955 | . 944 |
| 93 | . 563 | . 094 | . 083 | . 071 | . 660 | . 048 | 1.037 | 1.025 | 1.014 | 1.003 | .991 |
| 94 | . 612 | . 143 | . 131 | . 120 | . 109 | .c97 | . 086 | . 074 | .c63 | . 051 | I.C40 |
| 95 | 1.662 | 1.193 | 1.182 | 1.170 | 1.159 | 1.147 | 1.136 | I. 124 | 1.113 | I.ICI | 1.090 |
| 96 | . 714 | . 244 | . 233 | . 222 | . 210 | . 199 | . 187 | . 176 | .164 | . 153 | . 141 |
| 97 | .767 | . 297 | . 286 | . 274 | . 263 | . 251 | . 240 | . 229 | . 217 | . 206 | . 194 |
| 98 | . 822 | . 352 | . 340 | . 329 | . 317 | . 306 | . 294 | . 283 | . 271 | . 260 | . 248 |
| 99 | 1.878 | 1.407 | 1.396 | 1.384 | 1.373 | 1.361 | 1.350 | 1.338 | 1.327 | 1.316 | I. 304 |
| 100 | $\Delta e \times \Delta B$ | +. 0157 | +.0161 | +.0165 | +.0168 | +.0172 | +.0176 | +0.180 | $+.0184$ | +.0188 | +.0191 |

Smithsonian Tables.

## Table 82.

REDUCTION OF PSYCHROMETRIC OBSERVATIONS. ENGLISH MEASURES.

$$
\begin{gathered}
\text { Values of } c=e^{\prime}-0.000367 B\left(l-t^{\prime}\right)\left(\mathrm{I}+\frac{t^{\prime}-32}{\mathrm{I}_{57} \mathrm{I}}\right) \\
B=30.00
\end{gathered}
$$

| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 |
| F. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| $62^{\circ}$ | 0.560 |  |  |  |  |  |  |  |  |  |  |
| 63 | . 580 | 0.008 |  |  |  |  |  |  |  |  |  |
| 64 | . 601 | 0.028 | 0.017 | 0.006 |  |  |  |  |  |  |  |
| 65 | . 623 | . 049 | . 038 | . 027 | 0.016 | 0.004 |  |  |  |  |  |
| 66 | . 645 | . 071 | . 060 | . 849 | . 037 | . 026 | 0.015 | 0.004 |  |  |  |
| 67 | . 667 | . 093 | . 082 | . 071 | . 060 | . 048 | . 037 | . 026 | c.015 | 0.003 |  |
| 68 | . 691 | .116 | . 105 | . 094 | . 083 | . 071 | . 060 | . 049 | . 038 | . 026 | 0.015 |
| 69 | . 715 | . 140 | . 129 | . 118 | . 106 | . 095 | . 084 | . 073 | . 061 | . 050 | . 039 |
| 70 | . 740 | . 165 | - 154 | . 142 | .131 | . 120 | . 108 | . 097 | . 086 | . 075 | . 063 |
| 71 | .766 | . 190 | . 179 | . 167 | .156 | . 145 | . 134 | . 122 | . 111 | . 100 | . 089 |
| 72 | . 792 | . 216 | . 205 | . 194 | . 182 | .171 | . 160 | . 148 | . 137 | . 126 | .114 |
| 73 | . 819 | . 243 | .232 | . 220 | . 209 | . 198 | . 186 | . 175 | .164 | . 153 | .141 |
| 74 | . 847 | . 271 | . 259 | . 248 | .237 | . 225 | .214 | . 203 | .191 | . 180 | . 169 |
| 75 | . 876 | . 299 | . 288 | .276 | . 265 | . 254 | . 243 | . 231 | . 220 |  | . 197 |
| 76 | . 9 c6 | . 328 | . 317 | . 306 | . 294 | . 283 | . 272 | . 260 | . 249 | . 238 | . 226 |
| 77 | . 936 | . 359 | -347 | -336 | . 325 | . 313 | . 302 | . 291 | . 279 | . 268 | . 257 |
| 78 | . 968 | . 390 | . 378 | - 367 | - 356 | - 344 | - 333 | . 322 | -310 | . 209 | . 288 |
| 79 | 1.000 | . 422 | 410 | - 399 | . 388 | . 376 | . 365 | - 354 | -342 | . 331 | . 320 |
| 80 | 1.03.3 | . 455 | . 443 | . 432 | . 421 | . 409 | - 398 | . 387 | . 375 | . 364 | . 353 |
| 81 | . 068 | . 489 | . 477 | . 466 | . 455 | . 443 | . 432 | . 420 | . 409 | . 398 | . 386 |
| 82 | .103 | . 524 | . 512 | . 501 | . 489 | - 478 | . 467 | . 455 | . 44 | . 433 | . 42 I |
| 83 | . 139 | . 559 | . 548 | . 537 | . 525 | . 514 | . 503 | . 491 | . 480 | . 469 | -457 |
| 84 | .176 | . 596 | . 585 | . 574 | . 562 | . 551 | . 540 | . 528 | . 517 | . 505 | . 494 |
| 85 | 1.215 | . 634 | . 623 | . 612 | . 600 | . 589 | . 578 | . 566 | -555 | -543 | . 532 |
| 86 | . 254 | . 673 | . 662 | . 651 | . 639 | . 628 | . 617 | . 605 | . 594 | . 582 | . 571 |
| 87 | . 295 | . 714 | . 702 | . 691 | .680 | . 668 | . 657 | . 645 | . 634 | . 623 | . 611 |
| 88 89 | . 336 r .370 | . 755 | . 744 | . 732 | . 721 | . 709 | . 698 | . 687 | . 675 | . 664 | . 652 |
|  | 1.379 | 0.798 | 0.780 | 0.775 | 0.763 | 0.752 | 0.740 | 0.729 | 0.718 | 0.706 | 0.695 |
| 90 | $\Delta e \times \Delta B$ | +. 19194 | +. 0198 | +.0202 | +.0205 | +.0209 | +.0213 | +.021年 | +.0221 | +.0225 | +.c228 |

EMITHSONIAN TABLES.

RELATIVE HUMIDITY.
TEMPERATURES FAHRENHEIT.

| $\begin{aligned} & \text { Air } \\ & \text { Temper- } \\ & \text { ature. } \end{aligned}$ | relative humidity, or percentage of saturation. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| F. | Vapor pressure (inches). |  |  |  |  |  |  |  |  |  |
| $-30^{\circ}$ | 0.0007 | 0.0014 | 0.0021 | 0.0028 | 0.0035 | 0.0042 | 0.0049 | 0.0056 | 0.0063 | 0.0071 |
| 29 | . 0007 | . 0015 | . 0022 | .0030 | . 0037 | . 0045 | .0052 | . 0060 | . 0067 | . 0075 |
| 28 | . 0008 | .0016 | . 0024 | . 0032 | . 0040 | . 0048 | . 0056 | . 0064 | . 0072 | . 0080 |
| 27 | . 0008 | . 0017 | . 0025 | . 0034 | . 0042 | . 0051 | . 0059 | . 0068 | .0076 | . 0084 |
| 26 | . 0009 | . 0018 | . 0027 | . 0036 | . 0045 | . 0054 | .c063 | . 0072 | . $00 \mathrm{~S}_{\text {I }}$ | . 0090 |
| -25 | 0.0010 | 0.0019 | 0.0029 | 0.0038 | 0.0048 | 0.0057 | 0.0067 | 0.0076 | 0.0086 | 0.0095 |
| 24 | 10 | . 0020 | . 0030 | . 0040 | . 0050 | . 0060 | .0071 | .008I | . 0001 | . 0101 |
| 23 | . 001 I | . 0021 | .0032 | . 0043 | . 0053 | . 0064 | . 0075 | . 0086 | . 0096 | . 0107 |
| 22 | . 011 | .0023 | . 0034 | . 0045 | . 0057 | .006S | .0079 | .0091 | . 0102 | . 0113 |
| 21 | . 0012 | . 0024 | . 0036 | .0048 | . 0060 | .0072 | .0084 | .0096 | . 0108 | . 0120 |
| -20 | 0.0013 | 0.0025 | 0.0038 | 0.0051 | 0.0064 | 0.0076 | 0.0089 | 0.0102 | 0.0114 | 0.0127 |
| 19 | .0013 | . 0027 | . 0040 | . 0054 | . 0067 | . 0081 | . 0094 | . 0108 | . 0121 | . 0135 |
| 18 | .0014 | . 0029 | . 0043 | . 0057 | .0071 | . 0086 | . 0100 | . 0114 | . 0128 | . 0143 |
| 17 | .0015 | . 0030 | . 0045 | .0060 | . 0076 | . 0091 | . 0106 | . 0121 | . 0136 | . 0151 |
| 16 | .0016 | .0032 | . 0048 | .0064 | .0080 | .0096 | . 0112 | . 0128 | . 0144 | . 0160 |
| -15 | 0.0017 | 0.0034 | 0.0051 | 0.0068 | 0.0084 | O.OIOI | 0.0118 | 0.0135 | 0.0152 | 0.0169 |
| 14 | . 0018 | . 0036 | . 0054 | . 0071 | .0089 | . 0107 | . 0125 | . 0143 | .0161 | . 0179 |
| 13 | .0019 | .0038 | . 0057 | . 0076 | . 0094 | . 0113 | .OI32 | . 0151 | . 0170 | . 0189 |
| 12 | . 0020 | . 0040 | . 0060 | . 0080 | . 0100 | . 0120 | . 0140 | . 0160 | . 0180 | . 0200 |
| 11 | . 0021 | . 0042 | .0063 | . 0084 | . 0106 | . 0127 | . 0148 | . 0109 | . 0190 | . 22 I I |
| $-10$ | 0.0022 | 0.0045 | 0.0067 | 0.0089 | 0.0112 | 0.0134 | 0.0156 | 0.0178 | 0.0201 | 0.0223 |
| 9 | . 0024 | . 0047 | . 0071 | . 0094 | . 0118 | . 0141 | . 0165 | . 0188 | . 0212 | . 0236 |
| 8 | . 0025 | . 0050 | . 0075 | . 0099 | . 0124 | . 0149 | . 0174 | . 0199 | . 0224 | . 0249 |
| 7 | . 0026 | . 0053 | . 0079 | . 0105 | .0131 | . 0158 | .0184 | . 0210 | .0236 | .0263 |
| 6 | . 0028 | . 0055 | . 0083 | . OIII | . 0139 | . 0166 | .0194 | . 0222 | . 02.49 | . 0277 |
| - 5 | 0.0029 | 0.0058 | 0.0088 | 0.0117 | 0.0146 | 0.0175 | 0.0205 | 0.0234 | 0.0263 | 0.0292 |
| 4 | . 0031 | . 0062 | . 0093 | . Or 23 | . 0154 | . 0185 | . 2216 | . 0247 | . 0278 | . 0308 |
| 3 | . 0033 | . 0065 | . 0098 | . 0130 | .0163 | . 0195 | . 0228 | . 0260 | . 0293 | . 0325 |
| 2 | . 0034 | . 0069 | . 0103 | . 0137 | . 0171 | . 0206 | . 0240 | . 0274 | .0309 | . 0343 |
| 1 | .0036 | . 0072 | . 0108 | . 0145 | . 0181 | . 0217 | . 0253 | . 0289 | . 0325 | .0361 |
| $\pm 0$ | 0.0038 | 0.0076 | 0.0114 | 0.0152 | 0.0190 | 0.0229 | 0.0267 | 0.0305 | 0.0343 | 0.0381 |
| I | . 0040 | . 0080 | . 0120 | . 0161 | . 0201 | . 024 I | . 0281 | . 0321 | .0361 | . 0.401 |
| 2 | .0042 | . 0085 | . 0127 | . 0169 | . 0211 | . 0254 | . 0296 | .0.338 | . 3880 | . 0423 |
| 3 | . 0044 | . 0089 | . 0134 | . 0178 | . 0222 | . 0267 | . 0312 | .0.356 | . 0400 | . 0445 |
| 4 | . 0047 | . 0094 | . 0141 | . 0187 | . 0234 | . 0281 | . 0328 | . 0375 | . 0422 | . 0468 |
| 5 | 0.0049 | 0.0099 | 0.0148 | 0.0197 | 0.0247 | 0.0296 | 0.0345 | 0.0394 | 0.0444 | 0.0493 |
| 6 | . 0052 | . 0104 | . 0156 | . 0208 | . 0259 | . 0311 | . 0363 | . 0.415 | . 0467 | . 0519 |
| $7$ | . 0055 | . 0109 | . 0164 | . 0218 | . 0273 | . 0328 | . 0382 | . 0437 | . 0491 | . 0546 |
| 8 | . 0057 | . 0115 | . 0172 | . 0230 | .0287 | . 0344 | . 0402 | . 0459 | . 0517 | . 0574 |
| 9 | . 0060 | . 0121 | . 0181 | . 0241 | .0302 | . 0362 | . 0423 | . 0483 | . 0543 | . 0604 |
| 10 | 0.0063 | 0.0127 | 0.0190 | 0.0254 | 0.0317 | 0.0381 | 0.0444 | 0.0508 | 0.0571 | 0.0635 |
| 1 I | . 0067 | . 0133 | . 0200 | . 0267 | . 0334 | . 0400 | . 0467 | . 0534 | . 0600 | . 0667 |
| 12 | . 0070 | . 0140 | . 2210 | . 0280 | . 0350 | . 0421 | . 0491 | . 0561 | . 0631 | . 0701 |
| 13 | . 0074 | . 0147 | . 0221 | . 0295 | . 0368 | . 0442 | . 0515 | . 0589 | . 0663 | . 0736 |
| 14 | . 0077 | . 0155 | . 0232 | . 0309 | .0387 | . 0464 | . 0541 | .0619 | . 0696 | . 0773 |
| 15 | 0.0081 | 0.0162 | 0.0244 | 0.0325 | 0.0406 | 0.0487 | 0.0568 | 0.0650 | 0.0731 | 0.0812 |
| 16 | . 0085 | . 0170 | . 0256 | . 0341 | . 0426 | .0512 | . 0597 | . 0682 | . 0767 | . 0852 |
| 17 | . 0089 | . 0179 | . 0268 | . 0358 | . 0447 | . 0537 | . 0626 | . 0716 | . 0305 | . 0895 |
| 18 | . 0094 | . 0188 | . 0282 | .0376 | . 0470 | . 0563 | . 0657 | . 0751 | . 0845 | . 0939 |
| 19 | . 0099 | . 0197 | . 0296 | . 0394 | . 0493 | . 0591 | .0690 | .0788 | . 0887 | .0985 |
| 20 | 0.0103 | 0.0207 | 0.0310 | 0.0413 | 0.0517 | 0.0620 | 0.0723 | 0.0827 | 0.0930 | 0.1033 |

Table 83.
RELATIVE HUMIDITY.
TEMPERATURES FAHRENHEIT.

| $\begin{aligned} & \text { Air } \\ & \text { Temper- } \\ & \text { ature. } \end{aligned}$ | Relative humidity, or Percentage of saturation. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| F. | Vapor pressure (inches). |  |  |  |  |  |  |  |  |  |
| $20^{\circ}$ | 0.010 | 0.021 | 0.031 | 0.041 | 0.052 | 0.062 | 0.072 | 0.083 | 0.093 | 0.103 |
| 21 | . 011 | . 022 | . 033 | . 043 | . 054 | . 065 | . 076 | . 087 | . 098 | . 108 |
| 22 | . 011 | . 023 | . 034 | . 045 | . 057 | . 068 | .080 | . 091 | .102 | . 114 |
| 23 | . 012 | . 024 | . 036 | .648 | . 060 | . 071 | . 083 | . 095 | . 107 | . 119 |
| 24 | . 012 | . 025 | .0.37 | . 050 | . 062 | . 075 | .087 | . 100 | . 112 | . 125 |
| 25 | 0.013 | 0.026 | 0.039 | 0.052 | 0.065 | 0.078 | 0.092 | 0.105 | 0.118 | -.13I |
| 26 | . 014 | . 027 | . 041 | . 055 | . 068 | . 082 | .096 | . 110 | . 123 | . 137 |
| 27 | . 014 | . 029 | . 043 | .057 | . 072 | . 086 | . 100 | . 115 | . 129 | . 143 |
| 28 | . 015 | . 030 | . 045 | . 060 | . 075 | . 090 | .105 | . 120 | . 135 | . 150 |
| 29 | . 016 | . 031 | . 047 | . 063 | . 079 | . 094 | . 110 | . 126 | . 142 | . 157 |
| 30 | 0.016 | 0.033 | 0.049 | 0.066 | 0.082 | 0.099 | 0.115 | 0.132 | 0.148 | 0.165 |
| 31 | . 1017 | . 034 | . 052 | . 069 | . 086 | . 103 | . 121 | . 138 | . 155 | .172 |
| 32 | . 18 | . 036 | . 054 | . 072 | . 090 | . 108 | . 126 | . 144 | .162 | . 180 |
| 33 | . 019 | . 038 | . 056 | . 075 | .094 | . 113 | . 31 | . 150 | . 169 | . 188 |
| 34 | . 020 | . 039 | .c59 | .078 | . 0.98 | . 117 | . 137 | . 156 | . 176 | . 195 |
| 35 | 0.020 | c. 041 | 0.061 | 0.081 | 0.102 | O.122 | 0.142 | 0.163 | 0.183 | 0.203 |
| 30 | . 021 | . 042 | . 064 | . 085 | . 106 | . 127 | .148 | . 169 | . 191 | . 212 |
| 37 | . 022 | . 044 | 066 | . 088 | . 110 | . 132 | .154 | . 76 | . 198 | . 220 |
| 38 | . 023 | . 046 | . 069 | . 092 | . 115 | . 137 | .160 | .183 | . 206 | . 229 |
| 39 | . 024 | . 048 | . 071 | . 095 | .119 | . 143 | . 167 | .191 | . 214 | . 238 |
| 40 | 0.025 | 0.050 | 0.074 | 0.099 | 0.124 | 0.149 | 0.173 | 0.198 | 0.223 | 0.248 |
| 4 I | . 026 | .052 | . 077 | . 103 | . 129 | . 155 | . 180 | . 206 | .232 | . 258 |
| 42 | . 027 | . 054 | . 080 | .107 | . 134 | . 161 | .187 | . 214 | . 241 | . 268 |
| 43 | . 028 | . 056 | . 083 | .III | . 139 | .167 | . 195 | . 223 | . 250 | .278 |
| 44 | . 029 | . 058 | . 087 | . 116 | .145 | . 173 | . 202 | . 231 | . 260 | . 289 |
| 45 | 0.030 | 0.060 | c.090 | 0.120 | 0. 150 | 0.180 | 0.210 | 0.240 | 0.270 | 0.300 |
| 46 | . 031 | . 062 | . 094 | . 125 | . 156 | . 187 | . 218 | . 250 | . 281 | . 312 |
| 47 | . 032 | . 065 | . 097 | . 130 | . 162 | . 194 | . 227 | . 259 | . 292 | . 324 |
| 48 | . 034 | . 067 | . 101 | . 135 | . 168 | . 202 | . 236 | . 269 | .303 | . 336 |
| 49 | . 035 | . 050 | .105 | . 140 | . 175 | . 210 | . 245 | . 279 | . 314 | -349 |
| 50 | 0.036 | 0.073 | 0.109 | 0.145 | 0.181 | 0.218 | 0.254 | 0.290 | 0.326 | 0.363 |
| 51 | . 038 | . 075 | . 113 | . 151 | . 188 | . 226 | . 263 | . 301 | . 339 | . 376 |
| 52 | . 039 | . 078 | . 117 | .156 | . 195 | . 234 | . 273 | -312 | . 351 | -390 |
| 53 | . 041 | .08I | . 122 | . 162 | . 203 | . 243 | . 284 | . 324 | . 365 | . 405 |
| 54 | . 042 | .084 | . 126 | . 168 | . 210 | . 252 | . 294 | . 336 | . 378 | . 420 |
| 55 | 0.044 | 0.087 | 0.131 | 0.174 | 0.218 | 0.262 | 0.305 | 0.349 | 0.392 | 0.436 |
| 56 | . 045 | . 090 | . 136 | . 181 | . 226 | . 271 | .316 | . 362 | . 407 | . 452 |
| 57 | . 047 | . 094 | .141 | .187 | . 234 | . 281 | . 328 | . 375 | . 422 | . 469 |
| 58 | . 049 | .097 | . 14.6 | . 194 | . 243 | . 292 | . 340 | . 389 | . 437 | . 486 |
| 59 | . 050 | . 101 | . 151 | . 201 | . 252 | . 302 | . 353 | . 403 | . 453 | . 504 |
| 60 | 0.052 | 0.104 | -. 157 | 0.209 | 0.261 | 0.313 | 0.365 | 0.418 | 0.470 | 0.522 |
| 61 | . 054 | . 108 | . 162 | . 216 | . 270 | . 325 | . 379 | . 433 | . 487 | . 541 |
| 62 | . 056 | . 112 | . 168 | . 224 | . 280 | . 336 | . 392 | . 448 | . 504 | . 560 |
| 63 | . 058 | . 116 | . 174 | .232 | . 290 | . 348 | .406 | . 464 | . 522 | . 580 |
| 64 | . 060 | .120 | . 180 | . 241 | . 301 | . 361 | . 42 I | . 481 | . 541 | .601 |
| 65 | 0.062 | 0.125 | 0.187 | 0.249 | 0.311 | 0.374 | 0.436 | 0.498 | 0.560 | 0.623 |
| 66 | . 064 | . 129 | . 193 | . 258 | . 322 | . 387 | . 451 | . 516 | . 580 | . 645 |
| 67 | . 067 | .133 | . 200 | . 267 | . 334 | . 400 | . 467 | . 534 | . 601 | . 667 |
| 68 | . 069 | . 138 | . 207 | .276 | . 345 | .415 | . 484 | . 553 | . 622 | .691 |
| 69 | . 072 | . 143 | . 214 | . 286 | . 358 | . 429 | . 500 | . 572 | . 644 | . 715 |
| 70 | 0.074 | 0.148 | 0.222 | 0.296 | 0.370 | 0.444 | 0.518 | 0.592 | 0.666 | 0.740 |

RELATIVE HUMIDITY.
TEMPERATURES FAHRENHEIT.

| $\begin{aligned} & \text { Air } \\ & \text { Temper- } \\ & \text { ature. } \end{aligned}$ | relative ilumidity, or percentage of saturation. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| F. | Vapor pressure (inches). |  |  |  |  |  |  |  |  |  |
| $70^{\circ}$ | 0.074 | 0.148 | 0.222 | 0.296 | 0.370 | 0.444 | 0.518 | 0.592 | 0.666 | 0.740 |
| 71 | . 077 | . 153 | . 230 | . 306 | .383 | . 459 | . 536 | . 612 | . 689 | . 760 |
| 72 | . 079 | . 158 | . 238 | . 317 | . 396 | . 475 | - 554 | . 634 | . 713 | .792 |
| 73 | . 082 | . 164 | . 246 | . 328 | . 410 | . 491 | - 573 | . 655 | . 737 | . 819 |
| 74 | . 085 | . 169 | . 254 | . 339 | . 424 | . 508 | . 593 | . 678 | .762 | . 847 |
| 75 | 0.088 | 0. 175 | 0.263 | 0.350 | 0.438 | 0.526 | 0.613 | $0.7 C 1$ | 0.788 | 0.876 |
| 76 | . 091 | . 181 | .272 | . 362 | . 453 | . 543 | . 634 | . 724 | . 815 | . 906 |
| 77 | . 094 | . 187 | . 281 | . 374 | . 468 | . 562 | . 655 | . 749 | . 843 | . 936 |
| 78 | . 097 | . 194 | . 290 | . 387 | . 484 | .581 | . 677 | . 774 | . 871 | . 968 |
| 79 | . 100 | . 200 | . 300 | . 400 | . 500 | . 600 | .700 | . 800 | . 900 | 1.000 |
| 80 | 0.103 | 0.207 | 0.310 | 0.413 | 0.517 | 0.620 | 0.723 | 0.827 | 0.930 | 1.033 |
| 81 | . 107 | . 214 | . 320 | . 427 | . 534 | . 641 | . 747 | . 854 | . 961 | 1.068 |
| 82 | . 110 | . 221 | . 331 | . 44 I | . 551 | . 662 | . 772 | . 882 | . 993 | 1. 103 |
| 83 | . 114 | . 228 | . 342 | .456 | . 570 | . 684 | . 797 | .91I | 1.025 | 1.139 |
| 84 | . 118 | . 235 | . 353 | . 471 | . 588 | . 706 | . 824 | . 941 | 1. 059 | 1.17 76 |
| 85 | 0.121 | 0.243 | 0.364 | 0.486 | 0.607 | 0.729 | 0.850 | 0.972 | 1.093 | 1.215 |
| 86 | . 125 | . 251 | . 376 | . 502 | . 627 | . 753 | . 878 | 1.003 | I. 129 | 1. 254 |
| 87 | . 129 | . 259 | . 388 | . 518 | .647 | . 777 | . 906 | 1.036 | 1.165 | 1.295 |
| 88 | . 134 | . 267 | . 401 | . 535 | . 668 | . 802 | . 936 | 1.069 | 1.203 | 1.336 |
| 89 | . 138 | . 276 | . 414 | . 552 | . 690 | . 828 | . 966 | 1. 104 | 1.24 I | 1.379 |
| 90 | 0.142 | 0.285 | 0.427 | 0.569 | 0.712 | 0.854 | 0.996 | 1.139 | 1.281 | 1.423 |
| 91 | . 147 | . 294 | . 441 | . 588 | . 734 | . 88 I | 1.028 | 1.175 | 1.322 | 1.469 |
| 92 | . 152 | . 303 | -455 | . 606 | . 758 | . 909 | 1.061 | 1.212 | I. 364 | 1.515 |
| 93 | . 156 | . 313 | . 469 | . 625 | .782 | .938 | 1.094 | 1.2 .50 | 1.407 | 1.563 |
| 94 | .161 | . 322 | . 484 | . 645 | . 806 | . 967 | 1. 128 | 1. 290 | 1.45 I | 1.612 |
| 95 | 0.166 | 0.332 | 0.499 | 0.665 | 0.831 | 0.998 | 1.164 | 1.330 | 1. 496 | 1.662 |
| 96 | . 171 | . 343 | .514 | . 686 | . 857 | 1.029 | 1.200 | 1.371 | 1.543 | 1.714 |
| 97 | . 177 | . 353 | . 530 | .707 | . 884 | 1.060 | 1.237 | 1.414 | 1. 591 | 1.767 |
| 98 | . 182 | . 364 | . 547 | . 729 | . 911 | 1.093 | 1.275 | 1.458 | 1.640 | 1.822 |
| 99 | . 188 | . 376 | . 563 | .751 | . 939 | 1.127 | 1.315 | 1.502 | 1.690 | 1. 878 |
| 100 | 0.194 | 0.387 | 0.581 | 0.774 | 0.968 | 1.161 | 1.355 | 1. 548 | 1.742 | 1.936 |
| 101 | . 199 | . 399 | . 598 | . 798 | . 997 | 1.197 | 1.396 | 1.596 | 1.795 | 1.994 |
| 102 | . 206 | . 41 I | .616 | . 822 | 1.028 | 1.233 | 1.438 | 1. 644 | 1. 850 | 2.055 |
| 103 | . 212 | . 423 | . 635 | . 847 | 1.059 | 1.270 | 1.482 | 1.694 | 1.905 | 2.117 |
| 104 | . 218 | . 436 | . 654 | . 872 | 1.090 | 1.309 | 1.527 | 1.745 | 1.963 | 2.181 |
| 105 | 0.225 | 0.449 | 0.674 | 0.899 | 1.123 | 1.348 | 1.572 | 1.797 | 2.022 | 2.246 |
| 106 | . 231 | . 463 | . 694 | . 925 | 1.157 | 1.388 | 1.619 | 1. 851 | 2.082 | 2.314 |
| 107 | . 238 | .476 | . 715 | . 953 | 1.19 I | 1.429 | 1.668 | 1.906 | 2.144 | 2.382 |
| 108 | . 245 | . 491 | . 736 | . 981 | 1. 226 | 1.472 | 1.717 | 1.962 | 2.208 | 2.453 |
| 109 | . 253 | . 505 | .758 | 1.010 | 1.263 | 1.515 | 1.768 | 2.020 | 2.273 | 2.525 |
| 110 | 0.260 | 0.520 | 0.780 | 1.040 | 1.300 | 1.560 | 1.820 | 2.080 | 2.339 | 2.599 |
| III | . 268 | . 535 | . 8 c3 | 1.070 | 1.338 | 1.605 | 1.873 | 2.140 | 2.408 | 2.676 |
| 112 | . 275 | . 551 | . 826 | 1.101 | 1.377 | 1.652 | 1.027 | 2.203 | 2.478 | 2.754 |
| II3 | . 283 | . 567 | . 850 | 1.133 | 1.417 | 1.700 | 1.983 | 2.267 | 2.550 | 2.833 |
| 114 | . 292 | . 583 | . 875 | 1.166 | 1. $45^{8}$ | 1.749 | 2.04 I | 2.332 | 2.624 | 2.915 |
| 115 | 0.300 | 0.600 | 0.900 | 1.200 | 1.500 | 1.80c | 2.100 | 2.399 | 2.699 | 2.999 |
| 116 | . 309 | . 617 | . 926 | 1.234 | 1. 543 | 1.851 | 2.160 | 2.468 | 2.777 | 3.085 |
| 117 | . 317 | . 635 | . $95{ }^{2}$ | 1.269 | 1.587 | 1.904 | 2.221 | 2.539 | 2.856 | 3.173 |
| 118 | .326 | . 653 | . 979 | 1.305 | 1.632 | 1.958 | 2.285 | 2.611 | 2.937 | 3.264 |
| 119 | . 336 | . 671 | 1.007 | 1.342 | 1.678 | 2.014 | 2.349 | 2.685 | 3.021 | 3.356 |
| 120 | 0.345 | 0.69 c | 1.035 | 1.380 | 1.725 | 2.071 | 2.416 | 2.761 | 3.106 | 3.45 I |

Table 84.
REDUCTION OF PSYCHROMETRIC OBSERVATIONS.
METRIC MEASURES.
Values of $e=e^{\prime}-0.000660 B\left(t-t^{\prime}\right)\left(\mathrm{I}+0.00115 t^{\prime}\right)$


REDUCTION OF PSYCHROMETRIC OBSERVATIONS. METRIC MEASURES.
Values of $e=e^{\prime}-0.000660 B\left(t-t^{\prime}\right)\left(\mathrm{I}+0.00 \mathrm{I} \mathrm{I} 5 t^{\prime}\right)$
$B=760 \mathrm{~mm}$.

| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.0 | 1.1 | 1.2 | 1.3 | 1.4 | 1.5 | 1.6 | 1.7 | 1.8 | 1.9 | 2.0 |
| C. | mm. | mm. |  | mm. | mm. | mm. |  | mm. | mm. | mm. | mm. |
| $-25^{\circ}$ | 0.480 |  |  |  |  |  |  |  |  |  |  |
| 24 | . 530 |  |  |  |  |  |  |  |  |  |  |
| 23 | . 585 | 0.048 |  |  |  |  |  |  |  |  |  |
| 22 | . 646 | . 108 | 0.059 | 0.010 |  |  |  |  |  |  |  |
| -20 | .783 | . 244 | . 195 | . 146 | . 097 | 0.048 |  |  |  |  |  |
| 19 | . 862 | . 322 | . 273 | . 224 | . 175 | . 126 | 0.077 | 0.028 |  |  |  |
| 18 | . 947 | . 407 | . 358 | . 309 | . 260 | . 211 | .161 | . 112 | 0.063 | 0.014 |  |
| 17 | 1.041 | . 500 | . 450 | . 401 | . 352 | . 303 | . 254 | . 205 | . 155 | . 106 | 0.057 |
| 16 | I. 142 | . 600 | . 551 | .502 | . 453 | . 404 | -354 | . 305 | .256 | . 207 | . 57 |
| -15 | 1.252 | .710 | . 661 | . 612 | . 562 | . 513 | .464 | .414 | .365 | . 316 | . 267 |
| 14 | 1.373 | .830 | . 780 | . 731 | . 682 | . 632 | .583 | . 534 | . 484 | . 435 | . 386 |
| 13 | 1.503 | . 959 | . 910 | . 861 | . 8 I | .762 | . 712 | . 663 | .614 | . 564 | . 515 |
| 12 | 1.644 | 1.100 | 1.051 | 1.001 | . 952 | . 902 | . 853 | .803 | . 754 | .705 | . 655 |
| I I | 1.798 | 1.253 | I. 20.4 | 1.154 | 1.105 | 1.055 | 1.005 | .956 | .906 | . 857 | . 807 |
| $-10$ | +1.964 | 1.419 | 1.369 | 1.320 | 1.270 | 1.221 | 1.171 | 1.121 | 1.072 | 1.022 | . 973 |
| 9 | 2.144 | 1.598 | 1. 549 | 1.499 | 1.450 | 1.400 | 1.350 | 1.301 | 1.251 | 1.201 | 1.152 |
| 8 | 2.340 | 1.79.3 | 1.743 | 1.693 | 1.644 | 1.594 | 1.544 | 1. 495 | 1.445 | 1. 395 | 1. 346 |
| 7 | 2.550 | 2.003 | 1.953 | 1.904 | 1.854 | 1.804 | 1.754 | 1.705 | 1. 655 | 1. 605 | 1.555 |
| 6 | 2.778 | 2.231 | 2.181 | 2.131 | 2.081 | 2.031 | 1.981 | 1.932 | 1.882 | 1.832 | 1.782 |
| -5 | 3.025 | 2.476 | 2.426 | 2.376 | 2.327 | 2.277 | 2.227 | 2.177 | 2.127 | 2.077 | 2.027 |
| -5 | $\Delta e \times \Delta B$ | +0.072 | +0.079 | +0.085 | +0.092 | +0.098 | +0.105 | +0.112 | +0.118 | +0.125 | +0.131 |
| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |  |
|  | 0.0 | 2.1 | 2.2 | 2.3 | 2.4 | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 |
| C. | mm . | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. | mm. |
| $-15^{\circ}$ | $\Delta \times \Delta B$ | +0.136 | +0.143 | +0.149 | +0.156 | +0.162 | +0.169 | +0.175 | +o.182 | +o.188 | +0.195 |
| $-17^{\circ}$ | 1.041 | 0.008 |  |  |  |  |  |  |  |  |  |
| 16 | 1.142 | -. 108 | 0.059 | 0.010 |  |  |  |  |  |  |  |
| -15 | 1. 252 | 0.217 | . 168 | . 119 | 0.069 | 0.020 |  |  |  |  |  |
| 14 | 1.373 | .336 | . 287 | . 237 | . 188 | . 139 | 0.089 | 0.040 |  |  |  |
| 13 | 1.503 | . 465 | . 416 | . 366 | -317 | . 268 | . 218 | . 169 | 0.119 | 0.070 | 0.021 |
| 12 | 1.644 | . 006 | . 556 | . 507 | . 457 | . 408 | -358 | . 309 | . 259 | . 210 | . 160 |
| 11 | 1.798 | .758 | . 708 | . 659 | . 609 | . 560 | . 510 | .46I | . 411 | .362 | . 312 |
| $-10$ | 1.964 | . 923 | . 873 | . 824 | . 774 | . 72.5 | . 675 | . 626 | .576 | . 526 | . 477 |
| 9 | 2.144 | 1.102 | 1.052 | 1.003 | . 953 | . 903 | . 854 | . 804 | . 755 | . 70.5 | . 655 |
| 8 | 2.340 | 1.296 | 1.246 | 1.196 | 1.147 | 1.097 | 1.047 | . 998 | . 948 | . 898 | . 849 |
|  |  | 1.506 | 1.456 | 1.406 | 1.356 | 1.307 | 1.257 | 1.207 | 1.157 | 1.108 | 1.058 |
| 6 | 2.778 | 1.732 | 1.683 | 1.633 | 1. 583 | 1.533 | 1.483 | 1. 434 | 1.384 | 1.334 | 1.284 |
| - 5 | 3.025 | 1.977 | 1.928 | 1.878 | I. 828 | 1.778 | 1.728 | 1. 678 | 1. 628 | 1.579 | 1.529 |
| - 5 | $\Delta c \times \Delta B$ | +0.138 | +0.144 | +0.151 | +0.157 | +o.164 | +0.171 | +0.177 | +0.184 | +0.190 | +0.197 |

Smithsonian Tables.

Table 84.

## REDUCTION OF PSYCHROMETRIC OBSERVATIONS. METRIC MEASURES.

$$
\text { Values of } e=c^{\prime}-0.000660 B\left(t-t^{\prime}\right)\left(1+0.00115 t^{\prime}\right)
$$

$B=760 \mathrm{~mm}$.

| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3.1 | 3.2 | 3.3 | 3.4 | 3.5 | 3.6 | 3.7 | 3.8 | 3.9 | 4.0 |
| $\begin{aligned} & \mathrm{C} \\ & -10^{\circ} \Delta e \times \Delta B \end{aligned}$ | mm. | mm. +0.209 | mm. +0.215 | $\begin{gathered} \mathrm{mm} . \\ +0.222 \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +0.228 \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +0.235 \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +0.24 \mathrm{I} \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +0.248 \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +0.254 \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +0.261 \end{gathered}$ |
| $-12^{\circ}$ 11 | 0.111 .263 | 0.061 .213 | 0.012 .164 | O.II4 | 0.065 | 0.015 |  |  |  |  |
| $-10$ | . 427 | . 378 | . 328 | .278 | . 229 | . 179 | 0.130 | 0.080 | 0.031 |  |
| 9 | . 606 | . 556 | . 506 | . 457 | . 407 | -357 | . 308 | . 258 | . 209 | -. 159 |
| 8 | . 799 | . 749 | . 699 | . 650 | . 600 | - 5.50 | . 501 | . 451 | .401 | . 3.52 |
| 7 | 1. 008 | .958 | 909 | . 859 | . 809 | . 759 | . 710 | . 660 | . 610 | . 560 |
| 6 | 1.234 | 1.184 | 1.135 | 1.085 | 1.035 | .985 | . 935 | . 886 | . 836 | . 786 |
| -5 | 1.479 | 1.429 | 1.379 | 1.329 | I. 279 | 1. 229 | 1.180 | 1.130 | 1.080 | 1.030 |
| $-5 \Delta e \times \Delta B$ | $+0.203$ | +0.210 | +0.217 | +0.223 | +0.230 | +0.2.36 | +0.243 | +0.249 | +0.256 | +0.262 |
| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |
|  | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 | 4.9 | 5.0 |
| C. $-8^{\circ} \Delta e \times \Delta B$ | $\begin{gathered} \mathrm{mm} . \\ +0.268 \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +0.275 \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +0.28 \mathrm{I} \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +0.288 \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +0.204 \end{gathered}$ | mm. +0.301 | mm. +0.307 | $\begin{gathered} \mathrm{mm} . \\ +0.314 \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +0.320 \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +0.327 \end{gathered}$ |
| $-9^{\circ}$ | 0.109 | $0.060$ | 0.010 |  |  |  |  |  |  |  |
| 8 | 0.302 | 0.252 | . 202 | 0.153 |  | 0.053 | 0.004 |  |  |  |
| 7 | .510 .736 | . 4681 | . 411 | . 361 | .311 .537 | .262 .487 | .212 .437 | 0.162 .387 | 0.112 .338 | 0.063 .288 |
| -5 | 0.980 | 0.930 | 0.880 | 0.830 | 0.781 | 0.731 | 0.68 I | 0.631 | 0.58 I | 0.531 |
| $-5 \Delta_{c} \times \Delta B$ | +0.269 | +0.276 | +0.282 | +0.280 | +0.295 | +0.302 | +0.308 | +0.315 | +0.322 | +0.328 |
| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |
|  | 5.1 | 5.2 | 5.3 | 5.4 | 5.5 | 5.6 | 5.7 | 5.8 | 5.9 | 6.0 |
| c. | mm. | mm . | mm. | mm. | mm . | mm. | mm . | mm . | mm . | mm. |
| $\begin{gathered} -7^{\circ} \\ 6 \end{gathered}$ | $\begin{array}{r} 0.013 \\ .238 \end{array}$ | $0.188$ | 0.138 | 0.089 | 0.039 |  |  |  |  |  |
| -5 | 0.48 I | 0.431 | 0.382 | 0.332 | 0.282 | 0.232 | 0.182 | 0.132 | 0.082 | 0.033 |
| $-5 \Delta e \times \Delta B$ | +0.335 | +0.34 I | +0.348 | +0.354 | +0.361 | $+0.367$ | +0.374 | +0.381 | $+0.387$ | +0.304 |

Smithsonian tables.

## Table 84.

REDUCTION OF PSYCHROMETRIC OBSERVATIONS. METRIC MEASURES.
Values of $e=c^{\prime}-0.000660 B\left(t-t^{\prime}\right)\left(1+0.00115 t^{\prime}\right)$
$B=760 \mathrm{~mm}$.

| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
| c. | mm | mm. | mm. | mm. | mm. | mm. | mm. |  | mm. |  | mm. |
| $-5^{\circ}$ | $\Delta e \times \Delta B$ | +0.07 | +0.13 | +0.20 | +0.26 | +0.33 | +0.30 | +0.46 | +0.52 | +0.59 | 66 |
| $-5^{\circ}$ | 3.02 | 2.53 | 2.03 | 1.53 | 1.03 | 0.53 | 0.03 |  |  |  |  |
| 4 | 3.29 | 2.79 | 2.29 | I. 79 | 1.29 | 0.79 | 0.29 |  |  |  |  |
| 3 | 3.58 | 3.08 | 2.58 | 2.08 | 1.58 | 1.08 | 0.58 | 0.08 |  |  |  |
| 2 | 3.89 | 3.39 | 2.89 | 2.39 | 1.89 | 1.38 | 0.88 | 0.38 |  |  |  |
| 1 | 4.22 | 3.72 | 3.22 | 2.72 | 2.22 | 1.71 | 1.21 | 0.71 | . 21 |  |  |
| $\pm 0$ | $4 \cdot 58$ | 4.08 | $3 \cdot 58$ | 3.08 | 2.57 | 2.07 | 1.57 | 1.07 | 0.57 | 0.07 |  |
| +1 | 4.92 | 4.42 | 3.92 | 3.42 | 2.92 | 2.41 | 1.91 | 1.41 | 0.91 | 0.40 |  |
| 2 | 5.29 | 4.79 | 4.29 | 3.78 | 3.28 | 2.78 | 2.27 | 1.77 | 1.27 | 0.77 | 0.26 |
| 3 | 5.68 | 5.18 | 4.68 | 4.17 | 3.67 | 3.17 | 2.66 | 2.16 | I. 66 | 1.15 | 0.65 |
| 4 | 6.10 | 5.59 | 5.09 | 4.59 | 4.08 | 3.58 | 3.07 | 2.57 | 2.07 | I. 56 | 1.06 |
| 5 | 6.54 | 6.03 | 5.53 | 5.03 | $4 \cdot 52$ | 4.02 | 3.51 | 3.01 | 2.51 | 2.00 | 1.50 |
| 6 | 7.01 | 6.51 | 6.00 | $5 \cdot 50$ | 4.99 | 4.49 | 3.98 | 3.48 | 2.97 | 2.47 | 1.96 |
|  | 7.51 | 7.01 | 6.50 | 6.00 | 5.49 | 4.98 | 4.48 | 3.97 | 3.47 | 2.96 | 2.46 |
| 8 | 8.05 | 7.54 | 7.03 | 6.53 | 6.02 | 5.51 | 5.01 | 4.50 | 4.00 | 3.49 | 2.98 |
| 9 | 8.61 | 8.10 | 7.60 | 7.09 | 6.58 | 6.08 | $5 \cdot 57$ | 5.06 | $4 \cdot 56$ | 4.05 | $3 \cdot 54$ |
| 10 | 9.21 | 8.70 | 8.20 | 7.69 | 7.18 | 6.67 | 6.17 | 5.66 | 5.15 | 4.64 | 4.14 |
| 11 | 9.85 | 9.34 | 8.83 | 8.32 | 7.81 | 7.31 | 6.80 | 6.29 | 5.78 | 5.27 | 4.77 |
| 12 | 10.52 | 10.01 | 9.50 | 9.00 | 8.49 | 7.98 | 7.47 | 6.96 | 6.45 | 5.94 | 5.44 |
| 13 | I I . 24 | 10.73 | 10.22 | 9.71 | 9.20 | 8.69 | 8.18 | 7.67 | 7.16 | 6.65 | 6.14 |
| 14 | 11.99 | 11.48 | 10.97 | 10.46 | 9.95 | 9.44 | 8.93 | 8.42 | 7.91 | 7.4 I | 6.90 |
| 15 | 12.79 | 12.28 | 11.77 | 11.26 | 10.75 | 10.24 | 9.73 | 9.22 | 8.71 | 8.20 | 7.69 |
| 16 | I 3.64 | 13.13 | 12.62 | 12.11 | 11.60 | 11.09 | 10.58 | 10.07 | 9.56 | 9.04 | 8.53 |
| 17 | 14.54 | 14.03 | 13.52 | 13.00 | 12.49 | 11.98 | 11.47 | 10.96 | 10.45 | 9.94 | 9.42 |
| 18 | 15.49 | 14.98 | 14.46 | 13.95 | 13.44 | 12.93 | 12.42 | 11.90 | 11.39 | 10.88 | 10.37 |
| 19 | 16.49 | 15.98 | 15.46 | 14.95 | 14.44 | 13.93 | 13.41 | 12.90 | 12.39 | 11.88 | 11.36 |
| 20 | ${ }^{1} 7.55$ | 17.03 | 16.52 | 16.01 | 15.50 | 14.98 | 14.47 | 13.96 | 13.44 | 12.93 | 12.42 |
| 21 | 18.66 | 18.15 | 17.64 | 17.12 | 16.61 | 16.10 | 15.58 | 15.07 | 14.56 | 14.04 | 13.53 |
| 22 | 19.84 | 19.33 | 18.82 | 18.30 | 17.79 | 17.27 | 16.76 | 16.24 | 15.73 | 15.22 | 14.70 |
| 23 | 21.09 | 20.57 | 20.06 | 19.54 | 19.03 | 18.51 | 18.00 | 17.48 | 16.97 | 16.45 | 15.94 |
| 24 | 22.40 | 21.88 | 21.37 | 20.85 | 20.34 | 19.82 | 19.31 | 18.79 | 18.27 | 17.76 | 17.24 |
| 25 | 23.78 | 23.26 | 22.75 | 22.23 | 21.72 | 21.20 | 20.68 | 20.17 | 19.65 | 19.14 | 18.62 |
| 26 | 25.24 | 24.72 | 24.20 | 23.69 | 23.17 | 22.65 | 22.14 | 21.62 | 21.10 | 20.59 | 20.07 |
| 27 | 26.77 | 26.25 | 25.73 | 25.22 | 24.70 | 24.18 | 23.66 | 23.15 | 22.63 | 22.11 | 21.60 |
| 28 | 28.38 | 27.86 | 27.34 | 26.83 | 26.31 | 25.79 | 25.27 | 24.76 | 24.24 | 23.72 | 23.20 |
| 29 | 30.08 | 29.56 | 29.04 | 28.52 | 28.00 | 27.48 | 26.97 | 26.45 | 25.93 | 25.41 | 24.89 |
| 30 | 31.86 | 31.34 | 30.82 | 30.30 | 29.78 | 29.27 | 28.75 | 28.23 | 27.71 | 27.19 | 26.67 |
| 31 | 33.74 | 33.22 | 32.70 | 32.18 | 31.66 | 31.14 | 30.62 | 30.10 | 29.58 | 29.06 | 28.54 |
| 32 | 35.70 | 35.18 | 34.66 | 34.14 | 33.62 | 33.10 | 32.58 | 32.06 | 31.54 | 31.02 | 30.50 |
| 33 | 37.78 | 37.25 | 36.73 | 36.21 | 35.69 | 35.17 | 34.65 | 34.13 | 33.61 | 33.09 | 32.57 |
| 34 | 39.95 | 39.43 | 38.90 | 38.38 | 37.86 | 37.34 | 36.82 | 36.30 | 35.78 | 35.26 | 34.73 |
| 35 | 42.23 | 41.71 | 41.18 | 40.66 | 40.14 | 39.62 | 39.10 | 38.57 | 38.05 | 37.53 | 37.01 |
| 36 | 44.62 | 44.10 | 43.57 | 43.05 | 42.53 | 42.01 | 41.48 | 40.96 | 40.44 | 39.92 | 39.40 |
| 37 | 47.13 | 46.60 | 46.08 | 45.56 | 45.04 | 44.51 | 43.99 | 43.47 | 42.94 | 42.42 | 41.90 |
| 38 | 49.76 | 49.23 | 48.71 | 48.19 | 47.66 | 47.14 | 46.61 | 46.09 | 45.57 | 45.04 | 44.52 |
| 39 | 52.51 | 51.99 | 51.46 | 50.94 | 50.41 | 49.89 | 49.37 | 48.84 | 48.32 | 47.79 | 47.27 |
| 40 | 55.40 | 54.87 | 54.35 | 53.82 | 53.30 | 52.77 | 52.25 | 51.72 | 51.20 | 50.67 | 50.15 |
| 41 | 58.42 | 57.89 | 57.37 | 56.84 | 56.32 | 55.79 | 55.27 | 54.74 | 54.21 | 53.69 | 53.16 |
| 42 | 61.58 | 61.05 | 60.53 | 60.00 | 59.48 | 58.95 | 58.43 | 57.90 | 57.37 | 56.85 | 56.32 |
| 43 | 64.89 | 64.36 | 63.84 | 63.31 | 62.78 | 62.26 | 61.73 | 61.20 | 60.68 | 60.15 | 59.62 |
| 44 | 68.35 | 67.82 | 67.30 | 66.77 | 66.24 | 65.72 | 65.19 | 64.66 | 64.13 | 63.61 | 63.08 |
| 45 | 71.97 | 71.44 | 70.91 | 70.39 | 69.86 | 69.33 | 68.80 | 68.28 | 67.75 | 67.22 | 66.69 |
| 45 | $\Delta e \times \Delta B$ | +0.07 | +0.14 | +0.21 | +0.28 | +0.35 | +0.42 | +0.49 | +0.56 | +0.62 | +0.69 |

Smithsonian Tables.

