TABLE 1,-TEMPERATURE CONVERSION TABLE*
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# SMITHSONIAN PHYSICAL TABLES 

NINTH REVISED EDITION<br>(Fourth Reprint)

Prepared by<br>WILLIAM ELMER FORSYTHE



## CITY OF WASHINGTON

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## PREFACE TO THE NINTH REVISED EDITION

This edition of the Smithsonian Physical Tables consists of 901 tables giving data of general interest to scientists and engineers, and of particular interest to those concerned with physics in its broader sense. The increase in size over the Eighth Edition is due largely to new data on the subject of atomic physics. The tables have been prepared and arranged so as to be convenient and easy to use. The index has been extended. Each set of data given herein has been selected from the best sources available. Whenever possible an expert in each field has been consulted. This has entailed a great deal of correspondence with many scientists, and it is a pleasure to add that, almost without exception, all cooperated generously.

When work first started on this edition, Dr. E. U. Condon, then director of the National Bureau of Standards, kindly consented to furnish any assistance that the scientists of that institution were able to give. The extent of this help can be noted from an inspection of the book. Dr. Wallace R. Brode, associate director, National Bureau of Standards, gave valuable advice and constructive criticism as to the arrangement of the tables.
D. H. Menzel and Edith Jenssen Tebo, Harvard University, Department of Astronomy, collected and arranged practically all the tables on astronomy.

A number of experts prepared and arranged groups of related data, and others either prepared one or two tables or furnished all or part of the data for certain tables. Care has been taken in each case to give the names of those responsible for both the data and the selection of it. A portion of the data was taken from other published sources, always with the.consent and approval of the author and publisher of the tables consulted. Due credit has been given in all instances. Very old references have been omitted. Anyone in need of these should refer to the Eighth Edition.

It was our intention to mention in this preface the names of all who took part in the work, but the list proved too long for the space available. We wish, however, to express our appreciation and thanks to all the men and women from various laboratories and institutions who have been so helpful in contributing to this Ninth Edition.

Finally, we shall be grateful for criticism, the notification of errors, and new data for use in reprints or a new edition.

W. E. FORSYTHE

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January 1951

## EDITOR'S NOTE

The ninth edition of the Physical Tables was first published in June 1954. In the first reprint (1956), the second reprint (1959), and the third (1964) a few misprints and errata were corrected.


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## INTRODUCTION

## UNITS OF MEASUREMENT

The quantitative measure of anything is expressed by two factors-one, a certain definite amount of the kind of physical quantity measured, called the unit ; the other, the number of times this unit is taken. A distance is stated as 5 meters. The purpose in such a statement is to convey an idea of this distance in terms of some familiar or standard unit distance. Similarly quantity of matter is referred to as so many grams; of time, as so many seconds, or minutes, or hours.

The numerical factor definitive of the magnitude of any quantity must depend on the size of the unit in terms of which the quantity is measured. For example, let the magnitude factor be 5 for a certain distance when the mile is used as the unit of measurement. A mile equals 1,760 yards or 5,280 feet. The numerical factor evidently becomes 8,800 and 26,400 , respectively, when the yard or the foot is used as the unit. Hence, to obtain the magnitude factor for a quantity in terms of a new unit, multiply the old magnitude factor by the ratio of the magnitudes of the old and new units; that is, by the number of the new units required to make one of the old.

The different kinds of quantities measured by physicists fall fairly definitely into two classes. In one class the magnitudes may be called extensive, in the other, intensive. To decide to which class a quantity belongs, it is often helpful to note the effect of the addition of two equal quantities of the kind in question. If twice the quantity results, then the quantity has extensive (additive) magnitude. For instance, two pieces of platinum, each weighing 5 grams, added together weigh 10 grams; on the other hand, the addition of one piece of platinum at $100^{\circ} \mathrm{C}$ to another at $100^{\circ} \mathrm{C}$ does not result in a system at $200^{\circ} \mathrm{C}$. Volume, entropy, energy may be taken as typical of extensive magnitudes; density, temperature and magnetic permeability, of intensive magnitudes.

The measurement of quantities having extensive magnitude is a comparatively direct process. Those having intensive magnitude must be correlated with phenomena which may be measured extensively. In the case of temperature, a typical quantity with intensive magnitude, various methods of measurement have been devised, such as the correlation of magnitudes of temperature with the varying lengths of a thread of mercury.
Fundamental units.-It is desirable that the fewest possible fundamental unit quantities should be chosen. Simplicity should regulate the choicesimplicity first, psychologically, in that they should be easy to grasp mentally, and second, physically, in permitting as straightforward and simple definition as possible of the complex relationships involving them. Further, it seems desirable that the units should be extensive in nature. It has been found possible to express all measurable physical quantities in terms of five such units: first, geometrical considerations-length, surface, etc.-lead to the need of a length; second, kinematical considerations-velocity, acceleration, etc.-introduce time ; third, mechanics-treating of masses instead of immaterial points-in-
troduces matter with the need of a fundamental unit of mass; fourth, electrical, and fifth, thermal considerations require two more such quantities. The discovery of new classes of phenomena may require further additions.

As to the first three fundamental quantities, simplicity and good use sanction the choice of a length, $L$, a time interval, $T$, and a mass, $M$. For the measurement of electrical quantities, good use has sanctioned two fundamental quan-tities-the dielectric constant, $K$, the basis of the "electrostatic" system, and the magnetic permeability, $\mu$, the basis of the "electromagnetic" system. Besides these two systems involving electrical considerations, there is in common use a third one called the "absolute" system, which will be referred to later. For the fifth, or thermal fundamental unit, temperature is generally chosen. ${ }^{1}$

Derived units.-Having selected the fundamental or basic units-namely, a measure of length, of time, of mass, of permeability or of the dielectric constant, and of temperature-it remains to express all other units for physical quantities in terms of these. Units depending on powers greater than unity of the basic units are called "derived units." Thus, the unit volume is the volume of a cube having each edge a unit of length. Suppose that the capacity of some volume is expressed in terms of the foot as fundamental unit and the volume number is wanted when the yard is taken as the unit. The yard is three times as long as the foot and therefore the volume of a cube whose edge is a yard is $3 \times 3 \times 3$ times as great as that whose edge is a foot. Thus the given volume will contain only $1 / 27$ as many units of volume when the yard is the unit of length as it will contain when the foot is the unit. To transform from the foot as old unit to the yard as new unit, the old volume number must be multiplied by $1 / 27$, or by the ratio of the magnitude of the old to that of the new unit of volume. This is the same rule as already given, but it is usually more convenient to express the transformations in terms of the fundamental units directly. In the present case, since, with the method of measurement here adopted, a volume number is the cube of a length number, the ratio of two units of volume is the cube of the ratio of the intrinsic values of the two units of length. Hence, if $l$ is the ratio of the magnitude of the old to that of the new unit of length, the ratio of the corresponding units of volume is $l^{3}$. Similarly the ratio of two units of area would be $l^{2}$, and so on for other quantities.

## CONVERSION FACTORS AND DIMENSIONAL FORMULAE

For the ratio of length, mass, time, temperature, dielectric constant, and permeability units the small bracketed letters, $[l],[m],[t],[\theta],[k]$, and $[\mu]$ will be adopted. These symbols will always represent simple numbers, but the magnitude of the number will depend on the relative magnitudes of the units the ratios of which they represent. When the values of the numbers represented by these small bracketed letters as well as the powers of them involved in any particular unit are known, the factor for the transformation is at once obtained. Thus, in the above example, the value of $l$ was $1 / 3$, and the power involved in the expression for volume was 3 ; hence the factor for transforming from cubic feet to cubic yards was $l^{3}$ or $1 / 3^{3}$ or $1 / 27$ These factors will be called conversion factors.

[^0]To find the symbolic expression for the conversion factor for any physical quantity, it is sufficient to determine the degree to which the quantities, length, mass, time, etc., are involved. Thus a velocity is expressed by the ratio of the number representing a length to that representing an interval of time, or [ $L / T]$, and acceleration by a velocity number divided by an interval-of-time number, or $\left[L / T^{2}\right]$, and so on, and the corresponding ratios of units must therefore enter in precisely the same degree. The factors would thus be for the just-stated cases, $[l / t]$ and $\left[l / t^{2}\right]$. Equations of the form above given for velocity and acceleration which show the dimensions of the quantity in terms of the fundamental units are called dimensional equations. Thus $[E]=\left[M L^{2} T^{-2}\right]$ will be found to be the dimensional equation for energy, and $\left[M L^{2} T^{-2}\right]$ the dimensional formula for it. These expressions will be distinguished from the conversion factors by the use of bracketed capital letters.

In general, if we have an equation for a physical quantity,

$$
Q=C L^{a} M^{b} T^{c},
$$

where $C$ is a constant and $L, M, T$ represent length, mass, and time in terms of one set of units, and it is desired to transform to another set of units in terms of which the length, mass, and time are $L_{1}, M_{1}, T_{1}$, we have to find the value of $L_{1} / L, M_{1} / M, T_{1}^{\circ} / T$, which, in accordance with the convention adopted above, will be $l, m, t$, or the ratios of the magnitudes of the old to those of the new units.

Thus $L_{1}=L l, M_{1}=M m, T_{1}=T t$, and if $Q_{1}$ be the new quantity number,

$$
\begin{aligned}
Q_{1} & =C L_{1}{ }^{a} M_{1}{ }^{b} T_{1}{ }^{c}, \\
& =C L^{a} l^{a} M^{b} m^{b} T^{c} t^{c}=Q l^{a} m^{b} t^{c},
\end{aligned}
$$

or the conversion factor is $\left[l^{a} m^{b} t^{c}\right]$, a quantity precisely of the same form as the dimension formula [ $L^{a} M^{b} T^{c}$ ].

Dimensional equations are useful for checking the validity of physical equations. Since physical equations must be homogeneous, each term appearing in then must be dimensionally equivalent. For example, the distance moved by a uniformly accelerated body is $s=v_{0} t+\frac{1}{2} a t^{2}$. The corresponding dimensional equation is $[L]=[(L / T) T]+\left[\left(L / T^{2}\right) T^{2}\right]$, each term reducing to $[L]$.

Dimensional considerations may often give insight into the laws regulating physical phenomena. ${ }^{2}$ For instance, Lord Rayleigh, in discussing the intensity of light scattered from small particles, in so far as it depends upon the wavelength, reasons as follows: ${ }^{3}$

The object is to compare the intensities of the incident and scattered ray; for these will clearly be proportional. The number (i) expressing the ratio of the two amplitudes is a function of the following quantities:- $V$, the volume of the disturbing particle; $r$, the distance of the point under consideration from it; $\lambda$, the wavelength; $c$, the velocity of propagation of light ; $D$ and $D^{\prime}$, the original and altered densities: of which the first three depend only on space, the fourth on space and time, while the fifth and sixth introduce the consideration of mass. Other elements of the problem there are none, except mere numbers and angles, which do not depend upon the fundamental measurements of space, time, and mass. Since the ratio $i$, whose expression we seek, is of no dimensions in mass, it follows at once that $D$ and $D^{\prime}$ occur only under the form $D: D^{\prime}$, which is a simple number and may therefore be omitted. It remains to find how $i$ varies with $V, r, \lambda, c$.

Now, of these quantities, $c$ is the only one depending on time; and therefore, as $i$ is of no dimensions in time, $c$ cannot occur in its expression. We are left, then, with $V, r$, and $\lambda$; and from what we know of the dynamics of the question, we may be sure that $i$ varies directly as $V$ and inversely as $r$, and must therefore be proportional to $V \div \lambda^{2} r, V$ being of three di-

[^1]mensions in space. In passing from one part of the spectrum to another $\lambda$ is the only quantity which varies, and we have the important law:

When light is scattered by particles which are very small compared with any of the wavelengths, the ratio of the amplitudes of the vibrations of the scattered and incident light varies inversely as the square of the wavelength, and the intensity of the lights themselves as the inverse fourth power.

The dimensional and conversion-factor formulae for the more commonly occurring derived units are given in Table 30.

## TABLE 2.-SOME FUNDAMENTAL DEFINITIONS

Part 1.-Geometrical and mechanical units 4
Activity (power).-Time rate of doing work; unit, the watt.
Angle $(\phi)$.-The ratio of the length of its circular arc to its radius; unit, the radian.

Angstrom.-Unit of wavelength $=10^{-10}$ meter. (See Table 522.)
Angular acceleration $\left(\alpha=\frac{d \omega}{d t}\right)$.-The rate of change of angular velocity.
Angular momentum ( $I \omega$ ). -The product of its moment of inertia about an axis through its center of mass perpendicular to its plane of rotation and its angular velocity.

Angular velocity. - The time rate of change of angle.
Area.-Extent of surface. Unit, a square whose side is the unit of length. The area of a surface is expressed as $S=C L^{2}$, where the constant $C$ depends on the contour of the surface and $L$ is a linear dimension. If the surface is a square and $L$ the length of a side, $C$ is unity; if a circle and $L$ its diameter, $C$ is $\pi / 4$. (See Table 31.)

Atmosphere.-Unit of pressure. (See Table 260.)

$$
\begin{gathered}
\text { English normal }=14.7 \mathrm{lb} / \mathrm{in.}^{2}=29.929 \mathrm{in} . \mathrm{Hg}=760.1 \mathrm{~S} \mathrm{mmHg}\left(32^{\circ} \mathrm{F}\right) \\
\mathrm{U} . \mathrm{S} .
\end{gathered}=760 \mathrm{mmHg}\left(0^{\circ} \mathrm{C}\right)=29.921 \mathrm{in} . \mathrm{Hg}=14.70 \mathrm{lb} / \mathrm{in} .^{2} .
$$

Avogadro number.-Number of molecules per mole, $6.0228 \times 10^{23}$ molecules/mole.

Bar. ${ }^{4 a}$-International unit of pressure $10^{6}$ dyne $/ \mathrm{cm}^{2}$.
Barye.-cgs pressure unit, one dyne/ $\mathrm{cm}^{2}$.
Carat.-The diamond carat standard in U. S. $=200 \mathrm{mg}$. Old standard $=$ $205.3 \mathrm{mg}=3.168$ grains. The gold carat: pure gold is 24 carats; a carat is 1/24 part.

Circular area.-The square of the diameter $=1.2733 \times$ true area. True area $=0.785398 \times$ circular area.

Circular inch.-Area of circle 1 inch in diameter.
Cubit $=18$ inches

[^2]Dalton (atomic mass unit $\mathrm{M}_{0}$ ). -Unit of mass, $1 / 16$ mass of oxygen $\left({ }_{8} 0^{16}\right)$ atom, $1.66080 \times 10^{-24} \mathrm{~g}$ (Phys. scale). (See Table 26.)

Density.-The mass per unit volume. The specific gravity of a body is the ratio of a density to the density of a standard substance. Water and air are commonly used as the standard substance.

Digit.-3/4 in.; $1 / 12$ the apparent diameter of the sun or moon.
Diopter.-Unit of "power of a lens." The diopter $=$ the reciprocal of the focal length in meters.

Dyne.-The cgs, unit of force $=$ that unbalanced force which acting for 1 second on body of 1 gram mass produces a velocity change of $1 \mathrm{~cm} / \mathrm{sec}$.

Energy.-The work done by a force produces either a change in the velocity of a body or a change of its shape or position or both. In the first case it produces a change of kinetic energy, in the second, of potential energy.

Erg.-The cgs unit of work and energy $=$ the work done by 1 dyne acting through 1 centimeter.

Fluidity.-Reciprocal of viscosity.
Foot-pound.-The work which will raise 1 pound body 1 foot high for standard g.

Foot-poundal.-The work done when a force of 1 poundal acts through 1 foot.

Force $(f)$.-Force is the agent that changes the motion of bodies and is measured by the rate of change of momentum it produces on a free body.
$\mathrm{Gal}=$ gravity standard $=$ an acceleration of $1 \mathrm{~cm} \mathrm{sec}^{-2}$.
Giga $=10^{9}$.
Gram.-The standard of mass in the metric system. (See Table 31.)
Gram-centimeter.-The cgs gravitation unit of work.
Gram-molecule.-The mass in grams of a substance numerically equal to its molecular weight.

Gravitation constant.- $\left(G\right.$, in formula $\left.F=G m_{1} m_{2} / r^{2}\right)=6.670 \times 10^{-8}$ dyne $\mathrm{cm}^{2} \mathrm{~g}^{-2}$.

Gravity $(g)$.-The attraction of the earth for any mass. It is measured by the acceleration produced on the mass under standard conditions. This acceleration $g$ equals $980.665 \mathrm{~cm} \mathrm{sec}^{-2}$ or $32.17 \mathrm{ft} \mathrm{sec}^{-2}$.

Horsepower.-A unit of mechanical power. The English and American horsepower is defined by some authorities as 550 foot-pounds/sec and by others as 746 watts. The continental horsepower is defined by some authorities as $75 \mathrm{kgm} / \mathrm{sec}$ and by others as 736 watts.

Joule.-Unit of work (energy) $=10^{7}$ ergs. Joules $=\left(\right.$ volts $\left.^{2} \times \mathrm{sec}\right) /$ ohms $=$ watts $\times$ sec $=$ amperes $^{2} \times$ ohms $\times$ sec $=$ volts $\times$ amperes $\times$ sec.

Kilodyne.- 1,000 dynes. About 0.980 gram weight.

Kinetic energy.-The energy associated with the motion $=\frac{m v^{2}}{2}$ in ergs if $m$ is in grams and $v$ in $\mathrm{cm} / \mathrm{sec}$.

Linear acceleration $\left(a=\frac{d v}{d t}\right)$.-The rate of change of velocity.
Liter.-See Table 32.
Loschmidt number.-The number of molecules per $\mathrm{cm}^{3}$ of an ideal gas at $0^{\circ} \mathrm{C}$ and normal pressure $=2.6870 \times 10^{19}$ molecules $/ \mathrm{cm}^{3}$.

Megabaryes.-Unit of pressure $=1,000,000$ baryes $=1$ bar $=0.987$ atmosphere.

Meter.-See Table 31.
Micro.-A prefix indicating the millionth part. (See Table 901.)
Micron $(\mu)=$ one-millionth of a meter $=$ one-thousandth of a millimeter.
Mil.-One-thousandth of an inch.
Mile.-Statute $=5,280$ feet $;$ nautical or geographical $=6,080.20$ feet.
Milli.-A prefix denoting the thousandth part.
Modulus of elasticity.-Ratio of stress to strain. The dimension of strain, a change of length divided by a length, or change of volume divided by a volume, is unity.

Mole or mol.-Mass equal numerically to molecular weight of substance.
Momentum ( $M=m v$ ).-The quantity of motion in the Newtonian sense; the product of the mass and velocity of the body.

Moment of inertia (I) of a body about an axis is the $\Sigma m r^{2}$, where $m$ is the mass of a particle of the body and $r$ its distance from the axis.

Newton.-The unit of force in the MKS system $=10^{5}$ dynes. (See Table 3, part 2.)

Pound weight.-A force equal to the earth's attraction for a mass of 1 pound. This force, acting on 1 lb mass, will produce an acceleration of 32.17 $\mathrm{ft} / \mathrm{sec}^{2}$.

Poundal.-The ft-lb sec unit of force. That unbalanced force which acting on a body of 1 lb mass produces an acceleration of $1 \mathrm{ft} / \mathrm{sec}^{2}$.

Pi $(\pi)=3.1416$. (See Table 11.)
Power.-Activity $\left(p=\frac{d W}{d t}\right)$ is the time rate of doing work.
Radian.-An angle subtended by an arc equal to the radius. This angle equals $180^{\circ} / \pi=57.29578^{\circ}=57^{\circ} 17^{\prime} 45^{\prime \prime}=206265^{\prime \prime}$.

Resilience.-The work done per unit volume of a body in distorting it to the elastic limit or in producing rupture.

Slug.-Mass ( 32.17 lb ) acquiring acceleration $1 \mathrm{ft} \mathrm{sec}^{-2}$ when continuously acted upon by force of 1 lb weight.

## Smithsonian physical tables

Strain.-The deformation produced by a stress divided by the original dimension.

Stress.-The force per unit area of a body that tends to produce a deformation.

Tenth-meter. $-10^{-10}$ meter $=1$ angstrom.
Torque, moment of a couple, about an axis is the product of a force and the distance of its line of action from the axis.

Volume.-Extent of space. Unit, a cube whose edge is the unit of length. The volume of a body is expressed as $V=C L^{3}$. The constant $C$ depends on the shape of the bounding surfaces.

Velocity $\left(\mathrm{v}=\frac{d L}{d t}\right)$ is distance traversed per unit time.
Viscosity.-The property of a liquid by virtue of which it offers resistance to flow. The coefficient of viscosity is the tangential force that must be applied to the upper surface of a $1-\mathrm{cm}$ cube of the liquid on an edge to produce a velocity of $1 \mathrm{~cm} / \mathrm{sec}$ in the face when the lower face is at rest.

Work (W).-The work done by an unbalanced force is the product of the force by the component of the resulting displacement produced in the direction of the force.

Young's modulus.-Ratio of longitudinal stress within the proportional limit to the corresponding longitudinal strain.

## Part 2.—Heat Units ${ }^{5}$

Blackbody.-A body that absorbs all the radiation that falls upon it. From this definition and certain assumptions it can be shown that its total radiation $=$ $\sigma T^{4}$ (Stefan-Boltzmann Law) and that the spectral distribution of the radiation is given by the Planck Law: ${ }^{5 \mathrm{a}}$

$$
J_{\lambda}=\frac{A c_{1} \lambda^{-8}}{e^{\frac{c_{2}}{\lambda T}}-1}
$$

Brightness temperature ( $S$ ).-The temperature of a non-blackbody determined from its brightness (with an optical pyrometer, see Table 77) as if it were a blackbody. Such temperatures are always less than the true temperatures.

British thermal unit (Btu). -The amount of heat required to raise 1 pound of water at $60^{\circ} \mathrm{F}, 1^{\circ} \mathrm{F}$. This unit is defined for various temperatures, but the general usage seems to be to take the Btu as equal to 252 calories. (See calorie. See Table 7.)

Calorie.-The amount of heat necessary to raise 1 gram of water at $15^{\circ} \mathrm{C}$, $1^{\circ} \mathrm{C}$.

$$
\begin{aligned}
& { }^{5} \text { For dimensional formulas see Table } 30 \text {, part } 2 \text {. } \\
& { }_{5 \Omega} \text { An easier way to write this exponential term is: } \\
& \qquad . J_{\lambda}=c_{1} \lambda^{-3} /\left[\left(\exp \left(\frac{c z}{\lambda T}\right)\right)-1\right]
\end{aligned}
$$

This form will be used hereafter.

There are various calories depending upon the interval chosen. Sometimes the unit is written as the gram-calorie or the kilogram-calorie, the meaning of which is evident. There is some tendency to define the calorie in terms of its mechanical equivalent. Thus the National Bureau of Standards defines the calorie as 4.18400 joules. At the International Steam Table Conference held in London in 1929 the international calorie was defined as $1 / 860$ of the international watt hour (see Table 7), which made it equal to 4.1860 international joules. With the adoption of the absolute system of electrical units, this becomes $1 / 859.858$ watt hours or 4.18674 joules. The Btu was defined at the same time as 251.996 international calories. Thus, until such a time as these differences are taken care of, there will be some confusion.

Celsius temperature scale.-The present-day designation of the scale formerly known as the Centigrade scale.

Centigrade temperature scale.-The temperature scale that divides the interval between the ice point, taken as $0^{\circ} \mathrm{C}$, and the boiling point of water with $100^{\circ}$.

Coefficient of thermal expansion.-Ratio of the change of length per unit length (linear), or change of volume per unit volume (voluminal), to the change of temperature.

Color temperature ${ }^{6}\left(T_{S}\right)$.-The color temperature of a non-blackbody is the temperature at which it is necessary to operate the blackbody so that the color of its emitted light will match that of the source studied.

Emissivity.-Ratio of the energy radiated at any temperature by a nonblackbody to that radiated by a blackbody at the same temperature. The spectral emissivity is for a definite wavelength, and the total emissivity is for all wavelengths.

Enthalpy.-Total energy that a system possesses by virtue of its temperature. Thus, where $U$ is the internal energy, then the enthalpy $=U+P V$ where $P V$ represents the external work.

Entropy.-A measure of the extent to which the energy of the system is unavailable.

Fahrenheit temperature scale.-A scale based on the freezing point of water taken as $32^{\circ}$ and the boiling point of water taken as $212^{\circ}$.

Graybody.-A body that has a constant emissivity for all wavelengths.
Heat.-Energy transferred by a thermal process. Heat can be measured in terms of the dynamical units of energy, as the erg, joule, etc., or in terms of the amount of energy required to produce a definite thermal change in some substance, as for example the energy required per degree to raise the temperature of a unit mass of water at some temperature. The mechanical unit of heat has the dimensional formula of energy $\left(M L^{2} T^{-2}\right)$. The thermal unit $(H)$, as used in many of these tables, is $(M \theta)$ where $\theta$ denotes a temperature interval.

Joule's equivalent $(J)$ or the mechanical equivaient of heat.-Conversion factor for changing an expression of mechanical energy into an expression of thermal energy or vice versa ( $4.1855 \mathrm{~J} / \mathrm{cal}$ ).

[^3]Kelvin temperature scale.-Scale of temperature based on equal work for equal temperatures for a working substance in a carnot cycle $=$ Celsius (Centigrade) scale +273.16

Langley (ly).-A new unit of radiation, surface density, has been suggested ${ }^{7}$ which equals 1 calorie $\left(15^{\circ} \mathrm{C}\right)$ per $\mathrm{cm}^{2}$.

Latent heat.-Quantity of heat required to change the state of a unit mass of matter.

Pyron.-A unit of radiant intensity $=1 \mathrm{cal} \mathrm{cm}^{-2} \mathrm{~min}^{-1}$.
Radiant energy.-Energy traveling in the form of electromagnetic waves.
Radiant temperature.-The temperature obtained by use of a total radiation pyrometer when sighted upon a non-blackbody. This is always less than the true temperature.

Rankin temperature scale.-Absolute Fahrenheit scale $=$ Fahrenheit scale +459.7 .

Reaumur temperature scale.-A scale based upon the freezing point of water taken as $0^{\circ} \mathrm{R}$ and the boiling point of water taken as $80^{\circ} \mathrm{R}$.

Specific heat.-Ratio of the heat capacity of a substance to the heat capacity of an equal mass of water. When so expressed, the specific heat is a dimensionless number.

Standard temperature.-A temperature that depends upon some characteristic of some substance, such as the melting, boiling, or freezing point, that is used as a reference standard of temperature.

Thermal capacitance.-The heat capacity of a body is the limiting value, as $T$ approaches zero, of the ratio $\frac{\Delta Q}{\Delta T}$, where $\Delta T$ is the rise in temperature resulting from the addition to the body of a quantity of heat equal to $\Delta Q$.

Thermal conductivity.-Quantity of heat, $Q$, which flows normally across a surface of unit area per unit of time and per unit of temperature gradient normal to the surface. In thermal units it has the dimensional formula ( $H \theta^{-1} L^{-1} T^{-1}$ ) or ( $M L^{-1} T^{-1}$ ), in mechanical units ( $M L T^{-3} \theta^{-1}$ ).

Thermodynamic temperature.-See Kelvin temperature scale.
Thermodynamics.-Study of the flow of heat.
Thermodynamic laws: Zeroth laze.-Two systems that are in thermal equilibrium with a third are in thermal equilibrium with each other. First lazv: When equal quantities of mechanical effect are produced by any means whatever from purely thermal effects, equal quantities of heat are put out of existence or are created. Second lazu: It is impossible to transfer heat from a cold body to a hot body without the performance of mechanical work. Third laze: It is impossible by any means whatever to superpose only the images of several light sources to obtain an image brighter than the brightest of the source.
${ }^{7}$ Aldrich et al., Science, vol. 106, p. 225, 1947.

A system of units of electric and magnetic quantities requires four fundamental quantities. A system in which length, mass, and time constitute three of the fundamental quantities is known as an "absolute" system. There are two absolue systems of electric and magnetic units. One is called the electrostatic, in which the fourth fundamental quantity is the dielectric constant, and one is called the electromagnetic, in which the fourth fundamental quantity is magnetic permeability. Besides these two systems there will be described a third, to be known as the absolute system, that was introduced January 1, 1948. (See Table 4.)
In the electrostatic system, unit quantity of electricity, $Q$, is the quantity which exerts unit mechanical force upon an equal quantity a unit distance from it in a vacuum. From this definition the dimensions and the units of all the other electric and magnetic quantities follow through the equations of the mathematical theory of electromagnetism. The mechanical force between two quantities of electricity in any medium is

$$
F=\frac{Q Q^{\prime}}{K r^{2}},
$$

where $K$ is the dielectric constant, characteristic of the medium, and $r$ the distance between the two points at which the quantities $Q$ and $Q^{\prime}$ are located. $K$ is the fourth quantity entering into dimensional expressions in the electrostatic system. Since the dimensional formula for force is $\left[M L T^{-2}\right]$, that for $Q$ is [ $\left.M^{\frac{1}{2}} L^{\frac{1}{2}} T^{-1} K^{\frac{1}{2}}\right]$.
The electromagnetic system is based upon the unit of the magnetic pole strength (see Table 466). The dimensions and the units of the other quantities are built up from this in the same manner as for the electrostatic system. The mechanical force between two magnetic poles in any medium is

$$
F=\frac{m m^{\prime}}{\mu r^{2}},
$$

in which $\mu$ is the permeability of the medium and $r$ is the distance between two poles having the strengths $m$ and $m^{\prime} . \mu$ is the fourth quantity entering into dimensional expressions in the electromagnetic system. It follows that the dimensional expression for magnetic pole strength is $\left[M^{\frac{3}{2}} L^{\frac{1}{2}} T^{-1} \mu^{3}\right]$.

The symbols $K$ and $\mu$ are sometimes omitted in the dimensional formulae so that only three fundamental quantities appear. There are a number of objections to this. Such formulae give no information as to the relative magnitudes of the units in the two systems. The omission is equivalent to assuming some relation between mechanical and electrical quantities, or to a mechanical explanation of electricity. Such a relation or explanation is not known.

The properties $K$ and $\mu$ are connected by the equation $1 / V K \mu=v$, where $v$ is the velocity of an electromagnetic wave. For empty space or for air, $K$ and $\mu$ leeing measured in the same units, $1 \sqrt{ } K \mu=c$, where $c$ is the velocity of light in vacuo, $2.99776 \times 10^{10} \mathrm{~cm}$ per sec. It is sometimes forgotten that the omission of the dimensions of $K$ or $\mu$ is merely conventional. For instance, magnetic field intensity and magnetic induction apparently have the same dimensions when $\mu$ is omitted. This results in confusion and difficulty in understanding the theory of magnetism. The suppression of $\mu$ has also led to the use of the "centimeter" as a unit of capacity and of inductance; neither is physically the same as length.

Capacitance of an insulated conductor is proportional to the ratio of the quantity of electricity in a charge to the potential of the charge. The dimensional formula is the ratio of the two formulae for electric quantity and potential or [ $M^{\frac{1}{2}} L^{\frac{1}{2}} T^{-1} K^{\frac{3}{2}} / M^{\frac{1}{3}} L^{\frac{1}{2}} T^{-1} K^{-\frac{1}{2}}$ ] or [ $\left.L K\right]$.

Conductance of any part of an electric circuit, not containing a source of electromotive force, is the ratio of the current flowing through it to the difference of potential between its ends. The dimensional formula is the ratio of the formulae for current and potential or [ $M^{\frac{3}{3}} L^{\frac{3}{2}} T^{-2} K^{3} / M^{3} L^{\frac{3}{2}} T^{-1} K^{-\frac{1}{2}}$ ] or $\left[L T^{-1} K\right]$.

Electrical conductivity, like the corresponding term for heat, is quantity per unit area per unit potential gradient per unit of time. The dimensional formula is $\left[M^{\frac{3}{3}} L^{\frac{3}{2}} T^{-1} K^{\frac{1}{3}} / L^{2}\left(M^{\frac{1}{3}} L^{\frac{3}{2}} T^{-1} K^{-\frac{1}{3}} / L\right) T\right.$ ] or [ $T^{-1} K$ ].

Electric current (statampere-unit quantity) is quantity of electricity flowing through a cross section per unit of time. The dimensional formula is the ratio of the formulae for electric quantity and for time or $\left[M^{3} L^{\frac{1}{2}} T^{-1} K^{\ddagger} / T\right]$ or [ $M^{\frac{3}{2}} L^{\frac{1}{2}} T^{-2} K^{\frac{1}{3}}$.

Electric field intensity strength at a point is the ratio of the force on a quantity of electricity at a point to the quantity of electricity. The dimensional formula is therefore the ratio of the formulae for force and electric quantity or $\left[M L T^{-2} / M^{\frac{3}{2}} L^{\frac{1}{2}} T^{-1} K^{3}\right]$ or $\left[M^{3} L^{-4} T^{-1} K^{-3}\right]$.

Electric potential difference and electromotive force (emf) (statvoltwork $=1 \mathrm{erg}$ ). -Change of potential is proportional to the work done per unit of electricity in producing the change. The dimensional formula is the ratio of the formulae for work and electrical quantity or $\left[M L^{2} T^{-2} / M^{3} L^{\frac{1}{2}} T^{-1} K^{3}\right]$ or [ $\left.M^{3} L^{3} T^{-1} K^{-4}\right]$.

Electric surface density of an electrical distribution at any point on a surface is the quantity of electricity per unit area. The dimensional formula is the ratio of the formulae for quantity of electricity and for area or $\left[M^{\frac{1}{2}} L^{-\frac{1}{2}} T^{-1} K^{\frac{1}{3}}\right]$.

Quantity of electricity has the dimensional formula $\left[M^{3} L^{\frac{1}{2}} T^{-1} K^{3}\right]$, as shown above.

Resistance is the reciprocal of conductance. The dimensional formula is [ $L^{-1} T K^{-1}$ ].

Resistivity is the reciprocal of conductivity. The dimensional formula is [ $T K^{-1}$ ].

Specific inductive capacity is the ratio of the inductive capacity of the substance to that of a standard substance and therefore is a number.

Exs.-Find the factor for converting quantity of electricity expressed in ft -grain-sec units to the same expressed in cgs units. The formula is [ $\left.m^{3} l \sqrt{2} t^{-1} k^{3}\right]$, in which $m=0.0648$, $l=30.48, t=1, k=1$; the factor is $0.0648^{3} \times 30.48^{\frac{1}{2}}$, or 42.8 .

Find the factor required to convert electric potential from mm-mg-sec units to cgs units. The formula is [ $m^{3} l^{3} t^{-1} k^{-\frac{1}{2}}$ ], in which $m=0.001, l=0.1, t=1, k=1$; the factor is $0.001^{\frac{1}{2}} \times 0.1^{\frac{1}{2}}$, or 0.01 .

Find the factor required to convert electrostatic capacity from ft -grain-sec and specificinductive capacity 6 units to cgs units. The formula is $[l k]$ in which $l=30.48, k=6$; the factor is $30.48 \times 6$, or 182.88 .

Many of the magnetic quantities are analogues of certain electric quantities. The dimensions of such quantities in the electromagnetic system differ from those of the corresponding electrostatic quantities in the electrostatic system only in the substitution of permeability $\mu$ for $K$.

Conductance is the reciprocal of resistance, and the dimensional formula is [ $L^{-1} T \mu^{-1}$ ].

Conductivity is the quantity of electricity transmitted per unit area per unit potential gradient per unit of time. The dimensional formula is $\left[M^{\frac{1}{2}} L^{\frac{3}{4}} \mu^{-\frac{3}{2}} /\right.$ $\left.L^{2}\left(M^{\frac{1}{2}} L^{\frac{3}{2}} T^{-2} / L\right) T\right]$ or $\left[L^{-2} T \mu^{-1}\right]$.

Current, $I$ (abampere-unit magnetic field, $r=1 \mathrm{~cm}$ ), flowing in circle, radius $r$, creates magnetic field at its center, $2 \pi I / r$. Dimensional formula is product of formulae for magnetic field intensity and length or $\left[M^{3} L^{3} T^{-1} \mu^{-\frac{1}{2}}\right]$.

Electric field intensity is the ratio of electric potential or electromotive force and length. The dimensional formula is $\left[M^{\frac{1}{2}} L^{\frac{1}{2}} T^{-2} \mu^{\frac{1}{2}}\right]$.

Electric potential, or electromotive force (emf) (abvolt-work=1 erg), as in the electrostatic system, is the ratio of work to quantity of electricity. The dimensional formula is [ $M L^{2} T^{-2} / M^{\frac{1}{2}} L^{\frac{1}{2}} \mu^{-\frac{1}{2}}$ ] or $\left[M^{\frac{3}{2}} L^{\frac{3}{2}} T^{-2} \mu^{\frac{1}{2}}\right]$.

Electrostatic capacity is the ratio of quantity of electricity to difference of potential. The dimensional formula is $\left[L^{-1} T^{2} \mu^{-1}\right]$.

Intensity of magnetization ( $I$ ) of any portion of a magnetized body is the ratio of the magnetic moment of that portion and its volume. The dimensional formula is [ $M^{\frac{3}{3}} L^{\frac{1}{2}} T^{-1} \mu^{\frac{3}{2}} / L^{3}$ ] or $\left[M^{\frac{1}{2}} L^{-\frac{1}{2}} T^{-1} \mu^{\frac{1}{3}}\right]$.

Magnetic field strength, magnetic intensity or magnetizing force ( $J$ ) is the ratio of the force on a magnetic pole placed at the point and the magnetic pole strength. The dimensional formula is therefore the ratio of the formulae for a force and magnetic quantity, or $\left[M L T^{-2} / M^{\frac{1}{3}} L^{\frac{1}{2}} T^{-1} \mu^{\frac{2}{2}}\right]$ or $\left[M^{\frac{3}{3}} L^{-\frac{1}{3}} T^{-1} \mu^{-\frac{1}{2}}\right]$.

Magnetic flux ( $\Phi$ ) characterizes the magnetized state of a magnetic circuit. Through a surface enclosing a magnetic pole it is proportional to the magnetic pole strength. The dimensional formula is that for magnetic pole strength.

Magnetic induction $(B)$ is the magnetic flux per unit of area taken perpendicular to the direction of the magnetic flux. The dimensional formula is [ $\left.M^{\frac{1}{2}} L^{\frac{1}{2}} T^{-1} \mu^{\frac{1}{3}} / L^{2}\right]$ or $\left[M^{\frac{1}{3}} L^{-\frac{1}{2}} T^{-1} \mu^{\frac{1}{2}}\right]$.

Magnetic moment $(M)$ is the product of the pole strength by the length of the magnet. The dimensional formula is $\left[M^{\frac{1}{2}} L^{\frac{5}{2}} T^{-1} \mu^{\frac{1}{2}}\right]$.

Magnetic pole strength or quantity of magnetism ( $m$ ) has already been shown to have the dimensional formula [ $M^{\frac{1}{2}} L^{\frac{3}{2}} T^{-1} \mu^{\frac{1}{2}}$ ].

Magnetic potential or magnetomotive force at a point is measured by the work which is required to bring unit quantity of positive magnetism from zero potential to the point. The dimensional formula is the ratio of the formulae for work and magnetic quantity $\left[M L^{2} T^{-2} / M^{\frac{1}{2}} L^{\frac{1}{2}} T^{-1} \mu^{\frac{1}{2}}\right]$ or $\left[M^{\frac{1}{2}} L^{\frac{1}{2}} T^{-1} \mu^{-\frac{3}{2}}\right]$.

Magnetic reluctance is the ratio of magnetic potential difference to magnetic flux. The dimensional formula is $\left[L^{-1} \mu^{-1}\right]$.

Magnetic susceptibility ( $\kappa$ ) is the ratio of intensity of magnetization produced and the intensity of the magnetic field producing it. The dimensional formula is $\left[M^{\frac{3}{4}} L^{-\frac{1}{2}} T^{-1} \mu^{\frac{3}{2}} / M^{\frac{3}{3}} L^{-\frac{1}{3}} T^{-1} \mu^{-\frac{1}{2}}\right]$ or $[\mu]$.

Mutual inductance of two circuits is the electromotive force produced in one per unit rate of variation of the current in the other. The dimensional formula is the same as for self-inductance.

Peltier effect, coefficient of, is measured by the ratio of the quantity of heat and quantity of electricity. The dimensional formula is [ $M L^{2} T^{-2} / M M^{3} L^{3} \mu^{-3}$ ] or $\left[M^{3} L^{3} T^{-2} \mu^{3}\right]$, the same as for electromotive force.

Quantity of electricity is the product of the current and time. The dimensional formula is $\left[M^{3} L^{3} \mu^{-\frac{1}{2}}\right]$.

Resistance of a conductor is the ratio of the difference of potential between its ends and the constant current flowing. The dimensional formula is [ $M^{3} L^{3} T^{-2} \mu^{\frac{3}{3}} / M^{\frac{3}{3}} L^{\frac{3}{2}} T^{-1} \mu^{-\frac{1}{3}}$ ] or $\left[L T^{-1} \mu\right]$.

Resistivity is the reciprocal of conductivity as just defined. The dimensional formula is $\left[L^{2} T^{-1} \mu\right]$.

Self-inductance is for any circuit the electromotive force produced in it by unit rate of variation of the current through it. The dimensional formula is the product of the formulae for electromotive force and time divided by that for current or $\left[M^{\frac{1}{3}} L^{\frac{3}{2}} T^{-2} \mu^{3} \times T \div M^{\frac{1}{3}} L^{\frac{3}{2}} T^{-1} \mu^{-\frac{3}{3}}\right]$ or $[L \mu]$.
Thermoelectric power is measured by the ratio of electromotive force and temperature. The dimensional formula is $\left[M^{\frac{1}{2}} L^{\frac{1}{2}} T^{-\frac{2}{2}} \mu^{\frac{1}{-1}}\right]$.

Exs.-Find the factor required to convert intensity of magnetic field from ft-grain-min units to cgs units. The formula is $\left[m^{\frac{1}{2}} l^{-\frac{1}{2}} t^{-1} \mu^{-\frac{1}{2}}\right] ; m=0.0648, l=30.48, t=60$, and $\mu=1$; the factor is $0.0648^{1} \times 30.48^{-\frac{1}{2}}$, or 0.046108 .

How many cgs units of magnetic moment make one ft-grain-sec unit of the same quantity? The formula is $\left[m^{\frac{1}{1}} l t^{-1} \mu^{\frac{1}{2}}\right] ; m=0.0648 . l=30.48, t=1$, and $\mu=1$; the number is $0.0648^{\frac{1}{2}} \times 30.48^{\frac{5}{2}}$, or 1305.6 .

If the intensity of magnetization of a steel bar is 700 in cgs units, what will it be in mm-mg-sec units? The formula is [ $\left.m^{\frac{1}{2}} l^{\frac{1}{2}} t^{-1} \mu^{\frac{1}{2}}\right] ; m=1000, l=10, t=1, \mu=1$; the intensity is $700 \times 1000^{\frac{1}{2}} \times 10^{\frac{1}{2}}$, or 70000 .

Find the factor required to convert current from cgs units to earth-quadrant-10 $0^{-11}$ gram-sec units. The formula is $\left[m^{\frac{1}{2}} l^{\frac{1}{2}} t^{-1} \mu^{-\frac{1}{2}}\right] ; m=10^{11}, l=10^{-\theta}, \mu=1$; the factor is $10 \stackrel{12}{2} \times 10^{-2}$, or 10 .

Find the factor required to convert resistance expressed in cgs units into the same expressed in earth-quadrant- $10^{-11}$ gram-sec units. The formula is $\left[l t^{-1} \mu\right] ; l=10^{-9}, t=1$, $\mu=1$; the factor is $10^{-0}$.

## TABLE 3.-FUNDAMENTAL STANDARDS

## Part 1.-Selection of fundamental quantities

The choice of the nature of the fundamental quantities already made does not sufficiently define the system for measurements. Some definite unit or arbitrarily chosen standard must next be taken for each of the fundamental quantities. This fundamental standard should have the qualities of permanence, reproducibility, and availability and be suitable for accurate measures. Once chosen and made it is called the primary standard and is generally kept at some central bureau-for instance, the International Bureau of Weights and Measures at Sèvres, France. A primary standard may also be chosen and made for derived units (e.g., the new absolute (1948) ohm standard), when it is simply a standard closely representing the unit and accepted for practical
purposes, its value having been fixed by certain measuring processes. Secondary or reference standards are accurately compared copies, not necessarily duplicates, of the primaries for use in the work of standardizing laboratories and the production of working standards for everyday use.

Standard of length.-The primary standard of length which now almost universally serves as the basis for physical measurements is the meter. It is defined as the distance between two lines at $0^{\circ} \mathrm{C}$ on a platinum-iridium bar deposited at the International Bureau of Weights and Measures. This bar is known as the International Prototype Meter, and its length was derived from the "métre des Archives," which was made by Borda. Borda, Delambre, Laplace, and others, acting as a committee of the French Academy, recommended that the standard unit of length should be the ten-millionth part of the length, from the equator to the pole, of the meridian passing through Paris. In 1795 the French Republic passed a decree making this the legal standard of length, and an arc of the meridian extending from Dunkirk to Barcelona was measured by Delambre and Mechain for the purpose of realizing the standard. From the results of that measurement the meter bar was made by Borda. The meter is now defined as above and not in terms of the meridian length; hence, subsequent measures of the length of the meridian have not affected the length of the meter.

Standard of mass.-The primary standard of mass now almost universally used as the basis for physical measurements is the kilogram. It is defined as the mass of a certain piece of platinum-iridium deposited at the International Bureau of Weights and Measures. This standard is known as the International Prototype Kilogram. Its mass is equal to that of the older standard, the "kilogram des Archives," made by Borda and intended to have the same mass as a cubic decimeter of distilled water at the temperature of $4^{\circ} \mathrm{C}$.

Copies of the International Prototype Meter and Kilogram are possessed by the various governments and are called National Prototypes.

Standard of time.-The unit of time universally used is the mean solar second, or the 86400 th part of the mean solar day. It is based on the average time of one rotation of the earth on its axis relatively to the sun as a point of reference $=1.00273791$ sidereal second.

Standard of temperature.-The standard scale of temperature, adopted by the International Committee of Weights and Measures (1887), depends on the constant-volume hydrogen thermometer. The hydrogen is taken at an initial pressure at $0^{\circ} \mathrm{C}$ of 1 meter of mercury, $0^{\circ} \mathrm{C}$, sea-level at latitude $45^{\circ}$. The scale is defined by designating the temperature of melting ice as $0^{\circ}$ and of condensing steam as $100^{\circ}$ under standard atmospheric pressure.

Thermodynamic (Kelvin) Scale (Centigrade degrees).-Such a scale independent of the properties of any particular substance, and called the thermodynamic, or absolute scale, was proposed in 1848 by Lord Kelvin. The temperature is proportional to the average kinetic energy per molecule of a perfect gas.

International temperature scale.-See Table 37.
Numerically different systems of units.-The fundamental physical quantities which form the basis of a system for measurements have been chosen and the fundamental standards selected and made. Custom has not however
generally used these standards for the measurement of the magnitudes of quantities but rather multiples or submultiples of them. For instance, for very small quantities the micron ( $\mu$ ) or one-millionth of a meter is often used. The following table ${ }^{8}$ gives some of the systems proposed, all built upon the fundamental standards already described. The centimeter-gram-second (cm-g-sec or cgs) system proposed by Kelvin is the only one generally accepted.

Part 2.-Some proposed systems of units

|  | Weber and Gauss | Kelvin cgs | $\begin{gathered} \text { Moon } \\ 1891 \end{gathered}$ | $\begin{aligned} & \text { Giorgi } \\ & \text { MKS } \\ & \text { (Prim. } \\ & \text { Stds.) } \end{aligned}$ | France 1914 | B. A. Com., 1863 | $\begin{aligned} & \text { Practical } \\ & \text { (B. A. } \\ & \text { Com.; } \\ & \text { 1873) } \end{aligned}$ | $\begin{aligned} & \text { Strout } \\ & 1891 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Length | mm | cm | dm | m | m | m | $10^{\circ} \mathrm{cm}$ | $10^{9} \mathrm{~cm}$ |
| Mass | mg | g | Kg | Kg | $10^{6} \mathrm{~g}$ | g | $10^{-11} \mathrm{~g}$ | $10^{-9} \mathrm{~g}$ |
| Time | sec | sec | $\frac{\mathrm{sec}}{10}$ | sec | sec | sec | sec | sec |

Further, the choice of a set of fundamental physical quantities to form the basis of a system does not necessarily determine how that system shall be used in measurements. In fact, upon any sufficient set of fundamental quantities, a great many different systems of units may be built. The electrostatic and electromagnetic systems are really systems of electric quantities rather than units. They were based upon the relationships $F=Q Q^{\prime} / K r^{2}$ and $m n^{\prime} / \mu r^{2}$, respectively. Systems of units built upon a chosen set of fundamental physical quantities may differ in two ways: (1) the units chosen for the fundamental quantities may be different ; (2) the defining equations by which the system is built may be different.

The electrostatic system generally used is based on the centimeter, gram, second, and dielectric constant of a vacuum. Other systems have appeared, differing from this in the first way-for instance using the foot, grain, and second in place of the centimeter, gram, and second. A system differing from it in the second way is that of Heaviside which introduces the factor $4 \pi$ at different places than is usual in the equations. There are similarly several systems of electromagnetic units in use.

Gaussian systems.-"The complexity of the interrelations of the units is increased by the fact that not one of the systems is used as a whole, consistently for all electromagnetic quantities. The 'systems' at present used are therefore combinations of certain of the systems of units."

Some writers ${ }^{9}$ on the theory of electricity prefer to use what is called a Gaussian system, a combination of electrostatic units for purely electrical quantities and electromagnetic units for magnetic quantities. There are two such Gaussian systems in vogue-one a combination of cgs electrostatic and cgs electromagnetic systems, and the other a combination of the two corresponding Heaviside systems.

When a Gaussian system is used, caution is necessary when an equation contains both electric and magnetic quantities. A factor expressing the ratio between the electrostatic and electromagnetic units of one of the quantities has to be introduced. This factor is the first or second power of $c$, the number

[^4]of electrostatic units of electric charge in one electromagnetic unit of the same.
There is sometimes a question as to whether electric current is to be expressed in electrostatic or electromagnetic units, since it has both electric and magnetic attributes. It is usually expressed in electrostatic units in the Gaussian system.

It may be observed from the dimensions of $K$ given in Table 2, part 3, that $[I / K \mu]=\left[L^{2} / T^{2}\right]$ which has the dimensions of a square of a velocity. This velocity was found experimentally to be equal to that of light, when $K$ and $\mu$ were expressed in the same system of units. Maxwell proved theoretically that $1 / \sqrt{K} \mu$ is the velocity of any electromagnetic wave. This was subsequently proved experimentally. When a Gaussian system is used, this equation becomes $c / \sqrt{ } K \mu=\tau^{\prime}$. For the ether $K=1$ in electrostatic units and $\mu=1$ in electromagnetic units. Hence $c=v$ for the ether, or the velocity of an electromagnetic wave in the ether is equal to the ratio of the cgs electromagnetic to the cgs electrostatic unit of electric charge. This constant $c$ is of primary importance in electrical theory. Its most probable value is $2.99776 \times 10^{10}$ centimeters per second.

## Part 3.-Electrical and magnetic units

Absolute ("practical") electromagnetic system (1948).-This electromagnetic system is based upon the units of $10^{9} \mathrm{~cm}, 10^{-11} \mathrm{~g}$, the sec and $\mu$ of the ether. The principal quantities are the resistance unit, the ohm $=10^{9} \mathrm{emu}$ units; the current unit, the ampere $=10^{-1}$ emu units; and the electromotive force unit, the volt $=10^{8}$ emu units. (See Table 6.)

The International electric units.-The units used before January 1, 1948, in practical electrical measurements, however, were the "International Units." They were derived from the "practical" system just described, or as the latter is sometimes called, the "absolute" system. These international units were based upon certain concrete standards that were defined and described. With such standards electrical comparisons can be more accurately and readily made than could absolute measurements in terms of the fundamental units. Two electric units, the international ohm and the international ampere, were chosen and made as nearly equal as possible to the ohm and ampere of the "practical" or "absolute" system. ${ }^{10}$

## QUANTITY OF ELECTRICITY

The unit of quantity of electricity is the coulomb. The faraday is the quantity of electricity necessary to liberate 1 gram equivalent in electrolysis. It is equivalent to 96,488 absolute coulombs (Birge).

Standards.-There are no standards of electric quantity. The silver voltameter may be used for its measurement since under ideal conditions the mass of metal deposited is proportional to the amount of electricity which has flowed.

## CAPACITY

The unit used for capacity is the microfarad or the one-millionth of the farad, which is the capacity of a condenser that is charged to a potential of 1 volt by 1 coulomb of electricity. Capacities are commonly measured by comparison with standard capacities. The values of the standards are determined by

[^5]measurement in terms of resistance and time. The standard is some form of condenser consisting of two sets of metal plates separated by a dielectric. The condenser should be surrounded by a metal shield connected to one set of plates rendering the capacity independent of the surroundings. An ideal condenser would have a constant capacity under all circumstances, with zero resistance in its leads and plates, and no absorption in the dielectric. Actual condensers vary with the temperature, atmospheric pressure, and the voltage, frequency, and time of charge and discharge. A well-constructed air condenser with heavy metal plates and suitable insulating supports is practically free from these effects and is used as a standard of capacity.

Practically, air-condenser plates must be separated by 1 mm or more and so cannot be of great capacity. The more the capacity is increased by approaching the plates, the less the mechanical stability and the less constant the capacity. Condensers of great capacity use solid dielectrics, preferably mica sheets with conducting plates of tinfoil. At constant temperature the best mica condensers are excellent standards. The dielectric absorption is small but not quite zero, so that the capacity of these standards found varies with different methods of measurement, so for accurate results care must be taken.

## INDUCTANCE

The henry, the unit of self-inductance and also the unit of mutual inductance, is the inductance in a circuit when the electromotive force induced in this circuit is 1 volt, while the inducing current varies at the rate of 1 ampere per second.

Inductance standards.-Inductance standards are measured in international units in terms of resistance and time or resistance and capacity by alter-nate-current bridge methods. Inductances calculated from dimensions are in absolute electromagnetic units. The ratio of the international to the absolute henry is the same as the ratio of the corresponding ohms.

Since inductance is measured in terms of capacity and resistance by the bridge method about as simply and as conveniently as by comparison with standard inductances, it is not necessary to maintain standard inductances. They are however of value in magnetic, alternating-current, and absolute electrical measurements. A standard inductance is a circuit so wound that when used in a circuit it adds a definite amount of inductance. It must have either such a form or so great an inductance that the mutual inductance of the rest of the circuit upon it may be negligible. It ustually is a wire coil wound all in the same direction to make self-induction a maximum. A standard, the inductance of which may be calculated from its dimensions, should be a single layer coil of very simple geometrical form. Standards of very small inductance, calculable from their dimensions, are of some simple device, such as a pair of parallel wires or a single turn of wire. With such standards great care must be used that the mutual inductance upon them of the leads and other parts of the circuit is negligible. Any inductance standard should be separated by long leads from the measuring bridge or other apparatus. It must be wound so that the distributed capacity between its turns is negligille; otherwise the apparent inductance will vary with the frequency.

## POWER AND ENERGY

Power and energy, although mechanical and not primarily electrical quantities, are measurable with greater precision by electrical methods than in any
other way. The watt and the electric units were so chosen in terms of the cgs units that the product of the current in amperes by the electromotive force in volts gives the power in watts (for continuous or instantaneous values). The watt is defined as the energy expended per second by an unvarying electric current of 1 ampere under an electric pressure of 1 volt.
Standards and measurements.-No standard is maintained for power or energy. Measurements are always made in electrical practice in terms of some of the purely electrical quantities represented by standards.

## MAGNETIC UNITS

Cgs units are generally used for magnetic quantities. American practice is fairly uniform in names for these units: the cgs unit of magnetomotive force is called the gilbert; magnetic intensity, the oersted; magnetic induction, the gauss; magnetic flux, the maxwell, following the definitions of the American Institute of Electrical Engineers (1894).

Oersted, the cgs emu of magnetic intensity exists at a point where a force of 1 dyne acts upon a unit magnetic pole at that point, i.e., the intensity 1 cm from a unit magnetic pole.

Maxwell, the cgs emu magnetic flux is the flux through a $\mathrm{cm}^{2}$ normal to a field at 1 cm from a unit magnetic pole.

Gauss, the cgs etnu of magnetic induction has such a value that if a conductor 1 cm long moves through the field at a velocity of $1 \mathrm{~cm} / \mathrm{sec}$, length and induction mutually perpendicular, the induced emf is 1 abvolt.
Gilbert, the cgs emu of magnetomotive force is a field such that it requires 1 erg of work to bring a unit magnetic pole to the point.

A unit frequently used is the ampere-turn. It is a convenient unit since it eliminates $4 \pi$ in certain calculations. It is derived from the "ampere turn per cm ." The following table shows the relations between a system built on the ampere-turn and the ordinary magnetic units. ${ }^{11}$
${ }^{11}$ Dellinger, International system of electric and magnetic units, Nat. Bur. Standards Bull., vol. 13, p. 599, 1916.

Part 4.-The ordinary and the ampere-turn magnetic units

| Quantity |  | Ordinary magnetic units | Ampere-turn units | Ordinary units in 1 ampereturn unit |
| :---: | :---: | :---: | :---: | :---: |
| Magnetomotive force | $\mathfrak{F}$ | gilbert | ampere-turn | $4 \pi / 10$ |
| Magnetizing force | H | gilbert per cm | ampere-turn per cm | $4 \pi / 10$ |
| Magnetic flux | $\Phi$ | maxwell | maxwell | 1 |
| Magnetic induction | B | $\left\{\begin{array}{l}\text { maxwell per } \\ \mathrm{cm}^{2} \text { gauss }\end{array}\right.$ | $\left\{\begin{array}{l}\text { maxwell per } \mathrm{cm}^{2} \\ \text { gauss }\end{array}\right.$ | 1 |
| Permeability | $\mu$ |  |  |  |
| Reluctance | $R$ | oersted | $\left\{\begin{array}{l} \text { ampere-turn per } \\ \text { maxwell } \end{array}\right.$ | $4 \pi / 10$ |
| Magnetization intensity | J |  | maxwell per $\mathrm{cm}^{2}$ | $1 / 4 \pi$ |
| Magnetic susceptibility | $\kappa$ |  |  | $1 / 4 \pi$ |
| Magnetic pole strength. | m |  | maxwell | $1 / 4 \pi$ |

In pursuance of a decision of the International Committee on Weights and Measures, the National Bureau of Standards introduced, as of January 1, 1948, revised values of the units of electricity. This consummated a movement, initiated in 1927 by the American Institute of Electrical Engineers, asking that the National Bureau of Standards undertake the additional research necessary in order that the absolute ohm and absolute ampere based on the cgs electromagnetic system and the absolute volt, watt, and other units derived from them could be legalized in place of the international ohm and ampere and their derived units. This work was done, and the magnitude of the old international units in terms of the adopted absolute units is given in Table 5. This means that the electrical units now in use represent, as nearly as it is possible to make them, exact multiples of the cgs emu system, with the numerical relations shown in Table 6. Units of the new system will actually be maintained, as were the old international units, by groups of standard resistors and of standard cells, and consequently the change to be made is most simply represented by stating the relative magnitudes of the ohms and of the volts of the two systems.

During the period of transition to the new units, in order to avoid any doubt as to the units used in giving precise data, the International Committee on Weights and Measures recommended that the abbreviations int. and abs. be used with the names of the electrical units. In a few years this will be unnecessary, except when referring to old data.

The international units were intended to be exact multiples of the units of the centimeter-gram-second electromagnetic system, but to facilitate their reproduction, the ampere, the ohm, and the volt were defined by reference to three physical standards, namely (1) the silver voltameter, (2) a specified column of mercury, and (3) the Clark standard cell. This procedure was recommended by the International Electrical Congress of 1893 in Chicago and was incorporated in an Act of Congress of July 12, 1894. However, modifications of the international system were found to be necessary or expedient for several reasons. The original proposals were not sufficiently specific to give the precision of values that soon came to be required, and the independent definitions of three units brought the system into confict with the customary simple form of Ohm's Law, $I=E / R$. Furthermore, with the establishment of national standardizing laboratories in several of the larger countries, other laboratories no longer needed to set up their own primary standards, and facility of reproduction of those standards became less important than the reliability of the units.

In preparation for the expected change in units, laboratories in several countries made absolute measurements of resistance and of current. The results of these measurements and the magnitudes of the international units as maintained in the national laboratories of France, Great Britain, Germany, Japan, the U.S.S.R., and the United States were correlated by periodic comparisons of standard resistors and of standard cells sent to the International Bureau of Weights and Measures. Nearly all the absolute measurements at the National Bureau of Standards were carried out under the direct supervision of Harvey L. Curtis, and the results of such measurements at the Bureau accepted by the International Committee on Weights and Measures at its meeting in Paris in October 1946 are as follows :

1 mean international ohm $=1.00049$ absolute ohms
1 mean international volt $=1.00034$ absolute volts

[^6]The mean international units to which the above equations refer are the averages of units as maintained in the national laboratories of the six countries (France, Germany, Great Britain, Japan, U.S.S.R., and U.S.A.) which took part in this work before the war. The units maintained by the National Bureau of Standards differ from these average units by a few parts in a million, so that the conversion factors for adjusting values of standards in this country will be as follows:

> 1 mean international ohm U.S. $=1.000495$ absolute ohms
> 1 mean international volt U.S. $=1.000333$ absolute volts

Other electrical units will be changed by amounts shown in Table 5. The factors given should be used in converting values given in international units in National Bureau of Standards certificates to the new absolute system.

## table 5.-RELATIVE MAGNITUDE OF THE OLD INTERNATIONAL ELECTRICAL UNITS AND THE NEW 1948 ABSOLUTE ELECTRICAL UNITS

| 1 mean international ohm | $=1.00049$ absointe ohms |
| :--- | :--- | :--- |
| 1 mean international volt | $=1.00034$ absolute volts |
| 1 international ohm (U.S.) | $=1.00495$ absolute ohms |
| 1 international volt (U.S.) | $=1.00033$ absolute volts |
| 1 international ampere | $=0.999835$ absolute ampere |
| 1 international coulomb | $=0.99835$ absolute coulomb |
| 1 international henry | $=1.000495$ absolute henries |
| 1 international farad | $\equiv 0.999505$ absolute farad |
| 1 international watt | $=1.000165$ absolute watts |
| 1 international joule | $=1.000165$ absolute joules |

## TABLE 6.-RELATIVE VALUES OF THE THREE SYSTEMS OF ELECTRICAL UNITS

| Quantity | Symbol | Absolute unit |  | Electromagnetic system emu |  |  | Electrostatic system * esu |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Current strength |  | 1 ampere | $=$ | $10^{-1}$ | abampere | $=$ | $3 \times 10^{8}$ statampere |
| Potential difference | . E | 1 volt | 二 | $10^{8}$ | abvolts | 二 | $1 / 300$ statvolt |
| Resistance | R | 1 ohm | = | $10^{8}$ | abohms | = | (1/9) $\times 10^{-11}$ statohm |
| Energy | W | 1 joule | = | $10^{7}$ | ergs | = | $10^{7}$ ergs |
| Power | P | 1 watt | = | $10^{7}$ | ergs/sec | $=$ | $10^{7} \mathrm{ergs} / \mathrm{sec}$ |
| Capacitance |  | 1 farad | = | $10^{-8}$ | abfarads | $=$ | $9 \times 10^{11}$ statafarad |
| Inductance |  | 1 henry | $=$ | $10^{9}$ | abhenries | $=$ | $(1 / 9) \times 10^{-11} \text { stata- }$ |
| Charge | Q | 1 coulomb |  |  | abcoulom |  | $3 \times 10^{9}$ statcoulomb |

[^7]TABLE 7.-CONVERSION FACTORS FOR UNITS OF ENERGY *


[^8]Abbreviations: int., international ; emu, electromagnetic units; esu, electrostatic units; cgs, centimeter-gram-second units.

Resistance:
1 international ohm $=$
1.00051 absolute ohms
1.0001 int . ohms (France, before 1911)
1.00016 Board of Trade units (England, 1903)
1.01358 B. A. units
1.00283 "legal ohms" of 1884
1.06300 Siemens units

1 absolute ohm =
0.99949 int. ohms

1 "practical" emu
$10^{\circ} \mathrm{cgs}$ emu
$1.11262 \times 10^{-12}$ cgs esu

## Current:

1 international ampere $=$
0.99995 absolute ampere
1.00084 int. amperes (U. S. before 1911)
1.00130 int. amperes (England, before 1906)
1.00106 int. amperes (England, 190608)
1.00010 int. amperes (England, 190910)
1.00032 int. amperes (Germany, before 1911)
1.0002 int. amperes (France, before 1911)

1 absolute ampere $=$
1.00005 int. amperes

1 "practical" emu
0.1 cgs emu
$2.99776 \times 10^{\circ}$ esu
Electromotive force:
1 international volt =
1.00046 absolute volts
1.00084 int. volts (U. S. before 1911)
1.00130 int. volts (England, before 1906)
1.00106 int. volts (England, 1906-08)
1.00010 int. volts (England, 1909-10)
1.00032 int. volts (Germany, before 1911)
1.00032 int. volts (France, before 1911)

1 absolute volt $=$
0.99954 int. volt

1 "practical" emu
$10^{4}$ cgs emu
0.00333560 cgs esu

Quantity of electricity:
(Same as current equivalents.)
1 international coulomb $=$
1/3600 ampere-hour
1/96494 faraday

## Capacity:

1 international farad= 0.99949 absolute farad

1 absolute farad = 1.00051 int. farads

1 "practical" emu
$10^{-0} \mathrm{cgs} \mathrm{emu}$
$8.98776 \times 10^{11}$ cgs esu

## lnductance:

1 international henry $=$
1.00051 absolute henries

1 absolute henry $=$
0.99949 int. henry

1 "practical" emu
$10^{\circ} \mathrm{emu}$
$1.11262 \times 10^{-12}$ cgs esu
Energy and power:
(standard gravity $=980.665 \mathrm{~cm} / \mathrm{sec}^{-2}$ ) -
1 international joule $=$
1.00041 absolute joules

1 absolute joule $=$
0.99959 int. joule
$10^{7}$ ergs
0.737560 standard foot-pound
0.101972 standard kilogram-meter
$0.277778 \times 10^{-6}$ kilowatt-hour

## Resistivity :

1 ohm- $\mathrm{cm}=0.393700$ ohm-inch
$=10,000$ ohm (meter, $\mathrm{mm}^{2}$ )
$=12.732 .4 \mathrm{ohm}$ (meter, mm )
$=393,700$ microhm-inch
$=1,000,000$ microhm- cm
$=6,015,290 \mathrm{ohm}$ (mil, foot)
$1 \mathrm{ohm}($ meter, gram$)=5710.0 \mathrm{ohm}($ mile, pound)

Magnetic quantities:

| 1 int. gilbert | $=0.99995$ absolute gil- |
| :---: | :---: |
| 1 abso | $=1.00005$ int. gilberts |
| 1 int. maxwell | $\begin{aligned} & =1.00046 \text { absolute } \\ & \text { maxwells } \end{aligned}$ |
| 1 absolute maxwel | $=\begin{aligned} & 0.99954 \text { int. max- } \\ & \text { well } \end{aligned}$ |
| 1 gilbert | $=0.7958$ ampere-turn |
| 1 gilbert per cm | $\begin{aligned} & =0.7958 \text { ampere-turn } \\ & \text { per cm } \\ & =2.021 \text { ampere-turns } \\ & \text { per inch } \end{aligned}$ |
| 1 maxwell | line |
| axwell perc | $=10^{-8}$ volt-second <br> 6.452 maxwells per in. ${ }^{2}$ |

[^9]TABLE 9.-DERIVATIVES AND INTEGRALS

|  | $\int . x^{n} d . x$ | $=\frac{x^{n+1}}{n+1} \text {, unless } n=-1$ |
| :---: | :---: | :---: |
| $d u z=\left(1 \frac{d z}{d x}+2 \cdot \frac{d u}{d x}\right) d x$ | $\int \frac{d . r}{x}$ | $=\log x$ |
| $d \frac{u}{v} \quad=\left(\frac{v \frac{d u}{d \cdot v}-u \frac{d v^{2}}{d v}}{v^{2}}\right) d . r$ | $\int c^{s} d x$ | $=e^{*}$ |
| $d . x^{n} \quad=n \cdot x^{n-1} d x$ | $\int c^{a c^{a x}} d . r$ | $=\frac{1}{a} e^{a s}$ |
| $d f(u)=d \frac{f(u)}{d u} \cdot \frac{d u}{d r} \cdot d x$ | $\int . x^{m m^{\text {cosex }}} d x$ | $=\frac{x^{m} c^{a r}}{a}-\frac{m}{a} \int_{-1}^{m-1} c^{a \alpha x} d x$ |
| $d c^{*} \quad=c^{*} d . r$ | $\int \log x d x$ | $=x \log x-x$ |
| $d c^{a s}=a e^{a x} d x$ | $s_{u} d v$ | $=u v-\int v d u$ |
| ${ }^{2} \log \cdot x=\frac{1}{x} d x$ | $\int(a+b x)^{n} d x$ | $=\frac{(a+b, r)^{n+1}}{(n+1) b}$ |
| $d x^{x} \quad=x^{x}(1+\log$, $x) d . t$ |  |  |
| $d \sin x=\cos x d x$ | $\int\left(a^{2}+x^{2}\right)^{-1} d x$ | $=\frac{1}{a} \tan ^{-1} \frac{x}{a}=\frac{1}{a} \sin ^{-1} \quad \begin{array}{r} x \\ \vee x^{2}+a^{2} \end{array}$ |
| $d \cos x=-\sin x d x$ | $\int\left(a^{2}-x^{2}\right)^{-1} d x$ | $=\frac{1}{2 a} \log \frac{a+x}{a-x}$ |
| $d \tan x=\sec ^{2} x d x$ | $\int\left(a^{2}-x^{2}\right)^{-\frac{4}{4}} d x$ | $=\sin ^{-1} \frac{x}{a}$, or $-\cos ^{-1} \frac{x}{a}$ |
| $d \cot x=-\csc ^{2} x d x$ | $\int x\left(a^{2} \pm x^{2}\right)^{-4} d x$ | $= \pm\left(a^{2} \pm x^{2}\right)^{\text {m }}$ |
| $d \sec x=\tan x \sec x d x$ | $\int \sin ^{2} \cdot x d x$ | $=-\frac{1}{2} \cos x \sin x+\frac{1}{2} x$ |
| $d \csc x=-\cot x \cdot \csc . t d x$ | $\int \cos ^{2} x d x$ | $=\frac{1}{1} \sin x \cos x+\frac{1}{2} x$ |
| $d \sin ^{-1} \cdot x=\left(1-x^{2}\right)^{-4} d x$ | $\int \sin x \cos x d x$ | $=\frac{1}{2} \sin ^{2} x$ |
| $d \cos ^{-1} \cdot x=-\left(1-x^{2}\right)^{-\frac{4}{4}} d x$ | $\int(\sin x \cos x)^{-1} d x$ | $=\log \tan x$ |
| $d \tan ^{-1} \cdot x=\left(1+x^{2}\right)^{-1} d x$ | $\int \tan x d x$ | $=-\log \cos x$ |
| $d \cot ^{-2} x=-\left(1+x^{2}\right)^{-1} d x$ | $\int \tan ^{2} x d x$ | $=\tan x-x$ |
| $d \sec ^{-1} x=x^{-1}\left(x^{2}-1\right)^{-\frac{1}{4}} d x$ | $\int \cot x d x$ | $=\log \sin x$ |
| $d \csc ^{-1} x=-x^{-1}\left(x^{2}-1\right)^{-\frac{1}{4}} d x$ | $\int \cot ^{2} x d x$ | $=-\cot \cdot x-x$ |
| $d \sinh x=\cosh x d x$ | $\int \csc . x d x$ | $=\log \tan \frac{1}{2} x$ |
| $d \cosh x=\sinh x d x$ | $\int x \sin x d x$ | $=\sin x-x \cos x$ |
| $d \tanh \cdot x=\operatorname{sech}^{2} \cdot x d x$ | $\int x \cos x d x$ | $=\cos x+x \sin x$ |
| $d \operatorname{coth} . x=-\operatorname{csch}^{2} x d x$ | $\int \tanh x d x$ | $=\log \cosh x$ |
| $d \operatorname{sech} x=-\operatorname{sech} x \tanh . x d x$ | $\int \operatorname{coth} x d x$ | $=\log \sinh x$ |
| $d \operatorname{csch} x=-\operatorname{csch} x^{*} \operatorname{coth} x d x$ | $\int \operatorname{sech} x d x$ | $=2 \tan ^{-1} c^{x}=g d u$ |
| $d \sinh ^{-1} x=\left(x^{2}+1\right)^{-\frac{4}{4}} d x$ | $\int \operatorname{csch} x d x$ | $=\log \tanh \frac{x}{2}$ |
| $d \cosh ^{-1} x=\left(x^{2}-1\right)^{-\frac{4}{4}} d x$ | $\int x \sinh x d x$ | $=r \cosh x-\sinh x$ |
| $d \tanh ^{-1} x=\left(1-x^{2}\right)^{-1} d x$ | $\int . x \cosh x d x$ | $=x \sinh x-\cosh x$ |
| $d \operatorname{coth}^{-1} x=\left(1-x^{2}\right)^{-1} d x$ | $\int \sinh ^{2} x d x$ | $=\frac{1}{2}(\sinh x \cosh x-x)$ |
| $d \operatorname{sech}^{-1} x=-x^{-1}\left(1-x^{2}\right)^{-\frac{1}{4}} d . r$ | $\int \cosh ^{2} x d x$ | $\left.=\frac{1}{(\sinh } x \cosh x+x\right)$ |
| $d \operatorname{csch}^{-1} x=-x^{-1}\left(x^{2}+1\right)^{-4} d x$ | $\int \sinh x \cosh x d x$ | $=\cosh (2 x)$ |

$$
\begin{align*}
& (x+y)^{n}=x^{n}+\frac{x}{1} x^{n-1} y+\frac{n(n-1)}{2!} x^{n-2} y^{2}+\ldots \\
& \frac{n(n-1) \ldots(n-m+1)}{m!} x^{n-m} y^{m}+\ldots \quad\left(y^{2}<x^{2}\right) \\
& (1 \pm x)^{n}=1 \pm n x+\frac{n(n-1) x^{2}}{2!} \pm \frac{n(n-1)(n-2) x^{2}}{3!}+\ldots+ \\
& \frac{( \pm 1)^{k} n!x^{k}}{(n-k)!k!}+\ldots\left(x^{2}<1\right) \\
& (1 \pm x)^{-n}=1 \mp n x+\frac{n(n+1)}{2!} x^{2} \mp \frac{n(n+1)(n+2) x^{8}}{3!}+\cdots \\
& (\mp 1)^{k} \frac{(n+k-1) x^{k}}{(n-1)!k!}+\ldots\left(x^{2}<1\right) \\
& \begin{array}{l}
(1 \pm x)^{-1}=1 \mp x+x^{2} \mp x^{3}+x^{4} \mp x^{5}+\ldots \\
(1 \pm x)^{-2}=1 \mp 2 x+3 x^{2} \mp 4 x^{3}+5 x^{4} \mp 6 \lambda^{5}+\ldots \\
f(x+h)=f(x)+h f^{\prime}(x)+\frac{h^{2}}{2!} f^{\prime \prime}(x)+\ldots+\frac{h^{n}}{n!} f^{(n)}(x)+\ldots
\end{array}  \tag{2}\\
& f(x)=f(0)+\frac{x}{1} f^{\prime}(o)+\frac{x^{2}}{2!} f^{\prime \prime}(0)+\ldots \frac{x^{n}}{n!} f^{(n)}(o)+\ldots \\
& e=\lim \left(1+\frac{1}{n}\right)^{n}=1+\frac{1}{1!}+\frac{1}{2!}+\frac{1}{3!}+\frac{1}{4!}+\ldots \\
& e^{x}=1+x+\frac{x^{2}}{2!}+\frac{x^{3}}{3!}+\frac{x^{4}}{4!}+\ldots  \tag{2}\\
& a^{x}=1+x \log a+\frac{(x \log a)^{2}}{2!}+\frac{(x \log a)^{3}}{3!}+\ldots  \tag{2}\\
& \log x=\frac{x-1}{x}+\frac{1}{2}\left(\frac{x-1}{x}\right)^{2}+\frac{1}{3}\left(\frac{x-1}{x}\right)^{3}+\ldots  \tag{1}\\
& =(x-1)-\frac{1}{2}(x-1)^{2}+\frac{1}{3}(x-1)^{3}-\ldots  \tag{2>x>0}\\
& =2\left[\frac{x-1}{x+1}+\frac{1}{3}\left(\frac{x-1}{x+1}\right)^{3}+\frac{1}{5}\left(\frac{x-1}{x+1}\right)^{5}+\ldots .\right]  \tag{x>0}\\
& \text { ( } x^{2}<1 \text { ) } \\
& \text { Taylor's } \\
& \text { series } \\
& \log (1+x)=x-\frac{1}{2} x^{2}+\frac{1}{3} x^{2}-\frac{1}{4} x^{4}+\ldots .  \tag{2}\\
& \sin x=\frac{1}{2 i}\left(e^{1 x}-e^{-1 x}\right)=x-\frac{x^{3}}{3!}+\frac{x^{5}}{5!}-\frac{x^{7}}{7!}+\ldots \\
& \cos x=\frac{1}{2}\left(e^{4 x}+e^{-4 x}\right)=1-\frac{x^{2}}{2!}+\frac{x^{4}}{4!}-\frac{x^{6}}{6!}+\ldots=1-\mathrm{versin} x \\
& \tan x=x+\frac{x^{3}}{3}+\frac{2 x^{5}}{15}+\frac{17 x^{7}}{315}+\frac{62}{2835} x^{0}+\ldots \\
& \left(x^{2}<\frac{\pi^{2}}{4}\right) \\
& \left(x^{2}<1\right)  \tag{2}\\
& =\frac{\pi}{2}-\frac{1}{x}+\frac{1}{3 x^{3}}-\frac{1}{5 x^{5}}+\ldots  \tag{2}\\
& \sinh x=\frac{1}{2}\left(e^{x}-e^{-x}\right)=x+\frac{x^{3}}{3!}+\frac{x^{5}}{5!}+\frac{x^{7}}{7!}+\cdots  \tag{2}\\
& \cosh x=\frac{1}{2}\left(e^{x}+e^{-x}\right)=1+\frac{x^{2}}{2!}+\frac{x^{4}}{4!}+\frac{x^{0}}{6!}+\ldots  \tag{2}\\
& \text { (continued) }
\end{align*}
$$

$$
\begin{aligned}
& \tanh x=x-\frac{1}{3} x^{3}+\frac{2}{15} x^{5}-\frac{17}{315} x^{7}+\ldots \\
& \left(x^{2}<\frac{1}{4} \pi^{2}\right) \\
& \sinh ^{-1} x=x-\frac{1}{2} \frac{x^{3}}{3}+\frac{1}{2} \cdot \frac{3}{4} \cdot \frac{x^{-5}}{5}-\frac{1}{2} \cdot \frac{3}{4} \cdot \frac{5}{6} \frac{x^{7}}{7}+\ldots \\
& \left(x^{2}<1\right) \\
& =\log 2 . x+\frac{1}{2} \frac{1}{2 \cdot r^{2}}-\frac{1}{2} \frac{3}{4} \frac{1}{4 \cdot x^{4}}+\frac{1}{2} \frac{3}{4} \frac{5}{6} \frac{1}{6 x^{0}}-\ldots \\
& \left(x^{2}>1\right) \\
& \cosh ^{-1} x=\log 2 x-\frac{1}{2} \frac{1}{2 x^{2}}-\frac{1}{2} \frac{3}{4} \frac{1}{4 x^{4}}-\frac{1}{2} \frac{3}{4} \frac{5}{6} \frac{1}{6 x^{0}}-\ldots \\
& \tanh ^{-1} x=x+\frac{1}{3} x^{3}+\frac{1}{5} x^{5}+\frac{1}{7} x^{7}+\ldots \\
& \left(x^{2}<1\right) \\
& \operatorname{gd} x=\phi=x-\frac{1}{6} \cdot x^{3}+\frac{1}{24} x^{5}-\frac{61}{5040} x^{7}+\ldots \\
& \text { ( } x \text { small) } \\
& =\frac{\pi}{2}-\operatorname{sech} . x-\frac{1}{2} \frac{\operatorname{sech}^{3} x}{3}-\frac{1}{2} \frac{3}{4} \frac{\operatorname{sech}^{5} x}{5}-\ldots
\end{aligned}
$$

$$
\begin{aligned}
& \text { ( } x \text { large) } \\
& \left(\phi<\frac{\pi}{2}\right) \\
& f(x)=\frac{1}{2} b_{0}+b_{1} \cos \frac{\pi \cdot x}{c}+b_{2} \cos \frac{2 \pi \cdot x}{c}+\ldots \\
& +a_{1} \sin \frac{\pi x}{c}+a_{2} \cos \frac{2 \pi x}{c}+\ldots(-c<x<c) \\
& a_{m}=\frac{1}{c} \int-{ }_{c}^{+} f(x) \sin \frac{m \pi x}{c} d x \\
& b_{\mathrm{m}}=\frac{1}{c} \int-c \quad+(x) \cos \frac{m \pi x}{c} d x
\end{aligned}
$$

## TABLE 11.-MATHEMATICAL CONSTANTS

| $c=2.7182818285$ | $\begin{gathered} \text { Numbers } \\ \pi=3.1415926536 \end{gathered}$ | $\begin{gathered} \text { Logarithms } \\ 0.4971498727 \end{gathered}$ |
| :---: | :---: | :---: |
| $c^{-1}=0.3678794412$ | $\pi^{2}=9.8696044011$ | 0.9942997454 |
| $M=\log _{10}{ }^{2}=0.4342944819$ | $\frac{1}{\pi}=0.3183098862$ | 9.5028501273 |
| $(M)^{-1}=\log _{e} 10=2.3025850930$ | $\checkmark \pi=1.7724538509$ | 0.2485749363 |
| $\log _{10} \log _{10} 0=9.6377843113$ | $\frac{\mathrm{V} \pi}{2}=0.8862269255$ | 9.9475449407 |
| $\log _{10} 2=0.3010299957$ | $\frac{1}{V \pi}=0.5641895835$ | 9.7514250637 |
| $\log _{e} 2=0.6931471806$ | $\frac{2}{V \pi}=1.1283791671$ | 0.0524550593 |
| $\log _{10 .} \mathrm{r}=\mathrm{M} \cdot \log _{\text {e }} . \mathrm{x}$ | $\sqrt{ } \frac{\pi}{2}=1.2533141373$ | 0.0980599385 |
| $\log _{B} x=\log _{e} x \cdot \log _{B} C$ | $\sqrt{\frac{2}{\pi}}=0.7978845608$ | 9.9019400615 |
| $=\log _{e} x \div \log _{e} B$ | $\frac{\pi}{4}=0.7853981634$ | 9.8950898814 |
| $\log _{e} \pi=1.1447298858$ | $\frac{\vee \pi}{4}=0.4431134627$ | 9.6465149450 |
| $\rho=0.4769362762$ * |  | 0.6220886093 |
| $\log \rho=9.6784603565$ | $\frac{c}{\sqrt{2 \pi}}=1.0844375514$ | 0.0352045477 |

* Probable error, modulus of precision.

Part 1.-Numerical

| $n$ |  |  | $\frac{1}{n}$ |  |  | $n:=1.2 .3 .4 \ldots n$ |  |  |  | n |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1. |  |  |  |  |  |  |  | 1 | 1 |
| 2 | 0.5 |  |  |  |  |  |  |  |  | 2 |
| 3 | . 16666 | 66666 | 66666 | 66666 | 66667 |  |  |  | 6 | 3 |
| 4 | . 04166 | 66666 | 66666 | 66666 | 66667 |  |  |  | 24 | 4 |
| 5 | . 00833 | 33333 | 33333 | 33333 | 33333 |  |  |  | 120 | 5 |
| 6 | 0.00138 | 88888 | 88888 | 88888 | 88889 |  |  |  | 720 | 6 |
| 7 | . 00019 | 84126 | 98412 | 69841 | 26984 |  |  |  | 5040 | 7 |
| 8 | . 00002 | 48015 | 87301 | 58730 | 15873 |  |  |  | 40320 | 8 |
| 9 | . 00000 | 27557 | 31922 | 39858 | 90653 |  |  | 3 | 62880 | 9 |
| 10 | . 00000 | 02755 | 73192 | 23985 | 89065 |  |  | 36 | 28800 | 10 |
| 11 | 0.00000 | 00250 | 52108 | 38544 | 17188 |  |  | 399 | 16800 | 11 |
| 12 | . 00000 | 00020 | 87675 | 69878 | 68099 |  |  | 4790 | 01600 | 12 |
| 13 | . 00000 | 00001 | 60590 | 43836 | 82161 |  |  | 62270 | 20800 | 13 |
| 14 | . 00000 | 00000 | 11470 | 74559 | 77297 |  | 8 | 71782 | 91200 | 14 |
| 15 | . 00000 | 00000 | 00764 | 71637 | 31820 |  | 130 | 76743 | 68000 | 15 |
| 16 | 0.00000 | 00000 | 00047 | 79477 | 33239 |  | 2092 | 27898 | 88000 | 16 |
| 17 | . 00000 | 00000 | 00002 | 81145 | 72543 |  | 35568 | 74280 | 96000 | 17 |
| 18 | . 00000 | 00000 | 00000 | 15619 | 20697 | 6 | 40237 | 37057 | 28000 | 18 |
| 19 | . 00000 | 00000 | 00000 | 00822 | 06352 | 121 | 64510 | 04088 | 32000 | 19 |
| 20 | . 00000 | 00000 | 00000 | 00041 | 10318 | 2432 | 90200 | 81766 | 40000 | 20 |

## Part 2.-Logarithmic

Logarithms of the products $1.2 .3 . \ldots . . . n, n$ from 1 to 100.

| $n$ | $\log (n)$ ) | $n$ | $\log (n!)$ | $n$ | $\log (n)$ ) | $n$ | $\log (n)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.000000 | 26 | 26.605619 | 51 | 66.190645 | 76 | 111.275425 |
| 2 | 0.301030 | 27 | 28.036983 | 52 | 67.906648 | 77 | 113.161916 |
| 3 | 0.778151 | 28 | 29.484141 | 53 | 69.630924 | 78 | 115.054011 |
| 4 | 1.380211 | 29 | 30.946539 | 54 | 71.363318 | 79 | 116.951638 |
| 5 | 2.079181 | 30 | 32.423660 | 55 | 73.103681 | 80 | 118.854728 |
| 6 | 2.857332 | 31 | 33.915022 | 56 | 74.851869 | 81 | 120.763213 |
| 7 | 3.702431 | 32 | 35.420172 | 57 | 76.607744 | 82 | 122.677027 |
| 8 | 4.605521 | 33 | 36.938686 | 58 | 78.371172 | 83 | 124.596105 |
| 9 | 5.559763 | 34 | 38.470165 | 59 | 80.142024 | 84 | 126.520384 |
| 10 | 6.559763 | 35 | 40.014233 | 60 | 81.920175 | 85 | 128.449803 |
| 11 | 7.601156 | 36 | 41.570535 | 61 | 83.705505 | 86 | 130.384301 |
| 12 | 8.680337 | 37 | 43.138737 | 62 | 85.497896 | 87 | 132.323821 |
| 13 | 9.794280 | 38 | 44.718520 | 63 | 87.297237 | 88 | 134.268303 |
| 14 | 10.940408 | 39 | 46.309585 | 64 | 89.103417 | 89 | 136.217693 |
| 15 | 12.116500 | 40 | 47.911645 | 65 | 90.916330 | 90 | 138.171936 |
|  | 13.320620 | 41 | 49.524429 | 66 | 92.735874 | 91 | 140.130977 |
| 17 | 14.551069 | 42 | 51.147678 | 67 | 94.561949 | 92 | 142.094765 |
| 18 | 15.806341 | 43 | 52.781147 | 68 | 96.394458 | 93 | 144.063248 |
| 19 | 17.085095 | 44 | 54.424599 | 69 | 98.233307 | 94 | 146.036376 |
| 20 | 18.386125 | 45 | 56.077812 | 70 | 100.078405 | 95 | 148.014099 |
| 21 | 19.708344 | 46 | 57.740570 | 71 | 101.929663 | 96 | 149.996371 |
| 22 | 21.050767 | 47 | 59.412668 | 71 | 103.786996 | 97 | 151.983142 |
| 23 | 22.412494 | 48 | 61.093909 | 73 | 105.650319 | 98 | 153.974368 |
| 24 | 23.792706 | 49 | 62.784105 | 74 | 107.519550 | 99 | 155.970004 |
| 25 | 25.190646 | 50 | 64.483075 | 75 | 109.394612 | 100 | 157.970004 |

## TABLE 13.-FORMULAS FOR MOMENTS OF INERTIA, RADII OF GYRATION, AND WEIGHTS OF VARIOUS SHAPED SOLIDS

In each case the axis is supposed to traverse the center of gravity of the body. The axis is one of symmetry. The mass of a unit of volume is 2 e.

| Splacre of radius $r$ Roly | Diameter | $\begin{aligned} & \text { Weight } \\ & \frac{4 \pi z c r^{3}}{3} \end{aligned}$ | Moment of $\frac{8 \pi \text { r }^{5}}{15}$ | Square of radius of gyration $\rho_{0}{ }^{2}$ $\frac{2 r^{2}}{5}$ |
| :---: | :---: | :---: | :---: | :---: |
| Spheroid of revolution, pular axis $2 n$, erpuatorial diametcr $2 r$ | Polar axis | $\frac{4 \pi z e a r^{2}}{3}$ | $\frac{8 \pi z e a r}{}{ }^{4}$ | $\frac{2 r^{2}}{5}$ |
| Fllipsoid, axis $2 a, 2 b, 2 c .$. | Axis $2 a$ | $\frac{4 \pi z e a b c}{3}$ | $\frac{4 \pi \text { acalce }\left(h^{2}+c^{2}\right)}{15}$ | $\frac{b^{2}+c^{2}}{5}$ |
| Spherical shell, external radints $r$, internal $r^{\prime}$........ | 1)iameter | $\frac{4 \pi r^{\prime}\left(r^{3}-r^{\prime 3}\right)}{3}$ | $\frac{8 \pi z c^{\prime}\left(r^{5}-r^{\prime 5}\right)}{15}$ | $\frac{2\left(r^{5}-r^{\prime 5}\right)}{5\left(r^{3}-r^{13}\right)}$ |
| Ditto, insensibly thin, radius $r$, thickness $d r$.. | 1)iameter | $4 \pi 2 w r^{2} d r$ | $\frac{8 \pi z u r^{4} d r}{3}$ | $\frac{2 r^{2}}{3}$ |
| Circular cylinder, length $2 a$, radius $r$ | Longitudinal axis $2 a$ | $2 \pi z 6 a r^{2}$ | $\pi z<a{ }^{4}$ | $\frac{r^{2}}{2}$ |
| Elliptic culinder, length $2 u$, transverse axes $26,2 c$. | Longitudinal axis $2 a$ | $2 \pi z{ }^{\text {a }}$ abc | $\frac{\pi r e a b c}{} \frac{\left.b^{2}+c^{2}\right)}{2}$ | $\frac{b^{2}+c^{2}}{4}$ |
| Hollow circular cylinder. length $2 a$, external radius $r$, internal $r^{\prime} \ldots \ldots$. | Longitudinal axis $2 a$ | $2 \pi z \mathrm{ca}\left(r^{2}-r^{\prime 2}\right)$ | $\pi 2800\left(r^{4}-r^{\prime 4}\right)$ | $\frac{r^{2}+r^{\prime 2}}{2}$ |
| Ditto, insensibly thin, thickness $d r$ | Longitudinal axis $2 a$ | $4 \pi z c^{\prime} a r d r$ | $4 \pi z \operatorname{car}^{3} d r$ | $r^{2}$ |
| Circular cylinder, length $2 a$, radius $r$ | Transverse diameter | $2 \pi z \cdots a r^{2}$ | $\frac{\pi \tau \mathrm{c} a r^{2}\left(3 r^{2}+4 a^{2}\right)}{6}$ | $\frac{r^{2}}{4}+\frac{a^{2}}{3}$ |
| Elliptic cylinder, length $2 a$ transwerse axes $2 a, 2 h$.. | Transverse axis 2h | $2 \pi z c a b c$ | $\frac{\text { Tuialic }\left(3 c^{2}+4 a^{2}\right)}{6}$ | $\frac{c^{2}}{4}+\frac{a^{2}}{3}$ |
| Hollow circular cylinder, length $2 a$, external radius $r$. internal $r^{\prime}$....... | Transverse diameter | $2 \pi z \sim a\left(r^{2}-r^{\prime 2}\right)$ | $\frac{\pi \tau i^{\prime} a}{6}\left\{\begin{array}{c} 3\left(r^{4}-r^{\prime 4}\right) \\ +4 a^{2}\left(r^{2}-r^{\prime 2}\right) \end{array}\right\}$ | $\frac{r^{2}+r^{\prime 2}}{4}+\frac{a^{2}}{3}$ |
| Ditto, insensibly thin, thickness $d r$ | Transverse diameter | $4 \pi z c a r d r$ | $\pi z e a\left(2 r^{3}+\frac{4}{3} a^{2} r\right) d r$ | $\frac{r^{2}}{2}+\frac{a^{2}}{3}$ |
| Rectangular prism, dimensions $2 a, 2 l, 2 c \ldots \ldots \ldots$ | Axis $2 a$ | 8uabc | $\frac{\left.8 a c a l c(1)^{2}+c^{2}\right)}{3}$ | $\frac{b^{2}+c^{2}}{3}$ |
| Rhombic prism, length $2 a$, diagonals $2 k, 2 c, \ldots .$. | Axis $2 a$ | treabc | $\frac{2 \text { zeabc }\left(b^{2}+c^{2}\right)}{3}$ | $\frac{b^{2}+c^{2}}{6}$ |
| Ditto | Diagonal 2b, | 4reabc | $\frac{2 \text { acalc }\left(c^{2}+2 a^{2}\right)}{3}$ | $\frac{c^{2}}{6}+\frac{a^{2}}{3}$ |

Fur further mathematical data see Smithsonian Mathematical Tables, Becker and Van Orstrand (Hyperbolic. Circular and Exponential Functions) ; Smithsonian Mathematical Formulae and Tables of Flliptic Functions, Adans and Hippisley; Smithsonian Elliptic Functions Tables, Spenceley; Sunithsonian Logarithmic Tables, Spenceley and Epperson; Functionentafeln, Jahnke und Emde (xtgx, $\mathrm{x}^{-1} \mathrm{tgx}$, Roots of Transcondental Equations, $a+b i$ and $r e^{\rho^{i}}$, Exponentials, Hyperbolic Functions,
$\int_{0}^{x} \frac{\sin u}{u} d u, \int_{x}^{x} \frac{\cos u}{u} d u, \int_{2}^{-x} \frac{c^{-u}}{u} d u$, Fresnel Integral, Gamma Function, Gauss Integral $\frac{2}{\sqrt{\pi}} \int_{0}^{x} c^{-x^{3}} d x$, Pearson Function $c^{-3 \pi \nu} \int_{0}^{\pi} \sin ^{r} e^{\nu x} d x$, Elliptic Integrals and Functions, Spherical and Cylindrical Functions, etc.). For further references see under Tables, Mathematical, in the 16th ed. Encyclopædia Britannica. See also Carr's Synopsis of Pure Mathematics and Mellor's Higher Mathematics for Students of Chemistry and Physics.

|  |  |  |  |  |  |  |  |  |  |  | P. P. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 | 2 | 3 | 4 | 5 |
| 10 | 0000 | 0043 | 0086 | 0128 | 0170 | 0212 | 0253 | 0294 | 0334 | 0374 | 4 | 8 | 12 | 17 | 21 |
| 11 | 0414 | 0453 | 0492 | 0531 | 0569 | 0607 | 0645 | 0682 | 0719 | 0755 | 4 | 8 | 11 | 15 | 19 |
| 12 | 0792 | 0828 | 0864 | 0899 | 0934 | 0969 | 1004 | 1038 | 1072 | 1106 | 3 | 7 | 10 | 14 | 17 |
| 13 | 1139 | 1173 | 1206 | 1239 | 1271 | 1303 | 1335 | 1367 | 1399 | 1430 | 3 | 6 | 10 | 13 | 16 |
| 14 | 1461 | 1492 | 1523 | 1553 | 1584 | 1614 | 1644 | 1673 | 1703 | 1732 | 3 | 6 | 9 | 12 | 15 |
| 15 | 1761 | 1790 | 1818 | 1847 | 1875 | 1903 | 1931 | 1959 | 1987 | 2014 | 3 | 6 | 8 | 11 | 14 |
| 16 | 2041 | 2068 | 2095 | 2122 | 2148 | 2175 | 2201 | 2227 | 2253 | 2279 | 3 | 5 | 8 | 11 | 13 |
| 17 | 2304 | 2330 | 2355 | 2380 | 2405 | 2430 | 2455 | 2480 | 2504 | 2529 | 2 | 5 | 7 | 10 | 12 |
| 18 | 2553 | 2577 | 2601 | 2625 | 2648 | 2672 | 2695 | 2718 | 2742 | 2765 | 2 | 5 | 7 | 9 | 12 |
| 19 | 2788 | 2810 | 2833 | 2856 | 2878 | 2900 | 2923 | 2945 | 2967 | 2989 | 2 | 4 | 7 | 9 | 11 |
| 20 | 3010 | 3032 | 3054 | 3075 | 3096 | 3118 | 3139 | 3160 | 3181 | 3201 | 2 | 4 | 6 | 8 | 11 |
| 21 | 3222 | 3243 | 3263 | 3284 | 3304 | 3324 | 3345 | 3365 | 3385 | 3404 | 2 | 4 | 6 | 8 | 10 |
| 22 | 3424 | 3444 | 3464 | 3483 | 3502 | 3522 | 3541 | 3560 | 3579 | 3598 | 2 | 4 | 6 | 8 | 10 |
| 23 | 3617 | 3636 | 3655 | 3674 | 3692 | 3711 | 3729 | 3747 | 3766 | 3784 | 2 | 4 | 5 | 7 |  |
| 24 | 3802 | 3820 | 3838 | 3856 | 3874 | 3892 | 3909 | 3927 | 3945 | 3962 | 2 | 4 | 5 | 7 | 9 |
| 25 | 3979 | 3997 | 4014 | 4031 | 4048 | 4055 | 4082 | 4099 | 4116 | 4133 | 2 | 3 | 5 | 7 | 9 |
| 26 | 4150 | 4166 | 4183 | 4200 | 4216 | 4232 | 4249 | 4265 | 4281 | 4298 | 2 | 3 | 5 | 7 | 8 |
| 27 | 4314 | 4330 | 4346 | 4362 | 4378 | 4393 | 4409 | 4425 | 4440 | 4456 | 2 | 3 | 5 | 6 | 8 |
| 28 | 4472 | 4487 | 4502 | 4518 | 4533 | 4548 | 4564 | 4579 | 4594 | 4609 | 2 | 3 | 5 | 6 | 8 |
| 29 | 4624 | 4639 | 4654 | 4669 | 4683 | 4698 | 4713 | 4728 | 4742 | 4757 | 1 | 3 | 4 | 6 | 7 |
| 30 | 4771 | 4786 | 4800 | 4814 | 4829 | 4843 | 4857 | 4871 | 4886 | 4900 | , | 3 | 4 | 6 | 7 |
| 31 | 4914 | 4928 | 4942 | 4955 | 4969 | 4983 | 4997 | 5011 | 5024 | 5038 | 1 | 3 | 4 | 6 | 7 |
| 32 | 5051 | 5065 | 5079 | 5092 | 5105 | 5119 | 5132 | 5145 | 5159 | 5172 | 1 | 3 | 4 | 5 | 7 |
| 33 | 5185 | 5198 | 5211 | 5224 | 5237 | 5250 | 5263 | 5276 | 5289 | 5302 | 1 | 3 | 4 | 5 | 6 |
| 34 | 5315 | 5328 | 5340 | 5353 | 5366 | 5378 | 5391 | 5403 | 5416 | 5428 | 1 | 3 | 4 | 5 | 6 |
| 35 | 5441 | 5453 | 5465 | 5478 | 5490 | 5502 | 5514 | 5527 | 5539 | 5551 | 1 | 2 | 4 | 5 | 6 |
| 36 | 5563 | 5575 | 5587 | 5589 | 5611 | 5623 | 5635 | 5647 | 5658 | 5670 | 1 | 2 | 4 | 5 |  |
| 37 | 5682 | 5694 | 5705 | 5717 | 5729 | 5740 | 5752 | 5763 | 5775 | 5786 | 1 | 2 | 3 | 5 | 6 |
| 38 | 5798 | 5809 | 5821 | 5832 | 5843 | 5855 | 5866 | 5877 | 5888 | 5899 | 1 | 2 | 3 | 5 | 6 |
| 39 | 5911 | 5922 | 5933 | 5944 | 5955 | 5966 | 5977 | 5988 | 5999 | 6010 | 1 | 2 | 3 | 4 | 6 |
| 40 | 6021 | 6031 | 6042 | 6053 | 6064 | 6075 | 6085 | 6096 | 6107 | 6117 | 1 | 2 | 3 | 4 | 5 |
| 41 | 6128 | 6138 | 6149 | 6160 | 6170 | 6180 | 6191 | 6201 | 6212 | 6222 | 1 | 2 | 3 | 4 | 5 |
| 42 | 6232 | 6243 | 6253 | 6263 | 6274 | 6284 | 6294 | 6304 | 6314 | 6325 | 1 | 2 | 3 | 4 | 5 |
| 43 | 6335 | 6345 | 6355 | . 6365 | 6375 | 6385 | 6395 | 6405 | 6415 | 6425 | 1 | 2 | 3 | 4 | 5 |
| 44 | 6435 | 6444 | 6454 | 6464 | 6474 | 6484 | 6493 | 6503 | 6513 | 6522 | 1 | 2 | 3 | 4 | 5 |
| 45 | 6532 | 6542 | 6551 | 6561 | 6571 | 6580 | 6590 | 6599 | 6609 | 6618 | 1 | 2 | 3 | 4 | 5 |
| 46 | 6628 | 6637 | 6646 | 6656 | 6665 | 6675 | 6684 | 6693 | 6702 | 6712 | 1 | 2 | 3 | 4 | 5 |
| 47 | 6721 | 6730 | 6739 | 6749 | 6758 | 6767 | 6776 | 6785 | 6794 | 6803 | 1 | 2 | 3 | 4 | 5 |
| 48 | 6812 | 6821 | 6830 | 6839 | 6848 | 6857 | 6866 | 6875 | 6884 | 6893 | 1 | 2 | 3 | 4 | 4 |
| 49 | 6902 | 6911 | 6920 | 6928 | 6937 | 6946 | 6955 | 6964 | 6972 | 6981 | 1 | 2 | 3 | 4 | 4 |
| 50 | 6990 | 6998 | 7007 | 7016 | 7024 | 7033 | 7042 | 7050 | 7059 | 7067 | 1 | 2 | 3 | 3 | 4 |
| 51 | 7076 | 7084 | 7093 | 7101 | 7110 | 7118 | 7126 | 7135 | 7143 | 7152 | 1 | 2 | 3 | 3 | 4 |
| 52 | 7160 | 7168 | 7177 | 7185 | 7193 | 7202 | 7210 | 7218 | 7226 | 7235 | 1 | 2 | 2 | 3 | 4 |
| 53 | 7243 | 7251 | 7259 | 7267 | 7275 | 7284 | 7292 | 7300 | 7308 | 7316 | 1 | 2 | 2 | 3 | 4 |
| 54 | 7324 | 7332 | 7340 | 7348 | 7356 | 7364 | 7372 | 7380 | 7388 | 7396 | 1 | 2 | 2 | 3 | 4 |
|  |  |  |  |  |  | (cont | inued) |  |  |  |  |  |  |  |  |


|  |  |  |  |  |  |  |  |  |  |  | P. P. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 | 2 | 3 | 4 | 5 |
| 55 | 7404 | 7412 | 7419 | 7427 | 7435 | 7443 | 7451 | 7459 | 7466 | 7474 | 1 | 2 | 2 | 3 | 4 |
| 56 | 7482 | 7490 | 7497 | 7505 | 7513 | 7520 | 7528 | 7536 | 7543 | 7551 | 1 | 2 | 2 | 3 | 4 |
| 57 | 7559 | 7566 | 7574 | 7582 | 7589 | 7597 | 7604 | 7612 | 7619 | 7627 | 1 | 2 | 2 | 3 | 4 |
| 58 | 7634 | 7642 | 7649 | 7657 | 7664 | 7672 | 7679 | 7686 | 7694 | 7701 | 1 | I | 2 | 3 | 4 |
| 59 | 7709 | 7716 | 7723 | 7731 | 7738 | 7745 | 7752 | 7760 | 7767 | 7774 | 1 | 1 | 2 | 3 | 4 |
| 60 | 7782 | 7789 | 7796 | 7803 | 7810 | 7818 | 7825 | 7832 | 7839 | 7846 | 1 | 1 | 2 | 3 | 4 |
| 61 | 7853 | 7860 | 7868 | 7875 | 7882 | 7889 | 7896 | 7903 | 7910 | 7917 | 1 | 1 | 2 | 3 | 4 |
| 62 | 7924 | 7931 | 7938 | 7945 | 7952 | 7959 | 7966 | 7973 | 7980 | 7987 | 1 | 1 | 2 | 3 | 3 |
| 63 | 7993 | 8000 | 8007 | 8014 | 8021 | 8028 | 8035 | 8041 | 8048 | 8055 | 1 | 1 | 2 | 3 | 3 |
| 64 | 8062 | 8069 | 8075 | 8082 | 8089 | 8096 | 8102 | 8109 | 8116 | 8122 | 1 | 1 | 2 | 3 | 3 |
| 65 | 8129 | 8136 | 8142 | 8149 | 8156 | 8162 | 8169 | 8176 | 8182 | 8189 | 1 | 1 | 2 | 3 | 3 |
| 66 | 8195 | 8202 | 8209 | 8215 | 8222 | 8228 | 8235 | 8241 | 8248 | 8254 | 1 | 1 | 2 | 3 | 3 |
| 67 | 8261 | 8267 | 8274 | 8280 | 8287 | 8293 | 8299 | 8306 | 8312 | 8319 | 1 | 1 | 2 | 3 | 3 |
| 68 | 8325 | 8331 | 8338 | 8344 | 8351 | 8357 | 8363 | 8370 | 8376 | 8382 | 1 |  | 2 | 3 | 3 |
| 69 | 8388 | 8395 | 8401 | 8407 | 8414 | 8420 | 8426 | 8432 | 8439 | 8445 | 1 | 1 | 2 | 3 | 3 |
| 70 | 8451 | 8457 | 8463 | 8470 | 8476 | 8482 | 8488 | 8494 | 8500 | 8506 | 1 | , | 2 | 2 | 3 |
| 71 | 8513 | 8519 | 8525 | 8531 | 8537 | 8543 | 8549 | 8555 | 8561 | 8567 | 1 | 1 | 2 | 2 | 3 |
| 72 | 8573 | 8579 | 8585 | 8591 | 8597 | 8603 | 8609 | 8615 | 8621 | 8627 | 1 | 1 | 2 | 2 | 3 |
| 73 | 8633 | 8639 | 8645 | 8651 | 8657 | 8663 | 8669 | 8675 | 8681 | 8686 | 1 | 1 | 2 | 2 | 3 |
| 74 | 8692 | 8698 | 8704 | 8710 | 8716 | 8722 | 8727 | 8733 | 8739 | 8745 | 1 | 1 | 2 | 2 | 3 |
| 75 | 8751 | 8756 | 8762 | 8768 | 8774 | 8779 | 8785 | 8791 | 8797 | 8802 | 1 | 1 | 2 | 2 | 3 |
| 76 | 8808 | 8814 | 8820 | 8825 | 8831 | 8837 | 8842 | 8848 | 8854 | 8859 | 1 |  | 2 | 2 | 3 |
| 77 | 8865 | 8871 | 8876 | 8882 | 8887 | 8893 | 8899 | 8904 | 8910 | 8915 | 1 | , | 2 | 2 | 3 |
| 78 | 8921 | 8927 | 8932 | 8938 | 8943 | 8949 | 8954 | 8960 | 8965 | 8971 |  |  | 2 | 2 | 3 |
| 79 | 8976 | 8982 | 8987 | 8993 | 8998 | 9004 | 9009 | 9015 | 9020 | 9025 |  | 1 | 2 | 2 | 3 |
| 80 | 9031 | 9036 | 9042 | 9047 | 9053 | 9058 | 9063 | 9069 | 9074 | 9079 | 1 | , | 2 | 2 | 3 |
| 81 | 9085 | 9090 | 9096 | 9101 | 9106 | 9112 | 9117 | 9122 | 9128 | 9133 | 1 | 1 | 2 | 2 | 3 |
| 82 | 9138 | 9143 | 9149 | 9154 | 9159 | 9165 | 9170 | 9175 | 9180 | 9186 | 1 | , | 2 | 2 | 3 |
| 83 | 9191 | 9196 | 9201 | 9206 | 9212 | 9217 | 9222 | 9237 | 9232 | 9238 | 1 | 1 | 2 | 2 | 3 |
| 84 | 9243 | 9248 | 9253 | 9258 | 9263 | 9269 | 9274 | 9279 | 9284 | 9289 | 1 | 1 | 2 | 2 | 3 |
| 85 | 9294 | 9299 | 9304 | 9309 | 9315 | 9320 | 9325 | 9330 | 9335 | 9340 | 1 |  | 2 | 2 | 3 |
| 86 | 9345 | 9350 | 9355 | 9360 | 9365 | 9370 | 9375 | 9380 | 9385 | 9390 | 1 | 1 | 2 | 2 | 3 |
| 87 | 9395 | 9400 | 9405 | 9410 | 9415 | 94?0 | 9425 | 9430 | 9435 | 9440 | 0 | 1 | 1 | 2 |  |
| 88 | 9445 | 9450 | 9455 | 9460 | 9465 | 9469 | 9474 | 9479 | 9484 | 9489 | 0 | 1 | 1 | 2 | 2 |
| 89 | 9494 | 9499 | 9504 | 9509 | 9513 | 9518 | 9523 | 9528 | 9533 | 9538 | 0 | 1 | 1 | 2 |  |
| 90 | 9542 | 9547 | 9552 | 9557 | 9562 | 9566 | 9571 | 9576 | 9581 | 9586 | 0 | 1 | 1 | 2 | 2 |
| 91 | 9590 | 9595 | 5600 | 9605 | 9609 | 9614 | 9619 | 9624 | 9628 | 9633 | 0 | , |  | 2 | 2 |
| 92 | 9638 | 9643 | 9647 | 9652 | 9657 | 9661 | 9666 | 9671 | 9675 | 9680 | 0 | 1 | 1 | 2 | 2 |
| 93 | 9685 | 9689 | 9694 | 9699 | 9703 | 9708 | 9713 | 9717 | 9722 | 9727 | 0 | 1 | 1 | 2 | 2 |
| 94 | 9731 | 9736 | 9741 | 9745 | 9750 | 9754 | 9759 | 9763 | 9768 | 9773 | 0 | 1 | 1 | 2 | 2 |
| 95 | 9777 | 9782 | 9786 | 9791 | 9795 | 9800 | 9805 | 9809 | 9814 | 9818 | 0 | 1 | 1 | 2 | 2 |
| 96 | 9823 | 9827 | 9832 | 9836 | 9841 | 9845 | 9850 | 9854 | 9859 | 9863 | 0 | 1 | 1 | 2 | 2 |
| 97 | 9868 | 9872 | 9877 | 9881 | 9886 | 9890 | 9894 | 9899 | 9903 | 9908 | 0 | 1 | 1 | 2 | 2 |
| 98 | 9912 | 9917 | 9921 | 9926 | 9930 | 9934 | 9939 | 9943 | 9948 | 9952 | 0 | 1 | 1 | 2 | 2 |
| 99 | 9956 | 9961 | 9965 | 9969 | 9974 | 9978 | 9983 | 9987 | 9991 | 9996 | 0 | 1 | 1 | 2 | 2 |

(continued)

| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 100 | 0000 | 0004 | 0009 | 0013 | 0017 | 0022 | 0026 | 0030 | 0035 | 0039 | 0043 |
| 101 | 0043 | 0048 | 0052 | 0056 | 0060 | 0065 | 0069 | 0073 | 0077 | 0082 | 0086 |
| 102 | 0086 | 0090 | 0095 | 0099 | 0103 | 0107 | 0111 | 0116 | 0120 | 0124 | 0128 |
| 103 | 0128 | 0133 | 0137 | 0141 | 0145 | 0149 | 0154 | 0158 | 0162 | 0166 | 0170 |
| 104 | 0170 | 0175 | 0179 | 0183 | 0187 | 0191 | 0195 | 0199 | 0204 | 0208 | 0212 |
| 105 | 0212 | 0216 | 0220 | 0224 | 0228 | 0233 | 0237 | 0241 | 0245 | 0249 | 0253 |
| 106 | 0253 | 0257 | 0261 | 0265 | 0269 | 0273 | 0278 | 0282 | 0286 | 0290 | 0294 |
| 107 | 0294 | 0298 | 0302 | 0306 | 0310 | 0314 | 0318 | 0322 | 0326 | 0330 | 0334 |
| 108 | 0334 | 0338 | 0342 | 0346 | 0350 | 0354 | 0358 | 0362 | 0366 | 0370 | 0374 |
| 109 | 0374 | 0378 | 0382 | 0386 | 0390 | 0394 | 0398 | 0402 | 0406 | 0410 | 0414 |
| 110 | 0414 | 0418 | 0422 | 0426 | 0430 | 0434 | 0438 | 0441 | 0445 | 0449 | 0453 |
| 111 | 0453 | 0457 | 0461 | 0465 | 0469 | 0473 | 0477 | 0481 | 0484 | 0488 | 0492 |
| 112 | 0492 | 0496 | 0500 | 0504 | 0508 | 0512 | 0515 | 0519 | 0523 | 0527 | 0531 |
| 113 | 0531 | 0535 | 0538 | 0542 | 0546 | 0550 | 0554 | 0558 | 0561 | 0565 | 0569 |
| 114 | 0569 | 0573 | 0577 | 0580 | 0584 | 0588 | 0592 | 0596 | 0599 | 0603 | 0607 |
| 115 | 0607 | 0611 | 0615 | 0618 | 0622 | 0626 | 0630 | 0633 | 0637 | 0641 | 0645 |
| 116 | 0645 | 0648 | 0652 | 0656 | 0660 | 0663 | 0667 | 0671 | 0674 | 0678 | 0682 |
| 117 | 0682 | 0686 | 0689 | 0693 | 0697 | 0700 | 0704 | 0708 | 0711 | 0715 | 0719 |
| 118 | 0719 | 0722 | 0726 | 0730 | 0734 | 0737 | 0741 | 0745 | 0748 | 0752 | 0755 |
| 119 | 0755 | 0759 | 0763 | 0766 | 0770 | 0774 | 0777 | 0781 | 0785 | 0788 | 0792 |
| 120 | 0792 | 0795 | 0799 | 0803 | 0806 | 0810 | 0813 | 0817 | 0821 | 0824 | 0828 |
| 121 | 0828 | 0831 | 0835 | 0839 | 0842 | 0846 | 0849 | 0853 | 0856 | 0860 | 0864 |
| 122 | 0864 | 0867 | 0871 | 0874 | 0878 | 0881 | 0885 | 0888 | 0892 | 0896 | 0899 |
| 123 | 0899 | 0903 | 0906 | 0910 | 0913 | 0917 | 0920 | 0924 | 0927 | 0931 | 0934 |
| 124 | 0934 | 0938 | 0941 | 0945 | 0948 | 0952 | 0955 | 0959 | 0962 | 0966 | 0969 |
| 125 | 0969 | 0973 | 0976 | 0980 | 0983 | 0986 | 0990 | 0993 | 0997 | 1000 | 1004 |
| 126 | 1004 | 1007 | 1011 | 1014 | 1017 | 1021 | 1024 | 1028 | 1031 | 1035 | 1038 |
| 127 | 1038 | 1041 | 1045 | 1048 | 1052 | 1055 | 1059 | 1062 | 1065 | 1069 | 1072 |
| 128 | 1072 | 1075 | 1079 | 1082 | 1086 | 1089 | 1092 | 1096 | 1099 | 1103 | 1106 |
| 129 | 1106 | 1109 | 1113 | 1116 | 1119 | 1123 | 1126 | 1129 | 1133 | 1136 | 1139 |
| 130 | 1139 | 1143 | 1146 | 1149 | 1153 | 1156 | 1159 | 1163 | 1166 | 1169 | 1173 |
| 131 | 1173 | 1176 | 1179 | 1183 | 1186 | 1189 | 1193 | 1196 | 1199 | 1202 | 1206 |
| 132 | 1206 | 1209 | 1212 | 1216 | 1219 | 1222 | 1225 | 1229 | 1232 | 1235 | 1239 |
| 133 | 1239 | 1242 | 1245 | 1248 | 1252 | 1255 | 1258 | 1261 | 1265 | 1268 | 1271 |
| 134 | 1271 | 1274 | 1278 | 1281 | 1284 | 1287 | 1290 | 1294 | 1297 | 1300 | 1303 |
| 135 | 1303 | 1307 | 1310 | 1313 | 1316 | 1319 | 1323 | 1326 | 1329 | 1332 | 1335 |
| 136 | 1335 | 1339 | 1342 | 1345 | 1348 | 1351 | 1355 | 1358 | 1361 | 1364 | 1367 |
| 137 | 1367 | 1370 | 1374 | 1377 | 1380 | 1383 | 1386 | 1389 | 1392 | 1396 | 1399 |
| 138 | 1399 | 1402 | 1405 | 1408 | 1411 | 1414 | 1418 | 1421 | 1424 | 1427 | 1430 |
| 139 | 1430 | 1433 | 1436 | 1440 | 1443 | 1446 | 1449 | 1452 | 1455 | 1458 | 1461 |
| 140 | 1461 | 1464 | 1467 | 1471 | 1474 | 1477 | 1480 | 1483 | 1486 | 1489 | 1492 |
| 141 | 1492 | 1495 | 1498 | 1501 | 1504 | 1508 | 1511 | 1514 | 1517 | 1520 | 1523 |
| 142 | 1523 | 1526 | 1529 | 1532 | 1535 | 1538 | 1541 | 1544 | 1547 | 1550 | 1553 |
| 143 | 1553 | 1556 | 1559 | 1562 | 1565 | 1569 | 1572 | 1575 | 1578 | 1581 | 1584 |
| 144 | 1584 | 1587 | 1590 | 1593 | 1596 | 1599 | 1602 | 1605 | 1608 | 1611 | 1614 |
| 145 | 1614 | 1617 | 1620 | 1623 | 1626 | 1629 | 1632 | 1635 | 1638 | 1641 | 1644 |
| 146 | 1644 | 1647 | 1649 | 1652 | 1655 | 1658 | 1661 | 1664 | 1667 | 1670 | 1673 |
| 147 | 1673 | 1676 | 1679 | 1682 | 1685 | 1688 | 1691 | 1694 | 1697 | 1700 | 1703 |
| 148 | 1703 | 1706 | 1708 | 1711 | 1714 | 1717 | 1720 | 1723 | 1726 | 1729 | 1732 |
| 149 | 1732 | 1735 | 1738 | 1741 | 1744 | 1746 | 1749 | 1752 | 1755 | 1758 | 1761 |

## (continued)

TABLE 14.-LOGARITHMS (concluded)

| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 150 | 1761 | 1764 | 1767 | 1770 | 1772 | 1775 | 1778 | 1781 | 1784 | 1787 | 1790 |
| 151 | 1790 | 1793 | 1796 | 1798 | 1801 | 1804 | 1807 | 1810 | 1813 | 1816 | 1818 |
| 152 | 1818 | 1821 | 1824 | 1827 | 1830 | 1833 | 1836 | 1838 | 1841 | 1844 | 1847 |
| 153 | 1847 | 1850 | 1853 | 1855 | 1858 | 1861 | 1864 | 1867 | 1870 | 1872 | 1875 |
| 154 | 1875 | 1878 | 1881 | 1884 | 1886 | 1889 | 1892 | 1895 | 1898 | 1901 | 1903 |
| 155 | 1903 | 1906 | 1909 | 1912 | 1915 | 1917 | 1920 | 1923 | 1926 | 1928 | 1931 |
| 156 | 1931 | 1934 | 1937 | 1940 | 1942 | 1945 | 1948 | 1951 | 1953 | 1956 | 1959 |
| 157 | 1959 | 1962 | 1965 | 1967 | 1970 | 1973 | 1976 | 1978 | 1981 | 1984 | 1987 |
| 158 | 1987 | 1989 | 1992 | 1995 | 1998 | 2000 | 2003 | 2006 | 2009 | 2011 | 2014 |
| 159 | 2014 | 2017 | 2019 | 2022 | 2025 | 2028 | 2030 | 2033 | 2036 | 2038 | 2041 |
| 160 | 2041 | 2044 | 2047 | 2049 | 2052 | 2055 | 2057 | 2060 | 2063 | 2066 | 2068 |
| 161 | 2068 | 2071 | 2074 | 2076 | 2079 | 2082 | 2084 | 2087 | 2090 | 2092 | 2095 |
| 162 | 2095 | 2098 | 2101 | 2103 | 2106 | 2109 | 2111 | 2114 | 2117 | 2119. | 2122 |
| 163 | 2122 | 2125 | 2127 | 2130 | 21.33 | 2135 | 2138 | 2140 | 2143 | 2146 | 2148 |
| 164 | 2148 | 2151 | 2154 | 2156 | 2159 | 2162 | 2164 | 2167 | 2170 | 2172 | 2175 |
| 165 | 2175 | 2177 | 2180 | 2183 | 2185 | 2188 | 2191 | 2193 | 2196 | 2198 | 2201 |
| 166 | 2201 | 2204 | 2206 | 2209 | 2212 | 2214 | 2217 | 2219 | 2222 | 2225 | 2227 |
| 167 | 2227 | 2230 | 2232 | 2235 | 2238 | 2240 | 2243 | 2245 | 2248 | 2251 | 2253 |
| 168 | 2253 | 2256 | 2258 | 2261 | 2263 | 2266 | 2269 | 2271 | 2274 | 2276 | 2279 |
| 169 | 2279 | 2281 | 2284 | 2287 | 2289 | 2292 | 2294 | 2297 | 2299 | 2302 | 2304 |
| 170 | 2304 | 2307 | 2310 | 2312 | 2315 | 2317 | 2320 | 2322 | 2325 | 2327 | 2330 |
| 171 | 2330 | 2333 | 2335 | 2338 | 2340 | 2343 | 2345 | 2348 | 2350 | 2353 | 2355 |
| 172 | 2355 | 2358 | 2360 | 2363 | 2365 | 2368 | 2370 | 2373 | 2375 | 2378 | 2380 |
| 173 | 2380 | 2383 | 2385 | 2388 | 2390 | 2393 | 2395 | 2398 | 2400 | 2403 | 2405 |
| 174 | 2405 | 2408 | 2410 | 2413 | 2415 | 2418 | 2420 | 2423 | 2425 | 2428 | 2430 |
| 175 | 2430 | 2433 | 2435 | 2438 | 2440 | 2443 | 2445 | 2448 | 2450 | 2453 | 2455 |
| 176 | 2455 | 2458 | 2460 | 2463 | 2465 | 2467 | 2470 | 2472 | 2475 | 2477 | 2480 |
| 177 | 2480 | 2482 | 2485 | 2487 | 2490 | 2492 | 2494 | 2497 | 2499 | 2502 | 2504 |
| 178 | 2504 | 2507 | 2509 | 2512 | 2514 | 2516 | 2519 | 2521 | 2524 | 2526 | 2529 |
| 179 | 2529 | 2531 | 2533 | 2536 | 2538 | 2541 | 2543 | 2545 | 2548 | 2550 | 2553 |
| 180 | 2553 | 2555 | 2558 | 2560 | 2562 | 2565 | 2567 | 2570 | 2572 | 2574 | 2577 |
| 181 | 2577 | 2579 | 2582 | 2584 | 2586 | 2589 | 2591 | 2594 | 2596 | 2598 | 2601 |
| 182 | 2601 | 2603 | 2605 | 2608 | 2610 | 2613 | 2615 | 2617 | 2620 | 2622 | 2625 |
| 183 | 2625 | 2627 | 2629 | 2632 | 2634 | 2636 | 2639 | 2641 | 2643 | 2646 | 2648 |
| 184 | 2648 | 2651 | 2653 | 2655 | 2658 | 2660 | 2662 | 2665 | 2667 | 2669 | 2672 |
| 185 | 2672 | 2674 | 2676 | 2679 | 2681 | 2683 | 2686 | 2688 | 2690 | 2693 |  |
| 186 | 2695 | 2697 | 2700 | 2702 | 2704 | 2707 | 2709 | 2711 | 2714 | 2716 | 2718 |
| 187 | 2718 | 2721 | 2723 | 2725 | 2728 | 2730 | 2732 | 2735 | 2737 | 2739 | 2742 |
| 188 | 2742 | 2744 | 2746 | 2749 | 2751 | 2753 | 2755 | 2758 | 2760 | 2762 | 2765 |
| 189 | 2765 | 2767 | 2769 | 2772 | 2774 | 2776 | 2778 | 2781 | 2783 | 2785 | 2788 |
| 190 | 2788 | 2790 | 2792 | 2794 | 2797 | 2799 | 2801 | 2804 | 2806 | 2808 | 2810 |
| 191 | 2810 | 2813 | 2815 | 2817 | 2819 | 2822 | 2824 | 2826 | 28.8 | 2831 | 2833 |
| 192 | 2833 | 2835 | 2838 | 2840 | 2842 | 2844 | 2847 | 2849 | 2851 | 2853 | 2856 |
| 193 | 2856 | 2858 | 2860 | 2862 | 2865 | 2867 | 2869 | 2871 | 2874 | 2876 | 2878 |
| 194 | 2878 | 2880 | 2882 | 2885 | 2887 | 2889 | 2891 | 2894 | 2896 | 2898 | 2900 |
| 195 | 2900 | 2903 | 2905 | 2907 | 2909 | 2911 | 2914 | 2916 | 2918 | 2920 | 2923 |
| 196 | 2923 | 2925 | 2927 | 2929 | 2931 | 2934 | 2936 | 2938 | 2940 | 2942 | 2945 |
| 197 | 2945 | 2947 | 2949 | 2951 | 2953 | 2956 | 2958 | 2960 | 2962 | 2964 | 2967 |
| 198 | 2967 | 2969 | 2971 | 2973 | 2975 | 2978 | 2980 | 2982 | 2984 | 2986 | 2989 |
| 199 | 2989 | 2991 | 2993 | 2995 | 2997 | 2999 | 3002 | 3004 | 3006 | 3008 | 3010 |

TABLE 15.-CIRCULAR (TRIGONOMETRIC) FUNCTIONS*

|  |  | Sines |  | Cosines |  | Tangents |  | Cotangents |  | $90^{\circ} 00^{\prime}$ | 1.5708 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Radi- ans | $\begin{aligned} & \text { De- } \\ & \text { grees } \end{aligned}$ | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. |  |  |
| 0.0000 | $0^{\circ} 00^{\prime}$ | . 0000 | $\infty$ | 1.0000 | 0.0000 | . 0000 | $\infty$ | $\infty$ | $\infty$ |  |  |
| 0.0029 | 10 | .0029 | 7.4637 | 1.0000 | . 0000 | . 0029 | 7.4637 | 343.77 | 2.5363 | 50 | 1.5679 |
| 0.0058 | 20 | . 0058 | . 7648 | 1.0000 | . 0000 | . 0058 | . 7648 | 171.89 | . 2352 | 40 | 1.5650 |
| 0.0087 | 30 | . 0087 | . 9408 | 1.0000 | . 0000 | . 0087 | . 9409 | 114.59 | . 0591 | 30 | 1.5621 |
| 0.0116 | 40 | . 0116 | 8.0658 | . 9999 | . 0000 | . 0116 | 8.0658 | 85.940 | 1.9342 | 20 | 1.5592 |
| 0.0145 | 50 | . 0145 | . 1627 | . 9959 | . 0000 | . 0145 | . 1627 | 68.750 | . 8373 | 10 | 1.5563 |
| 0.0175 | $1^{\circ} 00^{\prime}$ | . 0175 | 8.2419 | . 9998 | 9.9999 | . 0175 | 8.2419 | 57.290 | 1.7581 | $89^{\circ} 00^{\prime}$ | 1.5533 |
| 0.0204 | 10 | . 0204 | . 3088 | . 9998 | . 9999 | . 0204 | . 3089 | 49.104 | . 6911 | 50 | 1.5504 |
| 0.0233 | 20 | . 0233 | . 3668 | . 9997 | . 9999 | . 0233 | . 3669 | 42.964 | . 6331 | 40 | 1.5475 |
| 0.0262 | 30 | . 0262 | . 4179 | . 9997 | . 9999 | . 0262 | . 4181 | 38.188 | . 5819 | 30 | 1.5446 |
| 0.0291 | 40 | . 0291 | . 4637 | . 9996 | . 9998 | . 0291 | . 4638 | 34.368 | . 5362 | 20 | 1.5417 |
| 0.0320 | 50 | . 0320 | . 5050 | . 9995 | . 9998 | . 0320 | . 5053 | 31.242 | . 4947 | 10 | 1.5388 |
| 0.0349 | $2^{\circ} 00^{\prime}$ | . 0349 | 8.5428 | . 9994 | 9.9997 | . 0349 | 8.5431 | 28.636 | 1.4569 | $88^{\circ} 00^{\prime}$ | 1.5359 |
| 0.0378 | 10 | . 0378 | . 5776 | . 9993 | . 9997 | . 0378 | . 5779 | 26.432 | . 4221 | 50 | 1.5330 |
| 0.0407 | 20 | . 0407 | . 6097 | . 9992 | . 9996 | . 0407 | . 6101 | 24.542 | . 3899 | 40 | 1.5301 |
| 0.0436 | 30 | . 0436 | . 6397 | . 9990 | . 9996 | . 0437 | . 6401 | 22.904 | . 3599 | 30 | 1.5272 |
| 0.0465 | 40 | . 0465 | . 6677 | . 9989 | . 9995 | . 0465 | . 6682 | 21.470 | . 3318 | 20 | 1.5243 |
| 0.0495 | 50 | . 0494 | . 6940 | . 9988 | . 9995 | . 0495 | . 6945 | 20.206 | . 3055 | 10 | 1.5213 |
| 0.0524 | $3^{\circ} 00^{\prime}$ | . 0523 | 8.7188 | . 9986 | 9.9994 | . 0524 | 8.7194 | 19.081 | 1.2806 | $87^{\circ} 00^{\prime}$ | 1.5184 |
| 0.0553 | 10 | . 0552 | . 7423 | . 9985 | . 9993 | . 0553 | . 7429 | 18.075 | . 2571 | 50 | 1.5155 |
| 0.0582 | 20 | . 0581 | . 7645 | . 9983 | . 9993 | . 0582 | . 7652 | 17.169 | . 2348 | 40 | 1.5126 |
| 0.0611 | 30 | . 0610 | . 7857 | . 9981 | . 9992 | . 0612 | . 7865 | 16.350 | . 2135 | 30 | 1.5097 |
| 0.0640 | 40 | . 0640 | . 8059 | . 9980 | . 9991 | . 0641 | . 8067 | 15.605 | . 1933 | 20 | 1.5068 |
| 0.0669 | 50 | . 0669 | . 8251 | . 9978 | . 9990 | . 0670 | . 8261 | 14.924 | . 1739 | 10 | 1.5039 |
| 0.0698 | $4^{\circ} 00^{\prime}$ | . 0698 | 8.8436 | . 9976 | 9.9989 | . 0699 | 8.8446 | 14.301 | 1.1554 | $86^{\circ} 00^{\prime}$ | 1.5010 |
| 0.0727 | 10 | . 0727 | . 8613 | . 9974 | . 9989 | . 0729 | . 8624 | 13.727 | . 1376 | 50 | 1.4981 |
| 0.0756 | 20 | . 0756 | . 8783 | . 9971 | . 9988 | . 0758 | . 8795 | 13.197 | . 1205 | 40 | 1.4952 |
| 0.0785 | 30 | . 0785 | . 8946 | . 9969 | . 9987 | . 0787 | . 8960 | 12.706 | . 1040 | 30 | 1.4923 |
| 0.0814 | 40 | . 0814 | . 9104 | . 9967 | . 9986 | . 0816 | . 9118 | 12.251 | . 0882 | 20 | 1.4893 |
| 0.0844 | 50 | . 0843 | . 9256 | . 9964 | . 9985 | . 0846 | . 9272 | 11.826 | . 0728 | 10 | 1.4864 |
| 0.0873 | $5^{\circ} 00^{\prime}$ | . 0872 | 8.9403 | . 9962 | 9.9983 | . 0875 | 8.9420 | 11.430 | 1.0580 | $85^{\circ} 00^{\prime}$ | 1.4835 |
| 0.0902 | 10 | . 0901 | . 9545 | . 9959 | . 9982 | . 0904 | . 9563 | 11.059 | . 0437 | 50 | 1.4806 |
| 0.0931 | 20 | . 0929 | . 9682 | . 9957 | . 9981 | . 0934 | . 97.01 | 10.712 | . 0299 | 40 | 1.4777 |
| 0.0960 | 30 | . 0958 | . 9816 | . 9954 | . 9980 | . 0963 | . 9836 | 10.385 | . 0164 | 30 | 1.4748 |
| 0.0989 | 40 | . 0987 | . 9945 | . 9951 | . 9979 | . 0992 | . 9966 | 10.078 | . 0034 | 20 | 1.4719 |
| 0.1018 | 50 | . 1016 | 9.0070 | . 9948 | . 9977 | . 1022 | 9.0093 | 9.7882 | 0.9907 | 10 | 1.4690 |
| 0.1047 | $6^{\circ} 00^{\prime}$ | . 1045 | 9.0192 | . 9945 | 9.9976 | . 1051 | 9.0216 | 9.5144 | 0.9784 | $84^{\circ} 00^{\prime}$ | 1.4661 |
| 0.1076 | 10 | . 1074 | . 0311 | . 9942 | . 9975 | . 1080 | . 0336 | 9.2553 | . 9664 | 50 | 1.4632 |
| 0.1105 | 20 | . 1103 | . 0426 | . 9939 | . 9973 | . 1110 | . 0453 | 9.0098 | . 9547 | 40 | 1.4603 |
| 0.1134 | 30 | . 1132 | . 0539 | . 9936 | . 9972 | . 1139 | . 0567 | 8.7769 | . 9433 | 30 | 1.4574 |
| 0.1164 | 40 | . 1161 | . 0648 | . 9932 | . 9971 | . 1169 | . 0678 | 8.5555 | . 9322 | 20 | 1.4544 |
| 0.1193 | 50 | . 1190 | . 0755 | . 9929 | . 9969 | . 1198 | . 0786 | 8.3450 | . 9214 | 10 | 1.4515 |
| 0.1222 | $7^{\circ} 00^{\prime}$ | . 1219 | 9.0859 | . 9925 | 9.9968 | . 1228 | 9.0891 | 8.1443 | 0.9109 | $83^{\circ} 00^{\prime}$ | 1.4486 |
| 0.1251 | 10 | . 1248 | . 0961 | . 9922 | . 9966 | . 1257 | . 0995 | 7.9530 | . 9005 | 50 | 1.4457 |
| 0.1280 | 20 | . 1276 | . 1060 | . 9918 | . 9964 | . 1287 | . 1096 | 7.7704 | . 8904 | 40 | 1.4428 |
| 0.1309 | 30 | . 1305 | . 1157 | . 9914 | . 9963 | . 1317 | . 1194 | 7.5958 | . 8806 | 30 | 1.4399 |
| 0.1338 | 40 | . 1334 | . 1252 | . 9911 | . 9961 | . 1346 | . 1291 | 7.4287 | . 8709 | 20 | 1.4370 |
| 0.1367 | 50 | . 1363 | . 1345 | . 9907 | . 9959 | . 1376 | . 1385 | 7.2687 | . 8615 | 10 | 1.4341 |
| 0.1396 | $8^{\circ} 00^{\prime}$ | . 1392 | 9.1436 | . 9903 | 9.9958 | . 1405 | 9.1478 | 7.1154 | 0.852? | $82^{\circ} 00^{\prime}$ | 1.431? |
| 0.1425 | 10 | . 1421 | . 1525 | . 9899 | . 9956 | . 1435 | . 1569 | 6.9682 | . 9431 | 50 | 1.4283 |
| 0.1454 | 20 | . 1449 | . 1612 | . 9894 | . 9954 | . 1465 | . 1658 | 6.8269 | . 8342 | 40 | 1.4254 |
| 0.1484 | 30 | . 1478 | . 1697 | . 9890 | . 9952 | . 1495 | . 1745 | 6.6912 | . 8255 | 30 | 1.4224 |
| 0.1513 | 40 | . 1507 | . 1781 | . 9886 | . 9950 | .1524 | . 1831 | 6.5606 | . 8169 | 20 | 1.4195 |
| 0.1542 | 50 | . 1536 | . 1863 | . 9881 | . 9948 | . 1554 | . 1915 | 6.4348 | . 8085 | 10 | 1.4166 |
| 0.1571 | $9^{\circ} 00^{\prime}$ | . 1564 | 9.1943 | . 9877 | 9.9946 | . 1584 | 9.1997 | 6.3138 | 0.8003 | $81^{\circ} 00^{\prime}$ | 1.4137 |
|  |  | Nat. | L.og. | Nat. | I.ng. | Nat. | L_og. | Nat. | I.og. |  |  |
|  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { De- } \\ & \text { grees } \end{aligned}$ | Radians |

[^10]

34 TABLE 15.-CIRCULAR (TRIGONOMETRIC) FUNCTIONS (continued)

|  |  | Sines |  | Cosines |  | Tangents |  | Cotangents |  | $72^{\circ} 00^{\prime}$ | 1.2566 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Radi- ans | $\begin{aligned} & \text { De- } \\ & \text { grees } \end{aligned}$ | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. |  |  |
| 0.3142 | $18^{\circ} 00^{\prime}$ | . 3090 | 9.4900 | . 9511 | 9.9782 | . 3249 | 9.5118 | 3.0777 | 0.4882 |  |  |
| 0.3171 | 10 | . 3118 | . 4939 | . 9502 | . 9778 | . 3281 | . 5161 | 3.0475 | . 4839 | 50 | 1.2537 |
| 0.3200 | 20 | . 3145 | . 4977 | . 9492 | . 9774 | . 3314 | . 5203 | 3.0178 | . 4797 | 40 | 1.2508 |
| 0.3229 | 30 | . 3173 | . 5015 | . 9483 | . 9770 | . 3346 | . 5245 | 2.9887 | . 4755 | 30 | 1.2479 |
| 0.3258 | 40 | . 3201 | . 5052 | . 9474 | . 9765 | . 3378 | . 5287 | 2.9600 | . 4713 | 20 | 1.2450 |
| 0.3287 | 50 | . 3228 | . 5090 | . 9465 | . 9761 | . 3411 | . 5329 | 2.9319 | . 4671 | 10 | 1.2421 |
| 0.3316 | $19^{\circ} 00^{\prime}$ | . 3256 | 9.5126 | . 9455 | 9.9757 | . 3443 | 9.5370 | 2.9042 | 0.4630 | $71^{\circ} 00^{\prime}$ | 1.2392 |
| 0.3345 | 10 | . 3283 | . 5163 | . 9446 | . 9752 | . 3476 | . 5411 | 2.8770 | . 4589 | 50 | 1.2363 |
| 0.3374 | 20 | . 3311 | . 5199 | . 9436 | . 9748 | . 3508 | . 5451 | 2.8502 | . 4549 | 40 | 1.2334 |
| 0.3403 | 30 | . 3338 | . 5235 | . 9426 | . 9743 | . 3541 | . 5491 | 2.8239 | . 4509 | 30 | 1.2305 |
| 0.3432 | 40 | . 3365 | . 5270 | . 9417 | . 9739 | . 3574 | . 5531 | 2.7980 | . 4469 | 20 | 1.2275 |
| 0.3462 | 50 | . 3393 | . 5306 | . 9407 | . 9734 | . 3607 | . 5571 | 2.7725 | . 4429 | 10 | 1.2246 |
| 0.3491 | $20^{\circ} 00^{\prime}$ | . 3420 | 9.5341 | . 9397 | 9.9730 | . 3640 | 9.5611 | 2.7475 | 0.4389 | $70^{\circ} 00^{\prime}$ | 1.2217 |
| 0.3520 | 10 | . 3448 | . 5375 | . 9387 | . 9725 | . 3673 | . 5650 | 2.7228 | . 4350 | 50 | 1.2188 |
| 0.3549 | 20 | . 3475 | . 5409 | . 9377 | . 9721 | . 3706 | . 5689 | 2.6985 | . 4311 | 40 | 1.2159 |
| 0.3578 | 30 | . 3502 | . 5443 | . 9367 | . 9716 | . 3739 | . 5727 | 2.6746 | . 4273 | 30 | 1.2130 |
| 0.3607 | 40 | . 3529 | . 5477 | . 9356 | . 9711 | . 3772 | . 5766 | 2.6511 | . 4234 | 20 | 1.2101 |
| 0.3636 | 50 | . 3557 | . 5510 | . 9346 | . 9706 | . 3805 | . 5804 | 2.6279 | . 4196 | 10 | 1.2072 |
| 0.3665 | $21^{\circ} 00^{\prime}$ | . 3584 | 9.5543 | . 9336 | 9.9702 | . 3839 | 9.5842 | 2.6051 | 0.4158 | $69^{\circ} 00^{\prime}$ | 1.2043 |
| 0.3694 | 10 | . 3611 | . 5576 | . 9325 | . 9697 | . 3872 | . 5879 | 2.5826 | . 4121 | 50 | 1.2014 |
| 0.3723 | 20 | . 3638 | . 5609 | . 9315 | . 9692 | . 3906 | . 5917 | 2.5605 | . 4083 | 40 | 1.1985 |
| 0.3752 | 30 | . 3665 | . 5641 | . 9304 | . 9687 | . 3939 | . 5954 | 2.5386 | . 4046 | 30 | 1.1956 |
| 0.3782 | 40 | . 3692 | . 5673 | . 9293 | . 9682 | . 3973 | . 5991 | 2.5172 | . 4009 | 20 | 1.1926 |
| 0.3811 | 50 | . 3719 | . 5704 | . 9283 | . 9677 | . 4006 | . 6028 | 2.4960 | . 3972 | 10 | 1.1897 |
| 0.3840 | $22^{\circ} 00^{\prime}$ | . 3746 | 9.5736 | . 9272 | 9.9672 | . 4040 | 9.6064 | 2.4751 | 0.3936 | $68^{\circ} 00^{\prime}$ | 1.1868 |
| 0.3869 | 10 | . 3773 | . 5767 | . 9261 | . 9667 | . 4074 | . 6100 | 2.4545 | . 3900 | 50 | 1.1839 |
| 0.3898 | 20 | . 3800 | . 5798 | . 9250 | . 9661 | . 4108 | . 6136 | 2.4342 | . 3864 | 40 | 1.1810 |
| 0.3927 | 30 | . 3827 | . 5828 | . 9239 | . 9656 | . 4142 | . 6172 | 2.4142 | . 3828 | 30 | 1.1781 |
| 0.3956 | 40 | . 3854 | . 5859 | . 9228 | . 9651 | . 4176 | . 6208 | 2.3945 | . 3792 | 20 | 1.1752 |
| 0.3985 | 50 | . 3881 | . 5889 | . 9216 | . 9646 | . 4210 | . 6243 | 2.3750 | . 3757 | 10 | 1.1723 |
| 0.4014 | $23^{\circ} 00^{\prime}$ | . 3907 | 9.5919 | . 9205 | 9.9640 | . 4245 | 9.6279 | 2.3559 | 0.3721 | $67^{\circ} 00^{\prime}$ | 1.1694 |
| 0.4043 | 10 | . 3934 | . 5948 | . 9194 | . 9635 | . 4279 | . 6314 | 2.3369 | . 3686 | 50 | 1.1665 |
| 0.4072 | 20 | . 3961 | . 5978 | . 9182 | . 9629 | . 4314 | . 6348 | 2.3183 | . 3652 | 40 | 1.1636 |
| 0.4102 | 30 | . 3987 | . 6007 | . 9171 | . 9624 | . 4348 | .638,3 | 2.2998 | . 3617 | 30 | 1.1606 |
| 0.4131 | 40 | . 4014 | . 6036 | . 9159 | . 9618 | . 4383 | . 6417 | 2.2817 | . 3583 | 20 | 1.1577 |
| 0.4160 | 50 | . 4041 | . 6065 | . 9147 | . 9613 | . 4417 | . 6452 | 2.2637 | . 3548 | 10 | 1.1548 |
| 0.4189 | $24^{\circ} 00^{\prime}$ | . 4067 | 9.6093 | . 9135 | 9.9607 | . 4452 | 9.6486 | 2.2460 | 0.3514 | $66^{\circ} 00^{\prime}$ | 1.1519 |
| 0.4218 | 10 | . 4094 | . 6121 | . 9124 | . 9602 | . 4487 | . 6520 | 2.2286 | . 3480 | 50 | 1.1490 |
| 0.4247 | 20 | . 4120 | . 6149 | . 9112 | . 9596 | . 4522 | . 6553 | 2.2113 | . 3447 | 40 | 1.1461 |
| 0.4276 | 30 | . 4147 | . 6177 | . 9100 | . 9590 | . 4557 | . 6587 | 2.1943 | . 3413 | 30 | 1.1432 |
| 0.4305 | 40 | . 4173 | . 6205 | . 9088 | . 9584 | . 4592 | . 6620 | 2.1775 | . 3380 | 20 | 1.1403 |
| 0.4334 | 50 | . 4200 | . 6232 | . 9075 | . 9579 | . 4628 | . 6654 | 2.1609 | . 3346 | 10 | 1.1374 |
| 0.4363 | $25^{\circ} 00^{\prime}$ | . 4226 | 9.6259 | . 9063 | 9.9573 | . 4663 | 9.6687 | 2.1445 | 0.3313 | $65^{\circ} 00^{\prime}$ | 1.1345 |
| 0.4392 | 10 | . 4253 | . 6286 | . 9051 | . 9567 | . 4699 | . 6720 | 2.1283 | . 3280 | 50 | 1.1316 |
| 0.4422 | 20 | . 4279 | . 6313 | . 9038 | . 9561 | . 4734 | . 6752 | 2.1123 | . 3248 | 40 | 1.1286 |
| 0.4451 | 30 | . 4305 | . 6340 | . 9026 | . 9555 | . 4770 | . 6785 | 2.0965 | . 3215 | 30 | 1.1257 |
| 0.4480 | 40 | . 4331 | . 6366 | . 9013 | . 9549 | . 4806 | . 6817 | 2.0809 | . 3183 | 20 | 1.1228 |
| 0.4509 | 50 | . 4358 | . 6392 | . 9001 | . 9543 | . 4841 | . 6850 | 2.0655 | . 3150 | 10 | 1.1199 |
| 0.4538 | $26^{\circ} 00^{\prime}$ | . 4384 | 9.6418 | . 8988 | 9.9537 | . 4877 | 9.6882 | 2.0503 | 0.3118 | $64^{\circ} 00^{\prime}$ | 1.1170 |
| 0.4567 | 10 | . 4410 | . 6444 | . 8975 | . 9530 | . 4913 | . 6914 | 2.0353 | . 3086 | 50 | 1.1141 |
| 0.4596 | 20 | . 4436 | . 6470 | . 8962 | . 9524 | . 4950 | . 6946 | 2.0204 | . 3054 | 40 | 1.1112 |
| 0.4625 | 30 | . 4462 | . 6495 | . 8949 | . 9518 | . 4986 | . 6977 | 2.0057 | . 3023 | 30 | 1.1083 |
| 0.4654 | 40 | . 4488 | . 6521 | . 8936 | . 9512 | . 5022 | . 7009 | 1.9912 | . 2991 | 20 | 1.1054 |
| 0.4683 | 50 | . 4514 | . 6546 | . 8923 | . 9505 | . 5059 | . 7040 | 1.9768 | . 2960 | 10 | 1.1025 |
| 0.4712 | $27^{\circ} 00^{\prime}$ | .45409 .6570 |  | . 89109.9499 |  | . 50959.7072 |  | 1.96260 .2928 |  | $63^{\circ} 00^{\prime}$ | 1.0996 |
|  |  | $\underbrace{\text { Nat. } \quad \text { Log. }}_{\text {Cosines }}$ |  | Nat. | Log. | $\underbrace{\text { Nat. Log. }}_{\text {Cotangents. }}$ |  | $\underbrace{\text { Nat. Log. }}_{\text {Tangents }}$ |  | $\begin{aligned} & \text { De- } \\ & \text { grees } \end{aligned}$ | Radians |
|  |  |  |  | Sin |  |  |  |  |  |  |  |

(continued)

# TABLE 15.-CIRCULAR (TRIGONOMETRIC) FUNCTIONS (continued) 



| Radi- | $\begin{aligned} & \text { De. } \\ & \text { grees } \end{aligned}$ | Sines |  | Cosines |  | Tangents |  | Cotangents |  | $54^{\circ} 00^{\prime}$ | 0.9425 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Nat. | Log. | Nat. | Log. | Nat. | Log. | Nat. | Log. |  |  |
| 0.6283 | $36^{\circ} 00^{\prime}$ | . 5878 | 9.7692 | . 8090 | 9.9080 | . 7265 | 9.8613 | 1.3764 | 0.1387 |  |  |
| 0.6312 | 10 | . 5901 | . 7710 | . 8073 | . 9070 | . 7310 | . 8639 | 1.3680 | . 1361 | 50 | 0.9396 |
| 0.6341 | 20 | . 5925 | . 7727 | . 8056 | . 9061 | . 7355 | . 8666 | 1.3597 | . 1334 | 40 | 0.9367 |
| 0.6370 | 30 | . 5948 | . 7744 | . 8039 | . 9052 | . 7400 | . 8692 | 1.3514 | . 1308 | 30 | 0.9338 |
| 0.6400 | 40 | . 5972 | . 7761 | . 8021 | . 9042 | . 7445 | . 8718 | 1.3432 | . 1282 | 20 | 0.9308 |
| 0.6429 | 50 | . 5995 | . 7778 | . 8004 | . 9033 | . 7490 | . 8745 | 1.3351 | . 1255 | 10 | 0.9279 |
| 0.6458 | $37^{\circ} 00^{\prime}$ | . 6018 | 9.7795 | . 7986 | 9.9023 | . 7536 | 9.8771 | 1.3270 | 0.1229 | $53^{\circ} 00^{\prime}$ | 0.9250 |
| 0.6487 | 10 | . 6041 | . 7811 | . 7969 | . 9014 | . 7581 | . 8797 | 1.3190 | . 1203 | 50 | 0.9221 |
| 0.6516 | 20 | . 6065 | . 7828 | . 7951 | . 9004 | . 7627 | . 8824 | 1.3111 | . 1176 | 40 | 0.9192 |
| 0.6545 | 30 | . 6088 | . 7844 | . 7934 | . 8995 | . 7673 | . 8850 | 1.3032 | . 1150 | 30 | 0.9163 |
| 0.6574 | 41) | . 6111 | . 7861 | . 7916 | . 8985 | . 7720 | . 8876 | 1.2954 | . 1124 | 20 | 0.9134 |
| 0.6603 | $51)$ | . 6134 | . 7877 | . 7898 | . 8975 | . 7766 | . 8902 | 1.2876 | . 1098 | 10 | 0.9105 |
| 0.6632 | $38^{\circ} 00^{\prime}$ | . 6157 | 9.7893 | . 7880 | 9.8565 | . 7813 | 9.8928 | 1.2799 | 0.1072 | $52^{\circ} 00^{\prime}$ | 0.9076 |
| 0.6661 | 10 | . 6180 | . 7910 | . 7862 | . 8955 | . 7860 | . 8954 | 1.2723 | . 1046 | 50 | 0.9047 |
| 0.6690 | 20 | . 6202 | . 7926 | . 7844 | . 8945 | . 7907 | . 8980 | 1.2647 | . 1020 | 40 | 0.9018 |
| 0.6720 | 30 | . 6225 | . 7941 | . 7826 | . 8935 | . 7954 | . 9006 | 1.2572 | . 0994 | 30 | 0.8988 |
| 0.6749 | 40 | . 6248 | . 7957 | . 7808 | . 8925 | . 8002 | . 9032 | 1.2497 | . 0968 | 20 | 0.8959 |
| 0.6778 | 50 | . 6271 | . 7973 | . 7790 | . 8915 | . 8050 | . 9058 | 1.2423 | . 0942 | 10 | 0.8930 |
| 0.6807 | $39^{\circ} 00^{\prime}$ | . 6293 | 9.7989 | .7771 | 0.8905 | . 8098 | 9.9084 | 1.2349 | 0.0916 | $51^{\circ} 000^{\prime}$ | 0.8901 |
| 0.6836 | 10 | . 6316 | . 8004 | . 7753 | . 8895 | . 8146 | . 9110 | 1.2276 | . 0890 | 50 | 0.8872 |
| 0.6865 | 20 | . 6338 | . 8020 | -. 7735 | . 8884 | . 8195 | . 9135 | 1.2203 | . 0865 | 40 | 0.8843 |
| 0.6894 | 30 | . 6361 | . 8035 | . 7716 | . 8874 | . 8243 | . 9161 | 1.2131 | . 0839 | 30 | 0.8814 |
| 0.6923 | 40 | . 6383 | . 8050 | . 7698 | . 8864 | . 8292 | . 9187 | 1.2059 | . 0813 | 20 | 0.8785 |
| 0.6952 | 50 | . 6406 | . 8066 | . 7679 | . 8853 | . 8342 | . 9212 | 1.1988 | . 0788 | 10 | 0.8756 |
| 0.6981 | $40^{\circ} 00^{\prime}$ | . 6428 | 9.8081 | . 7660 | 9.8843 | . 8391 | 9.9238 | 1.1918 | 0.0762 | $50^{\circ} 00^{\prime}$ | 0.8727 |
| 0.7010 | 10 | . 6450 | . 8096 | . 7642 | . 8832 | . 8441 | . 9264 | 1.1847 | . 0736 | 50 | 0.8698 |
| 0.7039 | 20 | . 6472 | . 8111 | . 7623 | . 8821 | . 8491 | . 9289 | 1.1778 | . 0711 | 40 | 0.8668 |
| 0.7069 | 30 | . 6494 | . 8125 | . 7604 | . 8810 | . 8541 | . 9315 | 1.1708 | . 0685 | 30 | 0.8639 |
| 0.7098 | 40 | . 6517 | . 8140 | . 7585 | . 8800 | . 8591 | . 9341 | 1.1640 | . 0659 | 20 | 0.8610 |
| 0.7127 | 50 | . 6539 | . 8155 | . 7566 | . 8789 | . 8642 | .9366 | 1.1571 | . 0634 | 10 | 0.8581 |
| 0.7156 | $41^{\circ} 00^{\prime}$ | . 6561 | 9.8169 | . 7547 | 9.8778 | . 8693 | 9.9392 | 1.1504 | 0.0608 | $49^{\circ} 00^{\prime}$ | 0.8552 |
| 0.7185 | 10 | . 6583 | . 8184 | . 7528 | . 8767 | . 8744 | . 9417 | 1.1436 | . 0583 | 50 | 0.8523 |
| 0.7214 | 20 | . 6604 | . 8198 | . 7509 | . 8756 | . 8796 | . 9443 | 1.1369 | . 0557 | 40 | 0.8494 |
| 0.7243 | 30 | . 6626 | . 8213 | . 7490 | . 8745 | . 8847 | . 9468 | 1.1303 | . 0532 | 30 | 0.8465 |
| 0.7272 | 40 | . 6648 | . 8227 | . 7470 | . 8733 | . 8899 | . 9494 | 1.1237 | . 0506 | 20 | 0.8436 |
| 0.7301 | 50 | . 6670 | . 8241 | . 7451 | . 8722 | . 8952 | . 9519 | 1.1171 | . 0481 | 10 | 0.8407 |
| 0.7330 | $42^{\circ} 00^{\prime}$ | . 6691 | 9.8255 | . 7431 | 9.8711 | . 9004 | 9.9544 | 1.1106 | 0.0456 | $48^{\circ} 00^{\prime}$ | 0.8378 |
| 0.7359 | 10 | . 6713 | . 8269 | . 7412 | . 8659 | . 9057 | . 9570 | 1.1041 | . 0430 | 50 | 0.8348 |
| 0.7389 | 20 | . 6734 | . 8283 | . 7392 | . 8688 | . 9110 | . 9595 | 1.0977 | . 0405 | 40 | 0.8319 |
| 0.7418 | 30 | . 6756 | . 8297 | . 7373 | . 8676 | . 9163 | . 9621 | 1.0913 | . 0379 | 30 | 0.8290 |
| 0.7447 | 40 | . 6777 | . 8311 | . 7353 | . 8665 | . 9217 | . 9646 | 1.0850 | . 0354 | 20 | 0.8261 |
| 0.7476 | 50 | . 6799 | . 8324 | . 7333 | . 8653 | . 9271 | . 9671 | 1.0786 | . 0329 | 10 | 0.8232 |
| 0.7505 | $43^{\circ} 00^{\prime}$ | . 6820 | 9.8338 | . 7314 | 9.8641 | . 9325 | 9.9697 | 1.0724 | 0.0303 | $47^{\circ} 00^{\prime}$ | 0.8203 |
| 0.7534 | 10 | . 6841 | . 8351 | . 7294 | . 8629 | . 9380 | . 9722 | 1.0661 | . 0278 | 50 | 0.8174 |
| 0.7563 | 20 | . 6862 | . 8365 | . 7274 | . 8618 | . 9435 | . 9747 | 1.0599 | . 0253 | 40 | 0.8145 |
| 0.7592 | 30 | . 6884 | . 8378 | . 7254 | . 8606 | . 9490 | . 9772 | 1.0538 | . 0228 | 30 | 0.8116 |
| 0.7621 | 40 | . 6905 | . 8391 | . 7234 | . 8594 | . 9545 | . 9798 | 1.0477 | . 0202 | 20 | 0.8087 |
| 0.7650 | 50 | . 6926 | . 8405 | . 7214 | . 8582 | . 9601 | . 9823 | 1.0416 | . 0177 | 10 | 0.8058 |
| 0.7679 | $44^{\circ} 00^{\prime}$ | . 6947 | 9.8418 | . 7193 | 0.8569 | . 9657 | 9.9848 | 1.0355 | 0.0152 | $46^{\circ} 00^{\prime}$ | 0.8029 |
| 0.7709 | 10 | . 6967 | . 8431 | . 7173 | . 8557 | . 9713 | . 9874 | 1.0295 | . 0126 | 50 | 0.7999 |
| 0.7738 | 20 | . 6988 | . 8444 | . 7153 | . 8545 | . 9770 | . 9899 | 1.0235 | . 0101 | 40 | 0.7970 |
| 0.7767 | 30 | . 7009 | . 8457 | . 7133 | . 8532 | . 9827 | . 9924 | 1.0176 | . 0076 | 30 | 0.7941 |
| 0.7796 | 40 | . 7030 | . 8469 | . 7112 | . 8520 | . 9884 | . 9949 | 1.0117 | . 0051 | 20 | 0.7912 |
| 0.7825 | 50 | . 7050 | . 8482 | . 7092 | . 8507 | . 9942 | . 9975 | 1.0058 | . 0025 | 10 | 0.7883 |
| 0.7854 | $45^{\circ} 00^{\prime}$ | . 7071 | 9.8495 | . 7071 | 9.8495 | 1.0000 | 0.0000 | 1.0000 | 0.0000 | $45^{\circ} 00^{\prime}$ | 0.7854 |
|  |  | $\underbrace{\text { Nat. }}$ | Log. | $\underbrace{\text { Nat. }}$ | Log. | Nat. | Log. | Nat. | Log. | De. | Radi. |
|  |  |  |  |  |  | Cotan | gents | Tang |  | grees | ans |

## TABLES 16-25.-TREATMENT OF EXPERLMIENTAL DAT. ${ }^{*}$

## TABLE 16. METHODS OF AVERAGING DATA

When a number of measurements are made of any quantity variations will be found. The question is: What is the best representat ve value for the (fwantity thus measured: and how shall the precision of the measurements be stated? The arithmetic mean of all the readings is generally taken as the best value. To tell something about the precision of the final result any one of five measures of variation which are discussed in books dealing with this subject may be given. These measures of deviation are:

$$
\begin{aligned}
p & =\text { probable error } \\
a & =\text { the average deviation (from the aritlumetic mean) } \\
\sigma & =\text { the standard deviation } \\
1 / h & =\text { the reciprocal of the modulus of precision } \\
k / z c & =\text { the reciprocal of the "precision constant" }
\end{aligned}
$$

Of these precision indexes the standard deviation, $\sigma$, is most easily computed. For the set of observed values $x_{1}, x_{2}, \ldots r_{n}$ of equal weight, the $\sigma$ for a single ubservation is given by
and for the mean by

$$
\sigma=\sqrt{\frac{\Sigma(\cdot r-F)^{2}}{n-1}} \cong \sqrt{\frac{\Sigma(. r-\bar{r})^{2}}{n}}
$$

$$
\sigma=\frac{\sigma}{\sqrt{n}}=\sqrt{\frac{\overline{\Sigma(x-\bar{r})^{2}}}{n(n-1)}} \cong \sqrt{\frac{\sqrt{(x-r)^{2}}}{n^{2}}}
$$

The ratios of these precision indexes to one another for a normal (or Gaussian) distribution are:

$$
\begin{aligned}
& f: a: \sigma: 1 h: k a: 0.47(1936: 1 \vee \bar{\pi}: \vee \overline{(12)}: 1.000: \sqrt{\pi} \\
& \text { or soughly as } p: a: \sigma: 1 h: k a: 7: 8: 10: 17: 25
\end{aligned}
$$

Most experimental data can be represented by an equation of some form. One of the recommended methods for determining the coefficients of such ecquations is the use of a least-squares solution. This means that an attempt is made to find values for the coefficients such that the sum of the squares of the deviations of the expermental points from the resulting curve has the least pussible value. Certain tables are of help in making such solutions (Tables 16-26), and reference should be made to books or papers on this subject for their use.