Table 84.
REDUCTION OF PSYCHROMETRIC OBSERVATIONS.
METRIC MEASURES.
Values of $e=e^{\prime}-0.000660 B\left(t-t^{\prime}\right)\left(\mathrm{I}+0.00115 t^{\prime}\right)$
$B=760 \mathrm{~mm}$.

| $t^{\prime}$ | $t-t^{\prime}$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| $\begin{gathered} \text { C. } \\ +5^{\circ} \end{gathered}$ | $\stackrel{\mathrm{mm} .}{\Delta c \times \Delta B}$ | $\begin{gathered} \mathrm{mm} . \\ +0.73 \end{gathered}$ | $\begin{aligned} & \mathrm{mm} . \\ & +0.80 \end{aligned}$ | $\begin{aligned} & \mathrm{mm} . \\ & +0.86 \end{aligned}$ | $\begin{aligned} & \mathrm{mm} . \\ & +0.93 \end{aligned}$ | $\begin{gathered} \mathrm{mm} . \\ +1.00 \end{gathered}$ | $\begin{aligned} & \mathrm{mm} . \\ & +\mathrm{I} .06 \end{aligned}$ | $\begin{aligned} & \mathrm{mm.} \\ & +\mathrm{I} .13 \end{aligned}$ | $\begin{gathered} \mathrm{mm} . \\ +1.19 \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +1.26 \end{gathered}$ | $\begin{gathered} \mathrm{mm} . \\ +1.33 \end{gathered}$ |
| $+3^{\circ}$ | 5.68 | 0.15 |  |  |  |  |  |  |  |  |  |
| 4 | 6.10 | 0.56 | 0.05 |  |  |  |  |  |  |  |  |
| 5 | 6.54 | 0.99 | 0.49 |  |  |  |  |  |  |  |  |
| 6 | 7.01 | I. 46 | 0.95 | 0.45 |  |  |  |  |  |  |  |
| 7 | 7.51 | 1.95 | 1.45 | 0.94 | 0.43 |  |  |  |  |  |  |
| 8 | 8.05 | 2.48 | 1.97 | 1.46 | 0.96 | 0.45 |  |  |  |  |  |
| 9 | 8.61 | 3.04 | 2.53 | 2.02 | 1.52 | 1.01 | 0.50 |  |  |  |  |
| 10 | 9.21 | 3.63 | 3.12 | 2.61 | 2.11 |  | 1.09 | 0.58 | 0.08 |  |  |
| 11 | 9.85 | 4.26 | $3 \cdot 75$ | 3.24 | 2.73 | 2.23 | 1. 72 | 1.21 | 0.70 | 0.20 |  |
| 12 | 10.52 | 4.93. | 4.42 | 3.91 | 3.40 | 2.89 | 2.38 | 1.88 | 1.37 | 0.86 | 0.35 |
| 13 | 11.24 | 5.63 | 5.13 | 4.62 | 4.11 | 3.60 | 3.09 | 2.58 | 2.07 | 1. 56 | 1.05 |
| 14 | 11.99 | 6.39 | 5.88 | $5 \cdot 37$ | 4.86 | $4 \cdot 35$ | 3.84 | 3.33 | 2.82 | 2.31 | 1.80 |
| 15 | 12.79 | 7.18 | 6.67 | 6.16 | 5.65 | 5.14 | 4.63 | 4.12 | 3.61 | 3.10 | 2.59 |
| 16 | 13.64 | 8.02 | 7.51 | 7.00 | 6.49 | 5.98 | 5.47 | 4.96 | 4.45 | 3.94 | 3.43 |
| 17 | 14.54 | 8.91 | 8.40 | 7.89 | 7.38 | 6.87 | 6.36 | 5.85 | 5.33 | 4.82 | $4 \cdot 31$ |
| 18 | 15.49 | 9.86 | 9.34 | 8.83 | 8.32 | 7.81 | 7.30 | 6.78 | 6.27 | 5.76 | 5.25 |
| 19 | 16.49 | 10.85 | 10.34 | 9.83 | 9.31 | 8.80 | 8.29 | 7.78 | 7.26 | 6.75 | 6.24 |
| 20 | I 7.55 | 11.90 | 11.39 | 10.88 | 10.36 | 9.85 | 9.34 | 8.82 | 8.31 | 7.80 | 7.29 |
| 21 | 18.66 | 13.01 | 12.50 | 11.99 | 11.47 | 10.96 | 10.45 | 9.93 | 9.42 | 8.90 | 8.39 |
| 22 | 19.84 | 14.19 | 13.67 | 13.16 | 12.64 | 12.13 | 11.62 | 11.10 | 10.59 | 10.07 | 9.56 |
| 23 | 21.09 | 15.42 | 14.91 | 14.39 | 13.88 | 13.36 | 12.85 | 12.33 | 11.82 | 11.30 | 10.79 |
| 24 | 22.40 | 16.73 | 16.21 | 15.70 | 15.18 | 14.67 | 14.15 | 13.64 | 13.12 | 12.60 | 12.09 |
| 25 | 23.78 | 18.10 | 17.59 | 17.07 | 16.56 | 16.04 | 15.52 | 15.01 | 14.49 | 13.98 | 13.46 |
| 26 | 25.24 | 19.55 | 19.04 | 18.52 | 18.00 | 17.49 | 16.97 | 16.45 | 15.94 | 15.42 | 14.90 |
| 27 | 26.77 | 21.08 | 20.56 | 20.04 | 19.53 | 19.01 | 18.49 | 17.98 | 17.46 | 16.94 | 16.42 |
| 28 | 28.38 | 22.68 | 22.17 | 21.65 | 21.13 | 20.61 | 20.10 | 19.58 | 19.06 | 18.54 | 18.02 |
| 29 | 30.08 | 24.37 | 23.86 | 23.34 | 22.82 | 22.30 | 21.78 | 21.26 | 20.75 | 20.23 | 19.71 |
| 30 | 31.86 | 26.15 | 25.63 | 25.11 | 24.60 | 24.08 | 23.56 | 23.04 | 22.52 | 22.00 | 21.48 |
| 31 | 33.74 | 28.02 | 27.50 | 26.98 | 26.46 | 25.94 | 25.42 | ${ }^{24.90}$ | 24.38 | 23.86 | 23.34 |
| 32 | 35.70 | 29.98 | 29.46 | 28.94 | 28.42 | 27.90 | 27.38 | 26.86 | 26.34 | 25.82 | 25.30 |
| 33 | 37.78 | 32.05 | 31.53 | 31.01 | 30.49 | 29.97 | 29.44 | 28.92 | 28.40 | 27.88 | 27.36 |
| 34 | 39.95 | 34.21 | 33.69 | 33.17 | 32.65 | 32.13 | 31.61 | 31.09 | 30.57 | 30.04 | 29.52 |
| 35 | 42.23 | 36.49 | 35.97 | 35.44 | 34.92 | 34.40 | 33.88 | 33.36 | 32.83 | 32.31 | 31.79 |
| 36 | 44.62 | 38.87 | 38.35 | 37.83 | 37.31 | 36.78 | 36.26 | 35.74 | 35.22 | 34.69 | 34.17 |
| 37 | 47.13 | 41.37 | 40.85 | 40.33 | 39.8 I | 39.28 | 38.76 | 38.24 | 37.71 | 37.19 | 36.67 |
| 38 | 49.76 | 44.00 | 43.47 | 42.95 | 42.43 | 41.90 | 41.38 | 40.86 | 40.33 | 39.81 | 39.29 |
| 39 | 52.51 | 46.74 | 46.22 | 45.70 | 45.17 | 44.65 | 44.12 | $+3.60$ | 43.08 | 42.55 | 42.03 |
| 40 | 55.40 | 49.62 | 49.10 | 48.58 | 48.05 | 47.53 | 47.00 | 46.48 | 45.95 | 45.43 | 44.90 |
| 41 | 58.42 | 52.64 | 52.11 | 51.59 | 51.06 | 50.54 | 50.01 | 49.49 | 48.96 | 48.44 | 47.91 |
| 42 | 61.58 | 55.80 | 55.27 | 54.74 | 54.22 | 53.69 | 53.17 | 52.64 | 52.12 | 51.59 | 51.06 |
| 43 | 64.80 | 59.10 | 58.57 | 58.05 | 57.52 | 56.99 | 56.47 | 55.94 | 55.41 | 54.89 | 54.36 |
| 44 | 68.35 | 62.55 | 62.03 | 61.50 | 60.97 | 60.45 | 59.92 | $59 \cdot 39$ | 58.86 | 58.34 | 57.81 |
| 45 | 71.97 | 66.16 | 65.64 | 65.11 | 64.58 | 64.05 | 63.53 | 63.00 | 62.47 | 61.94 | 61.42 |
| 45 | $\Delta e \times \Delta B$ | +0.76 | $+0.83$ | +0.90 | +0.97 | +1.04 | +I.II | +1.18 | +1.25 | +1.32 | +1.39 |

## REDUCTION OF PSYCHROMETRIC OBSERVATIONS.

METRIC MEASURES
Values of $e=e^{\prime}-0.000660 B\left(t-t^{\prime}\right)\left(1+0.00115 i^{\prime}\right)$
$B=; 60 \mathrm{~mm}$.


| Air Temperature. | RELATIVE HUMIDITY, OR PERCENTAGE OF SATURATION. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 20 | 30 | 40 | 50 | 60 | \% 70 | 80 | 90 | 100 |
| C. | Vapor pressure (millimeters). |  |  |  |  |  |  |  |  |  |
| $-45^{\circ}$ | O. OI | O.OI | 0.02 | 0.02 | 0.c3 | 0.03 | 0.04 | 0.04 | 0.05 | 0.05 |
| 44 | O. OI | O. OI | 0.02 | -. 02 | 0.03 | 0. 0.4 | -. 04 | 0.05 | 0.05 | 0.06 |
| 43 | O. OI | O. OI | 0.02 | 0.03 | 0.03 | 0. 0.4 | c. 05 | 0.05 | -. 06 | 0.07 |
| 42 | O. OI | 0.02 | 0.02 | 0.03 | 0. 0.4 | 0.05 | 0.05 | 0.06 | 0.07 | 0.08 |
| 4 I | 0.01 | 0.02 | c. 03 | 0.03 | O. 64 | 0.05 | 0.06 | 0.07 | -0.08 | 0.09 |
| $-40$ | 0.01 | 0. 02 | 0.03 | 0. 04 | 0.05 | 0.06 | 0. 07 | 0. 08 | 0.09 | O. 10 |
| 39 | O. OI | 0.02 | 0.03 | 0. 04 | 0.05 | 0.06 | 0.08 | 0.00 | -. 10 | O. II |
| 38 | O.OI | 0.02 | 0.04 | 0.05 | 0.06 | 0.07 | 0.08 | c. 10 | O. II | O. 12 |
| 37 | 0.01 | 0.03 | 0.04 | 0.05 | 0.07 | 0.08 | 0.00 | O. 11 | O. 12 | O. 14 |
| 36 | 0.02 | 0.03 | 0.05 | 0.06 | 0.08 | 0.09 | O. I I | O. 12 | O. I4 | O. 15 |
| $-35$ | 0.02 | 0.03 | 0.05 | 0.07 | 0.08 | O. 10 | O. 12 | 0.13 | -. 15 | O. 17 |
| 34 | 0. 02 | 0. 0.4 | 0.06 | 0.08 | 0.09 | O. II | O. I3 | -. 15 | -. 17 | -.19 |
| 33 | 0.02 | 0. 0.4 | 0.06 | 0.08 | 0.10 | -. I 3 | -. 15 | -. 17 | -.19 | -. 21 |
| 32 | 0.02 | 0.05 | 0.07 | 0.09 | O. 12 | -. 14 | -. 16 | -. 19 | 0. 21 | 0. 23 |
| 31 | 0.03 | 0.05 | 0.08 | 0.10 | -. 13 | -. 16 | -. IS | -. 21 | -. 23 | O. 26 |
| $-30$ | 0.03 | 0.06 | 0.09 | O. 12 | O. 14 4 | O. 17 | 0. 20 | 0. 2.5 | -. 26 | O. 29 |
| 20 | 0.03 | 0.06 | -. 10 | O. 13 | -. 16 | -. I9 | 0. 22 | 0. 26 | -. 29 | 0.32 |
| 28 | 0.04 | 0.07 | O. II | -. 14 | -. 18 | 0. 21 | -. 25 | -. 28 | -. 32 | 0.35 |
| 27 | 0.0 .4 | 0.08 | - 12 | -. 16 | 0. 20 | -0. 24 | -. 27 | 0. 31 | -. 35 | 0.39 |
| 26 | 0.04 | 0.09 | -. I3 | O. 17 | 0. 22 | O. 26 | 0. 30 | 0. 35 | -. 39 | 0.43 |
| $-25$ | 0.05 | O. 10 | O. I4 | O. 19 | O. 24 | O. 29 | 0. 34 | -0.3S | 0.43 | -. 48 |
| 24 | 0.05 | O. II | -. I6 | -. 21 | 0. 27 | 0. 32 | 0.37 | -0. 42 | -. 48 | 0. 53 |
| 23 | 0.06 | O. 12 | -. 18 | O. 23 | 0. 29 | 0.35 | 0. 41 | 0. 47 | -. 53 | -. 59 |
| 22 | 0.06 | 0. 13 | -. 19 | -. 26 | 0.32 | 0. 39 | 0.45 | -. 52 | -. $5^{8}$ | 0.65 |
| 2 I | 0.07 | O. 14 | - 21 | -. 28 | 0.36 | -0. 43 | 0. 50 | -. 57 | -. 64 | 0.71 |
| $-20$ | 0.08 | -. 16 | 0. 24 | 0.31 | 0.39 | 0.47 | 0.55 | 0.63 | 0.71 | -. 78 |
| 19 | O. CO | O. I 7 | -. 26 | 0. 34 | 0. 43 | O. 52 | 0.60 | 0.69 | 0. 78 | -. 86 |
| 18 | 0.09 | -. 19 | -. 28 | 0.38 | 0.47 | 0. 57 | 0.66 | -0.76 | 0.85 | 0.95 |
| I 7 | O. 10 | 0. 21 | 0. 31 | 0.42 | 0. 52 | 0. 62 | 0.73 | -. 83 | 0.94 | I. 04 |
| I 6 | O. II | -. 23 | 0. 34 | 0. $4^{6}$ | -0. 57 | 0.69 | 0. So | 0.91 | 1.03 | I. I4 |
| $-15$ | O. 13 | 0. 25 | 0. $3^{8}$ | 0. 50 | 0.63 | 0. 75 | 0.88 | 1. 00 | I. I3 | I. 25 |
| 14 | -. 14 | 0. 27 | 0. 41 | 0. 55 | 0.69 | 0. 82 | 0.06 | 1. 10 | I. 24 | I. 37 |
| I 3 | O. I 5 | 0.30 | 0.45 | 0.60 | 0.75 | 0.90 | 1.05 | I. 20 | I. 35 | I. 50 |
| I 2 | O. 16 | 0.33 | -. 49 | 0.66 | 0.82 | 0.99 | I. I5 | I. 32 | I. 48 | 1. 64 |
| I I | -. 18 | -. 36 | - 54 | 0. 72 | 0.90 | I. 08 | I. 26 | I. 44 | I. 62 | 1. 80 |
| $-10$ | O. 20 | 0.39 | -0. 59 | -. 79 | 0.98 | I. 18 | I. 38 | I. 57 | 1.77 | 1. $9^{6}$ |
| 9 | -. 21 | 0.43 | -. 64 | 0.86 | 1.07 | I. 29 | I. 50 | 1. 72 | I. 93 | 2. 14 |
| 8 | 0. 23 | 0.47 | 0.70 | 0.94 | 1.17 | I. 40 | I. 64 | 1. 87 | 2 . 11 | 2.34 |
| 7 | O. 26 | 0. 51 | 0. 77 | I. 02 | 1. 28 | I. 53 | I. 79 | 2.04 | 2.30 | 2. 55 |
| 6 | -. 28 | 0.56 | 0.83 | I. II | I. 39 | 1. 67 | I. 94 | 2.22 | 2.50 | 2. 78 |
| $-5$ | 0.30 | 0. 60 | 0.91 | I. 21 | I. 51 | I. 8 I | 2.12 | 2.42 | 2. 72 | 3.02 |
| 4 | 0.33 | 0. 66 | 0.99 | I. $3^{2}$ | I. 65 | 1.97 | 2.30 | 2.63 | 2.96 | 3.29 |
| 3 | 0. 36 | 0.72 | I. 07 | I. 43 | I. 79 | 2.15 | 2. 50 | 2.86 | 3.22 | $3 \cdot 58$ |
| 2 | 0. 39 | 0. 78 | I. I 7 | I. 55 | I. 94 | 2.33 | 2.72 | 3.11 | $3 \cdot 50$ | 3.89 |
| I | 0.42 | -0.84 | I. 27 | 1. 69 | 2. I I | 2. 53 | 2.95 | $3 \cdot 38$ | 3.80 | 4.22 |
| $\pm 0$ | 0.46 | 0.92 | I. 37 | I. 83 | 2. 29 | 2.75 | 3.21 | 3.66 | 4. I 2 | $4 \cdot 58$ |
| + I | 0.49 | 0.98 | I. $4^{8}$ | I. 07 | 2.46 | 2.95 | 3.45 | 3.94 | 4.43 | 4.92 |
| 2 | 0. 53 | 1.06 | I. 59 | 2. 12 | 2.65 | 3.17 | 3.70 | 4.23 | 4.76 | 5.29 |
| 3 | 0.57 | I. I 4 | 1. 70 | 2. 27 | 2.84 | 3.41 | 3.98 | $4 \cdot 5.5$ | 5. 1 I | 5.68 |
| 4 | 0.6I | I. 22 | I. 83 | 2.44 | 3.05 | 3.66 | 4.27 | 4.88 | 5.49 | 6.10 |
| $+5$ | 0.65 | 1.3I | I. 96 | 2.62 | 3.27 | 3.92 | 4. $5^{8}$ | 5.23 | 5.89 | 6.54 |

RELATIVE HUMIDITY.
TEMPERATURE CENTIGRADE.

| AirTemperature. | Relative humidity, or percentage of s.ituration. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| C. | Vapor pressure (millimeters). |  |  |  |  |  |  |  |  |  |
| $5^{\circ}$ | 0. 7 | 1. 3 | 2.0 | 2.6 | $3 \cdot 3$ | 3.9 | 4.6 | 5.2 | 5.9 | 6.5 |
| 6 | 0. 7 | 1. 4 | 2.1 | 2.8 | 3.5 | 4.2 | 4.9 | 5.6 | 6.3 | 7.0 |
| 7 | 0.8 | I. 5 | 2.3 | 3.0 | 3.8 | 4.5 | $5 \cdot 3$ | 6.0 | 6.8 | 7.5 |
| 8 | 0.8 | 1. 6 | 2.4 | 3.2 | 4.0 | 4.8 | 5.6 | 6.4 | 7.2 | 8.0 |
| 9 | 0.9 | I. 7 | 2.6 | $3 \cdot 4$ | $4 \cdot 3$ | 5. 2 | 6.0 | 6.9 | 7.7 | 8.6 |
| 10 | 0.9 | 1.8 | 2.8 | $3 \cdot 7$ | 4.6 | $5 \cdot 5$ | 6.4 | $7 \cdot 4$ | 8.3 | 9.2 |
| 11 | 1.0 | 2.0 | 3.0 | 3.9 | 4.9 | 5.9 | 6.9 | 7.9 | 8.9 | 9.8 |
| 12 | I. I | 2. I | 3.2 | 4.2 | $5 \cdot 3$ | 6.3 | $7 \cdot 4$ | 8.4 | 0.5 | 10. 5 |
| 13 | I. I | 2.2 | $3 \cdot 4$ | 4.5 | 5.6 | 6.7 | 7.9 | 9.0 | 10. I | II. 2 |
| 14 | I. 2 | 2.4 | 3.6 | 4.8 | 6.0 | 7.2 | 8.4 | 9.6 | 10.8 | 12.0 |
| 15 | 1.3 | 2.6 | 3.8 | 5.1 | 6.4 | 7.7 | 9.0 | IC. 2 | II. 5 | 12.8 |
| 16 | 1. 4 | 2. 7 | 4.1 | $5 \cdot 5$ | 6.8 | 8.2 | 9.5 | 10.9 | 12.3 | 13.6 |
| 17 | I. 5 | 2.9 | $4 \cdot 4$ | 5.8 | $7 \cdot 3$ | 8.7 | 10.2 | I 1.6 | 13.1 | 14.5 |
| 18 | 1. 5 | 3. I | 4.6 | 6.2 | 7.7 | 9.3 | 10.8 | 12.4 | 13.9 | 15.5 |
| 19 | I. 6 | $3 \cdot 3$ | $4 \cdot 9$ | 6.6 | 8.2 | 9.9 | II. 5 | I3. 2 | 14.8 | 16.5 |
| 20 | I. 8 | 3.5 | $5 \cdot 3$ | 7.0 | 8.8 | 10.5 | 12.3 | 14.0 | 15.8 | 17.5 |
| 21 | 1.9 | $3 \cdot 7$ | 5.6 | 7.5 | 9.3 | II. 2 | 13.1 | 14.9 | 16.8 | 18.7 |
| 22 | 2.C | 4.0 | 6.0 | 7.9 | 9.9 | II. 9 | 13.9 | 15.9 | 17.9 | 19.8 |
| 23 | 2.1 | 4.2 | 6.3 | 8.4 | 10.5 | 12.7 | 14.8 | 16.9 | 19.0 | 2 I . 1 |
| 24 | 2.2 | $4 \cdot 5$ | 6.7 | 9.0 | II. 2 | 13.4 | 15.7 | 17.9 | 20.2 | 22.4 |
| 25 | 2.4 | 4.8 | 7. I | 9. 5 | 11.9 | 14.3 | 16.6 | 19.0 | 21.4 | 23.8 |
| 26 | 2.5 | 5.0 | 7.6 | 10. I | 12.6 | 15.1 | 17.7 | 20.2 | 22.7 | 25.2 |
| 27 | 2.7 | 5.4 | 8.0 | 10. 7 | 13.4 | 16.1 | 18.7 | 21.4 | 24.1 | 26.8 |
| 28 | 2.8 | $5 \cdot 7$ | 8.5 | II. 4 | 14.2 | 17.0 | 19.9 | 22.7 | 25.5 | 28.4 |
| 29 | 3.0 | 6.0 | 9.0 | 12.0 | 15.0 | 18.0 | 21. I | 24.1 | 27.1 | 30. 1 |
| 30 | 3. 2 | 6.4 | 9.6 | 12.7 | 15.9 | 19. I | 22.3 | 25.5 | 28.7 | 31.9 |
| 31 | 3. 4 | 6.7 | 10. 1 | 13.5 | 16.9 | 20.2 | 23.6 | 27.0 | 30.4 | 33.7 |
| 32 | 3. 6 | 7. I | 10.7 | 14.3 | 17.9 | 21.4 | 25.0 | 28.6 | 32.1 | 35.7 |
| 33 | 3.8 | 7.6 | II. 3 | 15.1 | 18.9 | 22.7 | 26.4 | 30.2 | 34.0 | 37.8 |
| 34 | 4.0 | 8.0 | 12.0 | 16.0 | 20.0 | 24.0 | 28.0 | 32.0 | 36.0 | 39.9 |
| 35 | 4.2 | 8.4 | 12.7 | 16.9 | 21. I | 25.3 | 29.6 | 33.8 | 38.0 | 42.2 |
| 36 | 4.5 | 8.9 | 13.4 | 17.8 | 22.3 | 26.8 | 31.2 | 35.7 | 40.2 | 44.6 |
| 37 | 4.7 | 9.4 | 14.1 | 18.9 | 23.6 | 28.3 | 33.0 | 37.7 | 42.4 | 47.1 |
| 38 | 5.0 | 10.0 | 14.9 | 19.9 | 24.9 | 29.9 | 34.8 | 39.8 | 44.8 | 49.8 |
| 39 | $5 \cdot 3$ | 10. 5 | 15.8 | 21.0 | 26.3 | 31.5 | 36.8 | 42.0 | 47.3 | 52.5 |
| 40 | 5. 5 | II. I | 16.6 | 22. 2 | 27.7 | 33.2 | 38.8 | $44 \cdot 3$ | 49.9 | 55.4 |
| 41 | 5.8 | II. 7 | 17. 5 | 23.4 | 29.2 | 35. I | 40.9 | 46.7 | 52.6 | 58.4 |
| 42 | 6.2 | 12.3 | I8. 5 | 2.4 .6 | 30.8 | 36.9 | 43. 1 | 49.3 | 55.4 | 61.6 |
| 43 | 6.5 | 13.0 | 19. 5 | 26.0 | 32.4 | 38.9 | 45.4 | 51.9 | 58.4 | 64.9 |
| 44 | 6.8 | 13.7 | 20. 5 | 27.3 | 34.2 | 41.0 | 47.8 | 54.7 | 61.5 | 68.4 |
| 45 | 7.2 | 14.4 | 21.6 | 28.8 | 36.0 | 43.2 | 50.4 | 57.6 | 64.8 | 72.0 |
| 46 | 7.6 | 15.2 | 22.7 | 30.3 | 37.9 | 45.5 | 53.0 | 60.6 | 68.2 | 75.8 |
| 47 | 8.0 | 15.9 | 23.9 | 31.9 | 39.9 | 47.8 | 55.8 | 63.8 | 71.7 | 79.7 |
| 48 | 8.4 | 16.8 | 25.1 | 33. 5 | 41.9 | 50.3 | 58.7 | 67.1 | 75.4 | 83.8 |
| 49 | 8.8 | 17.6 | 26.4 | $35 \cdot 3$ | 44. I | 52.9 | 61.7 | 70.5 | 79.3 | 88.1 |
| 50 | 9.3 | 18. 5 | 27.8 | 37. I | 46.3 | 55.6 | 64.8 | 74. I | 83.4 | 92.6 |
| 51 | 9.7 | 19.5 | 29.2 | 38.9 | 48.7 | 58.4 | 68.1 | 77.9 | 87.6 | 97.3 |
| 52 | 10. 2 | 20. 4 | 30.7 | 40.9 | 51.1 | 61.3 | 7 7 .6 | 81.8 | 92.0 | 102. 2 |
| 53 | 10.7 II. 3 | 21. 5 | 32.2 33.8 | 42.9 | 53.7 | 64.4 | 75. I | 85.9 | 96.6 | 107.3 |
| 54 | 11.3 | 22.5 | 33.8 | 45. I | 56.3 | 67.6 | 78.9 | 90. I | 101. 4 | I12.7 |
| 55 | II 8 | 23.6 | 35.5 | 47.3 | 59. I | 70.9 | 82.7 | 94.6 | 106.4 | 118.2 |

Table 86.
RATE OF DECREASE OF VAPOR PRESSURE WITH ALTITUDE FOR MOUNTAIN STATIONS.
(According to the empirical formula of Dr. J. Hann.)

$$
\frac{\varepsilon}{\epsilon_{0}}=10-\frac{h}{6_{300}}
$$

$\varepsilon, \epsilon_{0}=$ Vapor pressures at an upper and a lower station respectively.
$h=$ Difference of altitude in meters.

| Difference of Altitude. |  | $\frac{\varepsilon}{\epsilon_{0}}$. | Differense of Altitude. |  | $\frac{e}{e_{0}}$. | Difference of Altitude. |  | $\frac{e}{c_{0}}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Meters. 200 | $\begin{aligned} & \text { Feet. } \\ & 056 \end{aligned}$ | 0.93 | Meters. I 800 | Feet. $5905$ | 0. 52 | Meters. 3.400 | $\begin{aligned} & \text { Feet. } \\ & \text { I } 1155 \end{aligned}$ | O. 29 |
| $+\infty 0$ | I3I 2 | . 86 | 2000 | 0362 | 48 | 3000 | IISII | . 27 |
| 000 | 1968 | . So | 2200 | 7218 | 45 | 3800 | 12407 | . 25 |
| S00 | 2625 | 75 | 2400 | -574 | 42 | 4000 | 13123 | . 23 |
| 1000 | 3281 | 0.60 | 2600 | S530 | 0.30 | +500 | 14764 | O. I9 |
| 1200 | 3937 | . 64 | 2800 | 9186 | . 36 | 5000 | $16+04$ | . I6 |
| 1400 | 4593 | . 60 | 3000 | $08_{4} 2$ | . 33 | 5500 | 18045 | . I3 |
| 1000 | $52+9$ | . 56 | 3200 | 10499 | . 3 I | 6000 | 19685 | . I I |

Table 87. DEPTH OF WATER CORRESPONDING TO THE WEIGHT OF A CYLINDRICAL SNOW CORE 2.655 INCHES IN DIAMETER.
(One-fifth pound equals 1 inch.)

| Weight los. | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. | Inches. |
| 0 | 0.00 | 0.05 | O. IO | O. I5 | 0. 20 | 0. 25 | 0. 30 | 0.35 | 0. 40 | 0.45 |
| . I | -. 50 | -. 55 | -. 60 | -. 65 | -. 70 | -0. 75 | -. So | -. 85 | 0.90 | 0.95 |
| . 2 | I. 00 | 1. 05 | I. 10 | I. I5 | I. 20 | I. 25 | I. 30 | 1.35 | 1. 40 | I. 45 |
| . 3 | I. 50 | 1. 55 | I. 60 | I. 65 | 1. 70 | 1. 75 | I. So | I. 85 | 1. 00 | I. 95 |
| . 4 | 2.00 | 2.05 | 2. 10 | 2. 15 | 2. 20 | 2.25 | 2.30 | 2.35 | 2.40 | 2.45 |
| 5 | 2.50 | 2.55 | 2.60 | 2.65 | 2. 70 | 2. 75 | 2. So | 2. 85 | 2.90 | 2.95 |
| . 6 | 3.00 | 3.05 | 3. 10 | 3.15 | 3.20 | 3. 25 | 3.30 | $3 \cdot 35$ | $3 \cdot 40$ | 3.45 |
| . 7 | 3.50 | 3. 55 | 3.60 | 3.65 | 3. 70 | 3.75 | 3. So | 3.85 | 3.90 | 3.95 |
| . 8 | 4.00 | 4.05 | 4.10 | +.15 | +. 20 | 4. 25 | $+30$ | 4.35 | 4.40 | 4.45 |
| . 9 | 4.50 | +. 55 | + 60 | +. 65 | 4.70 | 4.75 | 4. So | 4.85 | 4.90 | 4.95 |
| 1.0 | 5.00 | 5.05 | 5.10 | 5.15 | 5.20 | 5.25 | $5 \cdot 30$ | $5 \cdot 35$ | $5 \cdot 10$ | 5.45 |
| I. I | 5.50 | 5.55 | 5.60 | 5.65 | 5.70 | 5.75 | 5. So | 5. $\mathrm{S}_{5}$ | 5.90 | 5.95 |
| I. 2 | 6.00 | 6.05 | 6.10 | 6.15 | 6.20 | 6. 25 | 6.30 | 6.35 | 6.40 | 6.45 |
| I. 3 | 6.50 | 6.55 | 6.60 | 6.65 | 6. 70 | 6.75 | 6. So | 6. $\mathrm{S}_{5}$ | 6.90 | 6.95 |
| I. 4 | 7.00 | 7.05 | 7.10 | 7. 15 | 7.20 | 7.25 | 7.30 | 7.35 | $7 \cdot 40$ | $7 \cdot 45$ |
| 15 | 7.50 | 7.55 | 7.60 | 7.65 | 7.70 | 7.75 | 7.80 | 7.85 | 7.90 | 7.95 |
| I. 6 | 8. 00 | 8. 05 | S. 10 | S. 15 | 8. 20 | S. 25 | S. 30 | 8. 35 | 8. 40 | 8.45 |
| I. 7 | S. 50 | 8. 55 | S. 60 | S. 65 | 8. 70 | 8. 75 | 8. 80 | S. $8_{5}$ | 8.90 | 8.95 |
| I. S | 9. 00 | 9.05 | 9.10 | 9.15 | 9. 20 | 9.25 | 9.30 | 9.35 | 9.40 | 9.45 |
| I. 9 | 9. 50 | $9 \cdot 55$ | 9.60 | 9.65 | 9.70 | 9.75 | 9. So | 9. $8_{5}$ | 9.90 | 0.95 |
| 2.0 | 10. 00 | 10.05 | 10. 10 | 10. 15 | 10. 20 | 10. 25 | 10. 30 | 10.35 | 10.70 | 10.45 |
| 2. I | 10. 50 | 10. 55 | 10. 60 | 10.65 | 10. 70 | 10. 75 | Io. So | 10. $\mathrm{S}_{5}$ | 10.00 | 10.95 |
| 2.2 | II $1 . \infty$ | 11.05 | II. 10 | II. 15 | II. 20 | II 1.25 | II. 30 | 11.35 | II 1.40 | 11.45 |
| 2.3 | II. 50 | 11. 55 | 11. 60 | 11.65 | II. 70 | II. 75 | I I . So | 11.85 | II. 90 | II 195 |
| 2.4 | I 2.00 | 12.05 | 12.10 | 12. 15 | 12.20 | 12. 25 | 12.30 | 12.35 | 12.40 | 12.45 |
| 2.5 | I 2.50 | 12. 55 | 12.60 | 12.65 | 12. 70 | I2.75 | 12. So | 12.85 | 12.90 | 12.95 |
| 2.6 | 13.00 | 13.05 | 13.10 | 13.15 | 13.20 | 13.25 | 13.30 | 13.35 | 13.40 | 13.45 |
| 2.7 | 13.50 | I3. 55 | 13.60 | 13.65 | 13.70 | 13. 75 | I3. So | 13.85 | 13.90 | 13.95 |
| 2.8 | 14. 00 | 14.05 | 14. 10 | 14.15 | 14. 20 | 14. 25 | It. 30 | 14.35 | 14.40 | 14.45 |
| 2.9 | 14. 50 | 14.55 | 14.60 | 14.65 | 14.70 | 14.75 | If. So | 14.85 | 14.90 | 14.95 |

Table 88.
DEPTH OF WATER CORRESPONDING TO THE WEICHT OF SNOW OR RAIN COLLECTED IN AN 8-INCH GAGE. (One pound equals 0.5507 inch.)

table 89.
QUANTITY OF RAINFALL CORRESPONDING TO GIVEN DEPTHS.


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$\begin{aligned} g_{\phi} & =97 S .039\left(1+0.005294 \sin ^{2} \phi-0.000007 \sin ^{2} 2 \phi\right) \\ & =080.621\left(1-0.0026 .40 \cos 2 \phi+0.000007 \cos ^{2} 2 \phi\right)\end{aligned}$

| $\phi$ | $g_{\phi}$ | ф | $g_{\phi}$ | $\phi$ | $g_{\phi}$ | $\phi$ | $g_{\phi}$ | $\phi$ | $g_{\phi}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Dynes. |  | Dynes. |  | Dynes. |  | Dynes. | - , | Dynes. |
|  | 978.039 | 2000 | 978.642 | 3700 | 979.908 | $54 \bigcirc 0$ | 981. 422 | 7100 | 982.665 |
| 1 ○ | . 041 | 20 | .661 |  | . 937 |  | . 450 |  | . 684 |
|  | . 045 | 40 | .681 | 40 | . 966 | 40 | . 479 | 40 | . 702 |
| 3 - | . 05.3 | 2100 | 701 | 38 oo | 995 | 55 ○0 | . 507 | 72 oo | . 720 |
| 4 - | . 064 | 20 | 721 | 20 | 980. 024 | 20 | - 535 |  | . 738 |
|  |  | 40 | $74^{2}$ | 40 | . 054 | 40 | - 564 | 40 | . 755 |
| 500 | . 078 | 2200 | 762 | 3900 | . 083 | 56 | - 592 | 73 ○0 | . 772 |
| 20 | . 084 | 20 | . 783 | 20 | -113 | 20 | . 620 |  | . 789 |
| 40 | . 089 | 40 | . 805 | 40 | . 142 | 40 | . 647 | 40 | . 805 |
| 600 | . 095 | 2300 | . 826 | 4000 | 172 | 57 0 | . 675 | 74 ○0 | . 822 |
| 20 | . 102 | 20 | 848 | 20 | 201 |  | . 703 | 20 | 837 |
| 40 | 108 | 40 | 870 | 40 | 231 | 40 | . 730 | 40 | . 853 |
| 700 | 115 | 24 oo | 892 | 4100 | 261 | 58 -0 | . 757 | 75 ○0 | 868 |
| 20 | 12.3 | 20 | . 914 |  | . 291 |  | 784 |  | 883 |
| 40 | 131 | 40 | . 037 | 40 | . 321 | 40 | $8_{11}$ | 40 | . 898 |
| 8 ○ | 139 | 2500 | . 960 | 4200 | 350 | 59 oo | . 838 | 7600 | . 912 |
| 20 | 147 | 20 | . 083 | 20 | . 380 | 20 | . 865 | 20 | . 926 |
| 40 | 156 | 40 | 979.006 | 40 | 410 | 40 | . 891 | 40 | . 940 |
| $9 \bigcirc$ | 165 | 26 oo | -30 | 4300 | 440 | $60 \sim 0$ | . 917 | 77 O | . 953 |
| 20 | 174 | 20 | . 054 | 20 | 471 | 20 | . 943 | 20 | . 966 |
| 40 | 184 | 40 | . 077 | 40 | . 501 | 40 | . 969 | 40 | . 979 |
| 10 00 | 194 | $27 \quad 0$ | 102 | $4+\infty$ | 531 | 6100 | . 995 | 7800 | . 992 |
| 20 | 205 | 20 | 126 | 20 | 561 | 20 | 082.020 |  | 983.004 |
| 40 | 215 | 40 | 151 | 40 | 591 | 40 | . 046 | 40 | . 016 |
| 1100 | . 227 | 28 oo | 175 | 4500 | . 621 | 6200 | . 071 | 7900 | . 027 |
| 20 | . 238 | 20 | 201 | 20 | 651 | 20 | . 096 | 20 | . 039 |
| 40 | 250 | 40 | 226 | 40 | 68 I | 40 | 121 | 40 | . 049 |
| 1200 | . 262 | 2900 | 251 | 4600 | 711 | 63 ○0 | 145 | So oo | . 060 |
| 20 | 274 | 20 | 277 | 20 | 741 | 20 | 160 | 20 | . 070 |
| 40 | 287 | 40 | 302 | 40 | 772 | 40 | 194 | 40 | 080 |
| 1300 | 300 | 30 oo | . 328 | 47 ¢ | 802 | 6400 | 217 | 81 0 | . 090 |
| 20 | 313 | 20 | . 354 | 20 | 832 | 20 | 241 | 20 | . 099 |
| 40 | . 327 | 40 | . 381 | 40 | 862 | 40 | . 265 | 40 | . 108 |
| 1400 | . 341 | 3100 | 407 | 48 ○0 | 892 | 65 co | . 288 | 8200 | . 116 |
| 20 | 355 | 20 | $43+$ | 20 | 922 | 20 | . 311 | 20 | 124 |
| 40 | - 369 | 40 | 460 | 40 | 952 | 40 | . 334 | 40 | .132 |
| 1500 | -384 | 3200 | 487 | $49 \bigcirc 0$ | 981 | 66 oo | . 356 | 8300 | . 140 |
| 20 | . 399 | 20 | 515 | 20 | 98i. OII | 20 | -379 | 20 | . 147 |
| 40 | 415 | 40 | 542 | 40 | 0.41 | 40 | 401 | 40 | . 153 |
| 16 -0 | 430 | 3300 | . 569 | $50 \sim 0$ | 071 | 67 00 | 423 | 84+ 0 | . 160 |
| 20 | 447 | 20 | 597 | 20 | 100 | 20 | 445 | 20 | 166 |
| 40 | 463 | 40 | . 624 | 40 | 130 | 40 | 466 | 40 | . 172 |
| 17 ¢ | 479 | $3+\infty$ | . 652 | 5100 | 160 | 68 oo | 487 | 8500 | 177 |
| 20 | 496 | 20 | . 680 | 20 | I 80 | 20 | . 508 | 20 | 182 |
| 40 | 514 | 40 | . 708 | 40 | 218 | 40 | 528 | 40 | 187 |
| 18 о | 531 | 3500 | . 736 | $52 \times$ | 248 | 69 oo | 549 |  |  |
| 20 | 549 | 20 | . 765 | 20 | 277 | 20 | 560 | S6 00 | 102 |
| 40 | 567 | 40 | 793 | 40 | 306 | 40 | 580 | 8700 | 20.3 |
| 1900 | 585 | 3600 | . 822 | 53 oo | 335 | 70 00 | 608 | 88 00 | 210 |
| 20 | 604 | 20 | 850 | 20 | 364 | 20 | 628 | S9 00 | 215 |
| 40 | 978.623 | 40 | 979.879 | 40 | 981. 393 | 40 | 982.647 | 00 - | 083.217 |

Table 91.
RELATIVE ACCELERATION OF GRAVITY AT DIFFERENT LATITUDES.
Ratio of the acceleration of gravity at sea level for cach ro' of latitude, to its acceleration at latitude $45^{\circ}$.
$\frac{g_{\phi}}{g_{45}}=\mathrm{I}-0.002640 \cos 2 \phi+0.000007 \cos ^{2} 2 \phi$

| Latitude. | $0^{\prime}$ | $10^{\prime}$ | $20^{\prime}$ | $30^{\prime}$ | $40^{\prime}$ | $50^{\prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | 0. 997367 | 0. 997367 | -. 997367 | 0. 907367 | -. 997368 | -. 997368 |
| 1 | . 997369 | . 997369 | . 997370 | 097371 | 997371 | . 997372 |
| 2 | . 997373 | . 997374 | . 997376 | 997377 | . 997378 | . 997380 |
| 3 | . 997381 | . 997383 | . 997385 | . 997387 | . 997388 | . 997390 |
| 4 | . 997393 | . 997395 | . 997397 | . 997399 | . 997402 | . 997404 |
| 5 | 0.997407 | 0. 997410 | 0.997412 | -. 997415 | -. 097418 | -. 99742 I |
| 6 | . 997424 | . 997428 | . 99743 I | . 997434 | . 097438 | . 997441 |
| 7 | . 997445 | . 997449 | . 997453 | . 997456 | . 997460 | . 997465 |
| 8 | . 997469 | . 997473 | . 997477 | . 997482 | . 997486 | . 99749 I |
| 9 | . 997496 | . 997500 | . 997505 | 997510 | 997515 | 997520 |
| 10 | 0. 997525 | 0. 99753 I | -0.997536 | 0. 997541 | -. 997547 | -. 997553 |
| 11 | . 997558 | . 997564 | . 997570 | . 997576 | . 997582 | . 997588 |
| 12 | . 997594 | . 997600 | . 997607 | 997613 | . 997620 | - 997626 |
| 13 | . 997633 | . 997640 | . 997646 | 997653 | . 997660 | . 997667 |
| 14 | . 997674 | . 997682 | . 997689 | 997696 | . 997704 | 09771 I |
| 15 | 0.997719 | 0. 997727 | -. 997734 | 0. 997742 | -. 997750 | -. 997758 |
| 16 | . 997766 | . 997774 | . 997783 | 997791 | . 997799 | . 997808 |
| 17 | . 997816 | . 997825 | . 997833 | 997842 | . 997851 | . 997860 |
| 18 | . 997869 | . 997878 | . 997887 | 997896 | . 997905 | 097915 |
| 19 | . 997924 | 997934 | . 997943 | 997953 | . 997962 | . 097972 |
| 20 | -. 997982 | 0.997992 | -. $99800{ }_{2}$ | -. 998012 | - 0.998022 | -. 998032 |
| 21 | . 908042 | . 998052 | . 998063 | . 998073 | . 90808 | . 998094 |
| 22 | . 998104 | 998115 | . 998 I 26 | 998137 | . 998148 | . 998 I 59 |
| 23 | . 998170 | 998181 | . 998192 | . 998203 | . 998214 | . 998225 |
| 24 | . 998237 | 998248 | . 998260 | 998271 | . 998283 | . 998294 |
| 25 | 0.998306 | -. 998318 | -. 998330 | -. 99834 I | -. 998353 | -. 998365 |
| 20 | . 998377 | . 998389 | . 998402 | . 9984 r4 | . 998426 | . 998438 |
| 27 | . 998451 | . 998463 | . 998476 | . 998488 | . 998501 | . 9985 I 3 |
| 28 | . 998526 | . 998539 | . 99855 I | . 998564 | . 998577 | . 998590 |
| 29 | . 998603 | . 9986 I6 | . 998629 | . 998642 | . 998655 | . 998669 |
|  | -. 998682 | C. 998695 | -. 998708 | -. 998722 | -. 998735 | -. 998749 |
| 3 I | . 998762 | . 998776 | . 998789 | . 998803 | . 998817 | . 998830 |
| 32 | . 998844 | . 998858 | . 998872 | . 998886 | . 998899 | . 998913 |
| 33 | . 998927 | . 998941 | . 998956 | . 998970 | . 998984 | . 998998 |
| 34 | . 999012 | . 999026 | . 99904 I | . 999055 | . 999069 | - 999084 |
| 35 | 0. 999098 | 0.999112 | 0.999127 | -. 999141 | -. 999156 | -. 999170 |
| 36 | . 999185 | . 999199 | . 999214 | . 999229 | . 999243 | . 999258 |
| 37 | . 999273 | . 999288 | . 999302 | . 999317 | . 999332 | . 999347 |
| 38 | . 999362 | . 999377 | . 999392 | . 999406 | . 99942 I | . 999436 |
| 39 | . 999451 | . 999466 | . 999482 | . 999497 | . 999512 | . 999527 |
| 40 | -. 999542 | 0. 999557 | O. $99957^{2}$ | -. 099587 | -. 999602 | -. 999618 |
| $4{ }^{1}$ | . 999633 | . 999648 | . 999663 | . 999678 | . 999694 | . 999709 |
| 42 | . 999724 | . 999739 | . 999755 | . 999770 | . 999785 | . 999801 |
| 43 | . 999816 | . 999831 | . 999847 | . 999862 | . 999877 | . 999893 |
| 44 | . 999908 | .999923 | . 999939 | . 999954 | . 999969 | . 999985 |
| 45 | 1.000000 | I. 000015 | I. 000031 | 1. 000046 | 1. 000061 | 1.000077 |

Table 91.
RELATIVE ACCELERATION OF GRAVITY AT DIFFERENT LATITUDES.
Ratio of the acceleration of gravity at sea level for each $10^{\prime}$ of latitude, to its acceleration at latitude $45^{\circ}$.
$\frac{g_{\phi}}{g_{45}}=\mathrm{I}-0.002640 \cos 2 \phi+0.000007 \cos ^{2} 2 \phi$

| Latitude. | $0^{\prime}$ | $10^{\prime}$ | $20^{\prime}$ | $30^{\prime}$ | $40^{\prime}$ | $50^{\prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 45 | 1. 000000 | I. 000015 | 1.00003 I | I. 000046 | 1.000061 | 1. 000077 |
| 46 | 092 | 108 | 123 | 138 | 153 | 169 |
| 47 | 184 | 200 | 215 | 230 | 246 | 261 |
| 48 | 276 | 291 | 307 | 322 | 337 | 352 |
| 49 | 368 | 383 | 398 | 413 | 428 | 444 |
| 50 | 1. 000459 | I. 000474 | 1. 2000489 | I. 000504 | 1. 000519 | 1. 000534 |
| 51 | 549 | 564 | 579 | 594 | 609 | 624 |
| 52 | 639 | 654 | 669 | 684 | 699 | 713 |
| 53 | 728 | 743 | 758 | 773 | 787 | 802 |
| 54 | SI6 | 831 | 846 | 860 | 875 | 889 |
| 55 | 1. 000904 | 1. 000918 | 1. 000933 | I. 000947 | 1.000961 | 1.000976 |
| 56 | 0990 | 1004 | 1018 | 1033 | 1047 | 1061 |
| 57 | 1075 | 1089 | 1103 | 1117 | 1131 | 1145 |
| 58 | I 159 | 1173 | 1186 | 1200 | 1214 | 1227 |
| 59 | 1241 | 1255 | 1268 | 1282 | 1295 | 1308 |
| 60 | 1. 001322 | I. 001335 | 1. 001348 | 1. 001362 | 1.001375 | 1. 001388 |
| 61 | 1401 | 1414 | 1427 | 1440 | 1453 | 1466 |
| 62 | 1478 | 1491 | 1504 | 1517 | 1529 | 1542 |
| 63 | 1554 | 1567 | 1579 | 1591 | 1604 | 1616 |
| 64 | 1628 | 1640 | 1652 | 1664 | 1676 | 1688 |
| 65 | I. 001700 | 1. 001712 | 1. 001723 | 1. 001735 | I. COI 747 | 1. 001758 |
| 66 | 1770 | 1781 | 1792 | 1804 | 1815 | 1826 |
| 67 | 1837 | 1848 | 1859 | 1870 | 1881 | 1892 |
| 68 | 1903 | 1913 | 1924 | 1935 | 1945 | 1955 |
| 69 | I966 | 1976 | 1986 | 1996 | 2007 | 2017 |
| 70 | 1.002026 | 1. 002036 | 1. 002046 | 1. 002056 | I. 002066 | 1.002075 |
| 71 | 2085 | 2094 | 2104 | 2II3 | 2122 | 2131 |
| 72 | 2140 | 2149 | 2158 | 2167 | 2176 | 2185 |
| 73 | 2194 | 2202 | 2211 | 2219 | 2227 | 2236 |
| 74 | 2244 | 2252 | 2260 | 2268 | 2276 | 2284 |
| 75 | I. 002292 | 1. 002299 | I. 002307 | 1.002314 | :. 002322 | 1. 002329 |
| 76 | - 2336 | 2344 | 2351 | 2358 | 2365 | 2372 |
| 77 | 2378 | 2385 | 2392 | 2398 | 2405 | 2411 |
| 78 | 2418 | 2424 | 2430 | 2436 | 2442 | 2448 |
| 79 | 2454 | 2460 | 2465 | 2471 | 2476 | 2.482 |
| 80 | 1. 002487 | I. 002492 | I. 002497 | 1. 002502 | 1. 002507 | 1.002512 |
| 81 | 2517 | 2522 | 2527 | 2531 | 2536 | 2540 |
| 82 | 2544 | 2548 | 2553 | 2557 | 2561 | 2564 |
| 83 | 2568 | 2572 | 2576 | 2579 | 2582 | 2586 |
| 84 | 2589 | 2592 | 2595 | 2598 | 2601 | 2604 |
| 85 | 1. 002607 | 1. 002609 | 1. 002612 | 1.002614 | 1.002617 | 1.002619 |
| 86 | 2621 | 2623 | 2625 | 2627 | 2629 | 2631 |
| 87 | 2632 | 2634 | 2636 | 2637 | 2638 | 2639 |
| 88 | 26.41 | 2642 | 2643 | 2643 | 2644 | 2645 |
| 89 | 2645 | 2646 | 2646 | 2647 | 2647 | 2647 |
| 90 | I. 002647 |  |  |  |  |  |

SMITHSONIAN TABLES.

LENGTH OF ONE DEGREE OF THE MERIDIAN AT DIFFERENT LATITUDES.

| Latitude. | Meters. | Statute Miles. | Geographlc Miles. <br> $1^{\prime}$ of the Eq. | Latitude. | Meters. | Statute Miles. | Geographic Miles. <br> $1^{\prime}$ of the Eq. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0{ }^{\circ}$ | I 10568.5 | 68.703 | 59.594 | $45^{\circ}$ | 111132.1 | 69.054 | 59.898 |
| 1 | 110568.8 | 68.704 | 59.594 | 46 | III 151.9 | 69.067 | 59.908 |
| 2 | 110569.8 | 68.705 | 59.595 | 47 | III 171.6 | 69.079 | 59.919 |
| 3 | 110571.5 | 68.706 | 59.596 | 48 | III 191. 3 | 69.091 | 59.929 |
| 4 | I IO 573.9 | 68.707 | 59.597 | 49 | II I 210.9 | 69.103 | 59.940 |
| 5 | I 10577.0 | 68.709 | 59.598 | 50 | III 230.5 | 69.115 | 59.95I |
| 6 | 110580.7 | 68.71 I | 59.600 | 5 I | I I I 249.9 | 69.127 | 59.961 |
| 7 | I 10585.1 | 68.714 | 59.603 | 52 | I I I 269.2 | 69.139 | 59.972 |
| 8 | 110590.2 | 68.717 | 59.606 | 53 | I II 288.3 | 69.151 | 59.982 |
| 9 | I 10 595.9 | 68.72 I | 59.609 | 54 | III 307.3 | 69.163 | 59.992 |
| 10 | 110602.3 | 68.725 | 59.612 | 55 | III 326.0 | 69.175 | 60.002 |
| II | I 10609.3 | 68.729 | 59.616 | 56 | I I I 344.5 | 69.186 | 60.012 |
| 12 | 110617.0 | 68.734 | 59.620 | 57 | I I I 362.7 | 69. 198 | 60.022 |
| 13 | I 10625.3 | 68.739 | 59.625 | 5 S | II 138 So .7 | 69.209 | 60.032 |
| 14 | I 10634.2 | 68.745 | 59.629 | 59 | I II 398.4 | 69.220 | 60.041 |
| 15 | I Io 643.7 | 68.751 | 59.634 | 60 | III 415.7 | 69.230 | 60.051 |
| 16 | I 10653.8 | 68.757 | 59.640 | 61 | III 432.7 | 69.241 | 60.060 |
| 17 | I 10664.5 | 68.763 | 59.646 | 62 | II I 449.4 | 69.251 | 60.069 |
| 18 | I 10675.7 | 68.770 | 59.652 | 63 | I I 1465.7 | 69.261 | 60.077 |
| 19 | I 10687.5 | 68.778 | 59.658 | 64 | II I 48 r .5 | 69.271 | 60.086 |
| 20 | I Io 699.9 | 68.786 | 59.665 | 65 | I I I 497.0 | 69.281 | 60.094 |
| 21 | I10712.8 | 68.794 | 59.672 | 66 | III 512.0 | 69.290 | 60.102 |
| 22 | I 10726.2 | 68.502 | 59.679 | 67 | I I I 526.5 | 69.299 | 60.110 |
| 23 | I 10740.1 | 68.810 | 59.686 | 68 | II 1540.5 | 69.308 | 60.118 |
| 24 | I 10754.4 | 68.819 | 59.694 | 69 | I I 1554.1 | 69.316 | 60.125 |
| 25 | I 10 769.2 | 68.829 | 59.702 | 70 | III 567.1 | 69.324 | 60.132 |
| 26 | 1 10 7 S 4.5 | 68.838 | 59.710 | 71 | II I 579.7 | $69.33^{2}$ | 60. 139 |
| 27 | 110800.2 | 68.848 | 59.719 | 72 | III 591.6 | 69.340 | 60.145 |
| 28 | ı 10816.3 | 68.858 | 59.727 | 73 | 111603.0 | 69.347 | 60.151 |
| 29 | 110832.8 | 68.868 | 59.736 | 74 | 111613.9 | 69.354 | 60.157 |
| 30 | I 10 849.7 | 68.879 | 59.745 | 75 | 111624.1 | 69.360 | 60.163 |
| 31 | I 10866.9 | 68.889 | 59.755 | 76 | III 633.8 | 69.366 | 60.168 |
| 32 | 110884.4 | 68.900 | 59.764 | 77 | III 642.8 | 69.372 | 60.173 |
| 33 | 110902.3 | 68.91 I | 59.774 | 78 | III 651.2 | 69.377 | 60.177 |
| 34 | 110920.4 | 68.923 | 59.784 | 79 | III 659.0 | 69.382 | 60.182 |
| 35 | 110938.8 | 68.934 | 59.794 | 80 | III 666.2 | 69.386 | 60.186 |
| 36 | 110957.4 | 68.946 | 59.804 | SI | III 672.6 | 69.390 | 60.189 |
| 37 | 110976.3 | 68.957 | 59.814 | 82 | III 678.5 | 69.394 | 60.192 |
| 38 | 110995.3 | 68.969 | 59.824 | 83 | II I 683.6 | 69.397 | 60.195 |
| 39 | III OI4.5 | 68.981 | 59.834 | 84 | In I 688. 1 | 69.400 | 60.197 |
| 40 | 111033.9 | 68.993 | 59.845 | 85 | III 691.9 | 69.402 | 60.199 |
| 4 I | 111053.4 | 69.005 | 59.855 | 86 | II I 695.0 | 69.404 | 60.201 |
| 42 | 111073.0 | 69.017 | 59.866 | 87 | III 697.4 | 69.405 | 60.202 |
| 43 | 111092.6 | 69.029 | 59.876 | 88 | III 1699.2 | 69.407 | 60.203 |
| 44 | III II2.4 | 69.042 | 59.887 | 89 | III 700.2 | 69.407 | 60.204 |
| 45 | III 132.1 | 69.054 | 59.898 | 90 | III 700.6 | 69.407 | 60.204 |

8mithsonian Tables.

## Table 93.

LENGTH OF ONE DEGREE OF THE PARALLEL AT DIFFERENT LATITUDES.

| Latilude. | Meters. | Statute Miles. | Geographic Miles. <br> $1^{\prime}$ of the Eq. | Latitude. | Meters. | Statute Miles. | Geographic Miles. <br> $I^{\prime}$ of the Eq. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | I I I 32 I .9 | 69.171 | 60.000 | $45^{\circ}$ | 78850.0 | 48.995 | 42.498 |
| 1 | 1 II 305.2 | 69.162 | 59.991 | 46 | 77466.5 | 48. 135 | 41.753 |
| 2 | I I I 254.6 | 69.130 | 59.964 | 47 | 76059.2 | 47.261 | 40.994 |
| 3 | 111170.4 | 69.078 | 59.918 | 48 | 74628.5 | 46.372 | 40.223 |
| 4 | I I I O52.6 | 69.005 | 59.855 | 49 | 73174.9 | 45.469 | $39.44{ }^{\circ}$ |
| 5 | I IO 901.2 | 68.911 | 59.773 | 50 | 71698.9 | 44.552 | 38.644 |
| 6 | I 10716.2 | 68.796 | 59.673 | 5 I | 70200.8 | 43.621 | 37.837 |
| 7 | I 10497.7 | 68.660 | 59.556 | 52 | 68681.1 | 42.676 | 37.018 |
| 8 | I 10245.8 | 68.593 | 59.420 | 53 | 67140.3 | 41.710 | 36.187 |
| 9 | 109960.5 | 68.326 | 59.266 | 54 | 65578.8 | 40.749 | 35.346 |
| 10 | 109641.9 | 68.128 | 59.095 | 55 | 63997.1 | 39.766 | 34.493 |
| II | 109 290. 1 | 67.909 | 58.905 | 56 | 62395.7 | 38.771 | 33.630 |
| 12 | Io8 905.2 | 67.670 | 58.697 | 57 | 60775.1 | 37.764 | 32.757 |
| 13 | IoS 457.3 | 67.411 | $5 \mathrm{S.472}$ | 58 | 59135.7 | 36.745 | 31.873 |
| 14 | 108036.6 | 67.131 | 58.229 | 59 | 5747 S. I | 35.715 | 30.979 |
| 15 | 107553.1 | 66.830 | 57.969 | 60 | 55802.8 | 34.674 | 30.076 |
| 16 | 107037.0 | 66.510 | 57.690 | 61 | 54 I10.2 | 33.622 | 29.164 |
| 17 | 106488.5 | 66.169 | 57.395 | 62 | 52400.9 | 32.560 | 28.243 |
| 18 | 105907.7 | 65.808 | 57.082 | 63 | 50675.4 | 31.488 | 27.313 |
| 19 | IO5 294.7 | 65.427 | 56.751 | 64 | 48934.3 | 30.406 | 26.374 |
| 20 | 104 649.8 | 65.026 | 56.404 | 65 | 47 178.0 | 29.315 | 25.428 |
| 21 | 103973.2 | 64.606 | 56.039 | 66 | 45 407. I | $2 \mathrm{S.215}$ | 24.473 |
| 22 | $103265 . \mathrm{C}$ | 64.166 | 55.657 | 67 | 43622.2 | 27.106 | 23.51 I |
| 23 | IO2 525.4 | 63.706 | 55.259 | 68 | 41823.8 | 25.988 | 22.542 |
| 24 | IOI 754.6 | 63.227 | 54. 4 $_{43}$ | 69 | 40012.4 | 2.4 .862 | 21.566 |
| 25 | 100 953.6 | 62.729 | 54.41 I | 70 | 38 ISS.6 | 23.729 | 20.583 |
| 26 | 100 I 20.6 | 62.212 | 53.963 | 71 | 36353.0 | 22.589 | 19.593 |
| 27 | 99257.8 | 61.676 | 53.498 | 72 | 34506.2 | 21.441 | 18.598 |
| 28 | 98364.8 | 61.121 | 53.016 | 73 | 32648.6 | 20.287 | 17.597 |
| 29 | 97441.9 | 60.548 | 52.519 | 74 | 30780.9 | 19.126 | 16.590 |
| 30 | 96459.3 | 59.956 | 52.006 | 75 | 28903.6 | 17.960 | 15.578 |
| 31 | $\bigcirc 5507.3$ | 59.345 | 51.476 | 76 | 27017.4 | 16.788 | 14.562 |
| 32 | 94496.2 | 58.717 | 50.93 I | 77 | 25122.8 | 15.611 | 13.541 |
| 33 | 93.456 .3 | 58.07 I | 50.371 | 78 | 23220.4 | 14.428 | 12.515 |
| 34 | 92387.9 | 57.407 | 49.795 | 79 | 21310.8 | 13.242 | 11.486 |
| 35 | 91 291.3 | 56.726 | 49.204 | 80 | 19394.6 | 12.051 | 10.453 |
| 36 | 90166.8 | 56.027 | 48.598 | SI | 17472.4 | 10.857 | 9.417 |
| 37 | 89014.8 | 55.311 | 47.977 | 82 | I5 544.7 | 9.659 | S. 378 |
| 3 S | 87835.6 | 54.578 | 47.34 I | 83 | 13612.2 | 8.458 | 7.337 |
| 39 | S6629.6 | 53.829 | 46.691 | S4 | II 675.5 | 7.255 | 6.293 |
| 40 | S5 397.0 | 53.063 | 46.027 | 85 | 9735.1 | 6.049 | 5.247 |
| 4 I | St 138.4 | 52.28 I | 45.349 | 86 | 7791.7 | 4.84 I | 4.200 |
| 42 | 82854.0 | 51.483 | 44.656 | 87 | 5845.9 | 3.632 | 3.151 |
| 43 | SI 544.2 | 50.669 | 43.950 | 88 | 3898.3 | 2.422 | 2. IOI |
| 44 | So 209.4 | 49.840 | 43.23 I | 89 | I 949.4 | 1.2II | 1.051 |
| 45 | 78550.0 | 48.995 | 42.498 | 90 | 0.0 | 0.000 | 0.000 |


| $\begin{aligned} & \text { Declination } \\ & \text { of } \\ & \text { one Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0^{\circ}$ | $5^{\circ}$ | $10^{\circ}$ | $15^{\circ}$ | $20^{\circ}$ | $25^{\circ}$ | $30^{\circ}$ | $35^{\circ}$ | $40^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $-23^{\circ} 27^{\prime}$ | 127 | II 50 | II 32 | II I4 | 10 55 | 1035 | 1013 | 948 | 919 |
| 2320 | 127 | II 50 | II 32 | II 14 | IO 56 | IO 36 | 1014 | 949 | 920 |
| -23 0 | 127 | II 50 | II 33 | II 15 | Io 57 | 1037 | 1015 | 951 | 923 |
| -2240 | 127 | II 50 | II 33 | 1116 | 1058 | 1038 | 1017 | 953 | 926 |
| 2220 | 127 | II 5I | 1134 | I 17 | IO 59 | 1040 | 1019 | 955 | 929 |
| 22 O | 127 | II 5I | II 34 | 1118 | II 0 | 10 41 | 1020 | 958 | 931 |
| -2140 | 127 | II 51 | 1135 | II 19 | II | 10 43 | 1022 | 100 | 934 |
| -21 20 | 127 | II 52 | II 35 | II 19 | II | 1044 | 1024 | 10 | 937 |
| 210 | 127 | II 52 | $\begin{array}{ll}\text { II } & 36\end{array}$ | II 20 | II 4 | 1046 | 1026 | 10 4 | 940 |
| -2040 |  | II 52 | II 37 | II 21 | II | 1047 | 1028 | 106 | 942 |
| -20 20 | 127 | II 52 | 1137 | II 22 | II 6 | IO 49 | 1029 | 108 | 945 |
| 20 O | 127 | 1153 | II 38 | 1123 | II 7 | Io 50 | 1031 | Io II | 947 |
| - 1940 | 127 | II 53 | 1138 | II 23 | II 8 | 1051 | 1033 | 10 I3 | 950 |
| - I9 20 |  | II 53 | II 39 | II 24 | II 9 | Io 53 | 10 35 | $10 \quad 15$ | 953 |
| $-190$ | 127 | II 53 | II 39 | II 25 | II 10 | IO 54 | 1037 | 10 17 | 955 |
| -1840 | 127 | II 54 | II 40 | II 26 | II II | Io 55 | 1038 | $10 \quad 19$ | 958 |
| - IS 20 | 127 | II 54 | 1140 | 1127 | II 12 | 1057 | 1040 | 1021 | 101 |
| $-180$ | 127 | II 54 | II 41 | II 28 | II 13 | IO 58 | 1042 | 1023 | 103 |
| -1740 | 127 | II 54 | 1141 | 1128 | II I4 | 1059 | 1043 | IO 26 |  |
| -1720 | 127 | II 55 | II 42 | II 29 | II 15 | II I | IO 45 | 1028 | 108 |
| $-170$ | 127 | II 55 | II 42 | II 30 | II 16 | II 2 | 10 47 | 1030 | Io Io |
| -1640 | 127 | II 55 | II 43 | II 31 | 1117 | II 4 | IO 49 | 1032 | 10 I3 |
| 1620 | 127 | II 55 | II 43 | 1131 | II 18 | II 5 | 1050 | IO 34 | 10 16 |
| -16 0 | 127 | II 56 | II 44 | II 32 | II 19 | II | Io 52 | 10 36 | IO 18 |
| $-1540$ | 127 | II 56 | II 44 | II 33 | II 20 | II 8 | 1053 | 1038 | 1020 |
| - I5 20 | 127 | II 56 | II 45 | I I 34 | II 21 | II 9 | Io 55 | 1040 | 1023 |
| - I5 0 | 127 | II 56 | II 45 | II 34 | II 22 | II 10 | IO 57 | 10 42 | 1025 |
| -1440 | 127 | II 57 | II 46 | II 35 | II 23 | II II | IO 59 | IO 44 | 10 28 |
| -14 20 | 127 | II 57 | II 46 | II 36 | II 25 | 1113 | II 0 | 10 46 | 1030 |
| - I4 o | 127 | II 57 | II 47 | II 37 | II 26 | II 14 | II | 1048 | 10 32 |
| -1340 | 127 | II 57 | II 47 | II 37 | II 27 | II 16 | II 4 | 1050 | 1035 |
| - 1320 | 7 | II 58 | II 48 | II 38 | II 28 | 1117 | II 5 | 1052 | 10 37 |
| $-130$ | 127 | II $5^{8}$ | II $4^{8}$ | II 39 | II 29 | II I8 | II 7 | Io 54 | 10 40 |
| - 1240 | 127 | II 58 | II 49 | II 40 | II 30 | II 19 | II 8 | 10 56 | 1042 |
| 1220 | 127 | II 58 | II 49 | II 40 | II 31 | II 2I | II 10 | 10 58 | IO 44 |
| 120 | 127 | II 58 | II 50 | II 41 | II 32 | II 22 | II II | II 0 | 1047 |
| - 1140 | 127 | II 59 | II 50 | II 42 | II 33 | II 23 | II 13 | II 2 | 10 49 |
| - II 20 | 127 | II 59 | II 51 | II 43 | II 34 | II 25 | II I5 | II 4 | Io 52 |
| I 10 | 127 | II 59 | 1151 | II 43 | II 35 | II 26 | II 16 | II 6 | 1054 |
| - 1040 | 127 | II 59 | II 52 | II 44 | II 36 | 1127 | 11 IS | II 8 | 10 56 |
| - 1020 | 127 | 120 | II 52 | II 45 | II 37 | II 28 | II 20 | II Io | Io 59 |
| - 100 | 127 | 120 | II 53 | II 46 | II 38 | II 30 | II 21 | II 12 | II I |
| - 940 | 127 | 120 | II 53 | II 46 | II 39 | II 31 | II 23 | II 14 | II 3 |
| - 920 | 127 | 120 | II 54 | II 47 | II 40 | 1132 | II 24 | II 16 | $\begin{array}{ll}\text { II } & 5\end{array}$ |
| - 90 | 127 | 12 | II 54 | II 47 | II 41 | II 34 | II 26 | 1117 | II S |
| - 840 | $\begin{array}{ll}12 & 7 \\ \\ 12 & 7\end{array}$ | 12 I | II 55 | II 48 | II 42 | II 35 | II 28 | II 19 | II 10 |
| -- 820 | 127 | 12 | II 55 | II 49 | II 43 | II II | II 29 | II 2I | II 12 |
| - 80 | 127 | 12 | II 56 | II 50 | II 44 | 1137 | II 3I | II 23 | II 14 |

## Table 94.

DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of } \\ & \text { the Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $42^{\circ}$ | $44^{\circ}$ | $46^{\circ}$ | $48^{\circ}$ | $50^{\circ}$ | $52^{\circ}$ | $54^{\circ}$ | $56^{\circ}$ | $58^{\circ}$ | $60^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $-23^{\circ} 27^{\prime}$ | 97 | 853 | 835 | 822 | 84 | 744 | 722 | 656 | 627 | 552 |
| $-2320$ | 98 | S 54 | 839 | 823 | 85 | 745 | 724 | 655 | 629 | 554 |
| $-230$ | 9 II | 858 | 843 | 828 | 8 10 | 750 | 729 | 74 | 636 | 62 |
| -22 40 | 914 | 9 I | 846 | 831 | 814 | 755 | 734 | 7 10 | 643 |  |
| -22 20 | 917 | 94 | 850 | 835 | 8 I8 | 8 \% | 739 | 716 | 649 | 617 |
| 22 | 920 | 97 | 853 | 838 | 822 | S 4 | 744 | 722 | 655 | 625 |
| -2140 | 923 | 9 IO | S 57 | S 42 | 826 | $8 \quad 9$ | 749 | 727 | 7 | 632 |
| -21 20 | 926 | 9 I3 | 9 I | 846 | S 30 | 813 | 754 | 732 | 7 S | 638 |
| - 21 | 92 S | 917 | 94 | 850 | 834 | 8 IS | 759 | 738 | 714 | 646 |
| $-2040$ | 931 | 920 | 97 | 853 | 838 | 822 | 84 | 743 | 720 | 652 |
| $-2020$ | 934 | 923 | 9 II | ¢ 57 | S 42 | 826 | 8 8 | 749 | 725 | 659 |
| - 200 | 937 | 926 | 914 | 9 I | 846 | 831 | 8 I3 | 754 | 731 | 75 |
| $-1940$ | 940 | 929 | 9 I7 | 94 | 850 | 835 | 8 I8 | 759 | 737 | 712 |
| -19 20 | 943 | 932 | 920 | 97 | 854 | 839 | 823 | 84 | 743 | 7 I8 |
| - 190 | 946 | 9. 35 | 924 | 9 II | 858 | 843 | 827 | 89 | 748 | 725 |
| $-1840$ | 948 | 93 S | 927 | 915 | 92 | 847 | S 32 | 8 I 4 | 754 | 731 |
| - I8 20 | 95 I | 94 I | 930 | 9 I9 | 96 | 852 | 836 | S 19 | 759 | 737 |
| $-180$ | 954 | 944 | 934 | 922 | 9 10 | 856 | S 41 | 824 | 85 | 743 |
| -1740 | 956 | 947 | 937 | 925 | 9 I3 | 90 | S 45 | 829 | 8 ı 10 | 749 |
| -1720 | 959 | 950 | 940 | 929 | 917 | 94 | 850 | 834 | 815 | 755 |
| $-170$ | IO 2 | 953 | 943 | 932 | 921 | 98 | 854 | 838 | 820 | 8 I |
| - 1640 | IO 5 | 956 | 946 | 935 | 925 | 9 I2 | 858 | 843 | 826 | 86 |
| - 1620 | $10 \quad 7$ | 959 | 949 | 939 | 928 | 916 | 92 | S 47 | 831 | 8 I2 |
| 16 o | 10 IO | IO I | 952 | 943 | 932 | 920 | 97 | 852 | 836 | 817 |
| -- 1540 | 1012 | IO 4 | 955 | 946 | 935 | 924 | 9 II | 857 | 841 | 823 |
| -- I5 20 | 10 I5 | 107 | 958 | 949 | 939 | 928 | 9 I5 | 92 | 846 | 829 |
| -- 15 o | 10 IS | 1010 | 10 I | 952 | 943 | 931 | 919 | 96 | 85 I | 834 |
| $-1440$ | 1020 | 1013 | IO 4 | 956 | 946 | 935 | 923 | 9 II | 856 | 840 |
| - I4 20 | IO 23 | 1016 | 10 7 | 959 | 949 | 939 | 928 | 9 I5 | 9 I | 845 |
| $\rightarrow$ I4 0 | IO 26 | Io I9 | 1010 | IO 2 | 953 | 943 | 932 | 919 | 96 | 850 |
| $-1340$ | 10 28 | 1021 | 1013 | 105 | 956 | 947 | 936 | 924 | 9 II | 856 |
| - I3 20 | 1031 | 1024 | 1016 | Io S | 100 | 950 | 940 | 928 | 916 | 9 I |
| - I3 0 | Io 33 | IO 26 | Io I9 | IO II | 103 | 954 | 944 | 933 | 920 | 96 |
| $-1240$ | 10 36 | 1029 | 1022 | 1015 | 107 | 95 S | 948 | 937 | 925 | 9 II |
| - 1220 | Io 38 | 10 32 | 1025 | 10 I 8 | 10 IO | 10 I | 952 | 94 I | 930 | 917 |
| - 120 | 104 I | IO 35 | 1028 | 1021 | 1013 | 105 | 956 | 946 | 935 | 922 |
| - 1140 | Io 44 | Io 38 | 1031 | IO 25 | 1017 | IO 9 | 10 O | 950 | 939 | 927 |
| - II 20 | Io 46 | 1040 | Io 34 | 1028 | 1020 | 1013 | IO 4 | 955 | 944 | 932 |
| - II | IO 49 | Io 43 | 10 37 | 1031 | 1023 | 10.16 | 108 | 959 | 949 | 937 |
| $-1040$ | 1051 | 1046 | 1040 | 1034 | IO 27 | 1019 | IO 12 | 103 | 953 | 942 |
| - 1020 | 10 53 | Io 49 | 1043 | 10 37 | 1031 | 1023 | 1016 | 107 | 958 | 947 |
| - 100 | IO 56 | 10 51 | 1046 | 1040 | 1034 | 1027 | 1019 | 10 II | IO 3 | 952 |
| - 940 | IO 59 | 1054 | 1049 | 1043 | 1037 | 1031 | 1023 | 1016 | IO 7 | 957 |
| - 920 | II 1 | 1056 | 10 $5^{2}$ | 1046 | 10 40 | Io 34 | 10 27 | 1020 | 10 II | 102 |
| - 90 | II 3 | IO 59 | IO 55 | Io 49 | 1044 | Io 37 | 10 3r | 1024 | 1016 | 107 |
| - 840 | II 6 | II 2 | IO 57 | IO 52 | 1047 | 1041 | 1034 | 1028 | 1020 | IO II |
| - S 20 | II 8 | II 4 | II 0 | 1055 | 1050 | 10 44 | Io 38 | IO 32 | 1025 | 1016 |
| - 80 | 1110 | II 7 | II 3 | Io 58 | 10 53 | 1048 | 10 42 | 10 36 | IO 29 | 1021 |

DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of of } \\ & \text { the Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0^{\circ}$ | $5^{\circ}$ | $10^{\circ}$ | $15^{\circ}$ | $20^{\circ}$ | $25^{\circ}$ | $30^{\circ}$ | $35^{\circ}$ | $40^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. II 50 | h. m. II 44 | $\begin{array}{ll} \text { h. } & \mathrm{m} . \\ \text { II } & 37 \end{array}$ | $\begin{aligned} & \mathrm{h} . \mathrm{m} . \\ & \text { II } 3 \mathrm{I} \end{aligned}$ | $\begin{array}{ll} \text { h. } & \mathrm{m} . \\ \text { II } & 23 \end{array}$ | $\begin{array}{ll} \mathrm{h} . & \mathrm{m} . \\ \text { II } & 14 \end{array}$ |
| $-8^{\circ} 0^{\prime}$ | 127 | 12 I | II 55 | II 50 | $\text { II } 44$ |  |  | $\begin{array}{lll}11 & 23 \\ \text { II } & 25\end{array}$ | $\begin{array}{ll}\text { II } & 14 \\ \text { II } & 17\end{array}$ |
| - 740 | 127 | 12 I | $\begin{array}{ll}\text { II } & 56 \\ \text { II } & 56\end{array}$ | $\begin{array}{ll}\text { II } & 50 \\ \text { II } & 5\end{array}$ | $\begin{array}{ll}\text { II } & 45 \\ \text { I I } & 46\end{array}$ | $\begin{array}{ll}\text { II } & 3 \\ \text { II } & 40\end{array}$ | $\begin{array}{ll}\text { II } & 32 \\ \text { II } & 34\end{array}$ | II 25 II 27 | $\begin{array}{ll} \text { II } 17 \\ \text { II } & 19 \end{array}$ |
| -720 | 127 | 12 I | $\begin{array}{ll}\text { II } & 56 \\ \text { II } & 57\end{array}$ | $\begin{array}{ll}\text { II } & 5 \\ \text { II } & 52\end{array}$ | II 46 II 47 | $\begin{array}{ll}\text { II } & 40 \\ \text { II } & 41\end{array}$ | $\begin{array}{lll}11 & 34 \\ \text { II } & 35\end{array}$ | II 27 II 29 | $\begin{array}{lll}\text { II } & 19 \\ \text { II } & 22\end{array}$ |
| $-70$ | 127 | 122 | II 57 | II 52 | $\begin{array}{ll}11 & 47 \\ \text { II } & 48\end{array}$ | $\begin{array}{ll}\text { II } & 41 \\ \text { II } & 42\end{array}$ | $\begin{array}{lll}11 & 35 \\ \text { II } & 37\end{array}$ | $\begin{array}{ll}11 & 29 \\ \text { II } & 31\end{array}$ | $\begin{array}{ll}11 & 24\end{array}$ |
| -640 | 127 | 122 | $\begin{array}{ll}11 & 57 \\ \text { II } & 58\end{array}$ | $\begin{array}{ll}\text { II } & 53 \\ \text { II } & 53\end{array}$ | II 48 II 49 | $\begin{array}{ll}\text { II } & 42 \\ \text { II } & 43\end{array}$ | II 37 <br> II 3 | $\begin{array}{ll}\text { II } & 31 \\ \text { II } & 32 \\ \text { II }\end{array}$ | $\begin{array}{lll}\text { II } & 24 \\ \text { II } & 26\end{array}$ |
| -6 20 | 127 | 122 | $\begin{array}{ll}\text { II } & 58 \\ \text { II } & 5\end{array}$ | $\begin{array}{lll}\text { II } & 53 \\ \text { II } & 54\end{array}$ | $\begin{array}{lll}\text { II } & 49 \\ \text { II } & 50\end{array}$ | $\begin{array}{ll}\text { II } & 43 \\ \text { II } 45\end{array}$ | $\begin{array}{ll}\text { II } & 3 \\ \text { II } & 40\end{array}$ | $\begin{array}{ll}\text { II } & 32 \\ \text { II } & 34\end{array}$ | II 2 S |
| -6 o | 127 | 122 | II $5^{8}$ | II 54 | II 50 | $\begin{array}{lll}\text { II } & 45 \\ \text { II } & 46\end{array}$ | $\begin{array}{ll}11 & 40 \\ \text { II } 41\end{array}$ | $\begin{array}{lll}\text { II } & 34 \\ \text { II } & 36\end{array}$ |  |
| -5 40 | 127 | 123 | $\begin{array}{ll}\text { II } 59 \\ \text { II } & 59\end{array}$ | II 55 | II 51 II 52 | II 46 II 47 | $\begin{array}{lll}11 & 41 \\ \text { II } 43\end{array}$ | $\begin{array}{ll}11 & 36 \\ \text { II } & 3 \\ 8\end{array}$ | II II 3 |
| - $5^{20}$ | 127 | $\begin{array}{ll}12 & 3 \\ 12 & \end{array}$ | $\begin{array}{ll}11 & 59 \\ \text { I2 }\end{array}$ | $\begin{array}{ll}\text { II } & 55 \\ \text { II } & 56\end{array}$ | II 52 II 53 | $\begin{array}{ll}\text { II } & 47 \\ \text { I } 149\end{array}$ | $\begin{array}{ll}11 & 43 \\ \text { II } 44\end{array}$ | II 40 | II 35 |
| -5 | 127 | 123 | 120 | II 56 | II 53 | II 49 II 50 | $\begin{array}{ll}\text { II } & 44 \\ \text { II } & 46\end{array}$ |  | $\begin{array}{ll}11 & 37\end{array}$ |
| -4 40 | 127 | 123 | 12 O | II 57 II 58 | $\begin{array}{ll}\text { II } & 54 \\ \text { II } & 55\end{array}$ | $\begin{array}{ll}\text { II } & 50 \\ \text { II } & 51\end{array}$ | $\begin{array}{ll}\text { II } & 46 \\ \text { II } & 47\end{array}$ | II 42 II 44 | II 37 II 40 |
| $-420$ | 127 | 124 | $\begin{array}{ll}\text { I2 } & 1 \\ 12 & 1\end{array}$ | $\begin{array}{ll}\text { II } & 5 \\ \text { II } & 58\end{array}$ | I 155 II 56 | $\begin{array}{ll}\text { II } & 51 \\ \text { II } & 52\end{array}$ | $\begin{array}{ll}11 & 47 \\ \text { II } 49\end{array}$ | II 46 | II $4^{2}$ |
| -4 0 | 127 | 124 | 12 I | II $5^{8}$ | II 56 | II 52 | 1149 | 1146 | 1142 |
| -340 | 127 | 124 | 122 | II 59 | II 57 | 1153 | II 51 | II 47 | II 44 II 46 |
| -320 | 127 | 124 | 122 | 120 | II $5{ }^{\text {S }}$ | II 55 II 56 | $\begin{array}{lll}\text { II } & 52 \\ \text { II } & 54\end{array}$ | $\begin{array}{ll}\text { II } & 49 \\ \text { II } & 51\end{array}$ | $\begin{array}{ll}11 & 46 \\ \text { II } 49\end{array}$ |
| -30 | 127 | 125 | 123 | 12 I | II 58 | II 56 | II 54 | II 51 |  |
| -2 40 | 127 | 125 | 123 | 12 | II 59 | II 5 S | II 55 | II 53 |  |
| -2 20 | 127 | 125 | 124 | 12 2. | 120 | II 59 | II 157 | I I 55 <br> 15  | $\begin{array}{ll}\text { II } & 53 \\ \text { II } & 55\end{array}$ |
| $-20$ | 127 | 125 | 124 | 123 | 12 I | 120 | II 55 | II 57 | II 55 |
| -1 40 | 127 | 12 | 124 | 124 | 122 | 12 | 120 | II 59 | II $5^{8}$ |
| - 120 | 127 | 126 | 125 | 124 | 123 | 12 | 122 | 12 I | 12 O |
| 10 | 127 | 126 | 125 | 125 | 124 | 124 | 123 | 122 | $12 \quad 2$ |
| -0 40 | 127 | 126 | 126 | 125 | 125 | 125 | 125 | 124 | $\begin{array}{ll}12 & 4 \\ \\ 12 & 7\end{array}$ |
| -0 20 | 127 | 126 | 126 | 126 | 126 | 126 | 126 | 126 | 127 |
| 0 | 127 | 127 | 127 | 127 | 127 | 127 | 128 | 128 | 129 |
| +0 20 | 127 | 127 | 127 | 128 | 128 | 128 | 129 | 1210 | 12 II |
| - 40 | 127 | 127 | 128 | I2 8 | 129 | 1210 | 12 II | 12 I2 | 1213 |
| 10 | 127 | 12 | 12 S | 129 | 1210 | 12 II | 1213 | $\begin{array}{lll}12 & 14 \\ 12\end{array}$ | $\begin{array}{ll}12 & 15 \\ 12 & 17\end{array}$ |
| 120 | 127 | 128 | 129 | 1210 | 12 II | 12 I3 | 1214 | 1216 | 1217 |
| I 40 | 127 | 128 | 129 | 1210 | 1212 | 1214 | 1216 | 1217 | 1220 |
| 20 | 127 | 128 | 1210 | 12 II | 1213 | 1215 | $\begin{array}{lll}12 & 17\end{array}$ | 1219 | $\begin{array}{ll}12 & 22 \\ 12 & 25\end{array}$ |
| 220 | 127 | 128 | 1210 | 1212 | 1214 | 1216 | 1219 | 1221 | $\begin{array}{ll}12 & 25 \\ 12\end{array}$ |
| 240 | 127 | 129 | 12 II | 1213 | 1215 | 1217 | 1220 | 1223 | 1227 |
| 30 | 7 | 129 | 12 II | 1213 | 1216 | 1219 | 1222 | 1225 | $\begin{array}{ll}12 & 29\end{array}$ |
| 320 | 127 | 129 | 1212 | 1214 | 12 I 7 | 1220 | 1223 | 1227 | 1231 |
| 340 | 127 | 129 | 1212 | 1215 | 12 IS | 1221 | 1225 | 1229 | 1233 |
| 40 | 127 | 1210 | 1213 | 1216 | 1219 | 1222 | 1226 | 1231 | 1235 |
| 420 | 127 | 1210 | 12 I 3 | 1216 | 1220 | 1223 | 1228 | $\begin{array}{ll}12 & 32 \\ 12\end{array}$ | 1238 |
| 440 | 127 | 1210 | 1214 | 1217 | 1221 | 1225 | 1229 | 1234 | 1240 |
| 50 | 127 | 1210 | 1214 | 12 I 8 | 1222 | 1226 | 1231 | 1236 | 1243 |
| 520 | 127 | 1210 | 12 I 5 | 1219 | 1223 | 1228 | 1232 | 1235 | 1245 |
| 540 | 127 | 12 II | 12 I 5 | 1219 | 1224 | 1229 | 1234 | 1240 | 1247 |
| 60 | 27 | 12 II | 1216 | 1220 | 1225 | 1230 | $\begin{array}{ll}12 & 35\end{array}$ | 1242 | 1249 |
| 620 | 127 | 12 II | 1216 | 1221 | $\begin{array}{ll}12 & 26\end{array}$ | 1231 | $\begin{array}{lll}12 & 37 \\ \text { I2 } & 39\end{array}$ | 1244 1246 | $\begin{array}{lll}12 & 52 \\ 12 & 54\end{array}$ |
| 640 | 127 | 12 II | 1216 | 1222 | 1227 | 1232 | 1239 | 1246 |  |
| 70 | 127 | 1212 | 1217 | 1222 | 1228 | 1234 | 1240 | 1245 | 1256 1258 |
| 720 | 127 | $\begin{array}{lll}12 & 12 \\ 12\end{array}$ | $\begin{array}{lll}12 & 17 \\ 12 & \text { IS }\end{array}$ | $\begin{array}{ll}12 & 23 \\ 12 & 23\end{array}$ | $\begin{array}{ll}12 & 29 \\ 12 & 30\end{array}$ | $\begin{array}{ll}12 & 35 \\ 12 & 36\end{array}$ | 1242 1243 | 125 1252 | 13 I |
| 740 | 12 | 1212 | 12 IS | 1223 | 1230 | 123 1238 | 1245 | 1253 | 13 |
| 80 |  | 1213 | 1218 | 1224 | 1231 | 1238 | 1245 | 1253 | 13 3 |

Table 94.
DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of of } \\ & \text { the Sun. } \end{aligned}$ | LATITUDE NORTII. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $42^{\circ}$ | $44^{\circ}$ | $46^{\circ}$ | $48^{\circ}$ | $50^{\circ}$ | $52^{\circ}$ | $54^{\circ}$ | $56^{\circ}$ | $58^{\circ}$ | $60^{\circ}$ |
|  | h. im. | h. m. | h. m. | h. m. | 11. 11. | h. 11. | h. m. | h. m. | h. m. | h. m. |
| $-8^{\circ} 0^{\prime}$ | 11 II | II 7 | II 3 | II 58 | IO 53 | 1048 | IO 43 | 10 36 | Io 30 | 1021 |
| -740 | 1113 | II 10 | II 5 | II | IO 57 | 10 52 | IO 46 | 1040 | 10 34 | IO 26 |
| -7 20 | II 16 | 1112 | 115 | II 4 | II O | IO 55 | Io 50 | 1044 | Io 38 | 1031 |
| $-7 \quad 0$ | II 19 | II 15 | II II | I 17 | 113 | IO 59 | 10 54 | 1048 | IO 42 | IO 35 |
| $-640$ | II 21 | II 17 | 1114 | 11 IO | II 7 | 11 | 1058 | 10 52 | Io 47 | IO 40 |
| - 620 | II 23 | II 20 | 1117 | 1113 | II Io | II 5 | 11 | IO $5^{6}$ | IO 51 | IO 45 |
| -6 o | II 26 | II 23 | II 20 | I I 16 | II 13 | I I 9 | II 5 | II 0 | IO 55 | 1050 |
| $-540$ | II 28 | II 25 | II 23 | II 19 | II 16 | $\begin{array}{ll}\text { II } & 13\end{array}$ | 118 | I I 4 | 10 59 | IO 55 |
| $-520$ | II 31 | II 28 | II 25 | 1122 | II 19 | II 16 | II 13 | II S | II 4 | IO 59 |
| -5 | II 33 | 1131 | II 28 | II 25 | II 23 | II 19 | II 16 | II 12 | II S | II 4 |
| -4 40 | II 35 | I 133 | 1131 | II 2 S | II 26 | II 23 | II 20 | II 16 |  | II S |
| -420 | II $33^{\circ}$ | II 36 | II 34 | 1131 | II 29 | II 26 | II 23 | II 20 | II 17 | II I3 |
| - 0 | II 40 | II 3 S | II 37 | I I 34 | II 32 | II 30 | II 27 | I I 24 | 112 I | 11 If |
| -3 40 | II 43 | II 41 | II 39 | II 37 | II 35 | II 33 | 1131 | II 2 S | II 26 | II 22 |
| 320 | II 45 | II 43 | II 42 | I I 40 | II 3 S | II 37 | II 35 | $\begin{array}{ll}\text { I I } & 32 \\ \text { II }\end{array}$ | II 30 | II 27 |
| $-30$ | II 47 | II 46 | II 45 | II 43 | II 42 | II 40 | II 38 | II $3^{6}$ | I I 3.4 | I I 32 |
| -240 | II 50 | II 49 | II 47 | I I $4^{6}$ | II 45 | II 44 | II 42 | II 40 | II 35 | II 37 |
| -2 20 | II 52 | II 51 | 1150 | II 49 | II 48 | II 47 | I I 46 | II 44 | II 43 | II 41 |
| -2 0 | II 55 | I I 54 | II 53 | II 52 | II 52 | II 50 | II 49 | II 4 S | I I 47 | I I 46 |
| -140 | II 57 | II 56 | I I 55 | II 55 | II 55 | II 54 | II 53 | II 52 | II 51 | I I 50 |
| I 20 | II 59 | II 59 | II 58 | II 5 S | II $5^{3}$ | II 57 | I I 57 | II 56 | I I 56 | I I 55 |
| I O | 122 | 122 | 12 I | 121 | 12 I | 12 I | 12 I | 120 | 120 | I I 59 |
| -0 40 | 124 | 124 | 124 | 124 | 124 | 12 | 12 | 12 | 124 | 124 |
| O 20 | 127 | 127 | 127 | 127 | 127 | 127 | 12 S | 12 S | 12 S | 129 |
| +00 | 129 | 129 | 12 IO | 12 10 | 1210 | 12 11 | 12 II | 1212 | 12 I 3 | 12 I 3 |
| - 20 | 12 II | 1212 | 1213 | 1213 | 12 I 4 | 1214 | 12 I 5 | 1216 | 1217 | 12 IS |
| - 40 | 1214 | 12 I4 | 1215 | 1216 | 1217 | 1217 | 1219 | 1220 | 1221 | 1223 |
| 10 | 1216 | 1217 | 12 IS | 1219 | 1220 | 1221 | 1222 | 1224 | 1225 | 1227 |
| I 20 | 1219 | 1220 | 1220 | 1222 | 1223 | 1225 | 1226 | 1228 | 1229 | $\begin{array}{ll}12 & 32\end{array}$ |
| I 40 | 1221 | 1222 | 1223 | 1225 | 1226 | 1228 | 1230 | 1232 | $12 \quad 34$ | 1237 |
| 20 | 1223 | 1225 | 1226 | 1228 | 1229 | 1231 | 1234 | 1236 | 1238 | 1241 |
| 220 | 1226 | 1225 | 1229 | 1231 | 1232 | 1235 | 1237 | 1240 | 1243 | 1246 |
| 240 | 1228 | 1230 | 1232 | 1234 | 1236 | 1235 | 124 I | 1244 | 1247 | 1250 |
| 30 | 1231 | 1232 | 1235 | 1237 | 1239 | 1241 | 1244 | 1248 | 1251 | 1255 |
| 320 | $\begin{array}{ll}12 & 33\end{array}$ | 1235 | 1237 | 1240 | 1242 | 1245 | 1248 | 1252 | 1255 | 130 |
| 340 | I2 35 | 1238 | 1240 | 1243 | 1246 | 1249 | 1252 | 1256 | 130 | 134 |
| 40 | 1238 | 1240 | 1243 | 1246 | 1249 | 1252 | 1256 | 130 |  | 139 |
| 420 | 1240 | 1243 | 1246 | 1249 | 1252 | 1255 | 1259 | I3 4 | 13 S | 1314 |
| 440 | 1243 | 1246 | 1249 | $125^{2}$ | 1255 | I2 59 | 133 | 13 S | 1313 | 1319 |
| 50 | 1245 | 1248 | 1251 | 1255 | 1258 | 132 | 137 | I3 12 | 1317 | 1323 |
| 520 | 1247 | 1251 | 1254 | 1258 | I3 2 | 136 | 13 II | 1316 | 1322 | 1328 |
| 540 | 1250 | 1253 | 1257 | 13 I | 135 | 13 Io | 1314 | 1320 | 1326 | I3 33 |
| 60 | 1253 | I2 56 | 1259 | I3 4 | 13 S | 1313 | 13 IS | 1324 | 13 31 | 1338 |
| 620 | 1255 | I2 59 | 132 | 137 | 13 II | 1316 | 1322 | 1328 | 1335 | I3 43 |
| 640 | 1258 | 13 | I3 5 | 1310 | 1314 | 1320 | 1326 | I3 32 | 1339 | I3 47 |
| 70 | 130 | 134 | 13 S | 1313 | 13 IS | 1323 | 1329 | $13 \quad 36$ | 1344 | $135^{2}$ |
| 720 | 132 | 137 | 13 II | 1316 | 1321 | I3 27 | 1333 | 1340 | 1348 | 1357 |
| 740 | 135 | I3 9 | 1314 | I3 19 | 1325 | 13 31 | 1337 | 1344 | I3 53 | 142 |
| 80 | I3 7 | I3 12 | 1317 | I3 22 | 1328 | 1334 | 1341 | I3 48 | 1357 | $14 \quad 7$ |


| $\begin{aligned} & \text { Declination } \\ & \text { of } \\ & \text { te Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0^{\circ}$ | $5^{\circ}$ | $10^{\circ}$ | $15^{\circ}$ | $20^{\circ}$ | $25^{\circ}$ | $30^{\circ}$ | $35^{\circ}$ | $40^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $+8^{\circ} 0^{\prime}$ | 127 | 1213 | 12 IS | 1224 | 1231 | 1238 | 1245 | 1253 | 133 |
| S 20 | 127 | 12 I3 | 1219 | 1225 | 1232 | 1239 | 1247 | 1255 | 135 |
| 840 | 127 | 12 I3 | 1219 | 1226 | 1233 | 1240 | 1248 | 1257 | 13 S |
| 90 | 127 | 1213 | 1220 | 1226 | I2 $3+$ | 124 I | 1250 | 1259 | 1310 |
| 920 | 127 | 12 I 3 | 1220 | I2 27 | 1235 | 1243 | 1252 | 131 | 1313 |
| 940 | 127 | 12 I 4 | 1221 | 1228 | $12 \quad 36$ | 1244 | 1253 | 133 | $\mathrm{I}_{3} 14$ |
| 100 | 127 | 12 I 4 | 1221 | 1229 | 1237 | 1245 | 1255 | 135 | 1317 |
| 1020 | 127 | 1214 | 1222 | 1229 | 1238 | 1247 | 1256 | 137 | 1319 |
| 1040 | 127 | 1214 | 1222 | 1230 | 1239 | 1248 | 1258 | I3 9 | I3 22 |
| 110 | 127 | 12 I5 | 1223 | 1231 | 1240 | 12.49 | 1259 | 13 II | 1324 |
| II 20 | 127 | 12 I5 | 1223 | 1232 | 1241 | 1250 | 13 I | 1313 | 1326 |
| 1140 | 12, 7 | 1215 | 1224 | 1232 | 1242 | 1252 | I3 2 | I3 I5 | I3 29 |
| 120 | 127 | 1215 | $\begin{array}{ll}12 & 2.4\end{array}$ | 1233 | 1243 | 1253 | I3 4 | 1317 | 1331 |
| 1220 | 127 | 1216 | 1225 | 1234 | 1244 | 1255 | I3 6 | 13 I9 | 1334 |
| 1240 | 127 | 1216 | 1225 | 1235 | 1245 | 1256 | 13 S | 1321 | 1336 |
| 130 | 127 | 1216 | 1226 | 1235 | 1246 | 1257 | I3 9 | I3 23 | 1338 |
| 1320 | 127 | 1216 | 1226 | 1236 | $12+7$ | 1258 | 1311 | I3 25 | 1341 |
| 1340 | 127 | 1217 | 1227 | 1237 | 1248 | 130 | 1313 | 1327 | 1343 |
| 140 | 12 | 12 I 7 | 1227 | 1238 | 1249 | 13 | 13 It | I3 29 | 1346 |
| 1420 | 12 | 1217 | 1225 | 1239 | 1250 | 13 | I3 16 | 1331 | 1348 |
| 1440 | 127 | 1217 | 1225 | 1240 | 1251 | 134 | 1317 | 1333 | I3 5I |
| 150 | 127 | 1218 | 1229 | 1240 | 1252 | 135 | 1319 | 13.35 | 1353 |
| 1520 | $12 \quad 7$ | 12 IS | 1229 | 1241 | 1253 | 137 | 1321 | 1337 | 1356 |
| 1540 | 127 | 12 I8 | 1230 | 1241 | 1254 | 13 8 | 1323 | I3 39 | 1358 |
| 160 | 127 | 12 I 9 | 1230 | 1242 | 1255 | $13 \quad 9$ | I3 25 | I3 4I | 14 I |
| 1620 | 127 | 1219 | 1231 | 1243 | 1256 | 13 II | I3 26 | I3 43 | 143 |
| 1640 | 127 | 1219 | 1231 | 1244 | 1258 | 1312 | 1328 | 1345 | 146 |
| 170 | 127 | 12 I 9 | 1232 | 1245 | 1259 | 1313 | 1329 | I3 47 | 148 |
| 1720 | 127 | 1220 | 1232 | 1246 | 130 | 1315 | 1331 | 1350 | I4 II |
| 1740 | $12 \%$ | 1220 | 1233 | 1246 | 13 I | I3 16 | 1333 | 1352 | 14 I4 |
| 180 | 127 | 1220 | 1233 | 1247 | 131 | 1317 | I3 35 | I3 54 | 1416 |
| 1820 | 127 | 1220 | 1234 | 1248 | 133 | $\begin{array}{ll}13 & 19\end{array}$ | 1337 | I3 56 | 1419 |
| 1840 | 127 | 1221 | 1234 | 1249 | 134 | 1320 | 1338 | 1358 | 1422 |
| 190 | 127 | 1221 | 1235 | 1250 | 135 | 1322 | 1340 | If 0 | 1424 |
| 1920 | 127 | 1221 | 1235 | 1251 | 136 | 1323 | ${ }^{1} 342$ | 142 | 1426 |
| 1940 | $12 \quad 7$ | 1222 | 1236 | $125^{2}$ | 137 | 1325 | I3 44 | 145 | 1429 |
| 200 | 127 | 1222 | 1236 | 1252 | 13 S | 1326 | 1346 | 147 | I4 32 |
| $20 \quad 20$ | 127 | 1222 | 1237 | 1253 | 1310 | 1328 | I3 47 | 1410 | 1435 |
| 2040 | 127 | 1222 | 1237 | 1254 | I3 II | 1329 | 1349 | 1412 | I4 37 |
| 210 | 127 | 1223 | 1238 | 1255 | 1312 | 1331 | 13 5I | 1414 | 1440 |
| 2120 | 127 | 1223 | 1239 | 1256 | 1313 | 1332. | 1353 | 1416 | 1443 |
| 2140 | 127 | 1223 | 1239 | 1256 | 13 I4 | 1334 | I3 55 | 1419 | 1446 |
| 220 | 127 | 122.4 | 1240 | $125 \%$ | 1316 | I3 35 | 1356 | 1421 | I4 49 |
| $22 \quad 20$ | 127 | i2 2.4 | 1241 | 1258 | I3 17 | I3 37 | 1358 | 1423 | 1452 |
| 2240 | 127 | 122.4 | 1241 | 1259 | 13 IS | $13{ }^{1} 8$ | 140 | 1425 | 1454 |
| 230 | 127 | 1225 | 1242 | 130 | 1319 | 1340 | $14 \quad 2$ | I+ 28 | I4 57 |
| 2320 | 127 | 1225 | 1242 | 13 I | 1320 | 1341 | I4 4 | 1430 | 150 |
| 2327 | 127 | 1225 | 1243 | 13 | 1320 | I3 4I | 145 | 1431 | I5 I |