An example of one method of finding the coneficients of such selected equations (based on "Treatment of Experimental Data," by Worthing and Geffiner. published by Wiley. 1943) follows.

## Part 1.-Least squares adjustment of measurements of linearly related quantities

Let $Q_{1} . Q_{2} \ldots Q_{k}$ be the $k$ adjusted, but initially unknown. values of the linearly related quantities. Let $\lambda_{1}, X_{2} \ldots X_{n}$ be $n(>k)$ measured values of (ors of linear combinations of two or more, $Q$ 's.

Let $\Delta_{1}, \Lambda_{2} \ldots \Delta_{n}$ be the adjustments or corrections that must be applied to the measured $X$ 's to tield consistent least-squares values for the $Q$ 's. See below for a simple illustration.

As obscratation cquations we have

$$
\begin{align*}
& a_{1} Q_{1}+b_{1} Q_{2}+\ldots k_{2} Q_{k}-X_{1}=\Delta_{1} \\
& a_{2} Q_{1}+b_{2} Q_{2}+\ldots k_{2} Q_{k}-X_{z}=د_{2}  \tag{1}\\
& \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \\
& a_{n} Q_{1}+b_{n} Q_{2}+\ldots k_{n} Q_{k}-X_{n}=د_{n}
\end{align*}
$$

of which $a_{1}, b_{i} \ldots k_{i}$ are constants. whose values are frequently $+1,-1$, or 0 .
From the observation equations $k$ normal ciguations are formed. For equally weighted observed values of $X$. they are

$$
\begin{align*}
& \left.\left[a_{i} a_{i}\right] Q_{1}+\left[a_{i} b_{i}\right] Q+\left[a_{i} c_{i}\right] Q_{3}+\ldots \mid a_{i} k_{i}\right] Q_{k}-\left[a_{1} \mathcal{X}_{i}\right]=0 \tag{2}
\end{align*}
$$

$$
\begin{aligned}
& \left.\left.\left[k_{i} a_{i}\right] Q_{2}+\left[k_{i} h_{i}\right] Q_{2}+\mid k_{i} i_{i}\right] Q_{3}+\ldots \mid k_{i} k_{i}\right] Q_{k}-\left[k_{i} X_{i}\right]=0
\end{aligned}
$$

[^11](continuct)
of which, as representative bracketed [ ] coefficients, we have
\[

$$
\begin{aligned}
& {\left[a_{1} a_{4}\right]=a_{1} a_{1}+a_{2} a_{2}+a_{3} a_{3}+\ldots a_{n} a_{n}} \\
& {\left[a_{1} b_{1}\right]=a_{1} b_{1}+a_{2} b_{2}+a_{3} b_{3}+\ldots a_{n} b_{n}} \\
& {\left[a_{1} X_{1}\right]=a_{1} X_{1}+a_{2} X_{2}+a_{3} X_{3}+\ldots a_{n} X_{n}} \\
& \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \\
& {\left[k_{1} a_{i}\right]=k_{1} a_{1}+k_{2} a_{2}+k_{3} a_{3}+\ldots k_{n} a_{n}}
\end{aligned}
$$
\]

Solutions of equation (2) yield the least-squares adjusted values of $Q_{1}, Q_{2} \ldots Q_{k}$.
For unequally weighted values of $X$, that is $z v_{1}, \tau v_{2}, \ldots \psi_{n}$ for $X_{1} X_{3} \ldots X_{n}$, the normal equations become

$$
\begin{align*}
& {\left[w_{1} a_{i} a_{i}\right] Q_{1}+\left[w_{1} a_{i} b_{1}\right] Q_{2}+\left[w_{1} a_{i} c_{i}\right] Q_{3}+\ldots\left[w_{1} a_{i} k_{1}\right] Q_{k}-\left[w_{i} a_{i} X_{i}\right]=0} \\
& {\left[w_{i} b_{i} a_{1}\right] Q_{1}+\left[w_{i} b_{i} b_{i}\right] Q_{2}+\left[w w_{i} b_{i} c_{1}\right] Q_{3}+\ldots\left[w w_{i} b_{i} k_{i}\right] Q_{k}-\left[w_{i} b_{i} X_{i}\right]=0} \tag{4}
\end{align*}
$$

$$
\left[w_{i} k_{i} a_{i}\right] Q_{1}+\left[w_{i} k_{i} b_{i}\right] Q_{2}+\left[z w_{i} k_{i} c_{1}\right] Q_{3}+\ldots\left[w_{i} k_{i} k_{i}\right] Q_{k}-\left[z w_{i} k_{i} X_{i}\right]=0
$$

of which

$$
\begin{align*}
& {\left[w_{1} a_{i} a_{i}\right]=v e_{r} a_{1} a_{1}+\tau v_{2} a_{2} a_{2}+w w_{3} a_{3} a_{3}+\ldots w_{n} a_{n} a_{n}} \\
& {\left[w_{i} a_{i} b_{4}\right]=w_{1} a_{1} b_{1}+\tau w_{2} a_{2} b_{2}+w w_{3} a_{3} b_{3}+\ldots w_{n} a_{n} b_{n}} \tag{5}
\end{align*}
$$

$$
\left[w_{1} k_{1} a_{4}\right]=w w_{1} k_{1} a_{1}+w w_{2} k_{2} a_{2}+w w_{3} k_{3} a_{3}+\ldots z v_{n} k_{n} a_{n}
$$

The weights $w_{1}, w_{2} \ldots w_{n}$ associated with the $X_{1}, X_{2} \ldots X_{n}$ and with the successive observation equations are taken as inversely proportional to the squares of the probable errors (or of the standard deviations) of the corresponding $X$ 's. It is customary to take simple rounded numbers for the proportional values. A precise set of $28,50,41$, and 78 may be rounded to $3,5,4$, and 8 .

As a simple application, consider the elevations of stations $B, C$, and $D$ above $A$. Let those elevations in order be $Q_{1}, Q_{2}$, and $Q_{3}$. Let the quantities measured and the observed elevations be such as to yield the following observation equations:

$$
\begin{align*}
Q_{1}-10 \mathrm{ft} & =\Delta_{1} \\
Q_{2}-18 \mathrm{ft} & =\Delta_{2} \\
Q_{3}-4 \mathrm{ft} & =\Delta_{3}  \tag{6}\\
-Q_{1}+Q_{2}-9 \mathrm{ft} & =\Delta_{4} \\
Q_{2}-Q_{3}-12 \mathrm{ft} & =\Delta_{\mathrm{s}} \\
Q_{1}-Q_{3}-5 \mathrm{ft} & =\Delta_{6}
\end{align*}
$$

The coefficients $a_{1}, b_{1}$, and $c_{1}$ are seen to be 1,0 , and 0 . The values of the other coefficients are obvious. Substitution in equation (2) yields for the normal equations

$$
\begin{array}{r}
3 Q_{2}-Q_{2}-Q_{3}-6 \mathrm{ft}=0 \\
-Q_{1}+3 Q_{2}-Q_{3}-39 \mathrm{ft}=0  \tag{7}\\
-Q_{1}-Q_{2}+3 Q_{3}+13 \mathrm{ft}=0
\end{array}
$$

Solutions of equation (7) yield $9 \frac{1}{2} \mathrm{ft}, 17 \frac{3}{4} \mathrm{ft}$, and $4 \frac{3}{4} \mathrm{ft}$ for the elevations of $B, C$, and $D$ above $A$.

## Part 2.-Least-squares equations of the type $y=a+b x$, to represent a series of observed ( $x, y$ ) values

For equally weighted pairs of $(x, y)$ of which the errors of measurement are associated with the determinations of the $y$ 's

$$
\begin{align*}
& a=\frac{\Sigma x^{2} \Sigma y-\Sigma x \Sigma x y}{n \Sigma x^{2}-(\Sigma x)^{2}}=\frac{\overline{x^{2}} \bar{y}-\bar{x} \overline{x y}}{\overline{x^{2}}-\overline{x^{2}}} \\
& b=\frac{n \Sigma x y-\Sigma x \Sigma \Sigma}{n \Sigma x^{2}-(\Sigma x)^{2}}=\frac{\overline{x y}-\overline{x y}}{\overline{x^{2}}-\bar{x}^{2}} \tag{8}
\end{align*}
$$

of which

$$
\begin{aligned}
& n x=\Sigma x, n \cdot \overline{x^{2}}=\Sigma x^{2}, \overline{x y}=n \Sigma x y \\
& \bar{n}^{2} \cdot \bar{x}^{2}=(\Sigma x)^{2}, \text { etc. }
\end{aligned}
$$

The probable errors of the $a$ and the $b$ of equation (8) are given by

$$
\begin{align*}
& p_{a}=0.675 \sqrt{\frac{1}{n-2}\left[\frac{\overline{x^{2}} \overline{y^{2}}-2 \bar{x} \bar{y} \overline{x y}+\overline{x^{2}} \overline{y^{2}}}{\overline{x^{2}}-\bar{x}^{2}}-a^{2}\right]} \\
& p_{b}=0.675 \sqrt{\frac{1}{n-2}\left[\frac{\overline{y^{2}}-\overline{y^{2}}}{\overline{x^{2}}-\overline{x^{2}}}-b^{2}\right]} \tag{9}
\end{align*}
$$

For unequally weighted measurements of which the errors of measurement are associated with the determinations of the $y$ 's,

$$
\begin{align*}
& a=\frac{\Sigma w_{i} x_{i}{ }^{2} \Sigma w_{i} y_{i}-\Sigma w_{i} x_{i} \Sigma w_{i} x_{i} y_{i}}{\Sigma w^{\prime} \Sigma w_{i} x_{i}{ }^{2}-\left(\Sigma w_{i} x_{i}\right)^{2}} \\
& b=\frac{\Sigma w^{2} w_{i} x_{i} y_{i}-\Sigma w_{i} x_{i} \Sigma w_{i} y_{i}}{\Sigma w_{i} \Sigma w_{i} x_{i}{ }^{2}-\left(\Sigma w_{i}^{\prime} x_{i}\right)^{2}} \tag{10}
\end{align*}
$$

Where the errous of measurement are associated with the $x$-determination only, the corresponding coefficients of an equation of the type $x=a^{\prime}+b^{\prime} y$ can be obtained by merely interchanging $x$ and $y$ in equation (8).

Where the errors of measurement are associated with both the $x$ - and the $y$-determinations, the expressions are complicated. ${ }^{13}$

[^12]
## Part 3.-Least-squares equation of the type $y=a+b x+c x^{2}+d x^{3}$ to represent $a$ series of observed $(x, y)$ values

For the general case involving irregularly spaced $x$-values, the formulae for $a, b, c$, etc., are very complex. ${ }^{14}$ However, for the case of equally weighted observations with errors of measurement associated entirely with the $y$-values in which succeeding $x$-values are equally spaced, the mechanics of the computations for least-squares constants are very greatly simplified, thanks to tables computed by Baily ${ }^{35}$ and by Cox and Matuschak. ${ }^{16}$ The procedure requires a change of the $x$-variable to yield a new $X$-variable with a zero-value at the midpoint of the series. In case of an even number of terms, the shift is given by

$$
\begin{equation*}
X_{e}=\frac{x-\bar{x}}{\Delta x} \tag{11}
\end{equation*}
$$

of which $\Delta x$ is the even spacing between successive $x$-values; and, if the number of terms is odd, the shift is given by

$$
\begin{equation*}
X_{0}=\frac{x-\bar{x}}{\Delta x / 2} \tag{12}
\end{equation*}
$$

The further procedure consists in determining the appropriate summations indicated in Table 17, the appropriate $k$-terms given as a function of the number of terms $n$ in Tables 19 and 20 , combining the appropriate summations and $k$-terms, to give parameters for the equation $y=f(X)$, and finally transferring the function to the original coordinate system to yield $y=f_{2}(x)$.

How to apply the simplified procedure to determine the coefficient of $x^{2}$ in the leastsquares equation $y=a+b x+c x^{2}$ to represent the $x y$ values of the first two columns of the following tabulations is shown in the remainder of the tabulation.

| $x$ |  |  |  |  |
| :---: | :---: | :---: | ---: | :---: |
| $\frac{x}{(\mathrm{sec})}$ | $\frac{y}{(\mathrm{~cm})}$ | $X$ | $\frac{X^{2} y}{(\mathrm{~cm})}$ | $c^{\prime}=k_{5} \Sigma X^{2} y-k_{4} \Sigma y$ |
| 3 | 12.0 | -5 | 300.0 | $n=6$ |
| 6 | 20.6 | -3 | 185.4 | $k_{5}=16,741,071 \times 10^{-10}$ |
| 9 | 33.7 | -1 | 33.7 | $k_{4}=19,531,250 \times 10^{-9}$ |
| 12 | 51.1 | +1 | 51.1 | $k_{5} \Sigma X^{2} y=6.2005 \mathrm{~cm}$ |
| 15 | 72.9 | +3 | 656.1 | $k_{4} \Sigma y=5.6523 \mathrm{~cm}$ |
| 18 | 99.1 | +5 | 2477.5 | $c^{\prime}=0.5482 \mathrm{~cm}$ |
|  | -- |  | --- | $\Delta x=3 \mathrm{sec}$ |
|  | 289.4 |  | 3703.8 | $c$ |

[^13]40

## TABLE 17.-SHOWING THE MAKE.UP OF THE CONSTANTS OF THE LEASTSQUARES EQUATION OF THE TYPE $y=a+b x+c x^{2}+d x^{3}$ FOR EQUA. TIONS OF VARYING DEGREES WHEN THE ABBREVIATED METHOD OF BAILEY AND OF COX AND MATUSCHAK IS USED*

This method is applicable only when succeeding values of $x$ have a common difference and are equally weighted. The independent variable, changed if necessary, must have a zero value at the midpoint of the scries with succeeding values differing by unity if the number of terms is odd and by two if even. Values for the various $k$ 's, as computed by Cox and Matuschak, are to be found in Tables 14 and 20.

| Degree of equation | Parameters |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $a$ | $b$ | c | d |
| 1 | $k, \Sigma y$ | $k_{2} \Sigma x y$ |  |  |
| 2 | $k_{3} \Sigma y^{\prime}-k_{4} \Sigma x^{2} y$ | $k_{2} \Sigma x y$ | $k_{5} \Sigma x^{2} y-k_{4} \Sigma y^{\prime}$ |  |
| 3 | $k_{3} \Sigma y-k_{s} \Sigma x^{2} y$ | $k_{0} \Sigma . r y-k_{i} \Sigma x^{3} y$ | $k_{5} \Sigma x^{2} y-k_{5} \Sigma y$ | $k_{8} \Sigma x^{3} y-k_{7} \Sigma x y$ |

* For references, see footnotes 15 and 16 , p. 39.

TABLE 18.-VALUES OF $P=\frac{2}{\sqrt{\pi}} \int_{0}^{h x} e^{-(h x) 2} d(h x)$
$P$, the probability of an observational error having a value positive or negative equal to or less than $x$ when $h$ is the measure of precision, $P=\frac{2}{V \pi} \int_{0}^{h_{x}} e^{-(h x) 2} d(h x) \cdot h^{2}=\left(\frac{1}{2} m \Delta x^{2}\right)$ where $m=$ no. obs. of deviation $\Delta x$.

| $h \boldsymbol{x}$ | $\mathbf{0}$ | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{0 . 0}$ |  | .01128 | .02256 | .03384 | .04511 | .05637 | .06762 | .07886 | .09008 | .10128 |  |
| $\mathbf{1}$ | .11246 | .12362 | .13476 | .14587 | .15695 | .16800 | .17901 | .18999 | .20094 | .21184 |  |
| .2 | .22270 | .23352 | .24430 | .25502 | .26570 | .27633 | .28690 | .29742 | .30788 | .31828 |  |
| .3 | .32863 | .33891 | .34913 | .35928 | .36936 | .37938 | .38933 | .39921 | .40901 | .41874 |  |
| .4 | .42839 | .43797 | .44747 | .45689 | .46623 | .47548 | .48466 | .49375 | .50275 | .51167 |  |
| $\mathbf{0 . 5}$ | .52050 | .52924 | .53790 | .54646 | .55494 | .56332 | .57162 | .57982 | .58792 | .59594 |  |
| .6 | .60386 | .61168 | .61941 | .62705 | .63459 | .64203 | .64938 | .65663 | .66378 | .67084 |  |
| .7 | .67780 | .68467 | .69143 | .69810 | .70468 | .71116 | .71754 | .72382 | .73001 | .73610 |  |
| .8 | .74210 | .74800 | .75381 | .75952 | .76514 | .77067 | .77610 | .78144 | .78669 | .79184 |  |
| .9 | .79691 | .80188 | .80677 | .81156 | .81627 | .82089 | .82542 | .82987 | .83423 | .83851 |  |
| $\mathbf{1 . 0}$ | .84270 | .84681 | .85084 | .85478 | .85865 | .86244 | .86614 | .86977 | .87333 | .87680 |  |
| .1 | .88021 | .88353 | .88679 | .88997 | .89308 | .89612 | .89910 | .90200 | .90484 | .90761 |  |
| .2 | .91031 | .91296 | .91553 | .91805 | .92051 | .92290 | .92524 | .92751 | .92973 | .93190 |  |
| .3 | .93401 | .93606 | .93807 | .94002 | .94191 | .94376 | .94556 | .94731 | .94902 | .95067 |  |
| .4 | .95229 | .95385 | .95538 | .95686 | .95830 | .95970 | .96105 | .96237 | .96365 | .96490 |  |
| $\mathbf{1 . 5}$ | .96611 | .96728 | .96841 | .96952 | .97059 | .97162 | .97263 | .97360 | .97455 | .97546 |  |
| .6 | .97635 | .97721 | .97804 | .97884 | .97962 | .98038 | .98110 | .98181 | .98249 | .98315 |  |
| .7 | .98379 | .98441 | .98500 | .98558 | .98613 | .98667 | .98719 | .98769 | .98817 | .98864 |  |
| .8 | .98909 | .98952 | .98994 | .99035 | .99074 | .99111 | .99147 | .99182 | .99216 | .99248 |  |
| .9 | .99279 | .99309 | .99338 | .99366 | .99392 | .99418 | .99443 | .99466 | .99489 | .99511 |  |
| $\mathbf{2 . 0}$ | .99532 | .99552 | .99572 | .99591 | .99609 | .99626 | .99642 | .99658 | .99673 | .99688 |  |
| .1 | .99702 | .99715 | .99728 | .99741 | .99753 | .99764 | .99775 | .99785 | .99795 | .99805 |  |
| .2 | .99814 | .99822 | .99831 | .99839 | .99846 | .99854 | .99861 | .99867 | .99874 | .99880 |  |
| .3 | .99886 | .99891 | .99897 | .99902 | .99906 | .99911 | .99915 | .99920 | .99924 | .99928 |  |
| .4 | .99931 | .99935 | .99938 | .99941 | .99944 | .99947 | .99950 | .99952 | .99955 | .99957 |  |
| $\mathbf{2} \mathbf{5}$ | .99959 | .99961 | .99963 | .99965 | .99967 | .99969 | .99971 | .99972 | .99974 | .99975 |  |
| .6 | .99976 | .99978 | .99979 | .99980 | .99981 | .99982 | .99983 | .99984 | .99985 | .99986 |  |
| .7 | .99987 | .99987 | .99988 | .99989 | .99989 | .99590 | .99991 | .99991 | .99992 | .99992 |  |
| .8 | .99992 | .99993 | .99993 | .99994 | .99994 | .99994 | .99995 | .99995 | .99995 | .99996 |  |
| .9 | .99996 | .99996 | .99996 | .99997 | .99997 | .99997 | .99997 | .99997 | .99997 | .99998 |  |
| $\mathbf{3 . 0}$ | .99998 | .99999 | .99999 | 1.00000 |  |  |  |  |  |  |  |

TABLE 19.-VALUES OF THE CONSTANTS, $k_{n}$, ENTERING LEAST-SQUARES SOLUTIONS, USING THE ABBREVIATED METHOD OF BAILY AND OF COX AND MATUSCHAK, WHEN THE NUMBER OF TERMS, $n$, IS ODD*

The numbers in parentheses show the negative powers of 10 by which the adjacent numbers must be multiplied in order to obtain appropriate $k_{n}$ 's. To illustrate, $k_{2}$ for $n=13$ is $54,945,055 \times 10^{-10}$.

| $n$ | $k_{1}$ | $\mathrm{k}_{2}$ | $k_{3}$ | $k_{4}$ | $k_{5}$ | $k_{0}$ | $k_{7}$ | $k_{*}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 3333 3333(8) | $50000000(8)$ | $10000000(7)$ | 1000 0000(7) | 15000000 (7) |  |  |  |
| 5 | 20000000 | 10000000 | 4857 1429(8) | 1428 5714(6) | 71428571 (9) | 9027 7778(8) | 2361 1111(8) | 6944 4444(9) |
| 7 | 14285714 | 3571 4286(9) | 33333333 | 4761 9048(9) | 11504762 | 26256614 | 32407407 (9) | 4629 6296(10) |
| 9 | 11111111 | 16666667 | 25541126 | 21645022 | $32467532(10)$ | 11433782 | 8277 2166(10) | $70145903(11)$ |
| 11 | 9090 9091(9) | 90909091 (10) | 20745921 | 11655012 | 11655012 | 6037 9435(9) | 28813779 | 16187516 |
| 13 | 76923077 | 54945055 | 17482517 | $69930070(10)$ | $49950050(11)$ | 35846098 | 12140637 | $48562549(12)$ |
| 15 | 66666667 | 35714286 | 15113122 | 45248869 | 24240465 | 23045899 | 58306799 (11) | 17457125 |
| 17 | 58823529 | 24509803 | 13312693 | 30959752 | 12899897 | 15702041 | 30816420 | 7166 6093(13) |
| 19 | 52631579 | 17543860 | 11897391 | 22114109 | $73713696(12)$ | 11183168 | 17525617 | 32575497 |
| 21 | 47619048 | 12987013 | 10755149 | 16345211 | 44577848 | 8248 5070(10) | 10562015 | 16051694 |
| 23 | 43478261 | $98814229(11)$ | 9813 6646(9) | 12422360 | 28232637 | 62590791 | 6672 0719(12) | 8445 6606(14) |
| 25 | 40000000 | 76923077 | 90241546 | $96518357(11)$ | 18580453 | 48623545 | 43823595 | 46920337 |
| 27 | 37037037 | 61050061 | 83524904 | 76628352 | 12631047 | 38527423 | 29745336 | 27289299 |
| 29 | 34482759 | 49261084 | 77740700 | 61797058 | 8828 1512(13) | 31047316 | 20764076 | 16505625 |
| 31 | 32258065 | 40322581 | 72707048 | 50561230 | 63201537 | 25386983 | 14850296 | 10327049 |
| 33 | 30303030 | 33422460 | 68286552 | 41893590 | 46206166 | 21024471 | 10847991 | 6655 2091(15) |
| 35 | 28571429 | 28011204 | 64373464 | 35100035 | 34411799 | 17607811 | 80734407 (13) | 44020942 |
| 37 | 27027027 | 23707918 | 60885061 | 29700030 | 26052658 | 14893734 | 61087522 | 29798791 |
| 39 | 25641026 | 20242915 | 57755692 | 25353684 | 20016066 | 12710408 | 46910081 | 20592661 |
| 41 | 24390244 | 17421603 | 54932589 | 21815961 | 15582829 | 10934097 | 36504910 | 14497581 |
| 43 | 23255814 | 15101178 | 52372849 | 18907166 | 12277380 | 94741490 (11) | 28751015 | 10379428 |
| 45 | 22222222 | 13175231 | 50041234 | 16493485 | 97787451 (14) | 82631159 | 22892527 | $75453288(16)$ |
| 47 | 21276596 | 11563367 | 47908525 | 14473875 | 78662362 | 72501033 | 18410171 | 55619852 |
| 49 | 20408163 | 10204082 | 45950295 | 12771066 | 63855329 | 63962170 | 14941103 | 41526134 |
| 51 | 19607843 | 9049 7738(12) | 44145960 | 11325285 | 52270545 | 56713855 | 12227830 | 31369497 |

* For references, see footnotes 15 and 16, 1. 39
TABLE 20.-VALUES OF THE CONSTANTS, $k_{n}$, ENTERING LEAST-SQUARES SOLUTIONS, USING THE ABBREVIATED METHOD OF BAILY AND OF COX AND MATUSCHAK, WHEN THE NUMBER OF TERMS, $n$, IS EVEN *

| 4 | $k_{1}$ | $k_{2}$ | $k_{3}$ | $k_{4}$ | $k_{5}$ | $k_{6}$ | $k_{7}$ | $k_{8}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 2500 0000(8) | 5000 0000(9) | $64062500(8)$ | 7812 5030(9) | 15625000 (9) | 6336 8056(8) | 7118 0556(9) | 8680 5556(10) |
| 6 | 16666667 | 14285714 | 39453125 | 19531250 | 1674 1071(10) | 11267499 | $48707562(10)$ | $\begin{aligned} & 80805356(10) \\ & 24112654(11) \end{aligned}$ |
| 8 | 12500000 | 59523810 (10) | 28906250 | 7812 5000(10) | 3720 2381(11) | $41963534(9)$ | $48327441(11)$ | $24112654(11)$ 2630 4714(12) |
| 10 | 10000000 | 30303030 | 22890625 | 39062500 | 11837121 | 20401329 | 29643389 | 5058 5988(13) |
| 12 | 8333 3333(9) | 17482517 | 18973214 | 22321429 | $46828172(12)$ | 11494485 | 11466157 | 13489597 |
| 14 | 71428571 | 10989011 | 16210938 | 13950893 | 21462912 | 71256741 (10) | $51865517(12)$ | 4463 4695(14) |
| 16 | 62500000 | $73529412(11)$ | 14155506 | 93005952 (11) | 10941877 | 47259799 | 26220143 | 17227426 |
| 18 | 55555556 | 51599587 | 12565104 | 65104167 | 6046 8266(13) | 32967149 | 14407871 | 7465 2181(15) |
| 20 | 50000000 | 37593985 | 11297349 | 47348485 | 35600365 | 23917243 | 84483844 (13) | 35408149 |
| 22 | 45454545 | 28232637 | 10262784 | 35511364 | 22056748 | 17905616 | 52188071 | 18058156 |
| 24 | 41666667 | 21739130 | 9402 3164(9) | 27316434 | 14252052 | 13754794 | 33645781 | 9775 0702(16) |
| 26 | 38461538 | 17094017 | 86753091 | 21462912 | 95390720 (14) | 10795940 | 22480302 | 55616779 |
| 28 | 35714286 | 13683634 | 80528846 | 17170330 | 65786704 | $86295508(11)$ | 15482276 | 33011249 |
| 30 | 33333333 | 11123471 | 75139509 | 13950893 | 46554704 | 70068080 | 10944042 | 20319424 |
| 32 | 31250000 | 9164 2229(12) | 70427390 | 11488971 | 33691596 | 57671532 | 7913 1009(14) | 12908811 |
| 34 | 29411765 | 76394194 | 66272213 | 9574 1423(12) | 24867902 | 48037846 | 58362361 | 84314304 (17) |
| 36 | 27777778 | 64350064 | 62580624 | 80624358 | 18677458 | 40437597 | 43806481 | 56437105 |
| 38 | 26315789 | 54710581 | 59279058 | 68530703 | 14247547 | 34360952 | 33398722 | 38611239 |
| 40 | 25000000 | 46904315 | 56308741 | 57740602 | 11020751 | 29444203 | 25822837 | 26938074 |
| 42 | 23809524 | 40515355 | 53622160 | 50730520 | 8632 5332(15) | 25423116 | 20219092 | 19128753 |
| 44 | 22727273 | 35236081 | 51180477 | 44113495 | 68393016 | 22102564 | 16013580 | 13802431 |
| 46 | 21739130 | 30835646 | 48951643 | 38599309 | 54750792 | 19336316 | 12815606 | 10105351 |
| 48 | 20833333 | 27138515 | 46908968 | 33967392 | 44247580 | 17013314 | 10354426 | 7497 7742(18) |
| 50 | 20000000 | 24009604 | 45030048 | 30048077 | 36072121 | 15048177 | 84393542 (15) | 56314922 |

* For references, see footnotes 15 and 16, p. 39.

| $\boldsymbol{x}$ | $e^{x}$ | $\log e^{x}$ | $e^{-x}$ |  | $e^{x}$ | $\log e^{x}$ | $e^{-x}$ |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $1 / 64$ | 1.0157 | 0.00679 | 0.98450 | $1 / 3$ | 1.3956 | 0.14476 | 0.71653 |
| $1 / 32$ | .0317 | .01357 | .96923 | $1 / 2$ | .6487 | .21715 | .60653 |
| $1 / 16$ | .0645 | .02714 | .93941 | $3 / 4$ | 2.1170 | .32572 | .47237 |
| $1 / 10$ | .1052 | .04343 | .90484 | 1 | . .7183 | .43429 | .36788 |
| $1 / 9$ | .1175 | .04825 | .89484 | $5 / 4$ | 3.4903 | .54287 | .28650 |
| $1 / 8$ | 1.1331 | 0.05429 | 0.88250 | $3 / 2$ | 4.4817 | 0.65144 | 0.22313 |
| $1 / 7$ | .1536 | .06204 | .86688 | $7 / 4$ | 5.7546 | .76002 | .17377 |
| $1 / 6$ | .1814 | .07238 | .84648 | 2 | 7.3891 | .86859 | .13534 |
| $1 / 5$ | .2214 | .08686 | .81873 | $9 / 4$ | 9.4877 | .97716 | .10540 |
| $1 / 4$ | .2840 | .10857 | .77880 | $5 / 2$ | 12.1825 | 1.08574 | .08208 |

## TABLE 22.-FURTHER VALUES OF P

This table gives the values of the probability $P$, as defined in Table 18 , corresponding to different values of $x / r$ where $r$ is the "probable error." The probable error $r$ is equal to $0.47694 / h$.

| $\frac{x}{r}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 | . 00000 | . 00538 | . 01076 | . 01614 | . 02152 | . 02690 | . 03228 | . 03766 | . 04303 | . 04840 |
| 0.1 | . 05378 | . 05914 | . 06451 | . 06987 | . 07523 | . 08059 | . 08594 | . 09129 | . 09663 | . 10197 |
| 0.2 | . 10731 | . 11264 | . 11796 | . 12328 | . 12860 | . 13391 | . 13921 | . 14451 | . 14980 | . 15508 |
| 0.3 | . 16035 | . 16562 | . 17088 | . 17614 | . 18138 | . 18662 | . 19185 | . 19707 | . 20229 | . 20749 |
| 0.4 | . 21268 | . 21787 | . 22304 | . 22821 | . 23336 | . 23851 | . 24364 | . 24876 | . 25388 | . 25898 |
| 0.5 | . 26407 | . 26915 | . 27421 | . 27927 | . 28431 | . 28934 | . 29436 | . 29936 | . 30435 | . 30933 |
| 0.6 | . 31430 | . 31925 | . 32419 | . 32911 | . 33402 | . 33892 | . 34380 | . 34866 | . 35352 | . 35835 |
| 0.7 | . 36317 | . 36798 | . 37277 | . 37755 | . 38231 | . 38705 | . 39178 | . 39649 | . 40118 | . 40586 |
| 0.8 | . 41052 | . 41517 | . 41979 | . 42440 | . 42899 | . 43357 | . 43813 | . 44267 | . 44719 | . 45169 |
| 0.9 | . 45618 | . 46064 | . 46509 | . 46952 | . 47393 | . 47832 | . 48270 | . 48705 | . 49139 | . 49570 |
| 1.0 | . 50000 | . 50428 | . 50853 | . 51277 | . 51699 | . 52119 | . 52537 | . 52952 | . 53366 | . 53778 |
| 1.1 | . 54188 | . 54595 | . 55001 | . 55404 | . 55806 | . 56205 | . 56602 | . 56998 | . 57391 | . 57782 |
| 1.2 | . 58171 | . 58558 | . 58942 | . 59325 | . 59705 | . 60083 | . 60460 | . 60833 | . 61205 | . 61575 |
| 1.3 | . 61942 | . 62308 | . 62671 | . 63032 | . 63391 | . 63747 | . 64102 | . 64454 | . 64804 | . 65152 |
| 1.4 | . 65498 | . 65841 | . 66182 | . 66521 | . 66858 | . 67193 | . 67526 | . 67856 | . 68184 | . 68510 |
| 1.5 | . 68833 | . 69155 | . 69474 | . 69791 | . 70106 | . 70419 | . 70729 | . 71038 | . 71344 | . 71648 |
| 1.6 | . 71949 | . 72249 | . 72546 | . 72841 | . 73134 | . 73425 | . 73714 | . 74000 | . 74285 | . 74567 |
| 1.7 | . 74847 | . 75124 | . 75400 | . 75674 | . 75945 | . 76214 | . 76481 | . 76746 | . 77009 | . 77270 |
| 1.8 | . 77528 | . 77785 | . 78039 | . 78291 | . 78542 | . 78790 | . 79036 | . 79280 | . 79522 | . 79761 |
| 1.9 | . 79999 | . 80235 | . 80469 | . 80700 | . 80930 | . 81158 | . 81383 | . 81607 | . 81828 | . 82048 |
| 2.0 | . 82266 | . 82481 | . 82695 | . 82907 | . 83117 | . 83324 | . 83530 | . 83734 | . 83936 | . 84137 |
| 2.1 | . 84335 | . 84531 | . 84726 | . 84919 | . 85109 | . 85298 | . 85486 | . 85671 | . 85854 | . 86036 |
| 2.2 | . 86216 | . 86394 | . 86570 | . 86745 | . 86917 | . 87088 | . 87258 | . 87425 | . 87591 | . 87755 |
| 2.3 | . 87918 | . 88078 | . 88237 | . 88395 | . 88550 | . 88705 | . 88857 | . 89008 | . 89157 | . 89304 |
| 2.4 | . 89450 | . 89595 | . 89738 | . 89879 | . 90019 | . 90157 | . 90293 | . 90428 | . 90562 | . 90694 |
| 2.5 | . 90825 | . 90954 | . 91082 | . 91208 | . 91332 | . 91456 | . 91578 | . 91698 | . 91817 | . 91935 |
| 2.6 | . 92051 | . 92166 | . 92280 | . 92392 | . 92503 | . 92613 | . 92721 | . 92828 | . 92934 | . 93038 |
| 2.7 | . 93141 | . 93243 | . 93344 | . 93443 | . 93541 | . 93638 | . 93734 | . 93828 | . 93922 | . 94014 |
| 2.8 | . 94105 | . 94195 | . 94284 | . 94371 | . 94458 | . 94543 | . 94627 | . 94711 | . 94793 | . 94874 |
| 2.9 | . 94954 | . 95033 | . 95111 | . 95187 | . 95263 | . 95338 | . 95412 | . 95484 | . 95557 | . 95628 |
|  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 3 | . 95698 | . 96346 | . 96910 | . 97397 | . 97817 | . 98176 | . 98482 | . 98743 | . 98962 | . 99147 |
| 4 | . 99302 | . 99431 | . 99539 | . 99627 | . 99700 | . 99760 | . 99808 | . 99848 | . 99879 | . 99905 |
| 5 | . 99926 | . 99943 | . 99956 | . 99966 | . 99974 | . 99980 | . 99985 | . 99988 | . 99991 | . 99993 |

This factor occurs in the equation $r_{s}=0.6745 \sqrt{\frac{\Sigma v^{2}}{n-1}}$ for the probable error of a single observation, and other similar equations.

| $n$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 00 |  |  | 0.6745 | 0.4769 | 0.3894 | 0.3372 | 0.3016 | 0.2754 | 0.2549 | 0.2385 |
| 10 | 0.2248 | 0.2133 | . 2034 | . 1947 | . 1871 | . 1803 | . 1742 | . 1686 | . 1636 | . 1590 |
| 20 | . 1547 | . 1508 | . 1472 | . 1438 | . 1406 | . 1377 | . 1349 | . 1323 | . 1298 | . 1275 |
| 30 | . 1252 | . 1231 | . 1211 | . 1192 | . 1174 | . 1157 | . 1140 | . 1124 | . 1109 | . 1094 |
| 40 | . 1080 | . 1066 | . 1053 | . 1041 | . 1029 | . 1017 | . 1005 | . 0994 | . 0984 | . 0974 |
| 50 | 0.0964 | 0.0954 | 0.0944 | 0.0935 | 0.0926 | 0.0918 | 0.0909 | 0.0901 | 0.0893 | 0.0886 |
| 60 | . 0878 | . 0871 | . 0864 | . 0857 | . 0850 | . 0843 | . 0837 | . 0830 | . 0824 | . 0818 |
| 70 | . 0812 | . 0806 | . 0800 | . 0795 | . 0789 | . 0784 | . 0779 | . 0774 | . 0769 | . 0764 |
| 80 | . 0759 | . 0754 | . 0749 | . 0745 | . 0740 | . 0736 | . 0732 | . 0727 | . 0723 | . 0719 |
| 90 | . 0715 | . 0711 | . 0707 | . 0703 | . 0699 | . 0696 | . 0692 | . 0688 | . 0685 | . 0681 |

TABLE 24.-VALUES OF THE FACTOR $0.6745 \sqrt{\frac{1}{n(n-1)}}$
This factor occurs in the equation $r_{0}=0.6745 \sqrt{\frac{\Sigma v^{2}}{n(n-1)}}$ for the probable error of the arithmetical mean.

| $n$ |  | $\mathbf{1}$ | $\mathbf{2}$ |  | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $\mathbf{n}$ |  |  | 0.4769 | 0.2754 | 0.1947 | 0.1508 | 0.1231 | 0.1041 | 0.0901 | 0.0795 |
| $\mathbf{0 0}$ | 0.0711 | 0.0643 | .0587 | .0540 | .0500 | .0465 | .0435 | .0409 | .0386 | .0365 |
| 10 | .0346 | .0329 | .0314 | .0300 | .0287 | .0275 | .0265 | .0255 | .0245 | .0237 |
| 20 | .0229 | .0221 | .0214 | .0208 | .0201 | .0196 | .0190 | .0185 | .0180 | .0175 |
| 30 | .0171 | .0167 | .0163 | .0159 | .0155 | .0152 | .0148 | .0145 | .0142 | .0139 |
| 40 | .0136 | 0.0134 | 0.0131 | 0.0128 | 0.0126 | 0.0124 | 0.0122 | 0.0119 | 0.0117 | 0.0115 |
| $\mathbf{5 0}$ | .0113 | .0111 | .0110 | .0108 | .0106 | .0105 | .0103 | .0101 | .0100 | .0098 |
| 60 | .0113 | .0096 | .0094 | .0093 | .0092 | .0091 | .0089 | .0088 | .0087 | .0086 |
| 70 | .0097 | .0084 | .0083 | .0082 | .0081 | .0000 | .0079 | .0078 | .0077 | .0076 |
| 80 | .0085 | .0075 | .0074 | .0073 | .0072 | .0071 | .0071 | .0070 | .0069 | .0068 |
| 0 | .0075 | .0075 |  |  |  |  |  |  |  |  |

Part 1.-Values of the factor $0.8453 \sqrt{\frac{1}{n(n-1)}}$
This factor occurs in the approximate equation $r=0.8453 \frac{\Sigma|v|}{\sqrt{n(n-1)}}$ for the probable error of a single observation.

| $n$ |  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $\mathbf{0 0}$ |  |  | 0.5978 | 0.3451 | 0.2440 | 0.1890 | 0.1543 | 0.1304 | 0.1130 | 0.0996 |
| 10 | 0.0891 | 0.0806 | .0736 | .0677 | .0627 | .0583 | .0546 | .0513 | .0483 | .0457 |
| 20 | .0434 | .0412 | .0393 | .0376 | .0360 | .0345 | .0332 | .0319 | .0307 | .0297 |
| 30 | .0287 | .0277 | .0268 | .0260 | .0252 | .0245 | .0238 | .0232 | .0225 | .0220 |
| 40 | .0214 | .0209 | .0204 | .0199 | .0194 | .0190 | .0186 | .0182 | .0178 | .0174 |
| $\mathbf{5 0}$ | 0.0171 | 0.0107 | 0.0164 | 0.0161 | 0.0158 | 0.0155 | 0.0152 | 0.0150 | 0.0147 | 0.0145 |
| 60 | .0142 | .0140 | .0137 | .0135 | .0133 | .0131 | .0129 | .0127 | .0125 | .0123 |
| 70 | .0122 | .0120 | .0118 | .0117 | .0115 | .0113 | .0112 | .0111 | .0109 | .0108 |
| 80 | .0106 | .0105 | .0104 | .0102 | .0101 | .0100 | .0099 | .0098 | .0097 | .0090 |
| 90 | .0094 | .0093 | .0092 | .0091 | .0090 | .0089 | .0089 | .0088 | .0087 | .0086 |

$$
\text { Part 2.-Values of } 0.8453 \frac{1}{n \sqrt{n-1}}
$$

This factor occurs in the approximate equation $r_{0}=0.8453 \frac{\Sigma|v|}{n \sqrt{n-1}}$ for the probable error of the arithmetical mean.

| $n$ |  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ | $\mathbf{9}$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $\mathbf{0 0}$ |  |  | 0.4227 | 0.1993 | 0.1220 | 0.0845 | 0.0630 | 0.0493 | 0.0399 | 0.0332 |
| 10 | 0.0282 | 0.0243 | .0212 | .0188 | .0167 | .0151 | .0136 | .0124 | .0114 | .0105 |
| 20 | .0097 | .0090 | .0084 | .0078 | .0073 | .0369 | .0065 | .0061 | .0058 | .0055 |
| 30 | .0052 | .0050 | .0047 | .0045 | .0043 | .0041 | .0040 | .0038 | .0037 | .0035 |
| 40 | .0034 | .0033 | .0031 | .0030 | .0029 | .0028 | .0027 | .0027 | .0026 | .0025 |
| $\mathbf{5 0}$ | 0.0024 | 0.0023 | 0.0023 | 0.0022 | 0.0022 | 0.0021 | 0.0020 | 0.0020 | 0.0019 | 0.0019 |
| 60 | .0018 | .0018 | .0017 | .0017 | .0017 | .0016 | .0016 | .0016 | .0015 | .0015 |
| 70 | .0015 | .0014 | .0014 | .0014 | .0013 | .0013 | .0013 | .0013 | .0012 | .0012 |
| 80 | .0012 | .0012 | .0011 | .0011 | .0011 | .0011 | .0011 | .0010 | .0010 | .0010 |
| 90 | .0010 | .0010 | .0010 | .0009 | .0009 | .0009 | .0009 | .0009 | .0009 | .0009 |

Some of the most important results of physical science are embodied in the numerical magnitudes of various universal physical constants. The accurate determination of such constants has engaged the time and labor of many of the most eminent scientists. Some of these constants can be evaluated by various methods. The experiments used to study and measure these constants, in many instances have yielded some function of two or more of the constants (see Table 26) such as $h / e ; e / m, F / N, h / m, m N, F(e / m), e^{2} /(m / h)$, etc., rather than the direct value of the constant. Each of the many relations has been investigated by various experimenters at various times, and each investigation normally produces a result more or less different from that of any other investigation. Under such conditions there arises a general and continuous need for a searching examination of the most probable value of each important constant. This makes necessary some comparison and analysis of all these experimental data to arrive at the most probable value. An important factor in such work is that there are but few of the constants that do not require for their evaluation a knowledge of certain other constants. These relations are so extensive that most of the physical constants can be calculated from the value of five or six of the selected principal constants and certain ratios.

Many such critical reviews of these natural constants and conversion factors have appeared in the last 30 to 40 years. The data and discussion given here for the constants and their probable errors are the values arrived at by three physicists, R. T. Birge, ${ }^{17}$ J. W. DuMond, and J. A. Bearden, and their associates, who have made some very careful reviews and critical studies of the published experimental data on these general physical constants and have published several papers giving what they consider as the most probable value. Reference should be made to their original papers for details.

Birge says in his 1941 paper that as a result of such critical work the situation in respect to these constants has vastly improved over values of about 10 years ago, and again one can say that such studies have resulted in more work and thus a more accurate set of constants.

In 1941 Birge ${ }^{17}$ published a very extended list of physical constants and gave calculated values of many other physical constants that depend upon the fundamental constants. Because of the extent of this list, and also because so many of the relations among these constants are given therein, this 1941 list is given here. Almost all these constants in this table (Table 26) are accurate within the limits given.

DuMond and Cohen ${ }^{18}$ prepared a table of some of these constants for the Atomic Energy Commission. A part of this appeared in the July 1953 issue of the Review of Modern Physics. Table 27 gives their values of a number of these physical constants.

Bearden and Watts ${ }^{184}$ in 1950 made a study of values of a number of physical constants, using some new values in their calculations. They are continuing this work and are now ${ }^{18 \mathrm{~b}}$ offering some new and more accurate values. Table 28 contains their 1950 values (corrected for their newer values) and newer calculated values of some additional constants.

A comparison of the final values of these fundamental physical constants arrived at by these physicists shows in a real manner the accuracy that may now be claimed. A number of the principal radiation constants were taken from these tables (Tables 26-28) and are given in Table 53. These values have been used for the calculations in the tables in this book since they were available when the work was started and since the newer values would make no practical changes.

[^14]
## Part 1.—Principal constants and ratios



## Part 2.-Atomic weights

(1) Physical scale $\left(\mathrm{O}^{16}=16.0000\right)$

$$
\begin{array}{ll}
{ }_{1} \mathrm{H}^{\mathrm{d}}=1.00813 \pm 0.00001_{7} \\
{ }_{1} \mathrm{H}=1.00827_{\mathrm{e}} \pm 0.0001_{7} & { }_{3} \mathrm{H}^{2}=2.01473 \pm 0.00001 \text {, }
\end{array}
$$

$$
{ }_{2} \mathrm{He}^{4}=4.00389 \pm 0.00007
$$

$$
\text { (from H }{ }^{1} / \mathrm{H}^{2} \text { abundance }=6900 \pm 100 \text { ) }
$$

$$
{ }^{2} \mathrm{C}^{12}=12.00386 \pm 0.0004 \quad{ }_{\circ} \mathrm{C}^{13}=13.00761 \pm 0.00015
$$

$$
\mathrm{C}=12.01465 \pm 0.00023
$$

$$
\text { (from } \mathrm{C}^{12} / \mathrm{C}^{13} \text { abundance }=92 \pm 2 \text { ) }
$$

$$
{ }_{7} \mathrm{~N}^{14}=14.00753 \pm 0.00005 \quad{ }_{7} \mathrm{~N}^{18}=15.0049 \pm 0.0002
$$

$$
\mathrm{N}=14.01121 \pm 0.00009_{\mathrm{s}}
$$

$$
\text { (from } N^{14} / N^{15} \text { abundance }=270 \pm 6 \text { ) }
$$

$$
{ }_{8} \mathrm{O}^{16}=16.0000 \quad{ }_{8} \mathrm{O}^{17}=17.0045 \quad{ }_{8} \mathrm{O}^{18}=18.0049
$$

$$
\mathrm{O}=16.00435_{7} \pm 0.00008_{0}
$$

$$
\text { [from abundance } \mathrm{O}^{18}: \mathrm{O}^{18}: \mathrm{O}^{17}=(506 \pm 10): 1:(0.204 \pm 0.008) \text { ] }
$$

(2) Chemical scale $(0=16.0000)$

Ratio physical to chemical scale :
$r=(16.004357 \pm 0.000086) / 16=1.00272 \pm 0.000005$
$\mathrm{H}^{1}=1.00785_{\mathrm{f}} \pm 0.00001_{\mathrm{g}}$ (from physical scale)
$\mathrm{H}^{2}=2.01418_{2} \pm 0.00002_{1}$ (from physical scale)
$\mathrm{H}=1.00800_{2} \pm 0.00001_{8}$ (from physical scale)
$\mathrm{He}^{4}=4.00280 \pm 0.00007$ (from physical scale)
$\mathrm{C}=12.01139 \pm 0.00024$ (from physical scale)
$\mathrm{N}=14.00740 \pm 0.00012$ (from physical scale)
$\mathrm{N}=14.0086 \pm 0.0007$ (direct observation)
$\mathrm{Na}=22.994 \pm 0.003$
$\mathrm{Cl}=35.457 \pm 0.001$
$\mathrm{Ca}=40.080 \pm 0.005$
$\mathrm{Ag}=107.880 \pm 0.002$
$\mathrm{I}=126.915 \pm 0.004$

[^15](continued)

Part 3.-Additional quantities evaluated or used in connection with Part 1

```
Ratio of esu to emu (direct) \(\ldots \ldots \ldots \ldots c^{\prime}=\left(2.9971_{2} \pm 0.0001\right) \times 10^{10} \mathrm{~cm}^{1 / 2} \mathrm{sec}^{-1 / 2} \mathrm{ohm}^{1 / 2}\)
    \(=\left(2.9978 \pm 0.0001_{0}\right) \times 10^{10} \mathrm{~cm} / \mathrm{sec}\)
Ratio of esu to emu (indirect) \(\ldots \ldots . c^{\prime}=c=(2.99776 \pm 0.0004) \times 10^{10} \mathrm{~cm} / \mathrm{ser}\)
Average density of earth.............. \(\delta=5.517 \pm 0.004 \mathrm{~g} / \mathrm{cm}^{3}\)
Maximum density of water..... \(\delta_{m}\left(\mathrm{H}_{2} \mathrm{O}\right)=0.999 \mathrm{~S}_{2} 2 \pm 0.000002 \mathrm{~g} / \mathrm{cm}^{3}\)
Acceleration of gravity (standard) \(\ldots . . g_{0}=980.665 \mathrm{~cm} / \mathrm{sec}^{2}\)
Acceleration of gravity \(\left(45^{\circ}\right) \ldots . . . g_{45}=980.616 \mathrm{~cm} / \mathrm{sec}^{2}\)
Density of oxygen gas \(\left(0^{\circ} \mathrm{C}, A_{45}\right) \ldots . L_{1}=1.42897 \pm 0.0003 \mathrm{~g} /\) liter
Limiting density of oxygen gas \(\left(0^{\circ} \mathrm{C}, A_{45}\right)\)
                                    \(L_{11 m}=1.427609 \pm 0.000037 \mathrm{~g} /\) liter
Factor converting oxygen \(\left(0^{\circ} \mathrm{C}, A_{45}\right)\)
    to ideal gas....................... \(1-a=1.000953_{5} \pm 0.000009_{4}\)
Specific gravity of \(\mathrm{Hg}\left(0^{\circ} \mathrm{C}, A_{0}\right)\) re-
    ferred to air-free water at maximum
```



```
Density of \(\ddot{\mathrm{Hg}}\left(0^{\circ} \stackrel{\mathrm{C}}{\mathrm{C}}, \dddot{A}_{0}\right) \ldots \ldots \ldots \ldots . D_{0}=13.59504_{0} \pm 0.00005_{\mathrm{r}} \mathrm{g} / \mathrm{cm}^{8}\)
Electrochemical equivalents (chemical
    scale) :
        Silver (apparent) \(\ldots . .\).
                (corrected) \(\ldots . . . . . . . . . E_{\text {Ag }}=(1.11807 \pm 0.00012) \times 10^{-8} \mathrm{~g} / \mathrm{abs}\) coul
    Iodine (apparent) \(\ldots \ldots . . . . . . E_{1}=(1.315026 \pm 0.000025) \times 10^{-3} \mathrm{~g} / \mathrm{int}\) coul
                        (corrected) \(\ldots \ldots . . . . . . . E_{1}=(1.31535 \pm 0.00014) \times 10^{-8} \mathrm{~g} / \mathrm{abs}\) coul
Effective calcite grating space \(\left(18^{\circ} \mathrm{C}\right)\)
    Siegbahn system \(\quad d^{\prime \prime}{ }_{18}=3.02904 \times 10^{-8} \mathrm{~cm}\)
True calcite grating space \(\left(20^{\circ} \mathrm{C}\right) \ldots d^{\prime}{ }_{20}=3.02951_{2} \times 10^{-8} \mathrm{~cm}\)
    Siegbahn system
True calcite grating space \(\left(20^{\circ} \mathrm{C}\right) \ldots d_{20}=\left(3.03567_{4} \pm 0.00018\right) \times 10^{-8} \mathrm{~cm}\)
    cgs system
Ratio of grating and Siegbahn scales of
    wavelengths
Density of calcite \(\left(20^{\circ} \mathrm{C}\right) \ldots \ldots \ldots \ldots . . \rho=2.71029 \pm 0.00003 \mathrm{~g} / \mathrm{cm}^{3}\)
Structural constant of calcite \(\left(20^{\circ} \mathrm{C}\right) \ldots \Phi=1.09594 \pm 0.00001\)
Molecular weight of calcite (chemical
    scale) \(\ldots .\). ........................... \(M=100.091_{4} \pm 0.005\)
Rydberg constant for hydrogen ( \(\mathrm{H}^{1}\) ) \(. R_{H}=109677.581_{2} \pm 0.007_{\mathrm{s}} \mathrm{cm}^{-1}\) (I.A. scale)
Rydberg constant for deuterium ( \(\mathrm{H}^{2}\) ) . . \(R_{D}=109707.419_{3} \pm 0.007_{5} \mathrm{~cm}^{-1}\) (I.A. scale)
Rydberg constant for helium........ \(R_{H e}=109722.263 \pm 0.012 \mathrm{~cm}^{-1}\) (I.A. scale)
Rydberg constant for infinite mass..... \(R_{s}=109737.303 \pm 0.017 \mathrm{~cm}^{-1}\) (I.A. scale)
                                    or \(\pm 0.05 \mathrm{~cm}^{-1}\) (cgs system)
```


## TABLE 26.-GENERAL PHYSICAL CONSTANTS ACCORDING TO BIRGE (continued)

Part 4.-Partial list of derived quantities
Planck's constant:

$$
\begin{aligned}
& h=\left\{\frac{2 \pi^{2} c^{3} F^{5}}{R_{\times} N_{0}{ }^{5}(c / m)}\right\}^{1 / 3} \ldots \ldots \ldots . .=\left(6.624_{2} \pm 0.002_{4}\right) \times 10^{-27} \mathrm{erg} \mathrm{sec} \\
& h / c=\left\{\frac{2 \pi^{2} c^{3} F^{2}}{R_{4} N_{0}^{2}(c / m)}\right\}^{1 / 3} \ldots \ldots \ldots . .=\left(4.1349_{0} \pm 0.0007_{1}\right) \times 10^{-7} \mathrm{erg} \sec \text { abs emu }{ }^{-1} \\
& h / \mathfrak{c}^{\prime}=h /(e c)=\left\{\frac{2 \pi^{2} F^{2}}{R_{x} N_{0}{ }^{2}(c / m)}\right\}^{1 / 3}=\left(1.3793_{3} \pm 0.0002_{3}\right) \times 10^{-17} \mathrm{erg} \text { sec abs esu }{ }^{-1}
\end{aligned}
$$

Atomic weight of electron: $\ldots . . . . . . . E=F /(c / m)$
(Physical scale) $\ldots . . . . . . . . . . . . .=\left(5.4862_{4} \pm 0.0017\right) \times 10^{-4}$
(Chemical scale) $\ldots . . . . . . . . . . . . . . . .=\left(5.4847_{5} \pm 0.0017\right) \times 10^{-4}$
Band spectra constant connecting wave
number and moment of inertia:
$h /\left(8 \pi^{2} c\right)=\left\{\frac{F^{5}}{256 \pi^{4} R_{e} N_{0}{ }^{5}(e / m)}\right\}^{1 / 3} \ldots .=\left(27.98_{c 5} \pm 0.01_{0}\right) \times 10^{-40} \mathrm{~g} \mathrm{~cm}$
Boltzmann constant:

$$
K=R_{0} / N_{0}=V_{0} A_{0} /\left(T_{0} N_{0}\right) \ldots \ldots \ldots=(1.38047, \pm 0.00026) \times 10^{-16} \mathrm{erg} / \mathrm{deg}
$$

Charge in electrolysis of 1 gram of H

$$
F / H=9572.1_{\mathrm{ra}} \pm 1.0 \mathrm{abs} . \mathrm{emu} / \mathrm{g}
$$

Charge in electrolysis of one gram of
$\mathrm{H}^{\mathrm{L}} \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \ldots \mathrm{c} / M_{n^{1}}=F H^{\prime}=9573.5_{60} \pm 1.0 \mathrm{absemu} / \mathrm{g}$
Compton shift at $90^{\circ}$ :

$$
h /(m c)=\left\{\frac{2 \pi^{2} F^{2}(c / m)^{2}}{R_{x} N_{0}^{2}}\right\}^{1 / 3} \ldots \ldots=\left(0.024265_{14} \pm 0.000005_{7}\right) \times 10^{-8} \mathrm{~cm}
$$

Energy in ergs of one abs volt-electron:

$$
E_{0}=10^{5} \mathrm{c}=10^{5} \mathrm{~F} / \mathrm{S}_{0} \ldots \ldots \ldots \ldots \ldots=\left(1.60203_{3} \pm 0.00034\right) \times 10^{-12} \mathrm{erg}
$$

Energy in calories per mole for one abs volt-electron per molecule:

$$
\frac{F(\text { abs coul } / \mathrm{gram-equiv.})}{J_{15}(\text { abs joules } / \mathrm{cal})} \ldots \ldots \ldots \ldots=23052 . \mathrm{s5} \pm 3.2 \mathrm{cal}_{15} \mathrm{~mole}^{-1}
$$

Fine structure constant:

$$
\begin{aligned}
a=2 \pi\left(c^{\prime}\right)^{2} /(h c)=\left\{\frac{4 \pi R_{x} F(c / m)}{N_{0}}\right\}^{1 / 3} & =\left(7.2976_{\mathrm{s}} \pm 0.0008_{6}\right) \times 10^{-3} \\
1 / a & =137.030_{2} \pm 0.016 \\
a^{2} & =(5.3255 \pm 0.0013) \times 10^{-5}
\end{aligned}
$$

Gas constant per mole:

$$
\begin{aligned}
& R_{\mathrm{n}}=V_{0}{ }_{0} A_{0} \gamma_{0} \ldots \ldots \ldots \ldots \ldots \ldots . . \\
& R^{\prime}{ }_{0}=R_{11} \times 10^{-7} / J_{15} \ldots \ldots . . . . . . .=1.98646_{\mathrm{i}} \pm 0.00021 \mathrm{cal}_{15} \mathrm{deg}^{-1} \mathrm{~mole}^{-1} \\
& R^{\prime \prime}{ }_{0}=l^{\prime \prime}{ }_{0} / T_{0} \ldots \ldots \ldots \ldots \ldots \ldots=\left(8.20544_{7} \pm 0.00037\right) \times 10^{-2} 1 \mathrm{~atm} \mathrm{deg}^{-1} \mathrm{~mole}^{-1} \\
& R^{\prime \prime \prime}{ }_{0}=R_{\mathrm{e}} / A_{0}=V_{0} / T_{0} \ldots \ldots \ldots \ldots .=82.0566_{\mathrm{i}} \pm 0.0037 \mathrm{~cm}^{3} \mathrm{~atm} \mathrm{deg}^{-1} \mathrm{~mole}^{-1}
\end{aligned}
$$

also:
$R_{0} T_{0}=I_{0.4_{0}} \ldots \ldots \ldots \ldots \ldots \ldots=\left(2.27115_{0} \pm 0.00006\right) \times 10^{10} \mathrm{erg}$ mole ${ }^{-1}$ Loschmidt number $\left(0^{\circ} \mathrm{C}, \ddot{A}_{v}\right) \mu_{0}=\mathscr{V}_{0} / \mathscr{V}_{0} .=\left(2.6870_{12} \pm 0.0005_{0}\right) \times 10^{1.2}$ molecules $/ \mathrm{cm}^{3}$ Magnetic moment of one Bohr magneton:

$$
\begin{aligned}
\mu_{1}= & (h / 4 \pi)(c / m)= \\
& \frac{1}{4 \pi}\left\{\frac{2 \pi^{2} c^{3} F^{5}(c / m)^{2}}{R_{x} N_{0}{ }^{5}}\right\}^{1 / 3} \ldots \ldots \ldots=\left(0.9273_{45} \pm 0.0003_{\mathrm{z}}\right) \times 10^{-50} \mathrm{erg} / \text { gauss }
\end{aligned}
$$

Magnetic moment per mole for one Bohr
magneton per molecule:

$$
\mu_{1} V_{0}=\frac{1}{4 \pi}\left\{\frac{2 \pi^{2} c^{3} F^{5}(c / m)^{2}}{R_{x} N_{0}^{2}}\right\}^{1 / 3} \ldots \ldots=5585.24 \pm 1.6 \mathrm{erg} \text { gauss }^{-1} \mathrm{~mole}^{-1}
$$

Mass of $a$-particle..Ma $=(H c-2 E) / N_{0}=\left(6.6442_{2} \pm 0.0012\right) \times 10^{-24} \mathrm{~g}$

# TABLE 26.-GENERAL PHYSICAL CONSTANTS ACCORDING TO BIRGE (concluded) 

Mass of atom of unit atomic weight,

$$
M_{0}=1 / N_{0}=(1.66035 \pm 0.00031) \times 10^{-24} \mathrm{~g}
$$

Mass of electron;

$$
m=e /(e / m)=\left(F / N_{0}\right) /(e / m)=\left(9.1066_{0} \pm 0.0032\right) \times 10^{-28} \mathrm{~g}
$$

Mass of $\mathrm{H}^{1}$ atom......... $M_{H} 1=H^{1} / N_{0}=\left(1.67339_{3} \pm 0.0031\right) \times 10^{-24} \mathrm{~g}$
Mass of proton. $\ldots . . M_{P}=\left(H^{1}-E\right) / N_{0}=\left(1.67248_{2} \pm 0.00031\right) \times 10^{-24} \mathrm{~g}$
Ratio mass $\mathrm{H}^{1}$ atom to mass electron:

$$
M_{H} 1 / m=(e / m)\left(H^{1} / F\right) \quad \ldots \ldots \ldots . .=1837.5_{01} \pm 0.5_{\varepsilon}
$$

Ratio mass proton to mass electron:

$$
M_{p / m}=(e / m)\left(\frac{\left(H^{1}-E\right)}{F}\right) \ldots \ldots \ldots=1836.5_{e 1} \pm 0.5_{\mathrm{b}}
$$

First radiation constant..... $c_{2}^{* *}=8 \pi h c^{2}=(4.9908 \pm 0.0024) \times 10^{-18} \mathrm{erg} \mathrm{cm}$

$$
=h c^{2}=(0.59542 \pm 0.0024) \times 10^{-5} \mathrm{erg} \mathrm{~cm}^{2} \mathrm{sec}^{-1}
$$

Second radiation constant :

$$
=2 \pi h c^{2}=(3.7403 \pm 0.0024) \times 10^{-8} \mathrm{erg} \mathrm{~cm}^{2} \mathrm{sec}^{-1}
$$

$$
c_{2}=h c / k=\frac{T_{0} c^{2}}{V_{0} A_{0}}\left\{\frac{2 \pi^{2} F^{6}}{R_{\infty} N_{0}^{2}(e / m)}\right\}^{1 / 3}=1.4384_{8} \pm 0.0003_{4} \mathrm{~cm} \mathrm{deg}
$$

Specific charge of $\alpha$-particle:

$$
2 e / M_{a}=\frac{2 F}{H e-2 E} \cdots \cdots \cdots \cdots \cdots=4822.3_{3} \pm 0.5_{1} \mathrm{abs} \mathrm{emu} / \mathrm{g}
$$

Specific charge of proton:

$$
\varepsilon / M_{P}=\frac{F}{H^{1}-E} \ldots \ldots \ldots \ldots \ldots=9578.7_{\mathrm{r}} \pm 1.0 \mathrm{abs} \mathrm{emu} / \mathrm{g}
$$

Radiation density constant,

$$
a=8 \pi^{8} k^{4} /\left(15 c^{3} h^{8}\right)=
$$

$$
\left(\frac{V_{0} A_{0}}{T_{0}}\right) \frac{4 \pi^{3} N_{0} R_{\infty}(c / m)}{15 c^{6} F^{5}} \cdots \cdots \cdots \cdots=\left(7.569_{42} \pm 0.004_{0}\right) \times 10^{-15} \mathrm{erg} \mathrm{~cm}^{-8} \mathrm{deg}^{-1}
$$

Stefan-Boltzmann constant : $\dagger$

$$
\begin{aligned}
\sigma=a c / 4=2 \pi^{5} k^{4} /\left(15 c^{2} h^{3}\right) \quad \ldots \ldots \ldots & =\left(\frac{V_{0} A_{0}}{T_{0}}\right)^{4} \frac{\pi^{3} N_{0} R_{\infty}(e / m)}{15(F c)^{5}} \\
& =\left(5.672_{83} \pm 0.003_{7}\right) \times 10^{-8} \mathrm{erg} \mathrm{~cm}^{-2} \mathrm{deg}^{-4} \mathrm{sec}^{-1}
\end{aligned}
$$

Wien's displacement-law constant..... $A=c_{2} / 4.965114=0.28971_{8} \pm 0.00007 \mathrm{~cm}$ deg
Wavelength associated with 1 abs volt:
$\lambda_{0}=10^{-8} c^{2}\left(h / e^{\prime}\right)=\frac{c^{2}}{10^{8}}\left\{\frac{2 \pi^{2} F^{2}}{R_{\infty} N_{0}^{2}(e / m)}\right\}^{1 / 3}=(12395.4 \pm 2.1) \times 10^{-8} \mathrm{~cm}$ abs volt
Wave number associated with 1 abs volt:

$$
s_{0}=1 / \lambda_{0}=\frac{10^{8}}{c^{2}}\left\{\frac{R_{\propto} N_{0}{ }^{2}(e / m)}{2 \pi^{2} F^{2}}\right\}^{1 / 3}=8067.4_{v} \pm 1.4 \mathrm{~cm} / \text { abs volt }
$$

Zeeman displacement per gauss $\left.(e / m) /(4 \pi c)=4.6699_{1} \pm 0.0013\right) \times 10^{-5} \mathrm{~cm} /$ gauss

[^16]Part 5.-Birge's 1944 values of 3 constants


TABLE 27.-TABLE OF LEAST-SQUARES ADJUSTED OUTPUT VALUES OF PHYSICAL CONSTANTS (BY DUMOND AND ASSOCIATES)
(November 1952)

## Part 1.-Auxiliary constants used

These auxiliary constants are quantities which are uncorrelated (observationally) with the variables of the least-squares adjustment.
Rydberg wave number for infinite mass. $R_{x}=109737.309 \pm 0.012 \mathrm{~cm}^{-1}$
Rydberg wave numbers for the light nuclei

$$
R_{H}=109677.576 \pm 0.012 \mathrm{~cm}^{-1}
$$

$$
R_{D}=109707.419 \pm 0.012 \mathrm{~cm}^{-1}
$$

$$
R_{H e}=109717.345 \pm 0.012 \mathrm{~cm}^{-1}
$$

Atomic mass of neutron

$$
R_{H e}=109722.267 \pm 0.012 \mathrm{~cm}^{-1}
$$

Atomic mass of hydrogen.................. $H=1.008142 \pm 000003$
Atomic mass of deuterium.............. $D=2.014735 \pm 0.000006$
Gas constant per mole (physical scale). $R_{0}=(8.31662 \pm 0.00038) \times 10^{7} \mathrm{erg}_{\mathrm{mole}}{ }^{-1} \mathrm{deg}^{-1} \mathrm{C}$
Standard volume of a perfect gas
(physical scale)
$. V_{0}=22420.7 \pm 0.6 \mathrm{~cm}^{3} \mathrm{atmos}^{-1} \mathrm{~mole}^{-1}$

Part 2.—Least-squares adjusted output values
(The quantity following each $\pm$ sign is the standard error by external consistency)
Velocity of light. .........................c $=299792.9 \pm 0.8 \mathrm{~km} \mathrm{sec}^{-1}$
Avogadro's constant (physical scale) $\ldots . N=(6.02472 \pm 0.00036) \times 10^{23}(\text { molecules mol })^{-1}$
Loschmidt's constant (physical scale)

$$
L_{0}=N / \ddot{V}_{0}=(2.68713 \pm 0.00016) \times 10^{19} \text { molecules } \mathrm{cm}^{-3}
$$

Electronic charge $. . . . . . . . . . . . . . . . . . . e=(4.80288 \pm 0.00021) \times 10^{-10} \mathrm{esu}$
$\because=c / c=(1.60207 \pm 0.00007) \times 10^{-20} \mathrm{emu}$
Electron rest mass...................... $m=(9.1085 \pm 0.0006) \times 10^{-28} \mathrm{~g}$
Proton rest mass................ $m_{p}=M_{p} / N=(1.67243 \pm 0.00010) \times 10^{-24} \mathrm{~g}$
Neutron rest mass.............. $m_{n}=n / N=(1.67474 \pm 0.00010) \times 10^{-24} \mathrm{~g}$
Planck's constant $\ldots . . \ldots \ldots . . . . . . . . . h=(6.6252 \pm 0.0005) \times 10^{-27} \mathrm{erg} \sec$
$\hbar=h /(2 \pi)=(1.05444 \pm 0.00009) \times 10^{-27} \mathrm{erg} \mathrm{sec}$
Conversion factor from Siegbahn X-units
to milliangstroms ................. $\lambda_{o} / \lambda_{s}=1.002063 \pm 0.000034$
Faraday constant (physical scale) $F=N e=(2.89360 \pm 0.00007) \times 10^{14}$ esu (g mol $)^{-1}$

$$
F^{\prime}=N_{e} / c=(9652.01 \pm 0.25) \text { emu }(\mathrm{gm} \mathrm{~mol})^{-1}
$$

Charge-to-mass ratio of the electron.. $\varepsilon / m=(5.27299 \pm 0.00016) \times 10^{17}$ esu g $^{-1}$ $c^{\prime} / m=e /(m c)=(1.7588 \pm 0.00005) \times 10^{7} \mathrm{emug}^{-1}$
Ratio $h / e \ldots \ldots . . . . . . . . . . . . . . . . h / e=(1.37943 \pm 0.00005) \times 10^{-17} \mathrm{erg} \sec (\mathrm{esu})^{-1}$
Fine structure constant $\ldots \ldots a=e^{2} /(\hbar c)=(7.29726 \pm 0.00008) \times 10^{-3}$ $1 / a=137.0377 \pm 0.0016$ $a / 2 \pi=(1.161396 \pm 0.000013) \times 10^{-3}$
$a^{2}=(5.32501 \pm 0.00012) \times 10^{-5}$
$1-\left(1-a^{2}\right)^{\frac{1}{2}}=(0.266254 \pm 0.000006) \times 10^{-4}$
Atomic mass of the electron (physical

Ratio of mass of hydrogen to mass of
proton ${ }^{\text {s }}$

$$
H / H^{+}=\left[1-\frac{N m}{H}\left(1-\frac{1}{2} a^{2}\right)\right]^{-1}=1.000544610 \pm 0.000000013
$$

Atomic mass of proton................ $H^{+}=1.007593 \pm 0.000003$
Ratio of proton mass to electron mass.

$$
\mathrm{H}^{+} / \mathrm{Nm}=1836.13 \pm 0.04
$$

Reduced mass of electron in hydrogen
atom $\ldots \ldots \ldots \ldots \ldots \ldots \ldots \mu=m H^{+} / H=(9.1035 \pm 0.0006) \times 10^{-29} \mathrm{~g}$
Schrödinger constant for a fixed nucleus

$$
2 m / \hbar^{2}=(1.63844 \pm 0.00016) \times 10^{-7} \mathrm{erg}^{-1} \mathrm{~cm}^{-2}
$$

Schrödinger constant for the hydrogen
atom $\ldots \ldots \ldots \ldots . . . . . . . . . . . .2 \mu / \hbar^{2}=(1.63755 \pm 0.00016) \times 10^{27} \mathrm{erg}^{-1} \mathrm{~cm}^{-2}$
First Bohr radius. ......... $a_{0}=\hbar^{2} /\left(m e^{2}\right)=(5.29171 \pm 0.00006) \times 10^{-9} \mathrm{~cm}=a /\left(4 \pi R_{x}\right)$

[^17]Radius of electron orbit in normal $H^{1}$,
referred to center of mass.

$$
a_{0}^{\prime}=a_{0}\left(1-a^{2}\right)^{3}=(5.29157 \pm 0.00006) \times 10^{-8} \mathrm{~cm}
$$

Separation of proton and electron in nor-
mal $H^{1}$

$$
a_{0}^{\prime \prime}=a_{0}^{\prime} R_{\alpha} / R_{H I}=(5.29445 \pm 0.00006) \times 10^{-0} \mathrm{~cm}
$$

Compton waveiength of the electron.

$$
\begin{aligned}
& \lambda_{c e}=h /(m c) \\
& \lambda_{c e}=\lambda_{c e} /(2 \pi)=(24.2625 \pm 0.0006) \times 10^{-11} \mathrm{~cm}=a^{2} /\left(2 R_{\infty}\right) \\
&3.86150 \pm 0.00009) \times 10^{-11} \mathrm{~cm}=a^{2} /\left(4 \pi R_{\infty}\right)
\end{aligned}
$$

Compton wavelength of the proton......

$$
\begin{aligned}
\lambda_{c p}=h / m_{p} c & =(13.2139 \pm 0.0004) \times 10^{-14} \mathrm{~cm} \\
\star_{c p} & =\lambda_{c p} /(2 \pi)
\end{aligned}=(2.10307 \pm 0.00007) \times 10^{-14} \mathrm{~cm}
$$

Compton wavelength of the neutron.....

$$
\lambda_{c n}=h / m_{n} c=(13.1958 \pm 0.0004) \times 10^{-14} \mathrm{~cm}
$$

$$
\lambda_{c n}=\lambda_{c n} /(2 \pi)=(2.10017 \pm 0.00007) \times 10^{-14} \mathrm{~cm}
$$

Classical electron radius.... $r_{0}=c^{2} /\left(m c^{2}\right)=(2.81784 \pm 0.00010) \times 10^{-13} \mathrm{~cm}=a^{3} /\left(4 \pi R_{x}\right)$

$$
r_{0}{ }^{2}=(7.9402 \pm 0.0005) \times 10^{-20} \mathrm{~cm}^{2}
$$

Thompson cross section

$$
\frac{8}{3} \pi r_{0}^{2}=(6.65196 \pm 0.0005) \times 10^{-25} \mathrm{~cm}^{2}
$$

Fine structure doublet separation in
hydrogen

$$
\begin{aligned}
\Delta E_{u} & =\frac{1}{16} R_{u} a^{2}\left[1+\frac{a}{\pi}+\left(\frac{5}{8}-\frac{5.946}{\pi^{2}}\right) a^{2}\right] \\
& =0.365869 \pm 0.000008 \mathrm{~cm}^{-1} \\
& =10968.49 \pm 0.25 \mathrm{Mc} \mathrm{sec}^{-1}
\end{aligned}
$$

Fine structure separation in deuterium

$$
\begin{aligned}
\Delta E_{D}=\Delta E_{n} R_{D} / R_{n} & =0.365969 \pm 0.000008 \mathrm{~cm}^{-1} \\
& =10971.48 \pm 0.25 \mathrm{Mc} / \mathrm{sec}^{-1}
\end{aligned}
$$

Zeeman displacement per gauss

$$
(c / m c) /(4 \pi c)=(4.66879 \pm 0.00015) \times 10^{-5} \mathrm{~cm}^{-1} \text { gauss }^{-1}
$$

Boltzmann's constant $\ldots \ldots \ldots k=R_{0} / N=(1.38042 \pm 0.00010) \times 10^{-16} \mathrm{ergs}^{\mathrm{er}} \mathrm{deg}^{-1}$ $k=(8.6164 \pm 0.0004) \times 10^{-8} \mathrm{ev} \mathrm{deg}^{-1}$

$$
1 / k=11605.7 \pm 0.5 \mathrm{deg}^{-1} .
$$

First radiation constant.......c.c. $=8 \pi h c=(4.9919 \pm 0.0004) \times 10^{-15} \mathrm{erg} \mathrm{cm}$
Second radiation constant.......c.c $=h c / k=(1.43884 \pm 0.00008) \mathrm{cm} \mathrm{deg}$
Atomic specific heat constant. ........ $c_{2} / c=(4.79946 \pm 0.00027) \times 10^{-11} \mathrm{sec} \mathrm{deg}$
Wien displacement law constant ${ }^{\mathrm{b}} \ldots \lambda_{\text {max }} T=c_{2} /(4.96511423)=0.28979 \pm 0.00005 \mathrm{~cm} \mathrm{deg}$
Stefan-Boltzmann constant

$$
\sigma=\left(\pi^{2} / 60\right)\left(k^{4} / \hbar c^{2}\right)=(0.56686 \pm 0.00005) \times 10^{-4} \mathrm{erg} \mathrm{~cm}^{-2} \mathrm{deg}^{-4} \mathrm{sec}^{-1}
$$

Sackur-Tetrode constant $\ldots \ldots \ldots . S_{0} / R_{0}=\frac{5}{2}+\ln \left\{\left(2 \pi R_{0}\right)^{3 / 2} h^{-3} N^{-4}\right\}$

$$
\begin{aligned}
& =-5.57324 \pm 0.00011 \\
S_{0} & =-(46.3505 \pm 0.0017) \times 10^{7} \mathrm{erg} \mathrm{~mole}^{-1} \mathrm{deg}^{-1}
\end{aligned}
$$

Bohr masneton

$$
\mu_{0} \mp h e /(4 \pi m c)=\frac{1}{2} e \star_{c o}=(0.92732 \pm 0.00006) \times 10^{-80} \mathrm{erg}_{\mathrm{gauss}}{ }^{-1}
$$

Anomalous electron moment correction...

$$
\left[1+\frac{a}{2 \pi}-2.973 \frac{a^{2}}{\pi^{2}}\right]=\mu_{0} / \mu_{0}=1.001145356 \pm 0.000000013
$$

Magnetic moment of the electron....... $\mu_{0}=(0.92838 \pm 0.00006) \times 10^{-20} \mathrm{erg}_{\mathrm{g}}$ gauss $^{-1}$
Nuclear magneton

$$
\left.\mu_{n}=h c /\left(4 \pi m_{p} c\right)=\mu_{0} N m / H^{+}=0.505038 \pm 0.000036\right) \times 10^{-23} \mathrm{erg} \mathrm{gauss}^{-1}
$$

Proton moment $\ldots . . \ldots . . . . . . . . . . . . \mu \mu=2.79277 \pm 0.00006$ nuclear magnetons

$$
=(1.41045 \pm 0.00009) \times 10^{-23} \mathrm{erg}^{2} \text { gauss }^{-1}
$$

Gyromagnetic ratio of the proton in hy-
drogen (uncorrected for diamagnetism)

$$
\gamma^{\prime}=(2.67520 \pm 0.00008) \times 10^{4} \text { radians sec }^{-1} \text { gauss }^{-1}
$$

Gyromagnetic ratio of the proton (cor-

Multiplier of (Curie constant) ${ }^{\frac{1}{2}}$ to give
magnetic moment per molecule. $(3 k / N)^{\frac{1}{2}}=(2.62178 \pm 0.00017) \times 10^{-20}\left(\mathrm{erg} \text { mole deg }{ }^{-1}\right)^{\frac{1}{1}}$

[^18](continued)

TABLE 27.-TABLE OF LEAST-SQUARES ADJUSTED OUTPUT VALUES OF PHYSICAL CONSTANTS (concluded)

de Broglie wavelengths, $\lambda_{D}$ of elementary
particles ${ }^{\text {c }}$
Electrons ............................... $\lambda_{D_{e}}=(7.27373 \pm 0.00016) \mathrm{cm}^{2} \mathrm{sec}^{-1} / \mathrm{v}$ $=(1.55226 \pm 0.00008) \times 10^{-13} \mathrm{~cm}(\mathrm{erg})^{\frac{1}{2}} / \sqrt{E}$ $=(1.226377 \pm 0.000032) \times 10^{-7} \mathrm{~cm}(\mathrm{ev})^{\frac{1}{2}} / \sqrt{E}$
Protons . ................................. $n_{p}=(3.96145 \pm 0.00013) \times 10^{-3} \mathrm{~cm}^{2} \mathrm{sec}^{-1} / \mathrm{v}$
$=(3.62261 \pm 0.00020) \times 10^{-15} \mathrm{~cm}(\mathrm{erg})^{\frac{1}{2}} / \sqrt{E}$
$=(2.86208 \pm 0.00012) \times 10^{-9} \mathrm{~cm}(\mathrm{ev})^{\frac{3}{2}} / \sqrt{E}$
Neutrons $\ldots \ldots . . . . . . . . . . . . . \lambda_{D n}=(3.95599 \pm 0.00013) \times 10^{-3} \mathrm{~cm}^{2} \mathrm{sec}^{-1} / \mathrm{v}$

$$
=(3.62005 \pm 0.00020) \times 10^{-15} \mathrm{~cm}(\mathrm{erg})^{1} / \sqrt{E}
$$

$$
=(2.86005 \pm 0.00012) \times 10^{-9} \mathrm{~cm}(\mathrm{ev})^{\frac{1}{2}} / \sqrt{E}
$$

Energy of $2200 \mathrm{~m} / \mathrm{sec}$ neutron....... $E_{2220}=0.0252977 \pm 0.0000006 \mathrm{ev}$
Velocity of $1 / 40 \mathrm{ev}$ neutron. .......... $v_{0.025}=2187.017 \pm 0.028 \mathrm{~m} / \mathrm{sec}$
The Rydberg and related derived constants

$$
\begin{aligned}
R_{x} & =109737.309 \pm 0.012 \mathrm{~cm}^{-1} \\
R_{x} c & =(3.289847 \pm 0.000008) \times 10^{15} \mathrm{sec}^{-1} \\
R_{x} c & =(2.17961 \pm 0.00018) \times 10^{-11} \mathrm{ergs}^{-1} \\
\frac{R_{x} h c^{2} \times 10^{-8}}{e} & =13.6050 \pm 0.0005 \mathrm{ev}
\end{aligned}
$$

Hydrogen ionization potential.......... $I_{0}=13.5978 \pm 0.0005 \mathrm{ev}$

$$
=R_{H} \frac{h c^{2}}{c}\left[1+\frac{a^{2}}{4}+\cdots\right] \times 10^{-8}
$$

[^19]Part $1 \dagger$ (atomic weights according to the physical scale unless otherwise indicated)


[^20]
## Part $2 \ddagger$



TABLE 28.-GENERAL PHYSICAL CONSTANTS ACCORDING TO BEARDEN AND ASSOCIATES (concluded)

Energy equivalent of electron mass. . $m c^{2}=(.510969 \pm .000009) \mathrm{Mev}$
Energy associated with $1^{\circ} \mathrm{K}$
$\left(R_{0} / \mathscr{F}\right) \times 10^{-8}=(8.61632 \pm .00042) \times 10^{-5} \mathrm{ev}$
Temperature associated with $1 \mathrm{ev} \ldots . . T_{0}=(11605.9 \pm .6) \mathrm{deg} \mathrm{K}$
Grating space calcite at $20^{\circ} \mathrm{C} \ldots \ldots d_{20}=(3.03567 \pm .00005) \times 10^{-8} \mathrm{~cm}$
Density of calcite at $20^{\circ} \mathrm{C}$. . . . . . . . . . . . . $\rho=(2.71030 \pm .00003) \mathrm{g} \mathrm{cm}^{-3}$
Compton wavelength of electron....h/mc $=(2.426045 \pm .000025) \times 10^{-10} \mathrm{~cm}$
Zeeman displacement per gauss $c /(4 \pi m c)=(4.668885 \pm .00008) \times 10^{-5} \mathrm{~cm}^{-1} \mathrm{gauss}^{-1}$
Doublet separation in hydrogen.

$$
\frac{1}{16} \quad R_{H} a^{2}=(.3649900 \pm .0000037) \mathrm{cm}^{-1}
$$

## TABLE 29.-SPELLING AND ABBREVIATIONS OF THE COMMON UNITS OF WEIGHT AND MEASURE

The spelling of the metric units is that adopted by the International Committee on Weights and Measures and given in the law legalizing the metric system in the United States (1866). The use of the same abbreviation for singular and plural is recommended. It is also suggested that only small letters be used for abbreviations except in the case of A for acre, where the use of the capital letter is general.

| Unit | Abbreviation | Unit | Abbreviation |
| :---: | :---: | :---: | :---: |
| acre | A | kilogram | kg |
| are | a | kiloliter | kl |
| a voirdupois | av | kilometer | km |
| barrel | bbl | link | 1 l. |
| board foot | bd ft | liquid | liq |
| bushel | bu | liter | 1 |
| carat, metric | c | meter | m |
| centare | ca | metric ton | t |
| centigram | cg | micron | $\mu$ |
| centiliter | cl | mile | mi |
| centimeter | cm | milligram | mg |
| chain | ch | milliliter | ml |
| cubic centimeter | $\mathrm{cm}^{8}$ | millimeter | mm |
| cubic decimeter | $\mathrm{dm}^{3}$ | millimicron | $\mathrm{m} \mu$ |
| cubic dekameter | $\mathrm{dkm}^{3}$ | minim | min. or $m$ |
| cubic foot | $\mathrm{ft}^{3}$ | ounce | $o z$ |
| cubic hectometer | $\mathrm{hm}^{3}$ | ounce, apothecaries' | oz ap or 3 |
| cubic inch | in. ${ }^{3}$ | ounce, avoirdupois | ozav |
| cubic kilometer | $\mathrm{km}^{3}$ | ounce, fluid | floz |
| cubic meter | $\mathrm{m}^{3}$ | ounce, troy | ozt |
| cubic mile | $\mathrm{mi}^{3}$ | peck | pk |
| cubic millimeter | $\mathrm{mm}^{3}$ | pennyweight | dwt |
| cubic yard | $y^{\text {d }}$ | pint | nt |
| decigram | dg | pound | ib |
| deciliter | dl | pound, apothecaries' | lb ap |
| decimeter | dm | pound, a voirdupois | lb av |
| decistere | ds | pound, troy | 1 bt |
| dekagram | dkg | quart | qt |
| dekaliter | dkl | rod | rd |
| dekameter | dkm | scruple, apothecaries' | sap or 3 |
| dekastere | dks | square centimeter | $\mathrm{cm}^{2}$ |
| dram | dr | square chain | $\mathrm{ch}^{2}$ |
| dram, apothecarics' | drap or 3 | square decimeter | $\mathrm{dm}^{2}$ |
| dram, a voirdupois | drav | square dekameter | dkm ${ }^{2}$ |
| dram, fluid | $f \mathrm{dr}$ | square foot | $\mathrm{ft}^{2}$ |
| fathom | fath | square hectometer | $\mathrm{hm}^{2}$ |
| foot | ft | square inch | in. ${ }^{2}$ |
| firkin | fir | square kilometer | $\mathrm{km}^{2}$ |
| furlong | fur | squarë meter | $\mathrm{m}^{2}$ |
| gallon | gal | square mile | $m i^{2}$ |
| grain | gr | square millimeter | $\mathrm{mm}^{2}$ |
| gram | g | square rod | $r d^{2}$ |
| hectare | ha | square yard | $y d^{2}$ |
| hectogram | hg | stere | s |
| hectoliter | hl | ton | tn |
| hectometer | hm | ton, metric | $t$ |
| hogshead | hhd | troy | t |
| hundredweight | cwt | yard | yd |

## TABLE 30.-DIMENSIONAL EQUATIONS OF FUNDAMENTAL AND DERIVED UNITS

Conversion factors.-The dimensional formulas given in this table have many uses. One is to assist in changing a quantity from one system of units to another (see page 2). A simple scheme for transforming an expression from one set of units to another is given in Weniger's text, "Fundamentals of College Physics." Place the known number of the quantity with its units properly given, equal to an unknown number, $x$, of the same quantity properly expressed in the desired units. Proceed to cancel, treating the units just like algebraic quantities. Suppose it be desired to express 60 meters per second in miles per hour. Write:

$$
\frac{60 \mathrm{~m}}{\mathrm{sec}}=\frac{x \mathrm{mi}}{\mathrm{hr}}
$$

Cancel sec and $h r$ and write 3600 near the larger unit. Cancel $m$ and $m i$ and write 1609.3 near the larger unit. This gives:

$$
\frac{60 \mathrm{~m}}{\mathrm{sec}}=\frac{x \mathrm{mi}}{\mathrm{hr}} \quad \frac{1609.3}{3600}
$$

Solving, $X=134$, and the desired expression is $134 \mathrm{mi} / \mathrm{hr}$.
More complicated expressions are handled in a similar manner. In a heat-flow problem, suppose it becomes necessary to express $15 \mathrm{Btu} \mathrm{hr}^{-1} \mathrm{ft}^{-2}$ with a temperature gradient of $1^{\circ} \mathrm{F}$ per ft in terms of cal $\mathrm{sec}^{-1} \mathrm{~cm}^{-2}$ with a gradient of $1^{\circ} \mathrm{C} / \mathrm{cm}$. Write:

$$
\frac{15 \mathrm{Btu}}{\mathrm{hr} \mathrm{ft}{ }^{2}} \times \frac{\mathrm{ft}}{{ }^{\circ} \mathrm{F}}=\frac{x \mathrm{cal}}{\sec \mathrm{~cm}^{2}} \times \frac{\mathrm{cm}}{{ }^{\circ} \mathrm{C}}
$$

Cancel $f t$ in numerator and denominator, and cm similarly. Remember that 1 Btu is 252 cal, and cancel. A scc goes into 1 hr 3600 times. Cancel cm and ft and write 30.48 . Remember that $9^{\circ} \mathrm{F}$ equal $5^{\circ} \mathrm{C}$. Solving, $x=0.062$. (See Table 2.)

If the numeric before the known quantity is unity, $x$ comes out as the conversion factor for these units.
The dimensional formulæ lack one quality which is needed for completeness, an indication of their vector characteristics; such characteristics distinguish plane and solid angle, torque and energy, illumination and brightness.

## Part 1.-Fundamental units

The fundamental units most commonly used are: length $[l]$; mass $[m]$; time $[t]$; temperature $[\theta]$; and for the electrostatic system, dielectric constant $[k]$; for the electromagnetic system, permeability $[\mu]$. The formulæ will also be given for the International System of electric and magnetic units based on the units length, resistance [ $r$ ], current [ $i$ ], and time.

When writing fractions, using the solidus, care is required to make the meaning definite: i.e., Btu/hr/ $/ \mathrm{ft}^{2}\left({ }^{\circ} \mathrm{F} / \mathrm{m}\right)$, or $\mathrm{Btu} /(\mathrm{hr})\left(\mathrm{ft}^{2}\right)\left({ }^{\circ} \mathrm{F} / \mathrm{nn}\right)$ is not clear, but $\mathrm{Btu} /\left[\mathrm{hr} \times \mathrm{ft}^{2} \times\left({ }^{\circ} \mathrm{F} / \mathrm{m}\right]\right.$ is definite. DERIVED UNITS (continued)

## Part 2.-Derived units (geometric and heat)

|  |  | $\begin{gathered} \text { Conversion } \\ \text { factor } \\ {\left[m^{\left[!y^{2} t^{2}\right.}\right]} \end{gathered}$ |  | Name of units | $\begin{aligned} & \text { Conversion } \\ & \text { factor } \\ & {\left[m^{\left.r \mid v t=H^{\prime}\right]}\right.} \end{aligned}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Name of unit | $x$ | $\overbrace{y}$ | $z$ | (Heat and light) | $r$ | $y$ | $z$ | $v$ |
| Area, surface | 0 | 2 | 0 | Quantity of heat : |  |  |  |  |
| Volume | 0 | 3 | 0 | thermal units | 1 | 0 | 0 | 1 |
| Angle | 0 | 0 | 0 | thermometric units. | 0 | 3 | 0 | 1 |
| Solid angle | 0 | 0 | 0 | dynamical units | , | 2 | -2 | 0 |
| Curvature . | 0 | -1 | 0 | Coefficient of thermal |  |  |  |  |
| Angular velocity | 0 | 0 | -1 | expansion ...... | 0 | 0 | 0 | -1 |
| Linear velocity | 0 |  | -1 | Thermal conductivity : |  |  |  |  |
| Angular acceleration | 0 | 0 | -2 | thermal units .... | 1 | -1 | -1 | 0 |
| Linear acceleration | 0 | 1 | -2 | thermometric units |  |  |  |  |
| Density | 1 | -3 | 0 | or diffusivity... dymamical mints ... | 0 1 | 2 | -1 -3 | - |
| Moment of inertia..... | 1 | 2 | 0 |  |  |  |  |  |
| Intensity of attraction. | 0 | 1 | -2 | Thermal capacity | 1 | 0 | 0 | 0 |
| Momentum | 1 | 1 | -1 | Latent heat: |  |  |  |  |
| Moment of momentum. | 1 | 2 | -1 | thermal units | 0 | 0 | 0 |  |
| Angular momentum .. | 1 | 2 | -1 | dynamical units | 0 | 2 | -2 | 0 |
| Force | 1 | 1 | -2 | Joule's equivalent.... | 0 | 2 | -2 | $-1$ |
| Moment of couple, torque ............ | 1 | 2 | -2 | Entropy : |  |  |  |  |
| Work. energy . . . . . | 1 | 2 | -2 | heat in thermal units. heat in dynamical | 1 | 0 | 0 | 0 |
| Power, activity ....... | 1 | 2 | -3 | minits | 1 | 2 | -2 | 1 |
| Intensity of stress..... | , | -1 | -2 |  |  |  |  |  |
| Modulus of elasticity.. | 1 | -1 | -2 | L.uminous intensity Illumination | 0 | 0 -2 | 0 | $1^{*}$ |
| Compressibility |  | 1 | 2 | Brightness |  | -2 | 0 | 1* |
| Resilience | , | -1 | -2 | Visibility |  | -2 | 3 | 1* |
| Viscosity | 1 | -1 | -1 | Luminous efficiency.. |  | -2 | 3 | 1* |

[^21](continuted)

Part 3.-Derived units (electrical and magnetic)


[^22]TABLE 31.-FUNDAMENTAL UNITS OF LENGTH, AREA, VOLUME, AND MASS

| Part 1-Some definitions and legal relations |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} 1 \mathrm{in} .^{*} & =(1 / 0.3937) \mathrm{cm}=2.54000508 \mathrm{~cm} \\ 1 \mathrm{lb} * & =453.5924277 \mathrm{~g} \\ 1 \mathrm{gal}^{*} & =2231 \mathrm{in}^{3}=3.785329 \text { liter } \\ 1 \mathrm{I} . \mathrm{T} . \mathrm{cal}^{\dagger} & =4.18674 \text { joules } \\ 1 \mathrm{Btu}^{\dagger} & \equiv 1.00064 \mathrm{cal}_{15} \\ & =251.996 \mathrm{l} . \mathrm{T} . \mathrm{cal} \\ & =252.161 \mathrm{cal}_{15} \end{aligned}$ |  |  |  |  |  |  |
| Part 2.-Conversion factors, units of length |  |  |  |  |  |  |
| $1 \mathrm{~cm}=$ | $1{ }^{\text {cm }}$ | $0.01^{\mathrm{m}}$ | $\begin{gathered} \text { in. } \\ 0.3937 \end{gathered}$ | $\begin{gathered} \mathrm{ft} \\ 0.032808333 \end{gathered}$ | $\begin{gathered} \mathrm{yd} \\ 0.010936111 \end{gathered}$ |  |
| $1 \mathrm{~m}=$ | 100 | 1 | 39.37 | 3.2808333 | 1.0936111 |  |
| 1 in . $=$ | 2.5400051 | 0.025400051 | 1 | 0.083333333 | 0.027777778 |  |
| $1 \mathrm{ft}=$ | 30.480061 | 0.30480061 | 12 | 1 | 0.33333333 |  |
| $1 \mathrm{yd}=$ | 91.440183 | 0.91440183 | 36 | 3 | 1 |  |
| Part 3.-Conversion factors, units of area |  |  |  |  |  |  |
|  | $\mathrm{cm}^{2}$ | $\mathrm{m}^{2}$ | in. ${ }^{2}$ | $\mathrm{ft}^{2}$ | $\mathrm{yd}^{2}$ |  |
| $1 \mathrm{~cm}^{2}=$ | 1 | $10^{-4}$ | 0.15499969 | $1.0763867 \times 10^{-8}$ | $1.1959853 \times 10^{-4}$ |  |
| $1 \mathrm{~m}^{2}=$ | $10^{4}$ | 1 | 1549.9969 | 10.763867 | $1.1959853 \times 10$ |  |
| $1 \mathrm{in}^{.}{ }^{2}=$ | 6.4516258 | $6.4516258 \times 10^{-4}$ | 1 | $6.9444444 \times 10^{-3}$ | $7.7160494 \times 10^{-4}$ |  |
| $1 \mathrm{ft}^{2}=$ |  |  | 144 | $1$ | $0.11111111$ |  |
| $1 \mathrm{yd}^{2}=$ | 8361.3070 | 0.83613070 | 1296 | 9 |  |  |
| Part 4.-Conversion factors, units of volume |  |  |  |  |  |  |
|  | $\mathrm{cm}^{3}$ | in. ${ }^{3}$ | $\mathrm{ft}^{3}$ | ml | liter | gal |
| $1 \mathrm{~cm}^{3}=$ | 1 | 0.061023378 | $3.5314455 \times 10^{-5}$ | 0.9999720 | $0.9999720 \times 10^{-3}$ | $2.6417047 \times 10^{-4}$ |
| $1 \mathrm{in}^{3}=$ | 16.387162 | 1 | $5.7870370 \times 10^{-4}$ | 16.38670 | $1.638670 \times 10^{-2}$ | $4.3290043 \times 10^{-8}$ |
| $1 \mathrm{ft}^{3}=$ | $2.8317017 \times 10^{4}$ | $1.728 \times 10^{3}$ |  | $2.831622 \times 10^{4}$ | $28.31622 \times 1$ | 7.4805195 |
| $1 \mathrm{ml}=$ | $1.000028 \times 1{ }^{\text {s }}$ | 0.06102509 | $3.531544 \times 10^{-5}$ | 1 | $0.001$ | $2.641779 \times 10^{-4}$ |
| 1) liter = | $1.000028 \times 10^{3}$ | ${ }^{631.02509}$ | 0.03531544 | $10^{3}$ | $\frac{1}{3} 785329$ | $0.2641779$ |
| $1 \mathrm{gal}=$ | $3.7854345 \times 10^{3}$ | 231 | 0.13368056 | $3.785329 \times 10^{3}$ | 3.785329 |  |
| Part 5.-Conversion factors, units of mass |  |  |  |  |  |  |
|  | g | kg | 1 b | metric ton | ton |  |
| $1 \mathrm{~g}=$ | 1 | $10^{-3}$ | $2.2046223 \times 10^{-8}$ | $10^{-6}$ | $1.1023112 \times 10^{-6}$ |  |
| $1 \mathrm{~kg}=$ | $10^{3}$ | 1 | 2.2046223 | $10^{-3}$ | $1.1023112 \times 10^{-8}$ |  |
| 1 metric $1 \mathrm{lb}=$ | $4.5359243 \times 10^{2}$ | 0.45359243 | 1 | $4.5359243 \times 10^{-4}$ | 0.0005 |  |
| 1 metric ton 1 ton $=$ | $10^{8}$ | $10^{3}$ | 2204.6223 | 1 | 1.1023112 |  |
| 1 ton= | $9.0718486 \times 10^{5}$ | 907.18486 | 2000 | 0.90718486 |  |  |

TABLE 32.-TABLES FOR CONVERTING U. S. WEIGHTS AND MEASURES*
Part 1.-Metric to customary



In the United Staies since 1893 all units in the above table have been derived from the same standartls of leroth and mass. Therefore all equivalents (except those involving the liter) depend only on wimerical definitions. The liter is the volume of one kilograna of pure water at the temperatne of its maximum density and under a pressure equivalent to 760 millineters of nemeury. The liter was determined by the International Bureau of Weights and Measures in 1910 to equal $1.000027 \mathrm{dm}^{3}$. (National Bureau of Standards.)

[^23](continued)

Part 2.-Customary to metric


The length of the nautical mile given above, and adopted by the U. S. Coast and Geodetic Survey many years ago, is defined as that of a minute of arc of a great circle of a sphere whose surface equals that of the earth (Clarke's Spheroid of 1866).

## (continued)

## TABLE 32.-TABLES FOR CONVERTING U. S. WEIGHTS AND MEASURES

## (concluded)

Part 3.-Miscellaneous equivalents of U. S. and metric weights and measures ${ }^{18}$ (For other equivalents than those below, see Tables 30, 31, and 33.)

| LINE.\R MEASURES | MASS ME.ISURES |
| :---: | :---: |
| 1 mil (. 001 in.) $=25.4001 \mu$ | Avoirdupois zeights |
| $1 \mathrm{in} .=.000015783$ mile | $1 \mathrm{grain}=.064798918 \mathrm{~g}$ |
| 1 hand ( 4 in. $)=10.16002 \mathrm{~cm}$ | 1 dram av. $(27.34375 \mathrm{gr})=1.771845 \mathrm{~g}$ |
| 1 link (. 66 ft ) $=20.11684 \mathrm{~cm}$ | $1 \mathrm{oz} \mathrm{av}.(16 \mathrm{dr}$ av. $)=28.349527 \mathrm{~g}$ |
| $1 \mathrm{span}(9 \mathrm{in})=.22.86005 \mathrm{~cm}$ | 1 lb av ( $16 \mathrm{oz} \mathrm{av}$.or 7000 gr ) |
| 1 fathom ( 6 ft ) $=1.828804 \mathrm{~m}$ | $=14.583333$ oz ap. ( 5 ) or oz t. |
| $1 \mathrm{rod}\left(5 \frac{1}{2} \mathrm{yd}\right)(25 \mathrm{links})=5.02910 \mathrm{~m}$ | $=1.2152778$ or $7000 / 5760 \mathrm{lb} \mathrm{ap}$. |
| 1 chain ( 4 rods) $=20.11684 \mathrm{~m}$ | or t. |
| 1 light year $\left(9.5 \times 10^{12} \mathrm{~km}\right)=5.9 \times 10^{12}$ miles | $\begin{aligned} & =453.5924277 \mathrm{~g} \\ 1 \mathrm{~kg} & =2.204622341 \mathrm{lb} \mathrm{av} . \end{aligned}$ |
| 1 parsec $\left(31 \times 10^{12} \mathrm{~km}\right)=19 \times 10^{12}$ miles | $1 \mathrm{~g}=15.432356 \mathrm{gr}=.5643833 \mathrm{drav}$. |
| ${ }_{6.1}^{1 / 4} \mathrm{in} .=.397 \mathrm{~mm} \quad \stackrel{3}{1.2} \mathrm{in} .=.794 \mathrm{~mm}$ | $=.03527396$ oz av. |
| $\frac{1}{16} \mathrm{in} .=1.588 \mathrm{~mm} \quad \frac{1}{8} \mathrm{in} .=3.175 \mathrm{~mm}$ | 1 short hundred weight ( 100 lb ) |
| ${ }_{4}^{1} \mathrm{in} .=6.350 \mathrm{~mm} \quad{ }^{\frac{1}{2}} \mathrm{in} .=12.700 \mathrm{~mm}$ | $=45.359243 \mathrm{~kg}$ |
| 1 angstrom unit $=.0000000001 \mathrm{~m}$ | 1 long hundred weight (112 1b) |
| 1 micron $(\mu)=.000001 \mathrm{~m}=.00003937 \mathrm{in}$. | $=50.802352 \mathrm{~kg}$ |
| 1 millimicron ( $\mathrm{m} \mu)=.000000001 \mathrm{~m}$ | 1 short ton (2000 lb) |
| $1 \mathrm{~m}=4.970960$ links $=1.093611 \mathrm{yd}$ | $=907.18486 \mathrm{~kg}$ |
| $=.198838 \mathrm{rod}=.0497096$ chain | 1 long ton ( 2240 lb ) $=1016.04704 \mathrm{~kg}$ |
| SQU.IRE MEASURES | 1 metric ton $=0.98420640$ long ton |
| $1 \mathrm{sq} . \mathrm{link}\left(62.7264 \mathrm{in}^{2}{ }^{2}\right)=404.6873 \mathrm{~cm}^{2}$ | $=1.1023112$ short tons |
| $1 \mathrm{sq} . \mathrm{rod}(625 \mathrm{sq}$. links $)=25.29295 \mathrm{~m}^{2}$ |  |
| 1 sq. chain ( 16 sq. rods) $=404.6873 \mathrm{~m}^{2}$ | Troy weights |
| 1 acre (10 sq. chains) $=4046.873 \mathrm{~m}^{2}$ | 1 pennyweight (dwt 24 gr ) $=1.555174 \mathrm{~g}$ |
| 1 sq. mile ( 640 acres $)=2.589998 \mathrm{~km}^{2}$ | $\mathrm{gr}, \mathrm{oz}$, pd are same as apothecary |
| $1 \mathrm{~km}^{2}=.3861006$ sq. mile |  |
| $1 \mathrm{~m}^{2}=24.7104$ sq. links $=10.76387 \mathrm{ft}^{2}$ | Apothecaries' weights |
| $=.039537$ sq. $\quad$ rod $=.00247104$ sq. | $1 \mathrm{gr}=64.798918 \mathrm{mg}$ |
| chain | $1 \mathrm{scruple}(3,20 \mathrm{gr})=1.2959784 \mathrm{~g}$ |
| CUBIC ME.\SURES | $1 \mathrm{dram}(3,3-)=3.8879351 \mathrm{~g}$ |
| 1 board ( ${ }^{\text {c }}$ | $1 \mathrm{oz}(\underset{5}{2}, 83) \quad=31.103481 \mathrm{~g}$ |
| 1 board foot (144 in. ${ }^{8}$ ) $=2359.8 \mathrm{~cm}^{8}$ | $1 \mathrm{lb}(12 \overline{3}, 5760 \mathrm{gr})=373.24177 \mathrm{~g}$ |
| $1 \operatorname{cord}\left(128 \mathrm{ft}^{8}\right)=3.625 \mathrm{~m}^{3}$ | $1 \mathrm{~g}=15.432356 \mathrm{gr}=0.771618$ Э |
| CAPACITY MEASURES | $=0.25720593=.03215074 \%$ |
| $1 \mathrm{minim}(\mathrm{m})=.0616102 \mathrm{ml}$ | $1 \mathrm{~kg}=32.1507423=2.6792285 \mathrm{lb}$ |
| 1 fl . dram $(60 \mathrm{ml})=3.69661 \mathrm{ml}$ | 1 metric carat $=200 \mathrm{mg}=3.0864712 \mathrm{gr}$ |
| $\begin{aligned} & 1 \mathrm{f} . \mathrm{oz}(8 \mathrm{fl} . \mathrm{dr})=1.80469 \mathrm{in} .^{8} \\ & =29.5729 \mathrm{ml} \end{aligned}$ | U. S. $\frac{1}{2}$ dollar should weigh 12.5 g and the |
| ```1 gill (4 f. oz.) = 7.21875 in. }\mp@subsup{}{}{3}=118.29 ml``` | smaller silver coins in proportion. |
| $1 \mathrm{liq} . \mathrm{pt}\left(28.875 \mathrm{in}^{8}\right.$ ) $=.4731671$ |  |
| 1 liq. qt $\left(57.75\right.$ in. $^{\text {s }}$ ) $=.9463331$ |  |
| 1 gallon (4 qt, $231 \mathrm{in}^{\text {a }}{ }^{\text {a }}$ ) $=3.7853321$ |  |
| 1 dry pt $\left(33.6003125\right.$ in. ${ }^{\text {8 }}$ ) $=.5505991$ |  |
| 1 dry qt $\left(67.200625\right.$ in. $\left.^{3}\right)=1.1011981$ |  |
| $1 \mathrm{pk}\left(8\right.$ dry qt, $\left.537.605 \mathrm{in} .^{8}\right)=8.809581$ |  |
| $1 \mathrm{bu}\left(4 \mathrm{pk}, 2150.42 \mathrm{in}{ }^{\text {a }}\right.$ ) ${ }^{\text {a }}$ ) 35.23831 |  |
| 1 firkin (9 gallons) $=34.067991$ |  |
| $\begin{aligned} 1 \text { liter } & =264178 \text { gal }=1.05671 \text { liq. qt } \\ & =33.8147 \mathrm{fl} . \mathrm{oz}=270.518 \mathrm{fl} . \mathrm{dr} \end{aligned}$ |  |
| $1 \mathrm{ml} .=16.2311 \mathrm{minims}$. |  |
| $\begin{aligned} 1 \mathrm{dkl} & =18.1620 \mathrm{dry} \mathrm{pt}=9.08102 \mathrm{dry} \mathrm{qt} \\ & =1.13513 \mathrm{pk}=.28378 \mathrm{bu} \end{aligned}$ |  |

[^24](For U. S. Weights and Measures, see Table 32.)
Part 1.-Metric to imperial


Note.-The Meter is the length, at the temperature of $0^{\circ} \mathrm{C}$, of the platinum-iridium bar deposited at the International Bureau of Weights and Measures at Sèvres, near Paris, France.
The present legal equivalent of the meter is 39.370113 inches, as above stated.
The Kilogram is the mass of a platinum-iridium weight deposited at the same place.
The Liter contains 1 kilogram weight of distilled water at its maximum density ( $4^{\circ} \mathrm{C}$ ), the barometer being at 760 millimeters.

[^25] (continued)

TABLE 33.-EQUIVALENTS OF METRIC AND BRITISH IMPERIAL WEIGHTS AND MEASURES (continued)
(For U. S. Weights and Measures, see Table 32.)
Part 2.-Metric to imperial, multiples

|  | Linear measure |  |  |  |  | Measure ${ }^{\text {of capacity }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { Millimeters } \\ \text { to } \\ \text { inches } \end{gathered}$ | $\begin{gathered} \text { Meters } \\ \text { to } \\ \text { feet } \end{gathered}$ | $\begin{gathered} \text { Meters } \\ \text { to } \\ \text { yards } \end{gathered}$ | $\underset{\substack{\text { Kiloo- } \\ \text { moters } \\ \text { to miles }}}{\text { cosen }}$ |  | $\begin{gathered} \text { Liters } \\ \text { to } \\ \text { pints } \end{gathered}$ | Dekaliters to gallons | Hecto. liters to bushels | $\begin{gathered} \text { Kilo- } \\ \text { liters to } \\ \text { quarters } \end{gathered}$ |
| 1 | 0.03937011 | 3.28084 | 1.09361 | 0.62137 | 1 | 1.75980 | 2.19975 | 2.74969 | 3.43712 |
| 2 | 0.07874023 | 6.56169 | 2.18723 | 1.24274 | 2 | 3.51961 | 4.39951 | 5.49938 | 6.87423 |
| 3 | 0.11811034 | 9.84253 | 3.28084 | 1.86412 | 3 | 5.27941 | 6.59926 | 8.24908 | 10.31135 |
| 4 | 0.15748045 | 13.12337 | 4.37446 | 2.48549 | 4 | 7.03921 | 8.79902 | 10.99877 | 13.74846 |
| 5 | 0.19685056 | 16.40421 | 5.46807 | 3.10686 | 5 | 8.79902 | 10.99877 | 13.74846 | 17.18558 |
| 6 | 0.23622068 | 19.68506 | 6.56169 | 3.72823 | 6 | 10.55882 | 13.19852 | 16.49815 | 20.62269 |
| 7 | 0.27559079 | 22.96590 | 7.65530 | 4.34960 | 7 | 12.31862 | 15.39828 | 19.24785 | 24.05981 |
| 8 | 0.31496090 | 26.24674 | 8.74891 | 4.97097 | 8 | 14.07842 | 17.59803 | 21.99754 | 27.49692 |
| 9 | 0.35433102 | 29.52758 | 9.84253 | 5.59235 | 9 | 15.83823 | 19.79778 | 24.74723 | 30.93404 |


| $\underbrace{\text { Square measure }}$ |  |  |  |  | Weight (Avoirdupois) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Square |  |  |  |  |  |  |  |  |
|  | centimeters | Square meters | Square meters |  | Milli- |  | Kilo• | $\begin{aligned} & \text { Kilo- } \\ & \text { grams } \end{aligned}$ | Quintals |
|  | to | to | to | Hectares |  |  | to |  |
|  | square inches | square feet | square <br> yards | to |  | $\begin{aligned} & \text { to } \\ & \text { grains } \end{aligned}$ |  | $\begin{aligned} & \text { to } \\ & \text { grains } \end{aligned}$ | $\begin{aligned} & \text { to } \\ & \text { pounds } \end{aligned}$ | hundredweights |
| 1 | 0.15500 | 10.76393 | 1.19599 | 2.4711 | 1 | 0.01543 | 15432.356 | 2.20462 | 1.96841 |
| 2 | 0.31000 | 21.52786 | 2.39198 | 4.9421 | 2 | 0.03086 | 30864.713 | 4.40924 | 3.93683 |
| 3 | 0.46500 | 32.29179 | 3.58798 | 7.4132 | 3 | 0.04630 | 46297.069 | 6.61387 | 5.90524 |
| 4 | 0.62000 | 43.05572 | 4.78397 | 9.8842 | 4 | 0.06173 | 61729.426 | 8.81849 | 7.87365 |
| 5 | 0.77500 | 53.81965 | 5.97996 | 12.3553 | 5 | 0.07716 | 77161.782 | 11.02311 | 9.84206 |
| 6 | 0.93000 | 64.58357 | 7.17595 | 14.8263 | 6 | 0.09259 | 92594.138 | 13.22773 | 11.81048 |
| 7 | 1.08500 | 75.34750 | 8.37194 | 17.2974 | 7 | 0.10803 | 108026.495 | 15.43236 | 13.77889 |
| 8 | 1.24000 | 86.11143 | 9.56794 | 19.7685 | 8 | 0.12346 | 123458.851 | 17.63698 | 15.74730 |
| 9 | 1.39501 | 96.87536 | 10.76393 | 22.2395 | 9 | 0.13889 | 138891.208 | 19.84160 | 17.71572 |
|  |  | ubic measure |  | Apothecaries' measure |  | Avoirdupo (cont.) |  |  | Apothecaries weight |
|  | Cubic decimeters to cubic inches | Cubic meters to cubic feet | Cubic meters to. cubic yards | Cubic centimeters to fluid drachms |  | $\begin{aligned} & \text { Milliers } \\ & \text { or } \\ & \text { tonnes to } \\ & \text { tons } \end{aligned}$ | $\begin{gathered} \text { Grams } \\ \text { to } \\ \text { ounces } \\ \text { troy } \end{gathered}$ | Grams <br> to penny- | $\begin{gathered} \text { Grams } \\ \text { to } \\ \text { scruples } \end{gathered}$ |
| 1 | 61.02390 | 35.31476 | 1.30795 | 0.28157 | 1 | 0.98421 | 0.03215 | 0.64301 | 0.77162 |
| 2 | 122.04781 | 70.62952 | 2.61591 | 0.56314 | 2 | 1.96841 | 0.06430 | 1.28603 | 1.54324 |
| 3 | 183.07171 | 105.94428 | 3.92386 | 0.84471 | 3 | 2.95262 | 0.09645 | 1.92904 | 2.31485 |
| 4 | 244.09561 | 141.25904 | 5.23182 | 1.12627 | 4 | 3.93683 | 0.12860 | 2.57206 | 3.08647 |
| 5 | 305.11952 | 176.57379 | 6.53977 | 1.40784 | 5 | 4.92103 | 0.16075 | 3.21507 | 3.85809 |
| 6 | 366.14342 | 211.88855 | 7.84772 | 1.68941 | 6 | 5.90524 | 0.19290 | 3.85809 | 4.62971 |
| 7 | 427.16732 | 247.20331 | 9.15568 | 1.97098 | 7 | 6.88944 | 0.22506 | 4.50110 | 5.40132 |
| 8 | 488.19123 | 282.51807 | 10.46363 | 2.25255 | 8 | 7.87365 | 0.25721 | 5.14412 | 6.17294 |
| 9 | 549.21513 | 317.83283 | 11.77159 | 2.53412 | 9 | 8.85786 | 0.28936 | 5.78713 | 6.94456 |

(continued)
(For U. S. Weights and Measures, see Table 32.)
Part 3.-Imperial to metric

LINEAR MEASURE


## SQUARE MEASURE

| $1 \mathrm{in.}^{2}$. . . . $=$ | $6.4516 \mathrm{~cm}^{2}$ |
| :---: | :---: |
| $1 \mathrm{ft}^{2}\left(144 \mathrm{in}^{2}{ }^{\text {a }}\right.$ ) | $9.2903 \mathrm{dm}^{2}$ |
| $1 \mathrm{YD}^{2}\left(9 \mathrm{ft}^{2}\right) . .=$ | $0.836126 \mathrm{~m}^{2}$ |
| 1 perch ( $30 \frac{1}{4} \mathrm{yd}^{2}$ ) $=$ | $25.293 \mathrm{~m}^{2}$ |
| $1 \mathrm{rood}(40$ perches $)=$ | 10.117 ares |
| 1 ACRE (4840 $\mathrm{yd}^{2}$ ) | 0.40468 hectare |
| $1 \mathrm{mi}^{2}$ (640 acres) | 9.00 hectares |

CUBIC ME.ISURE
$1 \mathrm{in}^{3}{ }^{3}$. . . . $=16.387 \mathrm{~cm}^{3}$
$1 \mathrm{ft}^{8}\left(1728 \mathrm{in}^{3}\right)=\left\{\begin{array}{c}0.028317 \mathrm{~m}^{3} \text { or } 28.317 \\ \mathrm{dm}^{3}\end{array}\right.$
$1 \mathrm{yd}^{8}\left(27 \mathrm{ft}^{8}\right) .=0.76455 \mathrm{~m}^{3}$

## APOTHECARIES' MEASURE

$\left.\begin{array}{l}1 \text { gallon ( } 8 \text { pints or } \\ 160 \text { fluid ounces })\end{array}\right\}=4.5459631$ liters
1 fluid ounce, f 3 ( 8 drachms)
$\left.\begin{array}{l}1 \text { fluid drachm, f } 3 \\ (60 \text { minims) }\end{array}\right\}=3.5515 \mathrm{~cm}^{3}$
$1 \underset{\text { grain weight })}{\operatorname{minim}, ~} \quad(0.91146\}=0.05919 \mathrm{~cm}^{8}$
Note.-The apothecaries' gallon is of the same capacity as the Imperial gallon.

MEASLRE OF CAP.ICITY
1 gill $\cdot$. . $=1.42$ deciliters
1 pint ( 4 gills) . . $=0.568$ liter
1 quart ( 2 pt ) . . . $=1.136$ liters
1 gallon ( 4 qt ) $\quad .=4.5459631$ liters
1 peck (2 gal) . . $=9.092$ liters
1 bushel ( 8 gal ) . . $=3.637$ dekaliters
1 quarter ( 8 bu ) . $=2.909$ hectoliters

## AVOIRDUPOIS WEIGHT



## TROY WEIGHT

$\left.\begin{array}{c}1 \text { troy ounCe }(480 \\ \begin{array}{c}\text { grains av }) \\ 1 \begin{array}{c}\text { pennyweight } \\ \text { grains) }\end{array}\end{array}(24\end{array}\right\}=31.1035$ grams
$=1.5552$ grams
Note.-The troy grain is of the same weight as the avoirdupois grain.

## APOTHECARIES' WEIGHT

1 ounce ( 8 drachms) ..$=31.1035$ grams
1 drachm, 3 i ( 3 scruples $)=3.888$ grams
1 scruple, Эi (20 grains) $=1.296$ grams
Note.-The apothecaries' ounce is of the same weight as the troy ounce. The apothecaries' grain is also of the same weight as the avoirdupois grain.

Note.-The Yard is the length at $62^{\circ} \mathrm{F}$, marked on a bronze bar deposited with the Board of Trade.
The Pound is the weight of a piece of platinum weighed in vacuo at the temperature of $0^{\circ} \mathrm{C}$, and which is also deposited with the Board of Trade.
The Gallon contains 10 lb weight of distilled water at the temperature of $62^{\circ} \mathrm{F}$, the barometer being at 30 inches.
(continued)

TABLE 33.-EQUIVALENTS OF BRITISH IMPERIAL AND METRIC WEIGHTS AND MEASURES (concluded)
(For U. S. Weights and Measures, see Table 32.)
Part 4.-Imperial to metric, multiples

|  | $\mathrm{Linear}^{\text {measure }}$ |  |  |  |  | Measure of capacity |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches centimeters | $\begin{gathered} \text { Feet } \\ \text { to } \\ \text { meters } \end{gathered}$ | $\begin{aligned} & \text { Yards } \\ & \text { to } \\ & \text { meters } \end{aligned}$ | $\begin{gathered} \text { Miles } \\ \text { to } \\ \text { kilo- } \\ \text { meters } \end{gathered}$ |  | $\begin{aligned} & \text { Quarts } \\ & \text { to } \\ & \text { liters } \end{aligned}$ | $\begin{aligned} & \text { Gallons } \\ & \text { to } \\ & \text { liters } \end{aligned}$ | $\begin{gathered} \text { Bushels } \\ \text { to } \\ \text { deka- } \\ \text { liters } \end{gathered}$ | Quarters <br> to <br> heto- <br> liters |
| 1 | 2.539998 | 0.30480 | 0.91440 | 1.60934 | 1 | 1.13649 | 4.54596 | 3.63677 | 2.90942 |
| 2 | 5.079996 | 0.60960 | 1.82880 | 3.21869 | 2 | 2.27298 | 9.09193 | 7.27354 | 5.81883 |
| 3 | 7.619993 | 0.91440 | 2.74320 | 4.82803 | 3 | 3.40947 | 13.63789 | 10.91031 | 8.72825 |
| 4 | 10.159991 | 1.21920 | 3.65760 | 6.43737 | 4 | 4.54596 | 18.18385 | 14.54708 | 11.63767 |
| 5 | 12.699989 | 1.52400 | 4.57200 | 8.04671 | 5 | 5.68245 | 22.72982 | 18.18385 | 14.54708 |
| 6 | 15.239987 | 1.82880 | 5.48640 | 9.65606 | 6 | 6.81894 | 27.27578 | 21.82062 | 17.45650 |
| 7 | 17.779984 | 2.13360 | 6.40080 | 11.26540 | 7 | 7.95544 | 31.82174 | 25.45739 | 20.36591 |
| 8 | 20.319982 | 2.43840 | 7.31519 | 12.87474 | 8 | 9.09193 | 36.36770 | 29.09416 | 23.27533 |
| 9 | 22.859980 | 2.74320 | 8.22959 | 14.48408 | 9 | 10.22842 | 40.91367 | 32.73093 | 26.18475 |


|  | Square measure |  |  |  |  | Weight (avoirdupois) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Square inches to square centimeters | Square feet to square decimeters | Square yards to square meters | Acres to hectares |  | Grains to milligrams | $\begin{aligned} & \text { Ounces } \\ & \text { to } \\ & \text { grams } \end{aligned}$ | Pounds to kilograms | Hun-dredweights quintals |
| 1 | 6.45159 | 9.29029 | 0.83613 | 0.40468 | 1 | 64.79892 | 28.34953 | 0.45359 | 0.50802 |
| 2 | 12.90318 | 18.58058 | 1.67225 | 0.80937 | 2 | 129.59784 | 56.69905 | 0.90718 | 1.01605 |
| 3 | 19.35477 | 27.87086 | 2.50838 | 1.21405 | 3 | 194.39675 | 85.04858 | 1.36078 | 1.52407 |
| 4 | 25.80636 | 37.16115 | 3.34450 | 1.61874 | 4 | 259.19567 | 113.39811 | 1.81437 | 2.03209 |
| 5 | 32.25794 | 46.45144 | 4.18063 | 2.02342 | 5 | 323.99459 | 141.74763 | 2.26796 | 2.54012 |
| 6 | 38.70953 | 55.74173 | 5.01676 | 2.42811 | 6 | 388.79351 | 170.09716 | 2.72155 | 3.04814 |
| 7 | 45.16112 | 65.03201 | 5.85288 | 2.83279 | 7 | 453.59243 | 198.44669 | 3.17515 | 3.55616 |
| 8 | 51.61271 | 74.32230 | 6.68901 | 3.23748 | 8 | 518.39135 | 226.79621 | 3.62874 | 4.06419 |
| 9 | 58.06430 | 83.61259 | 7.52513 | 3.64216 | 9 | 583.19026 | 255.14574 | 4.08233 | 4.57221 |


|  | Cubic measure |  |  | Apothecaries' Measure |  | Avoirdupois |  |  | Apothecaries |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cubic inches to cubic centimeters | Cubic feet to cubic meters | Cubic yards to cubic meters | Fluid drachms to cubic centimeters |  | Tons to milliers or tonnes | $\begin{aligned} & \text { Ounces } \\ & \text { to } \\ & \text { grams } \end{aligned}$ | Pennyweights to grams | Scruples to grams |
| 1 | 16.38702 | 0.02832 | 0.76455 | 3.55153 | 1 | 1.01605 | 31.10348 | 1.55517 | 1.29598 |
| 2 | 32.77404 | 0.05663 | 1.52911 | 7.10307 | 2 | 2.03209 | 62.20696 | 3.11035 | 2.59196 |
| 3 | 49.16106 | 0.08495 | 2.29366 | 10.65460 | 3 | 3.04814 | 93.31044 | 4.66552 | 3.88794 |
| 4 | 65.54808 | 0.11327 | 3.05821 | 14.20613 | 4 | 4.06419 | 124.41392 | 6.22070 | 5.18391 |
| 5 | 81.93511 | 0.14158 | 3.82276 | 17.75767 | 5 | 5.08024 | 155.51740 | 7.77587 | 6.47989 |
| 6 | 98.32213 | 0.16990 | 4.58732 | 21.30920 | 6 | 6.09628 | 186.62088 | 9.33104 | 7.77587 |
| 7 | 114.70915 | 0.19822 | 5.35187 | 24.86074 | 7 | 7.11233 | 217.72437 | 10.88622 | 9.07185 |
| 8 | 131.09617 | 0.22653 | 6.11642 | 28.41227 | 8 | 8.12838 | 248.82785 | 12.44139 | 10.36783 |
| 9 | 147.48319 | 0.25485 | 6.88098 | 31.96380 | 9 | 9.14442 | 279.93133 | 13.99657 | 11.66381 |

TABLE 34.-VOLUME OF A GLASS VESSEL FROM THE WEIGHT OF ITS EQUIVALENT VOLUME OF MERCURY OR WATER

If a glass vessel contains at $t^{\circ} \mathrm{C}, P$ grams of mercury, weighed with brass weights in air at 760 mmHg pressure, then its volume in $\mathrm{cm}^{3}$
at the same temperature, $t: V=P R=P \frac{p}{d}$,
at another temperature, $t_{1}: V=P R_{1}=P \frac{p}{d}\left\{1+\gamma\left(t_{1}-t\right)\right\}$
$p=$ the weight, reduced to vacuum, of the mass of mercury or water which, weighed with brass weights, equals 1 gram;
$a=$ the density of mercury or water at $t^{\circ} \mathrm{C}$,
and $\gamma$ the cubical expansion coefficient of glass.

| Temperature | ${ }^{\text {Water }}$ |  |  | Mercury |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $R$ | $R_{2}, t_{1}=10^{\circ}$ | $R_{1}, t_{1}=20^{\circ}$ | R | $R_{1}, t_{1}=10^{\circ}$ | $R_{1}, t_{1}=20^{\circ}$ |
| $0^{\circ}$ | 1.001192 | 1.001443 | 1.001693 | 0.0735499 | 0.0735683 | 0.0735867 |
| 1 | 1133 | 1358 | 1609 | 5633 | 5798 | 5982 |
| 2 | 1092 | 1292 | 1542 | 5766 | 5914 | 6098 |
| 3 | 1068 | 1243 | 1493 | 5900 | 6029 | 6213 |
| 4 | 1060 | 1210 | 1460 | 6033 | 6144 | 6328 |
| 5 | 1068 | 1193 | 1443 | 6167 | 6259 | 6443 |
| 6 | 1.001092 | 1.001192 | 1.001442 | 0.0736301 | 0.0736374 | 0.0736558 |
| 7 | 1131 | 1206 | 1456 | 6434 | 6490 | 6674 |
| 8 | 1184 | 1234 | 1485 | 6568 | 6605 | 6789 |
| 9 | 1252 | 1277 | 1527 | 6702 | 6720 | 6904 |
| 10 | 1333 | 1333 | 1584 | 6835 | 6835 | 7020 |
| 11 | 1.001428 | 1.001403 | 1.001653 | 0.0736969 | 0.0736951 | 0.0737135 |
| 12 | 1536 | 1486 | 1736 | 7103 | 7066 | 7250 |
| 13 | 1657 | 1582 | 1832 | 7236 | 7181 | 7365 |
| 14 | 1790 | 1690 | 1940 | 7370 | 7297 | 7481 |
| 15 | 1935 | 1810 | 2060 | 7504 | 7412 | 7596 |
| 16 | 1.002092 | 1.001942 | 1.002193 | 0.0737637 | 0.0737527 | 0.0737711 |
| 17 | 2261 | 2086 | 2337 | 7771 | 7642 | 7826 |
| 18 | 2441 | 2241 | 2491 | 7905 | 7757 | 7941 |
| 19 | 2633 | 2407 | 2658 | 8039 | 7872 | 8057 |
| 20 | 2835 | 2584 | 2835 | 8172 | 7988 | 8172 |
| 21 | 1.003048 | 1.002772 | 1.003023 | 0.0738306 | 0.0738103 | 0.0738288 |
| 22 | 3271 | 2970 | 3220 | 8440 | 8218 | 8403 |
| 23 | 3504 | 3178 | 3429 | 8573 | 8333 | 8518 |
| 24 | 3748 | 3396 | 3647 | 8707 | 8449 | 8633 |
| 25 | 4001 | 3624 | 3875 | 8841 | 8564 | 8748 |
| 26 | 1.004264 | 1.003862 | 1.004113 | 0.0738974 | 0.0738679 | 0.0738864 |
| 27 | 4537 | 4110 | 4361 | 9108 | 8794 | 8979 |
| 28 | 4818 | 4366 | 4616 | 9242 | 8910 | 9094 |
| 29 30 | 5110 5410 | 4632 | 4884 | 9376 | 9025 | 9210 |
| 30 | 5410 | 4908 | 5159 | 9510 | 9140 | 9325 |

## Reductions of weighings in air to vacuo

When the weight $M$ in grams of a body is determined in air, a correction is necessary for the buoyancy of the air equal to $M \delta\left(1 / d-1 / d_{1}\right)$ where $\delta=$ the density (wt. of $1 \mathrm{~cm}^{3}$ in grams $=0.0012$ ) of the air during the weighing, $d$ the density of the body, $d_{1}$ that of the weights. $\delta$ for various barometric values and humidities may be determined from Tables 631-632. The following table is computed for $\delta=0.0012$. The corrected weight $=$ $M+k M / 1000$.

| Density weighed$\qquad$ | Correction factor, $k$ |  |  | Density oirhed weighe | Correction factor, $k$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\overbrace{\substack{\text { Pt. Ir. } \\ \text { weirhts } \\ d_{1}=21.5}}$ | $\underset{\substack{\text { Brass } \\ \text { weights } \\ 8.4}}{ }$ | $\begin{aligned} & \text { Quartz or } \\ & \text { Al. weights } \\ & 2.65 \end{aligned}$ |  | $\overbrace{\substack{\text { Pt Ir. } \\ \text { weights } \\ d_{1}=21.5}}$ | $\underset{\substack{\text { Brass } \\ \text { weights } \\ 8.4}}{ }$ | Ouartz or <br> Al. weights 2.65 |
| . 5 | $+2.34$ | $+2.26$ | + 1.95 | 1.6 | +0.69 | +0.61 | $+0.30$ |
| . 6 | +1.94 | +1.86 | +1.55 | 1.7 | + . 65 | + . 56 | + . 25 |
| . 7 | +1.66 | +1.57 | +1.26 | 1.8 | + . 62 | + . 52 | + . 21 |
| . 75 | +1.55 | +1.46 | +1.15 | 1.9 | + . 58 | +. 49 | + . 18 |
| . 80 | + 1.44 | +1.36 | +1.05 | 2.0 | + . 54 | + . 46 | +. 15 |
| . 85 | +1.36 | +1.27 | +0.96 | 2.5 | +. 43 | + . 34 | + . 03 |
| . 90 | +1.28 | +1.19 | + . 88 | 3.0 | + . 34 | +. 26 | - . 05 |
| . 95 | +1.21 | +1.12 | + .81 | 4.0 | +. 24 | + . 16 | -. 15 |
| 1.00 | +1.14 | +1.06 | + . 75 | 6.0 | + . 14 | +. 06 | -. 25 |
| 1.1 | +1.04 | +0.95 | +. 64 | 8.0 | +. 09 | + . 01 | -. 30 |
| 1.2 | +0.94 | + 86 | + . 55 | 10.0 | +. 06 | -. 02 | -. 33 |
| 1.3 | + . 87 | + . 78 | +. 47 | 15.0 | +. 03 | - . . 06 | -. 37 |
| 1.4 | + .80 | +. 71 | +. 40 | 20.0 | +. 004 | - . 08 | -. 39 |
| 1.5 | + . 75 | + .66 | +. 35 | 22.0 | -. 001 | - . 09 | - . 40 |

## TABLE 36.-REDUCTIONS OF DENSITIES IN AIR TO VACUO

(This correction may be accomplished through the use of the above table for each separate weighing.)
If $s$ is the density of the substance as calculated from the uncorrected weights, $S$ its true density, and $L$ the true density of the liquid used, then the vacuum correction to be applied to the uncorrected density, $s$, is $0.0012(1-s / L)$.
Let $W_{s}=$ uncorrected weight of substance, $W_{i}=$ uncorrected weight of the liquid displaced by the substance, then by definition, $s=L W_{s} / W_{l}$. Assuming $D$ to be the density of the balance of weights, $W_{s}\{1+0.0012(1 / S-1 / D)\}$ and $W_{1}\{1+0.0012$ ( $1 / L-1 / D$ ) \} are the true weights of the substance and liquid respectively (assuming that the weighings are made under normal atmospheric corrections, so that the weight of $1 \mathrm{~cm}^{8}$ of air is 0.0012 gram ).
Then the true density $S=\frac{W_{s}\{1+0.0012(1 / S-1 / D)\}}{W_{\imath}\{1+0.0012(1 / L-1 / D)\}} L$
But from above $W_{s} / W_{t}=s / L$, and since $L$ is always large compared with 0.0012 ,

$$
S-s=0.0012(1-s / L)
$$

The values of $0.0012(1-s / L)$ for densities up to 20 and for liquids of density 1 (water), 0.852 (xylene), and 13.55 (mercury) follow:

| Density of substance $s$ | Corrections |  |  | Density of sub. stance | Corrections |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $L=1$ | $L=0.852$ | $L=13.55$ |  | $L=1$ | $L=13.55$ |
|  | Water | Xylene | Mercury | $s$ | Water | Mercury |
| 0.8 | + 0.00024 | - | - | 11. | -0.0120 | + 0.0002 |
| 0.9 | + . 00012 | - | - | 12. | - . 0132 | + .0001 |
| 1. | 0.0000 | $-0.0002$ | $+0.0011$ | 13. | - . 0144 | 0.0000 |
| 2. | - . .0012 | - . 0016 | + . 0010 | 14. | - . 0156 | 0.0000 |
| 3. | - . 0024 | -. 0030 | + . 0009 | 15. | - . 0168 | - . 0001 |
| 4. | - . 0036 | -. . 0044 | + . 0008 | 16. | -. 0180 | -. 0002 |
| 5. | - . 0048 | -. 0058 | + . 0008 | 17. | -. 0192 | -. 0003 |
| 6. | -. 0060 | -. 00073 | + . 0007 | 18. | - . 0204 | -. 0004 |
| 7. | - . 0072 | - . 0087 | + . 0006 | 19. | - . 0216 | -. 0005 |
| 8. | - . 0084 | - . 0101 | + . 0005 | 20. | - . 0228 | - . 0006 |
| 9. | - . 0096 | -. 0115 | +. 0004 |  |  |  |
| 10. | -. . 0108 | - . 0129 | +. 0003 |  |  |  |

TABLE 37.-THE INTERNATIONAL TEMPERATURE SCALE OF $1948{ }^{20}$
The International Temperature Scale that was adopted in 1927 was revised during 1948 and is designed to conform as nearly as practicable to the thermodynamic Celsius ${ }^{21}$ (Centigrade) scale as now known. This 1948 International Temperature Scale incorporates certain refinements based on experience to make it more uniform and reproducible than its predecessor. The new scale is essentially the same as the one it displaces, but it was improved by changing certain formulas and values for temperatures and constants.

Only three of the revisions in the definition of the scale result in appreciable changes in the numerical values assigned to measured temperatures. The change in the value for the silver point from $960.5^{\circ} \mathrm{C}$ to $960.8^{\circ} \mathrm{C}$ changes temperatures measured with the standard thermocouple. The adoption of a different value for the radiation constant $c_{2}$ changes all temperatures above the gold point, while the use of the Planck radiation formula instead of the Wien formula affects the very high temperatures. (See Table 40 for the magnitude of the changes due to these two causes for high temperatures.) The 1948 temperature scale, like the 1927 scale, is based upon six fixed points (Table 38) and upon specified formulas for the relations between temperature and the indications of the instruments calibrated at these fixed points. Temperature on the 1948 scale will be designated as ${ }^{\circ} \mathrm{C}$, or ${ }^{\circ} \mathrm{C}$ (Int. 1948) and denoted by the symbol $t$.

The means available for interpolation between the fixed points lead to a division of the scale into four parts:
(a) From $0^{\circ} \mathrm{C}$ to the freezing points of antimony the temperature $t$ is defined by the formula

$$
R_{t}=R_{0}\left(1+A t+B t^{2}\right)
$$

where $R_{t}$ is the resistance, at temperature $t$, of a standard platinum resistance thermometer.
(b) From the oxygen point (Table 38) to $0^{\circ} \mathrm{C}$ the temperature $t$ is similarly defined by the formula

$$
R_{t}=R_{0}\left[1+A t+B t^{2}+C(t-100) t^{3}\right]
$$

(c) From the freezing point of antimony to the gold point (Table 38) the temperature $t$ is defined by the formula

$$
E=a+b t+c t^{2},
$$

where $E$ is the electromotive force of a standard thermocouple of platinum and platinumrhodium alloy, when one junction is at $0^{\circ} \mathrm{C}$ and the other at temperature $t$.

Recommendations are given for the construction, calibration, and use of these two types of measuring devices.
(d) Above the gold point the temperature $t$ is defined by the formula

$$
\frac{J_{\mathrm{t}}}{J_{\Delta \mathrm{u}}}=\frac{\exp \left[c_{2} /\left(\lambda\left(t_{\Delta u}+T_{0}\right)\right)\right]-1^{*}}{\exp \left[c_{2} /\left(\lambda\left(t+T_{0}\right)\right)\right]-1}
$$

where $J_{t}$ and $J_{A \mathrm{u}}$ are the radiant energies per unit wavelength interval at wavelength $\lambda$, emitted per unit time by unit area of a blackbody at temperature $t$, and at the gold point $t_{\text {Au }}$, respectively.
$c_{2}$ is 1.438 cm degrees.
$T_{0}$ is the temperature of the ice point in ${ }^{\circ} \mathrm{K}$.
$\lambda$ is a wavelength of the visible spectrum.
$e$ is the base of Naperian logarithms.
Secondary fixed points.-In addition to the six fundamental and primary fixed points (Table 38), a number of secondary fixed points are available and may be useful for various purposes. Some of the more constant and reproducible of these fixed points and their temperatures on the International Temperature Scale of 1948 are listed in Table 41. The relation between this new temperature scale and the thermodynamic Celsius scale is discussed in this paper also.

The resulting changes in the 1927 International Temperature Scale below the gold point $\left(1063^{\circ} \mathrm{C}\right)$ to correct it to the 1948 International Temperature Scale are given in Table 39.
The use of the Planck formula and a wavelength interval within the visible spectrum to determine temperatures presupposes the use of an optical pyrometer. (See Table 77.)

[^26]TABLE 38.-FUNDAMENTAL AND PRIMARY FIXED POINTS UNDER THE STANDARD PRESSURE OF 1013250 DYNES/CM $=$

|  | Temperature |
| :---: | :---: |
| Temperature of equilibrium between liquid oxygen and its vapor (oxyger: point) | - 182.970 |
| Temperature of equilibrium between ice and air saturated water (ice point) fundamental fixed point. | 0 |
| Temperature of equilibrium between liquid water and its vapor (steam point) fundcmental fixed point. | 100 |
| Temperature of equilibrium between liquid sulfur and its vapor (sulfur point) | 444.600 |
| Temperature of equilibrium between solid and liquid silver (silver point) | 960.8 |
| Temperature of equilibrium between solid and liquid gold (gold point) | 1063.0 |

TABLE 39.-DIFFERENCES BETWEEN THE INTERNATIONAL TEMPERATURE SCALES OF 1948 AND 1927 IN THE THERMOCOUPLE RANGE

| Temperature |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{C}$ (Int. 1948) | $\begin{aligned} & { }^{\circ} \mathrm{C} \text { (Int. 1948) } \\ & { }^{\circ} \mathrm{C} \text { minus } \text { (Int. 1927) } \end{aligned}$ | ${ }^{\circ} \mathrm{C}$ (Int. 1948) | $\begin{aligned} & { }^{\circ} \mathrm{C} \text { ( (Int. 1948) } \\ & { }^{\circ} \mathrm{C} \text { (Ininus. } \end{aligned}$ | ${ }^{\circ} \mathrm{C}$ (Int. 1948) | $\begin{aligned} & { }^{\circ} \mathrm{C} \text { ( Int. 1948) } \\ & \text { minus } \\ & { }^{\circ} \mathrm{C} \text { (Int. 1927) } \end{aligned}$ |
| 630.5 | . 00 | 800 | . 42 | 950 | . 32 |
| 650 | +. 08 | 839.5 | .43. (max.) | 960.8 | . 30 |
| 700 | . 24 | 850 | . 43 | 1000 | . 20 |
| 750 | . 35 | 900 | . 40 | 1050 | . 05 |
|  |  |  |  | 1063 | . 00 |

TABLE 40.-CORRESPONDING TEMPERATURES ON THE INTERNATIONAL TEMPERATURE SCALES OF 1948 AND 1927

| $\begin{gathered} { }^{\circ} \mathrm{C} \\ \text { (Int. 1948) } \end{gathered}$ | $\begin{gathered} { }^{\circ} \mathrm{C} \\ \text { Int. 1927) } \end{gathered}$ | Corresponding Fahrenheit temperatures |  | $\begin{gathered} { }^{\circ} \mathrm{C} \\ \text { Int. 1948) } \end{gathered}$ | $\stackrel{\circ}{(\text { Int. }}{ }^{\mathrm{C}}$ | Corresponding Fahrenheit temperatures |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | (1948) | (1927) |  |  | (1948) | (1927) |
| 630.50 | 630.50 | 1166.9 | 1166.9 | 2100 | 2107 | 3812 | 3825 |
| 650 | 649.92 | 1202 | 1201.9 | 2200 | 2208 | 3992 | 4007 |
| 700 | 699.76 | 1292 | 1291.6 | 2300 | 2310 | 4172 | 4189 |
| 750 | 749.65 | 1382 | 1381.4 | 2400 | 2411 | 4352 | 4372 |
|  |  |  |  | 2500 | 2512 | 4532 | 4554 |
| 800 | 799.58 | 1472 | 1471.2 |  |  |  |  |
| 850 | 849.57 | 1562 | 1561.2 | 2600 | 2613 | 4712 | 4736 |
| 900 | 899.60 | 1652 | 1651.3 | 2700 | 2715 | 4892 | 4919 |
| 950 | 949.68 | 1742 | 1741.4 | 2800 | 2816 | 5072 | 5102 |
|  |  |  |  | 2900 | 2918 | 5252 | 5285 |
| 960.80 | 960.50 | 1761.4 | 1760.9 | 3000 | 3020 | 5432 | 5468 |
| 1000 | 999.80 | 1832 | 1831.6 |  |  |  |  |
| 1050 | 1049.95 | 1922 | 1921.9 | 3100 | 3122 | 5612 | 5651 |
| 1063.00 | 1063.00 | 1945.4 | 1945.4 | 3200 | 3223 | 5792 | 5834 |
|  |  |  |  | 3300 | 3325 | 5972 | 6018 |
| 1100 | 1100.2 | 2012 | 2012 | 3400 | 3428 | 6152 | 6202 |
| 1200 | 1200.6 | 2192 | 2193 | 3500 | 3530 | 6332 | 6386 |
| 1300 | 1301.1 | 2372 | 2374 |  |  |  |  |
| 1400 | 1401.7 | 2552 | 2555 | 3600 | 3632 | 6512 | 6570 |
| 1500 | 1502.3 | 2732 | 2736 | 3700 | 3735 | 6692 | 6754 |
|  |  |  |  | 3800 | 3837 | 6872 | 6939 |
| 1600 | 1603.0 | 2912 | 2917 | 3900 | 3940 | 7052 | 7124 |
| 1700 | 1703.8 | 3092 | 3099 | 4000 | 4043 | 7232 | 7309 |
| 1800 | 1804.6 | 3272 | 3280 |  |  |  |  |
| 1900 | 1905.5 | 3452 | 3462 | 4100 | 4146 | 7412 | 7495 |
| 2000 | 2006.4 | 3632 | 3644 | 4200 | 4249 | 7592 | 7681 |
|  |  |  |  | 4300 | 4353 | 7772 | 7867 |



TABLE 42.-CORRESPONDING TEMPERATURES ON THE INTERNATIONAL TEMPERATURE SCALE OF 1948 AND RESULTS USING WIEN'S EQUATION

| $t,{ }^{\circ} \mathrm{C}$ <br> (Int. 1948 ) | $t_{w},{ }^{\circ} \mathrm{C}$ | $t,{ }^{\circ} \mathrm{C}$ <br> (Int. 1948 ) | $t_{w,},{ }^{\circ} \mathrm{C}$ | $t,{ }^{\circ} \mathrm{C}$ <br> (Int. 1948 ) | $t_{\boldsymbol{w},}{ }^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1063 | 1063.0 | 2500 | 2500.2 | 4000 | 4005.4 |
| 1500 | 1500.0 | 3000 | 3000.7 | 4500 | 4511.3 |
| 2000 | 2000.0 | 3500 | 3502.1 | 5000 | 5021.5 |

## TABLE 43.-CORRECTION FOR TEMPERATURE OF EMERGENT MERCURIAL THERMOMETER THREAD

When the temperature of a portion of a thermometer stem with its mercury thread differs much from that of the bulb, a correction is necessary to the observed temperature unless the instrument has been calibrated for the experimental conditions. This stem correction is proportional to $n \beta(T-t)$, where $n$ is the number of degrees in the exposed stem, $\beta$ the apparent coefficient of expansion of mercury in the glass, $T$ the measured temperature, and $t$ the mean temperature of the exposed stem. For temperatures up to $100^{\circ} \mathrm{C}$, the value of $\beta$ is for Jena $16^{111}$ or Greiner and Friedrich resistance glass, 0.000159 , for Jena $59^{111}$, 0.000164 , and when of unknown composition it is best to use a value of about 0.000155 . The formula requires a knowledge of the temperature of the emergent stem. This may be approximated in one of three ways: (1) by a "fadenthermometer"; (2) by exploring the temperature distribution of the stem and calculating its mean temperature; and (3) by suspending along the side of, or attaching to, the stem, a single thermometer.

TABLE 44.-STEM CORRECTION FOR CENTIGRADE THERMOMETER ${ }^{22}$

| Values of $0.000155 n(T-t)$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ( $T-{ }^{t}$ |  |  |  |  |  |  |  |
| $n$ | $10^{\circ}$ | $20^{\circ}$ | $30^{\circ}$ | $40^{\circ}$ | $50^{\circ}$ | $60^{\circ}$ | $70^{\circ}$ | $80^{\circ}$ |
| $10^{\circ} \mathrm{C}$ | 0.02 | 0.03 | 0.05 | 0.06 | 0.08 | 0.09 | 0.11 | 0.12 |
| 20 | 0.03 | 0.06 | 0.09 | 0.12 | 0.16 | 0.19 | 0.22 | 0.25 |
| 30 | 0.05 | 0.09 | 0.14 | 0.19 | 0.23 | 0.28 | 0.33 | 0.37 |
| 40 | 0.06 | 0.12 | 0.19 | 0.25 | 0.31 | 0.37 | 0.43 | 0.50 |
| 50 | 0.08 | 0.16 | 0.23 | 0.31 | 0.39 | 0.46 | 0.54 | 0.62 |
| 60 | 0.09 | 0.19 | 0.28 | 0.37 | 0.46 | 0.56 | 0.65 | 0.74 |
| 70 | 0.11 | 0.22 | 0.33 | 0.43 | 0.54 | 0.65 | 0.76 | 0.87 |
| 80 | 0.12 | 0.25 | 0.37 | 0.50 | 0.62 | 0.74 | 0.87 | 0.99 |
| 90 | 0.14 | 0.28 | 0.42 | 0.56 | 0.70 | 0.84 | 0.98 | 1.12 |
| 100 | 0.16 | 0.31 | 0.46 | 0.62 | 0.78 | 0.93 | 1.08 | 1.24 |

${ }^{22}$ Taken from Smithsonian Meteorological Tables.

## TABLE 45.-REDUCTION OF GAS THERMOMETERS TO THERMODYNAMIC SCALE

The final standard scale is Kelvin's thermodynamic scale, independent of the properties of any substance, a scale resulting from the use of a gas thermoneter using a perfect gas. A discussion of this is given by Buckingham, ${ }^{228}$ "The thermodynamic correction of the centigrade constant-pressure scale at the given temperature is very nearly proportional to the constant pressure at which the gas is kept" and "the thermodynamic correction to the centigrade constant-volume scale is approximately proportional to the initial pressure at the ice point." These two rules are very convenient, since from the corrections for any one pressure, one can calculate approximately those for the same gas at any other pressure.

The highest temperature possible is limited by the container for the gas. Day and Sosman carried a platinum-rhodium gas thermometer up to the melting point of palladium. For most work, however, the region of the gas thermometer should be considered as ending at about $1000^{\circ} \mathrm{C}\left(1273^{\circ} \mathrm{K}\right)$.
Note: All corrections in the following table are to be added alycbraically.

| ${ }^{\text {Temp. }}{ }^{\text {C }}$ C | $273.16^{\circ} \mathrm{K}$ (ice point) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Constant pressure $=100 \mathrm{~cm}$ |  |  | Constant vol., $p_{0}=100 \mathrm{~cm}, t_{0}=0^{\circ} \mathrm{C}$ |  |  |
|  | He | H | N | He | H | N |
| - 240 | - | $+1.0$ | - | +0.02 | +0.18 | - |
| - 200 | $+0.13$ | + . 26 |  | + . 01 | $+.06$ |  |
| - 100 | + . 04 | +. 03 | $+0.40$ | . 000 | + . 010 | $+0.06$ |
| - 50 | + . 012 | +. 02 | +. 12 | . 000 | $+.004$ | + . 02 |
| + 25 | -. 003 | -. 003 | -. 020 | . 000 | . 000 | - . 006 |
| $+\quad 50$ $+\quad 15$ | - . 003 | -. 003 | - . 025 | . 000 | . 000 | -. 006 |
| + 75 | - . 003 | - . 003 | -. 017 | . 000 | . 000 | - . 004 |
| +150 | $+.007$ | $+.01$ | $+.04$ | $+.000$ | +. 001 | $+.01$ |
| + 200 +150 | $+.01$ | +. 02 | +.11 | . 000 | $+.002$ | +. 04 |
| + 450 | +. 1 | +0.04 | +. 5 | 0.00 | $+0.01$ | +. 2 |
| $+1000$ | $+0.3$ | - | $+1.7$ | - | - | + 7 |
| $+1500$ | - | - | + 3 . | - | - | +1.3 |

[^27]
## Comparlsons

Prior to the adoption of the 1927 International Temperature Scale, the Pt-Pt10\% Rh thermocouple was almost universally used for scales $450^{\circ}$ to $1100^{\circ} \mathrm{C}$, and defining equations were quadratic or cubic depending upon the number of calibration points.

The scale based on the work of Holborn and Day was calibrated at the freezing point of $\mathrm{Zn}\left(419.0^{\circ} \mathrm{C}\right), \mathrm{Sb}\left(630.6^{\circ} \mathrm{C}\right)$, and $\mathrm{Cu}\left(1084.1^{\circ} \mathrm{C}\right)$, and a quadratic equation, $E=a+v t+$ $\mathrm{ct}^{2}$, for interpolation. This was almost universally used from 1900-1909. Work of Waidner, Burgess, 1909, and Day, Sosman, 1910-1912, necessitated a readjustment. In 1912 the Bureau of Standards redefined its scale, assigning values determined with the resistance thermometer to the Zn and Sb points, while the freezing point of Cu was taken as $1083.0^{\circ} \mathrm{C}$. This 1912 scale, used from 1912-1916, will be called the $\mathrm{Zn}, \mathrm{Sb}, \mathrm{Cu}$ temperature scale.
A scale proposed by Sosman and revised by Adams was realized by using a standard reference table, giving the average $t$-emf relation for thermocouple used by Day and Sosman. A deviation curve, determined by any other couple by calibration at several points would be plotted relating the difference between observed emf and the emf from the reference table against the obs. emf of the couple. This scale, although very convenient, is not completely defined and no comparison is made here.

In 1916, the Physikalische-Technische Reichsanstalt adopted a scale with the couple calibrated at the Sd point $\left(320.9^{\circ} \mathrm{C}\right), \mathrm{Sb}\left(630^{\circ} \mathrm{C}\right), \mathrm{Au}\left(1063^{\circ} \mathrm{C}\right)$, and $\operatorname{Pd}\left(1557^{\circ} \mathrm{C}\right)$. No comparison will be made here.

A scale adopted by the Bureau of Standards in 1916 was defined by calibration at the Zn and Al points with a Cu point $\left(1083.0^{\circ} \mathrm{C}\right)$. This was used from 1916-1926 and is here designated the $\mathrm{Zn}, \mathrm{Al}, \mathrm{Cu}$ scale.

The scale adopted by the P.-T.R. and the Bureau of Standards in 1924 was calibrated at Zn and Sb points (determined by resistance thermometer), the Ag point $\left(960.5^{\circ} \mathrm{C}\right)$, and the Au point $\left(1063.0^{\circ} \mathrm{C}\right)$. It will be designated the $\mathrm{Zn}, \mathrm{Sb}, \mathrm{Ag}, \mathrm{Au}$ scale.

The 1927 7th Annual Conference of Weights and Measures ( 31 nations) unanimously adopted what is between $660^{\circ}$ and $1063^{\circ} \mathrm{C}$ the $\mathrm{Zn}, \mathrm{Sb}, \mathrm{Ag}, \mathrm{Cu}$ scale with the Zn point omitted. The table below shows a comparison of the various scales. The following values for the freezing points were used:

| $\mathrm{Zn} 419.47^{\circ} \mathrm{C}$ | $\mathrm{Al} 659.23^{\circ} \mathrm{C}$ | Au | $1063.0^{\circ} \mathrm{C}$ |
| :--- | :--- | :--- | :--- |
| $\mathrm{Sb} 630.52^{\circ} \mathrm{C}$ | $\mathrm{Ag} 960.5^{\circ} \mathrm{C}$ | $\mathrm{Cu}\left(\right.$ reducing atm $\left.{ }^{\circ}\right)$ | $1083.0^{\circ} \mathrm{C}$ |

## Temperature differences between 1927 I.T.S. and various older scales

|  | I.T.S.- | I.T.S | T.S |  | I.T.S | I.T.S.- | I.T |  | I.T.S.- | I.T.S.- |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{ZnSb}$ | ZnAl - | ZnSb | ${ }^{\circ} \mathrm{C}$ | $\mathrm{ZnSb}_{\mathrm{Cu}}$ | ZnAl - | $\mathrm{ZnSb}$ |  | $\mathrm{ZnSb}^{\text {che }}$ | ZnA1. | ZnSb |
|  |  |  |  | ${ }^{\circ} \mathrm{C}$ |  |  | Ag.lu | ${ }^{\circ} \mathrm{C}$ |  | Cu | u |
| 600 | - ${ }^{\circ} .08$ | ${ }^{\circ} .00$ | - ${ }^{\circ} .04$ | 900 | - ${ }^{\circ} .26$ | $-^{\circ} .21^{\circ}$ | - ${ }^{\circ} .03$ | 1050 | - ${ }^{\circ} .04$ | - ${ }^{\circ} .03$ | ${ }^{\circ} .00$ |
| 700 | -. 16 | -. 08 | -. 08 | 950 | -. 23 | -. 18 | -. 01 | 1063 | -. 01 | . 00 | . 00 |
| 750 | . 24 | . 16 | -. 09 | 960.5 | -. 21 | -. 16 | . 00 | 1083 | +. 04 | $+.03$ | -. 01 |
| 800 | - . 28 | -. 20 | -. 08 | 1000 | -. 15 | -. 12 | . 01 | 1100 | + . 08 | + . 08 | . 03 |
| 850 | - . 29 | -. 22 | - . 06 |  |  |  |  |  |  |  |  |

## REFERENCE TABLES FOR THERMOCOUPLES ${ }^{23}$

The emf developed by thermocouples of the same materials, even very carefully made, differ slightly for the same temperature. It has been found convenient to compare the emf of a couple being calibrated with that of a standard thermocouple of the same materials. If the differences in emf's between the standard and the calibrated couple be plotted against the temperature, the temperature for an observed emf can be read very accurately. Reference tables for three types of thermocounles follow.