Table 94.
DURATION OF SUNSHINE AT DIFFERENT LATITUDES

| $\begin{aligned} & \text { Declin } \text { "fion } \\ & \text { the Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $42^{\circ}$ | $44^{\circ}$ | $46^{\circ}$ | $48^{\circ}$ | $50^{\circ}$ | $52^{\circ}$ | $54^{\circ}$ | $56^{\circ}$ | $58^{\circ}$ | $60^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $+8^{\circ} 0^{\prime}$ | 137 | 1312 | 1317 | 1322 | 1328 | 1334 | 1341 | 1349 | 1358 | 147 |
| S 20 | 13 Io | 1314 | I3 20 | 1325 | 1331 | 1338 | I3 45 | 1353 | $14 \quad 2$ | 1412 |
| 840 | 1312 | 1317 | 1323 | 1328 | I3 34 | 1341 | I3 49 | I3 57 | 146 | 1417 |
| 90 | 1315 | 1320 | 1325 | 1331 | 1338 | 1345 | 1353 | 14 I | 14 II | 1422 |
| 920 | 1317 | I3 23 | 1328 | I3 34 | I3 4I | 1349 | I3 56 | 145 | 1415 | I4 26 |
| 940 | 1320 | I 325 | I3 3I | $133^{8}$ | I3 44 | 1352 | 140 | 14 Io | 1420 | 1431 |
| 100 | I3 22 | 1328 | I3 34 | 134 I | 1348 | 1356 | I4 4 | 1414 | 1425 | 1436 |
| 1020 | I3 25 | 13 31 | 1337 | 1344 | 1351 | 1359 | 148 | 1418 | 1429 | 1441 |
| 1040 | 1328 | I3 34 | I3 40 | 1347 | I3 55 | 143 | $14 \quad 12$ | 1422 | 1434 | 14 47 |
| 110 | I3 30 | I3 36 | I3 43 | 1350 | 1358 | 147 | 1416 | 1427 | 1438 | 1452 |
| II 20 | I3 32 | 1339 | I3 46 | 1353 | 14 I | 14 10 | 1420 | 1431 | 1443 | 1457 |
| II 40 | I3 35 | I3 4I | I3 49 | I 356 | 145 | 1414 | 1424 | 1435 | 1448 | 152 |
| 120 | 1338 | 1344 | 1352 | 140 | 14 S | 1418 | 1428 | 1440 | 1453 | 158 |
| 1220 | I3 40 | I3 47 | I3 55 | 143 | 1412 | 1422 | 1432 | 1444 | I4 58 | 15 I3 |
| 1240 | 1343 | I3 50 | 1358 | 146 | 1416 | 1425 | 1437 | I4 49 | I5 2 | 1518 |
| 130 | I3 46 | I3 53 | 14 I | 14 Io | 1419 | 1429 | I4 4I | 1453 | I5 7 | $15 \quad 23$ |
| 1320 | I3 48 | I3 56 | I4 4 | 1413 | 1422 | 1433 | 1445 | 1458 | 1513 | 1529 |
| 1340 | I3 $5^{\circ}$ | I3 58 | 147 | 1416 | 1426 | 1437 | 1449 | $15 \quad 2$ | 1517 | 1535 |
| 140 | 1353 | 14 I | 14 IO | 1419 | 1429 | 1441 | 1453 | 15 | 1522 | 1540 |
| 1420 | I3 56 | 144 | 1413 | 1423 | I4 33 | I4 45 | 1457 | 15 II | 1528 | 1546 |
| 1440 | I3 59 | I4 7 | 1416 | 1426 | 1437 | I4 49 | 152 | 1516 | 1533 | 1551 |
| 150 | 14 | 1410 | 1419 | I4 29 | I4 40 | 1452 | 156 | 1521 | 1538 | 1557 |
| 1520 | I4 4 | 1413 | I4 22 | 1433 | I4 44 | 1.456 | 1510 | 1526 | 1543 | $16 \quad 2$ |
| 1540 | 147 | 1416 | I4 26 | 1436 | 1448 | I5 0 | I5 14 | I5 30 | I5 48 | 168 |
| 160 | 14 IO | 1419 | 1429 | 1440 | 1452 | 154 | 1519 | I5 35 | 1553 | 1614 |
| 1620 | 1412 | 1422 | 1432 | 1443 | 1455 | 15 S | 1523 | I5 40 | 1559 | 1620 |
| 1640 | 1415 | 1425 | 1435 | 1446 | 1459 | 1513 | 1528 | I5 45 | 164 | 1626 |
| 170 | 1417 | 1428 | $143^{8}$ | I4 50 | 153 | 1517 | 1532 | 1550 | 16 ıo | 1632 |
| 1720 | 1420 | 1431 | 1441 | I4 53 | 157 | 1521 | 1537 | 1555 | 1615 | 1638 |
| 1740 | 1423 | I4 34 | 1445 | 1457 | 1510 | I5 25 | 1541 | 16 O | 1620 | 1645 |
| 180 | 1426 | I4 37 | 1448 | 15 I | 1514 | I5 29 | 1546 | 165 | 1626 | 1651 |
| 1820 | 1429 | I4 40 | 1452 | 154 | 1518 | I5 34 | 1550 | 16 Io | 1632 | 1658 |
| I8 40 | 1432 | 1443 | 1455 | 158 | 1522 | 1538 | 1555 | 16 I5 | 1638 | 174 |
| 190 | 1435 | 1446 | 1458 | 15 II | 1526 | I5 42 | 160 | 1620 | 1644 | 17 II |
| 1920 | 1437 | I4 49 | 15 I | 1515 | 1530 | 1546 | 16 | 1625 | 1650 | 1717 |
| 1940 | 1440 | I4 52 | $15 \quad 5$ | 1519 | I5 34 | 1551 | 1610 | 1631 | 1656 | 1724 |
| 200 | 1443 | 1455 | 158 | 1522 | $15 \quad 38$ | 1555 | 1615 | 1637 | $17 \quad 2$ | 1731 |
| 2020 | 1446 | 1458 | 15 II | 1526 | 1542 | 16 O | 1620 | 1642 | 178 | 1738 |
| 2040 | 1449 | $15 \quad 2$ | 1515 | I5 30 | I5 46 | 164 | 1625 | 1647 | 1714 | I7 46 |
| 210 | 1452 | 155 | 15 I9 | 1534 | I5 50 | $16 \quad 9$ | 1630 | 1653 | 1720 | 1753 |
| 2120 | 1455 | 158 | I5 22 | I5 38 | I5 55 | 1613 | 1635 | 1659 | 1727 | 18 I |
| 2140 | 1458 | 15 II | 1526 | 1542 | I5 59 | 1618 | 1640 | I7 5 | 1734 | 188 |
| 220 | I5 I | 1514 | 1529 | I5 46 | 163 | 1623 | 1645 | 17 II | 1740 | I8 16 |
| 2220 | I5 4 | 1518 | I5 33 | I5 49 | 167 | 1628 | 1650 | $\begin{array}{ll}17 & 17\end{array}$ | 1747 | 1824 |
| 2240 | I5 7 | $-522$ | I5 37 | 1553 | I6 12 | 1632 | 1656 | 1723 | I7 54 | 1832 |
| 230 | I5 10 |  | I5 40 | 1557 | 1616 | 1637 | 17 I | 1729 | 18 I | 1841 |
| 2320 | 1513 | I5 28 | 1544 | 16 I | 1621 | 1642 | I7 7 | 1735 | I8 8 | 1849 |
| 2327 | 1514 | 1529 | I5 46 | 163 | 1623 | 1644 | 179 | 1737 | I8 II | I8 52 |

DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of } \\ & \text { the Sun. } \end{aligned}$ | IATITUDE NORTH. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $60^{\circ}$ | $61^{\circ}$ | $62^{\circ}$ | $63^{\circ}$ | $64^{\circ}$ | $65^{\circ}$ | $66^{\circ}$ | $67^{\circ}$ | $68^{\circ}$ | $69^{\circ}$ | $70^{\circ}$ |
|  | h. m. | h. m. | h. m. | h.m. | h. m. | h. m. | h. m. | h.m. | h.m. | h. m. | h.m. |
| $-23^{\circ} 27^{\prime}$ | 552 | 53 I | 58 | 442 | 4 II | 334 | 246 | 129 |  |  |  |
| $-2320$ | 555 | 534 | 512 | 446 | 416 | 340 | 253 | 14 I |  |  |  |
| -23 0 | 62 | 543 | 521 | 456 | 428 | 353 | 3 II | 2 II |  |  |  |
| -22 40 | 6 10 | 551 | 530 | 56 | 439 | 47 | 327 | 235 | - 59 |  |  |
| - 2220 | 617 | 559 | 539 | 516 | 450 | 420 | 343 | 256 | I 43 |  |  |
| -22 0 | 625 | 67 | 547 | 525 | 5 I | 432 | 358 | 3 I 4 | 213 |  |  |
| -2140 | 632 | 6 I4 | 556 | 534 | 5 II | 443 | 4 II | 331 | 238 | 1 I |  |
| 2I 20 | 639 | 622 | 64 | 543 | 520 | 455 | 424 | 347 | 259 | 145 |  |
| 210 | 646 | 629 | 612 | 552 | 530 | 55 | 436 | 4 I | 318 | 216 |  |
| -2040 | 652 | 637 | 620 | 6 I | 540 | 516 | 448 | 416 | 335 | 241 | 12 |
| - 2020 | 659 | 644 | 627 | 69 | 549 | 526 | 459 | 429 | 351 | 32 | I 47 |
| 20 O | 75 | 65 I | 634 | 617 | 558 | 535 | 5 Io | 441 | 46 | 322 | 219 |
| - 1940 | 712 | 658 | 642 | 625 | $6 \quad 6$ | 545 | 521 | 453 | 420 | 339 |  |
| - 1920 | 7 I8 | 74 | 649 | 633 | 614 | 554 | 531 | 55 | 434 | 355 | 36 |
| -19 0 | 725 | 7 II | 656 | 64 I | 623 | 63 | 54 I | 516 | 447 | 4 II | 326 |
| - 1840 | 731 | 717 | 74 | 648 | 631 | 612 | 551 | 526 | 459 | 425 | 344 |
| - 1820 | 737 | 724 | 710 | 655 | 639 | 620 | 61 | 537 | 5 II | 439 | 41 |
| 18 o | 743 | 731 | 717 | 73 | 647 | 629 | 610 | 547 | 522 | $45^{2}$ | 416 |
| - 1740 | 749 | 737 | 724 | 710 | 655 | 638 | 6 19 | 557 | 5.33 | 55 | 431 |
| $-1720$ | 755 | 743 | 731 | 717 | 72 | 646 | 628 | 67 | 543 | 517 | 445 |
| $-170$ | 8 I | 749 | 737 | 724 | 79 | 653 | 636 | 616 | 554 | 528 | 458 |
| -16 40 | 86 | 755 | 744 | 731 | 717 | 7 I | 644 | 626 | 64 | 540 | 5 II |
| - 16 20 | 812 | 8 8 1 | 750 | 738 | 724 | $\begin{array}{ll}7 & 9\end{array}$ | 652 | 635 | 614 | 551 | 523 |
| - 160 | 817 | 87 | 756 | 744 | 731 | 717 | 71 | 644 | 624 | $6 \quad 2$ | 535 |
| -1540 | 823 | 813 | $8 \quad 2$ | 751 | 738 | 725 | 78 | 652 | 634 | 612 | 547 |
| $-1520$ | 829 | 819 | 88 | 758 | 745 | 732 | 717 | 71 | 643 | 622 | 559 |
| $-150$ | 834 | 825 | 8 I5 | 84 | 752 | 739 | 725 | $\begin{array}{ll}7 & 9\end{array}$ | 652 | 632 | 610 |
| -14 40 | 840 | 831 | 821 | 8 10 | 759 | 746 | 732 | 717 | 7 I | 642 | 620 |
| $-1420$ | 845 | 836 | 827 | 817 | 88 | 753 | 740 | 726 | 7 10 | 651 | 631 |
| $-140$ | 850 | 842 | 833 | 823 | 812 | 8 I | 747 | 734 | 7 58 | 71 | 64 I |
| $-1340$ | 856 | S 47 | 838 | 829 | 819 | 87 | 755 | 741 | 726 | 7 Io | 651 |
| - 1320 | 91 | 853 | 844 | 835 | 825 | 814 | 82 | 749 | 735 | 719 | 71 |
| $-130$ | 96 | 858 | 850 | 841 | 832 | 821 | 8 10 | 757 | 743 | 728 | 7 10 |
| $-1240$ | 9 II | 94 | 856 | 847 | 838 | 828 | 817 | 85 | 751 | 737 | 720 |
| - 1220 | 917 | 9 IO | 92 | 853 | 844 | 834 | 824 | 812 | 759 | 745 | 729 |
| 120 | 922 | 915 | 97 | 859 | 850 | 84 I | 831 | 820 | 87 | 753 | 738 |
| - 1140 | 927 | 920 | 913 | 95 | 856 | 847 | 838 | 827 | 8 I5 | 82 | 747 |
| II 20 | 932 | 925 | 919 | 9 II | 93 | 854 | 844 | 834 | 823 | 810 | 756 |
| II O | 937 | 931 | 924 | 917 | 98 | 90 | 85 I | 84 I | 83 I | 818 | 85 |
| -1040 | 942 | 936 | 929 | 922 | 915 | 97 | 858 | 849 | 838 | 826 | 814 |
| - IO 20 | 947 | 941 | 935 | 928 | 921 | 913 | 95 | 856 | 846 | 834 | 822 |
| 10 O | 952 | 946 | 940 | 934 | 927 | 919 | 9 II | 93 | 853 | 842 | 831 |
| - 940 | 957 | 951 | 946 | 940 | 933 | 926 | 918 | 910 | 9 O | 850 | 839 |
| - 920 | IO 2 | 956 | 951 | 945 | 939 | 932 | 925 | 916 | 98 | 858 | 847 |
| -90 | IO 7 | 102 | 956 | 950 | 944 | 938 | 931 | 923 | 915 | 95 | 855 |
| - 840 | IO II | 107 | 102 | 956 | 950 | 944 | 937 | 930 | 922 | 913 | 93 |
| - 820 | 1016 | 1012 | IO 7 | IO 2 | 956 | 950 | 944 | 937 | 929 | 921 | 9 II |
| - 50 | 1021 | 1017 | 1012 | 10 7 | 102 | 956 | 950 | 943 | 936 | 928 | 919 |

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Table 94.
DURATION OF SUNSHINE AT DIFFERENT LATITUDES.


DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { the of Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $60^{\circ}$ | $61^{\circ}$ | $62^{\circ}$ | $63^{\circ}$ | $64^{\circ}$ | $65^{\circ}$ | $66^{\circ}$ | $67^{\circ}$ | $68^{\circ}$ | 69 | $70^{\circ}$ |
|  | h. mı. | h. 11 m | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $-8^{\circ} \quad 0^{\prime}$ | IO 21 | 1017 | 1012 | IO 7 | 102 | 956 | 950 | 943 | 936 | 928 | 919 |
| -7 40 | IO 26 | 1022 | 1017 | 10 I3 | Io 8 | 102 | 956 | 950 | 943 | 935 | 927 |
| -7 20 | 1031 | 1027 | 1023 | 10 I8 | 1013 | IO 8 | 103 | 957 | 950 | 943 | 935 |
| -7 | 1035 | 1032 | 1028 | 1023 | 1019 | IO I4 | 109 | IO 4 | 957 | 950 | 943 |
| --6 40 | 1040 | 1037 | 1033 | 10 29 | 1025 | IO 20 | 1015 | Io 10 | 10.4 | 957 | 951 |
| -6 20 | 1045 | IO 42 | 1038 | IO 34 | 1031 | 10 26 | 1022 | 1016 | IU 11 | 105 | 958 |
| -6 o | 1050 | IO 47 | 10 43 | 1040 | 1036 | 10 32 | 1028 | 1023 | 1018 | 1012 |  |
| -5 40 | 1055 | IO 52 | 1049 | IO 45 | 1041 | 1038 | 1034 | 1029 | 10 25 | 1019 | IO 14 |
| -5 20 | 10 59 | 10 56 | 10 54 | 1050 | 1047 | 10 44 | 10 40 | 10 36 | 1031 | 1026 | 1021 |
| -5 | II 4 | II I | IO 59 | 10 56 | 1053 | 1050 | 10 46 | 1042 | 1038 | IO 34 | 1029 |
| -4 40 | 118 | II 6 | II 4 | II | 1058 | 1055 | IO 52 | 1049 | 1045 | 1041 | IO 36 |
| 420 | 1113 | II II | II 9 | 117 | 114 | II I | 1058 | 1055 | 1052 | 1048 | Io 44 |
| -4 0 | 1118 | II 16 | 1114 | II 12 | II 10 | II 7 | II 4 | II | 1058 | IO 55 | 1051 |
| -3 40 | II 22 | II 21 | 1119 | 1117 | 1115 | I 13 | II 10 | 118 | II 5 | II 2 | 1059 |
| 320 | II 27 | II 26 | II 24 | II 22 | 1120 | II I9 | II 16 | II 14 | 11 II | 119 | 115 |
| -3 0 | II 32 | 1131 | II 29 | 1128 | II 26 | I I 24 | II 22 | II 20 | 11 IS | II 16 | 1113 |
| -2 40 | 1137 | I1 35 | II 34 | 1133 | II 31 | I 130 | 1128 | 11 27 | 1125 | II 23 | 1121 |
| 220 | II 41 | II 40 | 1139 | 1138 | 11 37 | II 36 | 1134 | II 33 | 1132 | 1130 | 1128 |
| 2 | II 46 | I I 45 | II 44 | I I 43 | II 43 | II 41 | II 40 | II 40 | II 38 | II 37 | 1135 |
| -1 40 | I 150 | II 50 | II 49 | I I 49 | 1148 | 1147 | II 46 | II 46 | II 45 | II 44 | 1143 |
| 20 | II 55 | II 55 | II 54 | II 54 | II 53 | 1153 | II 52 | 1152 | II 52 | II 51 | II 50 |
| 1 | I I 59 | II 59 | II 59 | II 59 | I1 59 | 11 59 | II 58 | 1158 | II 58 | 1158 | II $5^{8}$ |
| -0 40 | 124 | 124 | 124 | 124 | 124 | 124 | 124 | 124 | 125 | 125 | 125 |
| -0 20 | 129 | 129 | 129 | 1210 | 1210 | 1210 | 1210 | 12 II | 12 II | 1212 | 1212 |
|  | 1213 | 1214 | 1214 | 1215 | 1215 | 1216 | 1216 | 1217 | 1218 | 1219 | 1219 |
| +0 20 | 1218 | 1219 | 1219 | 1220 | 1220 | 1222 | 1222 | 1223 | 1225 | 1226 | 1227 |
| O 40 | 1222 | 1223 | 1224 | 1225 | 1226 | 1227 | 1228 | 1229 | 1231 | 1233 | 1234 |
|  | 1227 | 1228 | 1229 | 1231 | 1232 | 1233 | 1234 | 1236 | 1238 | 1240 | 1241 |
| I 20 | 1232 | 1233 | 1234 | 1236 | 1237 | 1239 | 1240 | 1242 | 1244 | 1247 | 1249 |
| 140 | 1237 | 1238 | 1239 | 1241 | 1243 | 1244 | 1246 | I2 49 | 1251 | 1254 | 1256 |
|  | 1241 | 1243 | 1244 | 1246 | 1248 | 1250 | 1252 | 1255 | 1258 | 13 I | $\begin{array}{ll}13 & 4\end{array}$ |
| 220 | 1246 | 1247 | 1249 | 1252 | 1253 | 1256 | 1259 | 13 1 | 134 | 138 | 1311 |
| 240 | 1250 | 1252 | 1254 | 1257 | 1259 | 132 | 135 | 137 | 1311 | 1315 | I3 19 |
| 30 | 1255 | 1257 | 1259 | 131 | 135 | 138 | 13 II | 1314 | 1317 | 1322 | 1326 |
| 320 | 130 | $1 \begin{array}{ll}1 & 2\end{array}$ | 135 | 137 | 1310 | 1313 | $\begin{array}{lll}13 & 17\end{array}$ | 1320 | 1324 | 1329 | 1334 |
| 340 | I3 4 | 137 | 1310 | 1313 | 1316 | 1319 | 1323 | 1327 | 1331 | 1336 | 1341 |
| 40 | 139 | 1312 | 1315 | 13 I8 | 1322 | 1325 | 1329 | 1333 | 1338 | 1343 | 1349 |
| 420 | 1314 | 1317 | 1320 | 1323 | 1327 | 1331 | I 335 | 1340 | 1345 | I3 50 | 1356 |
| 440 | 1319 | 1322 | 1325 | 1329 | $133^{2}$ | 1337 | 1341 | 1346 | 1352 | I3 58 | 144 |
| 50 | 1323 | 1327 | 1330 | 1334 | 1338 | 1343 | 1347 | 1353 | 1358 | 145 | 1411 |
| 520 | 1328 | 1332 | 1335 | I3 40 | I3 44 | 1349 | 1354 | 1359 | 14 | 1412 | 1419 |
| 540 | 1333 | 1337 | I3 41 | 1345 | 1350 | 1355 | 14 - | 146 | 1412 | 1419 | 1427 |
| 63 | 1338 | 1342 | 1346 | 1350 | I3 55 | 141 | I4 46 | 1413 | 1419 | 1426 | 1435 |
| 620 | I3 43 | 1347 | I3 51 | 1356 | 14 I | $14 \quad 7$ | 1412 | 1419 | 14 26 | 1434 | 1443 |
| 640 | I3 47 | 1352 | 1356 | 141 | 147 | 1413 | 1418 | 1426 | 1433 | 1442 | 1451 |
| 70 | I3 52 | 1357 | 14 I | 147 | 1412 | 1419 | 1425 | I4 32 | 1440 | 1449 | 1459 |
| 720 | 1357 | 142 | 147 | 1413 | 14 IS | 1425 | 1431 | 1439 | 1448 | 1457 | 15 7 <br> 15  |
| 740 | 142 | 147 | 1412 | 14 IS | 1424 | 1431 | 1438 | 1446 | 1455 | 154 | 1515 |
| 80 | 147 | 1412 | 1417 | 1423 | 1430 | 1437 | 1445 | I4 $5^{2}$ | 152 | 1512 | I5 23 |

table 94.
DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of } \\ & \text { of Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $71^{\circ}$ | $72^{\circ}$ | $73^{\circ}$ | $74^{\circ}$ | $75^{\circ}$ | $76^{\circ}$ | $77^{\circ}$ | $78^{\circ}$ | $79^{\circ}$ | $80^{\circ}$ |
|  | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
| $-8^{\circ} 0^{\prime}$ | 9 10 | 859 | S 47 | S 33 | S 17 | 758 | 737 | 710 | 638 | 556 |
| -740 | 9 IS | 9 os | S 56 | 843 | S 28 | S II | 750 | 726 | 656 | 6 I8 |
| 720 | 926 | 917 | 96 | 853 | S 39 | 823 | 84 | 741 | 714 | 638 |
| 7 0 | 935 | 926 | 916 | 93 | S 50 | S 35 | 817 | 756 | 731 | 658 |
| -640 | 943 | 934 | 925 | 914 | 9 I | S 47 | S 30 | S II | 747 | 717 |
| -620 | 951 | 943 | 934 | 924 | 912 | 859 | 843 | 825 | 83 | 736 |
| 6 - | 959 | 952 | 943 | 934 | 923 | 9 II | 856 | 839 | 819 | 754 |
| -540 | 107 | 101 | 953 | 944 | 934 | 922 | 99 | 853 | 834 | 811 |
| 520 | 1015 | 10 9 | $10 \quad 2$ | 953 | 944 | 934 | 922 | 97 | 850 | 828 |
| -5 | 10 23 | 1017 | IO II | 103 | 955 | 945 | 934 | 920 | 95 | 846 |
| -440 | 1031 | 10 26 | 1020 | 1013 | 105 | 956 | 946 | 934 | 919 | $9 \quad 2$ |
| -4 20 | 10 39 | 1034 | 10 29 | 1022 | 1015 | 10 7 | 958 | 947 | 934 | 918 |
| 40 | 10 47 | Io 43 | 10 38 | 1032 | 10 26 | 1018 | 1010 | 100 | 949 | 934 |
| -340 | 1055 | 1051 | 10 46 | 1041 | 10 36 | 1029 | IO 22 | 1013 | IO 3 | 950 |
| -320 | II 3 | Io 59 | 1055 | 1051 | 1046 | 1040 | 10 34 | Io 26 | 1017 | 106 |
| $-30$ | II II | II 8 | II 4 | II 0 | Io 56 | 1051 | 1045 | 10 39 | 1031 | 1022 |
| -240 | II 19 | II 16 | II 13 | II 10 | II 6 | II 2 | 10 57 | 1052 | 10 45 | 10 37 |
| 220 | II 26 | II 24 | II 22 | II 19 | II 16 | II 13 | 118 | 114 | 1059 | 1052 |
| 20 | I I 34 | II 32 | II 31 | II 28 | II 26 | II 23 | II 20 | 1117 | II I3 | II 8 |
| -140 | II 42 | 1141 | II 39 | 11138 | II 36 | I I 34 | II 32 | II 29 | II 26 | II 23 |
| 120 | II 49 | II 49 | II 48 | II 47 | II 46 | II 45 | II 43 | II 42 | II 40 | II 38 |
| - 10 | II 57 | II 57 | II 56 | II 56 | II 56 | I I 55 | II 55 | II 55 | II 54 | II 53 |
| -040 | 125 | 125 | 125 | 125 | 126 | 126 | 127 | 127 | 128 | 128 |
| -0 20 | 1213 | 1213 | 1214 | 1215 | 1216 | 1217 | 1218 | 1220 | 1221 | 1223 |
| 00 | 1220 | 1222 | 1222 | 1224 | 12. 26 | 1228 | 1229 | 1232 | 1235 | 1238 |
| +020 | 1228 | 1230 | 1231 | 1234 | 1236 | 1238 | 1241 | 1244 | 1249 | 1253 |
| - 40 | 1236 | 1238 | 1240 | 1243 | 1246 | 1249 | 1253 | 1257 | 132 | I3 9 |
| 10 | 1244 | 1246 | 1249 | 1252 | 1256 | 130 | 135 | 1310 | 1316 | I3 24 |
| I 20 | 1252 | 1255 | 1258 | $13 \quad 2$ | 136 | I3 II | 1316 | 1323 | 1330 | I3 40 |
| I 40 | 1259 | 133 | 137 | 13 II | 1316 | 1322 | 1328 | I3 36 | 13 44 | I 355 |
| 20 | $\begin{array}{ll}13 & 7\end{array}$ | 13 II | 1316 | 1320 | I3 26 | 1332 | 1340 | I3 49 | 1359 | 14 II |
| 220 | 1315 | 1319 | I3 25 | 1330 | I3 36 | I3 43 | $135^{2}$ | 141 | 1413 | 1427 |
| 240 | I3 23 | 1328 | 1333 | 1340 | I3 46 | I3 54 | 144 | 1414 | 1428 | 1443 |
| 30 | I3 3I | I3 36 | 1342 | 1349 | I3 57 | 14 | 1416 | 1428 | 1442 | 1459 |
| 320 | 1339 | I3 44 | 13 51 | 1359 | 147 | 1417 | 1428 | 1441 | 1456 | 1516 |
| 340 | I 347 | 1353 | 14 I | 148 | 1417 | 1428 | 1440 | 1455 | 15 II | I5 33 |
| 40 | 1355 | $14 \quad 2$ | 14 Io | 1418 | 1428 | 1440 | 1453 | 158 | 1527 | 1550 |
| 420 | 143 | 1410 | 1419 | 1428 | 1438 | 1451 | $15 \quad 5$ | I5 22 | 15.43 | 167 |
| 440 | 14 II | $14 \quad 19$ | 1428 | 1438 | 1449 | 152 | 1518 | I5 36 | 1558 | 1625 |
| 50 | 1419 | 1428 | 1437 | 1448 | 150 | 1514 | 1531 | 1550 | $16 \quad 14$ | 1644 |
| 520 | 1427 | 1437 | 1446 | 1458 | 15 II | 1526 | 1544 | 165 | 1631 | 173 |
| 540 | 1435 | 1445 | 1456 | I5 8 | 1522 | 1538 | 1557 | I6 20 | 1647 | 1722 |
| 60 | 1444 | 1454 | $15 \quad 5$ | 15 I9 | 1533 | 1550 | 16 II | I6 35 | 175 | 1743 |
| 620 | 1452 | $15 \quad 3$ | 15 | $15 \quad 29$ | 1544 | $16 \quad 3$ | 1625 | 1651 | 1723 | 185 |
| 640 | I5 I | 1512 | 1525 | I5 40 | 1556 | 1616 | 1639 | 17 | 1741 | $18 \quad 27$ |
|  | 15 IO | 1522 | 1535 | 1550 | 168 | 1629 |  | 1723 | 18 I | 1850 |
| 720 | 15 I8 | 1231 | 1545 | 161 | 1620 | 1642 | 178 | 1740 | 1821 | 1916 |
| 740 | 1527 | 1540 | 1555 | 1612 | 1632 | 1655 | 1723 | $175^{\text {S }}$ | 1842 | 1944 |
| 80 | I5 35 | I5 50 | $16 \quad 5$ | 1623 | 1644 | 179 | 1739 | I8 16 | 195 | 2015 |

DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of of } \\ & \text { the Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $60^{\circ}$ | $61^{\circ}$ | $62^{\circ}$ | $63^{\circ}$ | $64^{\circ}$ | $65^{\circ}$ | $66^{\circ}$ | $67^{\circ}$ | $68^{\circ}$ | $69^{\circ}$ | $70^{\circ}$ |
| $+8^{\circ} 0^{\prime}$ | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. | h. m. |
|  | 147 | 1412 | 1417 | 1423 | 1430 | 1437 | 1445 | 1453 | $15 \quad 2$ | 1512 | 1523 |
| +820 | 1412 | 14 I; | 1423 | I4 29 | 1436 | I4 43 | 1452 | 150 | 1510 | I5 20 | 1532 |
| 8 | 1417 | 1422 | 1428 | I4 35 | 1442 | 1450 | $145^{8}$ | 157 | 1517 | 1528 | 1540 |
|  | 1422 | 1427 | 1434 | 1441 | 1448 | 1456 | 15 | 1514 | 1525 | 1536 | 1549 |
| 920 | 1427 | 1432 | I4 39 | 1446 | 1454 | $15 \quad 2$ | 15 II | 1521 | 1532 | 1544 | 1557 |
| 940 | 1432 | $143^{8}$ | 1445 | $145^{2}$ | 150 | 159 | 15 I8 | 1528 | 1540 | 1552 | 166 |
| 100 | 1437 | 1443 | 1450 | $145^{8}$ | 156 | 1515 | 1525 | 1535 | 1547 | 16 | 1615 |
| 10 | 1442 | 1449 | 1456 | 154 | 1513 | 1522 | 1532 | 1543 | 1555 | 16 S | 1624 |
| 10 40 | 1447 | 1454 | $15 \quad 2$ | 15 Io | I5 19 | 1528 | 1539 | 1550 | 163 | 1617 | 1633 |
| $\begin{array}{cc} 11 & 0 \\ \text { II } & 20 \end{array}$ | 1452 | 1459 | 157 | 1516 | 1525 | 1535 | 1546 | 1558 | 16 II | 1626 | 1642 |
|  | 1457 | $15 \quad 5$ | 1513 | I5 22 | 1531 | 1541 | 1553 | 165 | 1619 | 1634 | 1652 |
|  | 152 | 1510 | 1519 | 1528 | 1538 | 1548 | 160 | 16 I3 | 1627 | 1643 | 171 |
|  | 158 | 1516 | 1525 | 1534 | 1544 | 1555 | 167 | 1621 | 1635 | 1652 | 17 II |
|  | 1513 | 1521 | 1531 | 1540 | 1550 | $16 \quad 2$ | 1615 | 1629 | 1644 | 17 1 | 1721 |
| $\begin{array}{ll}12 & 20 \\ 12 & 40\end{array}$ | 15 IS | 1527 | 1536 | 1546 | 1557 | 169 | 1622 | 1637 | 1653 | 17 II | 1731 |
| 13 | 1523 | 1533 | 1542 | 1553 | 16. 4 | 1616 | 1630 | 1645 | $17 \quad 2$ | 1720 | 1741 |
|  | 1529 | 1539 | 1548 | 1559 | 1611 | 1623 | 1637 | 1653 | 1710 | 1730 | 1752 |
| $\begin{array}{ll}13 & 20 \\ 13 & 40\end{array}$ | I 535 | I 544 | I5 55 | 165 | 1617 | 1631 | 1645 | 17 I | 1719 | 1740 | 183 |
| 140 | 1540 | 1550 | 161 | 1612 | 1624 | 1638 | 1653 | 1710 | 1729 | 1750 | 1814 |
| 1420 | 1546 | I $55^{6}$ | 167 | 1619 | 1631 | 1646 | 17 | 17 19 <br> 17 28 | 1738 | IS O |  |
| 14 | 155 I | 162 | 16 I 3 | 1625 | 1638 | 1653 | 179 | 1728 | 1748 | 18 II | 8 |
| 150 | 1557 | 168 | 1619 | 1632 | 1646 | 17 | 1717 | 1737 | 1758 | 1822 | 1850 |
| 1520 | 162 | 1614 | 1626 | 1639 | 1653 | 179 | 1726 | 1746 | I8 8 | 1833 | 193 |
| 15 | 168 | 1620 | 1632 | 1646 | 17 I | 1717 | I7 35 | 1755 | 1818 | 1845 | 1916 |
| 160 | 1614 | 1626 | 1639 | 1653 | 178 | 1725 | 1744 | I8 5 | 1829 | I8 57 | 1930 |
| 16 | 1620 | 1632 | 1646 | 17 - | 1716 | 1733 | 1753 | 1815 | 1840 | 1910 | 1945 |
| 16 | 1626 | 1639 | 1652 | $17 \quad 7$ | 1723 | 1741 | 182 | I8 25 | IS 51 | 1923 | 201 |
| 17 | 1632 | 1645 | 1659 | 1714 | 1731 | 1750 | 1811 | 1835 | 193 | 1936 | 2017 |
| 172 | 1638 | 1652 | 176 | 1722 | 1739 | 1759 | 1821 | 1846 | 1915 | 1950 | 2035 |
| 1740 | 1645 | 1658 | 1713 | 1729 | 1747 | 188 | 1831 | 1857 | 1928 | 206 | 2055 |
| 180 | 1651 | 175 | 1720 | 1737 | 1756 | 1817 | 184 I | 198 | 1941 | 2022 | 2117 |
| IS 20 | 1658 | 1712 | 1728 | 1745 | 185 | 1826 | 1852 | 1920 | 1955 | 2040 | 2142 |
| 18 | 174 | 1719 | 1735 | 1753 | 1814 | 1836 | 193 | 1933 | 2010 | 2059 | 22 I3 |
| 190 | 17 II | 1726 | 1743 | 182 | 1823 | 1846 | 1914 | 1946 | 2026 | 2120 | 2258 |
| 1920 | 1717 | 1733 | 1751 | 18 IO | 1832 | IS 56 | 1925 | 20 | 2044 | 2145 |  |
| 1940 | 1724 | I7 4I | 1759 | 1819 | 1841 | 197 | 1937 | 2014 | 213 | 2216 |  |
| 200 | 1731 | 1748 | 187 | IS 28 | 1851 | 1919 | 1950 | 2030 | 2123 | 2259 |  |
|  | 1738 | 1756 | 1815 | 1837 | 19 I | 1930 | 20.4 | 2047 | 2447 |  |  |
| $20 \quad 20$ $20 \quad 40$ | 1745 | I8 4 | I8 23 | 1846 | 1912 | 1942 | 2019 | 2 I 5 | 2217 |  |  |
| 210 | 1752 | 18 II | IS 32 | I8 56 | 1923 | 1925 | 2034 | 21 26 | 23 I |  |  |
| 2120 | 18 o | 1820 | 1841 | 196 | I9 34 | 208 | 2050 | 2150 |  |  |  |
| 2140 | 188 | 1828 | I8 50 | 1916 | 1946 | 2022 | 218 | 22 I9 |  |  |  |
| 220 | IS 16 | I8 37 | 19 o | 1927 | 1958 | 2037 | 2129 | $23 \quad 2$ |  |  |  |
| 2220 | I8 24 | I8 46 | 1910 | 1938 | 20 II | 2053 | 2152 |  |  |  |  |
| 2240 | IS 32 | I8 55 | 1920 | 1950 | 2025 | 2111 | 22 21 |  |  |  |  |
| 230 | 1841 | 194 | 1931 | $20 \quad 2$ | 2040 | 2131 | $23 \quad 3$ |  |  |  |  |
| $\begin{array}{lll}23 & 20 \\ 23 & 27\end{array}$ | 1849 | 1913 | 1941 | 2014 | 2056 | 2154 |  |  |  |  |  |
|  | IS 52 | 19 I7 | I9 46 | 2019 | 212 | 223 |  |  |  |  |  |

Table 94.
DURATION OF SUNSHINE AT DIFFERENT LATITUDES.

| $\begin{aligned} & \text { Declination } \\ & \text { of } \\ & \text { the Sun. } \end{aligned}$ | LATITUDE NORTH. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $71^{\circ}$ | $72^{\circ}$ | $73^{\circ}$ | $74^{\circ}$ | $75^{\circ}$ |
| $+8^{\circ} 0^{\prime}$ | 1. m1. | h. m. | h. m. | h. m. | h. m. |
|  | 1535 | 1550 | 165 | 1623 | 1644 |
| 820 | 1544 | 1559 | 1616 | 1635 | 1657 |
| S 40 | 1553 | 169 | 1626 | 1646 | 1710 |
| 90 | 163 | $16 \quad 19$ | 1637 | 1658 | 1723 |
| 920 | 1612 | 1629 | 1648 | 1710 | 1737 |
| 940 | 1622 | 1639 | 1659 | 1723 | 1751 |
| 100 | 1631 | 1650 | 17 II | 1735 | IS 5 |
| 1020 | 1641 | 17 o | 1722 | 1749 | IS 20 |
| Io 40 | 1650 | 17 II | 1734 | IS 2 | IS 36 |
| 110 | 17 I | 1722 | 1747 | IS I6 | If 52 |
| II 20 | 17 II | 1734 | 1759 | 1831 | 199 |
| II 40 | 1722 | 1745 | IS I3 | IS 46 | 1927 |
|  | 1732 | 1757 | IS 26 | 19 I | 1946 |
| 1220 | 1743 | IS 9 | IS 40 | 19 IS | 207 |
| 1240 | 1755 | 1822 | IS 55 | I9 35 | 2029 |
| 130 | 186 | 1835 | 19 II | I9 54 | 2055 |
| 1320 | IS 18 | IS 49 | 1926 | 2014 | 2123 |
| I 340 | IS 30 | 192 | 1943 | 2035 | 21 59 |
| $\begin{array}{cc} 14 & 0 \\ 14 & 20 \end{array}$ | IS 43 | 1917 | $20 \quad 1$ | 210 | 2250 |
|  | IS 56 | 1933 | 2020 | 2128 |  |
| 1440 | 19 Io | I9 49 | 2041 | 222 |  |
| 151515 | 1924 | $20 \quad 7$ | 2 I 5 | 2252 |  |
|  | I9 40 | 2026 | 2132 |  |  |
| 15 15 15 | I9 55 | 2046 | 225 |  |  |
| $\begin{array}{cc}16 & 0 \\ 16 & 20\end{array}$ | 2013 | 2110 | 2254 |  |  |
|  | 2031 | 2136 |  |  |  |
| 1640 | 2051 | 22 S |  |  |  |
| $\begin{array}{cc} 17 & 0 \\ 17 & 20 \\ 17 & 40 \end{array}$ | 2113 | 2256 |  |  |  |
|  | $\begin{array}{ll}21 & 39\end{array}$ |  |  |  |  |
|  | 22 II |  |  |  |  |
| 1740 | $76^{\circ}$ | $77^{\circ}$ | $78^{\circ}$ | $79^{\circ}$ | $80^{\circ}$ |
| + $8^{\circ} 0^{\prime}$ |  | 1739 | 1816 | 195 | 2015 |
| S 20 | 1723 | 1755 | IS 35 | 1929 | 2050 |
| 8 | 1738 | 1812 | 1856 | 1956 | 2133 |
| 90 | 1753 | 1830 | 1917 | 2025 | 2235 |
| 920 | IS 8 | IS 48 | 19 4I | 2059 |  |
| 940 | IS 25 | 19 S | 206 | 21 40 |  |
| 100 | IS 41 | 192 S | 2031 | 2239 |  |
| 1020 | IS 59 | 1950 | 216 |  |  |
| IO $4^{\circ}$ | 19 IS | 2015 | 2I 46 |  |  |
| 110 | 1938 | 2041 | 2243 |  |  |
| II 20 | 1959 | 2113 |  |  |  |
| II 40 | 2023 | 2150 |  |  |  |
| 120 | 2049 | 2246 |  |  |  |
| 1212 20 | 2119 |  |  |  |  |
|  | 2155 |  |  |  |  |

TABLE 95.
DECLINATION OF THE SUN FOR THE YEAR 1899, AT GREEN-

WICH APPARENT NOON.

| Day of Month. | Jan. | $F e b$. | Mur. |
| :---: | :---: | :---: | :---: |
| 1 | $-23^{\circ} 0^{\prime}$ | $-17^{\circ} \quad 4^{\prime}$ | $-7^{\circ} 33^{\prime}$ |
| 4 | -22 44 | $16 \quad 12$ | $6 \quad 24$ |
| 7 | $22 \quad 22$ | 15 I6 | $5 \quad 14$ |
| 10 | 2157 | $14 \quad 19$ | 44 |
| 13 | 2128 | 1319 | 253 |
| 16 | 2055 | 12 I8 | 142 |
| 19 | $20 \quad 19$ | II 14 | - 031 |
| 21 | 1953 | 1031 | +or6 |
| 24 | 19 II | 925 | 127 |
| 27 | 1826 | 8 IS | 239 |
| 30 | $17 \quad 38$ | . . | 343 |
|  | Apr. | May. | June. |
| 1 | $+4^{\circ} 34^{\prime}$ | $+15^{\circ} 6^{\prime}$ | $+22^{\circ} 4^{\prime}$ |
| 4 | 543 | 1559 | $22 \quad 27$ |
| 7 | 651 | 1650 | 2246 |
| 10 | $7 \quad 58$ | 1738 | 23 I |
| 13 | 94 | 1824 | 23 I3 |
| 16 | 109 | 197 | $23 \quad 22$ |
| 19 | 1112 | 1947 | $23 \quad 26$ |
| 2 I | 1153 | $20 \quad 12$ | $23 \quad 27$ |
| 2.4 | 1253 | $20 \quad 47$ | 2325 |
| 27 | 1351 | 2119 | 2320 |
| 30 | $144^{8}$ | 2 I 47 | 23 II |
|  | July. | Aug. | Sept. |
| 1 | $+23^{\circ} 7^{\prime}$ | $+15^{\circ} \mathrm{I}^{\prime}$ | $+8^{\circ} 17^{\prime}$ |
| 4 | 2253 | 17.15 | 7 II |
| 7 | 2236 | 1626 | 64 |
| 10 | 2215 | 1534 | 456 |
| 13 | 2150 | 1440 | $3 \quad 47$ |
| 16 | $2 \mathrm{I} \quad 22$ | 1344 | 238 |
| 19 | 20 51 | 1246 | 128 |
| 21 | $20 \quad 29$ | 127 | + o 42 |
| 24 | 1952 | II 6 | - 0 29 |
| 27 | 19 I 3 | 104 | I 39 |
| 30 | 1831 |  | 249 |
|  | Oct. | Noz'. | Dec. |
| I | $3^{\circ} 12^{\prime}$ | $-14^{\circ} 27^{\prime}$ | $-21^{\circ} 50^{\prime}$ |
| 4 | 422 | $15 \quad 24$ | 2216 |
| 7 | 5 31 | 16 I8 | 2238 |
| Io | 640 | 17 Io | $22 \quad 56$ |
| 13 | 7 4 | 18 o | 23 IO |
| 16 | 855 | 1846 | $23 \quad 20$ |
| 19 | 10 O | 1929 | $23 \quad 26$ |
| 2 I | 1043 | 1956 | $23 \quad 27$ |
| 24 | I I 47 | 2035 | $23 \quad 26$ |
| 27 | 1248 | 2 I 9 | $23 \quad 20$ |
| 30 | I3 49 | 2140 | 23 10 |

DURATION OF ASTRONOMICAL TWILIGHT.
(Interval between sunrise or sunset and the time when the true position of the sun's center is $18^{\circ}$ below the borizon.)