[^28]
table 49.-CORRESPONDING VALUES OF TEMPERATURE AND ELECTRO. MOTIVE FORCE FOR IRON-CONSTANTAN THERMOCOUPLES
(Reference junctions at $0^{\circ} \mathrm{C}$ )

|  | Electromotive force mv mv | ${ }^{\text {Temp. }}{ }^{\text {C }}$. | Electro motive mv | ${ }^{\text {Temp }}{ }^{\circ} \mathrm{C}$. | Electromotive mv | ${ }^{\text {Temp }} \mathrm{C}$. | Electro motive force mv |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0 | . 00 | 400 | 22.06 | 800 | 45.68 |
|  |  | 10 | . 52 | 410 | 22.61 | 810 | 46.33 |
|  |  | 20 | 1.05 | 420 | 23.16 | 820 | 46.99 |
|  |  | 30 | 1.58 | 430 | 23.71 | 830 | 47.65 |
|  |  | 40 | 2.12 | 440 | 24.26 | 840 | 48.30 |
|  |  | 50 | 2.66 | 450 | 24.81 | 850 | 48.96 |
|  |  | 60 | 3.20 | 460 | 25.36 | 860 | 49.62 |
|  |  | 70 | 3.75 | 470 | 25.91 | 870 | 50.28 |
|  |  | 80 | 4.30 | 480 | 26.46 | 880 | 50.94 |
|  |  | 90 | 4.85 | 490 | 27.01 | 890 | 51.59 |
|  |  | 100 | 5.40 | 500 | 27.57 | 900 | 52.22 |
|  |  | 110 | 5.95 | 510 | 28.13 | 910 | 52.84 |
|  |  |  | 6.51 | 520 | 28.69 | 920 | 53.43 |
|  |  | 130 | 7.07 | 530 | 29.25 | 930 | 54.02 |
|  |  | 140 | 7.63 | 540 | 29.81 | 940 | 54.61 |
|  |  | 150 | 8.19 | 550 | 30.38 | 950 | 55.21 |
|  |  | 160 | 8.75 | 560 | 30.95 | 960 | 55.80 |
|  |  | 170 | 9.31 | 570 | 31.52 | 970 | 56.39 |
|  |  | 180 | 9.87 | 580 | 32.10 | 980 | 56.99 |
|  |  | 190 | 10.43 | 590 | 32.68 | 990 | 57.59 |
| -200 | --8.27 | 200 | 10.99 | 600 | 33.26 33.85 | 1000 | 58.19 |
| - 190 | -8.02 |  | 11.55 |  | 33.85 |  |  |
| - 180 | $-7.75$ | 220 | 12.11 | 620 | 34.44 |  |  |
| - 170 | $-7.46$ | 230 | 12.67 | 630 | 35.02 |  |  |
| -160 | -7.14 | 240 | 13.23 | 640 | 35.62 |  |  |
| -150 | $-6.80$ | 250 | 13.79 | 650 | 36.22 |  |  |
| - 140 | -6.44 | 260 | 14.35 | 660 | 36.82 |  |  |
| -130 | -6.06 | 270 | 14.90 | 670 | 37.43 |  |  |
| -120 | - 5.66 | 280 | 15.45 | 680 | 38.04 |  |  |
| -110 | -5.25 | 290 | 16.00 | 690 | 38.66 |  |  |
| $-100$ | -4.82 | 300 | 16.55 | 700 | 39.28 |  |  |
| - 90 | -4.38 | 310 | 17.11 | 710 | 39.90 |  |  |
| - 80 | -3.93 | 320 | 17.66 | 720 | 40.53 |  |  |
| - 70 | -3.47 | 330 | 18.21 | 730 | 41.16 |  |  |
| - 60 | -3.00 | 340 | 18.76 | 740 | 41.80 |  |  |
| - 50 | $-2.52$ | 350 | 19.31 | 750 | 42.45 |  |  |
| - 40 | $-2.03$ | 360 | 19.86 | 760 | 43.09 |  |  |
| - 30 | -1.53 | 370 | 20.41 | 770 | 43.74 |  |  |
| - 20 | -1.03 | 380 | 20.96 | 780 | 44.39 |  |  |
| - 10 | -0.52 | 390 | 21.51 | 790 | 45.04 |  |  |
| 0 | . 00 | 400 | 22.06 | 800 | 45.68 |  |  |

TABLE 50.-CORRESPONDING VALUES OF TEMPERATURE AND ELECTROMOTIVE FORCE FOR IRON-CONSTANTAN THERMOCOUPLES
(Reference junctions at $32^{\circ} \mathrm{F}$ )

| $\underset{\substack{\text { Temp. }}}{ }$ | Electromotive force mv | $\stackrel{\text { Temp. }}{\circ} \mathrm{F}$. | Electro. motive force m |  | Electromotive force mv |  | Electromotive force mv | $\underset{\mathrm{F}}{\text { Temp. }}$ | Electromotive mv |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0 | -. 92 | 500 | 14.35 | 1000 | 29.69 | 1500 | 46.70 |
|  |  | 10 | -. 63 | 510 | 14.65 | 1010 | 30.00 | 1510 | 47.06 |
|  |  | 20 | -. 35 | 520 | 14.96 | 1020 | 30.32 | 1520 | 47.43 |
|  |  | 30 | -. 06 | 530 | 15.27 | 1030 | 30.63 | 1530 | 47.79 |
|  |  | 40 | +. 23 | 540 | 15.57 | 1040 | 30.95 | 1540 | 48.16 |
|  |  | 50 | . 52 | 550 | 15.88 | 1050 | 31.27 | 1550 | 48.52 |
|  |  | 60 | . 82 | 560 | 16.19 | 1060 | 31.59 | 1560 | 48.89 |
|  |  | 70 | 1.11 | 570 | 16.49 | 1070 | 31.91 | 1570 | 49.25 |
|  |  | 80 | 1.41 | 580 | 16.80 | 1080 | 32.23 | 1580 | 49.62 |
|  |  | 90 | 1.70 | 590 | 17.11 | 1090 | 32.55 | 1590 | 49.98 |
|  |  | 100 | 2.00 | 600 | 17.42 | 1100 | 32.87 | 1600 | 50.35 |
|  |  | 110 | 2.30 | 610 | 17.72 | 1110 | 33.19 | 1610 | 50.71 |
|  |  | 120 | 2.60 | 620 | 18.03 | 1129 | 33.52 | 1620 | 51.08 |
|  |  | 130 | 2.90 | 630 | 18.33 | 1130 | 33.85 | 1630 | 51.45 |
|  |  | 140 | 3.20 | 640 | 18.64 | 1140 | 34.17 | 1640 | 51.81 |
|  |  | 150 | 3.50 | 650 | 18.94 | 1150 | 34.50 | 1650 | 52.17 |
|  |  | 160 | 3.81 | 660 | 19.25 | 1160 | 34.83 | 1660 | 52.51 |
|  |  | 170 | 4.11 | 670 | 19.55 | 1170 | 35.16 | 1670 | 52.84 |
|  |  | 180 | 4.42 | 680 | 19.86 | 1180 | 35.48 | 1680 | 53.17 |
|  |  | 190 | 4.72 | 690 | 20.17 | 1190 | 35.82 | 1690 | 53.50 |
| -300 | $-7.87$ | 200 | 5.03 | 700 | 20.47 | 1200 | 36.15 | 1700 | 53.83 |
| - 290 | $-7.75$ | 210 | 5.34 | 710 | 20.78 | 1210 | 36.48 | 1710 | 54.16 |
| - 280 | - 7.55 | 220 | 5.64 | 720 | 21.08 | 1220 | 36.82 | 1720 | 54.48 |
| - 270 | - 7.38 | 230 | 5.95 | 730 | 21.39 | 1230 | 37.16 | 1730 | 54.81 |
| - 260 | - 7.20 | 240 | 6.26 | 740 | 21.69 | 1240 | 37.50 | 1740 | 55.14 |
| -250 | - 7.02 |  |  | 750 | 22.00 | 1250 | 37.84 | 1750 | 55.47 |
| - 240 | -6.83 | 260 | 6.88 | 760 | 22.30 | 1260 | 38.18 | 1760 | 55.80 |
| - 230 | -6.63 | 270 | 7.19 | 770 | 22.61 | 1270 | 38.52 | 1770 | 56.13 |
| - 220 | -6.43 | 280 | 7.50 | 780 | 22.91 | 1280 | 38.86 | 1780 | 56.46 |
| -210 | $-6.22$ | 290 | 7.81 | 790 | 23.22 | 1290 | 39.21 | 1790 | 56.79 |
| - 200 | $-6.01$ | 300 | 8.12 | 800 | 23.52 | 1300 | 39.55 | 1800 | 57.12 |
| - 190 | $-5.79$ | 310 | 8.43 | 810 | 23.83 | 1310 | 39.89 |  |  |
| -180 | $-5.57$ | 320 | 8.75 | 820 | 24.13 | 1320 | 40.24 |  |  |
| - 170 | $-5.34$ | 330 | 9.06 | 830 | 24.44 | 1330 | 40.59 |  |  |
| -160 | -5.11 | 340 | 9.37 | 840 | 24.74 | 1340 | 40.94 |  |  |
| -150 | -4.87 | 350 | 9.68 | 850 | 25.05 | 1350 | 41.30 |  |  |
| -140 | - 4.63 | 360 | 10.00 | 860 | 25.36 | 1360 | 41.65 |  |  |
| - 130 | -4.38 | 370 | 10.31 | 870 | 25.66 | 1370 | 42.01 |  |  |
| - 120 | $-4.13$ | 380 | 10.62 | 880 | 25.97 | 1380 | 42.36 |  |  |
| - 110 | $-3.88$ | 390 | 10.93 | 890 | 26.28 | 1390 | 42.72 |  |  |
| - 100 | $-3.63$ | 400 | 11.24 | 900 | 26.58 | 1400 | 43.08 |  |  |
| - 90 | -3.37 | 410 | 11.56 | 910 | 26.89 | 1410 | 43.44 |  |  |
| - 80 | -3.11 | 420 | 11.87 | 920 | 27.20 | 1420 | 43.80 |  |  |
| - 70 | -2.85 | 430 | 12.18 | 939 | 27.51 | 1430 | 44.16 |  |  |
| - 60 | -2.58 | 440 | 12.49 | 940 | 27.82 | 1440 | 44.52 |  |  |
| - 50 | -2.31 | 450 | 12.80 | 950 | 28.13 | 1450 | 44.88 |  |  |
| - 40 | $-2.04$ | 460 | 13.11 | 960 | 28.44 | 1460 | 45.24 |  |  |
| - 30 | -1.76 | 470 | 13.42 | 970 | 28.75 | 1470 | 45.61 |  |  |
| - 20 | - 1.48 | 480 | 13.73 | 980 | 29.06 | 1480 | 45.97 |  |  |
| - 10 | -1.20 | 490 | 14.04 | 990 | 29.38 | 1490 | 46.33 |  |  |
| 0 | - . 92 | 500 | 14.35 | 1000 | 29.69 | 1500 | 46.70 |  |  |

TABLE 51.-STANDARD FAHRENHEIT TABLE FOR CHROMEL.ALUMEL* THERMOCOUPLES


[^29]TABLE 52.-SYMBOLS AND DEFINING EXPRESSIONS FOR RADIANT ENERGY ${ }^{\text {na }}$

Radiant energy is energy traveling in the form of electromagnetic waves. It is measured in units of energy such as ergs, joules, calories, and kilowatt hours. Some units, symbols, and abbreviations used in discussing radiant energy are as follows:

| Designation | Symbol and defining expression | Unit | Proposed term ${ }^{28}$ |
| :---: | :---: | :---: | :---: |
| Radiant energy | U |  | Radiant energy |
| Spectral radiant energy. | $U_{\lambda}=\frac{d U}{d \lambda}$ |  | Spectral radiant energy |
| Radiant energy density. | $u=\frac{d U}{d V}$ | $\mathrm{erg} / \mathrm{cm}^{8}$ | Radiant energy density |
| Radiant flux | $\phi(P)=\frac{d U}{d t}$ | watt, erg/sec | Radiant flux (radiance *) |
| Radiant flux density... | $W=\frac{d \phi}{d A}$ | watt/cm ${ }^{2}$ | $\begin{aligned} & \text { Radiant flux } \\ & \left(\text { radiancy }{ }^{*}\right. \text { ) density } \end{aligned}$ |
| source $\qquad$ | $J=\frac{d \phi}{d \omega}$ | watt/steradian | Radiant intensity |
| Spectral radiant intensity | $J_{\lambda}=\frac{d J}{d \lambda}$ | watt/steradian | Spectral radiant intensity |
| Radiant flux density of a source per unit solid angle | $B,(N)=\frac{d W}{d \omega}$ | watt/(steradian $\mathrm{cm}^{2}$ ) | Steradiancy * |
| Radiant intensity of a source per unit area.. | $B=\frac{d J}{d A}$ | watt/(steradian $\mathrm{cm}^{2}$ ) | Steradiancy* |
| Radiant flux per unit area | $E=\frac{d \phi}{d A}$ |  | Irradiancy |

The standard radiator is the blackbody, which may be defined as a body that absorbs all the radiation that falls upon it, i.e., it neither reflects nor transmits any of the incident radiation. From this simple definition and some very plausible assumptions it can be shown that the blackbody radiates more energy than any other temperature radiator when both are at the same temperature. The total amount of energy (i.e., for all wavelengths) radiated by a blackbody depends upon the temperature raised to the fourth power and a constant $\sigma$ that had to be measured:

$$
W=\sigma T^{4}
$$

If a blackbody is radiating to another blackbody it will at the same time receive radiation from the second blackbody and, under the proper geometrical conditions, the net radiation lost by the first blackbody is

$$
W=\sigma\left(T_{1}^{4}-T_{2}^{4}\right)
$$

The spectral distribution of this radiation is given by the Planck equation:

$$
J_{\lambda}=c_{1} \lambda^{-5} /\left[\exp \left(c_{2} / \lambda T\right)-1\right] \dagger
$$

For values of the product $\lambda T$ less than $3000 \mu \mathrm{deg}$, the Wien equation

$$
J_{\lambda}=c_{1} \lambda^{-5} /\left[\exp \left(c_{2} / \lambda T\right)\right]
$$

gives values that are correct to better than 1 percent.
The values of a number of the radiation constants have been selected from Table 26 and are given in Table 53. All the blackbody calculations given were made with these constants. Some calculated results ${ }^{24}$ for the total radiation $W$ for a series of temperatures and of $J_{\lambda}$ for a range of temperatures and for wavelengths have been calculated and are given in Tables 54-56.

[^30]| Velocity of light. | $c=2.99776 \times 10^{10} \mathrm{~cm} \mathrm{sec}^{-1}$ |
| :---: | :---: |
| Planck's constant | $h=6.6242 \times 10^{-27}$ erg_sec |
| Boltzmann's constant. | $k=1.3805 \times 10^{-18} \mathrm{erg} \mathrm{deg}^{-1}$ |
| Stefan-Boltzmann constant* | $\sigma=5.673 \times 10^{-5} \mathrm{erg} \mathrm{cm}^{-2} \mathrm{deg}^{-4} \mathrm{sec}^{-1}$ |
| Wien's displacement law... | $J_{\lambda}=A c_{1} \lambda^{-5} F(\lambda T)$ |
| The principal corollaries are: | $\lambda_{m} T=b$ |
|  | $\frac{J_{m}}{A T^{8}}=b_{1}$ |

The first corollary is sometimes given as the Wien's displacement law, and $b$ as the displacement constant.
Wien displacement constant........................ $b=0.2897 \mathrm{~cm}$ deg
First radiation constant $\dagger$

$$
\begin{aligned}
\text { All lengths in } \mathrm{cm}, d \lambda=1 \mathrm{~cm} \ldots \ldots \ldots \ldots \ldots & c_{1}=3.740 \times 10^{-5} \mathrm{erg} \mathrm{sec}^{-1} \mathrm{~cm}^{2} \\
\text { Area } \mathrm{cm}^{2}, \lambda \text { in } \mu, d \lambda=0.01 \mu \ldots \ldots \ldots \ldots & c_{1}=3.740 \times 10^{9} \mathrm{erg} \mathrm{sec}^{-1} \mathrm{~cm}^{2} \\
\text { Second radiation constant.................................... } & c_{2}=1.4380 \mathrm{~cm} \mathrm{deg}
\end{aligned}
$$

The unit of energy chosen for the above values is the erg. Any other unit of energy (or power) may be used if the proper conversion factor is used (Table 7).

Values of $c_{2}$ used at different times.-This second radiation constant has been determined many times in the last 40 years. Shown below are the values used at different times. [A new determination of the value of $c_{2}$ by G. A. W. Rutgers (Physica, vol. 15, p. 985,1949 ) gives two values: $14325 . \pm 20$ and $14310 . \pm 20 \mu$ deg.]

| Date | National Bureau of Standards | Nela <br> Park |
| :---: | :---: | :---: |
| 1911 | $14500 \mu^{\circ} \mathrm{K}$ | $14500 \mu^{\circ} \mathrm{K}$ |
| 1915. | - | 14460 |
| 1917. | . 14350 | 14350 |
| 1922. | $14320 \ddagger$ | 14350 |
| 1925. | . 143208 | 14320 |
| 1936. | . 14320 \|| | 14320 |
| 1944. | . 14320 | 14320 |
| 1949. | . 14380 | - |

*For $2 \pi$ solid angle. $\dagger$ For the general case, $c_{1}$ may be written in the following symbolic form:

$$
c_{1}=\text { numeric } \frac{\left(\text { wavelength unit) }{ }^{5} \times\right. \text { power unit }}{\text { area } \times \text { wavelength interval } \times \text { solid angle }}
$$

This form shows that the value of the numeric depends upon the several units used-in this case 5 . If $J_{\lambda_{0}}$ is the normal intensity, i.e., per unit solid angle perpendicular to the surface, $\pi J_{\lambda_{0}}$ gives the radiation per $2 \pi$ solid angle. The energy radiated within a unit solid angle around the normal, is $0.92 J_{0}$. The above values are for a plane blackbody; for a spherical blackbody the radiation for $2 \pi$ solid angle equals $2 \pi J_{0}$.

For calculations the use of the radiation constants $\sigma$ and $c_{2}$ as given follows directly and causes but little trouble. The numeric for $c_{2}$ must be expressed in the unit of wavelength times the absolute temperature. If the wavelength is expressed in $\mu$ the numeric becomes 14380 .

When Planck's equation is used for calculations, it may be written as follows for blackbody of area A:

$$
J_{\lambda} d \lambda=\left(A c_{1} \lambda-5 /\left[\exp \left(c_{2} / \lambda T\right)-1\right]\right) d \lambda
$$

where $d \lambda$ is the wavelength interval for which the radiation is to be calculated. The first value of $c_{1}$ given in the table is for all dimensions in centimeters-a condition almost never met in practice. The second value is for the wavelength expressed in microns and $d \lambda=0.01 \mu$.

If this second value of $c_{2}$ be used in calculation with Planck's equation and summed step by step, the results will be the total energy per second, per $2 \pi$ solid angle, per unit area for the wavelength interval covered, $\lambda$ expressed in $\mu$.
$\ddagger$ I. G. Priest, in January 1922, used $c_{2}=14350$ in his work on color temperature. $\$$ J. F. Skogland in 1929, used $c_{2}=14330$ in his tables of spectral energy distrihution of a blacklody.
D. B. Judd, in 1933, used $c_{2}=14350$ in his calculations related to the I.C.I. standard observer.
TABLE 54.-RADIATION IN ERGS ( $\mathrm{W} \times 10^{n}$ ) AND GRAM-CALORIES ( $\mathrm{W}^{\prime} \times 10^{n \prime}$ ) PER CM ${ }^{2}$ PER SEC, FOR $2 \pi$ SOLID ANGLE,

| $\begin{gathered} \text { Temp. } \\ { }^{\circ} \mathrm{C} \end{gathered}$ | $\mathrm{erg} \mathrm{cm}{ }^{-2} \mathrm{sec}^{-1}$ |  | cal cm-2 ${ }^{\text {sec }}{ }^{-1}$ |  | $\sigma=5.672 \times 10^{-5} \mathrm{erg} \mathrm{cm}^{-2} \mathrm{deg}^{-4} \mathrm{sec}^{-1}$ |  |  |  |  |  |  |  | $\overbrace{}^{\text {cal } \mathrm{cm}^{-2} \mathrm{sec}^{-1}}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\underset{{ }^{\circ} \mathrm{C}}{\text { Temp. }}$ | $\mathrm{erg} \mathrm{cm}^{-2} \mathrm{sec}^{-1}$ |  | $\overbrace{}^{\text {cal cm}}{ }^{-2} \mathrm{sec}^{-1}$ |  | $\underset{{ }^{\circ} \mathrm{K}}{\text { Temp. }}$ | erg cm-2 ${ }^{\text {sec }}{ }^{-1}$ |  |  |  |
|  |  |  |  |  |  | $\overbrace{\mathrm{W}}$ | $n$ |  | ${ }^{\text {W }}{ }^{\prime}$ |  | $\overparen{W}$ | $n$ | W' | $\overline{n^{\prime}}$ |
| -270 | 5.656 | -3 | 1.351 | $-10$ | 4 | 3.347 | 5 | 7.998 | -3 | 309 * | 4.5944 | 5 | 1.0978 | -2 |
| -250 | 1.632 | 1 | 3.899 | $-7$ | 6 | 3.445 | 5 | 8.231 | $-3$ | 373.16 | 1.0998 | 6 | 2.6280 | -2 |
| -200 | 1.625 | 3 | 3.883 | $-5$ | 8 | 3.545 | 5 | 8.470 | $-3$ | 400 | 1.4520 | 6 | 3.4700 | -2 |
| -190 | 2.713 | 3 | 6.482 | $-5$ | 10 | 3.646 | 5 | 8.713 | -3 | 500 | 3.5450 | 6 | 8.4707 | -2 |
| $-180$ | 4.272 | 3 | 1.021 | $-4$ | 12 | 3.751 | 5 | 8.962 | -3 | 600 | 7.3509 | 6 | 1.7565 | -1 |
| -160 | 9.301 | 3 | 2.222 | $-4$ | 14 | 3.857 | 5 | 9.216 | $-3$ | 700 | 1.3619 | 7 | 3.2542 | -1 |
| $-150$ | 1.305 | 4 | 3.118 | $-4$ | 16 | 3.965 | 5 | 9.475 | $-3$ | 800 | 2.3233 | 7 | 5.5515 | $-1$ |
| $-140$ | 1.783 | 4 | 4.261 | $-4$ | 18 | 4.076 | 5 | 9.740 | -3 | 900 | 3.7214 | 7 | 8.8922 | -1 |
| $-130$ | 2.382 | 4 | 5.693 | $-4$ | 20 | 4.189 | 5 | 1.001 | -2 | 1000 | 5.6720 | 7 | 1.3553 | 0 |
| -120 | 3.121 | 4 | 7.458 | $-4$ | 22 | 4.305 | 5 | 1.029 | -2 | 1500 | 2.8715 | 8 | 6.8614 | 0 |
| $-110$ | 4.020 | 4 | 9.605 | $-4$ | 24 | 4.423 | 5 | 1.057 | -2 | 2000 | 9.0752 | 8 | 2.1685 | 1 |
| $-100$ | 5.100 | 4 | 1.219 | $-3$ | 26 | 4.543 | 5 | 1.086 | $-2$ | 2500 | 2.2156 | 9 | 5.2942 | 1 |
| -90 | 6.383 | 4 | 1.525 | $-3$ | 28 | 4.666 | 5 | 1.115 | $-2$ | 3500 | 8.5115 | 9 | 2.0338 | 2 |
| -80 | 7.896 | 4 | 1.887 | $-3$ | 30 | 4.791 | 5 | 1.145 | -2 | 4500 | 2.3259 | 10 | 5.5577 | 2 |
| -70 | 9.662 | 4 | 2.309 | $-3$ | 32 | 4.919 | 5 | 1.175 | -2 | 5500 | 5.1902 | 10 | 1.2402 | 3 |
| - 60 | 1.171 | 5 | 2.798 | -3 | 34 | 5.049 | 5 | 1.206 | -2 |  |  |  |  |  |
| - 50 | 1.407 | 5 | 3.361 | -3 | 36 | 5.182 | 5 | 1.238 | -2 |  |  |  |  |  |
| - 40 | 1.676 | 5 | 4.006 | -3 | 38 | 5.317 | 5 | 1.271 | -2 |  |  |  |  |  |
| - 30 | 1.983 | 5 | 4.738 | $-3$ | 40 | 5.455 | 5 | 1.304 | -2 |  |  |  |  |  |
| - 20 | 2.330 | 5 | 5.567 | $-3$ | 42 | 5.596 | 5 | 1.337 | -2 |  |  |  |  |  |
| $-10$ | 2.720 | 5 | 6.500 | $-3$ | 44 | 5.739 | 5 | 1.371 | -2 |  |  |  |  |  |
| $-8$ | 2.804 | 5 | 6.700 | $-3$ | 46 | 5.885 | 5 | 1.406 | -2 |  |  |  |  |  |
| - 6 | 2.890 | 5 | 6.904 | -3 | 48 | 6.034 | 5 | 1.442 | -2 |  |  |  |  |  |
| - 4 | 2.977 | 5 | 7.114 | -3 | 50 | 6.186 | 5 | 1.478 | -2 |  |  |  |  |  |
| - 2 | 3.067 | 5 | 7.327 | $-3$ | 52 | 6.341 | 5 | 1.515 | -2 |  |  |  |  |  |
| 0 | 3.158 | 5 | 7.546 | $-3$ | 54 | 6.498 | 5 | 1.553 | -2 |  |  |  |  |  |
| 2 | 3.252 | 5 | 7.769 | - 3 | 56 | 6.658 | 5 | 1.591 | -2 |  |  |  |  |  |

[^31]
## TABLE 55.-CALCULATED SPECTRAL INTENSITIES $J_{\lambda}$ FOR A RANGE OF WAVELENGTHS FOR A BLACKBODY OF UNIT AREA FOR A RANGE OF TEMPERATURES FROM $50^{\circ} \mathrm{K}$ TO $25,000^{\circ} \mathrm{K}$ *

These values have been calculated for $c_{1}=\frac{3740 \text { micron }^{5} \text { watts }}{\mathrm{cm}^{2} d \lambda 2 \pi \text { solid angles }} ; c_{2}=14380 \mu: \mathrm{deg} ; d \lambda=$ $0.1 \mu, J_{\lambda}=$ tabular $J_{\lambda} \times 10^{n}$ watts for $\mathrm{cm}^{2}$ for $2 \pi$ solid angle per $0.1 \mu$.

|  | $50^{\circ}$ |  | $75^{\circ}$ |  | $100^{\circ}$ |  | $150^{\circ}$ |  | $200^{\circ}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\lambda$ | $J_{\lambda}$ | $n$ | $J_{\lambda}$ | $n$ | $J_{\lambda}$ | $n$ | $J_{\lambda}$ | $n$ | $J_{\lambda}$ |  |
| 1.0 | 4.675 | -122 | 2.0145 | -80 | 1.3224 | -59 | 8.679 | -39 | 2.2235 | -28 |
| 1.5 | 2.6529 | -81 | 1.5131 | -53 | 1.1427 | -39 | 8.634 | -26 | 7.503 | -19 |
| 2.0 | 4.133 | - 61 | 2.7124 | --40 | 6.949 | -30 | 1.7803 | -19 | 2.8499 | -14 |
| 2.5 | 4.186 | - 49 | 1.8865 | -32 | 4.005 | -24 | 8.501 | -16 | 1.2384 | -11 |
| 3.0 | 3.5716 | - 41 | 2.6982 | -27 | 2.344 | -20 | 2.0377 | -13 | 6.007 | -10 |
| 3.5 | 1.4652 | - 35 | 1.1519 | -23 | 1.0214 | -17 | 9.057 | -12 | 8.529 | -9 |
| 4.0 | 2.1714 | - 31 | 5.564 | -21 | 8.906 | -16 | 1.4255 | -10 | 5.703 | -8 |
| 5.0 | 1.2515 | - 25 | 2.6566 | -17 | 3.8701 | -13 | 5.638 | -9 | 6.806 | -7 |
| 6.0 | 7.326 | - 22 | 6.367 | -15 | 1.8773 | -11 | 5.534 | -8 | 3.0050 | - 6 |
| 7.0 | 3.1917 | - 19 | 2.8304 | -13 | 2.6652 | -10 | 2.5096 | -7 | 7.701 | - 6 |
| 8.0 | 2.7831 | $-17$ | 4.455 | -12 | 1.7823 | -9 | 7.131 | -7 | 1.4265 |  |
| 9.0 | 8.386 | - 16 | 3.5449 | -11 | 7.288 | -9 | 1.4984 | -6 | 2.1492 |  |
| 10.0 | 1.2094 | - 14 | 1.7620 | -10 | 2.1269 | -8 | 2.5671 | - 6 | 2.8224 |  |
| 12.0 | 5.867 | - 13 | 1.7294 | -9 | 9.391 | -8 | 5.100 | - 6 | 3.7662 | - |
| 14.0 | 8.3288 | - 12 | 7.843 | -9 | 2.4062 | -7 | 7.393 |  | 4.115 | - |
| 16.0 | 5.570 | - 11 | 2.2284 | -8 | 4.458 | $-7$ | 8.937 | -6 | 4.032 | - |
| 18.0 | 2.2775 | - 10 | 4.682 | -8 | 6.716 | -7 | 9.674 | - 6 | 3.7137 | - |
| 20.0 | 6.647 |  | 8.022 | -8 | 8.820 | - 7 | 9.763 | - 6 | 3.3001 |  |
| 25.0 | 3.8640 | - 9 | 1.7882 | - 7 | 1.2204 | -6 | 8.458 | -6 | 2.2874 | - |
| 30.0 | 1.0564 | 8 | 2.5801 | -7 | 1.2857 | - 6 | 6.571 | -6 | 1.5411 | - |
| 40.0 | 2.7563 | 8 | 3.0513 | $-7$ | 1.0313 | -6 | 3.6674 |  | 7.255 |  |
| 50.0 | 3.8137 | 8 | 2.6437 | $-7$ | 7.148 | -7 | 2.0625 | - 6 | 3.7257 | - |
| 100.0 | 3.4809 |  | 1.3255 | -7 | 2.7160 | -7 | 6.084 | -? | 9.800 | -7 |
|  | 2.2338 | 8 | 6.445 | -7 | 1.1788 | -7 | 2.3256 | -7 | 3.5536 | -7 |
|  | $273.16^{\circ}$ |  | $300^{\circ}$ |  | $373.16^{\circ}$ |  | $500^{\circ}$ |  | $600^{\circ}$ |  |
| $\lambda$ | $J_{\lambda}$ | $n$ | $J_{\lambda}$ | $n$ | $J_{\lambda}$ | $n$ | $J_{\lambda}$ | $n$ | $J_{\lambda}$ | $n$ |
| 1.0 | 5.132 | - 20 | 5.698 | -18 | 6.870 | -14 | 1.2094 | -9 | 1.4597 | - 7 |
| 1.5 | 2.8227 | - 13 | 6.520 | -12 | 3.4290 | -9 | 2.3203 | - 6 | 5.667 | - 5 |
| 2.0 | 4.329 | - 10 | 4.562 | -9 | 5.009 | - 7 | 6.647 | - 5 | 7.302 | - |
| 2.5 | 2.7422 | - 8 | 1.8043 | -7 | 7.741 | - 6 | 3.8640 | -4 | 2.6287 | - |
| 3.0 | 3.6847 | - 7 | 1.7710 | -6 | 4.061 | -5 | 1.0564 |  | 5.223 | - |
| 3.5 | 2.0910 | - 6 | 8.031 | - 6 | 1.1772 | -4 | 1.9230 | $-3$ | 7.570 | - |
| 4.0 | 7.029 |  | 2.2819 | - 5 | 2.3911 | -. 4 | 2.7563 | -3 | 9.152 |  |
| 5.0 | 3.2026 | - 5 | 8.215 | -5 | 5.383 | -4 | 3.8137 | -3 | 9.9983 | - |
| 6.0 | 7.443 | - 5 | 1.6321 | -4 | 7.825 | - 4 | 4.018 | -3 | 9.024 | - |
| 7.0 | 1.2065 | 4 | 2.3657 | -4 | 9.085 | -4 | 3.7175 | $-3$ | 7.496 | - |
| 8.0 | 1.5856 | 4 | 2.8600 | -4 | 9.310 | -4 | 3.2227 | - 3 | 6.007 |  |
| 9.0 | 1.8307 | 4 | 3.0957 | -4 | 8.875 | -4 | 2.7040 | $-3$ | 4.748 | - |
| 10.0 | 1.9447 | - 4 | 3.1245 | -4 | 8.102 | -4 | 2.2338 | -3 | 3.7449 | - |
| 12.0 | 1.8931 | - 4 | 2.8201 | -4 | 6.312 | -4 | 1.5050 |  | 2.3601 |  |
| 14.0 | 1.6573 | - 4 | 2.3425 | -4 | 4.736 | -4 | 1.0224 | - 3 | 1.5319 | - 3 |
| 16.0 | 1.3798 | - 4 | 1.8770 | -4 | 3.5255 | -4 | 7.085 | - 4 | 1.0272 | - |
| 18.0 | 1.1229 | -- 4 | 1.4838 | -4 | 2.6366 | -4 | 5.021 | - 4 | 7.103 | - |
| 20.0 | 9.057 | - 5 | 1.1703 | -4 | 1.9919 | -4 | 3.6384 | - 4 | 5.049 | - |
| 25.0 | 5.309 | - 5 | 6.600 | -5 | 1.0432 | -4 | 1.7735 | -4 | 2.3814 | - |
| 30.0 | 3.2185 | 5 | 3.9044 | -5 | 5.890 | -5 | 9.570 |  | 1.2584 | - |
| 40.0 | 1.3385 | - 5 | 1.5780 | -5 | 2.2537 | -5 | 3.4705 | -5 | 4.451 |  |
| 50.0 | 6.414 | - 6 | 7.442 | - 6 | 1.0306 | -5 | 1.5393 | -5 | 1.9460 | - |
| 75.0 | 1.5488 | - 6 | 1.7613 | -6 | 2.3463 | - 6 | 3.3726 | - 6 | 4.189 |  |
| 100.0 | 5.398 | - 7 | 6.081 | - 7 | 7.954 | - 7 | 1.1225 |  | 1.3811 |  |

[^32]TABLE 55.-CALCULATED SPECTRAL INTENSITIES J $\mathrm{J}_{\lambda}$ FOR A RANGE OF WAVELENGTHS FOR A BLACKBODY OF UNIT AREA FOR A RANGE

OF TEMPERATURES FROM $50^{\circ} \mathrm{K}$ TO $25,000^{\circ} \mathrm{K}$ (continued)

| $\lambda$ | $J_{\lambda}$ | n |
| :---: | :---: | :---: |
| . 10 | 3.22+1 | - 70 |
| . 20 | 1.0851 | - 32 |
| . 30 | 1.4647 | - 20 |
| . 40 | 1.1129 | - 14 |
| . 45 | 9.103 | - 13 |
| . 50 | 2.9182 | - 11 |
| . 55 | 4.759 | - 10 |
| . 60 | 4.692 | - 9 |
| . 65 | 3.1506 | - 8 |
| . 70 | 1.5675 | - 7 |
| . 75 | 6.1514 | - 6 |
| . 80 | 1.9924 | - 6 |
| . 90 | 1.3423 | 5 |
| 1.00 | 5.840 | - 5 |
| 1.50 | 3.0769 | - 3 |
| 2.00 | 1.4607 | 2 |
| 2.50 | 2.8902 | - 2 |
| 3.00 | 3.8565 | 2 |
| 4.00 | 4.129 | 2 |
| 5.00 | 3.3793 | - 2 |
| 10.00 | 7.429 | - 3 |
| 50.00 | 2.7665 | - 5 |
| 100.00 | 1.8994 | - |

$\lambda$

| .10 | 7.543 | -27 |
| ---: | :--- | ---: |
| .20 | 5.249 | -11 |
| .30 | 4.190 | -6 |
| .40 | 7.740 | $=4$ |
| .45 | 3.9513 | -3 |
| .50 | 1.3771 | -2 |
| .55 | 3.6546 | -2 |
| .60 | 7.935 | $=2$ |
| .65 | 1.4810 | $=1$ |
| .70 | 2.4599 | -1 |
| .75 | 3.7284 | -1 |
| .80 | 5.254 | -1 |
| .90 | 8.845 | -1 |
| 1.00 | 1.2691 | 0 |
| 1.50 | 2.4072 | 0 |
| 2.00 | 2.1930 | 0 |
| 2.50 | 1.6350 | 0 |
| 3.00 | 1.1538 | 0 |
| 4.00 | 5.735 | -1 |
| 5.00 | 3.0360 | -1 |
| 10.00 | 3.0578 | -2 |
| 50.00 | 6.908 | $=5$ |
| 100.00 | 4.497 | -6 |


| $2000{ }^{\circ}$ |  |
| :---: | :---: |
| $J_{\lambda}$ | $n$ |
| 2.2235 | -23 |
| 2.8499 | -9 |
| 6.007 | -5 |
| 5.703 | -3 |
| 2.3321 | -2 |
| 6.806 | - 2 |
| 1.5618 | - 1 |
| 3.0050 | - 1 |
| 5.0622 | - 1 |
| 7.701 | - 1 |
| 1.0817 | 0 |
| 1.4265 |  |
| 2.1492 | 0 |
| 2.8224 | 0 |
| 4.115 | 0 |
| 3.3001 | 0 |
| 2.2874 | 0 |
| 1.5411 | 0 |
| 7.255 | -1 |
| 3.7257 | -1 |
| 3.5536 |  |
| 7.7413 | -5 |
| 5.020 |  |

TABLE 55.-CALCULATED SPECTRAL INTENSITIES $J_{\lambda}$ FOR A RANGE OF WAVELENGTHS FOR A BLACKBODY OF UNIT AREA FOR A RANGE OF TEMPERATURES FROM $50^{\circ} \mathrm{K}$ TO $25,000^{\circ} \mathrm{K}$ (concluded)


Auxiliary table for a short method of calculating $J_{\lambda}$ for any temperature. (Menzel, Harvard University.)
Let $J_{0}=$ intensity for $T_{0}=10,000{ }^{\circ} \mathrm{K}$; for another temperature $T^{\circ} \mathrm{K}$ :

$$
J / J_{0}=\left[\lambda_{0}{ }^{6}\left(\exp \left(c_{2} / \lambda_{0} T_{0}\right)-1\right)\right] /\left[\lambda^{5}\left(\exp \left(c_{2} / \lambda T\right)-1\right)\right]
$$

For ease of calculation $T_{0}$ was taken as $10,000{ }^{\circ} \mathrm{K} . J_{\lambda}=$ tabular $J_{\lambda} \times 10^{n}$ watts, for $\mathrm{cm}^{2}$ for $2 \pi$ solid angle per $0.1 \mu$. Choose $\lambda=\lambda_{0} T_{0} / T$; then $J_{\lambda}=J_{0}\left(T / T_{0}\right)^{5}$. As an example find $J_{\lambda}$ for $0.5 \mu$ and $6000{ }^{\circ} \mathrm{K}$ from value of $J_{\lambda}$ for $0.3 \mu$ given in Table 55. $0.5 \mu=0.3 \mu 10,000 / 6000$. $J_{\lambda}$ for $0.3 \mu=1.2857 \times 10^{4}$. $J_{\lambda}$ for $\lambda=0.5 \mu=1.2857 \times 10^{4} \times(6,000 / 10,000)^{6}=9.998 \times 10^{2}$.

| $\underbrace{10,000^{\circ}}$ |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\lambda$ | $J_{2}$ | $n$ | $\lambda$ | $J_{\text {, }}$ | n | $\lambda$ | $J_{1}$ | n | $\lambda$ | $J_{2}$ | $n$ |
| . 0100 | 1.3224 | -49 | . 1450 | 2.8776 | 3 | . 5500 | 5.869 | 3 | 4.500 | 5.383 | 0 |
| . 0150 | 1.1427 | -29 | . 1500 | 3.3806 | 3 | . 6000 | 4.816 | 3 | 5.000 | 3.5918 | 0 |
| . 0200 | 6.949 | -20 | . 1600 | 4.458 | 3 | . 6500 | 3.9614 | 3 | 6.000 | 1.7761 | 0 |
| . 0250 | 4.005 | -14 | . 1700 | 5.586 | 3 | . 7000 | 3.2718 | 3 | 7.000 | 9.756 | 1 |
| . 0300 | 2.3444 | -10 | . 1800 | 6.716 | 3 | . 7500 | 2.7160 | 3 | 8.000 | 5.797 | 1 |
| . 0350 | 1.0214 | $-7$ | . 1900 | 7.805 | 3 | . 8000 | 2.2670 | 3 | 9.000 | 3.6548 | -1 |
| . 0400 | 8.906 | - 6 | . 2000 | 8.820 | 3 | . 8500 | 1.9031 | 3 | 10.00 | 2.4184 | 1 |
| . 0450 | 2.6833 | -4 | . 2100 | 9.735 | 3 | . 9000 | 1.6067 | 3 | 12.00 | 1.1807 | -1 |
| . 0500 | 3.8700 | - 3 | . 2200 | 1.0536 | 4 | . 9500 | 1.3641 | 3 | 14.00 | 6.433 | 2 |
| . 0550 | 3.2828 | -2 | . 2300 | 1.1215 | 4 | 1.000 | 1.1643 | 3 | 16.00 | 3.7904 | -2 |
| . 0600 | 1.8773 | -1 | . 2400 | 1.1769 | 4 | 1.100 | 8.613 | 2 | 18.00 | 2.3790 | -2 |
| . 0650 | 7.950 | -1 | . 2500 | 1.2204 | 4 | 1.200 | 6.494 | 2 | 20.00 | 1.5667 | -2 |
| . 0700 | 2.6652 | 0 | . 2600 | 1.2524 | 4 | 1.300 | 4.980 | 2 | 25.00 | 6.4692 | -3 |
| . 0750 | 7.427 | 0 | . 2700 | 1.2739 | 4 | 1.400 | 3.8782 | 2 | 30.00 | 3.1346 | -3 |
| . 0800 | 1.7823 | 1 | . 2800 | 1.2859 | 4 | 1.500 | 3.0625 | 2 | 35.00 | 1.6954 | -3 |
| . 0850 | 3.7891 | 1 | . 2900 | 1.2895 | 4 | 1.600 | 2.4487 | 2 | 40.00 | 9.979 | -4 |
| . 0900 | 7.288 | 1 | . 3000 | 1.2857 | 4 | 1.700 | 1.9805 | 2 | 45.00 | 6.236 | -4 |
| . 0950 | 1.2894 | 2 | . 3200 | 1.2601 | 4 | 1.800 | 1.6183 | 2 | 50.00 | 4.099 | -4 |
| . 1000 | 2.1269 | 2 | . 3400 | 1.2163 | 4 | 1.900 | 1.3348 | 2 | 55.00 | 2.8042 | -4 |
| . 1050 | 3.3049 | 2 | . 3600 | 1.1606 | 4 | 2.000 | 1.1106 | 2 | 60.00 | 1.9793 | -4 |
| . 1100 | 4.881 | 2 | . 3800 | 1.0977 | 4 | 2.200 | 7.867 | 1 | 65.00 | 1.4390 | -4 |
| . 1150 | 6.899 | 2 | . 4000 | 1.0313 | 4 | 2.400 | 5.724 | 1 | 70.00 | 1.0698 | -4 |
| . 1200 | 9.391 | 2 | . 4200 | 9.640 | 3 | 2.600 | 4.262 | 1 | 80.00 | 6.306 | -5 |
| . 1250 | 1.2365 | 3 | . 4400 | 8.977 | 3 | 2.800 | 3.2372 | 1 | 90.00 | 3.9340 | -5 |
| . 1300 | 1.5819 | 3 | . 4600 | 8.335 | 3 | 3.000 | 2.5026 | 1 | 100.00 | 2.5793 | -5 |
| . 1350 | 1.9732 | 3 | . 4800 | 7.724 | 3 | 3.500 | 1.4015 | 1 |  |  |  |
| . 1400 | 2.4062 | 3 | . 5000 | 7.148 | 3 | 4.000 | 8.443 | 0 |  |  |  |

The adoption of a new value for $c_{2}$ changes the calculated values for $J_{\lambda}$ by an amount that varies indirectly with both the wavelength and the temperature for values of $\lambda T$ $<3000$, as follows:

$$
\frac{d J_{\lambda}}{J_{\lambda}}=\frac{-d c_{2}}{\lambda T}
$$

that is, a larger value of $c_{2}$ results in a smaller value of $J_{\lambda}$. Values of this correction factor for this change in $c_{2}$ have been calculated and are given in the tables for five temperatures and a range of wavelengths that cover the visible spectrum. As these percentage correction factors are given they are the percentage of the $J_{\lambda}$ for $14320 \mu$ deg that must be subtracted from it to give $J_{19330}$.

A change in $c_{2}$ also results in a different value of the extrapolated temperature as measured with an optical pyrometer for a definite ratio of brightness. Thus

$$
\left(\frac{1}{T_{0}}-\frac{1}{T_{1}}\right)=\frac{c_{2}^{1}}{c_{2}}\left(\frac{1}{T_{0}}-\frac{1}{T_{0}^{1}}\right)
$$

To the accuracy necessary for most work, values for other wavelengths, other temperatures, or other values of $c_{2}$ within these ranges can be found by interpolation.

Part 1.-Percentage change in $J_{\lambda}$ for a change in $c_{2}$ from 14320 to $14380 \mu$ degrees

| $\lambda$ in $\mu$ | ${ }^{2000}$ | ${ }^{2300}{ }^{\text {¢ }}$ K | ${ }^{2600}{ }_{0}{ }^{\text {K }}$ | ${ }^{2900} \mathrm{~K}$ | $\stackrel{3200}{ }{ }^{\mathrm{K}}$ | $\lambda$ in $\mu$ | ${ }^{2000}$ | ${ }^{23000}$ | ${ }^{2600} \mathrm{~K}$ | $\stackrel{2900}{ }{ }^{\mathrm{K}}$ | ${ }^{3200}{ }^{\circ} \mathrm{K}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 32 | 9.8 | 8.5 | 7.5 | 6.7 | 6.0 | . 58 | 5.3 | 4.6 | 4.1 | 3.6 | 3.3 |
| . 34 | 9.2 | 7.9 | 7.0 | 6.3 | 5.7 | . 60 | 5.1 | 4.4 | 3.9 | 3.5 | 3.2 |
| . 36 | 8.7 | 7.5 | 6.6 | 5.9 | 5.3 | . 62 | 4.9 | 4.3 | 3.8 | 3.4 | 3.1 |
| . 38 | 8.2 | 7.1 | 6.3 | 5.6 | 5.0 | . 64 | 4.8 | 4.1 | 3.7 | 3.3 | 3.0 |
| . 40 | 7.8 | 6.7 | 5.9 | 5.3 | 4.8 | . 66 | 4.6 | 4.0 | 3.6 | 3.2 | 2.9 |
| . 42 | 7.4 | 6.4 | 5.7 | 5.0 | 4.6 | . 68 | 4.5 | 3.9 | 3.5 | 3.1 | 2.8 |
| . 44 | 7.0 | 6.1 | 5.4 | 4.8 | 4.4 | . 70 | 4.4 | 3.8 | 3.4 | 3.0 | 2.7 |
| . 46 | 6.7 | 5.8 | 5.1 | 4.6 | 4.2 | . 72 | 4.2 | 3.7 | 3.3 | 2.9 | 2.6 |
| . 48 | 6.4 | 5.6 | 4.9 | 4.4 | 4.0 | . 74 | 4.1 | 3.6 | 3.2 | 2.8 | 2.6 |
| . 50 | 6.2 | 5.3 | 4.7 | 4.2 | 3.8 | . 76 | 4.0 | 3.5 | 3.1 | 2.8 | 2.5 |
| . 52 | 5.9 | 5.1 | 4.5 | 4.1 | 3.7 | . 78 | 3.9 | 3.4 | 3.0 | 2.7 | 2.4 |
| . 54 | 5.7 | 4.9 | 4.4 | 3.9 | 3.5 | . 80 | 3.8 | 3.3 | 2.9 | 2.6 | 2.3 |
| . 56 | 5.5 | 4.8 | 4.2 | 3.8 | 3.4 |  |  |  |  |  |  |

Part 2.-Change in temperatures, $\Delta T$, extrapolated from 1336 to the temperature $T$ given, $c_{2}$ changed from 14320 to $14380_{\mu}$ degrees

| $T^{\circ} \mathrm{K}$ | $1500^{\circ} \mathrm{K}$ | $1800^{\circ} \mathrm{K}$ | $2000^{\circ} \mathrm{K}$ | $2500^{\circ} \mathrm{K}$ | $3000^{\circ} \mathrm{K}$ | $3500^{\circ} \mathrm{K}$ | $4000^{\circ} \mathrm{K}$ | $5000^{\circ} \mathrm{K}$ |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\Delta T$ | -.6 | -2.4 | -4.1 | -8.7 | -15.5 | -22.3 | -33.0 | -56.4 |

Photometry is the measurement of light, and light has been defined by the Illuminating Engineering Society as radiant energy evaluated according to its capacity to produce visual sensations.

# TABLE 58.-THE EYE AS A MEASURING INSTRUMENT FOR RADIATION 

Part 1.—Theory


#### Abstract

As a measuring instrument for radiation, the eye is very selective, that is, it does not


 respond equally to radiation of various wavelengths. The data in Part 2 give the relative sensitivity of the eye to radiation of different wavelengths. Another peculiarity of the eye is that its relative sensitivity changes with the intensity of the radiation that falls upon it. This is shown by the data in Table 59. Also the absolute sensitivity of the eye varies with the intensity of the radiation that falls upon it. This is shown by the data given in Table 60 .The data ${ }^{20}$ on which Table 60 is based are not very extensive, but inasmuch as there is now some active work on this subject by Lowry of the Eastman Kodak Co. there should soon be available data for a wider range of field brightness. The data in Table 59 show that the sensitivity of the eye to radiation of lower intensity increases faster toward the blue end of the spectrum than in the red end. This is called the Purkinje effect.

For light measurement at very low brightness care must be taken as to the standards used. From the data given in Table 59 it can be shown that sources giving light of different colors that were rated as equal by the average eye adapted to a field brightness of about 1 to 2 millilamberts would be rated quite differently for low field brightness, that is, for the eye adapted to a field brightness of $10^{-5}$ millilamberts.

If the brightness given by two sources such as daylight and a carbon lamp be set equal for a field brightness 1 to 2 millilamberts and then these brightnesses both reduced mechanically to about $10^{-5}$ millilamberts, the field of the daylight source would seem to be about $2 \frac{1}{2}$ times as bright as that of the carbon lamp.

[^33]Part 2.-Relative luminosity factors ${ }^{2 n}\left[K_{\lambda}\right]$ (unity at wavelength of maximum luminosity)

| $\lambda$ in | Standard | Values interpolated at intervals of one millimicron |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| m $\mu$ | factors | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 380 | . 00004 | .000045 | . 000049 | . 000054 | . 000059 | .000064 | . 000071 | . 000080 | . 000090 | . 000104 |
| 390 | . 00012 | . 000138 | . 000155 | . 000173 | . 000193 | . 000215 | . 000241 | . 000272 | . 000308 | . 000350 |
| $+00$ | . 0004 | . 00045 | . 00049 | . 00054 | . 00059 | . 00064 | . 000071 | . 00080 | . 00090 | . 00104 |
| 410 | . 0012 | . 00138 | . 00156 | . 00174 | . 00195 | . 00218 | . 00244 | . 00274 | . 00310 | . 00352 |
| 420 | . 0040 | . 00455 | . 00515 | . 00581 | . 00651 | . 00726 | . 00806 | . 00889 | . 00976 | . 01066 |
| 430 | . 0116 | . 01257 | . 01358 | . 01463 | . 01571 | . 01684 | . 01800 | . 01920 | . 02043 | . 02170 |
| 440 | . 023 | . 0243 | . 0257 | . 0370 | . 0284 | . 0298 | . 0313 | . 0329 | . 0345 | . 0362 |
| 450 | . 038 | . 0399 | . 0418 | . 0438 | . 0459 | . 0480 | . 0502 | . 0525 | . 0549 | . 0574 |
| 460 | . 060 | . 0627 | . 0654 | . 0681 | . 0709 | . 0739 | . 0769 | . 0802 | . 0836 | . 0872 |
| 470 | . 091 | . 0950 | .0993 | . 1035 | . 1080 | . 1126 | . 1175 | . 1225 | . 1278 | . 1333 |
| 480 | . 139 | . 1448 | . 1507 | . 1567 | . 1629 | . 1693 | . 1761 | . 1833 | . 1909 | . 1991 |
| 490 | . 208 | . 2173 | . 2270 | . 2371 | . 2476 | . 2586 | . 2701 | . 2823 | . 2951 | . 3087 |
| 500 | . 323 | . 3382 | . 3544 | . 3714 | . 3890 | . 4073 | . 4259 | . 4450 | . 4642 | . 4836 |
| 510 | . 503 | . 5229 | . 5436 | . 5648 | . 5865 | . 6082 | . 6299 | . 6511 | . 6717 | . 6914 |
| 520 | . 710 | . 7277 | . 7449 | . 7615 | . 7776 | .7932 | . 8083 | . 8225 | . 8363 | . 8495 |
| 530 | . 862 | . 8739 | . 8851 | . 8956 | . 9056 | . 9149 | . 9238 | . 9320 | . 9398 | . 9471 |
| 540 | . 954 | . 9604 | . 9661 | . 9713 | . 9760 | . 9803 | . 9840 | . 9873 | . 9902 | . 9928 |
| 550 | . 995 | . 9969 | . 9983 | . 9994 | 1.0000 | 1.0002 | 1.0001 | . 9995 | . 9984 | . 9969 |
| 560 | . 995 | . 9926 | . 9898 | . 9865 | . 9828 | . 9786 | . 9741 | . 9691 | . 9638 | . 9581 |
| 570 | . 953 | . 9455 | . 9386 | . 9312 | . 9235 | . 9154 | . 9069 | . 8981 | . 8890 | . 8796 |
| 580 | . 870 | . 8600 | . 8496 | . 8388 | . 8277 | . 8163 | . 8046 | . 7928 | . 7809 | . 7690 |
| 590 | . 757 | . 7449 | . 7327 | . 7302 | . 7076 | . 6949 | . 6822 | . 6694 | . 6565 | . 6437 |
| 600 | . 631 | .6183 | . 6054 | . 5926 | . 5797 | . 5668 | . 5539 | . 5410 | . 528 ? | . 5156 |
| 610 | . 503 | . +905 | . 4781 | . 4658 | . 4535 | . 4412 | . 4291 | . 4170 | . 4049 | . 3929 |
| 630 | . 381 | . 3690 | . 3570 | . 3449 | . 3329 | . 3210 | . 3092 | . 2977 | . 2864 | . 2755 |
| 630 | . 265 | . 2548 | . 2450 | . 2354 | . 2261 | . 2170 | . 2082 | . 1996 | . 1912 | . 1830 |
| 640 | . 175 | .1673 | . 1596 | . 1523 | . 1453 | . 13816 | .1316 | . 1251 | . 1188 | . 1128 |
| 650 | . 107 | . 1014 | . 0961 | . 0910 | . 0862 | . 0816 | . 0771 | . 0729 | . 0688 | . 0648 |
| 660 | . 061 | . 0574 | . 0539 | . 0506 | . $0+775$ | . 0446 | . $0+18$ | . 0391 | . 0366 | . 0343 |
| 670 | . 032 | . 0299 | . 0288 | . 0263 | . 0247 | .0232 | . 0219 | . 0206 | . 0194 | . 0182 |
| 680 | . 017 | . 01585 | .01477 | . 01376 | . 01281 | . 01192 | . 01108 | . 01030 | . 00956 | . 00886 |
| 690 700 | .0082 | .00759 .00381 | . 00705 | . 00656 | . 00612 | . 00572 | . 00536 | . 00503 | . 00471 | . 00440 |
| 700 710 | .0041 | . 000381 | . 00355 | .00332 | . 00310 | .00291 | .00273 | . 00256 | .00241 | . 00225 |
| 720 | . 00105 | . 000975 | . 000907 | . 000845 | . 0000788 | . 0000736 | . 001.387 | .001297 $.00064 t$ | . 0001212 | . 0001130 |
| 730 | . 00053 | . 000482 | . 000447 | . $000+15$ | . 0000387 | . 000360 | . 0000888 | . $0006+1$ | . 0000601 | .000560 .000270 |
| 740 | .00025 | . 000231 | . 000214 | . 000198 | . 000185 | .000172 | . 000160 | . 000149 | . 000139 | . 000130 |
| 750 | .00012 | . 000111 | . 000103 | . 000096 | . 000090 | . 000084 | . 000078 | . 000074 | . 000069 | . 000064 |
| 760 | . 00006 | . 000056 | . 000052 | . 000048 | . 000045 | . 000042 | . 000039 | . 000037 | .000035 | . 000032 |

[^34](Logarithms of field brightness in first line)

| Wavelength $\mathrm{m} \mu$ | ICI | -0.5 | -1.0 | -1.5 | -2.0 | -2.5 | -3.0 | -3.5 | -4.0 | -4.187* | -4.50 | -5.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 350 |  |  |  |  |  |  |  |  | . 0002 | . 000265 | . 0003 | . 0003 |
| 360 |  |  |  |  |  |  | . 0003 | . 0004 | . 0007 | . 00073 | . 0008 | . 0008 |
| 370 |  |  |  |  | . 0002 | . 0005 | . 0009 | . 0013 | . 0018 | . 0019 | . 0020 | . 0022 |
| 380 | .00004 | . 00000 | . 0001 | . 0002 | . 0008 | . 0015 | . 0025 | . 0034 | . 0045 | . 0048 | . 0051 | . 0055 |
| 390 | . 00012 | . 0001 | . 0002 | . 0008 | . 0022 | . 0040 | . 0063 | . 0083 | . 0104 | . 0112 | . 0119 | . 0127 |
| 400 | . 0004 | . 0004 | . 0008 | . 0022 | . 0059 | . 0098 | . 0147 | . 0185 | . 0228 | . 0243 | . 0253 | . 0270 |
| 410 | . 0012 | . 0014 | . 0023 | . 0062 | . 0140 | . 0227 | . 0305 | . 0370 | . 0452 | . 0485 | . 0500 | . 0530 |
| 420 | . 0040 | . 0044 | . 0069 | . 0152 | . 0280 | . 0427 | . 0580 | . 0690 | . 0820 | . 087 | . 0900 | . 0950 |
| 430 | . 0116 | . 0121 | . 0165 | . 0292 | . 0505 | . 0755 | . 101 | . 118 | . 138 | . 145 | . 149 | . 157 |
| 440 | . 023 | . 0240 | . 0300 | . 0496 | . 0850 | . 123 | . 160 | . 183 | . 216 | . 225 | . 230 | . 239 |
| 450 | . 038 | . 0395 | . 0490 | . 0810 | . 136 | . 187 | . 237 | . 268 | . 310 | . 321 | . 326 | . 339 |
| 460 | . 060 | . 0627 | . 0775 | . 127 | . 202 | . 277 | . 339 | . 376 | . 423 | . 434 | . 441 | . 455 |
| 470 | . 091 | . 0960 | . 118 | . 191 | . 301 | . 394 | . 467 | . 510 | . 551 | . 560 | . 568 | . 576 |
| 480 | . 139 | . 146 | . 180 | . 288 | . 432 | . 540 | . 604 | . 649 | . 685 | . 695 | . 702 | . 714 |
| 490 | . 208 | . 220 | . 274 | . 426 | . 592 | . 688 | . 734 | . 782 | . 814 | . 827 | . 830 | . 842 |
| 500 | . 323 | . 340 | . 416 | . 603 | . 744 | . 826 | . 864 | . 902 | . 930 | . 932 | . 941 | . 948 |
| 510 | . 503 | . 524 | . 617 | . 766 | . 876 | . 935 | . 962 | . 977 | . 992 | . 997 | . 997 | . 999 |
| 520 | . 710 | . 726 | . 792 | . 894 | . 965 | . 992 | . 999 | . 988 | . 974 | . 963 | . 960 | . 953 |
| 530 | . 862 | . 872 | . 910 | . 972 | 1.000 | . 982 | . 951 | . 924 | . 883 | . 871 | . 862 | . 848 |
| 540 | . 954 | . 959 | . 979 | 1.000 | . 969 | . 909 | . 842 | . 796 | . 744 | . 734 | . 715 | . 697 |
| 550 | . 995 | . 997 | 1.000 | . 971 | . 886 | . 785 | . 698 | . 642 | . 583 | . 555 | . 552 | . 531 |
| 560 | . 995 | . 992 | . 973 | . 898 | . 760 | . 640 | . 543 | . 478 | . 419 | . 390 | . 388 | . 365 |
| 570 | . 952 | . 944 | . 907 | . 782 | . 617 | . 485 | . 384 | . 330 | . 281 | . 263 | . 260 | . 243 |
| 580 | . 870 | . 860 | . 802 | . 648 | . 468 | . 340 | . 259 | . 218 | . 182 | . 167 | . 164 | . 155 |
| 590 | . 757 | . 742 | . 673 | . 509 | . 333 | . 227 | . 166 | . 137 | . 112 | . 102 | . 101 | . 0945 |
| 600 | . 631 | . 616 | . 544 | . 374 | . 224 | . 145 | . 101 | . 0830 | . 0670 | . 0613 | . 060 | . 0560 |
| 610 | . 503 | . 490 | . 416 | . 257 | . 142 | . 0870 | . 0600 | . 0488 | . 0388 | . 0366 | . 0348 | . 0324 |
| 620 | . 381 | . 366 | . 296 | . 168 | . 0845 | . 0504 | . 0344 | . 0280 | . 0225 | . 0212 | . 0202 | . 0188 |
| 630 | . 265 | . 250 | . 197 | . 102 | . 0480 | . 0282 | . 0194 | . 0156 | . 0127 | . 0118 | . 0114 | . 0105 |
| 640 | . 175 | . 162 | . 122 | . 0590 | . 0270 | . 0146 | . 0107 | . 0085 | . 0070 | . 00653 | . 0062 | . 0058 |
| 650 | . 107 | . 0990 | . 0710 | . 0327 | . 0147 | . 0084 | . 0058 | . 0046 | . 0037 | . 00353 | . 0034 | . 0032 |
| 660 | . 061 | . 0560 | . 0390 | . 0174 | . 0078 | . 0045 | . 0031 | . 0025 | . 0020 | . 00189 | . 0018 | . 0017 |
| 670 | . 032 | . 0303 | . 0206 | . 0090 | . 0041 | . 0024 | . 0017 | . 0013 | . 0011 | . 00098 | . 0010 | . 0009 |
| 680 | . 017 | . 0153 | . 0103 | . 0046 | . 0022 | . 0014 | . 0009 | . 0007 | . 0006 | . 00050 | . 0005 | . 0005 |
| 690 | . 0082 | . 0076 | . 0052 | . 0024 | . 0011 | . 0007 | . 0004 | . 0003 | . 0003 | . 00025 | . 0002 | . 0002 |
| 700 | . 0041 | . 0038 | . 0026 | . 0012 | . 0006 | . 0003 | . 0002 | . 0002 | . 00016 | . 00013 | . 0001 | . 0001 |
| 710 | . 0021 | . 0019 | . 0014 | . 0006 | . 0003 | . 0002 | . 0001 |  |  |  |  |  |
| 720 | . 00105 | . 0010 | . 0007 | . 0003 | . 0001 |  |  |  |  |  |  |  |
| 730 | . 00052 | . 0005 | . 0003 | . 0001 |  |  |  |  |  |  |  |  |
| 740 | . 00025 | . 0002 | . 0002 |  |  |  |  |  |  |  |  |  |
| 750 | . 00012 | . 0001 |  |  |  |  |  |  |  |  |  |  |
| 760 | . 00006 |  |  |  |  |  |  |  |  |  |  |  |
| 770 | . 00003 | $\ldots$ | . . . |  | $\ldots$ | .... | $\ldots$ | .... | .... |  |  |  |

${ }^{27}$ L. A. Jones, private communication.

* Average of Weaver and Hecht's values.


## TABLE 60.-BLANCHARD'S DATA RELATING INSTANTANEOUS THRESHOLD TO FIELD BRIGHTNESS**

| Field bright- <br> ness $*$ | Instantaneous <br> threshold $\dagger$ | Relative <br> sensitivity $\ddagger$ <br> $(\mathrm{n})$ |  | Ratio $\S$ |
| :---: | :---: | :---: | :---: | :---: |

[^35]
## Part 1.-Contrast or photometric sensibility

For the following table the eye was adapted to a field of 0.1 millilambert and the sensitizing field flashed off. A neutral gray test spot (angular size at eye, $5 \times 2.5^{\circ}$ ) the two halves of which had the contrast indicated ( $\frac{1}{2}$ transparent, $\frac{1}{2}$ covered with neutral screen of transparency $=$ contrast indicated) was then observed and the brightness of the transparent part measured necessary to just perceive the contrast after the lapse of the various times. One eye only used, natural pupil. Values are log brightness of brighter field in millilamberts.


## Part 2.-Glare Sensibility

When an eye is adapted to a certain brightness and is then exposed suddenly to a much greater brightness, the latter may be called glaring if uncomfortable and instinctively avoided. Observers naturally differ widely. The data are the means of three observers, and are $\log$ brightnesses in millilamberts. The glare intensity may be taken as roughly 1700 times the cube root of the field intensity in millilamberts. Angle of glare spot, $4^{\circ}$.

| Log. field $\ldots \ldots$ | -6.0 | -4.0 | -2.0 | -1.0 | .0 | +1.0 | 2.0 | 3.0 | 4.0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Log. glare $\ldots$. | 1.35 | 1.90 | 2.60 | 2.90 | 3.28 | 3.60 | 3.90 | 4.18 | 4.48 |

## Part 3.-Rate of adaptation of sensibility

This table furnishes a measure of the rate of increase of sensibility after going from light into darkness, and the values were obtained immediately from the instant of turning off the sensitizing field. Both eyes were used, natural pupil, angular size of test spot, $4.9^{\circ}$, viewed at 35 cm . Retinal light persists only 10 to 20 minutes when one has been recently in darkness, then in a dimly lighted room; it persists fully an hour when a subject has been in bright sunlight for some time. A person who has worked much in the dark "gets his eyes" quicker than one who has not, but his final sensitiveness may be no greater.

| Sensitizing field |  | Logarithmic thresholds in millilamberts after |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0 sec | 1 sec | 2 sec | 5 sec | 10 sec | 20 sec | 40 sec | 60 sec | 5 min | 30 min | 60 min |
| White | 0.1 ml . | -2.79 | -3.82 | -4.13 | -4.50 | $-4.75$ | -4.96 | -5.16 | -5.32 | -5.68 | -5.91 | -6.06 |
|  | 1.0 ml . | -2.20 | -2.99 | $-3.27$ | -3.79 | -4.15 | -4.51 | $-4.82$ | -5.06 | -5.52 | -5.86 | -6.04 |
|  | 10.0 ml . | -1.60 | $-2.30$ | -2.53 | -3.08 | $-3.54$ | -3.94 | -4.31 | -4.61 | -5.22 | -5.83 | -6.01 |
| Blue ${ }^{1}$ | 100.0 ml . | -0.90 | -1.66 | $-2.00$ | --2.46 | -2.64 | -2.88 | -3.20 | -3.84 | -4.76 | -5.77 | -5.97 |
|  | 0.1 ml . | -2.82 | -3.92 | -4.36 | -4.91 | $-5.27$ | $-5.53$ | -5.68 | -5.81 | -6.23 |  |  |
| Green | 0.1 ml . | -2.69 | -4.08 | -4.39 | $-4.82$ | -5.11 | -5.26 | $-5.43$ | $-5.56$ | $-5.80$ | - |  |
| Yellow | 0.1 ml . | -2.61 | -3.84 | -4.17 | -4.41 | -4.65 | -4.78 | -5.02 | $-5.09$ | -5.39 |  |  |
| Red | 0.1 ml . | -2.32 | -2.69 | $-2.98$ | $-3.37$ | $-3.57$ | -3.65 | $-3.73$ | $-3.80$ | -4.02 |  |  |

* For reference, see footnote 25, p. 87.

TABLE 62.-MINIMUM ENERGY NECESSARY TO PRODUCE THE SENSATION

| Ives | erg sec |
| :---: | :---: |
| Russell | $7.7 \times 10^{-10}$ " ${ }^{\text {c }}$ |
| Reeves | $19.5 \times 10^{-10}$ |
| Buisson | . $12.6 \times 10^{-10}$ " |
| Taylor | Minimum threshold for dark-adapted eye, a surface, at a brightness of $1.8 \times 10^{-7}$ millilamberts, source color temperature $2850^{\circ} \mathrm{K}$. |
| Hecht | $2.2-5.7 \times 10^{-10}$ ergs at cornea, considering losses the amount of energy that reaches the retina is such that I quanta is absorbed by from 5-14 retinal rods. |

Astrophys. Journ., vol. 44, p. 124, 1916.
Astrophys. Journ., vol. 45, p. 60, 1917.
Astrophys. Journ., vol. 46, p. 167, 1917.
Journ. de phys., vol. 7, p. 68, 1917.
Journ. Opt. Soc. Amer., vol. 32, p. 506, 1942.

Journ. Opt. Soc. Amer., vol. 32, p. 42, 1942.

## TABLE 63.-APPARENT DIAMETER OF PUPIL AND FLUX DENSITY AT RETINA

Flashlight measures of the pupil (both eyes open) viewed through the eye lens and adapted to various field intensities. For eye accommodated to 25 cm , ratio apparent to true pupil, 1.02 , for the unaccommodated eye, 1.14 . The pupil size varies considerably with the individual. It is greater with one eye closed; e.g., it was found to be for 0.01 millilambert, 6.7 and 7.2 mm ; for $0.6 \mathrm{ml}, 5.3$ and 6.5 ; for $6.3 \mathrm{ml}, 4.1$ and 5.7 ; for $12.6 \mathrm{ml}, 4.1$ and 5.7 mm for both eyes and one eye open respectively for a certain individual. At the extreme intensities the two values approach each other. The ratio of the extreme pupil openings is about $\frac{1}{16}$, whereas the light intensities investigated vary over $1,000,000$-fold.

| Field millila mberts | Observed | $\begin{aligned} & (1.14 / 1.02) \\ & \times \text { obs. } \end{aligned}$ | $\begin{aligned} & \text { Effective } \\ & \text { area } \end{aligned}$ | Flux at retina, lumens per mm |
| :---: | :---: | :---: | :---: | :---: |
| . 00001 | 8 mm | 8.96 mm | $64 \mathrm{~mm}^{2}$ | $8.4 \times 10^{-12}$ |
| . 001 | 7.6 | 8.51 |  | $7.6 \times 10^{-10}$ |
| . 1 | 6.5 | 7.28 | 42 | $5.6 \times 10^{-8}$ |
| 10 | 4.0 | 4.48 | 16 | $2.1 \times 10^{-8}$ |
| 1000 | 2.07 | 2.35 | 4.3 | $5.8 \times 10^{-5}$ |

## TABLE 64.-MISCELLANEOUS EYE DATA

Light passing to the retina traverses in succession (a) front surface of the cornea (curvature, 7.9 mm ) ; (b) cornea (equivalent water path for energy absorption, 0.06 cm ); (c) back surface cornea (curv., 7.9 mm ) ; (d) aqueous humour (equiv. $\mathrm{H}_{2} \mathrm{O}, 0.34 \mathrm{~cm}$, $n=1.337$ ) ; (c) front surface lens (c, 10 mm ) ; ( $f$ ) lens (equiv. $\mathrm{H}_{2} \mathrm{O}, 0.42 \mathrm{~cm}, n=1.445$ ); (g) back surface lens (c, 6 mm ) ; ( $h$ ) vitreous humour (equiv. $\mathrm{H}_{2} \mathrm{O}, 1.46 \mathrm{~cm}, n=1.337$ ). An equivalent simple lens has its principal point 2.34 mm behind (a), nodal point 0.48 mm in front of ( $g$ ), posterior principal focus 22.73 mm behind ( $a$ ), anterior principal focus 12.83 mm in front of $(a)$, curvature, 5.125 mm . At the rear surface of the retina $(0.15 \mathrm{~mm}$ thick) are the rods ( $30 \times 2 \mu$ ) and cones ( 10 ( 6 outside fovea) $\mu$ long). Rods are more numerous, 2 to 3 between 2 cones, over $3,000,000$ cones in eye. Macula lutea, yellow spot, on temporal side, 4 mm from center of retina, long axis 2 mm . Central depression, fovea centralis, 0.3 mm diameter, 7000 cones alone present, $6 \times 2$ or $3 \mu$. In region of distinct vision (fovea centralis) smallest angle at which two objects are seen separate is $50^{\prime \prime}$ to $70^{\prime \prime}=3.65$ to $5.14 \mu$ at retina; 50 cones in $100 \mu$ here; $4 \mu$ between centers, $3 \mu$ to cone, $1 \mu$ to interval. Distance apart for separation greater as depart from fovea. No vision in blind spot, nasal side, 2.5 mm from center of eye, 15 mm in diameter.
Persistence of vision as related to color and intensity is measured by increasing speed of rotating sector until flicker disappears: for color, $0.4 \mu, 0.031 \mathrm{sec} ; 0.45 \mu, 0.020 \mathrm{sec} ; 0.5 \mu$, $0.015 \mathrm{sec} ; 0.57 \mu, 0.012 \mathrm{sec} ; 0.68 \mu, 0.014 \mathrm{sec} ; 0.76 \mu, 0.018 \mathrm{sec} ;$ for intensity, 0.06 metercandle, $0.028 \mathrm{sec} ; 1 \mathrm{mc}, 0.020 \mathrm{sec} ; 6 \mathrm{mc}, 0.014 \mathrm{sec} ; 100 \mathrm{mc}, 0.010 \mathrm{sec} ; 142 \mathrm{mc}, 0.007 \mathrm{sec}$.
Sensibility to small differences in color has two pronounced maxima (in yellow and green) and two slight ones (extreme blue, extreme red). The sensibility to small differences in intensity is nearly independent of the intensity (Fechner's law) as indicated by the following data due to König:

| $d I / I$, | $I / I_{0}$ | $\begin{gathered} 1,000,- \\ 000 \end{gathered}$ | 100.000 | 10,000 | 1000 | 100 | 50 | 10 | 5 | 1 | 0.1 | $I_{8}$ in mc |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | white. | . 036 | . 019 | . 018 | . 018 | . 030 | . 032 | . 048 | . 059 | . 123 | . 377 | . 00072 |
|  | . $60 \mu$. | - | . 024 | . 016 | . 020 | . 028 | . 038 | . 061 | . 103 | . 212 | - | . 0056 |
|  | $.50 \mu$. | - | - | . 018 | . 018 | . 024 | . 025 | . 036 | . 049 | . 080 | . 133 | .00017 |
|  | . $43 \mu$. | - | - | - | . 018 | . 025 | . 027 | . 040 | . 049 | . 074 | . 137 | . 00012 |

TABLE 65.-DISTRIBUTION COEFFICIENTS FOR EQUAL.ENERGY STIMULUS 1931 I.C.I. standard observer ${ }^{28}$
The fact that almost any color can be produced by the proper mixture of red, green, and blue light, has been used as a basis of a system of color specifications that has been adopted by the International Commission on Illumination. In the system adopted by that Commission in 1931, the primaries are called the $X, Y$, and $Z$ stimuli. The properties of the standard observer are given by his tristimulus specifications of the spectrum stimuli as a function of wavelength. This table gives this specification for the equal energy spectrum.

[^36]TABLE 65.-DISTRIBUTION COEFFICIENTS FOR EQUAL-ENERGY
STIMULUS (concluded)

| Wave length ( $\mathrm{m} \mu \mathrm{\mu}$ ) | Coefficients |  |  | Wave. (m $\mu$ ) | Coefficients |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | \% | $y$ | $z$ |  | . | y | $\bar{z}$ |
| 380 | . 0014 | . 0000 | . 0065 | 580 | . 9163 | . 8700 | . 0017 |
| 385 | . 0022 | . 0001 | . 0105 | 585 | . 9786 | . 8163 | . 0014 |
| 390 | . 0042 | . 0001 | . 0201 | 590 | 1.0263 | . 7570 | . 0011 |
| 395 | . 0076 | . 0002 | . 0362 | 595 | 1.0567 | . 6949 | . 0010 |
| 400 | . 0143 | . 0004 | . 0679 | 600 | 1.0622 | . 6310 | . 0008 |
| 405 | . 0232 | . 0006 | . 1102 | 605 | 1.0456 | . 5668 | . 0006 |
| 410 | . 0435 | . 0012 | . 2074 | 610 | 1.0026 | . 5030 | . 0003 |
| 415 | . 0776 | . 0022 | . 3713 | 615 | . 9384 | . 4412 | . 0002 |
| 420 | ¢1344 | . 0040 | . 6456 | 620 | . 8544 | . 3810 | . 0002 |
| 425 | ¢2148 | . 0073 | 1.0391 | 625 | . 7514 | . 3210 | . 0001 |
| 430 | . 2839 | . 0116 | 1.3856 | 630 | . 6424 | . 2650 | . 0000 |
| 435 | . 3285 | . 0168 | 1.6230 | 635 | . 5419 | . 2170 | . 0000 |
| 440 | . 3483 | . 0230 | 1.7471 | 640 | . 4479 | . 1750 | . 0000 |
| 445 | . 3481 | . 0298 | 1.7826 | 645 | . 3608 | . 1382 | . 0000 |
| 450 | . 3362 | . 0380 | 1.7721 | 650 | . 2835 | . 1070 | . 0000 |
| 455 | . 3187 | . 0480 | 1.7441 | 655 | . 2187 | . 0816 | . 0000 |
| 460 | . 2908 | . 0600 | 1.6692 | 660 | . 1649 | . 0610 | . 0000 |
| 465 | . 2511 | . 0739 | 1.5281 | 665 | . 1212 | . 0446 | . 0000 |
| 470 | . 1954 | . 0910 | 1.2876 | 670 | . 0874 | . 0320 | . 0000 |
| 475 | . 1421 | . 1126 | 1.0419 | 675 | . 0636 | . 0232 | . 0000 |
| 480 | . 0956 | . 1390 | . 8130 | 680 | . 0468 | . 0170 | . 0000 |
| 485 | . 0580 | . 1693 | . 6162 | 685 | . 0329 | . 0119 | . 0000 |
| 490 | . 0320 | . 2080 | . 4652 | 690 | . 0227 | . 0082 | . 0000 |
| 495 | . 0147 | . 2586 | . 3533 | 695 | . 0158 | . 0057 | . 0000 |
| 500 | . 0049 | . 3230 | . 2720 | 700 | . 0114 | . 0041 | . 0000 |
| 505 | . 0024 | . 4073 | . 2123 | 705 | . 0081 | . 0029 | . 0000 |
| 510 | . 0093 | . 5030 | . 1582 | 710 | . 0058 | . 0021 | . 0000 |
| 515 | . 0291 | . 6082 | . 1117 | 715 | . 0041 | . 0015 | . 0000 |
| 520 | . 0633 | . 7100 | . 0782 | 720 | . 0029 | . 0010 | . 0000 |
| 525 | . 1096 | . 7932 | . 0573 | 725 | . 0020 | . 0007 | . 0000 |
| 530 | . 1655 | . 8620 | . 0422 | 730 | . 0014 | . 0005 | . 0000 |
| 535 | . 2257 | . 9149 | . 0298 | 735 | . 0010 | . 0004 | . 0000 |
| 540 | . 2904 | . 9540 | . 0203 | 740 | . 0007 | . 0003 | . 0000 |
| 545 | . 3597 | . 9803 | . 0134 | 745 | . 0005 | . 0002 | . 0000 |
| 550 | . 4334 | . 9950 | . 0087 | 750 | . 0003 | . 0001 | . 0000 |
| 555 | . 5121 | 1.0002 | . 0057 | 755 | . 0002 | . 0001 | . 0000 |
| 560 | . 5945 | . 9950 | . 0039 | 760 | . 0002 | . 0001 | . 0000 |
| 565 | . 6784 | . 9786 | . 0027 | 765 | . 0001 | . 0000 | . 0000 |
| 570 | . 7621 | . 9520 | . 0021 | 770 | . 0001 | . 0000 | . 0000 |
| 575 | . 8425 | . 9154 | . 0018 | 775 | . 0000 | . 0000 | . 0000 |
| 580 | . 9163 | . 8700 | . 0017 | 780 | . 0000 | . 0000 | . 0000 |
| Totals.. | ... | $\ldots$ | ..... | ... | 21.3713 | 21.3714 | 21.3715 |

TABLE 66.-RELATIVE MAGNITUDE OF UNITS OF ILLUMINATION

| Units | Lux | Phot | Milliphot | Foot-candle |
| :---: | :---: | :---: | :---: | :---: |
| 1 lux | $=1$ | . 0001 | . 1 | . 0929 |
| 1 phot | $=10,000$ | 1. | 1000. | 929. |
| 1 milliphot | $=10$ | . 001 |  | . 929 |
| 1 foot-candle | 10.76 | . 001076 | 1.076 | 1. |

Candlepower $c$ candles at visual threshold of steady point source of white light seen against white hackground brightness $b$ millimicrolanbert (m $m$ ) at range $r$ sea miles through an atmosphere of attenuation a per sea mile is given by

$$
C=3.7 \times 10^{-2}(1+b): r^{2} a^{-r},
$$

which is valid within a factor of 3 for $b$ from total darkness to full daylight. For practical signaling or mavigation multiply $c$ by at least 100.

| Ranger <br> sea mile | Threehold $\%$ candles, $b=100 \mathrm{~m} \mu \mathrm{~L}$., at night |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $a=1$ | $a=0.8$ | $a=0.6$ | $a=0.4$ |
| 1 | . 04 | . 05 | . 06 | . 09 |
| 2 | . 15 | . 23 | . 41 | . 9 |
| 3 | . 33 | . 65 | 1.5 | 5.2 |
| 5 | .91 | 2.9 | 12 | 90 |
| 7 | 1.8 | 8.6 | 62 | 1100 |
| 10 | 3.6 | 34 | 610 | 35000 |

Knoll, H. . ... Tousey, R., and Hulhurt. E. O., Journ. Opt. Soc. Amer., vol. 36, p. 480, 1946.

## TABLE 68.-THE BRIGHTNESS OF THE SUN

From the definition of a lumen, the lumen output from a point source within a unit solid angle is numerically equal to the candlcpower of the source. This also holds for any radiating source that behaves as a point, such as a spherical blackbody,* or any spherical radiator of uniform brightness that obeys the Lambert cosine law of radiation, providing the measurements are nade at such a distance from the source that the inverse square law is obeyed. (See Table 74.) As an example of this, consider the brightness of the sun. The sun when directly overhead on a clear day gives an illumination of about 10,000 footcandles. This is equal to 10,000 lumens per $\mathrm{ft}^{2}{ }^{2}$ (See Table 73.) To change this to lumens for a unit solid angle, multiply by the radius of the earth's orbit squared (i.e., $2.41 \times 10^{23}$ $\mathrm{ft}^{2}$ ). Thus, the candlepower of the sun is $2.41 \times 10^{27}$. To get the brightness per $\mathrm{cm}^{2}$ divide this by the projected area of the sun in $\mathrm{cm}^{2}$ (i.e., $1.52 \times 10^{22}$ ), which gives about 160,000 $\mathrm{c} / \mathrm{cm}^{2}$ for the brightness of the sun as observed at the earth's surface. This, of course, assumes that the sun's surface is of uniform brightness and that its radiation obeys the Lambert cosine law. The data (Table 813) on the distribution of energy of the solar spectrum give a brightness of the sun of $146,000 \mathrm{c} / \mathrm{cm}^{2}$.

[^37]
## TABLE 69.-SOME OBSOLETE PHOTOMETRIC STANDARDS

(In use prior to 1948.)
In Germany the Hefner lamp was most used; in England the Pentane lamp and sperm candles; in France the Carcel lamp was preferred; in America the Pentane and Hefner lamps were used to some extent, but candles were largely employed in gas photometry. For the photometry of electric lamps, and in accurate photometric work, electric lamps, standardized at a national standardizing institution, were employed.
The "international candle" designated the value of the candle as maintained by cooperative effort between the national laboratories of England, France, and America; and the value of various photometric units in terms of this is given in the following table (Circular No. 15 of the Bureau of Standards) :

1 international candle $=1$ Pentane candle.
1 international candle $=1$ Bougie decimale.
1 international candle $=1$ American candle.
1 international candle $=1.11$ Hefner unit.
1 international candle $=0.104$ Carcel unit.

1. Standard Pentane lamp, burning pentane.............. 10.0 candles.
2. Standard Hefner lamp, burning amyl acetate........... 0.9 candles.
3. Standard Carcel lamp, burning colza oil................. 9.6 candles.
4. Standard English sperm candle, approximately......... 1.0 candles.

The international candle was in reality taken from the candlepower of a number of incandescent lamps, operated under definite conditions and kept at the standard laboratories of France, Britain, and the United States.
(Adapted from Reports of Committee on Nomenclature and Standards of Illuminating Engineering Society, 1942.)

Apostilb $=0.1$ millilambert.
Brightness of a luminous surface may be expressed in two ways:
(1) $b_{t}=d I / d A \cos \theta$ where $\theta$ is the angle between normal to surface and the line of sight; normal brightness when $\theta$ is zero.
(2) $b_{F}=d F / d A$ assuming that the surface is a perfect diffuser, obeying cos law of emission or reflection. Unit, the lambert.
Candle per $\mathrm{cm}^{2}=3.1416$ lamberts $=1$ stilb.
Candle per in. ${ }^{2}=.4868$ lambert $=486.8$ millilamberts.
Foot-candle $=1$ lumen incident per $\mathrm{ft}^{2}=1.076$ milliphots $=10.76$ lux.
Illumination on surface $=E=$ flux density on surface $=d F / d A$ ( $A$ is surface area) $=$ $F / A$ when uniform. Units, meter-candle, foot-candle, phot, lux.
Lambert, the cgs unit of brightness, is the brightness of a perfectly diffusing surface radiating or reflecting one lumen per $\mathrm{cm}^{2}$. Equivalent to a perfectly diffusing surface with illumination of one phot. A perfectly diffusing surface emitting one lumen per $\mathrm{ft}^{2}$ has a brightness of 1.076 millilamberts. Brightness in candles per $\mathrm{cm}^{2}$ is reduced to lamberts by multiplying by $\pi$.

Lambert $=1$ lumen emitted per $\mathrm{cm}^{2}$ of a perfectly diffusing surface.
Lambert $=.3183$ candle per $\mathrm{cm}^{2}=2.054$ candles per $\mathrm{in}^{2}$.
Lumen is emitted by .07958 spherical candle.
Lumen emitted per $\mathrm{ft}^{2}=1.076$ millilamberts (perfect diffusion).
Luminous efficiency $=F / \Phi$ expressed in lumens/watt.
Luminous flux $=F$ or $\psi=$ rate of flow of radiation measured according to power to produce visual sensation. Although strictly thus defined, for photometric purposes it may be regarded as an entity, since the rate of flow for such purposes is invariable. Unit is the lumen, the flux emitted in a unit solid angle (steradian) by a point source of unit candle power.

Luminous intensity of (approximate) point source $=I=$ solid-angle ( $\omega$ ) density of luminous flux in direction considered $=d F / d \omega$, or $F / \omega$ when the intensity is uniform. Unit, the candle.
Luminosity factor of radiation of wave-length $\lambda=K_{\lambda}=$ ratio of luminous to radiant flux for that $\lambda,=F_{\lambda} / \Phi_{\lambda}$.

Lux $=1$ lumen incident per $\mathfrak{m}^{2}=.0001$ phot $=.1$ milliphot.
Mechanical equivalent of light $=$ ratio of $\Phi / F$ for the $\lambda$ of max. visibility expressed in (ergs $/ \mathrm{sec}$ )/lumen or watts/lumen; it is the reciprocal of max. luminosity. See Table 58.

Millilambert $=.929$ lumen per $\mathrm{ft}^{2}$ (perfect diffusion).
Milliphot $=.001$ phot $=.929$ foot-candle.
Phot $=1$ lumen incident per $\mathrm{cm}^{2}=10,000$ lux $=1000$ milliphots.
Photon $=$ small bundle of energy ( $h v$ ), also called a quantum.
Radiant flux $=\Phi=$ rate of flow of radiation as energy, measured as ergs per second or watts.

Specific luminous radiation, $E^{\prime}=$ luminous flux density emitted by a surface, or the flux emitted per unit of emissive area, expressed in lumens per $\mathrm{cm}^{2}$. For surfaces obeying Lambert's cosine law, $E^{\prime}=\pi b_{0}$.

Spectral luminous flux at wavelength $\lambda=\left(K_{\lambda}\right)\left(\Phi_{\lambda}\right)$. Spectral luminous curve expresses this as a function of $\lambda$ and is different for various sources.

One spherical candle emits 12.57 lumens.
Uniform point source of one candle emits $4 \pi$ lumens.

TABLE 71.-RELATIVE MAGNITUDES OF UNITS OF BRIGHTNESS


[^38]This standard of light intensity is the brightness of a blackbody at the temperature of freezing platinum. The blackbody used was made of thorium oxide and was immersed in the melting platinum: very pure platinum ( 99.997 percent) was used. Reproducible to 0.1 percent, the brightness was found to be 58.84 international candles per $\mathrm{cm} .^{2}$. This $W^{1}$ aidner-Burgess standard, taking the brightness of the blackbody at the freezing point of platinum as 60 candles per $\mathrm{cm}^{2}$, was adopted by the International Committee on Weights and Measures in 1937 as the new unit of light intensity and was put into effect January 1, $1948 .{ }^{31}$

The light from the blackbody at the temperature of freezing platinum is not greatly different in color from that given by carbon-filament standard lamps, as the color temperature of the lamp filaments is about $2100^{\circ} \mathrm{K}$, whereas the freezing point of platinum is $2042^{\circ} \mathrm{K}$. In this range of color the new unit of intensity is about 1.9 percent smaller than the old international candle, and sources of light are correspondingly given higher numerical ratings. However, when light sources of higher color temperature are compared with these basic standards, the accepted spectral luminosity factors give slightly lower values for the "whiter" sources than were obtained by visual measurements when the present international units were established. The difference between the two scales therefore grows less as the color temperature of the sources measured is increased, and for sources in the range of ordinary vacuum tungsten-filament lamps, around $2500^{\circ} \mathrm{K}$, the new scale crosses the international scale as used in the United States. Furthermore, when the range of standards was extended to gas-filled tungsten-filament lamps and other new types, the measurements were made by methods nearly in accord with the luminosity factors. Consequently the present ratings of tungsten-filament lamps in this country will be practically unaffected by the change, no type being changed by more than 1 percent.

[^39]TABLE 73.-SYMBOLS AND DEFINING EXPRESSIONS FOR.PHOTOMETRY*

| DesignationSymbol and <br> defining <br> equation | Unit | Proposed |
| :---: | :---: | :---: |
| Luminous flux .................. $F$ | Lumen | 1 m |
| Luminous intensity (candlepower).. $\quad I=\frac{d F}{d \omega}$ | Candle | c |
| Illumination $\dagger \ldots \ldots \ldots \ldots \ldots . E=\frac{d F}{d / A}$ | Foot-candle <br> Lux, Phot | $\begin{aligned} & \mathrm{ft-c} \\ & \mathrm{~lx}, \mathrm{ph} \end{aligned}$ |
| Quantity of light................ $Q=F d t$ $t=$ time in hours | Lumen-hour | 1 m -hr |
|  | Candle per unit area Stilb | $\begin{aligned} & \mathrm{c} / \mathrm{in}^{2}{ }^{2} \\ & \mathrm{c} / \mathrm{cm}^{2} \\ & \mathrm{sb}=\mathrm{c} / \mathrm{cm}^{2} \end{aligned}$ |

The mechanical equivalent of light $m$ is the least amount of mechanical energy in watts necessary to produce 1 lumen. This energy must, of course, produce light at the wavelength ( $\lambda=0.556 \mu$ ) where the average eye has its maximum sensitivity.

Suppose $B_{u}$ is the brightness of a blackbody in candles per $\mathrm{cm}^{2}$, then

$$
B_{0}=\frac{1}{m \pi} \int\left[c_{1} \lambda^{-5} /\left(\exp \left(c_{2} / \lambda T\right)-1\right)\right] K_{\lambda} d \lambda
$$

where $K_{\lambda}$ is the relative luminosity factor (Table 58). The integration is taken over the visible spectrum. The constant $c_{1}$ is to be so chosen as to give the energy per unit wavelength for a $2 \pi$ solid angle, then $m$ is the mechanical equivalent of light. Using the new value of the brightness of the blackbody at the platinum point ( 60 candles $/ \mathrm{cm}^{2}$ ) and making the above calculation for the platinum point ( $2042.16{ }^{\circ} \mathrm{K}$ ) using the new radiation constants (Table 53), gives $m=0.00147$ watts/lumen. The reciprocal of this, 680 lumens/ watt, is the value generally given.
Equivalents and conversion factors for photometry.-The total flux from a source of unit spherical candlepower is 12.57 hmmens.

$$
\begin{aligned}
1 \text { lux } & =1 \text { lumen incident per } \mathrm{m}^{2} \\
1 \text { phot } & =1 \text { lumen incident per } \mathrm{cm}^{2} \\
1 \text { foot-candle } & =1 \text { lumen incident per } \mathrm{ft}^{2}
\end{aligned}
$$ VARIOUS DISTANCES

| d/L | $d=$ distance ; $L=$ length or diameter of (disk) source. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Line | Disk | $d / L$ | Line | Disk |
| 5 | 99.31 | 99.0 | 12 | 99.88 | 99.83 |
| 10 | 99.83 | 99.74 | 15 | 99.94 | 99.90 |
|  |  |  | 20 | 99.98 | 99.95 |

## TABLE 75.-SPECTRAL LUMINOUS INTENSITIES

From Planck's equation and constants given in Table 53 and the relative luminosity factors (Table 58) the spectral luminous intensities were calculated for a series of wavelengths ( $d \lambda=.01 \mu$ ), and for a number of temperatures and then reduced to equal total luminous intensities. These relative values tor the brightness (photometric) of the blackbody at different temperatures hold for measurements made with a field brightness above about 1 millilambert but do not hold for measurements made for low field brightness. Some time ago some engineers engaged in photometry found a need for agreement for a standard for low intensity. It was then decided ${ }^{32}$ to use a source at a color temperature of $2360{ }^{\circ} \mathrm{K}$. Recently ${ }^{33}$ the International Committee on Weights and Measures adopted the blackbody at the freezing point of platinum $\left(2042^{\circ} \mathrm{K}\right)$ as the standard for low-intensity brightness in photometry.

| $\lambda$ in | $\begin{aligned} & 2000 \\ & { }^{2} \mathrm{~K} \end{aligned}$ | ${ }^{20}{ }^{\circ} \mathrm{K}$. ${ }^{*}$ | ${ }^{2100}{ }^{\circ} \mathrm{K}$ | ${ }^{2200}$ | ${ }^{23} \mathrm{C}$ | 2400 ${ }^{\mathrm{K}} \mathrm{K}$ | $\begin{gathered} 2500 \\ { }^{\circ} \mathrm{K} \end{gathered}$ | $\begin{gathered} 2600 \\ \circ \mathrm{~K} \end{gathered}$ | $\begin{gathered} 2700 \\ 0 \mathrm{~K} \end{gathered}$ | $2800$ | $2900$ | $3000$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 38 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 |
| . 39 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 |
| . 40 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00000 | . 00001 |
| . 41 | . 00000 | . 00000 | . 00001 | . 00001 | . 00001 | .00001 | . 00001 | . 00001 | . 00002 | . 00002 | . 00002 | . 00002 |
| . 42 | . 00002 | . 00002 | . 00002 | . 00003 | . 00004 | . 00004 | . 00005 | . 00006 | . 00007 | . 00007 | . 00008 | . 00009 |
| . 43 | . 00008 | . 00008 | . 00009 | . 00011 | . 00013 | . 00015 | . 00018 | . 00020 | . 00023 | . 00025 | . 00028 | . 00030 |
| . 44 | . 00019 | . 00021 | . 00023 | . 00028 | . 00032 | . 00037 | . 00042 | . 00047 | . 00053 | . 00058 | . 00064 | . 00069 |
| . 45 | . 00041 | . 00044 | . 00049 | . 00057 | . 00065 | . 00074 | . 00083 | . 00093 | . 00102 | . 00111 | . 00121 | . 00131 |
| . 46 | . 00083 | . 00088 | . 00096 | . 00111 | . 00125 | . 00140 | . 00155 | . 00171 | . 00186 | . 00202 | . 00217 | . 00233 |
| . 47 | . 00157 | . 00167 | . 00180 | . 00204 | . 00228 | . 00252 | . 00276 | .00301 | . 00325 | . 00349 | . 00372 | . 00396 |
| . 48 | . 00297 | . 00313 | . 00336 | . 00374 | . 00413 | . 00452 | . 00490 | . 00528 | . 00565 | . 00602 | . 00638 | . 00673 |
| . 49 | . 00544 | . 00570 | . 00606 | . 00667 | . 00728 | . 00786 | . 00845 | . 00902 | . 00957 | . 01011 | . 01063 | . 01114 |
| . 50 | . 01024 | . 01067 | . 01125 | . 01223 | . 01318 | . 01411 | . 01501 | . 01587 | . 01670 | . 01750 | . 01827 | . 01901 |
| . 51 | . 01915 | . 01983 | . 02075 | . 02229 | . 02376 | . 02517 | . 02652 | . 02780 | . 02903 | . 03019 | . 03131 | . 03237 |
| . 52 | . 03217 | . 03313 | . $034+2$ | . 03654 | . 03853 | . 04042 | . 04220 | . 04387 | . 04545 | . 04694 | . 04834 | . 04967 |
| . 53 | . 04609 | . 04721 | . 04871 | . 05112 | . 05336 | . 05544 | . 05739 | . 05919 | . 06087 | . 06243 | . 06388 | . 06524 |
| . 54 | . 05972 | . 06086 | . 06236 | . 06475 | . 0669 ? | . 06890 | . 07073 | . 07238 | . 07390 | . 07530 | . 07659 | . 07776 |
| . 55 | . 07240 | . 07341 | . 07473 | . 07678 | . 07861 | . 08022 | . 08168 | . 08297 | . 08412 | . 08517 | . 08613 | . 08695 |
| . 56 | . 08356 | . 08432 | . 08528 | . 08675 | . 08800 | . 08905 | . 08996 | . 09073 | . 09139 | . 09198 | . 09243 | . 09284 |
| . 57 | . 09167 | . 09207 | . 09255 | . 09323 | . 09374 | . 09409 | . 09433 | . 09449 | . 09457 | . 09459 | . 09455 | . 09447 |
| . 58 | . 09545 | . 09544 | . 09539 | . 09518 | . 09488 | . $09+49$ | . 09405 | . 09358 | . 09307 | . 09256 | . 09203 | . 09150 |
| . 59 | . 09408 | . 09366 | . 09307 | . 09203 | . 09098 | . 08992 | . 08889 | . 08786 | . 08686 | . 08591 | . 08498 | . 08409 |
| . 60 | . 08833 | . 08757 | . 08654 | . 08483 | . 08319 | . 08163 | . 08013 | . 07873 | . 07739 | . 07611 | . 07491 | . 07379 |
| . 61 | . 07890 | . 07791 | . 07658 | . 07443 | . 07243 | . 07056 | . 06882 | . 06720 | . 06570 | . 06428 | . 06296 | . 06173 |
| . 62 | . 06663 | . 06554 | . 06409 | . 06178 | . 05966 | . 05774 | . 05595 | . 05432 | . 05281 | . 05141 | . 05012 | . 04893 |
| . 63 | . 05143 | . 05039 | . 04904 | . 04689 | . 04495 | . 04322 | . 04162 | . 04018 | . 03886 | . 03765 | . 03654 | . 03552 |
| . 64 | . 03752 | . 03663 | . 03547 | . 03366 | . 03204 | . 03061 | . 02930 | . 02813 | . 02708 | . 02610 | . 02522 | . 02442 |
| . 65 | . 02523 | . 02455 | . 02366 | . 02228 | . 02107 | . 02000 | . 01904 | . 01818 | . 01741 | . 01671 | . 01608 | . 01550 |
| . 66 | . 01576 | . 01528 | . 01466 | . 01371 | . 01287 | . 01215 | . 01150 | . 01092 | . 01041 | . 00995 | . 00953 | . 00916 |
| . 67 | .00902 | . 00872 | . 00833 | . 00773 | . 00721 | . 00677 | . 00637 | . 00602 | . 00571 | . 00544 | . 00519 | . 00497 |
| . 68 | . 00521 | . 00502 | . 00477 | . 00440 | . 00408 | . 00381 | . 00357 | . 00335 | . 00317 | . 00300 | . 00285 | . 00272 |
| . 69 | . 00272 | . 00262 | . 00248 | . 00227 | . 00209 | . 00194 | . 00181 | . 00169 | . 00159 | . 00150 | . 00142 | . 00135 |
| . 70 | . 00147 | . $0001+1$ | . 00133 | . 00121 | . 00111 | . 00103 | . 00095 | . 00088 | . 00083 | . 000078 | . 00073 | . 00069 |
| . 71 | . 00081 | . 00077 | . 000073 | . 00066 | . 00060 | . 00055 | . 00051 | . 000047 | . 00044 | . 00041 | . 00039 | . 00037 |
| . 72 | . 000044 | . 00041 | . 00039 | . 00035 | . 000032 | . 00029 | . 00026 | . 00024 | . 00023 | . 00021 | .00020 | . 00019 |
| . 73 | . 00023 | . 00022 | . 00020 | . 00018 | . 00016 | . 00015 | . 00014 | . 00013 | . 00012 | . 00011 | . 00010 | . 00009 |
| . 74 | . 00012 | . 00011 | . 00010 | . 00009 | . 000008 | . 000007 | . 00007 | . 00006 | . 00006 | . 00005 | . 00005 | . 00005 |
| . 75 | . 00006 | . 000006 | . 00005 | . 00005 | . 00004 | . 00004 | . 00003 | . 00003 | . 00003 | . 00003 | . 00002 | . 00002 |
| . 76 | . 00003 | . 00003 | . 00003 | . 00002 | . 00002 | . 00002 | . 00002 | . 00002 | . 00001 | . 00001 | . 00001 | . 00001 |
| Relative light |  |  |  |  |  |  |  |  |  |  |  |  |
| output: | . 775 | 1.000 | 1.399 | 2.398 | 3.927 | 6.178 | 9.383 | 13.810 | 19.765 | 27.594 | 37.661 | 50.372 |
| $\lambda \max$ : | . 5825 | . 5830 | . 5805 | . 5785 | . 5770 | . 5755 | . 5745 | . 5730 | . 5715 | . 5705 | . 5695 | . 5685 |

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## TABLE 76.-BRIGHTNESS OF BLACKBODY, CROVA WAVELENGTH, MECHANICAL EQUIVALENT OF LIGHT, LUMINOUS INTENSITY, and luminous efficiency of blackbody

The values of the luminous intensity $I$ in candles and the luminous flux $F$ in lumens have been calculated using Planck's equation and the values of the luminosity factors $K_{\text {s }}$ given in Table 58. The basis of these values is the value of the Waidner-Burgess standard of light intensity.
The following equation is used :

$$
B_{0}=\frac{1}{m \pi} \int J(\lambda T) K_{\lambda} d \lambda,
$$

where $B_{0}=60$ candles per $\mathrm{cm}^{2}, T=2042.16^{\circ} \mathrm{K}$, and $m=$ the minimum mechanical equivalent of light expressed in watts per lumen.
The radiation constants (Table 53) used in these calculations and the value given in the table as the brightness of the blackbody at this temperature (2042.16) give for the reciprocal of the mechanical equizalcht of light 680 lumens per zott. This means that 1 watt of radiated energy at about $\lambda=0.555 \mu$ will give 680 lumens.
White light has sometimes been defined as that emitted by a blackbody at a temperature of $6000{ }^{\circ} \mathrm{K}$.

The crova wavelength for a blackbody is that wavelength $\lambda_{c}$, at which the spectral luminous intensity varies at the same rate as the total luminous intensity varies for a change in the temperature.

| ${ }^{\text {Temperature }}$ | $\begin{gathered} \text { Total } \\ \text { intensity } \\ \text { watts } / \mathrm{cm}^{2} \end{gathered}$ | Brightness candles $/ \mathrm{cm}^{2}$ | Lumens/ $/ \mathrm{cm}^{2}$ | Lumens/watt | $\begin{aligned} & \text { Crova } \\ & \text { wave } \\ & \text { length } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1200 | 11.16 | . 0140 | . 04 | 0035 |  |
| 1400 | 21.79 | . 245 | . 77 | .035 |  |
| 1600 | 37.18 | 2.145 | 6.74 | . 18 |  |
| 1700 | 47.38 | 5.28 | 16.57 | . 35 | . $584 \mu$ |
| 1800 | 59.55 | 11.78 | 37.00 | . 62 |  |
| 1900 | 73.92 | 24.23 | 76.11 | 1.03 |  |
| 2000 | 90.76 | 46.47 | $1.460 \times 10^{2}$ | 1.61 | . 578 |
| 2042.16 | 98.65 | $60.00{ }^{\dagger}$ | $1.885 \times 10^{2}$ | 1.91 |  |
| 2200 | $1.3288 \times 10^{2}$ | $1.439 \times 10^{2}$ | $4.520 \times 10^{2}$ | 3.40 |  |
| 2500 | $2.2158 \times 10^{2}$ | $5.628 \times 10^{2}$ | $1.7679 \times 10^{3}$ | 7.98 | . 572 |
| 2700 | $3.0146 \times 10^{2}$ | $1.186 \times 10^{3}$ | $3.726 \times 10^{3}$ | 12.36 |  |
| 3000 | $4.5946 \times 10^{2}$ | $3.021 \times 10^{3}$ | $9.491 \times 10^{3}$ | 20.7 | . 568 |
| 3500 | $8.5122 \times 10^{2}$ | $1.031 \times 10^{4}$ | $3.183 \times 10^{4}$ | 37.4 | . 564 |
| 4000 | $1.4521 \times 10^{3}$ | $2.525 \times 10^{4}$ | $7.932 \times 10^{4}$ | 54.6 |  |
| 4500 | $2.3260 \times 10^{3}$ | $5.158 \times 10^{4}$ | $1.620 \times 10^{5}$ | 69.7 | . 560 |
| 5000 | $3.5453 \times 10^{3}$ | $9.164 \times 10^{4}$ | $2.879 \times 10^{5}$ | 81.2 | . 558 |
| 5500 | $5.1906 \times 10^{3}$ | $1.4705 \times 10^{5}$ | $4.620 \times 10^{5}$ | 89.0 | . 557 |
| 6000 | $7.3514 \times 10^{3}$ | $2.186 \times 10^{5}$ | $6.868 \times 10^{5}$ | 93.4 | . 556 |
| 6500 | $1.0126 \times 10^{4}$ | $3.065 \times 10^{5}$ | $9.629 \times 10^{5}$ | 95.1 | . 555 |
| 7000 | $1.3619 \times 10^{4}$ | $4.103 \times 10^{5}$ | $1.289 \times 10^{6}$ | 94.6 | . 555 |
| 7500 | $1.7948 \times 10^{4}$ | $5.294 \times 10^{5}$ | $1.663 \times 10^{6}$ | 92.7 |  |
| 8000 | $23234 \times 10^{4}$ | $6.630 \times 10^{5}$ | $2.083 \times 10^{8}$ | 89.6 | . 554 |
| 10,000 | $5.6724 \times 10^{4}$ | $1.3221 \times 10^{6}$ | $4.153 \times 10^{6}$ | 73.2 |  |

[^41]An optical pyrometer is a device for measuring the temperature of a high-temperature radiating body by comparing its brightness for a selected wavelength interval (within the visible spectrum to be sure) with that of some standard selected source. The wavelength, or wavelength interval, is generally selected by the use of a red glass in the eycpiece. This gives rise to the term effective wavelength. (See Table 562.) The effective wavelength of a monochromatic screen for a definite temperature interval has been defined as the wavelength for which the relative brightness, as calculated from Wien's equation for this temperature interval, is the same as the ratio of the integral luminosities for these two temperatures, as measured through the red screen.

Various devices are used to make these comparisons, and different devices have been used as the comparison source. It seems that most users of the optical pyrometer today prefer to use the disappearing-filament type, which has a small filament as the comparison source.

The optical pyrometer as generally calibrated gives the true temperature of blackbodies but not of other radiators. If one radiating characteristic of any other radiator-e.g., its emissivity-is known, true temperatures can be determined of such radiators, e.g., an incandescent tungsten filament, by the use of the optical pyrometer. The emissivities of a number of sources are given in Table 78.

The true temperature $T$ of a non-blackbody may be determined from its brightness temperature, $S_{\lambda}$ (the apparent temperature), and its emissivity $\mathfrak{c}_{\lambda}$ from the following relation:

$$
\frac{1}{T}-\frac{1}{S_{\lambda}}=\frac{\lambda \log c_{\lambda}}{c_{2} \log c}
$$

For some calculated values see Table 79.
This entire subject is extensively treated in "Temperature, Its Measurement and Control," a report of a symposium on this subject published by the Reinhold Publishing Co. in 1941.

## TABLES 78-84.-EMISSIVITIES OF A NUMBER OF MATERIALS

## TABLE 78.—NORMAL SPECTRAL EMISSIVITIES FOR SOME ELEMENTS AND ALLOYS

The emissivity, spectral or total, of any non-blackbody shows the relation between the intensity of its radiation and that of the blackbody when both are at the same temperature. Spectral emissivities have been measured for a number of materials for different temperatures and different wavelength intervals and are shown in Part 1.

## Part 1.-At temperatures generally above $1000{ }^{\circ} \mathrm{K}^{\text {s }}$

Room temperature values are given in a few instances where they, along with values at higher temperatures, form a connected series and where the values given for the higher temperatures depend on those given for low temperatures.

| Material Carbon | $\begin{aligned} & \text { Temperature } \\ & { }^{2} \mathrm{~K} \\ & \hline . \quad 1600 \\ & 2500 \end{aligned}$ | Emıssivity |  |  |  |  |  | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Red |  | Green |  | ${ }^{\text {Blue }}$ |  |  |
|  |  | $\begin{gathered} \overparen{\lambda \text { in } \mu} \\ .66 \\ .66 \end{gathered}$ | $\begin{gathered} \mathbf{c}_{\lambda} \\ .89 \\ .84 \end{gathered}$ | $\overbrace{\lambda \text { in } \mu}$ | $e_{\lambda}$ | 入in $\mu$ | $e_{\lambda}$ |  |
| Copper | $\begin{array}{r} 1275 \\ 1350 \\ 1375 \\ 1450 \\ 1500 \end{array}$ | $\begin{aligned} & .66 \\ & .66 \\ & .66 \\ & .66 \\ & .66 \end{aligned}$ | $\begin{aligned} & .105 \\ & .120 \\ & .150 \\ & .140 \\ & .13 \end{aligned}$ |  |  |  |  | Solid <br> Solid <br> Liquid <br> Liquid <br> Liquid |
| Iron .... | $\begin{aligned} & .1480-1500 \\ & 1000 \\ & 10 \end{aligned}$ | $\begin{aligned} & .66 \\ & .65 \end{aligned}$ | $\begin{aligned} & .27 \\ & .37 \end{aligned}$ |  |  |  |  | Solid <br> Solid and liquid |
| Konal | . 1200 | . 665 | . 43 |  |  |  |  |  |
| Molybdenum | $\begin{array}{r} 300 \\ 1300 \\ 2000 \\ 2750 \end{array}$ | $\begin{aligned} & .665 \\ & .665 \\ & .665 \\ & .665 \end{aligned}$ | $\begin{aligned} & .420 \\ & .378 \\ & .353 \\ & .332 \end{aligned}$ |  |  | $\begin{array}{r} .467 \\ .467 \\ .467 \\ .467 \end{array}$ | $\begin{aligned} & .425 \\ & .395 \\ & .380 \\ & .365 \end{aligned}$ |  |
| Nickel | 1200-1650 | . 665 | . 375 | . 535 | . 425 | 460 | . 450 | Solid |
| Tantalum | $\begin{array}{r} 300 \\ 1400 \\ 2100 \\ 2800 \end{array}$ | $\begin{aligned} & .665 \\ & .665 \\ & . .65 \\ & .665 \end{aligned}$ | $\begin{aligned} & .493 \\ & .442 \\ & .415 \\ & .390 \end{aligned}$ |  |  | $\begin{aligned} & .467 \\ & .467 \\ & .467 \\ & .467 \end{aligned}$ | $\begin{aligned} & .565 \\ & .505 \\ & .460 \\ & \cdots \end{aligned}$ |  |

[^42]Part 2.-Emissivity of a number of metals at their melting point ${ }^{35}$
( $c_{\lambda}$ expressed in percent)

| Metal | $\lambda=.55 \mu$ |  | $\lambda=.65 \mu$ |  | Metal | $\lambda=.55 \mu$ |  | $\lambda=\underbrace{65 \mu}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Solid | Liquid | Solid | Liquid |  | Solid | Liquid | Solid | Liquid |
| Beryllium | 61 | 81 | 61 | 61 | Niobium | 61 |  | 49 | 40 |
| Chromium | 53 |  | 39 | 39 | Palladium | 38 |  | 33 | 37 |
| Cobalt |  |  | 36 | 37 | Platinum | 38 |  | 33 | 38 |
| Copper | 38 | 36 | 10 | 15 | Rhodium |  |  | 29 | 30 |
| Erbium |  | 30 | 55 | 38 | Silver | <35 | < 35 | 4 | 7 |
| Gold | <38 | <38 | 14 | 22 | Thorium | 36 |  | 36 | 40 |
| Iridium |  |  | 30 |  | Titanium | 75 | 75 | 63 | 65 |
| Iron |  |  | 37 | 37 | Uranium | 77 |  | 54 | 34 |
| Manganese |  |  | 59 | 59 | Vanadium | 29 |  | 35 | 32 |
| Moly bdenum |  |  | 43 | 40 | Ytterbium |  |  | 35 | 35 |
| Nickel ...... |  | 46 | 36 | 37 | Zirconium | . |  | 32 | 30 |
| ${ }^{35}$ Internationa | ritical | Tables. |  |  |  |  |  |  |  |

TABLE 78.-NORMAL SPECTRAL EMISSIVITIES FOR SOME ELEMENTS AND ALLOYS (concluded)
Part 3.-Emissivities of tungsten ${ }^{*}$

| Tempera ture ${ }^{\circ} \mathrm{K}$ | Wavelength |  |  |  |  |  |  |  |  |  |  |  | Total emissivity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | . $30 \mu$ | . 38 | . 467 | . 665 | . 8 | 1.0 | 1.5 | 1.8 | 2.0 | 2.5 | 3.0 | 4.0 |  |
| 1200 | . 503 | . 495 | .483 | . 452 | . 428 | . 390 | . 275 | . 177 | . 148 | . 127 | . 116 | . 100 | . 138 |
| 1500 | . 502 | . 492 | . 476 | . +45 | . 422 | . 385 | . 280 | . 191 | . 164 | . 145 | . 132 | . 115 | . 192 |
| 1800 | . 500 | . 488 | . 472 | . 439 | . +17 | . 382 | . 284 | . 206 | . 180 | . 161 | . 148 | . 127 | . 236 |
| 2000 | . 498 | . 485 | . +69 | . 435 | . +14 | . 380 | . 287 | . 215 | . 191 | . 170 | . 158 | . 135 | . 259 |
| 2200 | .496 | .483 | . +66 | . +31 | . +10 | . 378 | . 290 | . 225 | . 201 | . 180 | . 167 | . 144 | . 278 |
| 2500 | .493 | . 477 | . +62 | . +25 | .405 | . 375 | . 295 | . 240 | . 217 | . 195 | . 180 | . 155 | . 301 |
| 2600 | .493 | . 476 | . +60 | .423 | . 403 | . 373 | . 297 | . $2+5$ | . 222 | . 200 | . 184 | . 159 | . 309 |
| 2700 | . 491 | . +75 | . +59 | .421 | . 401 | . 372 | . 298 | . 249 | . 228 | . 205 | . 188 | . 163 | . 315 |
| 2800 | .490 | . 473 | . +58 | . +19 | . 399 | . 371 | . 299 | . 254 | . 233 | . 210 | . 192 | . 167 | . 321 |
| 2900 | .489 | .472 | . 456 | . +17 | . 398 | . 370 | . 300 | . 259 | . 239 | . 215 | . 197 | . 170 | . 329 |
| 3000 | . 488 | .470 | . 455 | . +15 | . 396 | . 368 | . 302 | . 264 | . $2+5$ | . 230 | . 200 | . 173 | . 334 |
| 3200 | . 486 | . +68 | . +5 ? | . +11 | . 393 | . 366 | . 305 | . 273 | . 255 | .231 | . 208 | . 180 | . 341 |
| 3400 | .484 | . 465 | . 450 | . 407 | . 388 | . 363 | . 308 | . 283 | . 265 | . $2+1$ | . 216 | . 186 | . 348 |

${ }^{30}$ Forsythe, WY. E., and Adims, E. Q., Journ. Opt. Soc. Imer., vol. 35, p. 108, 1945.

For $\lambda=1.27 \mu$ the spectral emissivity is constant and equals 0.335 .
Part 4.-Emissivities of some metals specially prepared by heat-treating and out-gassing ${ }^{37}$

| Element | $\lambda$ in $\mu$ | Emissivity | Tempera- ture ${ }^{\circ} \mathrm{K}$ | Flement | $\lambda$ in $\mu$ | Emissivity | $\begin{aligned} & \text { Tempera- } \\ & \text { ture } \\ & \circ \mathrm{K} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Chromium | . 66 | . 334 | 1050-1560 | Palladium |  | . 311 | 1200-1400 |
| Cobalt |  | . 327 | 1240-1378 |  |  | . 291 | 1200-1400 |
|  |  | . 342 | 1378-1450 | Platinum |  | .295-. 310 | 1200-1800 |
| Iron a |  | . 344 | below 1178 | Rhodium |  | . 242 | 1300-2000 |
| $\gamma$ |  | . 325 | 1178-1677 | Tantalum |  | .439-. 384 | 1200-2400 |
| $\delta$ |  | . 337 | 1677-1725 | Thorium |  | . 380 | 1300-1700 |
| Molybdenum |  | . 382 | 1300-2100 | Tungsten |  | . 46 | 12002200 |
| Nickel |  | . 350 | 1200-1400 | Uranium | . 6605 | . 453 | 1180-1320 |
| Niobium |  | . 374 | 1300-2200 |  |  | . 416 | 1325-1370 |

[^43]TABLE 79.-CORRECTIONS IN ${ }^{\circ} \mathrm{C}$ TO ADD TO BRIGHTNESS TEMPERATURE READINGS, FOR DIFFERENT EMISSIVITY, TO OBTAIN THE TRUE TEMPERATURE *

Pyrometer using red light, wavelength, $\lambda=.665 \mu$. and $c_{2}=14380 \mu{ }^{\circ} \mathrm{K}$ at observed
temperatures degrees Kelvin, of

| Emissivity | temperatures degrees Kelvin, of |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1000 | 1100 | 1200 | 1300 | 1400 | 1500 | 1600 | 1700 | 1800 |
| . 10 | 119.2 | 145.9 | 175.8 | 208.9 | 245.3 | 285.1 | 328.6 | 375.7 | 426.8 |
| . 20 | 80.4 | 98.1 | 117.7 | 139.3 | 162.8 | 188.5 | 216.3 | 246.2 | 278.4 |
| . 30 | 59.0 | 71.8 | 85.9 | 101.4 | 118.3 | 136.7 | 156.5 | 177.7 | 200.5 |
| . 40 | 44.2 | 53.8 | 64.3 | 75.8 | 88.3 | 101.8 | 116.4 | 132.0 | 148.6 |
| . 50 | 33.1 | 40.2 | 48.0 | 56.5 | 65.8 | 75.8 | 86.5 | 98.0 | 110.2 |
| . 60 | 24.2 | 29.3 | 35.0 | 41.2 | 47.9 | 55.1 | 62.9 | 71.1 | 79.9 |
| . 70 | 16.8 | 20.3 | 24.2 | 28.5 | 33.1 | 38.0 | 43.4 | 49.0 | 55.1 |
| . 80 | 10.4 | 12.6 | 15.1 | 17.7 | 20.5 | 23.6 | 26.9 | 30.3 | 34.1 |
| . 85 | 7.5 | 9.3 | 10.9 | 12.6 | 14.9 | 17.1 | 19.5 | 22.0 | 24.7 |
| . 90 | 4.9 | 5.9 | 7.1 | 8.3 | 9.6 | 11.0 | 12.6 | 14.2 | 15.9 |
| . 95 | 2.4 | 2.9 | 3.4 | 4.0 | 4.7 | 5.3 | 6.1 | 6.9 | 7.7 |

[^44]TABLE 79.-CORRECTIONS IN ${ }^{\circ} \mathrm{C}$ TO ADD TO BRIGHTNESS TEMPERATURE READINGS, FOR DIFFERENT EMISSIVITY, TO OBTAIN THE TRUE TEMPERATURE (concluded)

| Emissivity | Pyrometer using red light, wavelength, $\lambda=.665 \mu$, and $c_{2}=14380 \mu{ }^{\circ} \mathrm{K}$ at olserved temperatures degrees Kelvin, of |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1900 | 2000 | 2200 | 2400 | 2600 | 2800 | 3000 | 3600 |
| . 10 | 481.9 | 541.2 | 673.0 | 823.9 | 995.2 | 1189.5 | 1408.3 | 2237.8 |
| . 20 | 312.9 | 349.8 | 430.7 | 521.9 | 623.8 | 737.2 | 862.5 | 1317.6 |
| . 30 | 224.8 | 250.6 | 307.0 | 370.1 | 440.0 | 517.2 | 601.6 | 902.4 |
| . 40 | 166.3 | 185.2 | 226.1 | 271.7 | 330.4 | 377.0 | 436.9 | 648.0 |
| . 50 | 123.2 | 137.0 | 166.9 | 200.0 | 236.4 | 276.1 | 319.2 | 469.6 |
| . 60 | 89.3 | 99.2 | 120.6 | 144.2 | 170.1 | 198.3 | 228.9 | 334.6 |
| . 70 | 61.5 | 68.2 | 82.8 | 98.9 | 116.5 | 135.6 | 156.2 | 227.2 |
| . 80 | 38.0 | 42.1 | 51.1 | 60.9 | 71.6 | 83.3 | 95.9 | 138.9 |
| . 85 | 27.5 | 30.5 | 37.0 | 44.1 | 51.8 | 60.2 | 69.2 | 100.1 |
| . 90 | 17.7 | 19.7 | 23.8 | 28.4 | 33.3 | 38.7 | 44.5 | 64.2 |
| . 95 | 8.6 | 9.5 | 11.5 | 13.7 | 16.1 | 18.7 | 21.5 | 31.0 |

TABLE 80.-COMPUTATION OF TOTAL EMISSIVITY VALUES FOR VARIOUS
GLASS SAMPLES AT LOW TEMPERATURES ${ }^{* 8}$

| Sampie | Thickness (mm) | Apparent emissivity * |  |  | Computed transmittance $\dagger$ |  |  | Temperature differential $\ddagger$ |  |  | Corrected emissivity |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }^{5}{ }^{\circ} \mathrm{C}$ | $\begin{aligned} & 320 \\ & { }^{\circ} \mathrm{C} \end{aligned}$ | ${ }^{10}{ }^{100} \mathrm{C}$ | 500 | 320 | 100 | 500 | 320 | 100 | 475 | $\underbrace{}_{320}$ | 100 |
| Fused quartz | 1.96 | . 78 | . 80 | . 75 | . 266 | . 134 | . 023 | 19 | 8 | 1 | . 67 | . 76 | . 775 |
| Corex D | 3.40 | . 80 | . 80 | . 76 | . 113 | . 041 | . 002 | 49 | 18 | 2 | . 91 | . 90 | . 83 |
| Nonex | 1.57 | . 82 | . 82 | . 78 | . 145 | . 041 | . 004 | 31 | 12 | 1.5 | . 82 | . 87 | . 835 |

Dissipating of energy by lamp bulbs.-The bulb of a 120 -volt 500 -watt lamp dissipates 18.5 percent of the input energy to the lamp. About 10 percent is lost by radiation and 8.5 percent by conduction and convection by the surrounding air. The losses from other similar lamp bulbs probably agree with this.

[^45]
## TABLE 81.-RELATIVE EMISSIVITIES FOR TOTAL RADIATION

Emissive power of blackbody $=1$. Receiving surface platinum black at $25^{\circ} \mathrm{C}$; oxidized at $600+{ }^{\circ} \mathrm{C}$.

|  | Temperature, ${ }^{\circ} \mathrm{C}$ |  |  |
| :---: | :---: | :---: | :---: |
|  | 200 | 400 | 600 |
| Silver | . 020 | . 030 | . 038 |
| Platinum (1) | . 060 | . 086 | . 110 |
| Oxidized zinc |  | . 110 |  |
| Oxidized aluminum | . 113 | . 153 | . 192 |
| Calorized copper, oxidized. | . 180 | . 185 | . 190 |
| Cast iron | . 210 |  |  |
| Oxidized nickel | . 369 | . 424 | . 478 |
| Oxidized monel | . 411 | . 439 | . 463 |
| Calorized steel, oxidized. | . 521 | . 547 | . 570 |
| Oxidized copper | . 568 | . 568 | . 568 |
| Oxidized brass. | . 610 | . 600 | . 589 |
| Oxidized lead | . 631 |  |  |
| Oxidized cast iron. | . 643 | . 710 | . 777 |
| Oxidized steel | . 790 | . 788 | . 787 |

For radiation properties of bodies at temperatures so low that the radiations of wavelength greater than $20 \mu$ or thereabouts are important, doubt must exist because of the possible and perhaps probable lack of blackness of the receiving body to radiations of those wavelengths or greater. For instance, see Tables 568 and 573 for the trarsparency of soot.

TABLE 82.-TOTAL EMISSIVITY VALUES OF VARIOUS MATERIALS AT LOW TEMPERATURES *

| Material | Condition | At $100^{\circ} \mathrm{C}$ | $320^{\circ} \mathrm{C}$ | $500^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: |
| Alleghany alloy No. | Polished | . 11 |  |  |
| Alleghany metal . . | No. 4 polish | . 13 |  |  |
| Aluminum | Commercial sheet | . 09 |  |  |
| Aluminum | Polish | . 095 |  |  |
| Aluminum | Rough polish | . 18 |  |  |
| Aluminum paint |  | . 29 |  |  |
| Brass | Polished | . 059 |  |  |
| Carbon | Rough plate | . 77 | . 77 | . 72 |
| Carbon, graphitized | Rough plate | . 76 | . 75 | . 71 |
| Chromium | Polished | . 075 |  |  |
| Copper | Polished | . 052 |  |  |
| Copper-nickel | Polished | . 059 |  |  |
| Iron | Dark gray surface | . 31 |  |  |
| Iron | Roughly polished | . 27 |  |  |
| Lamp black | Rough deposit | . 84 |  | . 78 |
| Molybdenum | Polished | . 071 |  |  |
| Nickel | Polished | . 072 |  |  |
| Nickel-silver | Polished | . 135 |  |  |
| Radiator paint, black |  | . 84 |  |  |
| Radiator paint, bronze |  | . 51 |  |  |
| Radiator paint, cream |  | . 77 |  |  |
| Radiator paint, white |  | . 79 |  |  |
| Silver ............. | Polished | . 052 |  |  |
| Stainless steel | Polished | . 074 |  |  |
| Steel | Polished | . 066 |  |  |
| Tin | Polished | . 069 |  |  |
| Tin | Commercial coat | . 084 |  |  |
| Tungsten | Polished coat | . 066 |  |  |
| Zinc . | Commercial coat | . 21 |  |  |

* For reference, see footnote 38, p. 100.

TABLE 83.-PERCENTAGE EMISSIVITIES OF METALS AND OXIDES

| True temperature ${ }^{\circ} \mathrm{C}$ | 500 | 600 | 700 | 800 | 900 | 1000 | 1100 | 1200 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $60 \mathrm{FeO} .40 \mathrm{Fe}_{2} \mathrm{O}_{3}$ Total | 85 | 85 | 86 | 87 | 87 | 88 | 88 | 89 |
| in air......... $\lambda=.65 \mu$ | - | - | - | 98 | 97 | 95 | 93 | 92 |
| NiO . . . . . . . . . . . . . Total | - | 54 | 62 | 68 | 72 | 75 | 81 | 86 |
| .............. $\lambda=$. $65 \mu$ | - | - | 98 | 96 | 94 | 92 | 88 | 87 |

Platinum:

| True temp. ${ }^{\circ} \mathrm{C} .$. | 0 | 100 | 200 | 300 | 400 | 500 | 750 | 1000 | 1200 | 1400 | 1600 | 1700 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| App. ${ }^{*}$ temp. ${ }^{\circ} \mathrm{C} \ldots$ | - | - | - | - | - | - | - | 486 | 630 | 780 | 930 | 1005 |
| Total emiss. Pt.. | 31 | 4.0 | 5.1 | 6.1 | 7.0 | 8.0 | 10.3 | 12.4 | 14.0 | 15.5 | 16.9 | 17.5 |


| Oxides: $\quad \lambda=.65 \mu$ | NiO | $\mathrm{Co}_{3} \mathrm{O}_{4}$ | $\mathrm{Fe}_{3} \mathrm{O}_{4}$ | $\mathrm{Mn}_{3} \mathrm{O}_{4}$ | $\mathrm{TiO}_{2}$ | $\mathrm{ThO}_{2}$ | $\mathrm{Y}_{2} \mathrm{O}_{3}$ | BeO | $\mathrm{NhO}_{x}$ | $\mathrm{~V}_{2} \mathrm{O}_{3}$ | $\mathrm{Cr}_{2} \mathrm{O}_{3}$ | $\mathrm{r}_{3} \mathrm{O}_{3}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Solid | $\ldots \ldots \ldots \ldots$ | 89 | 77 | 63 | $\ldots$ | 52 | 57 | 61 | 37 | 71 | 69 | 60 | 30 |
| Liquid | $\ldots \ldots \ldots$ | 68 | 63 | 53 | 47 | 51 | 69 | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 31 |

[^46]TABLE 84.-TOTAL RADIATION FROM BARE AND SOOT.COVERED NICKEL ${ }^{3}$ (watts/cm ${ }^{2}$ )

| ${ }^{\circ} \mathrm{K}$ | 400 | 500 | 600 | 700 | 800 | 900 | 1000 | 1200 | 1400 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Soot-covered Ni | . 096 | . 28 | . 59 | 1.87 | 3 | 3 | 4.8 |  |  |
| Polished Ni initial heat.. | . 0092 | . 032 | . 079 | . 166 | . 31 | . 55 | . 91 | 2.17 | 4.49 |
| " after above.. | . 0066 | . 023 | . 058 | . 123 | . 24 | . 44 | . 76 | 2.04 | 4.49 |

TABLES 85-102.-CHARACTERISTICS OF SOME LIGHT-SOURCE MATERIALS, AND SOME LIGHT SOURCES


TABLE 86.—RADIATION AND OTHER PROPERTIES OF TANTALUM *1

| ${ }^{\circ} \mathrm{K}$ | Emissivity |  | $\mathrm{Temperature}^{\text {a }}$ |  |  | Resistivity <br> $\mu$-ohmcm | Radiation watt/ $\mathrm{cm}^{2}$ | $\frac{T d n}{n d T}$ | Total emissivity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Bright- |  |  |  |  |  |  |
|  | . $665 \mu$ | . $463 \mu$ | $\begin{aligned} & \text { ness } \\ & .665 \mu \end{aligned}$ | Color ${ }^{\circ} \mathrm{K}$ | tion - K |  |  |  |  |
| 300 | . 493 | . 56 |  |  |  |  |  |  |  |
| 1000 | . 459 | . 52 | 966 |  |  |  |  | ... | . |
| 1200 | . 450 | . 51 | 1149 |  | .... | . . . |  |  | . . . |
| 1400 | . 442 | . 50 | 1329 |  |  |  |  |  |  |
| 1600 | . 434 | . 49 | 1506 | 1642 | 1062 | 67.6 | 7.3 | 4.80 | . 194 |
| 1800 | . 426 | . 48 | 1680 | 1859 | 1222 | 74.1 | 12.8 | 4.80 | . 213 |
| 2000 | . 418 | . 47 | 1851 | 2075 | 1390 | 80.5 | 21.2 | 4.80 | . 232 |
| 2200 | . 411 | . 46 | 2018 | 2288 | 1556 | 86.9 | 33.4 | 4.80 | . 251 |
| 2400 | . 404 | . 45 | 2180 | 2497 | 1730 | 92.9 | 50.7 | 4.80 | . 269 |
| 2600 | . 397 | . 44 | 2339 | 2705 | 1901 | 99.1 | 75 | 4.80 | . 287 |
| 2800 | . 390 |  | 2495 | 2911 | 2080 | 105.0 | 106 | 4.80 | . 304 |
| 3000 | . 384 |  | 2647 |  |  |  | .... |  |  |
| 3300 mp | . 375 |  | 2870 |  |  |  |  |  |  |

${ }^{41}$ Worthing, A. G., Phys. Rev., vol. 28, p. 190, 1926.

TABLE 87.-RADIATION AND OTHER PROPERTIES OF MOLYBDENUM *

| ${ }^{\circ} \mathrm{K}$ | $\overbrace{\text { Emissivity }}$ |  | Temperature |  |  | Resistivity $\mu$-ohmcm | $\begin{gathered} \text { Bright- } \\ \text { ness } \\ \text { normally } \\ \text { candles } \\ \mathrm{cm}^{2} \end{gathered}$ | $\begin{aligned} & \text { Radia- } \\ & \text { tion } \\ & \text { in- } \\ & \text { tensity } \\ & \text { watts/ } \\ & \mathrm{cm}^{2} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{gathered} \text { Bright- } \\ \begin{array}{c} \text { ness } \\ S_{. \operatorname{ses} \mu \mu} \\ { }^{\circ} \mathrm{K} \end{array} \end{gathered}$ | $\begin{gathered} \text { Color } \\ { }^{\circ} \mathrm{K} \end{gathered}$ | $\begin{aligned} & \text { Radia- } \\ & \text { tion } \\ & \circ \mathrm{K} \end{aligned}$ |  |  |  |  |
|  | . $665 \mu$ | . $475 \mu$ |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| 273 | . 420 | . 425 |  |  |  | 5.14 |  |  |  |
| 1000 | . 390 | . 403 | 958 | 1004 | 557 | 23.9 | . 0001 | . 55 |  |
| 1400 | . 375 | . 393 | 1316 | 1411 | 864 | 35.2 | . 089 | 3.18 | . 093 |
| 1600 | . 367 | . 388 | 1489 | 1616 | 1024 | 41.1 | . 765 | 6.30 | . 40 |
| 1800 | . 360 | . 383 | 1658 | 1823 | 1187 | 47.0 | 4.13 | 11.3 | 1.22 |
| 2000 | . 353 | . 379 | 1824 | 2032 | 1354 | 53.1 | 15.9 | 19.2 | 2.75 |
| 2200 | . 347 | . 375 | 1986 | 2244 | 1523 | 59.2 | 48.5 | 30.7 | 5.28 |
| 2400 | . 341 | . 371 | 2143 | 2456 | 1693 | 65.5 | 123 | 47.0 | 8.70 |
| 2600 | . 336 | . 368 | 2297 | 2672 | 1866 | 71.8 | 270 | 69.5 | 13.0 |
| 2800 | . 331 | . 365 | 2448 | 2891 | 2039 | 78.2 | 540 | 98 | 18.4 |
| 2895 | . 328 | . 363 | 2519 | 2997 | 2122 | 81.4 | 730 | 116 |  |

*For reference, see footnote 41, above.

TABLE 88.-RELATION BETWEEN BRIGHTNESS TEMPERATURE AND COLOR TEMPERATURE FOR VARIOUS SUBSTANCES

| Brightness temperature | Corresponding color temperature for- |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Untreated carbon | Gem | Platinum | Nernst glower | Osmium | Tantalum | Tungsten |
| $1400^{\circ} \mathrm{K}$ | 1414 |  | $1568{ }^{\circ} \mathrm{K}$ | 1538 | 1444 | 1507 | 1492 |
| 1500 | 1515 |  | 1692 | 1642 | 1562 | 1631 | 1607 |
| 1600 | 1616 | 1620 | 1821 | 1747 | 1680 | 1758 | 1723 |
| 1700 | 1718 | 1735 | 1952 | 1852 | 1799 | 1883 | 1841 |
| 1800 | 1820 | 1852 | 2086 | 1954 | 1919 | 2010 | 1961 |
| 1900 | 1923 | 1962 |  | 2053 | 2045 | 2137 | 2082 |
| 2000 | 2028 | 2064 |  | 2146 | 2168 | 2265 | 2206 |
| 2200 | 2240 | 2255 | . . . | 2310 | 2427 | 2500 | 2457 |
| 2400 |  |  |  |  | 2688 | 2785 | 2718 |
| 2600 |  | .... |  |  |  |  | 2988 |
| 3000 |  |  |  | . . . |  |  | 3564 |

TABLE 89.-COLOR MINUS BRIGHTNESS TEMPERATURE FOR CARBON

| Brightness temp. ${ }^{\circ} \mathrm{K} \ldots$ | $1600^{\circ}$ | $1700^{\circ}$ | $1800^{\circ}$ | $1900^{\circ}$ | $2000^{\circ}$ | $2100^{\circ}$ | $2200^{\circ}$ |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Color-brightness | $\ldots \ldots$ | 2 | 7 | 12 | 16 | 22 | 28 | 33 |

## TABLE 90.-RELATIVE BLUE BRIGHTNESS, B, AND BRIGHTNESS IN CANDLES PER $C^{2}{ }^{2} \mathrm{C}$, OF SOME INCANDESCENT OXIDES AT VARIOUS RED $(0.665 \mu)$ BRIGHTNESS TEMPERATURES, $S_{\lambda}$



TABLE 91.-COLOR TEMPERATURE, BRIGHTNESS TEMPERATURE, AND BRIGHTNESS OF VARIOUS ILLUMINANTS

| Source | $T$ 。 | $S(\lambda=.665)$ | Brightness $\mathrm{c} / \mathrm{cm}^{2}$ |
| :---: | :---: | :---: | :---: |
| Gas flame: |  |  |  |
| Batswing | 2160 |  |  |
| Candle shape about 1 | 1875 |  |  |
| Hefner as a whole... | 1880 |  |  |
| Candle: |  |  |  |
| Sperm | 1930 |  |  |
| Paraffin | 1925 |  |  |
| Pentane 10-cp. std. | 1920 |  |  |
| Kerosene: |  |  |  |
| Flat wick | 2055 | : 500 | 1.27 |
| Round wick | 1920 | 1530 | 1.51 |
| 4 wpc carbon. | 2080 | 2030 | 54.9 |
| 3.1 wpc treated carbon | 2165 | 2065 | 70.6 |
| 2.5 wpc gem. | 2195 | 2130 | 78.1 |
| 2 wpc osmium. | 2185 | 2035 | 60.8 |
| 2 wpc tantalum | 2260 | 2000 | 53.1 |
| Acetylene as a whole. | 2380 |  |  |
| One spot | 2465 | 1660 | 6.69 |
| Mees burner | 2360 | 1730 | 10.8 |
| 1.25 wpc tungsten. | 2400 | 2150 | 125 |
| 2.3 wpc Nernst. | 2400 | 2320 | 258 |
| Sun: |  |  |  |
| Outside atmosphere | 6500 |  | 224000 |
| At earth's surface... | 5600 |  | 165000 |
| Clear sky |  |  | . 4 |
| Moon |  |  | . 5 |
| Welsbach mantle |  |  | 9.0 |

Low intensity and high intensity carbon arcs

| Positive carbon | Amperes | Arc $\dagger$ volts | Lumens per are watt |
| :---: | :---: | :---: | :---: |
| Low-intensity carbons |  |  |  |
| 10 mm low intensity. | 20 | 55 | 14.9 |
| 12 | 32 | 55 | 15.7 |
| 13 " " | 40 | 55 | 16.3 |
| High-intensity projection carbons 30 |  |  |  |
| 6 mm "suprex".... | 40 | 37 | 28.6 |
| 7 " " | 50 | 37 | 29.7 |
| 8 " | 70 | 40 | 34.6 |
| 9 " rotating positive | 85 | 58 | 26.4 |
| 11 " " " | 115 | 55 | 32.5 |
| 13.6 " | 125 | 68 | 27.0 |
| " " " | 150 | 78 | 35.0 |
| " " | 170 | 75 | 33.6 |
| 16 " | 225 | 75 | 32.2 |
| High-intensity searchlight carbons |  |  |  |
| 10 mm rotating positive | 100 | 75 | 32.3 |
| 12 " " | 120 | 75 | 33.0 |
| 16 " " | 150 | 78 | 32.0 |
| 16 " " | 195 | 90 | 31.5 |

Vertical trim ac and dc flame arcs

| Carbons |  | Amperes | $\begin{gathered} \text { Arc } \\ \text { volts } \end{gathered}$ | Upper polarity | Lumens per arc watt |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Upper | Lower |  |  |  |  |
| $\frac{1}{2}^{\prime \prime}$ WF | $\frac{1}{2}^{\prime \prime}$ WF |  |  | $+$ |  |
| Photo $\ddagger$ | Photo $\ddagger$ | 40 | 55 ac | - | 39 |
| " | " | 40 | 55 dc | $+$ | 55 |
| " | " | 40 | 55 dc | - | 50 |
| $\frac{1}{2}{ }^{\prime \prime} 2 \mathrm{~F}$ § | " | 40 | 55 dc | - | 44 |
| Alternating-current high-intensity carbon arcs |  |  |  |  |  |
| Carbon |  |  | Arc volts |  | Lumens per arc watt |
| 7 mm |  |  | 26 ac |  | 60.5 |
| 8 mm |  |  | 29 ac |  | 61.5 |
| 9 mm |  |  | 26 ac |  | 68.5 |

[^47]
## TABLE 93.-EFFICIENCIES OF SOME EARLY INCANDESCENT LAMPS OF ABOUT 60-WATT SIZE ${ }^{42}$

|  | Lumens per watt | Life |
| :---: | :---: | :---: |
| Edison's early carbon lamp | 1.8 | 600 hr |
| Treated carbon lamp. | 3.2 | 600 |
| Gem lamp | 4.0 | 600 |
| Nernst glower | 5.0 | 600 |
| Tantalum lamp | 4.9 | 900 |
| Osmium lamp | 4.9 |  |
| Tungsten lamp (1907) | 7.8 | 1,000 |
| Tungsten lamp (1949) coiled | 14.0 | 1,000 |

[^48]TABLE 94.-INCREASE IN TUNGSTEN LAMP EFFICIENCY OVER A PERIOD OF YEARS

| Lamp | Date measured | Temperature ${ }^{\circ} \mathrm{K}$ | Efficiency in lumens per watt |
| :---: | :---: | :---: | :---: |
| 100-watt squirted filament | 1908 † | 2,355 | 8.8 |
| 100-watt drawn wire | $1909 \dagger$ | 2,360 | 9.3 |
| 100-watt drawn wire | 1915 † | 2,475 | 10.3 |
| 100-watt gas-filled | 1921 | 2,740 | 12.6 |
| 100 -watt gas-filled | 1932 | 2,800 | 14.3 |
| 100-watt gas-filled | 1936 | 2,845 | 14.9 |
| 100-watt gas-filled * | 1936 | 2,855 | 15.5 |
| 100-watt gas-filled * coiled coil. | 1948 | 2,860 | 16.3 |
| * 750 hours life. † Vacuum lamps. |  |  |  |

TABLE 95.-TEMPERATURE AND EFFICIENCY OF SOME TUNGSTENFILAMENT LAMPS *


| 10 kw. | 120 | 23.3 | 10,000 | 280,000 | 28 | 3300 | 33,000 |
| :--- | :--- | :--- | :--- | ---: | ---: | ---: | ---: |
| 50 kw. | 120 | 416 | 50,000 | $1,400,000$ | 28 | 3300 | 166,000 |

[^49]TABLE 95.-TEMPERATURE AND EFFICIENCY OF SOME TUNGSTEN. FILAMENT LAMPS (concluded)

Lamp for type B Kodachrome


TABLE 96.—SOME CHARACTERISTICS OF FLUORESCENT CHEMICALS *

| Phosphor | $\underset{\substack{\text { Lamp } \\ \text { color }}}{\text { Lem }}$ | Exciting range, $\uparrow$ | Sensitivity peak, | Emitted range, | Emitted peak, |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Calcium tungstate | blue | 2200-3000 | 2720 | 3100-7000 | 4400 |
| Magnesium tungstate | blue-white | 2200-3200 | 2850 | 3600-7200 | 4800 |
| Zinc silicate ............ | green | 2200-2960 | 2537 | 4600-6400 | 5250 |
| Calcium halophosphates.. | white | 2000-2600 | 2500 | 3500-6800 | 4800, 5800 |
| Cadmium silicate ....... | yellow-pink | 2200-3200 | 2400 | 4800-7400 | 5950 |
| Cadmium borate ......... | pink | 2200-3600 | 2500 | 5200-7500 | 6150 |
| BL phosphor $\mathrm{BaSi}_{2} \mathrm{O}_{5}$ with $\mathrm{Pb} \quad$.................... | blue ultra | 2200-2700 | 2500 | 3100-4100 | 3500 |
| Calcium phosphate with Ce and Mn............ |  | 2200-3400 | 3130 | $\begin{aligned} & 5600-8100 \\ & \text { plus UV } \end{aligned}$ | 6500 |

[^50]TABLE 97.-ENGINEERING DATA ON SOME LAMPS OF THE INTEGRAL, ALL-GLASS SEALED BEAM TYPE*


[^51]TABLE 98.-MERCURY ARCS *


[^52]| Dimensions，electrical data |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal lamp |  |  |  |  |  | 15 | 15 |  |  |  | 40 | 40 |  |  |
|  | 4 | 6 | 8 | 13 | 14 | （T－8） | （T－12） | 20 | 25 | 30 | （T－12） | （T－17） | 85 | 100 |
| Nom．length |  | 9＂ | 12＂ | $21^{\prime \prime}$ | 15＂ | 18＂ | 18＂ | $24^{\prime \prime}$ | 33＂ | 36＂ | 48＂ | 60＂ | 60＂ | 60＂ |
| Diameter ． | $\frac{8}{8 \prime \prime}$ | $\frac{5}{8 \prime \prime}$ | 知＂ | $8^{\prime \prime}$ | $1{ }^{\prime \prime}$ | 1 | $11^{\prime \prime}$ | $1^{\prime \prime}{ }^{\prime \prime}$ | $1{ }^{\prime \prime \prime}$ | 1 | 12＂ | 21 ＂＇ | $21^{\prime \prime}$ | $21^{\prime \prime}$ |
| Bulb ．．． |  | T－5 | T－5 | T－5 | T－12 | T． 8 | T－12 | T－12 | T－12 | T－8 | T． 12 | T－17 | T－17 | T－17 |
| Lamp amps \＄ |  | ． 145 | ． 16 | ． 16 | ． 395 | ． 31 | ． 33 | ． 36 | ． 52 | ． 355 | ． 42 | ． 40 | 1.6 | 1.50 |
| Lamp volts 8 | 36 | 48 | 57 | 100 | 38 | 55 | 46 | 59 | 53 | 98 | 106 | 110 | 57 | 71 |


| Lumen output and brightness－4500 white lamps｜｜ |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lumens | 200 | 310 | 545 | 460 | 585 | 555 | 860 | 1380 | 2100 | 2100 | 4000 | 4000 |
| Lumens／watt | 33 | 39 | 42 | 33 | 39 | 37 | 43 | 46 | 53 | 53 | 47 | 40 |
| Brightness： |  |  |  |  |  |  |  |  |  |  |  |  |
| Footlamberts | 2500 | 2770 | 2520 | 1310 | 1980 | 1250 | 1360 | 2120 | 1610 | 920 | 1760 | 1760 |
| Candles／in．${ }^{2}$ | 5.5 | 6.1 | 5.6 | 2.9 | 4.4 | 2.8 | 3，0 | 4.7 | 3.6 | 2.0 | 3.9 | 3.9 |

4500 white slimline lamps for multiple operation

| Nominal length， inches | Dim． inches | Bulb | Lamp current， Ma | Nominal lamp watts | Lamp volts | Rec．min． starting voltage | Footlamberts and （candles／in．${ }^{2}$ ） | Lumen output and lpw |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 42 | $\frac{9}{4}$ | T－6 | $\begin{aligned} & 120 \\ & 200 \end{aligned}$ | 18 25 | 175 150 | 450 | $1570(3.5)$ | $990(55)$ $320(53)$ |
|  |  |  | 300 | 33 | 130 |  | 2570 （5．7） | 1620（49） |
| 64 | $\frac{3}{4}$ | T－6 | 120 | 27.5 | 270 | 600 | 1580 （3．5） | 1570（57） |
|  |  |  | 200 | 39 | 230 |  | 2170（4．8） | 2150（55） |
|  |  |  | 300 | 51 | 200 |  | 2620（5．8） | 2600（57） |
| 72 | 1 | T－8 | 120 | 26 | 240 | 600 | 1200（2．7） | 1590（61） |
|  |  |  | 200 | 38 | 220 |  | 1700 （3．8） | 2250（59） |
|  |  |  | 300 | 51 | 200 |  | 2200 （4．9） | 2850（56） |
| 96 | 1 | T－8 | 120 | 34 | 320 | 750 | 1200 （2．7） | 2100（62） |
|  |  |  | 200 | 51 | 295 |  | $1700(3.8)$ | 3050 （60） |
|  |  |  | 300 | 69 | 265 |  | 2200（4．9） | 3950（57） |

[^53]TABLE 100．—CHARACTERISTICS＊OF TYPICAL PHOTOFLASH LAMPS

|  |  |  |  |  |  |  |  | 合 |  | \％ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fast | SM | 3 | 6 | 7 | $4.7 \pm$ | ． 908 | 3300 | B11 | $2{ }^{3}$ | S．S．Bay |
|  | SF | 3－9 | 6 | 5 | 5.0 | ． 80 | 3400 | B12 | $2{ }^{\frac{3}{8}}$ | S．C．Bay |
| Medium | 5 | 3 | 21 | 13 | 16 | 1.2 | 3800 | B11 | $2{ }^{\text {s }}$ | S．C．Bay |
|  | Press 25 | 3－9 | 20 | 14 | 20 | 1.25 | 4000 | B12 | 23 | S．C．Bay |
|  | 0 | 3－125 | 20 | 14 | 20 | 1.2 | 4000 | S13 | $3{ }^{\text {d }}$ | Medium |
|  | 11 | 3 | 21 | 13 | 30 | 1.8 | 3800 | A15 | 4 | Medium |
|  | Press 40 | 3－125 | 20 | 17 | 30 | 1.6 | 4000 | A15 | 315 | Medium |
|  | 22 | 3－125 | 21 | 14 | 63 | 4.0 | 3800 | A19 | 5 | Medium |
|  | 2 | 3－125 | 20 | 18 | 62 | 3.0 | 4000 | A19 | $4 \frac{3}{4}$ | Medium |
| Slow | 50 | 3－125 | 30 | 17 | 95 | 5.0 | 3800 | A21 | $5 \frac{3}{8}$ | Medium |
|  | 3 | 3－125 | 30 | 18 | 110 | 5.0 | 4000 | A23 | $6{ }^{\frac{5}{8}}$ | Medium |
| Focal plane | 6 |  |  | 30 | 16 | ． 62 | 3800 | B11 | 2 2 | S．C．Bay |
|  | 26 |  |  | 24 | 15 | ． 60 | 3800 |  |  | S．C．Bay |
|  | 31 | 3 | $\cdots$ | 53 | 77 | 1.5 | 3800 | A21 | $5{ }^{\frac{3}{8}}$ | Medium |
|  | 2A | 3－9 | $\cdots$ | 64 | 77 | 1.0 | 4000 | A21 | $5 \frac{8}{8}$ | Medium |
| Blue for color photography | 5B | 3 | 21 | 13 | 7.5 | ． 55 | 6000 | B11 | $2 \frac{5}{8}$ | S．C．Bay |
|  | Press 25B | 3－9 | 20 | 14 | 8.0 | ． 50 | 6000 | B12 | 2 2 | S．C．Bay |
|  | 118 |  | 21 | 14 | 13.0 | ． 82 | 6000 |  |  |  |
|  | Press 40B |  | 20 | 17 | 14 | ． 75 | 6000 |  |  |  |
|  | 22B | 3－125 | 21 | 14 | 29 | 1.8 | 6000 | A19 | 5 | Medium |
|  | 2B | 3－125 | 20 | 18 | 28 | 1.35 | 6000 | A19 | $4{ }^{3}$ | Medium |
|  | 50B | 3－125 | 30 | 17 | 43 | 2.3 | 6000 | A21 | $5{ }^{\frac{3}{8}}$ | Medium |
|  | 3B | 3－125 | 30 | 18 | 50 | 2.25 | 6000 | A23 |  | Medium |

[^54]TABLE 101.-PHYSICAL AND ELECTRICAL CHARACTERISTICS OF FLASHTUBES AND FLASHLAMPS DESIGNED PRIMARILY FOR PHOTOGRAPHIC APPLICATIONS


[^55]TABLE 102.-COLOR OF LIGHT EMITTED BY VARIOUS SOURCES

| Source | Color, percent white white | Hue | Source | Color, percent white | Hue |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Sunlight | 100 |  | N -filled tungsten, .50 wpc. | 45 | 584 |
| Average clear sky | 60 | 472 | N-filled tungsten, 35 wpc. | 53 | 584 |
| Standard candle | 13 | 593 | Mercury vapor arc. | 70 | 490 |
| Hefner lamp | 14 | 593 | Helium tube | 32 | 598 |
| Pentane lamp | 15 | 592 | Neon tube | 6 | 605 |
| Tungsten glow lamp, 1.25 wpc. | 35 | 588 | Crater of carbon arc, 1.8 amp . | 59 | 585 |
| Carbon glow lamp, 3.8 wpc.... | 25 | 592 | Crater of carbon arc, 3.2 amp . | 62 | 585 |
| Nernst glower, 1.50 wpc | 31 | 587 | Crater of carbon arc, 5.0 amp . | 67 | 583 |
| N -filled tungsten, 1.00 wpc . | 34 | 586 | Acetylene flame (flat)....... | 36 | 586 |

## TABLES 103-110.-COOLING BY RADIATION AND CONVECTION

## TABLE 103.-AT ORDINARY PRESSURES

According to McFarlane the rate of loss of heat by a sphere placed in the center of a spherical enclosure which has a blackened surface, and is kept at a constant temperature of about $14^{\circ} \mathrm{C}$, can be expressed by the equations

$$
c=.000238+3.06 \times 10^{-6} t-2.6 \times 10^{-8} t^{2}
$$

when the surface of the sphere is blackened. or

$$
\varepsilon=.000168+1.98 \times 10^{-8} t-1.7 \times 10^{-8} t^{2},
$$

when the surface is that of polished copper. In these equations, $e$ is the amount of heat lost in cgs units, that is, the quantity of heat, small calories, radiated per second per square centimeter of surface of the sphere, per degree difference of temperature $t$, and $t$ is the difference of temperature between the sphere and the enclosure. The medium through which the heat passed was moist air. The following table gives the results.

| Differ- <br> ence of <br> temper. <br> ature <br> $t$ | Polished <br> surface | Blackened <br> surface | Ratio |
| :---: | :---: | :---: | :---: |
| 5 | .000178 | .000252 | .707 |
| 10 | .000186 | .000266 | .699 |
| 15 | .000193 | .000279 | .692 |
| 20 | .000201 | .000289 | .695 |
| 25 | .000207 | .000298 | .694 |
| 30 | .000212 | .000306 | .693 |
| 35 | .000217 | .000313 | .693 |
| 40 | .000220 | .000319 | .693 |
| 45 | .000223 | .000323 | .690 |
| 50 | .000225 | .000326 | .690 |
| 55 | .000226 | .000328 | .690 |
| 60 | .000226 | .000328 | .690 |

## TABLE 104.-AT DIFFERENT PRESSURES

Experiments made in Tait's Laboratory show the effect of pressure of the enclosed air on the rate of loss of heat. In this case the air was dry and the enclosure kept at about $8^{\circ} \mathrm{C}$.

| Polished surface |  | Blackened surface |  |
| :---: | :---: | :---: | :---: |
| $t$ | et | $t$ | ${ }_{\text {ct }}$ |
| Pressure 76 cmHg |  |  |  |
| 63.8 | . 00987 | 61.2 | . 01746 |
| 57.1 | . 00862 | 50.2 | . 01360 |
| 50.5 | . 00736 | 41.6 | . 01078 |
| 44.8 | . 00628 | 34.4 | . 00860 |
| 40.5 | . 00562 | 27.3 | . 00640 |
| 34.2 | . 00438 | 20.5 | . 00455 |
| 29.6 | . 00378 | - | - |
| 23.3 | . 00278 | - |  |
| 18.6 | . 00210 | - |  |

Pressure 10.2 cmHg

| 67.8 | .00492 | 62.5 | .01298 |
| :--- | :---: | :---: | :---: |
| 61.1 | .00433 | 57.5 | .01158 |
| 55 | .00383 | 53.2 | .01048 |
| 49.7 | .00340 | 47.5 | .00898 |
| 44.9 | .00302 | 43.0 | .00791 |
| 40.8 | .00268 | 28.5 | .00490 |
|  |  |  |  |
| Pressure 1 cmHg |  |  |  |
| 65 | .00388 | 62.5 | .01182 |
| 60 | .00355 | 57.5 | .01074 |
| 50 | .00286 | 54.2 | .01003 |
| 40 | .00219 | 41.7 | .00726 |
| 30 | .00157 | 37.5 | .00639 |
| 23.5 | .00124 | 34.0 | .00569 |
| - | - | 27.5 | .00446 |
| - | - | 24.2 | .00391 |

## TABLE 105.-COOLING OF PLATINUM WIRE IN COPPER ENVELOPE

Bottomley gives for the radiation of a bright platinum wire to a copper envelope when the space between is at the highest vacuum attainable the following numbers:

$$
\begin{aligned}
& t=408^{\circ} \mathrm{C}, \text { et }=378.8 \times 10^{-4}, \text { temperature of enclosure } 16^{\circ} \mathrm{C} . \\
& t=505^{\circ} \mathrm{C}, \text { et }=726.1 \times 10^{-4}, \quad " \quad " \quad 17^{\circ} \mathrm{C} .
\end{aligned}
$$

It was found at this degree of exhaustion that considerable relative change of the vacuum produced very small change of the radiating power. The curve of relation between degree of vacuum and radiation becomes asymptotic for high exhaustions. The following table illustrates the variation of radiation with pressure of air in enclosure.

| Temp. of enclosure $16^{\circ} \mathrm{C}, t=408^{\circ} \mathrm{C}$ |  | Temp. of enclosure $17^{\circ} \mathrm{C}, t=505^{\circ} \mathrm{C}$ |  |
| :---: | :---: | :---: | :---: |
| Pressure in mm | ${ }^{\text {ct }}$ | Pressure in mm | ${ }^{c t}$ |
| 740. | $8137.0 \times 10^{-4}$ | . 094 | $1688.0 \times 10^{-4}$ |
| 440. | 7971.0 | . 053 | 1255.0 " |
| 140. | 7875.0 | . 034 | 1126.0 " |
| 42. | 7591.0 " | . 013 | 920.4 " |
| 4. | 6036.0 " | . 0046 | 831.4 " |
| . 444 | 2683.0 " | . 00052 | 767.4 " |
| . 070 | 1045.0 " | . 00019 | 746.4 " |
| . 034 | 727.3 " | Lowest reached $\}$ | 726.1 " |
| . 012 | 539.2 " | but not measured $\}$ | 726.1 |
| . 0051 | 436.4 378.8 |  |  |
| . 00007 | 378.8 " |  |  |

TABLE 106.-EFFECT OF PRESSURE ON LOSS OF HEAT AT DIFFERENT TEMPERATURES

The temperature of the enclosure was about $15^{\circ} \mathrm{C}$. The numbers give the total radiation in calories per square centimeter per second.

| Temp. of wire in ${ }^{\circ} \mathrm{C}$ | Pressure in $\underbrace{\mathrm{mmHg}}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 10.0 | 1.0 | . 25 | . 025 | About |
| 100 | . 14 | . 11 | . 05 | . 01 | . 005 |
| 200 | . 31 | . 24 | . 11 | -. 02 | . 0055 |
| 300 | . 50 | . 38 | . 18 | . 04 | . 0105 |
| 400 | . 75 | . 53 | . 25 | . 07 | . 025 |
| 500 | - | . 69 | . 33 | . 13 | . 055 |
| 600 | - | . 85 | . 45 | . 23 | . 13 |
| 700 | - |  | - | . 37 | . 24 |
| 800 | - | - | - | . 56 | . 40 |
| 900 | - | - | - | - | . 61 |

Note.-An interesting feature (because of its practical importance in electric lighting) is the effect of difference of surface condition on the radiation of heat. The energy required to keep up a certain degree of incandescence in a lamp when the filament is dull black and when it is "flashed" with coating of hard carbon, was found to be as follows :

Dull black filament, 57.9 watts.
Bright " " 39.8 watts.

Loss of heat by air from surfaces takes place by radiation, conduction, and convection. The two latter are generally inextricably mixed. For horizontal air spaces, upper surface warm, the loss is all radiation and conduction; with warm lower surface the loss is greater than for similar vertical space.

Vertical spaces: The following table shows that for spaces of less than 1 cm width the loss is nearly proportional to the space width, when the radiation is allowed for; for greater widths the increase is less rapid, then reaches a maximum, and for yet greater widths is slightly less.

Heat conduction and thermal resistances, radiation eliminated, air space 20 cm high

| $\underset{\substack{\text { Air } \\ \text { space, } \\ \mathrm{cm}}}{\text { and }}$ | Heat conduction cal hr-1 $\mathrm{cm}^{-10} \mathrm{C}-1$ Temperature difference |  |  |  | Thermal resistance Reciprocal of conductance Temperature difference |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{\circ}$ | $15^{\circ}$ | $20^{\circ}$ | $25^{\circ}$ | $10^{\circ}$ | $15^{\circ}$ | $20^{\circ}$ | $25^{\circ}$ |
| . 5 | . 46 | . 46 | . 46 | . 46 | 2.17 | 2.17 | 2.17 | 2.17 |
| 1.0 | . 24 | . 24 | . 24 | . 24 | 4.25 | 4.20 | 4.15 | 4.10 |
| 1.5 | . 160 | . 172 | . 182 | . 192 | 6.25 | 5.80 | 5.50 | 5.20 |
| 2.0 | . 161 | . 178 | . 200 | . 217 | 6.20 | 5.60 | 5.00 | 4.60 |
| 3.0 | . 172 | . 196 | . 208 | . 217 | 5.80 | 5.10 | 4.80 | 4.60 |

Variation with height of air space: Max. thermal resistance $=4.0$ at 1.4 cm air space, 10 cm high; 6.0 at $1.6 \mathrm{~cm}, 20 \mathrm{~cm}$ high; 8.9 at $2.5 \mathrm{~cm}, 60 \mathrm{~cm}$ high.

## TABLE 108.-CONVECTION OF HEAT IN AIR AT ORDINARY TEMPERATURES *

In very narrow layers of air between vertical surfaces at different temperatures the convection currents, in the main, flow up one side and down the other, with eddyless (streamline) motion. It follows that these currents transport heat to or from the surfaces only when they turn and flow horizontally, from which fact it follows, in turn, that the convective heat transfer is independent of the height of the surface. It is, according to the laws of eddyless flow, proportional to the square of the temperature difference. and to the cube of the distance between the surfaces. As the flow becomes more rapid (e.g., for a $20^{\circ}$ difference and a distance of 1.2 cm ) turbulence enters, and the above relations begin to change. For the dimensions tested, convection in horizontal layers was a little over twice that in vertical.

## Heat transfer, in the usual cgs unit, i.e., calories per second per degree of thermal head per $\mathrm{cm}^{2}$ of flat surface at $22.8^{\circ}$ mean temperature

Where two values are given, they show the range among determinations with different methods of getting the temperature of the outer plate. It will be seen that the value of the convection is practically unaffected by this difference of method.

| Thermal head | 8 mm gap |  | 12 mm gap |  | 24 mmgap |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Convection | Total | Convection | Total | Convection |
| $.99^{\circ}$ | - | - | $\left.\begin{array}{rrr} .000 & 083 & 9 \\ .000 & 084 & 8 \end{array}\right\}$ | - | . 000065 | - |
| $1.98{ }^{\circ}$ | $\left\{\begin{array}{rr}.000 & 109 \\ & 110\end{array}\right.$ | - | $\left.\begin{array}{l}.000 \\ .000 \\ \hline 084 \\ 085 \\ 2\end{array}\right\}$ | $\begin{array}{r} .0000001 \\ 0004 \end{array}$ | - | - |
| $4.95^{\circ}$ | . 000111 | . 000001 | $\left\{\begin{array}{r}.0000866 \\ 881\end{array}\right.$ |  | . 000090 | over . 000025 |
| $9.89{ }^{\circ}$ | $\left\{\begin{array}{rr}.000 & 112 \\ & 113\end{array}\right.$ | .000003 003 | .0000937 952 | $\left.\begin{array}{l}.000 \\ .000 \\ 011\end{array}\right\}$ | . 000106 | over . 000040 |
| $19.76^{\circ}$ | . 000116 | . 000007 | $\left\{\begin{array}{rr}.000 & 1077 \\ 1094\end{array}\right.$ | $\left.\begin{array}{r}.000 \\ 024 \\ 026\end{array}\right\}$ | . 000126 | over . 000060 |

[^56]
## TABLE 109.-CONVECTION AND CONDUCTION OF HEAT BY GASES AT HIGH TEMPERATURES

The loss of heat from wires at high temperatures occurs as if by conduction across a thin film of stationary gas adhering to the wire (vertical and horizontal losses very similar). Thickness of film is apparently independent of temperature of wire, but probably increases with the temperature of the gas and varies with the diameter of the wire according to the formula $b \log (b / a)=2 B$, where $B=$ constant for any gas, $b=$ diameter of film, $a$, of wire. The rate of convection (conduction) of heat is the product of two factors, one the shape factor, $s$, involving only $a$ and $B$, the other a function $\phi$ of the heat conductivity of the gas. If $W=$ the energy loss in watts $/ \mathrm{cm}$, then $W=\mathrm{s}\left(\phi_{2}-\phi_{1}\right)$, $s$ may be found from the relation

$$
\frac{s}{\pi} e^{-\frac{2 \pi}{s}}=\frac{a}{B} ; \phi=4.19 \int_{0}^{\tau} k d t,
$$

where $k$ is the heat conductivity of the gas at temperature $T$ in calories $/ \mathrm{cm}^{\circ} \mathrm{C} . \phi_{2}$ is taken at the temperature $T_{2}$ of the wire, $\phi_{1}$ at that of the atmosphere. The following may be taken as the conductivities of the corresponding gases at high temperatures:

$$
\begin{aligned}
& \text { For hydrogen } \ldots \ldots \ldots . k=28 \times 10^{-6} \sqrt{T}\left\{(1+.0002 T) /\left(1+77 T^{-1}\right)\right\} \\
& \quad \text { air } \ldots \ldots \ldots \ldots k=4.6 \times 10^{-6} \sqrt{T}\left\{(1+.0002 T) /\left(1+124 T^{-1}\right)\right\} \\
& \quad \text { mercury vapor } \ldots . k=2.4 \times 10^{-6} \vee \bar{T}\left\{1 /\left(1+960 T^{-1}\right)\right\} .
\end{aligned}
$$

To obtain the heat loss: $B$ may be assumed proportional to the viscosity of the gas and inversely proportional to the density. For air [see Table 110 part 2] $B$ may be taken as 0.43 cm ; for $\mathrm{H}_{2}, 3.05 \mathrm{~cm}$; for Hg vapor as 0.078 . Obtain $s$ from Part 1 below from $a / B$; then from Part 2 obtain $\phi_{2}$ and $\phi_{1}$ for the proper temperatures; the loss will be $s\left(\phi_{2}-\phi_{1}\right)$ in watts $/ \mathrm{cm}$.