SMITHSONIAN TABLES.
(Interval between sunrise or sunset and the time when the true position of the sun's center is $6^{\circ}$ below the horizon.)
[Minutes.]

| Date. | north latitude. |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0^{\circ}$ | $10^{\circ}$ | 20 | $25^{\circ}$ | $30^{\circ}$ | $32^{\circ}$ | $34^{\circ}$ | $36^{\circ}$ | $38^{\circ}$ | $40^{\circ}$ | $42^{\circ}$ | $44^{\circ}$ | 46 | $48^{\circ}$ | $50^{\circ}$ |
| Jan. I | 22 | 22 | 24 | 25 | 27 | 27 | 28 | 28 | 29 | 30 | 32 | 33 | 34 | 36 | 39 |
| II | 22 | 22 | 24 | 25 | 26 | 27 | 28 | 28 | 29 | 30 | 31 | 32 | 33 | 35 | 38 |
| 21 | 22 | 22 | 23 | 24 | 26 | 26 | 27 | 27 | 28 | 29 | 30 | 32 | 33 | 34 | 37 |
| Feb. I | 22 | 22 | 23 | 24 | 25 | 26 | 27 | 27 | 27 | 28 | 29 | 31 | 32 | 34 | 35 |
| II | 22 | 22 | 22 | 23 | 25 | 26 | 26 | 27 | 27 | 28 | 29 | 30 | 31 | 33 | 34 |
| 1 | 21 | 22 | 22 | 23 | 24 | 25 | 25 | 26 | 27 | 28 | 28 | 29 | 30 | 32 | 33 |
| Mar. I | 21 | 22 | 22 | 23 | 24 | 24 | 25 | 26 | 27 | 28 | 28 | 29 | 30 | 31 | 33 |
| 11 | 21 | 21 | 22 | 23 | 24 | 24 | 25 | 26 | 26 | 27 | 27 | 29 | 30 | 31 | 32 |
| 21 | 21 | 21 | 22 | 23 | 24 | 24 | 25 | 26 | 26 | 27 | - 27 | 28 | 30 | 31 | 33 |
| Apr. I | 21 | 21 | 22 | 23 | 24 | 25 | 25 | 26 | 27 | 28 | 28 | 29 | 30 | 32 | 33 |
| II | 21 | 22 | 22 | 23 | 24 | 25 | 26 | 26 | 27 | 28 | 28 | 29 | 31 | 32 | 34 |
| 21 | 22 | 22 | 22 | 23 | 25 | 25 | 26 | 27 | 28 | 28 | 29 | 30 | 32 | 34 | 35 |
| May i | 22 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 28 | 29 | 30 | 32 | 33 | 35 | 36 |
| 11 | 22 | 22 | 23 | 24 | 26 | 27 | 28 | 29 | 29 | 30 | 31 | 33 | 35 | 36 | 39 |
| 21 | 22 | 22 | 24 | 25 | 27 | 28 | 28 | 29 | 30 | 31 | 33 | 35 | 36 | 38 | 4 I |
| June I | 22 | 22 | 24 | 25 | 27 | 28 | 28 | 29 | 31 | 32 | 34 | 36 | 37 | 40 | 43 |
| 11 | 22 | 23 | 24 | 26 | 28 | 28 | 29 | 30 | 31 | 33 | 34 | 36 | 38 | 41 | 44 |
| 21 | 22 | 23 | 25 | 26 | 28 | 29 | 29 | 30 | 31 | 33 | 34 | 36 | 38 | $4^{2}$ | 44 |
| July I | 22 | 23 | 24 | 26 | 28 | 28 | 29 | 30 | 31 | 33 | 34 | 36 | 38 | 4 I | 44 |
| II | 22 | 22 | 24 | 25 | 27 | 28 | 28 | 29 | 31 | 32 | 34 | 36 | 37 | 40 | 43 |
| 21 | 22 | 22 | 24 | 2.5 | 27 | 28 | 28 | 29 | 30 | 31 | 33 | 35 | 36 | 38 | 4 I |
| Aug. I | 22 | 22 | 23 | 24 | 26 | 27 | 28 | 29 | 29 | 30 | 31 | 33 | 35 | 36 | 39 |
| II | 22 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 28 | 29 | 30 | 32 | 33 | 35 | 36 |
| 21 | 22 | 22 | 22 | 23 | 25 | 25 | 26 | 28 | 28 | 28 | 29 | 30 | 32 | 34 | 35 |
| Sept. I | 21 | 22 | 22 | 23 | 24 | 25 | 26 | 26 | 27 | 28 | 28 | 29 | 31 | 32 | 34 |
|  | 21 | 21 | 22 | 23 | 24 | 25 | 25 | 26 | 27 | 28 | 28 | 29 | 30 | 31 | 33 |
| 21 | 21 | 21 | 22 | 23 | 24 | 24 | 25 | 26 | 26 | 27 | 27 | 29 | 30 | 31 | 32 |
| Oct. ${ }^{1}$ | 21 | 21 | 22 | 23 | 24 | 24 | 25 | 26 | 26 | 27 | 27 | 29 | 30 | 31 | 32 |
| II | 21 | 22 | 22 | 23 | 24 | 24 | 25 | 26 | 27 | 28 | 28 | 29 | 30 | 31 | 33 |
| 2 I | 21 | 22 | 22 | 23 | 24 | 25 | 25 | 26 | 27 | 28 | 28 | 29 | 30 | 32 | 33 |
|  | 22 | 22 | 22 | 23 | 25 | 25 | 26 |  | 28 | 28 | 29 | 30 |  |  | 34 |
| 11 | 22 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 28 | 29 | 30 | 31 | 32 | 33 | 35 |
| 21 | 22 | 22 | 23 | 24 | 26 | 26 | 27 | 28 | 28 | 29 | 30 | 32 | 33 | 34 | 37 |
| Dec. ${ }^{\text {I }}$ | 22 | 22 | 24 | 25 | 26 | 27 | 28 | 28 | 29 |  |  |  |  |  | 38 |
| II | 22 | 22 | 24 | 25 | 27 | 27 | 20 | 28 | 29 | 30 | 32 | 33 | 34 | 36 | 39 |
| 21 | 22 | 23 | 24 | 25 | 27 | 27 | 28 | 28 | 29 | 31 | 32 | 33 | 34 | 37 | 39 |

BMITHSONIAN TABLES.

Table 98.

## RELATIVE INTENSITY OF SOLAR RADIATION,

Mean intensity $J$ for 24 hours of solar radiation on a horizontal surface at the top of the atmosphere and the solar constant $A$,
in terms of the mean solar constant $A_{0}$.


Table 99.
RELATIVE AMOUNTS OF SOLAR RADIATION RECEIVED ON A HORIZONTAL SURFACE DURING THE YEAR AT DIFFERENT LATITUDES.

|  | ATMOSPHERIC TRANSMISSION COEFFICIENT. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| (North.) | 1.0 | 0.9 | 0.8 | 0.7 | 0.6 |
| Equator. | 439 | 374 | 316 | 262 | 213 |
| $10^{\circ}$ | 43.3 | 368 | 310 | 257 | 209 |
| $20^{\circ}$ | 416 | 350 | 293 | 2.42 | 195 |
| $30^{\circ}$ | 386 | 322 | 206 | 213 | 171 |
| $40^{\circ}$ | 347 | 28.4 | 231 | 185 | 144 |
| $50^{\circ}$ | 301 | 239 | 100 | I 49 | 114 |
| $60^{\circ}$ | 249 | 191 | 1.48 | 113 | 84 |
| $70^{\circ}$ | 207 | 152 | I 13 | 83 | 60 |
| $80^{\circ}$ | 192 | 13.4 | 94 | 6.4 | 43 |
| $90^{\circ}$ | ISI | 125 | S5 | 56 | 35 |

Table 100.
AIR MASS, M, CORRESPONDING TO DIFFERENT ZENITH DISTANCES OF THE SUN.

| Sun's zenitis distance. | Sun's zenith distance. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 1 | $2^{\circ}$ | 3 | 4 | 5 | $6^{\circ}$ | $7^{\circ}$ | $8^{\circ}$ | $9^{\circ}$ |
|  | AIR MISS. |  |  |  |  |  |  |  |  |  |
| 0 | 1. 00 |  |  |  |  |  |  |  |  |  |
| 10 | I. 02 |  |  |  |  | I. 04 |  |  |  |  |
| 20 | I. 06 | 1. 07 | 1. 08 | 1. 09 | I. O9 | I. 10 | 1. II | I. 12 | I. 13 | I. 14 |
| 30 | I. I 5 | I. 17 | I. 18 | I. 19 | I. 20 | 1. 22 | 1. 23 | I. 25 | I. 27 | I. 28 |
| 40 | 1. 30 | 1. 32 | I. 34 | I. 37 | I. 39 | I. 41 | I. 44 | I. 46 | r. 49 | I. 52 |
| 50 | 1. 55 | 1. 59 | 1. 62 | I. 66 | 1. 70 | I. 74 | 1. 78 | 1. 83 | 1. 88 | I. 9.4 |
| 60 | 2.00 | 2.06 | 2. 12 | 2. 19 | 2. 27 | 2.36 | 2.45 | 2.55 | 2.65 | 2.77 |
| 70 | 2.90 | 3.05 | 3. 21 | $3 \cdot 39$ | $3 \cdot 59$ | 3.82 | 4.07 | 4.37 | 4.72 | 5.12 |
| So | 5.60 | 6. IS | 6. 88 | 7. 77 | 8.00 | 10. 30 | 12.44 | $15 \cdot 36$ | 19.79 | 26.96 |

Table 101.
RELATIVE ILLUMINATION INTENSITIES.

| Source of illumination. | Intensity | Ratio to zenithal full moon. |
| :---: | :---: | :---: |
| Zenithal sun | Foot-candles. 9600. 0 | 465000.0 |
| Sky at sunset | 33.00 | 1650.0 |
| Sky at end of civil twilight. | 0.40 | 20.0 |
| Zenithal full moon. | 0.02 | I. 0 |
| Quarter moon | 0. 002 | o. I |
| Starlight. | 0.00008 | 0.004 |

## MISCELLANEOUS TABLES.

Weight in grams of one cidic centineter of alr.
English measures-Temperature term ..... Table 102
Humidity term ; auxiliary table ..... Table ioz
Humidity and pressure terms, com- bined ..... Table iot
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Table 102.

## WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Temperature term: $\delta_{t}=\frac{0.0012930}{1+0.002039\left(t-32^{\circ}\right)}$ Fahrenheit temperatures. I cubic centimeter of dry air at the temperature of $32^{\circ} \mathrm{F}$. and pressure 760 mm ., under the standard value of gravity, weighs 0.0012930 gram .

| Tempera- | $\delta_{t}$ | Log $\delta_{t}$ | Tempera- | $\delta_{t}$ | $\log \delta_{t}$ | $\begin{aligned} & \text { Tempera- } \\ & \text { ture } \end{aligned}$ | $\delta_{t}$ | $\log \delta_{t}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | 0.00 | -10 | , | 0.00 | -10 | $\mathrm{F}_{75}$ | 0.00 | -10 |
| $-45^{\circ}$ | 15338 | 7.18577 | $30^{\circ}$ | 12983 | 7.11339 | $75^{\circ}$ | 11888 | 7.07512 |
| -40 | 15155 | . 18056 | 31 | 12956 | . 11247 | 76 | 11866 | . $07+30$ |
| -35 | 14976 | . 17540 | 32 | 12930 | . 11160 | 77 | 11843 | . 07346 |
| -30 | 14801 | .17029 | 33 | 12904 | .11073 | 78 | 1182 I | . 07265 |
| -25 | 14630 | .16524 | 34 | 12877 | .10981 | 79 | 11799 | .07185 |
| -20 | $\stackrel{\text { O.00 }}{14463}$ | 7.16026 | 35 | 0.00 | 7.10894 | 80 | 0.00 11777 | 7.07103 |
| -18 | 14398 | $\stackrel{.}{.15831}$ | 36 | 12825 | . 10806 | 81 | 11756 | . 07026 |
| 16 | 14333 | . 5634 | 37 | 12800 | . 10721 | 82 | 11734 | . 06946 |
| -14 | 14268 | . 54336 | 38 | 12774 | . 10633 | 83 | 11712 | . 06863 |
| $-12$ | 14204 | . 524 I | 39 | 12748 | . 10544 | 84 | 11691 | . 06785 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| -10 | 14141 | 7.15048 | 40 | 12722 | 7.10456 | 85 | 11669 | 7.06703 |
| -8 | 14078 | .14854 | $4{ }^{1}$ | 12697 | . 10370 | 86 | 11648 | . 06625 |
| 6 | 14016 | . 14663 | 42 | 12672 | . 10285 | 87 | 11626 | . 06543 |
| 4 | 13954 | . 14470 | 43 | 12646 | . 10195 | 88 | 11605 | . 06466 |
| 2 | 13893 | . 14279 | 44 | 12621 | . 10109 | 89 | 11584 | . 06387 |
| $\pm 0$ | 0.00 13832 | 7.14088 | 45 | O. 00 <br> 12596 | 7.10023 | 90 | ${ }_{1}^{0.00} 11563$ | 7.06307 |
| + I | I 3803 | . 13997 | 46 | 12571 | . 09937 | 91 | 11542 | . 06228 |
|  | 13773 | . 13903 | 47 | 12546 | .09851 | 92 | 11521 | .06149 |
| 3 | 13743 | . 13808 | 48 | 12522 | . 09767 | 93 | 11500 | . 06070 |
| 4 | 13713 | .13713 | 49 | 12497 | . 09682 | 94 | 11479 | . 05992 |
| 5 | 0.00 13683 | 7.13618 | 50 | ${ }_{12472}^{0.00}$ | 7.09594 | 95 | 0.00 I 1458 | 7.05913 |
| 6 | 13654 | . 13527 | 51 | $12+48$ | . 09511 | 96 | 11438 | . 05835 |
| 7 | 13625 | . 13434 | 52 | $12+24$ | .09426 | 97 | 11417 | . 05755 |
| 8 | 13595 | . 13338 | 53 | 12399 | . 09338 | 98 | 11396 | . 05675 |
| 9 | 13566 | .13245 | 54 | 12375 | . 09256 | 99 | 11376 | . 05600 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| 10 | 13537 | 7.13152 | 55 | 12351 | 7.09171 | 100 | 11356 | 7.05523 |
| 11 | 13508 | . 13062 | 56 | 12327 | . 09087 | 101 | 11335 | .05442 |
| 12 | 13480 | . 12970 | 57 | 12303 | . 09002 | 102 | 11315 | . 05367 |
| 13 | 13451 | . 12875 | 58 | 12279 | . 08916 | 103 | 11295 | . 05290 |
| 14 | 13423 | . 12785 | 59 | 12255 | . 08831 | 104 | 11275 | . 05213 |
| 15 | 0.00 13394 | 7.12691 | 60 | ${ }^{0.00} 12232$ | 7.08750 | 105 | $\xrightarrow{0.00} 11254$ | 7.05I3I |
| 16 | 13366 | . 12600 | 61 | 12208 | . 08665 | 106 | 11235 | . 05058 |
| 17 | 13338 | . 12510 | 62 | 12185 | . 08583 | 107 | 11215 | . 04982 |
| 18 | 13310 | . 12419 | 63 | 12161 | . 08497 | 108 | 11195 | . 04902 |
| 19 | 13282 | . 12328 | 64 | 12138 | .08416 | 109 | 11175 | . 04824 |
| 20 | 0.00 | 7.12235 | 65 | 0.00 12115 | 7.08334 | 110 | ${ }_{\substack{0.00 \\ 1156}}$ | 7.04752 |
| 21 | 13227 | . 121214 | 66 | 12092 | . 08251 | 112 | 11117 | . 04599 |
| 22 | 13199 | . 12054 | 67 | 12069 | .08168 | 114 | 11078 | . 04447 |
| 23 | 13172 | . 11966 | 68 | 12046 | . 08085 | 116 | 11039 | . 04293 |
| ${ }^{2}+$ | 13144 | . 11873 | 69 | 12023 | . 08003 | 118 | 11001 | . 04145 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| 25 | 13117 | 7.11783 | 70 | 12000 | 7.07918 .07839 | 120 | 10963 | 7.03994 |
| 27 | 13090 | . 11604 | 72 | 11955 | . 07755 | 130 | 10869 | . 03250 |
| 28 | 13036 | .11514 | 73 | 11933 | . 07675 | 135 | 10686 | . 02883 |
| 29 | 13010 | . 11428 | 74 | 11910 | . 07593 | 140 | 10597 | . 02518 |

Smithsonian Tables

## WEICHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.

Humidity term: Values of 0378 e.
Auxiliary to Table 104.
(See Tables 74 and 75.) $e=$ Vapor pressure in inches.

Temperature by normal hydrogen thermometer.

| DewPoint |  | 0.378 e | DewPoint. | Vapor Pressure. <br> (*) | 0.378 e | DewPoint. | Vapor Pressure. 0.3 (Water.) | 0.378 e | DewPoint. | Vapor Pressure. (Water.) | 0.378 e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F. | Inch. | Inch. | F. | Inch. | Inch. | F. | Inch. | Inch. |  | Inches. In | Inches. |
| $-60^{\circ}$ | 0.0010 | 0.000 | $-10^{\circ}$ | 0.0223 | 0.008 | $40^{\circ}$ | 0.24770 | 0.094 | $90^{\circ}$ | 1.423 | 0.538 |
| -60 | . 001 I | . 000 | 9 | . 0236 | . 009 | 41 | . 2575 | . 097 | 91 | 1. 469 | . 555 |
| 58 | . 0011 | . 00 | 8 | . 0249 | . 009 | 42 | . 2677 | .101 | 92 | I. 515 | . 573 |
| 57 | . 0012 | . 000 | 7 | . 0263 | . 010 | 43 | . 2782 | . 106 | 93 | 1.563 | . 591 |
| 56 | . 0013 | - | 6 | . 0277 | . 010 | 44 | . 2801 | . 100 | 94 | 1.612 | . 609 |
| -55 | 0.0014 | 0.001 | 5 | 0.0292 | 0.011 | 45 | 0.3003 | 0.114 | 95 | 1.662 | 0.628 |
| 54 | . 0015 | . 001 | 4 | . 0308 | . 012 | 46 | . 3120 | . 18 | 96 | 1.714 | . 648 |
| 53 | .0016 | . 001 | 3 | . 0325 | . 012 | 47 | -3240 | I2 | 97 08 | 1.767 1.822 | . 689 |
| 52 | . 0017 | . 001 | 2 | . 0343 | . 013 | 48 | . 3365 | .127 .132 | 99 | 1.878 | . 710 |
| 51 | .0018 | . 001 |  | . 0361 | . 014 | 49 50 | .3493 0.3626 | -.137 | 100 | 1.936 | 0.732 |
| $-50$ | 0.0020 | 0.001 | $\begin{array}{ll} \pm & 0 \\ +\quad 1\end{array}$ | 0.0381 .0401 | 0.014 .015 | 5 I | 0.3626 .3763 | . 142 | IOI | 1.994 | . 754 |
| 49 | . 0021 | . .001 | + 1 | . 0401 | .015 .016 | 5 | . 3905 | . 147 | 102 | 2.055 | . 777 |
| 47 | . 0024 | . 001 | 3 | . 0445 | . 017 | 53 | . 4052 | . 153 | 103 | 2.117 | . 800 |
| 46 | . 0026 | . 001 | 4 | . 0468 | . 018 | 54 | . 4203 | . 159 | 104 | 2.181 | . 824 |
| -45 | 0.0028 | 0.001 | $+5$ | 0.0493 | 0.019 | 55 | 0.4359 | -. 165 | 105 | 2.246 | 0.849 |
| 44 | . 0029 | . 001 | 6 | . 0519 | . 020 | 56 | . 4521 | . 171 | 106 | 2.314 | . 875 |
| 43 | .0031 | . 01 | 7 | . 0546 | . 021 | 57 | . 4687 | . 177 | 107 | 2.382 | .900 |
| 42 | . 0033 | . 001 | 8 | . 0574 | . 022 | 58 | . 4859 | . 184 | 108 | 2.453 | . 927 |
| 41 | . 0036 | . 001 | 9 | . 0604 | . 023 | 59 | . 5037 | . 190 | 109 | 2.525 | . 954 |
| -40 | 0.co38 | 0.001 | $+10$ | 0.0635 | 0.024 | 60 | 0.5220 | 0.197 | 110 | 2.599 2.676 | 0.982 1.012 |
| 39 | . 0040 | . 002 | 11 | . 0667 | . 025 | 61 | . 5409 | .204 .212 | III | 2.676 2.754 | 1.012 |
| 38 | . 0043 | . 002 | 12 | . 0701 | .027 .028 | 62 63 | .5604 .5805 | .212 .219 | II3 | 2.754 2.833 | 1.041 |
| 37 | . 0046 | . 002 | I3 | . 0736 | . 0228 | 64 | . 6013 | . 227 | 114 | 2.915 | 1.102 |
| 36 -35 | . 0049 | . 002 | +15 | .0773 0.0812 | 0.031 | 65 | 0.6226 | 0.235 | 115 | 2.999 | 1.I34 |
| $\begin{array}{r}-35 \\ \hline 34\end{array}$ | 0.0052 | 0.002 .002 | 15 +15 | 0.0812 .0852 | 0.031 .032 | 66 | . 6447 | . 244 | 116 | 3.085 | I. 166 |
| 34 33 | .0055 | . 002 | 17 | . 0895 | . 034 | 67 | . 6674 | . 252 | 117 | 3.173 | 1.199 |
| 32 | . 0062 | 2 | 18 | . 0939 | . 035 | 68 | . 6909 | . 261 | 118 | 3.264 | 1. 234 |
| 31 | . 0066 | . 003 | 19 | . 0985 | . 037 | 69 | . 7150 | . 270 | 119 | 3.356 |  |
| -30 | 0.0070 | 0.003 | +20 | 0.1033 | 0.039 | 70 | 0.7399 | 0.280 | 120 | 3.451 | 1. 304 |
| 29 | . 0075 | . 003 | 21 | . 1084 | . 041 | 71 | . 7655 | . 289 | 121 | 3.548 | 1.341 |
| 28 | . 0080 | . 003 | 22 | .1136 | . 043 | 72 | . 7919 | . 299 | 122 | 3.647 | 1.379 $\mathbf{1 . 4 1 7}$ |
| 27 | . 0084 | . 003 | 23 | . 1191 | . 045 | 73 | .8191 .8471 | . 310 | 123 124 | 3.749 3.853 | 1.41756 1.45 |
| 26 | . 0090 | . 003 | 24 | . 1248 | . 047 | 74 | . 8471 | . 320 | 124 125 | 3.853 3.960 | 1.456 1.497 |
| -25 | 0.0095 | 0.004 | +25 | 0. 1308 | 0.049 | 75 | 0.8760 .9056 | 0.331 .343 | 125 126 | 3.960 4.069 | 1.497 <br> 1.538 <br> 1.580 |
| 24 | . 0101 | . 004 | 26 | . 1370 .1435 | .052 <br> .054 | 76 | . 9056 | .343 .354 | 127 | 4.180 | 1.580 |
| 23 | . 0107 | . 004 | 27 28 | .1435 .1502 | 2 $\begin{aligned} & .054 \\ & .057\end{aligned}$ | 77 78 | . 93677 | . .366 | 128 | 4.294 | 1.623 |
| 22 | . 0113 | . 004 | 28 29 | .1502 .1573 | 2-057 | 79 | . I .0001 | . 378 | 129 | 4.412 | 1.668 |
| -21 | .0120 0.0127 | . 0.005 | + +30 | -. 1646 | 0.062 | 80 | I. 0334 | 0.391 | 130 | 4.531 | 1.713 |
| -20 19 | 0.0127 .0135 | $\begin{array}{r}\text {. } \\ .005 \\ \hline\end{array}$ | +31 31 | 0.1646 .1723 | - 066 | 81 | 1.0676 | - 404 | 131 | 4.654 | 4 I .759 |
| 18 | . 0143 | . 0005 | - 32 | . 1803 | 3 .068 | 82 | I.,1029 | . 417 | 132 | 4.779 | 1.806 |
| 17 | . 0151 | . 006 | 33 | . 1877 | 7 . 071 | 83 | 1.1392 | - 431 | 133 | 4.907 | 1.85 |
| 16 | . 0160 | . 006 | - 34 | . 1954 | 4 . 074 | 84 | 1. 1765 | - 445 | 134 | 5.038 | 1.90 |
| -15 | 0.0169 | -0.006 | +35 | 0.2034 | $4 \quad 0.077$ | 85 | 1.2149 | 0.459 | 135 | 5.172 | 1.95 |
| 14 | . 0179 | . .007 | 76 | . 2117 | 7 .080 | 86 | 1.2543 | - 474 | 136 | 5.309 | 92.00 |
| 13 | . 0189 | $9 . .007$ | 737 | . 2202 | $2 . .083$ | 87 | 1. 2949 | -480 | 137 | 5.449 | $9{ }^{2.06}$ |
| 12 | . 0200 | -.008 | 8 38 | . 2291 | $1 \quad .087$ | 88 | 1.3365 | 5 . 505 | 138 | 5.592 | 2.11 |
| 1 I | . 0211 | 1 . 008 | 839 | . 2382 | 2.090 | - 89 | 1.3794 | 4 . 521 | 139 | 5.739 |  |
| 10 | 0.0223 | 30.008 | 840 | 0.2477 | $7 \quad 0.094$ | 90 | 1.4234 | 40.538 | 140 | 5.889 | 9 2.22 |

Smithsonian tables.

Table 104.
WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.
Humidity and pressure terms combined: $\frac{\delta}{\delta_{0}}=\frac{h}{29.92 \mathrm{I}}=\frac{B-0.378 e}{29.92 \mathrm{I}}$.
$B=$ Barometric pressure in inches; $e=$ Vapor pressure in inches.

| h. | $\frac{\mathrm{h}}{29.921}$. | $\log \frac{h}{29.92 \mathrm{I}}$. | h. | $\frac{\mathrm{h}}{29.291}$. | $\log \frac{\mathrm{h}}{29.92 \mathrm{I}}$. | h. | $\frac{\mathrm{h}}{29.92 \mathrm{I}}$. | $\log \frac{h}{29.92 \mathrm{I}}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inch's. |  | - 10 | Inches. |  | - 10 | Inches |  | - 10 |
| 10.0 | 0.3342 | 9.52.402 | 15.0 | 0.5013 | 9.70012 | 20.0 | 0.6684 | 9.82505 |
| 10.I | . 3376 | . 52835 | 15.1 | . 50.47 | .70300 | 20.1 | .6718 | . 82722 |
| 10.2 | . 3409 | . 53262 | 15.2 | . 5080 | .70587 | 20.2 | .675I | . 8293 S |
| 10.3 | - 3442 | . 53686 | 15.3 | . 5113 | . 7081 I | 20.3 | . 6784 | . 83152 |
| 10.4 | . 3476 | -54106 | I5.4 | -5I47 | .71154 | 20.4 | .68ı8 | . 83365 |
| 10.5 | 0.3509 | 9.54521 | 15.5 | c. 518 So | 9.71.435 | 20.5 | 0.6851 | 9. $8_{357} 8$ |
| 10.6 | . 3543 | . 54933 | I5.6 | .52I4 | .71715 | 20.6 | . 6885 | . 83789 |
| 10.7 | . 3576 | . 5534 I | 15.7 | . 5247 | . 71992 | 20.7 | .6918 | . 83999 |
| 10.8 | . 3609 | . 55745 | 15.8 | . 5281 | . 72268 | 20.8 | . 6952 | . 84209 |
| 10.9 | . 3643 | . 56145 | I5.9 | .5314 | . 72542 | 20.9 | . 6985 | . 84417 |
| 11.0 | 0.3676 | 9.56542 | 16.0 | 0.5347 | 9.728 I 4 | 21.0 | 0.7018 | 9. 84624 |
| II.I | . 3710 | . 56935 | 16.1 | . 5381 | .73085 | 21.1 | . 7052 | . 8483 I |
| 11.2 | - 3743 | - 57324 | I6.2 | . 5414 | .73354 | 2 I .2 | .7085 | . 55036 |
| 11.3 | . 3777 | . 57710 | 16.3 | . $5+48$ | . 7362 I | 21.3 | .7119 | . 55240 |
| II. 4 | -3SIO | . 58093 | 16.4 | .548I | .73887 | 21.4 | .7152 | . $S_{5444}$ |
| 11.5 | 0.3S43 | 9.5S472 | 16.5 | 0.5515 | $9.74{ }^{151}$ | 21.5 | 0.7186 | 9. 85646 |
| II. 6 | . 3 S77 | . 58848 | 16.6 | . 5548 | .74413 | 21.6 | .7219 | . 55848 |
| 11.7 | . 3910 | . 59221 | 16.7 | .5581 | . 74674 | 21.7 | . 7252 | . 86048 |
| II.S | . $39+4$ | . 59591 | 16.8 | . 5615 | .74933 | 21.8 | . 7286 | . 86248 |
| 11.9 | - 3977 | . 59957 | 16.9 | . 56.48 | .75191 | 21.9 | .7319 | . S 6447 |
| 12.0 | 0.4011 | c. 6032 I | 17.0 | 0.5682 | 9.75447 | 22.0 | 0.7353 | 9. 56645 |
| 12.I | . 40.44 | .6068i | 17.1 | . 5715 | .75702 | 22.1 | .7386 | . 56842 |
| 12.2 | . 4077 | .6103S | 17.2 | . 5748 | . 75955 | 22.2 | . 7420 | . 87038 |
| 12.3 | .4111 | .6I393 | 17.3 | . 5782 | .76207 | 22.3 | . 7453 | . 87233 |
| 12.4 | .4144 | . 61745 | 17.4 | . $5^{\text {SI } 5}$ | . 76.457 | 22.4 | .7486 | . 87427 |
| 12.5 | 0.4178 | 9.62093 | 17.5 | 0.5S49 | 9.76706 | 22.5 | 0.7520 | 9. 87621 |
| 12.6 | . 42 I I | . 62439 | 17.6 | . 5 SS2 | . 76954 | 22.6 | . 7553 | .87Si3 |
| 12.7 | . 4244 | . 62782 | 17.7 | . 5916 | . 77200 | 22.7 | .7587 | . 88005 |
| 12.8 | .4278 | . 63123 | 17.8 | - 5949 | . 77444 | 22.8 | .7620 | .S8196 |
| 12.9 | . 43 II | .6346I | 17.9 | . 5982 | .77687 | 22.9 | .7653 | . 88356 |
| 13.0 | 0.4345 | 9.63797 | 18.0 | 0.6016 | 9.77930 | 23.0 | 0. 7687 | 9.8S575 |
| I3. I | . 4378 | .64130 | IS. I | . 60.49 | .78izo | 23. I | .7720 | . SS764 |
| 13.2 | .4412 | . 64460 | IS. 2 | $.608_{3}$ | .784 10 | 23.2 | .7754 | . S895 I |
| 13.3 | . 4445 | .64788 | IS. 3 | .6116 | . 786.48 | 23.3 | .7787 | . 89138 |
| I 3.4 | . 4478 | .65113 | IS.4 | .6I49 | .78884 | 23.4 | .7821 | . 89324 |
| 13.5 | 0.4512 | 9.65436 | 18.5 | 0.6183 | 9.79120 | 23.5 | 0. 7854 |  |
| 13.6 | . 4545 | . 65756 | i8.6 | . 6216 | . 79354 | 23.6 | . 7887 | . 89693 |
| 13.7 | . 4579 | . 66074 | 18.7 | . 6250 | . 79587 | 23.7 | . 792 I | . 89877 |
| I 3.8 | .4612 | . 66390 | 18.8 | .6283 | .798i8 | 23.8 | . 7954 | . 90060 |
| I 3.9 | . 46.46 | .66704 | 18.9 | . 6317 | . 50049 | 23.9 | .7988 | .902 .42 |
| 14.0 | 0.4679 | 9.67015 | 19.0 | 0.6350 | 9. $\mathrm{SO} 27^{7} \mathrm{~S}$ | 24.0 | 0. So 21 | 9.90424 |
| 14. I | . 4712 | . 67324 | 19.I | . 6383 | . 80506 | 2.4. 1 | . 8054 | . 90604 |
| 14.2 | . 4746 | . 6763 I | 19.2 | . 6.417 | . 80733 | 2.4 .2 | . $\mathrm{SoS8}$ | .90784 |
| 14.3 | .4779 | . 67936 | 19.3 | . 6450 | . So95S | 2.4 .3 | . SI2 I | .90963 |
| 14.4 | .4SI 3 | . 68239 | 19.4 | .6484 | . $\mathrm{SIIS}_{3}$ | 2.4 .4 | .SI55 | .91141 |
| 14.5 | 0.4846 | 9.65539 | 19.5 | 0.6517 | 9. SI 406 | 24.5 | o. SISS | 9.91319 |
| 14.6 | . 4879 | . 68537 | 19.6 | . 655 I | . Si62S | 2.4 .6 | . 8222 | . 91496 |
| 14.7 | . 4913 | . 69134 | 19.7 | . 6584 | . Sis49 | 24.7 | . 2255 | .91672 |
| 14.8 | . 4946 | . 69429 | 19.8 | . 6617 | . 82069 | 2.4 .8 | . S 2 S 9 | .91848 |
| 14.9 | .498o | . 6972 r | 19.9 | . 665 I | . 82288 | 24.9 | .$S_{322}$ | . 92022 |

WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.
Humidity and pressure terms combined: $\frac{\delta}{\delta_{0}}=\frac{h}{29.92 \mathrm{I}}=\frac{B-0.378 e}{29.92 \mathrm{I}}$.
$B=$ Barometric pressure in inches; $e=$ Vapor pressure in inches.

| h. | $\frac{h}{29.921}$ | $\log \frac{h}{29.92 I}$ | h. | $\frac{\mathrm{h}}{29.92 \mathrm{I}}$ | $\log \frac{\mathrm{h}}{29.92 \mathrm{I}}$ | h. | $\frac{h}{29.921}$ | $\log \frac{\mathrm{h}}{29.92 \mathrm{I}}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inches. |  | - 10 | Inches. |  | - 10 | Inches. |  | - 10 |
| 25.00 | 0.8355 | 9.92196 | 27.25 | 0.9107 | 9.95939 | 29.50 | 0.9859 | 9.99385 |
| 25.05 | . 8372 | . 92283 | 27.30 | . 9124 | . 96019 | 29.55 | . 9876 | . 99458 |
| 25. 10 | . 8.389 | . 92370 | 27.35 | .914I | . 96008 | 29.60 | . 9893 | . 99532 |
| 25. 15 | . 8.405 | .92456 | 27.40 | .9157 | . 96177 | 29.65 | . 9909 | . 99605 |
| 25.20 | . 8.422 | . 92542 | 27.45 | .9174 | .96256 | 29.70 | . 9926 | . 99678 |
| 25.25 | o. 8439 | 9.92628 | 27.50 | 0.9191 | 9.96336 | 29.75 | 0.9943 | 9.9975 I |
| 25.30 | . 8456 | . 92714 | 27.55 | . 9208 | . 96414 | 29.80 | . 9960 | . 99824 |
| 25.35 | . 8472 | . 92800 | 27.60 | . 9224 | . 96493 | 29.85 | . 9976 | . 99897 |
| 25.40 | . 8489 | . 92886 | 27.65 | . 9241 | . 96572 | 29.90 | . 9993 | . 99970 |
| 25.45 | . 5506 | . 9297 I | 27.70 | .925 S | . 96650 | 29.95 | 1. 0 OIO | 0.00042 |
| 25.50 | 0.8522 | 9.93056 | 27.75 | 0.9274 | 9.96728 | 30.00 | 1.0026 | 0.00115 |
| 25.55 | . 8539 | . 93141 | 27.80 | . 9291 | . 96807 | 30.05 | I. 0043 | .00187 |
| 25.60 | . 8556 | . 93226 | 27.85 | . 9308 | . 96885 | 30. 10 | 1.0060 | . 00259 |
| 25.65 | . 8573 | . 9331 I | 27.90 | . 9325 | . 96963 | 30.15 | 1.0076 | . 00331 |
| 25.70 | .85S9 | . 93396 | 27.95 | . 9341 | . 97040 | 30.20 | 1.0093 | . 00403 |
| 25.75 | 0.8606 | 9.93480 | 28.00 | $0.935^{8}$ | 9.97118 | 30.25 | I. Ol 10 | 0.00475 |
| 25.80 | . 8623 | . 93564 | 28.05 | . 9375 | . 97195 | 30.30 | 1. 0127 | . 00547 |
| 25.85 | . 8639 | .93648 | 28. 10 | . 9391 | . 97273 | 30.35 | I. 0143 | . 00618 |
| 25.90 | . 8656 | . 93732 | 28.15 | . 9408 | . 97350 | 30.40 | 1.0160 | .00690 |
| 25.95 | . 8673 | .93816 | 28.20 | - 9425 | . 97427 | 30.45 | 1.0177 | .00761 |
| 26.00 | 0. 8690 | 9.93900 | 28.25 | 0.944 I | 9.97504 | 30.50 | 1.0193 | 0.00832 |
| 26.05 | . 8706 | . 93983 | 28.30 | . 9458 | .975SI | 30.55 | 1.0210 | . 00903 |
| 26. 10 | . 8723 | . 94066 | 28.35 | . 9475 | . 97657 | 30.60 | 1.0227 | . 00975 |
| 26. 15 | . 8740 | .94149 | 28.40 | . 9492 | . 97734 | 30.65 | 1. 0244 | . 01045 |
| 26.20 | . 8756 | . 94233 | 28.45 | . 9508 | .97810 | 30.70 | 1.0260 | .OIII6 |
| 26.25 | 0. 8773 | 9.94315 | 28.50 | 0.9525 | 9.97887 | 30.75 | 1.0277 | 0.01187 |
| 26.30 | . 8790 | . 94398 | 28.55 | . 9542 | . 97963 | 30.80 | 1.0294 | . 01257 |
| 26.35 | . 8806 | . 94480 | 28.60 | . 9558 | . 98039 | 30.85 | 1.0310 | . 01328 |
| 26.40 | . 8823 | . 94563 | 28.65 | . 9575 | .98is | 30.90 | 1.0327 | . 01398 |
| 26.45 | .8840 | . 94645 | 28.70 | . 9592 | .98i91 | 30.95 | 1. 0344 | . 01468 |
| 26.50 | 0. 8857 | 9.94727 | 28.75 | 0.9609 | 9.98266 | 31.00 | 1.0361 | 0.01539 |
| 26.55 | . 8873 | .94So9 | 2 2. So | . 9625 | . 98342 | 31.05 | 1.0377 | . 01608 |
| 26.60 | . 8890 | .94891 | 28.85 | . 9642 | . 98417 | 31.10 | 1. 0394 | .01678 |
| 26.65 | . 8907 | . 94972 | 28.90 | . 9659 | . 98492 | 3 I. 15 | 1.04II | . 01748 |
| 26.70 | . 8924 | . 95054 | 28.95 | .9675 | .98567 | 31.20 | 1. 0427 | . 01818 |
| 26.75 | 0.8940 | 9.95135 | 29.00 | 0.9692 | 9.98642 | 31.25 | I. 0444 | ヘ.01887 |
| 26.80 | . S 957 | . 95216 | 29.05 | . 9709 | . 98717 | 31.30 | I. 0461 | . 01957 |
| 26.85 | . 8974 | . 95297 | 29. 10 | . 9726 | . 98792 | 31.35 | 1.0478 | . 02026 |
| 26.90 | . 8990 | .95378 | 29.15 | . 9742 | .9SS66 | 3 I .40 | 1.0494 | . 02095 |
| 26.95 | .9007 | . 95458 | 29.20 | . 9759 | . 98941 | 3 I .45 | I. 051 I | . 02164 |
| 27.00 | 0.9024 | 9.95539 | 29.25 | 0.9776 | 9.99015 | 31.50 | 1.0528 | 0.02233 |
| 27.05 | . 9040 | . 95619 | 29.30 | . 9792 | . 99089 | 3155 | I. 0544 | . 02302 |
| 27.17 | .9057 | . 95699 | 29.35 | . 9809 | . 99163 | 31.60 | 1.0561 | . 02371 |
| 27.15 | . 9074 | . 95779 | 29.40 | . 9826 | . 99237 | 31.65 | 1.0578 | . 02439 |
| 27.20 | .9091 | .95859 | 29.45 | .9843 | . 993 II | 31.70 | 1.0594 | . 02508 |

## Table 105.

WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.
Temperature term: $\delta_{t, 760}=\frac{0.0012930}{1+0.003670}$. Centigrade temperature.
I cubic centimeter of dry air at the temperature of $0^{\circ} \mathrm{C}$. and pressure 760 mm ., under the standard value of gravity, weighs o.001 2930 gram.

| t. | $\delta_{t, 760}$ | $\log \delta_{t, 760}$ | t. | $\delta_{t, 760}$ | $\log \delta_{t, 760}$ | t. | $\delta_{t, 760}$ | $\log \delta_{t, 760}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C. | 0.00 | -10 | C | 0.00 | $-10$ |  | 0.00 | -10 |
| $-34^{\circ}$ | 14774 | 7.16950 | $-4.5^{\circ}$ | 13147 | 7.11883 | ${ }^{\circ} .0$ | 12129 | 7.08383 |
| -33 | 14712 | .16768 | $-4.0$ | 13123 | . 11804 | 18.5 | 12108 | . 08309 |
| $-32$ | 14651 | . 16587 | -3.5 | 13098 | . 11720 | 19.0 | 12087 | . 08232 |
| -3I | 14590 | . 16407 | -3.0 | 13074 | . 11642 | 19.5 | 12066 | .08156 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| $-30$ | 14529 | 7.16224 | -2.5 | 13050 | 7.11562 | 20.0 | 12046 | 7.08085 |
| -29 | 14470 | . 16047 | -2.0 | 13026 | . 11481 | 20.5 | 12025 | . 08009 |
| $-28$ | 14410 | . 15866 | -1.5 | 13002 | . 11.401 | 21.0 | 12005 | . 07937 |
| -27 | 14352 | . 1569 I | -1.0 | 12978 | - II 321 | 21.5 | 11984 | . 07860 |
| -26 | I 4294 | . 15515 | $-0.5$ | 12954 | . 11241 | 22.0 | 11964 | . 07788 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| -25 | 14236 | 7.15339 | 0.0 | 12930 | 7.11160 | 22.5 | I 1944 | 7.07716 |
| -24 | 14179 | . 15166 | +0.5 | 12906 | . 11079 | 23.0 | 11924 | .07642 |
| -23 | 14122 | . 14990 | 1.0 | 12883 | . 11002 | 23.5 | 11903 | . 07566 |
| -22 | I 4065 | .14714 | 1.5 | 12859 | . 10921 | 24.0 | 11883 | . 07493 |
| -2I | 14010 | . 14645 | 2.0 | 12836 | .10844 | 24.5 | I 1863 | .07419 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| -20.0 | 13955 | 7.14472 | 2.5 | 12812 | 7.10762 | 25.0 | I 1843 | 7.07346 |
| -19.5 | 13927 | . I 4386 | 3.0 | 12789 | . 10684 | 25.5 | 11823 | . 07273 |
| -19.0 | 13899 | . I 4298 | $3 \cdot 5$ | 12766 | . 10607 | 26.0 | 11804 | . 07204 |
| -18.5 | 13872 | .14215 | 4.0 | 12743 | . 10527 | 26.5 | 11784 | .07131 |
| -18.0 | 13844 | . 14126 | $4 \cdot 5$ | 12720 | .10450 | 27.0 | 11764 | .07056 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| $-17.5$ | 13818 | 7.14044 | 5.0 | 12698 | 7.10372 | 27.5 | 11745 | 7.06986 |
| -17.0 | 13790 | . 13956 | $5 \cdot 5$ | 12675 | . 10294 | 28.0 | 11725 | . 06912 |
| -16.5 | 13763 | . 13871 | 6.0 | 12651 | . 10212 | 28.5 | 11706 | . 06841 |
| -16.0 | 13737 | . 13790 | 6.5 | 12629 | . IOI 38 | 29.0 | I 1686 | . 06767 |
| -15.5 | 13710 | . 13705 | 7.0 | 12606 | . 10058 | 29.5 | I I 667 | . 06697 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| -15.0 | 13684 | 7.13621 | 7.5 | 12584 | 7.09982 | 30.0 | 11648 | 7.06625 |
| $-14.5$ | 13657 | . 13536 | 8.0 | 12561 | . 09902 | 30.5 | 11628 | . 06550 |
| $-14.0$ | 13630 | - 13450 | 8.5 | 12539 | . 09828 | 31.0 | 11609 | . 06479 |
| -13.5 | 13604 | . 13368 | 9.0 | 12517 | . 09750 | 31.5 | 11590 | .06408 |
| -13.0 | 13578 | . 13285 | $9 \cdot 5$ | 12494 | . 09670 | 32.0 | 11571 | . 06337 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| $-12.5$ | 13552 | 7.13201 | 10.0 | 12472 | 7.09594 | 32.5 | 11552 | 7.06266 |
| $-12.0$ | 13526 | .13II 7 | 10.5 | 12450 | . 09517 | 33.0 | 11533 | .06I94 |
| -11.5 | 13500 | . 13034 | II .0 | 12428 | . 09440 | 33.5 | 11514 | . 06123 |
| -11.0 | $13+74$ | . 12950 | II. 5 | 12406 | . 09363 | 34.0 | 11496 | . 06055 |
| $-10.5$ | 13448 | . 12866 | 12.0 | 12384 | . 09286 | 34.5 | 11477 | . 05984 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| -10.0 | 13423 | 7.12785 | 12.5 | 12363 | 7.09214 | 35.0 | 11458 | 7.05911 |
| - 9.5 | 13397 | .12701 | 13.0 | 12341 | . 09135 | 35.5 | I I $444^{\circ}$ | .05843 |
| - 9.0 | 13372 | . 12620 | 13.5 | 12320 | . 09061 | 36.0 | II42I | . 05772 |
| - 8.5 | 13346 | . 12535 | 14.0 | 12298 | . 08983 | 36.5 | 11403 | . 05702 |
| - 8.0 | 1332 I | . 12454 | 14.5 | 12277 | .08910 | 37.0 | 11384 | . 05629 |
|  | 0.00 132 |  | 15.0 | 0.00 |  | 37.5 | 0.00 11366 |  |
|  | 13 | 7.1 |  | 122 | 7.08 | 38.0 | 11347 | 7.05562 .05488 |
| $-6.5$ | 13246 | . 12210 | 16.0 | 12213 | . 08683 | 38.5 | 11329 | . 05419 |
| - 6.0 | 13221 | . 12126 | 16.5 | 12192 | . 08608 | 39.0 | 11311 | . 05352 |
| - 5.5 | 13196 | . 12044 | 17.0 | 12171 | . 08533 | 39.5 | 11293 | . 05282 |
| - 5.0 | 0.00 13172 | 7.11966 | 17.5 | 0.00 12150 | 7.08458 | 40.0 | $\begin{aligned} & 0.00 \\ & 11275 \end{aligned}$ | 7.05213 |

Table 105.
WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.
Temperature term. (Continued)

| t. | $\delta_{t, 760}$ | $\log \delta_{t, 760}$ | t. | $\delta_{t, 760}$ | $\log \delta_{t, 760}$ | t. | $\delta_{t, 760}$ | $\log \delta_{t, 760}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C. | 0.00 | -10 | C. | 0.00 | - 10 | C. | 0.00 | - 10 |
| $+40^{\circ}$ | 11275 | 7.05213 | $+50^{\circ}$ | 10925 | 7.03842 | $+60^{\circ}$ | 10597 | 7.02518 |
| 41 | 11239 | . 05074 | 51 | 10891 | .03707 | 61 | 10565 | . 02388 |
| 42 | 11203 | . 04933 | 52 | 10858 | . 03576 | 62 | 10534 | . 02258 |
| 43 | 11168 | . 04798 | 53 | 10825 | . 03443 | 63 | 10502 | .02128 |
| 44 | 11132 | . 04657 | 54 | 10792 | . 03309 | 64 | 10471 | . 01999 |
|  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |
| 45 | 11097 | 7.04521 | 55 | 10758 | 7.03173 | 65 | 10440 | 7.01870 |
| 46 | 11063 | .04387 | 56 | 10726 | .03044 | 66 | 10409 | . 01742 |
| 47 | 11028 | . 04251 | 57 | 10693 | . 02910 | 67 | 10378 | .01611 |
| 48 | 10993 | .04112 | 58 | 10661 | . 02780 | 68 | 10348 | . 01486 |
| 49 | 10959 | .03977 | 59 | 10629 | .02649 | 69 | 10317 | . 01355 |

Table 106.
Humidity term: Values of 0.378 e. Auxiliary to Table 107.
$e=$ lapor pressure in mm .
(See Tables 76 and 77).

| Dewpoint | $e$ <br> Vapor Pressure (Ice) | $0.378 e$ | Dewpoint | $e$ <br> Vapor Pressure (IVater) | $0.378 e$ | Dewpoint | $e$ <br> Vapor Pressure (W'ater) | $0.378 e$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} C_{5} \\ -50^{\circ} \end{gathered}$ | mm. | mm . | $\mathrm{C}_{0}{ }^{\circ}$ | mm | mm . | C. |  | mm. |
| -50 | 0. | 0.01 |  | 4.580 | 1.73 |  | 31.860 | 12.04 |
|  | 0.054 | 0.02 | 2 | 4.927 | 1.86 | 31 | 33.735 | 12.75 |
| -35 | 0.169 | 0.06 | 3 | 5.682 | 2.15 | 33 | 35.785 37.775 | 13.50 14.28 |
| $-30$ | 0.288 | 0.11 | 4 | 6.098 | 2.31 | 34 | 39.947 | 15.10 |
| -25 | 0.480 | 0.18 | 5 | 6.541 | 2.47 | 35 | 42.227 | 15.96 |
| 24 | 0.530 | 0.20 | 6 | 7.012 | 2.66 | 36 | 44.619 | 16.87 |
| 23 | 0.585 | 0.22 | 7 | 7.513 | 2.84 | 37 | 47.127 | 17.81 |
| 22 | 0.646 | 0.24 | 8 | 8.045 | 3.04 | 38 | 49.756 | 18.81 |
| 21 | 0.712 | 0.27 | 9 | 8.610 | 3.25 | 39 | 52.510 | 19.85 |
| -20 | 0.783 | 0.30 | 10 | 9.210 | 3.48 | 40 | 55.396 | 20.94 |
| 19 | 0.862 | 0.33 | 11 | 9.8 .46 | 3.72 | 41 | 58.417 | 22.08 |
| 18 | 0.947 | 0.36 | 12 | 10.521 | 3.98 | 42 | 61.580 | 23.28 |
| 17 | 1.041 | 0.39 | 13 | 11.235 | 4.25 | 43 | 64.889 | $24 \cdot 53$ |
| 16 | $1.1+2$ | 0.43 | 14 | 11.992 | 4.53 | 44 | 68.350 | 25.84 |
| -15 | 1.252 | 0.47 | 15 | 12.794 | 4.84 | 45 | 71.968 | 27.20 |
| 14 | 1.373 | 0.52 | 16 | 13.642 | 5.16 | 46 | 75.751 | 28.63 |
| 13 | 1.503 | 0.57 | 17 | 14.539 | 5.50 | 47 | 79.703 | 30.13 |
| 12 | 1.644 | 0.62 | 18 | 15.487 | 5.85 | 48 | 83.830 | 31.69 |
| 11 | 1.798 | 0.68 | 19 | 16.489 | 6.23 | 49 | 88.140 | 33.32 |
| $-10$ | 1.964 | 0.74 | 20 | 17.548 | 6.63 | 50 | 92.64 | 35.02 |
| 9 | 2.144 | 0.81 | 21 | 18.665 | 7.06 | 51 | 97.33 | 36.79 |
| 8 | 2.340 | 0.88 | 22 | 19.8 .44 | 7.50 | 52 | 102.23 | 38.64 |
| 7 | 2.550 | 0.96 | 23 | 21.087 | 7.97 | 53 | 107.33 | 40.57 |
| 6 | 2.778 | 1.05 | 24 | 22.398 | 8.47 | 54 | 112.66 | 42.59 |
| $-5$ | 3.025 | 1.14 | 25 | 23.780 | 8.99 | 55 | 118.20 | 44.68 |
| 4 | 3.291 | I. 24 | 26 | 25.235 | 9.54 | 56 | 123.98 | 46.86 |
| 3 | 3.578 | 1.35 | 27 | 26.767 | 10.12 | 57 | 130.00 | 49.14 |
| 2 | 3.887 | 1.47 | 28 | 28.380 | 10.73 | 58 | 136.26 | 51.51 |
| 1 | 4.220 | 1.60 | 29 | 30.076 | 11.37 | 59 | 142.78 | 53.97 |
| 0 | $4 \cdot 580$ | 1.73 | 30 | 31.860 | 12.04 | 60 | 149.57 | 56.54 |