Part 1.-s as function of $a / B$

| $s$ | $a / B$ | $s$ | $a / B$ | $s$ | $a / B$ | $s$ | $a / B$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| .0 | .0 | $535 \times 10^{-6}$ | 5.0 | .453 | 10 | 1.696 | 30 |
| .5 | .753 | 7.738 |  |  |  |  |  |
| 1.0 | $.584 \times 10^{-3}$ | 6.0 | .671 | 12 | 2.263 | 32 | 8.370 |
| 1.5 | $.725 \times 10^{-2}$ | 6.5 | .788 | 16 | 2.844 | 34 | 8.995 |
| 2.0 | $2.75 \times 10^{-2}$ | 7.0 | .908 | 18 | 3.438 | 36 | 9.622 |
| 2.5 | .0644 | 7.5 | 1.032 | 20 | 4.040 | 38 | 10.25 |
| 3.0 | .1176 | 8.0 | 1.160 | 22 | 5.263 | 40 | 10.87 |
| 3.5 | .185 | 8.5 | 1.291 | 24 | 5.877 | 42 | 11.50 |
| 4.0 | .265 | 9.0 | 1.424 | 26 | 6.505 | 46 | 12.14 |
| 4.5 | .354 | 9.5 | 1.561 | 28 | 7.122 | 48 | 13.14 |
| 5.0 | .453 | 10.0 | 1.696 | 30 | 7.738 | 50 | 14.03 |

Part 2.-Table of $\phi$ in watts per cm as function of absolute temp. ( ${ }^{\circ} \mathrm{K}$ )

| $T^{\circ} \mathrm{K}$ | $\mathrm{H}_{2}$ | Air | Hg | $T^{\circ} \mathrm{K}$ | $\mathrm{H}_{2}$ | Air | Hg |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | .0000 | .0000 | - | $1500^{\circ}$ | 4.787 | .744 | .1783 |
| 100 | .0329 | .0041 | - | 1700 | 5.945 | .931 | .228 |
| 200 | .1294 | .0168 | - | 1900 | 7.255 | 1.138 | .284 |
| 300 | . .278 | .0387 | - | 2100 | 8.655 | 1.363 | .345 |
| 400 | .470 | .0669 | - | 2300 | 10.18 | 1.608 | .411 |
| 500 | .700 | .1017 | .0165 | 2500 | 11.82 | 1.871 | .481 |
| 700 | 1.261 | .189 | .0356 | 2700 | 13.56 | - | .556 |
| 900 | 1.961 | .297 | .0621 | 2900 | 15.54 | - | .636 |
| 1100 | 2.787 | .426 | .0941 | 3100 | 17.42 | - | .719 |
| 1300 | 3.726 | .576 | .1333 | 3300 | 19.50 | - | .807 |
| 1500 | 4.787 | .744 | .1783 | 3500 | 21.79 | - | .898 |

# Part 1.-Wires of platinum sponge served as radiators to room-temperature 

 surroundings| Observed heat losses in watts per cm |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| eter | Absolute temperatures |  |  |  |  |  |  |  |  |  |  |  |
| cm | $900^{\circ}$ | $1000^{\circ}$ | $110{ }^{\circ}$ | $1200^{\circ}$ | $1300^{\circ}$ | $1400^{\circ}$ | $1500^{\circ}$ | $1600^{\circ}$ | $1700^{\circ}$ | $1800^{\circ}$ | $1900^{\circ}$ | $2000^{\circ}$ |
| . 0690 | 1.70 | 2.26 | 3.01 | 3.88 | 4.92 | 6.18 | 7.70 | 9.63 | 12.15 | 15.33 | 19.25 | 23.75 |
| . 0420 | 1.35 | 1.75 | 2.26 | 2.84 | 3.53 | 4.29 | 5.33 | 6.60 | 8.25 | 10.20 | 12.45 | 14.75 |
| . 0275 | 1.12 | 1.40 | 1.76 | 2.23 | 2.73 | 3.23 | 3.91 | 4.67 | 5.72 | 7.00 | 8.64 | 10.45 |
| . 0194 | . 92 | 1.15 | 1.39 | 1.74 | 2.12 | 2.54 | 3.04 | 3.64 | 4.32 | 5.10 | 6.10 | 7.35 |
| Heat losses corrected for radiation, watts per cm (A-C) |  |  |  |  |  |  |  |  |  |  |  |  |
| . 0690 | . 91 | 1.05 | 1.23 | 1.36 | 1.45 | 1.51 | 1.54 | 1.66 | 2.00 | 2.56 | 3.40 | 4.30 |
| . 0420 | . 87 | 1.02 | 1.17 | 1.31 | 1.42 | 1.45 | 1.57 | 1.76 | 2.08 | 2.43 | 2.80 | 3.26 |
| . 0275 | . 80 | . 92 | 1.05 | 1.22 | 1.35 | 1.37 | 1.46 | 1.50 | 1.67 | 1.91 | 2.32 | 2.70 |
| . 0194 | . 70 | . 81 | . 89 | 1.03 | 1.15 | 1.23 | 1.31 | 1.40 | 1.47 | 1.51 | 1.64 | 1.88 |
| Computed radiation, watts per $\mathrm{cm}, \sigma=5.61 \times 10^{-12} *$ |  |  |  |  |  |  |  |  |  |  |  |  |
| . 0690 | . 79 | 1.21 | 1.78 | 2.52 | 3.47 | 4.67 | 6.16 | 7.97 | 10.15 | 12.77 | 15.85 | 19.45 |
| . 0420 | . 48 | . 73 | 1.09 | 1.53 | 2.11 | 2.84 | 3.74 | 4.84 | 6.17 | 7.77 | 9.65 | 11.85 |
| . 0275 | . 32 | . 48 | . 71 | 1.01 | 1.38 | 1.86 | 2.45 | 3.17 | 4.05 | 5.09 | 6.32 | 7.75 |
| . 0195 | . 22 | . 34 | . 50 | . 71 | 97 | 1.31 | 1.73 | 2.24 | 2.85 | 3.59 | 4.46 | 5.47 |
| Conduction loss by silver leads, watts per cm |  |  |  |  |  |  |  |  |  |  |  |  |
| . 0420 | . 42 | . 46 | . 49 | . 61 | . 75 | . 88 | 1.00 | 1.07 | 1.13 | 1.22 | - |  |
| . 0275 | . 18 | . 21 | . 28 | . 35 | . 43 | . 48 | . 55 | . 57 | . 60 | . 67 | - |  |
| . 0195 | . 06 | . 08 | . 08 | . 09 | . 11 | . 12 | . 14 | . 15 | . 22 | . 23 | - | - |
| Convection loss by air, watts per cm |  |  |  |  |  |  |  |  |  |  |  |  |
| . 0420 | . 45 | . 56 | . 68 | . 70 | . 67 | . 57 | . 59 | .69 | . 95 | 1.21 | - | - |
| . 0275 | . 62 | . 71 | . 77 | . 87 | . 92 | . 89 | . 91 | . 93 | 1.07 | 1.24 | - |  |
| . 0195 | . 64 | . 73 | . 81 | . 94 | 1.04 | 1.11 | 1.17 | 1.25 | 1.29 | 1.30 | - | - |

* This value is lower than the presently (1950) accepted value of 5.67 .

Part 2.-Wires of bright platinum $40-50 \mathrm{~cm}$ long served as radiators to surroundings at $300^{\circ} \mathrm{K}$


[^57]
## TABLES 111-125-TEMPERATURE CHARACTERISTICS OF MATERIALS

table 111.-MELTING AND BOILING POINTS OF THE CHEMICAL ELEMENTS (Metals in boldface type are often used as standard melting points.)

| Element |  |  | Melting ${ }^{\circ} \mathrm{C}$ C ${ }^{\circ} \mathrm{C}$ | $\underset{\substack{\text { Boiling } \\ \text { point } \\ \text { poic }}}{ }$ | Element | $\begin{gathered} \text { Symbol } \\ \text { and } \\ \text { atomic No. } \end{gathered}$ | Melting $\begin{aligned} & \text { point } \\ & { }^{\circ} \mathrm{C} \end{aligned}$ | Boiling ${ }^{\text {point }}$ ${ }^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actinium | Ac | 89 | 1197 |  | Neodymium | Nd 60 | 1024 |  |
| Aluminum | Al | 13 | 660.1 | 2450 | Neon | Ne 10 | $-248.59$ | - 246.08 |
| Antimony | Sb | 51 | 630.5 | 1637 | Nickel | Ni 28 | 1453 | 2850 |
| Argon | Ar | 18 | - 189.37 | - 185.86 | Niobium | Nb 41 | 2480 | 5000 |
| Arsenic | As | 33 | 817 | 613 | Nitrogen | N 7 | - 209.97 | - 195.80 |
| Astatine | At | 85 |  |  | Osmium | Os 76 | 2700 | 4400 |
| Barium | Ba | 56 | 710 | 1637 | Oxygen | O 8 | - 218.79 | - 182.97 |
| Beryllium | Be | 4 | 1283 | 2480 | Palladium | Pd 46 | 1552 | 3100 |
| Bismuth | Bi | 83 | 271.3 | 1560 | Phosphorus | P 15 | 44.2 | 280 |
| Boron | B | 5 |  |  | Platinum | Pt 78 | 1769 | 3800 |
| Bromine | Br | 35 | - 7.20 | 59 | Plutonium | Pu 94 | 639 |  |
| Cadmium | Cd | 48 | 321.03 | 765 | Polonium | Po 84 | 254 | 960 |
| Calcium | Ca | 20 | 850 | 1492 | Potassium | K 19 | 63.2 | 766 |
| Carbon | C | 6 |  |  | Praseodymium | Pr 59 | 935 | 3000 |
| Cerium | Ce | 58 | 804 | 2900 | Promethium . | Pm 61 |  |  |
| Cesium | Cs | 55 | 28.64 | 685 | Protactinium | Pa 91 |  |  |
| Chlorine | Cl | 17 | - 100.99 | - 34.06 | Radium | Ra 88 | 700 |  |
| Chromium | Cr | 24 | 1903 | 2640 | Radon | Rn 86 | - 71 | - 62 |
| Cobalt | Co | 27 | 1492 | 3150 | Rhenium | Re 75 | 3150 | 5600 |
| Copper | Cu | 29 | 1083.0 | 2580 | Rhodium | Rh 45 | 1960 | 3960 |
| Dysprosium | Dy | 66 | 1500 | 2300 | Rubidium | .Rb 37 | 38.8 | 701 |
| Erbium | Er | 68 | 1500 | 2600 | Ruthenium | .Ru 44 | 2400 | 4000 |
| Europium | Eu | 63 |  |  | Samarium | Sm 62 | 1050 | 1600 |
| Fluorine | F | 9 | - 219.61 | - 188.44 | Scandium | Sc 21 | 1400 | 3900 |
| Francium | Fr | 87 |  |  | Selenium | . Se 34 | 217.4 | 684.8 |
| Gadolinium | Gd | 64 | 1420 |  | Silicon | .Si 14 | 1410 |  |
| Gallium |  | 31 | 29.80 | 2240 | Silver | Ag 47 | 960.8 | 2190 |
| Germanium |  | 32 | 938 | 2800 | Sodium | Na 11 | 97.82 | 890 |
| Gold | Au | 79 | 1063.0 | 2700 | Strontium | Sr 38 | 770 | 1370 |
| Hafnium | Hf | 72 | 2220 | 5200 | Sulfur | . ${ }^{16}$ | 119 | 444.60 |
| Helium | He | 2 |  | - 269.93 | Tantalum | .Ta 73 | 2980 | 5500 |
| Holmium | Но | 67 | 1500 |  | Technetium | Tc 43 |  |  |
| Hydrogen | H | 1 | - 259.19 | - 252.76 | Tellurium | Te 52 | 450 | 990 |
| Indium | In | 49 | 156.61 | 2000 | Terbium | Tb 65 | 1450 |  |
| Iodine | I | 53 | 113.6 | 183 | Thallium | T1 81 | 303.6 | 1460 |
| Iridium |  | 77 | 2443 |  | Thorium |  | 1695 |  |
| Iron |  | 26 | 1535 | 2900 | Thulium | Tm 69 | 1650 |  |
| Krypton |  | 36 | - 157.3 | - 153.35 | Tin ${ }^{\text {Titanium }}$ | Ti 22 | 1675 | 3300 |
| Lanthanum |  | 57 | 920 | 3370 | Tungsten | W 74 | 3380 | 5500 |
| Lead | Pb | 82 | 327.3 | 1750 | Uranium | U 92 | 1132 | 4000 |
| Lithium | Li | 3 | 180.55 | 1331 | Vanadium | . V 23 | 1890 | 3400 |
| Lutetium | Lu | 71 | 1700 |  | Xenon ... | Xe 54 | - 112.5 | -108.1 |
| Magnesium |  | 12 | 650 | 1120 | Ytterbium | Yb 70 | 824 |  |
| Manganese | Mn | 25 | 1244 | 2050 | Yttrium . | Y 39 |  |  |
| Mercury | Hg | 80 | - 38.87 | 356.57 | Zinc | Zn 30 | 419.50 | 908 |
| Molybdenum | Mo | 42 | 2610 |  | Zirconium | Zr 40 | 1852 | 4400 |

TABLE 112.-MELTING PARAMETERS OF ARGON ${ }^{43}$

| Pressure, $\mathrm{kg} / \mathrm{cm}^{2}$ | Melting point | $\frac{d T}{d p}$ | $\begin{gathered} \left.\mathrm{cm}^{v} / \mathrm{g}\right) \end{gathered}$ | Latent heat kg cal/g |
| :---: | :---: | :---: | :---: | :---: |
| 1 | $83.9^{\circ} \mathrm{K}$. | . 0238 | . 0795 | 280 |
| 1,000 | 106.4 | . 0211 | . 0555 | 280 |
| 2,000 | 126.3 | . 0192 | . 0425 | 279 |
| 3,000 | 144.9 | . 0178 | . 0340 | 277 |
| 4,000 | 161.9 | . 0165 | . 0280 | 275 |
| 5,000 | 177.8 | . 0155 | . 0240 | 276 |
| 6,000 | 192.9 | . 0146 | . 0210 | 277 |

[^58]
## TABLE 113.-MELTING TEMPERATURES IN ${ }^{\circ} \mathrm{C}$ FOR A NUMBER OF LIQUIDS AS A FUNCTION OF PRESSURE "

| $\begin{aligned} & \text { Pres- } \\ & \text { sure } \\ & \mathrm{kg} / \mathrm{cm}^{2} \end{aligned}$ | Ethyl alcohol | n-Butyl alcohol | Ethyl bromide | n-Propyl bromide | Chloroform | Carbon bisulfide | Chlorobenzene | Methylene chloride | Water |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 5,000 | $\begin{aligned} & -117.3^{\circ} \mathrm{C} \\ & -76 \end{aligned}$ | $\begin{aligned} & -89.8^{\circ} \mathrm{C} \\ & -33 \end{aligned}$ | $\begin{aligned} & -119^{\circ} \mathrm{C} \\ & -70 \end{aligned}$ | $\begin{aligned} & -110^{\circ} \mathrm{C} \\ & -56 \end{aligned}$ | $\begin{aligned} & -63.5^{\circ} \mathrm{C} \\ & +10 \end{aligned}$ | $\begin{aligned} & -111.6^{\circ} \mathrm{C} \\ & -51 \end{aligned}$ | $\begin{aligned} & -45.2^{\circ} \mathrm{C} \\ & +25 \end{aligned}$ | $\begin{aligned} & -96.7^{\circ} \mathrm{C} \\ & -46 \end{aligned}$ |  |
| 10,000 | - 39 | $+12$ | - 29 | - 8 | $+76$ | 0 | $\left.\begin{array}{l}+80 \\ +30\end{array}\right\}^{+}$ | 0 | . |
| 15,000 | - 5 | $+49$ | + 5 | + 34 | +137 | + 46 | +130 | $+42$ | $+52.5{ }^{\circ} \mathrm{C}$ |
| 20,000 | $+25$ | +80 | + 34 | + 71 | +192 | + 89 | +166 | +82 | +72.8 |
| 25,000 | 54 | 108 | 58 | 105 | 243 | 130 | 222 | 120 | 102.8 |
| 39,000 | 82 | 132 | 80 | 138 |  | 170 |  | 157 | 137.1 |
| 35,000 | 109 | 155 |  | 169 | . | 209 |  | . . | 166.6 |
| 40,000 | . . | . . | - | 197 | - | . | . | . | 192.3 |

[^59]TABLE 114.-VOLUME-PRESSURE RELATION FOR ARGON*
Volume, $\mathrm{cm}^{8}$

| Pres. <br> sure <br> $\mathrm{kg} / \mathrm{cm}^{2}$ | $+55^{\circ} \mathrm{C}$ | $+25^{\circ} \mathrm{C}$ | $0^{\circ} \mathrm{C}$ | $-90^{\circ} \mathrm{C}$ | $-101.4^{\circ} \mathrm{C}$ | $-117^{\circ} \mathrm{C}$ | $-135.1^{\circ} \mathrm{C}$ | $-153.5^{\circ} \mathrm{C}-172^{\circ} \mathrm{C}$ |
| ---: | :---: | ---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 700 | - | 1.262 | 1.179 | - | - | - | - | .724 |
| 800 | - | 1.175 | 1.105 | - | - | - | - | .690 |
| 1,000 | - | 1.060 | 1.006 | - | - | - | - | .697 |
| 1,300 | - | .962 | .920 | - | - | - | - | .677 |
| 1,600 | - | .898 | .864 | - | - | - | - | .657 |
| 2,000 | .880 | .846 | .818 | - | - | - |  |  |
| 2,500 | .831 | .808 | .785 | - | .687 | - | .653 | - |
| 3,500 | .772 | .751 | .733 | .661 | .656 | .638 | - | - |
| 4,500 | .730 | .712 | .697 | .641 | .632 | - | - | - |
| 5,500 | .698 | .682 | .669 | .624 | - | - | - | - |
| 6,000 | .685 | - | - | - | - | - | - | - |
| 10,000 | .617 | - | - | - | - | - | - | - |
| 12,000 | .596 | - | - | - | - | - | - | - |
| 15,000 | .573 | - | - | - | - | - | - | - |

*For reference, see footnote 43, p. 117.

TABLE 115.-MELTING PARAMETERS OF NITROGEN *

| Pressure <br> $\mathrm{kg} / \mathrm{cm}^{2}$ <br> $\rho$ | Melting <br> point | $63.2^{\circ} \mathrm{K}$ | $\frac{d T}{d \phi}$ | .0209 |
| :---: | :---: | :---: | :---: | :---: |

*For reference, see foot note 43, p. 117.

Volume, $\mathrm{cm}^{3}$

| Pressure <br> $\mathrm{kg} / \mathrm{cm}^{2}$ | $+23.5^{\circ} \mathrm{C}$ | $0^{\circ} \mathrm{C}$ | $-50^{\circ} \mathrm{C}$ | $-100^{\circ} \mathrm{C}$ | $-140^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | ---: | ---: |
| 3,000 | 1.2374 | 1.2069 | 1.1422 | 1.0754 | 1.0226 |
| 4,000 | 1.1615 | 1.1391 | 1.0881 | 1.0327 | .9876 |
| 5,000 | 1.1061 | 1.0870 | 1.0451 | .9997 | .9613 |
| 6,000 | 1.0652 | 1.0487 | 1.0117 | .9729 | .9412 |

* For reference, see footnote 43 , p. 117.

TABLE 117.-EFFECT OF PRESSURE ON MELTING POINT

|  | Substance | Melting point at $1 \mathrm{~kg} / \mathrm{cm}^{2}$ | Highest experimental pressure $\mathrm{kg} / \mathrm{cm}^{2}$ | $\begin{aligned} & d t / d p \\ & \text { at } 1 \mathrm{~kg} / \mathrm{cm}^{2} \end{aligned}$ | $\begin{aligned} & \Delta t \text { (observed) } \\ & \text { for } 1000 \mathrm{~kg} / \mathrm{cm}^{2} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Hg |  | -38.85 | 12,000 | . 00511 | 5.1 * |
| K |  | 59.7 | 2,800 | . 0136 | 13.8 |
| Na |  | 97.62 | 12,000 | . 00860 | +12.3 $\dagger$ |
| Bi |  | 271.0 | 12,000 | $-.00342$ | $-3.5 \dagger$ |
| Sn |  | 231.9 | 2,000 | . 00317 | 3.17 |
| Bi |  | 270.9 | 2,000 | -. 00344 | - 3.44 |
| Cd |  | . 320.9 | 2,000 | . 00609 | 6.09 |
| Pb |  | 327.4 | 2,000 | . 00777 | 7.77 |

* $\Delta t$ (observed) for $10,000 \mathrm{~kg} / \mathrm{cm}^{2}$ is $50.8^{\circ}$. $\quad \dagger \mathrm{Na}$ melts at $177.5^{\circ}$ at $12,000 \mathrm{~kg} / \mathrm{cm}^{2} ; \mathrm{K}$ at $179.6^{\circ}$; Bi at $218.3^{\circ} ; \mathrm{Pb}$ at $644^{\circ}$. Luckey obtains melting point for tungsten as follows: 1 atm, $3623^{\circ} \mathrm{K}$; 8, 3594; 18, 3572; 28, 3564.

TABLE 118.-EFFECT OF PRESSURE ON FREEZING OF WATER*

| Pressure $\mathrm{kg} / \mathrm{cm}^{2}$ | Freezing point | Phases in equilibrium |
| :---: | :---: | :--- |
| 1 | .0 | Ice I-liquid |
| 1,000 | -8.8 | Ice I-liquid |
| 2,000 | -20.15 | -22.0 |
| 2,115 | -18.40 | Ice I-liquid |
| 3,000 | -17.0 | Ice I-ice III-liquid liquid (triple point) |
| 3,530 | -13.7 | Ice III-ice V-liquid (triple point) |
| 4,000 | -1.6 | Ice V—liquid |
| 6,000 | +.16 | Ice V—liquid |
| 6,380 | 12.8 | Ice V—ice VI-liquid (triple point) |
| 8,000 | 37.9 | Ice VI-liquid |
| 12,000 | 57.2 | Ice VI-liquid |
| 16,000 | 73.6 | Ice VI-liquid |
| 20,000 |  |  |

* For reference, see footnote 43, p. 117.

TABLE 119.-EFFECT OF PRESSURE ON BOILING POINT

| Metal | Pressure | ${ }^{\circ} \mathrm{C}$ | Metal | Pressure | ${ }^{\circ} \mathrm{C}$ | Metal | Pressure | $\circ \mathrm{C}$ |
| :--- | :---: | :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| Bi | $\ldots$ | 10.2 cmHg | 1200 | Ag | $\ldots$ | 26.3 cmHg | 1780 | Pb |
| Bi | $\ldots$ | 25.7 cmHg | 1310 | Cu | $\ldots$ | 10.0 cmHg | 1980 | Pb |
| Bi | $\ldots$ | 6.3 atm | 1740 | Cu | $\ldots$ | 25.7 cmHg | 6.3 atm | 1410 |
| Bi | $\ldots$ | 11.7 atm | 1950 | Sn | $\ldots$ | 10.1 cmHg | 1970 | Pb |
| Bi | $\ldots$ | 11.7 atm | 2100 |  |  |  |  |  |
| Ag | $\ldots$ | 16.5 atm | 10.3 cmHg | 1660 | Sn | $\ldots$ | 26.2 cmHg | 2100 |
| Pb | $\ldots$ | 10.5 cmHg | 1315 | Zn | $\ldots$ | 21.5 atm | 1230 |  |

TABLE 120.-DENSITIES AND MEITING AND BOILING POINTS OF INORGANIC COMPOUNDS *

| Substance | Chemical formula | Density about $20^{\circ} \mathrm{C}$ | Melting point, ${ }^{\circ} \mathrm{C}$ | $\underset{\text { point, }}{\substack{\text { Boiling } \\ \text { C }}}$ | Pressure mmHg |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Aluminum chloride | $\mathrm{AlCl}_{3}$ | 2.44 | $190 \ddagger$ | 182.7 | 752 |
| nitrate | $\mathrm{Al}\left(\mathrm{NO}_{3}\right)_{3}+9 \mathrm{H}_{2} \mathrm{O}$ |  | 70.0 | $134 \dagger$ |  |
| oxide | $\mathrm{Al}_{2} \mathrm{O}_{3}$ | 4.00 | 2050 | 2580 | 53 |
| Ammonia | $\mathrm{NH}_{3}$ |  | - 77.7 | - 33.35 | 760 |
| Ammonium nitrate | $\mathrm{NH}_{4} \mathrm{NO}_{3}$ | 1.72 | 169.6 | $210{ }^{\dagger}$ | ... |
| phosphite | $\mathrm{NH}_{4} \mathrm{H}_{2} \mathrm{PO}_{3}$ |  | 123 | $145 \dagger$ |  |
| sulfate | $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{SO}_{4}$ | 1.77 | 146.9 † | $\ldots{ }^{\text {. }}$ + |  |
| Antimony pentachloride | $\mathrm{SbCl}_{3}$ | 2.35 | 2.8 | 140 | 68 |
| trichloride | $\mathrm{SbCl}_{3}$ | 3.14 | 73.4 | 223 | 760 |
| Arsenic hydride | $\mathrm{AsH}_{3}$ |  | -113.5 | - 54.8 | 760 |
| trichloride | $\mathrm{AsCl}_{3}$ | 2.20 | - 18 | 130.2 | 760 |
| Barium chloride | $\mathrm{BaCl}_{2}$ | 3.86 | 962 | 1560 | 760 |
| nitrate | $\mathrm{Ba}\left(\mathrm{NO}_{3}\right)_{2}$ | 3.24 | 592 |  |  |
| perchlorate | $\mathrm{Ba}\left(\mathrm{ClO}_{4}\right)_{2}$ |  | 505 |  |  |
| Bismuth trichloride. | $\mathrm{BiCl}_{3} \ldots$ | 4.75 | 232.5 | 447 | 760 |
| Boric acid | $\mathrm{H}_{3} \mathrm{BO}_{3}$ | 1.46 | 185 |  |  |
| anhydride | $\mathrm{B}_{2} \mathrm{O}_{3}$ | 1.79 | 450 |  |  |
| Borax (sodium borate) | $\mathrm{Na}_{2} \mathrm{~B}_{4} \mathrm{O}_{7}$ | 2.36 | 741 | $1570{ }^{\dagger}$ |  |
| Cadmium chloride ... | $\mathrm{CdCl}_{2}$ | 4.05 | 561 |  |  |
| nitrate | $\mathrm{Cd}\left(\mathrm{NO}_{3}\right)_{2}+4 \mathrm{H}_{2} \mathrm{O}$ | 2.45 | 59.5 |  |  |
| Calcium chloride | $\mathrm{CaCl}_{2}$ | 2.26 | 774.0 |  |  |
| chloride | $\mathrm{CaCl}_{2}+6 \mathrm{H}_{2} \mathrm{O}$ | 1.68 | 29.6 | 200 |  |
| nitrate | $\mathrm{Ca}\left(\mathrm{NO}_{3}\right)_{2}$ | 2.36 | 561 |  |  |
| nitrate | $\mathrm{Ca}\left(\mathrm{NO}_{3}\right)_{2}+4 \mathrm{H}_{2} \mathrm{Oa}$ | 1.82 | 42.3 |  |  |
| oxide | CaO | 3.40 | 2570 | 2850 |  |
| Carbon tetrachloride | $\mathrm{CCl}_{4}$ | 1.59 | - 24 | 76.7 | 760 |
| dioxide | $\mathrm{CO}_{2}$ |  | $-56.6^{8}$ | - 78.5 | subl. |
| disulfide | $\mathrm{CS}_{2}$ | 1.26 | $-111.6$ | 46.2 | 760 |
| monoxide | CO |  | -207 | -192 | 760 |
| trichloride | $\mathrm{C}_{2} \mathrm{Cl}_{8}$ | 1.63 | 184 | 185 |  |
| Chloric (per) acid. | $\mathrm{HClO}_{4}$ | 1.764 | $-112$ | $39 \dagger$ | 56 |
| Chlorine dioxide .. | $\mathrm{ClO}_{2}$ |  | - 59 | 9.9 | 731 |
| Chrome alum .. | $\mathrm{KCr}\left(\mathrm{SO}_{4}\right)_{2}+12 \mathrm{H}_{2}$ | 1.83 | 89 |  |  |
| nitrate | $\mathrm{Cr}_{2}\left(\mathrm{NO}_{3}\right)_{6}+18 \mathrm{H}_{2} \mathrm{O}$ |  | 37 | 170 | 760 |
| Chromium oxide | $\mathrm{CrO}_{3} \ldots . . . .$. | 5.21 | 1990 |  |  |
| Cobalt sulfate.. | $\mathrm{CoSO}_{4}$ | 3.710 | 989 |  |  |
| Cupric chloride | $\mathrm{CuCl}_{2} \ldots$ | 3.05 | 498 | + |  |
| nitrate. | $\mathrm{Cu}\left(\mathrm{NO}_{3}\right)_{2}+3 \mathrm{H}_{2} \mathrm{O}$ | 2.05 | 114.5 | $170{ }^{\dagger}$ | 760 |
| Cuprous chloride | $\mathrm{Cu}_{2} \mathrm{Cl}_{2}$ | 3.7 | 421 | 1366土 | 760 |
| Hydrogen bromide | HBr |  | $-88.5$ | - 67.0 | 760 |
| chloride | HCl |  | $-111.3$ | - 83.7 | 755 |
| fluoride | HF | . 99 | - 92.3 | 19.4 | 755 |
| iodide | HI |  | - 50.8 | $-35.7$ | 760 |
| peroxide | $\mathrm{H}_{2} \mathrm{O}_{2}$ | 1.5 | - 2 | 152.1 | 47 |
| phosphide | $\mathrm{PH}_{3}$ |  | 133.5 | - 87.4 | . . . |
| sulfide .. | $\mathrm{H}_{2} \mathrm{~S}$ |  | - 82.9 | - 62 |  |
| Iron chloride | $\mathrm{FeCl}_{3}$ | 2.80 | 282 | 315 |  |
| nitrate | $\mathrm{Fe}\left(\mathrm{NO}_{3}\right)_{3}+9 \mathrm{H}_{2} \mathrm{O}$ | . 1.68 | 47.2 | + |  |
| sulfate | $\mathrm{FeSO}_{4}+7 \mathrm{H}_{2} \mathrm{O}$... | . 1.90 | 64 | 1 |  |
| Lead chloride | $\mathrm{PbCl}_{2}$. | . 5.8 | 501 | 950土 | 760 |
| Magnesium chloride | MgCl 2 | . 2.18 | 708 | 1412 |  |
| oxide . | MgO | . 3.4 | 2800 |  |  |
| nitrate | $\mathrm{Mg}\left(\mathrm{NO}_{3}\right)_{2}+6 \mathrm{H}_{2} \mathrm{O}$ | . 1.46 | 100 | $\dagger$ | 760 |
| sulfate . . | $\mathrm{MgSO}_{4}$ …...... | . 2.66 | $1124{ }^{\dagger}$ |  |  |
| Manganese chloride . | $\mathrm{MnCl}_{2}+4 \mathrm{H}_{2} \mathrm{O}$ | . 2.01 | 58 | $\dagger$ | 760 |
| nitrate .. | $\mathrm{Mn}\left(\mathrm{NO}_{3}\right)_{2}+6 \mathrm{H}_{2} \mathrm{O}$ | . 1.82 | 26 | $129 \dagger$ | 760 |
| sulfate | $\mathrm{MnSO}_{4}$ | . 3.25 | 700 | $850{ }^{+}$ |  |
| Mercuric chloride . . . | $\mathrm{HgCl}_{2} \ldots$ | . 5.42 | 276 | 302 |  |

[^60](continued)

# TABLE 120.-DENSITIES AND MELTING AND BOILING POINTS OF INORGANIC COMPOUNDS (concluded) 

| Substance | Chemical formula | $\begin{aligned} & \text { Density } \\ & \text { about } \\ & 20^{\circ} \mathrm{C} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \text { Melting } \\ & \text { point, }{ }^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \text { Boiling } \\ & \text { point, } \end{aligned}$ | $\underset{\substack{\text { Pressure } \\ \text { mmHz }}}{ }$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Mercurous chloride | $\mathrm{Hg}_{2} \mathrm{Cl}_{2}$ | 7.10 | $302 \pm$ | 384 |  |
| Nickel carbonyl | $\mathrm{NiC}_{4} \mathrm{O}_{4}$ | 1.32 | - 25 | 43 | 760 |
| nitrate | $\mathrm{Ni}\left(\left(\mathrm{NO}_{3}\right)_{2}+6 \mathrm{H}_{2} \mathrm{O}\right.$ | 2.05 | 56.7 | $136.7{ }^{\dagger}$ | 760 |
| oxide | NiO | 6.69 | 2090 |  |  |
| Nitric acid | $\mathrm{HNO}_{3}$ | 1.502 | - 42 | 86 | 760 |
| anhydride | $\mathrm{N}_{2} \mathrm{O}_{5}$ | 1.64 | 30 | $48^{\dagger}$ | 760 |
| oxide | NO |  | $-163.6$ | -151.8 | 760 |
| peroxide | $\mathrm{N}_{2} \mathrm{O}_{4}$ | 1.49 | - 9.3 | $21.3 \dagger$ | 760 |
| Nitrous anhydride | $\mathrm{N}_{2} \mathrm{O}_{3}$ | 1.45 | -102 | $3.5 \dagger$ | 760 |
|  | $\mathrm{N}_{2} \mathrm{O}$ |  | -102.4 | $3.5 \dagger$ | 760 |
| Phosphoric acid (ortho) | $\mathrm{H}_{3} \mathrm{PO}_{4}$ | 1.83 | 42.45 |  |  |
| Phosphorous acid ..... | $\mathrm{H}_{3} \mathrm{PO}_{3}$ | 1.65 | 73.6 |  |  |
| disulfide | $\mathrm{P}_{3} \mathrm{~S}_{8}$ |  | 298 | $3371 \mid$ | 760 |
| oxychloride | $\mathrm{POCl}_{3}$ | 1.68 | 1.3 | 108 | 760 |
| pentasulfide | $\mathrm{P}_{2} \mathrm{~S}_{5}$ | 2.03 | 276 | 514 | 760 |
| trichloride | $\mathrm{PCl}_{3}$ | 1.57 | -91 | 75.5 | 750 |
| trisulfide | $\mathrm{P}_{4} \mathrm{~S}_{3}$ | 2.03 | 172.5 | 407.5 | 760 |
| Potassium acid phosphate. | $\mathrm{KH}_{2} \mathrm{PO}$ | 2.34 | $252.6{ }^{\dagger}$ | . |  |
| carbonate ... | $\mathrm{K}_{2} \mathrm{CO}_{3}$ | 2.43 | 891 |  |  |
| chlorate | $\mathrm{KClO}_{3}$ | 2.34 | 368.4 | $400 \dagger$ |  |
| chloride | KCl | 1.99 | 776 | 1500 | 760 |
| chromate | $\mathrm{K}_{2} \mathrm{CrO}_{4}$ | 2.72 | 968.3 | $\dagger$ |  |
| cyanide | KCN | 1.52 | 634 |  |  |
| dichromate | $\mathrm{K}_{2} \mathrm{Cr}_{2} \mathrm{O}_{7}$ | 2.69 | 398 |  |  |
| hydroxide | KOH | 2.04 | 360 | 1320 | 760 |
| nitrate .. | $\mathrm{KNO}_{3}$ | 2.10 | 334 | $400{ }^{\dagger}$ |  |
| perchlorate | $\mathrm{KClO}_{4}$ | 2.52 | 610 | $410 \dagger$ | 760 |
| sulfate | $\mathrm{K}_{2} \mathrm{SO}_{4}$ | 2.66 | 1076 | $\dagger$ |  |
| Silver chloride | AgCl | 5.56 | 455 | 1550 |  |
| nitrate | $\mathrm{AgNO}_{3}$ | 4.35 | 212 | $444 \dagger$ |  |
| perchlorate | $\mathrm{AgClO}_{4}$ | 2.81 | $486{ }^{\dagger}$ |  |  |
| phosphate | $\mathrm{Ag}_{3} \mathrm{PO}_{4}$ | 6.37 | 849 |  |  |
| metaphosphate | $\mathrm{AgPO}_{3}$ |  | 482 |  |  |
| sulfate ..... | $\mathrm{AgSO}_{4}$ | 5.45 | 652 | $1085 \dagger$ |  |
| Sodium carbonate | $\mathrm{Na}_{2} \mathrm{CO}_{3}$ | 2:51 | 851 | $\dagger$ |  |
| chlorate | $\mathrm{NaClO}_{3}$ | 2.48 | 248 | ${ }_{141}^{\dagger}$ |  |
| chloride | NaCl | 2.17 | 801 | 1413 | 760 |
| hydroxide | NaOH | 2.13 | 318 |  |  |
| hyposulfite | $\mathrm{Na}_{2} \mathrm{O}_{4}+2 \mathrm{H}_{3} \mathrm{O}$ |  | 52 † | $\dagger$ | 760 |
| metaphosphate | $\mathrm{NaPO}_{3}$ | 2.18 | 640 | $\begin{array}{r} \text { subl. } \\ >1100 \end{array}$ |  |
| nitrate ...... | $\mathrm{NaNO}_{3}$ | 2.26 | 310 | $380 \dagger$ |  |
| perchlorate | $\mathrm{NaClO}_{4}$ | 2.53 | 482 † | $\dagger$ |  |
| pyrophosphate | $\mathrm{Na}_{4} \mathrm{P}_{2} \mathrm{O}_{7}$ | 2.45 | 880 |  |  |
| sulfate | $\mathrm{Na}_{2} \mathrm{SO}_{4}$ | 2.67 | 884 | $\dagger$ |  |
| sulfate | $\mathrm{Na}_{2} \mathrm{SO}_{4}+10 \mathrm{H}_{2} \mathrm{O}$ | 1.46 | 32.88 |  |  |
| tetraborate | $\mathrm{Na}_{2} \mathrm{~B}_{4} \mathrm{O}_{7}$ | 2.36 | 741 | 1570 | 760 |
| Sulfur dioxide | $\mathrm{SO}_{2}$ |  | - 72.7 | - 10 | 760 |
| trioxide | $\mathrm{SO}_{3} \mathrm{a}$ | 1.91 | 16.8 | 44.9 | 760 |
| Sulfuric acid | $\mathrm{H}_{2} \mathrm{SO}_{4}$ | 1.83 | 10.5 | $338{ }^{\dagger}$ | 760 |
| acid acid (pyro) | $\mathrm{H}_{2} \mathrm{SO}_{4}+\mathrm{H}_{2} \mathrm{O}$ | 1.79 |  | $290 \dagger$ | 760 |
| acid (pyro) | $\mathrm{H}_{2} \mathrm{~S}_{2} \mathrm{O}_{7}$ | 1.89 | 35 | ${ }^{\dagger}$ |  |
| Tin, stannic chloride | ${ }_{\substack{\mathrm{SnCl}_{4} \\ \mathrm{SnCl}_{2}}}$ | 2.23 3.39 | - 33 | 114 | 760 |
| stannous chloride Water | $\mathrm{SnCl}_{2}$ | 3.39 (24 | 45 246 | 623 | 760 |
| Water ...... | $\mathrm{H}_{2} \mathrm{O}$ | 0.998 | 0 | 100 | 760 |
| Zinc chloride | $\mathrm{ZnCl}_{2}$ | 2.91 | 262 | 732 | 760 |
| nitrate | $\mathrm{Zn}\left(\mathrm{NO}_{3}\right)_{2}+6 \mathrm{H}_{2} \mathrm{O}$ | 2.06 | $36.4{ }^{\dagger}$ | 131 | 760 |
| sulfate | $\mathrm{ZnSO}_{4}+7 \mathrm{H}_{2} \mathrm{O}$ | 1.97 | $39 \dagger$ | $\dagger$ |  |

[^61]TABLE 121.-DENSITIES AND MELTING AND BOILING POINTS OF ORGANIC COMPOUNDS

| Substance | Chemicalformula $\quad$Density <br> $\mathrm{g} / \mathrm{cm}^{3}$ | ${ }_{\text {Temp }}{ }_{\text {C }}{ }^{\text {c }}$ | $\underset{\substack{\text { Melting } \\ \text { point } \\ \text { oin }}}{\substack{\text { nel }}}$ | $\begin{gathered} \text { Boiling } \\ \text { point } \\ \text { Point } \end{gathered}$ | Pressure 1 atm unless otherwise stated |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Paraffin series: $\mathrm{C}_{\mathrm{n}} \mathrm{H}_{2 \mathrm{n}+2}$. | Normal | compounds | only |  |
| Methane | $\mathrm{CH}_{4}$.......... . 415 | -164 | -184 | -161.4 |  |
| Ethane | $\mathrm{C}_{2} \mathrm{H}_{8}$........ . 546 | - 88 | -172.0 | - 88.3 |  |
| Propane | $\mathrm{C}_{3} \mathrm{H}_{8}$........ . . 595 | - 44 | -189.9 | - 42.0 |  |
| Butane | C. $\mathrm{H}_{10} \ldots \ldots .$. . . . 6011 | 0 | -135.0 | $+\quad .6$ |  |
| Pentane | $\mathrm{C}_{5} \mathrm{H}_{12}$........ . 631 | 20 | -138.0 | + 36.2 |  |
| Hexane | $\mathrm{C}_{0} \mathrm{H}_{14}$. . . . . . . . 660 | 20 | - 94.3 | 69.0 |  |
| Heptane | $\mathrm{C}_{7} \mathrm{H}_{18} \ldots . . . .$. . . 684 | 20 | - 90.0 | 98.4 |  |
| Octane | $\mathrm{C}_{8} \mathrm{H}_{18} \ldots . . . \mathrm{C}^{\text {. }} .704$ | 17 | - 56.5 | 124.6 |  |
| Nonane | $\mathrm{C}_{9} \mathrm{H}_{20}$. . . . . . . . 718 | 20 | - 53 | 150.6 |  |
| Decane | $\mathrm{C}_{10} \mathrm{H}_{22} \ldots . . . .{ }^{\text {a }} .747$ | 20 | - 32.0 | 174 |  |
| Undecane | $\mathrm{C}_{11} \mathrm{H}_{24} \ldots \ldots . .{ }^{\text {a }}$. 741 | 20 | - 26.5 | 197 |  |
| Dodecane | $\mathrm{C}_{12} \mathrm{H}_{20} \ldots \ldots . . .768$ | 20 | - 12 | 216 |  |
| Tridecane | $\mathrm{C}_{13} \mathrm{H}_{28} \ldots \ldots . . .857$ | 20 | - 6.2 | 234 |  |
| Tetradecane | $\mathrm{C}_{14} \mathrm{H}_{30} \ldots . . . .{ }^{\text {a }} 765$ | 20 | + 5.5 | 252.5 |  |
| Pentadecane | $\mathrm{C}_{15} \mathrm{H}_{32} \ldots \ldots . . .{ }^{\text {a }}$. 772 | 20 | + 10 | 270.5 |  |
| Hexadecane | $\mathrm{C}_{10} \mathrm{H}_{34} \ldots \ldots . . .{ }^{\text {a }}$. 775 | 20 | 20 | 287.5 |  |
| Heptadecane | $\mathrm{C}_{17} \mathrm{H}_{38} \ldots \ldots . .{ }^{\text {a }}$. 778 | 20 | 22.5 | 303 |  |
| Octadecane | $\mathrm{C}_{18} \mathrm{H}_{38} \ldots . . . .{ }^{\text {a }}$. 777 | 20 | 28 | 317 |  |
| Nonadecane | $\mathrm{C}_{10} \mathrm{H}_{40} \ldots . . . .{ }^{\text {a }} .777$ | 32 | 32 | 330 |  |
| Eicosane | $\mathrm{C}_{20} \mathrm{H}_{42} \ldots . . . . . . .778$ | 37 | 38 | 205 | 15 mmHg |
| Heneicosane | $\mathrm{C}_{21} \mathrm{H}_{44} \ldots . . . .^{\text {. }} .775$ | 45 | 40.4 | 215 | 15 mmHg |
| Docosane | $\mathrm{C}_{22} \mathrm{H}_{48} \ldots . . .{ }^{\text {che }} .778$ | 44 | 44.4 | 224.5 | 15 mmHg |
| Tricosane | $\mathrm{C}_{23} \mathrm{H}_{48} \ldots \ldots . . .{ }^{\text {a }}$. 779 | 48 | 47.7 | 320.7 |  |
| Tetracosane | $\mathrm{C}_{24} \mathrm{H}_{50} \ldots . . . . .{ }^{\text {a }} .779$ | 61 | 54 | 324 |  |
| Pentacosane | $\mathrm{C}_{25} \mathrm{H}_{52} \ldots . . .$. . 779 | 20 | 54 | 284 | 40 mmHg |
| Hexacosane | $\mathrm{C}_{26} \mathrm{H}_{54} \ldots \ldots . . . . .779$ | 20 | 60 | 296 | 40 mmHg |
| Heptacosane | $\mathrm{C}_{22} \mathrm{H}_{58}$. . . . . . . 779 | 60 | 59.5 | 270 | 15 mmHg |
| Octacosane |  | 20 | 65 | 318 | 40 mmHg |
| Nonacosane | $\mathrm{C}_{29} \mathrm{H}_{80} \ldots . . . . .{ }^{\text {c }} 780$ | 20 | 63.6 | 348 | 40 mmHg |
| Triacontane | $\mathrm{C}_{30} \mathrm{H}_{02}$....... . 780 | 20 | 70 | 235 | 1.0 mmHg |
| Hentriacontane | $\mathrm{C}_{31} \mathrm{H}_{84} \ldots \ldots . .{ }^{\text {a }}$. 781 | 68 | 68.1 | 302 | 15 mmHg |
| Dotriacontane | $\mathrm{C}_{32} \mathrm{H}_{68} \quad . . . . . .{ }^{\text {a }} .775$ | 79 | 75 | 310 | 15 mmHg |
| Tetratriacontane | $\mathrm{C}_{34} \mathrm{H}_{70} \quad . . . . . . .^{781}$ | 20 | 76.5 | 255 | 1.0 mmHg |
| Pentatriacontane | . $\mathrm{C}_{35} \mathrm{H}_{72} \ldots . . .{ }^{\text {a }}$. 782 | 75 | 74.7 | 331 | 15 mmHg |
| Hexatriacontane | $\ldots \mathrm{C}_{34} \mathrm{H}_{74}$. ...... . 782 | 76 | 76.5 | 265 | 1.0 mmHg |


(continued)

# TABLE 121.-DENSITIES AND MELTING AND BOILING POINTS OF ORGANIC COMPOUNDS (continued) 

| Substance | Chemical formula | Density | ${ }^{\text {Temp }}$ C ${ }^{\text {c }}$ | $\underset{\substack{\text { Melting } \\ \text { point } \\{ }^{\circ} \mathrm{C}}}{\text { Mely }}$ | Boiling ${ }^{\text {point }}$ | Pressure 1 atm unless stated |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Acetylene | $\mathrm{C}_{\mathrm{n}} \mathrm{H}_{2 \mathrm{n}-2}$. | Normal | compoun | only |  |
| Acetylene | $\ldots \mathrm{C}_{2} \mathrm{H}_{2}$ | . 613 | -80 | -81.8 | -83.6 |  |
| Ally lene | $\mathrm{C}_{3} \mathrm{H}_{4}$ | . 660 | $-13$ | -104.7 | - 27.5 |  |
| Ethylacetylene | $\mathrm{C}_{4} \mathrm{H}_{8}$ | . 668 |  | -130 | + 18.5 |  |
| Propylacetylene | $\mathrm{C}_{5} \mathrm{H}_{8}$ | . 722 |  | -95 | + 40 |  |
| Butylacetylene | $\mathrm{C}_{6} \mathrm{H}_{10}$ |  |  | -150 | 71.5 |  |
| Amylacetylene | . $\mathrm{C}_{7} \mathrm{H}_{12}$ | . 738 | 13 | - 70 | 110.5 |  |
| Hexylacetylene | $\mathrm{C}_{8} \mathrm{H}_{4}$ | . 770 | 0 |  | 125 |  |
| Undecylidene |  |  |  |  | 213 |  |
| Dodecylidene |  | . 810 | - 9 | - 9 | 105 | 15 mmHg |
| Tetradecylidene |  | . 806 | + 6.5 | + 6.5 | 134 | " " ${ }^{\text {c }}$ |
| Hexadecylidene |  | . 804 | 20 | 20 | 160 | " " |
| Octadecylidene |  | . 802 | 30 | 30 | 184 | " " ، |

Monatomic alcohols: $\mathrm{C}_{\mathrm{n}} \mathrm{H}_{2 n+1} \mathrm{OH}$. Normal compounds only

| Methyl alcohol | $\mathrm{CH}_{3} \mathrm{OH}$ | . 792 | 20 | - 97.8 | 64.5 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ethyl alcohol | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{OH}$ | . 789 | 20 | -117.3 | 78.5 |  |
| Propyl alcohol | $\mathrm{C}_{3} \mathrm{H}_{2} \mathrm{OH}$ | . 804 | 20 | -127 | 97.8 |  |
| Butyl alcohol | C. $\mathrm{H}_{4} \mathrm{OH}$ | . 810 | 20 | - 89.8 | 117.7 |  |
| Amyl alcohol | $\mathrm{C}_{5} \mathrm{H}_{11} \mathrm{OH}$ | . 817 | 20 | - 78.5 | 137.9 |  |
| Hexyl alcohol | $\mathrm{C}_{6} \mathrm{H}_{13} \mathrm{OH}$ | . 820 | 20 | - 51.6 | 155.8 |  |
| Heptyl alcohol | $\mathrm{C}_{7} \mathrm{H}_{18} \mathrm{OH}$ | . 817 | 22 | - 34.6 | 175.8 |  |
| Octyl alcohol | $\mathrm{C}_{8} \mathrm{H}_{12} \mathrm{OH}$ | . 827 | 20 | $-16.3$ | 194 |  |
| Nonyl alcohol | $\mathrm{C}_{6} \mathrm{H}_{19} \mathrm{OH}$ | . 828 | 20 |  | 215 |  |
| Decyl alcohol | $\mathrm{C}_{10} \mathrm{H}_{21} \mathrm{OH}$ | . 829 | 20 | + + | 231 |  |
| Undecyl alcohol | $\mathrm{C}_{11} \mathrm{H}_{23} \mathrm{OH}$ | . 833 | 20 | +19 | 146 | 30 mmHg |
| Dodecyl alcohol | $\mathrm{C}_{12} \mathrm{H}_{25} \mathrm{OH}$ | . 831 | 20 | 24 | 259 |  |
| Tridecyl alcohol | $\mathrm{C}_{13} \mathrm{H}_{27} \mathrm{OH}$ | . 822 | 31 | 30.5 | 156 | 15 mmHg |
| Tetradecyl alcohol | $\mathrm{C}_{14} \mathrm{H}_{29} \mathrm{OH}$ | . 824 | 38 | 38 | 167 | 15 mmHg |
| Pentadecyl alcohol | $\mathrm{C}_{15} \mathrm{H}_{32} \mathrm{OH}$ |  |  | 46 |  | . |
| Cetyl alcohol | $\mathrm{C}_{16} \mathrm{H}_{33} \mathrm{OH}$ | . 798 | 79 | 49.3 | 344 |  |
| Octadecyl alcohol | $\mathrm{C}_{18} \mathrm{H}_{27} \mathrm{OH}$ | . 812 | 59 | 58.5 | 210.5 | 15 mmHg |



|  | Ethyl ethers: $\mathrm{C}_{\mathrm{n}} \mathrm{H}_{2 \mathrm{n}+2} \mathrm{O}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Ethyl-methyl | $\mathrm{C}_{3} \mathrm{H}_{8} \mathrm{O}$ | . . 73 | 20 |  |  |
| -propyl | $\mathrm{C}_{5} \mathrm{H}_{12} \mathrm{O}$ | . . 747 | 20 | $<-79$ | 61.4 |
| -isopropyl |  | . 745 | 0 |  | 54 |
| -n. butyl | $\mathrm{C}_{6} \mathrm{H}_{14} \mathrm{O}$ | . 752 | 20 |  | 91.4 |
| -iso-butyl |  | . 751 | 20 |  | 80 |
| -iso-amyl | $\mathrm{C}_{7} \mathrm{H}_{16} \mathrm{O}$ | . 764 | 18 |  | 112 |
| -n. hexyl | $\mathrm{C}_{8} \mathrm{H}_{18} \mathrm{O}$ | . 63 |  |  | 137 |
| " -n. heptyl | $\mathrm{C}_{6} \mathrm{H}_{20} \mathrm{O}$ | . . 790 | 16 |  | 166.6 |
| -n. octyl. | $\mathrm{C}_{12} \mathrm{H}_{22} \mathrm{O}$ | . 794 | 17 |  | 183 |

(continued)

TABLE 121.-DENSITIES AND MELTING AND BOILING POINTS OF ORGANIC COMPOUNDS (concluded)

| Miscellaneous |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Substance | Chemical formula | Density and temperature ${ }^{\circ} \mathrm{C}$ |  | $\underset{\substack{\text { Melting } \\ \text { point }}}{\text { Po } \mathrm{C}}$ | $\underset{\substack{\text { Boiling } \\ \text { point } \\ \text { oc }}}{\text { cosen }}$ |
| Acetic acid | $\mathrm{CH}_{3} \mathrm{COOH}$ | 1.115 | 0 | 16.7 | 118.5 |
| Acetone | $\mathrm{CH}_{3} \mathrm{COCH}_{3}$ | . 792 | 0 | - 94.6 | 56.1 |
| Aldehyde | $\mathrm{C}_{2} \mathrm{H}_{4} \mathrm{O}$ | . 783 | 0 | -124 | 20.8 |
| Aniline | $\mathrm{C}_{6} \mathrm{H}_{5} \mathrm{NH}_{2}$ | 1.038 | 0 | - 6 | 183.9 |
| Beeswax |  | . $96 \pm$ |  | 62 |  |
| Benzene | $\mathrm{C}_{6} \mathrm{H}_{6}$ | . 879 | 20 | 5.48 | 80.2 |
| Benzoic acid | $\mathrm{C}_{7} \mathrm{H}_{8} \mathrm{O}_{2}$ | 1.293 | 4 | 121 | 249 |
| Benzophenone | $\left(\mathrm{C}_{0} \mathrm{H}_{5}\right)_{2} \mathrm{CO}$ | 1.090 | 50 | 48 | 305.9 |
| Butter |  | . 90 |  | 25 |  |
| Cauphor | $\mathrm{C}_{10} \mathrm{H}_{18} \mathrm{O}$ | . 99 | 10 | 176 | 209 |
| Carbolic acid | $\mathrm{C}_{6} \mathrm{H}_{5} \mathrm{OH}$ | 1.060 | 21 | 41 | 182 |
| Carbon bisulfide | $\mathrm{CS}_{2}$ | 1.292 | 0 | -108 | 46.2 |
| tetrachloride | $\mathrm{CCl}_{4}$ | 1.582 | 21 | - 28 | 76.7 |
| Chlorobenzene | $\mathrm{C}_{6} \mathrm{H}_{5} \mathrm{Cl}$ | 1.111 | 15 | - 40 | 132 |
| Chloroform | $\mathrm{CHCl}_{3}$ | 1.4989 | 15 | -63.3 | 61.2 |
| Cyanogen | $\mathrm{C}_{2} \mathrm{~N}_{2}$ |  |  | - 35 | -21 |
| Ethyl bromide | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Br}$ |  | 15 | -117 | 38.4 |
| chloride | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Cl}$ | . 918 | 8 | -141.6 | 12 |
| ether | $\mathrm{C}_{4} \mathrm{H}_{12} \mathrm{O}$ | . 716 | 0 | -116 | 34.6 |
| iodide | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{I}$ | 1.944 | 14 | 108 | 72 |
| Formic acid | HCOOH | 1.242 | 0 | 8.6 | 100.8 |
| Gasoline |  | . $68 \pm$ | . |  | 70-90 |
| Glucose | $\mathrm{CHO}(\mathrm{HCOH}$ | 1.56 |  | 146 |  |
| Glycerine | $\mathrm{C}_{3} \mathrm{H}_{3} \mathrm{O}_{3}$ | 1.269 | 0 | 17 | 290 |
| Iodoform | $\mathrm{CHI}_{3}$ | 4.01 | 25 | 119 |  |
| Lard |  | . 90 |  | $29 \pm$ |  |
| Methyl chloride | $\mathrm{CH}_{3} \mathrm{Cl}$ | . 0992 | -24 | - 98 | -24.1 |
| iodide | $\mathrm{CH}_{3} \mathrm{I}$ | 2.285 | 15 | -64 | 42.3 |
| Naphthalene | $\mathrm{C}_{6} \mathrm{H}_{4} \cdot \mathrm{C}_{4} \mathrm{H}_{4}$ | 1.152 |  | 80 | 218 |
| Nitrobenzene | $\mathrm{C}_{6} \mathrm{H}_{5} \mathrm{O}_{2} \mathrm{~N}$ | 1.212 | 7.5 | 5 | 211 |
| Nitroglycerine | $\mathrm{C}_{3} \mathrm{H}_{5} \mathrm{~N}_{3} \mathrm{O}_{8}$ | 1.60 |  | 3 |  |
| Oleomargarine |  | .92-. 93 | 20 | 35-38 |  |
| Olive oil |  |  |  | $20 \pm$ | $300 \pm$ |
| Oxalic acid | $\mathrm{C}_{2} \mathrm{H}_{2} \mathrm{O}_{4} \cdot 2 \mathrm{H}_{2} \mathrm{O}$ | 1.68 |  | 190 |  |
| Paraffin wax, soft |  |  |  | $\begin{aligned} & 35-52 \\ & 52-56 \end{aligned}$ | $\begin{array}{r} 350-390 \\ 390-430 \end{array}$ |
| Pyrogallol | $\mathrm{C}_{6} \mathrm{H}_{3}(\mathrm{OH})_{3}$ | 1.46 | 40 | 133 | 293 |
| Spermaceti |  | . 95 | 15 | $45 \pm$ |  |
| Starch | $\mathrm{C}_{6} \mathrm{H}_{10} \mathrm{O}_{5}$ | 1.56 |  | none |  |
| Stearine | $\left(\mathrm{C}_{18} \mathrm{H}_{35} \mathrm{O}_{2}\right)_{3} \mathrm{C}_{3}$ | . 925 | 65 | 71 |  |
| Sugar, cane | $\mathrm{C}_{12} \mathrm{H}_{22} \mathrm{O}_{12}$ | 1.588 |  |  |  |
| Tallow, beef ... |  | . 94 | 15 | $27-38$ |  |
| mutton |  | . 94 | 15 | 32-41 |  |
| Tartaric acid | $\mathrm{C}_{4} \mathrm{H}_{4} \mathrm{O}_{8}$ | 1.754 |  | 170 |  |
| Toluene | $\mathrm{C}_{4} \mathrm{H}_{5} \mathrm{CH}_{3}$ | . 822 | 0 | -92 | 110.31 |
| Xylene (o) | $\mathrm{C}_{6} \mathrm{H}_{4}\left(\mathrm{CH}_{3}\right)_{2}$ | . 863 | 20 | - 28 | 142 |
| (m) | $\mathrm{C}_{6} \mathrm{H}_{4}\left(\mathrm{CH}_{3}\right)_{2}$ | . 864 | 20 | 54 | 140 |
| (p) | $\mathrm{C}_{6} \mathrm{H}_{4}\left(\mathrm{CH}_{3}\right)_{2}$ | . 861 | 20 | 15 | 138 |


|  | Melting points, ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Perce | lage | tal | econd | colum |  |  |  |
| Metals | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| Pb Sn | 327 | 295 | 276 | 262 | 240 | 220 | 190 | 185 | 200 | 216 | 232 |
| Bi | 327 | 290 |  |  | 179 | 145 | 126 | 168 | 205 |  | 271 |
| Te | 327 | 710 | 790 | 880 | 917 | 760 | 600 | 480 | 410 | 425 | 452 |
| Ag | 327 | 460 | 545 | 590 | 620 | 650 | 705 | 775 | 840 | 905 | 961 |
| Na | 327 | 360 | 420 | 400 | 370 | 330 | 290 | 250 | 200 | 130 | 97.5 |
| Cu | 327 | 870 | 920 | 925 | 945 | 950 | 955 | 985 | 1005 | 1020 | 1083 |
| Sb | 327 | 250 | 275 | 330 | 395 | 440 | 490 | 525 | 560 | 600 | 630 |
| Al Sb | 660 | 750 | 840 | 925 | 945 | 950 | 970 | 1000 | 1040 | 1010 | 630 |
| Cu | 660 | 630 | 600 | 560 | 540 | 580 | 610 | 755 | 930 | 1055 | 1083 |
| Au | 660 | 675 | 740 | 800 | 855 | 915 | 970 | 1025 | 1055 | 675 | 1063 |
| Ag | 660 | 625 | 615 | 600 | 590 | 580 | 575 | 570 | 650 | 750 | 961 |
| Zn | 660 | 640 | 620 | 600 | 580 | 560 | 530 | 510 | 475 | 425 | 419 |
| Fe | 660 | 860 | 1015 | 1110 | 1145 | 1145 | 1220 | 1315 | 1425 | 1500 | 1533 |
| Sn | 660 | 645 | 635 | 625 | 620 | 605 | 590 | 570 | 560 | 540 | 232 |
| Sb Bi | 631 | 610 | 590 | 575 | 555 | 540 | 520 | 470 | 405 | 330 | 271 |
| Ag | 631 | 595 | 570 | 545 | 520 | 500 | 505 | 545 | 680 | 850 | 961 |
| Sn | 631 | 600 | 570 | 525 | 480 | 430 | 395 | 350 | 310 | 255 | 232 |
| Zn | 631 | 555 | 510 | 540 | 570 | 565 | 540 | 525 | 510 | 470 | 419 |
| Ni Sn | 1453 | 1380 | 1290 | 1200 | 1235 | 1290 | 1305 | 1230 | 1060 | 800 | 232 |
| Na Bi | 97.5 | 425 | 520 | 590 | 645 | 690 | 720 | 730 | 715 | 570 | 271 |
| Cd | 97.5 | 125 | 185 | 245 | 285 | 325 | 330 | 340 | 360 | 390 | 321 |
| Cd Ag | 321 | 420 | 520 | 610 | 700 | 760 | 805 | 850 | 895 | 940 | 961 |
| T1 | 321 | 300 | 285 | 270 | 262 | 258 | 245 | 230 | 210. | 235 | 303 |
| Zn | 321 | 280 | 270 | 295 | 313 | 327 | 340 | 355 | 370 | 390 | 419 |
| Au Cu | 1063 | 910 | 890 | 895 | 905 | 925 | 975 | 1000 | 1025 | 1060 | 1083 |
| Ag | 1063 | 1062 | 1061 | 1058 | 1054 | 1049 | 1039 | 1025 | 1006 | 982 | 961 |
| Pt | 1063 | 1125 | 1190 | 1250 | 1320 | 1380 | 1455 | 1530 | 1610 | 1685 | 1769 |
| K Na | 63 | 17.5 | -10 | -3.5 | 5 | 11 | 26 | 41 | 58 | 77 | 97.5 |
| Hg | 63 |  |  |  |  | 90 | 110 | 135 | 162 | 265 |  |
| T1 | 63 | 133 | 165 | 188 | 205 | 215 | 220 | 240 | 280 | 305 | 303 |
| CuNi | 1083 | 1180 | 1240 | 1290 | 1320 | 1335 | 1380 | 1410 | 1430 | 1440 | 1453 |
| Ag | 1083 | 1035 | 990 | 945 | 910 | 870 | 830 | 788 | 814 | 875 | 961 |
| Sn | 1083 | 1005 | 890 | 755 | 725 | 680 | 630 | 580 | 530 | 440 | 232 |
| Zn | 1083 | 1040 | 995 | 930 | 900 | 880 | 820 | 780 | 700 | 580 | 419 |
| Ag Zn | 961 | 850 | 755 | 705 | 690 | 660 | 630 | 610 | 570 | 505 | 419 |
| $\mathrm{Sn}^{\text {n }}$ | 961 | 870 | 750 | 630 | 550 | 495 | 450 | 420 | 375 | 300 | 232 |
| Na Hg | 97.5 | 90 | 80 | 70 | 60 | 45 | 22 | 55 | 95 | 215 |  |

TABLE 123.-MELTING POINT ${ }^{\circ} \mathrm{C}$ OF LOW-MELTING-POINT ALLOYS *

|  | $\overbrace{}^{\text {Percent }}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cadmium | 10.8 | 10.2 | 14.8 | 13.1 | 6.2 | 7.1 | 6.7 |  |  |  |
| Tin | 14.2 | 14.3 | 7.0 | 13.8 | 9.4 | - | - |  |  |  |
| Lead | 24.9 | 25.1 | 26.0 | 24.3 | 34.4 | 39.7 | 43.4 |  |  |  |
| Bismuth |  | 50.4 | 52.2 | 48.8 | 50.0 | 53.2 | 49.9 |  |  |  |
| Solidification at | $65.5^{\circ}$ | $67.5^{\circ}$ | $68.5^{\circ}$ | $68.5^{\circ}$ | $76.5^{\circ}$ | $89.5{ }^{\circ}$ | $95^{\circ}$ |  |  |  |
|  |  |  |  |  | Perc |  |  |  |  |  |
| Lead |  | 25.8 | 25.0 | 43.0 | 33.3 | 10.7 | 50.0 | 35.8 | 20.0 | 70.9 |
| Tin | 15.5 | 19.8 | 15.0 | 14.0 | 33.3 | 23.1 | 33.0 | 52.1 | 60.0 | 9.1 |
| Bismuth |  | 54.4 | 60.0 | 43.0 | 33.3 | 66.2 | 17.0 | 12.1 | 20.0 | 20.0 |
| Solidification at |  | $101^{\circ}$ | $125^{\circ}$ | $128^{\circ}$ | $145^{\circ}$ | $148^{\circ}$ | $161^{\circ}$ | $181^{\circ}$ | $182^{\circ}$ | $234^{\circ}$ |

[^62]Values are given, for the more important crystals, of the inversion temperature in ${ }^{\circ} \mathrm{C}$, the heat of inversion in $\mathrm{cal} / \mathrm{g}$ and the inversion volume change in $\mathrm{cm}^{3} / \mathrm{g}$. No monotropic inversions have been included.
$h_{1}$, inversion temperature on heating; m, metastable inversion temperature; e, estimated; g , gradual inversion (not to be confused with slow retarded inversions).


[^63]TABLE 124.-REVERSIBLE TRANSITIONS IN CRYSTALS (continued)

| Substance | Phases | Transition $t^{\circ} \mathrm{C}$ | Pressure atm | Transition heat $\mathrm{cal} / \mathrm{g}$ | Transition volume change $\mathrm{cm}^{3} / \mathrm{g}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C}_{6} \mathrm{H}_{6}$ (Benzene) | I-II | $\{100$ | 11680 | 8.68 | . 0105 |
|  | I-II | \{218 | 11680 | $7.73{ }^{\circ}$ | . $0132^{\text {e }}$ |
|  | L-I | \{ 5.4 | 1 | 30.2 | . 1317 |
|  | L-I | \{218 | 11680 | $33.25{ }^{\text {e }}$ | . $0369{ }^{\text {e }}$ |
|  | L-II | 218 | 11680 | $25.5{ }^{\text {e }}$ | . $0501{ }^{\text {e }}$ |
| $\mathrm{C}_{6} \mathrm{H}_{5} \mathrm{OH}$ (Phenol) | L-I | $\{40.9$ | $1 \frac{1}{1}$ | 29.8 | . 0567 |
|  | L-I | (64 | 2015 | 24.8 | . 0270 |
|  | L-II | 64 | 2015 | 30 | . 0825 |
|  | I-II | 64 | 2015 | 5.2 | . 0555 |
| $\mathrm{CH}_{3} \mathrm{C}_{8} \mathrm{H}_{4} \mathrm{OH}$ (o.Cresol). | L-I | $\{30.8$ | 1 | 33.8 | . 0838 |
|  |  | $\{103.2$ | 5900 | 34.2 | . 0317 |
|  | L-II | 103.2 | 5900 | 35 | . 0555 |
|  | I-II | 103.2 | 5900 | . 8 | . 0238 |
| Camphor \% | I-II | 87.1 | 1 | . 25 | . 00187 |
| $\mathrm{C}_{6} \mathrm{H}_{11} \mathrm{OH}$ | I-II | -9 | 1 | 9.38 |  |
| $\mathrm{C}_{6} \mathrm{H}_{5} \mathrm{NH}_{2} \mathrm{HNO}_{3}$ |  | 97.6 |  |  |  |
| CaSO. |  | 1193 |  |  |  |
| $\mathrm{CaCO}^{\text {- }}$ | I-II | 970 h | high $\mathrm{CO}_{2}$ |  |  |
| $\mathrm{CaO} . \mathrm{SiO}_{2}$ |  | $1190 \pm 10$ |  | Ca. 10 |  |
| $2 \mathrm{CaO} . \mathrm{SiO}_{2}$ |  | 1420, 675 |  |  | 10\%, 675 |
| Co ...... | Curie point | $\sim 1100$ | . . . | 1.3 | .... |
|  | I-II | 1015 |  |  |  |
|  | II-III | 400 |  |  |  |
| CoO | .... | $350 \pm 10$ |  |  |  |
| CoOH | . . . | 223 |  | 11.8 |  |
| CsCl | ... | 460 |  | 8 |  |
| $\mathrm{CsClO}_{4}$ | .... | 219 | .... | . . . | $\ldots$ |
| $\mathrm{Cs}_{2} \mathrm{SO} 4$ | .... | 660 |  |  |  |
| $\mathrm{CsNO}_{3}$ |  | 153.5 | 1 | 4.3 | . 00405 |
| $\mathrm{Cs}_{2} \mathrm{Ca}_{2}\left(\mathrm{SO}_{4}\right)_{3}$ |  | 722 |  |  | .... |
| $\mathrm{Cu}_{2} \mathrm{Br}_{2} \ldots \ldots$ | I-II-III | 390, 470 |  |  |  |
| $\mathrm{Cu}_{2} \mathrm{I}_{2}$ | I-II-III | 402, 440 | 1 |  |  |
|  | II-III | 200 | 9600 | 1.091 | . 00485 |
|  | II-III | 100 | 11560 | . 948 | . 00535 |
| $\mathrm{Cu}_{2} \mathrm{~S}$ |  | 91 | . . . . | 5.6 |  |
| $\mathrm{Cu}_{2} \mathrm{Se}$ |  | 110 | .... | 5.4 | . . . |
| $\mathrm{Cu}_{2} \mathrm{Te}$$\mathrm{Fe} .$. |  | 351, 387 | . . . |  | .... |
|  | Curie point | 730 | . . . | $6.7 \pm$ | . . . |
|  | $\beta-\gamma$ | 920 | . . . | $6.7 \pm$ | . . . |
|  | $\boldsymbol{\gamma} \boldsymbol{\delta}$ | 1400 |  | 2 |  |
| $\mathrm{Fe}_{3} \mathrm{O}_{4}$ | Curie point | $570 \pm$ |  |  | .... |
| $\mathrm{Fe}_{2} \mathrm{O}_{3}$ | II-III | -163 to -148 | .... | 2.25 | . . . . |
|  | I-II | $500 \pm$ | .... | .... | . . . |
|  |  | 140 | .... |  |  |
| FeS FeS 2 | pyrite, marcasite |  | .... | .... | .... |
|  |  | 80 |  | .... | . |
| $\mathrm{Fe}_{3} \mathrm{P}$ |  | 440 | . | . . . | .... |
| $\mathrm{FeTiO}_{3}$ |  | 215 |  |  |  |
| $\mathrm{HgI}_{2}$ | red-yellow | 127.5 | ... | 1.3 | . 00342 |
| $\mathrm{Hg}_{2} \mathrm{I}_{2}$ | green-yellow | . . . |  | . $5 \pm$ | . . . |
| HgS .................. | $\left\{\begin{array}{l}\text { cinnabar } \\ \text { metacinnabar }\end{array}\right\}$ | $386 \pm$ |  |  | .... |
| $\begin{aligned} & \mathrm{ICl}_{\mathrm{KOH}}^{\mathrm{KClO}_{3}} \end{aligned}$ | ruby-brown |  |  |  |  |
|  | I-İI | 248 | 5500 | 27.1 | $\ldots$ |
|  | II-III | $P=5500$ | +10.9t |  |  |
|  | $\Delta v_{i}=.02510$ | $2.2 t \times 10^{-6} \Delta h_{1}$ | ¢ $=.165 \mathrm{a}$ | $0^{\circ}, .281$ | $200^{\circ}$ |
| KClO |  | 295 146.4 |  | - 765 | 00095 |
| $\mathrm{K}_{2} \mathrm{~S}$ | I-II | $\left\{\begin{array}{l} 146.4 \\ t=146.4 \end{array}\right.$ | $4+.0124 p$ | . 765 | . 00095 |
| $\mathrm{KNO}_{3}$ | I-II | $\{127.7$ | 1 | 10.5 | . 00484 |
|  | I-II | $\{128$ | 81 | 10.3 | . 0049 |
|  | I-III | 128 | 81 | 5.6 | . 0138 |
|  | II-III | $\{128$ | 81 | 4.7 | . 0089 |
|  | I-III | $\{21.3$ | 2840 | 1.3 | . 0156 |
|  | III-IV | 21.3 | 2840 | 5.1 | . 0284 |
|  | II-IV | 21.3 | 2840 | 3.8 | . 0440 |
| MITHSONIAN PHYSICAL TABLES | (continucd) |  |  |  |  |

TABLE 124.-REVERSIBLE TRANSITIONS IN CRYSTALS (continued)

| Substance | Phases | $\begin{gathered} \text { Transition } \\ t^{\circ} \mathrm{C} \end{gathered}$ | $\begin{gathered} \text { Pressure } \\ \mathrm{atm} \end{gathered}$ | Transition heat cal $/ \mathrm{g}$ | $\begin{gathered} \text { Transition } \\ \text { volumee } \\ \text { change } \\ \mathrm{cm}^{\mathrm{a}} / \mathrm{g} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{K}_{2} \mathrm{SO}_{4}$ |  | 588 |  | 13 |  |
| KHSO4 | I-II | $\{180.5$ | 17 | . 71 | . 00066 |
|  | 1-11 | $\{198.6$ | 1773 | 2.29 | . 00197 |
|  | II-III | \{164.2 | 11 | 3.61 | . 00566 |
|  | IT-II | $\{118.2$ | 2810 | 3.30 | . 00570 |
|  | II-IV | $\{198.6$ | 1773 | . 166 | . 000113 |
|  | H-IV | \{118.2 | 2810 | . 134 | . 00110 |
|  | I-IV | 198.6 | 1773 | 2.03 | . 00310 |
|  | III-IV | 118.2 | 2810 | 3.44 | . 00680 |
| $\mathrm{KPO}_{3}$ |  | 450 | :... | .... | .... |
| $\mathrm{K}_{4} \mathrm{P}_{2} \mathrm{O}_{7}$ | .... | 278 | :... | .... | .... |
| $\mathrm{K}_{2} \mathrm{CO}_{3}$ |  | 410 |  |  |  |
| KCNS | .... | 143 | 1 | 3.10 | . 00306 |
| $\mathrm{K}^{\mathrm{K}} \mathrm{K}_{2} \mathrm{~Pb}\left(\mathrm{SO}_{4}\right)_{2}$ | .... | 544 | $\ldots$ | .... | .... |
|  | .... | 215 |  |  |  |
| ${ }_{\text {K }} \mathrm{K}_{2} \mathrm{~K}_{2} \mathrm{CrO}_{2} \mathrm{O}_{4}$ | .... | 666 | $\ldots$ | 12.6 |  |
|  | .... | 243 |  | 1.40 |  |
| $\mathrm{K}_{2} \mathrm{MoO}_{4}$ | .... | 327, 454, 477 | $\ldots$ |  |  |
| $\mathrm{K}_{2} \mathrm{WO}_{4}$ | $\ldots$ | 388 | .... | 8.2 |  |
|  | .... | 575 | $\ldots$ | 1.6 |  |
| $\mathrm{K}_{2} \mathrm{Ca}_{2}\left(\mathrm{SO}_{4}\right)_{3}$ | .... | 937 | .... | .... | $\ldots$ |
| $\mathrm{K}_{2} \mathrm{Sr}\left(\mathrm{SO}_{4}\right)_{3}$ | $\ldots$ | 775 | .... | .... |  |
| KLiSO4 | .... | 435 |  |  |  |
| $\mathrm{KNO}_{2}$ | I-II | $\{122.3$ | 5000 | 11.7 | . 0315 |
| $\mathrm{K} \mathrm{O}\left(\mathrm{SiO}_{2}\right)_{2}$ |  | 290 | 100 | ... |  |
| $2 \mathrm{~K}_{2} \mathrm{O}\left(\mathrm{Al}_{2} \mathrm{O}_{3}\right)\left(\mathrm{SiO}_{2}\right)_{4}{ }^{\text {a }}$ | $\ldots$ | 714 | .... | ... |  |
| $\mathrm{LiClO}_{3} \ldots \ldots . . . . .$. | .... | 41.5, 99 | .... |  |  |
| $\mathrm{Li}_{2} \mathrm{SO}_{4} \ldots \ldots \ldots \ldots .$. | .... | 580 | $\ldots$ | $55 \pm 1$ |  |
| $(\mathrm{MgO})_{8}\left(\mathrm{~B}_{3} \mathrm{O}_{3}\right)_{8} \mathrm{MgCl}$ | .... | 266 |  | 1.8 |  |
| $\mathrm{MgO} . \mathrm{SiO}_{2}{ }^{\text {b }}$. $\ldots \ldots \ldots$ | $\ldots$ |  |  | $\ldots$ |  |
| Mn MnSO 4 | $\ldots$ | 742,1191 | $\ldots$ | $\ldots$ |  |
| $\mathrm{MnO}_{2}$ | .... | -185 to -175 |  | . 88 | $\ldots$ |
| MnO | .... | -153 to -163 |  | 2.08 | $\ldots$ |
| $\mathrm{N}_{2}$ | .... | -237.6. | .... | $1.9{ }^{\circ}$ |  |
| NH 4 Cl | I-II | -184.3 | $\ldots$ | $1{ }_{16} 3$ | . 0985 |
| $\mathrm{NH}_{4} \mathrm{Br}$ |  | $-38^{\circ}$ |  |  |  |
|  | I-II | 137.8 | 1 | 7.78 | . 0647 |
| NH4 | I-II | -42.5 ${ }^{\circ} \mathrm{l}$ | 1 | 4.80 | . 0561 |
| $\mathrm{NH}_{4} \mathrm{ClO}_{4}$ |  | 240 |  |  |  |
| NH.HSO4 | I-II-III | 126.2 | 1800 | $\ldots$ |  |
|  | II-III-IV | 176.9 | 5480 |  |  |
| $\left(\mathrm{NH}_{4}\right)_{3} \mathrm{H}\left(\mathrm{SO}_{4}\right)_{2}$ |  | 134 | .... | .... |  |
| NH4CNS | I-II | 120 |  |  |  |
|  | II-III | 87.7 |  | 10.36 | . 0409 |
| $\mathrm{NH}_{4} \mathrm{NO}_{3}$ | L-I | 169.5 | 1 | ${ }_{12}^{12.9}$ |  |
|  | I-II | $\left\{\begin{array}{l}125.5 \\ 186.7\end{array}\right.$ | 8730 | 12.6 | . 00475 |
|  | I-VI | 186.7 | 8730 | 12.3 | . 00855 |
|  | II-VI | \{ 169.2 | 8870 | . 27 | . 00309 |
|  |  | 186.7 | 8730 | . 33 | . 00380 |
|  | II-III | $\{84$ | 83 |  | . 00758 |
|  |  | 63.3 | 830 | 2.48 | . 00925 |
|  | III-IV | $\left\{\begin{array}{l}32 \\ 63.3\end{array}\right.$ | 830 | 4.67 | . 02135 |
|  |  | \{ 63.3 | 830 | 6.51 | . 01210 |
|  | IT-IV | 169.2 | 8870 | 11.84 | . 01267 |
|  | IV-VI | 169.2 | 8870 | 12.1 | . 00958 |
|  | IV-V | -18 | 1 | 1.6 | . 017 |
| NaOH | .... | 300 | .... | 24.7 | .... |
| $\mathrm{NaClO}_{4}$ |  | 308 | $\ldots$ | .... | $\ldots$ |
| $\mathrm{NaClO}_{3}$ |  | 248 |  |  |  |
| $\mathrm{Na}_{2} \mathrm{SO}_{4}$ | IV-III | 185 241 | ..... | $\begin{array}{r} 8.6 \\ 15.5 \end{array}$ | $\begin{aligned} & .0034 \\ & .0070 \end{aligned}$ |
| (continued) |  |  |  |  |  |


| Substance | Phases | Transition <br> $t^{\circ} \mathrm{C}$ | $\underset{\text { atm }}{\substack{\text { Pressure }}}$ | $\begin{gathered} \text { Transition } \\ \text { heat } \\ \text { cal } / \mathrm{g} \end{gathered}$ | Transition change $\mathrm{cm}^{3} / \mathrm{g}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{NaF} . \mathrm{Na}_{2} \mathrm{SO} 4$ | .... | 105 | .... | .... | .... |
| $\mathrm{Na}_{2} \mathrm{CO}_{2} \ldots$ | $\ldots$ | 430 | $\ldots$ |  |  |
| $\mathrm{NaNO}_{3}$ |  | $275{ }^{\circ}$ |  | (8 $\pm 2$ ) | (.0081) |
| $\mathrm{Na}_{2} \mathrm{AlF}_{0}$ |  | 568 | .... | 59 |  |
| $\mathrm{Na}_{2} \mathrm{MoO}_{4}$ |  | 424, 585, 623 | .... |  |  |
| $\mathrm{Na}_{2} \mathrm{WO}_{4}$ | I-L | 581.6 | .... | 25.1 | . 018 |
|  | II-I | 588.8 |  | 3.3 | . 00 |
|  | III-II | 695.5 |  | 19.4 | . 035 |
| NaAlSiO 4 | neph.-carn. carnegieite | $\begin{gathered} 1250 \\ 226,650-690 \end{gathered}$ | $\cdots$ | cal | . |
| $\mathrm{NaC}_{2} \mathrm{H}_{3} \mathrm{O}_{2}{ }^{\text {e }}$ |  | -1988 |  | cal |  |
| Ni | Curie point | 355 | .... | .... |  |
| $\mathrm{Ni}_{3} \mathrm{~S}_{2}$ |  | 545 | .... | .... |  |
| $\mathrm{Ni}_{6} \mathrm{As}_{3}$ |  | 970 |  |  |  |
| Oxygen | I-II | -229.5 | $\ldots$ | 6.2 |  |
|  | II-III | -249.5 |  | . 75 |  |
| Phosphorus | L-I | $\left\{\begin{array}{l}44.2 \\ 196\end{array}\right.$ | 1 | 4.90 | . 0193 |
|  |  | $\int^{196} 1$ | 6000 | 43.9 | . 012846 |
|  | I-II | \{ 68.4 | 12000 | 55.2 | . 00684 |
| PbO | red-yellow | 587 | .... |  | .... |
| PbSO. | , | 870 | .... | 13.4 | .... |
| $\mathrm{PbCrO}_{4}$ | .... | 707, 783 | .... | .... |  |
| PbWO. |  | 877 | . |  |  |
| RbOH | $\ldots$ | 245 | $\ldots$ | 16.8 |  |
| $\mathrm{RbClO}_{4}$ | $\ldots$ | 279 | .... | .... | $\ldots$ |
| $\mathrm{Rb}_{2} \mathrm{SO}_{4}$ | $\ldots$ | 653 | $\ldots$ | $\ldots$ |  |
| $\mathrm{Rb}_{2} \mathrm{Ca}_{2}\left(\mathrm{SO}_{4}\right)_{3}$ |  | 787,915 | .... | .... |  |
| RbLiSO4 |  | 142 | $\ldots$ | $\ldots$ |  |
| $\mathrm{RbNO}_{3}$ | I-II | 219 |  |  |  |
|  | II-III | 164.4 | 1 | 7.12 | . 00688 |
|  |  | 218.6 | 5810 | 5.93 | . 00434 |
| RbCl | ... | 50 | 5525 | .... | .... |
| RbBr | .... | 50 | 4925 | .... | .... |
| RbI |  | 50 | 4050 |  |  |
| Sulphur | 1-II | 95.5 | 1 | 2.7 | $\ldots$ |
|  | L-I-II | 155 | 1410 | .... |  |
| $\mathrm{Sb}_{2} \mathrm{O}_{3}$ | rhomb.-reg. | 570 | .... | $\ldots$ | $\ldots$ |
| $\mathrm{SbCl}_{3} \mathrm{SiO}_{3}$ | I-II-III | 65, 69.5 | $\ldots$ |  |  |
|  | I-II | 573 | .... | 2.6 | $\ldots$ |
|  | I-II | $215{ }^{\text {n }}$ | .... | 2.7 |  |
| $\mathrm{SiO}_{2}{ }^{\wedge}$ | II-IIII | $150{ }^{\text {n }}$ | $\ldots$ | . 63 |  |
| $\mathrm{SiO}_{2}$ | e, ${ }^{\text {a }}$ | 867 | $\ldots$ | $8.7{ }^{\circ}$ | .... |
|  | 0,1 | 1250 |  | $25^{\circ}$ |  |
|  | A, 1 | 1470 | $\ldots$ | $7.5{ }^{\text {e }}$ |  |
| Sn | $\ldots$ | 161 |  | . 2 | small |
|  | .... | 18 | $\ldots$ | 4.4 |  |
| $\mathrm{SnO}_{2}$ | .... | 430,540 | .... | .... |  |
| SrSO4 | .... | 1152 |  | .... |  |
| $\mathrm{SrCO}_{2}$ | .... | 925 | high $\mathrm{CO}_{2}$ | .... | .... |
| T1C1O |  | 226 | . | ... |  |
| TII |  | 173 |  |  |  |
| $\mathrm{TiNO}_{3}$ | I-II | 144.6 | 1 | 2.86 | . 00244 |
|  | II-III | 75 | 1 | . 89 | . 00073 |
| Tl picrate | .... | 44 | .... |  | . 018 |
| T1 | .... | 230 | .... | . $3 \pm$ |  |
| $\mathrm{TiBr}_{4}$ | .... | -15 | $\ldots$ | ... | .... |
| $\mathrm{W}_{2} \mathrm{C}$ | . | 2400 |  |  |  |
| ZnS ${ }^{\text {a }}$ |  | 1020 | .... | $\ldots$ |  |
| $\mathrm{ZrO}_{2}$ | .... | ca 1000 | .... | $\ldots$ | $\ldots$ |

[^64]TABLE 125．－TRANSFORMATION AND MELTING TEMPERATURES OF LIME－ ALUMINA－SILICA COMPOUNDS AND EUTECTIC MIXTURES＊

| Percent |  |  |  |  | Transformation |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Substance |  | CaO | $\mathrm{Al}_{2} \mathrm{O}_{3}$ | $\mathrm{SiO}_{2}$ |  |  |  |  | Temp．${ }^{\circ} \mathrm{C}$ |
| $\mathrm{CaSiO}_{3}$ |  | 48.2 | － | 51.8 | Melting $\dagger$ |  |  |  | $1540 \pm 2$ |
| $\mathrm{CaSiO}_{3}$ |  | 48.2 | － | 51.8 | $\alpha$ to $\beta$ and reverse |  |  |  | $1200 \pm 2$ |
| $\mathrm{Ca}_{2} \mathrm{SiO}_{4}$ |  | 65. | － | 35. | Mclting ．．．．．．．．． |  |  |  | $2130 \pm 10$ |
|  |  | 65. | － | 35. | $\gamma$ to $\beta$ and reverse |  |  |  | 675士5 |
|  |  | 65. | － | 35. | $\beta$ to $a$ and reverse |  |  |  | $1420 \pm 2$ |
| $\mathrm{Ca}_{3} \mathrm{Si}_{2} \mathrm{O}_{7}$ |  | 58.2 | － | 41.8 | Dissociation into C | $\mathrm{O}_{4}$ an | nd liqu | uid．． | $1475 \pm 5$ |
| $\mathrm{Ca}_{3} \mathrm{SiO}_{5}$ |  | 73.6 | － | 26.4 | Dissociation into Ca | $\mathrm{SiO}_{4}$ | and C | aO．． | $1900 \pm 5$ |
| $\mathrm{Ca}_{3} \mathrm{Al}_{2} \mathrm{O}_{0}$ |  | 62.2 | 37.8 | － | Dissociation into Ca | and | liquid |  | 1535土5 |
| $\mathrm{Ca}_{5} \mathrm{Al}_{6} \mathrm{O}_{14}$ |  | 47.8 | 52.2 | － | Melting ．．．．．．．．．． |  |  |  | $1455 \pm 5$ |
| $\mathrm{CaAl}_{2} \mathrm{O}_{4}$ |  | 35.4 | 64.6 | － | Melting |  |  |  | $1600 \pm 5$ |
| $\mathrm{Ca}_{3} \mathrm{Al}_{10} \mathrm{O}_{18}$ |  | 24.8 | 75.2 | － | Melting |  |  |  | $1720 \pm 10$ |
| $\mathrm{Al}_{2} \mathrm{SiO}_{5}$ |  | 8 | 62.8 | 37.1 | Melting |  |  |  | $1816 \pm 10$ |
| $\mathrm{CaAl}_{2} \mathrm{Si}_{2} \mathrm{O}_{8}$ |  | 20.1 | 36.6 | 43.3 | Melting |  |  |  | $1550 \pm 2$ |
| $\mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7}$ |  | 40.8 | 37.2 | 22.0 | Melting |  |  |  | $1590 \pm 2$ |
| $\mathrm{Ca}_{3} \mathrm{Al}_{2} \mathrm{SiO}_{8}$ |  | 50.9 | 30.9 | 18.2 | Dissociation into C and liquid | $\mathrm{O}_{4}+$ | $\mathrm{a}_{2} \mathrm{Al}_{2}$ | ${ }_{2} \mathrm{SiO}_{7}$ | $1335 \pm 5$ |
| Crystalline phases | Eutectics Percent |  |  | Melting lemp． ${ }^{\circ} \mathrm{C}$ | Eutectics Percent |  |  |  | Melting temp． ${ }^{\circ} \mathrm{C}$ |
|  |  | $\overbrace{\mathrm{Al}_{2} \mathrm{O}_{3}}$ | $\mathrm{SiO}_{2}$ |  | Crystalline phases |  |  |  |  |
| $\mathrm{CaSiO}_{3}, \mathrm{SiO}_{2}$ | 37 | － | 63. | 1436 | $\mathrm{CaAl} \mathrm{Si}_{2} \mathrm{O}_{8}$ |  |  |  |  |
| $\left.\mathrm{Ca}, \mathrm{SiO}_{3} \mathrm{O}_{2}\right\}$ | 54.5 |  | 45.5 | 1455士 | $\mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7}$ | 38. | 20. |  | 1265 |
| $\left.3 \mathrm{CaO}, 2 \mathrm{SiO}_{2}\right\}$ | 54.5 | － | 45.5 | $1455 \pm$ | $\mathrm{Ca}_{2} \mathrm{SiO}_{4}$ |  |  |  |  |
| $\left.\begin{array}{l} \mathrm{Ca}_{2} \mathrm{SiO}_{4} \\ \mathrm{CaO} . \end{array}\right\}$ | 67.5 | － | 32.5 | 2065士 | $\left.\begin{array}{l} \mathrm{CaAl}_{2} \mathrm{Si}_{2} \mathrm{O}_{8} \\ \mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7} \end{array}\right\}$ |  |  |  |  |
| $\mathrm{Al}_{2} \mathrm{SiO}_{5}, \mathrm{SiO}_{2}$ | － | 13. | 87. |  | $\left.\begin{array}{l}\mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7} \\ \mathrm{Al}_{2} \mathrm{O}_{3}\end{array}\right\}$ |  |  |  | 1380 |
| $\mathrm{Al}_{2} \mathrm{SiO}_{5}, \mathrm{Al}_{2} \mathrm{O}_{3}$ | － | 64. | 36. | 1810 | $\mathrm{Ca}_{2} \mathrm{SiO}_{4}$ \} |  |  |  |  |
| $\mathrm{CaAl}_{2} \mathrm{Si}_{2} \mathrm{O}_{8}$ | 34.1 | 18.6 | 47.3 | 1299 | $\mathrm{CaAl}_{2} \mathrm{O}_{4}$ | 49.5 | 43.7 | 6.8 | 1335 |
| $\mathrm{CaSiO}_{3},$ | 34.1 | 18.6 | 47.3 | 1299 | $\mathrm{Ca}_{5} \mathrm{Al}_{8} \mathrm{O}_{14}$ |  |  |  |  |
| $\left.\begin{array}{l} \mathrm{CaAl}_{2} \mathrm{Si}_{2} \mathrm{O}_{8} \\ \mathrm{SiO}_{2} \end{array}\right\}$ | 10.5 | 19.5 | 70. | 1359 |  |  |  |  |  |
| $\left.\mathrm{CaAl}_{2} \mathrm{Si}_{2} \mathrm{O}_{8}\right\}$ |  |  |  |  |  |  |  |  |  |
| $\left.\mathrm{SiO}_{2}, \mathrm{CaSiO}_{3}\right\}$ | 23.2 | 14.8 | 62. | 1165 |  |  |  |  |  |
| $\left.\mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7}\right\}$ | 49.6 | 23.7 | 26.7 | 1545 |  | tuple | poin |  |  |
| $\left.\mathrm{Ca}_{2} \mathrm{SiO}_{4}\right\}$ | 49.6 | 23.7 | 26.7 | 1545 | $\mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7}$ |  |  |  |  |
| $\left.\begin{array}{l} \mathrm{Al}_{2} \mathrm{O}_{3} \\ \mathrm{CaAl}_{2} \mathrm{Si}_{2} \mathrm{O}_{8} \end{array}\right\}$ | 19.3 | 39.3 | 41.4 | 1547 | $\begin{aligned} & \mathrm{Ca}_{3} \mathrm{Si}_{2} \mathrm{O}_{7} \\ & \mathrm{Ca}_{2} \mathrm{SiO}_{4} \end{aligned}$ |  | 11.9 | 39.9 | 1335 |
| $\left.\mathrm{CaAl}_{2} \mathrm{Si}_{2} \mathrm{O}_{8}\right\}$ | 9.8 | 19.8 | 70.4 | 1345 | $\mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7}$ |  |  |  |  |
| $\left.\mathrm{Al}_{2} \mathrm{SiO}_{3}, \mathrm{SiO}_{2}\right\}$ | 9.8 | 19.8 | 70.4 | 1345 | $\mathrm{Ca}_{2} \mathrm{SiO}_{4}$ | 48.3 | 42. | 9.7 | 1380 |
| $\mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7}$ | 35. | 50.8 | 14.2 | 1552 | $\mathrm{CaAl}_{2} \mathrm{O}_{4}$ |  |  |  |  |
| $\mathrm{Ca}_{3} \mathrm{Al}_{10} \mathrm{O}_{18}{ }^{8}$ | 35. | 50.8 | 14.2 | 1552 | $\mathrm{CaAl}_{2} \mathrm{Si}_{2} \mathrm{O}_{8}$ |  |  |  |  |
| $\left.\begin{array}{l} \mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7} \\ \mathrm{CaAl}_{2} \mathrm{O}_{4} \end{array}\right\}$ | 37.8 | 52.9 | 9.3 | 1512 | $\mathrm{Al}_{2} \mathrm{O}_{3}$ <br> $\mathrm{Al}_{2} \mathrm{SiO}_{5}$ |  | 36.5 | 47.9 | 1512 |
| $\begin{aligned} & \mathrm{CaAl}_{2} \mathrm{O}_{4} \\ & \mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7} \end{aligned}$ | 37.8 | 52.9 | 9.3 | 1512 | $\begin{aligned} & \mathrm{Al}_{2} \mathrm{SiO}_{5} \\ & \mathrm{Ca}_{3} \mathrm{Al}_{10} \mathrm{O}_{18} \end{aligned}$ |  |  |  |  |
| $\mathrm{CaAl}_{2} \mathrm{O}_{4}$ | 37.5 | 53.2 | 9.3 | 1505 | $\mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7}$ | 31.2 | 44.5 | 24.3 | 1475 |
| $\mathrm{Ca}_{3} \mathrm{Al}_{10} \mathrm{O}_{18}$ |  |  |  |  | $\mathrm{Al}_{2} \mathrm{O}_{3}$ |  |  |  |  |
| $\mathrm{CaAl}_{2} \mathrm{Si}_{2} \mathrm{O}_{8}$ | 30.2 | 36.8 | 33. | 1385 |  |  |  |  |  |
| $\mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7}$ |  |  |  |  |  |  |  |  |  |
| $\left.\begin{array}{l} \mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7} \\ \mathrm{Ca}_{3} \mathrm{Si}_{2} \mathrm{O}_{7} \end{array}\right\}$ | 47.2 | 11.8 | 41. | 1310 |  |  |  |  |  |
| $\mathrm{CaSiO}_{3}$ |  |  |  | 1310 |  | druple | poin |  |  |
| $\left.\begin{array}{l} \mathrm{Ca}_{2} \mathrm{Al}_{2} \mathrm{SiO}_{7} \\ \mathrm{CaSiO}_{3} \end{array}\right\}$ | 45.7 | 13.2 | 41.1 | 1316 | $\left.\begin{array}{l} 3 \mathrm{CaO} .2 \mathrm{SiO}_{2} \\ 2 \mathrm{CaO} . \mathrm{SiO}_{2} \end{array}\right\}$ | 55.5 | － | 44.5 | 1475 |

[^65]
## TABLE 126.—LOWERING OF FREEZING POINTS BY SALTS IN SOLUTION

In the first column is given the number of gram-molecules (anhydrous) dissolved in 1000 $g$ of water; the second contains the molecular lowering of the freezing point ; the freezing point depression is the product of these two columns. After the chemical formula is given the molecular weight. Temperatures in ${ }^{\circ} \mathrm{C}$.


TABLE 126.-LOWERING OF FREEZING POINTS BY SALTS IN SOLUTION (concluded)


## TABLE 127.-RISE OF BOILING POINT PRODUCED BY SALTS DISSOLVED IN WATER

This tables gives the number of g of the salt which, when dissolved in 100 g of water, will raise the boiling point by the amount stated in the headings of the different columns. The pressure is supposed to be 76 cmHg .


Column 1 gives the name of the principal refrigerating substance, $A$ the proportion of that substance, $B$ the proportion of a second substance named in the column, $C$ the proportion of a third substance, $D$ the temperature of the substances before mixture, $E$ the temperature of the mixture, $F$ the lowering of temperature, $G$ the temperature when all snow is melted, when snow is used, and $H$ the amount of heat absorbed in heat units (calories when $A$ is grams). Temperatures are in ${ }^{\circ} \mathrm{C}$.


[^66](For automobile radiators, etc.)


* This table was prepared from data furnished by F. G. Church, of the National Carbon Co., and A. J. Kathman, of Procter \& Gamble Co. † Glycerine and ethylene glycol are practically nonvolatile. All types must be suitably inhibited to prevent cooling-system corrosion. Commercial antifreeze solutions based on ethylene glycol (Prestone) and on glycerine (Zerex) are in use at the present time.


## TABLES 130-141.—HEAT FLOW AND THERMAL CONDUCTIVITY

TABLE 130.-CONVERSION FACTORS BETWEEN UNITS OF HEAT FLOW


TABLE 131.-THERMAL CONDUCTIVITY OF VARIOUS SUBSTANCES
Part 1.-Various Substances

| Substance, temperature ${ }^{\circ} \mathrm{C}$ | $\begin{gathered} k_{1} \\ \mathrm{cgs} \end{gathered}$ | Suhstance temperature ${ }^{\circ} \mathrm{C}$ | $\begin{gathered} k, \\ c g s \end{gathered}$ | Substance <br> temperature ${ }^{\circ} \mathrm{C}$ | $\begin{gathered} k, \\ c g s \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Aniline BP 183, - 160.. | . 000112 | Lime | . 00029 | Quartz $\perp$ to axis, -190. | . 0586 |
| Carbon, gas | . 010 | Mica | . 0018 | "t 10 | . 0173 |
| Carbon, graphite | . 012 | Flagstone $\perp$ to c'eavare. | . 0063 | " , 100 | . 0133 |
| Carborundum | . 00050 | Micaceous $\\|$ to cleavage. | . 0044 | Quartz \\| to axis, 0 | . 0325 |
| Concrete, cinder | . 00022 | Naphthalene MP -160 | . 0013 | Rock salt, 0. Rock salt, 30 | .0167 .0150 |
| Diatomaceous earth | . 00013 | Naphthalene MP 79 | . 00081 | Rubber, vulcanized, |  |
| Earth's crust | . 004 | Naphthol- $\beta$ MP 122, |  | -160 | . 00033 |
| Fire-hrick | . 00028 | -160 | . 00068 | Rubher, 0 | . 00037 |
| Fluorite, -190 | . 093 | Naphthol, 0 | . 00062 | Ruhber, para | . 00045 |
| Fluorite, 0 | . 025 | Nitrophenol MP 114, |  | Sawdust ... | . 00012 |
| Glycerine, - 160 | . 00077 | -160........ | . 00106 | Snow, fresh, dens.=.11. | . 00026 |
| Iceland spar, -190. | . 038 | Nitrophenol. 0 | . 00065 | Vaseline, 20 | . 00022 |
| Iceland spar, 0. | . 0103 | Paraffin MP 54, -160 | .00062 | Vulcanite | . 00087 |

Part 2.-Rocks ${ }^{45}$

${ }^{45}$ Birch, Francis, Handhook of physical constants, Geological Society of America, 1942. Used by permission.

TABLE 132.-THERMAL CONDUCTIVITY OF WATER AND SALT SOLUTIONS

| Substance ${ }^{\circ} \mathrm{C}$ | $\begin{gathered} k t \\ c \mathrm{cgs} \end{gathered}$ | Solution in water | Density | ${ }^{\circ} \mathrm{C}$ | $\begin{gathered} k g \\ \mathrm{cgs} \end{gathered}$ | Solution in water | Density | ${ }^{\circ} \mathrm{C}$ | $\begin{gathered} k t \\ \mathrm{cgs} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\int 0$ | . 00150 | CuSO 4 | 1.160 | 4.4 | . 00118 | $\mathrm{H}_{2} \mathrm{SO}_{4}$ | 1.054 | 20.5 | . 00126 |
| Water 11 | . 00147 | KCl | 1.026 | 13. | . 00116 | -6 | 1.180 | 21. | . 00130 |
| Water $\left\{\begin{array}{l}115 \\ 25\end{array}\right.$ | . 00136 | NaCl | 1.178 | 4.4 | . 00115 | $\mathrm{ZnSO}_{4}$ | 1.134 | 4.5 | . 00118 |
| 20 | . 00143 | " | - | 26.3 | . 00135 | ${ }^{4}$ | 1.136 | 4.5 | . 00115 |

TABLE 133.-CONVERSION FACTORS BETWEEN UNITS OF HEAT FLOW FOR DIFFERENT GRADIENTS

| $\frac{\mathrm{cal}}{\mathrm{sec} \mathrm{cm}}{ }^{2}{ }^{\text {cm }}{ }^{\text {c }}$ | $\frac{\text { watts }}{\mathrm{cm}^{2}} \frac{\mathrm{~cm}}{{ }^{\circ} \mathrm{C}}$ | $\frac{\left.\mathrm{kg} \mathrm{cal}_{\mathrm{hr}} \frac{\mathrm{~m}}{\mathrm{o}^{\mathrm{C}}}\right)}{}$ | $\frac{\text { Btu }}{\mathrm{ft}^{2} \mathrm{hr}} \frac{\mathrm{ft}}{{ }^{\circ} \mathrm{F}}$ | $\frac{\mathrm{hp}}{\mathrm{ft}^{2}} \frac{\mathrm{in}}{{ }^{\circ} \mathrm{C}}$ | $\frac{\mathrm{hp}}{\mathrm{ft}^{2}} \frac{\mathrm{ft}}{{ }^{\mathrm{F}}}$ | $\frac{h p}{f^{2}} \frac{i n}{\sigma_{F}}$ | $\frac{\text { watts }}{\text { in. }^{2}} \frac{\text { in. }}{{ }^{\circ} \mathrm{C}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1 \frac{\mathrm{cal}}{\mathrm{sec} \mathrm{cm}}{ }^{2} \frac{\mathrm{~cm}}{{ }^{\circ} \mathrm{C}}=1$. | 4.185 | 360 | 241.9 | 2.053 | $9.503 \times 10^{-2}$ | 1.141 | 10.63 |
| $1 \frac{\text { watts }}{\mathrm{cm}^{2}} \frac{\mathrm{~cm}}{{ }^{\circ} \mathrm{C}}=.2390$ | 1. | 86.02 | 57.78 | . 4907 | $2.271 \times 10^{-2}$ | . 2727 | 2.540 |
| $1 \frac{\mathrm{~kg} \mathrm{cal}}{\mathrm{hr} \mathrm{m}^{2}} \frac{\mathrm{~m}}{{ }^{\circ} \mathrm{C}}=2.778 \times 10^{-8}$ | $1.163 \times 10^{-2}$ | 1. | $6.720 \times 10^{-1}$ | $5.703 \times 10^{-8}$ | $2.640 \times 10^{-6}$ | $3.170 \times 10^{-8}$ | $2.953 \times 10^{-2}$ |
| $1 \quad \frac{\mathrm{Btu}}{\mathrm{ft}^{2} \mathrm{hr}} \frac{\mathrm{ft}}{{ }^{\circ} \mathrm{F}}=4.134 \times 10^{-3}$ | $1.730 \times 10^{-2}$ | 1.488 | 1. | $8.487 \times 10^{-8}$ | $3.929 \times 10^{-4}$ | $4.717 \times 10^{-8}$ | 4.394 |
| $1 \quad \frac{\mathrm{hp}}{\mathrm{ft}^{2}} \frac{\mathrm{in} .}{{ }^{\circ} \mathrm{C}}=.4871$ | 2.039 | 175.4 | 117.8 | 1. | $4.629 \times 10^{-2}$ | . 5558 | 5.178 |
| $1 \quad \frac{\mathrm{hp}}{\mathrm{ft}^{2}} \frac{\mathrm{ft}}{{ }^{\circ} \mathrm{F}}=10.52$ | 44.03 | 3787. | 2546. | 21.60 | 1. | 12.00 | 111.8 |
| $1 \frac{\mathrm{hp}}{\mathrm{ft}^{2}}{ }^{\circ} \mathrm{in} \mathrm{F}=.8764$ | 3.668 | 315.5 | 212.0 | 1.8 | $8.333 \times 10^{-2}$ | 1. | 9.316 |
| $1 \frac{\text { watts }}{\mathrm{in}^{2}{ }^{2}} \frac{\mathrm{in} .}{{ }^{\circ} \mathrm{C}}=9.407 \times 10^{-2}$ | . 3937 | 33.87 | 22.76 | . 1931 | $8.939 \times 10^{-8}$ | . 1073 | 1. |

## 138 TABLE 134.-THERMAL CONDUCTIVITY, METALS AND ALLOYS

The coefficient $k$ is the quantity of heat in small calories which is transmitted per second through a plate one centimeter thick per square centimeter of its surface when the difference of temperature between the two faces of the plate is $1^{\circ} \mathrm{C}$. The coefficient $k$ is found to vary with the absolute temperature of the plate, and is expressed approximately by the equation $k_{t}=k_{0}\left[1+a\left(t-t_{0}\right)\right]$. $k_{0}$ is the conductivity at $t_{0}$, the lower temperature of the bracketed pairs in the table, $k_{t}$ that at temperature $t$, and $a$ is a constant. $k_{t}$ in g -cal per degree $C$ per sec across $\mathrm{cm}^{3}=0.239 \times k_{t}$ in watts per degree $C$ per sec across $\mathrm{cm}^{3}$.

| Substance | $t^{\circ} \mathrm{C}$ | $\begin{gathered} k t \\ \mathrm{cgs} \end{gathered}$ | a | Substance | $t^{\circ} \mathrm{C}$ | $\begin{gathered} k, \\ \mathrm{cgs} \end{gathered}$ | a |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Aluminum | -190 | 497 |  | Mercury | 0 | . 0148 \} |  |
|  | 30 | . 497 | $+.0030$ |  | 50 | . 0189 \} | $+.0055$ |
| ." | 76.4 | . 550 |  | Molybdenum | 17 | . 346 | -. 0001 |
| Antimony | 100 | . 0442 \} | -. 00104 | Nickel | -160 | $.129$ |  |
| Bismuth . | $\begin{array}{r} 100 \\ -186 \end{array}$ | $\begin{aligned} & .0396\} \\ & .025 \end{aligned}$ | -. 00104 | " | 18 0 | .1420 <br> .125 |  |
| Bismuth | $\begin{array}{r} -186 \\ 18 \end{array}$ | . 025 | . 0021 | " | 100 | . 13885 | $-.00032$ |
| "........ | 100 | . 0161 \} | -. 0021 | " | 200 | . 1325 \} | -. 00095 |
| Brass | -160 | . 181 |  | " | 700 | . 0669 | -. 0009 |
| "، yellow..... | 17 | . 260 |  | " | 1000 1200 | $.064\}$ | $-.00047$ |
| yellow | 0 | . 246 | +.0024 +.0015 | Palladium | 18 | . 1683 |  |
| Cadmium, pure | -160 | . 239 |  |  | 100 | . 182 | +.0010 |
|  | 18 | . 2222 \} | -. 00038 | Platinum | 18 | $\left.\begin{array}{l} .1664 \\ .1733 \end{array}\right\}$ | $+.00051$ |
| ren | 100 | . 215 | -. 00038 | Pt 10\% Ir | 17 | . 074 | $+.0002$ |
| $\begin{aligned} & \text { Constantan } \\ & (60 \mathrm{Cu}+40 \dddot{\mathrm{Ni}}) . . \end{aligned}$ | $\begin{array}{r} 18 \\ 100 \end{array}$ | $\left.\begin{array}{l} .0540 \\ .0640 \end{array}\right\}$ | $+.00227$ | $\mathrm{Pt}^{\text {Pt }} 10 \% \mathrm{Rh}$ | 17 | . 072 | +. 0002 |
| Copper,* pure ... | -160 | . 1.079 | - | Platinoid | 18 | . 060 |  |
|  | 18 | . 918 \} | -. 00013 | Potassium | 57.4 | . 216 | -. 0013 |
| " " .... | 100 | . 908 ) | -.00013 | Rhodium | 17 | . 210 | -. 0010 |
| German silver | 0 | . 070 | $+.0027$ | Silver, pure | -160 | . 998 |  |
| Gold | -190 | . 793 | $-.00007$ | . | 18 | 1.006 | -. 00017 |
| Graphite | 17 17 | . 7035 | $+.0003$ | Sodium |  | .992 .321 | -.00017 |
| Iridium | 17 | . 141 | $-.0005$ |  | 88.1 | . 288 \} | -. 0012 |
| Iron,t pure | 18 | . 161$\}$ |  | Steel | 18 | . 110 | - |
| "', " | 100 | . 151 | . 0008 | Tantalum | 17 | . 130 | -. 0001 |
| Iron, wrought | -160 | . 152 | - | " | 1700 | . 174 | - |
| Iron, polycrystalline |  | 173 |  | " | 1900 2100 | . 186 | $+.00032$ |
| polycrystaline.. <br> Iron, |  |  |  | Tin |  | . 155 | -. 00069 |
| polycrystalline . . | 100 | . 163 | -. 0008 |  | -100 | .145 | -. 00069 |
| Iron, polycrystalline. . | 200 | . 147 | -. 0008 | Tungsten | -160 17 1600 | . 192 | -. 0001 |
| Iron, polycrystalline . . | 800 |  |  | " | 1600 2000 | . 272 \} | $+.00023$ |
| Iron, steel, 1\% ¢ C. . | 18 | . 108 \} | -. 0001 | " | 2400 | . 3134 | $+.00016$ |
|  | 100 -160 | . 1073 | -.0001 | Wood's alloy | 280 | . 319 | - |
| lead, pure |  | .092 .083 |  | Zinc, pure .. |  | . 278 | - |
|  | 100 | . 081 \} | -. 0001 | Zinc, polycrystalli |  | $.2807$ |  |
| Magnesium | $\left.\begin{array}{l} 0 \text { to } \\ 100 \end{array}\right\}$ | . 376 | - | Zinc, |  |  | - |
| Manganin | -160 | . 035 | - | Zinc, |  |  |  |
| " (84 Cu +4 | 18 | . 0519 | $+.0026$ | polycrystallin | 400 | . 231 |  |
| Ni 12 Mn ). | 100 | . 0630 ) | $+.0026$ | Zinc, liquid | 500 | . 144 | - |

[^67]TABLE 135.-THERMAL CONDUCTIVITY OF INSULATING MATERIALS**

|  |  |  | Conductivity |  |
| :---: | :---: | :---: | :---: | :---: |
| Material | $\begin{gathered} \text { Density } \\ \mathrm{g} / \mathrm{cm}^{3} \end{gathered}$ | $t^{\circ} \mathrm{C}$ | $\overbrace{\substack{\text { joule } \\\left(\mathrm{cm}^{2} \text { sec } \\ \mathrm{cm}\right)}}{ }^{\circ} \mathrm{C} /$ | $\underset{\substack{\mathrm{cal} / \mathrm{cm} /{ }^{2} \mathrm{sec} \\(\mathrm{~cm})}}{ }{ }^{\circ} \mathrm{C} /$ |
| Air, 76 cmHg . | . 00129 | 0 | . 00023 | . 000055 |
| Asbestos wool | . 40 | - 100 | . 00068 | . 000162 |
| ". ${ }^{\text {a }}$ | . 40 | 0 | . 00090 | . 000215 |
| " | . 40 | $+100$ | . 00101 | . 00024 |
| " with 85 percent MgO | . 3 | 30 | . 00075 | . 000179 |
| Brick, very porous, dry........... | $.71$ | 20 | . 00174 | . 00042 |
| ". machine-made, dry moist, $1.2 \%$ | $1.54$ | 0 | . 00038 | . 000091 |
| vol. ............................ |  | 50 | . 00096 | . 00023 |
| Calorox, fluffy mineral matter... | . 064 | 30 | . 00032 | . 000076 |
| Celluloid, white | 1.4 | 30 | . 00021 | . 000050 |
| Cement mortar | 2.0 | 90 | . 0055 | . 0013 |
| Chalk |  |  | . 0092 | . 0022 |
| Charcoal | . 18 | 20 | . 00055 | . 00013 |
| Coke dust | 1.0 | 20 | . 0015 | . 00036 |
| Concrete | 1.6 | 0 | . 008 | . 002 |
| Cork | . 05 | 0 | . 00032 | . 000076 |
|  | . 05 | 100 | . 00041 | . 000098 |
| " | . 35 | 0 | . 00061 | . 000146 |
| " $\quad .$. ........................ | . 35 | 100 | . 00079 | . 000189 |
| Cotton, tightly packed. | . 08 | - 150 | . 00038 | . 000091 |
|  | . 08 | 0 +150 | . 000056 | . 0000133 |
| " " " | . 08 | +150 | . 00076 | . 00018 |
| Cotton wool tightly packed..... | . 08 | 30 | . 00042 | . 00010 |
| Diatomite (binders may increase | . 20 | 0 | . 00052 | . 00012 |
| Diatomite, ditto .............. | . 20 | 400 | . 00094 | . 00022 |
|  | . 50 | 0 | . 00086 | . 00021 |
| " ${ }^{\text {" }}$ | . 50 | 400 | . 00157 | . 00037 |
| Ebonite | 1.19 | -190 | . 00138 | . 00033 |
| " | 1.19 | - 78 | . 00157 | . 00038 |
|  | 1.19 | 0 | . 00160 | . 00038 |
| Felt, flax fibers | . 27 | 30 30 | . 00047 | . 000011 |
| wool | . 15 | 40 | . 00063 | . 000151 |
| " | . 33 | 30 | . 00052 | . 000124 |
| Flannel .... |  |  |  | . 000023 |
| Fuller's earth | . 53 | 30 | . 00101 | . 00024 |
| Glass, lead . |  | 15 | . 0060 | . 00143 |
| " soda | 2.59 | 20 | . 0072 | . 00172 |
| " wool | 2.59 .22 | 100 50 | . 0076 | .00182 .000100 |
| " | . 22 | 100 | . 00050 | . 000120 |
| " "، ..................... | . 22 | 200 | . 00065 | . 000155 |
| de 100 mes | . 22 | 300 | . 00081 | . 000195 |
| Graphite, 100 mesh. | . 48 | 40 | . 0018 | . 00044 |
| "، 20 to 40 mesh. | . 42 | 40 40 | . 00388 | . 00093 |
| Horsehair, compressed . | . 17 | 20 | . 00051 | . 000122 |
| Ice | . 92 | 0 | . 022 | . 0053 |
| Leather, chamois |  | 85 | . 00063 | . 000151 |
| " cowhide |  | 85 | . 00176 | . 000421 |
| " sole | 1.0 | 30 | . 0016 | . 00038 |
| Linen |  | 20 | . 00086 | . 00021 |
| Linoleum, cork | . 54 | 20 | . 00080 | . 000191 |
| Mica, average ................... |  | 50 | . 0050 | . 0012 |

[^68](continued)

TABLE 135.-THERMAL CONDUCTIVITY OF INSULATING MATERIALS (continued)


## TABLE 135.-THERMAL CONDUCTIVITY OF INSULATING MATERIALS (concluded)

| Substance | $\underset{\substack{\text { Density } \\ \mathrm{g} / \mathrm{cm}^{3}}}{ }$ | ${ }^{\circ} \mathrm{C}$ | $\begin{aligned} & k t \\ & \mathrm{cgs} \end{aligned}$ | Substance | kg cgs |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Asbestos fiber | . 201 | 500 | . 00019 | Asbestos paper | . 00043 |
| 85\% magnesia asbestos | . 216 | $\left\{\begin{array}{l}100 \\ 500\end{array}\right.$ | . 000016 | Blotting paper | . 00015 |
| Cotton | . 021 | 100 | . 000111 | Portland cement | . 0020 |
|  | . 101 |  | . 000071 | Ebonite, $t, 49^{\circ}$ | . 00037 |
| Eiderdown | . 0021 | 150 | . 00015 | Glass, mean | . 002 |
|  | . 109 |  | . 000046 | Ice ..... | . 0057 |
| Lampblack, Cabot number | . 193 | $\left\{\begin{array}{l}100 \\ 500\end{array}\right.$ | . 0000074 | Leather, cow-hide | . 000042 |
| Quartz, mesh 200. | 1.05 | 500 | . 00024 | Linen | . 00021 |
|  | . 093 | $\{200$ | . 000091 | Silk. | . 000095 |
| Poplox, popped N | . 093 | (500 | . 000160 | Caen stone, limes | $.0043$ |



TABLE 136.-THERMAL CONDUCTIVITY OF VARIOUS SUBSTANCES ${ }^{4 n}$


[^69]TABLE 137.-THERMAL CONDUCTIVITY OF ORGANIC MATERIALS AND WATER
Part 1

| Substance | ${ }^{\circ} \mathrm{C}$ | $\begin{gathered} k t \\ c g s \end{gathered}$ | Substance | ${ }^{\circ} \mathrm{C}$ | $\begin{aligned} & k t \\ & \mathrm{cgs} \end{aligned}$ | Substance | ${ }^{\circ} \mathrm{C}$ | $\begin{aligned} & k t \\ & \mathrm{cgs} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Acetic acid | 9-15 | .0,472 | Carbon disulfide | 0 | .03387 | Oils: olive | - | . 03395 |
| Alcohols: methyl. | 11 | .0:352 | Chloroform | 9-15 | . 03288 | castor |  | . 03425 |
| Alhyl.. | 11 | . $0: 346$ | Ether | 9-15 | . 03303 | Toluene | 0 | . 03349 |
| amyl. | 0 | .0:345 | Glycerine | 25 | . 0368 | Vaseline | 25 | . 0344 |
| Aniline | 0 | .03434 | Oils: petroleum | 13 | .03355 | Xylene | 0 | . 03343 |
| Benzene | 9-15 | .0:333 | turpentine | 13 | . 03325 |  |  |  |

Part 2*

| Substance | ${ }^{\text {Temp. }}$ | Conductivity at 1 atm watt $\mathrm{cm}^{-1}$ $\mathrm{deg}^{-1}$ | Substance | ${ }^{\mathrm{Temp}}{ }^{\circ} \mathrm{C} .$ | Conductivity at 1 atm watt $\mathrm{cm}^{-1}$ $\mathrm{deg}^{-1}$ | Substance | $\stackrel{\text { Temp. }}{{ }^{\circ} \mathrm{C}}$ | Conductivity at 1 atm watt $\mathrm{cm}^{-1}$ $\mathrm{deg}^{-1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Normal pentane. |  | $\begin{aligned} & 1.347 \times 10^{-8} \\ & 1.285 \end{aligned}$ | Carbon disulfide. |  | $\begin{aligned} & 1.599 \times 10^{-3} \\ & 1.515 \end{aligned}$ | Water | $\begin{aligned} & 30 \\ & 75 \end{aligned}$ | $\begin{aligned} & 6.026 \times 10^{-3} \\ & 6.445 \end{aligned}$ |
| Sulfuric ether.. | $\begin{aligned} & 30 \\ & 75 \end{aligned}$ | $\begin{aligned} & 1.377 \\ & 1.347 \end{aligned}$ | Petroleum ether. | 30 75 | $\begin{aligned} & 1.306 \\ & 1.264 \end{aligned}$ | Water | 0 10 20 | $\begin{aligned} & 5.524 \\ & 5.692 \\ & 5.859 \end{aligned}$ |
| Acetone ....... | 30 75 | $\begin{aligned} & 1.795 \\ & 1.687 \end{aligned}$ | Kerosene . . . | 30 75 | 1.494 1.394 |  | $\begin{aligned} & 30 \\ & 30 \\ & 40 \\ & 50 \\ & 60 \\ & 70 \\ & 80 \end{aligned}$ | $\begin{aligned} & 1.026 \\ & 6.194 \\ & 6.361 \\ & 6.529 \\ & 6.696 \\ & 6.863 \end{aligned}$ |

* For reference, see footnote 45 , p. 136.


## TABLE 138.-THERMAL CONDUCTIVITY OF GASES

The conductivity of gases, $k_{t}=\frac{1}{4}(9 \gamma-5) \mu C_{v}$, where $\gamma$ is the ratio of the specific heats, $C_{p} / C_{v}$, and $\mu$ is the viscosity coefficient (Jeans, Dynamical theory of gases, 1916). Theoretically $k_{t}$ should be independent of the density and has been found to be so by Kundt and Warburg and others within a wide range of pressure below one atm. It increases with the temperature.

| Gas | $t^{\circ} \mathrm{C}$ | $\begin{gathered} k t \\ c g s \end{gathered}$ | Gas | $t^{\circ} \mathrm{C}$ | $\begin{gathered} k_{t} \\ c g s \end{gathered}$ | Gas | $t^{\circ} \mathrm{C}$ | $\begin{aligned} & k t \\ & \mathrm{kgs} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 人ir* | -191 | . 0000180 | CO | 100 | . 0000496 | Hg | 203 | . 0000185 |
| '، | 0 | . 0000566 | $\mathrm{C}_{3} \mathrm{H}_{4}$ | 0 | . 0000395 | $\mathrm{N}_{3}$ | -191 | . 0000183 |
| " | 100 | . 0000719 | He | -193 | . 000146 |  |  | . 0000568 |
| A | -183 | . 0000142 |  | 0 | . 000344 | " | 100 | . 0000718 |
|  | 0 | . 0000388 | " | 100 | . 000398 | $\mathrm{O}_{2}$ | -191 | . 0000172 |
| " | 100 | . 0000509 | $\mathrm{H}_{2}$ | -192 | . 000133 |  | 0 | . 0000570 |
| CO | 0 | . 0000542 |  | 0 | . 000416 | " | 100 | . 0000743 |
| CO | - 78 | . 0000219 | C | 100 | . 000499 | NO | 8 | . 000046 |
|  | 0 | . 0000332 | $\mathrm{CH}_{4}$ | 0 | . 0000720 | $\mathrm{N}_{2} \mathrm{O}$ | 0 | . 0000353 |

[^70]The diffusivity of a substance $=h^{2}=k / c \rho$, where $k$ is the conductivity for heat, $c$ the specific heat and $\rho$ the density (Kelvin). The values are mostly for room temperatures, about $18^{\circ} \mathrm{C}$.

| Material | Diffusivity | Material | Diffusivity |
| :---: | :---: | :---: | :---: |
| Aluminum | . 860 | Coal | . 002 |
| Antimony | . 135 | Concrete (cinder) | . 0032 |
| Bismuth | . 069 | Concrete (stone) | . 0048 |
| Brass (yellow) | . 339 | Concrete (light slag) | . 006 |
| Cadmium | 467 | Cork (ground) | . 0017 |
| Copper | 1.140 | Ebonite | . 0010 |
| Gold | 1.209 | Glass (ordinary) | . 0057 |
| Iron (wrought, also | . 173 | Granite | . 0127 |
| Ifon (cast, also $1 \%$ | . 121 | Ice | . 0112 |
| lead | . 245 | Limestone | . 0081 |
| Magnesium | . 932 | Marble (white) | . 0097 |
| Mercury | . 45 | Paraffin | . 00098 |
| Nickel | . 155 | Rock material (earth aver.) | . 0118 |
| Palladium | . 261 | Rock material (crustal rocks) | . 0064 |
| Platinum | . 243 | Sandstone | . 0113 |
| Silver | 1.700 | Snow (fresh) | . 0033 |
| Tin | . 407 | Soil (clay or sand, slightly d | . 005 |
| Zinc | . 413 | Soil (very dry). | . 0031 |
| Air 1 atm | . 179 | Water | . 0017 |
| Asbestos (loose) | . 0025 | Wood (pine, cross grain) | . 00068 |
| Brick (average fire) | . 0052 | Wood (pine with grain). | . 0023 |
| Brick (average build | . 0044 |  |  |

TABLE 140.-THERMAL CONDUCTIVITY—LIQUIDS, PRESSURE EFFECT ${ }^{47}$

| No.* | Liquid | ${ }^{\circ} \mathrm{C}$ | Conduc. tivity at $0 \mathrm{~kg} / \mathrm{cm}^{2}$ (cgs | Conductivity relative to unity ( $0 \mathrm{~kg} / \mathrm{cm}^{2}$ ) as function of pressure in $\mathrm{kg} / \mathrm{cm}^{2}$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 1000 | 2000 | 4000 | 6000 | 8000 | 10000 | 11000 | 12000 |
| 1 | Methyl | 30 | . 000505 | 1.201 | 1.342 | 1.557 | 1.724 | 1.864 | 1.986 | 2.043 | 2.097 |
|  | alcohol | 75 | . 000493 | 1.212 | 1.365 | 1.601 | 1.785 | 1.939 | 2.072 | 2.133 | 2.191 |
| 2 | Ethyl | 30 | . 000430 | 1.221 | 1.363 | 1.574 | 1.744 | 1.888 | 2.014 | 2.070 | 2.122 |
|  | alcohol | 75 | . 000416 | 1.233 | 1.400 | 1.650 | 1.845 | 2.007 | 2.152 | 2.217 | 2.278 |
| 3 | Isopropyl | 30 | . 000367 | 1.205 | 1.352 | 1.570 | 1.743 | 1.894 | 2.028 | 2.091 | 2.150 |
|  | alcohol | 75 | . 000363 | 1.230 | 1.399 | 1.638 | 1.812 | 1.962 | 2.093 | 2.154 | 2.211 |
| 4 | Normal butyl | 30 | . 000400 | 1.181 | 1.307 | 1.495 | 1.648 | 1.780 | 1.900 | 1.955 | 2.008 |
|  | alcohol . . | 75 | . 000391 | 1.218 | 1.358 | 1.559 | 1.720 | 1.859 | 1.985 | 2.043 | 2.099 |
| 5 | Isoamyl | 30 | . 000354 | 1.184 | 1.320 | 1.524 | 1.686 | 1.828 | 1.955 | 2.013 | 2.069 |
|  | alcoho | 75 | . 0000348 | 1.207 | 1.348 | 1.557 | 1.724 | 1.868 | 1.998 | 2.063 | 2.126 |
| 6 | Ether | 30 | . 000329 | 1.305 | 1.509 | 1.800 | 2.009 | 2.177 | 2.322 | 2.388 | 2.451 |
|  |  | 75 | . 000322 | 1.313 | 1.518 | 1.814 | 2.043 | 2.231 | 2.394 | 2.469 | 2.537 |
| 7 | Acetone | 30 | . 000429 | 1.184 | 1.315 | 1.511 | 1.659 | 1.786 | 1.900 | Fr | zes |
|  |  | 75 | . 000403 | 1.181 | 1.325 | 1.554 | 1.738 | 1.891 | 2.024 | 2.083 | 2.137 |
| 8 | Carbo | 30 | $.000382$ | 1.174 | 1.310 | 1.512 | 1.663 | 1.783 | 1.880 | 1.923 | 1.962 |
|  | bisulphide | 75 | $.000362$ | 1.208 | 1.366 | 1.607 | 1.789 | 1.935 | 2.054 | 2.107 | 2.154 |
| 9 | Ethyl | 30 | . 000286 | 1.193 | 1.327 | 1.517 | 1.657 | 1.768 | 1.858 | 1.895 | 1.928 |
|  | bromide | 75 | . 000273 | 1.230 | 1.390 | 1.609 | 1.772 | 1.907 | 2.022 | 2.073 | 2.121 |
| 10 | Ethyl | 30 | . 000265 | 1.125 | 1.232 | 1.394 | 1.509 | 1.592 | 1.662 | 1.694 | 1.724 |
|  | iodide | 75 | . 000261 | 1.148 | 1.265 | 1.442 | 1.570 | 1.671 | 1.757 | 1.799 | 1.837 |
| 11 | Water | 30 | . 00144 | 1.058 | 1.113 | 1.210 | 1.293 | 1.366 | 1.428 | 1.456 | Freez |
|  |  | 75 | . 00154 | 1.065 | 1.123 | 1.225 | 1.308 | 1.379 | 1.445 | 1.476 | 1.506 |
| 12 | Toluol | 30 | . 000364 | 1.159 | 1.286 | 1.470 | 1.604 | 1.716 |  | (2.394 ${ }^{\dagger}$ |  |
|  |  | 75 | . 000339 | 1.210 | 1.355 | 1.573 | 1.738 | 1.872 | 1.987 | 2.039 | 2.089 |
| 13 | Normal | 30 | $.000322$ | 1.281 | 1.483 | 1.777 | 1.987 | 2.163 | 2.325 | 2.404 | 2.481 |
|  | pentane | $75$ | $.000307$ | 1.319 | 1.534 | 1.855 | 2.112 | 2.335 | 2.543 | 2.642 | 2.740 |
| 14 | Petroleum | $30$ | $.000312$ | 1.266 | 1.460 | 1.752 | 1.970 | 2.143 | 2.279 | 2.333 | 2.379 |
|  | ether | $75$ | $.000302$ | 1.268 | 1.466 | 1.780 | 2.026 | 2.232 | 2.409 | 2.488 | 2.561 |
| 15 | Kerosene | 75 | . 000333 | 1.185 | 1.314 | 1.502 | 1.654 | 1.792 | 1.925 | 1.990 | 2.054 |

[^71]
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TABLE 141.-THERMAL RESISTIVITIES AT $20^{\circ} \mathrm{C}$ EXPRESSED IN FOURIERS FOR A cm ${ }^{3}$

The fourier ${ }^{48}$ is defined as that thermal resistance that will transfer heat energy at the rate of 1 joule per sec ( 1 watt) for each degree (C) temperature difference between the terminal surfaces (equivalent roughly to a prism of Ag or Cu 4 cm long by $1 \mathrm{~cm}^{2}$ cross section).

| Silver | . 239 | Water ............ 170 | Rubber * (over |  |
| :---: | :---: | :---: | :---: | :---: |
| Copper | . 258 | Mica* ( $\perp$ to | 90\%) | 700 |
| Aluminum | . 49 | laminations . ..... 200 | Wood (Virginia |  |
| Brass ( $30 \% \mathrm{Zn}$ ) | . 93 | Firebrick * ........ 200 | pine across |  |
| Iron | 1.6 | [Firebrick $25^{\circ} \mathrm{C}$ | grain). | 710 |
| Nickel | 1.7 | to $\left.1000^{\circ} \mathrm{C}\right] \ldots . .$. . 90 | Paper * | 1000 |
| Steel (1\% C) | 2.1 | Brick masonry * .... 250 | Asbestos* (wool) | 1100 |
| Constantan | 4.4 | Leather * . . . . . . . . . 600 | Cork* | 2000 |
| Mercury | 12.0 | Hydrogen .......... 600 | Cotton batting |  |
| [ Ice at $0^{\circ} \mathrm{C}$ ] | 45 | Hard rubber ....... 610 | (loose) ... | 2500 |
| Glass* | 133 | Helium ............ 690 | Wool (loose) | 2500 |
| Concrete* | 140 |  |  | 4100 |
|  |  |  | Carbon dioxide | 6700 |

[^72]TABLE 142.-EXPANSION OF THE ELEMENTS*
Part 1.-Coefficients of linear $\dagger$ thermal expansion of chemical elements (Polycrystalline)

| Element | Temperature or temperature range ${ }^{\circ} \mathrm{C}$ | Coefficient of linear thermal expansion $\times 10^{6}$ per ${ }^{\circ} \mathrm{C}$ |  | Element | Temperature or temperature range ${ }^{\circ} \mathrm{C}$ | Coefficient of linear thermal expansion $\times 10^{8}$ per ${ }^{\circ} \mathrm{C}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Aluminum | -191 to 0 | 18.0 | 1,3** | Gold | -190 to 16 | 13.1 | 1,5, |
|  | +20 to 100 | 23.8 |  |  | 0 to 100 | 14.2 | 30,32 |
|  | 20 to 300 | 25.7 |  |  | 0 to 400 | 14.9 |  |
|  | 20 to 600 | 28.7 |  |  | 0 to 700 | 15.8 |  |
|  |  |  |  |  | 0 to 900 | 16.5 |  |
| Antimony $\ddagger$ | -190 to 20 | 8. to 10. | 4,5,6 |  |  |  |  |
|  | +20 to 100 | 8.4 to 11.0 |  | Indium | -180 to 20 | 26.7 | 33 |
|  | $\begin{aligned} & 20 \text { to } 300 \\ & 20 \text { to } 500 \end{aligned}$ | $\begin{aligned} & 9.2 \text { to } 11.4 \\ & 9.5 \text { to } 11.6 \end{aligned}$ |  |  | +20 to 100 | 30.5 |  |
| Arsenic | 40 | 5.6 | 7 | Iridium | -183 to 19 | 5.7 | 5,34 |
|  |  | 18.1 to 21.0 | 8 |  | 0 to 1000 | 7.9 |  |
| Barium | 0 to 300 | 18.1 to 21.0 | 8 |  | 0 to 1700 | 8.7 |  |
| Beryllium | -120 to 0 | 8.1 | 9,10 |  |  |  |  |
|  | +20 to 100 | 12.3 |  | Iron | -182 to 0 | 9.1 | 1,35 |
|  | 20 to 300 20 to 700 | 14.0 16.8 |  |  | -100 to 0 0 to 20 | 10.4 | 30,36 |
|  | 1200 | 23.7 |  |  | 20 to 100 | 12.1 |  |
|  |  |  |  |  | 20 to 300 | 13.4 |  |
| Bismuth $\ddagger$ | -190 to 17 | 13. to 17. | 5,11 |  | 20 to 600 | 14.7 |  |
|  | - 15 to 100 $+\quad 75$ to 265 | $13.4 \text { to } 14$ |  |  | 20 to 900 | 15.0 |  |
| Boron |  |  |  | Lead | -190 to 20 | 26.7 | 2,5, |
|  | 20 to 750 | 8.3 | 12 |  | +20 to 100 | 29.2 | 37,38, |
| Cadmium | -220 | 20.6 | 13,4 |  | 20 to 200 20 to 300 | 30.0 | 39,40, 41,42 |
|  | $-160$ | 27.4 |  |  | 20 to 300 | 31.3 | 41,42 |
|  | $+\begin{aligned} & 10 \\ & 20\end{aligned}$ to 100 | 29.7 31.8 |  | Lithium | -178 | 17.0 | 43,44 |
|  | 20 to 100 | 31.8 |  |  | - 98 | 36.3 |  |
| Calcium | -150 | 18.0 | 8,14, |  | - 3 | 45.7 |  |
|  | - 50 | 20.9 | 15 |  | 0 to 95 | 56. |  |
|  | $+30$ | 22.5 |  |  |  |  |  |
|  | 20 to 100 0 to 300 | 25.2 22.0 |  | Magnesium | -190 to 20 20 to 100 | 21.3 25.9 | 5,30, 32,39, |
|  | 0 to 300 | 22.0 |  |  | 20 to 100 20 to 300 | 25.9 28.0 | 32,39, 45,46, |
| Carbon ... Diamond | -180 to 0 | . 4 | 16.17, |  | 20 to 500 | 29.8 |  |
|  | 0 to 78 | 1.2 | 18 |  |  |  |  |
|  | 0 to 400 | 2.8 |  | Manganese : |  |  | 46,48 |
|  | 0 to 750 | 4.5 |  | Alpha phase. | -190 to 0 | 15.9 |  |
| Graphite | 20 to 100 | . 6 to 4.3 |  | Alpha phase. | -183 to 0 | 17.6 |  |
|  | 20 to 400 | 1.3 to 4.8 |  |  | 0 to 20 | 22.3 |  |
|  | 20 to 800 | 1.8 to 5.3 |  |  | 0 to 100 | 22.8 |  |
| Chromium |  |  |  |  | 0 to 300 | 25.2 |  |
|  | $\begin{aligned} & -216 \text { to } 0 \\ & -100 \text { to } 0 \end{aligned}$ | 4.1 5.1 | 19,20 | Beta phase.. | -183 to 0 | 12.8 to 20.4 |  |
|  | -ro to 100 | 5.7 to 8.3 |  | Gamma phase. | 0 to 20 -70 to 0 | 18.7 13.6 |  |
|  | 0 to 300 | 7.8 to 8.9 |  | Gamma phase. | - 0 to 20 | 14.8 |  |
|  | 0 to 700 | 9.1 to 10.3 |  |  |  |  |  |
| Cobalt | 20 to 100 | 12.4 | 21,22 | Molybdenum \& . | -190 to 0 | 4.2 |  |
|  | 20 to 400 | 14.0 |  |  | $\begin{array}{r} -100 \text { to } 0 \\ 20 \text { to } 100 \end{array}$ | 3.8 to 5.3 | $\begin{aligned} & 46,49, \\ & 50,51 \end{aligned}$ |
| Copper | -253 to 10 | 11.7 |  |  | 25 to 500 | 4.7 to 5.8 |  |
|  | -191 to 16 | 14.1 | 26,27, |  | 27 to 2127 | 7.2 | 52 |
|  | +25 to 100 | 16.8 | 28,29, | Neodymium | 100 to 260 | . 4 | 52 |
|  | 25 to 300 | 17.8 | 30 |  |  |  |  |
|  | 0 to 500 | 18.2 |  | Nickel | -253 to 10 | 8.1 |  |
|  | 0 to 1000 | 20.3 |  |  | -192 to 16 0 to 100 | 10.0 13.1 | $\begin{gathered} \text { 25,26,27, } \\ 46,53 \mathrm{a}, \end{gathered}$ |
| Germanium | 20 to 230 | 6.0 | 31 |  | 0 to 300 | 14.4 | 118 |
|  | 230 to 450 | 7.3 |  |  | 25 to 600 | 15.5 |  |
|  | 450 to 840 | 7.5 |  |  | 25 to 900 | 16.3 |  |

[^73]
## (continued)


(continued)

Part 2.-Coefficients of linear $\mathbb{I}$ thermal expansion of chemical elements (crystals)


If there is random orientation of the crystals in a polycrystalline element such as antimony or cadmium, the coefficient of linear expansion of the polycrystalline element may be computed from the following equation:

$$
a=\frac{1}{3}(a \|+2 a \perp)
$$

where $a \|$ is the coefficient of linear expansion of the crystal parallel to its axis, and $a \perp$ is the coefficient of linear expansion of the crystal in the direction perpendicular to its axis. (See Part 1 for determined coefficients of linear expansion of polycrystalline elements.)

Part 3.-Coefficients of cublcal thermal expansion of chemical elements


## Authorities

1. Nix and MacNair, 1941; 2. Nix and MacNair, 1942; 3. Hidnert, 1923; 4. Dorsey, 1907 ; 5. Grüneisen, 1910; 6. Hidnert, 1935; 7. Fizeau, 1869; 8. Cath and Steenis, 1936; 9. Hidnert and Sweeney, 1927; 10. Losana, 1939; 11. Jacobs and Goetz, 1937; 12. Dupuy \& Hackspill, 1933; 13. Grüneisen \& Goens, 1924; 14. Erfling, 1942; 15. Bastien, 1934; 16. Röntgen, 1912; 17. Joly, 1898; 18. Hidnert, 1934 ; 19. Erfling, 1939; 20. Hidnert, 1941; 21. Schulze, 1927; 22. Masumoto, 1931; 23. Hidnert and Krider, 1933; 24. Matthies, 1936; 25. Krupkowski, 1929; 26. Henning, 1907; 27. Aoyama and Ito, 1939; 28. Hidnert, 1922; 29. Dittenberger, 1902; 30. Esser and Eusterbrock, 1941 ; 31. Nitka, 1937; 32. Austin, 1932; 33. Hidnert and Blair, 1943; 34. Holborn and Valentiner, 1907; 35. Hidnert, 1942; 36. Souder and Hidnert, 1922; 37. Dorsey, 1908; 38. Lindemann, 1911; 39. Ebert, 1928; 40. Rauramo and Saarialho, 1911; 41. Friend and Vallance, 1924; 42. Hidnert and Sweeney, 1932; 43. Simon and Bergman, 1930; 44. Bridgman, 1936; 45. Hidnert and Sweeney, 1928; 46. Disch, 1921; 47. Schulze, 1921; 48. Erfling, 1940; 49. Schad and Hidnert, 1919; 50. Hidnert and Gero, 1924; 51. Worthing, 1926; 52. Jaeger, Bottema, and Rosenbohm, 1938; 53. Souder and Hidnert, 1922; 53a. Hidnert, 1930; 54. Scheel, 1907; 55. Holzmann, 1931; 56. Scheel and Heuse, 1907; 57. Hagan, 1911; 58. Valentiner and Wallot, 1915; 59. Sweeney, 1929; 60. Ebert, 1938; 61. Hume-Rothery and Lonsdale, 1945 ; 62. Bridgman, 1933; 63. Borelius and Paulson, 1946; 64. Schulze, 1930; 65. Keesom and Jansen, 1927; 66. Scheel, 1921; 67. Owen and Roberts, 1939; 68. Siegel and Quimby, 1938; 69. Hagan, 1883; 70. Hidnert, 1929; 71. Hidnert and Sweeney, 1933; 72. Kroll, 1939; 73. Grube and Vosskühler, 1934; 74. Bochvar and Maurakh, 1930; 75. Hidnert, 1943; 76. Greiner and Ellis, 1948;77. Adenstedt, 1949; 78. Hidnert and Sweeney, 1924; 79. Dodge, 1918; 80. Forsythe, 1927; 81. Worthing, 1917; 82. Souder and Hidnert, 1924; 83. Bauer and Sieglerschmidt, 1929; 84. Bridgman, 1924; 85. Kossolapow and Trapesnikow, 1936: 86. Roberts, 1924; 87. Goetz and Hergenrother, 1932; 88. McLennan and Monkman, 1929; 89. Shinoda, 1934; 90. Kossolapow and Trapesnikow, 1935; 91. Pierry, 1946; 92. Backhurst, 1922; 93. Frevel and Ott, 1935; 94. Shinoda, 1933; 95. Goens and Schmid, 1931; 96. Hill, 1935; 97. Grüneisen and Sckell, 1934; 98. Owen and Roberts, 1937; 99. Becker, 1931; 100. Straumanis, 1940; 101. Bridgman, 1925; 102. Ievens, Straumanis, and Karlsons, 1938; 103. Staker, 1942; 104. Owen and Iball, 1933: 105. Pfaff. 1859; 106. Uffelmann, 1930; 107. Krishnan, 1944; 108. Hack spill, 1913; 109. Klemm, 1931; 110. Richards and Boyer, 1921 ; 111. Dewar, 1902; 112. Sapper and Biltz, 1931; 113. Straumanis and Sauka, 1942; 114. Bernini and Cantoni, 1914; 115. Leduc, 1891; 116. Spring, 1881 ; 117. Griffiths and Griffiths, 1915; 118. Schad, 1927.

## TABLE 143.-COEFFICIENTS OF LINEAR THERMAL EXPANSION OF SOME ALLOYS *

| Alloy $\dagger$ | Temperature or tempera${ }^{\circ} \mathrm{C}$ ture | Coefficient $\ddagger$ of linear thermal ex. $\underset{\text { pansion }}{ } \times{ }^{\circ} \mathrm{C}{ }^{10^{6}}$ | Authority |
| :---: | :---: | :---: | :---: |
| Aluminum-beryllium, 4.2 to 32.7 Be....... | $\begin{aligned} & 20 \text { to } 100 \\ & 20 \text { to } 500 \end{aligned}$ | $\begin{aligned} & 22.4 \text { to } 17.8 \\ & 26.6 \text { to } 22.2 \end{aligned}$ | 1 ** |
| Aluminum-copper, 99.9 $\mathrm{Cu} \ldots \ldots . . . . . . . . .$. |  | $\begin{aligned} & 22.0 \\ & 23.8 \\ & 19.7 \\ & 20.8 \end{aligned}$ | 2 |
|  | $\begin{aligned} & 20 \text { to } 100 \\ & 20 \text { to } 300 \\ & 20 \text { to } 100 \\ & 20 \text { to } 300 \end{aligned}$ | $\begin{aligned} & 21.9 \\ & 23.7 \\ & 18.2 \\ & 19.5 \end{aligned}$ | 2 |
|  | $\begin{aligned} & 20 \text { to } 100 \\ & 20 \text { to } 300 \\ & 20 \text { t } 100 \\ & 20 \text { to } 300 \\ & 20 \text { to } 100 \\ & 20 \text { to } 300 \end{aligned}$ | $\begin{aligned} & 22.2 \text { to } 19.4 \\ & 24.8 \text { to } 22.1 \\ & 18.5 \\ & 19.0 \\ & 14.7 \\ & 17.1 \end{aligned}$ | 3,2 |
| Aluminum-zinc, 0 to 50 Zn . | 20 to 100 | 23.6 to 26.5 | 4 |
| Brass, 3 to 40 Zn ... | $\begin{aligned} & 25 \text { to } 100 \\ & 25 \text { to } 300 \end{aligned}$ | $\begin{aligned} & 16.9 \text { to } 19.7 \\ & 17.7 \text { to } 21.2 \end{aligned}$ | 5 |
| Bronze, 4.2 to 10.1 Sn. | $\begin{aligned} & 25 \text { to } 100 \\ & 25 \text { to } 300 \end{aligned}$ | $\begin{aligned} & 17.1 \text { to } 17.8 \\ & 17.8 \text { to } 19.0 \end{aligned}$ | 5 |
| Cast iron | $\begin{aligned} & 20 \text { to } 100 \\ & 20 \text { to } 400 \end{aligned}$ | $\begin{array}{r} 8.7 \text { to } 11.1 \\ 11.5 \text { to } 12.7 \end{array}$ | 6 |
| Cobalt-iron-chromium, 53.0 to $55.5 \mathrm{Co}, 35.0$ to $37.5 \mathrm{Fe}, 9.0$ to 10.5 Cr . | 20 to 60 | -1.1 to +1.7 | 7 |
| Copper-beryllium, 3.0 Cu . | $\begin{aligned} & 20 \text { to } 100 \\ & 20 \text { to } 300 \end{aligned}$ | $\begin{aligned} & 15.9 \text { to } 17.3 \\ & 16.4 \text { to } 17.4 \end{aligned}$ | 8 |
| Copper-nickel, $\begin{array}{r}19.5 \mathrm{Ni} \\ 49.8 \mathrm{Ni}\end{array}$ | $\begin{array}{r} -182 \text { to } 0 \\ 0 \text { to } 40 \\ -182 \text { to } 0 \\ 0 \text { to } 40 \end{array}$ | $\begin{aligned} & 13.0 \\ & 14.7 \\ & 11.8 \\ & 13.7 \end{aligned}$ | 9 |
| Copper-tin (see Bronze) |  |  |  |
| Copper-zinc (see Brass) |  |  |  |
|  | $\begin{aligned} & 20 \text { to } 300 \\ & 20 \text { to } 300 \end{aligned}$ | $\begin{aligned} & 6.1 \text { to } 6.8 \\ & 8.0 \text { to } 10.0 \end{aligned}$ | 10 |
| Duralumin | $\begin{aligned} & 20 \text { to } 100 \\ & 20 \text { to } 500 \end{aligned}$ | $\begin{aligned} & 21.9 \text { to } 23.8 \\ & 25.4 \text { to } 27.6 \end{aligned}$ | 3 |
| Fernico, 54 Fe , 31 Ni , $15 \mathrm{Co} . . . . . . . . . . . . . .$. | 25 to 300 | 5.0 | 11 |
| Invar, $64 \mathrm{Fe}, 36 \mathrm{Ni}$. | 0 to 100 | 0 to 2 | 12 |
| Iron-aluminum, . 5 to 10.5 Al . . . . . . . . . . . | 20 to 100 | 11.6 to 12.2 | 13 |
| Iron-chromium, 1 to 40 Cr ................. | 20 to 100 | 12.4 to 9.4 | 12 |

[^74](continued)

# TABLE 143.-COEFFICIENTS OF LINEAR THERMAL EXPANSION OF SOME ALLOYS (continued) 

| Alloy | Temperature or temperature range ${ }^{\circ} \mathrm{C}$ | Coefficient of linear thermal expansion $\times 10^{6}$ per ${ }^{\circ} \mathrm{C}$ | Authority |
| :---: | :---: | :---: | :---: |
| Iron-cobalt 9.9 to 49.4 Co. | 30 to 100 | 11.2 to 9.3 | 14 |
| Iron-manganese, 2.8 to 14.4 Mn . | 20 to 100 | 12.7 to 16.9 | 13 |
| Iron-nickel, 3.6 Ni | 20 to 100 | 10.9 | 15, 12, |
| 34.5 Ni | 20 to 100 | 3.7 | 14 |
| 36 Ni | 0 to 100 | 0 to 2 |  |
| 40 to 50 Ni . | 30 to 100 | 4.1 to 9.7 |  |
| Iron-nickel-chromium, 6.6 to $74.7 \mathrm{Fe}, 1.3$ to $70.1 \mathrm{Ni}, 4.9$ to $26.7 \mathrm{Cr} . . . . . . . . . . . . . . .$. | 20 to 100 | 8.7 to 18.4 | 16 |
|  | 20 to 1000 | 13.1 to 20.6 |  |
| Iron-nickel-cobalt, 62.5 to $64.0 \mathrm{Fe}, 30.5$ to $34.0 \mathrm{Ni}, 3.5$ to $6.0 \mathrm{Co...........}. \mathrm{}. \mathrm{}$. | 20 |  | 14,17 |
| 61.3 Fe, 31.8 Ni, 6.0 Co. | 20 to 100 | . 9 | 14,17 |
| 58.7 Fe, 32.4 Ni, 8.2 Co. | 20 to 240 | 2.4 |  |
|  | 20 to 200 | 1.7 |  |
|  | 20 to 295 | 2.6 |  |
| Iron-silicon, 1.0 to 8.4 Si . | 20 to 100 | 12.2 to 11.3 | 13 |
| Kanthal (A, A-1, and D) \%. | 20 to 100 | 11.4 to 11.7 | 18 |
| Kovar (see Fernico) | 20 to 900 | 13.9 to 15.1 |  |
| Lead-antimony, 2.9 to 39.6 Sb . | 20 to 100 | 28.2 to 20.4 | 8 |
| Magnesium-aluminum, $\begin{aligned} & 10.4 \mathrm{Al} \\ & 30 \mathrm{Al} \ldots\end{aligned}$ | 20 to 100 | 25.9 | 19, 20 |
|  | 20 to 200 | 27.2 |  |
|  | 0 to 100 | 23.7 |  |
|  | 0 to 200 | 25.1 |  |
| Magnesium-tin, 20.4 Sn.................... | 30 to 100 | 24.3 | 21 |
|  | 30 to 300 | 24.7 |  |
| 46.3 Sn | 30 to 100 | 21.1 |  |
|  | 30 to 300 | 21.3 |  |
| Magnesium-zinc, 20 Zn | 40 to 100 | 29.5 | 22 |
|  | 40 to 100 | 30.2 |  |
| Manganin | 20 to 100 | 18.1 | 23, 24 |
|  | 0 to 400 | 18.9 |  |
|  | 0 to 800 | 21.1 |  |
| Monel Metal | 25 to 100 | 13.5 to 14.5 | 15,13 |
|  | 25 to 600 | 15.9 to 16.7 |  |
| Nickel-chromium, 20.4 Cr | 20 to 100 | 13.0 | 16,25 |
|  | 20 to 1000 | 17.2 |  |
|  | 20 to 100 | 13.5 |  |
|  | 20 to 1000 | 17.7 |  |
| Nickel silver, 62.0 to $63.2 \mathrm{Cu}, 10.0$ to 20.2 Ni , 17.4 to 27.1 Zn . | 0 to 100 | 14.8 to 15.4 | 26 |
|  | 0 to 400 | 16.8 to 17.4 |  |

[^75]TABLE 143.-COEFFICIENTS OF LINEAR THERMAL EXPANSION OF SOME ALLOYS (concluded)

| Alloy | Temperature or temperature range ${ }^{\circ} \mathrm{C}$ | Coefficient of linear thermal expansion $\times 10^{6}$ per ${ }^{\circ} \mathrm{C}$ | Authority |
| :---: | :---: | :---: | :---: |
| Platinum-iridium, 20 Ir | -190 to 0 | 7.5 | 27 |
|  | 0 to 100 | 8.3 |  |
|  | 0 to 1000 | 9.6 |  |
|  | 0 to 1600 | 10.5 |  |
| Platinum-rhodium, 20 Rh................ | 0 to 500 | 9.6 | 28 |
|  | 0 to 1000 | 10.4 |  |
|  | 0 to 1400 | 11.0 |  |
| SAE carbon steels ll. | 20 to 100 | 8.8 to 14.4 | 12 |
| SAE stainless chromium irons. | 20 to 100 | 9.4 to 10.7 | 12 |
| Speculum metal | 20 to 100 | 16.0 | 29 |
|  | 20 to 100 | 10.0 | 30, 16 |
|  | 20 to 100 | 16.4 |  |
| Stellite, 55 to $80 \mathrm{Co}, 20$ to $40 \mathrm{Cr}, 0$ to 10 W , 0 to 2 C . |  |  | 31 |
|  | $20 \text { to } 600$ | $\begin{aligned} & 11.0 \text { to } 14.1 \\ & 13.6 \text { to } 16.5 \end{aligned}$ | 31 |
| Tantalum carbide | 20 to 2377 | 8.2 | 32 |
| $\begin{aligned} \text { Tungsten carbide } & +5.9 \mathrm{Co} \\ & +13.0 \mathrm{Co}\end{aligned}$ | 20 to 100 | 4.5 | 33 |
|  | 20 to 403 | 5.2 |  |
|  | 20 to 100 | 5.2 |  |
|  | 20 to 400 | 6.0 |  |
| Zinc-aluminum, 22.6 Al. . . . . . . . . . . . . . . . | 20 to 100 | 26.0 | 34.4 |
|  | 20 to 200 | 28.3 |  |
|  | 20 to 100 | 26.5 |  |
|  | 20 to 200 | 27.6 |  |

\# Coefficients of expansion of other S.IE steels (free-cutting, manganese, nickel, nickel-chromium, molybdenum, chromium, chromium-vanadium and chromium-nickel austenitic steels) are given in Metals Handbook of the American Society for Metals.

## Authorities

1. Hidnert and Sweeney, 1927; 2. Kempf, 1933; 3. Hidnert, 1925; 4. Schulze, 1921 ; 5. Hidnert, 1921 ; 6. Bolton, 1936; 7. Masumoto, 1934 ; 8. Hidnert, 1936; 9. Aoyama and Ito, 1938; 10. Hull and Burger, 1934 ; 11. Hull, Burger, and Navias, 1941; 12. Various; 13. Schulze, 1928; 14. Masumoto, 1931 ; 15. Souder and Hidnert, 1922; 16. Hidnert, 1931 ; 17. Scott, 1930; 18. Hidnert, 1938; 19. Hidnert and Sweeney, 1928; 20. Takahasi and Kikuti, 1936; 21. Grube and Vosskuhler, 1934; 22. Grube and Burkhardt, 1929: 23. Schulze, 1933; 24. Ebert, 1935 ; 25. Dean, 1930; 26. Cook, 1936; 27. Physikalische-Technische Reichanstalt, 1920; 28. Day and Sosman, 1910; 29. Scheel, 1921; 30. Hidnert, 1928; 31. Souder and Hidnert, 1921; 32. Becker and Ewest, 1930; 33. Hidnert, 1937; 34. Hidnert, 1924.

TABLE 144.-COEFFICIENTS OF LINEAR THERMAL EXPANSION OF SOME fiISCELLANEOUS MATERIALS *

| Material | Temperature or temperature range ${ }^{\circ} \mathrm{C}$ | Coefficient of linear thermal expansion $\times 10^{8}$ per ${ }^{\circ} \mathrm{C}$ | Au. thority | Material | Tempera. ture or temperature ${ }^{\circ} \mathrm{C}$ C | Coefficient of linear thermal expansion $\times 10^{9}$ per ${ }^{\circ} \mathrm{C}$ | Au. thority |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alum: |  |  | 1** | Mica, muscovite: Parallel to |  |  |  |
| Ammonium | 20 to 50 | 9.5 |  |  |  |  |  |
| Ammonium chrome | 20 to 50 | 10.6 |  | cleavage plane | 0 to 100 | 8.5 | 14 |
| Potassium | 20 to 50 | 11.0 |  | Perpendicular |  |  |  |
| Thallium | 20 to 50 | 13.1 |  | to cleavage |  |  | 15 |
| Amber | 0 to 50 |  |  | plane $\dagger$.. | to 300 | 8 to 25 |  |
|  |  | 53 | 2 |  |  |  |  |
| Bakelite | 20 to 60 | 21 to 33 | 3 | Mica, phlogopite: \|| to cleavage | 0 to 100 | 13.5 | 14 |
|  |  |  |  | plane ..... |  |  |  |
| Beryl <br> Brick, clay build. ing ........ | 20 to 100 | . 3 to 1.6 | 4 | $\perp$ to cleavage plane $\dagger$. | 20 to 100 | 1 to 179 | 15 |
|  | 10 to +40 | 3.0 to 12.4 | 5 |  |  |  |  |
|  | 0 to 500 |  |  | Porcelain | 20 to 200 | 1.6 to 19.6 | 3 |
| Carborundum |  | 8.4 | 6 | Quartz, crystalline |  |  | 16 |
|  | 0 to 1800 | 9.2 |  |  |  |  |  |
| Concrete | 13 to +27 | 6.8 to 12.7 | 7 | \|| to axis ..... | 0 to 100 | 8.0 |  |
|  | 13 to +88 | 7.5 to 14.0 |  |  | 0 to 300 0 to 500 | 9.6 12.2 |  |
| Dental amalgam. | 20 to 50 | 22 to 28 | 8 | $\perp$ to axis | 0 to 100 | 14.4 |  |
|  |  |  |  |  | 0 to 300 | 16.9 |  |
| Glass : <br> Miscellaneous. <br> Pyrex ....... |  |  | 9 | Quartz, fused (silica) | $20 \text { to } 100$$20 \text { to } 1000$ | 20.9 |  |
|  | 0 to 300 | . 8 to 12.8 |  |  |  | $.5$ | 9 |
|  | 20 to 100 20 to 300 | $\begin{aligned} & 3.1 \text { to } 3.5 \\ & 3.0 \text { to } 3.6 \end{aligned}$ |  |  |  |  |  |
| $\begin{aligned} & \text { Granites (Ameri- } \\ & \operatorname{can}) \end{aligned} \text {........ }$ | - 20 to 60 | 4.8 to 8.3 | 10 | Rocks (American): Igneous | $\begin{aligned} & 20 \text { to } 100 \\ & 20 \text { to } 100 \\ & 20 \text { to } 100 \end{aligned}$ | 3.4 to 11.9 | 17 |
|  | $\begin{aligned} & -250 \\ & =200 \\ & =150 \\ & =100 \\ & -\quad 50 \end{aligned}$ | $\begin{array}{r} -6.1 \\ +.8 \\ 16.8 \\ 33.9 \\ 4.9 \\ 52.7 \end{array}$ | 11 |  |  |  | 9 |
|  |  |  |  | Sedimentary.. |  | 2.3 to 11.0 |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  | Rubber (hard) $\ddagger$. | § | 50 to 84 |  |
|  |  |  |  | Slate | 20 to 100 | 6.3 to 8.3 | 17 |
| Magnesia | 20 to 500 | 12.4 | $\begin{array}{r} 6,12 \\ 13 \end{array}$ | Tooth:Root | 20 to 50 | 8.3 | 8 |
| Marble | 20 to 1000 | 13.7 |  |  |  |  |  |
|  | 25 to 100 | 5 to 16 | 3 | Across crown. <br> Root and crown | 20 tc 50 | 11.4 |  |
|  |  |  |  |  |  | 7.8 |  |
|  |  |  |  |  | 20 to 50 |  |  |
|  |  |  |  | Wood: | \$ |  | 9 |
|  |  |  |  | Across grain. . | 8 | $32 \text { to } 73$ | 9 |

[^76] ous temperature ranges between $0^{\circ} \mathrm{C}$ and $100^{\circ} \mathrm{C}$.

## Authorities

1. Klug and Alexander, 1942; 2. Sweeney, 1928; 3. Souder and Hidnert, 1919; 4. Geller and Insley, 1932; 5. Ross, 1941: 6. Ebert and Tingwaldt, 1936; 7. Koenitzer, 1936; 8. Souder and Peters, 1920; 9. Various; 10. Hockman and Kessler, 1950; 11. Jakob and Erk, 1928; 12. White, 1938; 13. Austin, 1931; 14. Ebert, 1935; 15. Hidnert and Dickson, 1945; 16. Compiled by Sosman, 1927; 17. Griffith, 1936.

If $V_{0}$ is the volume at $0^{\circ}$ then at $t^{\circ}$ the expansion formula is $V_{t}=V_{0}(1+a t+$ $\left.\beta t^{2}+\gamma t^{3}\right)$. The table gives values of $\alpha, \beta$ and $\gamma$ and $k$, the true coefficient of cubical expansion, at $20^{\circ}$ for some liquids and solutions. $\Delta t$ is the temperature range of the observation.

\begin{tabular}{|c|c|c|c|c|c|}
\hline Liquid \& ${ }^{\Delta}{ }_{\text {c }}$ C \& a $10^{3}$ \& $\beta 10^{3}$ \& $\gamma 10^{9}$ \& $k$
at $200^{3}$

a <br>
\hline Acetic acid \& 16-107 \& 1.0630 \& . 12636 \& 1.0876 \& 1.071 <br>
\hline Acetone \& 0-54 \& 1.3240 \& 3.8090 \& - . 87983 \& 1.487 <br>
\hline \multicolumn{6}{|l|}{Alcohol: ${ }^{\text {a }}$. ${ }^{\text {a }}$} <br>
\hline Amyl \& -15-80 \& . 9001 \& . 6573 \& 1.18458 \& . 902 <br>
\hline Ethyl, 30\% by vol. \& 18-39 \& . 2928 \& 10.790 \& -11.87 \& <br>
\hline " $50 \%$ " \& 0-39 \& . 7450 \& 1.85 \& . 730 \& <br>
\hline " $99.3 \%$ \& 27-46 \& 1.012 \& 2.20 \& - \& 1.12 <br>
\hline 500 atm pres \& 0-40 \& . 866 \& - \& - \& <br>
\hline " 3000 \& 0-40 \& . 524 \& \& \& <br>
\hline Methyl \& 0-61 \& 1.1342 \& 1.3635 \& . 8741 \& 1.199 <br>
\hline Benzene \& 11-81 \& 1.17626 \& 1.27776 \& . 80648 \& 1.237 <br>
\hline Bromine \& 0-59 \& 1.06218 \& 1.87714 \& - . 30854 \& 1.132 <br>
\hline \multicolumn{6}{|l|}{Calcium chloride :} <br>
\hline $5.8 \%$ solution \& 18-25 \& . 07878 \& 4.2742 \& - \& . 250 <br>
\hline 40.9\% " \& 17-24 \& . 42383 \& . 8571 \& \& . 458 <br>
\hline Carbon disulfide \& -34-60 \& 1.13980 \& 1.37065 \& 1.91225 \& 1.218 <br>
\hline 500 atm pressure \& 0-50 \& . 940 \& - \& - \& <br>
\hline 3000 " " \& 0-50 \& . 581 \& \& \& <br>
\hline Carbon tetrachloride \& 0-76 \& 1.18384 \& . 89881 \& 1.35135 \& 1.236 <br>
\hline Chloroform \& 0-63 \& 1.10715 \& 4.66473 \& - 1.74328 \& 1.273 <br>
\hline Ether \& -15-38 \& 1.51324 \& 2.35918 \& 4.00512 \& 1.656 <br>
\hline Glycerine \& - \& . 4853 \& . 4895 \& - \& . 505 <br>
\hline \multicolumn{6}{|l|}{Hydrochloric acid:} <br>
\hline Mercury ....... \& 0-100 \& . 18182 \& . 0078 \& \& . 18186 <br>
\hline Olive oil \& \& . 6821 \& 1.1405 \& - . 539 \& . 721 <br>
\hline Pentane \& 0-33 \& 1.4646 \& 3.09319 \& 1.6084 \& 1.608 <br>
\hline \multicolumn{6}{|l|}{Potassium chloride: 2605 2080 - 363} <br>
\hline $24.3 \%$
Phenol
solution \& 16-25 \& . 26945 \& 2.080
.10732 \& 4446 \& .353
1.090 <br>
\hline Phenol Petroleum \& 36-157 \& \& \& . 4446 \& 1.050 <br>
\hline Petroleum: ${ }_{\text {Density }} 8467$ \& 24-120 \& . 8994 \& 1.396 \& - \& . 955 <br>
\hline \multicolumn{6}{|l|}{Sodium chloride:} <br>
\hline 20.6\% solution \& 0-29 \& . 3640 \& 1.237 \& - \& . 414 <br>
\hline \multicolumn{6}{|l|}{Sodium sulfate:} <br>
\hline \multicolumn{6}{|l|}{Sulfuric acid:} <br>
\hline 10.9\% solution \& 0-30 \& . 2835 \& 2.580 \& - \& . 387 <br>
\hline 100.0\% \& 0-30 \& . 5758 \& $-.432$ \& \& . 558 <br>
\hline Turpentine \& - 9-106 \& . 9003 \& 1.9595 \& -. 44998 \& . 973 <br>
\hline Water ... \& 0-33 \& -. 06427 \& 8.5053 \& $-6.7900$ \& . 207 <br>
\hline
\end{tabular}

Temperatures in ${ }^{\circ} \mathrm{C}$


## TABLE 147.-SPECIFIC HEAT OF THE CHEMICAL ELEMENTS

When one temperature is given the true specific heat is given, otherwise the mean specific heat cal ${ }^{\circ} \mathrm{C}^{-1} \mathrm{~g}^{-1}$ between the given limits.


TABLE 147.-SPECIFIC HEAT OF THE CHEMICAL ELEMENTS (continued)


TABLE 147.-SPECIFIC HEAT OF THE CHEMICAL ELEMENTS (concluded)

| Element | $t^{\circ} \mathrm{C}$ | Spht | Element | $t^{\circ} \mathrm{C}$ | $\mathrm{Sp}_{\mathrm{p}} \mathrm{ht}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Tellurium | $-188 .+18$ | . 047 | Tungsten | -247.1 | . 0012 |
|  | 15, 100 | . 0483 |  | -218.4 | . 0098 |
|  | 15, 200 | . 0487 |  | -173.1 | . 0205 |
| Thallium | -135 | . 288 |  | -73.1 | . 0288 |
|  |  | . 311 |  | + 26.9 | . 0321 |
|  | 20, 100 | . 0326 |  | 100 | . 0320 |
| Thorium | -253, -196 | . 0197 |  | 500 | . 0344 |
| Thorium | 0, 100 | . 0276 |  | 1000 | . 0367 |
| Tin | . -203.5 | . 0385 |  | 1500 | . 0390 |
|  | -186.7 | . 0422 | Uranium | 0, 98 | . 0280 |
|  | -150 | . 0450 | Vanadium | 0, 100 | . 1153 |
|  | -100 | . 0483 | Zinc | 0, 100 | . 095 |
|  | - 50 | . 0512 |  | -252.4 | . 0071 |
|  | 0 | . 0536 |  | - 201.3 | . 0740 |
|  | + 25 | . 0548 |  | - 100 | . 0814 |
|  | 100 | . 0577 |  | - | . 0871 |
|  | 1100 | . 0758 |  | 0 | . 0913 |
| Titanium | -185, +20 | . 082 |  | 100 | . 0957 |
|  | 0, 100 | . 1125 |  | 300 | . 1043 |
|  |  |  |  | 400 | . 1089 |

TABLE 148.-FORMULAE FOR TRUE SPECIFIC HEATS

| Element |  |  | $\begin{gathered} \text { Range } \\ { }^{\circ} \mathrm{C} \mathrm{C} \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| Antimony | $.0493+$ | . 000012 t | 0-500 |
| Bismuth | $.0292+$ | . $000012 t$ | 0-200 |
| Chromium | $.1055+$ | . $00010 t-.00000015 t^{2}$ | 0-400 |
| Cobalt | $.1000+$ | . 000067 t | 0-400 |
| Copper | $.0915+$ | . $000024 t$ | 0-300 |
| Iron | $.1060+$ | . 000096 t | 0-400 |
| Lead | $.0295+$ | . $00002 t$ | 0-300 |
| Magnesium | . $2370+$ | . $000142 t-.0000001 t^{2}$ | 0-400 |
| Nickel | $.1020+$ | . $000118 t-.00000006 t^{2}$ | 0-300 |
| Platinum | $.03162+$ | $.00000617 t+2.33 \times 10^{-10} t^{2}$ | 0-1625 |
| Silver | $.0556+$ | . 000008 t | 0-400 |
| Tin . | $.0525+$ | . $000052 t$ | 0-200 |
| Zinc | $.0913+$ | . $000044 t$ | 0-300 |

TABLE 149.--HEAT CAPACITIES, TRUE AND MEAN SPECIFIC HEATS, AND LATENT HEATS AT FUSION
The constants $a, b$, and $c$ of the equations for the heat capacity: $W=a+b t+c t^{2}$; for the mean specific heat: $s=a t^{-1}+b+c t$; and for the true specific heat: $s^{\prime}=b+2 c t$; the latent heats at fusion are also given.

| Element | Temperature range | $a$ | $b$ | $c \times 10^{6}$ | Latent heat cal/g | Ele. ment | Tempera ture range ${ }^{\circ} \mathrm{C}$ | $a$ | $b$ | $c \times 10^{6}$ | Latent heat cal/g |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cr | 0-1500 | - | . 10233 | 33.47 | - | Ag | 0-961 | 3. | . 05725 | 5.48 | 26.0 |
| Mo | 0-1500 | - | . 06162 | 10.99 | - |  | 961-1300 | 53.17 | . 00710 | 28.30 |  |
| W | 0-1500 | - | . 03325 | 1.07 | - | $\mathrm{Alu}^{\text {d }}$ | 0-1064 |  | . 03171 | 1.30 | 15.9 |
| Pt | 0-1500 | - | . 03121 | 3.54 | - |  | 1064-1300 | 26.35 | . 01420 | 8.52 | - |
| Sn | 0-232 | - | . 06829 |  | 13.8 | Cu | 0-1084 |  | . 10079 | 3.05 | 41.0 |
|  | 232-1000 | 14.33 | . 07020 | $-18.30$ |  |  | 1084-1300 | 130.74 | -. 04150 | 65.6 |  |
| Bi | 0-270 | - | . 03141 | 5.22 | 10.2 | Mn | 0-1070 | $\bigcirc$ | . 12037 | 25.41 | $36.6$ |
|  | 270-1000 | 10.31 | . 03107 | 5.41 | 10.8 |  | 1130-1210 | $-7.41$ | . 17700 | - | $24.14^{*}$ |
| Cd | 0-321 | - | . 05550 | 6.28 | 10.8 |  | 1230-1250 | 3.83 | . 19800 | 5 4 |  |
|  | 321-1000 | 6.30 | . 06952 | 6.37 | 5 | Ni | 0-320 | - | . 10950 | 52.40 | $56.1{ }^{*}$ |
| Pb | 0-327 | 6.0 | . 03591 | 11.47 | 5.47 |  | 330-1451 | . 4.41 | . 12931 | . 11 | 1.33* |
|  | 327-1000 | 6.07 | . 02920 | $-3.30$ | - |  | 1451-1520 | 50.21 | . 13380 | - | 58.2 |
| Zn | 0-419 | 14.34 | . 08777 | 43.48 -16.10 | 23.0 | Co | $0-950$ $1100-1478$ | 22.00 | .09119 .11043 |  | $\begin{aligned} & 58.2 \\ & 14.70^{*} \end{aligned}$ |
|  | 419-1000 | 14.34 | . 13340 | -16.10 |  |  | $1100-1478$ $1478-1600$ | 22.00 57.72 | .11043 .14720 | 14.57 | $14.70^{*}$ |
| So | $0-630$ $630-1000$ | 39.42 | . 05179 | 3.00 2.96 | 38.9 | Fe | 1478-1600 | 57.72 | .14720 .10545 | 56.84 | 49.4 |
| A] | 0-657 |  | . 22200 | 38.57 | 94.0 |  | 785-919 | $-1.63$ | . 1592 | - | 6.56** |
|  | 657-1000 | 102.39 | . 21870 | 24.00 | - |  | 919-1404 | 18.31 | . 14472 | . 05 | 6.67* |
|  |  |  |  |  |  |  | 1405-1528 | -77.18 | . 21416 | - | 1.94* |
|  |  |  |  |  |  |  | 1528-1600 | 70.03 | . 15012 | - | - |

[^77]|  |  |  |
| :---: | :---: | :---: | :---: | :---: |

Part 2*

|  | $\mathrm{C}_{p}$ (joules per gram) for temperatures in ${ }^{\circ} \mathrm{C}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Compound Mineral -200 | $0^{\circ}$ | $200^{\circ}$ | $400^{\circ}$ | $800^{\circ}$ | $1200^{\circ}$ |
| $\mathrm{Al}_{2} \mathrm{O}_{3} \ldots \ldots . . . .$. corundum ... . 069 | . 72 | 1.00 | 1.10 | 1.19 | 1.26 |
| $\mathrm{Al}_{2} \mathrm{Si}_{2} \mathrm{O}_{7} \cdot 2 \mathrm{H}_{2} \mathrm{O}^{*}$. kaolin | . 99 | 1.17 | 1.35 |  |  |
| $2(\mathrm{AlF}) \mathrm{O} \cdot \mathrm{SiO}_{2}$. . topaz | (.83 a | $50^{\circ}$ ) | . . . |  |  |
| $\mathrm{Be}_{3} \mathrm{Al}_{2} \mathrm{Si}_{6} \mathrm{O}_{18} \ldots \ldots$ beryl | (.84 a |  |  |  |  |
| $\mathrm{CaAl}_{2} \mathrm{Si}_{2} \mathrm{O}_{8} \ldots . . .{ }^{\text {. }}$ anorthite | . 70 | . 95 | 1.05 | 1.17 | 1.27 |
| $\mathrm{CaCO}_{3} \ldots . . . .$. . calcite . . . . . . . 28 | . 793 | 1.00 | 1.13 |  |  |
| $\mathrm{CaF}_{2}$. . . . . . . . . . fluorite . . . . . . 22 | . 85 | . 89 | . 93 | 1.01 | 1.10 |
|  | . 69 | . 98 | 1.06 | 1.15 | 1.20 |
| $\mathrm{CaSO}_{4} \cdot 2 \mathrm{H}_{2} \mathrm{O} \ldots .$. gypsum . . . . . . 322 | 1.03 |  | . . . | . . . |  |
| $\mathrm{CaWO}_{4}$......... scheelite | (. 40 a |  |  |  |  |
| $\mathrm{Fe}_{2} \mathrm{O}_{3} \ldots \ldots . . . .$. hematite | . 61 | . 79 | . 90 | 1.08 |  |
|  | . 606 |  |  |  |  |
| $\beta$ troilite |  | . 635 | . 66 | . 71 |  |
| $\mathrm{FeS}_{2}$. . . . . . . . . pyrite . . . . . . . 075 | . 500 | .59.4 | . 69 | ... |  |
| $\mathrm{H}_{2} \mathrm{O}$. . . . . . . . . . ice .......... . 653 | 2.06 |  |  |  |  |
| HgS ........... a cinnabar | . 214 | . 227 | . 240 |  |  |
| KCl . . . . . . . . . . sylvite . . . . . . . 418 | . 682 | . 715 | . 749 |  |  |
| $\mathrm{KNO}_{3}$. . . . . . . . a niter . . . . . . . 326 |  |  |  |  |  |
| $\beta$ niter | 1.19 |  |  |  |  |
| liquid |  | 1.22 |  |  |  |
| $\mathrm{Mg}_{3} \mathrm{Al}_{2} \mathrm{Si}_{3} \mathrm{O}_{12} \ldots .$. garnet | (. 74 | $58^{\circ}$ ) |  |  |  |
| $\mathrm{MgCO}_{3} \ldots . . . .$. magnesite ... . 161 | . 864 |  |  |  |  |
| $\mathrm{MgO} . . . . . . .$. . periclase . . . . . 066 | . 870 | 1.09 | 1.16 | 1.24 | 1.30 |
| $\mathrm{Mg}_{3} \mathrm{H}_{2} \mathrm{Si}_{4} \mathrm{O}_{12} \ldots .$. talc. |  |  |  |  |  |
| NaCl . . . . . . . . . halite . . . . . . . 466 | . 855 | . 915 | . 975 | 1.095 |  |
| de liquid |  |  |  | 1.14 |  |
| $\mathrm{Na}_{2} \mathrm{~B}_{4} \mathrm{O}_{7} \cdot 10 \mathrm{H}_{2} \mathrm{O}$. borax ...... $\mathrm{ip}^{\text {a }}$ | (.161 | $35^{\circ}$ ) |  | 1.14 |  |
| PbS ............ galena ....... . 142 | . 207 | . 221 | . 235 |  |  |
| $\mathrm{SiO}_{2} \ldots . . . . .$. a quartz ..... . 173 | . 698 | . 969 | 1.129 |  |  |
| $\beta$ quartz $\alpha$ cristobalite . . . crise | . $69{ }^{\circ}$ | $1.01^{\circ}$ |  | 1.174 | 1.327 |
| $\beta$ cristobalite . . . |  |  | $1 . \ddot{0} \dot{4}$ | 1.171 | $1.21{ }^{\circ}$ |
| glass . ....... . 184 | .70 | . 95 | 1.06 | 1.21 | 1.34 |
|  | . 45 | . 53 | . 56 | . 587 | . . . |
| *For reference, see foot note 45, p. 136. |  |  |  |  |  |

(continued)

Part 3

| Rock | $\mathrm{C}_{\mathrm{p}}$ (joules per gram) for temperatures in ${ }^{\circ} \mathrm{C}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $0^{\circ}$ | $200^{\circ}$ | $400^{\circ}$ | $800^{\circ}$ | $1200^{\circ}$ |
| Igneous |  |  |  |  |  |
| $\left.\begin{array}{l} \text { Granite : } \\ 65 \% \text { orthoclase } \\ 25 \% \text { quartz } \\ 9 \% \text { albite } \\ 1 \% \text { magnetite } \end{array}\right\} \text {. }$ | . 65 | . 95 | 1.07 | 1.13 | $\ldots$ |
| Basalt : <br> Syracuse <br> Aetna <br> Kilauea | . 85 | 1.04 | 1.145 | 1.32 | 1.49 |
| Metamorphic Gneiss | . 74 | 1.01 | $\ldots$ | $\ldots$ | $\ldots$ |
| Sandstone: Micaceous Japanese (mean of 4) English (mean of 8) | ( $\begin{aligned} & .93 \\ & .73 \\ & .81 \\ & \text { ( } 81\end{aligned}$ |  |  |  |  |
| Clay, amorphous | . 75 | . 94 | 1.13 | 1.51 | $\ldots$ |
| Limestone <br> English (mean of 3) Japanese (mean of 10) | $(1.00$ (.68 (.83 |  |  |  |  |

TABLE 151.-ATOMIC HEATS $\left(50^{\circ} \mathrm{K}\right)$, SPECIFIC HEATS $\left(50^{\circ} \mathrm{K}\right)$, ATOMIC VOLUMES OF THE ELEMENTS

|  |  |  | \# E 咅 |  | 范 |  |  |  | كِ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Li . . . . . 1924 | 1.35 | 13.0 | Fe | . 0175 | . 98 | 7.1 | Sb | . 0240 | 2.89 | 18.2 |
| Be . . . . 0137 | . 125 | 4.9 | Ni | . 0208 | 1.22 | 6.7 | I | . . 0361 | 4.59 | 25.7 |
| B . . . . 0212 | . 24 | 4.5 | Co | . . 0207 | 1.22 | 6.8 | Te | . . 0288 | 3.68 | 21.2 |
| $\mathrm{C}^{* *} \ldots . .0137$ | . 16 | 5.1 | Cu | . . 0245 | 1.56 | 7.1 | Cs | . . 0513 | 6.82 | 71.0 |
| C $\ddagger$. . . . . 0028 | . 03 | 3.4 | Zn | . 0384 | 2.52 | 9.2 | Ball | . . . 0350 | 4.80 | 36.0 |
| Na ... . 1519 | 3.50 | 23.6 | As | . . 0258 | 1.94 | 15.9 | La | .. . 0322 | 4.60 | 22.6 |
| Mg ... . 0713 | 1.74 | 14.1 | Se | . . 0361 | 2.86 | 18.5 | Ce | .. . 0330 | 4.64 | 20.3 |
| A1 . . . 0413 | 1.12 | 10.0 | Br | . . .0453 | 3.62 | 24.9 | W | . . . 0095 | 1.75 | 9.8 |
| Si§ ... . 0303 | . 86 | 14.2 | Rb | . . 0711 | 6.05 | 55.8 | Os | . . . 0078 | 1.49 | 8.5 |
| Si' . . . 0303 | . 77 | 11.4 | Sr ${ }^{\text {* }}$ | . . 0550 | 4.82 | 34.5 | Ir | . . . 0099 | 1.92 | 8.6 |
| P, yel. . . 0774 | 2.40 | 17.0 | Zr | . . 0262 | 2.38 | 21.8 | Pt | . . 0135 | 2.63 | 9.2 |
| P, red. . . 0431 | 1.34 | 13.5 | Mo | . . . 0141 | 1.36 | 9.3 | Au | .. . 0160 | 3.16 | 10.2 |
| S . . . . 0546 | 1.75 | 16. | Ru | . . 0109 | 1.11 | 9.0 | Hg | . . 0232 | 4.65 | 14.8 |
| Cl .... . 0967 | 3.43 | 24.6 | Rh | . . 0134 | 1.38 | 8.5 | Tl | . . . 0235 | 4.80 | 17.2 |
| K .... . 1280 | 5.01 | 44.7 | Pd | . . 0190 | 2.03 | 9.2 | Pb | . . . 0240 | 4.96 | 18.3 |
| Ca ... . 0714 | 2.86 | 25.9 | Ag | . . 0242 | 2.62 | 10.2 |  | . . 0218 | 4.54 | 21.3 |
| Ti .... . 0205 | . 99 | 10.7 | $\mathrm{Cd}^{\text {d }}$ | . . 0308 | 3.46 | 13.0 | Th | . . 0197 | 4.58 | 21.1 |
| Cr . . . . 0142 | 70 | 7.6 | Sn | . 0286 | 3.41 | 20.3 | U | . . 0138 | 3.30 | 12.8 |
| Mn . . . . 0229 | 1.26 | 7.4 |  |  |  |  |  |  |  |  |
| * cal g ${ }^{-1}{ }^{\circ} \mathrm{C}^{-1}$. | $\dagger$ cal g | atom ${ }^{-1}$ |  | Graphite. | $\ddagger$ Diam |  | § Fused. | \% Crystalliz |  | mpure. |

$(1 \mathrm{cal}=4.1840 \mathrm{~J})$

|  | Specific heat of water |  |  |  |  | Specific heat of mercury |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | C, |  | $C_{p}$ |  | $C_{p}$ |  | $C_{p}$ |  | $C_{p}$ |
| $\stackrel{\text { Temp. }}{{ }^{\circ} \mathrm{C}}$ | ${ }^{\text {cal g }}{ }^{\circ} \mathrm{C}^{-1}$ | ${ }^{\text {Temp. }}{ }^{\circ}$ | ${ }^{\text {cal }} \mathrm{g}^{-1} \mathrm{C}^{-1}$ | $\stackrel{T_{0}}{{ }^{\circ} \mathrm{C}} \mathrm{P} .$ | ${ }^{\text {cal }} \mathrm{C}^{-1}$ | $\stackrel{\text { Temp. }}{{ }^{\circ} \mathrm{C}}$ | ${ }^{\text {cal }} \mathrm{C}^{-1} \mathrm{~g}^{-1}$ | ${ }^{\mathrm{T} e \mathrm{Cmp}} \mathrm{C} .$ | ${ }^{\text {cal }}{ }^{\circ} \mathrm{C}^{-1}$ |
| 0 | 1.0080 | 25 | . 9989 | 70 | 1.0013 | 0 | . 03346 | 90 | . 03277 |
| 5 | 1.0043 | 26 | . 9989 | 75 | 1.0021 | 5 | . 03340 | 100 | . 03269 |
| 10 | 1.0019 | 27 | . 9988 | 80 | 1.0029 | 10 | . 03335 | 110 | . 03262 |
| 15 | 1.0004 | 28 | . 9987 | 85 | 1.0039 | 15 | . 03330 | 120 | . 03255 |
| 16 | 1.0002 | 29 | . 9987 | 90 | 1.0050 | 20 | . 03325 | 130 | . 03248 |
| 17 | 1.0000 | 30 | . 9987 | 95 | 1.0063 | 25 | . 03320 | 140 | . 03241 |
| 18 | . 9998 | 35 | . 9986 | 100 | 1.0076 | 30 | . 03316 | 150 | . 0324 |
| 19 | . 9996 | 40 | . 9987 | 120 | 1.0162* | 35 | . 03312 | 170 | . 0322 |
| 20 | . 9995 | 45 | . 9989 | 140 | 1.0223* | 40 | . 03308 | 190 | . 0320 |
| 21 | . 9993 | 50 | . 9992 | 160 | 1.0285* | 50 | . 03300 | 210 | . 0319 |
| 22 | . 9992 | 55 | . 9996 | 180 | 1.0348* | 60 | . 03294 |  |  |
| 23 | . 9991 | 60 | 1.0001 | 200 | 1.0410* | 70 | . 03289 |  |  |
| 24 | . 9990 | 65 | 1.0006 | 220 | 1.0476* | 80 | . 03284 |  |  |

* Nat. Bur. Standards Journ. Res., RP 1228, vol. 23, p. 197, 1939.
* Barnes-Regnault.

TABLE 153.-SPECIFIC HEAT OF VARIOUS LIQUIDS

| Liquid | ${ }^{\text {Temp }}{ }_{\text {c }}$ | $\begin{gathered} \text { Spec } \\ \text { Seat } \\ \text { cgs } \end{gathered}$ | Liquid |  | ${ }^{\text {Temp }}{ }^{\text {c }}$ | Spec |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alcohol, ethyl | -20 | . 505 | Ethyl ether |  | 0 | . 529 |
|  | 0 | . 548 | Glycerine |  | 15-50 | . 576 |
| " " | 40 | . 648 | $\mathrm{KOH}+30 \mathrm{H}_{2} \mathrm{O}$ |  | 18 | . 876 |
| Alcohol, methyl | 5-10 | . 590 | " +100 " |  | 18 | . 975 |
| Anilin ........ | ${ }_{15}^{15-20}$ | . 601 |  |  | 18 18 | . 942 |
|  | 30 | . 520 | $\mathrm{NaCl}+10 \mathrm{H}_{2} \mathrm{O}$ |  | 18 | . 791 |
| " ... | 50 | . 529 | " + 200 |  | 18 | . 978 |
| Benzole, $\mathrm{C}_{6} \mathrm{H}_{6}$ | 10 | . 340 | Naphthalene, $\mathrm{C}_{10} \mathrm{H}$ |  | 80-85 | . 396 |
|  | 40 | . 423 |  |  | 90-95 | . 409 |
| $\mathrm{C}_{6} \mathrm{H}_{8}$ | 65 | . 482 | Nitrobenzole |  | 14 | . 350 |
| $\mathrm{CaCl}_{2}$, sp. gr. 1.14 | -15 | . 764 |  |  | 28 | . 362 |
|  |  | . 775 | Oils: Castor |  |  | . 434 |
| " " " | +20 | . 787 | Citron |  | 5.4 | . 438 |
| " " " 1.20 | -20 | . 695 | Olive |  | 6.6 | . 471 |
| " " | 0 | . 712 | Sesame |  |  | . 387 |
| " " " | $+20$ | . 725 | Turpentine |  |  | . 411 |
| "، "، "1 1.26 | -20 | . 651 | Petroleum ..... |  | 21-58 | . 511 |
| " " " " | 0 | . 663 | Sea water, sp. gr. | 1.0043. | 17.5 | . 980 |
| " " ${ }^{\text {c }}$ " " | +20 | . 676 | " " " " | 1.0235. | 17.5 | . 938 |
| $\begin{gathered} \mathrm{CuSO}_{4}+50 \mathrm{H}_{2} \mathrm{O} \\ " 200 \\ " 400 " \end{gathered}$ | 12-15 | . 848 | " | 1.0463. | 17.5 | . 903 |
|  | 12-14 | . 951 | Toluol, $\mathrm{C}_{6} \mathrm{H}_{8}$ |  | 10 | . 364 |
| $\underset{\mathrm{C}_{12} \mathrm{H}_{11} \mathrm{~N}}{\text { Diphymine }}$ | 13-17 | . 975 |  |  | 65 85 | . 493 |
|  | 53 | . 464 | $\mathrm{ZnSO}_{4}+50 \mathrm{H}_{2} \mathrm{O}$ |  | 20-52 | . 842 |
|  | 65 | . 482 | " +200 " |  | 20-52 | . 952 |

Expressed in calories so per gram per degree C

| Temp |  |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |

TABLE 155.-HEAT CONTENT OF SATURATED LIQUID AMMONIA
Heat content $=H=\epsilon+p v$, where $\epsilon$ is the internal or intrinsic energy.
Temperature ${ }^{\circ} \mathrm{C} \ldots-50^{\circ}-40^{\circ}-30^{\circ}-20^{\circ}-10^{\circ} \quad 0^{\circ}+10^{\circ}+20^{\circ}+30^{\circ}+40^{\circ}+50^{\circ}$ $H=\epsilon+p v \quad \ldots . .-53.8-43.3-32.6-21.8-11.0 \quad 0.0+11.1+22.4-33.9-45.5-57.4$

TABLE 156.-SPECIFIC HEAT OF MINERALS AND ROCKS

${ }^{50}$ Nat. Bur. Standards Journ. Res., vol. 38, p. 593, 1947.

Part 1

| Gases | $\begin{gathered} \text { Density } \\ \text { (/liter } \\ \text { (normal) } \end{gathered}$ | $\begin{gathered} \text { Heat capacity, } \\ C_{p} \text { in } \mathrm{J} / \mathrm{g} \\ \text { Temperature }{ }^{\circ} \mathrm{C} \end{gathered}$ |  |  | $\begin{gathered} \text { Constants in } \\ C_{p}=a+b T-c T-2 \\ \mathrm{~J} / \mathrm{g}-c{ }^{\text {Cemperature }}= \\ \text { absolute } \end{gathered}$ |  |  | $\begin{aligned} & \text { Tem- } \\ & \text { pera- } \\ & \text { ture } \\ & \text { range } \\ & { }^{\circ} \mathrm{C} \text { C } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0 | 400 | 1200 | a | $10^{3} \mathrm{~b}$ | ${ }^{10-5} c$ |  |
| Air | 1.2920 | 1.004 | 1.057 | 1.16 | . 968 | . 132 | 0 | 0-2000 |
| Ammonia | . 7598 | 2.06 | 2.74 | 3.86 | 1.822 | 1.395 | . 1102 | 0-1500 |
| Argon * | 1.782 | . 521 | . 521 | . 521 | . 521 | 0 | 0 | 0 |
| Bromine | 7.1308 | . 225 | .232 | . 236 | 223 | . 01 | 0 | 0-1400 |
| Carbon dioxide | 1.9630 | . 82 | 1.12 | 1.32 | . 894 | . 7 | . 197 | 0-2000 |
| Carbon monoxide | 1.2492 | 1.04 | 1.103 | 1.245 | . 980 | . 18 | 0 | 0-2000 |
| Chlorine | 3.1638 | . 497 | . 511 | . 537 | . 48 | . 033 | 0 | 0-1700 |
| Fluorine | 1.6954 | . 774 | . 818 | . 906 | . 744 | . 11 | 0 | 0-2700 |
| Helium * | . 1785 | 5.2 | 5.2 | 5.2 | 5.2 | 0 | 0 | $0-$ |
| Hydrogen * H | . 045 | 20.6 | 20.6 | 20.6 | 20.6 |  | 0 | $0-$ |
| $\mathrm{H}_{2}$ | . 0899 | 14.23 | 14.87 | 16.14 | 13.796 | 1.59 | 0 | 0-2000 |
| Hydrogen bromide | 3.6104 | . 363 | . 381 | . 416 | . 352 | . 434 | 0 | 0-1700 |
| Hydrogen chloride | 1.6269 | . 795 | . 834 | . 911 | . 769 | . 096 | 0 | 0-1700 |
| Hydrogen fluoride | . 8926 | 1.431 | 1.50 | $1.63+$ | 1.384 | . 169 | 0 | 0-1700 |
| Hydrogen iodide | 5.7075 | . 234 | . 245 | . 266 | . 227 | . 027 | 0 | 0-1700 |
| Hydrogen sulfide | 1.5203 | 1.025 | 1.21 | 1.527 | . 962 | . 385 | . 0314 | 0-1500 |
| Iodine .... | 11.3250 | . 15 | . 15 | . 15 | . 15 | 0 | 0 | $0-$ |
| Krypton * | 3.7365 | . 25 | . 25 | . 25 | . 25 | 0 | 0 | $0-$ |
| Mercury * Hg | 8.9501 | . 104 | . 104 | . 104 | . 104 | 0 | 0 | $0-$ |
| $\mathrm{Hg}_{2}$ | 17.9003 | . 094 | . 094 | . 094 | . 094 | 0 | 0 | $0-$ |
| Neon * | . 9005 | 1.03 | 1.03 | 1.03 | 1.03 | 0 |  | $0-$ |
| Nitric oxide | 1.3388 | 1.00 | 1.047 | 1.142 | . 968 | . 118 | 0 | 0-2000 |
| Nitrogen | 1.2499 | 1.037 | 1.08 | 1.21 | . 962 | . 167 | -. 021 | 0-1500 |
| Nitrous oxide | 1.9638 | . 85 | . 954 | 1.162 | . 779 | . 26 | 0 | 0-2000 |
| Oxygen | 1.4277 | . 916 | 1.025 | 1.143 | . 944 | . 136 | . 0486 | 0-2000 |
| Phosphorus pentao | 6.3371 |  | 1.084 | 1.084 | 1.084 | 0 | 0 | 360-1100 |
| Potassium * K | 1.744 | . 532 | . 532 | . 532 | . 532 | 0 | 0 |  |
| K | 3.4889 | . 482 | . 482 | . 482 | . 482 | 0 | 0 | 0-1700 |
| Sodium* Na | 1.026 | . 904 | . 904 | . 904 | . 904 | 0 | 0 | 0 |
| $\mathrm{Na}_{2}$ | 2.052 | . 82 | . 82 | . 82 | . 82 | 0 | 0 | $0-$ |
| Sulfur | 2.8607 | . 565 | . 773 | . 589 | . 56 | . 0196 | 0 | 30-2000 |
| Sulfur dioxide | 2.858 | . 61 | . 79 | . 875 | . 762 | . 082 | . 132 | 0-2000 |
| Water |  | 1.847 | 2.052 | 2.478 | 1.69 | . 535 | -. 008 | 0-2000 |
| Xenon * | 5.8579 | . 158 | . 158 | . 158 | . 158 | 0 | 0 | $0-$ |

[^78](continued)

Part 2

| Substance | $\begin{gathered} \text { Range of } \\ \text { temperature }{ }^{\circ} \mathrm{C} \end{gathered}$ | Specific heat (cgs) constant pressure $C_{p}$ | $\begin{gathered} \text { Range of } \\ \text { temperature }{ }^{\circ} \mathrm{C} \end{gathered}$ | Mean ratio of specific heats $C_{p} / C_{v}$ |
| :---: | :---: | :---: | :---: | :---: |
| Acetone, $\mathrm{C}_{3} \mathrm{H}_{6} \mathrm{O}$ | 26-110 | . 3468 |  |  |
| Alcohol, $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{OH}$ | 108-220 | . 4534 | $\begin{array}{r} 53 \\ 100 \end{array}$ | $\begin{aligned} & 1.133 \\ & 1.134 \end{aligned}$ |
| Alcohol, $\mathrm{CH}_{3} \mathrm{OH}$ | 101-223 | . 4580 | 100 | 1.256 |
| Benzene, $\mathrm{C}_{6} \mathrm{H}_{5}$ | $\begin{array}{r} 34-115 \\ 35-180 \\ 116-218 \end{array}$ | $\begin{aligned} & .2990 \\ & .3325 \\ & .3754 \end{aligned}$ | $\begin{aligned} & 20 \\ & 60 \\ & 99.7 \end{aligned}$ | $\begin{aligned} & 1.403 \\ & 1.403 \\ & 1.105 \end{aligned}$ |
| Chloroform, $\mathrm{CHCl}_{3}$ | $\begin{aligned} & 27-118 \\ & 28-189 \end{aligned}$ | $\begin{aligned} & .1441 \\ & .1489 \end{aligned}$ | $\begin{aligned} & 22-78 \\ & 99.8 \end{aligned}$ | $\begin{aligned} & 1.102 \\ & 1.150 \end{aligned}$ |
| Ether, $\mathrm{C}_{4} \mathrm{H}_{10} \mathrm{O}$ | $\begin{aligned} & 69-224 \\ & 25-111 \end{aligned}$ | $\begin{aligned} & .4797 \\ & .4280 \end{aligned}$ | $\begin{aligned} & 42-45 \\ & 12-20 \end{aligned}$ | $\begin{aligned} & 1.029 \\ & 1.024 \end{aligned}$ |
| Hydrochloric acid, HCl . | $\begin{aligned} & 13-100 \\ & 22-214 \end{aligned}$ | $\begin{aligned} & .1940 \\ & .1867 \end{aligned}$ | $\begin{array}{r} 20 \\ 100 \end{array}$ | $\begin{aligned} & 1.389 \\ & 1.400 \end{aligned}$ |
| Mercury |  |  | 310 | 1.666 |
| Water vapor, $\mathrm{H}_{2} \mathrm{O}$. | $\begin{array}{r} 0 \\ \cdots \\ \\ \\ 180 \end{array}$ | $\begin{aligned} & .4655 \\ & .421 \\ & .51 \end{aligned}$ | $\begin{array}{r} 78 \\ 94 \\ 100 \end{array}$ | $\begin{aligned} & 1.274 \\ & 1.33 \\ & 1.305 \end{aligned}$ |

TABLE 158.-SPECIFIC HEAT OF SILICATES


TABLE 159.-LATENT HEAT OF FUSION AND VAPORIZATION ${ }^{51}$
( $\mathrm{Kg} \mathrm{cal} / \mathrm{mol}$ )
Part 1

| Metals | L.m | $L_{v}$ | Ionic <br> sulistances | I.m | $\mathrm{L}_{\mathrm{v}}$ | Molecular sulistances | Lm | $L_{v}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Al | . 2.55 | 67.6 | AgBr | 2.18 |  | A | . 280 | 1.88 |
| Ag | 2.70. | 69.4 | AgCl | 3.15 |  | $\mathrm{CCl}_{4}$ | . 577. | 8.0 |
| Au | 3.03 | 90.7 | $\mathrm{AgNO}_{3}$ | 2.76 |  | $\mathrm{CH}_{4}$ | 224. | 2.33 |
| Bi | 2.51 | 47.8 | $\mathrm{BaCl}_{2}$. | 5.75 |  | $\mathrm{C}_{\mathrm{n}} \mathrm{H}_{4}$ | 2.35 | 8.3 |
| Cd | 1.46. | 27.0 | $\mathrm{CaCl}_{2}$ | 6.03 |  | $\mathrm{CH}_{3} \mathrm{COOH}$ | 2.64 | 20.3 |
| Co | 3.66. |  | $\mathrm{HgBr}_{2}$ | 4.62 |  | $\mathrm{CH}: \mathrm{OH}$ | . 525. | 9.2 |
| Cr | 3.93. | 89.4 | $\mathrm{HgI}_{2}$ | 4.50 |  | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{OH}$ | 1.10 | 10.4 |
| Cs | . 50 | 18.7 | KBr | 2.84 | 159 | $\mathrm{Cl}_{2}$ | 1.63 | 7.43 |
| Cu | 3.11. | 81.7 | KCl | 6.41 | 165 | CO | . 200. | 1.90 |
| Fe | 3.56. | 96.5 | $\mathrm{K}_{2} \mathrm{Cr}_{2} \mathrm{O}_{7}$ | 8.77 |  | $\mathrm{CO}_{2}$ | 1.99 | 6.44 |
| Ga | 1.34. |  | KF | 6.28. | 190 | $\mathrm{H}_{2}$ | . 028. | . 22 |
| Hg | . 58. | 15.5 | $\mathrm{KNO}_{3}$ | 2.57 |  | HPr | . 620 | 5.79 |
| In | . 78. |  | KOH | 1.61 |  | HCl | . 506. | 4.85 |
| K | . 58. | 21.9 | LiNO: | 6.06 |  | $\mathrm{H}_{2} \mathrm{O}$ | 1.43 | 11.3 |
| Mg | 1.16 | 34.4 | NaCl | 7.22 | 183 | $\mathrm{N}_{2}$. | . 218. | 1.69 |
| Mn | 3.45 | 69.7 | NaF | 7.81. | 213 | $\mathrm{NH}_{3}$ | 1.84 | 7.14 |
| Na | . 63. | 26.2 | $\mathrm{NaClO}_{3}$ | 5.29 |  | NO | . 551. | 3.82 |
| Ni | 4.20 | 98.1 | $\mathrm{NaNO}_{3}$ | 3.76 |  | $\mathrm{O}_{2}$ | . 096. | 2.08 |
| Pb | 1.22 | 46.7 | NaOH | 1.60 |  |  |  |  |
| Pt | 5.33. | 125. | $\mathrm{PbBr}_{2}$ | 4.29. |  |  |  |  |
| Rb | . 53. | 20.6 | $\mathrm{PbCl}_{2}$ | 5.65. |  |  |  |  |
| Sb | 4.77 | 54.4 | $\mathrm{PbI}_{2}$ | 5.18. |  |  |  |  |
| Sc | 1.22. |  | ${ }^{\mathrm{T} 1 \mathrm{Br}}$ | 5.99 |  |  |  |  |
| Sn | 1.72. |  | TlCl . | 4.26. |  |  |  |  |
| T1 | . 76. | 43.0 |  |  |  |  |  |  |
| Zn | 1.60 | 31.4 |  |  |  |  |  |  |

Part 2

| Substance |
| :---: | :---: | :---: | :---: | :---: |

[^79]| Element | $t^{\circ} \mathrm{C}$ | Cal/g | Element | $t^{\circ} \mathrm{C}$ | $\mathrm{Cal} / \mathrm{g}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Sb | 755 | 320 | I .... | 174 | 24 |
| A | 1 atm . | 37.6 | Kr | - 151 | 28 |
| Ba | 1537 | 308 | Pb | 1170 | 175 |
| Bi | 920 | 190 | Li | 1336 | 511 |
| Br | $60 \pm$ | 43 | Mg | 1110 | 136 |
| Cd | 778 | 240 | Hg | 358 | 71 |
| Ca | 143.9 | 101 | N | - 195.6 | 47.6 |
| Cl | - 63 | 63 | $\mathrm{O}_{2}$ | - 182.9 | 50.9 |
| F | - 188.2 | 40.5 | Sr | 1336 | 410 |
| He | - 271.3 | 5.6 | Xe | - 108.6 | 25.1 |
| $\mathrm{H}_{2}$ | - 253 | 108 | Zn | 918 | 475 |

TABLE 161.-LATENT HEAT OF VAPORIZATION OF LIQUIDS

| Substance | Formula | $t^{\circ} \mathrm{C}$ | Latent heat vaporization cal/g | Total heat from $0^{\circ} \mathrm{C}$ $\mathrm{cal} / \mathrm{g}$ |
| :---: | :---: | :---: | :---: | :---: |
| Alcohol: Ethyl | $\mathrm{C}_{2} \mathrm{H}_{0} \mathrm{O}$ | 78.1 | 205 | 255 |
|  |  | 0 | 236 | 236 |
|  | " | 100 |  | 267 |
|  | " | 150 |  | 285 |
| Methyl | CH4O | 64.5 | 267 | 307 |
|  |  | 0 | 289 |  |
|  | " | 100 | 246 | ... |
|  | " | 150 | 206 |  |
|  | " | 200 | 152 |  |
|  | " | 238.5 | 44.2 |  |
| Aniline | $\mathrm{C}_{6} \mathrm{H}_{7} \mathrm{~N}$ | 184 | 110 |  |
| Benzene | $\mathrm{C}_{6} \mathrm{H}_{6}$ | 80.1 | 92.9 | 127.9 |
| Carbon dioxide, solid | $\mathrm{CO}_{4}$ |  |  | 138.7 |
|  |  | -25 | 72.23 | ... |
|  | " | ${ }^{0}$ | 57.48 | $\cdots$ |
|  | " | 12.35 | 44.97 | ... |
|  | " | 22.04 | 31.8 |  |
|  | " | 30.82 | 3.72 |  |
| disulfide | $\mathrm{CS}_{2}$ | 46.1 | 83.8 | 94.8 |
|  |  | 0 | 90 |  |
|  |  | 100 |  | 100.5 |
| Chloroform | $\mathrm{CHCl}_{3}$ | 60.9 | 58.5 | 72.8 |
| Ether | $\mathrm{C}_{4} \mathrm{H}_{40} \mathrm{O}$ | 34.5 | 88.4 | 107 |
|  |  | 0 | 94 | 94 |
|  | " | 50 | . | 115.1 |
|  | " | 120 |  | 140 |
| Ethyl $\begin{gathered}\text { bromide } \\ \text { chloride } \\ \text { iodide }\end{gathered}$ | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Br}$ | 38.2 | 60.4 |  |
|  | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Cl}$ | 12.5 |  | 98 |
|  | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{I}$ | 71 | 47 | ... |
| Heptane | $\mathrm{C}_{7} \mathrm{H}_{18}$ | 90 | 77.8 |  |
| Hexane | $\mathrm{Co}_{0} \mathrm{H}_{14}$ | 70 | 79.2 |  |
| Octane | $\mathrm{C}_{8} \mathrm{H}_{18}$ | 130 | 70.0 | $\ldots$ |
| Pentane ..... | $\mathrm{C}_{5} \mathrm{H}_{12}$ | 30 | 85.8 |  |
| Sulfur dioxide | $\mathrm{SO}_{4}$ | 0 | 91.2 | $\ldots$ |
| Toluol | $\mathrm{C}_{2} \mathrm{H}_{8}$ | 111 | 68.4 86.0 | $\ldots$ |
| Turpentine | $\mathrm{C}_{10} \mathrm{H}_{10}$ | 159.3 | 74.04 |  |

TABLE 162.-LATENT AND TOTAL HEAT OF VAPORIZATION, FORMULAE
$r=$ latent heat of vaporization at $t^{\circ} \mathrm{C} ; \mathrm{H}=$ total heat from fluid at $0^{\circ}$ to vapor at $t^{\circ} \mathrm{C}$. $T^{\circ}$ refers to Kelvin scale. Same units as preceding table.


TABLE 163.-LATENT HEAT OF VAPORIZATION OF AMMONIA
Calories per gram

| ${ }^{\circ} \mathrm{C}$ | 0 | 1 | 2 | 3 | + | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -40 | 331.7 | 332.3 | 333.0 | 333.6 | $33+3$ | 334.9 | 335.5 | 336.2 | 336.8 | 337.5 |
| -30 | 324.8 | 325.5 | 326.2 | 326.9 | 327.6 | 328.3 | 329.0 | 329.7 | 330.3 | 331.0 |
| -20 | 317.6 | 318.3 | 319.1 | 319.8 | 320.6 | 321.3 | 322.0 | 322.7 | 323.4 | 324.1 |
| -10 | 309.9 | 310.7 | 311.5 | 312.2 | 313.0 | 313.8 | 314.6 | 315.3 | 316.1 | 316.8 |
| -0 | 301.8 | 302.6 | 303.4 | 304.3 | 305.1 | 305.9 | 306.7 | 307.5 | 308.3 | 309.1 |
| +0 | 301.8 | 300.9 | 300.1 | 299.2 | 298.4 | 297.5 | 296.6 | 295.7 | 294.9 | 294.0 |
| +10 | 293.1 | 292.2 | 291.3 | 290.4 | 289.5 | 288.6 | 287.6 | 286.7 | 285.7 | 284.8 |
| +20 | 283.8 | 282.8 | 281.8 | 280.9 | 279.9 | 278.9 | 279.9 | 276.9 | 275.9 | 274.9 |
| +30 | 273.9 | 272.8 | 271.8 | 270.7 | 269.7 | 268.6 | 276.5 | 266.4 | 265.3 | 264.2 |
| +40 | 263.1 | 262.0 | 260.8 | 259.7 | 258.5 | 257.4 | 256.2 | 255.0 | 253.8 | 252.6 |

## TABLE 164.-"LATENT HEAT OF PRESSURE VARIATION" OF LIQUID AMMONIA

When a fluid undergoes a change of pressure, there occurs a transformation of energy into heat or vice versa, which results in a change of temperature of the substance unless a like amount of heat is abstracted or added. This change expressed as the heat so transformed per unit change of pressure is the "latent heat of pressure variation." It is expressed below as $J_{g^{-1}} \mathrm{~kg}^{-1} \mathrm{~cm}^{2}$.

| Temperature ${ }^{\circ} \mathrm{C}$. | -44.1 | -39.0 | -24.2 | -.2 | +16.5 | +26.5 | +35.4 | +40.3 |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Latent heat $\ldots .-.055$ | -.057 | - | .068 | -.088 | - | .107 | - | .123 | -.140 | - |

## TABLE 165.-THERMAL PROPERTIES OF SATURATED WATER AND STEAM

Accuracy: It is estimated that there is only 1 chance in 100 that the values given for $H$ differ from the truth by as much as 1 part in 2000 ; it is equally unlikely that the values for $L$ and $H^{\prime}$ are as much as 1.5 joules/g from the truth in the range of the experiments, $100^{\circ}-270^{\circ} \mathrm{C}$.

| $\begin{gathered} \text { Temperature } \\ { }^{\circ} \mathrm{C} \end{gathered}$ | Heat content of liquid, $H$ joules/g | Latent heat, $L$ joules/g | Heat content of vapor, $H^{\prime}$ joules/g | Entropy- |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{aligned} & \text { of liquid } \\ & \text { joules } / \mathrm{g}^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \text { of vapor } \\ & \phi^{3} \\ & \text { joules } / g^{\circ} \mathrm{C} \end{aligned}$ |
| 0. | 0 | 2494.02 | 2494.02 | 0 | 9.132 |
| 10. | 42.02 | 2472.26 | 2514.28 | . 1511 | 8.884 |
| 20. | 83.83 | 2450.17 | 2534.00 | . 2962 | 8.656 |
| 30. | 125.59 | 2427.73 | 2553.32 | . 4363 | 8.446 |
| 40. | 167.34 | 2404.90 | 2572.24 | . 5719 | 8.253 |
| 50. | 209.11 | 2381.64 | 2590.75 | . 7032 | 8.074 |
| 60. | 250.90 | 2357.91 | 2608.81 | . 8305 | 7.909 |
| 70. | 292.75 | 2333.65 | 2626.40 | . 9543 | 7.756 |
| 80. | 334.66 | 2308.32 | 2643.48 | 1.0746 | 7.613 |
| 90. | 376.65 | 2283.38 | 2660.03 | 1.1918 | 7.480 |
| 100. | 418.75 | 2257.24 | 2675.99 | 1.3064 | 7.356 |
| 110. | 460.97 | 2230.35 | 2691.32 | 1.4177 | 7.240 |
| 120. | 503.36 | 2202.65 | 2706.01 | 1.5268 | 7.130 |
| 130. | 545.93 | 2174.04 | 2719.97 | 1.6335 | 7.027 |
| 140. | 588.71 | 2144.44 | 2733.15 | 1.7381 | 6.929 |
| 150. | 631.75 | 2113.76 | 2745.51 | 1.8407 | 6.837 |
| 160. | 675.06 | 2081.89 | 2756.95 | 1.9416 | 6.749 |
| 170. | 718.66 | 2048.72 | 2767.38 | 2.0406 | 6.664 |
| 180. | 762.72 | 2014.10 | 2776.82 | 2.1384 | 6.584 |
| 190. | 807.15 | 1977.89 | 2785.04 | 2.2348 | 6.506 |
| 200. | . 852.02 | 1939.93 | 2791.95 | 2.3299 | 6.430 |
| 210. | 897.35 | 1900.00 | 2797.35 | 2.4239 | 6.357 |
| 220. | 943.24 | 1857.89 | 2801.13 | 2.5169 | 6.285 |
| 230. | 989.75 | 1813.33 | 2803.08 | 2.6091 | 6.213 |
| 240. | 1036.97 | 1766.02 | 2802.99 | 2.7007 | 6.143 |
| 250. | 1084.97 | 1715.59 | 2800.56 | 2.7919 | 6.072 |
| 260. | 1133.87 | 1661.60 | 2795.47 | 2.8828 | 6.000 |
| 270. | 1184.32 | 1603.51 | 2787.83 | 2.9746 | 5.927 |

Metric and common units, $0^{\circ}$ to $220^{\circ} \mathrm{C}$
Heat of liquid, $q$, heat required to raise $1 \mathrm{~kg}(1 \mathrm{lb})$ to corresponding temperature from $0^{\circ} \mathrm{C}$. Heat of vaporization, $r$, heat required to vaporize $1 \mathrm{~kg}(1 \mathrm{lb})$ at corresponding temperature to dry saturated vapor against corresponding pressure. Total heat, $H=r+q$.

|  | Pressure |  |  | Heat of the liquid |  | Heat of vaporization |  | Heat equivalent of internal works |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{-0}$ | $\mathrm{mmHg}^{\text {m }}$ | $\mathrm{kg} / \mathrm{cm}^{2}$ | 1b/in. ${ }^{2}$ | kg cal | Btu | kg cal | Btu | kg cal | Btu | 0 |
| $t$ | ¢ | - |  | , | - |  |  |  | ${ }^{\text {P }}$ |  |
| 0 | 4.579 | . 00623 | . 0886 | . 00 | . 0 | 595.4 | 1071.7 | 565.3 | 1017.5 | 32.0 |
| 5 | 6.541 | . 00889 | . 1265 | 5.04 | 9.1 | 592.8 | 1067.1 | 562.2 | 1011.9 | 41.0 |
| 10 | 9.205 | . 01252 | . 1780 | 10.06 | 18.1 | 590.2 | 1062.3 | 559.0 | 1006.2 | 50.0 |
| 15 | 12.779 | . 01737 | . 2471 | 15.06 | 27.1 | 587.6 | 1057.6 | 555.9 | 1000.5 | 59.0 |
| 20 | 17.51 | . 02381 | . 3396 | 20.06 | 36.1 | 584.9 | 1052.8 | 552.7 | 994.8 | 68.0 |
| 25 | 23.69 | . 03221 | . 4581 | 25.05 | 45.1 | 582.3 | 1048.1 | 549.5 | 989.7 | 77.0 |
| 30 | 31.71 | . 04311 | . 6132 | 30.04 | 54.1 | 579.6 | 1043.3 | 546.3 | 983.4 | 86.0 |
| 35 | 42.02 | . 05713 | . 8126 | 35.03 | 63.1 | 576.9 | 1038.5 | 543.1 | 977.6 | 95.0 |
| 40 | 55.13 | . 07495 | 1.0661 | 40.02 | 72.0 | 574.2 | 1033.5 | 539.9 | 971.7 | 104.0 |
| 45 | 71.66 | . 09743 | 1.3858 | 45.00 | 81.0 | 571.3 | 1028.4 | 536.5 | 965.7 | 113.0 |
| 50 | 92.30 | . 12549 | 1.7849 | 49.99 | 90.0 | 568.4 | 1023.2 | 533.0 | 959.6 | 122.0 |
| 55 | 117.85 | . 16023 | 2.279 | 54.98 | 99.0 | 565.6 | 1018.1 | 529.7 | 953.5 | 131.0 |
| 60 | 149.19 | . 20284 | 2.885 | 59.97 | 108.0 | 562.8 | 1013.1 | 526.4 | 947.5 | 140.0 |
| 65 | 187.36 | . 2547 | 3.623 | 64.98 | 117.0 | 559.9 | 1007.8 | 523.0 | 941.3 | 149.0 |
| 70 | 233.53 | . 3175 | 4.516 | 69.98 | 126.0 | 556.9 | 1002.5 | 519.5 | 935.0 | 158.9 |
| 75 | 289.0 | . 3929 | 5.589 | 74.99 | 135.0 | 554.0 | 997.3 | 516.0 | 928.8 | 167.0 |
| 80 | 355.1 | . 4828 | 6.867 | 80.01 | 144.0 | 551.1 | 991.9 | 512.6 | 922.6 | 176.0 |
| 85 | 433.5 | . 5894 | 8.383 | 85.04 | 153.1 | 548.1 | 986.5 | 509.1 | 916.3 | 185.0 |
| 90 | 525.8 | . 7149 | 10.167 | 90.07 | 162.1 | 544.9 | 980.9 | 505.4 | 909.9 | 194.0 |
| 91 | 546.1 | . 7425 | 10.560 | 91.08 | 163.9 | 544.3 | 979.8 | 504.7 | 908.5 | 195.8 |
| 92 | 567.1 | . 7710 | 10.966 | 92.08 | 165.7 | 543.7 | 978.7 | 504.0 | 907.2 | 197.6 |
| 93 | 588.7 | . 8004 | 11.384 | 93.09 | 167.5 | 543.1 | 977.6 | 503.3 | 906.0 | 199.4 |
| 94 | 611.0 | . 8307 | 11.815 | 94.10 | 169.3 | 542.5 | 976.5 | 502.6 | 904.7 | 201.2 |
| 95 | 634.0 | . 8620 | 12.260 | 95.11 | 171.2 | 541.9 | 975.4 | 501.9 | 903.4 | 203.0 |
| 96 | 657.7 | . 8942 | 12.718 | 96.12 | 173.0 | 541.2 | 974.2 | 501.1 | 902.1 | 204.8 |
| 97 | 682.1 | . 9274 | 13.190 | 97.12 | 174.8 | 540.6 | 973.1 | 500.4 | 900.8 | 206.6 |
| 98 | 707.3 | . 9616 | 13.678 | 98.13 | 176.6 | 539.9 | 971.9 | 499.6 | 899.4 | 208.4 |
| 99 | 733.2 | . 9970 | 14.180 | 99.14 | 178.5 | 539.3 | 970.8 | 498.9 | 898.2 | 210.2 |
| 100 | 760.0 | 1.0333 | 14.697 | 100.2 | 180.3 | 538.7 | 969.7 | 498.2 | 896.9 | 212.0 |
| 101 | 787.5 | 1.0707 | 15.229 | 101.2 | 182.1 | 538.1 | 968.5 | 497.5 | 895.5 | 213.8 |
| 102 | 815.9 | 1.1093 | 15.778 | 102.2 | 183.9 | 537.4 | 967.3 | 496.8 | 894.1 | 215.6 |
| 103 | 845.1 | 1.1490 | 16.342 | 103.2 | 185.7 | 536.8 | 966.2 | 496.1 | 892.9 | 217.4 |
| 104 | 875.1 | 1.1898 | 16.923 | 104.2 | 187.6 | 536.2 | 965.1 | 495.4 | 891.6 | 219.2 |
| 105 | 906.1 | 1.2319 | 17.522 | 105.2 | 189.4 | 535.6 | 964.0 | 494.7 | 890.3 | 221.0 |
| 106 | 937.9 | 1.2752 | 18.137 | 106.2 | 191.2 | 534.9 | 962.8 | 493.9 | 889.0 | 222.8 |
| 107 | 970.6 | 1.3196 | 18.769 | 107.2 | 193.0 | 534.2 | 961.6 | 493.1 | 887.6 | 224.6 |
| 108 | 1004.3 | 1.3653 | 19.420 | 108.2 | 194.8 | 533.6 | 960.5 | 492.4 | 886.3 | 226.4 |
| 109 | 1038.8 | 1.4123 | 20.089 | 109.3 | 196.7 | 532.9 | 959.3 | 491.6 | 885.0 | 228.2 |
| 110 | 1074.5 | 1.4608 | 20.777 | 110.3 | 198.5 | 532.3 | 958.1 | 490.9 | 883.6 | 230.6 |
| 111 | 1111.1 | 1.5106 | 21.486 | 111.3 | 200.3 | 531.6 | 956.9 | 490.2 | 882.3 | 231.8 |
| 112 | 1148.7 | 1.5617 | 22.214 | 112.3 | 202.1 | 530.9 | 955.7 | 489.4 | 880.9 | 233.6 |
| 113 | 1187.4 | 1.6144 | 22.962 | 113.3 | 203.9 | 530.3 | 954.5 | 488.7 | 879.5 | 235.4 |
| 114 | 1227.1 | 1.6684 | 23.729 | 114.3 | 205.8 | 529.6 | 953.3 | 487.9 | 878.2 | 237.2 |
| 115 | 1267.9 | 1.7238 | 24.518 | 115.3 | 207.6 | 528.9 | 952.1 | 487.1 | 876.8 | 239.0 |
| 116 | 1309.8 | 1.7808 | 25.328 | 116.4 | 209.4 | 528.2 | 950.8 | 486.3 | 875.4 | 240.8 |
| 117 | 1352.8 | 1.8393 | 26.160 | 117.4 | 211.2 | 527.5 | 949.5 | 485.5 | 873.9 | 242.6 |
| 118 | 1397.0 | 1.8993 | 27.015 | 118.4 | 213.0 | 526.9 | 948.4 | 484.8 | 872.6 | 244.4 |
| 119 | 1442.4 | 1.9611 | 27.893 | 119.4 | 214.9 | 526.2 | 947.2 | 484.0 | 871.3 | 246.2 |
|  |  |  |  | (cont | tinued) |  |  |  |  |  |

## Metric and common units, $0^{\circ}$ to $220^{\circ} \mathrm{C}$

If $A$ is the reciprocal of the mechanical equivalent of heat, $p$ the pressure, $s$ and $\sigma$ the specific volumes of the liquid and the saturated vapor, $s-\sigma$, the change of volume, then the heat equivalent of the external work is $A p u=A p(s-\sigma)$. Heat equivalent of internal work, $\rho=r-A p u$, Entropy $=\int d Q / T$, where $d Q=$ amount of heat added at absolute temperature $T$.


TABLE 166.-PROPERTIES OF SATURATED STEAM (continued)
Metric and common units, $0^{\circ}$ to $220^{\circ} \mathrm{C}$


TABLE 166.—PROPERTIES OF SATURATED STEAM (continued)
Metric and common units, $0^{\circ}$ to $220^{\circ} \mathrm{C}$

|  | Heat equiva- <br> lent of exter nal work |  | Entropy of the | Entropy of evapo ration | Specific volume |  | Density |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5\% | kg cal |  |  |  |  |  | $\mathrm{kg} / \mathrm{m}^{3}$ | $1 \mathrm{~b} / \mathrm{ft}^{\text {a }}$ | 츕 |
| $t$ | Apu | Apu | \% | $\frac{r}{T}$ | $\mathrm{m}^{3} / \mathrm{kg}$ | $\mathrm{ft}^{3} / \mathrm{lb}$ | $\frac{1}{5}$ | 1 | ${ }_{t}$ |
| 120 | 42.2 | 76.0 | . 3654 | 1.3372 | . 8914 | 14.28 | 1.122 | . 0700 | 248.0 |
| 121 | 42.3 | 76.2 | . 3680 | 1.3321 | . 8653 | 13.86 | 1.156 | . 0721 | 249.8 |
| 122 | 42.4 | 76.4 | . 3705 | 1.3269 | . 8401 | 13.46 | 1.190 | . 0743 | 251.6 |
| 123 | 42.5 | 76.5 | . 3731 | 1.3218 | . 8158 | 13.07 | 1.226 | . 0765 | 253.4 |
| 124 | 42.6 | 76.7 | . 3756 | 1.3167 | . 7924 | 12.69 | 1.262 | . 0788 | 255.2 |
| 125 | 42.7 | 76.8 | . 3782 | 1.3117 | . 7698 | 12.33 | 1.299 | . 0811 | 257.0 |
| 126 | 42.8 | 77.0 | . 3807 | 1.3067 | . 7479 | 11.98 | 1.337 | . 0835 | 258.8 |
| 127 | 42.9 | 77.1 | . 3833 | 1.3017 | . 7267 | 11.64 | 1.376 | . 0859 | 260.6 |
| 128 | 43.0 | 77.3 | . 3858 | 1.2967 | . 7063 | 11.32 | 1.416 | . 0883 | 262.4 |
| 129 | 43.0 | 77.4 | . 3884 | 1.2917 | . 6867 | 11.00 | 1.456 | . 0909 | 264.2 |
| 130 | 43.1 | 77.6 | . 3909 | 1.2868 | . 6677 | 10.70 | 1.498 | . 0935 | 266.0 |
| 131 | 43.2 | 77.7 | . 3934 | 1.2818 | . 6493 | 10.40 | 1.540 | . 0961 | 267.8 |
| 132 | 43.3 | 77.9 | . 3959 | 1.2769 | . 6315 | 10.12 | 1.583 | . 0988 | 269.6 |
| 133 | 43.3 | 78.0 | . 3985 | 1.2720 | . 6142 | 9.839 | 1.628 | . 1016 | 271.4 |
| 134 | 43.4 | 78.1 | . 4010 | 1.2672 | . 5974 | 9.569 | 1.674 | . 1045 | 273.2 |
| 135 | 43.5 | 78.3 | . 4035 | 1.2623 | . 5812 | 9.309 | 1.721 | . 1074 | 275.0 |
| 136 | 43.6 | 78.4 | . 4060 | 1.2574 | . 5656 | 9.060 | 1.768 | . 1104 | 276.8 |
| 137 | 43.6 | 78.5 | . 4085 | 1.2526 | . 5506 | 8.820 | 1.816 | . 1134 | 278.6 |
| 138 | 43.7 | 78.7 | . 4110 | 1.2479 | . 5361 | 8.587 | 1.865 | . 1165 | 280.4 |
| 139 | 43.8 | 78.8 | . 4135 | 1.2431 | . 5219 | 8.360 | 1.916 | . 1196 | 282.2 |
| 140 | 43.9 | 78.9 | . 4160 | 1.2383 | . 5081 | 8.140 | 1.968 | . 1229 | 284.0 |
| 141 | 43.9 | 79.1 | . 4185 | 1.2335 | . 4948 | 7.926 | 2.021 | . 1262 | 285.8 |
| 142 | 44.0 | 79.2 | . 4209 | 1.2288 | . 4819 | 7.719 | 2.075 | . 1296 | 287.6 |
| 143 | 44.0 | 79.3 | . 4234 | 1.2241 | . 4694 | 7.519 | 2.130 | . 1330 | 289.4 |
| 144 | 44.2 | 79.5 | . 4259 | 1.2194 | . 4574 | 7.326 | 2.186 | . 1365 | 291.2 |
| 145 | 44.2 | 79.6 | . 4283 | 1.2147 | . 4457 | 7.139 | 2.244 | . 1401 | 293.0 |
| 146 | 44.3 | 79.7 | . 4307 | 1.2100 | . 4343 | 6.957 | 2.303 | . 1437 | 294.8 |
| 147 | 44.4 | 79.9 | . 4332 | 1.2054 | . 4232 | 6.780 | 2.363 | . 1475 | 296.6 |
| 148 | 44.4 | 80.0 | . 4356 | 1.2008 | . 4125 | 6.609 | 2.424 | . 1513 | 298.4 |
| 149 | 44.5 | 80.1 | . 4380 | 1.1962 | . 4022 | 6.443 | 2.486 | . 1552 | 300.2 |
| 150 | 44.6 | 80.2 | . 4405 | 1.1916 | . 3921 | 6.282 | 2.550 | . 1592 | 302.0 |
| 151 | 44.6 | 80.4 | . 4429 | 1.1870 | . 3824 | 6.126 | 2.615 | . 1632 | 303.8 |
| 152 | 44.7 | 80.5 | . 4453 | 1.1824 | . 3729 | 5.974 | 2.682 | . 1674 | 305.6 |
| 153 | 44.8 | 80.6 | . 4477 | 1.1778 | . 3637 | 5.826 | 2.750 | . 1716 | 307.4 |
| 154 | 44.8 | 80.7 | . 4501 | 1.1733 | . 3548 | 5.683 | 2.818 | . 1759 | 309.2 |
| 155 | 44.9 | 80.9 | . 4525 | 1.1688 | . 3463 | 5.546 | 2.888 | . 1803 | 311.0 |
| 156 | 45.0 | 81.0 | . 4549 | 1.1644 | . 3380 | 5.413 | 2.959 | . 1847 | 312.8 |
| 157 | 45.0 | 81.1 | . 4573 | 1.1599 | . 3298 | 5.282 | 3.032 | . 1893 | 314.6 |
| 158 | 45.1 | 81.2 | . 4596 | 1.1554 | . 3218 | 5.154 | 3.108 | . 1940 | 316.4 |
| 159 | 45.2 | 81.4 | . 4620 | 1.1509 | . 3140 | 5.029 | 3.185 | . 1988 | 318.2 |
| 160 | 45.3 | 81.5 | . 4644 | 1.1465 | . 3063 | 4.906 | 3.265 | . 2038 | 320.0 |
| 161 | 45.3 | 81.6 | . 4668 | 1.1421 | . 2989 | 4.789 | 3.345 | . 2088 | 321.8 |
| 162 | 45.4 | 81.7 | . 4692 | 1.1377 | . 2920 | 4.677 | 3.425 | . 2138 | 323.6 |
| 163 | 45.5 | 81.8 | . 4715 | 1.1333 | . 2855 | 4.571 | 3.503 | . 2188 | 325.4 |
| 164 | 45.5 | 81.9 | . 4739 | 1.1289 | . 2792 | 4.469 | 3.582 | . 2238 | 327.2 |
| 165 | 45.6 | 82.0 | . 4763 | 1.1245 | . 2729 | 4.368 | 3.664 | . 2289 | 329.0 |
| 166 | 45.6 | 82.1 | . 4786 | 1.1202 | . 2666 | 4.268 | 3.751 | . 2343 | 330.8 |
| 167 | 45.7 | 82.2 | . 4810 | 1.1159 | . 2603 | 4.168 | 3.842 | . 2399 | 332.6 |
| 168 | 45.7 | 82.4 | . 4833 | 1.1115 | . 2540 | 4.070 | 3.937 | . 2457 | 334.4 |
| 169 | 45.8 | 82.5 | . 4857 | 1.1072 | . 2480 | 3.975 | 4.032 | . 2516 | 336.2 |

(continued)

TABLE 166.-PROPERTIES OF SATURATED STEAM (continued)
Metric and common units, $0^{\circ}$ to $220^{\circ} \mathrm{C}$

|  | Pressure |  |  | Heat of the liquid |  | Heat of vaporization |  | Heat equivalent of internal works |  | Hud |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{H}{ }$ | $\mathrm{mmHg}^{\text {g }}$ | $\mathrm{kg} / \mathrm{cm}^{2}$ | 1b/in. ${ }^{2}$ | kg cal | Btu | kg cal | Btu | kg cal | Btu |  |
| $t$ | $p$ | $p$ | f | $q$ | $q$ | $r$ | $r$ | $\rho$ | $\rho$ | $t$ |
| 170 | 5937 | 8.071 | 114.8 | 171.6 | 308.9 | 488.7 | 879.6 | 442.8 | 797.0 | 338.0 |
| 171 | 6081 | 8.268 | 117.6 | 172.6 | 310.7 | 487.9 | 878.3 | 441.9 | 795.6 | 339.8 |
| 172 | 6229 | 8.469 | 120.4 | 173.7 | 312.6 | 487.1 | 876.9 | 441.1 | 794.1 | 341.6 |
| 173 | 6379 | 8.673 | 123.4 | 174.7 | 314.5 | 486.3 | 875.4 | 440.2 | 792.5 | 343.4 |
| 174 | 6533 | 8.882 | 126.3 | 175.7 | 316.3 | 485.5 | 873.9 | 439.4 | 790.9 | 345.2 |
| 175 | 6689 | 9.094 | 129.4 | 176.8 | 318.2 | 484.7 | 872.4 | 438.5 | 789.3 | 347.0 |
| 176 | 6848 | 9.310 | 132.4 | 177.8 | 320.0 | 483.9 | 871.0 | 437.7 | 787.8 | 348.8 |
| 177 | 7010 | 9.531 | 135.6 | 178.8 | 321.8 | 483.1 | 869.5 | 436.8 | 786.2 | 350.6 |
| 178 | 7175 | 9.755 | 138.8 | 179.9 | 323.7 | 482.3 | 868.1 | 436.0 | 784.7 | 352.4 |
| 179 | 7343 | 9.983 | 142.0 | 180.9 | 325.6 | 481.4 | 866.6 | 435.0 | 783.1 | 354.2 |
| 180 | 7514 | 10.216 | 145.3 | 181.9 | 327.5 | 480.6 | 865.1 | 434.2 | 781.5 | 356.0 |
| 181 | 7688 | 10.453 | 148.7 | 183.0 | 329.3 | 479.8 | 863.6 | 433.3 | 779.9 | 357.8 |
| 182 | 7866 | 10.695 | 152.1 | 184.0 | 331.2 | 479.0 | 862.2 | 432.5 | 778.4 | 359.6 |
| 183 | 8046 | 10.940 | 155.6 | 185.0 | 333.0 | 478.2 | 860.7 | 431.6 | 776.9 | 361.4 |
| 184 | 8230 | 11.189 | 159.2 | 186.1 | 334.9 | 477.4 | 859.2 | 430.8 | 775.3 | 363.2 |
| 185 | 8417 | 11.44 | 162.8 | 187.1 | 336.8 | 476.6 | 857.7 | 429.9 | 773.7 | 365.0 |
| 186 | 8608 | 11.70 | 166.5 | 188.1 | 338.6 | 475.7 | 856.3 | 429.0 | 772.2 | 366.8 |
| 187 | 8802 | 11.97 | 170.2 | 189.2 | 340.5 | 474.8 | 854.7 | 428.0 | 770.5 | 368.6 |
| 188 | 8999 | 12.24 | 174.0 | 190.2 | 342.4 | 474.0 | 853.2 | 427.2 | 768.9 | 370.4 |
| 189 | 9200 | 12.51 | 177.9 | 191.2 | 344.2 | 473.2 | 851.7 | 426.3 | 767.4 | 372.2 |
| 190 | 9404 | 12.79 | 181.8 | 192.3 | 346.1 | 472.3 | 850.2 | 425.4 | 765.8 | 374.0 |
| 191 | 9612 | 13.07 | 185.9 | 193.3 | 347.9 | 471.5 | 848.7 | 424.5 | 764.2 | 375.8 |
| 192 | 9823 | 13.36 | 190.0 | 194.4 | 349.8 | 470.6 | 847.1 | 423.6 | 762.5 | 377.6 |
| 193 | 10038 | 13.65 | 194.1 | 195.4 | 351.7 | 469.8 | 845.6 | 422.8 | 761.0 | 379.4 |
| 194 | 10256 | 13.94 | 198.3 | 196.4 | 353.5 | 468.9 | 844.1 | 421.9 | 759.4 | 381.2 |
| 195 | 10480 | 14.25 | 202.6 | 197.5 | 355.4 | 468.1 | 842.5 | 421.0 | 757.7 | 383.0 |
| 196 | 10700 | 14.55 | 207.0 | 198.5 | 357.3 | 467.2 | 841.0 | 420.1 | 756.1 | 384.8 |
| 197 | 10930 | 14.87 | 211.4 | 199.5 | 359.2 | 466.4 | 839.5 | 419.2 | 754.6 | 386.6 |
| 198 | 11170 | 15.18 | 216.0 | 200.6 | 361.1 | 465.6 | 838.0 | 418.4 | 753.4 | 388.4 |
| 199 | 11410 | 15.51 | 220.6 | 201.6 | 362.9 | 464.7 | 836.4 | 417.4 | 751.3 | 390.2 |
| 200 | 11650 | 15.84 | 225.2 | 202.7 | 364.8 | 463.8 | 834.8 | 416.5 | 749.7 | 392.0 |
| 201 | 11890 | 16.17 | 230.0 | 203.7 | 366.7 | 462.9 | 833.8 | 415.6 | 748.1 | 393.8 |
| 202 | 12140 | 16.51 | 234.8 | 204.7 | 368.5 | 462.1 | 831.8 | 414.8 | 746.6 | 395.6 |
| 203 | 12400 | 16.85 | 239.7 | 205.8 | 370.4 | 461.2 | 830.2 | 413.8 | 744.9 | 397.4 |
| 204 | 12650 | 17.20 | 244.7 | 206.8 | 372.3 | 460.3 | 828.6 | 412.9 | 743.3 | 399.2 |
| 205 | 12920 | 17.56 | 249.8 | 207.9 | 374.1 | 459.4 | 827.0 | 412.0 | 741.6 | 401.0 |
| 206 | 13180 | 17.92 | 254.9 | 208.9 | 376.0 | 458.6 | 825.4 | 411.1 | 740.0 | 402.8 |
| 207 | 13450 | 18.29 | 260.1 | 210.0 | 377.9 | 457.7 | 823.8 | 410.2 | 738.3 | 404.6 |
| 208 | 13730 | 18.66 | 265.4 | 211.0 | 379.8 | 456.8 | 822.2 | 409.3 | 736.7 | 406.4 |
| 209 | 14010 | 19.04 | 270.8 | 212.0 | 381.6 | 455.9 | 820.6 | 408.4 | 735.1 | 408.2 |
| 210 | 14290 | 19.43 | 276.3 | 213.1 | 383.5 | 455.0 | 819.1 | 407.5 | 733.6 | 410.0 |
| 211 | 14580 | 19.82 | 281.9 | 214.1 | 385.4 | 454.1 | 817.4 | 406.6 | 731.9 | 411.8 |
| 212 | 14870 | 20.22 | 287.6 | 215.2 | 387.3 | 453.2 | 815.8 | 405.7 | 730.2 | 413.6 |
| 213 | 15170 | 20.62 | 293.3 | 216.2 | 389.2 | 452.4 | 814.3 | 404.9 | 728.7 | 415.4 |
| 214 | 15470 | 21.03 | 299.2 | 217.3 | 391.1 | 451.5 | 812.7 | 404.0 | 727.1 | 417.2 |
| 215 | 15780 | 21.45 | 305.1 | 218.3 | 392.9 | 450.6 | 811.0 | 403.1 | 725.4 | 419.0 |
| 216 | 16090 | 21.88 | 311.1 | 219.3 | 394.8 | 449.6 | 809.3 | 402.1 | 723.7 | 420.8 |
| 217 | 16410 | 22.31 | 317.3 | 220.4 | 396.7 | 448.7 | 807.7 | 401.2 | 722.1 | 422.6 |
| 218 | 16730 | 22.74 | 323.5 | 221.4 | 398.5 | 447.8 | 806.1 | 400.3 | 720.5 | 424.4 |
| 219 | 17060 | 23.19 | 329.8 | 222.5 | 400.4 | 446.9 | 804.5 | 399.4 | 718.9 | 426.2 |
| 220 | 17390 | 23.64 | 336.2 | 223.5 | 402.3 | 446.0 | 802.9 | 398.5 | 717.3 | 428.0 | (continued)

Metric and common units, $0^{\circ}$ to $220^{\circ} \mathrm{C}$

|  | Heat equivalent of external work |  | Entropy of the liquid | Entropy of evaporation <br> $r$ | Specific volume |  | Density |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -0 | kg cal | Btu |  |  | $\mathrm{m}^{3} / \mathrm{kg}$ | $\mathrm{ft}^{3} / 1 \mathrm{~b}$ | 1 | 1 | $\stackrel{\text { ¢ }}{\sim}$ |
| $t$ | $A p u$ | Apu | - | $\vec{T}$ | $s$ | $s$ | $\stackrel{1}{s}$ | $\stackrel{1}{s}$ | $t$ |
| 170 | 45.9 | 82.6 | . 4880 | 1.1029 | . 2423 | 3.883 | 4.127 | . 2575 | 338.0 |
| 171 | 46.0 | 82.7 | . 4903 | 1.0987 | . 2368 | 3.794 | 4.223 | . 2636 | 339.8 |
| 172 | 46.0 | 82.8 | . 4926 | 1.0944 | 2314 | 3.709 | 4.322 | . 2696 | 341.6 |
| 173 | 46.1 | 82.9 | . 4949 | 1.0901 | 2262 | 3.626 | 4.421 | . 2758 | 343.4 |
| 174 | 46.1 | 83.0 | . 4972 | 1.0859 | . 2212 | 3.545 | 4.521 | . 2821 | 345.2 |
| 175 | 46.2 | 83.1 | . 4995 | 1.0817 | . 2164 | 3.467 | 4.621 | . 2884 | 347.0 |
| 176 | 46.2 | 83.2 | . 5018 | 1.0775 | . 2117 | 3.391 | 4.724 | . 2949 | 348.8 |
| 177 | 46.3 | 83.3 | . 5041 | 1.0733 | . 2072 | 3.318 | 4.826 | . 3014 | 350.6 |
| 178 | 46.3 | 83.4 | . 5064 | 1.0691 | . 2027 | 3.247 | 4.933 | . 3080 | 352.4 |
| 179 | 46.4 | 83.5 | . 5087 | 1.0649 | . 1983 | 3.177 | 5.04 | . 3148 | 354.2 |
| 180 | 46.4 | 83.6 | . 5110 | 1.0608 | . 1941 | 3.109 | 5.15 | . 3217 | 356.0 |
| 181 | 46.5 | 83.7 | . 5133 | 1.0567 | . 1899 | 3.041 | 5.27 | . 3288 | 357.8 |
| 182 | 46.5 | 83.8 | . 5156 | 1.0525 | . 1857 | 2.974 | 5.38 | . 3362 | 359.6 |
| 183 | 46.6 | 83.8 | . 5178 | 1.0484 | . 1817 | 2.911 | 5.50 | . 3435 | 361.4 |
| 184 | 46.6 | 83.9 | . 5201 | 1.0443 | . 1778 | 2.849 | 5.62 | . 3510 | 363.2 |
| 185 | 46.7 | 84.0 | . 5224 | 1.0403 | . 1740 | 2.787 | 5.75 | . 3588 | 365.0 |
| 186 | 46.7 | 84.1 | . 5246 | 1.0362 | . 1702 | 2.727 | 5.88 | . 3667 | 366.8 |
| 187 | 46.8 | 84.2 | . 5269 | 1.0321 | . 1666 | 2.669 | 6.00 | . 3746 | 368.6 |
| 188 | 46.8 | 84.3 | . 5291 | 1.0280 | . 1632 | 2.614 | 6.13 | . 3826 | 370.4 |
| 189 | 46.9 | 84.3 | . 5314 | 1.0240 | . 1598 | 2.560 | 6.26 | . 3906 | 372.2 |
| 190 | 46.9 | 84.4 | . 5336 | 1.0200 | . 1565 | 2.507 | 6.39 | . 3989 | 374.0 |
| 191 | 47.0 | 84.5 | . 5358 | 1.0160 | . 1533 | 2.456 | 6.52 | . 4072 | 375.8 |
| 192 | 47.0 | 84.6 | . 5381 | 1.0120 | . 1501 | 2.405 | 6.66 | . 4158 | 377.6 |
| 193 | 47.0 | 84.6 | . 5403 | 1.0080 | . 1470 | 2.355 | 6.80 | . 4246 | 379.4 |
| 194 | 47.0 | 84.7 | . 5426 | 1.0040 | . 1440 | 2.306 | 6.94 | . 4336 | 381.2 |
| 195 | 47.1 | 84.8 | . 5448 | 1.0000 | . 1411 | 2.259 | 7.09 | . 4426 | 383.0 |
| 196 | 47.1 | 84.9 | . 5470 | . 9961 | . 1382 | 2.214 | 7.23 | . 4516 | 384.8 |
| 197 | 47.2 | 84.9 | . 5492 | . 9922 | . 1354 | 2.169 | 7.38 | . 4610 | 386.6 |
| 198 | 47.2 | 85.0 | . 5514 | . 9882 | . 1327 | 2.126 | 7.53 | . 4704 | 388.4 |
| 199 | 47.3 | 85.1 | . 5536 | . 9843 | . 1300 | 2.083 | 7.69 | . 4801 | 390.2 |
| 200 | 47.3 | 85.1 | . 5558 | . 9804 | . 1274 | 2.041 | 7.84 | . 4900 | 392.0 |
| 201 | 47.3 | 85.2 | . 5580 | . 9765 | . 1249 | 2.001 | 8.00 | . 4998 | 393.8 |
| 202 | 47.3 | 85.2 | . 5602 | . 9727 | . 1225 | 1.962 | 8.16 | . 510 | 395.6 |
| 203 | 47.4 | 85.3 | . 5624 | . 9688 | . 1201 | 1.923 | 8.33 | . 520 | 397.4 |
| 204 | 47.4 | 85.3 | . 5646 | . 9650 | . 1177 | 1.885 | 8.50 | . 531 | 399.2 |
| 205 | 47.4 | 85.4 | . 5668 | . 9611 | . 1153 | 1.847 | 8.67 | . 541 | 401.0 |
| 206 | 47.5 | 85.4 | . 5690 | . 9572 | . 1130 | 1.810 | 8.85 | . 552 | 402.8 |
| 207 | 47.5 | 85.5 | . 5712 | . 9534 | . 1108 | 1.774 | 9.03 | . 564 | 404.6 |
| 208 | 47.5 | 85.5 | . 5733 | . 9496 | . 1086 | 1.739 | 9.21 | . 575 | 406.4 |
| 209 | 47.5 | 85.5 | . 5755 | . 9458 | . 1065 | 1.705 | 9.39 | . 587 | 408.2 |
| 210 | 47.5 | 85.5 | . 5777 | . 9420 | . 1044 | 1.673 | 9.58 | . 598 | 410.0 |
| 211 | 47.5 | 85.5 | . 5799 | . 9382 | . 1024 | 1.640 | 9.77 | . 610 | 411.8 |
| 212 | 47.5 | 85.6 | . 5820 | . 9344 | . 1004 | 1.608 | 9.96 | . 622 | 413.6 |
| 213 | 47.5 | 85.6 | . 5842 | . 9307 | . 0984 | 1.577 | 10.16 | . 634 | 415.4 |
| 214 | 47.5 | 85.6 | . 5863 | . 9269 | . 0965 | 1.546 | 10.36 | . 647 | 417.2 |
| 215 | 47.5 | 85.6 | . 5885 | . 9232 | . 0947 | 1.516 | 10.56 | . 660 | 419.0 |
| 216 | 47.5 | 85.6 | . 5906 | . 9195 | . 0928 | 1.486 | 10.78 | . 673 | 420.8 |
| 217 | 47.5 | 85.6 | . 5927 | . 9157 | . 0910 | 1.458 | 10.99 | . 686 | 422.6 |
| 218 | 47.5 | 85.6 | . 5948 | . 9120 | . 0893 | 1.430 | 11.20 | . 699 | 424.4 |
| 219 | 47.5 | 85.6 | . 5969 | . 9084 | . 0876 | 1.403 | 11.41 | . 713 | 426.2 |
| 220 | 47.5 | 85.6 | . 5991 | . 9047 | . 0860 | 1.376 | 11.62 | . 727 | 428.0 |

## Common units, $400^{\circ}$ to $700^{\circ} \mathrm{F}$

Abridged from Steam tables and Mollicr's diagram, by Keenan. Printed by permission of the publisher, The American Society of Mechanical Engineers. For detailed discussion see Mechanical Engineering, February, 1929, $v$, specific vol., $\mathrm{ft}^{3} / \mathrm{lb}$; $h$, total heat, enthalpy, $\mathrm{Btu} / \mathrm{lb}$; $s$, entropy, Btu $\mathrm{lb}^{-1}{ }^{\circ} \mathrm{F}^{-1}$. The strict definition of total heat (internal energy + $144 / J$ ) is adhered to; zeros of both $h$ and $s$ are arbitrarily placed on the sat. liq. line at $32^{\circ} \mathrm{F}$. No internal energy values are tabulated but may be casily found by subtracting $144 \mathrm{pz} / \mathrm{J}$ from the total heat. The energy unit, the Btu, is $778.57 \mathrm{ft}-1 \mathrm{bb}(J)$ is $1 / 180$ of the change in total heat along the saturated liquid line between $32^{\circ}$ and $212^{\circ} \mathrm{F}$.

|  |  | Specificic volume |  |  | $\underbrace{\text { Total heat }}$ |  |  | $\underbrace{\text { Entropy }}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Temp. } \\ \stackrel{\mathrm{O}}{\mathrm{~F}} \\ \boldsymbol{p} \end{gathered}$ |  | $\begin{aligned} & \text { Sat. } \\ & \text { liq. } \\ & v_{q} \end{aligned}$ | $\begin{gathered} \text { Evap. } \\ v_{f g} \end{gathered}$ | $\begin{gathered} \text { Sat. } \\ \text { vapor } \\ v_{g} \end{gathered}$ | $\begin{aligned} & \text { Sat. } \\ & \text { liq. } \\ & \text { liq. } \end{aligned}$ | $\begin{gathered} \text { Evap. } \\ h_{f g} \end{gathered}$ | $\begin{aligned} & \text { Sat. } \\ & \text { vap. } \\ & h_{0} \end{aligned}$ | $\begin{aligned} & \text { Sat. } \\ & \text { liq. } \\ & s_{p} \end{aligned}$ | $\begin{gathered} \text { Evap. } \\ s_{f g} \end{gathered}$ | $\begin{gathered} \substack{\text { Sat. } \\ \text { vapor } \\ s_{g}} \end{gathered}$ |
| 400 | 247.25 | . 01865 | 1.8421 | 1.8608 | 375.0 | 826 | 1200 | . 5668 | . 9602 | 1.5270 |
| 405 | 261.67 | . 01873 | 1.7428 | 1.7615 | 380.4 | 821 | 1201 | . 5730 | . 9491 | 1.5221 |
| 410 | 276.72 | . 01880 | 1.6493 | 1.6681 | 385.9 | 816 | 1202 | . 5792 | . 9381 | 1.5173 |
| 415 | 292.44 | . 01888 | 1.5615 | 1.5804 | 391.3 | 811 | 1202 | . 5854 | . 9271 | 1.5125 |
| 420 | 308.82 | . 01896 | 1.4792 | 1.4982 | 396.8 | 806 | 1203 | . 5916 | . 9161 | 1.5077 |
| 425 | 325.91 | . 01904 | 1.4022 | 1.4212 | 402.4 | 801 | 1203 | . 5978 | . 9052 | 1.5029 |
| 430 | 343.71 | . 01911 | 1.3295 | 1.3486 | 407.9 | 796 | 1203 | . 6039 | . 8942 | 1.4982 |
| 435 | 362.27 | . 01919 | 1.2610 | 1.2802 | 413.5 | 790 | 1204 | . 6101 | . 8833 | 1.4934 |
| 440 | 381.59 | . 01928 | 1.1965 | 1.2158 | 419.1 | 785 | 1204 | . 6162 | . 8724 | 1.4887 |
| 445 | 401.70 | . 01936 | 1.1356 | 1.1550 | 424.7 | 779 | 1204 | . 6224 | . 8616 | 1.4839 |
| 450 | 422.61 | . 0195 | 1.0782 | 1.0977 | 430 | 774 | 1204 | . 6284 | . 8507 | 1.4792 |
| 455 | 444.35 | . 0195 | 1.0241 | 1.0436 | 436 | 768 | 1204 | . 6346 | . 8398 | 1.4744 |
| 460 | 466.94 | . 0196 | . 9730 | . 9927 | 442 | 762 | 1204 | . 6407 | . 8290 | 1.4696 |
| 465 | 490.40 | . 0197 | . 9249 | . 9446 | 447 | 756 | 1204 | . 6468 | . 8180 | 1.4649 |
| 470 | 514.76 | . 0198 | . 8793 | . 8991 | 453 | 750 | 1204 | . 6530 | . 8071 | 1.4601 |
| 475 | 540.04 | . 0199 | . 8361 | . 8560 | 459 | 744 | 1203 | . 6592 | . 7962 | 1.4554 |
| 480 | 566.26 | . 0200 | . 7951 | . 8151 | 465 | 738 | 1203 | . 6654 | . 7852 | 1.4506 |
| 485 | 593.47 | . 0201 | . 7563 | . 7764 | 471 | 731 | 1202 | . 6716 | . 7742 | 1.4458 |
| 490 | 621.67 | . 0202 | . 7195 | . 7398 | 477 | 725 | 1202 | . 6779 | . 7632 | 1.4410 |
| 495 | 650.87 | . 0204 | . 6847 | . 7050 | 483 | 718 | 1201 | . 6842 | . 7521 | 1.4362 |
| 500 | 681.09 | . 0205 | . 6516 | . 6721 | 489 | 711 | 1200 | . 6904 | . 7410 | 1.4314 |
| 505 | 712.40 | . 0206 | . 6201 | . 6408 | 495 | 704 | 1199 | . 6968 | . 7299 | 1.4266 |
| 510 | 744.74 | . 0207 | . 5903 | . 6110 | 502 | 697 | 1198 | . 7031 | . 7187 | 1.4218 |
| 515 | 778.16 | . 0209 | . 5618 | . 5826 | 508 | 690 | 1197 | . 7094 | . 7075 | 1.4170 |
| 520 | 812.72 | . 0210 | . 5347 | . 5557 | 514 | 682 | 1196 | . 7158 | . 6963 | 1.4121 |
| 525 | 848.43 | . 0211 | . 5090 | . 5301 | 521 | 675 | 1195 | . 7222 | . 6851 | 1.4073 |
| 530 | 885.31 | . 0213 | . 4845 | . 5058 | 527 | 667 | 1193 | . 7286 | . 6738 | 1.4024 |
| 535 | 923.39 | . 0214 | . 4614 | . 4828 | 533 | 659 | 1192 | . 7350 | . 6625 | 1.3975 |
| 540 | 962.73 | . 0216 | 4394 | .4610 | 540 | 651 | 1191 | . 7414 | . 6512 | 1.3926 |
| 545 | 1003.4 | . 0218 | 4184 | . 4401 | 547 | 643 | 1189 | . 7478 | . 6399 | 1.3877 |
| 550 | 1045.4 | . 0219 | . 3982 | . 4201 | 553 | 634 | 1188 | . 7543 | . 6285 | 1.3828 |
| 555 | 1088.7 | . 0221 | . 3789 | . 4010 | 560 | 626 | 1186 | . 7607 | . 6170 | 1.3778 |
| 560 | 1133.4 | . 0223 | . 3605 | . 3828 | 567 | 618 | 1184 | . 7672 | . 6056 | 1.3728 |
| 565 | 1179.7 | . 0225 | . 3429 | . 3654 | 574 | 609 | 1182 | . 7737 | . 5940 | 1.3677 |
| 570 | 1227.6 | . 0227 | . 3261 | . 3488 | 580 | 600 | 1180 | . 7802 | . 5825 | 1.3626 |
| 575 | 1276.7 | . 0229 | . 3101 | . 3330 | 587 | 591 | 1178 | . 7867 | . 5709 | 1.3576 |
| 580 | 1327.2 | . 0231 | . 2949 | . 3180 | 594 | 581 | 1176 | . 7932 | . 5592 | 1.3524 |
| 585 | 1379.2 | . 0234 | . 2804 | . 3037 | 602 | 572 | 1173 | . 7998 | . 5474 | 1.3472 |
| 590 | 1432.7 | . 0236 | . 2664 | . 2900 | 609 | 562 | 1171 | . 8064 | . 5356 | 1.3420 |
| 595 | 1487.8 | . 0239 | . 2530 | . 2769 | 616 | 552 | 1168 | . 8131 | . 5237 | 1.3368 |
| 600 | 1544.6 | . 0241 | . 2401 | . 2642 | 623 | 542 | 1166 | . 8198 | . 5118 | 1.3316 |
| 610 | 1663.2 | . 0247 | . 2159 | . 2406 | 638 | 521 | 1160 | . 8332 | . 4875 | 1.3208 |
| 620 | 1788.8 | . 0254 | . 1933 | . 2186 | 653 | 499 | 1153 | . 8470 | 4623 | 1.3093 |
| 630 | 1921.9 | . 0261 | . 1721 | . 1982 | 670 | 475 | 1144 | . 8612 | . 4358 | 1.2970 |
| 640 | 2062.8 | . 0269 | . 1522 | . 1791 | 687 | 448 | 1135 | . 8763 | . 4073 | 1.2836 |
| 650 | 2211.4 | . 0278 | . 1331 | . 1610 | 705 | 417 | 1122 | . 8924 | . 3764 | 1.2688 |
| 660 | 2368.6 | . 0290 | . 1148 | . 1437 | 725 | 384 | 1109 | . 9097 | . 3426 | 1.2523 |
| 670 | 2534.2 | . 0304 | . 0966 | . 1269 | 748 | 344 | 1092 | . 9287 | . 3049 | 1.2336 |
| 680 | 2709.7 | . 0322 | . 0781 | . 1102 | 773 | 299 | 1071 | . 9499 | . 2619 | 1.2119 |
| 690 | 2896.8 | . 0347 | . 0589 | . 0936 | 803 | 241 | 1044 | . 9755 | . 2098 | 1.1852 |
| 700 | 3096.4 | . 0394 | . 0353 | . 0747 | 846 | 157 | 1003 | 1.0117 | . 1354 | 1.1471 |
| 705 | 3202.0 | . 0462 | . 0135 | . 0597 | 888 | 73 | 962 | 1.0472 | . 0630 | 1.1102 |
| 706.1 | 3226.0 | . 0522 | 0 | . 0522 | 925 | 0 | 925 | 1.0785 | 0 | 1.0785 |

Common units, $212^{\circ}$ to $3000^{\circ} \mathrm{F}$


[^80]$402^{\circ}$ to $1000^{\circ} \mathrm{F}$

| Pressure <br> (abs.) <br> lb/in. ${ }^{2}$ | Tem-pera${ }^{\text {ture }} \mathrm{F}$ | Heat of liquid above $32^{\circ} \mathrm{F}$ Btu | Heat of vaporiBtu | Total heat Btu | Entropy of hiquid above 32 ${ }^{\circ} \mathrm{F}$ | Entropy of vapori. zation | Total entropy | Specific volume $\mathrm{ft}^{3} / 11 \mathrm{l}$ | Weight $\mathrm{lb} / \mathrm{ft}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 4 | 402 | 13.81 | 128.15 | 141.96 | . 0209 | . 1487 | . 1696 | 114.50 | . 008733 |
| . 8 | 444 | 15.36 | 127.24 | 142.60 | . 0227 | . 1408 | . 1635 | 59.72 | . 016745 |
| 1.0 | 458 | 15.89 | 126.92 | 142.81 | . 0233 | . 1383 | . 1616 | 48.45 | . 02064 |
| 1.5 | 485 | 16.90 | 126.33 | 143.23 | . 0244 | . 1337 | 1581 | 33.14 | . 03017 |
| 2.0 | 505 | 17.65 | 125.89 | 143.54 | . 0251 | . 1305 | . 1556 | 25.32 | . 03948 |
| 4.0 | 558 | 19.62 | 124.72 | 144.34 | . 0271 | . 1226 | . 1497 | 13.26 | . 07540 |
| 6.0 | 591 | 20.87 | 123.99 | 144.86 | . 0283 | . 1179 | . 1462 | 9.096 | . 10993 |
| 8.0 | 617 | 21.81 | 123.43 | 145.24 | . 0292 | . 1147 | . 1439 | 6.9630 | . 14361 |
| 10.0 | 637 | 22.58 | 122.98 | 145.56 | . 0299 | . 1121 | . 1420 | 5.6610 | . 17664 |
| 15.0 | 676 | 24.04 | 122.12 | 146.16 | . 0312 | . 1075 | . 1387 | 3.8923 | . 25691 |
| 20.0 | 706 | 25.15 | 121.46 | 146.61 | . 0322 | . 1042 | . 1364 | 2.983 | . 3352 |
| 25.0 | 730 | 26.05 | 120.93 | 146.98 | . 0330 | . 1016 | . 1346 | 2.429 | . 4117 |
| 30.0 | 751 | 26.81 | 120.48 | 147.29 | . 0336 | . 0995 | . 1331 | 2.053 | . 4871 |
| 35.0 | 769 | 27.49 | 120.08 | 147.57 | . 0342 | . 0977 | . 1319 | 1.7815 | . 5613 |
| 40.0 | 785 | 28.08 | 119.73 | 147.81 | . 0346 | . 0962 | . 1308 | 1.5762 | . 6344 |
| 45.0 | 799 | 28.62 | 119.42 | 148.04 | . 0351 | . 0949 | . 1300 | 1.4147 | . 7069 |
| 50 | 812 | 29.11 | 119.13 | 148.24 | . 0355 | . 0936 | . 1291 | 1.284 | . 7788 |
| 60 | 836 | 29.99 | 118.61 | 148.60 | . 0361 | . 0915 | . 1276 | 1.086 | . 9204 |
| 70 | 857 | 30.75 | 118.15 | 148.90 | . 0367 | . 0898 | . 1265 | . 9436 | 1.0597 |
| 80 | 875 | 31.44 | 117.75 | 149.19 | . 0372 | . 0882 | . 1254 | . 8349 | 1.1977 |
| 90 | 892 | 32.06 | 117.38 | 149.44 | . 0377 | . 0870 | . 1247 | -. 7497 | 1.3338 |
| 100 | 907 | 32.63 | 117.05 | 149.68 | . 0381 | . 0856 | . 1237 | . 6811 | 1.4682 |
| 110 | 921 | 33.16 | 116.74 | 149.90 | . 0385 | . 0845 | . 1230 | . 6242 | 1.6020 |
| 120 | 934 | 33.66 | 116.44 | 150.10 | . 0389 | . 0835 | . 1224 | . 5767 | 1.7340 |
| 130 | 947 | 34.12 | 116.17 | 150.29 | . 0392 | . 0826 | . 1218 | . 5360 | 1.8656 |
| 140 | 958 | 34.55 | 115.92 | 150.47 | . 0395 | . 0818 | . 1213 | . 5012 | 1.9952 |
| 150 | 969 | 34.96 | 115.67 | 150.63 | . 0398 | . 0809 | . 1207 | . 4706 | 2.125 |
| 180 | 1000 | 36.09 | 115.01 | 151.10 | . 0406 | . 0788 | . 1194 | . 3990 | 2.506 |

$-100^{\circ}$ to $+250^{\circ} \mathrm{F}$

| $\underset{\mathrm{F}}{\substack{\text { Oemp. }}}$ | Saturation |  |  |  |  |  | Latent heat of pressure variationBtu/lb $\frac{\mathrm{Btu} / \mathrm{lb}}{\mathrm{lb} / \mathrm{in} .^{2}}$ | Variation of $h$ with $p$ $t$ constant <br>  $\left(\frac{\partial h}{\partial p}\right)_{t}$ | Com- <br> pressi- <br> bility per <br> $\mathrm{lb} / \mathrm{in} .^{2}$ $\times 10^{i}$ $-\frac{1}{v}\left(\frac{\partial v}{\partial p}\right)_{t}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pressure (abs.) lb/in. ${ }^{2}$ | Volume$\mathrm{ft}^{3} / \mathrm{lb}$ | $\begin{aligned} & \text { Density } \\ & \mathrm{lb} / \mathrm{ft}^{3} \end{aligned}$ | SpecificheatBtu/lbof | $\begin{aligned} & \text { Heat } \\ & \text { content } \\ & \text { Btu/lb } \end{aligned}$ | Latent heat |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  | $\underline{1}$ |  |  | Btu/ lb |  |  |  |
| $t$ | $p$ | $v$ | $\bar{\nu}$ | ${ }^{\text {c }}$ | $h$ | $L$ |  |  |  |
| -100 | 1.24 | . 02197 | 45.52 | (1.040) | (-63.0) | (633) |  |  |  |
| - 90 | 1.86 | . 02216 | 45.12 | (1.043) | (-52.6) | (628) |  |  |  |
| - 80 | 2.74 | . 02236 | 44.72 | (1.046) | (-42.2) | (622) |  |  |  |
| - 70 | 3.94 | . 02256 | 44.32 | (1.050) | (-31.7) | (616) |  |  |  |
| - 60 | 5.55 | . 02278 | 43.91 | 1.054 | -21.18 | 610.8 | -. 0016 | . 0026 | 4.4 |
| - 50 | 7.67 | . 02299 | 43.49 | 1.058 | -10.61 | 604.3 | -. 0017 | . 0026 | 4.6 |
| - 40 | 10.41 | . 02322 | 43.08 | 1.062 | . 00 | 597.6 | -. 00018 | . 0025 | 4.8 |
| - 30 | 13.90 | . 02345 | 42.65 | 1.066 | $+10.66$ | 590.7 | -. 0019 | . 0025 | 5.1 |
| $-20$ | 18.30 | . 02369 | 42.22 | 1.070 | +21.36 | 583.6 | -. 0020 | . 0024 | 5.4 |
| $-10$ | 23.74 | . 02393 | 41.78 | 1.075 | 32.11 | 576.4 | $-.0021$ | . 0023 | 5.7 |
| 0 | 30.42 | . 02419 | 41.34 | 1.080 | 42.92 | 568.9 | -. 0022 | . 0022 | 6.0 |
| $+10$ | 38.51 | . 02446 | 40.89 | 1.085 | 53.79 | 561.1 | -. 0024 | . 0021 | 6.4 |
| + 20 | 48.21 | . 02474 | 40.43 | 1.091 | 64.71 | 553.1 | -. 0025 | . 0020 | 6.8 |
| 30 | 59.74 | . 02503 | 39.96 | 1.097 | 75.71 | 544.8 | $-.0027$ | . 0019 | 7.3 |
| 40 | 73.32 | . 02533 | 39.49 | 1.104 | 86.77 | 536.2 | -. 0029 | . 0018 | 7.8 |
| 50 | 89.19 | . 02564 | 39.00 | 1.112 | 97.93 | 527.3 | -. 0031 | . 0017 | 8.4 |
| 60 | 107.6 | . 02597 | 38.50 | 1.120 | 109.18 | 518.1 | -. 0033 | . 0015 | 9.1 |
| 70 | 128.8 | . 02632 | 38.00 | 1.129 | 120.54 | 508.6 | -. 0035 | . 0013 | 10.0 |
| 80 | 153.0 | . 02668 | 37.48 | 1.138 | 131.99 | 498.7 | -. 0038 | . 0011 | 10.9 |
| 90 | 180.6 | . 02707 | 36.95 | 1.147 | 143.54 | 488.5 | -. 0041 | . 0009 | 12.0 |
| $+100$ | 211.9 | . 02747 | 36.40 | 1.156 | 155.21 | 477.8 | $-.0045$ | . 0006 | 13.3 |
| 125 | 307.8 | . 02860 | 34.96 | (1.189) | (185) | (449) |  |  |  |
| 150 | 433.2 | . 02995 | 33.39 | (1.23) | (216) | (416) |  |  |  |
| 175 | 593.5 | . 03160 | 31.65 | (1.29) | (248) | (377) |  |  |  |
| 200 | 794.7 | . 03375 | 29.63 | (1.38) | (283) | (332) |  |  |  |
| 250 | 1347 | . 0422 | 23.7 | (1.90) | (365) | (192) |  |  |  |

TABLE 171.-COMBUSTION CONSTANTS OF SOME SUBSTANCES ${ }^{52}$

| Substance | Formula | $\begin{gathered} \text { Reciprocal of } \\ \text { density } \\ \mathrm{m}^{3} / 100 \mathrm{~kg} \end{gathered}$ | Spec. gravity$\mathrm{air}=1.000$ | Heat of combustion |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Btu/ft ${ }^{3}$ | $\mathrm{kg} \mathrm{cal} / \mathrm{m}^{3}$ |
| Carbon |  |  |  |  | 7840.* |
| Hydrogen | $\mathrm{H}_{2}$ | 1172. | $6.959 \times 10^{-2}$ | 275.0 | 2445. |
| Oxygen . |  | 73.7 | 1.1053 |  |  |
| Carbon monoxide | CO | 84.4 | . 9672 | 321.8 | 2860. |
| Paraffin series: $\mathrm{C}_{\mathrm{n}} \mathrm{H}_{2 \mathrm{n}+2}$ |  |  |  |  |  |
| Methane | $\mathrm{CH}_{4}$ | 147.0 | . 5543 | 913.1 | 8120. |
| Ethane | $\mathrm{C}_{2} \mathrm{H}_{5}$ | 77.6 | 1.04882 | 1641. | 14,600 |
| Propane | - $\mathrm{C}_{3} \mathrm{H}_{8}$ | 52.2 | 1.5617 | 2385. | 21,200 |
| Isobutane | - $\mathrm{C}_{4} \mathrm{H}_{10}$ | 39.5 | 2.06654 | 3105. | 27,600 |
| Olefin series: $\mathrm{C}_{\mathrm{n}} \mathrm{H}_{2 \mathrm{n}}$ |  |  |  |  |  |
| Ethylene | $\mathrm{C}_{2} \mathrm{H}_{4}$ | 83.6 | . 9740 | 1513.2 | 13,450 |
| Propylene | $\mathrm{C}_{3} \mathrm{H}_{6}$ | 56.3 | 1.4504 | 2186. | 19,400 |
| Isobutene | $\mathrm{C}_{4} \mathrm{H}_{8}$ | 42.2 | 1.9336 | 2869. | 25,500 |
| Aromatic series: $\mathrm{C}_{\mathrm{n}} \mathrm{H}_{2 \mathrm{n}-\mathrm{6}}$ |  |  |  |  |  |
| Benzene | $\mathrm{C}_{6} \mathrm{H}_{4}$ | 30.3 | 2.6920 | 3601. | 32,000 |
| Toluene | $\mathrm{C}_{7} \mathrm{H}_{8}$ | 25.6 | 3.1760 | 4284. | 38,100 |
| Xylene | $\mathrm{C}_{8} \mathrm{H}_{10}$ | 22.2 | 3.6618 | 4980. | 44,300 |
| Miscellaneous gases |  |  |  |  |  |
| Acetylene | $\mathrm{C}_{2} \mathrm{H}_{2}$ | 89.5 | . 9107 | 1448. | 12,870 |
| Naphthalene | - $\mathrm{C}_{10} \mathrm{H}_{5}$ | 18.4 | 4.4208 | 5654. | 50,300 |
| Methyl alcohol | . $\mathrm{CH}_{3} \mathrm{OH}$ | 73.7 | 1.1052 | 768.0 | 6830. |
| Ethyl alcohol | - $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{OH}$ | 51.3 | 1.5890 | 1450.5 | 12,900 |
| Ammonia | $\mathrm{NH}_{3}$ | 136.5 | . 5961 | 365.1 | 3245. |
| Sulfur | . S |  |  |  | 2210.* |
| Hydrogen sulfide | - $\mathrm{H}_{2} \mathrm{~S}$ | 68.5 | 1.1898 | 596. | 5300. |

${ }^{52}$ Shnidman, Louis (ed.), Gaseous fuels, p. 118, Amer. Gas Assoc., 1948.

* Expressed in cal/g.


## TABLE 172.-FLAME TEMPERATURES AS MEASURED BY VARIOUS METHODS *

| Gas | Burner |  | Temp ${ }^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: |
| Amyl acetate | Bunsen |  | 1420 |
|  | Meker | (center flame) | 1700 |
|  |  | (edge of flame) | 1850 |
| Propane | Meker |  | 1680 |
| City gas | Bunsen |  | 1760 |
| City gas + air | Blast |  | 1950 |
| City gas + oxygen | " |  | 2300 |
| Carbon monoxide + air | " |  | 1985 |
| 16\% [methane ( $\left.\mathrm{CH}_{4}\right)$ ] + air | " |  | . 1880 |
| $10 \%\left(90 \mathrm{CH}_{4}+10 \% 0\right)+\mathrm{air}$ | " |  | 1905 |
| $16 \%\left(80 \mathrm{CH}_{4}+20 \% 0\right)+$ air | " |  | 1975 |
| $10.8 \%\left(75 \mathrm{CH}_{4}+25 \% 0\right)+$ air | " |  | 2005 |
| $22 \%\left(60 \mathrm{CH}_{4}+40 \mathrm{H}_{2}\right)+$ air .. | " |  | 1910 |
| $32 \%\left(26 \mathrm{CH}_{4}+94 \mathrm{H}_{2}\right)+$ air | " |  | . 2015 |
| $\mathrm{H}_{2}+$ air | " |  | . 2045 |
| $9 \%\left(80 \mathrm{CH}_{4}+20 \mathrm{C}_{2} \mathrm{H}_{2}\right)+$ air | " |  | 1970 |
| (15CH4 $\left.+85 \mathrm{C}_{2} \mathrm{H}_{2}\right)+$ air | " |  | . 2275 |
| Pittsburgh natural gas with air | " |  | . 1950 |
| Butane-air ....... | " |  | . 2000 |
| Oxy-hydrogen | " |  | 2800 |
| Oxy-acetylene | " |  | 3500 |

[^81]Given in kg cal ${ }_{16}$ at constant pressure per gram-molecular weight in vacuo. When reterred to constant volume the values should be $0.58 \mathrm{~kg} \mathrm{cal}_{15}$ smaller (at about $18^{\circ} \mathrm{C}$ ) for each condensed gaseous molecule. Combustion products are $\mathrm{CO}_{2}$, liquid $\mathrm{H}_{2} \mathrm{O}$, etc. Benzoic acid was adopted at Lyons as a primary standard, its heat of combustion, $6324 \mathrm{~g} \mathrm{cal} 1_{15}$, per gram in air, 6319 in vacuo. This is tacitly assumed as heat of isothermal combustion at $20^{\circ} \mathrm{C}$. In absolute joules, 26,466 and 26,445 respectively. The following ratios may be taken as standard: Naphthalene/benzoic acid $=$ $1.5201(\mathrm{air})$; benzoic acid/sucrose $=1.6028$ (air) ; naphthalene/sucrose $=2.4364$ (air).

${ }^{53}$ Karasch, Nat. Bur. Standards Journ. Res., vol. 2, p. 359, 1929.

TABLE 174.-HEATS OF COMBUSTION OF MISCELLANEOUS COMPOUNDS

| Substance | Calories per g substance substance | Substance | Calories per g substance |
| :---: | :---: | :---: | :---: |
| Asphalt | 9530 | Oils : |  |
| Butter | 9200 | petroleum: |  |
| Carbon: amorphous | 8080 | crude | 11500 |
| charcoal | 8100 | light | 10000 |
| diamond | 7860 | heavy | 10200 |
| graphite | 7900 | rape | 9500 |
| Copper (to CuO ) | 590 | sperm | 10000 |
| Dynamite, $75 \%$.. | 1290 | Paraffin (to $\mathrm{CO}_{2}, \mathrm{H}_{2} \mathrm{O}$ i) | 11140 |
| Egg, white of.. | 5700 | Paraffin (to $\mathrm{CO}_{2}, \mathrm{H}_{2} \mathrm{O} \mathrm{g}$ ). | 10340 |
| Fgg, yolk of. | 8100 | Pitch ................. | 8400 |
| Fats, animal | 9500 | Sulfur, rhombic | 2200 |
| Hemoglobin | 5900 | Sulfur, monoclinic | 2240 |
| Hydrogen | 33900 | Tallow .......... | 9500 |
| Iron (to $\mathrm{Fe}_{2} \mathrm{O}_{3}$ ) | 1582 | Woods: beech, $13 \% \mathrm{H}^{2} \mathrm{O}$ | 4170 |
| Magnesium (to MgO | 6080 | birch, $12 \% \mathrm{H}_{2} \mathrm{O}$ | 4210 |
| Oils: cotton-seed ... | 9500 | oak, $13 \% \mathrm{H}_{2} \mathrm{O}$. | 3990 |
| lard olive | 9300 9400 | pine, $12 \% \mathrm{H}_{2} \mathrm{O}$. | 4420 |

## Part 1．－Coals

|  | Coal |  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ |  | $\stackrel{5}{5}$ | $\frac{E}{3}$ | $\begin{aligned} & \text { 駡 } \\ & \text { 苞 } \\ & \text { an } \end{aligned}$ | $\begin{aligned} & \text { 坒 } \\ & \text { 愈 } \end{aligned}$ |  | $\begin{aligned} & \text { E. } \\ & \text { E. } \\ & \text { O} \end{aligned}$ | $\stackrel{\infty}{\mathrm{J}}_{\infty}^{\infty}$ | $\stackrel{』}{\Xi}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | \｛ Low grade | 38.81 | 25.48 | 27.29 | 8.42 | ． 97 | 7.09 | 37.45 | ． 50 | 45.57 | 3526 | 6347 |
| Lignite | \｛ High grade | 33.38 | 27.44 | 29.62 | 9.56 | ． 94 | 6.77 | 41.31 | ． 67 | 40.75 | 3994 | 7189 |
| Sub－bitu－ | \｛ Low grade | 22.71 | 34.78 | 36.60 | 5.91 | ． 29 | 6.14 | 52.54 | 1.03 | 34.09 | 5115 | 9207 |
| minous | High grade | 15.54 | 33.03 | 46.06 | 5.37 | ． 58 | 5.89 | 60.08 | 1.05 | 27.03 | 5865 | 10557 |
| Bitu－ | \｛ Low grade | 11.44 | 33.93 | 43.92 | 10.71 | 4.94 | 5.39 | 60.06 | 1.02 | 17.88 | 6088 | 10958 |
| minous | High grade | 3.42 | 34.36 | 58.83 | 3.39 | ． 58 | 5.25 | 77.98 | 1.29 | 11.51 | 7852 | 14134 |
| Semi－bitu－ | \｛ Low grade | 2.7 | 14.5 | 75.5 | 7.3 | ． 99 | 4.58 | 80.65 | 1.82 | 4.66 | 7845 | 14121 |
| minous | \｛High grade | 3.26 | 14.57 | 78.20 | 3.97 | ． 54 | 4.76 | 84.62 | 1.02 | 5.09 | 8166 | 14699 |
| Semi－anthr | acite | 2.07 | 9.81 | 78.82 | 9.30 | 1.74 | 3.62 | 80.28 | 1.47 | 3.59 | 7612 | 13702 |
| Anthra－ | \｛ Low grade | 2.76 | 2.48 | 82.07 | 12.69 | ． 54 | 2.23 | 79.22 | ． 68 | 4.64 | 6987 | 12577 |
| cite | \｛ High grade | 3.33 | 3.27 | 84.28 | 9.12 | ． 60 | 3.08 | 81.35 | 79 | 5.06 | 7417 | 13351 |
| Oven | \｛ Low grade | 1.92 | 1.58 | 88.87 | 8.99 | 1.18 |  |  |  |  | 7946 | 14300 |
| coke | \｛ High grade | 1.14 | ． 04 | 94.66 | 3.57 | ． 69 | － | － | － | － | 8006 | 14410 |

Part 2．－Peats and Woods（air dried）

|  | $\begin{aligned} & \text { Vol. } \\ & \text { hydro- } \\ & \text { carbon } \end{aligned}$ | Fixed | Ash | $\underset{\text { fur }}{\text { Sul－}}$ | $\begin{gathered} \text { Hydro- } \\ \text { gen } \end{gathered}$ | Carbon | $\begin{gathered} \text { Nitro- } \\ \text { gen } \end{gathered}$ | $\underset{\text { Oxy. }}{\substack{\text { Oxen }}}$ | Calories per $g$ | $\begin{gathered} \text { Btu } \\ \text { per } \\ \text { pound } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Peats： |  |  |  |  |  |  |  |  |  |  |
| Franklin County，N．Y．．． | 67.10 | 28.99 | 3.91 | ． 15 | 5.93 | 57.17 | 1.48 | 31.36 | 5726 | 10307 |
| Sawyer County，Wis．．．． | 56.54 | 27.92 | 15.54 | ． 29 | 4.71 | 51.00 | 1.92 | 26.54 | 4867 | 8761 |
| Woods： |  |  |  |  |  |  |  |  |  |  |
| Oak，dry | － | － | ． 37 | － | 6.02 | 50.16 | ． 09 | 43.36 | 4620 | 8316 |
| Birch，dry | － | － | ． 29 | － | 6.06 | 48.88 | ． 10 | 44.67 | 4771 | 8588 |
| Pine，dry | － | － | ． 37 | － | 6.20 | 50.31 | ． 04 | 43.08 | 5085 | 9153 |

Part 3．－Liquid fuels＊

| Fuel <br> Aviation gasoline | $\begin{aligned} & \text { Gravity API } \dagger \\ & \ldots . .68 \end{aligned}$ | Btu per pound 20，420 | Btu per gallon $120,700$ |
| :---: | :---: | :---: | :---: |
| Motor gasoline | 58 | 20，120 | 125，800 |
| Kerosene | ．． 42 | 19，810 | 134，700 |
| Domestic fuel oil． | ． 32 | 19，450 | 141，200 |
| Diesel fuel oil． | 28 | 19，350 | 143，100 |
| Medium industrial fuel oil． | ． 18 | 18，930 | 149，400 |
| Heavy industrial fuel oil． | ． 11 | 18，590 | 153，900 |
| Petroleum ether | ． $68 \ddagger$ | 22，000 | 12，2208 |
| Alcohol，fuel or denatured w and denaturing material． | ．．．． $82 \ddagger$ | 11，600 | 6，4508 |

[^82]（continued）

## TABLE 175.-HEAT VALUES AND ANALYSES OF VARIOUS FUELS (concluded)

## Part 4.-Gases

| Substance Spec. gravity <br> Air $=1.000$ | Heat of combustion $\mathrm{kg} \mathrm{cal} / \mathrm{m}^{\mathrm{g}}$ | Flame temperature <br> ${ }^{\circ} \mathrm{C}$ (no excess air) |
| :---: | :---: | :---: |
| Natural gas . . . . . . . . . . . . . . . . . . . .60-1.29 | 8040-17,400 | 1965 |
| Propane (commercial) natural gas... 1.55 | 20,950 | 2015 |
| Propane (commercial) refinery gas.. 1.77 | 20,600 | - |
| Butane (commercial) natural gas.... 2.04 | 26,350 | 2005 |
| Butane (commercial) refinery gas.... 2.00 | 26,100 | - |
| Butane-air . ....................... . 1.16 | 4590. | - |
| Oil gas . . . . . . . . . . . . . . . . . . . . . . . 37 | 4535. | 2000 |
| Coal gas . . . . . . . . . . . . . . . . . . . . . . . 47 | 4320. | 1980 |
| Producer gas . . . . . . . . . . . . . . . . . . . 86 | 1182. | 1655 |
| Blue gas . . . . . . . . . . . . . . . . . . . . . . 57 | 2330. | - |

** For reference, see footnote 52, p. 179.

Part 5.-Gross calorific values of crude petroleum ${ }^{54}$

| Area | $\begin{aligned} & \text { Density } \\ & 20^{\circ} / 4^{\circ} \mathrm{C} \end{aligned}$ | Btu/lb | Cal/g | Area | $\begin{aligned} & \text { Density } \\ & 20^{\circ} / 4^{\circ} \mathrm{C} \end{aligned}$ | Btu/lb | $\mathrm{Cal} / \mathrm{g}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Borneo | . 898 | 19,370 | 10,760 | California | . 960 | 18,590 | 10,330 |
| India | . 863 | 18,800 | 10,490 | Ohio | . 838 | 19,710 | 10,950 |
| Japan | . 925 | 20,670 | 11,480 | Oklahoma | . 886 | 19,420 | 10,790 |
| Poland | . 899 | 20,010 | 11.120 | Pennsylvania | . 828 | 19,780 | 10,990 |
| Rumania | . 936 | 18,920 | 10,510 | Texas | . 943 | 18,950 | 10,520 |
| Canada | . 855 | 19,420 | 10,790 | Argentina | . 989 | 18,540 | 10,300 |
| Mexico | . . 966 | 18,180 | 10,100 | Patagonia | . 948 | 18,970 | 10,540 |
| Trinidad | . 941 | 18,360 | 10,200 |  |  |  |  |
| ${ }^{\text {of }}$ Science of Petroleum, vol. 2. |  |  |  |  |  |  |  |

Part 6.—Sugars ${ }^{\|}$

| Sugar | $\mathrm{kg} \mathrm{cal} / \mathrm{mol}$ | Sugar | kg cal/mol |
| :---: | :---: | :---: | :---: |
| $l$-Sorbose | 670.30 | $a-d$-Glucose | 669.58 |
| $\beta$ - $\alpha$-Levulose | 671.70 | $a-d$-Glucose hydrate | 666.73 |
| $\alpha-d$-Galactose | 666.76 | $\boldsymbol{a}$-Monopalmitin | 2778.78 |
| $\beta$-Lactose | 1345.47 | $\beta$-Monopalmitin | 2788.30 |
| $\beta$-Maltose monohydrate | 1360.50 | Ascorbic acid | 560.60 |
| $\alpha$-Lactose monohydrate | 1354.66 | $\boldsymbol{a}$-D-Glucose pentaacetate | 1718.62 |
| Sucrose | 1349.00 | $\beta$-D-Glucose pentaacetate | 1722.63 |

[^83]| Liquid $\ldots \ldots \ldots$. | $\mathrm{CCl}_{4}$ | $\mathrm{CHCl}_{3}$ | $4^{*}$ | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Br}$ | 32 | $39 *$ | No. 40 |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Freezing point $\ldots \ldots$ | ${ }^{\circ} \mathrm{C}$ | -23 | -63 | -81 | -119 | -139 | -145 | $-150 \pm$ | Compositions: * No. $4 ; \mathrm{CCl}_{4}, 49.4 \% ; \mathrm{CHCl}_{3}, 50.6 \%$. No. $32 ; \mathrm{CHCl}_{3}, 19.7 \% ; \mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Br}, 44.9 \% ; \mathrm{C}_{2} \mathrm{H}_{2} \mathrm{Cl}_{2}, 13.8 \% ; \mathrm{C}_{2} \mathrm{HCl}_{3}$, $21.6 \%$.

No. $39 ; \mathrm{CHCl}_{3}, 14.5 \%$; $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Br}, 33.4 \% ; \mathrm{C}_{2} \mathrm{H}_{2} \mathrm{Cl}_{2}, 10.4 \% ; \mathrm{C}_{2} \mathrm{HCl}_{3}$, $16.4 \%: \mathrm{CH}_{2} \mathrm{Cl}_{2}, 25.3 \%$.
No. $40 ; \mathrm{C}_{\mathrm{C}} \mathrm{HCl}_{3}, 17.9 \% ; \mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Cl}, 9.3 \% ; \mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Br}, 40.7 \% ; \mathrm{C}_{2} \mathrm{H}_{2} \mathrm{Cl}_{2}, 12.5 \%$; $\mathrm{C}_{2} \mathrm{HCl}_{3}, 19.6 \%$.

|  |  | $\begin{aligned} & u \\ & 0 \\ & 0 \\ & 0 \\ & 1 \end{aligned}$ | $\begin{aligned} & \circ \\ & i \\ & i \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 1 \\ & \hline 1 \end{aligned}$ | $\begin{gathered} \circ \\ \stackrel{\circ}{7} \\ \hline \end{gathered}$ | $\begin{gathered} \circ \\ \\ \hline \end{gathered}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{2} \\ & \stackrel{1}{2} \end{aligned}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{\text { i }}{\sim}$ | $\circ$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Viscosities in centipoises: | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Br}$ | 1.81 | 2.25 | 2.89 | 3.86 | 5.6 |  |  |  |  |
|  | No. 32 |  | 3.03 | 4.57 | 7.4 | 13.7 | 29.3 | 81 |  |  |
|  | No. 34 | 1.97 | 2.57 | 3.69 | 5.6 | 10 | 22.3 | 85 | 242 | 1480 |
|  | No. 40 |  | 2.88 | 3.89 | 5.9 | 10.2 | 22.5 | 71 | 170 | 631 |

[^84]
## TABLE 177.-DATA ON EXPLOSIVES

| Explosive | Vol. gas per $g$ in $\stackrel{\mathrm{cm}}{=} \mathrm{V}$ | Calories $\mathrm{g}=Q$ | $\begin{aligned} & \text { Coeffi- } \\ & \text { cient } \\ & =0 . V \\ & \doteqdot 100 \end{aligned}$ | $\begin{aligned} & \text { Coeffi- } \\ & \text { cient } \\ & G P \\ & =1 \end{aligned}$ | Calculated tempera$\stackrel{\text { ture }}{Q / C}$ <br> $C$, sp. ht.gases <br> $=$ $=.24$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Gunpowder | 280 | 738 | 207 | 1 | $2240{ }^{\circ} \mathrm{C}$ |
| Nitroglycerine | 741 | 1652 | 1224 | 6 | 6880 |
| Nitrocellulose, $13 \% \mathrm{~N}_{2}$ | 923 | 931 | 859 | 4.3 | 3876 |
| Cordite, Mk. I. (NG, 57 ; NC, 38; Vaseline, 5) |  | 1242 | 1082 | 5.2 | 5175 |
| Cordite, MD (NG, 30 ; NC, 65 ; Vaseline, 5). |  | 1031 | 915 | 4.4 | 4225 |
| Ballistite (NG, 50; NC, 50; Stabilizer, 5)... | 817 | 1349 | 1102 | 5.3 | 5621 3375 |
| Picric acid (Lyddite)..................... | 877 | 810 | 710 | 3.4 | 3375 |

Shattering power of explosive $=$ vol. gas per $\mathrm{g} \times$ cals $/ \mathrm{g} \times V_{d} \times$ density where $V_{d}$ is the velocity of detonation.

Trinitrotoluene: $V_{d}=7000 \mathrm{~m} / \mathrm{sec}$. Shattering effect $=.87$ picric acid.
Amatol (ammonium nitrate + trinitrotoluene, TNT): $V_{d}=4500 \mathrm{~m} / \mathrm{sec}$.
Ammonal (ammonium nitrate, TNT, Al): $1578 \mathrm{cal} / \mathrm{g} ; 682 \mathrm{~cm}^{3} \mathrm{gas} ; V_{d}=4000 \mathrm{~m} / \mathrm{sec}$.
Sabulite (ammonium nitrate, 78, TNT 8, Ca silicide 14): about same as ammonal.

TABLE 178.-TIME OF HEATING FOR EXPLOSIVE DECOMPOSITION

| Temperature ${ }^{\circ} \mathrm{C}$ | 170 | 180 | 190 | 200 | 220 | Ignition temperature |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | sec | sec | sec | sec | sec | ${ }^{\circ} \mathrm{C}$ † | ${ }^{\circ} \mathrm{C} \ddagger$ |
| Black powder | $n$ | $n$ | $n$ | $n$ | $n$ | 440 | - |
| Smokeless powder A | 600 | 195 | 130 | 45 | 23 | $\{300$ |  |
| Smokeless powder B | 190 | 130 | - | 90 | 25 | $\{300$ |  |
| Celluloid pyroxylin | 170 | 60 | - | 21 | 9 | - | - |
| Collodion cotton | 870 | 165 | 67 | 56 | 18 | 300 |  |
| Celluloid * | 160 | 100 | 60 | 50 | 30 | 590 | 450 |
| Safety matches | $n$ | 340 | 240 | 150 | 60 | - | - |
| Parlor matches | $n$ | $n$ | $n$ | 590 | 480 |  |  |
| Cotton wool | - | - | - | - | - | 900 |  |

[^85]TABLE 179.-CHEMICAL AND PHYSICAL PROPERTIES OF FIVE DIFFERENT CLASSES OF EXPLOSIVES


The total heat generated in a chemical reaction is independent of the steps from initial to final state. Heats of formation may therefore be calculated from steps chemically impracticable. Chemical symbols now represent the chemical energy in a gram-molecule or mol $(c)$; treat reaction equations like algebraic equations: $\mathrm{CO}+\mathrm{O}=\mathrm{CO}_{2}+68 \mathrm{~kg}$ cal ; subtract $\mathrm{C}+2 \mathrm{O}=\mathrm{CO}_{2}$ +97 kg cal, then $\mathrm{C}+\mathrm{O}=\mathrm{CO} 29 \mathrm{~kg}$ cal. We may substitute the negative values of the formation heats in an energy equation and solve $\mathrm{MgCl}_{2}+2 \mathrm{Na}=2 \mathrm{NaCl}+\mathrm{Mg}+\mathrm{xkg} \mathrm{cal} ;-151=$ $-196+x ; x=45 \mathrm{~kg}$ cal. Heats of formation of organic compounds can be found from the heats of combustion since burned to $\mathrm{H}_{2} \mathrm{O}$ and $\mathrm{CO}_{2}$. When changes are at constant volume, energy of external work is negligible; also generally for solid or liquid changes in volume. When a gas forms a solid or liquid at constant pressure, or vice versa, it must be allowed for. For N mols of gas formed (disappearing) at $\mathrm{T}_{\mathrm{k}}{ }^{\circ}$ the energy of the substance is decreased (increased) by $0.002 \cdot \mathrm{~N} \cdot \mathrm{~T}_{\mathrm{K}} \mathrm{kg}$ cal $\mathrm{H}_{2}+\mathrm{O}=\mathrm{H}_{2} \mathrm{O}+67.5 \mathrm{~kg}$ cal at $18^{\circ} \mathrm{C}$ at constant volume; $\frac{1}{2}\left(2 \mathrm{H}_{2}+\mathrm{O}_{2}-\right.$ $\left.2 \mathrm{H}_{2} \mathrm{O}=135.0+0.002 \times 3 \times 291=136.7\right)=68.4 \mathrm{~kg}$ cal.

The heat of solution is the heat, + or - , liberated by the solution of 1 mol of substance in so much water that the addition of more water will produce no additional heat effects. Aq signifies this amount of water; $\mathrm{H}_{2} \mathrm{O}$, one $\mathrm{mol} ; \mathrm{NH}_{3}+\mathrm{Aq}=\mathrm{NH}_{4} \mathrm{OH} \cdot \mathrm{Aq}+8 \mathrm{~kg}$ cal.

Part 1.-Heats of formation from elements in kilogram-calories
At ordinary temperatures

| Compound | Heat of formation | Compound | Heat of formation | Compound | Heat of formation | Compound | Heat of formation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Al}_{2} \mathrm{O}_{3}$ | 380. | HgO | 21.4 | KCl | 105.7 | $\mathrm{Li}_{2} \mathrm{SO}_{4}$ | 334.2 |
| $\mathrm{Ag}_{2} \mathrm{O}$ | 6.5 | $\mathrm{Na}_{2} \mathrm{O}$ | 100. | LiCl | 93.8 | $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{SO}_{4}$ | 283. |
| BaO | 126. | $\mathrm{Nd}_{2} \mathrm{O}_{3}$ | 435. | $\mathrm{MgCl}_{2}$ | 151.0 | $\mathrm{Na}_{2} \mathrm{SO}_{4}$ | 328.3 |
| $\mathrm{BaO}_{2}$ | 142. | NiO | 57.9 | $\mathrm{MnCl}_{2}$ | 112.3 | $\mathrm{MgSO}_{4}$ | 301.6 |
| $\mathrm{Bi}_{2} \mathrm{O}_{3}$ | 138. | $\mathrm{P}_{2} \mathrm{O}_{5}$ sgs | 370. | NaCl | 97.8 | $\mathrm{PbSO}_{4}$ | 216.2 |
| CO am | 29.0 | PbO | 50.3 | $\mathrm{NdCl}_{3}$ | 250. | $\mathrm{Tl}_{2} \mathrm{SO}_{4}$ | 221.0 |
| CO di | 26.1 | $\mathrm{PbO}_{2}$ | 62.4 | $\mathrm{NH}_{4} \mathrm{Cl}$ | 76.3 | $\mathrm{ZnSO}_{4}$ | 229.6 |
| $\mathrm{CO}_{2} \mathrm{am}$ | 97.0 | $\mathrm{Pr}_{2} \mathrm{O}_{3}$ | 412. | $\mathrm{NiCl}_{2}$ | 74.5 | $\mathrm{CaCO}_{3}$ | 270. |
| $\mathrm{CO}_{2} \mathrm{gr}$ | 94.8 | $\mathrm{Rb}_{2} \mathrm{O}$ | 89.2 | $\mathrm{PbCl}_{2}$ | 83.4 | $\mathrm{CuCO}_{3}$ | 143. |
| $\mathrm{CO}_{2} \mathrm{di}$ | 94.3 | $\mathrm{So}_{2} \mathrm{rh} \mathrm{sgg}$ | 70. | $\mathrm{PdCl}_{2}$ | 40.5 | $\mathrm{FeCO}_{3}$ | 179. |
| CaO | 152. | $\mathrm{SiC}_{2}$ | 191.0 | $\mathrm{PtCl}_{4}$ | 60.4 | $\mathrm{K}_{2} \mathrm{CO}_{3}$ | 280. |
| $\mathrm{CeO}_{2}$ | 225. | SnO | 66.9 | $\mathrm{SnCl}_{2}$ | 80.8 | $\mathrm{MgCO}_{3}$ | 267. |
| $\mathrm{Cl}_{2} \mathrm{O} \mathrm{g}$ | -16.5 | $\mathrm{SnO}_{2} \mathrm{Cr}$ | 137.5 | $\mathrm{SnCl}_{4}$ | 128. | $\mathrm{Na}_{2} \mathrm{CO}_{3}$ | 272. |
| CoO am | 50.5 | $\mathrm{SrO}_{2}$ | 135. | $\mathrm{SrCl}_{2}$ | 185. | $\mathrm{ZnCO}_{3}$ | 194. |
| CoO cr | 57.5 | $\mathrm{ThO}_{2}$ | 326. | $\mathrm{ThCl}_{4}$ | 300. | $\mathrm{AgNO}_{3}$ | 28.7 |
| $\mathrm{Co}_{3} \mathrm{O}_{4}$ | 193.4 | $\mathrm{TiO}_{2}$ am | 215.6 | TlCl | 48.6 | $\mathrm{Ca}\left(\mathrm{NO}_{3}\right)_{2}$ | 209. |
| $\mathrm{CrO}_{3}$ | 140. | $\mathrm{TiO}_{2} \mathrm{cr}$ | 218.4 | RbCl | 105.9 | $\mathrm{Cu}\left(\mathrm{NO}_{3}\right)_{2} 6 \mathrm{H}_{2} \mathrm{O}$ | 92.9 |
| $\mathrm{Cs}_{2} \mathrm{O}$ | 91.3 | $\mathrm{TlO}_{2}$ | 42.2 | $\mathrm{ZnCl}_{2}$ | 97.3 | $\mathrm{NHO}_{3} \mathrm{gggl}$ | 41.6 |
| $\mathrm{Cu}_{2} \mathrm{O}$ | 42.3 | $\mathrm{W}^{\left(\mathrm{O}_{2}\right.}$ | 131. | HBrglg | 8.6 | $\mathrm{KNO}_{3}$ | 119.2 |
| CuO | 37.2 | $\mathrm{WO}_{3}$ | 194. | $\mathrm{NH}_{4} \mathrm{Br}$ | 66. | $\mathrm{LiNO}_{3}$ | 112. |
| FeO | 65.7 | ZnO | 85.2 | HIgsg | - 6.2 | $\mathrm{NH}_{4} \mathrm{NO}_{3}$ | 88.3 |
| $\mathrm{Fe}_{2} \mathrm{O}_{3}$ | 196.5 | AgCl | 29.2 | HF ggg | 38. | $\mathrm{NaNO}_{3}$ | 111.0 |
| $\mathrm{Fe}_{3} \mathrm{O}_{4}$ | 270.8 | $\mathrm{Ag}_{2} \mathrm{Cl}$ | 29.5 | $\mathrm{Ag}_{2} \mathrm{~S}$ | 3.3 | $\mathrm{TlNO}_{3}$ | 58.2 |
| $\mathrm{H}_{2} \mathrm{Oggl}$ | 68.4 | $\mathrm{AlCl}_{3}$ | 161.4 | $\mathrm{CS}_{2} \mathrm{sgg}$ | -26.0 | $\mathrm{CH}_{4} \mathrm{sgg}$ | 20. |
| $\mathrm{H}_{2} \mathrm{O}_{2} \mathrm{gg}$ l | 46.8 | $\mathrm{AuCly}_{y}$ | 5.81 | CaS | 90.8 | $\mathrm{C}_{2} \mathrm{H}_{8} \mathrm{sgg}$ | 25. |
| $\mathrm{Hg}_{2} \mathrm{O}$. | 22.2 | $\mathrm{AuCl}_{3} \mathrm{y}$ | 22.8 | $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{~S}$ | 66.2 | $\mathrm{C}_{2} \mathrm{H}_{2} \mathrm{sgg}$ | -53. |
| HgO | 21.4 | $\mathrm{BaCl}_{2}$ | 197. | $\mathrm{Cu}_{2} \mathrm{~S}$ | 18.3 | HCN di gsgg | -30.5 |
| $\mathrm{K}_{2} \mathrm{O}$ | 91. | $\mathrm{BeCl}_{2}$ | 155. | CuS | 11.6 | $\mathrm{NH}_{3} \mathrm{ggg}$ | 12.0 |
| $\mathrm{La}_{2} \mathrm{O}_{3}$ | 447. | $\mathrm{BiCl}_{3}$ | 90.6 | $\mathrm{H}_{2} \mathrm{~S}$ gsg | 2.73 | $\mathrm{Ca}(\mathrm{OH})_{2}$ | 230. |
| $\mathrm{LiO}_{2}$ | 141.6 | $\mathrm{CCl}_{4} \mathrm{am}$ | 21.0 | $\mathrm{K}_{2} \mathrm{~S}$. | 103.4 | $\mathrm{NH}_{4} \mathrm{OH}$ | 88.8 |
| MgO | 143.6 | $\mathrm{CaCl}_{2}$ | 187. | MgS | 79.4 | NaOH | 102. |
| MnO | 90.8 | $\mathrm{CdCl}_{2}$ | 93.2 | $\mathrm{Na}_{2} \mathrm{~S}$ | 89.3 | $\mathrm{Na} \cdot \mathrm{H}_{2} \mathrm{O} \cdot \mathrm{Aq}-\mathrm{H}$ | 44.* |
| $\mathrm{MnO}_{2}$ | 123. | $\mathrm{CoCl}_{2}$ | 76.5 | PbS | 19.3 | $\frac{1}{2}\left(2 \mathrm{Na} \cdot \mathrm{O} \cdot \mathrm{H}_{2} \mathrm{O}\right)$ | 68.* |
| $\mathrm{Mn}_{3} \mathrm{O}_{4}$ | 325. | $\mathrm{CuCl}_{2}$ | 51.5 | $\mathrm{CaSO}_{4}$ | 262. | ${ }^{\frac{1}{2}}\left(\mathrm{Na}_{2} \mathrm{O} \cdot \mathrm{H}_{2} \mathrm{O} \cdot \mathrm{Aq}\right)$ | 30.* |
| $\mathrm{MoO}_{2}$ | 143. | CuCl | 34.1 | $\mathrm{CuSO}_{4}$ | 111.5 | KOH | 103.5 |
| $\mathrm{MoO}_{3}$ | 174. | $\mathrm{FeCl}_{2}$ | 82.1 | $\mathrm{H}_{2} \mathrm{SO}_{4} \mathrm{sggg}$ | 193. | $\mathrm{K} \cdot \mathrm{H}_{2} \mathrm{O} \cdot \mathrm{Aq}-\mathrm{H}$ | 45.* |
| $\mathrm{N}_{2} \mathrm{O} \mathrm{gggg}$ | -18.2 | $\mathrm{FeCl}_{3}$ | 96.0 | $-\mathrm{SO}_{3} \cdot \mathrm{H}_{2} \mathrm{O}^{*}$ | 21.3 | $\frac{1}{3}\left(2 \mathrm{~K} \cdot \mathrm{O} \cdot \mathrm{H}_{2} \mathrm{O}\right)$ | 69.* |
| NOggg | -21.6 | HCl ggl | 22. | $\mathrm{Hg}_{2} \mathrm{SO}_{4}$ | 175. | $\frac{1}{2}\left(\mathrm{~K}_{2} \mathrm{O} \cdot \mathrm{H}_{2} \mathrm{O} \cdot \mathrm{Aq}\right)$. | 35.5* |
| $\mathrm{NO}_{2}$ | - 8.1 | HgCl | 31.3 | $\mathrm{HgSO}_{4}$ | 165. |  |  |
| $\mathrm{Na}_{2} \mathrm{O}_{4}$ | - 2.6 | $\mathrm{HgCl}_{2}$ | 53.3 | $\mathrm{K}_{2} \mathrm{SO}_{4}$ | 344.3 |  |  |

[^86]TABLE 180.-THERMOCHEMISTRY. CHEMICAL ENERGY DATA (concluded)

## Part 2.-Heats of formation of ions in kilogram-calories

+ and - signs indicate signs of ions and the number of these signs the valency. For the ionization of each gram-molecule of an element divide the numbers in the table by the valency, e. g., $9.00 \mathrm{~g} \mathrm{Al}=9.00 \mathrm{~g} \mathrm{Al}^{+}+40.3 \mathrm{~kg} \mathrm{cal}$. When a solution is of such dilution that further dilution does not increase its conductivity, then the heats of formation of substances in such solutions may be found as follows: $\mathrm{FeCl}_{2} \mathrm{Aq}=+22.2+2 \times 39.1=100.4 \mathrm{~kg}$ cal. $\mathrm{CuSO}_{4} \mathrm{Aq}=-15.8$ $+214.0=198.2 \mathrm{~kg} \mathrm{cal}$.

| $\mathrm{Ag}+$ | $-25.3$ | $\mathrm{NH}_{4}+$ | +32.7 +37.5 | $\mathrm{AsO}_{4}-$ - | +215.0 | $\mathrm{IO}_{3}-$ | + 55.8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Al +++ | $+121.0$ | $\mathrm{NH}_{4} \mathrm{O}+$ | + 37.5 | $\mathrm{Br}-$ | + 28.2 | $\mathrm{IO}_{4}-$ | + 46.5 |
| Co + + | +170.0 | $\mathrm{Na}+$ | + 57.3 | $\mathrm{BrO}_{3}-$ | + 11.2 | $\mathrm{OH}-$ | + 54.4 |
| $\mathrm{Ca}++$ | +133.? | $\mathrm{Ni}++$ | + 16.0 | $\mathrm{CO}_{3}-$ | +160.8 | $\mathrm{PO}_{4}$ - - - | +298.0 |
| $\mathrm{Cd}++$ | + 18.4 | $\mathrm{Mg}++$ | +108.8 | $\mathrm{Cl}-$ | + 39.1 | $\mathrm{S}_{2} \mathrm{O}_{3}-$ - | +1386 |
| $\mathrm{Cu}++$ | - 16.0 | $\mathrm{Mn}++$ | + 50.2 | ClO- | + 26.0 | $\mathrm{S}_{3} \mathrm{O}_{6}$-- | +278.2 |
|  | -15.8? | $\mathrm{Pb}++$ | + 4.0 | $\mathrm{ClO}_{3}-$ | + 23.4 | $\mathrm{S}_{4} \mathrm{O}_{6}$-- | +260.8 |
| $\mathrm{Fe}++$ | + 22.2 | $\mathrm{Rb}+$ | +625.0 | $\mathrm{ClO}_{4}-$ | - 38.7 | $\mathrm{SO}_{3}$-- | +151.0 |
| $\mathrm{Fe}+++$ | - 9.3 | $\mathrm{Sn}+++$ | + 3.3 | $\mathrm{HCO}_{3}-$ | +163.0 | $\mathrm{SO}_{4}$ - - | +214.0 |
| H+ | 0.0 | $\mathrm{Sr}++$ | +119.6 | $\mathrm{HPO}_{2}-$ | +143.9 | Se - - | - 35.6 |
| $\mathrm{Hg}+$ | - 19.8 | $\mathrm{Tl}+$ | + 1.7 | $\mathrm{HPO}_{3}-$ | +229.6 | $\mathrm{SeO}_{3}$ - - | +119.6 |
| K+ | + 61.8 | $\mathrm{Zn}++$ | + 35.0 | $\mathrm{HPO}_{4}$ - - | +304.8 | $\mathrm{SeO}_{4}$ - - | +144.8 |
| $\mathrm{Li}+$ | +62.8 | 2n+ |  | HS - | + 1.2 | Te-- | - 34.8 |
|  |  |  |  | $\mathrm{NO}_{2}-$ | + 27.0 | $\mathrm{TeO}_{3}$ - - | + 77.0 |
|  |  |  |  | $\mathrm{NO}_{3}-$ | + 48.9 | TeO4-- | + 98.4 |
|  |  |  |  | I - | + 13.1 | S - - | - 12.6 |

## TABLE 181.—IGNITION TEMPERATURES OF GASEOUS MIXTURES

Ignition temperature taken as temperature necessary for hot body immersed in gas to cause ignition; slow combination may take place at lower temperatures. Gases were mixed with air. Practically same temperatures as with $\mathrm{O}_{2}$.

| Benzene and ai | $1062^{\circ} \mathrm{C}$ | Ether and air................. 1033 |
| :---: | :---: | :---: |
| Coal gas and air |  | Ethylene and air............... 1000 |
| CO and air.. | 931 | Hydrogen and air.............. 747 |

## TABLE 182.-HEATS OF NEUTRALIZATION IN KILOGRAM-CALORIES

The heat generated by the neutralization of an acid by a base is equal, for each gram-molecule of water formed, to 13.7 kg cal plus the heat produced by the amount of un-ionized salt formed, plus the sum of the heats produced in the completion of the ionizations of the acid and the base.

| Base | $\mathrm{HCl} \cdot \mathrm{aq}$ | $\mathrm{HNO}_{3}$-aq | $\mathrm{H}_{2} \mathrm{SO}_{4} \cdot \mathrm{aq}$ | HCN aq | $\mathrm{CH}_{3} \mathrm{COOH} \cdot \mathrm{aq}$ | $\mathrm{H}_{2} \cdot \mathrm{CO}_{3} \cdot \mathrm{aq}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{KOH} \cdot \mathrm{aq}$ | 13.7 | 13.8 | 15.7 | 2.9 | 13.3 | 10.1 |
| $\mathrm{NaOH} \cdot \mathrm{aq}$ | 13.7 | 13.7 | 15.7 | 2.9 | 13.3 | 10.2 |
| $\mathrm{NH}_{4} \mathrm{OH} \cdot \mathrm{aq}$ | 12.4 | 12.5 | 14.5 | 1.3 | 12.0 | 8. |
| ${ }_{\frac{1}{2}} \mathrm{Ca}(\mathrm{OH})_{2} \cdot \mathrm{aq}$ | 14.0 | 13.9 | 15.6 | 3.2 | 13.4 | 9.5 |
| $\frac{1}{2} \mathrm{Zn}(\mathrm{OH})_{2} \cdot \mathrm{aq}$ | 9.9 | 9.9 | 11.7 | 8.1 | 8.9 | 5.5 |
| $\frac{1}{2} \mathrm{Cu}(\mathrm{OH})_{2} \cdot \mathrm{aq}$ | 7.5 | 7.5 | 9.2 |  | 6.2 | - |

## TABLE 183.-HEATS OF DILUTION OF $\mathrm{H}_{2} \mathrm{SO}_{4}$

In kilogram-calories by the dilution of 1 gram-molecule of sulfuric acid by m gram molecules of water.

| $\mathrm{m} \ldots \ldots$. | 1 | 2 | 3 | 5 | 19 | 49 | 99 | 199 | 399 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| kg cal $\ldots$ | 6.38 | 9.42 | 11.14 | 13.11 | 16.26 | 16.68 | 16.86 | 17.06 | 17.31 |

Introduction and definitions.-The mechanical properties of most materials vary between wide limits; the following figures are given as being representative rather than what may be expected from an individual sample. Figures denoting such properties are commonly given either as specification or experimental values. Unless otherwise shown, the values below are experimental.

Credit for the information included on metals is due to the National Bureau of Standards ${ }^{55}$ and the publications of the Aluminum Co. of America, ${ }^{56}$ the American Brass Co., and the Chase Brass \& Copper Co. ${ }^{57}$

Most of the data shown in these tables are as determined at ordinary room temperature, averaging $20^{\circ} \mathrm{C}\left(68^{\circ} \mathrm{F}\right)$. The properties of most metals and alloys vary considerably from the values shown when the tests are conducted at higher or lower temperatures.

The following definitions govern the more commonly confused terms shown in the tables. In all cases the stress referred to in the definitions is equal to the total load at that stage of the test divided by the original cross-sectional area of the specimen (or the corresponding stress in the extreme fiber as computed from the flexure formula for transverse tests).
Brinell hardness numeral (abbreviated B. h. n.).-Ratio of pressure on a sphere used to indent the material to be tested to the area of the spherical indention produced. The standard sphere used is a $10-\mathrm{mm}$-diameter hardened steel ball. The pressures used are 3000 kg for steel and 500 kg for softer metals, and the time of application of pressure is 30 seconds. Values shown in the tables are based on spherical areas computed in the main from measurements of the diameters of the spherical indentations, by the following formula:

$$
\text { B. h. n. }=P \div \pi t D=P \div \pi D\left(D / 2-\sqrt{D^{2} / 4-d^{2} / 4}\right) \text {. }
$$

$P=$ pressure in kg, $t=$ depth of indentation, $D=$ diameter of ball, and $d=$ diameter of indentation-all lengths being expressed in mm. Brinell hardness values have a direct relation to tensile strength, and hardness determinations may be used to define tensile strengths by employing the proper conversion factor for the material under consideration.

Elastic limit.-Stress which produces a permanent elongation (or shortening) of 0.001 percent of the gage length, as shown by an instrument capable of this degree of precision (determined from set readings with extensometer or compressometer). In transverse tests the extreme fiber stress at an appreciable permanent deflection.

Erichsen value.-Index of forming quality of sheet metal. The test is conducted by supporting the sheet on a circular ring and deforming it at the center of the ring by a spherical pointed tool. The depth of impression (or cup) in mm required to obtain fracture is the Erichsen value for the metal. Erichsen standard values for trade qualities of soft metal sheets are furnished by the manufacturer of the machine corresponding to various sheet thicknesses.

Alloy steels are commonly used in the heat-treated condition, as strength increases are not commensurate with increases in production costs for annealed alloy steels. Corresponding strength values are accordingly shown for annealed alloy steels and for such steels after having been given certain recommended heat treatments of the Society of Automotive Engineers. The heat

[^87]treatments followed in obtaining the properties shown are outlined on the pages immediately following the tables on steel. It will be noted that considerable latitude is allowed in the indicated drawing temperatures and corresponding wide variations in physical properties may be obtained with each heat treatment. The properties vary also with the size of the specimens heat treated. The drawing temperature is shown with the letter denoting the heat treatment, wherever the information is available.

Modulus of elasticity (Young's modulus).-Ratio of stress within the proportional limit to the corresponding strain-as determined with an extensometer. Note.-All moduli shown are obtained from tensile tests of materials, unless otherwise stated.

Modulus of rupture.-Maximum stress in the extreme fiber of a beam tested to rupture, as computed by the empirical application of the flexure formula to stresses above the transverse proportional limit.

Proportional limit (abbreviated P-limit).-Stress at which the deformation (or deflection) ceases to lee proportional to the load (determined with extensometer for tension, compressometer for compression, and deflectometer for transverse tests).
Shore scleroscope hardness.-Height of rebound of diamond-pointed hammer falling by its own weight on the object. The hardness is measured on an empirical scale on which the average hardness of martensitic high carbon steel equals 100. On very soft metals a "magnifier" hammer is used in place of the commonly used "miversal" hammer and values may be converted to the corresponding "universal" value by multiplying the reading by $4 / 7$. The scleroscope hardness, when accurately determined, is an index of the tensile elastic limit of the metal tested.

Ultimate strength in tension or compression.-Maximum stress developed in the material during test.
Yield point.-Stress at which marked increase in deformation (or deflection) of specimen occurs without increase in loard (determined usually by drop of beam or with dividers for tension, compression, or transverse tests).