Table 107.
WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.
Humidity and pressure terms combined : $\frac{\delta}{\delta_{0}}=\frac{h}{760}=\frac{B-0.378 e}{760}$.
$B=$ Barometric pressure in mm. ; $e=$ Vapor pressure in mm.

| h. | $\frac{h}{760}$. | $\log \frac{h}{760}$. | h. | $\frac{h}{760}$. | $\log \frac{h}{760}$ | h. | $\frac{\mathrm{h}}{760} .$ | $\log \frac{h}{760}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm. |  | - 10 | mm. |  | - 10 | mm. |  | $-10$ |
| 300 | 0.3947 | 9.59631 | 400 | 0.5263 | 9.72125 | 450 | 0.5921 | 9.77240 |
| 302 | . 3974 | . 59919 | 401 | . 5276 | . 72233 | 45I | . 5934 | . 77336 |
| 304 | . 4000 | . 60206 | 402 | . 5289 | . 72341 | 452 | . 5947 | . 77432 |
| 306 | . 4026 | .6049I | 403 | . 5303 | . 72449 | 453 | . 5961 | . 77528 |
| 308 | . 4053 | . 60774 | 404 | . 5316 | . 72557 | 454 | . 5974 | . 77624 |
| 310 | 0.4079 | 9.61055 | 405 | 0.5329 | 9.72664 | 455 | 0.5987 | 9.77720 |
| 312 | . 4105 | .6I334 | 406 | . 5342 | . 72771 | 456 | . 6000 | .77815 |
| 314 | . 4132 | .61612 | 407 | . 5355 | . 72878 | 457 | . 6013 | . 77910 |
| 316 | . 4158 | . 61887 | 408 | . 5369 | . 72985 | 458 | . 6026 | .78005 |
| 318 | . 4184 | .6216I | 409 | . 5382 | .73091 | 459 | . 6040 | . 78100 |
| 320 | 0.42 II | 9.62434 | 410 | 0.5395 | 9.73197 | 460 | 0. 6053 | 9.78194 |
| 322 | . 4237 | . 62704 | 411 | . 5408 | . 73303 | 461 | . 6066 | . 78289 |
| 324 | .4263 | . 62973 | 412 | . 542 I | . 73408 | 462 | . 6079 | .78383 |
| 326 | . 4289 | . 63240 | 413 | . 5434 | .7351.4 | 463 | .6092 | .78477 |
| 328 | . 4316 | . 63506 | 414 | . 5447 | .73619 | 464 | .6105 | . 78570 |
| 330 | 0.4342 | 9.63770 | 415 | 0.5461 | 9.73723 | 465 | 0.6IIS | 9.78664 |
| 332 | . 4368 | . 64032 | 416 | . 5474 | . 73828 | 466 | .6I32 | .78757 |
| 334 | . 4395 | . 64293 | 417 | . 5487 | . 73932 | 467 | .6145 | . 78850 |
| 336 | . 4421 | . 64552 | 418 | . 5500 | . 74036 | 468 | .6158 | .78943 |
| 338 | . 4447 | . 64810 | 419 | . 5513 | . 74140 | 469 | .6171 | . 79036 |
| 340 | 0.4474 | 9.65066 | 420 | 0.5526 | 9.74244 | 470 | 0.6184 | 9.79128 |
| 342 | . 4500 | . 6532 I | 421 | . 5540 | . 74347 | 471 | . 6197 | . 79221 |
| 344 | . 4526 | . 65574 | 422 | - 5553 | . 74450 | 472 | . 6210 | . 79313 |
| 346 | . 4553 | . 65826 | 423 | . 5566 | . 74553 | 473 | . 6224 | . 79405 |
| 348 | . 4579 | . 66076 | 42.4 | . 5579 | . 74655 | 474 | . 6237 | . 79496 |
| 350 | 0.4605 | 9.66325 | 425 | 0. 5592 | 9.74758 | 475 | 0.6250 | 9.79588 |
| 352 | .4632 | . 66573 | 426 | . 5605 | . 74860 | 476 | . 6263 | . 79679 |
| 354 | . 4658 | . 66819 | 427 | . 5618 | .7496I | 477 | . 6276 | . 79770 |
| 356 | . 4684 | . 67064 | 428 | .5632 | .75063 | 478 | . 6289 | . 79861 |
| 358 | . 47 II | . 67307 | 429 | . 5645 | . 75164 | 479 | . 6303 | . 79952 |
| 360 | 0.4737 | 9.67549 | 430 | 0. 5658 | 9.75265 | 480 | 0.6316 | 9.80043 |
| 362 | .4763 | . 67790 | 431 | . 5671 | . 75366 | 481 | . 6329 | . 80133 |
| 364 | . 4789 | . 68029 | 432 | . 5684 | . 75467 | 482 | . 6342 | . So 223 |
| 366 | .4816 | . 68267 | 433 | . 5697 | . 75567 | 483 | . 6355 | . 80313 |
| 368 | .4842 | . 68503 | 434 | . 57 I I | . 75668 | 484 | . 6368 | . SO 403 |
| 370 | 0.4868 | 9.68739 | 435 | 0.5724 | 9.75768 | 485 | 0.6382 |  |
| 372 | . 4895 | . 68973 | 436 | . 5737 | . 75867 | 486 | . 6395 | . 80582 |
| 374 | . 4921 | . 69206 | 437 | . 5750 | . 75967 | 487 | . 6408 | . 80672 |
| 376 | . 4947 | . 69437 | 438 | .5763 | .76066 | 488 | . 6421 | . 80761 |
| 378 | . 4974 | . 69668 | 439 | . 5776 | .76165 | 489 | . 6434 | . 80550 |
| 380 | 0.5000 | 9.69897 | 440 | 0.5790 | 9.76264 | 490 | 0.6447 | 9.80938 |
| 382 | . 5026 | . 70125 | 441 | . 5803 | . 76362 | 491 | . 646 I | . 81027 |
| 384 | . 5053 | . 70352 | 442 | . 5816 | . 76461 | 492 | . 6474 | . Sili5 |
| 386 | . 5079 | .70577 | 443 | . 5829 | .76559 | 493 | .6487 | . 81203 |
| 388 | .5105 | . 70802 | 444 | .5842 | .76657 | 494 | . 6500 | .81291 |
| 390 | $0.513{ }^{2}$ | 9.71025 | 445 | 0.5855 | 9.76755 | 495 | 0.6513 | 9.81379 |
| 392 | -5I58 | . 71247 | 446 | . 5868 | . 76852 | 496 | . 6526 | . 81467 |
| 394 | . 5184 | . 71468 | 447 | . 5882 | . 76949 | 497 | . 6540 | . SI 556 |
| 396 | .5211 | . 71688 | 448 | . 5895 | . 77046 | 498 | . 6553 | . Si 642 |
| 398 | . 5237 | .71907 | 449 | . 5908 | . 77143 | 499 | . 6566 | .81729 |

Table 107.
WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.
Humidity and pressure terms combined : $\frac{\hbar}{\delta_{0}}=\frac{h}{760}=\frac{B-0.37 S e}{760}$.
$B=$ Barometric pressure in mm. ; $e=$ Vapor pressure in mm.

| h. | $\frac{h}{760}$. | Log $\frac{\mathrm{h}}{760}$. | h. | $\frac{\mathrm{h}}{760}$. | $\log _{760}{ }^{h}$. | h. | $\frac{\mathrm{h}}{760}$. | $\log \frac{h}{760}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm. |  | - Io | mm. |  | 10 | mm. |  | - 10 |
| 500 | 0.6579 | 9.81816 | 550 | 0.7237 | 9.85955 | 600 | 0.7895 | 9. 89734 |
| 501 | . 6592 | . 81902 | 551 | . 7250 | . 86034 | 601 | . 7908 | . 89806 |
| 502 | . 6605 | . 81989 | 552 | . 7263 | . 86112 | 602 | . 7921 | . 89878 |
| 503 | . 6618 | . 82075 | 553 | . 7276 | . 86191 | 603 | . 7934 | . 89950 |
| 504 | . 6632 | . 82162 | 554 | . 7290 | . 86270 | 604 | . 7947 | . 90022 |
| 505 | 0.6645 | 9.82248 | 555 | 0.7303 | 9.86348 | 605 | 0.7961 | 9.90094 |
| 506 | . 6658 | . 82334 | 556 | . 7316 | . 86426 | 606 | . 7974 | . 90166 |
| 507 | . 6671 | . 82419 | 557 | . 7329 | . 86504 | 607 | . 7987 | . 90238 |
| 508 | . 6684 | . 82505 | 558 | . 7342 | . 86582 | 608 | . 8000 | . 90309 |
| 509 | . 6697 | . 82590 | 559 | . 7355 | . 86660 | 609 | . 8013 | . 90380 |
| 510 | 0.6711 | 9.82676 | 560 | 0.7368 | 9. 86737 | 610 | 0.8026 | 9.90452 |
| 511 | . 6724 | . 82761 | 561 | . 7382 | . 86815 | 611 | . 8040 | . 90523 |
| 512 | . 6737 | . 82846 | 562 | . 7395 | .86892 | 612 | . 8053 | . 90594 |
| 513 | . 6750 | . 82930 | 563 | . 7408 | . 86969 | $6{ }^{1} 3$ | . 8066 | . 90665 |
| 514 | . 6763 | . 83015 | 564 | . 7421 | . 87046 | 614 | . 8079 | . 90735 |
| 515 | 0.6776 | 9.83099 | 565 | 0.7434 | 9.87123 | 615 | 0. 8092 | 9.90806 |
| 516 | . 6789 | . 83184 | 566 | . 7447 | . 87200 | 616 | . 8105 | . 90877 |
| 517 | .6803 | . 83268 | 567 | .7461 | . 87277 | 617 | .8118 | . 90947 |
| 518 | .6816 | . 83352 | 568 | . 7474 | . 87353 | 618 | . 8132 | . 91017 |
| 519 | . 6829 | . 83435 | 569 | . 7487 | . 87430 | 619 | . 8145 | . 91088 |
| 520 | 0.6842 | 9.83519 | 570 | 0.7500 | 9. 87506 | 620 | 0.8158 | 9.91158 |
| 521 | . 6855 | . 83602 | 571 | .7513 | . 87582 | 621 | . 8171 | .91228 |
| 522 | . 6869 | . 83686 | 572 | . 7525 | . 87658 | 622 | . 8184 | .91298 |
| 523 | . 6882 | . 83769 | 573 | . 7540 | . 87734 | 623 | .8197 | . 91367 |
| 524 | . 6895 | . 83852 | 574 | . 7553 | . 87810 | 624 | .8211 | . 91437 |
| 525 | 0. 6908 | 9.83934 | 575 | 0.7566 | 9.87885 | 625 | 0.8224 | 9.91507 |
| 526 | . 6921 | . 84017 | 576 | . 7579 | . 87961 | 626 | . 8237 | . 91576 |
| 527 | . 6934 | . 84100 | 577 | . 7592 | . 88036 | 627 | . 8250 | . 91645 |
| 528 | . 6947 | . 84182 | 578 | . 7605 | .88I II | 628 | . 8263 | . 91715 |
| 529 | . 6961 | . 84264 | 579 | . 7618 | . 88186 | 629 | . 8276 | . 91784 |
| 530 | 0.6974 | 9.84346 | 580 | 0.7632 | 9.88261 | 630 | 0.8289 | 9.91853 |
| 531 | . 6987 | . 84428 | 581 | . 7645 | . 88336 | 631 | . 8303 | . 91922 |
| 532 | . 7000 | . 84510 | 582 | . 7658 | . 88411 | 632 | . 8316 | . 91990 |
| 533 | . 7013 | . 84591 | 583 | . 7671 | . 88486 | 633 | . 8329 | . 92059 |
| 534 | . 7026 | . 84673 | 584 | . 7684 | . 88560 | 634 | . 8342 | . 92128 |
| 535 | 0.7040 | 9.84754 | 585 | 0.7697 | 9.88634 | 635 | 0.8355 | 9.92196 |
| 536 | . 7053 | . 84835 | 586 | . 7711 | . 88708 | 636 | . 8368 | . 92264 |
| 537 | . 7066 | . 84916 | 587 | . 7724 | . 88782 | 637 | . 8382 | . 92332 |
| 538 | . 7079 | . 84997 | 588 | . 7737 | . 88856 | 638 | . 8395 | . 92401 |
| 539 | .7092 | . 85078 | 589 | . 7750 | . 88930 | 639 | . 8408 | . 92469 |
| 540 | 0.7105 | 9.85158 | 590 | 0.7763 | 9.89004 | 640 | 0.8421 | 9.92537 |
| 541 | . 7118 | . 85238 | 591 | . 7776 | . 89077 | 641 | . 8434 | . 92604 |
| 542 | . 7132 | . 85318 | 592 | . 7789 | . 89151 | 642 | . 8447 | . 92672 |
| 543 | . 7145 | . 85399 | 593 | .7803 | . 89224 | 643 | . 8461 | . 92740 |
| 544 | . 7158 | . 85478 | 594 | . 7816 | . 89297 | 644 | . 8474 | . 92807 |
| 545 | 0.7171 | 9.85558 | 595 | 0.7829 | 9.89370 | 645 | 0.8487 | 9.98875 |
| 546 | . 7184 | . 85638 | 596 | . 7842 | . 89443 | 646 | . 8500 | . 92942 |
| 547 | . 7197 | . 85717 | 597 | . 7855 | . 89516 | 647 | . 8513 | -93009 |
| 548 | . 7211 | . 85797 | 598 | . 7868 | . 895889 | 648 | . 8526 | . 93076 |
| 549 | . 7224 | . 85876 | 599 | . 7882 | . 89662 | 649 | . 8539 | . 93143 |

Gmithbonian Tableg.

Table 107.
WEIGHT IN GRAMS OF ONE CUBIC CENTIMETER OF AIR.
Iumidity and pressure terms combined : $\frac{\hbar}{\delta_{0}}=\frac{h}{760}=\frac{B-0.378 e}{760}$.
$B=$ Barometric pressure in mm. ; $e=$ Vapor pressure in mm.

| h. | $\frac{h}{760} .$ | $\log _{760}{ }^{\text {h }}$ | h. | $\frac{h}{760}$. | $\log \frac{h}{760}$. | h. | $\frac{h}{760} .$ | $\log \frac{h}{760}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm. |  | - 10 | mm . |  | - 10 | mm. |  | - 10 |
| 650 | 0.8553 | 9.93210 | 700 | 0.92 II | 9.96428 | 750 | 0.9868 | 9.99425 |
| 651 | . S5 $^{\text {ch }}$ | . 93277 | 703 | . 9224 | . 96490 | 751 | . 9882 | . 99443 |
| 652 | . 8579 | .93341 | 702 | . 9237 | . 96552 | 752 | . 9895 | . 99540 |
| 653 | . 5592 | . 93410 | 703 | . 9250 | .96614 | 753 | . 9908 | . 99598 |
| 654 | . 5605 | . 93476 | 704 | . 9263 | . 96676 | 754 | . 9921 | . 99656 |
| 655 | 0.8618 | 9.93543 | 705 | 0.9276 | 9.96738 | 755 | 0.9934 | 9.99713 |
| 656 | . 8632 | . 93609 | 706 | . 9289 | . 96799 | 756 | . 9947 | . 99771 |
| 657 | . 8645 | . 93675 | 707 | . 9303 | . 96860 | 757 | . 9961 | . 99828 |
| 65 S | . 8658 | .9374I | 708 | . 9316 | . 96922 | 758 | . 9974 | . 99886 |
| 659 | . 8671 | .93So7 | 709 | . 9329 | . 96983 | 759 | .9987 | . 99943 |
| 660 | o. S684 | 9.93 S73 | 710 | 0.9342 | 9.97044 | 760 | 1.0000 | 0.00000 |
| 66I | . 5697 | . 93939 | 711 | . 9355 | . 97106 | 761 | . 0013 | . 00057 |
| 662 | . 8711 | . 94004 | 712 | . 9368 | .97167 | 762 | . 0026 | . OOI 14 |
| 663 | . 8724 | . 94070 | 713 | . 9382 | . 97228 | 763 | . 0039 | . 00171 |
| 664 | . 8737 | . 94135 | 714 | . 9395 | . 972 SS | 764 | . 0053 | . 00228 |
| 665 | 0. S 50 | 9.94201 | 715 | 0.940 S | 9.97349 | 765 | 1.0066 | 0.00285 |
| 666 | . S 763 | . 94266 | 716 | . 942 I | . 97410 | 766 | . 0079 | . 00342 |
| 667 | . 8776 | . 9433 I | 717 | . 9434 | . 97470 | 767 | . 0092 | . 00398 |
| 668 | . 5790 | . 94396 | 718 | . 9447 | . 9753 I | 76 S | . 0105 | . 00455 |
| 669 | . SSo3 | . 94461 | 719 | .946I | . 97592 | 769 | . OI 18 | . 0051 I |
| 670 | 0.88ı6 | 9.94526 | 720 | 0.9474 | 9.97652 | 770 | 1.0132 | 0.00568 |
| 671 | . SS29 | . 94591 | 721 | . 9487 | .97712 | 771 | . 0145 | . 00624 |
| 672 | . $\mathrm{SS}_{42}$ | . 94656 | 722 | . 9500 | . 97752 | 772 | . 0158 | . 00680 |
| 673 | .SS55 | . 94720 | 723 | . 9513 | . 97832 | 773 | . 0171 | . 00736 |
| 674 | .SS69 | . 94785 | 72.4 | . 9526 | . 97892 | 774 | . 0184 | . 00793 |
| 675 | 0.88S2 | 9.94849 | 725 | 0.9539 | 9.97952 | 775 | 1.0197 | 0.00849 |
| 676 | .S895 | . 94913 | 726 | . 9553 | .9SOI2 | 776 | . 0211 | . 00905 |
| 677 | . S 908 | . 94978 | 727 | . 9566 | .9So72 | 777 | . 0224 | .00961 |
| 678 | . S 921 | . 95042 | 728 | . 9579 | .9SI 32 | 778 | . 0237 | . 01017 |
| 679 | . 8934 | .95106 | 729 | . 9592 | .9Si9I | 779 | . 0250 | . 01072 |
| 680 | 0.8947 | 9.95170 | 730 | 0.9605 | 9.9S250 | 780 | 1.0263 | 0.01128 |
| 681 | . S960 | . 95233 | 731 | .96IS | . 98310 | 781 | . 0276 | .OII84 |
| $6 S_{2}$ | . 8974 | . 95297 | 732 | .9632 | . 98370 | $7 \mathrm{~S}_{2}$ | . 0289 | . 01239 |
| $6 S_{3}$ | . $\mathrm{S9} 87$ | .95361 | 733 | . 9645 | . 98429 | ${ }_{7} \mathrm{~S}_{3}$ | . 0303 | . 01295 |
| 684 | . 9000 | . 95424 | 734 | . 9658 | .984SS | 754 | . 0316 | . OI 350 |
| 685 | 0.9013 | 9.95488 | 735 | 0.9671 | 9.98547 | 785 | 1.0329 | 0.01406 |
| 686 | . 9026 | . 95551 | 736 | . 9684 | . 98606 | 786 | . 0342 | . 01461 |
| 687 | . 9039 | .95614 | 737 | . 9697 | . 98665 | 787 | . 0355 | . 01516 |
| 688 | .9053 | . 95677 | 73 S | .9711 | .98724 | 7 SS | .036S | .OI571 |
| 689 | . 9066 | . 95740 | 739 | . 9724 | .9S7S3 | 789 | . 0382 | . 01626 |
| 690 | 0.9079 | 9.95S04 | 740 | 0.9737 | 9.98842 | 790 | 1.0395 |  |
| 691 | .9092 | . 95566 | 741 | . 9750 | . 98900 | 791 | . 0408 | . 01736 |
| 692 | . 9105 | . 95929 | 7.42 | . 9763 | .9S959 | 792 | . 0421 | . 01791 |
| 693 | .9118 | . 95992 | 743 | . 9776 | .9901S | 793 | . 0434 | . OIS46 |
| 694 | .9132 | . 96054 | 744 | . 9789 | . 99076 | 794 | . 0447 | . O1901 |
| 695 | 0.9145 | 9.96117 | 745 | 0.9803 |  | 795 | 1.0461 | 0.01955 |
| 696 | . 9158 | .96180 | 746 | .98I6 | . 99192 | 796 | . 0474 | . 02010 |
| 697 | . 9171 | . 962.12 | 747 | . 9829 | . 99251 | 797 | . 0487 | . 02064 |
| 698 | . 9184 | . 96304 | 748 | . 9842 | . 99309 | 79 S | . 0500 | .02119 |
| 699 | .9197 | . 96366 | 749 | . 9855 | . 99367 | 799 | .05I3 | .02173 |

Table 108.
ATMOSPHERIC WATER-VAPOR LINES IN THE VISIBLE SPECTRUM.

| Wave lengths in Ångströms | Number of lines | Intensity | Wave lengths in Ångströms | Number of Iines | Intensity |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 5292.2 | 1 ? | -2 | 5915.628. |  | I |
| $5861.6-5869.8$ | 7 | -2 | $5915.8-5918.0$ | 6 | -1 |
| 5870.653... |  | I | 5918.423 |  | 4 |
| $587 \mathrm{I} .2-5875.6$ | 8 | -I | 5919.0... | I | -2 |
| 5876.126.... |  | 1 | 5919.059. |  | 5 |
| $5877.3-5879.2$ | 4 | -I | 5919.647. |  | 7 |
| 5879.608. |  | I | 5920.2 | 1 | -I |
| 5879.733 . |  | 1 | 5920.56+.. |  | I |
| $5880.5-5880.7$ | 2 | 0 | $5921.2-5922.4$ | 3 | -I |
| $5880.935 \ldots . .$. |  | 1 | $5922.522 \ldots$. |  | 2 |
| 5881.1 |  | o | $5922.7-5923.2$ | 2 | -I |
| 5881.872 |  | I | 5923.652. |  | 1 |
| $5882.0-5883.0$ | 3 | 0 | 5923.827. |  | 2 |
| $5883.908 \ldots$ |  | 5 | 5924.276 |  | 4 |
| $588+2-5885.6$ | 3 | -I | 5924.8 | 1 | -2 |
| 5885.981 . |  | 5 | 5925.007 |  | 2 |
| 5886.348. |  | 1 | 5926.6. | I | -2 |
| 5886.+ -5886.7 | 2 | o | 5928.296. |  | 2 |
| 5887.226 |  | 5 | 5928.8-5931.0. | 5 | $-2$ |
| 5887.664. |  | 3 | 5932.097. |  | 5 |
| 5887.8 | I | -1 | 5932.788. |  | 2 |
| 5888.708. |  | 2 | $5933.0-5940.0$ | 14 | -2 |
| 5889.1 | 1 | -I | 5940.427. |  | I |
| 5889.643 |  | 3 | $59+0.9$. | I | - 5 |
| 5889.888. |  | 2 | $59+1.080$ |  | 5 |
| $5890.2-5890.7$ | 2 | $\bigcirc$ | 5941.3 | I | -2 |
| 5891.186. |  | 1 | $59+1.632$ |  | 2 |
| 5891.5 | I | 0 | $59+2 \cdot 3$ | I | -2 |
| 5891.665 |  | 4 | $59+2.422$. |  | 1 |
| 5892.401 |  | 3 | $59+2 \cdot 576$. |  | 3 |
| 5893.1 | I | 0 | $59+4.317$. |  | 1 |
| $5893 \cdot 513 \cdots$. |  | 1 | $59+4.732$. |  | I |
| $589++-5896 .+$ | 5 | -I | $59+5.2-59+5.3$ | 2 | -1 |
| 5896.498. |  | 1 | $59+5.652$. |  | 1 |
| $5896.835 \cdots$ |  | 2 | 5946.010. |  | 3 |
| $5897.1-5897.9$ | 4 | -I | $59+6.7$ | 1 | 2 |
| $\begin{array}{llll}5898.173 & \ldots \\ 5898.4 & -5898.8\end{array}$ | 2 | 4 -2 | 5946.849 5947.070 |  | 2 |
| 5899.003.... |  | 2 | 5947.4-5949.0 | 4 | -2 |
| 5899.923. |  | 2 | 5949.176.. |  | 2 |
| 5900.048. |  | 4 | $5949.6-5954 \cdot 4$ | 11 | -I |
| $5900.4-5901.3$ | 3 | -1 | 5954.956. |  | 1 |
| 5901.472. |  | 6 | $5955.8-5956.3$ | 4 | 2 |
| 5902.0. | I | -2 | 5957.884 |  | I |
| 5902.151 |  | 1 | 5958.246. |  | - |
| 5902.8. | 1 | -2 | $5961.4-5966.3$ | 5 | -1 |
| 5903.536 |  | I | 5966.670. |  | I |
| $5903.7-5907.5$ | 13 | -1 | 5967.3 | 1 | -I |
| 5907.858. |  | I | 5967.843 |  | 2 |
| 5908.213. |  | I | 5968. I. | I | -2 |
| 5909.001. |  | 3 | 5968.280 . . . . . |  | - |
| 5909.5. | 1 | -I | $5969.0-5970.7$ | 3 | -1 |
| $5910.3-5910.6$ | 3 | -1 | 5975.114. |  | I |
| 5910.775.... |  | 2 | 5976.5. | 1 | -1 |
| $5910.9-5912.7$ | 7 | $-2$ | 5977.036 |  | 1 |
| 5913.000. |  | 3 | $5977 \cdot 4-6029.9$ | 27 | -I |
| $591+218$. |  | 6 | $6267.7-6350.7$ | 28 | -2 |
| $5914.93+$. |  | I | $6463.5-6479.5$ | 14 | -2 |
| $5915 \cdot+38$. |  | I | $6+60.070$ |  | I |

Table 108.
ATMOSPHERIC WATER-VAPOR LINES IN THE VISIBLE SPECTRUM.

| Wave lengths in Ảngströms | Number of lines | Intensity | W'ave lengths in Ångströms | Number of lines | Intensity |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $6480.3-6483.1$ | 3 | -3 | 69+1.0. | I | -2 |
| 6483.252..... |  | I | 6941.234. |  | 1 |
| $6483.5-6490.7$ | I 1 | -3 | 6942.163. |  | 2 |
| 6490.798.... |  | I | $69+2.387 \ldots$ |  | 1 |
| $6492.9-5493.3$ | 2 | -1 | $69+3.815$. |  | 3 |
| 6494.510. . . . |  | 1 | 6947.552.. |  | 5 |
| $6+95.864$. |  | 2 | $69+7.6 \ldots$ | I | -I |
| $6497.6-6514.3$ | 7 | -I | 6948.997. |  |  |
| $65 \text { I } 4.737 \ldots .$ |  | 2 | $69+9.067$ |  | I |
| $6515.9$ |  | -2 | 6950.77 \%. |  | I |
| 6516.527. |  | I | 6953.586... |  | 1 |
| 6516.632. |  | 2 | $6953.8-6955.7$. | 2 | -2 |
| 6517.1 -6519.2 | 3 | -I | 6956.416 . . . . . |  | 4 |
| $6519.5 \cdots$ |  | I | 6956.502. |  |  |
| $6521.9-6523.7$ | 4 | -3 | 6959.467.. |  | 3 |
| $6523.855$ |  | I | $6961.275$ |  | 4 |
| $6525.8 \quad-6530.6$ | 2 | $-2$ | 6964.564. |  |  |
| $6532.369$ |  | I | $6970.9$ | I | 0 |
| $6533 \cdot 949$ |  | 2 | $6977 \cdot 487$. |  | 3 |
| $6534.6-6542.3$ | 3 | -2 | 6981.474... |  | 1 |
| $65+3.912$ |  | 2 | 6984.9... | I | - |
| $6545.8-6547.7$ | 2 | -I | 6986.592. |  | 3 |
| $6548.627 \ldots .$ |  | , | $6987.9 \ldots$ | I | 0 |
| $6552.636 \ldots$ |  | 1 | $6989.00 \mathrm{I}$ |  | 3 |
| $6553.8-6558.2$ | 3 | -I | 6990.391. |  | I |
| $6560.570 . . . .$. |  | 1 | 6993.535. |  | 2 |
| $6561 . \mathrm{I}-657 \text { 1.0. }$ | 8 | -2 | $6994.124 .$ |  | 1 |
| $6572.099 \ldots .$ |  | I | 6998.7.. | 1 | 0 |
| $6573.5 \ldots$ | 1 | -3 | 6998.98 I. |  | $2$ |
| 6574.854 |  | I | 7004.3.. | 1 | 0 |
| $6576.4-66.43 .9$ | 22 | -2 | 7004.766..... |  | 2 |
| 6929.3......... | I | -I | 7005.1 -7009.9 | 2 | 0 |
| $6933.832 .$ |  | - | $7011.342 \ldots$. |  | 2 |
| 6937.716. |  | 2 | 7016.452. |  | 3 |
| $6938.27 \mathrm{I}$ |  | I | 7023.517. |  | $2$ |
| $6939.630 .$ |  | 2 | 7027.0. | I | 0 |
| 6940.198. |  | 2 | 7027.491 |  | 2 |

Table 109.
ATMOSPHERIC WATER-VAPOR BANDS IN THE INFRA-RED SPECTRUM.

| Name of band | Wavelengths | Transmission coefficient a | The infra-red bands may perhaps be composed of numerous fine lines which the bolographic apparatus does not separately distinguish. <br> Wide bands of very great atmospheric watervapor absorption are found in the infra-red spectrum as follows: |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a........... | $\begin{gathered} \mu \\ 0.718 \\ 0.814 \\ 0.896 \end{gathered}$ | 0.91 | Name | Wave lengths | Absorption at Washington |
|  |  | 0.90 0.63 |  | $\mu \quad \mu$ |  |
| $\sigma$ | 0.945 | 0.69 | $\rho \sigma$ | 0.926-0.978 | 0.3 to 0.5 |
|  | 0.974 | 0.91 |  | 1.095-1.165 | 0.5 to 0.8 |
| Ф | I.II9 | 0.54 |  | 1.319-1.498 | 0.7 to 1.0 |
| 中 | 1.134 | 0.60 |  | $1.762-1.977$ | 0.9 to I.0 |
|  | 1.172 | 0.92 |  | $2.520-2.845$ | $\text { I.o }\left\{\begin{array}{c} \text { Partly } \\ \mathrm{CO}_{2} \end{array}\right\}$ |
| In ${ }^{\text {l }} \mathrm{w}$ | 1.331 I. 451 | 0.74 0.36 |  |  | ( $\mathrm{CO}_{2}$ ) |
| 1n | 1.451 1.499 | 0.55 | See \ol. Smithsonia | nuls A strophy itution. | abservatory, |

Table 110.
TRANSMISSION PERCENTAGES OF RADIATION THROUGH MOIST AIR.


* These plares require multiplication by the following factors to allow for losses in $\mathrm{CO}_{2}$ gas. Under average sea-level outdoor conditions the $\mathrm{CO}_{2}$ (partial pressure $=0.0003$ atmos.) amounts to about 0.6 grams per cu.m. Paschen gives 3 times as much for indoor conditions.
$2 \mu$ to $3 \mu$, for ${ }_{4}^{2}$ grams in $m_{4}^{2}$ path (95); for $1_{4} 40$ grams in $m_{4}^{2}$ path ( 93 );
4 " 5 , ". " " " " (93) ; " " " " " " (70); more $\mathrm{CO}_{2}$ no further effect;
13 ". I 4 , slight allowance to be made;
I4 is 15,80 grams in $m^{2}$ path reduces energy to zero;
$\dagger$ These places require multiplication by 0.90 arc 0 .
65 for
0.65 for two air masses to allow for ozone absorption when the radiation comes from a celestial body.
F. Paschen gives (Annalen d. Physik. u. Chemie, 51, p. 14, 1804) the absorption of the radiation from a blackened strip at $500^{\circ} \mathrm{C}$. by a layer 33 centimeters thick of water vapor at $100^{\circ} \mathrm{C}$. and atmospheric pressure as follows:

| Wave length. | $\begin{array}{cc} \mu & \mu \\ 2.20-3.10 \end{array}$ | $\begin{array}{cc} \mu \quad \mu \\ 5.33-7.67 \end{array}$ | $\begin{array}{cc} \mu & \mu \\ 7.67-10(?) \end{array}$ |
| :---: | :---: | :---: | :---: |
| Percentage absorption. . | 80 | 94 | 94-13 |

The following table, due to Rubens and Aschkinass (Annalen d. Physik u. Chcmie, 64, p. 598, 1898), gives the absorption of radiation from a zircon burner by a layer 75 centimeters thick of water vapor saturated at $100^{\circ} \mathrm{C}$. This amount of vapor is about equivalent to a layer of water 0.45 millimeter thick or to $1.5 \%$ of the water in a total vertical atmospheric column whose dewpoint at sea-level is $10^{\circ} \mathrm{C}$. The region of spectrum examined includes most of the region of terrestrial radiation.

| Wave length. | $\begin{gathered} \mu \\ 7.0 \end{gathered}$ | $\begin{gathered} \mu \\ 8.0 \end{gathered}$ | $\begin{gathered} \mu \\ 9.0-12.0 \end{gathered}$ | $\begin{gathered} \mu \\ 12.4 \end{gathered}$ | $\begin{gathered} \mu \\ 12.8 \end{gathered}$ | $\begin{gathered} \mu \\ 13.4 \end{gathered}$ | $\mu$ 14.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Percentage absorption. | 75 | 40 | 6 | 20 | 13 | 28 | 22 |
| Wave length | $\begin{gathered} \mu \\ 14 \cdot 3 \end{gathered}$ | $\begin{gathered} \mu \\ 15.0 \end{gathered}$ | $\begin{gathered} \mu \\ 15.7 \end{gathered}$ | $\stackrel{\mu}{16.0}$ | $\begin{gathered} \mu \\ 17.5 \end{gathered}$ | $\begin{gathered} \mu \\ 18.3 \end{gathered}$ | $\begin{gathered} \mu \\ 20.0 \end{gathered}$ |
| Percentage absorption. | 43 | 35 | 65 | 52 | 88 | 80 | 100 |

Table 111.
ENERGY DISTRIBUTION AND ATMOSPHERIC TRANSMISSION OF SOLAR RADIATION.

| U. ${ }^{\top}$. glass deviation from $\omega_{1}$ | Wave <br> lengths | Trans-mis-sionfordryair | Trans-mission for water vapor | U. V. glass prismatic energy | Energy distribution |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Dry air | Moist air |  |  |  |
|  |  |  |  |  | Sun in zenith |  |  | Sun's zenith distance |  |
|  |  |  |  |  |  |  |  | $60^{\circ} .0$ | $70^{\circ} \cdot 7$ |
| $+230$ | $\mu$ | $a_{a \lambda}$0.556 |  |  |  | $e_{0 \lambda} a_{a \lambda} a_{s v \lambda} e_{0 \lambda} a_{a \lambda} a_{w e \lambda}^{2}$ |  | $e_{\theta \lambda} a_{a \lambda}^{2} a_{z, \lambda}^{2}$ | $e_{0 \lambda} a_{u \lambda \lambda}^{3} a_{u \lambda \lambda}^{y}$ |
|  | . 3504 |  |  | $127$ | 71 | 65 | 61 | 34 | 1I |
| 220 | . 3600 | . 592 | $\begin{array}{r} 0.926 \\ .934 \end{array}$ | 150 | 89 | 84 | 78 | 46 | 17 |
| 210 | . 3709 | . 630 | $.940$ | 179 | 113 | 106 | 100 | 63 | 26 |
| 200 | . 3838 | . 670 | . 945 | 191 | 128 | 121 | 114 | 76 | 34 |
| 190 | . 3974 | . 707 | $\begin{array}{r} .949 \\ .953 \end{array}$ | 246 | 174 | 165 | 156 | 1 II | 54 |
| 180 | . 4127 | . 743 |  | 396 | 294 | 280 | 267 | - 198 | 105 |
| 170 | . 4307 | . 779 | $\begin{array}{r} .953 \\ .957 \end{array}$ | +52 | 352 | 337 | 323 | 252 | 144 |
| 160 | . 4516 | . 815 | $\begin{aligned} & .957 \\ & .96 I \end{aligned}$ | 596 | 486 | 467 | 448 | 365 | 224 |
| 150 | . 4753 | . $8+7$ |  | 713 | 604 | 582 | 561 | 475 | 311 |
| 140 | . 5026 | . 876 | $.968$ | 808 | 708 | 685 | 663 | 581 | 406 |
| 130 | . $5344^{8}$ | . 902 | .971 | 897 | 810 | 786 | 763 | 689 | 506 |
| 120 | . $57+{ }^{2}$ | . 926 | $\begin{aligned} & .974 \\ & .976 \end{aligned}$ | 1063 | 984 | 959 | $93+$ | 865 | 666 |
| 115 | . 5980 | . 937 |  | 1177 | 1103 | 1077 | 1051 | 985 | 779 |
| 110 | . 6238 | . 947 | $\begin{aligned} & .976 \\ & .978 \end{aligned}$ | 1248 | II 81 | 1155 | 1130 | 1070 | 866 |
| 105 | . 6530 | . 955 | . 980 | 1330 | 1271 | 1245 | 1220 | 1166 | 968 |
| 100 | . 6858 | . 963 | . 981 | $1+20$ | 1368 | 1342 | 1316 | 1268 | 1069 |
| 95 | . 7222 | . 970 | . 982 | $1+41$ | 1398 | 1373 | $134^{8}$ | 1308 | I II 7 |
| 90 | . 7644 | . 976 | .984 | $1+42$ | 1408 | 1385 | 1363 | 1330 | 1160 |
| 85 | .8120 | .981 | .985 | I 431 | 1404 | 1383 | 1362 | 1337 | I 180 |
| 80 | . 8634 | . 985 | $\begin{array}{r} .986 \\ .987 \end{array}$ | 1410 | I 389 | 1370 | 1351 | 1331 | 1188 |
| 75 | . 9220 | . 989 |  | 1374 | 1358 | 1341 | 1324 | 1308 | 1181 |
| 70 | . 9861 | .991 | $\begin{aligned} & .987 \\ & .988 \end{aligned}$ | 132 I | 1307 | 1290 | 1273 | 1265 | 1144 |
| 65 | 1.062 | . 994 |  | 1242 | 1234 | 1219 | 1205 | 1197 | 1093 |
| 60 | 1.146 | . 995 | $\begin{array}{r} .988 \\ .988 \end{array}$ | 1084 | 1079 | 1066 | 1053 | 1048 | 959 |
| 55 | 1.225 | :996 | . 988 | 956 | 952 | 941 | 930 | 926 | 848 |
| 50 | 1.302 | . 997 |  | 826 | 824 | 814 | 804 | 802 | 735 |
| 45 | 1.377 | . 998 | $.988$ | 713 | 711 | 703 | 694 | 693 | 635 |
| 40 | I. 452 | . 998 |  | 629 | 628 | 620 | 613 | 612 | 561 |
| 35 | 1. 528 | . 9985 | $\begin{aligned} & .988 \\ & .988 \end{aligned}$ | $55^{8}$ | 557 | 550 | 544 | 543 | 498 |
| 30 | 1.603 | . 9988 | $\begin{array}{r} .988 \\ .988 \end{array}$ | 504 | 503 | 497 | 491 | 491 | 450 |
| 25 | 1.670 | . 9990 | . 987 | 455 | 454 | 449 | $4+3$ | $44^{2}$ | 403 |
| 20 | 1.738 | . 9992 |  | 412 | 412 | 406 | 401 | 40 I | 365 |
| + 10 | 1.870 | . 9993 | $.987$ | 320 | 320 | 316 | 312 | 311 | 284 |
| $\pm 0$ | 2.000 | . 9995 |  | 233 | 233 | 230 | 226 | 226 | 205 |
| - 10 | 2.123 | . 9996 | .986 .985 | 150 | 150 | 148 | 146 | 145 | 131 |
| 20 | 2.242 | . 9997 | .985 | 89 | 89 | 88 | 86 | 86 | 77 |
| 30 | 2.348 | . 9997 | $\begin{aligned} & .983 \\ & .982 \end{aligned}$ | 74 | 74 | 73 | 72 | 72 | 63 |
| $-40$ | 2.442 | 1.9998 |  | 68 | 68 | 67 | 66 | 66 | 58 |
| Cor. for u. v. not measured... |  |  |  | 1118 | 435 | 346 | 264 | 123 | 8 |
| Per cent of total |  |  |  | 3.1 | 1.3 | I. 2 | 1.0 | 0.5 | 0.0 |
| Total, .346-. 405 |  |  |  | 1788 | I I 49 | 1081 | 1018 | 659 | 284 |
| Per cent of total. |  |  |  | 5.0 | 3.5 | 3.7 | 3.7 | 2.7 | ${ }_{8} 1.5$ |
| Total, .405-.704 |  |  |  | $14+62$ | I 2885 | 12501 | I2 139 | 10874 | 8043 |
| Per cent of total. |  |  |  | 40.2 | 39.2 | 43.4 | 44.3 | 43.7 | 42.3 |
| Total, .704-2.442 |  |  |  | 17855 | 17672 | 17432 | 17194 | 17030 | 15322 |
| Cor. for i. r. not measured |  |  |  | 705 | 698 | 575 3090 | 473 3665 | 468 4275 | 190 4814 |
| Cor. for w. v. absorption |  |  |  | I 8560 | 18370 | 3090 14917 | 3665 14002 | 4275 13223 | 4814 10698 |
| Per cent of total...............Absorbed by permanent gases. |  |  |  | 185 51.7 | 1838.0 56 | 1 51.7 | $\begin{array}{r}\text { 51.1 } \\ \\ \hline\end{array}$ | 53.1 | 56.2 |
|  |  |  |  |  | 231 | 230 | 220 | 280 | 290 87 |
| Total spectrum. . . . . . . . . . . . |  |  |  | 35928 | 32608 | 28615 | 27203 | 24599 | 18743 |
| Atmospheric transmission . . . |  |  |  | 100 | 90.8 | 79.7 | 75.8 | 68.5 | 52.2 |

The International Meteorological Symbols were adopted at the Viemia meteorological congress of 1873 . A few additions and modifications have been made at subsequent international meteorological meetings. The forms of these symbols are more or less flexible. Those shown in the accompanying table are the forms which have generally been used in the United States. The principal variants found in the meteorological publications of the different countries are given in the Monthly Weather Reviezw (Wash., D. C.), May, 1916, p. 268.

Exponents.-An exponent added to a symbol indicates the degree of intensity, ranging from ${ }^{\circ}$ weak (light, etc.) to ${ }^{2}$ strong (heavy, etc.). Thus, $\bigcirc^{\circ}$, light rain; $\mathrm{O}^{2}$, heavy rain. German and French observers use the exponent ${ }^{1}$ to denote medium intensity, in accordance with the German and French versions of the report of the Vienna congress, and the German editions of the Codex. The English version of the above-mentioned report and the English edition of the Codex provide for the use of only two exponents, ${ }^{\circ}$ and ${ }^{2}$; hence in English-speaking countries the omission of the exponent indicates medium intensity.

Time of occurrence.-When hours of occurrence are added to symbols, the abbreviation $a$ is used for a.m., and $p$ for p.m. Thus, $\bigcirc$ roa $-\downarrow p$ denotes " rain from $10 \mathrm{a} . \mathrm{m}$. to $+\mathrm{p} . \mathrm{m} . " 12 a=$ noon : $12 p=$ midnight. The abbreviation $n$ means " during night." Stations taking tri-daily observations may use $a$ to mean between the first and second observation; $p$, between the second and third ; and $n$, between the third and the first.

For further information concerning the Intcrnational Symbols and other meteorological symbols, see " Meteorological Symbols," by C. Fitzhugh Talman, Monthly Weather Reriez" (Wash., D. C.), May, 1916, pp. 265-274.

## SMITHSONIAN TABLES.

Table 112.
INTERNATIONAL METEOROLOGICAL SYMBOLS．

| Symbol． | Meaning． | Remarks． |
| :---: | :---: | :---: |
| 0 | Rain． |  |
| ＊ | Snow． |  |
| 宜 | Rain and snow to－ gether（＂sleet＂ of British usage）． |  |
| 5 | Thunderstorm． | Thunder and lightning． |
| T | Thunder． | Without hightning． |
| $\leq$ | Lightning． | Without thunder；＂heat－lightning．＂ |
| － |  |  |
| $\triangle$ | Graupel． | Sometimes called soft hail．＂French，gresil．Re－ sembles little snow－pellets． |
| $=$ | Fog． |  |
| 三 | Ground fog． | Not exceeding the height of a man． |
| 三： | Wet fog． | One which wets exposed surfaces． |
| $\square$ | Hoarfrost． |  |
| － | Dew． |  |
| $\checkmark$ | Rime． | A rough frost deposit from fog． |
| $\infty$ | Glaze；Glazed frost．$\dagger$ | Ice coating due to rain，＂ice－storm．＂In America often called＂sleet．＂ |
| $\stackrel{+}{ }$ | Driving snow． | Ger．，Schneegestöber；Fr．，bourrasque de neigc． |
| $\leftarrow$ | Ice－crystals． | Ice－needles sometimes seen floating or slowly falling in the air in clear，cold weather． |
| 河 | Snow on ground． | Ground near station more than half covered． |
| － | Gale． | Wind of force 8－12，Beaufort scale．（Rept．Int．Met 1 Comm．，Berlin，1910，English ed．，p．17．）Formerly used for＂strong wind．＂A 3－barbed arrow is intro－ duced in the $2 d$ German ed．of the Int．Met＇l Codex to denote＂strong wind，＂but no authority is cited． According to the Observer＇s Handbook of the Britisin Met＇l Office＂the number of barbs on the arrow may conveniently be made to represent the strongest wind force noted，＂but there is no international sanction for such variants． |
| $\odot$ | Sunshine． | In German edition of Int．Met＇l Codex，but has never been definitely recognized by the international or－ ganization．（See Rept．Int．Met＇l Comm．，South－ port，I903，Engl．ed．，pp．i9 and ioi．）Widely used in German and Austrian publications． |
| $\oplus$ | Solar halo． |  |
| （1） | Solar corona． |  |
| $\pm$ | Lunar halo． |  |
| $\cup$ | Lunar corona． |  |
| $\bigcirc$ | Rainbow |  |
| $\bigcirc$ | Aurora． |  |
| $\infty$ | Zodiacal light． Haze． | Due to fine dust，or to the disturbance of atmospheric transparency by air－currents of different densities （＂optical turbidity＂），and not to water－drops．In practice，this is often difficult to distinguish from light fog $\left(\equiv^{\circ}\right)$ ，or＂mist＂of British observers． Prussian and Austrian observers underscore this symbol（ $\simeq$ ）to denote a definitely smoky atmosphere （＂Moorrauch＂）． |
| $\chi$ | Mirage． |  |
| $\bigcirc$ | Exceptional visibil－ ity． |  |
| $\equiv S:$ | Sand storm or dust storm． |  |
| $\begin{aligned} & \text { * Tru } \\ & \text { snowy } \\ & \text { particle } \\ & \text { national } \\ & 281-286 \\ & \dagger \text { Gla. } \end{aligned}$ | a hail，which occurs chiefly pellets，like miniature sno s of clear ice，called slec symbol．On the history <br> $z e$ is the official term in | y with summer thunderstorms，should be distinguished from the wballs，known as graupel，or soft hail（ $\Delta$ ）：also from the small t by the U．S．Weather Bureau，for which there is no inter－ of the word sleet see Monthly Weather Review＇，May，1916，pp． <br> he United States；glazed frost in Great Britain． |

The International Conference of Meteorologists held at Munich in I8gr recommended the following classification of clouds, elaborated by Messrs. Abercromby and Hildebrandsson:
a. Detached clouds with rounded upper outlines (most frequent in dry weather).
b. Clouds of great horizontal extent suggesting a layer or sheet (wet weather).
A. Upper Clouds, average altitude $9000^{m}$.
a. ı. Cirrus.
b. 2. Cirro-stratus.
B. Intermediate Clouds, between $3000^{m}$ and $7000^{m}$.
a. $\left\{\begin{array}{l}\text { 3. Cirro-cumulus. } \\ \text { 4. Alto-cumulus. }\end{array}\right.$
b. 5. Allo-cumulus.
C. Lower Clouds, below $2000^{m}$.
a. 6. Strato-cumulus.
b. 7. Nimbus.
D. Clouds of diurnal ascending currents.
a. 8. Cumulus; top $1800^{\mathrm{m}}$; base $1400^{\mathrm{m}}$.
b. 9. Cumulo-nimbus; top $3000^{m}$ to $8000^{m}$; base $1400^{m}$,
E. High Fogs, under $1000^{m}$.

1o. Stralus.