## TABLE 184.-INDUSTRIAL WOVEN-WIRE SCREENS*

Industrial wire cloth may be specified in any malleable metal, the physical characteristics of which will permit of its being commercially drawn into wirc and woven into cloth. This industrial wire screen is manufactured with openings from about 15 inches to a very fine wire cloth with openings of .0017 inch, using for larger screens rods 2 inches in diameter and for the smaller-opening cloth, wire .0014 inch in diameter.

| Industrial wire cloth specification, market grade |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mesh | Wire | Onen- | Percent | Mesh | Wire | Open- | Percent |
| lineal inch | diameter inch | ing inch | open <br> area | lineal inch | diameter inch | ing <br> inch | open <br> area |
| $1 \times 1$. | . 080 | . 920 | 84.6 | $30 \times 30$. | . 013 | . 0203 | 37.1 |
| $2 \times 2$. | . 063 | . 437 | 76.4 | $35 \times 35$. | . 011 | . 0176 | 37.9 |
| $3 \times 3$. | . 054 | . 279 | 70.1 | $40 \times 40 \ldots$ | . 010 | . 0150 | 36.0 |
| $4 \times 4$. | . . 047 | . 203 | 65.9 | $50 \times 50 \ldots$ | . . 009 | . 0110 | 30.3 |
| $5 \times 5$. | . 041 | . 159 | 63.2 | $60 \times 60$. | . 0075 | . 0092 | 30.5 |
| $6 \times 6$. | . . 035 | . 132 | 62.7 | $80 \times 80 \ldots$ | . . 0055 | . 0070 | 31.4 |
| $8 \times 8$. | . 028 | . 097 | 60.2 | $100 \times 100$. | . . 0045 | . 0055 | 30.3 |
| $10 \times 10$. | . . 025 | . 075 | 56.3 | $120 \times 120$. | . . 0037 | . 0046 | 30.7 |
| $12 \times 12$. | . 023 | . 060 | 51.8 | $150 \times 150$. | . . 0026 | . 0041 | 37.4 |
| $14 \times 14$. | . 020 | . 051 | 51.0 | $180 \times 180$. | . 0023 | . 0033 | 34.7 |
| $16 \times 16$. | . . 018 | . 0445 | 50.7 | $200 \times 200$. | . . 0021 | . 0029 | 33.6 |
| $18 \times 18$. | . . 017 | . 0386 | 48.3 | $250 \times 250$ | . 0016 | . 0024 | 36.0 |
| $20 \times 20$. | . 016 | . 0340 | 46.2 | $270 \times 270$. | . 0016 | . 0021 | 32.2 |
| $24 \times 24$. | . 014 | . 0277 | 44.2 | $325 \times 325$. | . 0014 | . 0017 | 30.0 |

[^88]TABLE 185.-SOME PHYSICAL PROPERTIES OF THE ELEMENTS


$$
\begin{aligned}
& \quad \begin{array}{c}
\text { Tensile } \\
\text { strength } \\
\mathrm{kg} / \mathrm{mm}^{2}
\end{array} \\
& \ldots \\
& \cdots \\
& \cdots .33 \\
& \cdots .15 \text { (sand cast) } \\
& 39.0 \text { (annealed) } \\
& 120 \text { (annealed } \\
& \quad \begin{array}{l}
\text { wire) }
\end{array} \\
& \cdots \quad \\
& \cdots 32.3 \\
& \cdots \\
& \cdots \\
& \cdots \\
& \cdots
\end{aligned}
$$

4

$$
\begin{aligned}
& \text { ن } \\
& 0 \\
& 0 \\
& 0 \\
& 0
\end{aligned}
$$



Element
${ }^{\circ} \mathrm{At}-62^{\circ} \mathrm{C}$.
TABLE 185.-SOME PHYSICAL PROPERTIES OF THE ELEMENTS (concluded)

| Rela. tive hard ness | Density at $20^{\circ} \mathrm{C}$ $\mathrm{g} / \mathrm{cm}^{8}$ | Melting point ${ }^{\circ} \mathrm{C}$ | Specific heat at r. t . ${ }^{\mathrm{cal}} \mathrm{og}^{-1}{ }^{-1}$ | Latent <br> heat of fusion $\mathrm{cal} / \mathrm{g}$ | Coeff. of linear thermal expansion <br> ${ }^{\circ} \mathrm{C}$ at r.t. $\times 10^{8}$ | Thermal conductivity at r.-t. watts $\mathrm{cm}^{-1}$ | Electrical resistivity microhm-cm | Modulus of elas$\underset{\mathrm{kg} / \mathrm{mm}^{2}}{\substack{\text { ticit } \\ \text { 2 }}}$ | Tensile strength $\mathrm{kg} / \mathrm{mm}^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7.7 | $>1050$ |  |  |  |  |  |  |  |
|  | 2.5 | 1400 |  |  |  |  |  |  |  |
| 2.0 | 4.81 | $217.4 \pm 5$ | . 084 | . . | 37 |  | $1.20\left(20^{\circ} \mathrm{C}\right)$ |  |  |
| 7.0 | 2.4 | $1410 \pm 20$ | . 176 |  | 2.8-7.3 | . 84 | $85 \times 10^{3}\left(20^{\circ} \mathrm{C}\right)$ | 11000 |  |
| 2.7 | 10.49 | $960.8 \pm .0$ | . 056 | 24.3 | 18.9 | 4.08 | $1.62\left(20^{\circ} \mathrm{C}\right)$ | 7200 | 15.1 (rod, annealed) |
| . 4 | . 97 | $97.82 \pm .2$ | . 295 | 27.5 | 71 | 1.35 | $4.2\left(0^{\circ} \mathrm{C}\right)$ | - ... |  |
| 1.8 | 2.6 | $770 \pm 10$ |  | 25 |  |  | $22.76\left(20^{\circ} \mathrm{C}\right)$ |  |  |
| 2.0 | 2.07 | $119 \pm .2$ | . 175 | 9.3 | $64 \ddagger$ | $26.4{ }^{\circ}$ | $2 \times 10^{23}\left(20^{\circ} \mathrm{C}\right)$ |  |  |
| 7 | 16.6 | $2980 \pm 100$ | . 036 |  | 6.6 | . 54 | $14.6\left(18^{\circ} \mathrm{C}\right)$ | 19000 | 50 (wire) |
| 3.3 | 6.24 | $2700 *$ 450 | . 047 | . | $16.8 \ddagger$ | . 060 |  | 210 |  |
|  |  | $1450 \pm 5$ | . | $\ldots$ |  | . 06 |  | 21 | 1.12 (wire) |
| 1.2 | 11.85 | $303.6 \pm 3$ | . 031 | 7.2 | 28 | . 39 | $17.65\left(0^{\circ} \mathrm{C}\right)$ |  |  |
|  | 11.5 | $1695 \pm 150$ | . 028 |  | $11.1 \pm$ |  | $18.62\left(20^{\circ} \mathrm{C}\right)$ |  | 56.0 (wire) |
| 1.8 | 7.30 | $231.91 \pm .1$ | . 054 | 14.4 | 23 | . 64 | $11.5\left(20^{\circ} \mathrm{C}\right)$ | 41100 | 1.4 |
| 4.0 | 4.54 | $1675 \pm 100$ | . 142 | 4 | 8.5 | 1.99 | $80\left(0^{\circ} \mathrm{C}\right)$ | 8500 |  |
| 7 | 19.3 | $3380 \pm 20$ | . 034 | 44 | 4.3 | 1.99 | $5.5\left(20^{\circ} \mathrm{C}\right)$ | 35000 | 270 (wire) |
|  | 18.7 | $1132 \pm 1$ | . 028 | . . . | ... |  | $60\left(18^{\circ} \mathrm{C}\right)$ | ... |  |
|  | 5.68 | $1890 \pm 50$ | . 115 | ... | ... |  | ... |  |  |
|  | $5.495{ }^{\text {d }}$ | $-112.5 \pm 1$ | $\therefore$ | ... | ... | $5.19{ }^{\circ}$ | . . | ... | $\ldots$ |
|  |  | 824 | ... | $\ldots$ |  | . . | ... |  |  |
|  | 5.51 | $1490 \pm 200$ |  |  |  |  |  |  |  |
| 2.5 | 7.14 | $419.50 \pm .1$ | . 09 | 24.1 | 17-39 $\dagger$ | 1.1 | $5.92\left(20^{\circ} \mathrm{C}\right)$ | 8400 | 10.5 |
| 4.5 | 6.4 | $1852 \pm 700$ | . 066 | ... | 5.6 | . . | $41.0\left(0^{\circ} \mathrm{C}\right)$ | 7500 | 30.0 (rod, annealed) |

[^89]TABLE 186.-MECHANICAL PROPERTIES OF ALUMINUM AND ALUMINUM ALLOYS **

| $\begin{aligned} & \text { səquinu } \\ & \text { ssəupieH } \end{aligned}$ | $\cdots 8$ | : | 8 | $\stackrel{3}{7}$ | $\underset{\sim}{\mathrm{O}}$ | : | - | $\pm$ | $\infty$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & i \\ & \dot{+} \end{aligned}$ | : | $\frac{1}{2}$ | $\underset{N}{+}$ | $\infty$ | : | $\ddagger$ | : | - |
| иоџе8иоэ 岂 |  | $\begin{aligned} & \underset{\dot{A}}{N} \\ & N \\ & N \end{aligned}$ | $\stackrel{*}{N}$ | . <br> N <br> $\stackrel{*}{N}$ | $\stackrel{\odot}{\text { N }}$ |  | . <br> N <br> 士 | $\underset{\sim}{N}$ | - |

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TABLE 186．－MECHANICAL PROPERTIES OF ALUMINUM AND ALUMINUM ALLOYS（continued）

| 8uวtis ${ }_{\text {® }}$ | 官 | $\begin{aligned} & \text { O} \\ & \underset{\sim}{\ddot{H}} \\ & \stackrel{y}{0} \end{aligned}$ | $\stackrel{\text { E. }}{\stackrel{\Delta}{む}}$ | だ | た | だ | だ | だ | 安 | $\underset{\underset{\Delta g}{E}}{ }$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ç ç ç | ֻ̊ | $\stackrel{\text { ヘٌ }}{\substack{~}}$ | $\stackrel{\text { č }}{\substack{4 \\ \hline}}$ | ペ | $\stackrel{80}{\mathrm{~N}}$ | ペ | $\begin{gathered} \text { ペ } \\ \text { Con } \end{gathered}$ | $\stackrel{\text { ¢ }}{\text { ¢ }}$ | ペ |
|  | $\bigcirc$ | $\alpha^{\infty}$ | $0$ | $\stackrel{0}{\circ}$ | $\cdots$ | $\stackrel{n}{N}$ | $\pm$ | $\mp$ | $\cdots$ | $\stackrel{\sim}{\square}$ |
|  | － | $\vdots$ | ： |  | ： | ： | ： | ： | ： | ： |





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| :---: |

Aluminum－copper－silicon alloys $\mathrm{Cu}-4.0, \mathrm{Si}-3.0 \quad$ Sand－cast（108） $\mathrm{Cu}-4.5, \mathrm{Si}-2.5 \quad$ Chill－cast：h．－t． Cu－7．0，Si－2．0，Sand－cast $\mathrm{Zn}-1.5, \mathrm{Fe}-1.2$
Aluminum－copper－zinc alloys $\mathrm{Cu}-7.0, \mathrm{Zn}-1.7, \quad$ Sand－cast（112） Aluminum－magnesium alloys $\mathrm{Mg}-1.0, \mathrm{Si}-.6 \quad$ Wrought；ann． $\mathrm{Mg}-1.3, \mathrm{Si}-.7$ （ra－2．5，Cr－ 25 （52S－H） Sand－cast（214） Chill－cast（A 214） Sand－cast h．－t．
$(220-\mathrm{T} 4)$ nese alloys
Wrought ；ann．（ $3 \mathrm{~S}-\mathrm{O}$ ）
$\mathrm{Mn}-1.25, \mathrm{Mg}-1.0$ Annealed

[^91]1
TABLE 186.-MECHANICAL PROPERTIES OF ALUMINUM AND ALUMINUM ALLOYS (concluded)

TABLE 187．－MECHANICAL PROPERTIES OF BRASSES AND BRONZES＊


|  | ¢ | 以すへm心 | 以すへの： | FinNm： | Nonm | Nignm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| प18uว」） ว！！suวป | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & \end{aligned}$ |  ๗Niñ゙ホ |  | $\begin{aligned} & \text { MNM } \\ & \text { mincio } \end{aligned}$ | $\begin{aligned} & \text { NーM } \\ & \text { MN } \\ & \text { Nin } \end{aligned}$ |  |
|  | $\begin{aligned} & \square Y \\ & \dot{\sim} \end{aligned}$ | $\rightarrow$ 以ñoos <br> サல゙オジウテ |  | $\begin{aligned} & \text { onvon } \\ & \text { Novinin } \end{aligned}$ | バびす | تivNM |
|  | $\begin{aligned} & i \\ & 0 \\ & \underset{x}{0} \\ & 0 \\ & i \end{aligned}$ | $\begin{aligned} & i \\ & 0 \\ & X \\ & \underset{X}{X} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & i \\ & 0 \\ & x \\ & \infty \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & \underset{x}{0} \\ & \underset{i}{2} \end{aligned}$ |  | $\begin{aligned} & 0 \\ & \underset{\sim}{x} \\ & \underset{-\infty}{9} \end{aligned}$ |
|  Kไ！n！ | $\begin{aligned} & \text { n } \\ & \text { ñ } \end{aligned}$ | $\begin{aligned} & \infty \\ & \underset{\sim}{0} \\ & 0 \end{aligned}$ | $$ | $\begin{aligned} & \infty \\ & \text { in } \\ & \text { in } \end{aligned}$ | $\underset{\underset{\sim}{\mathrm{N}}}{\substack{0}}$ | $\begin{aligned} & \text { K } \\ & \text { j} \end{aligned}$ |
|  | $\begin{aligned} & \text { + } \\ & \text { Ǹ } \end{aligned}$ | $\underset{\text { N }}{\mathrm{N}}$ | ষ্ | N్ల | $\stackrel{\Im}{\nabla}$ | ษ |
|  | $\stackrel{\infty}{+}$ | $\underset{\infty}{N}$ | $\begin{aligned} & N \\ & N \\ & \infty \end{aligned}$ | $\begin{aligned} & \hat{0} \\ & \infty \end{aligned}$ | $\cdots$ | ＋ |

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$$
\begin{aligned}
& \text { Hard-drawn } \\
& \text { Hard-drawn } \\
& \text { Hard-drawn }
\end{aligned}
$$

Hard-drawn
Hard-drawn
Hard-drawn
 $\stackrel{i}{\circ}$
$040^{\prime \prime}$ strip ; light ann. 040" strip; quarter hard .50 " strip; as hot-rolled ${ }^{1 \prime}$ " rod; soft ann. $1^{\prime \prime}$ rod; light ann.
$1^{\prime \prime}$ rod; quarter hard (9\%)
$1^{\prime \prime}$ rod; half hard ( $18 \%$ ) $1^{\prime \prime} \times .05^{\prime \prime}$ tube ; .025 mm ann. $.040^{\prime \prime}$ strip; half hard hard hard light ann.


No $\stackrel{\infty}{\circ} \stackrel{n}{\sim}$
$\stackrel{\infty}{\stackrel{\infty}{~}}$ ヘั๋ ษ
$\underset{\infty}{\text { Y }}$
$\underset{\infty}{\mathbb{N}} \underset{\infty}{\infty}$

Conductivity bronzes
$80 \%$ conductivity bronze - azuorq К!!и!
…әzuoдq Кұ!м!

## Special brasses

Naval brass
Antimonial $\ldots . . . . . . . .$. Cu-71; $\mathrm{Zn}-27.97$


Bushing bronze $\ldots \ldots \ldots . \mathrm{Cu}$ (90; $\mathrm{Zn}-9.5$;
TABLE 187.-MECHANICAL PROPERTIES OF BRASSES AND BRONZES (concluded)

|  |  | $\begin{aligned} & \stackrel{\stackrel{\rightharpoonup}{ज}}{\stackrel{y}{5}} \\ & \stackrel{0}{0} \\ & \mathrm{~g} / \mathrm{cm}^{3} \end{aligned}$ |  |  |  |  |  |  | $\begin{gathered} \text { un } \\ \stackrel{0}{0} \\ \stackrel{0}{L} \\ \text { w. } \\ \text { No. } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phosphor bronze 5\% <br>  | $.040^{\prime \prime}$ strip; .035 mm anm. <br> $.040^{\prime \prime}$ strip; hard (37\%) <br> $.040^{\prime \prime}$ strip; spring ( $60 \%$ ) <br> $.100^{\prime \prime}$ wire; spring ( $84 \%$ ) | 8.85 | . 157 | 12.28 | $1.78 \times 10^{-5}$ | 14.1 <br> 52.7 <br> 56.2 | $\begin{aligned} & 34.5 \\ & 56.9 \\ & 70.3 \\ & 98.2 \end{aligned}$ | $\begin{array}{r} 58 \\ 10 \\ 4 \\ 2 \end{array}$ | $\begin{aligned} & \text { F } 75 \text {, } \\ & \text { B } 28 \\ & \text { B } 87 \\ & \text { B } 93 \end{aligned}$ |
| Phosphor bronze $8 \%$ (grade C) $\ldots \ldots \ldots \ldots \underset{\mathrm{P}-.25}{\mathrm{Cu}} \underset{\mathrm{Cn}-7.75 \text {; }}{ }$ | $.040^{\prime \prime}$ strip; .035 mm ann. <br> $.040^{\prime \prime}$ strip; hard ( $37 \%$ ) <br> .040 " strip; spring ( $60 \%$ ) <br> $.100^{\prime \prime}$ wire ; spring ( $68 \%$ ) | 8.80 | . 120 | 15.65 | $1.82 \times 10^{-5}$ | $\begin{aligned} & 16.9 \\ & 50.6 \end{aligned}$ | $\begin{aligned} & 40.8 \\ & 65.4 \\ & 78.7 \\ & 98.2 \end{aligned}$ | $\begin{array}{r} 65 \\ 10 \\ 3 \end{array}$ | $\begin{gathered} \text { F-80; B-50 } \\ \text { B } 93 \\ \text { B } 98 \end{gathered}$ |
| 444 Bronze $\ldots \ldots \ldots \ldots . .$$\mathrm{Cu}-88 ; \mathrm{Sn}-4$; <br> $\mathrm{Zn}-4 ; \mathrm{Pb}-4$ | $.040^{\prime \prime}$ strip; .035 mm ann. $1^{\prime \prime}$ rod; hard $(20 \%)$ | 8.88 | . 206 | 9.07 | $1.72 \times 10^{-5}$ | $\cdots$ | $\begin{aligned} & 31.6 \\ & 457 \end{aligned}$ | $\begin{aligned} & 55 \\ & 20 \end{aligned}$ | F 65 |
| Olympic bronze <br> Olympic bronze, type A... Cu-96; Si-3; $\mathrm{Zn}-1$ | $.040^{\prime \prime}$ strip ; .070mm ann. <br> $.040^{\prime \prime}$ strip; spring ( $60 \%$ ) $1^{\prime \prime}$ rod; extra hard ( $50 \%$ ) <br> $.100^{\prime \prime}$ wire ; hard ( $60 \%$ ) <br> $.100^{\prime \prime}$ wire ; spring ( $80 \%$ ) | 8.52 | . 087 | 24.6 | $1.80 \times 10^{-5}$ | $\begin{aligned} & 14.75 \\ & 43.8 \\ & 42.2 \\ & 45.7 \\ & 49.3 \end{aligned}$ | $\begin{array}{r} 39.4 \\ 77.3 \\ 75.9 \\ 87.9 \\ 102.0 \end{array}$ | $\begin{array}{r} 63 \\ 4 \\ 13 \\ 5 \\ 3 \end{array}$ | $\begin{aligned} & \text { F } 75 \\ & \text { B } 97 \\ & \text { B } 95 \end{aligned}$ |
| Special engineering alloy <br> Tellurium copper ......... Cu-99.5 ; Te-. 5 | $\frac{1}{8}{ }^{\prime \prime}$ rod, $\frac{1}{2}$ hard ( $20 \%$ ) | 8.94 | . 848 | 1.915 | $1.79 \times 10^{-5}$ | 28.8 | 30.9 | 15 |  |


|  |  | $\begin{gathered} \stackrel{\rightharpoonup}{\omega} \\ \stackrel{y}{ \pm} \\ \text { cgs } \end{gathered}$ | $\begin{gathered} \text { n } \\ \text { cgs } \end{gathered}$ | 言 |  |  |  | $\begin{gathered} \stackrel{5}{\Sigma_{0}} \\ \vdots \\ \vdots \\ \mathrm{~kg} / \mathrm{mm}^{2} \end{gathered}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pure and commercial copper |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \text { Oxygen-free copper } \\ & \text { (OFHC); } \\ & \mathrm{Cu}-99.997 \end{aligned}$ | Rod, $\frac{1}{2}$ in. diam. cold-drawn ( $29 \%$ red) from .125 mm grain size | 8.95 | . 93 | 1.706* | 17.6* | 12,500 | $\ldots$ | 34.5(.5\% extn.) | 36.0 | $14^{\dagger}$ | $12.0\left(3 \times 10^{8}\right)$ | Rs 37 |
| $\begin{aligned} & \text { Oxygen-free copper } \\ & \text { (OFHC); } \\ & \text { Cu-99.996 } \end{aligned}$ | Rod, $\frac{3}{4}$ in. diam. cold-drawn ( $36 \%$ red) from .135 mm grain size | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 12,300 | $\ldots$ | 33 (.5\% extn.) | 33.5 | $20^{\dagger}$ | $\ldots$ | $\ldots$ |
| $\begin{aligned} & \text { Oxygen-free copper } \\ & \text { (OFHC); } \\ & \text { Cu-99.99 } \end{aligned}$ | Rod, hard-drawn | $\ldots$ | $\cdots$ | $\ldots$ | $\ldots$ | 13,000 | 3.45 | 12.7(.01\%) | 29.0 | 298 | $\ldots$ | $\ldots$ |
| Cu -99.95 | Sheet, . 020 in ., soft | $\ldots$ | ... | $\ldots$ | $\ldots$ |  | 4.8 | $\ldots$ | 22.0 | $35 \dagger$ | 7.7 (10 ${ }^{8}$ ) |  |
| " | Sheet, . 020 in., coldworked ( $21 \%$ red) | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |  | 11.0 | ... | 31.2 | $7.8^{\dagger}$ | $9.1\left(10^{8}\right)$ | $\mathrm{R}_{\mathrm{B}} 33$ |
| $\mathrm{Cu}-99.94 ; 0-.030$ | Rod, drawn ( $37 \%$ red) | $\ldots$ | $\ldots$ | ... | ... | 12,100 | 3.4 | 10.0(.01\%) | 26.0 | 328 | $\cdots$ | $\cdots$ |
| copper <br> Electrotough-pitch copper | Rod, 1 in. diam., hot-rolled | 8.92 | . 93 | 1.706* | 17.6* | 9,300 | $\ldots$ | $\begin{gathered} 4.55(.01 \% \\ \text { perm. }) \end{gathered}$ | 22.0 | $59 \dagger$ | $2.8 \pm$ | 41 |
| Electrotough-pitch copper | Cold-rolled | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 7.0 | 15 (.01\% perm.) | 36.5 | $13^{\dagger}$ | 11.0 | $\ldots$ |
| Copper-aluminum alloys |  |  |  |  |  |  |  |  |  |  |  |  |
| Al-3.96 | Cast, annealed |  | $\ldots$ | $\ldots$ | $\ldots$ |  | 4.30 | 6.1(.5\% extn.) | 24.3 | $84 \dagger$ | $\ldots$ | $\ldots$ |
| " | Forged, annealed | $\ldots$ | $\ldots$ | ... | $\ldots$ |  | 5.75 | 8.8(.5\% extn.) | 33.0 | $81{ }^{\dagger}$ | $\ldots$ | $\cdots$ |
| A1-8.0 | Sheet or plate, soft | 7.78 | . 17 | 11.8* | 17.8* |  |  | 17 (.5\% extn.) | 42 | $60^{\dagger}$ | $\ldots$ | Re 30 |
| " | Sheet or plate, hard |  |  | ... | ... | 10,500 |  | 42 (.5\% extn.) | 84 | $4{ }^{+}$ | $\ldots$ | $\mathrm{R}_{\mathrm{B}} 99$ |
| ** For references, $* \times 10^{-0} . \quad \dagger 2 \mathrm{in}$ | se footnotes 55 and 57 , p. $\ddagger$ Alternating torsion. | \& 4 V |  |  | (con | tinued) |  |  |  |  |  |  |


AND COPPER ALLOYS (continued)



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Copper-aluminum-iron alloys Al-5.39, Fe-5.14 Forged Al-8, Fe-2.5 Rod, soft Al-8.6, Fe-2.9 Sand-cast Al-9, Fe-3 Forged

Copper-aluminum-iron-manganese alloys Al-7.18, $\mathrm{Fe}-.62$, Sand-cast


|  | TABLE 188.-MECH | NIC |  | ERT | S | F COPP | PER AN | ND COPPER | ALLOYS | (contin |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| percent |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \stackrel{5}{0} \\ & \stackrel{.0}{\pi} \\ & \stackrel{\omega}{0} \\ & \text { percent } \end{aligned}$ |  |  |
| Copper-aluminum-manganese alloys |  |  |  |  |  |  |  |  |  |  |  |  |
| Al-7, Mn-1 | Sheet, . 2 in., coldrolled (50\% red) | ... | $\ldots$ | . . | . $\cdot$ | ... | 54.0 | $\ldots$ | 74 | $12 \dagger$ | . . | ... |
| Al-10, Mn-1 | Chill-cast |  |  |  |  | $\ldots$ | ... | 25.0 (yld. pt.) | 62.5 | $25 \dagger$ | . $\cdot$ | ... |
| Copper-aluminum-nickel alloys |  |  |  |  |  |  |  |  |  |  |  |  |
| Al-7, $\mathrm{Ni}-1$ | Sheet, . 2 in., coldrolled ( $50 \%$ red) | ... | $\cdots$ | . $\cdot$ | -• | ... | 60.0 | . | 80.0 | $6 \dagger$ | ... | ... |
| $\begin{aligned} & \mathrm{Al}-9.4, \mathrm{Ni}-7.4, \\ & \mathrm{Fe}-4.1 \end{aligned}$ | Rod, 1 in. diam., chill-cast | 7.57 | ... | . $\cdot$ | . | ... | ... | $\begin{gathered} 4.03(.15 \% \\ \text { perm. }) \end{gathered}$ | 67 | $5 \dagger$ | . $\cdot$ | 188 |
| $\begin{aligned} & \mathrm{Al}-10.1, \mathrm{Ni}-7.6, \\ & \mathrm{Si}-.4 \end{aligned}$ | Rod, 1 in. diam., chill-cast | 7.58 | . . | . $\cdot$ | . $\cdot$ | . $\cdot$ | . | 44 (.15\% perm.) | 63.5 | $2 \dagger$ | ... | . $\cdot$ |
| Copper-aluminum-silicon alioys |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \mathrm{Al}-7.2, \mathrm{Si}-1.88 \\ & \mathrm{Fe}-.11 \end{aligned}$ | Rod, 1 in. square, chill-cast from $2055^{\circ} \mathrm{F}$ | $\cdots$ | . | $\cdots$ | - $\cdot$ | . | . $\cdot$ | 22.0 (yld. pt.) | 53.0 | $19^{\text {a }}$ | . $\cdot$ | 139 |
| $\begin{aligned} & \mathrm{Al}-7.2, \mathrm{Si}-1.88 \text {, } \\ & \mathrm{Fe}-.11 \end{aligned}$ | Rod, $\frac{3}{4}$ in. diam., forged | $\cdots$ | . | $\cdots$ | - | . $\cdot$ | ... | 42 (yld. pt.) | 69.5 | $25^{\text {a }}$ | $\ldots$ | 186 |
| Copper-aluminum-zinc alloys |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \mathrm{Al}-8.89, \mathrm{Zn}-1.40, \\ & \mathrm{Fe}-.15 \end{aligned}$ | Rod, $\frac{3}{4}$ in. diam., extruded and drawn | $\cdots$ | . $\cdot$ | -•• | ... | 12,300 | 12.4 | $\begin{gathered} 29.3(.01 \% \\ \text { perm. }) \end{gathered}$ | 25.2 | 378 | . | -• |
| Copper-arsenic alloys |  |  |  |  |  |  |  |  |  |  |  |  |
| As-.33, Ag-. 10 | Rod, $\frac{7}{8}$ in. diam., drawn ( $7 \%$ red) | . $\cdot$ | . | . | $\cdots$ | $\cdots$ | 20.4 | $\begin{gathered} 7.7(.01 \% \\ \quad \text { perm. }) \end{gathered}$ | 25.2 | 478 | . | . |
| " " | Rod, $\frac{7}{8}$ in. diam., drawn ( $7 \%$ red) ann. 100 hr at $390^{\circ} \mathrm{F}$ | . | . | . $\cdot$ | $\cdots$ | . . | 10.4 | $\cdots$ | 24.7 | 468 | $\ldots$ | - |
| 21.3 in . ${ }^{\text {a }}$ (continued) |  |  |  |  |  |  |  |  |  |  |  |  |






(yld. pt.)
14.7 (yld. pt.)
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Sand-cast from 1750
$1900^{\circ} \mathrm{F}$
Copper-manganese alloys
Mn-13 ; Al-9
$\mathrm{Ni} 30.48 \mathrm{Mn}-22, \quad$ Rod, $\frac{3}{4}$ in. diam.,
cold-drawn (15\%
red) from .030 mm grain size
 red）from .030 mm
 $840^{\circ} \mathrm{F}$ Sand－cas $1400^{\circ} \mathrm{F}$ Rod， 1 hr at $1450^{\circ} \mathrm{F}$ ， Rod，cold－rolled $\mathrm{Ni}-30.48, \mathrm{Mn}-.22$,
$\mathrm{Fe}-.07$
Constantan
$\mathrm{Ni}-45, \mathrm{Mn}-.5-1.0$ ， $\mathrm{Ni}-44.77, \mathrm{Mn}-.89$, $\mathrm{Ni}-44.77, \mathrm{Mn}-.89$,
$\mathrm{Fe}-.66, \mathrm{C}-. \mathrm{U} 78$




$35.4(.2 \%)$
$60.0(.2 \%)$
$39.0(.01 \%$
perm. $)$




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$\begin{array}{cc}\text { percent } \\ \text { Copper-nickel-beryllium alloys } \\ \mathrm{Ni}-2.0, \mathrm{Be}-.2 & \text { Quenched from } \\ & 1650^{\circ} \mathrm{F} \text {, cold-drawn, } \\ & (56 \% \text { red }) \\ " \quad \text { " } & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \end{array}$
Copper-nickel-manganese alloys
Ni-13.5, Mn-5, Rod, 1 in. diam.,
extruded, colddrawn ( $10 \%$ red)
Rod, 1 in. diam., cold-drawn, 2 hr
Copper-nickel-silicon alloys
$\mathrm{Cu}-94.15, \mathrm{Ni}-5.14$, Sheet, .020 in., soft
Si-rem.
Copper-nickel-tin alloys
$\mathrm{Ni}-29.08, \mathrm{Sn}-.95, \quad$ Rod, 1 in. diam.,
cold-drawn
Copper-nickel-zinc alloys
Sheet or plate, soft
Sheet or plate, hard
$\mathrm{Ni}-20.22, \mathrm{Zn}-5.26, \quad$ Rod, $\frac{3}{4}$ in. diam.. cold-drawn $15 \%$
red) from .060 mm grain size, 2 hr
at $840^{\circ} \mathrm{F}$

SMITHSONIAN PHYSICAL TABLES



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|  | $\begin{aligned} & 8 \\ & 8 \\ & 1 \end{aligned}$ | 8 0 0 0 |  | $\begin{aligned} & 8 \\ & \text { I } \\ & \text { In } \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & n \end{aligned}$ | $\begin{aligned} & 8 \\ & \infty \\ & \cdots \end{aligned}$ | $\begin{aligned} & 8 \\ & 7 \\ & i \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 6 \\ & \hline 8 \end{aligned}$ |
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TABLE 188.-MECHANICAL

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ： | $\begin{aligned} & \text { o્ } \\ & \underset{\sim}{x} \\ & \underset{\sim}{0} \\ & 0 \\ & \end{aligned}$ | ： | $\begin{aligned} & \infty \\ & \stackrel{\infty}{0} \\ & \stackrel{\rightharpoonup}{0} \end{aligned}$ | $\begin{aligned} & \text { ®⿹\zh26灬 } \\ & \underset{y}{=} \\ & \hline \end{aligned}$ | ！ | － | ！ | $\begin{aligned} & \text { © } \\ & \underset{y}{\infty} \\ & \pm \end{aligned}$ |  |
| no！pesuorg ${ }_{\text {苞 }}^{\text {U．}}$ | $\stackrel{+}{\sim}$ | $\bar{m}$ | $\pm$ | $\stackrel{+}{\square}$ | $\stackrel{\overleftarrow{N}}{ }$ | $\stackrel{i}{n}$ | $\begin{aligned} & 8 \\ & 0 \\ & \hline \end{aligned}$ | $\stackrel{+}{8}$ | N | + $\sim$ $\vdots$ -1 |
|  | $\begin{aligned} & \text { ơ } \\ & \text { Non } \end{aligned}$ | 웅 | $\begin{aligned} & 0 \\ & \hline 8 \end{aligned}$ | $\underset{\sim}{n}$ | $i_{0}^{n}$ | $\begin{aligned} & \text { n } \\ & \infty \end{aligned}$ | $\begin{aligned} & \text { en } \\ & \text { n } \\ & \text { n } \end{aligned}$ | $\frac{0}{m}$ | $\bigcirc$ | N1 |
|  | o | ： |  | ！ | ： | ： |  | ： | $\vdots$ |  |
|  | $\vdots$ | $\stackrel{n}{a}$ | ： | $\frac{3}{m}$ | $\begin{aligned} & \text { y } \\ & \underset{N}{n} \end{aligned}$ | $\stackrel{\infty}{\infty}$ | $\vdots$ | ： | N゙ | ： |
|  | $\begin{aligned} & 8 \\ & 8 \\ & 8 \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 0 \\ & \hline \end{aligned}$ | $\vdots$ | $\begin{aligned} & \text { §ి } \\ & \text { ले } \end{aligned}$ | 8 $\cdots$ | $\begin{aligned} & 8 \\ & \infty \\ & 0 \end{aligned}$ | ： | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | 8 8 0 | ： |
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| шл－шчодтит <br>  | ： | ： | ： | ： | ： | ： | ！ | ： | ： | ： |
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| ${ }_{\text {St！}}$ | ！ | ¢ | $\stackrel{9}{7}$ | ： | ！ | ： | $\bigcirc$ | $\cdots$ | $\underset{\sim}{\sim}$ | $\underset{\infty}{\sim}$ |
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Copper wire: Hard-drawn (and hard-rolled flat copper of thicknesses corresponding to diameter of wire). Specification values. (A. S. T. M. B1-15, U. S. Navy Dept.)

Specific gravity 8.89 at $20^{\circ} \mathrm{C}\left(68^{\circ} \mathrm{F}\right)$.

| Diameter |  | Minimum tensile strength |  | Minimum elongation, percent in 254 mm ( 10 in. ) |
| :---: | :---: | :---: | :---: | :---: |
| ${ }_{\mathrm{mm}}$ | in. | kg/mm ${ }^{2}$ | 1b/in. ${ }^{2}$ |  |
| 11.68 | . 460 | 34.5 | 49,000 | 2.75 |
| 10.41 | . 410 | 35.9 | 51,000 | 3.25 |
| 9.27 | . 365 | 37.1 | 52,800 | 2.80 |
| 8.25 | . 325 | 38.3 | 54,500 | 2.40 |
| 7.34 | . 289 | 39.4 | 56,100 | 2.17 |
| 6.55 | . 258 | 40.5 | 57,600 | 1.98 |
| 5.82 | . 229 | 41.5 | 59,000 | . 1524 1.79 |
|  |  |  |  | in 1524 mm ( 60 in .) |
| 5.18 | . 204 | 42.2 | 60,100 | $1.24$ |
| 4.62 | . 182 | 43.0 | 61,200 | 1.18 |
| 4.12 | . 162 | 43.7 | 62,100 | 1.14 |
| 3.66 | . 144 | 44.3 | 63,000 | 1.09 |
| 3.25 | . 128 | 44.8 | 63,700 | 1.06 |
| 2.90 | . 114 | 45.2 | 64,300 | 1.02 |
| 2.59 | . 102 | 45.7 | 64,900 | 1.00 |
| 2.31 | . 091 | 46.0 | 65,400 | . 97 |
| 2.06 | . 081 | 46.2 | 65,700 | . 95 |
| 1.83 | . 072 | 46.3 | 65,900 | . 92 |
| 1.63 | . 064 | 46.5 | 66,200 | . 90 |
| 1.45 | . 057 | 46.7 | 66,400 | . 89 |
| 1.30 | . 051 | 46.8 | 66,600 | . 87 |
| 1.14 | . 045 | 47.0 | 66,800 | . 86 |
| 1.02 | . 040 | 47.1 | 67,000 | . 85 |

Note.-P-limit of hard-drawn copper wire must average 55 percent of ultimate tensile strength for four largest-size wires in table, and 60 percent of tensile strength for smaller sizes.

## TABLE 190.-COPPER WIRE—MEDIUM HARD-DRAWN

(A. S. T. M. B2-15) Minimum and maximum strengths.

| Diameter |  | Tensile strength |  |  |  | $\underset{\substack{\text { Elongation, } \\ \text { minimum percent } \\ \text { in } 254 \mathrm{~mm}(10 \mathrm{in} .)}}{\text {. }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\overbrace{\text { Minimum }}$ |  | $\underbrace{\text { Maximum }}$ |  |  |
| mm | in. | kg/mm ${ }^{2}$ | 1b/in. ${ }^{2}$ | $\mathrm{kg} / \mathrm{mm}^{2}$ | lb/in. ${ }^{2}$ |  |
| 11.70 | . 460 | 29.5 | 42,000 | 34.5 | 49,000 | 3.75 |
| 6.55 | . 258 | 33.0 | 47,000 | 38.0 | 54,000 | 2.50 |
|  |  |  |  |  |  | in 1524 mm ( 60 in .) |
| 4.12 | . 162 | 34.5 | 49,000 | 39.5 | 56,000 | 1.15 |
| 2.59 | . 102 | 35.5 | 50,330 | 40.5 | 57,330 | 1.04 |
| 1.02 | . 040 | 37.0 | 53,000 | 42.0 | 60,000 | . 88 |

Note.-Representative values only from table in specifications are shown above. P-limit of medium hard-drawn copper averages 50 percent of ultimate strength.

TABLE 191.-COPPER WIRE-SOFT OR ANNEALED
(A. S. T. M. B3-15) Minimum values.

| $\underbrace{\text { Diameter }}$ |  | Minimum tensile strength |  | Elongation in 254 |
| :---: | :---: | :---: | :---: | :---: |
| mm | in. | $\mathrm{kg} / \mathrm{mm}^{2}$ | lb/in. ${ }^{2}$ | percent ${ }^{\text {m }}$ |
| 11.70 to 7.37 | .460 to .290 | 25.5 | 36,000 | 35 |
| 7.34 to 2.62 | . 289 to .103 | 26.0 | 37,000 | 30 |
| 2.59 to . 53 | .102 to . 021 | 27.0 | 38,500 | 25 |
| .51 to .08 | . 020 to . 003 | 28.0 | 40,000 | 20 |

Note.-Experimental results show tensile strength of concentric-lay copper cable to approximate 90 percent of combined strengths of wires forming the cable.
TABLE 192.-MECHANICAL PROPERTIES OF IRON AND STEEL**





| Composition percent | Condition |
| :---: | :---: |
| Chromium steel |  |
| C-.20, Cr-.75, Mn-.57, Si-. 21 | bar, $\frac{3}{4}$ in. diam., normalized at $1700^{\circ} \mathrm{F}$ |
| $\mathrm{C}-.59, \mathrm{Cr}-.82, \mathrm{Mnn}-.83, \mathrm{Si}-.35$ | forged |
| Chromium-niobium steels C-.09, Cr-5.62, Nb-1.04 | bar, 1 in. diam., rolled |
| Chromium-copper steels $\underset{\mathrm{P}-.088}{\mathrm{C}-.11,} \mathrm{Cr}-.53, \quad \mathrm{Cu}-.37, \quad \mathrm{Si}-.82,$ | bar, 1 in. diam., normalized |
| Chromium-molybdenum steels |  |
| C-.08, Cr-5.81, Mo-. 45 | bar, $\frac{3}{4}$ in. diam., 4 hr at $1380^{\circ} \mathrm{F}$, а.-с. |
| $\begin{aligned} & \mathrm{C}-.10, \mathrm{Cr}-12.75, \mathrm{Mo}-.35, \mathrm{Mn}-.40, \\ & \mathrm{Si}-.40, \mathrm{~S}-.30, \mathrm{Ni}-.25 \end{aligned}$ | annealed |
|  | heat-treated |
| Chromium-titanium steels |  |
| C-.11, Cr-5.41, Ti-. 75 | bar, 1 in . diam., rolled 4 hr at $1380^{\circ} \mathrm{F}$, a.-c. |
| Chromium-tungsten steels |  |
| $\underset{\mathrm{Mn}-.49}{\mathrm{C}-46, \mathrm{Cr}-11.94, \text { W-4.80, Si-2.89, }}$ | oil-quenched from $1875^{\circ} \mathrm{F}$, tempered at $1470^{\circ} \mathrm{F}$ |
| Chromium-vanadium steels |  |
| C-. 58, Cr-.73, V-.18, Mn-. 68 | annealed at $1500^{\circ} \mathrm{F}$ |
| " | water-quenched from $1650^{\circ} \mathrm{F}$, tempered at $1050^{\circ} \mathrm{F}$ |
| $\mathrm{C}-.52, \mathrm{Cr}-.88, \mathrm{~V}-.21, \mathrm{Mn}-.66$ | $z^{3} \mathrm{hr}$ at $1600^{\circ} \mathrm{F}$, quenched in oil at $130^{\circ} \mathrm{F}$, tempered 1 hr at $810^{\circ} \mathrm{F}$ |

TABLE 192. -MECHANICAL PROPERTIES OF IRON AND STEEL (continued)

 $\stackrel{n}{\text { N }} \underset{\sim}{\text { N }}$ N 111



TC-3.41, GC-2.85, CC -.56, Si-2.44,

| Modulus of |
| :---: |
| elasticity |
| $\mathrm{kg} / \mathrm{mm}^{2}$ |

- 
- 

| 5,620 |
| :---: |
| (at $\frac{1}{2}$ load) |
| 11,400 |
| (at $\frac{1}{2}$ load) |

- 

17,550
20,000
-
-
-
-
-
-
(continued)

$$
\begin{array}{r}
\text { Condition } \\
\text { sheet, } .062 \text { in., rolled }
\end{array}
$$ P-.63, Mn-.57, S-. 070 , Ti-. 10 Alloy cast iron: TC-2.61, GC-1.73, Alloy cast iron: TC-2, Ni-18, Si-5, Cr-2, Mn-1, P-.01, S-.1 Malleable cast iron: TC-1.75-2.30,

$\begin{gathered}\mathrm{Si}-.85-1.20, \\ \mathrm{~S}-<12\end{gathered} \mathrm{Mn}-<.40, \quad \mathrm{P}-<.20$, $\xrightarrow{\text { Sure }-<.12}$
Pure iron: $\mathrm{Fe}-99.99$
Wrought iron: C-.017, Si-.122,
Wrought iron: C-.017, Si-. 122, P-. 084
Manganese steels C-.35, Mn-1.71, Si-. 30 Molybdenum steels $\mathrm{C}-.23, \mathrm{Mo}-.17, \mathrm{Mn}-.67, \mathrm{Si}-.52$, $\mathrm{C}-.24, \mathrm{Mo}-.22, \mathrm{Mn}-.85, \mathrm{Si}-.19$
$\mathrm{C}-.39, \mathrm{Cr}-.86, \mathrm{Mo}-.17, \mathrm{Mn}-.56$
annealed
cast
cast
cast
cast,

$$
\begin{aligned}
& \text { rod, } \frac{1}{3} \text { in., swaged ann. } 4 \mathrm{hr} \\
& \text { at } 1600^{\circ} \mathrm{F} \\
& \text { longitudinal }
\end{aligned}
$$

$$
\begin{aligned}
& \text { cast, annealed } \\
& \text { rod, } \frac{1}{4} \text { in., swaged ann. } 4 \mathrm{hr} \\
& \text { at } 1600^{\circ} \mathrm{F}
\end{aligned}
$$

transverse

$$
\text { annealed at } 1650^{\circ} \mathrm{F}
$$

$$
\text { plate, } \frac{5}{8} \text { in., rolled }
$$






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$$



$$
\begin{gathered}
\begin{array}{c}
\text { Modulus of } \\
\text { elasticity } \\
\mathrm{kg} / \mathrm{mm}^{2}
\end{array}
\end{gathered}
$$

$$
\begin{aligned}
& 21,000 \\
& 19,800
\end{aligned}
$$

$$
\begin{array}{r}
- \\
- \\
- \\
20,000
\end{array}
$$

| 8 |
| :--- |
| 8 |


| 8 | 8 |
| :--- | :--- |
| N |  |
| § |  |
| N |  |

bar, $1 \frac{1}{8}$ in. diam., h.-t.
hot-rolled
bar, $\frac{3}{4}$ in. diam., wrought; 1 hr at $1550^{\circ} \mathrm{F}, \circ$ o.-q. tem-
pered at $1000^{\circ} \mathrm{F}$ grain pered
size $7-8$ (ASTM std.),
, norHos8
H.006
H.000I
H.00ZI
$\mathrm{C}-.32, \mathrm{Ni}-1.92, \mathrm{Cr}-.86, \mathrm{Mo}-.30$, wrought, f.-c., from $1450^{\circ} \mathrm{F}$
$\mathrm{Mn}-.60, \mathrm{Si}-.16$

Nickel-chromium steels
C-.37, Ni-1.28, Cr-.52, Mn-. 55
$\underset{\mathrm{Si}-.18}{\mathrm{C}-.37, \mathrm{Ni}-1.33, \mathrm{Cr}-.65, \mathrm{Mn}-.75 \text {, }}$ C-.36, $\mathrm{Ni}-1.33, \mathrm{Mn}-.60, \mathrm{Cr}-.56$, $-.36, \mathrm{Ni}-1.33$, (basic open-hearth, deoxidized with Si and Al )

Nickel-chromium-molybdenum steel
TABLE 192. -MECHANICAL PROPERTIES OF IRON AND STEEL (continued)

Condition
Composition
Nickel-molybdenum steels C-.41, Ni-1.96, Mo-. 31
Nickel-copper steels
$\mathrm{C}-.08, \quad \mathrm{Ni}-2.00, \quad \mathrm{Cu}-1.00$,
$\mathrm{Si}-<.3$
Silicon steels
C-.07, Si-1.17, Mn-. 32
Silicon-manganese steels
C-.52, Si-1.95, Mn-1.05, Cr-. 05
C-.53, Si-1.96, Mn-. 83
Si-. 85 ,
Stainless steel
C-17, Cr-18, Ni-8 C-.07, Cr-18.95, Ni-7.69 C-13, $\mathrm{Cr}-24.5, \quad \mathrm{Ni}-20.3$,
C-.11, $\mathrm{Cr}-16.2, \mathrm{Ni}-11.5$

$$
\begin{aligned}
& \text { oil-quenched from } 1525^{\circ} \mathrm{F} \text {, } \\
& \text { tempered at } 1200^{\circ} \mathrm{F} \\
& \text { quenched from } 1525^{\circ} \mathrm{F} \text { into } \\
& \text { lead at } 840^{\circ} \mathrm{F} \text { (austem- } \\
& \text { pered) }
\end{aligned}
$$

$$
\text { plate, } \frac{1}{2}-\frac{3}{4} \text { in., rolled }
$$

rolled

$$
\begin{aligned}
& \text { oil-quenched from } 1600^{\circ} \mathrm{F} \text {, } \\
& \text { tempered at } 970^{\circ} \mathrm{F}
\end{aligned}
$$

$$
\frac{2}{3} \mathrm{hr} \text { at } 1600^{\circ} \mathrm{F} \text {, quenched in }
$$

$$
\begin{aligned}
& \text { water-quenched from } 1100^{\circ} \mathrm{F} \\
& \text { bar, } \frac{3}{8} \mathrm{in} \text {. diam., cold-rolled } \\
& \text { bar, } 1 \mathrm{in} \text {. diam., rolled } \\
& \text { water-quenched from } 2010^{\circ} \mathrm{F} \text {; } \\
& \text { room: }
\end{aligned}
$$

| Composition percent | Condition | Modulus of elasticity $\mathrm{kg} / \mathrm{mm}^{2}$ | Proportional $\mathrm{kg} / \mathrm{mm}^{2}$ $\qquad$ | Yield strength $\mathrm{kg} / \mathrm{mm}^{2}$ | Tensile strength $\mathrm{kg} / \mathrm{mm}^{2}$ | Elongation percent | $\begin{gathered} \text { Endurance } \\ \text { limit } \\ \mathrm{kg} / \mathrm{mm}^{2} \end{gathered}$ | Hardness number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C-.08, Cr-18.58, Ni-9.68, Ti-. 42 | air-cooled from $1920^{\circ} \mathrm{F}$ | - | - | 26.8 | 60.8 | $59(2 \mathrm{in}$. | - | - |
| C-.07, $\mathrm{Cr}-18.2$, Ni-9.42, Nb-.51 | water-quenched from $2100^{\circ} \mathrm{F}$ | - | - | 25.3 | 62.9 | 60 (2 in.) | - | 137 |
| $\begin{gathered} \mathrm{C}-.40, \mathrm{Cr}-15.21, \mathrm{Si}-.59, \mathrm{Mn}-.28, \\ \mathrm{Ni}-.18 \end{gathered}$ | bar, 1 in. diam., 1 hr at $1650^{\circ} \mathrm{F}$, w.-q., tempered 1 hr at $1200^{\circ} \mathrm{F}$ | - | 36.4 | - | 81.5 | 20 (2 in.) | $\begin{aligned} & 42.0 \\ & 21.1^{*} \end{aligned}$ | - |
| $\mathrm{C}-.20, \mathrm{Cr}-16.17, \mathrm{Mn}-1.06, \mathrm{Si}-.30$ | oil-quenched from $1740^{\circ} \mathrm{F}$, tempered 3 hr at $840^{\circ} \mathrm{F}$ | 23,100 | 35.7 | 62.5 | 133 | 10(2 in.) | - | 357 |
| C-.15, Cr-13.50, Si-. 11 | oil-quenched from $1740^{\circ} \mathrm{F}$, tempered at $1110^{\circ} \mathrm{F}$ | 22,000 | 57.8 | 77.3 | 92.8 | 21 (2 in.) | - | 285 |
| " | $\begin{aligned} & \text { oil-quenched from } 1740^{\circ} \mathrm{F} \text {, } \\ & \text { tempered at } 1290^{\circ} \mathrm{F} \end{aligned}$ | 22,200 | 42.3 | 50.7 | 68.5 | 28(2 in.) | - | 206 |
| C-. $09, \mathrm{Cr}-16.53$ | sheet, . 18 in ., hot-rolled | - | - | 73.0 | 93.5 | 4.5(8 in.) | - | $\mathrm{R}_{\text {L }} 103$ |
| " " | sheet, . 18 in ., ann. | - | - | 34.5 | 49.2 | 20 (8in.) | - | $\mathrm{R}_{\mathrm{B}} 82$ |
| $\underset{\mathrm{Ni}-.19}{\mathrm{C}-20,} \mathrm{Cr}-27.37, \quad \mathrm{Mn}-.32, \mathrm{Si}-.28,$ | annealed | - | 18.5 | 31.3 | 56.9 | 28(2 in.) | 30.9 | - |
| C-.08, Cr-5.81, Mo-. 45 | bar, $\frac{3}{4} \mathrm{in}$. diam., 4 hr at $1380^{\circ} \mathrm{F}$, a.-c. | - | - | $\begin{gathered} 39.4 \\ \text { (yld. pt.) } \end{gathered}$ | 60.4 | 29(2 in.) | - | 149 |
| Tungsten steels $\mathrm{C}-.71, \mathrm{~W}-17.30, \mathrm{Cr}-3.86, \mathrm{~V}-.75$ | normalized at $1740^{\circ} \mathrm{F}$; tempered at $1470^{\circ} \mathrm{F}$ | - | - | $\begin{gathered} 62 \\ \text { (yld. pt.) } \end{gathered}$ | 92 | 19(2 in.) | - | - |

S. A. E. carbon steel, No. 1050 or higher number specified (see carbon steels above). Steel used to be manufactured by acid open-hearth process, to be rolled, drawn, and then uniformly coated with pure tin to solder readily.

| Ameri can or <br> S. wire <br> gage | $\underbrace{\text { Diameter }}$ |  | $\begin{gathered} \text { Req'd } \\ \text { Rwists } \\ \text { in } 203.2 \\ \text { mmor or } \\ 8 \text { in. } \end{gathered}$ | Weight |  | $\begin{gathered} \text { Req'd } \\ \text { bends } \\ \text { thru } 90^{\circ} \end{gathered}$ | Spec. minimum tensile strength |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm | in. |  | $\overparen{\mathrm{kg} / 100}$ | $1 \mathrm{bb} / 100$ |  | kg |  | ${\mathrm{kg} / \mathrm{mm}^{2}}$ | $\mathrm{lb} / \mathrm{in}.{ }^{2}$ |
| 6 | 4.115 | . 162 | 16 | 10.44 | 7.01 | 5 | 2040 | 4500 | 154 | 219,000 |
| 7 | 3.665 | . 144 | 19 | 8.28 | 5.56 | 6 | 1680 | 3700 | 161 | 229,000 |
| 8 | 3.264 | . 129 | 21 | 6.55 | 4.40 | 8 | 1360 | 3000 | 164 | 233,000 |
| 9 | 2.906 | . 114 | 23 | 5.21 | 3.50 | 9 | 1135 | 2500 | 172 | 244,000 |
| 10 | 2.588 | . 102 | 26 | 4.12 | 2.77 | 11 | 910 | 2000 | 172 | 244,000 |
| 11 | 2.305 | . 091 | 30 | 3.28 | 2.20 | 14 | 735 | 1620 | 179 | 254,000 |
| 12 | 2.053 | . 081 | 33 | 2.60 | 1.74 | 17 | 590 | 1300 | 177 | 252,000 |
| 13 | 1.878 | . 072 | 37 | 2.06 | 1.38 | 21 | 470 | 1040 | 179 | 255,000 |
| 14 | 1.628 | . 064 | 42 | 1.64 | 1.10 | 25 | 375 | 830 | 181 | 258,000 |
| 15 | 1.450 | . 057 | 47 | 1.30 | . 87 | 29 | 300 | 660 | 182 | 259,000 |
| 16 | 1.291 | . 051 | 53 | 1.03 | . 69 | 34 | 245 | 540 | 186 | 264,000 |
| 17 | 1.150 | . 045 | 60 | . 81 | . 55 | 42 | 195 | 425 | 188 | 267,000 |
| 18 | 1.024 | . 040 | 67 | . 65 | . 43 | 52 | 155 | 340 | 190 | 270,000 |
| 19 | . 912 | . 036 | 75 | . 51 | . 34 | 70 | 125 | 280 | 193 | 275,000 |
| 20 | . 812 | . 032 | 85 | . 41 | . 27 | 85 | 100 | 225 | 197 | 280,000 |
| 21 | . 723 | . 028 | 96 | . 32 | . 22 | 105 | 80 | 175 | 200 | 284,000 |

Note.-Number of $90^{\circ}$ bends specified above to be obtained by bending sample about 4.76 mm (. 188 in .) radius, alternately, in opposite directions.

## TABLE 194.-STEEL WIRE-EXPERIMENTAL VALUES

Data from tests at General Electric Co. laboratories. Commercial steel music wire (hardened).

| Diameter |  | Ultimate strength tension <br> $\mathrm{kg} / \mathrm{mm}^{2} \mathrm{lb} / \mathrm{in} .^{2}$ |  | $\mathrm{Diameter}^{\text {d }}$ |  | Ultimate strength tension $\mathrm{kg} / \mathrm{mm}^{2} \mathrm{H} / \mathrm{in} .^{2}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm | in. |  |  | mm | in. |  |  |
| 12.95 | . 051 | 226.0 | 321,500 | 6.35 | . 025 | 262.0 | 372,500 |
| 11.70 | . 046 | 249.0 | 354,000 | 4.55 | . 018 | 265.5 | 378,000 |
| 9.15 | . 036 | 253.0 | 360,000 | 2.55* | . 010 | 386.5 | 550,000 |
| 7.60 | . 030 | 260.0 | 370,000 | 1.65* | . 0065 | 527.0 | 750,000 |
|  |  |  |  | $4.55{ }^{\dagger}$ | . 018 | 49.2 | 70,000 |

[^92]
## TABLE 195.-PLOW-STEEL HOISTING ROPE (BRIGHT)

Wire rope to be of best plow-steel grade, and to be composed of 6 strands, 19 wires to the strand, with hemp center. Wires entering into construction of rope to have an elongation in 203.2 mm or 8 in . of about $2 \frac{1}{2}$ percent.

| Diameter |  | Spec. minimum strength |  | Diameter |  | Spec. minimum strength |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm | in. | kg | 1 b | mm | in. | kg | lb |
| 9.5 | ${ }^{\frac{3}{8}}$ | 5,215 | 11,500 | 38.1 | $1 \frac{1}{2}$ | 74,390 | 164,000 |
| 12.7 | $\frac{1}{2}$ | 9,070 | 20,000 | 50.8 | 2 | 127,000 | 280,000 |
| 19.0 | $\frac{3}{4}$ | 20,860 | 46,000 | 63.5 | $2 \frac{1}{2}$ | 207.740 | 458,000 |
| 25.4 | 1 | 34,470 | 76,000 | 69.9 | $2 \frac{3}{4}$ | 249,350 | 550,000 |

Cast steel wire to be of hard crucible steel with minimum tensile strength of 155 $\mathrm{kg} / \mathrm{mm}^{2}$ or $220,000 \mathrm{lb} / \mathrm{in}^{2}$ and minimum elongation of 2 percent in 254 mm ( 10 in .).

Plow steel wire to be of hard crucible steel with minimum tensile strength of 183 $\mathrm{kg} / \mathrm{mm}^{2}$ or $260,000 \mathrm{lb} / \mathrm{in} .^{2}$ and minimum elongation of 2 percent in 254 mm ( 10 in .).

Annealed steel wire to be of crucible cast steel, annealed, with minimum tensile strength of $77 \mathrm{~kg} / \mathrm{mm}^{2}$ or $110,000 \mathrm{lb} / \mathrm{in.}^{2}$ and minimum elongation of 7 percent in 254 mm ( 10 in .).

Type A: 6 strands with hemp core and 19 wires to a strand ( $=6 \times 19$ ), or 6 strands with hemp core and 18 wires to a strand with jute, cotton, or hemp center.
Type B: 6 strands with hemp core, and 12 wires to a strand with hemp center.
Type C: 6 strands with hemp core, and 14 wires to a strand with hemp or jute center.
Type AA: 6 strands with hemp core, and 37 wires to a strand ( $=6 \times 37$ ) or 6 strands with hemp core and 36 wires to a strand with jute, cotton, or hemp center.


## TABLE 197.-STEEL-WIRE ROPE-EXPERIMENTAL VALUES

Wire rope purchased under Panama Canal Spec. 302 and tested by National Bureau of Standards, Washington, D. C.

| Description and analysis | $\underbrace{\text { Diameter }}$ |  | Ultimate strength |  | Ultimate strength(net area) net area) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | mm | in. | kg | 1b | kg/mm ${ }^{2}$ | 1b/in. ${ }^{2}$ |
| Plow steel, 6 strands $\times 19$ wires <br> C $90, \mathrm{~S} 034, \mathrm{P} 024 \mathrm{Mn}$ |  |  |  |  |  |  |
| $\mathrm{C} .90, \mathrm{~S} .034, \mathrm{P} .024, \mathrm{Mn}$ $48, \mathrm{Si} .172$ | 50.8 | 2 | 137,900 | 304,000 | 129.5 | 184,200 |
| Plow steel, 6 strands $\times 25$ wires |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| 46, Si $152 \ldots \ldots \ldots . .$. | 69.9 | $2 \frac{3}{4}$ | 314,800 | 694,000 | 151.2 | 214,900 |
|  |  |  |  |  |  |  |
| $\begin{aligned} & \text { C } .58, \text { S } .032, \text { P } .033, \text { Mn } \\ & .41, S i \\ & \text { Si } 160 \ldots \ldots \ldots \ldots . . \end{aligned}$ | 82.6 | $3{ }^{\frac{1}{4}}$ | 392,800 | 866,000 | 132.2 | 187,900 |
| Monitor plow steel, $6 \times 61$ plus |  |  |  |  |  |  |
| $\begin{aligned} & 6 \times 19, \mathrm{C} .82, \mathrm{~S} .025, \mathrm{P} .019, \\ & \mathrm{Mn} .23, \mathrm{Si} .169 \ldots \ldots \ldots . . . \end{aligned}$ | 82.6 | $3{ }_{4}^{1}$ | 425,000 | 937,000 | 142.5 | 202,400 |

[^93]TABLE 198.-MECHANICAL PROPERTIES OF MISCELLANEOUS ALLOYS**

| Composition percent | Condition | Density $\mathrm{g} / \mathrm{cm}^{3}$ | Modulus of elasticity $\mathrm{kg} / \mathrm{mm}^{2}$ | Proportional $\mathrm{kg} / \mathrm{mm}^{2}$ | Yield strength $\mathrm{kg} / \mathrm{mm}^{2}$ | Tensile strength $\mathrm{kg} / \mathrm{mm}^{2}$ | Elongation percent | Endurance limit $\mathrm{kg} / \mathrm{mm}^{2}$ | Hardness number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cadmium alloys $\mathrm{Cu}-1.5 ; \mathrm{Mg}-.95^{\circ}$ | Cast | $\ldots$ | 5,600 |  | $\begin{gathered} 5.48 \\ (.02 \% \text { offset }) \\ 9.84 \\ (.2 \% \text { off set }) \end{gathered}$ | 15.77 | 8.8(10 diam.) | 3.8 | 42 |
| Zn-5.0 | Rod, 1 in. diam., chill-cast from $660^{\circ} \mathrm{F}$; aged one month at r.-t. | 8.55 | $\ldots$ | $\ldots$ | $6 \%$ | 9.2 (rate of strain $\% /$ minute) | 6.5 (1.25 in.) | $\cdots$ | 32 |
| Cobalt alloys $\mathrm{Fe}-1.4 ; \mathrm{Ni}-1.1 ; \mathrm{C}-.24$ | Cast, ann. 2 hr at $1,650^{\circ} \mathrm{F}$ | $\ldots$ | 20,800 | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| $\begin{aligned} & \text { Co-45-55; Cr-30-35; } \\ & \text { W-12-17 } \end{aligned}$ | Cast | 8.76 | 24,900 | $\ldots$ | $\ldots$ | 45.7 | 0 (2 in.) | $\ldots$ | Rc 61 |
| Gold alloys $\mathrm{Cd}-4.6 ; \mathrm{Cu}-2.8 ; \mathrm{Zn}-1.0$ |  | $\ldots$ | $\ldots$ | 9.28 | $\ldots$ | 30.8 | 55 (2 in.) | $\ldots$ | 44 |
| $\mathrm{Cu}-6.3$; $\mathrm{Ag}-2.1$ | Strip, $\frac{3}{8}$ in., ann. $\frac{1}{3} \mathrm{hr}$ at $1365^{\circ} \mathrm{F}$ | $\ldots$ | $\ldots$ | 13.2 | $\ldots$ | 32.1 | 35 | $\ldots$ | $\ldots$ |
| $\begin{gathered} \mathrm{Cu}-15.6 ; \mathrm{Ag}-6.0 ; \mathrm{Pt}-2.78 ; \\ \mathrm{Z11-2.38} ; \mathrm{Ni}-1.98 \end{gathered}$ | Rod, $\frac{1}{8}$ in. diam., cast, w.-q. from $1290^{\circ} \mathrm{F}$ | $\ldots$ | 9,140 | 37.6 | $\cdots$ | 48.5 | 4 (3in.) | $\ldots$ | $\cdots$. |
| $\begin{gathered} \mathrm{Cu}-17.95 ; \mathrm{Ni}-17.60 \\ \mathrm{Zn}-6.0 ; \mathrm{Mn}-.4 \end{gathered}$ | Sheet, .050 in ., rolled ( $50 \%$ red) $\frac{1}{2} \mathrm{hr}$ at $1290^{\circ} \mathrm{F}$, a.-c. | $\ldots$ | $\ldots$ | $\ldots$ | $\begin{gathered} 45.0 \\ \text { (yld. pt.) } \end{gathered}$ | 72.4 | 44(2 in.) | $\ldots$ | $\cdots$ |
| $\begin{aligned} & \mathrm{Cu}-34.9 ; \mathrm{Ni}-12.14 ; \\ & \mathrm{Ag}-11.11 \end{aligned}$ | Sheet, .045 in., rolled ( $50 \%$ red), ann. $\frac{1}{3} \mathrm{hr}$ at $1300^{\circ} \mathrm{F}$, a.-c. | $\ldots$ | $\ldots$ | $\ldots$ | $\begin{gathered} 49.3 \\ \text { (y\|d. pt.) } \end{gathered}$ | 63.5 | 19(1.25 in.) | $\ldots$ | $\mathrm{R}_{\mathrm{B}} 94$ |
| $\underset{\mathrm{Zn}-8.65}{\mathrm{Ni}-17.0 ; \mathrm{Cu}-16.0 ;}$ | Sheet. 05 in., rolled ( $50 \%$ red), $\frac{1}{2} \mathrm{hr}$ at $1380^{\circ} \mathrm{F}$, a.-c. | $\ldots$ | $\ldots$ | $\ldots$ | $\begin{gathered} 45.3 \\ \text { (yld. pt.) } \end{gathered}$ | 73.8 | 43 (2 in.) | $\ldots$ | $\ldots$ |


TABLE 198．－MECHANICAL PROPERTIES OF MISCELLANEOUS ALLOYS（continued）
$\substack{\text { Endurance } \\ \text { limit } \\ \mathrm{kg} / \mathrm{mm}^{2}}$
．722（107）

$16(8 \mathrm{in}$.
$2(2 \mathrm{in}$.
$2.5(4 \sqrt{\text { area }})$
6.5
Elongation
percent
$4.6(8 \mathrm{in}$.

（u！8）tて
18（3in．）
$\overparen{E}$
in
N
N
 4．0（2 in．）
47
 －틀

.6
3.7

3．09（rate

of strain）  | N |
| :---: |
| $\infty$ |

8.4
1.34

$\underset{\substack{\text { Yield } \\ \text { strength } \\ \mathrm{kg} / \mathrm{mm}^{2}}}{\substack{ \\\hline}}$

Modulus of $\begin{gathered}\text { Propor－} \\ \text { tional } \\ \text { limit }\end{gathered}$
Modulus of
elasticity
elasticity
$\mathrm{kg} / \mathrm{mm}^{2}$ 14，050

7，000
$\stackrel{N}{0}$
15.8


育荡菏
Condition
Strip， .006 in．，w．－q．from
$1290^{\circ} \mathrm{F}$
Strip， .006 in．，w．－q．from
$1290^{\circ} \mathrm{F}$
Rod，$\frac{1}{8}$ in．diam．，cast，w．－q．
from $1290^{\circ} \mathrm{F}$
Cable sheath， 1 in．o．－d．
 Cast


Cast
Cable sheath， 2.87 in．o．－d．
$\times .159$ in．wall（ring $\underset{\substack{\times .159 \mathrm{in} . \\ \text { specimen）}}}{\text { wall（ring }}$ Rod，extruded from $2 \frac{15}{18} \mathrm{in}$.
to $\frac{3}{4}$ in．diam．at $350-$
$400^{\circ} \mathrm{F}$

Cast，h．－t．and aged


Magnesium alloys
Al－4．40；Mn－． 26
Al－10； $\mathrm{Mn}>.1 ; \mathrm{Si}<.5$ ；
$\mathrm{Cu}-13$
Manganese alloys
$\mathrm{Cu}-18 ; \mathrm{Ni}-10$

#  <br> $\mathrm{Bi}-.065$ ；Cu－ .013 ；Sb－． 0015 <br> Monotype： Sb－15．3；Sn－8．3 

| 8 |
| :--- |
| $\underset{7}{2}$ |
| $\underset{\sim}{2}$ |

12，240

（continued）
－$\quad$.
Hardness
山
岂
है
$\vdots \quad \vdots \quad \underset{\sim}{\circ}$ ²
苍


$$
\begin{aligned}
& 49.0 \\
& 88.0
\end{aligned}
$$

Elongation

$$
\begin{gathered}
\cdots \\
30(10 \mathrm{in} .)
\end{gathered}
$$

$$
30(2 \mathrm{in} .)
$$

$$
30(4 \mathrm{in} .)
$$

$$
6-9(2 \mathrm{in} .)
$$

$$
40(2 \text { in. })
$$ $\mathrm{kg} / \mathrm{mm}^{2}$


$\vdots \quad \vdots \quad \vdots \quad$ ヘั N゙ バ
TABLE 198．－MECHANICAL PROPERTIES OF MISCELLANEOUS ALLOYS（concluded）

$$
\begin{array}{ll}
\text { H. } \\
\text { N }
\end{array}
$$

$$
\begin{aligned}
& \infty \\
& 1 \\
& 1 \\
& 1
\end{aligned}
$$

ヘ̀

$$
\underset{\infty}{+}
$$

$$
\stackrel{n}{n}
$$

Condition
Rod，$\frac{7}{8}$ in．diam．，hot－rolled，
ann． 2 hr at $1650^{\circ} \mathrm{F}$ ，
slowly cooled

Sand－cast
Quenched Cast
Sand－cast
Cast
Cast （ねวsџ๐ \％で）

$$
\therefore \underset{\infty}{\infty} \quad \underset{\infty}{\infty}
$$

Sheet ann．
Wrought

Nickel $\begin{gathered}\text { percent } \\ \text { alloys }\end{gathered}$
$\mathrm{Al}-4.78 ; \mathrm{Mn}-.26 ; \mathrm{C}-.17$ ；
$\mathrm{Ni}-80 ; \mathrm{Cr}-13 ; \mathrm{Fe}-\mathrm{rem}$.
$\mathrm{Cr}-20$
$\mathrm{Cu}-29 ; \mathrm{Fe}-1.5 ; \mathrm{Si}-1.25 ;$
$\mathrm{Mn} .9 ; \mathrm{C}-.2 ; \mathrm{S}<.015$ $\mathrm{Ni}-60 ; \mathrm{Cr}-15 ; \mathrm{Mo}-7$
$\mathrm{Be}-.6-1.0 ; \mathrm{Fe}-\mathrm{rem}$. $\mathrm{Be}-.6-1.0 ; \mathrm{Fe}-\mathrm{rem}$.
$\mathrm{Mo}-30 ; \mathrm{Fe}-5$
Silver alloys Cu－5．75；Cd－1．75 Tin alloys
Sb－6．87； $\mathrm{Cu}-5.69 ; \mathrm{Pb}-.19$ ；
Fe－．03；As－． 02 ，
$\mathrm{Sb}-10.01 ; \mathrm{Cu}-9.88 ; \mathrm{Pb}-.19 ;$
$\mathrm{Fe}-.08$

$$
\begin{aligned}
& \text { Density } \\
& \mathrm{g} / \mathrm{cm}^{3}
\end{aligned}
$$

$$
\ldots
$$

$$
\begin{aligned}
& 8.3 \\
& 9.24
\end{aligned}
$$

$$
\begin{array}{ccc}
\begin{array}{c}
\text { Modulus of } \\
\text { elasticity } \\
\mathrm{kg} / \mathrm{mm}^{2}
\end{array} & \begin{array}{c}
\text { Propor. } \\
\text { tional } \\
\text { limit } \\
\mathrm{kg} / \mathrm{mm}^{2}
\end{array} & \begin{array}{c}
\text { Yield } \\
\text { strength } \\
\mathrm{kg} / \mathrm{mm}^{2}
\end{array} \\
21,500 & 9.4 & \begin{array}{c}
18.75 \\
(.01 \% \text { offset) }
\end{array} \\
21,800 & \ldots & \ldots \\
21,800 & \ldots & \begin{array}{c}
44.5 \\
\text { (yld. pt.) }
\end{array} \\
18,300 & \ldots & \begin{array}{c}
24.5 \\
(.2 \% \text { offset) }
\end{array} \\
15,500 & \ldots & \begin{array}{c}
41.8 \\
\text { (yld. pt.) } \\
38.5-40.0
\end{array} \\
\text { (yld. pt.) }
\end{array}
$$

$$
43(4 \sqrt{\text { area }})
$$

TABLE 199.-PHYSICAL PROPERTIES OF SOME SPECIAL.PURPOSE ALLOYS*

| Composition percent $\quad$ Density | Resistivity microhms cm | Temperature coeff. of resistance | Thermal conduc- tivity cgs | Thermal expansion per ${ }^{\circ} \mathrm{C}$ | Tensile strength $\mathrm{kg} / \mathrm{mm}^{2}$ | $\begin{aligned} & \text { Yield } \\ & \text { strength } \\ & \mathrm{kg} / \mathrm{mm}^{2} \end{aligned}$ | Young's $\mathrm{kg} / \mathrm{mm}^{2}$ | Hardness number Rockwell | $\begin{gathered} \text { Elongation } \\ \text { 2in. } \\ \text { percent } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alloys for strength with lightness |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \text { Duralumin }(\mathrm{A} 17 \mathrm{~S}) \\ & \mathrm{Al} 97, \mathrm{Cu} 2.5, \mathrm{Mg} .3 .2 .74 \end{aligned}$ | 4.3 |  | . 37 |  | 30 |  | 7200 | 70 |  |
| Super duralumin ( 24 S ) Al 93, Cu 4.5, Mn 6 |  |  |  |  |  |  |  |  |  |
| Mg 1.5 .......... 2.77 | 5.7 |  | . 29 | $\begin{gathered} 20-200^{\circ} \\ 12.9 \times 10^{-6} \end{gathered}$ | 50 |  | 7200 | 120 |  |
| Dow metal <br> Mg 92, Al 8.......... 1.81 | 13 |  |  |  | 23 |  | 4.6 |  |  |
| Beryllium alloys |  |  |  |  |  |  |  |  |  |
| Beryllium ${ }^{\dagger}$........... 1.83 | 4.3 |  | . 385 | $\begin{gathered} 20-200^{\circ} \\ 12.4 \times 10^{-8} \end{gathered}$ | 35 | 18.7 | $2.6 \times 10^{4}$ | 90-110 | .0-2.5 |
| Alloys $\dagger$ ¢ ${ }^{\dagger}$ |  |  |  |  |  |  |  |  |  |
| Be .45, Co 2.6, Bal Ct wrought $\ldots . . . . . . . .8 .75$ | 3.4 |  | . 50 |  | 81. | 63. | $1.26 \times 10^{3}$ | C23-28 | 10-15 |
| $\begin{aligned} & \mathrm{Be} 2.60, \mathrm{Ni} 1.10, \mathrm{Bal} \\ & \mathrm{Cu} \ldots \ldots \ldots \ldots \ldots . . \\ & 7.6 \end{aligned}$ | 7.8 |  | . 18 | $\begin{aligned} & 20-200^{\circ} \\ & 17 \times 10^{-8} \end{aligned}$ | 112. | 63. |  | C38 |  |
| $\begin{gathered} \mathrm{Be} 2.0, \mathrm{Co} \mathrm{.5,} \mathrm{Bal} \mathrm{Cu} \\ \text { cast } \ldots \ldots \ldots . \ldots . . .8 .1 \end{gathered}$ | 6.5 |  | . 30 |  | 115. | 98. | $1.33 \times 10^{3}$ | C37-42 |  |
| $\begin{gathered} \text { Be 2.0, Co .3, Bal Cu } \\ \text { wrought } \ldots \ldots . .{ }^{2} 8.21 \end{gathered}$ | 12.7 |  | . 16 |  | 49. | 21. | $1.12 \times 10^{3}$ | C85-95 | . $35-.50$ |
| Alloys for sealing to glass |  |  |  |  |  |  |  |  |  |
| $42 \%$ nickel iron ${ }^{8}$ |  |  |  |  |  |  |  |  |  |
|  |  |  | 03 | $5.4 \times 10^{-6}$ |  |  | $14.7 \times 10$ | cgs. |  |

TABLE 199.-PHYSICAL PROPERTIES OF SOME SPECIAL-PURPOSE ALLOYS (continued)
Elongation
2 in.
percent number
Rockwell percent (Specific heat

|  |  |
| :---: | :---: |
|  |  |
| $\stackrel{\text { 5 }}{\text { ¢ }}$ |  |
| ¢ |  |
| 运边 | 8 |
|  | $\cdots$ | $160 \begin{gathered}\text { (Specific heat } \\ \text { cgs } .12 \text { ) }\end{gathered}$ § There are several alloys of about this same composition that are made by different manufacturers. They all have al,out the same characteristics.

Uses:
a Heater and resistance.
b Standard resistances.
e I.ow thermal expansion.
d Thermocouples.
e Mirrors; is an exceedingly hard untarnishable metal.
i Mirrors and retecting gratings; takes good polish and does not tarnish easily.
\& An alloy sometimes used as a getter for clearing off last traces of gas in an evacuated vessel.
b Used for making special casting and in art work.
(continued)

$\underset{\substack{\text { expermal } \\ \text { expersion }}}{\text { io }}$
$20-600^{\circ}$
$11.4 \times 10^{-8}$
$100-500^{\circ}$
$4.2-5.4 \times 10^{-8}$
$20-100^{\circ}$
$10.3 \times 10^{-6}$
Radial $8.0-$
$10 \times 10^{-8}$
Axial $6.1-$
$6.5 \times 10^{-0}$
8
8
Density
$\begin{gathered}\text { percent } \\ \text { Chrom iron } \\ \mathrm{Fe} 70-72,\end{gathered}$
Cr

$\mathrm{Mn} .5-.8 \ldots \ldots \ldots . .7 .8$
8
$\stackrel{T}{~}$

$$
\underset{\substack{\text { Composition } \\ \text { percent }}}{ }
$$

Tensile
strengtlı
$\mathrm{kg} / \mathrm{mm}^{2}$
Fernico
$\mathrm{Fe} 54, \mathrm{Ni} 28$, Co $18 .$.
$\begin{array}{cc}44 & <10^{-6} \text { at } 25^{\circ} \mathrm{C} \\ 100 & 4 \times 10^{-4} \\ 81 & 1.08 \times 10^{-3}\end{array}$
$\begin{aligned} & 8 \times 10^{-9} \\ < & 10^{-8} \text { at } 25^{\circ} \mathrm{C}\end{aligned}$
total weight ...........
Miscellaneous
Constantin \& :
Cu 53.3, Ni 45, Mn 1, 8.4
Dumet
$\mathrm{Ni} 42, \mathrm{Fe} 58, \mathrm{Cu} 20-30$
total weight $\ldots \ldots$.
Fe. 6 .............. 8.4
Manganin $8^{\mathrm{b}}$
$\mathrm{Cu} 84, \mathrm{Mn}$
$\mathrm{Cu} 84, \mathrm{Mn} 12, \mathrm{Ni} 4 \ldots 8.5$
Nichrome §
$59.9 \mathrm{Ni}, 25$

Invar
Fe
c
$63.8, \mathrm{Ni}$
36, C .2..
8.05
TABLE 199.-PHYSICAL PROPERTIES OF SOME SPECIAL-PURPOSE ALLOYS (continued)
Temperature
coeff. of
resistance
3.2
$20-100$
24.5

| Linear expansio per ${ }^{\circ} \mathrm{C}$ | Specific heat cos cgs | Resistivity microhmcm | $\begin{gathered} \text { Thermal } \\ \text { conductivity } \\ \text { cgs } \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & 13.1 \times 10^{-0} \\ & 20-100^{\circ} \mathrm{C} \end{aligned}$ | . 107 | 4.25 | 1.92 watts |
| $\begin{aligned} & 12 \times 10^{-6} \\ & 20-100^{\circ} \mathrm{C} \end{aligned}$ | . 125 | 25. | . 297 watts |
| Brinell hardness-512 at 3000 kg |  |  |  |
| Spectral reflecting factor: <br> $\lambda .15, .20, .30, .50, .75,1.00,2.00,3.00,4.00,5.00,8.00$ <br> $.32, .42, .50, .64, .67, .689, .747, .792, .825, .848, .880$ |  |  |  |
| Spectral reflecting factor: <br> $\lambda .188, .200, .251, .288, .305, .357, .385, .420, .450, .500$ $.23, .25, .299, .377, .417, .51, .531, .564, .600, .632$ |  |  |  |
| $\text { 入 . } .550, .600, .650, .700,1.00,1.50,2.00,3.00,4.00,5.00$ |  |  |  |
| $\begin{gathered} \lambda .7 .00,9.00,11.00,14.00 \\ .901, .922, .929,936 \end{gathered}$ |  |  |  |



Speculum metal ${ }^{\text {t }}$. $67, \mathrm{Sn} 33$
Misch metal $8^{8}$
Ce $50-70$, Fe 1-5, La, Nd Pr
Pewter
$85 \mathrm{Sn}, 6.8 \mathrm{Cu}, 6 \mathrm{Bi}, 1.7 \mathrm{Sb}$
$\ddagger$ Hoskins Thermocouple (see Table 51).


TABLE 199.-PHYSICAL PROPERTIES OF SOME SPECIAL-PURPOSE ALLOYS (concluded)


| Carboloy cemented carbides |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Grade desig- <br> nation | Composition |  |  |  | Hardness Rockwell A 60 kg load |  |  | Traverse rupture psi | Young's psi |  | Ultimatelimit incompression |
|  | WC | Co | TaC | TiC |  |  |  |  |  |  |  |
| 44 A | 94 | 6 |  |  |  | 91.0 | 14.95 | $240{ }^{1}$ | $84.5{ }^{\text {k }}$ | $2.8{ }^{1}$ | $700{ }^{1}$ |
| 55A | 87 | 13 |  |  |  | 88.2 | 14.2 | 340 | 79.0 | 3.38 | 610 |
| 77 B | 57 | 16 | 27 |  |  | 85.0 | 13.55 | 285 | 88.0 | 4.03 | 610 |
| 78 B | 82 | 10 |  | 8 |  | 90.5 | 12.55 | 225 |  |  |  |
| 831 | 61 | 7 |  | 32 |  | 92.5 | 9.1 | 165 | 88.5 | 3.89 | 725 |
| Heat-treated steel ${ }^{1}$ |  |  |  |  |  |  |  |  |  |  |  |
| SAE 1095-. 9 C , $.3 \mathrm{Mn}, .04 \mathrm{P}, .05 \mathrm{~S}$ H.S.S. -17 W. 4 Cr. 11 |  |  |  |  |  | 39 Rc | 7.8 | $\ldots$ | 30 | 8.2 | 172 |
|  |  |  |  |  |  | 64 Rc | 8.6 |  | 32.5 | 7.1 | 600 |
| Hardness versus temperature, ${ }^{\circ} \mathrm{F}{ }^{\text {¢ }}$ |  |  |  |  |  |  |  |  |  |  |  |
| Grade |  |  | 200 |  | 400 |  | 600 | 800 |  |  | 1100 |
| 831 |  |  | 93.7 |  | 92.3 |  | 90.6 | 89.5 |  |  | 83.3 |
| 78B |  |  | 90.1 |  | 90.4 |  | 89.0 | 86.0 |  |  | 80.8 |
| 77 B |  |  | 87.0 |  | 85.8 |  | 82.8 | 82.5 |  |  | 77.9 |
| 44A |  |  | 90.5 |  | 90.0 |  | 88.0 | 86.5 |  |  | 84.1 |
| 55A |  |  | 88.0 |  | 87.1 |  | 85.5 | 83.0 |  |  | 77.0 |
| ${ }^{1}$ For comparison. |  | $10^{3}$ | 10. |  | ${ }_{7}$ Prer | pared by N. | Waldrop, C | Co. |  |  |  |



[^94]TABLE 201.-LOW-MELTING ALLOYS *

| Nam | Composition, percent |  |  |  |  | Melting point |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Bi | Cd | Pb | Sn | Other | ${ }^{\circ} \mathrm{F}$ | ${ }^{\circ} \mathrm{C}$ |
| Anatomical alloy | 53.5 |  | 17 | 19 | Hg 10.5 | 140 | 60 |
| Wood's alloy | 50 | 12.5 | 25 | 12.5 | - | 154.4 | 68 |
| Quaternary eutectic alloy. | 49.5 | 10.10 | 27.27 | 13.13 | - | 158 | 70 |
| Fusible alloy . $\quad . . . . . . .$. | 38.4 | 15.4 | 30.8 | 15.4 | - | 159.8 | 71 |
| Eutectic alloy ( $\mathrm{Bi}-\mathrm{Cd}-\mathrm{Pb}$ ) | 51.6 | 8.1 | 40.2 |  | - | 196.7 | 91.5 |
| Alloy for fine castings.. | 50 | - | 32.2 | 17.8 | - | 212 | 100 |
| Rose's alloy ........ | 50 | - | 28 | 22 | - | 212 | 100 |
| Bismuth solder | 40 | - | 40 | 20 | - | 235.4 | 113 |
| Eutectic alloy ( $\mathrm{Bi}-\mathrm{Sn}$ ) | 57 | - | - | 43 | - | 280.4 | 138 |
| Eutectic alloy(Bi-Cd) | 60 | 40 |  | - | - | 291.2 | 144 |
| Eutectic alloy ( $\mathrm{Bi}-\mathrm{Pb}-\mathrm{Sn}$ ) | 13.7 | - | 44.8 | 41.5 |  | 320 | 160 |
| Eutectic alloy ( $\mathrm{Cd}-\mathrm{Sn}$ ) |  | 32 |  | 68 | - | 350.6 | 177 |
| Eutectic alloy ( $\mathrm{Pb}-\mathrm{Sn}$ ) | - | - | 38 | 62 | - | 361.4 | 183 |

[^95]
## IABLE 202.-MECHANICAL PROPERTIES OF WHITE METAL BEARING ALLOYS (BABBITT METAL)

Experimental permanent deformation values from compression tests on cylinders 31.8 mm ( $1 \frac{1}{4} \mathrm{in}$.) diam. by 63.5 mm ( $2 \frac{1}{2} \mathrm{in}$.) long, tested at $21^{\circ} \mathrm{C}\left(70^{\circ} \mathrm{F}\right.$ ). (Set readings after removing loads.)

| $\begin{aligned} & \text { Alloy } \\ & \text { No. } \end{aligned}$ |  | Formula, percent |  |  | Pouring temp. |  | $\underbrace{\text { Weight }}$ |  | Permanent deformation \& $21{ }^{\circ} \mathrm{C}$ |  |  |  |  |  | $\underbrace{\text { Hardness }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | $\begin{aligned} & 54 \mathrm{~kg} \\ & 000 \mathrm{lb} \end{aligned}$ |  |  |  | $\begin{aligned} & 268 \mathrm{~kg} \\ & 000 \mathrm{lb} \end{aligned}$ |  | $\begin{aligned} & 36 \mathrm{~kg} \\ & 000 \mathrm{lb} \end{aligned}$ | $=\stackrel{\cup}{\bar{\sim}}$ | $\begin{aligned} & \text { by } \\ & 80 \\ & 80 \\ & \hline \end{aligned}$ |
|  | Sn | Sl) | Cu | Pb |  |  |  |  | $\mathrm{cm}^{3}$ | $\mathrm{ft}^{3}$ | m | in. | mm | in. | mm |  | L | (e) |
|  |  |  |  |  |  |  |  |  | Base |  |  |  |  |  |  |  |
| 1 | 91.0 | 4.5 | 4.5 | - | 440 | 824 | 7.34 | 458 | . 000 | . 0000 | . 025 | . 0010 | . 380 | . 0150 | 28.6 | 12.8 |
| 2 * | 89.0 | 7.5 | 3.5 | - | 432 | 808 | 7.39 | 461 | . 000 | . 0000 | . 038 | . 0015 | . 305 | . 0120 | 28.3 | 12.7 |
| 3 | 83.3 | 8.3 | 8.3 | - | 491 | 916 | 7.46 | 465 | . 025 | . 0010 | . 114 | . 0045 | . 180 | . 0070 | 34.4 | 15.7 |
| 4 | 75.0 | 12.0 | 3.0 | 10.0 | 360 | 680 | 7.52 | 469 | . 013 | . 0005 | . 064 | . 0025 | . 230 | . 0090 | 29.6 | 12.8 |
| 5 | 65.0 | 15.0 | 2.0 | 18.0 | 350 | 661 | 7.75 | 484 | . 025 | . 0010 | . 076 | . 0030 | . 230 | . 0090 | 29.6 | 11.8 |
|  |  |  |  |  |  |  |  | Lead | Base |  |  |  |  |  |  |  |
| 6 | 20.0 | 15.0 | 1.5 | 63.5 | 337 | 638 | 9.33 | 582 | . 038 | . 0015 | . 127 | . 0050 | . 457 | . 0180 | 24.3 | 11.1 |
| 7 | 10.0 | 15.0 | - | 75.0 | 329 | 625 | 9.73 | 607 | . 025 | . 0010 | . 127 | . 0050 | . 583 | . 0230 | 24.1 | 11.7 |
| 8 | 5.0 | 15.0 | - | 80.0 | 329 | 625 | 10.04 | 627 | . 051 | . 0020 | . 229 | . 0090 | 1.575 | . 0620 | 20.9 | 10.3 |
| 9 | 5.0 | 10.0 | - | 85.0 | 319 | 616 | 10.24 | 640 | . 102 | . 0040 | . 305 | . 0120 | 2.130 | . 0840 | 19.5 | 8.6 |
| 10 | 2.0 | 15.0 | - | 83.0 | 325 | 625 | 10.07 | 629 | . 025 | . 0010 | . 254 | . 0100 | 3.910 | . 1540 | 17.0 | 8.9 |
| 11 | - | 15.0 | - | 85.0 | 325 | 625 | 10.28 | 642 | . 025 | . 0010 | . 254 | . 0100 | 3.020 | . 1190 | 17.0 | 9.9 |
| 12 | - | 10.0 | - | 90.0 | 334 | 634 | 10.67 | 666 | . 064 | . 0025 | . 432 | . 0170 | 7.240 | . 2850 | 14.3 | 6.4 |

[^96]
## TABLE 203.-RIGIDITY MODULUS FOR A NUMBER OF MATERIALS

If to the four consecutive faces of a cube a tangential stress is applied, opposite in direction on adjacent sides, the modulus of rigidity is obtained by dividing the numerical value of the tangential stress per unit area ( $\mathrm{kg} / \mathrm{mm}^{2}$ ) by the number representing the change of angles on the nonstressed faces, measured in radians.


TABLE 204.-VARIATION OF THE RIGIDITY MODULUS WITH THE TEMPERATURE
$n_{t}=n_{0}\left(1-a t-\beta t^{2}-\gamma t^{3}\right)$, where $t=$ temperature Centigrade

| Substance | $n_{0}$ | a $10^{8}$ | $\beta 10^{8}$ | $\gamma 10^{10}$ | Sulstance | $n_{0}$ | a $10^{8}$ | $\beta 10^{8}$ | $\gamma 10^{10}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Brass | 2652 | 2158 | 48 | 32 | Iron | 8108 | 206 | 19 | -11 |
| " | 3200 | 455 | 36 | - | " . .... | 6940 | 483 | 12 |  |
| Copper | 3972 | 2716 | -23 | 47 | Platinum | 6632 | 111 | 50 | -8 |
|  | 3900 | 572 | 28 | - | Silver ... | 2566 | 387 | 38 | 11 |
|  |  |  |  |  | Steel . . . . | 8290 | 187 | 59 | $-9$ |



* Modulus of rigidity in $10^{11}$ dynes per $\mathrm{cm}^{2}$.


## TABLE 205.-INTERIOR FRICTION AT LOW TEMPERATURES

$C$ is the damping coefficient for infinitely small oscillations; $T$, the period of oscillation in seconds; $N$, the modulus of rigidity dynes $/ \mathrm{cm}^{2}$.

| Substance Length of wire i | $\underset{22.5}{\mathrm{Cu}_{2}}$ | $\begin{gathered} \mathrm{Ni} \\ 22.2 \end{gathered}$ | $\begin{gathered} \mathrm{Au} \\ 22.3 \end{gathered}$ | $\begin{gathered} \mathrm{Pd} \\ 2.2 \end{gathered}$ | $\begin{array}{r} \mathrm{Pt} \\ 23.0 \end{array}$ | $\begin{aligned} & \mathrm{Ag} \\ & 17.2 \end{aligned}$ | Quartz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diameter in mm. | . 643 | . 411 | . 609 | . 553 | . 812 | . 601 | . 612 |
| $100^{\circ} \mathrm{C} \quad C$ | 24.1 | 1.34 | 27.5 | 1.67 | 2.98 | 55.8 | - |
|  | 2.381 | 3.831 | 3.010 | 2.579 | 1.143 | 1.808 |  |
| $N \times 10^{-11}$ | 3.32 | 7.54 | 2.55 | 5.08 | 5.77 | 2.71 |  |
| $0^{\circ} \mathrm{C} \quad{ }^{\text {C }}$ | 5.88 | . 417 | 4.82 | 1.25 | 4.60 | 7.19 | 4.69 |
|  | 2.336 | 3.754 | 2.969 | 2.571 | 1.133 | 1.759 | 1.408 |
| $N \times 10^{-11}$ | 3.45 | 7.85 | 2.62 | 5.12 |  | 2.87 | 2.26 |
| $-195^{\circ} \mathrm{C} \quad{ }_{\text {C }}$ | 3.64 | . 556 | 6.36 | . 744 | 3.02 | 1.64 | 1.02 |
|  | 2.274 | 3.577 | 2.902 | 2.552 | 1.111 | 1.694 | 1.425 |
| $N \times 10^{-11}$ | 3.64 | 8.65 | 2.74 | 5.19 | 6.10 | 3.18 | 2.20 |

TABLE 206.-RATIO, $\rho$, OF TRANSVERSE CONTRACTION TO LONGITUDINAL EXTENSION UNDER TENSILE STRESS
(Poisson's Ratio)

| Metal | Pb | Au | Pd | Pt | Ag | Cu | At | Bi | Sn | Ni | Cd | Fe |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $\rho$ | .45 | .42 | .39 | .39 | .38 | .35 | .34 | .33 | .33 | .31 | .30 | .28 |

$\rho$ for: marbles, . 27 ; granites, . 24 ; basic-intrusives, . 26 ; glass, . 23 .

TABLE 207.-A SCALE OF HARDNESS BASED UPON THE RELATIVE HARDNESS OF SELECTED MATERIALS

Each material will scratch the one following it in the table.

| 10 Diamond | 8 Topaz | 6 Feldspar | 4 Fluorite | 2 Rock salt |
| :---: | :---: | :--- | :--- | :--- |
| 9 Corundum | 7 Quartz | 5 Apatite | 3 Calcite | 1 Talc |


| Agate . . . . . . 7. | Barite .......3.3 | Fluorite ...... 4. | Marble . . . 3-4. | Ross' metal.2.5-3.0 |
| :---: | :---: | :---: | :---: | :---: |
| Alabaster ....1.7 | J3ell-metal ....4. | Galena . . . . . . 2.5 | Meerschaum 2-3. | Serpentine .3-4. |
| Alum . . . . .2-2.5 | Beryl ....... 7.8 | Garnet . . . . . 7. | Mica ........2.8 | Silver ....2.5-3. |
| Aluminum ...2.9 | 13ismuth . . 3.2 .5 | Glass ....4.5-6.5 | Opal . . . . . .4-6. | Silver |
| Amber . . . . $2-2.5$ | 13oric acid .... 3 . | Gold . . . . 2.5-3. | Orthoclase ....6. | chloride ....1.3 |
| . Indalusite ...7.5 | 13rass ......3-4. | Graphite . . . 5 -1. | Palladium ....4.8 | Steel ......5-8.5 |
| Anthracite ...2.2 | Calamine .... 5. | Gypsum ..1.6-2. | Phosphor- | Stibnite . . . . 2 2. |
| Antimony ....3.3 | Calcite . . . . . 3. | Hematite . . . . 6. | bronze ..... 4. | Sulfur ...1.5-2.5 |
| Apatite . . . . 5. | Copper ...2.5-3. | Hornblende ...5.5 | Platin. | Talc . . . . . . . 1. |
| Aragonite ....3.5 | Corundum ...9. | Iridium . . . . . 6.5 | iridium ....6.5 | Tin ........1.5 |
| Arsenic .....3.5 | Diamond . ... 10. | Iridosmium ... 7. | Platinum .....4.3 | Topaz ..... 8. |
| Asliestos ..... 5. | Dolomite . .3.5-4. | Iron . . . . . 4-5. | Pyrite ......6.3 | Tourmaline ...7.3 |
| Asphalt . ...1-2. | Feldspar . . . . . 6. | Kaolin ...... 1. | Quartz ....... 7. | Wax ( $0^{\circ}$ ) ..... 2 |
| Augite ...... 6. | Flint ....... 7. | Loess ( $0^{\circ}$ ) ..... 3 | Rock-salt ....2. | Wood's metal. . 3 . |

TABLE 209.-RELATIVE HARDNESS OF THE ELEMENTS (MEANS)

| * $\mathrm{C} . . . .10$. | Ir ..... 6.5 | Zr | 4.5 | A1 | 2.9 | Mg | 2.0 | In | 1.2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B ..... 9.5 | Ge ..... 6.2 | Pt | 4.3 | Ag | 2.7 | Se | 2.0 | T1 | 1.2 |
| $\mathrm{Cr} . . .{ }^{9} 9$. | Rh..... 6. | Ti | 4.0 | Zn | 2.5 | Cd | 2.0 | Li |  |
| Ta .... 7. | Mo .... 6? | Fe | 4. | Au | 2.5 | Sr | 1.8 | K |  |
| Os .... 7. | Mn .... 5. | As | 3.5 | Ce | 2.5 | Sn | 1.8 | Na |  |
| W .... 7. | Co ..... 5. | Sb | 3. | Bi | 2.5 | Pb | 1.5 | Rb |  |
| Si .... 7. | $\mathrm{Ni} . . . . .5$. | Be | 3. | Te | 2.3 | Ga | 1.5 | Cs |  |
| Ru .... 6.5 | Pd ..... 4.8 | Cu | 3.0 | S | 2.0 | Hg | 1.5 |  |  |

* Diamond.

TABLES 210-217.--CHARACTERISTICS OF SOME BUILDING MATERIALS


230
TABLE 212.-EFFECT OF QUANTITY OF MIXING WATER ON STRENGTH OF CONCRETE ${ }^{\circ}$

| W/C ratio, U. S. gal. per sack of cement (94\#). | 5.0 | 5.5 | 6.0 | 6.5 | 7.0 | 7.5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Compressive days-lb/in. ${ }^{2}$ strength at 28 | 5000.0 | 4500.0 | 4100.0 | 3600.0 | 3300.0 | 2900.0 |

${ }^{\infty}$ Portland Cement Association, Design and control of concrete mixtures, 9th ed., p. 7.

TABLE 213.-COMPARISON OF STRENGTH AND ELASTIC PROPERTIES OF CONCRETE ${ }^{\text {b1 }}$
Modulus of elasticity psi $\times 10^{-6}$

| Compressive <br> strength psi | Modulus of <br> rupture psi | Compressive <br> (secant) | Flexural <br> (secant) | Dynamic <br> (sonic) |
| :---: | :---: | :---: | :---: | :---: |
| 2000 | 400 | 2.5 | 3.5 | 4.5 |
| 4000 | 600 | 4. | 5. | 5.5 |
| 6000 | 750 | 5.5 | 6.5 |  |
| 8000 | 850 | 6.5 | 6.5 | 7. |

Values given are approximations only since the ratios between the different properties depend on age, aggregates, cement, and other factors.
${ }^{61}$ Stanton, T. E., Amer. Soc. Test. Mat. Bull. No. 131, p. 17, 1944; Witte and Price, ibid., p. 20; Schuman and Tucker, Nat. Bur. Standards Journ. Res., vol. 31, p. 107, 1943; Gonnerman and Shuman, Proc. Amer. Soc. Test. Mat., vol. 28, p. 527, 1928.

* As determined on specimens with length to diameter ratio of 2 .


## TABLE 214.-EFFECT OF ENTRAINED AIR ON COMPRESSIVE STRENGTH OF CONCRETE ${ }^{62}$

| Cement <br> Sacks per $\mathrm{dd}^{3}$ | Percent change in strength due to 5 percent |
| :---: | :---: | :---: |
| 4.5 |  |
| added air * |  |

[^97]TABLE 215.-WEIGHTED AVERAGE STRENGTH AND WATER ABSORPTION FOR HARD AND SALMON BRICKS MADE IN U. S. A. ${ }^{83}$


[^98]| Brick strength 1b/in. ${ }^{2}$ | Cement mortar LC:1/4. | $\begin{gathered} \text { Cement. } \\ \text { lime } \\ \text { mortar } \\ 1 \mathrm{C}: 1 \mathrm{~L} ; 6 \mathrm{~S} \end{gathered}$ | $\begin{aligned} & \text { Lime } \\ & \text { mortar } \\ & 1 \mathrm{~L}: 3 \mathrm{~S} \end{aligned}$ | Brick strength lb/in. ${ }^{2}$ | Cement mortar 1C:1/4. $\mathrm{L}: 3 \mathrm{~S}$ * | $\begin{gathered} \text { Cement- } \\ \text { lime } \\ \text { mortar } \\ 1 \mathrm{C}: 1 \mathrm{~L} ; 6 \mathrm{~S} \end{gathered}$ | $\begin{gathered} \text { Lime } \\ \text { mortar } \\ 1 \mathrm{~L}: 3 \mathrm{~S} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $8000+$ | 2000 | 1200 | 800 | 2500-4500 | 700 | 560 | 275 |
| 4500-8000 | 1000 | 800 | 400 | 1500-2500 | 500 | 400 | 150 |

of Nat. Bur. Standards Res. Pap. RP 108.

* C-portland cement; L-Lime; S-sand, proportions by volume. See American Standard Associations Building Code Requirements for Masonry (A41.1-1944).

TABLE 217.-STRENGTH AND STIFFNESS OF AMERICAN BUILDING STONE*
(All values in pounds per square inch.)

| Stone | Density $\mathrm{lb} / \mathrm{ft}^{3}$ | Compressive strength (dry) psi | Flexure strength psi | Shear psi | Flexural modulus of elasticity psi | Compressive modulus of elasticity psi |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Granite | .. 165 | $\begin{aligned} & \text { (116 samples) } \\ & 24500(7700-53,000) \dagger \end{aligned}$ | $\begin{aligned} & 2810(1430-5190) \\ & (5 \text { samples }) \end{aligned}$ | $\begin{gathered} 4350 \text { ( } 3900-4600 \text { ) } \\ \text { (4 samples) } \end{gathered}$ | $\begin{array}{r} 2,526,000- \\ 12,950,000 \end{array}$ | 4,545,000.8,333,000 |
| Limestone | 148 | 2600-28,400 | $\begin{aligned} & 640-2000 \ddagger \\ & 470-19008 \end{aligned}$ | $\begin{aligned} & 830.3840 \dagger \\ & 800 \cdot 31008 \end{aligned}$ | $\begin{array}{r} 700,000 \\ 10,400,000 \ddagger \end{array}$ | 1,600,000-11,200,000 |
| Marble | . . 170 | 7850-29,530 | 900-4270 |  | $\begin{array}{r} 1,840,000- \\ 11,780,000 \end{array}$ |  |
| Sandstone | . 135 | 4470-34,900+ | $260.6570+$ |  |  |  |
| Slate .... | .. 170 |  | 500.14,100 |  | $\begin{array}{r} 9,800,000- \\ 18,000,000 \end{array}$ |  |

*Furnished by Herbert Insley, National Bureau of Standards. † Wet samples 12 percent less. $\ddagger$ Perpendicular to bed. \& Parallel to bed.

## TABLES 218-223.-PHYSICAL PROPERTIES OF LEATHER *

Most physical properties of leathers not only depend on the kind of skin and method of tannage but also vary widely from one hide to another of the same kind, from one location to another within the same hide, and in local random fashion. For example, the tensile strength of vegetable-tanned cattle hides shows coefficients of variation of 6 percent among bends (from different hides), 9 percent among locations (within a hide), and 11 percent for local random fluctuations. ${ }^{63}$ The Federal Specifications Board in the United States requires that at least 7 pieces of leather be sampled for most physical tests. ${ }^{\text {.6 }}$ In any use of a physical property of leather, such as designing an experiment or acceptance testing for commercial purchase, these variations and the consequent statistical precautions must be observed. The figures below, then, are illustrative, not precise values for any given type of leather.

[^99]TABLE 218.-TENSILE STRENGTH AND ELONGATION OF LEATHER ${ }^{67}$


[^100]
## TABLE 219.-DIFFUSION CONSTANTS OF WATER VAPOR THROUGH LEATHER, AS FRACTIONS OF THE DIFFUSION CONSTANT THROUGH AIR $\left(20^{\circ} \mathrm{C}\right)^{\text {as }}$

| Heavy <br> chrome upper | Box calf | Glove <br> capeskin | Patent <br> leather | Vegetable-tanned <br> insole |
| :---: | :---: | :---: | :---: | :---: |
| $.1-.2$ | $.21-.26$ | $.17-.26$ | .004 | .09 |

[^101]TABLE 220.-REAL AND APPARENT DENSITIES OF LEATHER ( $70^{\circ} \mathrm{F}$ AND 65 PERCENT, RELATIVE HUMIDITY) ${ }^{\circ 0}$

| Kind of leather | Apparent density | Real density |
| :---: | :---: | :---: |
| Raw bated skin | . 41 - . 45 | 1.43 |
| Formaldehyde tanned buckskin | . 56 | 1.52 |
| Chrome-tanned shoe upper. | . 88 | 1.34 |
| Vegetable-tanned sole | 1.03-1.15 | 1.46-1.49 |
| Chrome-tanned sole | 1.17 | 1.46 |
| Formaldehyde-tanned suede | . $50-.58$ | 1.55-1.62 |
| Vegetable-tanned goatskin | . 65 | 1.52 |

[^102]TABLE 221.-COEFFICIENT OF CUBICAL EXPANSION OF LEATHER
(Measured in water between $25^{\circ}$ and $75^{\circ} \mathrm{C}$ ) ${ }^{70}$

| Chrome | Chrome-vegetable | Vegetable | Alum-vegetable |
| :---: | :---: | :---: | :---: |
| $496-565 \times 10^{-0}$ | $339-298 \times 10^{-6}$ | $502-543 \times 10^{-0}$ | $590-599 \times 10^{-6}$ |
| Iron | Formaldehyde | Tendon collagen |  |
| $592 \times 10^{-6}$ | $532 \times 10^{-6}$ | $538 \times 10^{-6}$ |  |

Compressibility. ${ }^{71}$ - The lower limit of the coefficient of compressibility of vegetabletanned sole leather has been estimated at $33 \times 10^{-9}$ bar $^{-1}$. Commercial sole leathers subjected to $3000 \mathrm{lb} / \mathrm{in}^{2}{ }^{2}$ pressure for 3 minutes were compressed from 4 to 17 percent.
70 Weir, C. E., Journ. Amer. Leather Chem. Assoc., vol. 44, P. 79, 1949.
71 Weir, C. E., Journ. Amer. Leather Chem. Assoc., vol. 40, p. 404, 1945.

TABLE 222.-EFFECT OF RELATIVE HUMIDITY OF ATMOSPHERE AT $21^{\circ} \mathrm{C}$ ON PROPERTIES OF LEATHER ${ }^{72}$

| Percent <br> relative <br> humidity | Tensile <br> strength <br> 1b/in. | Stretch at <br> 2000 lh/in. <br> percent | Increase <br> in thickness <br> percent | Increase <br> in area <br> nercent |
| :---: | :---: | :---: | :---: | :---: |
| 0 | 4630 | Vegetable-tanned calfskin |  |  |
| 33 | 5210 | 16 | .0 | .0 |
| 52 | 5220 | 19 | 2.3 | 5.2 |
| 76 | 5280 | 19 | 4.9 | 5.7 |
| 97 | - | 21 | 9.6 | 6.4 |
|  |  | 21 |  | 7.3 |
| 0 | 3170 | Chrome-tanned calfskin |  |  |
| 33 | 4550 | 19 | .0 | .0 |
| 52 | 4840 | 25 | 1.6 | 7.9 |
| 76 | 5080 | 23 | 4.2 | 8.9 |
| 97 | 5420 | 24 | 14.0 | 10.2 |

${ }^{72}$ Evans, W. D., and Critchfield, C. L., Nat. Bur. Standards Journ. Res., vol. 11, p. 147, 1933.

TABLE 223.-THERMAL CONDUCTIVITY OF LEATHER*
cal $\mathrm{cm}^{-1} \mathrm{sec}^{-1}{ }^{\circ} \mathrm{C}^{-1}$

| Vegetahle sole leather | Calf skin upper | Kid suede | Hide bellies |
| :---: | :---: | :---: | :--- |
| $4.2 \times 10^{-4}$ | $2.0 \times 10^{-4}$ | $1.5 \times 10^{-4}$ | $2.3 \times 10^{-4}$ |

[^103]TABLES 224-229.-VALUES OF PHYSICAL CONSTANTS OF DIFFERENT RUBBERS*

Where a range is given, there are available several observations that differ. In most cases the differences are thought to be real, arising from differences in the rubber rather than from errors of observation. Where a single value is given, it is either because no other observations are available or because there seems to be no significant disagreement among values within the errors of observation. The latter values are marked with an asterisk (*). Where no values are given, no data have been found. Where dashes are shown, either the physical measurement is impossible or the values obtained are not significant. Values at $25^{\circ} \mathrm{C}$ and 1 atmosphere pressure.

Since these data were compiled from a number of sources, no specific references are given. A list of references follows:

Ball, J. M., and Maasen, G. C., American Society for Testing Materials Symposium on the Applications of Synthetic Rubbers, March 2, 1944. Bekkedahl, Norman, Natural rubbers-a general summary of their composition, properties, and uses, India Rubber World, vol. 116, p. 57, 1947 ; also in Compounding ingredients for rubber, published by India Rubber World, New York, 1947. Bekkedahl, N., and Roth, F. L., Unpublished observations of density and expansivity, 1948 . Boonstra, B. B. S. T., Properties of elastomers, chap. 4 of vol. 3 of Elastomers and plastomers, their chemistry, physics, and technology, edited by R. Houwink, Elsevier Publishing Co., New York, 1948. Dawson, T. R., and Porritt, B. D., Rubber physical and chemical properties, Research Association of British Rubber Manufacturers, Croydon, England, 1935. Dillon, J. H., Prettyman, I. B., and Hall, G. L., Hysteretic and elastic properties of rubberlike materials under dynamic shear stresses, Journ. Appl. Phys., vol. 15, p. 309, 1944 ; Rubber Chem. Techn., vol. 17, p. 597, 1944. Hamill, W. H., Mrowca, B. A., and Anthony, R. L., Specific heats of hevea, GR-S, and GR-I stocks, Ind. Eng. Chem., vol. 38, p. 106, 1946; Rubber Chem. Techn., vol. 19, p. 622, 1946. Kemp, A. R., and Malm, F. S., Hard rubber (ebonite), chap. 18 in Chemistry and technology of rubber, edited by C. C. Davis and J. T. Blake, Reinhold Publishing Corporation, New York, 1937. Prettyman, I. B., Physical properties of natural and synthetic rubber stocks, Handbook of Chemistry and Physics, 30th ed., p. 1301, Chemical Rubber Publishing Co., Cleveland, Ohio, 1947. Rands, Robert D., Jr., Ferguson, W. Julian, and Prather, John L., Specific heat and increases of entropy and enthalpy of the synthetic rubber GR-S from $0^{\circ}$ to $330^{\circ} \mathrm{K}$, Nat. Bur. Standards Journ. Res., vol. 33, p. 63, 1944 (RP1595). Selker, Alan H., Scott, Arnold H., and McPherson, Archibald T., Electrical and mechanical properties of the system Buna S-Gilsonite, Nat. Bur. Standards Journ. Res., vol. 31, p. 141, 1943 (RP1554). Wildschut, A. J., Technological and physical investigations on natural and synthetic rubbers. Elsevier Publishing Co., New York, 1946. Wood, Lawrence A., Bekkedahl, Norman, and Roth, Frank L., The measurement of densities of synthetic rubbers, Nat. Bur. Standards Journ. Res., vol. 29, p. 391, 1942 (RP1507) ; Ind. Eng. Chem., vol. 34, p. 1291, 1942; Rubber Chem. Techn., vol. 16, p. 244, 1943. Wood, L. A., and Tilton, L. W., Refractive index of natural rubber at different wavelengths, Proc. Second Rubber Techn. Conf., p. 142 (Institution of the Rubber Industry, London), 1948; Nat. Bur. Standards Journ. Res., vol. 43. p. 57, 1949 (RP2004). Wood, Lawrence A., Synthetic rubbers: a review of their compositions, properties, and uses, Nat. Bur. Standards Circ. C427, 1940; Rubber Chem. Techn., vol. 13, p. 861, 1940 ; India Rubber World, vol. 102, p. 33, 1940. Wood, Lawrence A., Values of the physical constants of rubber, Proc. Rubber Techn. Conf., p. 933 (Institution of the Rubber Industry, London), 1938; Rubber Chem. Techn., vol. 12, p. 130, 1939.

[^104]| Unit | Unvulcanized | Pure-gum vulcanizate | Vulcanizate containing about $33 \%$ carbon black | $\underset{\substack{\text { Ebonite } \\ \text { (hard rubber) }}}{\text { ( }}$ |
| :---: | :---: | :---: | :---: | :---: |
| Density $\ldots . . . . . . . . . . . . \mathrm{g} \mathrm{cm}^{-3}$ | .906-.916 | .92-1.0 | 1.12-1.15 | 1.13-1.18 |
| Expansivity $(1 / V)(\mathrm{dV} / \mathrm{dT}) \quad \ldots \ldots . .(\operatorname{deg} C)^{-1}$ | $67 \times 10^{-5}$ | $66 \times 10^{-5}$ | $53 \times 10^{-5}$ | $19 \times 10^{-5}$ |
| Thermal |  |  |  |  |
| Thermal conductivity $\ldots . . \begin{gathered}\text { cal sec } \\ \left(\operatorname{deg} \mathrm{cm}^{-1}\right.\end{gathered}$ | $32 \times 10^{-5}$ | $34 \times 10^{-5}$ | $39-45 \times 10^{-5}$ | $39-42 \times 10^{-6}$ |
| Specific heat $\qquad$ cal $\mathrm{g}^{-1}$ $(\operatorname{deg} \mathrm{C})^{-1}$ | . 45 | .44-. 51 | . 36 | . 34 |
| Heat of combustion...... cal $\mathrm{g}^{-1}$ | $10.82 \times 10^{3}$ | $10.63 \times 10^{3}$ | $9.61 \times 10^{3}$ | $7.92 \times 10^{3}$ |
| Second-order transition temperature ............ deg C | $-69 \text { to }-74$ | -72 |  | +80 |
| Optical |  |  |  |  |
| $\begin{aligned} & \text { Refractive index, } n_{D} \ldots \ldots . . \\ & d n_{D} / d T \ldots \ldots \ldots \ldots \ldots . .(\operatorname{deg} C)^{-1} \end{aligned}$ | $\stackrel{1.5191}{-37 \times 10^{-5}}$ | $\begin{aligned} & 1.5264 \\ & -37 \times 10^{-5} \end{aligned}$ | 二二 | 1.6 |
| Electrical |  |  |  |  |
| Dielectric constant (1000 cps) | 2.37-2.45 | 2.7 |  | 2.8-2.9 |
| Loss factor, $\tan \left(90^{\circ}-\theta\right)$ (1000 cps) |  | . 002 |  | . 005 |
| Conductivity ( 1 min ) $\ldots .$. mho $\mathrm{cm}^{-1}$ | $2.40 \times 10^{-17}$ | $10^{-17}$ |  | $10^{-17}$ |
| Mechanical |  |  |  |  |
| Compressibility <br> ( $1 / \mathrm{V}$ ) ( $\mathrm{dV} / \mathrm{dP}$ ) $\ldots . . .$. bar $^{-1}$ | $54 \times 10^{-6}$ | $51 \times 10^{-6}$ | $37 \times 10^{-8}$ | $24 \times 10^{-6}$ |
| Shear modulus $\ldots \ldots \ldots$. dynes $\mathrm{cm}^{-2}$ |  | $4 \times 10^{8}$ | $20 \times 10^{6}$ |  |
| Initial slope of stress-strain curve dynes $\mathrm{cm}^{-2}$ | -- | $10-20 \times 10^{8}$ | $30-60 \times 10^{6}$ | $55 \times 10^{0}$ |
| Ultimate elongation ...... percent | -- | $750-850$ | 550-650 |  |
| Tensile strength $\ldots \ldots . . . \mathrm{kg} \mathrm{cm}^{-2}$ |  | 170-250 | 250-350 | 600-800 |
| Complex dynamic shear mod-$\text { ulus }(60 \mathrm{cps}), \frac{\sigma^{\prime}+\mathrm{i} \sigma^{\prime \prime}}{\epsilon} \ldots$ |  |  |  |  |
| Real part $\mathrm{G}^{\prime}, \frac{\sigma^{\prime}}{\epsilon} \ldots \ldots .$. dynes $\mathrm{cm}^{-2}$ |  | $3-10 \times 10^{6}$ | $25 \times 10^{6}$ |  |
| Imaginary part $\mathrm{G}^{\prime \prime}, \frac{\sigma^{\prime \prime}}{6} \ldots$ dynes $\mathrm{cm}^{-2}$ |  | . $3-.6 \times 10^{6}$ | $3 \times 10^{6}$ |  |
| Resilience (ball rebound).. percent | 75 | 75 | 45-55 |  |

TABLE 225.-PROPERTIES OF GR-S (HYDROCARBON OF ABOUT 23.5 PERCENT BOUND STYRENE CONTENT)

|  | ${ }_{\text {Unit }}$ | Unvulcanized | Pure-gum <br> vulcanizate | Vulcanizate containing carbon black $\square$ |
| :---: | :---: | :---: | :---: | :---: |
| Density <br> Expansivity (1/V)(dV/dT) | $\begin{aligned} & \mathrm{g} \mathrm{~cm}^{-8} \\ & (\operatorname{deg~C})^{-1} \end{aligned}$ | $\begin{aligned} & .9325-.9335 \\ & 66 \times 10^{-5} \end{aligned}$ | $\begin{aligned} & .961 \\ & 66 \times 10^{-5} \end{aligned}$ | $\begin{aligned} & 1.15 \\ & 53 \times 10^{-5} \end{aligned}$ |
| Thermal |  |  |  |  |
| Specific heat Second-order transition temperature. | $\begin{aligned} & \operatorname{cal~g}^{-1}(\operatorname{deg} C)^{-1} \\ & \operatorname{deg} C \end{aligned}$ | $.45$ | . 43 | . 36 |
| Optical |  |  |  |  |
| Refractive index, $n_{D}$ $\mathrm{dn}_{\mathrm{D}} / \mathrm{dT}$ | $(\operatorname{deg} C)^{-1}$ | $\begin{aligned} & 1.534-1.535 \\ & -37 \times 10^{-5} \end{aligned}$ |  | -- |
| Electrical |  |  |  |  |
| Dielectric constant ( 1000 cps )........ |  |  | 2.85 |  |
| Loss factor, $\tan \left(90^{\circ}-\theta\right)(1000 \mathrm{cps}) .$. |  |  | . 003 |  |
| Mechanical |  |  |  |  |
| Shear modulus ... | dynes $\mathrm{cm}^{-2}$ | -- |  | $25 \times 10^{\text {a }}$ |
| Initial slope of stress-strain curve.... | dynes $\mathrm{cm}^{-2}$ | -- | $10-20 \times 10^{6}$ | $30-60 \times 10^{6}$ |
| Ultimate elongation ................ | percent | -- | 400-600 | $400-600$ |
| Tensile strength | $\mathrm{kg} \mathrm{cm}^{-2}$ | - | 14-28 | 170-280 |
| Complex dynamic shear modulus$(60 \mathrm{cps}), \frac{\sigma^{\prime}+\mathrm{i} \sigma^{\prime \prime}}{\epsilon}$ |  |  |  |  |
| Real part $\mathrm{G}^{\prime}, \frac{\sigma^{\prime}}{\epsilon} \ldots \ldots \ldots \ldots \ldots .$. | dynes $\mathrm{cm}^{-2}$ |  | $5 \times 10^{6}$ | $55 \times 10^{6}$ |
| Imaginary part $G^{\prime \prime}, \frac{\sigma^{\prime \prime}}{\epsilon} \ldots . . . . . . .$. | dynes $\mathrm{cm}^{-2}$ |  | $1-2 \times 10^{6}$ | $9 \times 10^{6}$ |
| Resilience (ball rebound)............ | percent |  | 65 | 40-50 |

TABLE 226.-PROPERTIES OF NEOPRENE (CHLOROBUTADIENE POLYMER)

|  | Unit | Unvulcanized | Pure-gum vulcanizate | Vulcanizate containing about $33 \%$ carbon black carbon black |
| :---: | :---: | :---: | :---: | :---: |
| Density <br> Expansivity (1/V)(dV/dT) | $\xrightarrow[(\mathrm{deg} \mathrm{C})^{-1}]{\mathrm{cm}^{-3}}$ | 1.23 | $\begin{aligned} & 1.30 \\ & 61 \times 10^{-5} \end{aligned}$ |  |
| Thermal |  |  |  |  |
| Second-order transition temperature. | deg C | -38 to -41 |  |  |
| Optical |  |  |  |  |
| Refractive Index no. $\mathrm{dn}_{\mathrm{D}} / \mathrm{dT}$ | $(\operatorname{deg} \mathrm{C})^{-1}$ | $\frac{1.558}{-36 \times 10^{-5}}$ |  | 二二 |
| Mechanical |  |  |  |  |
| Shear modulus ................ | dynes $\mathrm{cm}^{-2}$ | - |  | $14 \times 10^{6}$ |
| Initial slope of stress-strain curve. | dynes $\mathrm{cm}^{-2}$ | -- | $15-30 \times 10^{6}$ |  |
| Ultimate elongation | percent | -- | $800-1000$ |  |
| Tensile strength | $\mathrm{kg} \mathrm{cm}^{-2}$ | -- | 250-375 |  |
| Complex dynamic shear modulus ( 60 cps ),$\sigma^{\prime}+\mathrm{i} \sigma^{\prime \prime}$ |  |  |  |  |
| $\epsilon$ |  |  |  |  |
| Real part $\mathrm{G}^{\prime}, \frac{\sigma^{\prime}}{\epsilon}$ | dynes $\mathrm{cm}^{-2}$ |  | $6 \times 10^{8}$ | $30-36 \times 10^{6}$ |
| Imaginary part $\mathrm{G}^{\prime \prime}, \frac{\sigma^{\prime \prime}}{\epsilon} \ldots \ldots$. | dynes $\mathrm{cm}^{-2}$ |  | $1 \times 10^{6}$ | $6 \times 10^{6}$ |
| Resilience (ball rebound)............ | percent |  | 65 | 40-50 |

TABLE 227.-PROPERTIES OF GR-1 (BUTYL RUBBER, ISOBUTENE-ISOPRENE COPOLYMER)

| Unit | Unvulcanized | Pure-gum vulcanizate | Vulcanizate containing carbout black |
| :---: | :---: | :---: | :---: |
| Density $\ldots \ldots \ldots \ldots .$. | . 92 | $.93$ | $\begin{aligned} & 1.13 \\ & 46 \times 10^{-5} \end{aligned}$ |
| Thermal |  |  |  |
| Second-order transition temperature....... deg C | -67 to -73 |  |  |
| Optical |  |  |  |
| Refractive Index no. | 1.5091 |  | -- |
| Elcctrical |  |  |  |
| Dielectric constant |  | 2.1-2.6 |  |
| Mechanical |  |  |  |
| Shear modulus | -- |  | $18 \times 10^{6}$ |
| Initial slope of stress-strain curve....... dynes $\mathrm{cm}^{-2}$ | -- | $7-15 \times 10^{6}$ | $30-40 \times 10^{6}$ |
| Ultimate elongation................. . percent | -- | 750-950 | $650-850$ |
| Tensile strength ..................... $\mathrm{kg} \mathrm{cm}^{-2}$ | -- | 180-210 | 180-210 |
| Complex$\sigma^{\prime}+\mathrm{i} \sigma^{\prime \prime}$ dynamic shear modulus ( 60 cps ), |  |  |  |
| $\epsilon$, |  |  |  |
| Real part $\mathrm{G}^{\prime}, \frac{\sigma^{\prime}}{\epsilon} \ldots \ldots \ldots \ldots \ldots \ldots \ldots .$. dynes $\mathrm{cm}^{-2}$ |  | $4-10 \times 10^{\text {a }}$ | $36 \times 10^{6}$ |
| Imaginary part $\mathrm{G}^{\prime \prime}, \frac{\sigma^{\prime \prime}}{\epsilon} \ldots \ldots \ldots . \ldots . . .$. dynes $\mathrm{cm}^{-2}$ |  | $2-3 \times 10^{6}$ | $16 \times 10^{6}$ |
| Resilience (ball rebound)............... percent |  | 8 | 7 |

TABLE 228.-COMPRESSION OF RUBBER ${ }^{73}$
Commercial soft-packing, black, density about $1.9 \mathrm{~g} / \mathrm{cm}^{3}$ and $V_{0}=1 \mathrm{~cm}^{3}$
$\Delta V$

| Pressure <br> $\mathrm{kg} / \mathrm{cm}^{2}$ | $20^{\circ} \mathrm{C}$ | $-78.8^{\circ} \mathrm{C}$ | Pressure <br> $\mathrm{kg} / \mathrm{cm}^{2}$ | $20^{\circ} \mathrm{C}$ | $-78.8^{\circ} \mathrm{C}$ | Pressure <br> $\mathrm{kg} / \mathrm{cm}^{2}$ | $20^{\circ} \mathrm{C}$ | $-78.8^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5,000 | .1300 | .0794 | 20,000 | .2345 | .1772 | 35,000 | .2845 | .2254 |
| 10,000 | .1800 | .1235 | 25,000 | .2535 | .1958 | 40,000 | .2960 | .2364 |
| 15,000 | .2146 | .1538 | 30,000 | .2700 | .2119 | 45,000 | .3050 | .2460 |

[^105]TABLE 229.-COMPRESSION OF SYNTHETIC AND NATURAL RUBBERS *4

| $\underset{\substack{\text { Pressure } \\ \mathrm{kg} / \mathrm{cm}^{2}}}{\text { density }}$ | Duprene | Koroseal No. 89023 | $\begin{aligned} & \text { Neoprene } \\ & \text { No. } 8322 \end{aligned}$ | Buna S <br> No. 8774 | $\begin{gathered} \text { Ameripol } \\ \mathrm{D}-7700 \end{gathered}$ | $\begin{aligned} & \text { Hood } \\ & 844 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & \text { Goodrich } \\ & \text { D. } 402 \end{aligned}$ | $\begin{aligned} & \text { Goodrich } \\ & \text { D. } 420 \end{aligned}$ | $\underset{\text { D.453 }}{\substack{\text { Goodrich }}}$ | $\underset{\text { D.453 }}{\substack{\text { Goodrich }}}$ | $\underset{\text { gum }}{\substack{\text { Butyl }}}$ | Butyl tread | $\begin{aligned} & \text { Hevea } \\ & \text { gum } \end{aligned}$ | Hevea tread |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1.589 | 1.250 | 1.357 | 1.376 | 1.370 | 1.176 | 1.193 | 1.350 | 1.514 | 1.309 | . 967 | 1.125 | . 950 | 1.122 |
| 2000 | . 0302 | . 0511 | . 0460 | . 0465 | . 0367 | . 0407 | . 0422 | . 0385 | . 0329 | . 0432 | . 0519 | . 0423 | . 0535 | . 0462 |
| 5000 | . 0615 | . 0967 | . 0956 | . 0872 | . 0715 | . 0792 | . 0837 | . 0745 | . 0636 | . 0842 | . 0945 | . 0807 | . 1017 | . 0870 |
| 10,000 | . 0898 | . 1403 | . 1294 | . 1238 | . 1052 | . 1163 | . 1194 | . 1128 | . 0938 | . 1208 | . 1303 | . 1129 | . 1422 | . 1250 |
| 15,000 | . 1198 | . 1679 | . 1567 | . 1493 | . 1304 | . 1445 | . 1454 | . 1378 | . 1162 | . 1480 | . 1543 | . 1334 | . 1697 | . 1490 |
| 20,000 | . 1301 | . 1891 | . 1793 | . 1715 | . 1507 | . 1663 | . 1670 | . 1587 | . 1347 | . 1692 | . 1744 | . 1510 | . 1929 | . 1707 |
| 25,000 | . 1462 | . 2060 | . 1990 | . 1903 | . 1686 | . 1840 | . 1847 | . 1769 | . 1513 | . 1862 | . 1920 | . 1667 | . 2116 | . 1900 |
| Pressure of discontinuity | 3,500 |  | 4,800 | 6,300 | 4,900 |  | 4,800 |  |  |  | 6,200 |  |  | 6,500 |
| Amount of discontinuity | $2.0 \times 10^{-8}$ |  | $5.3 \times 10^{-6}$ | $3.4 \times 10^{-6}$ | $1.5 \times 10^{-6}$ |  | $3 \times 10^{-6}$ |  |  |  | $5 \times 10^{-6}$ |  |  | $2 \times 10^{-8}$ |
| $\Delta \mathrm{V} / \mathrm{V}_{0}$ at discontinuity | . 0516 |  | . 0939 | . 1012 | . 0707 |  | . 0851 |  |  |  | . 1083 |  |  | . 1026 |
| Ratio of width of hysteresis loop to maximum displacement | - $\begin{aligned} & \\ & \\ & .083\end{aligned}$ | . 059 | . 082 | . 087 | . 064 | . 067 | . 072 | . 080 | . 103 | . 077 | . 083 | . 090 | . 074 | . 073 |

[^106]TABLE 230．－CHARACTERISTICS OF A NUMBER OF PLASTICS ${ }^{75}$

| Material |  |  |  |  |  |  | 育会会 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Acrylic plastic | 1．18－1．19 | ． 91 | 1．485－1．500 | 9 | 4－6 | ． 35 | $>10^{15}$ | 450－500 | 3．5－4．5 | 11000－14000 | 3．3－4．5 | M88－M92 |
| Nylon | 1．14－1．09 | $\ldots$ | 1.53 | 10 | 5.8 | ． 4 | $4.5 \times 10^{13}$ | 385 | 4.1 | 13000 | 4 | R－118 |
| Polyvinyl formal | 1．2－1．3 | ．85－． 91 | 1.5 | 7.7 | 3.7 |  |  | 300－600 | 3．6－3．7 | 9000－17000 | 26 | M80－M90 |
| Allyl and polyester | 1．10－1．46 | $\ldots$ | 1．53－1．56 | 8．0－10． | 4．8－5．0 | ．26－． 55 | $>4 \times 10^{14}$ | 380 | 3．4－5． | 21000－23000† | 3－8．2 | M85－M119 |
| Cellulose nitrate | 1．35－1．40 | ．89－． 92 | 1．49－1．51 | 8．－12． | 5.5 | ．3－．4 | $10-15 \times 10^{10}$ | 300－600 | 7．－7．5 | 6000－11000 | 1．9－2．2 | R95－R115 |
| Polysterene | 1．05－1．06 | $\ldots$ | 1．59－1．60 | $6 .-8$. | 2．4－3．3 | ． 32 | $10^{17}-10^{18}$ | 500－700 | 2．4－2．6 | 11000－16000 | 4．－5． | M85－M95 |
| Phenolic molding | 1．3－1．5 | $\ldots$ | $\ldots$ | 3．－4．5 | 4.7 | ． $35-40$ | $1-100 \times 10^{11}$ | $\ldots$ | 5．－9． | $\ldots$ | 8．－12． | M110－M120 |
| Ethyl cellulose | 1．12－1．14 |  | 1.47 | 10－20 | 3．8－7 | ．3－．75 | $10^{12}-10^{24}$ | 350－500 | $\ldots$ | 11000－13000 ${ }^{\dagger}$ | 1．3－3．5 | R100－R110 |

[^107]| Name | Polymer |  | $\underset{\substack{\text { Monomer } \\ N_{\mathrm{D}}{ }^{20}}}{ }$ | $\underset{\substack{\text { Boiling } \\{ }^{\circ} \mathrm{C} \\ \nu}}{\text { point }}$ |
| :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{N}_{\mathrm{n}}{ }^{20}$ | $\nu$ * |  |  |
| Allyl methacrylate | 1.5196 | 49.0 | $\begin{aligned} & 1.4340 \\ & \text { at } 23^{\circ} \end{aligned}$ | $55 / 30 \mathrm{~mm}$ |
| Benzyl mellacrylate | 1.5680 | 36.5 | 1.514 | 233 |
| 4-cyctolaxyl-cyclohexyl metharcylate | 1.5250 | 53. | 1.4913 | $111 / 1 \mathrm{~mm}$ |
| Menthyl metharcylate | 1.5064 | 54.5 |  |  |
| Ethylene dimethacrylate | 1.5063 | 53.4 | 1.4547 | $92 / 3 \mathrm{~mm}$ |
| Methyl methacrylate | 1.490 | 56.25 | 1.417 |  |
| Styrene | 1.5916 | 31.0 | 1.5434 |  |
| O-chlorostyrene | 1.6098 | 31.0 | 1.567 | $47 / 37 \mathrm{~mm}$ |
| Pentachlorophenol methacrylate | 1.608 | 22.5 | ... | (MP $88.5^{\circ} \mathrm{C}$ ) |
| Vinyl naphthalene | 1.6818 | 20.9 | ... | 92-95/mm |

[^108]TABLE 232.-GENERAL PROPERTIES OF OPTICAL PLASTICS

| Index $\mathrm{N}_{\mathrm{D}} 20^{\circ} \mathrm{C}$.. Index tolerance . | Cyclo- <br> hexyl. <br> crylate | Sterene |  | $\begin{aligned} & \text { Cyclo- } \\ & \text { hexyl- } \\ & \text { metha. } \\ & \text { crylate } \end{aligned}$ | Sterene |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1.50645 | 1.59165 | Thermal exp. coeff.... | $9.0 \times 10^{-5} /{ }^{\circ} \mathrm{C}$ | $8.0 \times 10^{-5} /{ }^{\circ} \mathrm{C}$ |
|  | +. 0015 | +. 0015 | Thermal conductivity. | $2.31 \times 10^{-4}$ | $2.21 \times 10^{-4}$ |
| $\nu$ values ....... |  | 31.0 | Index charge per ${ }^{\circ} \mathrm{C}$. | $(\mathrm{cgs})$ -.000131 | $\begin{aligned} & \mathrm{cal} \mathrm{sec}^{-1} \mathrm{~cm}^{-10} \mathrm{C} \\ & -.000136 \end{aligned}$ |
| " " tolerance. |  | + + | Max. operating temp.. | $150^{\circ} \mathrm{F}$ | $150^{\circ} \mathrm{F}$ |
| Partial dispersion |  |  |  |  |  |
| $\mathrm{N}_{\mathrm{F}}-\mathrm{Nc}$. | . 00895 | . 01920 | Density | $1.095 \mathrm{~g} / \mathrm{cm}^{3}$ | $1.049 \mathrm{~g} / \mathrm{cm}^{3}$ |
| $\mathrm{N}_{\mathrm{n}}-\mathrm{Nc}$ | . 00258 | . 00536 | Moles hardness ...... | 2-3 |  |
| $\mathrm{N}_{\mathrm{F}}-\mathrm{N}_{\mathrm{D}}$ | . 00638 | . 01384 | Over-all visual trans- |  |  |
|  |  |  | mittance through sample $\frac{3}{8}$ in. thick | 99.1\% | 99.9\% |

The values of the properties of natural fibers are influenced by their source, extent of processing or purification, age, temperature and moisture content when tested, and method of test. Those of man-made fibers not only reflect these influences but they can be and commonly are varied to meet the requirements of use by suitable modifications in composition and manipulation of the fibers during production. These facts and the lack of strictly comparable data for all the principal fibers led to the decision to show in the tables the range in values of the properties reported in recent literature rather than selected values. The azlons, made from different proteins, are lumped together and so are the ordinary, medium, and high-tenacity rayons and the several varieties of resin fibers of each kind. References to literature giving more information and more detailed information are as follows:
Textile World's synthetic fiber table, 1949 rev., compiled by C. W. Bendigo, editor, Textile World, September 1949. Chemical engineering materials of construction, Ind. and Eng. Chem., 2d ed., vol. 40, p. 1773, 1948; 3d ed., vol. 41, p. 2091, 1949. Fiber properties chart-1948, Plastics Catalogue Corporation, New York. Smith, H. DeWitt, Textile fibers-an engineering approach to an understanding of their properties and utilization, Proc. Amer. Soc. Test. Mat., vol. 44, p. 543, 1944. A. S. T. M. standards on textile materials. Amer. Soc. Test. Mat., October 1949. Die Unterscheidung der Textilfasern, 2d ed., Verlag Leeman, Zurich, 1949. Morehead, F. F., Some comparative data on the cross-sectional swelling of textile fibers, Textile Res. Journ., vol. 17, p. 96, 1947. Preston, J. M., The temperature of contraction of fibers as an aid to identification, Journ. Textile Inst., vol. 40, p. T767, 1949. Abbott, N. J., and Goodings, A. C., Moisture absorption, density, and swelling properties of nylon filaments, Journ. Textile Inst., vol. 40, p. T232, 1949. Hutton, E. A., and Gartside, Joan, The moisture regain of silk, Journ. Textile Inst., vol. 40, p. T161, 1949. Hutton, E. A., and Gartside, Joan, The adsorption and desorption of water by nylon at $25^{\circ} \mathrm{C}$, Journ. Textile Inst., vol. 40, p. T170, 1949. MacMilian, W. G., Mukherjee, R. R., and Sen, M. K., The moisture relationships of jute, Journ. Textile Inst., vol. 37, p. T13, 1946. Albright, J. G., "Spider Silk," Science Teacher, October 1944.

* Prepared by W. D. Appel, of the National Bureau of Standards.
TABLE 233.-PHYSICAL PROPERTIES OF NATURAL FIBERS

|  | Cotton | Flax | Hemp | Jute | Ramie | Silk 8 | Wool |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Density ( $\mathrm{g} / \mathrm{cm}^{3}$ ) | 1.50-1.55 | 1.50 | 1.48 | 1.48 | 1.51 | 1.25-1.35 | 1.28-1.33 |
| Refractive index: ep | 1.573-1.581 | 1.594-1.596 | 1.585-1.591 | 1.577 | 1.595-1.599 | 1.591-1.595 | 1.553-1.556 |
|  | 1.529-1.534 | 1.528-1.532 | 1.526-1.530 | 1.536 | 1.527-1.540 | 1.538-1.543 | 1.542-1.547 |
| Tensile strength ( $1000 \mathrm{lb} / \mathrm{in} .^{2}$ ) . . . . . . . . . . . . . . . | 42-125 | $\ldots$ | ... | ... | ... | 45-83 | 15-28 |
| $\begin{aligned} & \text { Tenacity: dry }\left(\mathrm{g} / \text { denier }{ }^{*}\right) \\ & \text { wet (\% of dry) } \end{aligned}$ | 2.1-6.3 | $\ldots$ | ... | ... | ... | 2.9-5.2 | 1.0-1.7 |
|  | 110-130 | ... | ... | . $\cdot$ | . $\cdot$. | 75-95 | 76-97 |
| Elongation to break (\%)...................... . | 3-10 | $\ldots$ | . $\cdot$ | $\ldots$ | $\ldots$ | 13-31 | 20-50 |
| Recovery from strain |  |  |  |  |  |  |  |
| Elongation (\%)....................... . . . . . . . | 2 | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 2 | 2 |
| Recovery " . . . . . . . . . . . . . . . . . . . . . . . . . |  | . . . | ... | ... | . . | 92 | 99 |
| Elongation "، ........................ . . . . . . |  | . . . | ... | . . |  | 20 | 20 |
| Recovery " . . . . . . . . . . . . . . . . . . . . . . . . . |  | $\ldots$ | $\ldots$ | ... |  | 33 | 63 |
| Average stiffness ${ }^{\dagger}$ | 57 | 270 | 200 | 185 | 167 | 15 | 4 |
| Toughness index $\ddagger$ |  | 6 | 4 | 2 | 8 | 40 | 20 |
| Moisture regain at $65 \%$ R. H. and $70^{\circ} \mathrm{F}$ (\% of bone-dry weight) | $6.0-8.5$ | 7.0-8.5 | 8.0 | 10.6-13.6 | 6.0 | 8.1-15.5 | 13.0-16.2 |
| Swelling in water, cross-section swelling (\%)... | (8.-11. mer 21 | ized) | ... | . . . | 37 | 19 | 26 |
| Heat stability; temperature ${ }^{\circ} \mathrm{C}$ at or above which |  |  |  |  |  |  |  |
| fiber contracts |  |  |  |  |  | Does not contract | 240 |
| loses strength |  |  |  |  |  |  | 240 |
| softens |  |  | ... | . . |  |  |  |
| melts . . . decomposes |  |  |  |  |  |  |  |
| decomposes |  |  |  |  |  | chars | chars |
| * "Denier" is the weight in grams of 9,000 meters of the fiber. †The value for stiffness is a measure of the $\ddagger$ The toughness index is a measure of the ability of the fiber substance to absorb work. \& Spider silk has a de golden garden spider). |  |  |  |  |  |  |  |

TABLE 234.-PHYSICAL PROPERTIES OF RESIN AND RAYON FIBERS



[^109]

[^110]TABLE 237.-MECHANICAL PROPERTIES OF HARDWOODS GROWN IN UNITED STATES ${ }^{77}$

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|  |  | $\bigcirc$ | $\stackrel{\square}{\square}$ | $\stackrel{\infty}{\infty}$ | $\underset{\sim}{N}$ | $\begin{aligned} & \infty \\ & \underset{\sim}{i} \end{aligned}$ | $\stackrel{m}{i}$ | N | $\underset{\sim}{ \pm}$ | $\stackrel{W}{\mathrm{~N}}$ | $\begin{aligned} & \text { an } \\ & \end{aligned}$ | $\stackrel{8}{\gtrless}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\infty}{-1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { 気 } \\ & \text { 号 } \end{aligned}$ |  | 8, | $\begin{aligned} & \text { 옥 } \\ & =- \end{aligned}$ | 악 | $\frac{8}{i}$ | $\begin{aligned} & 0 \\ & \hline- \\ & \text { N } \end{aligned}$ | 8 | $\xrightarrow{8}$ | B | 욱 | $\stackrel{8}{\square}$ | $\stackrel{\infty}{\sim}$ | 앙 | 은 |
| $\stackrel{\sim}{3}$ |  | $\begin{aligned} & 8 \\ & 0 \\ & n \\ & n \end{aligned}$ | $\begin{aligned} & 8.8 \\ & 0 \\ & \text { on } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { Ni } \\ & \text { Nin } \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 6 \end{aligned}$ | $\begin{aligned} & 8 \\ & \frac{8}{0} \\ & \underline{0} \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{0}{8} \\ & 6 \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & n \\ & n \end{aligned}$ | $\stackrel{\circ}{\infty}$ | $\begin{aligned} & 8 \\ & \AA \\ & \pm \end{aligned}$ | $\frac{8}{\infty}$ | $\begin{aligned} & 8 \\ & \text { N } \\ & \text { O} \\ & 0 \end{aligned}$ | $\delta_{\infty}^{8}$ | প্ণী |







| Eit |  | oi | N | $8$ | Oㅇㅇ | $\underset{7}{8}$ | $\stackrel{8}{\mathrm{M}}$ | $\underset{i}{O}$ | $\begin{aligned} & \text { O} \\ & \text { O} \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline 1 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Ǹ } \end{aligned}$ | $\stackrel{8}{\circ}$ | 앙 | $\stackrel{\sim}{7}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \| |  | in | ì | $\underset{\sim}{\infty}$ | $\frac{8}{7}$ | $\underset{\sim}{\stackrel{~}{j}}$ | $\mathrm{N}_{\mathrm{N}}$ | $\stackrel{\infty}{\infty}$ |  | $\mathrm{m}_{2}$ | $\stackrel{6}{\nabla}$ | $\stackrel{\infty}{\infty}$ | $\underset{\sim}{0}$ | $8$ | $\begin{aligned} & \stackrel{8}{0} \\ & \underset{7}{2} \end{aligned}$ | $\frac{8}{\infty}$ |



|  |  | $\begin{aligned} & F \\ & \dot{m} \end{aligned}$ | $\stackrel{\sim}{\square}$ | $\stackrel{\infty}{\sim}$ | $\stackrel{\rightharpoonup}{\text { ¢ }}$ | 9 | $\stackrel{\sim}{\sim}$ | $\stackrel{\infty}{\circ}$ | $\stackrel{\text { ¢ }}{\text { ¢ }}$ | $\xrightarrow{\text { O}}$ | $\xrightarrow{\text { N}}$ | ¢ | $\underset{\sim}{7}$ |  | $\stackrel{\sim}{n}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| : |  | $\begin{aligned} & \text { 8 } \\ & \underset{\sim}{2} \end{aligned}$ | 읅 | $\begin{aligned} & \text { Ǹ } \\ & \underset{-}{2} \end{aligned}$ | $\stackrel{8}{\underset{\sim}{4}}$ | $\underset{\sim}{\mathrm{M}}$ | $\begin{aligned} & 8 \\ & \text { Ny } \end{aligned}$ | $\stackrel{\circ}{0}$ | in | $\xrightarrow{8}$ | $\xrightarrow{8}$ | - |  | $\stackrel{8}{4}$ | $\underset{\sim}{8}$ |  |





$\therefore$
Place of growth of
material tested

Common and botanical name Cherry, black (Prunus serotina) ............. Pa.
Cherry, pin
(Prunus pennsylvanica) ....... Tenn. Chestnut, American (Castanea dentata) (Castanopsis chro Dogwood, flowering
Dogwood, Pacific (Cornus nuttallii) Doveplum* Elder, blueberry* (Sambucus glauca)
Elm, American (Ulmus thomasi) Eucalyptus, bluegum
Calif.


Myinniulu







荡
Eugenia, redberry *
(Carya cordiformis)
Hickory, mockernut
Hickory, nutmeg
Hickory, nutmeg
(Carya myristic
Hickory, pignut
(Carya glabra)
Hickory, shagbark
(Carya ovata)
Hickory, shellbark
(Carya laciniosa)
Hickory, water ${ }^{*}$
(Carya aquatica)
Holly, American
(Ilex opaca)
Honeylocust



| $z^{*}$ ! $/ \mathrm{qI}$ <br>  <br>  <br>  | $\begin{aligned} & \text { on } \\ & \text { - } \end{aligned}$ | $\begin{aligned} & 0 \\ & \underset{\sim}{7} \\ & n \end{aligned}$ | $\begin{aligned} & \infty \\ & \underset{\sim}{\infty} \\ & \underset{N}{2} \end{aligned}$ | $\underset{\sim}{0}$ | $\begin{aligned} & 8 \\ & \stackrel{3}{7} \end{aligned}$ | $\begin{gathered} 8 \\ \text { in } \\ \end{gathered}$ | $\begin{aligned} & 8 \\ & \infty \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { © } \\ & \text { - } \\ & \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { B } \\ & 0 \\ & \sim \end{aligned}$ | $\underset{\sim}{\infty}$ | $\begin{aligned} & \text { N } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { or } \\ & \text { ñ } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| $\stackrel{5}{\omega}$ | $z^{\prime 4} / \mathrm{ql}$ <br> 7!u!l- 'u!e.y <br> 07 лe[nว!puadıad | $8$ | $\begin{aligned} & 8 \\ & 8 \\ & \text { N } \end{aligned}$ | $\begin{aligned} & 8 \\ & \infty \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 \\ & \cdots \\ & N \end{aligned}$ | $\begin{gathered} \underset{\sim}{6} \\ \underset{\sim}{n} \end{gathered}$ | \% | $8$ | $\begin{aligned} & \text { ® } \\ & \text { M } \end{aligned}$ | প্লু | $\begin{aligned} & 8 \\ & \stackrel{4}{4} \\ & \end{aligned}$ | $\stackrel{8}{\underset{N}{N}}$ | $\frac{0}{2}$ | $8$ | $\underset{\substack{0 \\ \hline \\ \hline \\ \hline \\ \hline}}{ }$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| E | $z^{*}$ U! / $q$ I ' 7 !u! $l^{-d}$ *u!es8 of [plened | $\begin{aligned} & \infty \\ & \substack{1 \\ 10} \end{aligned}$ | $\begin{aligned} & \text { M } \\ & \text { M } \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{\sim}{8} \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & \infty \\ & 0 \\ & 0^{0} \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 8 \end{aligned}$ | - | $\begin{aligned} & \underset{\sim}{\mathrm{M}} \\ & \text { M } \end{aligned}$ | $8$ | \& | $$ | 8 8 +8 | 8 $\sim$ $\sim$ |  | $\begin{aligned} & R \\ & \text { R } \\ & \text { in } \end{aligned}$ |








z. 4 /qI

|  unulxeus : Lieds of ュе!nכ!puəd.ad uo!sual | ถু |  | 8 | $\stackrel{\gtrless}{\wedge}$ |  |  |  | 8 | - | 8 | $\underset{\infty}{\infty}$ | 앙 | $\stackrel{\sim}{8}$ | $\stackrel{\circ}{\infty}$ | is |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  unuixem :ules <br>  | $\begin{aligned} & \text { O} \\ & \text { N } \end{aligned}$ | $\underset{\sim}{0}$ | - | $\stackrel{8}{\square}$ | c N | $\xrightarrow{8}$ |  | - | $\begin{aligned} & 8 \\ & 8 \\ & i \end{aligned}$ | $\stackrel{8}{1}$ | $\begin{aligned} & \text { O} \\ & \text { Ni } \end{aligned}$ | N | $\stackrel{?}{\infty}$ | 8 0 -1 | \% |
|  | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~N} \\ & \end{aligned}$ | $\begin{aligned} & 9 \\ & \underset{7}{7} \end{aligned}$ | $\begin{aligned} & \stackrel{8}{\infty} \\ & \underset{\sim}{2} \end{aligned}$ | $\underset{\sim}{\mathcal{F}}$ | $\begin{aligned} & 8 \\ & \text { N } \\ & \text { N } \end{aligned}$ | $\underset{i}{\text { G }}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \end{aligned}$ | $\stackrel{0}{2}$ | $\frac{0}{n}$ | $\xrightarrow{\text { ¢ }}$ | $\begin{aligned} & 0 \\ & \cdots \end{aligned}$ | 8 <br>  | \% | $\stackrel{8}{\sim}$ | - |
|  | $\begin{aligned} & \text { ion } \\ & \text { m} \end{aligned}$ | $\begin{aligned} & \text { 융 } \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{0}{n} \\ & \end{aligned}$ | $\begin{aligned} & \text { ®} \\ & \text { m } \end{aligned}$ | $\frac{0}{6}$ | $\begin{aligned} & \stackrel{\sim}{\mathrm{Y}} \\ & \underset{\sim}{n} \end{aligned}$ |  | $\begin{aligned} & \text { O} \\ & \text { } \\ & \text { f } \end{aligned}$ | - | $\begin{aligned} & \infty \\ & \infty \\ & \underset{\sim}{m} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{2} \\ & \hline \end{aligned}$ | ¢ | $\begin{aligned} & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { n } \\ & \text { n } \end{aligned}$ | $\begin{aligned} & 0 \\ & \text { No } \end{aligned}$ |


|  | z $4!/ q 1$ '\}!u!! ${ }^{\text {d }}$ | $\begin{aligned} & 8 \\ & 0 \\ & \infty \\ & \infty \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { g } \\ & \text { 寸 } \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & \infty \\ & \infty \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & 8_{0} \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{\sim}{8} \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{\sim}{8} \\ & \text { - } \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{N}{7} \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & \stackrel{y}{2} \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & = \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { N } \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & \end{aligned}$ | $\begin{aligned} & 8 \\ & 6 \\ & 6 \end{aligned}$ | 8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |









TABLE 237.-MECHANICAL PROPERTIES OF HARDWOODS GROWN IN UNITED STATES (continued)

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| $\underset{4}{\infty} \underset{\sim}{\infty} \underset{\sim}{\infty} \underset{\sim}{\infty} \underset{\sim}{\infty} \underset{\sim}{\infty} \underset{\sim}{\infty} \underset{\sim}{\infty} \underset{\sim}{\infty}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
|  |  |  |  |  |











Place of growth of
material tested


$$
\stackrel{F}{\square}: ~: ~
$$

                    Ind., Tenn
                                    Tenn.
    La., Mo. Ky．
Ariz．
Mo．，Wis．
Oreg．
Tenn．
Ky．，Tenn．
TABLE 238.-MECHANICAL PROPERTIES OF SOFT WOODS GROWN IN UNITED STATES**


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TABLE 238.-MECHANICAL PROPERTIES OF SOFT WOODS GROWN IN UNITED STATES (continued)

| . | $z^{\cdot 41 / q 1}$ ) ів | O | OB | $\underset{\sim}{2}$ | $8$ | $\stackrel{\circ}{\circ}$ | in | $8$ | $8$ | $\stackrel{\stackrel{N}{N}}{ }$ | $\underset{\sim}{\infty}$ | $\stackrel{i}{n}$ | $\stackrel{8}{\square}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{0}^{E}$ |  | $\begin{aligned} & \mathbb{O} \\ & \underset{\sim}{2} \end{aligned}$ | $\stackrel{\rightharpoonup}{3}$ | $\stackrel{\substack{\mathrm{N}}}{\underset{\sim}{1}}$ |  | $\begin{aligned} & \underset{O}{0} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \stackrel{Q}{6} \\ & \text { n } \end{aligned}$ | $\begin{aligned} & \underset{\infty}{2} \\ & \underset{N}{2} \end{aligned}$ |  |  | $\begin{gathered} \circ \\ \substack{\infty \\ +} \end{gathered}$ | $\stackrel{\stackrel{\rightharpoonup}{\mathrm{m}}}{\underset{\sim}{2}}$ | $\frac{8}{6}$ |




*イ!

(continued)

Meager data, may not be fully representative of species. Common and botanical name
Hemlock, mountain
(Tsuga mertensiana) ..
Hemlock, western Incense-cedar, California (Libocedrus decurrens)
Juniper
Larch, western
Pine, eastern white
(Pinus strobus)
Pine, jack
(Pinus bon
Pine, Jeff rey
Pine, limber *
(Pinus flexilis)
Pine, loblolly
(Pimus taeda)
Pine, lodgepole
Pine, longleaf
(Pimus palustris)
Pine, pitch
(Pinus rigida)

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 $\begin{aligned} & \text { Place of growth of } \\ & \text { material tested }\end{aligned}$
Mont., Alaska, Wash.
Calif.
Calif.
Calif.
N. H.
Mont., Idaho, Colo.
Tenn., N. H.
Wash., Alaska, Oreg.
N. H., Alaska, Wis.
Wis.
N. H., N. C.
Wis.
Wash.

TABLE 239.-DENSITY IN g/cm ${ }^{3}$ AND IN Ib/ft ${ }^{3}$ OF DIFFERENT KINDS OF WOOD

Wood is to be seasoned and of average dryness. Sec also Tables 237 and 238.

| Wood | $\mathrm{g} / \mathrm{cm}^{3}$ | $\mathrm{lb} / \mathrm{ft}^{3}$ | Wood | $\mathrm{g} / \mathrm{cm}^{3}$ | 1b $/ \mathrm{ft}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Alder | . $42-.68$ | 26-42 | Lancewood | .68-1.00 | 42-62 |
| Apple | .66-. 84 | 41-52 | Lignum vitae | 1.17-1.33 | 73-83 |
| Ash | .65-. 85 | 40-53 | Linden or lime-tree. | . $32-.59$ | 20-37 |
| Balsa | <Cork |  | Locust | .67-. 71 | 42-44 |
| Bamboo | . $31-.40$ | 19-25 | Log wood | . 91 | 57 |
| Basswood |  |  | Mahogany, Honduras. | . 65 | 41 |
| (See Linden) |  |  | Mahogany, Spanish | . 85 | 53 |
| Bcech | . $70-.90$ | 43-56 | Maple | .62-. 75 | 39-47 |
| Birch | . $51-.77$ | 32-48 | Oak . | .60-. 90 | 37-56 |
| Plue gum | 1.00 | 62 | Pear-tree | . $61-.73$ | 38-45 |
| Box . | .95-1.16 | 59-72 | Pine, eastern white | . $35-.50$ | 22-31 |
| Bullet-tree | 1.05 | 65 | Pine, larch . ...... | . $50-.56$ | 31-35 |
| Butternut | . 38 | 24 | Pine, pitch | . $83-.85$ | 52-53 |
| Cedar | . $49-.57$ | 30-35 | Pine, red. | . $48-.70$ | 30-44 |
| Cherry | . $70-.90$ | 43-56 | Pinc, Scotch | .43-. 53 | 27-33 |
| Cork | .22-. 26 | 14-16 | Pine, spruce | . 48 - . 70 | 30-44 |
| Dogwood | . 76 | 47 | Pine, yellow | . $37-.60$ | 23-37 |
| Ehony | 1.11-1.33 | 69-83 | Plum-tree . | . $66-.78$ | 41-49 |
| Elin . | . $54-.60$ | 34-37 | Poplar . | . $35-.5$ | 22-31 |
| Greenheart | .93-1.04 | 58-65 | Satinwood | . 95 | 59 |
| Hazel | . $60-.80$ | 37-49 | Sycamore | . $40-.60$ | 24-37 |
| Hickory | . $60-.93$ | 37-58 | Teak, African | . 98 | 61 |
| Holly | . 76 | 47 | Teak, Indian | . $66-.88$ | 41-55 |
| Iron-bark | 1.03 | 64 | Walnut .... | . $64-.70$ | 40-43 |
| Juniper | . 56 | 35 | Water gum |  |  |
| Laburnum | . 92 | 57 | Willow . . . . . . . . . | . $40-.60$ | 24-37 |

## TABLE 240.-DENSITY $\left(\mathrm{g} / \mathrm{cm}^{3}\right)$ OF SOME FOREIGN WOODS ON THE AMERICAN MARKET*

| Almon | . 464 | Olive | . 94 |
| :---: | :---: | :---: | :---: |
| Balsa | . 11 | Orangewood | . 70 |
| Boxwood, West Indian | .83-. 88 | Padouk . . . | .89-1.29 |
| Bullet-wood, Guiana | 1.03-1.23 | Prima vera | . 58 |
| Carreto | . 84 | Purple-heart | .72-. 97 |
| Cedar, Spanish | . 38 | Quebracho | 1.25 |
| Cocobola | 1.20 | Rosewood, Brazil | .77-. 84 |
| Cocus | 1.25 | Rosewood, Honduras | 1.09-1.23 |
| Fustic | . 68 | Sabicu | .90-. 96 |
| Koa | . 83 | Snakewood | 1.05-1.33 |
| Lauaan, red | . 41 | Tamarind | 1.32 |
| Mahogany, African | . 55 | Tanguile | . $47-.51$ |
| Mahogany, E. Indian. | . 38 | Wallaba | .93-. 94 |
| Mora | 1.07-1.09 | Zebrawood | 1.03 |
| Oak, English | .60-. 78 |  |  |

[^111]
## TABLES 241-253.-TEMPERATURE, PRESSURE, VOLUME, AND WEIGHT RELATIONS OF GASES AN゚D VAIORS

## TABLE 241.-SIMPLE GAS LAWS

Any amount of gas completely fills the space in which it is confined. The pressure it exerts upon the confining walls depends upon the temperature. A quantity of gas can not be specified by volume only; all three factors-volume, temperature, and pressuremust be stated. The relations between these three factors are expressed by means of the following equation,

$$
\begin{equation*}
p v=K T \tag{1}
\end{equation*}
$$

in which $p, v$, and $T$ represent simultaneous values of the pressure, volume, and absolute temperature of any definite quantity of gas, while $K$ is a constant, the numerical value of which depends upon the quantity of gas considered and the units in which pressure, volume, and temperature are measured.

While the behavior of gases at atmospheric pressure closely approximates the equation (1), the relation is not exact. The expansion of air is nearer one-272d of its volume at $273.16^{\circ} \mathrm{K}$ per degree. For most practical purposes such errors may be neglected.

If we take weights of gases proportional to their molecular weights, a new relation of the greatest importance develops: The zalue of the constant in equation (1) is the same for cach gas. It is customary to use as the unit of quantity, the mol, the number of grams of gas equal to the molecular weight. When 1 mol is the quantity considered, the resulting value of $K$ is designated $R$.

Values of $R$ in $P V=R T$ for one mol of ideal gas. -1 bar $=10^{6}$ dyne $/ \mathrm{cm}^{2}=0.987$ atm. $1 \mathrm{~kg} / \mathrm{cm}^{2}=0.968 \mathrm{~atm}$. Gram molar volume of ideal gas at $0^{\circ} \mathrm{C}=22,414.1 \mathrm{~cm}^{3}$. Pound molar volume of ideal gas at $32^{\circ} \mathrm{F}=359.05 \mathrm{ft}^{3}$. Ice point, $0^{\circ} \mathrm{C}=273.16^{\circ} \mathrm{K}$; $32^{\circ} \mathrm{F}=491.7^{\circ} \mathrm{R} . \quad 1$ liter $=1000.027 \mathrm{~cm}^{3}$.


With the mol the unit of quantity, $N$ the number of mol of gas, equation (1) becomes

$$
\begin{equation*}
p z^{\prime}=N R T \tag{2}
\end{equation*}
$$

By the use of equation (2), the above table, and a table of molecular weights, the solution of any problem involving volumes, tempcratures, pressures, and weights of gases is very simple.

Mixtures of gases.-Any quantity of gas fills the space in which it is confined and exerts a pressure upon the confining walls. If an additional quantity is added, the pressure is increased in direct proportion to the quantity added. One can regard the pressure exerted by each portion of the total quantity of gas as independent of the presence of the rest. This is true if the second portion of gas is different chemically from the first (Dalton's law), provided the gases do not react chemically.
(continued)

Vapor pressure and the effect of vapor pressure upon the measurement of gas.If a volatile liquid is introduced, a portion evaporates and exerts a pressure on the confining walls. The amount evaporated and the pressure exerted are independent of the presence of any other gas. If there is enough so that not all evaporates and if time is allowed for equilibrium, the pressure is independent of the volume of space and of the amount of liquid left unevaporated; but it does depend upon the temperature. For each volatile liquid there is therefore a definite saturation pressure or vapor pressure corresponding to every temperature. See Tables $360-369$.

When any gas is in contact with a volatile substance, the measured pressure is the pressure exerted by the gas plus the vapor pressure of the volatile material. With no change of temperature, this vapor pressure remains constant no matter how we change the total pressure. Hence for the purposes of volume conversion the saturated gas may be considered as a dry gas, the pressure of which is the partial pressure of the gas, or its equivalent, the difference between the total pressure and the saturated vapor pressure of the volatile material.

## TABLE 242.-VOLUME CONVERSIONS, FACTOR Z, FOR HIGH PRESSURES*

In the measurement of gases at high pressures the quantity $P V$ is no longer constant at constant temperature but varies with the pressure by amounts that differ for each gas. Consequently the relation $\frac{P_{1} V_{1}}{R T_{1}}=\frac{P_{2} V_{2}^{\prime}}{R T_{2}}$ no longer holds. As a correction factor, $Z=\frac{P V}{R T}$ is given for different values of some one or more of the variables. The values of $Z$ for different gases as given in the table are for different pressures and temperatures. The values extend to pressures of $100-200 \mathrm{~atm}$ and to temperatures of $200^{\circ} \mathrm{C}$. Values of this factor of hydrogen for temperatures ranging from $16^{\circ} \mathrm{K}$ to $600^{\circ} \mathrm{K}$ and for pressures ranging from a small fraction of an atmosphere (.01) to 100 atm are given in Table 254, Part 2. ${ }^{73}$ The value of this factor can be calculated for a wide range of pressures using the data given in some of the following tables.
This tables gives values of volume correcting factor $\mathrm{Z}(\mathrm{V}=1$ at 1 atm pressure and $0^{\circ} \mathrm{C}$ ).

|  | $\underbrace{\text { - ir }}$ |  |  |  |  | Argon |  |  |  | $\begin{aligned} & \text { Neon } \\ & 0^{\circ} \mathrm{C} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Atm | $0^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $100^{\circ} \mathrm{C}$ | $200^{\circ} \mathrm{C}$ |  | $0^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $100^{\circ} \mathrm{C}$ | $200^{\circ} \mathrm{C}$ |  |  |
| 10 | . 9952 | . 9997 | 1.0021 | 1.00 |  | . 9921 | . 9973 | 1.0000 | 1.0023 | 1.0045 |  |
| 25 | . 9877 | . 9987 | 1.0044 | 1.00 |  | . 9784 | . 9918 | . 9984 | 1.0044 |  | 0119 |
| 50 | . 9782 | . 9996 | 1.0100 | 1.01 |  | . 9577 | . 9842 | . 9971 | 1.0084 |  | 0235 |
| 75 | . 9722 | 1.002 | 1.0191 | 1.02 |  | . 9403 | . 9783 | . 9971 | 1.0138 |  | 0358 |
| 100 | . 9712 | 1.0077 | 1.0253 | 1.03 |  | . 9262 | . 9746 | . 9990 | 1.0197 |  | .0492) |
|  | Helium |  |  | Hydrogen |  |  |  | Oxygen |  |  |  |
| Atm | $0^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $100^{\circ} \mathrm{C}$ | $0^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $100^{\circ} \mathrm{C}$ | $200^{\circ} \mathrm{C}$ | $0^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | 100 C |
| 10 | 1.0050 | 1.0042 | 1.0035 | 1.0062 | 1.0056 | 1.0051 | 1.0042 | . 9908 | . 9933 | . 9965 | . 9993 |
| 25 | 1.0129 | 1.0108 | 1.0092 | 1.0156 | 1.0141 | 1.0127 | 1.0105 | . 9771 | . 9835 | . 9908 | . 9980 |
| 50 | 1.0260 | 1.0218 | 1.0185 | 1.0316 | 1.0285 | .1.025.5 | 1.0209 | . 9562 | . 9685 | . 9831 | . 9968 |
| 75 | 1.0392 | 1.0329 | 1.0279 | 1.0480 | 1.0429 | 1.0384 | 1.0315 | . 9378 |  | . 9771 | . 9971 |
| 100 | 1.0524 | 1.0440 | 1.0372 | 1.0646 | 1.0575 | 1.0514 | 1.0419 | . 9231 | - | . 9733 | . 9983 |
| 200 | - | - | - | 1.1333 | 1.1168 | 1.1036 | 1.0839 | . | - | - |  |
|  |  | Nitrogen |  |  | Meth | hane |  |  |  |  |  |
| Atm | $0^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $100^{\circ} \mathrm{C}$ | $0^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $100^{\circ} \mathrm{C}$ | $200^{\circ} \mathrm{C}$ |  |  |  |  |
| 10 | . 9975 | 1.0015 | 1.0035 | . 978 | . 989 | . 993 | . 999 |  |  |  |  |
| 50 | . 9835 | 1.0035 | 1.0125 | . 883 | . 941 | . 971 | . 997 |  |  |  |  |
| 100 | . 9835 | 1.0145 | 1.0295 | . 781 | . 896 | . 951 | . 998 |  |  |  |  |
| 150 | 1.0015 | 1.0385 | 1.0546 | (.730) | . 873 | . 943 | 1.004 |  |  |  |  |
| 200 | - | 1.0686 | 1.0836 |  | . 873 | .950 | 1.020 |  |  |  |  |

[^112]
## TABLE 243.-RELATIVE GAS VOLUMES AT VARIOUS PRESSURES

(Deduced by Cochrane, from the $p v$ curves of Amagat and other observers.)
Relative volumes when the pressure is reduced from the value given at the head of the column to 1 atmosphere; see also Nat. Bur. Standards Circ. 279.

| $\left(\mathrm{Temp} . \underset{=}{\mathrm{Gas}}=16^{\circ} \mathrm{C}\right)$ | Relative vo'ume the gas will occupy when the pressure is reduced to atmospheric from |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 atm | $\overline{50 \mathrm{~atm}}$ | 100 atm | 120 atm | 150 atm | 200 atm |
| "Perfect" gas | 1 | 50 | 100 | 120 | 150 | 200 |
| Helium . |  |  | 94.6 | 112.5 | 141 |  |
| Hydrogen | 1 | 48.5 | 93.6 | 111.3 | 136.3 | 176.4 |
| Nitrogen | 1 | 50.5 | 100.6 | 120.0 | 147.6 | 190.8 |
| Air | 1 | 50.9 | 101.8 | 121.9 | 150.3 | 194.8 |
| Argon |  |  | 106.3 | 127.6 | 161 |  |
| Oxygen |  |  | 105.2 |  |  | 212.6 |
| Oxygen (at $0^{\circ} \mathrm{C}$ ). |  | 52.3 | 107.9 | 128.6 | 161.9 | 218.8 |
| Carbon dioxide | 1 | 69 | 477* | 485* | 498* | 515* |
| * Carbon dioxide is liquid at pressures greater than 90 atmospheres. |  |  |  |  |  |  |

## TABLE 244.-VAN DER WAAL'S CONSTANTS FOR IMPERFECT GASES ${ }^{\circ}$

Van der Waal developed an equation to represent the pressure, temperature, and volume relation of a real gas. One form of this equation is

$$
\begin{aligned}
{\left[P+a\left(\frac{u}{V}\right)^{2}\right](V-n b) } & =n R t \\
n & =\text { number of molecules } \\
(V-n b) & =\text { effective volurre } \\
a & =\text { internal pressure constant }\left[\left(\text { dynes } / \mathrm{cm}^{2}\right) \times\left(\mathrm{cm}^{3} / \mathrm{mol}\right)\right] \\
b & =\text { reduction in effective volume }(V) \mathrm{per} \text { molecule }\left(\mathrm{cm}^{3} / \mathrm{mol}\right)
\end{aligned}
$$

$P$ (dynes $/ \mathrm{cm}^{2}$ ) $, V\left(\mathrm{~cm}^{3} / \mathrm{mol}\right), R$, and $T$ have their usual meanings.
The value of these constants ( $a$ and $b$ ) for various gases are given in the table. If Van der Waal's equation were correct, $V_{c} / 3=b$ ( $V_{c}$ critical volume).