## DEFINITIONS AND DESCRIPTIONS OF CLOUD FORMS.

I. Cirrus (Ci.). - Detached clouds of delicate and fibrous appearance, often showing a featherlike structure, generally of a whitish color. Cirrus clouds take the most varied shapes, such as isolated tufts, thin filaments on a blue sky, threads spreading out in the form of feathers, curved filaments ending in tufts, sometimes called Cirrus uncinus, etc.; they are sometimes arranged in parallel belts which cross a portion of the sky in a great circle, and by an effect of perspective appear to converge towards a point on the horizon, or, if sufficiently extended, towards the opposite point also. (Ci.-St. and Ci.-Cu., etc., are also sometimes arranged in similar bands.)
2. Cirro-stratus (Ci.-St.). - A thin, whitish shect of clouds sometimes covering the sky completely and giving it only a milky appearance (it is then called Cirro-nebula), at other times presenting, more or less distinctly, a formation like a tangled web. This sheet often produces halos around the Sun and Moon.
3. Cirro-cumulus (Ci.-Cu.). Mackerel sky. - Small globular masses or white flakes without shadows, or showing very slight shadows, arranged in groups and often in lincs.
4. Alto-stratus (A.-St.). - A thick sheet of a gray or bluish color, sometimes forming a compact mass of dark gray color and fibrous structure. At other times the sheet is thin, resembling thick Ci.-St., and through it the Sun or the Moon may be seen dimly gleaming as through ground glass. This form exhibits all changes peculiar to Ci.-St., but from measurements its average altitude is found to be about one half that of $\mathrm{Ci} .-\mathrm{St}$.
5. Alto-cumulus (A.-Cu.). - Largish globular masses, white or grayish, partially shaded, arranged in groups or lines, and often so closely packed that their edges appear confused. The detached masses are generally larger and more compact (resembling St.-Cu.) at the center of the group, but the thickness of the layer varies. At times the masses spread themselves out and assume the appearance of small waves or thin slightly curved plates. At the margin they form into finer flakes (resembling Ci--Cu.). They often spread themselves out in lines in one or two directions.
6. Strato-cumulus (St.-Cu.). - Large globular masses or rolls of dark clouds often covering the whole sky, especially in winter. Generally St.-Cu. presents the appearance of a gray layer irregularly broken up into masses of which the edge is often formed of smaller masses, often of wavy appearance resembling A.-Cu. Sometimes this cloud-form presents the characteristic appearance of great rolls arranged in parallel lines and pressed close up against one another. In their centers these rolls are of a dark color. Blue sky may be seen through the intervening spaces which are of a much lighter color. (Roll-cumulus in England, Wulstcumulus in Germany.) St.-Cu. clouds may be distinguished from Nb. by their globular or rolled appearance, and by the fact that they are not generally associated with rain.
7. Nimbus (Nb.), Rain Clouds. - A thick layer of dark clouds, without shape and with ragged edges, from which steady rain or snow usually falls. Through the openings in these clouds an upper layer of Ci.-St. or A.-St. may be seen almost invariably. If a layer of Nb.
scparates up in a strong wind into shreds, or if small loose clouds are visible floating underneath a large Nb., the cloud may be described as Fracto-nimbus (Fr.-Nb.) ("Seud" of sailors).
8. Cumulus (Cu.), Wool pack Clouds.-Thick clonds of which the upper surface is dome-shaped and exhibits protuberances while the base is horizontal. These elouds appear to be formed by a diurnal ascensional movement which is almost always noticeable. When the cloud is opposite the Sun, the surfaces facing the observer have a greater brilliance than the margins of the protuberances. When the light falls aslant, as is usually the case, these clouds throw deep shadows; when, on the contrary, the clouds are on the same side of the observer as the Sun, they appear dark with bright edges.

True cumulus has well defined upper and lower limits, but in strong winds a broken cloud resembling Cumulus is often seen in which the detached portions undergo continual change. This form may be distinguished by the name Fractocumulus (Fr.-Cu.).
9. Cumulo-nimbus (Cu.-Nb.), The Thunder-Cloud; Shower-Cloud.-Heavy masses of cloud risiny in the form of mountains, turrets or anvils, generally surmounted by a shect or screen of fibrous appearance (false Cirrus) and having at its base a mass of cloud similar to nimburs. From the base local showers of rain or snow (occasionally of hail or soft hail) usually fall. Sometimes the upper edges assume the compact form of cumulus, and form massive peaks round which delicate "false Cirrus" floats. At other times the edges themselves separate into a fringe of filaments similar to Cirrus clouds. This last form is particularly common in spring showers.

The front of thunder-elonds of wide extent frequently presents the form of a large are spread over a portion of a uniformly brighter sky.
10. Stratus (St.).-A uniform layer of cloud resembling a fog but not resting on the ground. When this sheet is broken up into irregular shreds in a wind, or by the summits of mountains, it may be distinguished by the name Fracto-stratus (Fr.-St.).

During summer all low clouds tend to assume forms resembling Cumulus, and may be described accordingly as Stratus cumuliformis, Nimbus cumuliformis, etc.

The term Mammato-cumulus is applied to a cloud having a mammillated lower surface, occurring especially in connection with severe local storms.

The ovoid form, with sharp edges, assumed by certain clouds, particularly during the oecurrence of sirocco, mistral or foehn, is indicated by the adjective lenticularis, e. g., Cumulus lenticularis (Cu. lent.), Stratus Icnticularis (St. lent.). Such clouds frequently show irridescence.

For pictures of typical cloud forms see
Clarke, George A. Clouds. London. 1920.
Great Britain, Meteorological office. Cloud forms according to the international elassification. $2 d$ ed. London. Io2r
Humphreys, William J. Fogs and clouds. Baltimore. 1926.
International meteorological committee. International cloud-atlas. 2d ed. Paris. 1910. [Abridged edition for use of observers. 1930.]
U. S. Weather bureau. Cloud forms according to the international system of classification. 2d ed. Washington. 1928.

Especially intended for the use of mariners, but sometimes used at land stations. The original notation was devised in 1805 by Admiral Sir F. Beaufort; it has since been slightly altered and amplified by British and American meteorologists. The following symbols are used by the marine observers of the U. S. Weather Bureau:

Upper Atmosphere:
b.-Blue sky.
c.-Cloudy sky.
o.-Overcast sky.

Lower Atmosphere:
v.-Visibility (exceptionally clear).
z.-Haze.
m. -Mist.
f.-Fog.

Precipitation:
d.-Drizzling.
p.-Passing showers.
r.-Rain.
s.-Snow.
1.--Hail.

Electric phenomena:
1.-Lightning.
t.-Thunder.

Wind:
q.-Squally.

The British Meteorological Office also uses the following:
e.-Wet air without rain.
g.-Gloom.
u.-Ugly or threatening appearance of the weather.
w.-Dew.
tl.-Thunderstorm.
KQ.-Line squall.
rs.-Sleet (rain and snow together).
fe.-Wet fog.
y.-Dry air (less than $60 \%$ relative humidity).
x.-Hoarfrost.

According to instructions to the marine meteorological observers of the U. S. Weather Bureau, the underscoring of a letter denotes great intensity and double underscoring very great intensity.
The following instructions appear in the Meteorological Observer's Handbook of the British Meteorological Office (1926 edition):
"Capital letters are used to indicate occasions when the phenomenon to be noted is of unusual intensity. At the other end of the scale, occasions of slight intensity are distinguished by adding a small suffix .. Thus,
R.-Heavy rain.
r.-Moderate.
ro.-Slight rain.
and similarly with other phenomena.
"Continuity is indicated by repeating the letter; thus,
RR.-Continuous heavy rain.
rr.-Continuous moderate rain.
"The prefix ' $i$ ' is used to indicate 'occasional' or 'intermittent'; thus,
if.-Occasional fog.
iro.-Intermittent slight rain."

INTERNATIONAL CODE FOR HORIZONTAL VISIBILITY.


SMITHSONIAN TABLES

LIST OF METEOROLOGICAL STATIONS.
Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)


Table 116.
LIST OF METEOROLOGICAL STATIONS.
Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

| CANADA <br> (Continued) | Latitude | Longitude from Greenwich |  | Height |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Feet | m. |
| Halifax. | $44^{\circ} 39^{\prime} \mathrm{N}$. |  | $36^{\prime} \mathrm{W}$. | 88 | 27 |
| *Hay River | 6051 | 115 | 20 | 529 | 161 |
| Hebron. | 5812 |  | 21 | 49 | 15 |
| Herschel Island | 6930 | 139 | 15 | 15 | 5 |
| *Kamloops. | 5041 |  | 29 | 1262 | 385 |
| Lac Seul.... | $50 \quad 17$ | 92 | 12 | 11.40 | 347 |
| Lake Harbor | 6250 | 70 | 40 | 52 | 16 |
| Lake Louise...... | $\begin{array}{rrr}51 & 23 \\ 49 & 0\end{array}$ |  | 8 | 5670 | 1728 |
| Le Pas. | 5349 | 101 | 15 | 860 | 262 |
| Mayo Landing. | 6335 | 135 | 51 | 1900 | 579 |
| Medicine Hat. | 501 | 110 | 37 | 2144 | 653 |
| *Minnedosa | 5015 | 99 | 50 | 1690 | 515 |
| *Mistassini Post | 5015 | 73 | 55 | 1255 | 383 |
| Montreal. | 4530 | 73 | 35 | 187 | 57 |
| *Moose Factory | $5 \mathrm{I} \quad 14$ | 80 | 30 | 30 | 9 |
| Nain.. | 5633 | 61 | 41 | 13 | 4 |
| * Natashquan .... | 508 | 61 | 48 | 20 | 6 |
| Northwest River | 533 | 60 | 10 |  |  |
| Norway House. | $53 \quad 58$ | 97 | 51 | 720 | 219 |
| Ottawa. | $45 \quad 24$ | 75 | 43 | 294 | 90 |
| Pagwa.. | 503 | 85 | 18 | 620 | 189 |
| Pangnirtung. | 6530 | 66 | 9 |  | ... |
| Parry Sound | $45 \quad 19$ | 80 | o | 635 | 194 |
| Ponds Inlet. | 72 <br> 8 | 78 | 30 | 13 | 4 |
| *Port Arthur | $48 \quad 27$ | 89 | 12 | 644 | 196 |
| *Port aux Basques | $47 \quad 35$ | 59 | 10 | 30 | 9 |
| Port Harrison... | $\begin{array}{ll}58 & 25\end{array}$ |  | 21 | 12 | 4 |
| *Port Nelson. | 57 o | 92 | 51 | 49 | 15 |
| *Prince Albert | 5310 | 105 | 38 | 1450 | 442 |
| *Prince Rupert | 5+ 18 | 130 | 18 | 170 | 52 |
| Qu'Appelle. | $50 \quad 30$ | 103 | 47 | 2115 | 645 |
| Quebec.......... ${ }^{\text {Queen Charlotte City }}$ | 4648 | 71 | 13 | 296 | 90 |
| Queen Charlotte City | $\begin{array}{ll}53 & 13\end{array}$ | 132 | 15 | ... |  |
| *Sable Island | 4357 | 60 | 6 | 25 | 8 |
| *Saint John. | 4517 | 66 | 4 | 119 | 36 |
| *Saint Johns. | 4734 |  | $+^{2}$ | 125 | 38 |
| *Southwest Point, Anticosti | $49 \quad 24$ | 63 | 33 | 30 | 9 |
| Sudbury.. | $46 \quad 27$ | 81 | $\stackrel{2}{5}$ | 857 | 261 |
| Swift Current | 5020 | 107 | 45 | 2392 | 729 |
| Sydney. | 46 IO | 60 | 10 | 48 | 15 |
| *Toronto. | 4340 |  | 24 | 379 | 116 |
| Trout Lake | $53 \quad 52$ | 89 | 46 | 1128 | 344 |
| Vancouver. | 49 I7 |  | 5 | 136 | 41 |
| *Victoria. | $48 \quad 24$ | 123 | 19 | 230 | 70 |
| White River | $48 \quad 35$ | 85 | 16 | 1244 | 379 |
| *Winnipeg. | $49 \quad 53$ | 97 | 7 | 760 | 232 |
| CANAL ZONE |  |  |  |  |  |
| Balboa Heights. | $8 \quad 58 \mathrm{~N}$. |  | 33 W. |  | 36 |
| Cristobal (Colon). Culebra. | $\begin{array}{rr} 91 & 21 \\ 9 & 3 \end{array}$ |  | $\begin{aligned} & 55 \\ & 39 \end{aligned}$ | 36 40 4 | 11 123 |

## LIST OF METEOROLOGICAL STATIONS.

Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)


Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

|  | Latitude |  | Longitude from Greenwich |  | Height |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Feet | m. |
| Motozintla. | $15^{\circ}$ | $22^{\prime} \mathrm{N}$. |  | $14^{\prime} \mathrm{W}$ | 4774 | ${ }^{1} 455$ |
| Oaxaca.. | 17 | 4 |  | 42 | 5128 | 1563 |
| Pachuca. | 20 | 8 | 98 | 45 | 7989 | 2435 |
| Panuco. |  | 24 | 105 | 58 | 2625 | 800 |
| Parral. | 26 | 58 | 105 | 40 | 5420 | 1652 |
| Payo Obispo. | 18 | 30 | 88 | 20 | 13 | 4 |
| Progreso.... |  | 17 | 89 | 40 | 46 | 14 |
| * Puerto Mexico | 18 | 9 | 94 | 24 | 46 | 14 |
| *Salina Cruz.... San Luis Potosi | 16 | 12 | 95 100 | $\begin{array}{r}12 \\ 58 \\ \hline\end{array}$ | 189 6158 | 56 |
| *Tacubaya (Mexico City) | 19 | 24 | 109 99 | 11 | 7575 | 1877 |
| Tampico... . . . . . . . . | 22 | 13 | 97 | 51 | - 59 | 18 |
| Tapachula. | 14 | 54 | 92 | 16 | 551 | 168 |
| Teapa. | 17 | 33 | 92 | 57 | 148 | 45 |
| Tehuacan. | 18 | 28 | 97 | 23 | 5420 | 1652 |
| Tenosique. | 17 | 29 | 91 | 26 | 197 | 60 |
| Tepic. | 20 | 31 | 104 | 53 | 3025 | 922 |
| Tuxtla Gutierrez. | 16 | 45 | 93 | 6 | 1759 | 536 |
| Valladolid. | 20 | 41 | 88 | 13 | 72 | 22 |
| Vera Cruz. | 19 | 12 | 96 | 8 | 52 | 16 |
| Victoria.. | 23 | 43 | 99 | 8 | 1040 | 317 |
| Zacatecas | 22 | 47 | 102 | 34 | 8570 | 2612 |
| UNITED STATES |  |  |  |  |  |  |
| *Abilene. | 32 | 23 N. |  | 40 W. | 1738 | 530 |
| Albany. | 42 | 39 | 73 | 45 | 97 | 30 |
| Alpena.. | 45 | 5 | 83 | 30 | 609 | 186 |
| Amarillo. | 35 | 13 | 101 | 50 | 3676 | 1120 |
| Anniston. | 33 | 39 | 85 | 50 | 741 | 226 |
| Apalachicola | 29 | 45 | 84 | 58 | 36 | 11 |
| Asheville. | 35 | 36 | 82 | 32 | 2253 | 687 |
| Atlanta. | 33 | 45 | 87 | 23 | 1173 | 358 |
| Atlantic City. | 39 | 22 | 74 | 25 | 52 | 16 |
| Augusta. | 33 | 28 | 81 | 54 | 182 | 55 |
| Austin. | 30 | 16 | 97 | 44 | 605 | 184 |
| Baker.. | 44 | 46 | 117 | 50 | 3471 | 1058 |
| Baltimore. | 39 | 17 | 76 | 37 | 123 | 37 |
| Bentonville.. | 36 | 22 | 94 | 12 | 1303 | 397 |
| Binghamton. | 42 | 6 | 75 | 55 | 871 | 265 |
| Birmingham. | 33 | 32 | 86 | 50 | 700 | 213 |
| *Bismarck. | 46 | 47 | 100 | 38 | 1674 | 510 |
| Block Island. | 41 | 10 | 71 | 36 | 26 | 8 |
| Boise. | 43 | 37 | 116 | 13 | 2739 | 835 |
| Boston... | 42 | 21 | 71 | 4 | 125 | 38 |
| Broken Arrow | 36 | 2 | 95 | 49 | 765 | 233 |
| Brownsville. | 26 | $\bigcirc$ | 97 | 26 | 57 | 17 |
| Buffalo... | 42 | 53 | 78 | 53 | 767 | 234 |
| Cairo | 44 | 29 | 73 | 12 | 403 | 123 |
| Cairo... | 37 | 0 | 89 | 10 | 358 | 109 |
| Canton. . . | 44 | 36 | 75 | 10 | 448 | 137 |
| Cape Henry.. | 36 | 56 | 76 | $\bigcirc$ | 18 | 5 |
| * Charles City. | 43 | 4 | 92 | 38 | 1015 | 309 |
| * Charleston. | 32 | 47 | 79 | 56 | 48 | 15 |
| Chattanooga. | 35 35 | 13 4 | 85 | 51 14 | 779 762 | 237 232 |

LIST OF METEOROLOGICAL STATIONS.
Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)


LIST OF METEOROLOGICAL STATIONS.
Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

| UNITED STATES (Continued) | Latitude |  | Longitude from Greenwich |  | Height |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Feet | m . |
| Jacksonville. |  | $20^{\prime} \mathrm{N}$ | $81^{\circ}$ | $39^{\prime} \mathrm{W}$. | 43 | I 3 |
| Kalispell... | 48 |  | 11.4 | 25 | 2973 | 906 |
| K゙ansas City. | 39 | 5 | 94 | 37 | 963 | 294 |
| Keokuk. | 40 | 22 | 91 | 26 | 614 | I 87 |
| *Key West. | 24 | 33 | 81 | 48 | 22 | 7 |
| Knoxville. | 35 | 56 | 83 | 58 | 995 | 303 |
| La Crosse. | 43 | 49 | 91 | 15 | 714 | 218 |
| Lander.. | 42 | 50 | 108 | 45 | 5372 | 1637 |
| Lansing. | 42 | 44 | 84 | 26 | 878 | 268 |
| Lewiston. | 46 | 25 | 117 | 2 | 757 | 231 |
| Lexington | 38 | 2 | 8.4 | 33 | 989 | 301 |
| Lincoln... | 40 | 49 | 96 | 45 | 1189 | 362 |
| Little Rock. | $3+$ | 45 | 92 | 16 | 357 | 109 |
| Los Angeles. | $3+$ | 3 | 118 | 15 | 338 | 103 |
| Louisville. . | 38 | 15 | 85 | 45 | 525 | 160 |
| Ludington.. | 43 | 57 | 86 | 27 | 637 | 19.4 |
| Lynchburg. | 37 | 25 | 79 | 9 | 681 | 208 |
| Macon.. . . | 32 | 50 | 83 | 38 | 370 | 113 |
| Madison. | 43 | 5 | 89 | 23 | 974 | 297 |
| Marquette | 46 | 34 | 87 | 24 | 734 | 22.4 |
| Memphis. | 35 | 9 | 90 | 3 | 399 | 122 |
| Meridian. | 32 | 21 | 88 | 40 | 375 | 114 |
| Miami. | 25 | 48 | 80 | 12 | 25 | 8 |
| Miles City. | 46 | 25 | 105 | 49 | 2371 | 723 |
| Mikwatkee. | 43 | 2 | 87 | 54 | 681 | 208 |
| Minneapolis. | 44 | 59 | 93 | 18 | 918 | 280 |
| *Mobile . . . . | 30 | 41 | 88 | 2 | 57 | 17 |
| *Modena.. | 37 | 48 | 113 | 54 | 5473 | 1668 |
| Montgomery | 32 | 23 | 86 | 18 | 223 | 68 |
| Moorhead. | 46 | 52 | 96 | 44 | 940 | 286 |
| Nantucket. | 41 | 17 | 70 | 6 | 12 | 4 |
| *Nashville. | 36 | 10 | 86 | 47 | 546 | 166 |
| New llaven | 41 | 18 | 72 | 56 | 106 | 32 |
| * New Orleans. | 29 | 57 | 90 | 4 | 53 | 16 |
| New York. | 40 | 43 | 74 | 0 | 314 | 96 |
| Norfolk. | 36 | 51 | 76 | 17 | 91 | 28 |
| Northfield. | 44 | 10 | 72 | 41 | 876 | 267 |
| North Head. | 46 | 16 | 124 | 4 | 211 | 64 |
| *North Platte. | 41 | 8 | 100 | 45 | 2821 | 860 |
| Oklahoma City | 35 | 26 | 97 | 33 | 1214 | 370 |
| Omaha... | 41 | 16 | 95 | 56 | 1105 | 337 |
| Oswego. | 43 | 29 | 76 | 35 | 335 | 102 |
| Palestine. | 31 | 45 | 95 | 40 | 510 | 155 |
| Parkersburg | 39 | 16 | 81 | 36 | 637 | 19.4 |
| Pensacola. . | 30 | 25 | 87 | 13 | 56 | 17 |
| Peoria. | 40 | 43 | 89 | 36 | 609 | 186 |
| Philadelphia | 39 | 57 | 75 | 9 | 114 | 35 |
| Phoenix.. | 33 | 28 | 112 | $\bigcirc$ | 1108 | 338 |
| Pierre... | $4+$ | 22 | 100 | 21 | 1572 | 479 |
| Pittsburgh. | 40 | 26 | 80 | 0 | 842 | 257 |
| Pocatello. . | 42 | 52 | 112 | 29 | 4477 | 1365 |
| Port Angeles. | 48 | 7 | 123 | 6 | 29 | 9 |
| Port Arthur. | 29 | 52 | 93 | 55 | 634 | 10 |
| Port Huron... | 43 | 0 | 82 | 26 | 638 | 19.4 |
| Portland, Me. | 43 | 39 | 70 | 15 | 103 | 31 |

## LIST OF METEOROLOGICAL STATIONS.

Note.-Stations with asterısk appear in the "Réseau Mondial" of the British
Meteorological Office for 1922. (London, 1929.)

| UNITED STATES <br> (Continued) | Latitude |  | Longitude from Greenwich |  | Height |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Feet | m. |
| *Portland, Ore. | $45^{\circ}$ | $32^{\prime} \mathrm{N}$ |  | $41^{\prime} \mathrm{W}$ | 1.53 | 47 |
| Providence. . |  | 50 | 71 | 25 | 160 | 49 |
| Pueblo.. |  | 18 | 104 | 36 | 4685 | 1428 |
| Raleigh.. |  | 45 | 78 | 37 | 376 | 115 |
| Rapid City. | 44 | 4 | 103 | 12 | 3259 | 993 |
| Reading. |  | 20 | 75 | 58 | 325 | 99 |
| Red Bluff |  | 10 | 122 | 15 | 332 | 101 |
| Reno. | 39 | 32 | 119 | 49 | 4532 | 1381 |
| Richmond. | 37 | 32 | 77 | 27 | 144 | 4 |
| Rochester | 43 | 8 | 77 | 42 | 523 | 159 |
| Roseburg. | 43 | 13 | 123 | 20 | 510 | 155 |
| Roswell. | 33 | 24 | 104 | 27 | 3566 | 1087 |
| Royal Center |  | 53 | 86 | 29 | 736 | 224 |
| Sacramento. | 38 | 35 | 121 | 30 | 69 | 21 |
| St. Joseph. | 39 | 49 | 94 | 51 | 967 | 295 |
| *St. Louis. | 38 | ${ }_{58}^{88}$ | 90 | 12 | 568 | 173 |
| St. Paul.. | 44 | 58 | 93 | 3 | 837 | 255 |
| *Salt Lake City.. | 40 | 46 | 111 | 54 | 4360 | 1329 |
| San Antonio | 29 | 27 | 98 | 28 | 693 | 211 |
| *San Diego. | 32 | 43 | 117 | 10 | 87 | 27 |
| Sandusky | 41 | 25 | 82 | 40 | 629 | 192 |
| Sandy Hook. | 40 | 28 | 74 | 1 | 22 | 7 |
| *San Francisco. | 37 | 48 | 122 | 26 | 155 | 47 |
| San Jose. | 37 | 20 | 121 | 54 | 141 | 43 |
| *Santa Fe. | 35 | 41 | 105 | 57 | 7013 | 2138 |
| Sault Ste. Maric | 46 | 30 | 84 | 21 | 614 | 187 |
| Savannah | 32 | 5 | 81 | 5 | 65 | 20 |
| Scranton |  | 24 | 75 | $4^{2}$ | 805 | 245 |
| Seattle. | 47 | 38 | 122 | 20 | 125 | 38 |
| Sheridan. | 44 | 48 | 106 | 57 | 3790 | 1155 |
| Shreveport | 32 | 20 | 93 | 40 | 249 | 76 |
| Sioux City | 42 | 29 | 96 | 24 | 1135 | $3+6$ |
| Spokane. | 47 | 40 | 117 | 25 | 1929 | 588 |
| Springfield, III. | 39 | 48 | 89 | 39 | 636 | 194 |
| Springfield, Mo. | 37 | 12 | 93 | 18 | 1324 | 404 |
| Syracuse... | 43 | 2 | 76 | 10 | 597 | 182 |
| Tacoma.. | 47 | 16 | 122 | 23 | 194 | 59 |
| Tampa.. | 27 | 57 | 82 | 27 | 35 | 11 |
| Tatoosh Island. | $4^{8}$ | 23 | 124 | $4+$ | 86 | 26 |
| Taylor. | 30 | 35 | 97 | 20 | 583 | 178 |
| Terre Haute. | 39 | 29 | 87 | 24 | 575 | 175 |
| Thomasville |  | 48 | 83 | 58 | 273 | 83 |
| Toledo... | 41 | 40 | 83 | 34 | 628 | 191 |
| Tonopah. | 38 | 4 | 117 | 4 | 6090 | 1856 |
| Topeka. | 39 | 3 | 95 | 41 | 987 | 301 |
| Trenton.. |  | 14 | 74 | 45 | 190 | 58 |
| Valentine. | 42 | 50 | 100 | 32 | 2598 | 792 |
| Vicksburg. | 32 | 22 | 90 | 53 | 247 | 75 |
| Walla Walla. | 46 | 2 | 118 | 20 | 991 | 302 |
| *Washington. | 38 | $5+$ | 77 | 3 | 112 | 34 |
| Wichita. | 37 | 41 | 97 | 20 | 1358 | $4{ }^{1 / 4}$ |
| Williston. | 48 | 9 | 103 | 35 | 1878 | 572 |
| Wilmington. | 34 | 14 | 77 | 57 | 78 | 24 |
| Winnemucca. |  | 58 | 117 | 43 | 4344 | 1324 |
| Wytheville. Yankton.. |  | 56 54 |  |  | 2304 1233 | 702 376 |
| Yellowstone Park |  |  |  |  | 6241 | 376 1902 |
| Yuma. |  | 45 | 114 | 36 | 141 | 43 |

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## LIST OF METEOROLOGICAL STATIONS.

Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

| BOLIVIALa Paz............ | Latitude |  | Longitude from Greenwich |  | Height |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{array}{lll}16^{\circ} & 30^{\prime} \mathrm{S} \\ 19 & 3\end{array}$ |  |  | $\begin{gathered} 9^{\prime} \mathrm{W} . \\ 16 \end{gathered}$ | $\begin{gathered} \text { Feet } \\ 11909 \\ 9344 \end{gathered}$ | $\begin{aligned} & 3630 \\ & 2848 \end{aligned}$ |
|  |  |  |  |  |  |  |
| *Sucre. |  |  |  |  |  |  |
| BRAZIL |  |  |  |  |  |  |
| Alto Itatiaya. | $22 \quad 25 \mathrm{~S}$. |  | $44 \quad 50 \mathrm{~W}$. |  | $\begin{array}{r}7152 \\ \hline 20\end{array}$ | 21806 |
| *Aracaju... |  | 55 | 37 | 3 |  |  |
| *Bahia (Ondina). |  |  | 38 31 |  | 154266 | 4781 |
| * Barra do Corda. | 530 |  | 45 |  |  |  |
| Belem (Para). |  | 27 | 48 | 29 | 43 | $\begin{array}{r} 13 \\ 895 \end{array}$ |
| *Bello Horizonte | 19 | 55 | 4355 |  | 2936 |  |
| Boa Vista. |  | 49 N. | 60 | 4 |  | $\begin{aligned} & 630 \\ & 897 \end{aligned}$ |
| * Brotas.. | 22 | 16 S . | 48 | 4 | 2067 |  |
| *Caetite.. | 14 | 3 | 42 | 37 | 2943 |  |
| Coary. |  | 22 | 63 3 |  | 509 |  |
| *Corumba. | 1859 |  | $\begin{array}{ll}57 & 39 \\ 49 & 17\end{array}$ |  |  | 155908 |
| *Curityba. |  | 25 |  |  | 2979 |  |
| *Cuyaba. | 15 | 36 | 56 |  | 541 | 165 |
| *Fernando Noronha | 3 | 50 | 3225 |  | 348 | 106 |
| Floriano Peixoto. | 9 | 1 | $\begin{array}{ll}67 & 26 \\ 66\end{array}$ |  | … $\quad \ldots$. |  |
| Fonte Boa. |  | 35 |  |  |  |  |  |  |
| Formosa. | 15 | 32 |  |  | 299285 | 91226 |
| Fortaleza (Porongaba) |  | 46 | $38 \quad 32$ |  |  |  |
| Goyaz..... | 15 | 55 | 60 |  | 1706 | 520 |
| *Manaos.... |  | 8 |  |  | 144 | 441080 |
| Morro do Chapeo | 11 | 33 | 41.14 |  | $\begin{aligned} & 35+3 \\ & 2326 \end{aligned}$ |  |
| Passo Fundo. | 28 | 16 | 3646 |  |  | 709677 |
| Pesquira. |  | $2+$ |  |  | 2221 |  |
| Pirapora.... | 17 | 21 | $\begin{array}{ll}44 & 57 \\ 51 & 13\end{array}$ |  | 1549 | 472 |
| *Porto Alegre... | 30 | 1 |  |  | $\begin{array}{r} 30 \\ 778 \\ 407 \end{array}$ | 11 |
| Porto Nacional | 10 | 39 | 4820 |  |  | 237124 |
| Porto Velho. ${ }^{\text {P }}$ | 8 | 47 | $\begin{array}{ll}63 & 55 \\ 39 & 15\end{array}$ |  |  |  |
| *Quixeramobim....... | 5 | 16 | $\begin{array}{ll}39 & 15 \\ 34 & 52\end{array}$ |  | 67998 | 207 |
| Recife (Pernambuco) | 8 | 4 |  |  | 30 |  |
| Remate de Males.. | 4 | 21 | $70 \quad 24$ |  |  | 98 | $\ldots$ |
| Rio Grande do Sul. | 32 | 2 | 52 | 6 | 10 | 361 |
| *Rio de Janeiro. | 22 | 54 | 43 10 |  | 200 |  |
| S. Felippe. |  | 43 | $\begin{array}{rr}69 & 57 \\ 67 & 3\end{array}$ |  | \% <br> 279 <br> 66 | 8520 |
| S. Luiz (Maranhao) |  | 32 | $44 \quad 17$ |  |  |  |
| São Paulo. | 23 | 33 | 46 | 38 | 2690 | 82020 |
| *Taperinha. |  | 30 | $54 \quad 20$ |  | 66 |  |
| Theophilo Ottoni. | 17 | 50 | 41 | 26 | 1001 | 305 |
| Theresopolis | 22 | 27 | 4255 |  | 3120 | 951350 |
|  | 20 | 47 | $47 \quad 56$ |  | 11482493 |  |
| Uberaba. | 19 | 41 |  |  | 760 |  |
| Uruguayana. |  | 45 | 57 | 5 |  | 243 | 74 |
| CHILE |  |  |  |  |  |  |
| Antofagasta. | $23 \quad 39 \mathrm{~S}$. |  | $70 \quad 25 \mathrm{~W}$. |  | 308 | 94 |
| Arica.... | 18 | 28 | $\begin{array}{ll}70 & 20 \\ 70\end{array}$ |  | 1649 | 515 |
| Bahia Felix. |  | 58 | 74 4 |  |  |  |
| Cabo Raper |  | 50 |  | 56 | 131 | 4028 |
| Caldera............... |  | 3 | $\begin{array}{rr}70 & 53 \\ 73 & 6\end{array}$ |  | 9239489 |  |
| ${ }^{*}$ *Conceplion (P. Toumbes) |  | 37 56 |  |  | $\begin{array}{r} 120 \\ 27 \end{array}$ |  |

Smithsonian Tables

Table 116.
LIST OF METEOROLOGICAL STATIONS.
Note.--Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

|  | Latitude |  | Longitude from Greenwich |  | Height |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Feet | m . |
| El Teniente. | $34^{\circ}$ | $6^{\prime} \mathrm{S}$ |  | $38^{\prime} \mathrm{VW}$. | 7001 | 2134 |
| * Evanjelistas. |  | 24 |  | 6 | 180 | 55 |
| *Iquique. . . . |  |  |  | 11 | 30 | 9 |
| *Juan Fernandez.. |  |  | 78 | 50 | 1132 | 345 |
| Lonquimay. | 38 |  | 71 | 14 | 3182 | 970 |
| Melinka... | 43 | 54 | 73 | 46 | 16 | 5 |
| Potrerillos.. | 26 | 30 | 69 | 27 | 9350 | 2850 |
| Puerto Montt. | 41 | 28 | 72 | 57 | 328 | 100 |
| * Punta Arenas.... | 53 | 10 | 70 | 54 | 92 | 28 |
| * Punta Dungeness. |  | 2.4 | 68 | 26 | 16 | 5 |
| *Santiago. | 33 | 27 | 70 | 42 | 1706 | 520 |
| Talca. |  | 26 | 71 | 40 | 322 | 98 |
| Temuco. | 38 | 45 | 72 | 38 | 361 | 110 |
| Valdivia............. | 39 | 48 | 73 | 14 | 30 | 9 |
| *Valparaiso (P. Angeles). | 33 | 1 | 7 I | 38 | 135 | 41 |
| COLOMBIA |  |  |  |  |  |  |
| Andagoya. | 5 | 4 N | 76 | 55 W . | 250 | 76 |
| *Bogota... |  | 36 | 74 | 5 | 8677 | 26.5 |
| Bucaramanga. | 6 | 52 | 73 | 34 | 3340 | 1018 |
| Buenaventura. | 3 | 53 | 77 | 10 |  | . . . |
| Pasto.. | I | 13 | 77 | 28 | 8510 | 2594 |
| Popayan | 2 |  | 76 | 36 | 5709 | 1740 |
| ECUADOR |  |  |  |  |  |  |
| Ambato. | I | 15 S. | 78 | 37 W | 8.19 | 2566 |
| Banos.. | 1 | 24 | 78 | 2.4 | 5906 | 1800 |
| Guay $\mathrm{Qu} \mathrm{S}^{\text {Quito. }}$ | 2 | 12 | 79 | 5 I | 40 | $12$ |
| Quito. |  | 14 |  | 30 | 9239 | $28 \mathrm{I} 6$ |
| GUIANA |  |  |  |  |  |  |
| * Cayenne. |  | 56 N. |  | 2 I W. | 20 | 6 |
| Dadanawa. |  | 48 |  | 26 | . . . |  |
| *Georgetown |  | 50 | 58 | 12 | 6 | 2 |
| *Paramaribo.. |  | 49 | 55 | 9 | 12 | 4 |
| Placer R'Awa. |  |  | 54 | 0 |  |  |
| PARAGUAY |  |  |  |  |  |  |
| *Asuncion. |  | 21 S. | 57 | 37 WV . | 305 | 93 |
| Mision Inglesa. | 23 | 23 | 58 | 23 | 361 | 110 |
| Puerto Bertoni. |  | 40 | 54 | 35 | 5 5 | 157 |
| PERU |  |  |  |  |  |  |
| *Arequipa. | 16 | 22 S. | 71 | 33 W | 7874 | 2.400 |
| Cerro de Pasco. | 10 | 46 | 76 | 6 | 14272 | 4350 |
| Cuzco.. | 13 | 31 | 72 | 3 | I 1319 | $3+50$ |
| El Misti. | 16 | 16 | 71 | 30 | 19200 | 5852 |
| Lima. |  |  |  | 3 | 512 | I 56 |
| Piura. | 5 | $9$ | 80 | 40 | 16.4 | 50 |
| URUGUAI |  |  |  |  |  |  |
| Durazno. |  | 19 S. |  | 33 W. | 299 | 9 I |
| *Montevideo |  | $5^{2}$ |  | 32 | 95 | 29 |

[^30]

Table 116.
LIST OF METEOROLOGICAL STATIONS.
Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

| CZECHO-SLOVAKIA | Latitude |  | Longitude from <br> Greenwich |  | Height |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Feet | m . |
| Brünn. |  | $11^{\prime} \mathrm{N}$. |  | $35^{\prime} \mathrm{E}$. | 820 | 250 |
| C. Budejovice. |  | 58 |  | 27 | 1283 | 391 |
| Cheb . . . . . . . |  | 4 |  | 26 | I 585 | 483 |
| Kosice. |  | 44 |  | 15 | 689 | 210 |
| Prague.. | 50 | 5 | 14 | 25 | 663 | 202 |
| DENMARK |  |  |  |  |  |  |
| * Copenhagen | 55 | 4 IN. |  | 33 E. | 43 | 13 |
| Fanö....... | 55 | 27 | 8 | 24 | 20 | 6 |
| Sand (Faroe Islands). | 61 | 52 | 6 | 49 | 7 | 2 |
| Tvingstrup. . . . . . . . | 55 | 53 | 9 | 55 | 217 | 66 |
| Vestervig... |  | 47 | 8 | 19 | 62 | 19 |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| FINLAND |  |  |  |  |  |  |
| *Helsingfors . . . . . . | 60 | 12 N . | 24 | 55 E . | 157 | 48 |
| Inari.. | 68 | 57 | 26 | 49 | 502 | 153 |
| Kajaani. | 64 | I 3 | 27 | 46 | 479 | 146 |
| *Kuopio. | 62 | 55 | 27 | 40 | 761 | 233 |
| Sodankyla. | 67 | 22 | 26 | 39 | 591 | 180 |
| Sortavala.. | 61 | 42 | 30 | 41 | 62 | 19 |
| Tammerfors. | 61 | 30 | 23 | 46 | 325 | 99 |
| Vaasa..... . | 63 | 5 |  | 37 | 30 | 9 |
| FRANCE |  |  |  |  |  |  |
| Aurillac... | 44 | 56 N | 2 | 26 E. | 2247 | 685 |
| Bordeaux. | 44 | 50 | 0 | 42 W | 243 | 74 |
| Brest.... | 48 | 23 | 4 | 30 | 210 | 64 |
| Charleville. . . | 49 | 46 | 4 | 43 E. | 476 | 145 |
| Chateaureaux. | 46 | 49 | I | 4 I | 512 | 156 |
| Cherbourg.. | 49 | 39 | 1 | 38 W. | 59 -81 | 18 |
| Dijon. . . . | 47 | 19 | 5 | 2 E . | 781 | 238 |
| Dunkerque. | 51 | 2 | 2 | 22 | 52 | 16 |
| Gap. . | 44 | 34 | 6 | 5 | 2425 | 739 |
| Havre. | 49 | 29 | 0 | 6 | 102 | 3 I |
| * Lyon. . | 45 | 41 | 4 | 47 | 981 | 299 |
| *Marseille.. . . . . . . . . . . | 43 | ${ }^{18}$ | 5 | 23 | 2.46 | 75 |
| Mont Blanc (Des Bosses) | 45 | 59 | 6 | 5 I | 14301 | 4359 |
| Mont Ventoux. . . . . . . . . | 44 | 10 | 5 | 17 | 6234 | 1900 |
| Nancy | 48 | 42 | 6 | 11. | 718 | 219 |
| *Nantes... . . . . . . . | 47 | 15 | 1 | 34 W. | 121 | 37 |
| Nice (observatory) . . . | 43 | 43 | 7 | 18 E . | 1138 | 347 |
| *Paris (Parc St. Maur). | 48 | 48 | 2 | 30 | 164 | 50 |
| Pic du Midi... . . . . . | 42 | 56 | 0 | -8 | 9380 | 2859 |
| Puy de Dome. <br> Rennes. | 45 | 46 | 2 | 58 | 4813 | 1467 |
| Rennes. Toulouse | 48 | 37 | I | 41 lV . | 105 | 32 |
| Toulouse. | 43 | 37 |  | 27 E. | 6.36 | 194 |
| GERMANY |  |  |  |  |  |  |
| Berlin... |  | 31 N | 13 | 22 E. | 184 | 56 |
| Bremen. | 53 | 5 | 8 | 47 | 52 | 16 |

## LIST OF METEOROLOGICAL STATIONS.

Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

| GERMANY <br> (Continued) | Latitude |  | Longitude from Greenwich |  | Height |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Feet | m. |
| Breslau. | $51^{\circ}$ | $7^{\prime} \mathrm{N}$ | $17^{\circ}$ | $5^{\prime} \mathrm{E}$. | 397 | 121 |
| Brocken. |  | 48 |  | 37 | 3785 | 1153 |
| Cassel. |  | 20 |  | 31 | 659 | 201 |
| Cologne. |  | 56 |  | 57 | 184 | 56 |
| Dresden. |  | 4 |  | 44 | 361 | 110 |
| Flensburg |  | 47 |  | 27 | 52 | 16 |
| Frankfort on the Main |  | 7 | 8 | 39 | 394 | 120 |
| Freiburg. |  | 59 |  | 51 | 912 | 278 |
| *Hamburg. | 53 | 33 | 9 | $5^{8}$ | 131 | 40 |
| Königsberg |  | 43 |  | 30 | 75 | 23 |
| Koslin. . . . | 54 | 12 | 16 | 11 | 15 I | 46 |
| Leipzig. | 51 | 20 | 12 | 23 | 404 | 123 |
| Munich.. |  | 9 | 11 | 34 | 1726 | 526 |
| Münster. |  | $5^{8}$ |  | 37 | 210 | 64 |
| Nuremberg | 49 | 27 |  | 3 | 1020 | 311 |
| Osterode. . | 53 | 42 | 19 | 58 | 367 | 112 |
| *Potsdam. | 52 | 23 | I 3 | 4 | 279 | 85 |
| Schneekoppe. | 50 | 44 | 15 | 44 | 5282 | 1610 |
| Stettin.. . . |  | 26 |  | 34 | 85 | 26 |
| Stuttgart. |  | 47 |  | 10 | 883 | 269 |
| Trier... |  | 25 | 6 | 39 | 486 | 148 |
| Zugspitze. |  | 25 |  | 59 | 9718 | 2962 |
| GREECE |  |  |  |  |  |  |
| Adrianople. | 4 I | 40 N. | 26 | 38 E . | 279 | 85 |
| *Athens... . | 37 | 58 | 23 | 43 | 351 | 107 |
| Corfu. | 39 | 37 |  | 57 | 108 | 33 |
| Mitylene | 39 | 6 | 26 | 34 | 131 | 40 |
| Naxos. . | 37 | 6 | 25 | 23 | 13 | 4 |
| Patras. | 38 | I 5 | 21 | 45 | 134 | 4 I |
| Salonika. | 40 | $3+$ | 22 | 59 | 230 | 70 |
| Tripolitza. | 37 | 3 I | 22 | 23 | 2182 | 665 |
| HUNGARY |  |  |  |  |  |  |
| *Budapest. | 47 | 3 I N. | 19 | 1 E. | 426 | 130 |
| Debreczen.. | 47 | 23 | 21 | 38 | 423 | 129 |
| Nagy-Kanizsa | 46 | 28 | 17 | 0 | 535 | 163 |
| Szeged...... . | 46 | 15 | 20 | 9 | 312 | 95 |
| ITALY |  |  |  |  |  |  |
| Avellino.. |  |  |  |  | 1214 | 370 |
| Bari. . | 41 | 8 | 16 | 52 | 39 | 12 |
| Belluno. | 46 | 9 | 12 | 23 | 1325 | 404 |
| Bologna.. | 44 | 30 | 11 | 18 | 180 | 55 |
| Catanzaro. | 38 | 55 | 16 | 36 | 1312 | 400 |
| Chieti. | 42 | 21 |  | 10 | 1119 | 341 |
| Fiume. . . | 45 | 20 | 14 | 24 | 79 | 24 |
| Florence. | 43 | 46 |  | 15 | 164 | 50 |
| Genoa. | 44 | 25 |  | 56 | 69 | 21 |
| Lecce. . | 40 | 21 | 18 | 10 | 256 | 78 |
| Livorno. | 43 | 33 |  | I 8 | 10 | 3 |
| Milan... | 45 | 28 |  | 9 8 | 482 | 147 |
| Naples.. |  |  |  | 18 | 489 | 149 |
| Perugia. | 43 | 7 |  | 2 I | 1617 | 493 |

Table 116.
LIST OF METEOROLOGICAL STATIONS.
Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)


LIST OF METEOROLOGICAL STATIONS.
Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

|  | Latitude |  | Longitude from Greenwich |  | Height |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Feet | m. |
| *Mehavn. |  | $\mathrm{I}^{\prime} \mathrm{N}$. |  | $47^{\prime} \mathrm{E}$. | 33 | 10 |
| Oslo. |  | 55 |  | 43 | 82 | 25 |
| Tromso. |  | 39 |  | 57 | 374 | 114 |
| *Trondhjem. |  | 26 |  | 25 | 194 | 59 |
| *Vardo.... |  | 22 |  | 8 | 46 | 14 |
| POLAND |  |  |  |  |  |  |
| Bialystok. | 53 | 8 N. | 23 | $\bigcirc$ E. | 463 | 141 |
| Cracow. . | 50 | 4 | 19 | 58 | 725 | 221 |
| Lemberg. | 49 | 50 | 24 | 1 | 1093 | 333 |
| Nowyport (Neufahrwasser) | 54 | 24 |  | 40 | 36 | 11 |
| Posen.. |  | 25 |  | 56 | 299 | 91 |
| Sarny. | 51 | 22 |  | 34 | 518 | 158 |
| Vilna. | 54 | 4 | 25 | 15 | 446 | 136 |
| *Warsaw. |  | 13 |  | 3 | 295 | 90 |
| PORTUGAL |  |  |  |  |  |  |
| Coimbra. | 40 | 12 N. | 8 | 25 W. | 459 | 140 |
| Lagos.. | 37 | 6 | 8 | 38 | 43 | 13 |
| *Lisbon. | 38 | 43 | 9 | 9 | 312 | 95 |
| Montalegre. | 41 | 49 | 7 | 45 | 3369 | 1027 |
| Oporto........ | 41 | 9 |  | 34 | 328 | 100 |
| Serra da Estrella |  | 25 | 7 | 33 | 4547 | 1386 |
| RUMANIA |  |  |  |  |  |  |
| Baia Mare. | 47 | 38 N | 23 | 35 E. | 741 | 226 |
| Braila.. | 45 | 16 |  | 58 | 39 | 12 |
| Brasov. | 45 | 39 | 25 | 36 | 1870 | 570 |
| *Bucharest. | 44 | 25 | 26 | 6 | 269 | 82 |
| Cernauti. | 48 | 17 |  | 26 | 738 | 225 |
| Cluj. | 46 | 46 | ${ }^{2} 3$ | 35 | 1191 | 363 |
| Constanta | 44 | 11 |  | 39 | 13 | 4 |
| Craiova. | 44 | 19 | 23 | 48 | 361 | 110 |
| Iasi.: | 47 | 10 | 27 | 29 | 328 | 100 |
| Sinaia. | 45 | 21 |  | 34 | 2822 | 860 |
| Sulina. | 45 | 9 | 29 | 40 | 7 | 2 |
| Timisoara. | 45 | 47 | 21 | 17 | 299 | 91 |
| SPAIN |  |  |  |  |  |  |
| Albacete. . | 39 |  |  | 51 W. | 2251 | 686 |
| Badajos.. | 38 | 54 |  | $5^{8} \mathrm{~F}$ | 640 | 195 |
| Barcelona | 41 | 23 | 2 | 10 E . | ${ }_{138}$ | 42 |
| Burgos.. | 42 | 20 | 3 | ${ }^{42} \mathrm{~W}$ W. | 2822 | 860 |
| Cadiz....... | 36 38 | 32 59 | 6 | 18 56 | 33 2060 | 10 628 |
| Ciudad Real. Coruña . . . | 38 43 | 59 23 | 3 | ${ }_{23}{ }^{6}$ | 2060 82 | 628 25 |
| Granada | 37 | 11 | 3 | 36 | 2260 | 689 |
| *Madrid. | 40 | 24 | 3 | 41 | 2188 | 667 |
| Malaga . | 36 | 43 | 4 | 25 | 131 | 40 |
| Murcia. | 37 | 59 | 1 | 8 | 197 | 60 |
| Oviedo. | 43 | 23 | 5 | 49 | 800 | 244 |
| Pamplona.. | 42 | 49 | 1 |  | 1519 | 463 |
| Salamanca. | 40 | 58 | 5 | 40 | 2661 | 8 II |
| San Sebastian. | 43 | 19 | 1 | 59 | 75 | 23 |

Table 116.
LIST OF METEOROLOGICAL STATIONS.
Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

| SPAIN <br> (Continued) | Latitude | Longitude from Greenwich | Height |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet | m. |
| Seville. | $37^{\circ} 23^{\prime} \mathrm{N}$. | $5^{\circ} 59^{\prime} \mathrm{W}$. | 98 | 30 |
| Soria.. | 4140 | 229 | 3471 | 1058 |
| Teruel. | $40 \quad 21$ | 17 | 3015 | 919 |
| Tortosa. | $40 \quad 49$ | o 30 E . | 164 | 50 |
| Valencia. | $\begin{array}{ll}39 & 28 \\ 41 & 39\end{array}$ | $\begin{aligned} & \text { O } \\ & 0\end{aligned} 23 \mathrm{~W}$. | 59 | 18 |
| SWEDEN |  |  |  |  |
| Abisko.. | 6821 N | 1849 E . | 1273 | 388 |
| Göteborg. | 5742 | 1158 | 52 | 16 |
| *Haparanda. | $65 \quad 50$ | $24 \quad 9$ | 30 | 9 |
| Harnosand. | 6238 | $17 \quad 57$ | 30 | 9 |
| Jönköping. | $57 \quad 47$ | $14 \quad 10$ | 322 | 98 |
| Kalmar.. | $56 \quad 40$ | 1622 | 33 | 10 |
| Karlstad. | 5923 | 1330 | 174 | 53 |
| Stensele., | 654 | 17 10 | 1076 | 328 |
| Stockholm. | 59 2I | 184 | 144 | 44 |
| Storlien. | $63 \quad 19$ | 126 | 1975 | 602 |
| Sveg. | $62 \quad 2$ | $14 \quad 19$ | 1191 | 363 |
| *Uppsala. | 59 5I | $17 \quad 38$ | 79 | 24 |
| SWITZERLAND |  |  |  |  |
| Basel. | $47 \quad 33 \mathrm{~N}$. | 735 E. | 909 | 277 |
| Bern.. | $46 \quad 57$ | 726 | 1877 | 572 |
| Chaumont.. | 47 I | 659 | 3697 | 1127 |
| Davos Platz | 4648 | 949 | 5121 | 1561 |
| Geneva. | $46 \quad 12$ | 69 | 1329 | 405 |
| Lugano. | 46 o | 857 | 906 | 276 |
| Pilatus Kulm | $46 \quad 59$ | 8 I6 | 6785 | 2068 |
| *äntis.. | 4715 | 920 | 8202 | 2500 |
| *Zurich. | $47 \quad 23$ | 833 | 1617 | 493 |
| TURKEY <br> Istanbul (Constantinople). | 412 N. | $28 \quad 47$ E. | 423 | 129 |
| UNION OF SOVIET SOCIALIST REPUBLICS |  |  |  |  |
| Alexandrovsk. | 6912 N. | $33 \quad 28$ E. | 105 | 32 |
| *Archangel. | 6434 | 40 | 20 | 6 |
| *Astrakhan.. | $46 \quad 21$ | $48 \quad 2$ | -66 | $-20$ |
| Baku, Transcaucasia. | $40 \quad 21$ | 4950 | 30 | 9 |
| Batum, Transcaucasia | 4139 | 4138 | 11 | 3 |
| Bezenchuk. | 5259 | $49 \quad 29$ | 154 | 47 |
| Divnoe.. | $45 \quad 51$ | $43 \quad 21$ | 230 | 70 |
| Dnepropetrovsk, Ukraire. | $48 \quad 27$ | 354 | 276 | 84 |
| Erivan, Transcaucasia... | $40 \quad 10$ | $44 \quad 30$ | 3253 | 992 |
| Gandzha, Transcaucasia. | 4140 | $46 \quad 21$ | 1450 | $44^{2}$ |
| Genichesk, Ukraine. | 46 II | 3450 | 11 | 3 |
| Kandalaksha. | 678 | 3226 | 49 | 15 |
| Kanin Nos. | $68 \quad 39$ | 4318 | 158 | 48 |
| Kargopol. | 6130 | $38 \quad 57$ |  |  |
| *Kazan. | $55 \quad 47$ | 498 | 262 | 80 |
| KKem........... | $64 \quad 57$ | $34 \quad 39$ | 33 | 10 |
| *Kharkov, Ukraine. | 50 o | $36 \quad 14$ | 459 | 140 |

LIST OF METEOROLOGICAL STATIONS.
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Table 116.