[^113]TABLE 244.-VAN DER WAAL'S CONSTANTS FOR IMPERFECT GASES (concluded)

| Gas | Formula | ${ }^{\text {a }}$ | $b$ | l'c/3 | Molecular volume of volume or liquid rquid | Electric moments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Neon | Ne | $0.21 \times 10^{12}$ | 17.1 | 14.7 | 16.7 | $0 \times 10^{-18}$ |
| Helium | He | . 035 | 23.6 | 20.5 | 27.4 |  |
| Hydrogen | $\mathrm{H}_{2}$ | 0.25 | 26.5 | 21.6 | 26.4 | 0 |
| Nitric oxide | NO | 1.36 | 27.8 | 19.1 | 23.7 |  |
| Water ... | $\mathrm{H}_{2} \mathrm{O}$ | 5.53 | 30.4 | 18.9 | 18.0 | 1.85 |
| Oxygen |  | 1.40 | 32.2 | 24.8 | 25.7 |  |
| Argon |  | 1.36 | 32.2 | 26.1 | 28.1 | 0 |
| Ammonia | $\mathrm{NH}_{3}$ | 4.22 | 36.9 | 24.2 | 24.5 | 1.44 |
| Nitrogen | $\mathrm{N}_{2}$ | 1.36 | 38.3 | 30.0 | 32.8 |  |
| Carbon monoxide | CO | 1.50 | 39.7 | 30.0 | 32.7 | 0.10 |
| Krypton | Kr | 2.35 | 39.7 | 36.0 | 38.9 |  |
| Hydrogen chloride | HCl | 3.72 | 40.7 | 29.8 | 30.8 | 1.03 |
| Nitrous oxide .... | $\mathrm{N}_{2} \mathrm{O}$ | 3.61 | 41.1 | 32.3 | 44.0 | . 25 |
| Carbon dioxide | $\mathrm{CO}_{2}$ | 3.64 | 42.5 | 32.8 | 41.7 |  |
| Methane | $\mathrm{CH}_{4}$ | 2.28 | 42.6 | 32.9 | 49.5 | 0 |
| Hydrogen sulfide | $\mathrm{H}_{2} \mathrm{~S}$ | 4.49 | 42.7 |  | 35.4 | . 93 |
| Hydrogen bromide | HBr | 4.51 | 44.1 |  | 37.5 | . 78 |
| Xenon ............ |  | 4.15 | 50.8 | 38.0 | 47.5 | . |
| Acetylene | $\mathrm{C}_{2} \mathrm{H}_{2}$ | 4.43 | 51.3 | 37.5 | 50.2 | , |
| Phosphine | $\mathrm{PH}_{3}$ | 4.69 | 51.4 | 37.7 | 49.2 | . 55 |
| Chlorine | $\mathrm{Cl}_{2}$ | 6.57 | 56.0 | 41.0 | 41.2 |  |
| Sulfur dioxide | $\mathrm{SO}_{2}$ | 6.80 | 56.1 | 41.0 | 43.8 | 1.61 |
| Ethylene | $\mathrm{C}_{2} \mathrm{H}_{4}$ | 4.46 | 56.1 | 42.3 | 49.3 | 0 |
| Silicon hydride | $\mathrm{SiH}_{4}$ | 4.38 | 57.6 |  | 47 | 0 |
| Methylamine | $\mathrm{CH}_{3} \mathrm{NH}_{2}$ | 7.23 | 59.6 |  | 44.5 | 1.31 |
| Fthane .... | $\mathrm{CH}_{3}-\mathrm{CH}_{3}$ | 5.46 | 63.5 | 47.6 | 54.9 |  |
| Methyl alcohol | $\mathrm{CH}_{3} \mathrm{OH}$ | 9.65 | 66.8 | 39.0 | 40.1 | 1.73 |
| Methyl chloride | $\mathrm{CH}_{3} \mathrm{Cl}$ | 7.56 | 64.5 | 45.4 | 49.2 | 1.97 |
| Methyl ether .... | $\left(\mathrm{CH}_{3}\right)_{2} \mathrm{O}$ | 8.17 | 72.2 |  |  | 1.29 |
| Carbon bisulfide |  | 11.75 | 76.6 | 67.5 | 59.0 |  |
| Dimethylamine | $\left(\mathrm{CH}_{3}\right)_{2} \mathrm{NH}$ | 9.77 | 79.6 |  | 66.2 |  |
| Propylene ... | $\mathrm{C}_{3} \mathrm{H}_{6}$ | 8.49 | 82.4 |  | 69.0 | 0 |
| Ethyl alcohol | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{OH}$ | 12.17 | 83.8 | 41.0 | 57.2 | 1.63 |
| Propane .... | $\mathrm{CH}_{3}-\mathrm{CH}_{2}-\mathrm{CH}_{3}$ | 8.77 | 84.1 |  | 75.3 |  |
| Chloroform | $\mathrm{CHCl}_{3}$ | 15.38 | 102 | 77.1 | 80.2 | 1.05 |
| Acetic acid | $\mathrm{CH}_{3} \mathrm{COOH}$ | 17.81 | 106 | 57.0 | 56.1 |  |
| Trimethylamine | $\left(\mathrm{CH}_{3}\right)_{3} \mathrm{~N}$ | 13.20 | 108 |  | 89.3 |  |
| iso-Butane .... | $\mathrm{CH}\left(\mathrm{CH}_{3}\right)_{3}$ | 13.10 | 114 |  | 96.3 |  |
| Benzene. | $\mathrm{C}_{6} \mathrm{H}_{0}$ | 18.92 | 120 | 85.5 | 86.7 |  |
| n-Butane | $\mathrm{CH}_{3}\left(\mathrm{CH}_{2}\right)_{2} \mathrm{CH}_{3}$ | 14.66 | 122 |  | 96.5 | 0 |
| Ethyl ether | $\left(\mathrm{C}_{3} \mathrm{H}_{5}\right)_{2} \mathrm{O}$ | 17.60 | 134 | 94.0 | 100 | 1.2 |
| Triethylamine | $\left(\mathrm{C}_{3} \mathrm{H}_{5}\right)_{3} \mathrm{~N}$ | 27.5 | 183 |  | 139 |  |
| Naphthalene | ${ }_{\text {Cin }} \mathrm{H}_{8}$ | 40.3 | 193 |  | 112 | . 69 |
| n-Octane ${ }_{\text {Decane }}$ |  | 37.8 49.1 | 236 289 | 162 | 162 |  |
| Decane | $\mathrm{CH}_{3}\left(\mathrm{CH}_{2}\right)_{x} \mathrm{CH}_{3}$ | 49.1 | 289 |  | 195 | 0 |

TABLE 245.-CORRECTING FACTORS: SATURATED GAS VOLUME TO VOLUME AT 760 mmHg AND $0^{\circ} \mathrm{C}$ *
Multiply observed volumes of saturated gas by factor to correct to volume of dry gas at .760 mmHg pressure $\left(0^{\circ} \mathrm{C}\right)$

| Tem-pera- | Pressure mmHg |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\left({ }^{\circ} \mathrm{C}\right.$ ) | 715 | 720 | 725 | 730 | 735 | 740 | 745 | 750 | 755 | 760 | 765 | 770 |
| $5^{\circ}$ | . 916 | . 922 | . 928 | . 935 | . 942 | . 948 | . 954 | . 961 | . 967 | . 974 | . 980 | 986 |
| 6 | . 912 | . 918 | . 924 | . 931 | . 937 | . 944 | . 950 | . 957 | . 963 | . 970 | . 976 | . 982 |
| 7 | . 908 | . 914 | . 920 | . 927 | . 933 | . 940 | . 946 | . 952 | . 959 | . 965 | . 972 | . 978 |
| 8 | . 904 | . 910 | . 916 | . 923 | . 929 | . 936 | . 942 | . 948 | . 955 | . 961 | . 967 | . 974 |
| 9 | . 900 | . 906 | . 912 | . 919 | . 925 | . 932 | . 938 | . 944 | . 951 | . 957 | . 963 | . 970 |
| 10 | . 896 | . 902 | . 908 | . 915 | . 921 | . 928 | . 934 | . 940 | . 946 | . 953 | . 959 | . 966 |
| 11 | . 892 | . 898 | . 904 | . 911 | . 917 | . 924 | . 920 | . 936 | . 942 | . 949 | . 955 | . 962 |
| 12 | . 888 | . 894 | . 900 | . 907 | . 913 | . 919 | . 925 | . 932 | . 939 | . 945 | . 951 | . 957 |
| 13 | . 884 | . 890 | . 896 | . 903 | . 909 | . 915 | . 921 | . 928 | . 934 | . 940 | . 947 | . 953 |
| 14 | . 880 | . 886 | . 892 | . 899 | . 905 | . 911 | . 917 | . 924 | . 930 | . 936 | . 942 | . 949 |
| 15 | . 876 | . 882 | . 888 | . 895 | . 901 | . 907 | . 913 | . 920 | . 925 | . 932 | . 938 | . 944 |
| 16 | . 872 | . 878 | . 884 | . 890 | . 896 | . 903 | . 939 | . 915 | . 921 | . 928 | . 934 | . 940 |
| 17 | . 868 | . 874 | . 880 | . 886 | . 892 | . 898 | . 905 | . 911 | . 917 | .923 | . 929 | . 936 |
| 18 | . 864 | . 870 | . 875 | . 882 | . 888 | . 894 | . 900 | . 907 | . 913 | . 919 | . 925 | . 931 |
| 19 | . 859 | . 865 | . 871 | . 878 | . 884 | . 890 | . 896 | . 902 | . 908 | .915 | . 920 | . 927 |
| 20 | . 855 | . 861 | . 867 | . 874 | . 879 | . 886 | . 892 | . 898 | . 904 | . 910 | . 916 | . 922 |
| 21 | . 851 | . 857 | . 863 | . 869 | . 875 | . 881 | . 887 | . 893 | . 899 | . 906 | . 912 | . 918 |
| 22 | . 847 | . 853 | . 858 | . 865 | . 871 | . 877 | . 883 | . 888 | . 894 | .901 | . 907 | . 913 |
| 23 | . 842 | . 848 | . 854 | . 860 | . 866 | . 872 | . 878 | . 884 | . 890 | . 897 | . 903 | . 909 |
| 24 | . 838 | . 844 | . 849 | . 856 | . 862 | . 868 | . 874 | . 880 | . 886 | . 892 | . 898 | . 904 |
| 25 | . 833 | . 839 | . 845 | . 851 | . 857 | . 863 | . 869 | . 875 | . 881 | . 888 | . 893 | . 899 |
| 26 | . 829 | . 835 | . 841 | . 847 | . 853 | . 859 | . 865 | . 871 | . 877 | . 883 | . 889 | . 895 |
| 27 | . 824 | . 830 | . 836 | . 842 | . 848 | . 854 | . 860 | . 866 | . 872 | . 878 | . 884 | . 890 |
| 28 | . 820 | . 825 | . 831 | . 837 | . 843 | . 849 | . 855 | . 861 | . 867 | . 873 | . 879 | . 885 |
| 29 | . 815 | . 821 | . 826 | . 832 | . 838 | . 844 | . 850 | . 856 | . 862 | . 868 | . 874 | . 880 |
| 30 | . 810 | . 816 | . 822 | . 828 | . 833 | . 840 | . 845 | . 851 | . 857 | . 863 | . 869 | . 875 |
| 31 | . 805 | . 811 | . 817 | . 823 | . 829 | . 835 | . 840 | . 846 | . 852 | . 858 | . 864 | . 870 |
| 32 | . 800 | . 806 | . 812 | . 818 | . 823 | . 830 | . 835 | . 841 | . 847 | . 853 | . 859 | . 865 |
| 33 | . 795 | . 801 | . 807 | . 813 | . 818 | . 824 | . 830 | . 836 | . 842 | . 848 | . 853 | . 860 |
| 34 | . 790 | . 796 | . 801 | . 807 | . 813 | . 819 | . 825 | . 831 | . 837 | . 842 | . 848 | . 854 |
| 35 | . 785 | . 790 | . 796 | . 802 | . 808 | . 814 | . 819 | . 825 | . 831 | . 837 | . 843 | . 849 |
| 36 | . 780 | . 785 | . 791 | . 797 | . 802 | . 808 | . 814 | . 820 | . 826 | . 832 | . 836 | . 843 |
| 37 | . 774 | . 780 | . 785 | . 791 | . 797 | . 803 | . 809 | . 814 | . 820 | .826 | . 832 | . 838 |
| 38 | . 769 | . 774 | . 780 | . 786 | . 791 | . 796 | . 803 | . 809 | . 814 | . 820 | . 826 | . 832 |
| 39 | . 763 | . 768 | . 774 | . 780 | . 785 | . 790 | .797 | . 803 | . 809 | . 814 | . 820 | . 826 |
| 40 | . 756 | . 763 | . 768 | . 774 | . 780 | . 786 | . 792 | . 797 | . 803 | . 809 | . 814 | . 820 |
| 41 | . 751 | . 757 | . 762 | . 768 | . 774 | . 780 | . 786 | . 791 | . 797 | . 803 | . 808 | . 814 |
| 42 | . 745 | . 751 | . 756 | . 762 | . 768 | . 774 | . 779 | . 785 | . 791 | . 796 | . 802 | . 808 |
| 43 | . 739 | . 745 | . 750 | . 756 | . 762 | . 767 | . 773 | . 779 | . 784 | . 790 | . 796 | . 802 |
| 44 | . 733 | . 738 | . 744 | . 750 | . 755 | . 761 | . 766 | . 772 | . 778 | . 784 | . 789 | 795 |
| 45 | . 726 | . 732 | . 737 | . 743 | . 749 | . 754 | . 760 | . 766 | . 771 | . 777 | . 783 | 788 |
| 46 | . 720 | . 725 | . 731 | . 737 | . 742 | . 748 | . 754 | . 759 | . 765 | . 770 | . 776 | . 782 |
| 47 | . 713 | . 719 | . 724 | . 730 | . 735 | . 741 | . 746 | . 752 | . 758 | . 764 | . 769 | . 775 |
| 48 | . 706 | . 712 | . 717 | . 723 | . 728 | . 734 | . 739 | . 745 | . 751 | . 756 | . 762 | 768 |
| 49 | . 700 | . 705 | . 710 | . 716 | . 721 | . 727 | . 732 | . 738 | . 744 | . 750 | . 755 | 761 |

[^114]Part 1.-Ordinary temperatures
As a measure of the compressibility, it is customary to use a coefficient, $1+\lambda=p_{1} v_{0} / p_{1} v_{1}, p_{0} v_{0}$ being at $0^{\circ} \mathrm{C}$.

| $\mathrm{H}_{2}$ | $1+\lambda=$ | $.99939 \pm .00001$ | CO | $1+\lambda=1.00081$ |
| :--- | ---: | ---: | :--- | ---: |
| $\mathrm{~N}_{2}$ | 1.00044 | .00001 | $\mathrm{CO}_{2}$ | 1.00668 |
| $\mathrm{O}_{2}$ | 1.000094 | .000013 | $\mathrm{~N}_{2} \mathrm{O}$ | 1.00747 |
| He | .99948 | .000005 |  |  |
| Ne | 1.99951 | .000025 |  |  |
| A | 1.00099 | .000026 |  |  |

Part 2.-Low temperatures
$\mathrm{pv}=1$ for $0^{\circ} \mathrm{C}, 1$ atmosphere

| $\underbrace{\text { Helium }}$ |  |  |  | Hydrogen |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $t^{\circ} \mathrm{C}$ | $\stackrel{p}{\text { atm }}$ | $p v$ | Density | $t^{\circ} \mathrm{C}$ | $\underset{\mathrm{atm}}{\text { p }}$ | $p v$ | Density |
| . 00 | 26.66 | 1.0146 | 26.28 | . 00 | 32.313 | 1.0188 | 31.715 |
|  | 38.95 | 1.0196 | 38.20 |  | 44.119 | 1.0266 | 43.284 |
| . | 58.58 | 1.0294 | 56.91 | -103.57 | 38.41 | . 6376 | 38.41 |
| $-103.63$ | 24.13 | . 6337 | 38.07 | . 58 | 51.49 | . 6433 | 80.04 |
|  | 49.96 | . 6479 | 77.08 | -204.70 | 16.75 | . 2404 | 69.68 |
| -269.69 | . 232 | . 01126 | 20.63 |  | 37.00 | . 2316 | 159.7 |
|  | . 353 | . 01041 | 33.92 | " | 44.63 | . 2300 | 194.0 |
| -270.52 | . 0308 | . 00911 | 3381 | -257.26 | . 06698 | . 05783 | 1.1582 |
|  | . 0649 | . 00858 | 7.535 |  | . 13153 | . 057104 | 2.3031 |


| $\underbrace{\text { Neon }}$ |  |  |  | $\underbrace{\text { Argon }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $t^{\circ} \mathrm{C}$ | $\underset{\text { atm }}{\text { b }}$ | $p v$ | Density | $t^{\circ} \mathrm{C}$ | $\stackrel{p}{\text { atm }}$ | $p v$ | Density |
| . 0 | 23.06 | 1.0089 | 21.87 | . 0 | 20.58 | . 9856 | 20.88 |
| " | 30.79 | 1.0147 | 30.34 |  | 31.57 | . 9774 | 32.30 |
| " | 84.66 | 1.0408 | 81.35 | -102.51 | 14.86 | . 5813 | 25.57 |
| -200.1 | 61.66 | . 2337 | 763.8 |  | 45.09 | . 4706 | 95.80 |
|  | 79.92 | . 2293 | 348.6 | " | 62.24 | . 3939 | 158.01 |
| -217.5 | 49.93 | . 1393 | 358.5 | $-130.38$ | 1277 | . 4663 | 27.39 |
|  | 64.97 | . 1269 | 511.8 | -159.62 | 11.99 | . 4262 | 28.12 |
| " | 79.42 | . 1256 | 632.2 | -149.60 | 11.15 | . 3821 | 29.18 |
| $\underbrace{\text { Oxygen }}$ |  |  |  | $\overbrace{}^{\text {Nitrogen }}$ |  |  |  |
| $t^{\circ} \mathrm{C}$ | $\stackrel{p}{\text { atm }}$ | $p v$ | Density | $t^{\circ} \mathrm{C}$ | $\stackrel{p}{\text { atm }}$ | $p v$ | Density |
| 0 | 20.92 | . 9813 | 21.32 | 0 | 33.14 | . 9886 | 33.52 |
| " | 49.79 | . 9573 | 52.01 | ، | 43.08 | . 9860 | 43.70 |
| - 80.03 | 21.01 | . 6550 | 32.09 | " ${ }^{\text {a }}$ | 58.63 | . 9834 | 59.62 |
|  | 34.18 | . 6213 | 55.02 | - 81.10 | 30.17 | . 6516 | 46.13 |
|  | 61.88 | . 5464 | 13.23 |  | 45.47 | . 6270 | 72.52 |
| -116.01 | 22.30 | . 4835 | 46.12 | 4 | 56.71 | . 6109 | 92.84 |
| . 1 | 43.95 | . 3541 | 124.1 | -146.32 | 22.92 | . 3340 | 68.62 |
| " | 55.05 | . 1667 | 330.2 | . | 30.14 | . 2656 | 113.48 |
|  |  |  |  | " | 36.49 | . 1058 | 344.5 |

TABLE 247.-RELATIVE VOLUMES FOR O, AIR, N, AND H AT VARIOUS PRESSURES AND TEMPERATURES
(Volume at $0^{\circ} \mathrm{C}$ and 1 atm being taken as $1,000,000$ )

|  | Oxygen |  |  | $\mathrm{Air}^{\text {a }}$ |  |  | Nitrogen |  |  | Hydrogen |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Atm | $0^{\circ}$ | $99^{\circ} .5$ | $199^{\circ} .5$ | $0^{\circ}$ | $99^{\circ} .4$ | $200{ }^{\circ} .4$ | $0^{\circ}$ | $99^{\circ} .5$ | $199^{\circ} .6$ | $0^{\circ}$ | $99^{\circ} .3$ | $200^{\circ} .5$ |
| 100 | 9265 |  |  | 9730 |  |  | 9910 |  |  |  |  |  |
| 200 | 4570 | 7000 | 9095 | 5050 | 7360 | 9430 | 5195 | 7445 | 9532 | 5690 | 7567 | 9420 |
| 300 | 3208 | 4843 | 6283 | 3658 | 5170 | 6622 | 3786 | 5301 | 6715 | 4030 | 5286 | 6520 |
| 400 | 2629 | 3830 | 4900 | 3036 | 4170 | 5240 | 3142 | 4265 | 5331 | 3207 | 4147 | 5075 |
| 500 | 2312 | 3244 | 4100 | 2680 | 3565 | 4422 | 2780 | 3655 | 4515 | 2713 | 3462 | 4210 |
| 600 | 2115 | 2867 | 3570 | 2450 | 3180 | 3883 | 2543 | 3258 | 3973 | 2387 | 3006 | 3627 |
| 700 | 1979 | 2610 | 3202 | 2288 | 2904 | 3502 | 2374 | 2980 | 3589 | 2149 | 2680 | 3212 |
| 800 | 1879 | 2417 | 2929 | 2168 | 2699 | 3219 | 2240 | 2775 | 3300 | 1972 | 2444 | 2900 |
| 900 | 1800 | 2268 | 2718 | 2070 | 2544 | 3000 | 2149 | 2616 | 3085 | 1832 | 2244 | 2657 |
| 1000 | 1735 | 2151 | - | 1992 | 2415 | 2828 | 2068 | -- |  | 1720 | 2093 |  |

TABLE 248.-RELATIVE VALUES OF pV FOR ETHYLENE

|  | $p v$ at $0^{\circ} \mathrm{C}$ and $1 \mathrm{~atm}=1$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Atm | $0^{\circ}$ | $10^{\circ}$ | $20^{\circ}$ | $30^{\circ}$ | $40^{\circ}$ | $60^{\circ}$ | $80^{\circ}$ | $100^{\circ}$ | $137^{\circ} .5$ | $198^{\circ} .5$ |
| 46 | $\sim$ | . 562 | . 684 | - | - | - | - | - | - | - |
| 48 | - | . 508 |  |  |  |  |  |  |  |  |
| 50 | . 176 | . 420 | . 629 | . 731 | . 814 | . 954 | 1.077 | 1.192 | 1.374 | 1.652 |
| 52 | - | , 240 | . 598 | - |  | - | - | - | - |  |
| 54 | - | . 229 | . 561 | $\cdots$ | - | - | - | - | - | - |
| 56 | - | . 227 | . 524 | - |  | - | -- |  |  |  |
| 100 | . 310 | . 331 | . 360 | . 403 | . 471 | . 668 | . 847 | 1.005 | 1.247 | 1.580 |
| 150 | . 441 | . 459 | . 485 | . 515 | . 551 | . 649 | . 776 | . 924 | 1.178 | 1.540 |
| 200 | . 565 | . 585 | . 610 | . 638 | . 669 | . 744 | . 838 | . 946 | 1.174 | 1.537 |
| 300 | . 806 | . 827 | . 852 | . 878 | . 908 | . 972 | 1.048 | 1.133 | 1.310 | 1.628 |
| 500 | 1.256 | 1.280 | 1.308 | 1.337 | 1.367 | 1.431 | 1.500 | 1.578 | 1.721 | 1.985 |
| 1000 | 2.289 | 2.321 | 2.354 | 2.387 | 2.422 | 2.493 | 2.566 | 2.643 | 2.798 |  |

TABLE 249.-RELATIVE VALUES OF pV FOR CARBON DIOXIDE

| Pressure in meters of mercury | Relative values of fv at- |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $18.2^{\circ} \mathrm{C}$ |  | 35.1 | 40.2 | 50.0 | 60.0 | 70.0 | 80.0 |  | 90.0 | $100.0{ }^{\circ} \mathrm{C}$ |
| 30 | liquid |  | 2360 | 2460 | 2590 | 2730 | 2870 | 2995 |  | 3120 | 3225 |
| 50 |  |  | 1725 | 1900 | 2145 | 2330 | 2525 | 2685 |  | 2845 | 2980 |
| 80 | 625 |  | 750 | 825 | 1200 | 1650 | 1975 | 2225 |  | 2440 | 2635 |
| 110 | 825 |  | 930 | 980 | 1090 | 1275 | 1550 | 1845 |  | 2105 | 2325 |
| 140 | 1020 |  | 1120 | 1175 | 1250 | 1360 | 1525 | 1715 |  | 1950 | 2160 |
| 170 | 1210 |  | 1310 | 1360 | 1430 | 1520 | 1645 | 1780 |  | 1975 | 2135 |
| 200 | 1405 |  | 1500 | 1550 | 1615 | 1705 | 1810 | 1930 |  | 2075 | 2215 |
| 230 | 1590 |  | 1690 | 1730 | 1800 | 1890 | 1990 | 2090 |  | 2210 | 2340 |
| 260 | 1770 |  | 1870 | 1920 | 1985 | 2070 | 2166 | 2265 |  | 2375 | 2490 |
| 290 | 1950 |  | 2060 | 2100 | 2170 | 2260 | 2340 | 2440 |  | 2550 | 2655 |
| 320 | 2135 |  | 2240 | 2280 | 2360 | 2440 | 2525 | 2620 |  | 2725 | 2830 |
|  | Relative values of pv: $\underbrace{p v \text { at } 0^{\circ} \mathrm{C} \text { and } 1 \mathrm{~atm}=1}$ |  |  |  |  |  |  |  |  |  |  |
| Atm | $0^{\circ}$ | $10^{\circ}$ | $20^{\circ}$ | $30^{\circ}$ | $40^{\circ}$ | $60^{\circ}$ | $80^{\circ}$ | $100^{\circ}$ | $137^{\circ}$ | $198^{\circ}$ | $258^{\circ}$ |
| 50 | . 105 | 5 . 114 | . 680 | . 775 | . 750 | . 984 | 1.096 | 1.206 | 1.380 |  |  |
| 100 | . 202 | 2.213 | . 229 | . 255 | . 309 | . 661 | . 873 | 1.030 | 1.259 | 1.582 | 1.847 |
| 150 | . 295 | 5 . 309 | . 326 | . 346 | . 377 | . 485 | . 681 | . 878 | 1.159 | 1.530 | 1.818 |
| 300 | . 559 | 9 . 578 | . 599 | . 623 | . 649 | . 710 | . 790 | . 890 | 1.108 | 1.493 | 1.820 |
| 500 | . 891 | 1 . 913 | . 938 | . 963 | . 990 | 1.054 | 1.124 | 1.201 | 1.362 | 1.678 |  |
| 1000 | 1.656 | 61.685 | 1.716 | 1.748 | 1.780 | 1.848 | 1.921 | 1.999 |  |  |  |

Original volume 100000 under one atmosphere of pressure and the temperature ${ }^{\circ} \mathrm{C}$ of the experiments as indicated at the top of the different columns.

| $\begin{aligned} & \text { Pressure } \\ & \text { in ittmo } \end{aligned}$ | Corresponding volume for experiments at temperature- |  |  | Volume | Pressure in atmospheres for ex. periments at temperature- |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $58^{\circ} .0$ | $99{ }^{\circ} .6$ | $183^{\circ} .2$ |  | $5 \mathrm{~K}^{\circ} .0$ | $99^{\circ} .6$ | $183^{\circ} .2$ |
| 10 | 8560 | 9440 |  |  |  |  |  |
| 12 | 6,360 | 7800 | - | 10000 | -- | 9.60 | - |
| 14 | 4040 | 6420 | - | 9000 | 9.60 | 10.35 | - |
| 16 |  | 5310 | - | 8000 | 10.40 | 11.85 |  |
| 18 | - | 4405 | - | 7000 | 11.55 | 13.05 | - |
| 20 | - | 4030 | - | 6000 | 12.30 | 14.70 | - |
| 24 | - | 3345 | - | 5000 | 13.15 | 16.70 | - |
| 28 | - | 2780 | 3180 | 4000 | -14.00 | 20.15 | - |
| 32 | - | 2305 | 2640 | 3500 | 14.40 | 23.00 |  |
| 36 | - | 1935 | 2260 | 3000 | - | 26.40 | 29.10 |
| 40 | - | 1450 | 2040 | 2500 | - | 30.15 | 33.25 |
| 50 | - | - | 1640 | 2000 | - | 35.20 | 40.95 |
| 60 | - | - | 1375 | 1500 | - | 39.60 | 55.20 |
| 70 | - | - | 1130 | 1000 | - | - | 76.00 |
| 80 | - | - | 930 | 500 | - | - | 117.20 |
| 90 |  | - | 790 |  |  |  |  |
| 100 | - |  | 680 |  |  |  |  |
| 120 | - | - | 545 |  |  |  |  |
| 140 | - | - | 430 |  |  |  |  |
| 160 | - | - | 325 |  |  |  |  |

## TABLE 251.-COMPRESSIBILITY OF AMMONIA

Original vohume 100000 under one atmosphere of pressure and the temperature ${ }^{\circ} \mathrm{C}$ of the experiments as indicated at the top of the different columns.

| $\begin{aligned} & \text { Pressure } \\ & \text { in atmo } \end{aligned}$ | Corresponding volume for experiments at temperature一 |  |  | Volume | Pressure in atmospheres for experiments at temperature - |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $46^{\circ} .6$ | $99^{\circ} .6$ | $183^{\circ} .6$ |  | $30^{\circ} .2$ | $46^{\circ} .6$ | $99^{\circ} .6$ | $183^{\circ} .0$ |
| 10 | 9500 | - | - | 10000 | 8.85 | 9.50 |  | - |
| 12.5 | 7245 | 7635 | - | 9000 | 9.60 | 10.45 |  |  |
| 1.5 | 5880 | 6,305 | - | 8000 | 10.40 | 11.50 | 12.00 | - |
| 20 | - | 4645 | 4875 | 7000 | 11.05 | 13.00 | 13.60 | - |
| 25 | - | 3560 | 3835 | 6000 | 11.80 | 14.75 | 15.55 | - |
| 30 | - | 2875 | 3185 | 5000 | 12.00 | 16.60 | 18.60 | 19.50 |
| 35 | - | 2440 | 2680 | 4000 | - | 18.35 | 22.70 | 24.00 |
| 41 | - | 2080 | 2345 | 3500 | - | 18.30 | 25.40 | 27.20 |
| 45 | - | 1795 | 2035 | 3000 | - | - | 29.20 | 31.50 |
| 50 | - | 1490 | 1775 | 2500 | - | - | 34.25 | 37.35 |
| 55 | - | 1250 | 1590 | 2000 | - | - | 41.45 | 45.50 |
| 60 | - | 975 | 1450 | 1500 | - | - | 49.70 | 58.00 |
| 70 | - | - | 1245 | 1000 | - | - | 59.65 | 93.60 |
| 80 | - | - | 1125 |  |  |  |  |  |
| 90 | - | - | 1035 |  |  |  |  |  |
| 100 | - | - | 950 |  |  |  |  |  |

Actual volumes rest upon Amagat's doubtful values at $3000 \mathrm{~kg} / \mathrm{cm}^{2}$. Densities at highest pressures indicate that the molecules or atoms are very nearly in contact in the sense of the kinetic theory.


80 Bridgman, P. W., Proc. Amer. Acad. Irts and Sci., vol. 59, p. 173, 1924.
TABLE 253.-GAGE PRESSURE (Ib/in. ${ }^{2}$ ) TO ATMOSPHERES (ABSOLUTE)*

| lb/in. ${ }^{2}$ | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1.00 | 1.68 | 2.36 | 3.04 | 3.72 | 4.40 | 5.08 | 5.76 | 6.44 | 7.12 |
| 100 | 7.80 | 8.48 | 9.17 | 9.85 | 10.53 | 11.21 | 11.89 | 12.57 | 13.25 | 13.93 |
| 200 | 14.61 | 15.29 | 15.97 | 16.65 | 17.33 | 18.01 | 18.69 | 19.37 | 20.05 | 20.73 |
| 300 | 21.41 | 22.09 | 22.77 | 23.45 | 24.14 | 24.82 | 25.50 | 26.18 | 26.86 | 27.54 |
| 400 | 28.22 | 28.90 | 29.58 | 30.26 | 30.94 | 31.62 | 32.30 | 32.98 | 33.66 | 34.34 |
| 500 | 35.02 | 35.70 | 36.38 | 37.06 | 37.74 | 38.42 | 39.11 | 39.79 | 40.47 | 41.15 |
| 600 | 41.83 | 42.51 | 43.19 | 43.87 | 44.55 | 45.23 | 45.91 | 46.59 | 47.27 | 47.95 |
| 700 | 48.63 | 49.31 | 49.99 | 50.67 | 51.35 | 52.03 | 52.71 | 53.39 | 54.08 | 54.76 |
| 800 | 55.44 | 56.12 | 56.80 | 57.48 | 58.16 | 58.84 | 59.52 | 60.20 | 60.88 | 61.56 |
| 900 | 62.24 | 62.92 | 63.60 | 64.28 | 64.96 | 65.64 | 66.32 | 67.00 | 67.68 | 68.36 |
| 1,000 | 69.04 | 69.73 | 79.41 | 71.09 | 71.77 | 72.45 | 73.13 | 73.81 | 74.49 | 75.17 |
| 1,100 | 75.85 | 76.53 | 77.21 | 77.89 | 78.57 | 79.25 | 79.93 | 80.61 | 81.29 | 81.97 |
| 1,200 | 82.65 | 83.34 | 84.01 | 84.70 | 85.38 | 86.06 | 86.74 | 87.42 | 88.10 | 88.78 |
| 1,300 | 89.46 | 90.14 | 90.82 | 91.50 | 92.18 | 92.86 | 93.54 | 94.22 | 94.90 | 95.58 |
| 1,400 | 96.27 | 96.95 | 97.63 | 98.31 | 98.98 | 99.67 | 100.3 | 101.0 | 101.7 | 102.4 |
| 1,500 | 103.1 | 103.8 | 104.4 | 105.1 | 105.8 | 106.5 | 107.1 | 107.8 | 108.5 | 109.2 |
| 1,600 | 109.9 | 110.6 | 111.3 | 111.9 | 112.6 | 113.3 | 114.0 | 114.6 | 115.3 | 116.0 |
| 1,700 | 116.7 | 117.4 | 118.0 | 118.7 | 119.4 | 120.1 | 120.8 | 121.4 | 122.1 | 122.8 |
| 1,800 | 123.5 | 124.2 | 124.8 | 125.5 | 126.2 | 126.9 | 127.6 | 128.2 | 128.9 | 129.6 |
| 1,900 | 130.3 | 131.0 | 131.6 | 132.3 | 133.0 | 133.7 | 134.4 | 135.0 | 135.7 | 136.4 |
| 2,000 | 137.1 | 137.8 | 138.4 | 139.1 | 139.8 | 140.5 | 141.2 | 141.9 | 142.5 | 143.2 |
| 2,100 | 143.9 | 144.6 | 145.2 | 145.9 | 146.6 | 147.3 | 148.0 | 148.7 | 149.3 | 150.0 |
| 2,200 | 150.7 | 151.4 | 152.1 | 152.7 | 153.4 | 154.1 | 154.8 | 155.5 | 156.1 | 156.8 |
| 2,300 | 157.5 | 158.2 | 158.9 | 159.5 | 160.2 | 160.9 | 161.6 | 162.3 | 162.9 | 163.6 |
| 2,400 | 164.3 | 165.0 | 165.7 | 166.3 | 167.0 | 167.7 | 168.4 | 169.1 | 169.8 | 170.4 |
| 2,500 | 171.1 | 171.8 | 172.5 | 173.2 | 173.8 | 174.5 | 175.2 | 175.9 | 176.6 | 177.2 |
| 2,600 | 177.9 | 178.6 | 179.3 | 180.0 | 180.6 | 181.3 | 182.0 | 182.7 | 183.4 | 184.0 |
| 2,700 | 184.7 | 185.4 | 186.1 | 186.8 | 187.4 | 188.1 | 188.8 | 189.5 | 190.2 | 190.8 |
| 2,800 | 191.5 | 192.2 | 192.9 | 193.6 | 194.2 | 194.9 | 195.6 | 196.3 | 197.0 | 197.7 |
| 2,900 | 198.3 | 199.0 | 199.7 | 200.4 | 201.1 | 201.7 | 202.4 | 203.1 | 203.8 | 204.4 |

[^115]
## TABLES 254-260.-THERMAL PROPERTIES OF GASES ${ }^{\text {si }}$

The properties given in Tables 254 and $256-258$ are taken from a series of tables of thermal properties of gases being compiled at the National Bureau of Standards at the suggestion of and with the cooperation of the National Advisory Committee for Aeronautics. The functions in these tables have been expressed in dimensionless form in order that they may be converted readily to any system of units. Conversion factors are listed for the most often used units. For more extensive data on various gases reference should be made to these tables. ${ }^{82}$
${ }^{81}$ Adapted from NBS-NACA Tables on thermal properties of gases, July 1949.
${ }^{82}$ Joseph Hilsenrath, Heat and Power Division, National Bureau of Standards.
TABLE 254.-PROPERTIES OF MOLECULAR HYDROGEN
Part 1.-Density, $\rho / \rho_{0}$

| $T{ }^{\circ} K / P$ | .01 atm | .1 atm | 1 atm | 10 atm | 100 atm | $T^{\circ} R$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | .13679 | 1.3792 |  |  |  | 36 |
| 50 | .054671 | .54710 | 5.5112 | 59.510 |  | 90 |
| 100 | .027333 | .27333 | 2.7338 | 27.379 | 258.83 | 180 |
| 150 | .018222 | .18220 | 1.8211 | 18.117 | 168.78 | 270 |
|  |  |  |  |  |  |  |
| 200 | .013666 | .13665 | 1.3657 | 13.574 | 127.01 | 360 |
| 250 | .010933 | .10932 | 1.0927 | 10.863 | 102.35 | 450 |
| 300 | .0091110 | .091100 | .91055 | 9.0575 | 85.896 | 540 |
| 350 | .0078094 | .078086 | .78055 | 7.7682 | 74.086 | 630 |
|  |  |  |  |  |  |  |
| 400 | .0068332 | .068332 | .68298 | 6.8006 | 65.165 | 720 |
| 450 | .0060740 | .060740 | .60715 | 6.0474 | 58.185 | 810 |
| 500 | .0054666 | .054666 | .54644 | 5.4448 | 52.563 | 930 |
| 550 | .0049696 | .049696 | .49676 | 4.9518 | 47.941 | 990 |
| 600 | .0045555 | .045555 | .45541 | 4.5400 | 44.070 | 1080 |


| To convert <br> tabulated <br> value of | to | having the <br> dimensions <br> indicated <br> below | multiply <br> by |
| :---: | :---: | :---: | :---: |
| $\rho / \rho_{0}$ | $\rho$ | $\mathrm{g} \mathrm{cm}^{-3}$ | $\mathrm{g} \mathrm{liter}^{-1}$ |
| $\mathrm{lb} \mathrm{in.-3}$ |  |  |  |
| $\mathrm{lb} \mathrm{ft}^{-3}$ | $8.98854 \times 10^{-5}$ |  |  |

Part 2.-Compressibility factor, $\mathbf{Z}=P V / R T$

| $T{ }^{\circ} \mathrm{K} / P$ | .01 atm | .1 atm | 1 atm | 10 atm | 100 atm | $T^{\circ} \mathrm{R}$ |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 20 | .9991 | .9909 |  |  |  | 36 |
| 50 | .9999 | .9992 | .9919 | .9186 |  | 90 |
| 100 | 1.0000 | 1.0000 | .9998 | .9983 | 1.0560 | 180 |
| 150 | 1.0000 | 1.0001 | 1.0006 | 1.0058 | 1.0796 | 270 |
| 200 | 1.0000 | 1.0001 | 1.0007 | 1.0068 | 1.0760 | 360 |
| 250 | 1.0000 | 1.0001 | 1.0006 | 1.0065 | 1.0682 | 450 |
| 300 | 1.0000 | 1.0001 | 1.0006 | 1.0059 | 1.0607 | 540 |
| 350 | 1.0000 | 1.0001 | 1.0005 | 1.0053 | 1.0541 | 630 |
|  |  |  |  |  |  |  |
| 400 | 1.0000 | 1.0000 | 1.0005 | 1.0048 | 1.0486 | 720 |
| 450 | 1.0000 | 1.0000 | 1.0004 | 1.0044 | 1.0439 | 810 |
| 500 | 1.0000 | 1.0000 | 1.0004 | 1.0040 | 1.0400 | 900 |
| 550 | 1.0000 | 1.0000 | 1.0004 | 1.0036 | 1.0366 | 990 |
| 600 | 1.0000 | 1.0000 | 1.0003 | 1.0034 | 1.0377 | 1080 |
|  |  |  |  |  |  |  |

(continued)

TABLE 254.-PROPERTIES OF MOLECULAR HYDROGEN (concluded)
Part 3.-Values of $R$ for hydrogen for temperatures in ${ }^{\circ} K$

| Pressure |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Density | atm | $\mathrm{kg} / \mathrm{cm}^{2}$ | mmHg | $\mathrm{bb} / \mathrm{in.}^{2}$ |
| $\mathrm{~g} / \mathrm{cm}^{3}$ | 40.7027 | 42.0551 | 30934.0 | 598.167 |
| $\mathrm{~mole} / \mathrm{cm}^{3}$ | 82.0567 | 84.7832 | 62363.1 | 1205.91 |
| mole $/ \mathrm{liter}^{\mathrm{lb} / \mathrm{ft}^{3}}$ | .0820544 | .0847809 | 62.3613 | 1.20587 |
| $\mathrm{~mole} / \mathrm{ft}^{3}$ | .651994 | .673658 | 495.515 | 9.58171 |

## TABLE 255.-DENSITY OF GASES AND VAPORS **

The following table gives the density as the weight in grams of a liter (normal liter) of the gas at $0_{3}{ }^{\circ} \mathrm{C}, 76 \mathrm{cmHg}$ pressure, also the weight in $1 \mathrm{~b} / \mathrm{ft}^{3}$, and standard gravity $930.655 \mathrm{~cm} / \mathrm{sec}^{2}$ (sea level, $45^{\circ}$ latitude), the specific gravity referred to dry, carbon-dioxide-free air, and to pure oxygen. Dry, carbon-dioxide-free air is of remarkably uniform density; Guye, Kovacs, and Wourtzel found maximum variations in the density of only 7 to 8 parts in 10,000 . For highest accuracy pure oxygen should be used as the standard gas for specific gravities. Observed densities are closely proportional to the molecular weights.

| Gas | Formula | Molecular weight | Weight of normal |  | Specific gravity |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |
|  |  |  | grams | pounds | Air $=1$ | $0_{2}=1$ |
| Acetylene | $\mathrm{C}_{2} \mathrm{H}_{2}$ | 26.036 | 1.173 | . 07323 | . 912 | . 825 |
| Air |  |  | 1.2920 | . 0805 | 1.000 | . 9047 |
| Ammonia | $\mathrm{NH}_{3}$ | 17.032 | . 7598 | . 04742 | . 5963 | . 5395 |
| Argon |  | 39.944 | 1.782 | . 1112 | 1.3787 | 1.2482 |
| Arsene | $\mathrm{AsH}_{3}$ | 77.93 | 3.48 | . 217 | 2.69 | 2.434 |
| Butane-iso | $\mathrm{C}_{4} \mathrm{H}_{10}$ | 58.12 | 2.673 | . 1669 | 2.067 | 1.870 |
| Butane-n | C. $\mathrm{H}_{20}$ | 58.12 | 2.519* | .15725* | 2.085* | 1.8868* |
| Carbon dioxide | $\mathrm{CO}_{3}$ | 44.01 | 1.9630 | . 1225 | 1.5290 | 1.3834 |
| Carbon monoxide | CO | 28.010 | 1.2492 | . 0779 | . 9671 | . 8750 |
| Carbon oxysulfide | COS | 60.076 | 2.72 | . 170 | 2.10 | 1.90 |
| Chlorine | $\mathrm{Cl}_{2}$ | 70.914 | 3.1638 | . 1974 | 2.486 | 2.249 |
| Chlorine monoxide | $\mathrm{Cl}_{2} \mathrm{O}$ | 86914 | 3.89 | . 243 | 3.01 | 2.721 |
| Ethane | $\mathrm{C}_{2} \mathrm{H}_{8}$ | 30.068 | 1.3566 | . 08469 | 1.0493 | . 9493 |
| Ethylene | $\mathrm{C}_{2} \mathrm{H}_{4}$ | 28.052 | 1.2604 | . 07860 | . 9749 | . 8820 |
| Fluorine |  | 38.00 | 1.6954 | . 1058 | 1.311 | 1.187 |
| Helium |  | 4.003 | . 1785 | . 01114 | . 1381 | . 1249 |
| Hydrogen | $\mathrm{H}_{2}$ | 2.016 | . 08988 | . 005611 | . 06952 | . 06290 |
| Hydrogen bromide | HBr | 80.924 | 36104 | . 2252 | 2.8189 | 2.5503 |
| Hydrogen chloride | HCl | 36.465 | 1.6269 | . 1016 | 1.2678 | 1.1471 |
| Hydrogen iodide . . | HI | 127.93 | 5.7075 | . 3562 | 4.480 | 4.052 |
| Hydrogen selenide | $\mathrm{H}_{2} \mathrm{Se}$ | 80.976 | 3.670 | . 229 | 2.839 | 2.568 |
| Hydrogen sulfide . | $\mathrm{H}_{2} \mathrm{~S}$ | 34.082 | 1.5203 | . 0949 | 1.190 | 1.077 |
| Krypton . . . . |  | 83.7 | 3.7365 | . 2332 | 2868 | 2.595 |
| Methane | $\mathrm{CH}_{4}$ | 16.042 | . 7152 | . 04462 | . 5544 | . 5016 |
| Methyl chloride | $\mathrm{CH}_{3} \mathrm{Cl}$ | 50.491 | 2.3076 | . 1440 | 1.7825 | 1.6125 |
| Methyl ether | $\left(\mathrm{CH}_{3} 3\right)_{2} \mathrm{O}$ | 46.068 | 2.1098 | . 13171 | 1.6318 | 1.4764 |
| Methyl fluoride | $\mathrm{CH}_{3} \mathrm{~F}$ | 34.034 | 1.5452 | . 09646 | 1.1951 | 1.0813 |
| Mono methylamine | $\mathrm{CH}_{3} \mathrm{NH}_{2}$ | 31.058 | 1.396 | . 08715 | 1.080 | . 9769 |
| Neon . ........... |  | 20.183 | . 9005 | . 05621 | . 6963 | . 63004 |
| Nitric oxide | NO | 30.008 | 1.3388 | . 0836 | 1.0366 | . 9378 |
| Nitrogen (chem.) | $\mathrm{N}_{3}$ | 28.016 | 1.2499 | . 07803 | . 9672 | . 8751 |
| Nitrogen ( atm ) . |  | - | 1.2568 | . 07846 | . 9722 | . 8795 |
| Nitrosyl chloride | NOCl | 65.465 | 2.992 | . 1868 | 2.314 | 2.094 |
| Nitrous oxide . . | $\mathrm{N}_{2} \mathrm{O}$ | 44.016 | 1.9638 | . 123255 | 1.5297 | 1.3840 |
| Oxygen |  | 32.000 | 14277 | . 08915 | 1.10527 | 1.0000 |
| Phosphine | $\mathrm{PH}_{3}$ | 34.004 | 1.5294 | . 09548 | 1.1829 | 1.0702 |
| Propane . | $\mathrm{C}_{3} \mathrm{H}_{8}$ | 44.094 | 2.020 | . 1261 | 1.562 | 1.414 |
| Silicon tetrafluoride | $\mathrm{SiF}_{4}$ | 104.06 | 4.684 | . 2924 | 3.623 | 3.278 |
| Sulfur dioxide | $\mathrm{SO}_{2}$ | 64.066 | 2.858 | . 1784 | 2.2638 | 2.0482 |
| Xenon . . . . . . . . . | Xe | 131.3 | 5.8579 | . 3657 | 4.525 | 4.094 |

[^116]TABLE 256.-THERMAL PROPERTIES OF DRY AIR (IDEAL GAS STATE)

|  | Specific heat | Enthalpy$\left(\mathrm{H}^{\circ}-\mathrm{E}_{0}{ }^{\circ}\right)$ | Entropy |  | Specific heat | Enthalpy | Entropy |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{C}_{\mathrm{p}}{ }^{\text {o }}$ |  | $S^{\circ}$ |  | $\mathrm{C}_{\mathrm{p}}{ }^{\text {o }}$ | $\left(\mathrm{H}^{\circ}-\mathrm{E}_{0}{ }^{\circ}\right)$ | $\underline{S}^{\circ}$ |
| ${ }^{\circ} \mathrm{K}$ | $\frac{\mathrm{p}}{\mathrm{R}}$ | $\mathrm{RT}{ }_{0}$ | R | ${ }^{\circ} \mathrm{K}$ | R | RT0 | R |
|  |  |  |  | 400 | 3.5305 | 5.1182 | 24.9301 |
| 10 | 3.5009 | . 1238 | 12.0382 | 410 | 3.5349 | 5.2476 | 25.0173 |
| 20 | 3.4941 | . 2518 | 14.4622 | 420 | 3.5397 | 5.3771 | 25.1026 |
| 30 | 3.4926 | . 3796 | 15.8748 | 430 | 3.5447 | 5.5067 | 25.1859 |
| 40 | 3.4918 | . 5075 | 16.8832 | 440 | 3.5499 | 5.6366 | 25.2675 |
| 50 | 3.4915 | . 6353 | 17.6633 | 450 | 3.5555 | 5.7667 | 25.3473 |
| 60 | 3.4914 | . 7631 | 18.2990 | 460 | 3.5613 | 5.8969 | 25.4255 |
| 70 | 3.4914 | . 8909 | 18.8367 | 470 | 3.5673 | 6.0274 | 25.5022 |
| 80 | 3.4913 | 1.0188 | 19.3034 | 480 | 3.5735 | 6.1581 | 25.5773 |
| 90 | 3.4913 | 1.1466 | 19.7145 | 490 | 3.5799 | 6.2891 | 25.6511 |
| 100 | 3.4913 | 1.2744 | 20.0824 | 500 | 3.5865 | 6.4202 | 25.7235 |
| 110 | 3.4914 | 1.4022 | 20.4152 | 510 | 3.5933 | 6.5517 | 25.7946 |
| 120 | 3.4914 | 1.5300 | 20.7190 | 520 | 3.6003 | 6.6833 | 25.8644 |
| 130 | 3.4914 | 1.6578 | 20.9984 | 530 | 3.6075 | 6.8153 | 25.9330 |
| 140 | 3.4914 | 1.7856 | 21.2572 | 540 | 3.6149 | 6.9475 | 26.0005 |
| 150 | 3.4915 | 1.9134 | 21.4980 | 550 | 3.6224 | 7.0799 | 26.0669 |
| 160 | 3.4916 | 2.0413 | 21.7234 | 560 | 3.6300 | 7.2127 | 26.1323 |
| 170 | 3.4916 | 2.1691 | 21.9351 | 570 | 3.6377 | 7.3456 | 26.1966 |
| 180 | 3.4917 | 2.2969 | 22.1346 | 580 | 3.6456 | 7.4790 | 26.2599 |
| 190 | 3.4919 | 2.4247 | 22.3234 | 590 | 3.6535 | 7.6126 | 26.3223 |
| 200 | 3.4922 | 2.5526 | 22.5026 | 600 | 3.6615 | 7.7465 | 26.3838 |
| 210 | 3.4924 | 2.6804 | 22.6729 | 610 | 3.6696 | 7.8807 | 26.4444 |
| 220 | 3.4927 | 2.8083 | 22.8354 | 620 | 3.6778 | 8.0152 | 26.5041 |
| 230 | 3.4932 | 2.9362 | 22.9907 | 630 | 3.6860 | 8.1500 | 26.5630 |
| 240 | 3.4937 | 3.0641 | 23.1394 | 640 | 3.6943 | 8.2851 | 26.6211 |
| 250 | 3.4945 | 3.1920 | 23.2820 | 650 | 3.7027 | 8.4205 | 26.6785 |
| 260 | 3.4953 | 3.3199 | 23.4191 | 660 | 3.7111 | 8.5562 | 26.7351 |
| 270 | 3.4963 | 3.4479 | 23.5510 | 670 | 3.7195 | 8.6922 | 26.7910 |
| 280 | 3.4975 | 3.5759 | 23.6782 | 680 | 3.7279 | 8.8285 | 26.8461 |
| 290 | 3.4989 | 3.7040 | 23.8009 | 690 | 3.7363 | 8.9651 | 26.9006 |
| 300 | 3.5005 | 3.8321 | 23.9196 | 700 | 3.7447 | 9.1021 | 26.9544 |
| 310 | 3.5024 | 3.9603 | 24.0344 | 710 | 3.7531 | 9.2393 | 27.0076 |
| 320 | 3.5044 | 4.0885 | 24.1456 | 720 | 3.7614 | 9.3768 | 27.0601 |
| 330 | 3.5068 | 4.2169 | 24.2535 | 730 | 3.7698 | 9.5147 | 27.1121 |
| 340 | 3.5093 | 4.3453 | 24.3582 | 740 | 3.7782 | 9.6528 | 27.1634 |
| 350 | 3.5122 | 4.4738 | 24.4600 | 750 | 3.7865 | 9.7913 | 27.2142 |
| 360 | 3.5153 | 4.6024 | 24.5590 | 760 | 3.7947 | 9.9301 | 27.2644 |
| 370 | 3.5186 | 4.7312 | 24.6553 | 770 | 3.8030 | 10.0692 | 27.3141 |
| 380 | 3.5224 | 4.8601 | 24.7492 | 780 | 3.8112 | 10.2085 | 27.3632 |
| 390 | 3.5263 | 4.9891 | 24.8408 | 790 | 3.8194 | 10.3482 | 27.4118 |
| 400 | 3.5305 | 5.1182 | 24.9301 | 800 | 3.8275 | 10.4882 | 27.4599 |

Conversion factors

| To convert tahulated value of | to | having the dimensions indicated below | $\underset{\text { by }}{\substack{\text { multiply }}}$ |
| :---: | :---: | :---: | :---: |
| $\mathrm{C}_{\rho}{ }^{\circ} / \mathrm{R}, \mathrm{S}^{\circ} / \mathrm{R}$ | $\mathrm{C}_{\rho}{ }^{\circ} . \mathrm{S}^{\circ}$ | cal $\mathrm{mol}^{-1}{ }^{\circ} \mathrm{K}^{-1}$ ( or ${ }^{\circ} \mathrm{C}^{-1}$ ) | 1.98719 |
|  |  | cal $\mathrm{g}^{-1}{ }^{\circ} \mathrm{K}^{-1}$ ( or ${ }^{\circ} \mathrm{C}^{-1}$ ) | . 0686042 |
|  |  | joules $\mathrm{g}^{-1}{ }^{\circ} \mathrm{K}^{-1}\left(\mathrm{or}^{\circ} \mathrm{C}^{-1}\right)$ | . 287040 |
|  |  | Btu ( lbmol$)^{-1}{ }^{\circ} \mathrm{R}^{-1}\left(\mathrm{or}^{\circ} \mathrm{F}^{-1}\right.$ ) | 1.98588 |
|  |  | Btu $\mathrm{lb}^{-1}{ }^{\circ} \mathrm{R}^{-1}$ ( or $^{\circ} \mathrm{F}^{-1}$ ) | . 0685590 |

(continued)

TABLE 256.-THERMAL PROPERTIES OF DRY AIR (IDEAL GAS STATE) (concluded)

|  | Specific |  | Entropy |  | Specific |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{C}_{\mathrm{p}}{ }^{\circ}$ | $\begin{aligned} & \text { Enthapy } \\ & \left(\mathrm{H}^{\circ}-\mathrm{E}_{0}{ }^{\circ}\right) \end{aligned}$ | Entropy S |  | $\begin{aligned} & \text { heat } \\ & C_{p}{ }^{\circ} \end{aligned}$ | $\begin{aligned} & \text { Enthalpy } \\ & \left(\mathrm{H}^{\circ}-\mathrm{E}_{0}{ }^{\circ}\right) \end{aligned}$ | Entropy S ¢ |
| ${ }^{\circ} \mathrm{K}$ | $\frac{\mathrm{p}}{\mathrm{R}}$ | RT。 | - | ${ }^{\circ} \mathrm{K}$ | $\frac{\mathrm{c}^{\text {p }}}{\mathrm{R}}$ | $\mathrm{RT}_{0}$ | $\frac{\mathrm{S}^{\text {a }}}{}$ |
| 800 | 3.8275 | 10.4882 | 27.4599 | 1900 | 4.3337 | 27.1375 | 31.0047 |
| 850 | 3.8670 | 11.1924 | 27.6931 | 1950 | 4.3452 | 27.9318 | 31.1175 |
| 900 | 3.9049 | 11.9037 | 27.9152 | 2000 | 4.3561 | 28.7281 | 31.2276 |
| 950 | 3.9409 | 12.6218 | 28.1273 | 2050 | 4.3666 | 29.5264 | 31.3353 |
| 1000 | 3.9750 | 13.3463 | 28.3303 | 2100 | 4.3767 | 30.3267 | 31.4407 |
| 1050 | 4.0070 | 14.0769 | 28.5250 | 2150 | 4.3864 | 31.1287 | 31.5438 |
| 1100 | 4.0371 | 14.8131 | 28.7121 | 2200 | 4.3958 | 31.9324 | 31.6447 |
| 1150 | 4.0653 | 15.5547 | 28.8922 | 2250 | 4.4048 | 32.7379 | 31.7436 |
| 1200 | 4.0917 | 16.3013 | 29.0658 | 2300 | 4.4135 | 33.5449 | 31.8405 |
| 1250 | 4.1166 | 17.0525 | 29.2333 | 2350 | 4.4219 | 34.3536 | 31.9355 |
| 1300 | 4.1398 | 17.8082 | 29.3953 | 2400 | 4.4301 | 35.1637 | 32.0287 |
| 1350 | 4.1615 | 18.5679 | 29.5519 | 2450 | 4.4380 | 35.9754 | 32.1201 |
| 1400 | 4.1820 | 19.3315 | 29.7036 | 2500 | 4.4456 | 36.7884 | 32.2099 |
| 1450 | 4.2012 | 20.0988 | 29.8507 | 2550 | 4.4530 | 37.6028 | 32.2980 |
| 1500 | 4.2193 | 20.8695 | 29.9935 | 2600 | 4.4602 | 38.4186 | 32.2845 |
| 1550 | 4.2364 | 21.6434 | 30.1321 | 2650 | 4.4672 | 39.2357 | 32.4695 |
| 1600 | 4.2525 | 22.4203 | 30.2669 | 2700 | 4.4740 | 40.0540 | 32.5531 |
| 1650 | 4.2678 | 23.2001 | 30.3979 | 2750 | 4.4807 | 40.8735 | 32.6353 |
| 1700 | 4.2823 | 23.9826 | 30.5255 | 2800 | 4.4871 | 41.6943 | 32.7160 |
| 1750 | 4.2962 | 24.7678 | 30.6499 | 2850 | 4.4933 | 42.5162 | 32.7955 |
| 1800 | 4.3093 | 25.5553 | 30.7711 | 2900 | 4.4994 | 43.3392 | 32.8737 |
| 1850 | 4.3218 | 26.3453 | 30.8893 | 2950 | 4.5053 | 44.1633 | 32.9507 |
| 1900 | 4.3337 | 27.1375 | 31.0047 | 3000 | 4.5109 | 44.9884 | 33.0264 |

## Conversion factors

| To convert tabulated |  |
| :---: | :---: |
| value of |  |
| $\left(\mathrm{H}^{\circ}-\mathrm{E}_{0}{ }^{\circ}\right) / \mathrm{RT}_{0}$ | to |
|  | $\left(\mathrm{H}^{\circ}-\mathrm{E}_{0}{ }^{\circ}\right)$ |


| having the dimensions <br> indicated below | multiply |
| :--- | :---: |
| cy | 542.821 |
| cal mol ${ }^{-1}$ | 18.7399 |
| cal g |  |
| joules g g |  |
| Btu $\left(\mathrm{lb} \mathrm{mol}^{-1} \mathrm{~m}^{-1}\right.$ | 78.4079 |
| Btu $\mathrm{lb}^{-1}$ | 976.437 |
|  | 33.7098 |



To convert tabulated $C_{p}{ }^{\circ} / R, S^{\circ} / R$

## Conversion factors

$\underset{\substack{\text { multiply } \\ \text { by }}}{ }$
1.98719
. 0709305
.296774
1.98588
. 0708837
(continued)
(IDEAL GAS STATE) (concluded)

|  | Specific heat $\mathrm{C}_{\mathrm{p}}{ }^{\circ}$ | $\begin{aligned} & \text { Enthalpy } \\ & \left(\mathrm{H}^{\circ}-\mathrm{E}_{0}{ }^{\circ}\right) \end{aligned}$ | Entropy $S^{\circ}$ |  | Specific heat $\mathrm{C}_{\mathrm{p}}{ }^{\text {b }}$ | Enthalpy $\left(\mathrm{H}^{\circ}-\mathrm{E}_{0}{ }^{\circ}\right)$ | Entropy $S^{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{K}$ | R | RT ${ }_{0}$ | R | ${ }^{\circ} \mathrm{K}$ | R | $\mathrm{RT}_{0}$ | R |
| 800 | 3.7806 | 10.4423 | 26.5658 | 2900 | 4.4460 | 43.0145 | 31.9327 |
| 850 | 3.8207 | 11.1380 | 26.7962 | 2950 | 4.4503 | 43.8287 | 32.0088 |
| 900 | 3.8596 | 11.8409 | 27.0156 | 3000 | 4.4545 | 44.6437 | 32.0836 |
| 950 | 3.8970 | 12.5508 | 27.2253 | 3050 | 4.4585 | 45.4595 | 32.1573 |
| 1000 | 3.9326 | 13.2674 | 27.4261 | 3100 | 4.4624 | 46,2759 | 32.2298 |
| 1050 | 3.9664 | 13.9904 | 27.6188 | 3150 | 4.4663 | 47.0931 | 32.3013 |
| 1100 | 3.9982 | 14.7193 | 27.8040 | 3200 | 4.4699 | 47.9109 | 32.3716 |
| 1150 | 4.0281 | 15.4539 | 27.9824 | 3250 | 4.4735 | 48.7295 | 32.4409 |
| 1200 | 4.0562 | 16.1939 | 28.1544 | 3300 | 4.4770 | 49.5486 | 32.5093 |
| 1250 | 4.0825 | 16.9388 | 28.3206 | 3350 | 4.4804 | 50.3684 | 32.5766 |
| 1300 | 4.1072 | 17.6883 | 28.4812 | 3400 | 4.4836 | 51.1888 | 32.6430 |
| 1350 | 4.1303 | 18.4422 | 28.6366 | 3450 | 4.4868 | 52.0098 | 32.7085 |
| 1400 | 4.1518 | 19.2002 | 28.7872 | 3500 | 4.4900 | 52.8314 | 32.7731 |
| 1450 | 4.1720 | 19.9621 | 28.9333 | 3550 | 4.4930 | 53.6535 | 32.8368 |
| 1500 | 4.1909 | 20.7275 | 29.0751 | 3600 | 4.4960 | 54.4762 | 32.8996 |
| 1550 | 4.2086 | 21.4963 | 29.2128 | 3650 | 4.4988 | 55.2994 | 32.9617 |
| 1600 | 4.2252 | 22.2682 | 29.3467 | 3700 | 4.5016 | 56.1232 | 33.0229 |
| 1650 | 4.2408 | 23.0430 | 29.4769 | 3750 | 4.5044 | 56.9474 | 33.0834 |
| 1700 | 4.2554 | 23.8206 | 29.6037 | 3800 | 4.5071 | 57.7722 | 33.1431 |
| 1750 | 4.2692 | 24.6008 | 29.7273 | 3850 | 4.5097 | 58.5974 | 33.2020 |
| 1800 | 4.2821 | 25.3834 | 29.8477 | 3900 | 4.5123 | 59.4231 | 33.2602 |
| 1850 | 4.2943 | 26.1684 | 29.9652 | 3950 | 4.5148 | 60.2493 | 33.3177 |
| 1900 | 4.3057 | 26.9554 | 30.0799 | 4000 | 4.5173 | 61.0759 | 33.3745 |
| 1950 | 4.3166 | 27.7446 | 30.1919 | 4050 | 4.5197 | 61.9030 | 33.4306 |
| 2000 | 4.3268 | 28.5356 | 30.3013 | 4100 | 4.5221 | 62.7306 | 33.4861 |
| 2050 | 4.3365 | 29.3285 | 30.4083 | 4150 | 4.5245 | 63.5585 | 33.5409 |
| 2100 | 4.3457 | 30.1232 | 30.5129 | 4200 | 4.5268 | 64.3868 | 33.5951 |
| 2150 | 4.3544 | 30.9194 | 30.6152 | 4250 | 4.5290 | 65.2156 | 33.6487 |
| 2200 | 4.3627 | 31.7172 | 30.7154 | 4300 | 4.5312 | 66.0448 | 33.7017 |
| 2250 | 4.3705 | 32.5165 | 30.8135 | 4350 | 4.5334 | 66.8745 | 33.7541 |
| 2300 | 4.3780 | 33.3172 | 30.9097 | 4400 | 4.5356 | 67.7045 | 33.8059 |
| 2350 | 4.3852 | 34.1192 | 31.0039 | 4450 | 4.5377 | 68.5349 | 33.8572 |
| 2400 | 4.3920 | 34.9225 | 31.0963 | 4500 | 4.5398 | 69.3657 | 33.9079 |
| 2450 | 4.3985 | 35.7270 | 31.1869 | 4550 | 4.5419 | 70.1968 | 33.9581 |
| 2500 | 4.4047 | 36.5327 | 31.2759 | 4600 | 4.5440 | 71.0284 | 34.0077 |
| 2550 | 4.4106 | 37.3395 | 31.3631 | 4650 | 4.5460 | 71.8603 | 34.0569 |
| 2600 | 4.4163 | 38.1473 | 31.4488 | 4700 | 4.5480 | 72.6927 | 34.1055 |
| 2650 | 4.4218 | 38.9562 | 31.5330 | 4750 | 4.5500 | 73.5253 | 34.1536 |
| 2700 | 4.4270 | 39.7661 | 31.6157 | 4800 | 4.5520 | 74.3583 | 34.2013 |
| 2750 | 4.4320 | 40.5769 | 31.6970 | 4850 | 4.5540 | 75.1917 | 34.2484 |
| 2800 | 4.4369 | 41.3886 | 31.7769 | 4900 | 4.5559 | 76.0255 | 34.2952 |
| 2850 | 4.4415 | 42.2011 | 31.8554 | 4950 | 4.5579 | 76.8497 | 34.3415 |
| 2900 | 4.4460 | 43.0145 | 31.9327 | 5000 | 4.5598 | 77.6941 | 34.3873 |

Conversion factors

| To convert tabulated |  |  |
| :---: | :---: | :---: |
| value of |  | multiply |
| $\left(\mathrm{H}^{\circ}-\mathrm{E}_{0}{ }^{\circ}\right) / \mathrm{RT}_{0}$ | to dimensions indicated below | by |
|  | cal mol |  |
|  | cal $\mathrm{g}^{-1}$ | 542.821 |
|  | joules $\mathrm{g}^{-1}$ | 19.3754 |
|  | Btu $\left(\mathrm{lb} \mathrm{mol}^{-1}\right.$ | 81.0699 |
|  | Btu $\mathrm{lb}^{-1}$ | 976.437 |
|  |  | 34.8528 |


(continued)

TABLE 258.-THERMAL PROPERTIES OF MOLECULAR OXYGEN
(IDEAL GAS STATE) (concluded)

|  | Specific heat C ${ }^{\circ}$ | Enthalpy $\left(\mathrm{H}^{\circ}-\mathrm{E}_{0}{ }^{\circ}\right)$ | Entropy |  | Specific heat $\mathrm{C}_{\mathrm{p}}{ }^{\circ}$ | $\begin{aligned} & \text { Enthalpy } \\ & \left(H^{\circ}-E_{0}^{\circ}\right) \end{aligned}$ | Entropy |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{K}$ | $\mathrm{Cl}_{-}^{\mathrm{p}} \mathrm{R}^{-}$ | $\mathrm{RT}_{0}$ | $\mathrm{R} \quad{ }^{\circ} \mathrm{K}$ |  | $\frac{\mathrm{c}}{\mathrm{p}}$ | - $\mathrm{RT}_{0}$ | $\frac{S^{\circ}}{\text { R }}$ |
| 800 | 4.0577 | 10.7950 | 28.36622900 |  | 4.7824 | 45.2601 | 34.0470 |
| 850 | 4.0970 | 11.5414 | 28.61342950 |  | 4.7944 | 46.1366 | 34.1289 |
| 900 | 4.1327 | 12.2946 | 28.8486 |  | 4.8062 | 47.0152 | 34.2096 |
| 950 | 4.1652 | 13.0541 | 29.07293050 |  | 4.8177 | 47.8961 | 34.2891 |
| 1000 | 4.1948 | 13.8193 | 29.2874 |  | 4.8291 | 48.7790 | 34.3675 |
| 1050 | 4.2219 | 14.5896 | $29.4927 \quad 3150$ |  | 4.8402 | 49.6640 | 34.4449 |
| 1100 | 4.2469 | 15.3647 | 29.6897 3200 |  | 4.8512 | 50.5509 | 34.5212 |
| 1150 | 4.2698 | 16.1442 | 29.87903250 |  | 4.8619 | 51.4398 | 34.5965 |
| 1200 | 4.2912 | 16.9278 | 30.06113300 |  | 4.8724 | 52.3307 | 34.6708 |
| 1250 | 4.3112 | 17.7151 | 30.2367 3350 |  | 4.8827 | 53.2236 | 34.7442 |
| 1300 | 4.3300 | 18.5059 | 30.40623400 |  | 4.8929 | 54.1183 | 34.8166 |
| 1350 | 4.3479 | 19.3002 | 30.57003450 |  | 4.9028 | 55.0148 | 34.8881 |
| 1400 | 4.3651 | 20.0976 | 30.7284 |  | 4.9125 | 55.9130 | 34.9587 |
| 1450 | 4.3815 | 20.8981 | 30.8819 3550 |  | 4.9220 | 56.8132 | 35.0285 |
| 1500 | 4.3975 | 21.7016 | 31.03073600 |  | 4.9312 | 57.7150 | 35.0974 |
| 1550 | 4.4130 | 22.5080 | 31.17513650 |  | 4.9403 | 58.6183 | 35.1654 |
| 1600 | 4.4282 | 23.3171 | 31.3155 |  | 4.9491 | 59.5233 | 35.2327 |
| 1650 | 4.4431 | 24.1290 | 31.45193750 |  | 4.9578 | 60.4301 | 35.2992 |
| 1700 | 4.4578 | 24.9437 |  |  | 4.9662 | 61.3384 | 35.3649 |
| 1750 | 4.4724 | 25.7609 | 31.71423850 |  | 4.9744 | 62.2482 | 35.4299 |
| 1800 | 4.4868 | 26.5809 | 31.8404 |  | 4.9825 | 63.1594 | 35.4941 |
| 1850 | 4.5011 | 27.4036 | 31.9636 |  | 4.9903 | 64.0721 | 35.5576 |
| 1900 | 4.5153 | 28.2288 | 32.0838 |  | 4.9979 | 64.9862 | 35.6204 |
| 1950 | 4.5295 | 29.0565 | 32.2013 |  | 5.0054 | 65.9022 | 35.6826 |
| 2000 | 4.5436 | 29.8869 | 32.3161 |  | 5.0126 | 66.8193 | 35.7441 |
| 2050 | 4.5576 | 30.7198 | 32.4285 |  | 5.0197 | 67.7371 | 35.8049 |
| 2100 | 4.5715 | 31.5554 | 32.5385 |  | 5.0265 | 68.6561 | 35.8650 |
| 2150 | 4.5854 | 32.3935 | 32.6462 4250 |  | 5.0332 | 69.5765 | 35.9245 |
| 2200 | 4.5993 | 33.2341 | 32.7518 |  | 5.0397 | 70.4983 | 35.9835 |
| 2250 | 4.6130 | 34.0771 | 32.8553 |  | 5.0460 | 71.4217 | 36.0418 |
| 2300 | 4.6267 | 34.9227 | 32.95684400 |  | 5.0521 | 72.3461 | 36.0995 |
| 2350 | 4.6404 | 35.7709 | 33.05654450 |  | 5.0580 | 73.2715 | 36.1566 |
| 2400 | 4.6540 | 36.6217 | 33.1543 ( 4500 |  | 5.0638 | 74.1976 | 36.2132 |
| 2450 | 4.6674 | 37.4747 | 33.2504 |  | 5.0693 | 75.1246 | 36.2691 |
| 2500 | 4.6808 | 38.3302 | 33.3449 |  | 5.0746 | 76.0528 | 36.3246 |
| 2550 | 4.6940 | 39.1882 | 33.4377 ( 4650 |  | 5.0797 | 76.9827 | 36.3794 |
| 2600 | 4.7071 | 40.0487 | 33.5289 |  | 5.0847 | 77.9135 | 36.4338 |
| 2650 | 4.7200 | 40.9114 | 33.61874750 |  | 5.0896 | 78.8445 | 36.4876 |
| 2700 | 4.7328 | 41.7765 | 33.7071 |  | 5.0943 | 79.7760 | 36.5410 |
| 2750 | 4.7454 | 42.6440 | 33.79404850 |  | 5.0987 | 80.7086 | 36.5938 |
| $\begin{aligned} & 2800 \\ & 2850 \\ & 2900 \end{aligned}$ | 4.7579 | 43.5138 | $\begin{aligned} & 33.8796 \\ & 33.9640 \\ & 34.0470 \end{aligned}$ | 4900 | 5.1028 | 81.6423 | 36.6461 |
|  | 4.7703 | 44.3858 |  | 4950 | 5.1068 | 82.5770 | 36.6980 |
|  | 4.7824 | 45.2601 |  | 5000 | 5.1109 | 83.5122 | 36.7493 |
|  |  |  | Conversion factors |  |  |  |  |
|  | To convert tabulated value of |  | to dimensions indicated below |  |  | $\underset{\text { by }}{\text { multiply }}$ |  |
|  | $\mathrm{H}^{\circ}-\mathrm{E}_{0}{ }^{\circ}$ |  | $\mathrm{cal} \mathrm{mol}{ }^{-1}$ |  |  | 542.821 |  |
|  | RT 。 |  | $\text { cal } \mathrm{g}^{-1}$ |  |  | 16.9632 |  |
|  |  |  |  | 70.9742 |  |
|  |  |  | Btu ( 1 b mol$)^{-1}$ |  | 976.437 |  |
|  |  |  | Btu 1b ${ }^{-1}$ |  | 30.5137 |  |

TABLE 259.-CRITICAL TEMPERATURES, PRESSURES, AND DENSITIES OF GASES **

| Substance | $\begin{gathered} \text { Critical } \\ \text { temperature } \\ \left(0^{\circ} \mathrm{C}\right) \end{gathered}$ | $\begin{aligned} & \text { Critical } \\ & \text { pressure } \\ & \left(\mathrm{kg} / \mathrm{cm}^{2}\right) \end{aligned}$ | Critical density ( $\mathrm{g} / \mathrm{cm}^{3}$ ) |
| :---: | :---: | :---: | :---: |
| Acetylene | 36 | 62 | . 231 |
| Air .... | -140.7 | 37.2 | .35* . $31 \dagger$ |
| Alcohol ( $\mathrm{C}_{2} \mathrm{H}_{6} \mathrm{O}$ ) | 243.1 | 63.1 | . 2755 |
| Alcohol ( $\mathrm{CH}_{4} \mathrm{O}$ ) | 240.0 | 78.7 | . 272 |
| Allylene | 128 |  |  |
| Ammonia | 132.4 | 115.5 | . 235 |
| Argon | -122 | 49.7 | . 531 |
| Benzene | 288.5 | 47.7 | . 304 |
| Bromine | 302 | $\cdots$ | 1.18 |
| iso-Butane | 134 | 37 | . . . |
| n-Butane | 153 | 36 | . |
| Carbon dioxide | 31.1 | 75.5 | . 46 |
| Carbon disulfide | 273 | 76 | $\cdots$ |
| Carbon monoxide | -139 | 36.2 | . 311 |
| Chlorine | 144.0 | 78.7 | . 573 |
| Chloroform | 263 | $\cdots$ | . 516 |
| Cyanogen | 128 | 59 |  |
| Ethane | 32.1 | 48.8 | . 21 ? |
| Ether (ethyl) | 193.8 | 35.5 | . 2625 |
| Ethyl chloride | 187.2 | 52 | . 33 |
| Ethylene | 9.7 | 50.9 | . 2159 |
| Helium . | -267.9 | 2.34 | . 0693 |
| Hydrogen | -239.9 | 13.2 | . 0310 |
| Hydrogen bromide | 90 | 84 |  |
| Hydrogen chloride | 51.4 | 84.5 | . 42 |
| Hydrogen iodide . | 151 | 82 | . . . |
| Hydrogen sulfide | 100.4 | 92 | ... |
| Iodine | 553 |  |  |
| Krypton | -63? | $56 ?$ | . 78 ? |
| Mercury | $1460 \pm 20$ | $1640 \pm 50$ | . 5 |
| Methane | -82.5 | 47.4 | . 162 |
| Methyl chloride | 143.1 | 65.8 | . 37 ? |
| Neon . . . . . . . . | -228.7 | 26.8 | . 484 |
| Nitric oxide | -94? | 65 | . 52 ? |
| Nitrogen | -147.1 | 34.7 | . 3110 |
| Nitrous oxide | 36.5 | 71.7 | . 45 ? |
| Oxygen | -118.8 | 51.4 | . 430 |
| Phosgene | 182 | 56 | . 52 |
| Propane | 95.6 | 43 | . . . |
| Radon | 104 | 64.1 | .. |
| Silicon hydride | -3.5 | 49.7 | . . . |
| Sulfur ......... | 1040 |  |  |
| Sulfur dioxide | 157.2 | 80.1 | . 52 ? |
| Sulfur trioxide | 218.3 | 86.5 | . 630 |
| Water | 374.0 | 224.9 | . 4 |
| Xenon | 16.6 | 60.2 | 1.155 |

[^117]TABLE 260.-CONVERSION FACTORS FOR VARIOUS PRESSURE UNITS *

|  | $\underbrace{\text { dyne } / \mathrm{cm}^{2}}$ | ${ }_{10-6}{ }^{\text {bar }}$ | $\underset{0^{\circ} \mathrm{C}}{\mathrm{mmHg}}$ | $\begin{gathered} \text { in. } \mathrm{Hg} \\ 0^{\circ} \mathrm{C} \\ \hline 053 \times 10-5 \end{gathered}$ | millibars | $\mathrm{lb} / \mathrm{in}^{2}{ }^{2}$ | $\begin{gathered} \mathrm{b} / \mathrm{ft}^{2} \\ 2088 \mathrm{t} \times \mathrm{to-3} \end{gathered}$ | $\mathrm{g} / \mathrm{cm}^{2}$ | cm water $20^{\circ} \mathrm{C}$ | in. water $20^{\circ} \mathrm{C}$ | $\underset{9 . \operatorname{atm}}{869 \times 10-7}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} 1 \text { dyne } / \mathrm{cm}^{2} \\ \text { (barye) } \end{array}$ | $=1$ | $10^{-6}$ |  |  | $10^{-3}$ | $1.4506 \times 10^{-5}$ | $2.0883 \times 10^{-3}$ | $1.0197 \times 10^{-3}$ |  |  | $9.869 \times 10^{-7}$ |
| 1 bar | $=10^{\circ}$ | 1 | $7.5006 \times 10^{2}$ | 29.53 | $10^{3}$ | 14.51 | $2.0883 \times 10^{3}$ | $1.0197 \times 10^{3}$ | $1.0216 \times 10^{3}$ | $4.022 \times 10^{2}$ | . 9869 |
| $1 \underset{\text { (Tor) }}{\mathrm{mmHg}}$ | $=1.3332 \times 10^{3}$ | $1.3332 \times 10^{-3}$ | 1 | $3.937 \times 10^{-2}$ | 1.3332 | $1.9339 \times 10^{-2}$ | 2.7847 | 1.3594 | 1.3620 | . 5363 | $1.3157 \times 10^{-8}$ |
| $1 \mathrm{in} . \mathrm{Hg}$ | $=3.386 \times 10^{4}$ | $3.386 \times 10^{-2}$ | 25.400 | 1 | 33.864 | . 4912 | 70.732 | 34.530 | 34.590 | 13.620 | $3.3417 \times 10^{-2}$ |
| 1 millibar | $=10^{3}$ | $10^{-3}$ | . 7501 | $2.953 \times 10^{-2}$ | 1 | $1.4506 \times 10^{-2}$ | 2.0888 | 1.0197 | 1.0216 | . 4022 | $9.869 \times 10^{-4}$ |
| $1 \mathrm{lb} / \mathrm{in}^{2}$ | $=6.894 \times 10^{4}$ | $6.894 \times 10^{-2}$ | 51.71 | 2.0368 | 68.95 | 1 | $1.44 \times 10^{2}$ | 70.30 | 70.43 | 27.731 | $6.804 \times 10^{-2}$ |
| $1 \mathrm{lb} / \mathrm{ft}^{2}$ | $=4.788 \times 10^{2}$ | $4.788 \times 10^{-4}$ | . 3591 | $1.414 \times 10^{-2}$ | . 4788 | $6.945 \times 10^{-8}$ | 1 | . 4882 | . 4891 | . 1926 | $4.725 \times 10^{-4}$ |
| $1 \mathrm{~g} / \mathrm{cm}^{2}$ | $=9.807 \times 10^{2}$ | $9.807 \times 10^{-4}$ | . 7356 | $2.8961 \times 10^{-2}$ | . 9807 | $1.4226 \times 10^{-2}$ | 2.0484 | 1 | 1.0018 | . 3945 | $9.678 \times 10^{-4}$ |
| 1 cm water | $\mathrm{C}=9.789 \times 10^{2}$ | $9.789 \times 10^{-4}$ | . 7342 | $2.891 \times 10^{-2}$ | . 9789 | $1.4198 \times 10^{-2}$ | 2.0446 | . 9981 | 1 | . 3937 | $9.661 \times 10^{-4}$ |
| 1 in . water | $\mathrm{C}=2.486 \times 10^{3}$ | $2.486 \times 10^{-3}$ | 1.865 | $7.343 \times 10^{-2}$ | 2.486 | $3.607 \times 10^{-2}$ | 5.193 | 2.535 | 2.5400 | 1 | $2.453 \times 10^{-8}$ |
| 1 atm | $=1.01325 \times 10^{6}$ | 1.01325 | $7.60 \times 10^{2}$ | 29.921 | $1.0133 \times 10^{3}$ | 14.70 | $2.1164 \times 10^{3}$ | $1.0332 \times 10^{3}$ | $1.0351 \times 10^{3}$ | $4.0758 \times 10^{2}$ | 1 |

* The tahle is based primarily upon the following data and assumptions: a, One atm pressure equals 760 mmHg at $0^{\circ} \mathrm{C}$ under standard gravity of $980.665 \mathrm{~cm} / \mathrm{sec}^{2}$.
b, The density of mercury at $0^{\circ} \mathrm{C}$ is $13.5951 \mathrm{~g} / \mathrm{cm}^{3}$. c, The density of water at $20^{\circ} \mathrm{C}$ is .99820 .


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TABLES 261-267.-THE JOULE-THOMSON EFFECT IN FLUIDS*
The Joule-Thomson effect is defined as the ratio of the change in temperature to the drop in pressure of a fluid driven by the drop in pressure through a porous partial blockage in the fluid flow tube. The space between the reading thermometers on each side of the porous obstruction is to be isolated as to exchange of heat energy but not as to work energy. Nor must the fluid gain a significant amount of directed kinetic energy between the thermometers. Under these circumstances the Joule-Thomson effect, $\mu=\left(\frac{d t}{d p}\right)_{n}$, where $\mathrm{h}=\mathrm{u}-\mathrm{pv}=$ enthalpy, and since $\mu$ is a function of both $t$ and $p$, the steps are preferably represented as infinitesimals. Since $\Delta p$ is always negative, $\mu$ is positive when $\Delta t$ is negative. For all the gases yet measured, $\mu$ is zero along a line in the $t p$ plane called the inversion line.

[^118]TABLE 261.-THE JOULE-THOMSON EFFECT ON AIR (WATER AND CARBON DIOXIDE FREE) ${ }^{83}$
$\mu$ as a function of $t$ and $p, t$ in ${ }^{\circ} \mathrm{C}, p$ in $\operatorname{atm}, \mu$ in ${ }^{\circ} \mathrm{C} / \mathrm{atm}$.

${ }^{83}$ Proc. Amer. Acad. Arts and Sci., vol. 60, p. 535, 1025; vol. 64, p. 287, 1930 (both corrected).

TABLE 262.-THE JOULE-THOMSON EFFECT ON HELIUM ${ }^{81}$
$\mu$ as a function to $t$ (and independent of pressure up to 200 atm ), $t$ in ${ }^{\circ} \mathrm{C}, \mu$ in ${ }^{\circ} \mathrm{C} / \mathrm{atm}$.

| $t^{\circ} \mathrm{C}$ | $-\mu \times 10^{2}$ | $t^{\circ} \mathrm{C}$ | $-\mu \times 10^{2}$ | $t^{\circ} \mathrm{C}$ | $-\mu \times 10^{2}$ | $t^{\circ} \mathrm{C}$ | $-\mu \times 10^{2}$ | $t^{\circ} \mathrm{C}$ | $-\mu \times 10^{2}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 300 | 5.97 | 150 | 6.45 | 50 | 6.31 | -50 | 6.05 | -155 | 5.03 |
| 250 | 6.29 | 100 | 6.38 | 25 | 6.24 | -100 | 5.84 | -180 | 4.12 |
| 200 | 6.41 | 75 | 6.35 | 0 | 6.16 | -140 | 5.40 | -190 | 3.80 |

[^119]$\mu$ as a function of $t$ and $p, t$ in ${ }^{\circ} \mathrm{C}, p$ in atm, $\mu$ in ${ }^{\circ} \mathrm{C} / \mathrm{atm}$.

| $t / p$ | 1 atm | 20 | 60 | 100 | 140 | 180 | 200 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $300^{\circ}$ | . 0643 | . 0607 | . 0530 | . 0445 | . 0370 | . 0370 | . 0276 |
| 250 | . 0980 | . 0910 | . 0785 | . 0665 | . 0555 | . 0485 | . 0468 |
| 200 | . 1377 | . 1280 | . 1102 | . 0950 | . 0823 | . 0715 | . 0675 |
| 150 | . 1845 | . 1720 | . 1485 | . 1285 | . 1123 | . 0998 | . 0945 |
| 125 | . 2105 | . 1980 | . 1707 | . 1480 | . 1300 | . 1153 | . 1100 |
| 100 | . 2413 | . 2277 | . 1975 | . 1715 | . 1490 | . 1320 | . 1255 |
| 75 | . 2695 | . 2557 | . 2285 | . 1993 | . 1710 | . 1505 | . 1415 |
| 50 | . 3220 | . 3015 | . 2650 | . 2297 | . 1947 | . 1700 | . 1580 |
| 25 | . 3720 | . 3490 | . 3077 | . 2628 | . 2213 | . 1850 | . 1745 |
| 0 | . 4307 | . 4080 | . 3600 | . 3010 | . 2505 | . 2050 | . 1883 |
| - 25 | . 5045 | . 4805 | . 4210 | . 3460 | . 2763 | . 2140 | . 1950 |
| - 50 | . 5960 | . 5720 | . 4963 | . 3970 | . 2840 | . 2037 | . 1860 |
| - 75 | . 7100 | . 6895 | . 5910 | . 4225 | . 2480 | . 1537 | . 1215 |
| -87.5 | . 7780 | . 7610 | . 6450 | . 3910 | . 1903 | . 1027 | . 0773 |
| -100 | . 8605 | . 8485 | . 6900 | . 2820 | . 1137 | . 0560 | . 0395 |
| -112.5 | . 9680 | . 9560 | . 6530 | . 1240 | . 0515 | +. 0198 | +. 0087 |
| -125 | 1.112 | 1.102 | . 1250 | +. 0415 | $+.0090$ | -. 0100 | -. 0165 |
| -137.5 | 1.333 | 1.342 | +. 0210 | -. 0020 | -. 0203 | -. 0350 | -. 0402 |
| -150 | 1.812 |  | -. 0025 | -. 0277 | -. 0403 | -. 0595 | -. 0640 |
| -160 | 2.385 |  |  |  |  |  |  |
| -170 | 3.017 |  |  |  |  |  |  |

85 Phys. Rev., vol. 46, p. 785, 1934 (corrected).

TABLE 264.-THE JOULE-THOMSON EFFECT IN NITROGEN ${ }^{86}$
$\mu$ as a function of $t$ and $p, t$ in ${ }^{\circ} \mathrm{C}, p$ in atm, $\mu$ in ${ }^{\circ} \mathrm{C} /$ atm.

| t/b | 1 atm | 20 | 33.5 | 60 | 100 | 140 | 180 | 200 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $300^{\circ} \mathrm{C}$ | . 0140 | . 0096 | . 0050 | -. 0013 | -. 0075 | -. 0129 | -. 0160 | -. 0171 |
| 250 | . 0331 | . 0256 | . 0230 | $+.0160$ | +. 0071 | +.0009 | -. 0037 | -. 0058 |
| 200 | . 0558 | . 0472 | . 0430 | . 0372 | . 0262 | . 0168 | $+.0094$ | $+.0070$ |
| 150 | . 0868 | . 0776 | . 0734 | . 0628 | . 0482 | . 0348 | . 0248 | . 0228 |
| 125 | . 1070 | . 0973 | . 0904 | . 0786 | . 0621 | . 0459 | . 0347 | . 0326 |
| 100 | . 1292 | . 1173 | . 1100 | . 0975 | . 0768 | . 0582 | . 0462 | . 0419 |
| 75 | . 1555 | . 1421 | . 1336 | . 1191 | . 0941 | . 0740 | . 0583 | . 0543 |
| 50 | . 1855 | . 1709 | . 1621 | . 1449 | . 1164 | . 0915 | . 0732 | . 0666 |
| 25 | . 2217 | . 2060 | . 1961 | . 1729 | . 1400 | . 1105 | . 0874 | . 0779 |
| 0 | . 2656 | . 2494 | . 2377 | . 2088 | . 1679 | . 1316 | . 1015 | . 0891 |
| - 25 | . 3224 | . 3013 | . 2854 | . 2528 | . 2001 | . 1506 | . 1101 | . 0932 |
| - 50 | . 3968 | . 3734 | . 3467 | . 3059 | . 2332 | . 1676 | . 1120 | . 0909 |
| - 75 | . 5033 | . 4671 | . 4318 | . 3712 | . 2682 | . 1735 | . 1026 | . 0800 |
| - 87.5 | . 5710 | . 5247 | . 4854 | . 4096 | . 2808 | . 1619 | . 0933 | . 0733 |
| -100 | . 6490 | . 5958 | . 5494 | . 4506 | . 2754 | . 1373 | . 0765 | . 0587 |
| -112.5 | . 7430 | . 6841 | . 6208 | . 4923 | . 2254 | . 0932 | . 0488 | . 0346 |
| -125 | . 8557 | . 7948 | . 7025 | . 4940 | . 1314 | . 0498 | $+.0167$ | $+.0032$ |
| -137.5 | . 9972 | . 9364 | . 7964 | . 2364 | . 0638 | +. 0177 | -. 0181 | -. 0175 |
| -150 | 1.2659 | 1.1246 | . 1704 | . 0601 | +. 0202 | $-.0056$ | -. 0211 | -. 0284 |
| -160 | 1.6328 | +. 0724 | +. 0311 | $+.0068$ | -. 0088 | -. 0175 | -. 0263 | -. 0315 |
| -170 | 2.0048 | -. 0108 | -. 0382 |  |  |  |  |  |
| -180 | 2.3923 |  |  |  |  |  |  |  |

[^120]TABLE 265.-THE JOULE-THOMSON EFFECT ON MIXTURES OF HELIUM AND ARGON $\left(\mu \times 10^{2}\right)^{87}$
$\mu$ as a function of $t$ and $p, t$ in ${ }^{\circ} \mathrm{C}, p$ in atm, $\mu$ in ${ }^{\circ} \mathrm{C} / \mathrm{atm}$.

| $t^{\circ} \mathrm{C} / \mathrm{p}$ | 1 | $\underset{20}{\text { Mixture }}$ | No. 1; $\underset{60}{\mathrm{He}} 75.8$ | $\begin{gathered} \text { percent, } A \\ 100 \end{gathered}$ | $\begin{gathered} 24.2 \text { percent } \\ 140 \end{gathered}$ | 180 | 200 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 250 | $-5.83$ | -5.95 | -6.15 | -6.37 | -6.56 | -6.77 | -6.85 |
| 200 | 5.55 | 5.66 | 5.90 | 6.13 | 6.34 | 6.55 | 6.63 |
| 150 | 5.11 | 5.24 | 5.52 | 5.77 | 5.99 | 6.21 | 6.34 |
| 100 | 4.47 | 4.61 | 4.91 | 5.18 | 5.45 | 5.72 | 5.88 |
| 50 | 3.61 | 3.76 | 4.08 | 4.40 | 4.68 | 5.01 | 5.19 |
| 0 | 2.40 | 2.57 | 2.92 | 3.30 | 3.65 | 4.03 | 4.22 |
| - 50 | -. 69 | -. 92 | -1.32 | $-1.75$ | 2.21 | 2.66 | 2.82 |
| $-100$ | $+3.37$ | +2.82 | +1.87 | + . 79 | - . 14 | -. 65 | $-.78$ |
|  |  | Mixture No. 2; He 50.6 percent, A 49.4 percent |  |  |  |  |  |
| 250 | $-2.84$ | -3.19 | -3.65 | -4.04 | -4.21 | -4.33 | -4.34 |
| 200 | 1.67 | 2.07 | 2.71 | 3.15 | 3.40 | 3.55 | 3.57 |
| 150 | $-.13$ | -. 67 | -1.50 | 2.01 | 2.32 | 2.56 | 2.62 |
| 100 | $+1.84$ | +1.15 | +.11 | -. 59 | $-1.01$ | -1.32 | 1.48 |
| 50 | 4.50 | 3.66 | 2.37 | $+1.39$ | $+.70$ | $+.14$ | $-.07$ |
| 0 | 8.19 | 7.20 | 5.51 | 4.12 | 2.96 | 1.99 | +1.57 |
| $-50$ | 13.84 | 12.61 | 10.27 | 8.14 | 6.28 | 4.53 | 3.63 |
| $-100$ |  |  | +17.79 | +14.17 | +10.36 | +6.90 | +5.40 |
| Mixture No. 3; He 33.5 percent, A 66.5 percent |  |  |  |  |  |  |  |
| 250 | $+1.34$ | + . 72 | -. 38 | -1.03 | -1.48 | -1.68 | -1.68 |
| 200 | 2.94 | 2.32 | $+1.25$ | $+.45$ | -. 13 | -. 38 | -. 38 |
| 150 | 5.05 | 4.41 | 3.23 | 2.22 | +1.41 | +. 92 | $+.83$ |
| 100 | 7.80 | 7.10 | 5.69 | 4.55 | 3.63 | 2.86 | 2.54 |
| 50 | 12.12 | 11.28 | 9.40 | 7.73 | 6.32 | 5.41 | 5.01 |
| 0 | 18.40 | 17.18 | 14.43 | 12.05 | 9.88 | 7.93 | 6.88 |
| - 50 | 27.90 | 25.82 | 21.93 | 17.96 | 13.83 | 9.63 | 7.73 |
| $-100$ | 43.30 | 41.15 | 34.30 | 27.20 | 17.55 | 10.07 | 7.10 |
| Mixturc No. 4; He 16.6 percent, A 83.4 percent |  |  |  |  |  |  |  |
| 250 | 5.75 | 5.15 | 3.85 | 2.70 | 1.90 | 1.20 | . 95 |
| 200 | 8.45 | 7.63 | 6.05 | 4.75 | 3.85 | 3.00 | 2.60 |
| 150 | 11.70 | 10.80 | 8.95 | 7.45 | 6.10 | 5.20 | 4.60 |
| 100 | 15.50 | 14.50 | 12.60 | 10.80 | 9.05 | 7.70 | 7.05 |
| 50 | 21.05 | 20.10 | 17.75 | 15.35 | 13.00 | 10.65 | 9.55 |
| 0 | 29.85 | 28.49 | 25.00 | 21.15 | 17.35 | 14.50 | 13.05 |
| - 50 | 44.15 | 41.80 | 36.15 | 30.10 | 22.90 | 17.55 | 15.60 |
| $-100$ | 70.80 | 66.10 | 51.00 | 29.95 | 19.75 | 11.35 | 8.00 |

${ }^{87}$ Journ. Chem. Phys., vol. 8, p. 627, 1940.
TABLE 266.-THE JOULE-THOMSON EFFECT IN CARBON DIOXIDE ${ }^{88}$
$\mu$ as a function of $t$ and $p, t$ in ${ }^{\circ} \mathrm{C}, p$ in atm, $\mu$ in ${ }^{\circ} \mathrm{C} / \mathrm{atm}$.

| $t / p$ | 1 atm | 20 | 60 | 73 | 100 | 140 | 180 | 200 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 300 | .2650 | .2425 | .2080 | .2002 | .1872 | .1700 | .1540 | .1505 |
| 250 | .3075 | .2885 | .2625 | .2565 | .2420 | .2235 | .2045 | .1975 |
| 200 | .3770 | .3575 | .3400 | .3325 | .3150 | .2890 | .2600 | .2455 |
| 150 | .4890 | .4695 | .4430 | .4380 | .4155 | .3760 | .3102 | .2910 |
| 125 | .5600 | .5450 | .5160 | .5069 | .4750 | .4130 | .3230 | .2915 |
| 100 | .6490 | .6375 | .6089 | .5920 | .5405 | .4320 | .3000 | .2555 |
| 90 | .6900 | .6785 | .6507 | .6309 | .5680 | .4290 | .2738 | .2300 |
| 80 | .7350 | .7240 | .6955 | .6725 | .5973 | .4050 | .2343 | .1960 |
| 70 | .7855 | .7750 | .7465 | .7175 | .6192 | .3505 | .1875 | .1600 |
| 60 | .8375 | .8325 | .8060 | .7675 | .6250 | .2625 | .1405 | .1245 |
| 50 | .8950 | .8950 | .8800 | .8225 | .5570 | .1720 | .1025 | .0930 |
| 40 | .9575 | .9655 | .9705 | .8769 | .2620 | .1075 | .0723 | .0660 |
| 30 | 1.0265 | 1.0430 | 1.0835 | .2870 | .1215 | .0678 | .0495 | .0445 |
| 20 | 1.1050 | 1.1355 | .1435 | .1075 | .0700 | .0420 | .0320 | .0272 |
| 10 | 1.1910 | 1.2520 | .0720 | .0578 | .0407 | .0235 | $.018 ?$ | .0142 |
| 0 | 1.2900 | 1.4020 | .0370 | .0310 | .0215 | .0115 | .0085 | .0045 |
| -25 | 1.6500 | .0000 | -.0028 | -.0039 | -.0050 | -.0062 | -.0080 | -.0115 |
| -50 | 2.4130 | -.0140 | -.0150 | -.0165 | -.0160 | -.0183 | -.0228 | -.0248 |
| -75 |  | -.0200 | -.0200 | -.0232 | -.0228 | -.0240 | -.0250 | -.0290 |

[^121]TABLE 267.-THE JOULE-THOMSON EFFECT IN MIXTURES OF HELIUM AND NITROGEN $\left(\mu \times 10^{2}\right)^{80}$
$\mu$ as a function of $t$ and $p, t$ in ${ }^{\circ} \mathrm{C}, p$ in atm, $\mu$ in ${ }^{\circ} \mathrm{C} / \mathrm{atm}$.


[^122]TABLE 268.—COMPRESSIBILITY OF LIQUIDS ${ }^{\text {º }}$
Part 1.—Relative volumes

|  | Ethyl alcohol $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{OH}$ |  | Isobutyl alcohol $\mathrm{C}_{4} \mathrm{H}_{0} \mathrm{OH}$ |  | Ether $\left(\mathrm{C}_{2} \mathrm{H}_{5}\right)_{2} \mathrm{O}$ |  | n-Proply alcohol $\mathrm{C}_{3} \mathrm{H}_{7} \mathrm{OH}$ |  | Amyl alcohol $\mathrm{C}_{5} \mathrm{H}_{11} \mathrm{OH}$ |  | Ethyl iodide $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{I}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| atm | 20 | $80^{\circ} \mathrm{C}$ | 20 | $80^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $80^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $80^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $80^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $80^{\circ} \mathrm{C}$ |
| 1 | 1.0212 | 1.0934 | 1.0195 | 1.0880 | $1.0315^{\circ}$ |  | 1.0173 | 1.0865 | 1.0181 | . 0814 | 1.0214 | . 0935 |
| 500 | . 9782 | 1.0319 | . 9740 | 1.0262 | . 9668. | . 0369 | . 9770 | 1.0305 | . 9788 | 1.0288 | . 9774 | 1.0351 |
| 1000 | . 9479 | . 9922 | . 9470 | . 9883 | . 9337 | . 9874 | . 9483 | . 9913 | . 9511 | . 9915 | . 9475 | . 9946 |
| 2000 | . 9059 | . 9380 | . 9078 | . 9385 | . 8850 | . 9189 | . 9124 | . 9424 | . 9138 | . 9427 | . 9070 | . 9397 |
| 3000 | . 8760 | . 9025 | . 8798 | . 9052 | . 8503 | . 8776 | . 8876 | . 9120 | . 8869 | . 9110 | . 8777 | . 9034 |
| 4000 | . 8517 | . 8756 | . 8575 | . 8802 | . 8246 | . 8481 | . 8677 | . 8893 | . 8658 | . 8877 | . 8555 | . 8760 |
| 6000 | . 8149 | . 8354 | . 8242 | . 8433 | . 7883 | . 8070 | . 8365 | . 8548 | . 8348 | . 8531 | . 8207 | . 8381 |
| 8000 | . 7888 | . 8061 | . 8001 | . 8181 | . 7613 | . 7779 | . 8138 | . 8301 | . 8116 | . 827.3 | . 7937 | . 8099 |
| 10,000 | . 7671 | . 7830 | . 7802 | . 7976 | . 7380 | . 7535 | . 7958 | . 8114 | . 7918 | . 8060 | . 7725 | . 7877 |
| 12,000 | . 7485 | . 7648 | $.7631^{\circ}$ | . 7799 | . 7178 | . 7326 | .7814 | . 7952 | .7754 | . 7902 | .7554 | . 7706 |
|  | $\begin{aligned} & \text { Phosp } \\ & \text { chlor } \end{aligned}$ | $\mathrm{PCl}_{3}$ | C | OH | $\mathrm{C}$ |  |  |  | C |  |  |  |
| m | $20^{\circ} \mathrm{C}$ | $80^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $80^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $80^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $80^{\circ} \mathrm{C}$ | $0^{\circ} \mathrm{C}$ | $80^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $80^{\circ} \mathrm{C}$ |
| 1 | 1.0234 | 1.103 ) | 1.0238 | 1.1005 |  |  | 1.0235 | 1.1092 | 1.0275 |  | 1.0279 |  |
| 500 | . 9852 | 1.0443 | . 9811 | 1.0400 | . 9696 | 1.0358 | . 9854 | 1.0458 | . 9776 |  | . 9818 |  |
| 1000 | . 9577 | 1.0040 | . 9494 | . 9993 | . 9253 | . 9797 | . 9567 | 1.0061 | . 9460 | . 9988 | . 9526 | 1.0082 |
| 2000 | . 9184 | . 9531 | . 9064 | . 9429 | . 8749 | . 9128 | . 9151 | . 9525 | . 9022 | . 9381 | . 9076 | . 9467 |
| 3000 | . 8902 | . 9192 | . 8763 | . 9065 | . 8415 | . 8715 | . 8852 | . 9154 | . 8714 | . 9020 | . 8748 | . 9073 |
| 4000 | . 8679 | . 8933 | . 8523 | . 8782 | . 8167 | . 8422 | . 8620 | . 8870 | . 8479 | . 8742 | . 8504 | . 8786 |
| 6000 | . 8348 | . 8561 | . 8163 | . 8381 | . 7796 | . 8008 | . 8265 | . 8468 | . 8131 | . 8339 | . 8143 | . 8370 |
| 8000 | . 8105 | . 8292 | . 7907 | . 8102 | . 7533 | . 7728 | . 7990 | . 8188 | . 7868 | . 8056 | . 7866 | . 8066 |
| 10,000 | . 7902 | . 8077 | . 7696 | . 7875 | . 7320 | . 7501 | . 7774 | . 7962 | . 7656 | . 7825 | freezes | . 7821 |
| 12,000 | . 7741 | . 7898 | . 7527 | . 7709 | . 7148 | . 7301 | . 7609 | . 7758 | . 7495 | .7648 | " | . 7617 |

Part 2.- $\beta=\left(1 / V_{0}\right)(d V / d P)$

| Substance | Temp ${ }^{\circ} \mathrm{C}$ | Pressure megabaryes | Compressibility per mega. baryes $\beta \times 10^{9}$ | Substance | Pressure <br> mega- <br> Temp ${ }^{\circ} \mathrm{C}$ baryes | Compressibility per megabaryes $\beta \times 10^{6}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Benzene | . 17 | 5 | 89 | Mercury | 221,000 | 3.91 |
|  | 20 | 200 | 77 |  | 22 12,000 | 2.37 |
|  | 20 | 400 | 67 | Oils: almond | . 155 | 53 |
| Chloroform | . 20 | 200 | 83 | castor | .. 15 | 46 |
|  | 20 | 400 | 70 | linseed | .. 15 | 51 |
| Glycerine | . 15 | 5 | 22 | olive | .. 15 | 55 |
| Kerosene | . 20 | 500 | 55 | rapeseed | . 20 | 59 |
|  | 20 | 1,000 | 45 | Toluene . . . | . 20200 | 74 |
|  | 20 | 12,000 | 8 |  | $20 \quad 400$ | 64 |
| Mercury | . 20 | 300 | 3.95 | Turpentine | . 20 | 74 |
|  | 22 | 500 | 3.97 |  |  |  |

[^123] 49, p. 3, 1913.

TABLE 269.-RELATIVE VOLUMES OF WATER FOR DIFFERENT PRESSURES ${ }^{\text {®1 }}$

| Pressure <br> $\mathrm{kg} / \mathrm{cm}^{2}$ <br> 0 | $\overbrace{0}$$0^{\circ} \mathrm{C}$ <br> 1.0000 | $50^{\circ} \mathrm{C}$ | $95^{\circ} \mathrm{C}$ |
| ---: | ---: | ---: | ---: |
| 500 | .9771 |  |  |
| 1,000 | .9567 | .9741 | .9984 |
| 1,500 | .9396 | .9582 | .9812 |
| 2,000 | .9248 | .9439 | .9661 |
| 3,000 | .8996 | .9201 | .9409 |
| 4,000 | .8795 | .8997 | .9194 |
| 5,000 | .8626 | .8824 | .9009 |
| 6,000 |  | .8668 | .8849 |
| 7,000 |  | .8530 | .8705 |
| 8,000 |  | .8407 | .8577 |
| 9,000 | .8296 | .8461 |  |
| 10,000 |  | .8192 | .8352 |
| 11,000 |  |  | .8256 |

TABLE 270.-RELATIVE VOL. UMES OF ETHER FOR DIF. FERENT PRESSURES ${ }^{\text {M }}$

| $\underset{\mathrm{kg}^{2} / \mathrm{cm}^{2}}{ }$ | Temperatures |  |
| :---: | :---: | :---: |
|  | $30^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ |
| 0 | 1.0495 |  |
| 500 | . 9761 |  |
| 1,000 | . 9364 |  |
| 1,500 | . 9085 |  |
| 2,000 | . 8858 |  |
| 2,500 | . 8671 | . 8909 |
| 3,000 | . 8511 | . 8726 |
| 4,000 | . 8255 | . 8446 |
| 5,000 | . 8055 | . 8225 |
| 6,000 | . 7888 | . 8038 |
| 7,000 | . 7742 | . 7884 |
| 8,000 | . 7616 | . 7747 |
| 9,000 | . 7504 | . 7629 |
| 10,000 | . 7399 | . 7519 |
| 11,000 | . 7305 | . 7418 |
| 12,000 | . 7225 | . 7329 |

${ }^{91}$ Bridgman, P. W., Proc. Amer. Acad. Arts and Sci., vol. 66, p. 219, 1931.

## TABLE 271.-COMPRESSIBILITY OF SOLIDS

If $V$ is the volume of the material under a pressure $P$ megabaryes and $V_{0}$ is the volume at atmospheric pressure, then the compressibility $\beta=-\left(1 / V_{0}\right)(d V / d P)$. Its unit is $\mathrm{cm}^{2} /$ megadynes (reciprocal megabaryes). $10^{6} / \beta$ is the bulk modulus in absolute units (dynes $/ \mathrm{cm}^{2}$ ). The following values of $\beta$, arranged in order of increasing compressibility, are for $P=0$ and room temperature. 1 megabarye $=10^{6}$ dynes $/ \mathrm{cm}^{2}=1.020 \mathrm{~kg} / \mathrm{cm}^{2}=$ 0.987 atm .

| Substance | $\begin{gathered} \text { Compression } \\ \text { per unit } \\ \text { vol. per } \\ \text { megabarye } \\ \times 10^{6} \end{gathered}$ | Bulk modulus, dynes/ $\mathrm{cm}^{2} \times 10^{12}$ | Substance | $\begin{gathered} \text { Compression } \\ \text { per unit } \\ \text { vol. per } \\ \text { megabarye } \\ \times 10^{8} \end{gathered}$ | Bulk modulus, dynes/ $\mathrm{cm}^{2} \times 10^{12}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Tungsten | . 27 | 3.7 | Gallium | 2.09 | . 48 |
| Boron | . 3 | 3.0 | Cadmium | 2.17 | . 46 |
| Silicon | . 32 | 3.1 | Plate glass | 2.23 | . 45 |
| Platinum | . 38 | 2.6 | Lead . . | 2.27 | . 44 |
| Nickel | . 43 | 23 | Thallium | 2.3 | . 43 |
| Molybdenum | . 46 | 2.2 | Antimony | 2.4 | . 42 |
| Tantalum .. | . 53 | 1.9 | Quartz . | 2.7 | . 37 |
| Palladium | . 54 | 1.9 | Magnesium | 2.9 | . 34 |
| Cobalt | . 55 | 1.82 | Bismuth . . | - 30 | . 33 |
| Nichrome | . 56 | 1.79 | Graphite | 3.0 | . 33 |
| Iron | . 60 | 1.67 | Silica glass | 3.1 | . 32 |
| Gold | . 60 | 1.67 | Arsenic . . | 4.5 | . 22 |
| Pyrite | . 7 | 1.4 | Calcium | . 5.7 | . 175 |
| Copper | . 75 | 1.33 | Strontium | . 8.4 | . 120 |
| Manganese | . 84 | 1.19 | Phosphorus (red) | - 9.2 | . 109 |
| Brass | . 89 | 1.12 | Selenium ....... | . 12.0 | . 083 |
| Chromium | . 9 | 1.12 | Ice . . . . . . . . . . . | . 120 | . 083 |
| Silver | . 99 | 1.01 | Sulfur .......... | . . 12.9 | . 078 |
| Mg. silicate, | 1.03 | . 91 | Iodine . . . . . . . . | . 13.0 | . 077 |
| Mg . silicate | 1.21 | . 82 | Sodium | . 15.6 | . 064 |
| Aluminum | 1.33 | . 75 | Hard rubber . . . . . | . 19.4 |  |
| Calcite | 1.39 | . 72 | Phosphorus (white) | ) 20.5 | . 049 |
| Tin | . 1.89 | . 53 |  |  |  | PETROLEUM OILS ${ }^{92}$

It was found that the compressibility and thermal expansion of two samples of the same specific gravity, but from different sources, differed more than 30 percent at the higher temperatures, whereas oils of the same specific gravity and the same viscosity had the same compressibility and thermal expansion within rather narrow limits. In other words, with a knowledge of the specific gravity and viscosity of the oils, it was possible to represent all the measured volumes within less than .5 percent over the entire range of temperature and pressure covered by the measurements.

| Kinematic viscosity $100^{\circ} \mathrm{F}$, cgs | $\begin{gathered} \text { Specific } \\ \text { gravity } \\ 60^{\circ} / 60^{\circ} \mathrm{F} \end{gathered}$ | Pressure $\mathrm{kg} / \mathrm{cm}^{2}$ | Relative volumes |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $0^{\circ} \mathrm{C}$ | $20^{\circ}$ | $50^{\circ}$ | $100^{\circ}$ | $200^{\circ}$ | $300^{\circ}$ | $400^{\circ}$ |
| . 020 | . 80 | 0 | 1.000 | 1.018 | 1.045 | 1.096 | 1.222 | 1.422 |  |
| " |  | 50 | . 996 | 1.014 | 1.041 | 1.089 | 1.205 | 1.370 | (1.63) |
| " | . 85 | 0 | 1.000 | 1.017 | 1044 | 1.093 | 1.213 | 1.396 | (1.71) |
| " |  | 50 | . 997 | 1.014 | 1.040 | 1.086 | 1.197 | 1.352 | (1.58) |
| " | . 90 | 0 | 1.000 | 1.017 | 1.043 | 1.090 | 1.204 | 1.375 | (1.67) |
| " | . | 50 | . 997 | 1.013 | 1.038 | 1.084 | 1.191 | 1.337 | (1.55) |
| . 050 | . 80 | 0 | 1.000 | 1.017 | 1.043 | 1.089 | 1.202 | 1.369 | (1.71) |
| " | " | 50 | . 997 | 1.013 | 1.038 | 1.083 | 1.189 | 1.333 | (1.56) |
| " | . 85 | 0 | 1.000 | 1.016 | 1.041 | 1.087 | 1.194 | 1.349 | (1.63) |
| " | 4 | 50 | . 997 | 1.013 | 1.037 | 1.081 | 1.182 | 1.318 | (1.51) |
| " | . 90 | 0 | 1.000 | 1.016 | 1.040 | 1.084 | 1.188 | 1.331 | (1.56) |
| " |  | 50 | . 997 | 1.012 | 1.036 | 1.078 | 1.176 | 1.304 | (1.48) |
| . 100 | . 85 | 0 | 1.000 | 1.016 | 1.040 | 1.083 | 1.185 | 1.325 | (1.54) |
| " |  | 50 | . 997 | 1.012 | 1.036 | 1.078 | 1.174 | 1.299 | (1.47) |
| " | . 95 | 0 | 1.000 | 1.015 | 1.038 | 1.079 | 1.174 | 1.297 | (1.47) |
| " |  | 50 | . 997 | 1.012 | 1.034 | 1.074 | 1.164 | 1.276 | (1.43) |
| . 500 | . 85 | 0 | 1.000 | 1.015 | 1.038 | 1.078 | 1.170 | 1.289 | (1.45) |
| " |  | 50 | . 997 | 1.012 | 1.034 | 1.073 | 1.161 | 1.269 | (1.41) |
| " | . 95 | 0 | 1.000 | 1.014 | 1.036 | 1.074 | 1.161 | 1.269 | (1.40) |
| " |  | 50 | . 998 | 1.012 | 1.033 | 1.070 | 1.152 | 1.252 | (1.37) |
| 1.000 | . 85 | 0 | 1.000 | 1.015 | 1.037 | 1.076 | 1.165 | 1.279 | (1.43) |
|  |  | 50 | . 997 | 1.012 | 1.034 | 1.071 | 1.157 | 1.260 | (1.39) |
| " | . 95 | 0 | 1.000 | 1.014 | 1.035 | 1.073 | 1.157 | 1.261 | (1.39) |
| " | " | 50 | . 998 | 1.011 | 1.032 | 1.068 | 1.149 | 1.244 | (1.36) |
| 2.000 | . 85 | 0 | 1.000 | 1.014 | 1.036 | 1.075 | 1.162 | 1.270 | (1.41) |
|  |  | 50 | . 998 | 1.011 | 1.033 | 1.070 | 1.153 | 1.253 | (1.37) |
| " | . 95 | 0 | 1.000 | 1.014 | 1.035 | 1.071 | 1.153 | 1.254 | (1.37) |
| " |  | 50 | . 998 | 1.011 | 1.032 | 1.067 | 1.145 | 1.239 | (1.35) |
| 5.000 | . 85 | 0 | 1.000 | 1.014 | 1.035 | 1.073 | 1.157 | 1.261 | (1.39) |
| " | " | 50 | . 998 | 1.011 | 1.032 | 1.068 | 1.149 | 1.245 | (1.36) |
| " | . 95 | 0 | 1.000 | 1.013 | 1.034 | 1.069 | 1.148 | 1.244 | (1.36) |
| " | " | 50 | . 998 | 1.011 | 1.031 | 1.065 | 1.141 | 1.229 | (1.33) |
| $210^{\circ} \mathrm{F}$, cgs | $60^{\circ} / 60^{\circ} \mathrm{F}$ | $\mathrm{kg} / \mathrm{cm}^{2}$ | $0^{\circ} \mathrm{C}$ | $20^{\circ}$ | $50^{\circ}$ | $100^{\circ}$ | $200^{\circ}$ | $300^{\circ}$ | $400^{\circ}$ |
| . 100 | . 90 | 0 | 1.000 | 1.014 | 1.036 | 1.074 | 1.161 | 1.269 | (1.41) |
| " |  | 50 | . 998 | 1.011 | 1.032 | 1.070 | 1.152 | 1.252 | (1.37) |
| " | . 95 | 0 | 1.000 | 1.014 | 1.035 | 1.071 | 1.154 | 1.256 | (1.38) |
| " | " | 50 | . 998 | 1.011 | 1.032 | 1.067 | 1.147 | 1.241 | (1.35) |
| " | 1.00 | 0 | 1.000 | 1.014 | 1.034 | 1.070 | 1.149 | 1.247 | (1.37) |
| " | " | 50 | . 998 | 1.011 | 1.031 | 1.066 | 1.142 | 1.232 | (1.34) |
| . 200 | . 90 | 0 | 1.000 | 1.014 | 1.035 | 1.072 | 1.155 | 1.258 | (1.39) |
| " | , | 50 | . 998 | 1.011 | 1.031 | 1.067 | 1.147 | 1.241 | (1.35) |
| " | 1.00 | 0 | 1.000 | 1.013 | 1.033 | 1.067 | 1.144 | 1.237 | (1.35) |
| " |  | 50 | . 998 | 1.011 | 1.030 | 1.064 | 1.137 | 1.223 | (1.32) |
| . 440 | . 90 | 0 | 1.000 | 1.013 | 1.034 | 1.070 | 1.151 | 1.248 | (1.36) |
| " | " | 50 | . 998 | 1.011 | 1.031 | 1.066 | 1.143 | 1.234 | (1.34) |
| " | 1.00 | 0 | 1.000 | 1.012 | 1.032 | 1.066 | 1.140 | 1.228 | (1.33) |
| " | " | 50 | . 998 | 1.010 | 1.029 | 1.063 | 1.134 | 1.214 | (1.31) |
| 1.100 | . 90 | 0 | 1.000 | 1.013 | 1.033 | 1.068 | 1.146 | 1.241 | (1.35) |
| " | " | 50 | . 998 | 1.010 | 1.030 | 1.065 | 1.139 | 1.225 | (1.33) |
| " | 1.00 | 0 | 1.000 | 1.012 | 1.031 | 1.063 | 1.134 | 1.218 | (1.32) |
| " | " | 50 | . 998 | 1.010 | 1.028 | 1.060 | 1.128 | 1.205 | (1.29) |

${ }^{92}$ Jessup, R. S., Nat. Bur. Standards Journ. Res., vol. 5, p. 985, 1930.
$-\Delta V^{Y} / V_{0}=a P-b P^{2}$, where $P$ is in bars $\left(10^{8}\right.$ dyne $\left./ \mathrm{cm}^{2}\right)$ and $V_{0}$ is the volume at 1 atm and $30^{\circ} \mathrm{C}$ (or room temp.). Pressure range, $1-12,000$ bars urless otherwise noted. $a=\beta_{0}=$ initial compressibility. Sce also Table 271.


[^124] WITH PRESSURE ${ }^{\text {®s }}$

|  | $\begin{aligned} & E \\ & \underset{y}{E} \\ & \hline \end{aligned}$ | $\begin{aligned} & \underline{3} \\ & \dot{B} \\ & \text { n } \end{aligned}$ | $\begin{aligned} & E \\ & \cdot \vec{H} \\ & \text { N } \\ & \text { N } \\ & 0 \end{aligned}$ |  | $\begin{aligned} & E \\ & \stackrel{y}{n} \\ & U \end{aligned}$ | 忽 | $\begin{aligned} & E \\ & \text { E } \\ & \text { E } \\ & \text { ت } \\ & \text { N } \end{aligned}$ | $\underset{\sim}{\underset{\sim}{E}}$ |  | $\begin{aligned} & E \\ & \overrightarrow{3} \\ & \text { 은 } \\ & \text { N } \end{aligned}$ | E E تِ ت ت | E |  |  | $\begin{aligned} & \text { E } \\ & \text { E } \\ & \text { 표 } \\ & \text { D } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2,500 | . 0204 | . 0334 | . 0677 | . 0696 | . 0999 | . 0024 | . 0027 | . 0040 | . 0040 | . 0026 | . 0100 | . 0109 | . 0090 | . 0078 | . 0024 |
| 5,000 | . 0389 | . 0624 | . 1152 | . 1224 | . 1585 | . 0047 | . 0052 | . 0079 | . 0078 | . 0054 | . 0194 | . 0234 | . 0174 | . 0152 | . 0048 |
| 10,000 | . 0715 | . 1115 | . 1862 | . 1982 | . 2392 | . 0094 | . 0099 | . 0154 | . 0152 | . 0111 | . 0370 | . 0549 | . 0329 | . 0289 | . 0095 |
| 15,000 | . 1005 | . 1511 | . 2374 | . 2506 | . 2981 | . 0139 | . 0143 | . 0225 | . 0213 | . 0168 | . 0526 | . $1655 \ddagger$ | . 0471 | . 0416 | . 0139 |
| 20,000 | . 1261 | . 1836 | . 2772 | . 2920 | . 3442 | . 0181 | . 0185 | . 0293 | . 0268 | . 0220 | . 0665 | . 1864 | . 0604 | . 0536 | . 0181 |
| 25,000 | . 1485 | . 2111 | . 3093 | . 3254 | . $3908 *$ | . 0219 | . 0224 | . 0358 | . 0323 | . 0267 | . $0827 \dagger$ | . 2027 | . 0729 | . 0650 | . 0219 |
| 30,000 | . 1689 | . 2350 | . 3360 | . 3530 | . 4261 | . 0256 | . 0261 | . 0420 | . 0375 | . 0312 | . 0952 | . 2154 | . 0848 | . 0757 | . 0255 |
| 35,000 | . 1872 | . 2559 | . 3584 | . 3760 | . 4559 | . 0294 | . 0297 | . 0480 | . 0426 | . 0356 | . 1072 | . 2257 | . 0961 | . 0858 | . 0290 |
| 40,000 | . 2040 | . 2740 | . 3774 | . 3954 | . 4816 | . 0329 | . 0332 | . 0537 | . 0476 | . 0399 | . 1189 | . 2342 | . 1069 | . 0955 | . 0324 |

[^125]| Pres. sure |  | $\begin{gathered} \begin{array}{c} \mathrm{NH}_{4} \mathrm{Br} \\ \mathrm{~cm}^{3} / 2.548 \mathrm{~g} \end{array} \\ \hline \end{gathered}$ | $\begin{gathered} \begin{array}{c} \mathrm{NH}_{1} \mathrm{I} \\ \mathrm{~cm}^{3} / 2.887 \mathrm{~g} \\ \hline \end{array} \\ \hline \end{gathered}$ | $\overbrace{}^{\begin{array}{c} \mathrm{AgCl} \\ \mathrm{~cm}^{3} / 5.589 \mathrm{~g} \end{array}}$ | $\overbrace{}^{\begin{array}{c} \mathrm{AgBr} \\ \mathrm{~cm}^{9} / 6.548 \mathrm{~g} \end{array}}$ | $\begin{gathered} \mathrm{AgI} \\ \mathrm{~cm}^{3} / 5.709 \mathrm{~g} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{kg} / \mathrm{cm}^{2}$ | $20^{\circ} \mathrm{C}-78.8^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}-78.8^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}-78.8^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}-78.8^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}-78.8^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}-78.8^{\circ} \mathrm{C}$ |
| 5,000 | . 0269 . 0217 | . 0257 . 0244 | . 0316 . 0321 | . 0113 . 0107 | . 0111 . 0103 | .1769* .1753* |
| 10,000 | . 0489.0395 | . 0487.0462 | . 0590.0582 | . 0216 . 0207 | . 0215 . 0202 | . 1896.1868 |
| 15,000 | . 0668 . 0545 | . 0694.0656 | . 0822.0804 | . 0312 . 0301 | . 0313 . 0297 | . 2001.1969 |
| 20,000 | . 0818.0675 | . 0880 . 0829 | . 1019.0989 | . 0401 . 0389 | . 0404.0386 | . 2095.2061 |
| 25,000 | . 0949.0794 | . 1049.0984 | . 1188 . 1144 | . 0484 . 0471 | . 0496.0476 | .2180 .2145 |
| 30,000 | . 1070.0906 | . 1203.1124 | . 1332.1279 | . 0562.0549 | . 0584.0562 | . 2257.2222 |
| 35,000 | . 1176.1010 | . 1340 . 1250 | . 1456.1397 | . 0634 . 0621 | . 0665 . 0641 | . 2326.2291 |
| 40,000 | . 1278.1111 | . 1465.1364 | . 1570.1504 | . 0704.0690 | . 0743 . 0716 | . 2396.2362 |
| 45,000 | . 1372.1207 | . 1576.1466 | . 1676.1608 | . 0772.0755 | . 0818.0789 | . 2462.2428 |
| 50,000 | . 1462.1301 | . 1676.1557 | . 1775.1702 | . 0838.0818 | .0890 . 0858 | . 2525.2490 |



[^126]Part 1.- $\Delta V / V_{0}=a P-b P^{2}$ where $P$ is in bars ( $10^{6} d y n e / \mathrm{cm}^{2}$ ) and $V_{0}$ is the volume at 1 atm and $30^{\circ} \mathrm{C}$ (or room temp.)

Pressure range, 1-12,000 bars

| Crystal and formulae | System | $\begin{gathered} 0^{\circ} \mathrm{C} \\ \mathrm{a} \times 10^{7} \end{gathered}$ | $30^{\circ} \mathrm{C}$ |  | $75^{\circ} \mathrm{C}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $3 \times 10^{7}$ | $\mathrm{b} \times 10^{12}$ | $3 \times 10^{7}$ | $\mathrm{b} \times 10^{12}$ |
| Andradite |  |  |  |  |  |  |
| $3 \mathrm{CaO} \cdot \mathrm{Fe}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2}$ | Cubic | - | 6.73 | . 86 | 6.70 | . 86 |
| Apatite: $3 \mathrm{Ca}_{3} \mathrm{P}_{2} \mathrm{O}_{3} \cdot \mathrm{CaF}_{2} \ldots$ | Hexagonal |  | 10.91 | 4.1 | 11.09 | 3.8 |
| Argentite: $\mathrm{Ag}_{2} \mathrm{~S}$...... | Cubic | 30 |  |  | 25.1 | 33.5 |
| Barite: $\mathrm{BaSO}_{4}$ | Orthorhombic | 17.1-18.1 | 17.60 | 11.9 | 17.92 | 12.6 |
| Beryl: $3 \mathrm{BeO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2}$. | Hexagonal | 5.7 | 5.403 | . 94 | 5.407 | . 94 |
| Calcite: $\mathrm{CaCO}_{3} . . . . . . .$. | Trigonal | 13.5 | 13.67 | 3.9 | 13.93 | 4.2 |
| Cobaltite: CoAs $\cdot \mathrm{S}$ | Cubic |  | 7.67 | 1.88 | 7.79 | 1.88 |
| Fluorite: $\mathrm{CaF}_{2}$ | Hexagonal | 12.6 | 12.26 | 6.49 | 12.59 | 6.61 |
| Galena: PbS | Cubic | 19.5-19.7 | 18.69 | 7.43 | 18.97 | 8.41 |
| Garnet (pyrope) : |  |  |  |  |  |  |
| Halite (Rock Salt) : NaCl . | Cubic | - | 42.60 | 51 | 44.26 | 52.6 |
| Hanksite: |  |  |  |  |  |  |
| $\mathrm{KCl} \cdot 2 \mathrm{Na}_{2} \mathrm{CO}_{3} \cdot 9 \mathrm{Na}_{2} \mathrm{SO}_{4}$ | Hexagonal | - | 24.57 | 24.5 | 25.54 | 26.7 |
| Jeffersonite | Monoclinic | - | 9.088 | 3.94 | 9.551 | 5.56 |
| Lithium fluoride: LiF | Cubic | - | 15.20 | 5.5 | 15.91 | 5.7 |
| Lithium iodide : LiI | Cubic | - | 60.0 | 110. |  |  |
| Magnetite: $\mathrm{Fe}_{3} \mathrm{O}_{4}$ | Cubic | 5.4-5.7 | 5.47 | . 82 | 5.45 | . 82 |
| Orthoclase: $\mathrm{KAl} \cdot \mathrm{Si}_{3} \mathrm{O}_{8} \ldots$ | Monoclinic |  | 21.23 | 14.5 | 21.16 | 13.9 |
| Periclase: MgO | Cubic | 7.2 | 5.98 | 1 | 6.06 | 1 |
| Potassium bromide: KBr | Cubic | - | 67.0 | 105.3 | 68.8 | 105.2 |
| Potassium fluoride: KF | Cubic | - | 33.0 | 31.9 | 33.2 | 31.9 |
| Potassium iodide: KI .... | Cubic |  | 85.3 | 155.4 | 87.7 | 155.4 |
| Pyrite: $\mathrm{FeS}_{3}$ | Cubic | 7.1 | 6.80 | . 87 | 6.82 | . 87 |
| Quartz: $\alpha \mathrm{SiO}_{2} \ldots \ldots .$. | Trigonal | - | 27.06 | 24.0 | 27.54 | 24.7 |
| Rochelle salt (see end of part 1) 3.8 |  |  |  |  |  |  |
| Sapphire (synthetic) : $\mathrm{Al}_{2} \mathrm{O}_{3}$ |  | 3.8 | 3.36 |  |  |  |
| Sphalerite : ZnS .......... | Cubic | 12.9-12.2 | 13.03 | 1.28 | 12.79 | 1.26 |
| Spodumene: $\mathrm{LiAl} \cdot \mathrm{Si}_{2} \mathrm{O}_{6}$ | Monoclinic | - | 7.033 | 1.49 | 7.073 | 2.28 |
| Sylvite: KCl $\ldots . . .$. | Cubic | - | 56.2 | 75.1 | 57.5 | 75.1 |
| Tourmaline (black) ...... | Trigonal | - | 8.16 | 1.95 | 8.62 | 2.15 |
| Topaz |  |  | 6.109 | 1.06 | 6.075 | 1.06 |
| Zircon: $\mathrm{ZrO}_{2} \cdot \mathrm{SiO}_{2}$ |  | 8.6 |  |  |  |  |
|  | $\underset{\mathrm{kg} / \mathrm{cm} \mathrm{cm}^{2}}{\text { Presser }}$ | $-\Delta \mathrm{V} / \mathrm{V}_{0}$ |  |  |  |  |
| Rochelle salt: $\mathrm{C}_{4} \mathrm{H}_{4} \mathrm{O}_{0} \mathrm{KNa}$ : | 2000 | . 01080 |  |  |  |  |
|  | 4000 | . 02016 |  |  |  |  |
|  | 6000 | . 02885 |  |  |  |  |
|  | 8000 | . 03716 |  |  |  |  |
|  | 10,000 | . 04501 |  |  |  |  |
|  | 12,000 | . 05237 |  |  |  |  |

[^127](continued)

## Part 2.-Elastic constants of rocks at ordinary pressure and temperature.

$\mathrm{E}=$ Young's modulus, in dynes $\mathrm{cm}^{-2}$
$\mathrm{G}=$ Modulus, of rigidity, in dynes $\mathrm{cm}^{-2}$
$\sigma=$ Poisson's ratio, dimensionless

The density is given, when known, in parentheses in the first column.


[^128]TABLE 277.-RELATIVE VOLUME OF QUARTZ CRYSTALS AND SIX GLASSES FOR DIFFERENT PRESSURES ${ }^{95}$

| Pressure $\mathrm{kg} / \mathrm{cm}^{2}$ | Quartz |  | Glass $A^{*}$ | Pyrex glass | Glass $C \dagger$ | Glass $D \ddagger$ | Borax glass |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | crystal | glass |  |  |  |  |  |
| 1 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 25,000 | . 946 | . 923 | . 934 | . 921 | . 945 | . 932 | . 877 |
| 30,000 | . 939 | . 909 | . 923 | . 907 | . 936 | . 924 | . 866 |
| 40,000 | . 926 | . 885 | . 905 | . 885 | . 920 | . 909 | . 845 |
| 50,000 | . 914 | . 864 | . 890 | . 867 | . 905 | . 894 | . 825 |
| 60,000 | . 902 | . 847 | . 875 | . 851 | . 891 | . 880 | . 808 |
| 70,000 | . 892 | . 832 | . 862 | . 838 | . 878 | . 867 | . 792 |
| 80,000 | . 883 | . 819 | . 849 | . 827 | . 866 | . 855 | . 778 |
| 90,000 | . 875 | . 808 | . 838 | . 817 | . 854 | . 844 | . 765 |
| 100,000 | . 868 | . 798 | . 828 | . 809 | . 842 | . 834 | . 753 |

[^129]$\Delta \mathrm{V} / \mathrm{V}_{0}$

| Pressure <br> $\mathrm{kg} / \mathrm{cm}^{2}$ | Quartz <br> glass | Pyrex | $A *$ | $C \dagger$ | $D \ddagger$ | Borax <br> 5,000 |
| ---: | :---: | :---: | :---: | :---: | :---: | ---: |
| 0,000 | .0141 | .0153 | .0159 | .0121 | .0144 | .0345 |
| 15,000 | .0452 | .0308 | .0300 | .0239 | .0281 | .0631 |
| 20,000 | .0610 | .0465 | .0425 | .0352 | .0411 | .0857 |
| 25,000 | .0772 | .0622 | .0535 | .0449 | .0542 | .1054 |
| 30,000 | .0933 | .0786 | .0656 | .0549 | .0678 | .1228 |
| 35,000 | .1068 | .0920 | .0770 | .0654 | .0806 | .1376 |
| 40,000 | .1194 | .1133 | .0866 | .0742 | .0927 | .1518 |

${ }^{06}$ Bridgman, P. W., Proc. Amer. Acad. Arts and Sci., vol. 73, p. 74, 1938.

* Glass $A$ is a potash lead silicate of very high lead content. †Glass $C$ is a soda potash lime silicate. $\quad \ddagger$ Glass $D$ is a lead zinc borosilicate.

TABLE 279.-SPECIFIC GRAVITIES CORRESPONDING TO THE BAUMÉ SCALE
The specific gravities are for $15.56^{\circ} \mathrm{C}\left(60^{\circ} \mathrm{F}\right)$ referred to water at the same temperature as unity. For specific gravities less than unity the values are calculated from the formula:

$$
\text { Degrees Baumé }=\frac{140}{\text { specific gravity }}-130 .
$$

For specific gravities greater than unity from:

$$
\text { Degrees Baumé }=145-\frac{145}{\text { specific gravity }}
$$

| Specific gravity | Specific gravities less than 1 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | . 07 | . 08 | . 09 |
|  | Degrees Baumé |  |  |  |  |  |  |  |  |  |
| . 60 | 103.33 | 99.51 | 95.81 | 92.22 | 88.75 | 85.38 | 82.12 | 78.95 | 75.88 | 72.90 |
| . 70 | 70.00 | 67.18 | 64.44 | 61.78 | 59.19 | 56.67 | 54.21 | 51.82 | 49.49 | 47.22 |
| . 80 | 45.00 | 42.84 | 40.73 | 38.68 | 36.67 | 34.71 | 32.79 | 30.92 | 29.09 | 27.30 |
| . 90 | 25.56 | 23.85 | 22.17 | 20.54 | 18.94 | 17.37 | 15.83 | 14.33 | 12.86 | 11.41 |
| Specific Specific gravities greater than 1 |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| Specific gravity | . 00 | . 01 | . 02 | . 03 | . 04 | . 05 | . 06 | .C7 | . 08 | . 09 |
| Degrees Baumé |  |  |  |  |  |  |  |  |  |  |
| 1.00 | . 00 | 1.44 | 2.84 | 4.22 | 5.58 | 6.91 | 8.21 | 9.49 | 10.74 | 11.97 |
| 1.10 | 13.18 | 14.37 | 15.54 | 16.68 | 17.81 | 18.91 | 20.00 | 21.07 | 22.12 | 23.15 |
| 1.20 | 24.17 | 25.16 | 26.15 | 27.11 | 28.06 | 29.00 | 29.92 | 30.83 | 31.72 | 32.60 |
| 1.30 | 33.46 | 34.31 | 35.15 | 35.98 | 36.79 | 37.59 | 38.38 | 39.16 | 39.93 | 40.68 |
| 1.40 | 41.43 | 42.16 | 42.89 | 43.60 | 44.31 | 45.00 | 45.68 | 46.36 | 47.03 | 47.68 |
| 1.50 | 48.33 | 48.97 | 49.60 | 50.23 | 50.84 | 51.45 | 52.05 | 52.64 | 53.23 | 53.80 |
| 1.60 | 54.38 | 54.94 | 55.49 | 56.04 | 56.58 | 57.12 | 57.65 | 58.17 | 58.69 | 59.20 |
| 1.70 | 59.71 | 60.20 | 60.70 | 61.18 | 61.67 | 62.14 | 62.61 | 63.08 | 63.54 | 63.99 |
| 1.80 | 64.44 | 64.89 | 65.33 | 65.76 | 66.20 | 66.62 |  |  |  |  |

$$
\left(15-56^{\circ} / 15.56^{\circ} \mathrm{C}\right) \text { for petroleum oils. }
$$

In order to avoid confusion and misunderstanding the American Petroleum Institute, the Bureau of Mines, and the National Bureau of Standards have agreed that a scale based on the modulus 141.5 shall be used in the United States Petroleum Industry and shall be known as the API scale. The United States Baumé scale based on the modulus 140 will continue to be used for other liquids lighter than water.

Calculated from the formula, degrees $\mathrm{API}=\frac{141.5}{\text { sp.gr. } 60^{\circ} / 60^{\circ} \mathrm{F}}-131.5$.

| Degrees |  |  |  |  |  |  |  |  |  |  |
| :---: | ---: | ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| API |  | .01 | .02 | .03 | .04 | .05 | .06 | .07 | .08 | .09 |
| $60^{\circ} / 60^{\circ} \mathrm{F}$ | .00 | .01 |  |  |  |  |  |  |  |  |
| .6 | 104.33 | 100.47 | 96.73 | 93.10 | 89.59 | 86.19 | 82.89 | 79.69 | 79.59 | 73.57 |
| .7 | 70.64 | 67.80 | 65.03 | 62.34 | 59.72 | 57.17 | 54.68 | 52.27 | 49.91 | 47.61 |
| .8 | 45.38 | 43.19 | 44.06 | 38.98 | 36.95 | 34.97 | 33.03 | 31.14 | 29.30 | 27.49 |
| .9 | 25.72 | 23.99 | 22.30 | 20.65 | 19.03 | 17.45 | 15.90 | 14.38 | 12.89 | 11.43 |
| 1.0 | 10.00 |  |  |  |  |  |  |  |  |  |

## TABLE 281.—DENSITY OF THE ELEMENTS, LIQUID OR SOLID

The density may depend considerably on previous treatment. To reduce to $\mathrm{lb} / \mathrm{ft}^{3}$ multiply by 62.4 .