## LIST OF METEOROLOGICAL STATIONS.

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| CHINA | Latitude | Longitude from Greenwich |  | Height |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Feet | m. |
| *Amoy.. | $24^{\circ} 27^{\prime} \mathrm{N}$. | $118{ }^{\circ}$ | $5^{\prime} \mathrm{E}$. | 13 | 4 |
| Batang.. | 301 | 99 | 3 | 6562 | 2000 |
| Changsha. | $28 \quad 12$ |  | 47 | 197 | 60 |
| Chefoo... | 3733 |  | 22 | 10 | 3 |
| Chengku | 3310 | 107 | 20 | 2000 | 610 |
| Chungking | $\begin{array}{ll}30 & 38 \\ 29 & 34\end{array}$ | 104 | 2 | 1700 | 518 |
| Foochow. | $\begin{array}{lll}25 & 34 \\ 25 & 59\end{array}$ | 119 | 37 | 66 | $\begin{array}{r}23 \\ 20 \\ \hline\end{array}$ |
| Fukow. | $34 \quad 9$ | 114 | 30 |  |  |
| Hangchow. | 3011 | 120 | 12 | 33 | 10 |
| *Hankow. | $30 \quad 35$ | 114 | 17 | 118 | 36 |
| *Hongkong. | $22 \quad 18$ | II4 | 10 | 105 | 32 |
| Ichang... | $30 \quad 42$ | 111 | 16 | 1699 | 518 |
| Kanchow. | $25 \quad 58$ | 114 | 46 |  |  |
| Kiukiang. | 2945 | 116 | 8 | 66 | 20 |
| Kweilin... | 20.1 | 110 | 16 | 33 | 10 |
| Kweiyang | 2618 | 106 | 40 | 3527 | 1075 |
| Lungchow: | $22 \quad 22$ | 106 | 45 | , |  |
| Nanking. | 325 | 118 | 49 | 52 | 16 |
| Ningyuenfu | $27 \quad 55$ | 102 | 18 |  |  |
| Pakhoi. | 2159 | 109 | 7 | 16 | 5 |
| Peiping (Peking).. | $39 \quad 54$ | 116 | 30 | 361 | 110 |
| Samshui (Canton)... | 236 | 112 | 53 | 33 | 10 |
| *Shanghai (Zikawei). | 3112 | 121 | 26 | 23 | 7 |
| Silung. | $24 \quad 27$ | 105 | 30 |  |  |
| Siwantse. | $40 \quad 58$ | 115 | 18 | 3828 | 1167 |
| Sunchow. | $23 \quad 17$ | 109 | 59 | ... |  |
| Szengenfu | $23 \quad 22$ | 108 | 2 |  | $\cdots$ |
| Taiyuanfu. | 3753 | 112 | 29 | 3051 | 930 |
| Tamingfu | $36 \quad 19$ | 115 | 12 |  |  |
| Tatungfu. | 407 | 113 | 13 | 4690 | 1430 |
| *Tengueh. | 2445 | 98 | 14 | 5357 | 1633 |
| *Tientsin. | 399 | 117 | 11 | 16 | 5 |
| Wenchow | $\begin{array}{ll}36 \\ 28 & 4 \\ \end{array}$ | 120 | 19 | 253 10 | 77 |
| Yunnanfu. | $25 \quad 2$ | 102 | 41 | 6211 | 1893 |
| EASTERN TURKESTAN Kashgar. | 3930 N. | 75 | $53 \mathrm{E}$. | 4255 | 1297 |
| FRENCH INDO-CHINA Battambang |  |  |  |  |  |
| Cape Padaran | $\begin{array}{lll}13 & 5 \\ 11 & 35\end{array}$ | 103 109 | 10 E. | 581 | 177 |
| Honba....... | 125 | 108 | 45 | 4869 | 1484 |
| Kampot. | $10 \quad 37$ | 104 | 11 | 4 |  |
| Laokay.. | 2230 | 103 | 57 | 305 | 93 |
| Luang Prabang | 1950 | 102 | 4 | 1050 | 320 |
| *Nhatrang. ${ }^{\text {P }}$ | 12 I | 109 | 12 | 13 | 4 |
| Phnom Penh. | 1132 | 104 | 52 | 43 | 13 |
| Phongsaly.. | 214 | 102 | 2 | 4619 | 1408 |
| *Phu Lien. | 2048 | 106 | 38 | 38 I | 116 |
| *Saigon....... | $10 \quad 47$ | 106 | 42 | 36 | 11 |
| Savannakhet. | 16 31 | 104 | 42 | 426 | 130 |
| Stungtreng. | 1328 | 105 | 59 |  |  |
| Tourane (Tientcha).. | 168 | 108 | 18 | 509 | 155 |
| Vien-tiane | 1759 | 102 | 33 | ... |  |
| Vinh.. | $18 \quad 38$ | 105 | 39 | 20 | 6 |

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LIST OF METEOROLOGICAL STATIONS.
Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

| IRAQ (MESOPOTAMIA)*Bagdad.................. | Latitude |  | Longitude from Greenwich |  | Height |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Feet | m. |
|  |  | $21^{\prime}$ N |  | $28^{\prime} \mathrm{E}$. | 106 | 32 |
| Basra.. Mosul. |  |  |  |  | 10 | 3 |
| JAPAN |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Hakodate. Hiroshima | 41 | 47 N | 140 | 43 E . | 13 | 4 |
| Hiroshima Ibukasan. | 34 35 | 23 25 | 132 136 | 27 | 10 | 3 |
| Kanazawa. |  | 25 | 136 136 | 24 39 | 4514 92 | 1376 28 |
| Kobe. . | 34 | 41 | 135 | 11 | 190 | 58 |
| *Kyoto | 35 | 1 | 135 | 44 | 141 | 43 |
| Matumoto | 36 | 14 | 137 | 59 | 1909 | 582 |
| *Miyako.. |  | 38 | 141 | 59 | 98 | 30 |
| Miyazaki. | 31 | 55 | 131 | 26 | 26 | 8 |
| *Nagasaki. | 32 | 44 | 129 | 52 | 436 | 133 |
| *Naha.. |  | ${ }^{13}$ | 127 | 41 | 26 | 8 |
| *Nemuro. | 43 | 20 20 | 1 | 35 | 13 <br> 89 | 4 |
| Niigata. | 37 | 55 | I 39 | 3 | 85 | 26 |
| Onahama | 36 | 56 | 140 | 54 | 20 | 6 |
| Otiai, Sakhalin. | 47 | 20 | 142 | 47 | 89 | 27 |
| Sakai.. | 35 | 33 | 133 | 14 | 10 | 3 |
| *Sapporo... | 43 | 4 | 141 | 21 | 56 | 17 |
| * Syana, Kurile Islands. | 45 | 14 | 147 | 53 | 128 | 39 |
| *Taihoku, Taiwan.. | 25 | $\stackrel{2}{0}$ |  | 31 | 30 | 9 |
| *Tokyo... . . . . ${ }^{\text {a }}$. | 23 | ${ }_{4}^{\text {I }}$ |  | 13 | 46 20 | 14 6 |
| Tukubasan |  | 13 | I 40 | 6 | 2854 | 870 |
| KOREA (CHOSEN) |  |  |  |  |  |  |
| Gensan..... . |  |  |  | 26 E. | 118 | 36 |
| Husan. |  | 6 |  | 11 | 39 | 12 |
| * Jinsen (Chemulpo) |  | 29 |  | 37 | 226 | 69 |
| Mokpo ... | 34 | 47 | 126 | 20 | 92 | 28 |
| Ryuganpo. | 39 | 56 | 124 | 22 | 20 | 6 |
| Tyukotin. | 41 | 47 | 126 | 53 | 1030 | 314 |
| *Yuki... | 42 | 40 | 130 | 24 | 210 | 64 |
| MALAY PENINSULA |  |  |  |  |  |  |
| Malacca.. | 2 | 14 | 102 | 14 | 23 | 7 |
| * Penang. | 5 | 34 | 100 | 20 | 16 | 5 |
| * Rhododendron Hill. | 4 | 28 | 101 | 23 | 5120 | 1561 |
| *Singapore. | 1 | 18 | 103 | 51 | 36 | 11 |
| MANCHURIA |  |  |  |  |  |  |
| Changchun.. |  |  |  |  |  |  |
| Dairen. <br> Harbin. | 38 | 54 | 121 | 38 | 315 | 96 |
| Harbin. | 45 | 46 | 126 | 50 | 482 | 147 618 |
| *Mukden. | 4 4 | 48 | 119 | 43 | $\begin{array}{r}2028 \\ 144 \\ \hline\end{array}$ | 618 |
| Tsitsihar. | 47 | Io |  | 49 | 499 | 44 152 |
| MONGOLIA |  |  |  |  |  |  |
| Chabernoor.... |  | 31 N. |  | 42 E . | 2854 | 870 |
| Sungshutsuitze. |  | 23 |  | 57 | 328 | 100 |

LIST OF METEOROLOGICAL STATIONS.
Note.-Stations with asterisk appear in the "Réseau Mondial" of the British
Meteorological Office for 1922. (London, 1929.)

| PALESTINE | Latitude | Longitude from Greenwich | Height |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet | m. |
|  | $32^{\circ}+8^{\prime} N$. | $34^{\circ} 59^{\prime} \mathrm{E}$. | 33 | 10 |
| Jericho... | 3 I 5 I | $\begin{array}{ll}35 & 27\end{array}$ | 820 | 250 |
| Jerusalem. | 3147 | 3513 | 2487 | 758 |
| Kasr Hadschla. | 3150 | 3530 | --1083 | -330 |
| Tiberias. | $\begin{array}{ll}32 & 47\end{array}$ | $35 \quad 32$ | $-653$ | -199 |
| PERSIA |  |  |  |  |
| *Bushire. | $28 \quad 59 \mathrm{~N}$. | 5053 E. | 14 | 4 |
| Ispahan. | $\begin{array}{ll}32 & 38\end{array}$ | 5136 | 5817 | 1773 |
| *Jask. . . | 2544 | 5747 | I3 | 4 |
| Kerman. | . 3030 | 57 O | - |  |
| Kermanshah. | 3. ${ }^{\text {P }} 18$ | $47 \quad 4$ | 4934 | 1504 |
| *Meshed. | $36 \quad 16$ | 5935 | 3104 | 9.46 |
| *Tehran. | 3541 | 5125 | 4002 | 1220 |
| SIAM |  |  |  |  |
| Bandon. | 93 N. | 9520 E . | $\cdots$ | . . . |
| Bangkok. | 1343 | 10025 | 9 | 3 |
| Bang Nara | $6 \quad 25$ | 10151 | - | 3 |
| Chantaboun. | 1235 | 1025 | . . ${ }^{\text {a }}$ |  |
| Chiengmai | 1845 | 9853 | 1003 | 306 |
| Chiengrai. | 1955 | 99 51 | - | . . . |
| Konken. | $16 \quad 28$ | 10239 |  | . . . |
| Korat........ | 1457 | 1024 | 105 | in |
| Nakon Sawan. | $15+1$ | 1002 | 105 | 32 |
| Nan..... | 1846 | 10044 | $\cdots$ | . ${ }^{\text {a }}$ |
| Pitsanoulok. | $16+8$ | 1007 | 48 | 15 |
| SYRIA |  |  |  |  |
| *Beirut. ... |  | $35 \quad 28$ E. | 112 | 34 |
| Deir-es-\%or | 35 | $40 \quad 2$ | 659 | 201 |
| Ksara. | 3349 | 3535 | 3028 | 923 |
| Muslimie. | $36 \quad 22$ | $37 \quad 2$ | 1483 | 452 |
| Palmyre. | 3434 | 383 | I325 | 404 |
| TIBET |  |  |  |  |
| Gartok. | 3 I 45 N. | $80 \quad 20$ E. | 15100 | 4602 |
| Gyantse... | 2855 | 8933 | 13110 | 3996 |
| Pharijong. | $27 \quad 39$ | $89 \quad 14$ | 14400 | 4389 |
| TURKEY |  |  |  |  |
| Adana. | $36 \quad 58 \mathrm{~N}$. | 3518 E. | 125 | 38 |
| Angora.. | $\begin{array}{ll}39 & 58\end{array}$ | 3248 | 2825 | 861 |
| Diarbekr. | $40 \quad 25$ | $37 \quad 50$ | 2346 | 715 1931 |
| Erzerum. | 3955 | 415 | 6345 | $193+$ |
| Sinope. Smyrna. | $\begin{array}{lr}42 & 1 \\ 38 & 27\end{array}$ | $\begin{array}{ll}35 & 19 \\ 27\end{array}$ | 59 115 | 18 35 |
| Smyrna. | $38 \quad 27$ | 27 15 | 115 | 35 |
| UNION OF SOVIET SOCIALIST REPUBLICS |  |  |  |  |
| *Akmolinsk.... . . . . . . . . . . . . |  |  | 1158 | 353 |
| Aktiubinsk. | $\begin{array}{ll}50 & 17 \\ 43 & 16\end{array}$ | $\begin{array}{ll}57 & 15 \\ 76 & 53\end{array}$ | 731 2760 | 223 84 |
| * Alma Ata | $\begin{array}{r}43 \\ \hline 64 \\ \hline\end{array}$ | $\begin{array}{r}76 \\ 177 \\ \hline\end{array}$ | 2760 | 841 23 |
| Anadyr. . . . . . . . . . . . . . . | $64 \quad 45$ | $177 \quad 33$ | 74 | 23 |

Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

| LNION OF SOTIET SOCIALIST REPUBLICS <br> (Continuea) | Latitude |  | Longitude from Greenwich |  | Height |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Feet | m. |
| Askabad. |  | $57^{\prime} \mathrm{N}$. |  | $23^{\prime} \mathrm{E}$. | 716 | 218 |
| Ayan. |  | 28 | 138 | 17 | 33 | 10 |
| Barguzin. |  | 27 | 109 | 38 | 161 | 49 |
| * Barnaul. |  | 20 | 83 | 47 | 519 | 158 |
| * Beresov. |  | 56 | 65 | 4 | 131 | 40 |
| Bering Island. |  | 12 | 165 | 59 | 17 | 5 |
| * Blagovyeschensk |  | 16 | 127 | 30 | 467 | 142 |
| Bodaibo. |  | 56 | 114 | 13 |  | . . |
| Bokhara. . . . |  | 43 | 64 | 33 | 729 | 222 |
| Bratskii Ostrog |  | 4 | 101 | 50 |  | . |
| Bulun . | 70 | 45 | 127 | 47 | 66 | 20 |
| * Cherdyn. |  | 24 | 56 | 31 | 685 | 209 |
| Cherniaeva |  | 47 | 126 | o | 693 | 211 |
| Chimbai. |  | 56 | 59 | 46 | , | $\ldots$ |
| *Chita. | 52 | 2 | 113 | 30 | 2254 | 687 |
| *Dickson. |  | 30 | 80 | 23 | 75 | 23 |
| Ekimchan | 53 | 5 | 132 | 58 | 1558 | 475 |
| Elgjai... . . . . . . . | 63 | 46 | 116 | 56 | 443 | I 35 |
| *Fort Alexandrovsk Guriev......... |  | 31 | 50 | 16 | $-77$ | -23 |
| Guriev. |  | 7 | 51 | 55 | $-70$ | -21 |
| Kazache |  | 17 | 104 | 20 | 1531 | 467 |
| Kharborovsk |  | 45 | 135 | 58 | 46 | 14 |
| Khatanga. | 71 | 32 | 102 | 9 | 230 | 75 |
| *Kirensk. | 57 | 47 | 108 | 7 | 935 | 285 |
| Kizil Orda. | 44 | 51 | 65 | 27 | 426 | 130 |
| Kolpashevo. | 58 | 18 | 82 | 55 | 256 | 78 |
| Koziravskaia | 55 | 55 | 159 | 38 |  |  |
| *Krasnovodsk. | 40 | O | 52 | 59 | -19 | -6 |
| Krasnoyarsk. | 56 | 1 | 92 | 5 I | 518 | 158 |
| Kurgan. |  | 27 | 65 | 19 | 252 | 77 |
| Markovo. | 64 | 45 | 170 | 50 | 66 | 20 |
| *Minusinsk | 53 | 43 | 91 | 41 | 965 | 294 |
| Mogocha... | 53 | 4 | 119 | 47 | 2038 | 621 |
| Morre Salle. . . . . | 69 | 43 | 66 | 48 | 46 | 14 |
| Muraviev Amurski | 45 | 53 | 133 | 38 | 220 | 67 |
| Nagornii Priisk. | 55 | 52 | 125 | O | . . | . |
| Naiakhan. . . . | 61 | 55 | 158 | 59 | 95 | 29 |
| * Nikolaiersk on the Amur | 53 | 8 | 140 | 43 | 69 | 2 I |
| Nizhne Kolymsk. | 68 | 32 | 160 | 59 | 16 | 5 |
| Novi Port. | 67 | 42 | 72 | 57 | 16 | 5 |
| *()hdorsk. | 66 | 31 | 66 | 35 | 115 | 35 |
| ()khotsk. | 59 | 21 | ${ }^{1} 43$ | 17 | 20 | 6 |
| ()la....... | 59 | 33 | ${ }^{1} 51$ | 13 | 16 | 5 |
| ()lekminsk |  | 22 | 120 | 26 | 502 | 153 |
| * ${ }^{\text {* }}$ ( merm . | 54 | 59 | 73 | 23 | 352 | 107 |
| *Perm. . . . . . . | 58 | 1 | 56 | 15 | 535 | 163 |
| * Petropavlovsk | 53 | $\bigcirc$ | 158 | 39 | 44 | 13 |
| Russkoe Uste. | 71 | 1 | 149 | 26 | 20 | 6 |
| Sagastyr. ... |  | 23 | 126 | 35 | 16 | 5 |
| Semipalatinsk. ... |  | 24 | 80 | 13 | 776 | 237 |
| Sovetskaia Gavan |  | 58 | 1.40 | 17 | 56 | 17 |
| * Sredne Kolymsk. | 67 | 30 | $15+$ | 50 | 99 | 30 |
| *Surgut. . . . (Ekaterinbury) | 61 56 | 15 | 73 | 24 | 131 | 40 |
| *Sverdlovsk (Ekaterinburg) | 56 | 50 | 60 | 38 | 922 | 281 |

LIST OF METEOROLOGICAL STATIONS.
Note.-Stations with asterisk appear in the "Réseau Mondial' of the British Meteorological Office for 1922. (London, 1929.)

| UNION OF SOVIET SOCIALIST REPUBLICS (Continued) | Latitude | Longitude from Greenwich | Height |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet | m. |
| *Tashkent | $4 \mathrm{I}^{\circ} 2 \mathrm{o}^{\prime} \mathrm{N}$. | $69^{\circ} 18^{\prime} \mathrm{E}$. |  |  |
| *Tobolsk. | 58 5 5 | 68 14 | 355 | 108 |
| *Tomsk. | 5630 | 8454 | 398 | 121 |
| Turgai. | 4938 | $63 \quad 27$ | 427 | 131 |
| Turkestan | $43 \quad 18$ | $68 \quad 17$ | 279 | 85 |
| *Turukhansk | $65 \quad 55$ | $87 \quad 37$ | 131 | 40 |
| Uralsk. | 51 15 | 517 | 112 | 34 |
| Ust Maiskoe | $60 \quad 25$ | $134 \quad 29$ | 58. | 177 |
| Ust Yeniseisk. | $69 \quad 38$ | $84 \quad 22$ | 79 | 24 |
| Verkhne Inbatskoe | 63 7 | 88 I | 98 | 30 |
| Verkhne Tamborskoe | 5040 | 13720 |  |  |
| *Verkhoiansk. | 6733 | $133 \quad 34$ | 328 | 100 |
| *Viluisk. | $63 \quad 45$ | 12135 |  | $\cdots$ |
| *Vladivostok | 437 | 13155 | 95 | 29 |
| *Yakutsk. | 62 I | 12943 | 358 | 109 |
| * Yeniseisk | $\begin{array}{ll}58 & 27\end{array}$ | 92 10 | 254 | 77 |
| Zaisan. | $47 \quad 28$ | 84 5 | 2139 | 652 |
| MALAY ARCHIPELAGO <br> EAST INDIES |  |  |  |  |
| *Amboina... | $\begin{array}{lll}3 & 42 & \mathrm{~S} .\end{array}$ | 128 IO E. | 13 | 5 |
| Balikpapan. | 15 | 11656 | 16 | 5 |
| Bandoeng. | 654 | 10738 | 2395 | 730 |
| *Batavia. | 6 II | 10650 | 26 |  |
| Buitenzorg. | 635 | 10647 | $\begin{array}{r}787 \\ \hline 26\end{array}$ | 240 8 |
| *Darı. . | 943 | 14313 | 26 | 8 |
| Dobo. | 514 | 134 12 17 |  |  |
| Finschhafen | 633 | $147 \quad 52$ | 16 | 5 |
| Hollandia | 2 8 32 | 14047 |  |  |
| Kalisat. | $8{ }^{8}$ | 1148 | 3609 | 1100 |
| *Kupang. | $\begin{array}{ll}10 & 16 \\ 5\end{array}$ | 12334 | 148 | 45 |
| Konstantinhafen | $5 \quad 29$ | $\begin{array}{ll} 145 & 51 \\ 119 & 28 \end{array}$ |  |  |
| Macasser <br> *Manokwari. | $\begin{array}{rrr}5 & 5 \\ 0 & 52\end{array}$ | $\begin{array}{ll} 119 & 28 \\ 134 & 20 \end{array}$ | ${ }^{7}$ | 2 19 |
| *Medan... |  | ${ }^{98} 41$ | 82 | 25 |
| *Menado. | 130 | 12450 | 30 | 7 |
| *Padang. | - 56 S . | 10022 | 23 | 7 |
| Pangerango. | 6 7 7 | 107 10 172 | 9908 | 3020 |
| *Pasuruan.. | $7 \quad 38$ | 112 55 <br> 109  | 16 | 5 |
| *Pontianak | - 1 | $\begin{array}{rrr}109 & 20 \\ 147 \\ 1480\end{array}$ | 10 130 | 3 |
| * Port Moresby | 9 <br> 10 | $\begin{array}{rrr}147 \\ 150 & 9 \\ 150\end{array}$ | 130 | 39 15 |
| *Samarai.. | $\begin{array}{rrrr}10 & 37 & \\ 5 & 50 & \mathrm{~N} .\end{array}$ | $\begin{array}{lr} 150 & 40 \\ 118 & 7 \end{array}$ | $\begin{array}{r}49 \\ 105 \\ \hline\end{array}$ | 15 32 |
| *Sandakan | $\begin{array}{lll} 5 & 50 & \mathrm{~N} . \\ 7 & 50 & \mathrm{~S} \end{array}$ | $\begin{array}{rr} 118 \\ 112 & 7 \\ 56 \end{array}$ | 105 5692 | 32 1735 |
| PHILIPPINE ISLANDS Aparri | $18 \quad 22 \mathrm{~N}$. | 12 I 38 E . | 13 | 4 |
| Baguio... | $16 \quad 25$ | $120 \quad 35$ | 4961 | 1512 |
| Dagupan. | 163 | 120 <br> 120 <br> 125 | 16 | 5 |
| Davao... Iloilo. | $\begin{array}{rr}7 & 1 \\ 10 & 42\end{array}$ | $\begin{array}{lll}125 & 35 \\ 122 & 34\end{array}$ | 10 20 | 3 6 |
| *Iwahig. | 944 | 11838 | 43 | 13 |
| Legaspi. | 139 | 12345 | 13 | 4 |
| *Manila. | 1435 | $120 \quad 59$ | 46 | 14 |
| *Surigao. | 948 | $125 \quad 29$ | 20 | 6 |
| Tacloban. | 11 15 | 1250 | ${ }_{6} 10$ | I |
| *Tagbilaran. | $\begin{array}{ll}9 & 38 \\ 6 & 54\end{array}$ | $\begin{array}{ll}123 & 51 \\ 122 & 5\end{array}$ | 69 10 | 21 |
| Zamboanga |  | 122 | 10 | 3 |

## LIST OF METEOROLOGICAL STATIONS.

Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)


LIST OF METEOROLOGICAL STATIONS.
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Table 116.
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Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

| GAMBIA | Latitude | Longitude from Greenwich | Height |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet | m. |
| * Bathurst. | $13^{\circ} 27^{\prime} \mathrm{N}$. | $16^{\circ} 34^{\prime} \mathrm{W}$ | 7 | 2 |
| *McCarthy Island. | $13 \quad 32$ | 1446 | 16 | 5 |
| GOLD COAST COLONY |  |  |  |  |
| * Accra. | 533 N. | - 12 W . | 60 | 18 |
| Axim. | 442 | 214 | 20 | 6 |
| Coomassie | 641 | 137 | 900 | 274 |
| Tamale. | 923 | - $5^{2}$ | 600 | 183 |
| KENYA COLONY <br> Fort Hall |  |  |  |  |
| Fisumu............ . . |  | $\begin{array}{ll}37 & 10 \\ 34 & 45\end{array}$ | 4410 3880 | 1344 1183 |
| *Lamu. | 216 | $40 \quad 50$ | 10 | 3 |
| Limoru. | 17 | 3639 | 7300 | 2225 |
| Masongoleni | 228 | $37 \quad 59$ | ... |  |
| Mombasa. | $4{ }^{4}$ | $39 \quad 42$ | 50 | ${ }^{1} 5$ |
| Moyale. | 3 31 N. <br> I 18  | $\begin{array}{rr}39 & 5 \\ 36\end{array}$ |  | 1661 |
| * Nairobi. | $1 \mathrm{I}^{18} \mathrm{~S}$ | $36 \quad 50$ | 5450 | 1661 |
| LIBERIA <br> Monrovia (Schieffen). | 6 IIN | 1033 W | 25 | 8 |
| LIBYA |  |  |  |  |
| Azizia. | 3232 N . | 13 I E. | 518 | 158 |
| Bengazi. | 326 | 204 | 82 | 25 |
| Cirene. | 3249 | 215 | 2067 | 630 |
| Misda. | 3139 | 13 I | I 345 | 410 |
| Tobruk | 323 | $23 \quad 59$ | 151 | 46 |
| Tripoli. | $32 \quad 54$ | 13 II | 59 | 18 |
| MADAGASCAR |  |  |  |  |
| Antsirane . . | 12125  <br> 25  | 4920 E. | 89 | 27 |
| Farafangana. | 2253 | $47 \quad 56$ | 33 | 10 |
| Mandritsara. | 1544 | 4850 | 945 | 288 |
| Marovoay.. | $16 \quad 3$ | $46 \quad 42$ | 148 | 45 |
| *Tamatave.. | $\begin{array}{rr}20 & 15 \\ 18 & 9\end{array}$ | $\begin{array}{ll}44 & 18 \\ 49 & 26\end{array}$ | 13 |  |
| *Tananarivo | $18 \quad 55$ | 47 | 4531 | $138{ }^{4}$ |
| MOROCCO |  |  |  |  |
| Casablanca. | $33 \quad 37 \mathrm{~N}$. | $7 \begin{array}{lll}7 & 34\end{array}$ | 131 | 40 |
| Fes. | 340 | 453 | 1365 | 416 |
| Marrakech | 3138 | 759 | ${ }^{1} 509$ | 460 |
| *Melilla. | $\begin{array}{ll}35 & 17\end{array}$ | 30 | 26 | 8 |
| Mogador | 31 | $9{ }^{3} 6$ | 36 | 11 |
| Oudja. | $34 \quad 39$ | 1 I 54 | 182 I | 555 |
| Rabat. | 34 | 6 8 | 210 | 64 |
| Safi..... | $\begin{array}{ll}32 & 18 \\ 35 & 49\end{array}$ | $\begin{array}{ll}8 & 50 \\ 5 & 52\end{array}$ | 230 148 | 70 45 |
| NIGERIA |  |  |  |  |
| Całabar. |  | 819 E. | ${ }^{1} 57$ | 48 |
| Debundja | $4{ }^{4} 5$ | $8 \quad 59$ | 30 | 9 |
| Forcados. | 523 | 526 | 4 | 1 |

## LIST OF METEOROLOGICAL STATIONS.

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Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

| SOUTH WEST AFRICA | Latitude | Longitude from Greenwich | Height |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet | m. |
| Bethany | $26^{\circ} 30^{\prime} \mathrm{S}$ | $17^{\circ} 10^{\prime} \mathrm{E}$. | 3067 | 935 |
| Franzfontein | 20 11 | 154 | 3773 | 1150 |
| Gibeon. | 258 | $17 \quad 46$ | 3707 | 1130 |
| Grootfontein. | 1933 | 187 | 5020 | 1530 |
| Luderitz Bay. | $26 \quad 39$ | 1510 | 13 | 4 |
| Mlt. Brukkaros. | $\begin{array}{lll}25 & 52\end{array}$ | $17 \quad 48$ | 5202 | 1586 |
| Swakopmund Warmbad... | $\begin{array}{ll}22 & 41 \\ 28\end{array}$ | $14 \quad 31$ | 26 | 8 |
| *Windhuk. | $\begin{array}{ll}22 & 34\end{array}$ | 17  | $5+63$ | 1665 |
| TANGANYIKA TERRITORY |  |  |  |  |
| Bismarckburg. | 828 S. | 3 l 8 E . | 2658 | 810 |
| Dar es Salaam. | 649 | $39 \quad 18$ | 26 | 8 |
| Kondoa Irangi | + 55 | $35 \quad 57$ | 4626 | 1410 |
| Lindi. | 10 0 | 3944 | 26 | 8 |
| Mahenge | 841 | 363 | 3363 | 1025 |
| Mwanza....... | 231 | $32 \quad 5+$ | 3740 | 1140 |
| New Langenburg | $9{ }_{5} 16$ | 3338 | 5085 | 1550 |
| Tabora.. | 5 I | 3249 | 4058 | 1237 |
| Tandala. | $9 \quad 23$ | $34 \quad 14$ | 6729 | 2051 |
| Tanga. | 54 | 397 | 92 | 28 |
| Ujiji. | 455 | 29 41 | 2690 | 820 |
| TUNIS |  |  |  |  |
| Bizerte. | $37 \quad 17 \mathrm{~N}$ | $9 \quad 52 \mathrm{E}$. | 33 | 10 |
| Dehibat. | $\begin{array}{ll}32 & 3 \\ 34 & \end{array}$ | 1043 | 1066 | 325 |
| Metlaoui | $34 \quad 22$ | $8 \quad 24$ | 735 | 224 |
| *Tunis. | $\begin{array}{lll}3+ & 4+ \\ 36 & 48\end{array}$ | 10 10 | 105 | $3^{2}$ |
| UGANDA |  |  |  |  |
| *Entebbe. | $0+\mathrm{N}$ | $32 \quad 28$ E. | 3850 | 1173 |
| Fort Portal | - 40 | $30 \quad 17$ | 5300 | 1615 |
| Kitgum. | 320 | 3253 | 3000 | 914 |
| Mbale. | $1 \quad 6$ | 3411 | 4000 | 1219 |
| Mbarara | - 37 S . | 3039 | 4800 | 1463 |
| UNION OF SOUTII AFRICA |  |  |  |  |
| Barberton.... | $\begin{array}{ll}30 & 42 \\ 25 & 47\end{array}$ | $\begin{array}{ll}26 & 40 \\ 31 & \\ \\ \text { 2 }\end{array}$ | +330 2885 | 1320 879 |
| Beaufort West | 32 21 | $22 \quad 36$ | 2850 | 869 |
| Bloemfontein | 297 | 2613 | 4518 | ${ }^{1} 377$ |
| * Cape Town. | $33 \quad 56$ | $18 \quad 29$ | 40 | 12 |
| * Clanwilliam. | $\begin{array}{ll}32 & 10 \\ 29 & 5\end{array}$ | $18 \quad 55$ | 245 | 75 |
| ${ }^{\text {* }}$ Eurban..... | $\begin{array}{ll}29 & 52 \\ 33\end{array}$ | $\begin{array}{ll}18 & 3\end{array}$ | 20 | 6 |
| Graaf Reinet | $\begin{array}{rrr}33 & 1 \\ 32 & 16\end{array}$ | $\begin{array}{ll}27 & 54 \\ 2+ & 32\end{array}$ | 150 $2+30$ | $\begin{array}{r}46 \\ 7 \\ \hline 1\end{array}$ |
| Grahamstown | 3318 | 26 26 | 1700 | 518 |
| Hlabisa. | 288 | $\begin{array}{ll}31 & 52\end{array}$ | 800 | 244 |
| *Johannesburg | 26 II | 28 3 | 5750 | 1753 |
| Kenhart... | 29 21 | $21 \quad 9$ | $270+$ | 824 |
| Kimberley. | $28 \quad 44$ | 2446 | $40+2$ | 1232 |
| Kokstad Komati Poort | $\begin{array}{ll}30 & 33 \\ 25 & 26\end{array}$ | $29 \quad 26$ 31 | 4280 | 1304 |
| Komati Poort | $25 \quad 26$ | 3156 | 620 | 189 |

[^31]Table 116.
LIST OF METEOROLOGICAL STATIONS.
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| UNION OF SOUTH AFRICA (Continued) | Latitude | Longitude from Greenwich | Height |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | Feet | m. |
| Kuruman. | $27^{\circ} 35^{\prime} \mathrm{S}$. | $\begin{array}{ll}23^{\circ} & 37^{\prime} \mathrm{E} \text { E. } \\ 27 & 55\end{array}$ | 4500 5000 | $\begin{aligned} & 1372 \\ & 152+ \end{aligned}$ |
| Lindley... |  | 27 25 | 4194 | 1278 |
| Mafeking. | 25 <br> $3+$ <br> 3 <br> 11 | 22 29 | 100 | 30 186 |
| Mossel Bay | $\begin{array}{ll}37 & 4 \\ 27\end{array}$ | $29 \quad 56$ | 3890 | 1186 |
| Newcastle. | 29 36 | 1752 | 3036 | 925 692 |
| Ookiep.......... | 2935 | $30 \quad 32$ | 2272 | 692 1302 |
| Pietermaritzio. Pietersburg. | $\begin{array}{ll}23 & 54 \\ 33 & 58\end{array}$ | $\begin{array}{ll}29 & 28 \\ 25 & 37\end{array}$ | 4276 17 | 54 |
| Port Elizabeth | $\begin{array}{ll}33 & 5 \\ 29 & 14\end{array}$ | 28 28 12 | 25 | 8 |
| $\underset{\text { Port Nolloth..... . . . . . . }}{\text { Pretoria.............. }}$ | $25+5$ | $28 \quad 12$ | 4350 | 1326 |
| AUSTRALASIA |  |  |  |  |
| AUSTRALIA |  | 13835 E. | 140 | 43 |
| *Adelaide................ | $\begin{array}{ll}3+ & 56 \\ 23 & 38\end{array}$ | 133 13 | 1926 | 587 1016 |
| *Alice Spring Armidale. ${ }^{\text {a }}$ | $30 \quad 32$ | $\begin{array}{lll}151 & 38\end{array}$ | 3333 | 1016 |
| Bendigo.. | $\begin{array}{ll}36 & 46 \\ 22 & 55\end{array}$ | $\begin{array}{lll}144 \\ 139 & 17 \\ 188\end{array}$ | 479 | 146 |
| * Boulia. | 30 | 145 <br> 8 | 364 | 111 |
| * Bourke.. | $27 \quad 28$ | $153-2$ | 137 | 42 305 |
| Broken Hill | $\begin{array}{ll}31 & 57 \\ 17 & 16\end{array}$ | $\begin{array}{ll}141 & 28 \\ 139 & 3+\end{array}$ | 1000 | 305 |
| Burketown | 17 <br> 35 <br> 15 | $\begin{array}{ll}139 & 3+ \\ 149 & 15\end{array}$ | (2000) | (610) |
| Canberra.... | $3+52$ | 1158 | 163 | 50 |
| Cape Leeuwin | 34 24 | 11339 | 15 645 | 5 197 |
| Charlotte Waters | $\begin{array}{ll}25 & 56 \\ 20 & 3\end{array}$ | $\begin{array}{lll}134 & 55 \\ 1+6 & 16\end{array}$ | $6+5$ 1019 | 197 311 |
| Chartertowers | 20 20 | 11921 | 35 | 1 I |
| Condon... | 15 15 | 14514 | 17 | 5 |
| Cooktown.. *Coolgardie. | $30 \quad 57$ | 12110 | 1388 | 423 |
| *Coolgardie... | 1616 | $133-23$ | 692 98 | 211 30 |
| *Darwin.... | 1288 | $\begin{array}{lll}130 & 51 \\ 123 & 40\end{array}$ | 52 | 16 |
| *Derby. | $\begin{array}{ll}17 & 18 \\ 32 & 18\end{array}$ | $\begin{array}{lll}123 & 40 \\ 148 & 35\end{array}$ | 863 | 263 |
| Dubbo.... | 33 | 12155 | 14 | 4 |
| Esperance.. | 1822 | $143 \quad 3{ }^{2}$ | 302 | 92 |
| * Georgetown | 2846 | 11436 | 13 | 4 374 |
| * ITalls Creek | $\begin{array}{rr}18 & 13 \\ 17\end{array}$ | 127 <br> 15 | 1227 55 | 374 17 |
| Harvey Creek | $\begin{array}{rr}17 & 9 \\ 3+\quad 30\end{array}$ | $\begin{array}{ll}1+5 & 55 \\ 1+4 & 56\end{array}$ | 305 | 93 |
| Hay..... | $\begin{array}{ll}17 & 3 \\ 17 & 23\end{array}$ | $\begin{array}{ll}1+4 \\ 145 & 23\end{array}$ | 2890 | 881 |
| Herberton | 42 4 | $147 \quad 20$ | 177 650 | 54 198 |
| * Inobart. | $\begin{array}{ll}24 & 15 \\ 34\end{array}$ | $\begin{array}{lll}14+ & 2+ \\ 14 & 35\end{array}$ | 650 1017 | 198 |
| *Katanning | $\begin{array}{ll}33 & 42 \\ 35 & 52\end{array}$ | $\begin{array}{ll}117 & 35 \\ 148 & 32\end{array}$ | 4640 | 1414 |
| Kiandra.... | $\begin{array}{ll}35 & 52 \\ 41 & 27\end{array}$ | 147 10 | 33 | 10 |
| *Launceston | 2840 | $122 \quad 23$ | 1529 +100 | 466 122 |
| *Mein.... | $\begin{array}{ll}13 & 13 \\ \\ 37 & 19\end{array}$ | 142 14 148 | ${ }_{1}^{+15}$ | 122 35 |
| *Melbourne | $\begin{array}{ll}37 & 49 \\ 26 & 32\end{array}$ | $\begin{array}{ll}1+4 & 5 \\ 1+7 & 52\end{array}$ | 1102 | 336 |
| *Mitchell.. | $\begin{array}{ll}26 & 32 \\ 21 & 53\end{array}$ | 1205 | 1266 | 386 |
| *Nullagine. Oatlands. | 4218 | 147 24 | 1400 2108 | 427 643 |
| Oatlands <br> Omeo. | 376 |  | 2108 |  |

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## LIST OF METEOROLOGICAL STATIONS.

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[^0]:    1 The value of the bar as here defined is a pressure of $1,000,000$ dynes per square centimeter, and is that employed by meteorological services, and recommended by inter-

[^1]:    national meteorological and aerological conferences. It is $1,000,000$ times greater than that given in the Smithsonian Physical Tables, 6th ed., 1914, p. 346 . The smaller value is generally employed by physicists and chemists. See Marvin, Charles F. Nomenclature of the Unit of Absolute Pressure. Monthly Weather Review, 1918, $46: 73$-75.
    ${ }^{1}$ Chappuis, Recueil de Constantes Physiques, Soc. Fr. Phys., 1913, p. 139. Leduc, Trav. et Mém., Bur. Int. Poids et Mes., xvi, p. 36, 1917.
    ${ }^{2}$ Comptes Rendus des Séances, Troisième Conférence Générale, p. 68. Trav. et Mém., Bur. Int. Poids et Mes., xir, igoz.

[^2]:    ${ }^{1}$ Derived from the equation of time for Washington apparent noon for the year 1899. See the American Ephemeris and Nautical Almanac, I899, pages 377-84.
    ${ }^{2}$ The length of the tropical year is not absolutely constant. The value here given is for the year 1900. Its decrease in 100 years is about 0.5 s . (See the American Ephemeris and Nautical Almanac 1918, page xvi.)

[^3]:    ${ }^{1}$ From Hand-Book of Metcorological Tables. By H. A. Hazen. Washington, 1888.

[^4]:    ${ }^{1}$ Investigations of gravity and isostasy, by William Bowie. U. S. Coast and Geodetic Survey, Special Publication No. 40, 1917, p. 134.
    ${ }^{2}$ Op. cit., p. $50 . \quad{ }^{3}$ Op. cit., p. $59 . \quad{ }^{4}$ Op. cit., p. $50 . \quad{ }^{5}$ Op. cit., p. 59.
    ${ }^{6}$ Bowie, op. cit., p. 134 .
    ${ }^{7}$ Bowie, op. cit., p. 93 .

[^5]:    ${ }^{1}$ In most cases the gravity anomaly may be obtained from Bowie's paper, op. cit., figure 1 I.
    ${ }^{2}$ In some cases this correction may be obtained from Bowie's paper, op. cit., pp. 50-52, but in many cases, and especially in mountainous districts, it must be separately computed for each station.

[^6]:    ${ }^{1}$ Indicated values for latitude and gravity correction apply only to mercurial barometers. For the case of aneroid barometers the $\eta$ is omitted (see pp. xlviii and xlix).

[^7]:    ${ }^{1}$ Comptes Rendus, Quatrième Conférence Générale Poids et Mesures, 1907, pp. 60-6r.
    ${ }^{2}$ Leduc, A. La masse du litre d'air dans les conditions normales. Comite international des poids et mesures. Travaux et mémoires, T. 16, 1917.
    ${ }^{3}$ Lehrbuch der Meteorologie, dritte Auflage, 1915, s. 5.

[^8]:    ${ }^{1}$ In accordance with the relation between the meter and the foot given on p . xxiii, this constant should be 60367 . (See Table 14.)

[^9]:    ${ }^{1}$ A fuller account of this Règlement may be found in the Avant-Propos of the Commission Internationale de la Haute Atmosphère, Comptes Rendus des Jours Internationaux 1923, published in 1927. This may be had on application to the Secretary of this Commission, c/o the Royal Meteorological Society, London.

[^10]:    ${ }^{1}$ The claim for the use of geopotential in measuring heights was set forth by Prof. V. Bjerknes and his collaborators in Vol. I of Dynamical Meteorology and Hydrography, published in English in 1910 by the Carnegie Institution of Washington. The terms "dynamic height" and "dynamic meter" were therein proposed.
    ${ }^{2}$ Helmert: Über die Reduction der auf der physischen Erdoberfläche beobachteten Schweerebeschleunigungen auf ein gemeinsames Niveau, Zweite Mitteilung. Sitzungsberichte der Akademie der Wissenschaften, Berlin, 1903, p. 650.

[^11]:    ${ }^{1}$ Bjerknes, V., and colleagues, Carnegie Inst. Washington, 1910.

[^12]:    ${ }^{1}$ Due to the use of a slightly different value for the coefficient of expansion, Prof. Ferrel's formula, upon which the table is computed, is

    $$
    d Z=-\frac{2628.4}{B}\left(\mathrm{I}+0.002034\left(\theta-32^{\circ}\right)\right)(\mathrm{I}+\beta)
    $$

[^13]:    ${ }^{1}$ Comptes Rendus, Paris, 1850 , vol. xxx., page 300.

[^14]:    ${ }^{1}$ Scheel, Karl und Heuse, Wilhelm. Bestimmung des Sättigungsdrucks von Wasserdampf unter $0^{\circ}$. Annalen der Physik, 1909, 29: 723-737.

    Bestimmung des Sättigungsdrucks von Wasserdampf zwischen $0^{\circ}$ und $+50^{\circ}$. Annalen der Physik, 1910, 31: 715-736.

    Holborn, L. und Henning, F. Über das Platinthermometer und den Sättigungsdruck des Wasserdampfes zwischen 50 und $200^{\circ}$. Annalen der Physik, 1908, 26: 833-883.

    Holborn, L. und Baumann, A. Über den Sättigungsdruck des Wasserdampfes oberhall. $200^{\circ}$. Annalen der Physik, 1910, 31: 945-970.

[^15]:    ${ }^{1}$ Annalen der Physik, 1907, 22: 609-630.
    ${ }^{2}$ Cederberg, Ivar W. Über eine exakte Dampfdruckberechnungsmethode. Physik. Zeitschr. xv: 697, 1914; Über die Temperaturabhängigkeit einiger physikalischen Eigenschaften des Wassers in seinen vershiedenen Aggregatzuständen. Physik. Zeitschr, xv: $824,1914$.

[^16]:    ${ }^{1}$ Scheel, K., and Heuse, W., op. cit., p. 1xi.
    ${ }^{2}$ Nernst, W. Verhandlungen der Deutschen Physikalischen Gesellshaft, vol. ir, no. 15, p. 313, Aug. 15, 1909.

    Nernst, W. Kinetische Theorie fester Körper; Vorträge über die kinetische Theorie der Materie und der Elektrizität. B. G. Teubner.
    ${ }^{3}$ Weber, S. Communications from the Physical Laboratory at the University of Leiden, no. I50; p. 37.

[^17]:    ${ }^{1}$ Thiesen, M. Die Dampfspannung über Eis. (Mitteilung aus der PhysikalischTechnischen Reichsanstalt.) Annalen der Plyysik, vol. 29, p. 1057, 1909.
    ${ }^{2}$ Weber, S. Loc. cit., pp. 50-52.
    Knudson, M. Annalen der Physik. Vierte Folge, Band 44, p. 536, 1914.

[^18]:    ${ }^{1}$ Nernst, W. Verhandlungen der Deutschen Physikalischen Gesellshaft, vol. 12, p. 568, 1910.
    ${ }^{2}$ Washburn, E. W. Monthly Weather Review, vol. 52, p. 488, 1924.
    ${ }^{3}$ International Critical Tables, vol. III, p. 210, McGraw-Hill Book Company, 1928.
    ${ }^{4}$ Holborn, L., Scheel, K., and Henning, F. "Wärmetabellen der PhysikalischTechnischen Reichsanstalt," Braunschweig, i919.

[^19]:    ${ }_{1}$ Marks, Lionel S., and Davis, Harvey N. Tables and diagrams of the thermal properties of saturated and superheated steam. New York, 1909.

[^20]:    ${ }^{1}$ The latest adopted value of $\delta=1.2028$ makes this factor 1.05822 , and in a few cases, especially at high temperatures, increases $I V^{\prime}$ by 0.001 over the values given in Tables 81 and 80 . ${ }^{2} 564.95$ with $\delta=1.2928, \quad{ }^{3} 11.7461$ with $\delta=1.2928$.

[^21]:    ${ }^{1}$ Gravity is here considered in terms of force (expressed in dynes) that is exerted on a mass of one gram rather than its numerical equivalent, acceleration (expressed in centimeters and seconds), for which there is no convenient expression.
    ${ }^{2}$ See Bowie, William, Investigations of Gravity and Isostasy. U.S. Coast and Geodetic Survey, Special Publication No. 40, 1917, page 134.

[^22]:    ${ }^{1}$ Kimball, Herbert H. " Duration and Intensity of Twilight," Monthly Weather Review 1916, 44:614-620.

[^23]:    ${ }^{1}$ Ball, Frederick. Altitude Tables for let. $31^{\circ}$ to $60^{\circ}$. London, 1907 ; [same] for lat. $0^{\circ}$ to $30^{\circ}$, London, 910.

[^24]:    ${ }^{1}$ Abbot, C. G. Smithsonian Solar Researches. Gerland’s Beitrage zur Geophysik, Bd. XVI, Heft 4, pp. 344-353, 1927.
    ${ }^{2}$ Fowle, F. E. Water vapor transparency to low-temperature radiation. Smithsonian Misc. Coll., vol. 68, no. 8, 1917.

[^25]:    ${ }^{1}$ Fowle, F. E. Atmospheric ozone: Its relation to some solar and terrestrial phenomena. Smithsonian Misc. Coll., vol. 81, No. 11, 1929.

[^26]:    Smithsonian Tables.

[^27]:    SMITHSONIAN TABLES.

[^28]:    Smithbonian Tables.

[^29]:    Smithsonian Tables

[^30]:    Note.-Stations with asterisk appear in the "Réseau Mondial" of the British Meteorological Office for 1922. (London, 1929.)

[^31]:    Smithsonian Tables