[^130]Note.-The density of a specimen depends considerably on its state and previous treatment; especially is this the case with porous materials.

| Material | $\mathrm{g} / \mathrm{cm}^{3}$ | $\mathrm{lb} / \mathrm{ft}^{3}$ | Material | $\mathrm{g} / \mathrm{cm}^{3}$ | $\mathrm{lb} / \mathrm{ft}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Agate | $2.5-2.7$ | 156-168 | Gum arabic | $1.3-1.4$ | 80-85 |
| Alabaster |  |  | Gypsum | 2.31-2.33 | 144-145 |
| Carbonate | 2.69-2.78 | 168-173 | Hematite | $4.9-5.3$ | 306-330 |
| Sulphate | 2.26-2.32 | 141-145 | Hormblende | 3.0 | 187 |
| Albite ... | 2.62-2.65 | 163-165 | Ice | . 917 | 57.2 |
| A mber | 1.06-1.11 | 66-69 | Ilmenite | $4.5-5$. | 280-310 |
| Amphiboles | 2.9-3.2 | 180-200 | I vory | 1.83-1.92 | 114-120 |
| Anorthite | 2.74-2.76 | 171-172 | Labradorite | $2.7-2.72$ | 168-170 |
| Anthracite | 1.4-1.8 | 87-112 | Lava, basaltic | 2.8-3.0 | 175-185 |
| Asbestos . | 2.0-2.8 | 125-175 | "* trachytic | $2.0-2.7$ | 125-168 |
| Asphalt | $1.1-1.5$ | 69-94 | Leather, dry | . 86 | 54 |
| Basalt . | $2.4-3.1$ | 150-190 | " greased | 1.02 | 64 |
| Beeswax | .96-. 97 | 60-61 | Lime, mortar | 1.65-1.78 | 103-111 |
| Beryl | 2.69-2.7 | 168-168 | " slaked | $1.3-1.4$ | 81-87 |
| Piotite | 2.7-3.1 | 170-190 | Limestone | 2.68-2.76 | 167-171 |
| Bone | 1.7-2.0 | 106-125 | Litharge : |  |  |
| Brick | 1.4-2.2 | 87-137 | Artificial | $9.3-9.4$ | 580-585 |
| Butter | .86-. 87 | 53-54 | Natural | $7.8-8.0$ | 490-500 |
| Calamine | $4.1-4.5$ | 255-280 | Magnetite . | $4.9-5.2$ | 306-324 |
| Camphor | . 99 | 62 | Malachite | $3.7-4.1$ | 231-256 |
| Caoutchouc | .92-. 99 | 57-62 | Marble | $2.6-2.84$ | 160-177 |
| Celluloid | 1.4 | 87 | Meerschaum | .99-1.28 | 62-80 |
| Cement, set | 2.7-3.0 | 170-190 | Mica | 2.6-3.2 | 165-200 |
| Chalk | $1.9-2.8$ | 118-175 | Muscovite | 2.76-3.00 | 172-225 |
| Charcoal, oak | . 57 | 35 | Ochre | 3.5 | 218 |
| " pine | . $28-.44$ | 18-28 | Oligoclase | 2.65-2.67 | 165-167 |
| Chrome yellow | 6.00 | 374 | Olivine . . | 3.27-3.37 | 204-210 |
| Chromite | 4.32-4.57 | 270-285 | Opal | 2.2 | 137 |
| Cinnabar | 8.12 | 507 | Orthoclase | 2.58-2.61 | 161-163 |
| Clay | 1.8-2.6 | 122-162 | Paper | . $7-1.15$ | 44-72 |
| Coal, soft | 1.2-1.5 | 75-94 | Paraffin | . $87-.91$ | 54-57 |
| Cocoa butter | .89-. 91 | 56-57 | Peat | . 84 | 52 |
| Coke | 1.0-1.7 | 62-105 | Pitch | 1.07 | 67 |
| Copal | 1.04-1.14 | 65-71 | Porcelain | $2.3-2.5$ | 143-156 |
| Cork | .22- . 26 | 14-16 | Porphyry | $2.6-2.9$ | 162-181 |
| Cork linoleum | . 55 | 34 | Pyrite .. | 4.95-5.1 | 309-318 |
| Corundum | $3.9-4.0$ | 245-250 | Ouartz | 2.65 | 165 |
| Diamond: |  |  | Quartzite | 2.73 | 170 |
| Anthracitic | 1.66 | 104 | Resin | 1.07 | 67 |
| Carbonado | 3.01-3.25 | 188-203 | Rock salt | 2.18 | 136 |
| Diorite | 2.52 | 157 | Rubber, hard | 1.19 | 74 |
| Dolomite | 2.84 | 177 | " soft | 1.1 | 69 |
| Ebonite | 1.15 | 72 | Rutile | 4.2 | 260 |
| Emery | 4.0 | 250 | Sandstone | 2.14-2.36 | 134-147 |
| Epidote | 3.25-3.5 | 203-218 | Serpentine | 2.50-2.65 | 156-165 |
| Feldspar | 2.55-2.75 | 159-172 | Slag, furnace | $2.0-3.9$ | 125-240 |
| Flint | 2.63 | 164 | Slate | $2.6-3.3$ | 162-205 |
| Fluorite | 3.18 | 198 | Soapstone | $2.6-2.8$ | 162-175 |
| Gamboge | 1.2 | 75 | Starch | 1.53 | 95 |
| Garnet . | 3.15-4.3 | 197-268 | Sugar | 1.61 | 100 |
| Gas carbon | 1.88 | 117 | Talc | $2.7-2.8$ | 168-174 |
| Gelatine | 1.27 | 180 | Tallow | .91-. 97 | 57-60 |
| Glass, common | $2.4-2.8$ | 150-175 | Tar . | 1.02 | 66 |
| " flint ... | $2.9-5.9$ | 180-370 | Topaz | 3.5-3.6 | 219-22.3 |
| Glue | 1.27 | 80 | Tourmaline | $3.0-3.2$ | 190-200 |
| Granite | 2.64-2.76 | 165-172 | Wax, sealing | 1.8 | 112 |
| Graphite | 2.30-2.72 | 144-170 | Zircon | 4.68-4.70 | 292-293 |


| Alloy | $\mathrm{g} / \mathrm{cm}^{3}$ | $\mathrm{lb} / \mathrm{ft}^{3}$ |
| :---: | :---: | :---: |
| Brasses ：yellow， $70 \mathrm{Cu}+30 \mathrm{Zn}$ ，cast | 8.44 | 527 |
| ＂＂${ }^{\text {＂}}$ ，rolled | 8.56 | 534 |
| drawn | 8.70 | 542 |
| ＂red， $90 \mathrm{Cu}+10 \mathrm{Zn}$ | 8.60 | 536 |
| ＂white， $50 \mathrm{Cu}+50 \mathrm{Zn}$ | 8.20 | 511 |
| Bronzes： $90 \mathrm{Cu}+10 \mathrm{Sn}$ | 8.78 | 548 |
| ＂ $85 \mathrm{Cu}+15 \mathrm{Sn}$ | 8.89 | 555 |
| ＂ $80 \mathrm{Cu}+20 \mathrm{Sn}$ | 8.74 | 545 |
| ＂ $75 \mathrm{Cu}+25 \mathrm{Sn}$ | 8.83 | 551 |
| German silver：Chinese， $26.3 \mathrm{Cu}+36.6 \mathrm{Zn}+36.8 \mathrm{Ni}$ | 8.30 | 518 |
| ＂＂Berlin（1） $52 \mathrm{Cu}+26 \mathrm{Zn}+22 \mathrm{Ni} .$. | 8.45 | 527 |
| ＂＂$"$（2） $59 \mathrm{Cu}+30 \mathrm{Zn}+11 \mathrm{Ni}$ | 8.34 | 520 |
| ＂＂$"$ ．（3） $63 \mathrm{Cu}+30 \mathrm{Zn}+6 \mathrm{Ni}$ | 8.30 | 518 |
| ＂nickelin ．．．．．．．．．．．．．．．．．．．．．．． | 8.77 | 547 |
| Lead and tin： $87.5 \mathrm{~Pb}+12.5 \mathrm{Sn}$ | 10.60 | 661 |
| ＂＂＂ $84 \mathrm{~Pb}+16 \mathrm{Sn}$ | 10.33 | 644 |
| ＂＂＂ $77.8 \mathrm{~Pb}+22.2 \mathrm{Sn}$ | 10.05 | 627 |
| ＂＂＂ $63.7 \mathrm{~Pb}+36.3 \mathrm{Sn}$ | 9.43 | 588 |
| ＂＂＂ $46.7 \mathrm{~Pb}+53.3 \mathrm{Sn}$ | 8.73 | 545 |
| ＂＂＂ $30.5 \mathrm{~Pb}+69.5 \mathrm{Sn}$ | 8.24 | 514 |
| Bismuth，lead，and cadmium ： $53 \mathrm{Bi}+40 \mathrm{~Pb}+7 \mathrm{Cd}$ | 10.56 | 659 |
| Wood＇s metal ： $50 \mathrm{Bi}+25 \mathrm{~Pb}+12.5 \mathrm{Cd}+12.5 \mathrm{Sn}$ | 9.70 | 605 |
| Cadmium and tin： $32 \mathrm{Cd}+68 \mathrm{Sn} \ldots . . . . . . .$. | 7.70 | 480 |
| Gold and copper ： $98 \mathrm{Au}+2 \mathrm{Cu}$ | 18.84 | 1176 |
| ＂＂$" \quad 96 \mathrm{Au}+4 \mathrm{Cu}$ | 18.36 | 1145 |
| ＂＂$\quad$＂ $4 \mathrm{Au}+6 \mathrm{Cu}$ | 17.95 | 1120 |
| ＂＂${ }^{\text {a }}$（ $\mathrm{Au}^{\text {a }} 10 \mathrm{Cu}$ | 17.16 | 1071 |
| ＂＂$\quad 86 \mathrm{Au}+14 \mathrm{Cu}$ | 16.47 | 1027 |
| Aluminum and copper： $10 \mathrm{Al}+90 \mathrm{Cu}$ | 7.69 | 480 |
| ＂＂ $4.5 \mathrm{Al}+95 \mathrm{Cu}$ | 8.37 | 522 |
| ＂＂$\quad$＂ $3 \mathrm{Al}+97 \mathrm{Cu}$ | 8.69 | 542 |
| Aluminum and zinc： $91 \mathrm{Al}+9 \mathrm{Zn}$ | 2.80 | 175 |
| Platinum and iridium ： $90 \mathrm{Pt}+10 \mathrm{Ir}$ | 21.62 | 1348 |
| ＂＂＂ $85 \mathrm{Pt}+15 \mathrm{Ir}$ | 21.62 | 1348 |
| ＂${ }^{\text {a }}$ ，66．67Pt +33.33 Ir | 21.87 | 1364 |
| Carboloy | 14.3 | 895 |
| Constantan： $60 \mathrm{Cu}+40 \mathrm{Ni}$ | 8.88 | 554 |
| Magnalium： $70 \mathrm{Al}+30 \mathrm{Mg}$ | 2.0 | 125 |
| Manganin ： $84 \mathrm{Cu}+12 \mathrm{Mn}+4 \mathrm{Ni}$ | 8.5 | 530 |
| Monel metal | 8.87 | 554 |
| Platinoid：German silver＋little tungsten． | 9.0 | 560 |
| Stellite：Co 59．5；Mo 22.5 ；Cr 10.8 ；Fe 3.1 ；Mn 2.0 | 83 | 518 |

TABLE 284．－PHYSICAL PROPERTIES OF SOME LIGHT HYDROCARBONS ${ }^{07}$

| Critical constants |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { E } \\ & \frac{0}{2} \\ & \text { U } \\ & 0 \\ & E \\ & E \end{aligned}$ |  | Temperature |  | Specific heats |  |  | $\stackrel{\stackrel{\rightharpoonup}{\omega}}{\stackrel{y}{U}}$ |  |  |  | $\cong$ |
|  |  |  |  | $C_{p}$ |  |  |  |  |  | E |  |
|  |  |  | $=$ |  |  |  |  |  |  | E | 邑 |
|  |  |  | ${ }_{4}^{4}$ |  |  |  |  |  |  | 产 | 号 |
|  |  |  | $\Sigma$ |  |  |  |  |  |  | ¢ |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | ${ }^{\circ} \mathrm{C}$ | atm | cal $\mathrm{g}^{-1}$ | ${ }^{\circ} \mathrm{C}^{-1}$ |  | $\mathrm{kg} / \mathrm{m}^{3}$ | $\mathrm{m}^{3} / \mathrm{kl}$ | atm | ${ }^{\circ} \mathrm{C}$ | $\mathrm{cal} / \mathrm{m}^{3}$ |
| Methane ．．．．． $\mathrm{CH}_{4}$ | 16.04 | 82.1 | 45.8 | ． 526 | .400 | ． 555 | ． 678 | －－ | －－ | 1880 | 9，000 |
| Fthylene ．．．．． $\mathrm{C}_{2} \mathrm{H}_{4}$ | 28.05 | 9.72 | 50.9 | ． 363 | ． 296 | ． 977 | 1.19 | －－ | －－ | 1975 | 14，350 |
| Ethane ．．．．．． $\mathrm{C}_{2} \mathrm{H}_{0}$ | 30.07 | 32.3 | 48.2 | .409 | ． 347 | 1.048 | 1.282 | 294.2 | 38.3 | 1895 | 15，900 |
| Propylene ．．．． $\mathrm{C}_{3} \mathrm{H}_{6}$ | 42.08 | 91.4 | 45.4 | ． 363 | ． 316 | 1.476 | 1.805 | 289 | 10.3 | 1935 | 21，100 |
| Propane ．．．．． $\mathrm{C}_{3} \mathrm{H}_{4}$ | 44.09 | 96.8 | 42.0 | ． 388 | ． 343 | 1.550 | 1.892 | 268 | 8.45 | 1925 | 22，800 |
| Butadiene－1，3 ． $\mathrm{C}_{4} \mathrm{H}_{\text {\％}}$ | 54.09 | 152.0 | 42.8 | ． 349 | ． 312 | 1.922 | 2.35 | 267 | 2.45 | －－ | 26，400 |
| Butene－1 ．．．．． $\mathrm{C}_{4} \mathrm{H}_{8}$ | 56.10 | 143.9 | 39.2 | ． 371 | ． 334 | 1.998 | 2.44 | 246 | 2.6 |  | 28，200 |
| cis－Butene－2 ．． $\mathrm{C}_{4} \mathrm{H}_{4}$ | 56.10 | 160 | 41.5 | ． 350 | .315 | 2.004 | 2.45 | 255.5 | 18.5 | 1930 | 28，300 |
| trans－Butene－2． $\mathrm{C}_{4} \mathrm{H}_{8}$ | 56.10 | 155.0 | 40.5 | ． 376 | ． 342 | 2.004 | 2.45 | 249.0 | 2.00 |  | 28，200 |
| Isobutylene ．．． $\mathrm{C}_{4} \mathrm{H}_{*}$ | 56.10 | 144.7 | 39.5 | ． 375 | ． 335 | 1.998 | 2.44 | 245.5 | 2.57 | －－ | 28，100 |
| Isobutane ．．．． $\mathrm{C}_{4} \mathrm{H}_{10}$ | 58.12 | 133.7 | 36.5 | ． 387 | ． 348 | 2.077 | 2.54 | 222 | 3.06 | 1900 | 30,000 |
| 11－Butane $\ldots . . \mathrm{C}_{4} \mathrm{H}_{1 n}$ | 58.12 | 152.2 | 37.5 | .397 | ． 361 | 2.084 | 2.55 | 229.5 | 2.13 | 1895 | 30，100 |



Density or mass in $\mathrm{g} / \mathrm{cm}^{3}$ and in $\mathrm{lb} / \mathrm{ft}^{3}$ of various liquids.

| Liquid | $\mathrm{g} / \mathrm{cm}^{3}$ | $\mathrm{lb} / \mathrm{ft}^{8}$ | Temp. ${ }^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: |
| Acetone | . 792 | 49.4 | $20^{\circ}$ |
| Alcohol, ethyl | . 807 | 50.4 | 0 |
| " methyl | . 810 | 50.5 | 0 |
| Aniline ....... | 1.035 | 64.5 | 0 |
| Benzene | . 899 | 56.1 | 0 |
| Bromine | 3.187 | 199.0 | 0 |
| Carbolic acid (crude) | .950-. 965 | 59.2-60.2 | 15 |
| Carbon disulfide .... | 1.293 | 80.6 | 0 |
| Chloroform .. | 1.489 | 93.0 | 20 |
| Cocoa butter | . 857 | 53.5 | 100 |
| Ether | . 736 | 45.9 | 0 |
| Gasoline | . 66 - . 69 | 41.0-43.0 |  |
| Glycerine | 1.260 | 78.6 | 0 |
| Japan wax | . 875 | 54.6 | 100 |
| Mercury | 13.595 | 849 | 0 |
| Milk ... | 1.028-1.035 | 64.2-64.6 |  |
| Naphtha (wood) | .848- . 810 | 52.9-50.5 | 0 |
| Naphtha (petroleum ether) | . 665 | 41.5 | 15 |
| Oils: Amber ............ | . 800 | 49.9 | 15 |
| Anise-seed | . 996 | 62.1 | 16 |
| Beef-tallow | . 931 - 938 | 58. | ... |
| Butterfat | . $91-.92$ | 56. | . . . |
| Camphor | . 910 | 56.8 |  |
| Castor . | . 969 | 60.5 | 15 |
| Clove | $1.04-1.06$ | 65. -66 . | 25 |
| Cocoanut | . 925 | 57.7 | 15 |
| Cod-liver | . $92-.93$ | 58. |  |
| Cottonseed | . 926 | 57.8 | 16 |
| Creosote | 1.040-1.100 | 64.9-68.6 | 15 |
| Kerosene | . 82 | 51.2 |  |
| Lard | . 920 | 57.4 | 15 |
| Lavender | . 877 | 54.7 | 16 |
| Lemon | . 844 | 52.7 | 16 |
| Linseed (boiled) | . 942 | 58.8 | 15 |
| Neat's-foot | .913-. 917 | 57.0-57.2 | . . . |
| Oleomargarine | . $92-.93$ |  |  |
| Olive ........ | . 918 | 57.3 | 15 |
| Palm | . 905 | 56.5 | 15 |
| Pentane | . 650 | 40.6 | 0 |
| " | . 623 | 38.9 | 25 |
| Peppermint | . $90-.92$ | 56-57 | 25 |
| Petroleum ...... | . 878 | 54.8 | 0 |
| Pine (light) | .795-. 805 | 49.6-50.2 | 15 |
| Pine . . . . . . . . | .850-. 860 | 53.0-54.0 | 15 |
| Poppy | . 924 | 57.7 |  |
| Rapeseed (crude) | . 915 | 57.1 | 15 |
| "، (refined) | . 913 | 57.0 | 15 |
| Resin ........... | . 955 | 59.6 | 15 |
| Sperm | . 88 | 55. | 25 |
| Soya-bean | . 919 | 57.3 | 30 |
|  | . 906 | 56.5 | 90 |
| Train or whale | .918-. 925 | 57.3-57.7 | 15 |
| Turpentine | . 873 | 54.2 | 16 |
| Valerian . | . 965 | 60.2 | 16 |
| Wintergreen | 1.18 | 74. | 25 |
| Pyroligneous acid | . 800 | 49.9 | 0 |
| Water ........ | 1.000 1.025 | 62.4 | 4 |
| Sea water | 1.025 | 64.0 |  |

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TABLE 287.-DENSITY OF PURE WATER FREE FROM AIR, $0^{\circ}$ TO $41^{\circ} \mathrm{C}$
Under standard pressure $(76 \mathrm{cmHg})$ at every tenth part of a degree from $0^{\circ}$ to $41^{\circ} \mathrm{C}$, in $\mathrm{g} / \mathrm{ml}$.*

|  | Tenths of degrees |  |  |  |  |  |  |  |  |  |  | Mean |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Degrees } \\ \hline \end{gathered}$ |  | 0 | 1 | 2 | 3 | .$_{4}$ | 5 | 6 | 7 | 8 | 9 | differences |
| 0 | . 999 | 8681 | 8747 | 8812 | 8875 | 8936 | 8996 | 9053 | 9109 | 9163 | 9216 | $+59$ |
| 1 |  | 9267 | 9315 | 9363 | 9408 | 9452 | 9494 | 9534 | 9573 | 9610 | 9645 | + 41 |
| 2 |  | 9679 | 9711 | 9741 | 9769 | 9796 | 9821 | 9844 | 9866 | 9887 | 9905 | + 24 |
| 3 |  | 9922 | 9937 | 9951 | 9962 | 9973 | 9981 | 9988 | 9994 | 9998 | 0000 | + 8 |
| 4 | 1.000 | 0000 | 9999 | 9996 | 9992 | 9986 | 9979 | 9970 | 9960 | 9947 | 9934 | - 8 |
| 5 | . 999 | 9919 | 9902 | 9884 | 9864 | 9842 | 9819 | 9795 | 9769 | 9742 | 9713 | $-24$ |
| 6 |  | 9682 | 9650 | 9617 | 9582 | 9545 | 9507 | 9468 | 9427 | 9385 | 9341 | - 39 |
| 7 |  | 9296 | 9249 | 9201 | 9151 | 9100 | 9048 | 8994 | 8938 | 8881 | 8823 | - 53 |
| 8 |  | 8764 | 8703 | 8641 | 8577 | 8512 | 8445 | 8377 | 8308 | 8237 | 8165 | $-67$ |
| 9 |  | 8091 | 8017 | 7940 | 7863 | 7784 | 7704 | 7622 | 7539 | 7455 | 7369 | -81 |
| 10 |  | 7282 | 7194 | 7105 | 7014 | 6921 | 6826 | 6729 | 6632 | 6533 | 6432 | $-95$ |
| 11 |  | 6331 | 6228 | 6124 | 6020 | 5913 | 5805 | 5696 | 5586 | 5474 | 5362 | $-108$ |
| 12 |  | 5248 | 5132 | 5016 | 4898 | 4780 | 4660 | 4538 | 4415 | 4291 | 4166 | $-121$ |
| 13 |  | 4040 | 3912 | 3784 | 3654 | 3523 | 3391 | 3257 | 3122 | 2986 | 2850 | $-133$ |
| 14 |  | 2712 | 2572 | 2431 | 2289 | 2147 | 2003 | 1858 | 1711 | 1564 | 1416 | $-145$ |
| 15 |  | 1266 | 1114 | 0962 | 0809 | 0655 | 0499 | 0343 | 0185 | 0026 | 9865 | $-156$ |
| 16 | . 998 | 9705 | 9542 | 9378 | 9214 | 9048 | 8881 | 8713 | 8544 | 8373 | 8202 | -168 |
| 17 |  | 8029 | 7856 | 7681 | 7505 | 7328 | 7150 | 6971 | 6791 | 6610 | 6427 | -178 |
| 18 |  | 6244 | 6058 | 5873 | 5686 | 5498 | 5309 | 5119 | 4927 | 4735 | 4541 | $-190$ |
| 19 |  | 4347 | 4152 | 3955 | 3757 | 3558 | 3358 | 3158 | 2955 | 2752 | 2549 | $-200$ |
| 20 |  | 2343 | 2137 | 1930 | 1722 | 1511 | 1301 | 1090 | 0878 | 0663 | 0449 | $-211$ |
| 21 |  | 0233 | 0016 | 9799 | 9580 | 9359 | 9139 | 8917 | 8694 | 8470 | 8245 | -221 |
| 22 | .997 | 8019 | 7792 | 7564 | 7335 | 7104 | 6873 | 6641 | 6408 | 6173 | 5938 | $-232$ |
| 23 |  | 5702 | 5466 | 5227 | 4988 | 4747 | 4506 | 4264 | 4021 | 3777 | 3531 | -242 |
| 24 |  | 3286 | 3039 | 2790 | 2541 | 2291 | 2040 | 1788 | 1535 | 1280 | 1026 | $-252$ |
| 25 |  | 0770 | 0513 | 0255 | 9997 | 9736 | 9476 | 9214 | 8951 | 8688 | 8423 | $-261$ |
| 26 | .996 | 8158 | 7892 | 7624 | 7356 | 7087 | 6817 | 6545 | 6273 | 6000 | 5726 | -271 |
| 27 |  | 5451 | 5176 | 4898 | 4620 | 4342 | 4062 | 3782 | 3500 | 3218 | 2935 | -280 |
| 28 |  | 2652 | 2366 | 2080 | 1793 | 1505 | 1217 | 0928 | 0637 | 0346 | 0053 | -289 |
| 29 | . 995 | 9761 | 9466 | 9171 | 8876 | 8579 | 8282 | 7983 | 7684 | 7383 | 7083 | -298 |
| 30 |  | 6780 | 6478 | 6174 | 5869 | 5564 | 5258 | 4950 | 4642 | 4334 | 4024 | $-307$ |
| 31 |  | 3714 | 3401 | 3089 | 2776 | 2462 | 2147 | 1832 | 1515 | 1198 | 0880 | -315 |
| 32 |  | 0561 | 0241 | 9920 | 9599 | 9276 | 8954 | 8630 | 8304 | 7979 | 7653 | -324 |
| 33 | . 994 | 7325 | 6997 | 6668 | 6338 | 6007 | 5676 | 5345 | 5011 | 4678 | 4343 | -332 |
| 34 |  | 4007 | 3671 | 3335 | 2997 | 2659 | 2318 | 1978 | 1638 | 1296 | 0953 | $-340$ |
| 35 |  | 0610 | 0267 | 9922 | 9576 | 9230 | 8883 | 8534 | 8186 | 7837 | 7486 | -347 |
| 36 | . 993 | 7136 | 6784 | 6432 | 6078 | 5725 | 5369 | 5014 | 4658 | 4301 | 3943 | -355 |
| 37 |  | 3585 | 3226 | 2866 | 2505 | 2144 | 1782 | 1419 | 1055 | 0691 | 0326 | $-362$ |
| 38 | . 992 | 9960 | 9593 | 9227 | 8859 | 8490 | 8120 | 7751 | 7380 | 7008 | 6636 | $-370$ |
| 39 |  | 6263 | 5890 | 5516 | 5140 | 4765 | 4389 | 4011 | 3634 | 3255 | 2876 | $-377$ |
| 40 41 | . 991 | $\begin{aligned} & 2497 \\ & 8661 \end{aligned}$ | 2116 | 1734 | 1352 | 0971 | 0587 | 0203 | 9818 | 9433 | 9047 | $-384$ |

[^131]TABLE 288.-VOLUNE IN $\mathrm{cm}^{3}$ AT VARIOUS TEMPERATURES OF A $\mathrm{cm}^{3}$ OF WATER FREE FROM AIR AT THE TEMPERATURE OF MAXIMUM DENSITY, $0^{\circ}$ to $36^{\circ} \mathrm{C}$

| ${ }^{\text {Temp. }}{ }^{\text {C }}$ | . 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1.000132 | 125 | 118 | 112 | 106 | 100 | 095 | 089 | 084 | 079 |
| 1 | 073 | 069 | 064 | 059 | 055 | 051 | 047 | 043 | 039 | 035 |
| 2 | 032 | 029 | 026 | 023 | 020 | 018 | 016 | 013 | 011 | 009 |
| 3 | 008 | 006 | 005 | 004 | 003 | 002 | 001 | 001 | 000 | 000 |
| 4 | 000 | 000 | 000 | 001 | 001 | 002 | 003 | 004 | 005 | 007 |
| 5 | 008 | 010 | 012 | 014 | 016 | 018 | 021 | 023 | 026 | 029 |
| 6 | 032 | 035 | 039 | 042 | 046 | 050 | 054 | 058 | 062 | 066 |
| 7 | 070 | 075 | 080 | 085 | 090 | 095 | 101 | 106 | 112 | 118 |
| 8 | 124 | 130 | 137 | 142 | 149 | 156 | 162 | 169 | 176 | 184 |
| 9 | 191 | 198 | 206 | 214 | 222 | 230 | 238 | 246 | 254 | 263 |
| 10 | 272 | 281 | 290 | 299 | 308 | 317 | 327 | 337 | 347 | 357 |
| 11 | 367 | 377 | 388 | 398 | 409 | 420 | 430 | 441 | 453 | 464 |
| 12 | 476 | 487 | 499 | 511 | 522 | 534 | 547 | 559 | 571 | 584 |
| 13 | 596 | 609 | 623 | 636 | 649 | 661 | 675 | 688 | 702 | 715 |
| 14 | 729 | 743 | 757 | 772 | 786 | 800 | 815 | 830 | 844 | 859 |
| 15 | 873 | 890 | 905 | 920 | 935 | 951 | 967 | 983 | 998 | 015 |
| 16 | 1.001031 | 047 | 063 | 080 | 097 | 113 | 130 | 147 | 164 | 182 |
| 17 | 198 | 216 | 233 | 252 | 269 | 287 | 305 | 323 | 341 | 358 |
| 18 | 378 | 396 | 415 | 433 | 452 | 471 | 490 | 510 | 529 | 548 |
| 19 | 568 | 588 | 606 | 626 | 646 | 667 | 687 | 707 | 728 | 748 |
| 20 | 769 | 790 | 811 | 832 | 853 | 874 | 895 | 916 | 938 | 960 |
| 21 | 981 | 002 | 024 | 046 | 068 | 091 | 113 | 135 | 158 | 181 |
| 22 | 1.002203 | 226 | 249 | 271 | 295 | 319 | 342 | 364 | 389 | 412 |
| 23 | 436 | 459 | 483 | 507 | 532 | 556 | 581 | 605 | 629 | 654 |
| 24 | 679 | 704 | 729 | 754 | 779 | 804 | 829 | 854 | 879 | 905 |
| 25 | 932 | 958 | 983 | 010 | 036 | 061 | 088 | 115 | 141 | 168 |
| 26 | 1.003195 | 221 | 248 | 275 | 302 | 330 | 357 | 384 | 412 | 439 |
| 27 | 467 | 495 | 523 | 550 | 579 | 607 | 635 | 663 | 692 | 720 |
| 28 | 749 | 776 | 806 | 836 | 865 | 893 | 922 | 951 | 981 | 011 |
| 29 | 1.004041 | 069 | 100 | 129 | 160 | 189 | 220 | 250 | 280 | 310 |
| 30 | 341 | 371 | 403 | 432 | 464 | 494 | 526 | 557 | 588 | 619 |
| 31 | 651 | 682 | 713 | 744 | 777 | 808 | 840 | 872 | 904 | 936 |
| 32 | 968 | 001 | 033 | 066 | 098 | 132 | 163 | 197 | 229 | 263 |
| 33 | 1.005296 | 328 | 361 | 395 | 427 | 461 | 496 | 530 | 562 | 597 |
| 34 | 631 | 665 | 698 | 732 | 768 | 802 | 836 | 871 | 904 | 940 |
| 35 | 975 | 009 | 044 | 078 | 115 | 150 | 185 | 219 | 255 | 290 |

TABLE 289.-INFLUENCE OF PRESSURE ON VOLUME OF WATER*

| $\mathrm{kg} / \mathrm{cm}^{2}$ | ${ }^{\circ} \mathrm{C}$ |  | $20^{\circ} \mathrm{C}$ | $40^{\circ} \mathrm{C}$ | $\mathrm{kg} / \mathrm{cm}^{2}$ | $20^{\circ} \mathrm{C}$ |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 1 | 1.0000 | 1.0016 | 1.0076 | 7,000 | .8404 | $40^{\circ} \mathrm{C}$ |
| 500 | .9771 | .9808 | .9873 | 8,000 | .82785 | .8360 |
| 1,000 | .9578 | .9630 | .9700 | 9,000 | .8160 | .8249 |
| 2,000 | .9260 | .9327 | .9403 | 10,000 | - | .8149 |
| 3,000 | .9015 | .9087 | .9164 | 11,000 | - | .8056 |
| 5,000 | .8632 | .8702 | .8778 | 12,000 | - | .7966 |
| 6,000 | .8480 | .8545 | .8623 | 12,500 | - | .7922 |

[^132]The mass of $1 \mathrm{~cm}^{3}$ at $4^{\circ} \mathrm{C}$ is taken as unity.

| ${ }^{\text {Temp. }}$ | Density | Volume | ${ }^{\text {Temp. }}{ }^{\circ} \mathrm{C} .$ | Density | Volume | ${ }^{\text {Temp. }}$ ¢ ${ }^{\text {c }}$ | Density | Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -10 | . 99815 | 1.00186 | +20 | . 99823 | 1.00177 | +50 | . 98807 | 1.01207 |
| -9 | 843 | 157 | 21 | 802 | 198 | 51 | 762 | 254 |
| -8 | 869 | 131 | 22 | 780 | 220 | 52 | 715 | 301 |
| - 7 | 892 | 108 | 23 | 757 | 244 | 53 | 669 | 349 |
| - 6 | 912 | 088 | 24 | 733 | 268 | 54 | 621 | 398 |
| - 5 | . 99930 | 1.00070 | 25 | . 99708 | 1.00293 | 55 | . 98573 | 1.01448 |
| -4 | 945 | 055 | 26 | 682 | 320 | 60 | 324 | 705 |
| - 3 | 958 | 042 | 27 | 655 | 347 | 65 | 059 | 979 |
| - 2 | 970 | 031 | 28 | 627 | 375 | 70 | . 97781 | 1.02270 |
| -1 | 979 | 021 | 29 | 598 | 404 | 75 | 489 | 576 |
| + 0 | . 99987 | 1.00013 | 30 | . 99568 | 1.00434 | 80 | . 97183 | 1.02899 |
| 1 | 993 | 007 | 31 | 537 | 465 | 85 | . 96865 | 1.03237 |
| 2 | 997 | 003 | 32 | 506 | 497 | 90 | 534 | 590 |
| 3 | 999 | 001 | 33 | 473 | 530 | 95 | 192 | 959 |
| 4 | 1.00000 | 1.00000 | 34 | 440 | 563 | 100 | . 95838 | 1.04343 |
| 5 | . 99999 | 1.00001 | 35 | . 99406 | 1.00598 | 110 | . 9510 | 1.0515 |
| 6 | 997 | 003 | 36 | 371 | 633 | 120 | . 9434 | 1.0601 |
| 7 | 993 | 007 | 37 | 336 | 669 | 130 | . 9352 | 1.0693 |
| 8 | 988 | 012 | 38 | 300 | 706 | 140 | . 9264 | 1.0794 |
| 9 | 981 | 019 | 39 | 263 | 743 | 150 | . 9173 | 1.0902 |
| 10 | . 99973 | 1.00027 | 40 | . 99225 | 1.00782 | 160 | . 9075 | 1.1019 |
| 11 | 963 | 037 | 41 | 187 | 821 | 170 | . 8973 | 1.1145 |
| 12 | 952 | 048 | 42 | 147 | 861 | 180 | . 8866 | 1.1279 |
| 13 | 940 | 060 | 43 | 107 | 901 | 190 | . 8750 | 1.1429 |
| 14 | 927 | 073 | 44 | 066 | 943 | 200 | . 8628 | 1.1590 |
| 15 | . 99913 | 1.00087 | 45 | . 99025 | 1.00985 | 210 | . 850 | 1.177 |
| 16 | 897 | 103 | 46 | . 98982 | 1.01028 | 220 | . 837 | 1.195 |
| 17 | 880 | 120 | 47 | 940 | 072 | 230 | . 823 | 1.215 |
| 18 | 862 | 138 | 48 | 896 | 116 | 240 | . 809 | 1.236 |
| 19 | 843 | 157 | 49 | 852 | 162 | 250 | . 794 | 1.259 |

Density or mass in $\mathrm{g} / \mathrm{cm}^{3}$ and the volume in $\mathrm{cm}^{3}$ of 1 g of mercury.

| ${ }_{{ }^{\circ} \mathrm{Cemp}}$ | $\underset{\mathrm{g} / \mathrm{cm}^{3}}{\substack{\text { Mass }}}$ | Volume of 1 g in $\mathrm{cm}^{3}$ | $\mathrm{Temp}_{{ }^{\circ} \mathrm{C}}$ | $\begin{aligned} & \text { Mass } \\ & \mathrm{g} / \mathrm{cm}^{3} \end{aligned}$ | Volume of 1 g in $\mathrm{cm}^{3}$ | ${ }^{\text {Temp. }}$ | $\begin{gathered} \text { Mass } \\ \mathrm{g} / \mathrm{cm}^{3} \end{gathered}$ | Volume of 1 g in $\mathrm{cm}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -10 | 13.6198 | . 0734225 | 20 | 13.5458 | . 0738233 | 140 | 13.2563 | . 0754354 |
| -9 | 6173 | 4358 | 21 | 5434 | 8367 | 150 | 2326 | 5708 |
| -8 | 6148 | 4492 | 22 | 5409 | 8501 | 160 | 2090 | 7064 |
| - 7 | 6124 | 4626 | 23 | 5385 | 8635 | 170 | 1853 | 8422 |
| - 6 | 6099 | 4759 | 24 | 5360 | 8768 | 180 | 1617 | 9784 |
| $-5$ | 13.6074 | . 0734893 | 25 | 13.5336 | . 0738902 | 190 | 13.1381 | . 0761149 |
| -4 | 6050 | 5026 | 26 | 5311 | 9036 | 200 | 1145 | 2516 |
| - 3 | 6025 | 5160 | 27 | 5287 | 9170 | 210 | 0910 | 3886 |
| -2 | 6000 | 5293 | 28 | 5262 | 9304 | 220 | 0677 | 5260 |
| -1 | 5976 | 5427 | 29 | 5238 | 9437 | 230 | 0440 | 6637 |
| - 0 | 13.5951 | . 0735560 | 30 | 13.5213 | . 0739572 | 240 | 13.0206 | . 0768017 |
| 1 | 5926 | 5694 | 31 | 5189 | 9705 | 250 | 12.9972 | 9402 |
| 2 | 5901 | 5828 | 32 | 5164 | 9839 | 260 | 9738 | 7090 |
| 3 | 5877 | 5961 | 33 | 5140 | 9973 | 270 | 9504 | 2182 |
| 4 | 5852 | 6095 | 34 | 5116 | 40107 | 280 | 9270 | 3579 |
| 5 | 13.5827 | . 0736228 | 35 | 13.5091 | . 0740241 | 290 | 12.9036 | . 0774979 |
| 6 | 5803 | 6362 | 36 | 5066 | 0374 | 300 | 8803 | 6385 |
| 7 | 5778 | 6496 | 37 | 5042 | 0508 | 310 | 8569 | 7795 |
| 8 | 5754 | 6629 | 38 | 5018 | 0642 | 320 | 8336 | 9210 |
| 9 | 5729 | 6763 | 39 | 4994 | 0776 | 330 | 8102 | 80630 |
| 10 | 13.5704 | . 0736893 | 40 | 13.4969 | . 0740910 | 340 | 12.7869 | . 0782054 |
| 11 | 5680 | 7030 | 50 | 4725 | 2250 | 350 | 7635 | 3485 |
| 12 | 5655 | 7164 | 60 | 4482 | 3592 | 360 | 7402 | 4921 |
| 13 | 5630 | 7298 | 70 | 4240 | 4936 |  |  |  |
| 14 | 5606 | 7431 | 80 | 3998 | 6282 |  |  |  |
| 15 | 13.5581 | . 0737565 | 90 | 13.3723 | . 0747631 |  |  |  |
| 16 | 5557 | 7699 | 100 | 3515 | 8981 |  |  |  |
| 17 | 5532 | 7832 | 110 | 3279 | 50305 |  |  |  |
| 18 | 5507 | 7966 | 120 | 3040 | 1653 |  |  |  |
| 19 | 5483 | 8100 | 130 | 2801 | 3002 |  |  |  |

The following table gives the density of solutions of various salts in water. The numbers give the weight in $\mathrm{g} / \mathrm{cm}^{3}$. For brevity the substance is indicated by formula only.

|  | Weight of the dissolved substance in 100 parts by weight of the solution |  |  |  |  |  |  |  |  | , |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Substance | 5 | 10 | 15 | 20 | 25 | 30 | 40 | 50 | 60 | - |
| $\mathrm{K}_{2} \mathrm{O}$ | 1.047 | 1.098 | 1.153 | 1.214 | 1.284 | 1.354 | 1.503 | 1.659 | 1.809 | 15. |
| KOH | 1.040 | 1.082 | 1.127 | 1.176 | 1.229 | 1.286 | 1.410 | 1.538 | 1.666 | 15. |
| $\mathrm{Na}_{2} \mathrm{O}$ | 1.073 | 1.144 | 1.218 | 1.284 | 1.354 | 1.421 | 1.557 | 1.689 | 1.829 | 15. |
| NaOH | 1.058 | 1.114 | 1.169 | 1.224 | 1.279 | 1.331 | 1.436 | 1.539 | 1.642 | 15. |
| $\mathrm{NH}_{3}$ | . 978 | . 959 | . 940 | . 924 | . 909 | . 896 |  |  |  | 16. |
| $\mathrm{NH}_{4} \mathrm{Cl}$ | 1.015 | 1.030 | 1.044 | 1.058 | 1.072 | $\cdots$ | - | - | - | 15. |
| KCl | 1.031 | 1.065 | 1.099 | 1.135 |  |  | - |  |  | 15. |
| NaCl | 1.035 | 1.072 | 1.110 | 1.150 | 1.191 |  |  | - |  | 15. |
| LiCl | 1.029 | 1.057 | 1.085 | 1.116 | 1.147 | 1.181 | 1.255 | - |  | 15. |
| $\mathrm{CaCl}_{2}$ | 1.041 | 1.086 | 1.132 | 1.181 | 1.232 | 1.286 | 1.402 |  |  | 15. |
| $\mathrm{CaCl}_{2}+6 \mathrm{H}_{2} \mathrm{O}$ | 1.019 | 1.040 | 1.061 | 1.083 | 1.105 | 1.128 | 1.176 | 1.225 | 1.276 | 18. |
| $\mathrm{AlCl}_{3}$ | 1.030 | 1.072 | 1.111 | 1.153 | 1.196 | 1.241 | 1.340 | -- | - | 15. |
| $\mathrm{MgCl}_{2}$ | 1.041 | 1.085 | 1.130 | 1.177 | 1.226 | 1.278 |  |  |  | 15. |
| $\mathrm{MgCl}_{2}+6 \mathrm{H}_{2} \mathrm{O}$ | 1.014 | 1.032 | 1.049 | 1.067 | 1.085 | 1.103 | 1.141 | 1.183 | 1.222 | 24. |
| $\mathrm{ZnCl}_{2}$ | 1.043 | 1.089 | 1.135 | 1.184 | 1.236 | 1.289 | 1.417 | 1.563 | 1.737 | 19.5 |
| $\mathrm{CdCl}_{2}$ | 1.043 | 1.087 | 1.138 | 1.193 | 1.254 | 1.319 | 1.469 | 1.653 | 1.887 | 19.5 |
| $\mathrm{SrCl}_{2}$ | 1.044 | 1.092 | 1.143 | 1.198 | 1.257 | 1.321 |  |  | - | 15. |
| $\mathrm{SrCl}_{2}+6 \mathrm{H}_{2} \mathrm{O}$ | 1.027 | 1.053 | 1.082 | 1.111 | 1.042 | 1.174 | 1.242 | 1.317 |  | 15. |
| $\mathrm{BaCl}_{2}$ | 1.045 | 1.094 | 1.147 | 1.205 | 1.269 |  |  |  |  | 15. |
| $\mathrm{BaCl}_{2}+2 \mathrm{H}_{2} \mathrm{O}$ | 1.035 | 1.075 | 1.119 | 1.166 | 1.217 | 1.273 |  |  |  | 21. |
| $\mathrm{CuCl}_{2}$ | 1.044 | 1.091 | 1.155 | 1.221 | 1.291 | 1.360 | 1.527 | - | - | 17.5 |
| $\mathrm{NiCl}_{2}$ | 1.048 | 1.098 | 1.157 | 1.223 | 1.299 |  |  | - | - | 17.5 |
| $\mathrm{HgCl}_{2}$ | 1.041 | 1.092 |  |  |  |  | - |  | - | 20. |
| $\mathrm{Fe}_{2} \mathrm{Cl}_{8}$ | 1.041 | 1.086 | 1.130 | 1.179 | 1.232 | 1.290 | 1.413 | 1.545 | 1.668 | 17.5 |
| $\mathrm{PtCl}_{4}$ | 1.046 | 1.097 | 1.153 | 1.214 | 1.285 | 1.362 | 1.546 | 1.785 |  |  |
| $\mathrm{SnCl}_{2}+2 \mathrm{H}_{2} \mathrm{O}$ | 1.032 | 1.067 | 1.104 | 1.143 | 1.185 | 1.229 | 1.329 | 1.444 | 1.580 | 15. |
| $\mathrm{SnCl}_{4}+5 \mathrm{H}_{2} \mathrm{O}$ | 1.029 | 1.058 | 1.089 | 1.122 | 1.157 | 1.193 | 1.274 | 1.365 | 1.467 | 15. |
| LiBr | 1.033 | 1.070 | 1.111 | 1.154 | 1.202 | 1.252 | 1.366 | 1.489 |  | 19.5 |
| KBr | 1.035 | 1.073 | 1.114 | 1.157 | 1.205 | 1.254 | 1.364 |  |  | 19.5 |
| NaBr | 1.038 | 1.078 | 1.123 | 1.172 | 1.224 | 1.279 | 1.408 | 1.563 |  | 19.5 |
| $\mathrm{MgBr}_{2}$ | 1.041 | 1.085 | 1.135 | 1.189 | 1.245 | 1.308 | 1.449 | 1.623 |  | 19.5 |
| $\mathrm{ZnBr}{ }_{2}$ | 1.043 | 1.091 | 1.144 | 1.202 | 1.263 | 1.328 | 1.473 | 1.648 | 1.873 | 19.5 |
| $\mathrm{CdBr}_{2}$ | 1.041 | 1.088 | 1.139 | 1.197 | 1.258 | 1.324 | 1.479 | 1.678 |  | 19.5 |
| $\mathrm{CaBr}_{2}$ | 1.042 | 1.087 | 1.137 | 1.192 | 1.250 | 1.313 | 1.459 | 1.639 |  | 19.5 |
| $\mathrm{BaBr}_{2}$ | 1.043 | 1.690 | 1.142 | 1.199 | 1.260 | 1.327 | 1.483 | 1.683 |  | 19.5 |
| $\mathrm{SrBr}_{2}$ | 1.043 | 1.089 | 1.140 | 1.198 | 1.260 | 1.328 | 1.489 | 1.693 | 1.953 | 19.5 |
| KI | 1.036 | 1.076 | 1.118 | 1.164 | 1.216 | 1.269 | 1.394 | 1.544 | 1.732 | 19.5 |
| LiI | 1.036 | 1.077 | 1.122 | 1.170 | 1.222 | 1.278 | 1.412 | 1.573 | 1.775 | 19.5 |
| NaI | 1.038 | 1.080 | 1.126 | 1.177 | 1.232 | 1.292 | 1.430 | 1.598 | 1.808 | 19.5 |
| $\mathrm{ZnI}_{2}$ | 1.043 | 1.089 | 1.138 | 1.194 | 1.253 | 1.316 | 1.467 | 1.648 | 1.873 | 19.5 |
| $\mathrm{CdI}_{2}$ | 1.042 | 1.086 | 1.135 | 1.192 | 1.251 | 1.317 | 1.474 | 1.678 | -- | 19.5 |
| $\mathrm{MgI}_{2}$ | 1.041 | 1.086 | 1.137 | 1.192 | 1.252 | 1.318 | 1.472 | 1.666 | 1.913 | 19.5 |
| $\mathrm{CaI}_{2}$ | 1.042 | 1.088 | 1.138 | 1.196 | 1.258 | 1.319 | 1.475 | 1.663 | 1.908 | 19.5 |
| $\mathrm{SrI}_{2}$ | 1.043 | 1.089 | 1.140 | 1.198 | 1.260 | 1.328 | 1.489 | 1.693 | 1.953 | 19.5 |
| $\mathrm{BaI}_{2}$ | 1.043 | 1.089 | 1.141 | 1.199 | 1.263 | 1.331 | 1.493 | 1.702 | 1.968 | 19.5 |
| $\mathrm{NaClO}_{3}$ | 1.035 | 1.068 | 1.106 | 1.145 | 1.188 | 1.233 | 1.329 | - | - | 19.5 |
| $\mathrm{NaBrO}_{3}$ | 1.039 | 1.081 | 1.127 | 1.176 | 1.229 | 1.287 | - | - | - | 19.5 |
| $\mathrm{KNO}_{3}$ | 1.031 | 1.064 | 1.099 | 1.135 |  |  |  | - | - | 15. |
| $\mathrm{NaNO}_{3}$ | 1.031 | 1.065 | 1.101 | 1.140 | 1.180 | 1.222 | 1.313 | 1.416 |  | 20.2 |
| $\mathrm{AgNO}_{3}$ | 1.044 | 1.090 | 1.140 | 1.195 | 1.255 | 1.322 | 1.479 | 1.675 | 1.918 | 15. |

[^133]TABLE 292.-DENSITY OF AQUEOUS SOLUTIONS (concluded)
Weight of the dissolved substance in 100 parts by weight of

IN g/mi

The densities in this table are numerically the same as specific gravities at the various temperatures in terms of water at $4^{\circ} \mathrm{C}$ as unity. Based upon work done at the National Bureau of Standards.

| Percent$\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{OH}$by weight | Temperatures |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{\circ} \mathrm{C}$ | $15^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $25^{\circ} \mathrm{C}$ | $30^{\circ} \mathrm{C}$ | $35^{\circ} \mathrm{C}$ | $40^{\circ} \mathrm{C}$ |
|  | . 99973 | . 99913 | . 99823 | . 99708 | . 99568 | . 99406 | . 99225 |
| 1 | 785 | 725 | 636 | 520 | 379 | 217 | 034 |
| 2 | 602 | 542 | 453 | 336 | 194 | 031 | . 98846 |
| 3 | 426 | 365 | 275 | 157 | 014 | . 98849 | 663 |
| 4 | 258 | 195 | 103 | . 98984 | . 98839 | 672 | 485 |
| 5 | 098 | 032 | . 98938 | 817 | 670 | 501 | 311 |
| 6 | . 98946 | . 98877 | 780 | 656 | 507 | 335 | 142 |
| 7 | 801 | 729 | 627 | 500 | 347 | 172 | . 97975 |
| 8 | 660 | 584 | 478 | 346 | 189 | 009 | 808 |
| 9 | 524 | 442 | 331 | 193 | 031 | . 97846 | 641 |
| 10 | 393 | 304 | 187 | 043 | . 97875 | 685 | 475 |
| 11 | 267 | 171 | 047 | . 97897 | 723 | 527 | 312 |
| 12 | 145 | 041 | . 97910 | 753 | 573 | 371 | 150 |
| 13 | 026 | . 97914 | 775 | 611 | 424 | 216 | . 96989 |
| 14 | . 97911 | 790 | 643 | 472 | 278 | 063 | 829 |
| 15 | 800 | 669 | 514 | 334 | 133 | . 96911 | 670 |
| 16 | 692 | 552 | 387 | 199 | . 96990 | 760 | 512 |
| 17 | 583 | 433 | 259 | 062 | 844 | 607 | 352 |
| 18 | 473 | 313 | 129 | . 96923 | 697 | 452 | 189 |
| 19 | 363 | 191 | . 96997 | 782 | 547 | 294 | 023 |
| 20 | 252 | 068 | 864 | 639 | 395 | 134 | . 95856 |
| 21 | 139 | . 96944 | 729 | 495 | 242 | . 95973 | 687 |
| 22 | 024 | 818 | 592 | 348 | 087 | 809 | 516 |
| 23 | . 96907 | 689 | 453 | 199 | . 95929 | 643 | 343 |
| 24 | 787 | 558 | 312 | 048 | 769 | 476 | 168 |
| 25 | 665 | 424 | 168 | . 95895 | 607 | 306 | . 94991 |
| 26 | 539 | 287 | 020 | 738 | 442 | 133 | 810 |
| 27 | 406 | 144 | . 95867 | 576 | 272 | . 94955 | 625 |
| 28 | 268 | . 95996 | 710 | 410 | 098 | 774 | 438 |
| 29 | 125 | 844 | 548 | 241 | . 94922 | 590 | 248 |
| 30 | . 95977 | 686 | 382 | 067 | 741 | 403 | 055 |
| 31 | 823 | 524 | 212 | . 94890 | 557 | 214 | . 93860 |
| 32 | 665 | 357 | 038 | 709 | 370 | 021 | 662 |
| 33 | 502 | 186 | . 94860 | 525 | 180 | . 93825 | 461 |
| 34 | 334 | 011 | 679 | 337 | . 93986 | 626 | 257 |
| 35 | 162 | . 94832 | 494 | 146 | 790 | 425 | 051 |
| 36 | . 94986 | 650 | 306 | . 93952 | 591 | 221 | . 92843 |
| 37 | 805 | 464 | 114 | 756 | 390 | 016 | 634 |
| 38 | 620 | 273 | . 93910 | 556 | 186 | . 92808 | 422 |
| 39 | 431 | 079 | 720 | 353 | . 92979 | 597 | 208 |
| 40 | 238 | . 93882 | 518 | 148 | 770 | 385 | . 91992 |
| 41 | 042 | 682 | 314 | . 92940 | 558 | 170 | 774 |
| 42 | . 93842 | 478 | 107 | 729 | 344 | . 91952 | 554 |
| 43 | 639 | 271 | . 92897 | 516 | 128 | 733 | 332 |
| 44 | 433 | 062 | 685 | 301 | . 91910 | 513 | 108 |
| 45 | 226 | . 92852 | 472 | 085 | 692 | 291 | . 90884 |
| 46 | 017 | 640 | 257 | . 91868 | 472 | 069 | 660 |
| 47 | . 92806 | 426 | 041 | 649 | 250 | . 90845 | 434 |
| 48 | 593 | 211 | . 91823 | 429 | 028 | 621 | 207 |
| 49 | 379 | . 91995 | 604 | 208 | . 90805 | 396 | . 89979 |
| 50 | 162 | 776 | 384 | . 90985 | 580 | 168 | 750 |
|  |  |  | (co | ued) |  |  |  |

TABLE 293.-DENSITY OF MIXTURES OF ETHYL ALCOHOL AND WATER IN g/mI (concluded)

| Percent <br> $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{OH}$ <br> by weight | Temperatures |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{\circ} \mathrm{C}$ | $15^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $25^{\circ} \mathrm{C}$ | $30^{\circ} \mathrm{C}$ | $35^{\circ} \mathrm{C}$ | $40^{\circ} \mathrm{C}$ |
| 50 | . 92162 | . 91776 | . 91384 | . 90985 | . 90580 | . 90168 | . 89750 |
| 51 | . 91943 | 555 | 160 | 760 | 353 | . 89940 | 519 |
| 52 | 723 | 333 | . 90936 | 534 | 125 | 710 | 288 |
| 53 | 502 | 110 | 711 | 307 | . 89896 | 479 | 056 |
| 54 | 279 | . 90885 | 485 | 079 | 667 | 248 | . 88823 |
| 55 | 055 | 659 | 258 | . 89850 | 437 | 016 | 589 |
| 56 | . 90831 | 433 | 031 | 621 | 206 | . 88784 | 356 |
| 57 | 607 | 207 | . 89803 | 392 | . 88975 | 552 | 122 |
| 58 | 381 | . 89980 | 574 | 162 | 744 | 319 | . 87888 |
| 59 | 154 | 752 | 344 | . 88931 | 512 | 085 | 653 |
| 60 | . 89927 | 523 | 113 | 699 | 278 | . 87851 | 417 |
| 61 | 698 | 293 | . 88882 | 466 | 044 | 615 | 180 |
| 62 | 468 | 062 | 650 | 233 | . 87809 | 379 | . 86943 |
| 63 | 237 | . 88830 | 417 | . 87998 | 574 | 142 | 705 |
| 64 | 006 | 597 | 183 | 763 | 337 | . 86905 | 466 |
| 65 | . 88774 | 364 | . 87948 | 527 | 100 | 667 | 227 |
| 66 | 541 | 130 | 713 | 291 | . 86863 | 429 | . 85987 |
| 67 | 308 | . 87895 | 477 | 054 | 625 | 190 | 747 |
| 68 | 074 | 660 | 241 | . 86817 | 387 | . 85950 | 507 |
| 69 | . 87839 | 424 | 004 | 579 | 148 | 710 | 266 |
| 70 | 602 | 187 | . 86766 | 340 | . 85908 | 470 | 025 |
| 71 | 365 | . 86949 | 527 | 100 | 667 | 228 | . 84783 |
| 72 | 127 | 710 | 287 | . 85859 | 426 | . 84986 | 540 |
| 73 | . 86888 | 470 | 047 | 618 | 184 | 743 | 297 |
| 74 | 648 | 229 | . 85806 | 376 | . 84941 | 500 | 053 |
| 75 | 408 | . 85988 | 564 | 134 | 698 | 257 | . 83809 |
| 76 | 168 | 747 | 322 | . 84891 | 455 | 013 | 564 |
| 77 | . 85927 | 505 | 079 | 647 | 211 | . 83768 | 319 |
| 78 | 685 | 262 | . 84835 | 403 | . 83966 | 523 | 074 |
| 79 | 442 | 018 | 590 | 158 | 720 | 277 | . 82827 |
| 80 | 197 | . 84772 | 344 | . 83911 | 473 | 029 | 578 |
| 81 | . 84950 | 525 | 096 | 664 | 224 | . 82780 | 329 |
| 82 | 702 | 277 | . 83848 | 415 | . 82974 | 530 | 079 |
| 83 | 453 | 028 | 599 | 164 | 724 | 279 | . 81828 |
| 84 | 203 | . 83777 | 348 | . 82913 | 473 | 027 | 576 |
| 85 | . 83951 | 525 | 095 | 660 | 220 | . 81774 | 322 |
| 86 | 697 | 271 | . 82840 | 405 | . 81965 | 519 | 067 |
| 87 | 441 | 014 | 583 | 148 | 708 | 262 | . 80811 |
| 88 | 181 | . 82754 | 323 | . 81888 | 448 | 003 | 552 |
| 89 | . 82919 | 492 | 062 | 626 | 186 | . 80742 | 291 |
| 90 | 654 | 227 | . 81797 | 362 | . 80922 | 478 | 028 |
| 91 | 386 | . 81959 | 529 | 094 | 655 | 211 | . 79761 |
| 92 | 114 | 688 | 257 | . 80823 | 384 | . 79941 | 491 |
| 93 | . 81839 | 413 | . 80983 | 549 | 111 | 669 | 220 |
| 94 | 561 | 134 | 705 | 272 | . 79835 | 393 | . 78947 |
| 95 | 278 | . 80852 | 424 | . 79991 | 555 | 114 | 670 |
| 96 | . 80991 | 566 | 138 | 706 | 271 | . 78831 | 388 |
| 97 | 698 | 274 | . 79846 | 415 | . 78981 | 542 | 100 |
| 98 | 399 | . 79975 | 547 | 117 | 684 | 247 | . 77806 |
| 99 | 094 | 670 | 243 | . 78814 | 382 | . 77946 | 507 |
| 100 | . 79784 | 360 | . 78934 | 506 | 075 | 641 | 203 |

TABLE 294.-DENSITY OF AQUEOUS MIXTURES OF METHYL ALCOHOL, CANE SUGAR, OR SULFURIC ACID

| $\begin{gathered} \text { Percent } \\ \text { by weight } \\ \text { of } \\ \text { substance } \end{gathered}$ | Methyl <br> D $\frac{15^{\circ}}{4^{\circ}} \mathrm{C}$ | $\begin{gathered} \text { Cane } \\ \text { Sugar } \\ \text { sugar } \end{gathered}$ | $\begin{aligned} & \text { Sulfuric } \\ & \text { acid } \\ & \text { D } \frac{20^{\circ}}{4^{\circ}} \mathrm{C} \end{aligned}$ | $\begin{gathered} \text { Percent } \\ \text { by weight } \\ \text { of } \\ \text { substance } \end{gathered}$ | $\begin{aligned} & \text { Methyl } \\ & \text { alacohol } \\ & \text { D } \frac{15^{\circ}}{4^{\circ}} \mathrm{C} \end{aligned}$ | $\begin{gathered} \text { Cane } \\ \text { sugar } \\ 20^{\circ} \end{gathered}$ | $\begin{aligned} & \text { Sulfuric } \\ & \text { acid } \\ & \text { D } \frac{20^{\circ}}{4^{\circ}} \mathrm{C} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 99913 | . 998234 | . 99823 | 50 | . 91852 | 1.229567 | 1.39505 |
| 1 | . 99727 | 1.002120 | 1.00506 | 51 | . 91653 | 1.235085 | 1.40487 |
| 2 | . 99543 | 1.006015 | 1.01178 | 52 | . 91451 | 1.240641 | 1.41481 |
| 3 | . 99370 | 1.009934 | 1.01839 | 53 | . 91248 | 1.246234 | 1.42487 |
| 4 | . 99198 | 1.013881 | 1.02500 | 54 | . 91044 | 1.251866 | 1.43503 |
| 5 | . 99029 | 1.017854 | 1.03168 | 55 | . 90839 | 1.257535 | 1.44530 |
| 6 | . 98864 | 1.021855 | 1.03843 | 56 | . 90631 | 1.263243 | 1.45568 |
| 7 | . 98701 | 1.025885 | 1.04527 | 57 | . 90421 | 1.268989 | 1.46615 |
| 8 | . 98547 | 1.029942 | 1.05216 | 58 | . 90210 | 1.274774 | 1.47673 |
| 9 | . 98394 | 1.034029 | 1.05909 | 59 | . 89996 | 1.280595 | 1.48740 |
| 10 | . 98241 | 1.038143 | 1.06609 | 60 | . 89781 | 1.286456 | 1.49818 |
| 11 | . 98093 | 1.042288 | 1.07314 | 61 | . 89563 | 1.292354 | 1.50904 |
| 12 | . 97945 | 1.046462 | 1.08026 | 62 | . 89341 | 1.298291 | 1.51999 |
| 13 | . 97802 | 1.050665 | 1.08744 | 63 | . 89117 | 1.304267 | 1.53102 |
| 14 | . 97650 | 1.054900 | 1.09468 | 64 | . 88890 | 1.310282 | 1.54213 |
| 15 | . 97518 | 1.059165 | 1.10199 | 65 | . 88662 | 1.316334 | 1.55333 |
| 16 | . 97377 | 1.063460 | 1.10936 | 66 | . 88433 | 1.322425 | 1.56460 |
| 17 | . 97237 | 1.067789 | 1.11679 | 67 | . 88203 | 1.328554 | 1.57595 |
| 18 | . 97096 | 1.072147 | 1.12428 | 68 | . 87971 | 1.334722 | 1.58739 |
| 19 | . 96955 | 1.076537 | 1.13183 | 69 | . 87739 | 1.340928 | 1.59890 |
| 20 | . 96814 | 1.080959 | 1.13943 | 70 | . 87507 | 1.347174 | 1.61048 |
| 21 | . 96673 | 1.085414 | 1.14709 | 71 | . 87271 | 1.353456 | 1.62213 |
| 22 | . 96533 | 1.089900 | 1.15480 | 72 | . 87033 | 1.359778 | 1.63384 |
| 23 | . 96392 | 1.094420 | 1.16258 | 73 | . 86792 | 1.366139 | 1.64560 |
| 24 | . 96251 | 1.098971 | 1.17041 | 74 | . 86546 | 1.372536 | 1.65738 |
| 25 | . 96108 | 1.103557 | 1.17830 | 75 | . 86300 | 1.378971 | 1.66917 |
| 26 | . 95963 | 1.108175 | 1.18624 | 76 | . 86051 | 1.385446 | 1.68095 |
| 27 | . 95817 | 1.112828 | 1.19423 | 77 | . 85801 | 1.391956 | 1.69268 |
| 28 | . 95668 | 1.117512 | 1.20227 | 78 | . 85551 | 1.398505 | 1.70433 |
| 29 | . 95518 | 1.122231 | 1.21036 | 79 | . 85300 | 1.405091 | 1.71585 |
| 30 | . 95366 | 1.126984 | 1.21850 | 80 | . 85048 | 1.411715 | 1.72717 |
| 31 | . 95213 | 1.131773 | 1.22669 | 81 | . 84794 | 1.418374 | 1.73827 |
| 32 | . 95056 | 1.136596 | 1.23492 | 82 | . 84536 | 1.425072 | 1.74904 |
| 33 | . 94896 | 1.141453 | 1.24320 | 83 | . 84274 | 1.431807 | 1.75943 |
| 34 | . 94734 | 1.146345 | 1.25154 | 84 | . 84009 | 1.438579 | 1.76932 |
| 35 | . 94570 | 1.151275 | 1.25992 | 85 | . 83742 | 1.445388 | 1.77860 |
| 36 | . 94404 | 1.156238 | 1.26836 | 86 | . 83475 | 1.452232 | 1.78721 |
| 37 | . 94237 | 1.161236 | 1.27685 | 87 | . 83207 | 1.459114 | 1.79509 |
| 38 | . 94067 | 1.166269 | 1.28543 | 88 | . 82937 | 1.466032 | 1.80223 |
| 39 | . 93894 | 1.171340 | 1.29407 | 89 | . 82667 | 1.472986 | 1.80864 |
| 40 | . 93720 | 1.176447 | 1.30278 | 90 | . 82396 | 1.479976 | 1.81438 |
| 41 | . 93543 | 1.181592 | 1.31157 | 91 | . 82124 | 1.487002 | 1.81950 |
| 42 | . 93365 | 1.186773 | 1.32043 | 92 | . 81849 | 1.494063 | 1.82401 |
| 43 | . 93185 | 1.191993 | 1.32938 | 93 | . 81568 | 1.501158 | 1.82790 |
| 44 | . 93001 | 1.197247 | 1.33843 | 94 | . 81285 | 1.508289 | 1.83115 |
| 45 | . 92815 | 1.202540 | 1.34759 | 95 | . 80999 | 1.515455 | 1.83368 |
| 46 | . 92627 | 1.207870 | 1.35686 | 96 | . 80713 | 1.522656 | 1.83548 |
| 47 | . 92436 | 1.213238 | 1.36625 | 97 | . 80428 | 1.529891 | 1.83637 |
| 48 | . 92242 | 1.218643 | 1.37574 | 98 | . 80143 | 1.537161 | 1.83605 |
| 49 | . 92048 | 1.224086 | 1.38533 | 99 | . 79859 | 1.544462 |  |
| 50 | . 91852 | 1.229567 | 1.39505 | 100 | . 79577 | 1.551800 |  |

## TABLE 295.-DENSITY, BRIX, AND BAUMÉ DEGREES, OF CANE-SUGAR SOLUTIONS

Degrees Brix, specific gravity, and degrees Baumé of sugar solutions.
Degrees Brix = percent sucrose by weight.
Specific gravities and degrees Baumé corresponding to the degrees Brix are for $\frac{20^{\circ}}{20^{\circ}} \mathrm{C}$.
The relation between the specific gravity and degrees Baumé is given by degrees Baumé $=$ $145-\frac{145}{\text { specific gravity }}$

| Degrees Brix or percent by wẹight | $\begin{gathered} \text { Specific } \\ \text { gravity at } \\ 20^{\circ} / 20^{\circ} \mathrm{C} \end{gathered}$ | $\begin{aligned} & \text { Degrees } \\ & \text { Baume } \\ & \text { (modu } \\ & \text { lus 145) } \end{aligned}$ | Degrees Brix or percent by weight | $\begin{gathered} \text { Srecific } \\ \text { gravity at } \\ 20^{\circ} / 20^{\circ} \mathrm{C} \end{gathered}$ | $\begin{aligned} & \text { Degrees } \\ & \text { Baumé } \\ & \text { (modu. } \\ & \text { lus } 1+5 \text { ) } \end{aligned}$ | Degrees Brix or percent by weight | $\begin{gathered} \text { Specific } \\ \text { gravity at } \\ 20^{\circ} / 20^{\circ} \mathrm{C} \end{gathered}$ | Degrees Baume (modu. <br> lus 145 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 0 | 1.00000 | . 00 | 40.0 | 1.17853 | 21.97 | 80.0 | 1.41421 | 42.47 |
| 1.0 | 1.00389 | . 56 | 41.0 | 1.18368 | 22.50 | 81.0 | 1.42088 | 42.95 |
| 2.0 | 1.00779 | 1.12 | 42.0 | 1.18887 | 23.04 | 82.0 | 1.42759 | 43.43 |
| 3.0 | 1.01172 | 1.68 | 43.0 | 1.19410 | 23.57 | 83.0 | 1.43434 | 43.91 |
| 4.0 | 1.01567 | 2.24 | 44.0 | 1.19936 | 24.10 | 84.0 | 1.44112 | 44.38 |
| 5.0 | 1.01965 | 2.79 | 45.0 | 1.20467 | 24.63 | 85.0 | 1.44794 | 44.86 |
| 6.0 | 1.02366 | 3.35 | 46.0 | 1.21001 | 25.17 | 86.0 | 1.45480 | 45.33 |
| 7.0 | 1.02770 | 3.91 | 47.0 | 1.21538 | 25.70 | 87.0 | 1.46170 | 45.80 |
| 8.0 | 1.03176 | 4.46 | 48.0 | 1.22080 | 26.23 | 88.0 | 1.46862 | 46.27 |
| 9.0 | 1.03586 | 5.02 | 49.0 | 1.22625 | 26.75 | 89.0 | 1.47559 | 46.73 |
| 10.0 | 1.03998 | 5.57 | 50.0 | 1.23174 | 27.28 | 90.0 | 1.48259 | 47.20 |
| 11.0 | 1.04413 | 6.13 | 51.0 | 1.23727 | 27.81 | 91.0 | 1.48963 | 47.66 |
| 12.0 | 1.04831 | 6.68 | 52.0 | 1.24284 | 28.33 | 92.0 | 1.49671 | 48.12 |
| 13.0 | 1.05252 | 7.24 | 53.0 | 1.24844 | 28.86 | 93.0 | 1.50381 | 48.58 |
| 14.0 | 1.05677 | 7.79 | 54.0 | 1.25408 | 29.38 | 94.0 | 1.51096 | 49.03 |
| 15.0 | 1.06104 | 8.34 | 55.0 | 1.25976 | 29.90 | 95.0 | 1.51814 | 49.49 |
| 16.0 | 1.06534 | 8.89 | 56.0 | 1.26548 | 30.42 | 96.0 | 1.52535 | 49.94 |
| 17.0 | 1.06968 | 9.45 | 57.0 | 1.27123 | 30.94 | 97.0 | 1.53260 | 50.39 |
| 18.0 | 1.07404 | 10.00 | 58.0 | 1.27703 | 31.46 | 98.0 | 1.53988 | 50.84 |
| 19.0 | 1.07844 | 10.55 | 59.0 | 1.28286 | 31.97 | 99.0 | 1.54719 | 51.28 |
| 20.0 | 1.08287 | 11.10 | 60.0 | 1.28873 | 32.49 | 100.0 | 1.55454 | 51.73 |
| 21.0 | 1.08733 | 11.65 | 61.0 | 1.29464 | 33.00 |  |  |  |
| 22.0 | 1.09183 | 12.20 | 62.0 | 1.30059 | 33.51 |  |  |  |
| 23.0 | 1.09636 | 12.74 | 63.0 | 1.30657 | 34.02 |  |  |  |
| 24.0 | 1.10092 | 13.29 | 64.0 | 1.31260 | 34.53 |  |  |  |
| 25.0 | 1.10551 | 13.84 | 65.0 | 1.31866 | 35.04 |  |  |  |
| 26.0 | 1.11014 | 14.39 | 66.0 | 1.32476 | 35.55 |  |  |  |
| 27.0 | 1.11480 | 14.93 | 67.0 | 1.33090 | 36.05 |  |  |  |
| 28.0 | 1.11949 | 15.48 | 68.0 | 1.33708 | 36.55 |  |  |  |
| 29.0 | 1.12422 | 16.02 | 69.0 | 1.34330 | 37.06 |  |  |  |
| 30.0 | 1.12898 | 16.57 | 70.0 | 1.34956 | 37.56 |  |  |  |
| 31.0 | 1.13378 | 17.11 | 71.0 | 1.35585 | 38.06 |  |  |  |
| 32.0 | 1.13861 | 17.65 | 72.0 | 1.36218 | 38.55 |  |  |  |
| 33.0 | 1.14347 | 18.19 | 73.0 | 1.36856 | 39.05 |  |  |  |
| 34.0 | 1.14837 | 18.73 | 74.0 | 1.37496 | 39.54 |  |  |  |
| 35.0 | 1.15331 | 19.28 | 75.0 | 1.38141 | 40.03 |  |  |  |
| 36.0 | 1.15828 | 19.81 | 76.0 | 1.38790 | 40.53 |  |  |  |
| 37.0 | 1.16329 | 20.35 | 77.0 | 1.39442 | 41.01 |  |  |  |
| 38.0 | 1.16833 | 20.89 | 78.0 | 1.40098 | 41.50 |  |  |  |
| 39.0 | 1.17341 | 21.43 | 79.0 | 1.40758 | 41.99 |  |  |  |

TABLE 296.-VELOCITY OF SOUND IN GASES ${ }^{08}$

| Gas | ${ }^{\text {Temp. }}$ | Velocity $\mathrm{m} / \mathrm{sec}$ | Gas | Temp. | Velocity $\mathrm{m} / \mathrm{sec}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Air, dry, 1 atm. | 0 | 331.7 | Hydrogen bromide | 0 | 200 |
| ". " 25 ". | 0 | 332.0 | Hydrogen chloride | 0 | 296 |
| " " 50 " | 0 | 334.7 | Hydrogen iodide . | 0 | 157 |
| " " 100 " | 0 | 350.6 | Hydrogen sulfide | 0 | 289 |
| " | 100 | 386 | Illuminating gas | 0 | 490.4 |
| " " | 500 | 553 | Methane ...... | 0 | 430 |
| " " . | 1000 | 700 | Neon | 0 | 435 |
| Ammonia | 0 | 415 | Nitric oxide | 10 | 324 |
| Argon | 0 | 319 | Nitrogen | 0 | 334 |
| Carbon dioxide | 0 | 259 | Nitrous oxide | 0 | 263 |
| Carbon monoxide | 0 | 338 | Oxygen | 0 | 316 |
| Chlorine | 0 | 206 | Silicon tetrafluoride | 0 | 167 |
| Ethane | 10 | 308 | Sulfur dioxide | 0 | 213 |
| Ethylene | 0 | 317 | Vapors: |  |  |
| Helium | 0 | 965 | alcohol | 0 | 230.6 |
| Hydrogen (heavy) | 0 | 890 | ether | 0 | 179.2 |
| Hydrogen (light). | 0 | 1284 | water | 0 100 | $\begin{aligned} & 401 \\ & 404.8 \end{aligned}$ |

* Tables 296 and 298-300 prepared by Urick and Weissler, Naval Research Laboratory
${ }^{08}$ Bergmann, Ultrasonics, 3d ed., p. 223, Edwards Brothers, Ann Arbor, Mich., 1944.


## TABLE 297.-VELOCITY OF SOUND IN SOLIDS

The velocity of sounds in solids varies as $V \overline{E / \rho}$, where $E$ is Young's modulus of elasticity and $\rho$ the density. These constants for most materials vary through a somewhat wide range. The numbers can be taken only as rough approximations to the velocity in any particular case. When temperatures are not marked, between $10^{\circ}$ and $20^{\circ}$ is to be understood.

| Substance | $t^{\circ} \mathrm{C}$ | $\mathrm{m} / \mathrm{sec}$ | Substance |  | $t^{\circ} \mathrm{C}$ | $\stackrel{\nu}{\mathrm{m} / \mathrm{sec}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ag hard | 20 | 2678 | Fe |  | 200 | 4720 |
|  | 100 | 2640 |  |  | 20 | 4990 |
| " " | 200 | 2480 | " |  | 100 | 4920 |
| Al |  | 5104 | " |  | 200 | 4790 |
| Au hard | 20 | 1743 | Mg |  |  | 4602 |
| " " | 100 | 1720 | Ni |  |  | 4973 |
| Cd |  | 2307 | Pb |  |  | 1322 |
| Co |  | 4724 | Pd |  |  | 3150 |
| Cu | 20 | 3560 | Pt |  | 20 | 2690 |
|  | 100 | 3290 | " |  | 100 | 2570 |
| " | 200 | 2950 | ' |  | 200 | 2460 |
| Fe | 20 | 5130 | Sn |  |  | 2500 |
|  | 100 | 5300 | Zn |  |  | 3700 |
| Ash, along the fiber. |  | 4670 | Brick |  |  | 3652 |
| " across the rings. |  | 1390 | Clay rock |  |  | 3480 |
| " along the rings. |  | 1260 | Cork . . . |  |  | 500 |
| Beech, along the fiber. |  | 3340 | Granite |  |  | 3950 |
| across the rings |  | 1840 | Marble |  |  | 3810 |
| "" along the rings . |  | 1415 | Paraffin |  | 15 | 1304 |
| Elm, along the fiber.. |  | 4120 | Slate . |  |  | 4510 |
| " across the rings. |  | 1420 | Tallow |  | 16 | 390 |
| " along the rings. |  | 1013 | Tuff |  |  | 2850 |
| Fir, along the fiber....... |  | 4640 | Glass |  |  | 5000 |
| Mahogany, along the fiber |  | 4135 | Glass |  |  | 6000 |
| Maple, along the fiber. . |  | 4110 | Ivory |  |  | 3013 |
| Oak, along the fiber. . |  | 3850 | Vul. rubber | (black) | $\left\{\begin{array}{r}0 \\ 50\end{array}\right.$ | 54 |
| Pine, along the fiber... |  | 3320 | "ul. rubber | (black) | $\{50$ | 31 |
| Poplar, along the fiber... |  | 4280 | " " | (red) | 0 | 69 |
| Sycamore, along the fiber. |  | 4460 | " " | " | 70 | 34 |
|  |  |  | Wax |  | 17 | 880 |
|  |  |  | " |  | 28 | 441 |


| Liquid | Temper. ature ${ }^{\circ} \mathrm{C}$ | Sound <br> velocity <br> $\mathrm{m} / \mathrm{sec}$ | $\underset{\mathrm{g} / \mathrm{ml}}{\substack{\text { Density }}}$ | Liquid | Temper${ }_{0}{ }^{\text {at }} \mathrm{C}$ | Sound velocity $\mathrm{m} / \mathrm{sec}$ | $\underset{\mathrm{g} / \mathrm{ml}}{\substack{\text { Density }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Acetone ${ }^{\text {c }}$ | 30 | 1146 | . 7788 | Silicon tetrachloride ${ }^{\text {a }}$ | 30 | 766.2 | 1.4622 |
| Alcohol, abs. ethyl ${ }^{\text {a }}$ | 30 | 1127.4 | . 7809 | Silicone |  |  |  |
| Alcohol methy ${ }^{\text {a }}$ | 30 | 1088.9 | . 7816 | DC 500-. $65 \mathrm{cs}^{\text {a }}$ | 30 | 873.2 | . 7535 |
| Alcohol, n-dodecyla | 30 | 1388.0 | . 8269 | DC 500-5.0 $\mathrm{cs}^{\text {a }}$ | 30 | 953.8 | . 9083 |
| Benzene ${ }^{\text {d }}$. ........ | 30 | 1276.4 | . 8685 | DC 500-50 cs ${ }^{\text {a }}$ | 30 | 981.6 | . 9540 |
| Carbon disulfide ${ }^{\text {b }}$ | 23 | 1149 | 1.258 | Sorbitol, $83 \%$ solut |  |  |  |
| Carbon tetrachloride ${ }^{\text {a }}$ | 30 | 905.8 | 1.5746 | in water ${ }^{\text {a }}$. ... | 30 | 2040 | 1.31 |
| Chloroform ${ }^{\text {" }}$ | 20 | 1002 | 1.488 | Turpentine ${ }^{\text {b }}$ | 27 | 1280 | . 893 |
| Ether ${ }^{\text {c }}$ | 30 | 949 | . 7019 | Water (distilled) ${ }^{\text {e }}$ | 0 | 1403.5 |  |
| Ethylene glycol ${ }^{\text {a }}$ | 30 | 1643.5 | 1.1068 |  | 10 | 1448.0 |  |
| Glycerine ${ }^{\text {c }}$ | 30 | 1905 | 1.2553 |  | 20 | 1483.1 |  |
| Heptane ${ }^{\text {c }}$ | 30 | 1112 | . 6751 |  | 30 | 1509.9 |  |
| Heptene ${ }^{\text {a }}$ | 30 | 1082 | . 6910 |  | 40 | 1529.5 |  |
| Heptyne ${ }^{\text {a }}$ | 30 | 1159.3 | . 7243 |  | 50 | 1543.5 |  |
| Hexadeca fluoro- |  |  |  |  | 60 | 1551.5 |  |
| heptane ${ }^{\text {d }}$ | 30 | 528.8 | 1.64 |  | 70 | 1555.3 |  |
| Mercury ${ }^{\text {b }}$ | 20 | 1451 | 13.595 |  | 80 | 1554.6 |  |
| Methylene iodide ${ }^{\text {d }}$ | 20 | 973.3 | 3.325 |  | 86 | 1552.4 |  |
|  |  |  |  |  | 94 | 1549.0 |  |

[^134]
## TABLE 299.-VELOCITY OF SOUND IN SEA WATER

(From various tables and formulae)

| Deptb <br> in <br> meters | ${ }^{\circ} \mathrm{C}$ | Sal. <br> ppt | $\overbrace{\text { Heck \& }}^{\text {Service }}$ | Wood | Br. Adm. <br> i927. | Br. Adm. <br> i | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

308 TABLE 300.-VELOCITY OF SOUND IN SEA WATER-DEPTH $=0$
(From Kuwahara)

|  | Meters per second |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{C}$ | $\mathrm{S}^{*}=31 \mathrm{ppt}$ | $\mathrm{S}=31 \mathrm{ppt}$ | $\mathrm{S}=35 \mathrm{ppt}$ | $\mathrm{S}=37 \mathrm{ppt}$ | $\mathrm{S}=39 \mathrm{ppt}$ |
| 0 | 1440.3 | 1442.9 | 1445.5 | 1448.1 | 1450.7 |
| 1 | 44.8 | 47.4 | 50.0 | 52.6 | 55.2 |
| 2 | 49.4 | 51.9 | 54.5 | 57.1 | 59.6 |
| 3 | 53.8 | 56.4 | 58.9 | 61.4 | 64.0 |
| 4 | 58.1 | 60.6 | 63.1 | 65.6 | 68.1 |
| 5 | 1462.3 | 1464.8 | 1467.3 | 1469.8 | 1472.3 |
| 6 | 66.5 | 68.9 | 71.4 | 73.9 | 76.3 |
| 7 | 70.5 | 73.0 | 75.4 | 77.9 | 80.3 |
| 8 | 74.5 | 76.9 | 79.3 | 81.7 | 84.2 |
| 9 | 78.3 | 80.7 | 83.1 | 85.5 | 87.9 |
| 10 | 1482.0 | 1484.4 | 1486.8 | 1489.2 | 1491.6 |
| 11 | 85.7 | 88.0 | 90.4 | 92.8 | 95.1 |
| 12 | 89.2 | 91.6 | 93.9 | 96.3 | 98.6 |
| 13 | 92.7 | 95.0 | 97.3 | 99.6 | 1502.0 |
| 14 | 96.0 | 98.3 | 1500.6 | 1502.9 | 05.2 |
| 15 | 1499.3 | 1501.6 | 1503.9 | 1506.2 | 1508.5 |
| 16 | 1502.5 | 04.7 | 07.0 | 09.3 | 11.5 |
| 17 | 05.6 | 07.9 | 10.1 | 12.3 | 14.6 |
| 18 | 08.6 | 10.8 | 13.0 | 15.2 | 17.5 |
| 19 | 11.5 | 13.7 | 15.9 | 18.1 | 20.3 |
| 20 | 1514.3 | 1516.5 | 1518.7 | 1520.9 | 1523.1 |
| 21 | 17.2 | 19.3 | 21.5 | 23.7 | 25.9 |
| 22 | 19.8 | 22.0 | 24.1 | 26.3 | 28.4 |
| 23 | 22.4 | 24.6 | 26.7 | 28.8 | 31.0 |
| 24 | 25.0 | 27.1 | 29.2 | 31.3 | 33.5 |
| 25 | 1527.5 | 1529.6 | 1531.7 | 1533.8 | 1535.9 |
| 26 | 29.9 | 32.0 | 34.1 | 36.2 | 38.3 |
| 27 | 32.3 | 34.3 | 36.4 | 38.5 | 40.6 |
| 28 | 34.6 | 36.6 | 38.7 | 40.8 | 42.9 |
| 29 | 36.9 | 39.0 | 41.0 | 43.1 | 45.1 |
| 30 | 1539.1 | 1541.2 | 1543.2 | 1545.3 | 1547.3 |
| * Sa | rts per thousa |  |  |  |  |

TABLE 301.-RELATIVE POWER AND FREQUENCY OF OCCURRENCE OF VOWEL AND CONSONANT SOUNDS ${ }^{100}$

Vowels

| Vowel indicated by italics in words | Relative power | Relative frequency of occurrence | Vowel indicated by italics in words | Relative power | Relative frequency of occurrence |
| :---: | :---: | :---: | :---: | :---: | :---: |
| see | 220 | 6.4 | saw | 680 | 4.2 |
| sit | 260 | 10.3 | tone | 470 | 4.7 |
| hate | 370 | 4.8 | foot | 460 | 3.0 |
| let | 350 | 6.6 | soon | 310 | 6.3 |
| sat | 490 | 6.9 | sun | 510 | 4.1 |
| father | 600 | 6.5 |  |  |  |

## Initial and final consonants

| Consonant | Rela- | Relative frequency of occurrence |  | Consonant | Relative power | Relative frequency of occurrence |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | tive power | Initial | Final |  |  | Initial | Final |
| p | 6 | 2.5 | 1.2 | S | 16 | 5.5 | 3.1 |
| b | 7 | 4.6 | . 4 | z | 16 | . 3 | 6.0 |
| k | 13 | 5.6 | 2.9 | zh (azure) | 20 | . 02 | . 01 |
| g | 15 | 4.3 | . 4 | sh ....... | 80 | 1.7 | . 3 |
| t | 15 | 7.9 | 14.3 | m | 52 | 5.9 | 5.5 |
| d | 7 | 6.2 | 4.4 | n | 36 | 5.0 | 12.5 |
| f | 5 | 5.0 | 12.5 | ng | 73 |  | 3.6 |
| $v$ | 12 | 1.3 | . 4.2 | 1 | 100 | 4.3 | 8.4 |
| th (voiced) | 11 | 6.7 | 1.3 | r | 210 | 2.8 | 13.1 |
| th (unvoiced) | 1 | 6.7 | 1.3 | ch | 42 | . 6 | . 5 |
|  |  |  |  | j ... | 23 | . 8 | . 1 |

[^135]
## TABLE 302.-SOUND LEVELS OF NOISE IN VARIOUS LOCATIONS

It is customary to compare the pressure of all sounds in air with 0.0002 dynes $/ \mathrm{cm}^{2}$. The sound-pressurc level of waves having a r.m.s. sound pressure of $p$ dynes $/ \mathrm{cm}^{2}$ is defined as $20 \log _{10}(p / 0.0002)$ decibels. ${ }^{\dagger}$

The following table gives some typical values of sound levels of noise in the locations indicated:

| Location | $\begin{gathered} \text { Sound } \\ \text { level } \\ \text { in db } \end{gathered}$ | Location | $\begin{gathered} \text { Sound } \\ \text { level } \\ \text { indb } \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| Electric power station, |  | Average office | 55 |
| generating room | 120 | Average residence | 5 |
| Boiler factory | 110 | Average residenc | 43 |
| Subway station, train | 100 | Quiet residence | 35 |
| Streetcar |  | Radio broadcast | 30 |
| Factory | 75 | Reference level, . |  |

[^136]In a study conducted by Dunn and White, ${ }^{101}$ the "long-time-interval average" power of speech, obtained by averaging data over time intervals of more than a minute of continuous speech, for the average of a group of male speakers was found to be 34 microwatts. The corresponding value for female speakers was 18 microwatts. At least 1 percent of the $\frac{1}{8}$-second intervals had an average power in excess of 230 microwatts for men and 150 microwatts for women, and a peak power in excess of 3600 microwatts for men and 1800 microwatts for women. The figure shows how the total power of average conversational speech is distributed with respect to frequency. These data give the power per cycles versus frequency and also the percentage power lying below a given frequency.


Fig. 1.-Speech power for men (continuous curves) and women (dotted curves) given in percentage power below any frequency. Curves A and B , power per cycle, curves C and $\mathrm{D}, \mathrm{Odb}=1$ microwatt.

[^137]TABLE 303.-PEAK POWER OF MUSICAL INSTRUMENTS ${ }^{102}$

| Watts |  | Watts |  | Watts |
| :---: | :---: | :---: | :---: | :---: |
| Orchestra, | Cymbals | 10 | Piccolo | . 08 |
| 75 pieces ....... 70 | Trombone | 6 | Flute | . 06 |
| Bass drum, large.. 25 | Piano.. | . 3 | Clarinet | . 05 |
| Pipe organ ....... 13 | Trumpet | . 3 | French horn | . 05 |
| Snare drum ...... 12 | Bass viol | . 2 | Triangle ... | . 05 |

[^138]The "pitch" of one's voice, i.e., his fundamental frequency, fluctuates considerably during conversational speech, and there is a great deal of variation from individual to individual. The average fundamental frequency for the average male voice in conversational English speech is in the neighborhood of 130 cps , while the corresponding value for the female voice is 230 cps .

The vocal cords, housed in the larynx, emit a pressure wave that is essentially "sawtooth" irl character. The numerous harmonics that result from this complex wave form are selectively transmitted to the open air. The throat, mouth, nose, and constrictions formed by the tongue and lips are most important in determining the frequency characteristics of the transmission system. The pressure spectrum of speech has many peaks. Apparently vowel sounds are distinguished by the position of these resonant peaks. The following table gives representative frequencies of the first two principal resonant peaks for different vowel sounds spoken by the average male adult:

| Vowel indicated by italics in the words | Frequency of 1 st | Frequency of 2 d |  | Frequency of 1 st | Frequency of 2 d |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | principal | principal | Vowel in- | principal | principal |
|  | resonant peak | resonant peak | dicated by italics in | resonant | resonant peak |
|  | cps | cps | the words | cps | cps |
| sce | 290 | 2375 | $\mathrm{s} a \mathrm{w}$ | 600 | 900 |
| sit | 440 | 2050 | foot | 500 | 1050 |
| let | 585 | 1875 | soon | 330 | 900 |
| sat | 725 | 1675 | sun | 650 | 1225 |
| father | 780 | 1125 | sir | 475 | 1375 |

${ }^{103}$ Potter, R. K., and Peterson, G. E., Journ. Acoust. Soc. Amer., vol. 20, p. 528, 1948.

## TABLE 305.-APPROXIMATE RANGE OF FUNDAMENTAL FREQUENCY ON ORCHESTRAL INSTRUMENTS

The values given are for average instruments in tune with A440 cps. The lower frequency limits of some special instruments are indicated in brackets.

| Instrument | Frequency range in cps |  | Instrument | Frequency range in cps |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lower limit | Upper limit |  | Lower limit | Upper limit |
| Violin | 195 | 2093 | Bb tenor saxophone | 103 | 623 |
| Viola | 131 | 1318 | Eb baritone saxophone.. | 69 | 416 |
| Cello | 65 | 880 | Trumpet ............. | 164 | 1047 |
| Bass . . . . . . . . . . . . (32) | 41 | 262 | French horn | 61 | 699 |
| Piccolo | 587 | 4186 | Trombone . ......... (51) | 82 | 524 |
| Flute . . . . . . . . . . . . . . . . . | 261 | 2043 | Bass tuba ............... | 41 | 234 |
| Oboe | 233 | 1397 | Piano | 27 | 4186 |
| English horn | 164 | 934 | Organ .............. (16) | 32 | 4186 |
| Clarinet . . . . . . . . . (138) | 146 | 1568 | Harp ... | 32 | 3136 |
| Bass clarinet ....... (65) | 73 | 467 | Soprano voice | 261 | 1568 |
| Bassoon | 58 | 623 | Tenor voice ............. | 123 | 1174 |
| Contra bassoon | 30 | 175 | Alto voice .............. | 174 | 933 |
| Eb alto saxophone ..... | 138 | 831 | Baritone voice ......... | 98 | 416 |
|  |  |  | Bass voice . ............ | . 65 | 294 |

## MUSICAL SCALES

The following definitions and Tables 307 and 308 are taken from the American Standard Acoustical Terminology Z24.1, 1949.
Just scale.-A just scale is a musical scale such that the frequency intervals are represented by the ratios of small integers.

Equally tempered scale.-An equally tempered scale is a series of notes selected from a division of the octave (usually) into 12 equal intervals.

Equally tempered semitone (half-step).-An equally tempered semitone is the interval between two sounds whose basic frequency ratio is the twelfth root of two.
Note.-The interval, in semitones, between any two frequencies is 12 times the logarithm on the base 2 of the frequency ratio.

Cent.-A cent is the interval between two sounds whose basic frequency ratio is the twelve-hundredth root of two.
Note.-The interval, in cents, between any two frequencies is 1200 times the logarithm on the base 2 of the frequency ratio. Thus, 1200 cents $=12$ semitones $=1$ octave.

## TABLE 306.-FREQUENCY RATIOS AND INTERVALS FOR JUST AND EQUALLY TEMPERED SCALES

|  | Just temperament |  | Equal temperament |  |
| :---: | :---: | :---: | :---: | :---: |
| Interval from starting point | Frequency ratio from starting point | Cents from starting point | Frequency ratio from point | $\begin{gathered} \text { Cents } \\ \text { from } \\ \text { starting } \\ \text { point } \end{gathered}$ |
| Unison | 1:1 | 0 | $1: 1$ | 0 |
| Minor second or semitone. | 16:15 | 111.731 | 1.059463:1 | 100 |
| Minor tone | 10:9 | 182.404 |  |  |
| Major second or whole tone | 9:8 | 203.910 | 1.122462:1 | 200 |
| Minor third | 6:5 | 315.641 | 1.189207:1 | 300 |
| Major third | 5:4 | 386.314 | $1.259921: 1$ | 400 |
| Perfect fourth | 4:3 | 398.045 | 1.334840 :1 | 500 |
| Augmented fourth | 45:32 | 590.224 | 1.414214:1 | 600 |
| Diminished fifth | 64:45 | 609.777 | 1.414214:1 | 600 |
| Perfect fifth | 3:2 | 701.955 | 1.498397:1 | 700 |
| Minor sixth | 8:5 | 813.687 | 1.587401:1 | 800 |
| Major sixth | 5:3 | 884.359 | 1.681793:1 | 900 |
| Harmonic minor seventh. | 7:4 | 958.826 |  |  |
| Grave minor seventh. | 16:9 | 996.091 |  |  |
| Minor seventh | 9:5 | 1017.597 | 1.781797:1 | 1000 |
| Major seventh | 15:8 | 1088.269 | 1.887749:1 | 1100 |
| Octave | 2:1 | 1200.000 | 2:1 | 1200 |

TABLE 307.-FREQUENCIES OF THE TONES OF THE USUAL EQUALLY TEMPERED SCALE, ARRANGED BY CORRESPONDING PIANO KEY NUMBERS, AND CALCULATED ACCORDING TO AMERICAN STANDARD PITCH

| Note | $\begin{gathered} \text { Key } \\ \text { No. } \end{gathered}$ | Freq. <br> cps | Key No. din | $\begin{aligned} & \text { Freq. } \\ & \text { cps } \end{aligned}$ | $\begin{aligned} & \text { Key } \\ & \text { No. } \end{aligned}$ | $\begin{gathered} \text { Freq. } \\ \text { cess } \end{gathered}$ | Key No. | Freq. cps | $\begin{gathered} \text { Key } \\ \text { No. } \end{gathered}$ | Freq. cps | $\begin{gathered} \text { Key } \\ \text { No. } \end{gathered}$ | $\begin{aligned} & \text { Freq. } \\ & \text { cps. } \end{aligned}$ | $\begin{gathered} \text { Key } \\ \text { No. } \end{gathered}$ | $\begin{gathered} \text { Freq. } \\ \text { cps } \end{gathered}$ | $\begin{gathered} \text { Key } \\ \text { No. } \end{gathered}$ | $\begin{gathered} \text { Freq. } \\ \text { cps. } \end{gathered}$ | $\begin{aligned} & \text { Note } \\ & \text { name } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | 1 | 27.500 | 13 | 55.000 | 25 | 110.000 | 37 | 220.000 | 49 | 440.000 | 61 | 880.000 | 73 | 1760.000 | 85 | 3520.000 | name |
| A\#-Bb | 2 | 29.135 | 14 | 58.270 | 26 | 116.541 | 38 | 233.082 | 50 | 466.164 | 62 | 932.328 | 74 | 1864.655 | 86 | 3729.310 | $\mathrm{A} \#-\mathrm{Bb}$ |
| B | 3 | 30.868 | 15 | 61.735 | 27 | 123.471 | 39 | 246.942 | 51 | 493.883 | 63 | 987.767 | 75 | 1975.533 | 87 | 3951.066 | B |
| C |  | 32.703 | 16 | 65.406 | 28 | 130.813 | 40 | 261.626 | 52 | 523.251 | 64 | 1046.502 | 76 | 2093.005 | 88 | 4186.009 | C |
| C\#-Db | 5 | 34.648 | 17 | 69.296 | 29 | 138.591 | 41 | 277.183 | 53 | 554.365 | 65 | 1108.731 | 77 | 2217.461 |  |  | C\#-Db |
| D | 6 | 36.708 | 18 | 73.416 | 30 | 146.832 | 42 | 293.665 | 54 | 587.330 | 66 | 1174.659 | 78 | 2349.318 |  |  | D |
| D\#-Eb | 7 | 38.891 | 19 | 77.782 | 31 | 155.563 | 43 | 311.127 | 55 | 622.254 | 67 | 1244.508 | 79 | 2489.016 |  |  | D\#-Eb |
| E | 8 | 41.203 | 20 | 82.407 | 32 | 164.814 | 44 | 329.628 | 56 | 659.255 | 68 | 1318.510 | 80 | 2637.021 |  |  | E |
| F | 9 | 43.654 | 21 | 87.307 | 33 | 174.614 | 45 | 349.228 | 57 | 698.456 | 69 | 1396.913 | 81 | 2793.826 |  |  | F |
| F\#-Gb | 10 | 46.249 | 22 | 92.499 | 34 | 184.997 | 46 | 369.994 | 58 | 739.989 | 70 | 1479.978 | 82 | 2959.955 |  |  | F\#-G |
|  | 11 | 48.999 | 23 | 97.999 | 35 | 195.998 | 47 | 391.995 | 59 | 783.991 | 71 | 1567.982 | 83 | 3135.964 |  |  |  |
| G\#-Ab | 12 | 51.913 | 24 | 103.826 | 36 | 207.652 | 48 | 415.305 | 60 | 830.609 | 72 | 1661.219 | 84 | 3322.438 |  |  | $\mathrm{G}-\mathrm{Ab}$ |

The following data describe the pressure field around the head of a speaker at a radius of 30 cm from the speaker's lips. The sound-pressure level is O). These data give the pressure distribution in the horizontal plane $\phi=0$, and the relative pressures overhead. ).



The minimum effective sound pressure of a specified signal that is capable of evoking an auditory sensation is called the threshold of audibility for that signal. The characteristics of the signal, the manner in which it is presented to the listener, and the point at which the sound pressure is measured must be specified. Two classes of ear-sensitivity determinations are shown in figure 2. M.A.P. is just-audible sound pressure measured at the observer's ear drum. M.A.F. is the sound pressure level that is just audible to an observer in an acoustical field free of reflecting surfaces (the sound-pressure level is measured after the observer's head is withdrawn from the field) ; the observer faces the source of sound and listens binaurally. These curves were derived by Sivian and White from measurements on young adult observers all having very good hearing. ${ }^{105}$ The average person cannot detect pressures as low as those given. He will have a threshold curve displaced upward on the chart. (See Table 309A for data on hearing losses.)


Fig. 2.-The variation of two classes of ear sensitivity. Curve 1, Monaural M.A.P. The ordinate for curve 1 is $20 \log _{10} p / p_{0}$ where $p=$ M.A.P. at ear drum $\left(\mathrm{dyne} / \mathrm{cm}^{2}\right)$ and $p_{0}=$ $2 \times 10^{-4}$ (dyne/ $\mathrm{cm}^{2}$ ). Curve 2, Binaural M.A.F. Observer facing source. ( $0 \mathrm{db}=10^{-16}$ watts $/ \mathrm{cm}^{2}$ ).

The term "differential sensitivity of frequency and intensity" refers to the smallest changes in frequency and intensity, respectively, that can be perceived by an observer with normal hearing. The values depend to some extent on the method of presentation of the test stimuli. For pure tones above 500 cps having levels greater than 40 db above threshold, the measurements of Shower and Biddulph indicate that the smallest perceptible difference in frequency has the approximate constant value of 0.3 percent. For levels greater than 40 db above threshold and for frequencies between 200 and 7000 cps , the measurements of Riesz and others indicate that the smallest perceptible difference in intensity varies from one-quarter to three-quarters of a decibel.

The range of frequency perceived by the average ear varies considerably; however, the figures of $20-20,000$ cycles are frequently quoted as covering the range heard by the average of a group of young adults having no hearing impairments

[^139]
## TABLE 309A.-DISTRIBUTION OF LOSS OF HEARING ACUITY ${ }^{100}$

The following data are part of the results of the hearing tests conducted by the Bell System at the New York and San Francisco World's Fairs in 1939. The first four columns indicate the percentages of the population having hearing losses of 25 db or more at various frequencies. A person having a loss of 25 db at all frequencies below 2000 cps may experience difficulty in understanding unamplified speech, as in an auditorium or church. The second four columns indicate the corresponding percentages for losses of 45 db or more. A person having such a loss experiences difficulty in understanding ordinary conversational speech at distances greater than 2 or 3 feet.

| Age group | 25.db loss Frequency in cps |  |  |  | 45-db loss Frequency in cps |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 440;880 | 1760 | 3520 | 7040 | 440;880 | 1760 | 3520 |
| 10-19 men | 1.7 | 1.6 | 4.5 | 8.0 | . 6 | . 6 | 1.8 |
| women | 1.8 | 1.2 | 1.2 | 2.5 | . 6 | . 4 | . 3 |
| 20-29 men | 1.1 | 1.2 | 7.0 | 9.5 | . 1 | . 3 | 2.7 |
| women | 1.8 | 1.6 | 2.2 | 3.5 | . 4 | . 3 | . 7 |
| 30-39 men | 1.8 | 3.5 | 15. | 19. | . 3 | . 6 | 6.0 |
| women | 3.5 | 3.5 | 5.5 | 10. | 1.2 | . 8 | 1.6 |
| 40-49 men | 5.5 | 9.5 | 32. | 39. | 1.4 | 2.6 | 16. |
| women | 7.0 | 7.0 | 11. | 24. | 2.1 | 1.5 | 3. |
| 50-59 men |  | 17. | 48. | 58. | 2.6 | 6.0 | 27. |
| women | 13. | 14. | 22. | 43. | 4.0 | 3.0 | 7. |

${ }^{100}$ Steinberg, Montgomery, and Gardner, Journ. Acoust. Soc. Amer., vol. 12, p. 291, 1940.

## TABLE 310.-ARCHITECTURAL ACOUSTICS ${ }^{107}$

Planning for good acoustics in a building requires careful consideration of noise control. This includes consideration of the selection of a site, the arrangement of the rooms within the building, the selection of the proper sound-insulation constructions, and the control of noise sources within the building. The design of a room where people gather to listen to speech or music should be such that its shape and size will ensure the most advantageous flow of properly diffused sound to all auditors. Absorptive and reflective materials and constructions should be selected and distributed to provide the optimum conditions for the growth, decay, and steady-state distribution of sound in the room. The reverberation characteristics of the room are controlled by the amount and placement of the absorptive material.

Reverberation time calculations.-Because of the importance of the proper control of reverberation in rooms, a standard of measure called reverberation time has been established. This is the time required for a specified sound to die away to one-thousandth of its initial pressure, which corresponds to a drop in sound-pressure level of 60 db . The reverberation time of a room is given by the following equation :

$$
T=\frac{0.049 V}{-2.30 S \log _{10}(1-\bar{\propto})+4 m V}
$$

where $V$ is the volume of the room, $S$ is the total surface area in square feet, and $\bar{\propto}$ is the average absorption coefficient for the room given by

$$
\bar{\propto}=\frac{\propto_{1} S_{1}+\propto_{2} S_{2}+\propto_{3} S_{3}+\ldots \ldots}{S_{1}+S_{2}+S_{3}+\ldots \ldots}=\frac{a}{S}
$$

where $\propto_{1}$ is the absorption coefficient of the area $S_{1}$, etc.
The second term in the denominator, $4 m V$, represents the effective absorption in the room contributed by the air. The attenuation coefficient $m$ at each frequency depends upon the humidity and temperature of the air. Except in very large rooms the absorption in air can be neglected below about 2000 cps . The values of $m$ for a temperature $68^{\circ} \mathrm{F}$ are given in figure 3 as a function of relative humidity for a number of frequencies.

[^140]

Fig. 3.-Attenuation coefficient $m$ per foot as a function of humidity.

TABLE 310A.-OPTIMUM REVERBERATION TIME (FIGS. 4 AND 5)
The following figures give the recommendations of Knudsen and Harris for optimum reverberation time for different types of rooms as a function of room volume. The optimum times for speech rooms, motion-picture theaters, and school auditoriums are given by a single line ; the optimum time for music by a broad band. The optimum reverberation time is not the same for all kinds of music. For example, slow organ and choral music require more reverberation than does a brilliant allegro composition played on woodwinds, piano, or harpsicord.

The optimum reverberation time vs. frequency characteristic for a room can be obtained from these charts in the following manner: After having specified the volume and purpose of the room, determine the optimum reverberation time at 512 cycles from the upper chart. Then, to obtain optimum reverberation time at any other frequencies multiply the 512 -cycle value by the appropriate ratio $R$ which is given in the lower chart. Note that $R$ is unity for frequencies above 500 cycles, and is given by a band for frequencies below 500 cycles. The ratio $R$ for large rooms may have any value within the indicated band; preferred ratios for small rooms are given by the lower part of the band.
(continued)

TABLE 310A.-OPTIMUM REVERBERATION TIME (FIGS. 4 AND 5) (concluded)


Fig. 4.-Optimum reverberation time as a function of volume of rooms for various types of sound for a frequency of about 512 cycles per second.


Fig. 5.-Ratio of the reverberation time for various frequencies as a function of the reverberation for 512 cycles per second.

## TABLES 311-338.-VISCOSITY OF FLUIDS AND SOLIDS *

The coefficient of viscosity of a substance is the tangential force required to move a unit area of a plane surface with unit speed relative to another parallel plane surface from which it is separated by a layer of the substance a unit thick. Viscosity measures the temporary rigidity it gives to the substance.

Fluidity is the reciprocal of viscosity expressed in poises. Kinematic viscosity is absolute viscosity divided by density. Specific viscosity is viscosity relative to that of some standard substance, generally water at some definite temperature. The dimensions of viscosity are $M L^{-1} T^{-1}$. It is generally expressed in cgs units as dyne-second per $\mathrm{cm}^{2}$ or poises.

The viscosity of fluids is generally measured by one of several methods depending on the magnitude of the viscosity value to be measured. For vapors and gases as well as for liquids of low viscosity, measurements of viscosity are made by the rate of flow of the fluid through a capillary tube whose length is great in comparison with its diameter. The equation generally used is

$$
\eta, \text { the viscosity, }=\frac{\gamma \pi g d^{4} t}{128 Q(l+\lambda)}\left(h-\frac{m v^{2}}{g}\right)
$$

where $\gamma$ is the density $\left(\mathrm{g} / \mathrm{cm}^{3}\right), d$ and $l$ are respectively the diameter and length in cm of the tube, $Q$ the volume in $\mathrm{cm}^{3}$ discharged in $t \mathrm{sec}, \lambda$ the Couette correction to the measured length of the tube, $h$ the average head in cm , $m$ the coefficient of kinetic energy correction, $m v^{2} / g$, necessary for the loss of energy due to turbulent, in distinction from viscous, flow, $g$ being the acceleration of gravity $\left(\mathrm{cm} / \mathrm{sec}^{2}\right), v$ the mean velocity in $\mathrm{cm} / \mathrm{sec}$. (See Herschel, Nat. Bur. Standards Techn. Pap. Nos. 100 and 112, 1917-1918, for discussion of this correction and $\lambda$.)

For liquids of medrum and high values of viscosity measurements are made by Margule's method of observing the torque on the inner of two concentric cylinders while the outer is rotated with constant angular speed with the viscous liquid filling the space between, or by noting the rate of fall of a solid sphere through the liquid.

For the method of concentric cylinders the equation is

$$
\eta \text {, the viscosity, }=\frac{K \theta\left(R_{1}{ }^{2}-R_{2}{ }^{2}\right)}{4 \pi \Omega R_{1}{ }^{2} R_{2}{ }^{2} L},
$$

where $K$ denotes the elastic constant of the torsion member supporting the inner cylinder of radius $R_{2} \mathrm{~cm}$ and length $L \mathrm{~cm}, \theta$ is the angular displacement of the inner cylinder from its position of equilibrium, $\Omega$ the angular speed of the outer rotating cylinder of radius $R_{1} \mathrm{~cm}$ in the corresponding units employed to measure $\theta$. The necessary corrections due to end effects of cylinders of finite length are given in the reference. ${ }^{108}$

For the falling sphere method, the equation is that of Stokes law as modified by R. G. Hunter : ${ }^{109}$

$$
\eta, \text { the viscosity, }=\frac{2}{9} \frac{R^{2}\left(d_{1}-d_{2}\right)}{V} \frac{\left(1-\frac{R}{}^{2 \cdot 2 \cdot 5}\right)}{\left(1+3.3 \frac{R}{h}\right)}
$$

where $\gamma$ denotes the radius in cm of the crucible containing the liquid of density $d_{2}\left(\mathrm{~g} / \mathrm{cm}^{3}\right)$, to a depth of $h \mathrm{~cm}, R$ the radius in cm of the sphere of density $d_{1}$ $\left(\mathrm{g} / \mathrm{cm}^{3}\right)$, and $V$ the velocity ( $\mathrm{cm} / \mathrm{sec}$ ) of the falling sphere.

[^141]For very viscous materials, measurements of viscosity are made by noting the rate of elongation of fibers under load or by observing the aperiodic motion of an elastic system displaced from its position of equilibrium and damped by the viscous material.
The formula for the rate of elongation of fibers as employed by H. R. Lillie ${ }^{110}$ is

$$
\eta, \text { the viscosity, }=\frac{L \times g \times k}{3 \pi R^{2} E},
$$

where $R$ is the radius in cm of the fiber of effective length, $L$ ( cm ), $g$ the mass in grams of the attached load, $k$ the acceleration of gravity $\left(\mathrm{cm} / \mathrm{sec}^{2}\right)$, and $E$ the rate of elongation in $\mathrm{cm} / \mathrm{sec}$.

For the aperiodic motion of the system consisting of the suspended inner cylinder of Margule's apparatus described above, the formula is

$$
\eta \text {, the viscosity, }=\frac{K\left(t_{2}-t_{1}\right) \log e}{4 \pi L \log _{10} \frac{\theta_{1}}{\theta_{2}}}\left(\frac{R_{2}{ }^{2}-R_{1}{ }^{2}}{R_{1}{ }^{2} R_{2}{ }^{2}}\right),
$$

where $t_{2}$ and $t_{1}$ denote the times in seconds of angular positions $\theta_{2}$ and $\theta_{1}$ of the suspended system from its position of equilibrium. The other characters have the same significance as in the formula above for the rotating cylinder method of measuring viscosity. (For reference, see footnote 108.)

The viscosity of solids may be measured in relative terms by the damping of the oscillations of suspended wires (see Table 323). Ladenburg (1906) gives the viscosity of Venice turpentine at $18.3^{\circ}$ as 1300 poises ; Trouton and Andrews (1904) of pitch at $0^{\circ}, 51 \times 10^{10}$, at $15^{\circ}, 1.3 \times 10^{10}$; of shoemaker's wax at $8^{\circ}, 4.7 \times 10^{6}$; of soda glass at $575^{\circ}, 11 \times 10^{12}$; Deeley (1908) of glacier ice as $12 \times 10^{13}$.
${ }^{110}$ Lillie, H. R., Journ. Amer. Cer. Soc., vol. 14, p. 502, 1931.

TABLE 311.—VISCOSITY OF WATER IN CENTIPOISES
(Temperature variation)
Part 1.-Low temperature

| ${ }^{\circ} \mathrm{C}$ | $\begin{aligned} & \text { Vis. } \\ & \text { Cosity } \\ & \text { cp } \end{aligned}$ | ${ }^{\circ} \mathrm{C}$ | $\begin{aligned} & \text { Vis- } \\ & \text { Cosity } \end{aligned}$ | ${ }^{\circ} \mathrm{C}$ | $\begin{gathered} \text { Vis. } \\ \text { Cis. } \\ \text { cp } \\ \text { cp } \end{gathered}$ | ${ }^{\circ} \mathrm{C}$ | $\begin{aligned} & \text { Vis- } \\ & \text { Visity } \\ & \text { cp } \end{aligned}$ | ${ }^{\circ} \mathrm{C}$ | $\underset{\substack{\text { Vis. } \\ \text { cosity } \\ \text { cp }}}{\text { Sic }}$ | ${ }^{\circ} \mathrm{C}$ | $\begin{gathered} \text { Vis. } \\ \text { Vosity } \\ c p \end{gathered}$ | ${ }^{\circ} \mathrm{C}$ | $\underset{\substack{\text { Vis- } \\ \text { cosity } \\ \text { cp }}}{ }$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1.7921 | 10 | 1.3077 | 20 | 1.0050 | 30 | . 8007 | 40 | . 6560 | 50 | . 5494 | 60 | . 4688 |
| 1 | 1.7313 | 11 | 1.2713 | 21 | . 9810 | 31 | . 7840 | 41 | . 6439 | 51 | . 5404 | 65 | . 4355 |
| 2 | 1.6728 | 12 | 1.2363 | 22 | . 9579 | 32 | . 7679 | 42 | . 6321 | 52 | . 5315 | 70 | . 4061 |
| 3 | 1.6191 | 13 | 1.2028 | 23 | . 9358 | 33 | . 7523 | 43 | . 6207 | 53 | . 5229 | 75 | . 3799 |
| 4 | 1.5674 | 14 | 1.1709 | 24 | . 9142 | 34 | . 7371 | 44 | . 6097 | 54 | . 5146 | 80 | . 3565 |
| 5 | 1.5188 | 15 | 1.1404 | 25 | . 8937 | 35 | . 7225 | 45 | . 5988 | 55 | . 5064 | 85 | . 3355 |
| 6 | 1.4728 | 16 | 1.1111 | 26 | . 8737 | 36 | . 7085 | 46 | . 5883 | 56 | . 4985 | 90 | . 3165 |
| 7 | 1.4284 | 17 | 1.0828 | 27 | . 8545 | 37 | . 6947 | 47 | . 5782 | 57 | . 4907 | 95 | . 2994 |
| 8 | 1.3860 | 18 | 1.0559 | 28 | . 8360 | 38 | . 6814 | 48 | . 5683 | 58 | . 4832 | 100 | . 2838 |
| 9 | 1.3462 | 19 | 1.0299 | 29 | . 8180 | 39 | . 6685 | 49 | . 5588 | 59 | . 4759 | 153 | . 181 |

(continued)

TABLE 311.-VISCOSITY OF WATER IN CENTIPOISES (concluded)
Part 2.-High temperature ${ }^{111}$

| ${ }^{\circ} \mathrm{C}$ | Viscosity | ${ }^{\circ} \mathrm{C}$ | Vis. cosity | ${ }^{\circ} \mathrm{C}$ | Viscosity | ${ }^{\circ} \mathrm{C}$ | Viscosity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 130 | ... | 155 | . 184 | 180 | . 155 | 205 | 136 |
| 135 |  | 160 | . 178 | 185 | . 151 | 210 | . 134 |
| 140 |  | 165 | . 173 | 190 | . 146 | 215 | . 131 |
| 145 | . 199 | 170 | . 166 | 195 | . 143 | 220 | . 129 |
| 150 | . 191 | 175 | . 160 | 200 | . 139 | 225 | . 128 |

${ }^{111}$ Based on measurements by Shugayev, V., Journ. Exp. and Theoret. Phys. (U.S.S.R.), vol. 4, p. 760, 1934.

Part 3.-Viscosity of heavy water in centipoises ${ }^{112}$ $99.65 \% \mathrm{D}_{2} \mathrm{O} ; \mathrm{d}_{4}{ }^{20}=1.10495$

|  | Vis. <br> cosity | ${ }^{\circ} \mathrm{C}$ | Vis. <br> cosity |  | Vis. <br> cosity |  | Vis. <br> cosity |
| :---: | :---: | ---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{C}$ | co | cp | ${ }^{\text {cp }} \mathrm{C}$ | cp |  |  |  |
| 4 | 2.25 | 8 | 1.81 | 12 | 1.56 | 16 | 1.37 |
| 5 | 2.10 | 9 | 1.73 | 13 | 1.51 | 17 | 1.33 |
| 6 | 1.99 | 10 | 1.67 | 14 | 1.46 | 18 | 1.29 |
| 7 | 1.90 | 11 | 1.61 | 15 | 1.41 | 19 | 1.25 |

${ }^{112}$ Data by Lemond, Henri, Compt. Rend., vol. 212, p. 81, 1941.

TABLE 312.-VISCOSITY OF ALCOHOL-WATER MIXTURES IN CENTIPOISES
(Temperature variation)

|  | Percentage by weight of ethyl alcohol |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{C}$ | 0 | 10 | 20 | 30 | 35 | 40 | 45 | 50 | 60 | 70 | 80 | 90 | 100 |
| 0 | 1.792 | 3.311 | 5.319 | 6.94 | 7.25 | 7.14 | 6.94 | 6.58 | 5.75 | 4.762 | 3.690 | 2.732 | 1.773 |
| 5 | 1.519 | 2.577 | 4.065 | 5.29 | 5.62 | 5.59 | 5.50 | 5.26 | 4.63 | 3.906 | 3.125 | 2.309 | 1.623 |
| 10 | 1.308 | 2.179 | 3.165 | 4.05 | 4.39 | 4.39 | 4.35 | 4.18 | 3.77 | 3.268 | 2.710 | 2.101 | 1.466 |
| 15 | 1.140 | 1.792 | 2.618 | 3.26 | 3.52 | 3.53 | 3.51 | 3.44 | 3.14 | 2.770 | 2.309 | 1.802 | 1.332 |
| 20 | 1.005 | 1.538 | 2.183 | 2.71 | 2.88 | 2.91 | 2.88 | 2.87 | 2.67 | 2.370 | 2.008 | 1.610 | 1.200 |
| 25 | . 894 | 1.323 | 1.815 | 2.18 | 2.35 | 2.35 | 2.39 | 2.40 | 2.24 | 2.037 | 1.748 | 1.424 | 1.096 |
| 30 | . 801 | 1.160 | 1.553 | 1.87 | 2.00 | 2.02 | 2.02 | 2.02 | 1.93 | 1.767 | 1.531 | 1.279 | 1.003 |
| 35 | . 722 | 1.006 | 1.332 | 1.58 | 1.71 | 1.72 | 1.73 | 1.72 | 1.66 | 1.529 | 1.355 | 1.147 | . 914 |
| 40 | . 656 | . 907 | 1.160 | 1.368 | 1.473 | 1.482 | 1.495 | 1.499 | 1.447 | 1.344 | 1.203 | 1.035 | . 834 |
| 45 | . 599 | . 812 | 1.015 | 1.189 | 1.284 | 1.289 | 1.307 | 1.294 | 1.271 | 1.189 | 1.081 | . 939 | . 764 |
| 50 | . 549 | . 734 | . 907 | 1.050 | 1.124 | 1.132 | 1.148 | 1.155 | 1.127 | 1.062 | . 968 | . 848 | . 702 |
| 60 | . 469 | . 609 | . 736 | . 834 | . 885 | . 893 | . 907 | . 913 | . 902 | . 856 | . 789 | . 704 | . 592 |
| 70 | . 406 | . 514 | . 608 | . 683 | . 725 | . 727 | . 740 | . 740 | . 729 | . 695 | . 650 | . 589 | . 504 |
| 80 | . 356 | . 430 | . 505 | . 567 | . 598 | . 601 | . 609 | . 612 | . 604 |  |  |  |  |

## (Temperature variation) <br> Viscosity values given as $\log _{10} \eta$ (poises)

| $\begin{aligned} & \text { Temp. } \\ & { }^{\circ} \mathrm{C} \mathrm{C} \end{aligned}$ | $\log _{10} \eta$ | ${ }^{\text {Temp }} \mathrm{C} .$ | $\log _{10} \eta$ | $\stackrel{\text { Temp. }}{{ }^{\circ} \mathrm{C}}$ | $\log _{10} \eta$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 22 | 13.96 | 50 | 7.48 | 100 | 2.40 |
| 24 | 13.41 | 55 | 6.67 | 105 | 2.15 |
| 26 | 12.86 | 60 | 5.97 | 110 | 1.90 |
| 28 | 12.34 | 65 | 5.35 | 115 | 1.70 |
| 30 | 11.82 | 70 | 4.80 | 120 | 1.50 |
| 32 | 11.32 | 75 | 4.29 | 125 | 1.32 |
| 34 | 10.83 | 80 | 3.82 | 130 | 1.16 |
| 36 | 10.35 | 85 | 3.40 | 135 | 1.01 |
| 40 | 9.44 | 90 | 3.02 | 140 | . 88 |
| 45 | 8.40 | 95 | 2.69 | 145 | . 75 |

As with other liquids in the temperature interval of high viscosities, measured values for glucose depend on the thermal treatment to which the sample is subjected prior to and during measurement. Prolonged holding at a given temperature followed by rapid cooling to a lower temperature at which viscosity is measured will result in increasing values with time. Decreasing viscosity valucs with time will result from the reverse temperature treatment. At temperatures of high viscosity, constant, or equilibrium, viscosity values will be found only after long holding at the given temperature or after slow and controlled cooling from conditions of low viscosity to the desired temperature.
${ }^{113}$ Barton, Spaght, and Richardson, Journ. Appl. Phys., vol. 5, p. 156, 1934.

TABLE 314.-VISCOSITY AND DENSITY OF GLYCEROL IN AQUEOUS
SOLUTION AT $20^{\circ} \mathrm{C}{ }^{*}$

| $\begin{aligned} & \text { \% Gly- } \\ & \text { cerol } \end{aligned}$ | Density $\mathrm{g} / \mathrm{cm}^{3}$ | Viscosity in centipoises | Kinematic viscosity $\dagger$ in centistokes | $\begin{gathered} \% \text { Gly } \\ \text { cerol } \end{gathered}$ | Density $\mathrm{g} / \mathrm{cm}^{3}$ | Viscosity in centipoises | Kinematic viscosity $\dagger$ in centistokes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | 1.0098 | 1.181 | 1.170 | 50 | 1.1258 | 5.908 | 5.248 |
| 10 | 1.0217 | 1.364 | 1.335 | 55 | 1.1393 | 7.664 | 6.727 |
| 15 | 1.0337 | 1.580 | 1.529 | 60 | 1.1528 | 10.31 | 8.943 |
| 20 | 1.0461 | 1.846 | 1.765 | 65 | 1.1662 | 14.51 | 12.44 |
| 25 | 1.0590 | 2.176 | 2.055 | 70 | 1.1797 | 21.49 | 18.22 |
| 30 | 1.0720 | 2.585 | 2.411 | 75 | 1.1932 | 33.71 | 28.25 |
| 35 | 1.0855 | 3.115 | 2.870 | 80 | 1.2066 | 55.34 | 45.86 |
| 40 | 1.0989 | 3.791 | 3.450 | 85 | 1.2201 | 102.5 | 84.01 |
| 45 | 1.1124 | 4.692 | 4.218 | 90 | 1.2335 | 207.6 | 168.3 |

[^142](Temperature variation)

| ${ }^{\circ} \mathrm{C}$ | Density <br> $\mathrm{g} / \mathrm{cm}^{3}$ | Viscosity <br> in poises | Kinematic viscosity in stokes | ${ }^{\circ} \mathrm{C}$ | Density $\mathrm{g} / \mathrm{cm}^{3}$ | Viscosity in poises | Kinematic viscosity in stokes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | . 9707 | 37.6 | 38.7 | 23 | . 9583 | 7.67 | 8.00 |
| 6 | . 9700 | 34.5 | 35.5 | 24 | . 9576 | 7.06 | 7.37 |
| 7 | . 9693 | 31.6 | 32.6 | 25 | . 9569 | 6.51 | 6.80 |
| 8 | . 9686 | 28.9 | 29.8 | 26 | . 9562 | 6.04 | 6.32 |
| 9 | . 9679 | 26.4 | 27.3 | 27 | . 9555 | 5.61 | 5.87 |
| 10 | . 9672 | 24.2 | 25.0 | 28 | . 9548 | 5.21 | 5.46 |
| 11 | . 9665 | 22.1 | 22.8 | 29 | . 9541 | 4.85 | 5.08 |
| 12 | . 9659 | 20.1 | 20.8 | 30 | . 9534 | 4.51 | 4.73 |
| 13 | . 9652 | 18.2 | 18.9 | 31 | . 9527 | 4.21 | 4.42 |
| 14 | . 9645 | 16.61 | 17.22 | 32 | . 9520 | 3.94 | 4.14 |
| 15 | . 9638 | 15.14 | 15.71 | 33 | . 9513 | 3.65 | 3.84 |
| 16 | . 9631 | 13.80 | 14.33 | 34 | . 9506 | 3.40 | 3.58 |
| 17 | . 9624 | 12.65 | 13.14 | 35 | . 9499 | 3.16 | 3.33 |
| 18 | . 9617 | 11.62 | 12.09 | 36 | . 9492 | 2.94 | 3.10 |
| 19 | . 9610 | 10.71 | 11.15 | 37 | . 9485 | 2.74 | 2.89 |
| 20 | . 9603 | 9.86 | 10.27 | 38 | . 9478 | 2.58 | 2.72 |
| 21 | . 9596 | 9.06 | 9.44 | 39 | . 9471 | 2.44 | 2.58 |
| 22 | . 9589 | 8.34 | 8.70 | 40 | . 9464 | 2.31 | 2.44 |

TABLE 316. -VISCOSITY OF GLYCERINE-WATER MIXTURES ${ }^{14}$
(Temperature variation)

|  |  | Viscosity in centipoises |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Sp. gravity | $\overbrace{20^{\circ} \mathrm{C}}$ | $25^{\circ} \mathrm{C}$ | $30^{\circ} \mathrm{C}$ |  |
| 1.00000 | 0 | 1.005 | .893 | .800 |
| 1.02370 | 10 | 1.311 | 1.153 | 1.024 |
| 1.04840 | 20 | 1.769 | 1.542 | 1.360 |
| 1.07395 | 30 | 2.501 | 2.157 | 1.876 |
| 1.10040 | 40 | 3.750 | 3.180 | 2.731 |
| 1.12720 | 50 | 6.050 | 5.041 | 4.247 |
| 1.15460 | 60 | 10.96 | 8.823 | 7.312 |
| 1.18210 | 70 | 22.94 | 17.96 | 14.32 |
| 1.20925 | 80 | 62.0 | 45.86 | 34.92 |
| 1.23585 | 90 | 234.6 | 163.6 | 624. |
| 1.26201 | 100 | 1499. | 945. |  |

${ }^{114}$ Landolt and Börnstein, 1935. Data by Sheely, Ind. Eng. Chem., vol. 24, p. 1060, 1932.

TABLE 317.-VISCOSITY OF GASOLINE AND KEROSENE IN CENTIPOISES ${ }^{115}$

| Gasoline No. | $\begin{aligned} & \text { Sp. } \mathrm{gr} \text { r. } \\ & \frac{15.6^{\circ}}{15.6^{\circ}} \end{aligned}$ | Temperature |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $5^{\circ} \mathrm{C}$ | $15^{\circ} \mathrm{C}$ | $25^{\circ} \mathrm{C}$ | $35^{\circ} \mathrm{C}$ | $45^{\circ} \mathrm{C}$ | $55^{\circ} \mathrm{C}$ |
| 1 | . 757 | . 690 | . 603 | . 518 | . 472 | . 426 | . 382 |
| 2 | . 748 | . 769 | . 663 | . 588 | . 516 | . 467 | . 412 |
| 3 | . 743 | . 775 | . 641 | . 541 | . 493 | . 441 |  |
| 4 | . 726 | . 495 | . 429 | . 379 | . 341 | . 309 | . 278 |
| 5 | . 722 | . 529 | . 457 | . 410 | . 360 | . 325 | . 293 |
| 6 | . 717 | . 568 | . 481 | . 418 | . 361 | . 339 |  |
| 7 | . 716 | . 508 | . 461 | . 391 | . 346 | . 312 | 294 |
| 8 | . 708 | . 493 | . 435 | . 389 | . 336 | . 301 | . 278 |
| 9 | . 702 | . 429 | . 383 | . 338 | . 312 | . 279 | . 250 |
| 10 | . 701 | . 435 | . 382 | . 349 | . 300 | . 268 | . 251 |
| 11 | . 699 | . 429 | . 372 | . 327 | . 299 | . 269 | . 236 |
| 12 | . 694 | . 399 | . 350 | . 317 | . 283 | . 259 | . 234 |
| 13 | . 680 | . 347 | . 310 | . 274 | . 242 | . 227 | . 211 |
| Kerosene | . 813 | 2.57 | 2.13 | 1.64 | 1.41 | 1.19 |  |

[^143](Temperature variation)
Compiled from Landolt and Börnstein, 1923. Based principally on work of Thorpe and Rogers, 1894-1897. Viscosity given in centipoises. One centipoise $=0.01$ dyne-second per $\mathrm{cm}^{2}$.

|  |  | Viscosity in centipoises |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Liquid | Formula | $0^{\circ} \mathrm{C}$ | $10^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $30^{\circ} \mathrm{C}$ | $40^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $70^{\circ} \mathrm{C}$ | $100^{\circ} \mathrm{C}$ |
| Acids: |  |  |  |  |  |  |  |  |  |
| Formic | $\mathrm{CH}_{2} \mathrm{O}_{2}$ | solid | 2.247 | 1.784 | 1.460 | 1.219 | 1.036 | . 780 | . 549 |
| Acetic | $\mathrm{C}_{2} \mathrm{H}_{4} \mathrm{O}_{2}$ | solid | solid | 1.222 | 1.040 | . 905 | . 796 | . 631 | . 465 |
| Acetic <br> (anhydrous) | $\mathrm{C}_{2} \mathrm{H}_{4} \mathrm{O}_{2}$ | 1.245 | 1.053 | . 907 | . 792 | . 699 | . 623 | . 507 | . 387 |
| Propionic . . | $\mathrm{C}_{3} \mathrm{H}_{6} \mathrm{O}_{2}$ | 1.521 | 1.289 | 1.102 | . 960 | . 845 | . 752 | . 607 | . 495 |
| Propionic <br> (anhydrous) | $\mathrm{C}_{3} \mathrm{H}_{6} \mathrm{O}_{2}$ | 1.610 | 1.330 | 1.119 | . 961 | . 836 | . 735 | . 584 | . 438 |
| Butyric ..... | $\mathrm{C}_{4} \mathrm{H}_{8} \mathrm{O}_{2}$ | 2.286 | 1.751 | 1.540 | 1.304 | 1.121 | . 975 | . 760 | . 551 |
| i-Butyric | $\mathrm{C}_{4} \mathrm{H}_{8} \mathrm{O}_{2}$ | 1.887 | 1.568 | 1.318 | 1.129 | . 980 | . 862 | . 683 | . 501 |
| Alcohols : |  |  |  |  |  |  |  |  |  |
| Methy] | $\mathrm{CH}_{4} \mathrm{O}$ | . 817 | . 690 | . 596 | . 520 | .457 | . 403 |  |  |
| Ethyl | $\mathrm{C}_{2} \mathrm{H}_{8} \mathrm{O}$ | 1.772 | 1.451 | 1.194 | . 992 | . 831 | . 701 | . 510 |  |
| Propyl | C: $\mathrm{H}_{8} \mathrm{O}$ | 3.883 | 2.918 | 2.256 | 1.779 | 1.405 | 1.131 | . 761 |  |
| i-Propyl | $\mathrm{C}_{3} \mathrm{H}_{8} \mathrm{O}$ | 4.565 | 3.246 | 2.370 | 1.757 | 1.331 | 1.029 | . 646 |  |
| Butyl .. | $\mathrm{C}_{4} \mathrm{H}_{10} \mathrm{O}$ | 5.186 | 3.873 | 2.948 | 2.267 | 2.782 | 1.411 | . 930 | . 540 |
| i-Butyl | $\mathrm{C}_{4} \mathrm{H}_{10} \mathrm{O}$ | 8.038 | 5.548 | 3.907 | 2.864 | 2.122 | 1.611 | . 976 | . 527 |
| Allyl . | $\mathrm{C}_{3} \mathrm{H}_{6} \mathrm{O}$ | 2.145 | 1.705 | 1.363 | 1.168 | . 914 | . 763 | . 553 |  |
| Aromatics : |  |  |  |  |  |  |  |  |  |
| Benzene | $\mathrm{C}_{6} \mathrm{H}_{6}$ | . 906 | . 763 | . 654 | . 567 | . 498 | . 444 | . 359 |  |
| Toluene | $\mathrm{C}_{-} \mathrm{H}_{8}$ | . 772 | . 671 | . 590 | . 525 | . 471 | . 426 | . 354 | . 278 |
| Orthoxylene | C $\times \mathrm{H}_{10}$ | 1.105 | . 937 | . 810 | . 709 | . 627 | . 560 | . 458 | . 352 |
| Metaxylene | $\mathrm{C}_{4} \mathrm{H}_{10}$ | . 806 | . 702 | . 620 | . 553 | . 497 | . 451 | . 375 | . 297 |
| Paraxylene | C. $\mathrm{H}_{10}$ | solid | . 739 | . 648 | . 574 | . 513 | . 463 | . 383 | . 300 |
| Ethyl Benzene | C. $\mathrm{H}_{10}$ | . 877 | . 761 | . 671 | . 595 | . 532 | . 481 | . 399 | . 311 |
| Bromides: |  |  |  |  |  |  |  |  |  |
| Ethyl | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Br}$ | . 487 | . 441 | . 402 | . 368 |  |  |  |  |
| Propyl | $\mathrm{C}_{3} \mathrm{H}_{7} \mathrm{Br}$ | ,651 | . 582 | . 524 | . 475 | . 433 | . 397 | . 338 |  |
| i-Propyl | $\mathrm{C}_{3} \mathrm{H}_{7} \mathrm{Br}$ | . 611 | . 545 | . 489 | . 443 | . 403 | . 368 |  |  |
| i-Butyl | $\mathrm{C}_{4} \mathrm{H}_{9} \mathrm{Br}$ | . 828 | . 726 | . 643 | . 575 | . 518 | . 470 | . 390 |  |
| Allyl | $\mathrm{C}_{3} \mathrm{H}_{5} \mathrm{Br}$ | . 626 | . 560 | . 504 | . 458 | . 419 | . 384 | . 328 |  |
| Ethylene | $\mathrm{C}_{2} \mathrm{H}_{4} \mathrm{Br}$ | 2.438 | 2.039 | 1.721 | 1.475 | 1.286 | 1.131 | . 903 | . 679 |
| Bromine |  | 1.267 | 1.120 | 1.005 | . 911 | . 831 | .761 |  |  |
| Chtorides: |  |  |  |  |  |  |  |  |  |
| Propyl | $\mathrm{C}_{3} \mathrm{H}_{7} \mathrm{Cl}$ | . 442 | . 396 | . 359 | . 326 | . 299 |  |  |  |
| i-Propyl | $\mathrm{C}_{3} \mathrm{H}_{7} \mathrm{Cl}$ | . 408 | . 365 | . 329 | . 299 |  |  |  |  |
| i-Butyl | $\mathrm{C}_{4} \mathrm{H}_{9} \mathrm{Cl}$ | . 568 | . 519 | . 462 | . 414 | . 373 | . 339 |  |  |
| Allyl. | $\mathrm{C}_{2} \mathrm{H}_{3} \mathrm{Cl}$ | . 413 | . 372 | . 337 | . 307 | . 283 |  |  |  |
| Methylene | $\mathrm{CH}_{3} \mathrm{Cl}_{2}$ | . 543 | . 488 | . 444 | . 406 | . 373 |  |  |  |
| Ethylene | $\mathrm{C}_{2} \mathrm{H}_{4} \mathrm{Cl}_{2}$ | 1.132 | . 966 | . 839 | . 736 | . 652 | . 584 | . 479 |  |
| Chloroform | $\mathrm{CHCl}_{3}$ | . 706 | . 633 | . 571 | . 519 | . 474 | . 435 |  |  |
| Carbon-tetra | $\mathrm{CCl}_{4}$ | 1.351 | 1.138 | . 975 | . 848 | . 746 | . 662 | . 534 |  |
| Ethers: |  |  |  |  |  |  |  |  |  |
| Diethyl | $\mathrm{C}_{4} \mathrm{H}_{10} \mathrm{O}$ | . 295 | . 268 | . 245 | . 223 |  |  |  |  |
| Methyl-Propyl | $\mathrm{C}_{4} \mathrm{H}_{10} \mathrm{O}$ | . 314 | . 285 | . 260 | . 237 |  |  |  |  |
| Ethyl-Propyl . | $\mathrm{C}_{5} \mathrm{H}_{12} \mathrm{O}$ | . 402 | . 360 | . 324 | . 294 | . 268 | . 245 |  |  |
| Methyl-iso-Buty | $\mathrm{C}_{5} \mathrm{H}_{12} \mathrm{O}$ | . 387 | . 346 | . 313 | . 284 | . 260 | . 239 |  |  |
| Dipropyl ..... | $\mathrm{C}_{n} \mathrm{H}_{44} \mathrm{O}$ | . 544 | . 479 | . 425 | . 381 | . 344 | . 311 | . 260 |  |
| Ethyl-iso-Butyl | $\mathrm{C}_{6} \mathrm{H}_{14} \mathrm{O}$ | . 487 | . 430 | . 384 | . 345 | . 311 | . 284 | . 237 |  |
|  |  |  | ontinue |  |  |  |  |  |  |

(Temperature variation)

| Liquid | Formula | Viscosity in centipoises |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $0^{\circ} \mathrm{C}$ | $10^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $30^{\circ} \mathrm{C}$ | $40^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $70^{\circ} \mathrm{C}$ | $100^{\circ} \mathrm{C}$ |
| Esters: |  |  |  |  |  |  |  |  |  |
| Methyl-formate .. | $\mathrm{C}_{2} \mathrm{H}_{4} \mathrm{O}_{2}$ | . 436 | . 391 | . 355 | . 325 |  |  |  |  |
| Ethyl-formate .... | $\mathrm{C}_{3} \mathrm{H}_{6} \mathrm{O}_{2}$ | . 510 | . 454 | . 409 | . 369 | . 336 | . 308 |  |  |
| Propyl-formate ... | $\mathrm{C}_{4} \mathrm{H}_{8} \mathrm{O}_{2}$ | . 672 | . 589 | . 521 | . 465 | . 417 | . 378 | . 314 |  |
| Methyl-acetate | $\mathrm{C}_{3} \mathrm{H}_{6} \mathrm{O}_{2}$ | . 484 | . 431 | . 388 | . 352 | . 320 | . 293 |  |  |
| Ethyl-acetate .. | $\mathrm{C}_{4} \mathrm{H}_{5} \mathrm{O}_{2}$ | . 583 | . 512 | . 455 | . 407 | . 367 | . 333 | . 279 |  |
| Propyl-acetate ... | $\mathrm{C}_{5} \mathrm{H}_{10} \mathrm{O}_{2}$ | . 773 | . 669 | . 585 | . 516 | . 460 | . 414 | . 341 | . 259 |
| Methyl-propionate. | $\mathrm{C}_{4} \mathrm{H}_{8} \mathrm{O}_{2}$ | . 587 | . 517 | . 460 | . 414 | . 375 | . 341 | . 286 |  |
| Ethyl-propionate | $\mathrm{C}_{5} \mathrm{H}_{10} \mathrm{O}_{2}$ | . 697 | . 608 | . 537 | . 477 | . 428 | . 387 | . 321 |  |
| Methyl-butyrate .. | $\mathrm{C}_{5} \mathrm{H}_{10} \mathrm{O}_{2}$ | . 763 | . 661 | . 580 | . 513 | . 459 | . 413 | . 341 | . 265 |
| $\begin{aligned} & \text { Methyl-iso- } \\ & \text { butyrate } \end{aligned}$ | $\mathrm{C}_{3} \mathrm{H}_{10} \mathrm{O}_{2}$ | . 676 | . 591 | . 523 | . 466 | . 419 | . 375 | . 315 |  |
| Iodides : |  |  |  |  |  |  |  |  |  |
| Methyl | $\mathrm{CH}_{3} \mathrm{I}$ | . 606 | . 548 | . 500 | . 460 | . 424 |  |  |  |
| Ethyl | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{I}$ | . 727 | . 654 | . 593 | . 540 | . 495 | . 456 | . 391 |  |
| Propyl | $\mathrm{C}_{3} \mathrm{H}_{3} \mathrm{I}$ | . 944 | . 833 | . 744 | . 669 | . 607 | . 552 | . 466 | . 371 |
| i-Propyl | $\mathrm{C}_{3} \mathrm{H}_{7} \mathrm{I}$ | . 884 | . 781 | . 697 | . 627 | . 568 | . 516 | . 435 |  |
| i-Butyl | C. $\mathrm{H}_{0} \mathrm{I}$ | 1.166 | 1.001 | . 875 | . 777 | . 697 | . 629 | . 522 | . 406 |
| Ally . | $\mathrm{C}_{3} \mathrm{H}_{3} \mathrm{I}$ | . 936 | . 826 | . 734 | . 660 | . 597 | . 544 | . 459 | . 365 |
| Paraffins: * ${ }^{119}$ |  |  |  |  |  |  |  |  |  |
| Pentane |  |  |  | . 274 | . 227 | vapor |  |  |  |
| Octane |  |  |  | . 707 | . 542 | . 429 |  |  |  |
| Hexane |  |  |  | . 382 | . 308 | . 254 |  |  |  |
| Heptane |  |  |  | . 521 | . 411 | . 333 |  |  |  |
| Sulfides: |  |  |  |  |  |  |  |  |  |
| Methyl | $\mathrm{C}_{2} \mathrm{H}_{8} \mathrm{~S}$ | . 361 | . 329 | . 301 | . 277 |  |  |  |  |
| Ethyl | $\mathrm{C}_{4} \mathrm{H}_{10} \mathrm{~S}$ | . 563 | . 501 | . 450 | . 407 | . 369 | . 338 | . 287 |  |
| Carbon di ....... | $\mathrm{CS}_{2}$ | . 438 | . 405 | . 376 | . 352 | . 330 |  |  |  |
| Turpentine ......... |  | 2.248 | 1.783 | 1.487 | 1.272 | 1.071 | . 926 | . 728 |  |
|  |  |  |  |  |  |  |  |  |  |

TABLE 319.-VISCOSITY OF SODIUM SILICATES ${ }^{117}$
(Temperature variation)
$\log _{10} \eta$ (poises) at

| $\begin{aligned} & \text { Wt. \% \% } \\ & \mathrm{Na}_{\mathrm{a}} \end{aligned}$ | $900^{\circ} \mathrm{C}$ | $1000^{\circ} \mathrm{C}$ | $1100^{\circ} \mathrm{C}$ | $1200^{\circ} \mathrm{C}$ | $1300^{\circ} \mathrm{C}$ | $1400^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 18.4 |  |  |  | 3.15 | 2.77 | 2.47 |
| 21.91 | 4.55 | 3.83 | 3.28 | 2.82 | 2.44 | 2.11 |
| 24.89 | 4.29 | 3.62 | 3.08 | 2.63 | 2.26 | 1.95 |
| 25.78 | 4.22 | 3.55 | 3.02 | 2.58 | 2.22 | 1.91 |
| 26.57 | 4.19 | 3.52 | 2.98 | 2.55 | 2.19 | 1.88 |
| 26.79 | 4.18 | 3.49 | 2.97 | 2.54 | 2.18 | 1.87 |
| 28.46 | 4.07 | 3.41 | 2.90 | 2.48 | 2.12 | 1.79 |
| 29.79 | 3.98 | 3.32 | 2.81 | 2.39 | 2.03 | 1.72 |
| 31.74 | 3.84 | 3.21 | 2.70 | 2.28 | 1.93 | 1.62 |
| 32.91 | 3.76 | 3.15 | 2.64 | 2.23 | 1.88 | 1.57 |
| 33.24 | 3.74 | 3.12 | 2.62 | 2.21 | 1.87 | 1.55 |
| 33.77 | 3.71 | 3.08 | 2.58 | 2.18 | 1.83 | 1.52 |
| 34.27 | 3.70 | 3.08 | 2.59 | 2.16 | 1.82 | 1.53 |
| 34.92 | 3.66 | 3.04 | 2.54 | 2.15 | 1.80 | 1.50 |
| 36.73 | 3.57 | 2.94 | 2.45 | 2.05 | 1.70 | 1.40 |
| 39.2 | 3.46 | 2.81 | 2.33 | 1.93 | 1.56 |  |
| 39.74 | 3.34 | 2.74 | 2.25 | 1.86 | 1.51 | 1.20 |
| 52.1 |  | 1.66 | 1.21 | . 91 | . 66 | . 47 |

[^144](Temperature variation)
Based on data by Dow Corning Corporation for DC 200 fluids.

| Fluid designation (centistokes at $25^{\circ} \mathrm{C}$ | Viscosity in poises |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $-25^{\circ} \mathrm{C}$ | $0^{\circ} \mathrm{C}$ | $25^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $100^{\circ} \mathrm{C}$ | $150^{\circ} \mathrm{C}$ |
| 1 | . 0163 | . 0118 | . 0083 | . 0064 | . 0052 |  |  |
| 2 | . 0472 | . 0287 | . 0173 | . 0129 | . 0100 | . 0079 | . 0056 |
| 5 | . 145 | . 077 | . 0452 | . 0301 | . 0221 | . 0173 | . 0116 |
| 10 | . 323 | . 159 | . 090 | . 059 | . 043 | . 032 | . 026 |
| 20 | . 683 | . 328 | . 184 | . 105 | . 082 | . 062 | . 040 |
| 50 | 2.39 | . 820 | . 467 | . 298 | . 208 | . 153 | . 094 |
| 100 | 3.22 | 1.61 | . 94 | . 59 | . 398 | . 285 | . 172 |
| 200 | 6.70 | 3.40 | 1.92 | 1.19 | . 798 | . 580 | . 346 |
| 500 | 15.9 | 8.15 | 4.84 | 2.89 | 1.94 | 1.36 | . 82 |
| 1000 | 34.4 | 17.00 | 9.70 | 6.04 | 4.02 | 2.80 | 1.57 |
| 12500 | 368.5 | 183.7 | 119.3 | 73.9 | 53.0 | 39.7 | 24.3 |
| 30000 | 1035. | 517. | 291.5 | 186.2 | 126.4 | 90.2 | 50.7 |
| 200,000 | 5820. | 3265. | 1940. | 1256. | 839. | 604. | 345. |

TABLE 321.-VISCOSITY IN THE SYSTEM ORTHOCLASE-ALBITE
(Temperature variation)
Values given as $\log _{10} \eta$, where $\eta=$ viscosity in poises.

| Wt. \% Orthoclase | 100 | 80 | 60 | 40 | 20 | 0 |
| :--- | ---: | :--- | :---: | :---: | :---: | :---: |
| Wt. \% Albite | 0 | 20 | 40 | 60 | 80 | 100 |
| $1300^{\circ} \mathrm{C}$ |  |  |  |  |  | 6.04 |
| $1350^{\circ} \mathrm{C}$ | 7.00 | 6.23 | 5.30 | 6.18 | 6.00 | 5.63 |
| $1400^{\circ} \mathrm{C}$ | 6.00 | 5.85 | 5.51 | 5.81 | 5.65 | 5.26 |
| $1450^{\circ} \mathrm{C}$ |  | 5.40 | 5.26 |  |  |  |

TABLE 322.-VISCOSITY OF SILICON DIOXIDE ${ }^{118}$
(Temperature variation)
Values given as $\log _{10} \eta ; \eta=$ viscosity in poises.

| Temperature | ${ }^{\circ} \mathrm{C}$ | 1250 | 1300 | 1350 | 1400 | 1450 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\log _{10} \eta$ | 13.40 | 12.19 | 11.46 | 10.69 | 10.02 | 9.42 |

[^145](Temperature variation)
Values given as $\log _{10} \eta$, where $\eta=$ viscosity in poises.

| Material | $1100^{\circ} \mathrm{C}$ | $1200^{\circ} \mathrm{C}$ | $1300^{\circ} \mathrm{C}$ | $1400^{\circ} \mathrm{C}$ | $1500^{\circ} \mathrm{C}$ | $1600^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Silica $\left(\mathrm{SiO}_{2}\right)$ | 15.57 | 13.68 | 12.06 | 10.66 | 9.20 | ... |
| Wollastonite $\left(\mathrm{CaSiO}_{3}\right)$ | $\ldots$ | $\ldots$ | $\cdots$ | $\cdots$ | . 486 | . 387 |
| $\begin{aligned} & \text { Diopside } \\ & \left(\mathrm{CaMgSi} \mathrm{Si}_{2} \mathrm{O}_{8}\right) \end{aligned}$ | $\ldots$ | $\ldots$ | 1.52 | 1.43 | . 267 | . 079 |
| Akermanite $\left(\mathrm{Ca}_{2} \mathrm{MgSi}_{2} \mathrm{O}_{7}\right)$ | $\ldots$ | $\ldots$ | 1.48 | . 656 | . 362 | . 146 |
| Monticellite ( $\mathrm{CaMgSiO}_{4}$ ) | $\ldots$ | $\cdots$ | $\cdots$ | $\cdots$ | . 241 | . 053 |
| Albite $\left(\mathrm{NaAlSi}_{3} \mathrm{O}_{8}\right)$ | ... | 7.17 | $\begin{aligned} & 5.82 \\ & 6.04 \end{aligned}$ | $\begin{aligned} & 4.60 \\ & 5.25 \end{aligned}$ |  | $\ldots$ |
| Orthoclase <br> ( $\mathrm{KAlSi}_{3} \mathrm{O}_{8}$ ) |  | $\ldots$ | ... | 7.0 | 6.2 |  |
| Anorthite $\left(\mathrm{CaAl}_{2} \mathrm{Si}_{2} \mathrm{O}_{8}\right)$ | $\ldots$ | $\ldots$ | $\ldots$ | 2.32 | 1.78 | 1.40 |
| $\begin{aligned} & \text { Gehlenite } \\ & \left(\mathrm{Ca}_{2} \mathrm{AlSiO}_{7}\right) \end{aligned}$ |  | $\ldots$ | $\ldots$ | $\ldots$ | . 911 | . 549 |

119 Birch, Handbook of physical constants, 1942. Measurements by: Volarovich and Leontieva, Trans. Soc. Glass Techn., vol. 20, p. 139, 1936. McCaffery, Trans. Amer. Inst. Min. and Met. Eng., vol. 100 , pp. 64, 86, 122, 125, 1932. Bowen, Trans. Anier. Geophys. V'nion, pt. 1, p. 249, 1934. Kani, Proc. Imp. Acad. (Tokyo), vol. 11, p. 334, 1935. Kani and Kuzu, Proc. Imp. Acad. (Tokyo), vol. 11, p. 383, 1935.

TABLE 324.-VISCOSITY OF BORON TRIOXIDE ${ }^{120}$
(Temperature variation)

| ${ }^{\circ} \mathrm{C}$ © C . | $\log _{10} \eta$ (poises) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | * | $\dagger$ | $\ddagger$ | § | \|| |
| 300 | . $\cdot$ | 9.64 | . . . | . . . |  |
| 400 | . $\cdot$ | 6.20 |  |  | 6.30 |
| 500 | 4.59 | . . . | 4.40 | . . | 4.47 |
| 600 | 3.68 |  |  |  | 3.49 |
| 700 | 2.93 | . . | . . . | 2.90 | 2.89 |
| 800 | 2.42 |  | . . . | 2.53 | 2.49 |
| 900 | 2.08 | . . | . . | 2.27 | 2.19 |
| 1000 | 1.87 |  |  | 2.10 | 1.96 |
| 1100 | 1.63 |  |  | 1.92 | 1.78 |
| 1200 |  | . . | . . | . . . | 1.62 |

120 Dane and Birch, Journ. Appl. Phys., vol. 9, p. 669, 1938, have shown that for pressures not in excess of $2000 \mathrm{~kg} / \mathrm{cm}^{2}$ the viscosity of boron trioxide is given for various pressures by the relation $\eta=\eta_{0} e^{a p}$; and at $359^{\circ} \mathrm{C}, a=15.10^{-4} \mathrm{~cm}^{2} / \mathrm{kg}$, and at $516^{\circ} \mathrm{C}, a=4.6 \times 10^{-4} \mathrm{~cm}^{2} / \mathrm{kg}$. Data from Birch, Handbook of physical constants, 1942, and from unpublished measurements by H. R. Lillie.
Observers of data by columns:

* Arndt, Zeit. Elektrotechn., vol. 13, p. 578, 1907.
$\dagger$ Parks and Spaght, Physics, vol. 6, p. 67, 1935.
$\ddagger$ Volarovich and Tolstoi, Trans. Soc. Glass Techn., vol. 18, p. 209, 1934.
§ Volarovich and Fridman, Acta Phys. (U.S.S.R.), vol. 6, p. 393, 1937.
if Lillie, unpublished data.

TABLE 325.-VISCOSITY IN THE SYSTEM DIOPSIDE-ALBITE-ANORTHITE*
(Temperature variation)
Values given as $\log _{10} \eta$, where $\eta=$ viscosity in poises.

| Wt. \% diopside | 100 | 80 | 60 | 40 | 20 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wt. \% albite | 0 | 20 | 40 | 60 | 80 | 100 |
| $1200^{\circ} \mathrm{C}$ |  |  |  | 3.99 | 5.08 |  |
| $1300{ }^{\circ} \mathrm{C}$ |  |  | 2.45 | 3.20 | 4.30 | 6.04 |
| $1400{ }^{\circ} \mathrm{C}$ | 1.60 | 1.93 | 2.04 | 2.64 | 3.63 | 5.26 |
| Wt. \% diopside | 20 | 40 | 60 | 80 |  |  |
| Wt. \% anorthite | 80 | 60 | 40 | 20 |  |  |
| $1300{ }^{\circ} \mathrm{C}$ |  | 3.77 | 2.18 |  |  |  |
| $1400{ }^{\circ} \mathrm{C}$ |  | 2.00 | 1.96 | 1.92 |  |  |
| $1500^{\circ} \mathrm{C}$ | 2.04 |  |  |  |  |  |
| Wt. \% albite | 80 | 60 | 40 | 20 |  |  |
| Wt. \% anorthite | 20 | 40 | 60 | 80 | 100 |  |
| $1300{ }^{\circ} \mathrm{C}$ | 5.51 | 4.67 |  |  |  |  |
| $1400^{\circ} \mathrm{C}$ | 4.63 | 3.89 | 3.40 |  |  |  |
| $1500^{\circ} \mathrm{C}$ |  |  | 2.66 | 2.28 |  |  |
| $1555{ }^{\circ} \mathrm{C}$ |  |  |  | 2.11 | 2.04 |  |
| Wt. \% diopside |  |  |  |  |  |  |
| Wt. \% albite | 20 | 40 | 20 | 60 | 40 | 20 60 |
| Wt. \% anorthite <br> $1200^{\circ} \mathrm{C}$ | 20 | 3.65 | 40 | 20 4.83 | 40 | 60 |
| $1300{ }^{\circ} \mathrm{C}$ | 2.23 | 2.92 | 2.67 | 3.88 | 3.57 |  |
| $1400{ }^{\circ} \mathrm{C}$ | 1.99 | 2.36 | 2.11 | 3.18 | 2.79 | 2.56 |

* For reference, see footnote 45, p. 136.

TABLE 326.-VISCOSITY OF MOLTEN METALS ${ }^{121}$
(Temperature variation)

| $\stackrel{\text { Temp. }}{{ }^{\circ} \mathrm{C}}$ | Lead | ${ }^{\text {Tin }}$ |  | ${ }^{\text {Temp. }} \mathrm{C} .$ | Antimony |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | * | $\dagger$ |  |  |
| 300 |  | 1.73 | 1.67 | 650 | 1.50 |
| 350 | 2.58 | 1.58 | 1.51 | 700 | 1.26 |
| 400 | 2.33 | 1.43 | 1.38 | 750 | 1.16 |
| 450 | 2.07 | 1.30 | 1.27 | 800 | 1.08 |
| 500 | 1.84 | 1.20 | 1.18 | 850 | 1.05 |
| 550 | 1.58 | 1.14 | 1.11 |  |  |
| 600 | 1.38 | 1.08 | 1.05 | Temp. |  |
| 650 |  |  | . 99 | ${ }^{\circ} \mathrm{C}$ | Copper |
| 700 | ... | ... | . 94 | 1100 | 3.33 |
| 750 |  |  | . 91 | 1150 | 3.22 |
| 800 |  |  | . 87 | 1200 | 3.12 |

[^146]Viscosities are given in cgs units, dyne-seconds per $\mathrm{cm}^{2}$, or poises.

| Liquid | ${ }^{\circ} \mathrm{C}$ | Viscosity | Liquid | ${ }^{\circ} \mathrm{C}$ | Viscosity |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Acetaldehyde | 0. | . 00275 | Oils : |  |  |
|  | 10. | . 00252 | * Filtered cylinder | 37.8 | 2.406 |
| " | 20. | . 00231 |  | 100.0 | . 187 |
| Air | -192.3 | . 00172 | * Dark cylinder | 37.8 | 4.224 |
| Aniline | 20. | . 04467 |  | 100.0 | . 240 |
|  | 60. | . 0156 | " ${ }^{\text {a }}$ | 37.8 | 7.324 |
| Bismuth | 285. | . 0161 | " " | 100.0 | . 341 |
|  | 365. | . 0146 | *"Extra L. L." | 37.8 | 11.156 |
| Black treacle | 12.3 | . 400 |  | 100.0 | . 451 |
| Copal lac | 22. | 4.80 | $\ddagger$ Linseed . 925 | 30. | . 331 |
| Hydrogen, liquid |  | . 00011 | " . 922 | 50. | . 176 |
| Menthol, solid | 14.9 | $2 \times 10^{12}$ | . 914 | 90. | . 071 |
| " ${ }^{\text {che }}$ liquid | 56.9 | . 069 | Olive . 9195. | 10. | 1.38 |
| Mercury | -20. | . 0184 |  | 15. | 1.075 |
|  | 0. | . 01661 | . 9130 | 20. | . 840 |
| " | 20. | . 01547 | " . 9065. | 30. | . 540 |
| " | 34. | . 01476 | " . 9000. | 40. | . 363 |
| " | 98. | . 01263 | . 8935. | 50. | . 258 |
| " | 193. | . 01079 | . 8800 | 70. | . 124 |
| " | 299. | . 00975 | $\dagger$ Rape | 15.6 | 1.118 |
| Oils: |  |  |  | 37.8 | . 422 |
| $\ddagger$ Dogfish-liver . 923 .. | 30. | . 414 | "، (........ | 100.0 | . 080 |
| " " . 918 .. | 50. | . 211 | " (another) | 15.6 | 1.176 |
| " . 908 | 90. | . 080 | " (another) | 100.0 | . 085 |
| Linseed .925. | 30. | . 331 | $\ddagger$ Soya bean 919 | 30.0 | . 406 |
| " 922. | 50. | . 176 | "، " 915 | 50.0 | . 206 |
| " 914. | 90. | . 071 | " . 906 | 90.0 | . 078 |
| * Spindle oil . 885 | 15.6 | . 453 | $\dagger$ Sperm | 15.6 | . 420 |
|  | 37.8 | . 162 |  | 37.8 | . 185 |
| " " ........ | 100.0 | . 033 | " | 100.0 | . 046 |
| * Light machinery |  |  | Phenol | 18.3 | . 1274 |
| 907£ ......... | 15.6 | 1.138 |  | 90.0 | . 0126 |
| * Light machinery | 37.8 | . 342 | Sulfur | 170. | 320.0 |
| " "" | 100.0 | . 049 |  | 180. | 550.0 |
| *"Solar red" engine.. | 15.6 | 1.915 | " | 187. | 560.0 |
|  | 37.8 | . 496 | " | 200. | 500.0 |
| " " " | 100.0 | . 058 | " | 250. | 104.0 |
| *"Bayonne" engine | 15.6 | 2.172 | " | 300. | 24.0 |
|  | 37.8 | . 572 | " | 340. | 6.2 |
| " " | 100.0 | . 063 | " | 380. | 2.5 |
| *"Queen's red" engine | 15.6 | 2.995 | " | 420. | 1.13 |
|  | 37.8 | . 711 | " ${ }^{\text {a }}$......... | 448. | . 80 |
| " | 100.0 | . 070 | Sulfuric acid ( $\rho=1$ | 25. | . 00973 |
| *"Galena" axle | 15.6 | 4.366 | $\dagger$ Tallow | 66. | . 176 |
| " " | 37.8 | . 909 |  | 100. | . 078 |
| * Heavy machinery | 15.6 | 6.606 | Zinc | 280. | . 0168 |
|  | 37.8 | 1.274 |  | 357. | . 0142 |
|  |  |  | " | 389. | . 0131 |

[^147]TABLE 328.-RATIO OF VISCOSITY AT HIGH TO THAT AT ATMOSPHERIC PRESSURE

| Pressure |  | Bayonne oil (mineral) | FFF cylinder (mineral) | Trotter (animal) | $\underbrace{\text { Rape }}$ | Castor |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| tons/in ${ }^{2}$ | $\mathrm{kg} / \mathrm{cm}^{2}$ |  |  |  | (vegetable) |  | (fish) |
| 1 | 157.5 | 1.3 | 1.4 | 1.2 | 1.1 | 1.2 | 1.2 |
| 2 | 315. | 2.0 | 2.0 | 1.6 | 1.4 | 1.6 | 1.5 |
| 4 | 630. | 4.0 | 4.5 | 2.4 | 2.3 | 2.7 | 2.4 |
| 6 | 945. | 7.8 | 8.9 | 3.5 | 3.5 | 4.2 | 3.5 |
| 8 | 1260. | 16.1 | - | 5.0 | - | 5.8 | - |

TABLE 329.-VISCOSITY OF LIQUEFIED PURE GASES AND VAPORS ${ }^{122}$
Viscosities in millipoises.
(Temperature variation)

| $\begin{aligned} & \text { Temp. } \\ & \hline \mathrm{K} \end{aligned}$ | $\mathrm{C}_{2} \mathrm{H}_{4}$ | $\mathrm{C}_{2} \mathrm{H}_{6}$ | $\mathrm{C}_{3} \mathrm{H}_{6}$ | $\mathrm{C}_{8} \mathrm{H}_{8}$ | ${ }^{\text {Temp. }}$ \% | $\mathrm{N}_{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 85 | ... |  |  | 118.5 | 66 | 2.49 |
| 90 | $\ldots$ |  | 125.5 | 74.2 | 68 | 2.26 |
| 95 | ... |  | 72.5 | 52.5 | 70 | 2.08 |
| 100 |  | 9.15 | 45.5 | 38.3 | 72 | 1.93 |
| 105 | 6.60 | 7.48 | 31.1 | 29.0 | 74 | 1.80 |
| 110 | 5.60 | 6.37 | 22.3 | 22.3 | 76 | 1.67 |
| 115 | 4.86 | 5.66 | 17.0 | 18.2 | 78 | 1.56 |
| 120 | 4.24 | 5.06 | 13.3 | 15.2 | 80 | 1.47 |
| 125 | 3.73 | 4.52 | 11.1 | 13.2 |  |  |
| 130 | 3.32 | 4.00 | 9.4 | 11.6 | Temp. |  |
| 135 | 2.96 | 3.58 | 8.2 | 10.3 | ${ }^{\circ} \mathrm{K}$. | $\mathrm{CH}_{4}$ |
| 140 | 2.66 | 3.23 | 7.2 | 9.3 | 95 | 1.82 |
| 145 | 2.43 | 2.92 | 6.2 | 8.2 | 100 | 1.53 |
| 150 | 2.22 | 2.66 | 5.6 | 7.3 | 105 | 1.34 |
| 155 | 2.03 | 2.44 | 5.0 | 6.5 | 110 | 1.21 |
| 160 | 1.86 | 2.27 | 4.5 | 5.5 |  |  |
| 165 | 1.71 | 2.12 | 4.0 | 5.0 |  |  |
| 170 | 1.58 | 2.00 | 3.5 | 4.5 |  |  |

122 Gerf, S. F., and Galkov, G. I., Journ. Techn. Phys. (U.S.S.R.), vol. 10, p. 725, 1940.

TABLE 330.-VISCOSITY OF PURE HYDROCARBONS ${ }^{123}$
Viscosities in centipoises; densities referred to water at $4^{\circ} \mathrm{C}$.

| ${ }^{\text {Temp. }}$. | Propane, $\mathrm{C}_{3} \mathrm{H}_{8}$ |  | $n$ - Butane, $\mathrm{C}_{4} \mathrm{H}_{10}$ |  | iso-Butane, $\mathrm{C}_{4} \mathrm{H}_{10}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Density | Viscosity | Density | Viscosity | Density | Viscosity |
| -70 | . 614 | . 287 | . 671 | . 460 | . 657 | . 533 |
| -60 | . 604 | . 253 | . 661 | . 403 | . 647 | . 455 |
| -50 | . 592 | . 227 | . 652 | . 354 | . 637 | . 393 |
| -40 | . 580 | . 205 | . 642 | . 314 | . 626 | . 343 |
| -30 | . 568 | . 184 | . 632 | . 281 | . 615 | . 301 |
| -20 | . 556 | . 168 | . 622 | . 253 | . 605 | . 267 |
| -10 | . 543 | . 152 | . 611 | . 229 | . 593 | . 239 |
| 0 | . 531 | . 138 | . 601 | . 209 | . 582 | . 215 |
| $+10$ | . 517 | . 126 | . 590 | . 191 | . 571 | . 195 |
| $+20$ | . 502 | . 116 | . 579 | . 174 | . 559 | . 176 |
| $+30$ | . 487 | . 108 | . 567 | . 159 | . 547 | . 160 |
| +40 | . 471 | . 099 | . 555 | . 146 | . 534 | . 146 |

[^148]Part 1.
$\log _{10} \eta$ (poises) at

| Glass | $500^{\circ} \mathrm{C}$ | $600^{\circ} \mathrm{C}$ | $700^{\circ} \mathrm{C}$ | $800^{\circ} \mathrm{C}$ | $900^{\circ} \mathrm{C}$ | $1000^{\circ} \mathrm{C}$ | $1100^{\circ} \mathrm{C}$ | $1200^{\circ} \mathrm{C}$ | $1300^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 13.76 | 9.85 | 7.03 | 5.42 | 4.37 | 3.52 | 2.93 | 2.47 | 2.09 |
| 2 |  |  |  | 5.84 | 4.79 | 3.99 | 3.41 | 2.93 | 2.50 |
| 3 |  |  |  | 5.38 | 4.29 | 3.52 | 2.94 | 2.48 | 2.08 |
| 4 |  |  |  | 5.74 | 4.48 | 3.60 | 2.96 | 2.47 | 2.03 |
| 5 | 15.20 | 12.35 | 9.82 | 7.87 | 6.48 | 5.52 | 4.77 | 4.16 | 3.67 |
| 6 | 13.82 | 10.85 | 8.55 | 6.81 | 5.68 | 4.88 | 4.20 | 3.65 | 3.22 |
| 7 |  | . . . | . . | . . | 1.55 | 1.24 | 1.00 | . 83 | . 69 |
| 8 |  |  |  | . . . | 2.17 | 1.81 | 1.55 | 1.33 | 1.16 |
| 9 |  |  |  | . . . |  | 4.20 | 3.54 | 3.02 | . . . |
| 10 |  |  | ... |  |  | 4.00 | 3.37 | 2.85 | . . . |
| 11 | ... |  | ... |  | 4.71 | 3.85 | 3.24 | 2.74 | . . . |
| 12 | . . . |  | . . . | . . . | . . | 3.89 | 3.34 | 2.91 |  |
| 13 |  |  |  |  |  | 4.06 | 3.47 | 3.01 | 2.67 |
| 14 | . . |  |  | 6.02 | 5.79 | 3.97 | 3.35 | 2.89 | 2.31 |
| 15 |  | 9.49 | 7.30 | 5.70 | 4.48 | 3.70 | 3.08 | 2.60 | 2.40 |

Part 2.
Composition (weight percentages)

| Glass | $\mathrm{SiO}_{2}$ | $\mathrm{B}_{2} \mathrm{O}_{3}$ | $\mathrm{Na}_{2} \mathrm{O}$ | $\mathrm{K}_{2} \mathrm{O}$ | MgO | CaO | ZnO | Pbo | $\mathrm{Al}_{2} \mathrm{O}_{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 69.73 |  | 20.96 | trace |  | 9.05 |  |  | .18* |
| 2 | 72.6 | 1.43 | 16.0 | . 68 | 1.7 | 6.40 |  |  | 1.0 * |
| 3 | 70.12 |  | 21.1 | trace |  | 8.77 |  |  | . 02 |
| 4 | 67.3 | 2.00 | 14.0 | ... |  | 7.0 | 7.0 |  | 2.50 |
| 5 | 81.0 | 13.00 | 4.00 | ... | $\ldots$ | ... |  |  | 2.0 |
| 6 | 75.0 | 15.00 | 5.0 |  | $\ldots$ | $\ldots$ | ... | 5.0 |  |
| 7 | 65.0 | ... | 7.5 | 7.5 | ... | $\ldots$ | ... | 20.0 |  |
| 8 | 60.0 | ... | 5.0 | 5.0 |  |  | ... | 30.0 |  |
| 9 | 73.97 | ... | 15.30 |  | 3.57 | 5.69 | ... | ... | .91* |
| 10 | 74.35 | $\ldots$ | 15.30 |  | . 18 | 9.03 |  |  | .85* |
| 11 | 72.27 | ... | 16.88 |  | . 35 | 8.79 |  |  | 1.72* |
| 12 | 62.50 |  | 7.50 | 6.70 |  |  |  | 22.00 | 1.30* |
| 13 | 75.0 | 10 | 10 |  |  |  |  |  | 5 |
| $14^{\dagger}$ | 56 | 7.5 | 4 | 10 |  |  |  |  | 2.5 |
| 15 | 73.18 |  | 19.38 |  | . 21 | 6.26 |  |  | 1.19* |

## Part 3.-Commercial glass $\ddagger$

$\log _{10} \eta$ (poises) at


[^149]
## Variation of viscosity with pressure and temperature

According to the kinetic theory of gases the coefficient of viscosity $\eta=\frac{1}{3}(\rho \bar{c}), \rho$ being the density, $\bar{c}$ the average velocity of the molecules, $l$ the average path. Since $l$ varies inversely as the number of molecules per unit volume, $\rho l$ is a constant and $\eta$ should be independent of the density and pressure of a gas (Maxwell's law). This has been found true for ordinary pressures; below ${ }^{1 / 80}$ atmosphere it may fail, and for certain gases it has been proved untrue for high pressures, e.g., $\mathrm{CO}_{2}$ at $33^{\circ}$ and above 50 atm . See Jeans, "Dynamical Theory of Gases."
If $B$ is the amount of momentum transferred from a plane moving with velocity $U$ and parallel to a stationary plane distant $d$, and $s$ is a quantity (coefficient of slip) to allow for the slipping of the gas molecules over the plane, then $\eta=(B / U)(d+2 s) ; s$ is of the same magnitude as $l$, probably between .7 (Timiriazeff) and .9 (Knudsen) of it; at low pressures $d$ becomes negligible compared with $2 s$ and the viscosity should vary inversely as the pressure.
$\bar{c}$ depends only on the temperature and the molecular weight. $\bar{c}$ varies as the $\sqrt{T}$, but $\eta$ has been found to increase much more rapidly. Meyer's formula, $\eta_{t}=\eta_{0}(1+a t)$, where $a$ is a constant and $\eta_{0}$ the viscosity at $0^{\circ} \mathrm{C}$, is a convenient approximate relation. Sutherland's formula

$$
\eta_{t}=\eta_{0} \frac{273+C}{T+C}\left(\frac{T}{273}\right)^{\frac{3}{2}}
$$

is the most accurate formula in use, taking into account the effect of molecular forces. It holds for temperatures above the critical and for pressures following approximately Boyle's law. It may be thrown into the form $T=K T^{\frac{1}{2}} / \eta-C$ which is linear of $T$ and $T^{\frac{3}{2}} / \eta$, with a slope equal to $K$ and the ordinate intercept equal to $-C$. Onnes (see Jeans) shows that this formula does not represent helium at low temperatures with anything like the accuracy of the simpler formula $\eta=\eta_{0}(T / 273.1)^{n}=A T^{n}$.

The following table ${ }^{125}$ contains the constant $a$ of Meyers formula, $C$ and $K$ of Sutherland's formula, $n$ and $A$ of the exponential formula, and the temperature range for which the constants of the latter two are applicable.

| Gas | Temperature range ${ }^{\circ} \mathrm{C}$ | $a \times 10^{3}$ | C | $K \times 10^{6}$ | $n$ | $A \times 10^{6}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Air | 23 to 750 | 2.90 | 117.9 | 14.82 | . 754 | 2.490 |
| Ammonia | - 77 to 441 |  | 472 | 15.42 | 1.041 | . 274 |
| Argon | -183 to 827 | 1.78 | 133 | 19.00 | . 766 | 2.782 |
| Benzene | 0 to 313 |  | 403 | 10.33 | . 974 | . 299 |
| Carbon dioxide | - 98 to 1052 | 3.48 | 233 | 15.52 | . 868 | 1.057 |
| Carbon monoxide |  | 2.69 | 102 | 13.5 | . 74 |  |
| Chloroform |  |  | 454 | 15.9 | ... |  |
| Ethylene |  | 3.50 | 226 | 10.6 |  |  |
| Helium | -258 to 817 |  | 97.6 | 15.13 | . 653 | 4.894 |
| Hydrogen | -258 to 825 | $\ldots$ | 70.6 | 6.48 | . 678 | 1.860 |
| Krypton |  | $\ldots$ | 188 |  |  |  |
| Mercury | -218 to 610 | ... | 996 | 63.00 | 1.082 | . 573 |
| Methane | 18 to 499 |  | 155 | 9.82 | . 770 | 1.360 |
| Neon |  |  | 252 |  |  |  |
| Nitrogen | -191 to 825 | 2.69 | 102 | 13.85 | . 702 | 3.213 |
| Nitrous oxide |  | 3.45 | 313 | 17.2 | . 93 |  |
| Oxygen | -191 to 829 |  | 110 | 16.49 | . 721 | 3.355 |
| Water vapor | 0 to 407 |  | 659 | 18.31 | 1.116 | . 170 |
| Xenon |  |  | 252 |  |  |  |

[^150]Part 1.-Viscosity of vapors
The values of $\eta$ given in the table are $10^{\circ}$ times the coefficients of viscosity in cgs units.

| Substance | ${ }^{\text {Temp. }}{ }^{\circ} \mathrm{C} .$ | $\eta$ | Substance | ${ }^{\text {Temp. }}$ ¢ ${ }^{\text {c }}$ | $\eta$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Acetone | 18.0 | 78. | Ether | 16.1 | 73.2 |
| Alcohol, Methyl | 66.8 | 135. |  | 36.5 | 79.3 |
| Alcohol, Ethyl | 78.4 | 142. | Ethyl chloride | 0. | 93.5 |
| Alcohol, Propyl, norm | 97.4 | 142. | Ethyl iodide | 72.3 | 216.0 |
| Alcohol, Isopropyl ... | 82.8 | 162. | Ethylene | 0.0 | 96.1 |
| Alcohol, Butyl, norm. | 116.9 | 143. | Mercury | 270.0 | 489. |
| Alcohol, Isobutyl | 108.4 | 144. |  | 300.0 | 532. |
| Alcohol, Tert. butyl. | 82.9 | 160. | " | 330.0 | 582. |
| Ammonia ......... | 20.0 | 108. | " | 360.0 | 627. |
| Benzene | 0. | 70. | " | 390.0 | 671. |
|  | 19.0 | 79. | Methane | 20.0 | 120.1 |
| " $\quad$....... | 100.0 | 118. | Methyl chloride | 0.0 | 98.8 |
| Carbon bisulfide | 16.9 | 92.4 |  | 15.0 | 105.2 |
| Carbon monoxide | 20.0 | 184.0 | " " | 302.0 | 213.9 |
| Chloroform | 0.0 | 95.9 | Methyl iodide | 44.0 | 232. |
| " | 17.4 | 102.9 | Water vapor | 0.0 | 90.4 |
| " | 61.2 | 189.0 |  | 16.7 | 96.7 |
| Ether | 0.0 | 68.9 | " ${ }^{\text {c }}$ | 100.0 | 132.0 |

Part 2.-Viscosity of gases and vapors ${ }^{120}$
(Temperature variation)

| ${ }^{\text {Temp. }}{ }^{\text {C }}$ | Viscosity in millipoises |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Air | Argon | Carbon dioxide | $\begin{aligned} & \text { Chlo- } \\ & \text { rine- } \end{aligned}$ | Helium | $\underbrace{}_{\substack{\text { Hydro- } \\ \text { gen }}}$ | $\underset{\substack{\text { Nitro- } \\ \text { gen }}}{ }$ | Oxygen | Xenon |
| -200 | . 053 |  |  |  |  | . 033 | ... | ... | $.222\left(15^{\circ} \mathrm{C}\right)$ |
| -150 | . 081 |  |  |  | ... | . 047 | $\ldots$ |  |  |
| -100 -50 | . 111 |  | . 087 | $\ldots$ | $\ldots$ | . 0671 | $\ldots$ |  | Nitric oxide $179\left(0^{\circ} \mathrm{C}\right)$ |
| -50 0 | . 179 |  | . 112 |  |  | . 083 |  |  |  |
| 50 | . 193 | . 241 | . 159 | .147 | . 207 | . 093 | . 189 | .217 | Nitrous oxide |
| 100 | . 216 | . 269 | . 181 | . 167 | . 228 | . 102 | . 207 | . 241 | $.138\left(0^{\circ} \mathrm{C}\right)$ |
| 150 | . 237 | . 297 | . 203 | . 189 | . 247 | . 111 | . 226 | . 264 |  |
| 200 | . 256 | . 321 | . 225 | . 208 | . 267 | . 120 | . 245 | . 287 | Krypton |
| 250 | . 275 | . 346 | . 245 | . 228 | . 285 | . 129 | . 263 | . 309 | $.246\left(15^{\circ} \mathrm{C}\right)$ |
| 300 | . 293 | . 367 | . 262 |  | . 305 | . 137 | . 280 | . 330 |  |
| 350 | . 310 | . 389 | . 280 | $\ldots$ | . 323 | . 145 | . 296 | . 349 | Carbon monoxide |
| 400 | . 327 | . 410 | . 299 | $\ldots$ | . 341 | . 153 | . 311 | . 368 | $.163\left(0^{\circ} \mathrm{C}\right)$ |
| 500 | . 357 | . 450 | . 331 | $\ldots$ | . 375 | . 167 | . 341 | . 403 |  |
| 600 | . 384 | . 488 | . 362 |  | . 408 | . 181 | . 367 | . 435 | Ammonia |
| 700 | . 411 | . 521 | . 391 |  | . 438 | . 195 | . 391 | . 466 | $.096\left(0^{\circ} \mathrm{C}\right)$ |
| 800 | . 437 | . 554 | . 417 |  | . 467 | . 208 | . 414 | . 494 |  |
| 900 | . 463 |  | . 421 | ... | ... |  |  |  |  |
| 1000 | . 499 |  | . 465 |  |  |  |  |  |  |
| 1100 | . 511 |  |  |  |  |  |  |  |  |

## TABLE 334.-PRESSURE EFFECT ON VISCOSITY OF PURE LIQUIDS ${ }^{17}$

This table gives $\log _{10}$ of the relative viscosity as a function of pressure and density, the viscosity at $30^{\circ} \mathrm{C}$ and atmospheric pressure taken as unity. For each compound first line $\log \eta / \eta_{0}$ at $30^{\circ} \mathrm{C}$, second line at $75^{\circ} \mathrm{C}$, third line $\eta_{30} / \eta_{75}$.

|  | Pressure $\mathrm{kg} / \mathrm{cm}^{2}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Substance | 1 | 500 | 1000 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | $\eta_{30}$ |
| Methyl | . 000 | . 094 | . 167 | . 286 | . 471 | . 616 | . 750 | . 874 | . 998 | $.00520$ |
| alcohol | 9.769 | 9.862 | 9.933 | . 043 | . 208 | . 334 | . 448 | . 555 | . 655 |  |
|  | 1.702 | 1.706 | 1.714 | 1.750 | 1.832 | 1.914 | 2.004 | 2.084 | 2.203 |  |
| Ethyl alcohol | . 000 | . 107 | . 200 | . 363 | . 617 | . 829 | 1.023 | 1.211 | 1.390 | . 01003 |
|  | 9.657 | 9.772 | 9.873 | . 045 | . 289 | . 473 | . 634 | . 778 | . 919 |  |
|  | 2.203 | 2.163 | 2.123 | 2.080 | 2.128 | 2.270 | 2.449 | 2.710 | 2.958 |  |
| n-Propyl alcohol | . 000 | . 151 | . 283 | . 494 | . 836 | 1.131 | 1.402 | 1.667 | 1.915 | . 01779 |
|  | 9.598 | 9.754 | 9.880 | . 074 | . 368 | . 610 | ${ }^{.827}$ | 1.033 | 1.223 |  |
|  | 2.523 | 2.495 | 2.529 | 2.630 | 2.938 | 3.319 | 3.758 | 4.305 | 4.920 |  |
| n-Butyl alcohol | . 000 | . 175 | . 321 | . 554 | . 934 | 1.289 | 1.609 | 1.912 | 2.208 | . 02237 |
|  | 9.548 | 9.724 | 9.867 | . 089 | . 312 | . 690 | . 941 | 1.172 | 1.396 |  |
|  | 2.845 | 2.838 | 2.858 | 2.932 | 3.343 | 3.991 | 4.679 | 5.521 | 6.518 |  |
| n-Amyl alcohol | . 000 | . 188 | . 341 | . 607 | 1.060 | 1.448 | 1.811 | 2.164 | 2.495 |  |
|  | 9.540 | 9.723 | 9.871 | . 105 | . 466 | . 772 | 1.049 | 1.313 | 1.562 |  |
|  | 2.884 | 2.917 | 2.951 | 3.177 | 3.926 | 4.742 | 5.781 | 7.096 | 8.570 |  |
| n -Pentane | . 000 | . 181 | . 315 | . 524 | . 847 | 1.112 | 1.360 | 1.615 | 1.846 | . 00220 |
|  | 9.811 | . 014 | . 163 | . 380 | . 676 | . 908 | 1.119 | 1.313 | 1.493 |  |
|  | 1.545 | 1.469 | 1.419 | 1.393 | 1.483 | 1.600 | 1.742 | 2.004 | 2.254 |  |
| n -Hexane | . 000 | . 184 | . 332 | . 561 | . 914 | 1.224 | 1.514 | 1.803 |  | . 00296 |
|  | 9.803 | . 028 | . 171 | . 379 | . 701 | . 961 | 1.198 | 1.426 | 1.646 |  |
| Ethyl chloride | 1.000 | . 134 | . 242 | . 405 | . 649 | . 837 | 1.008 | 1.172 | 1.323 |  |
|  | 9.850 | . 017 | . 131 | . 285 | . 514 | . 683 | . 834 | . 977 | 1.111 |  |
|  | 1.413 | 1.309 | 1.291 | 1.318 | 1.365 | 1.426 | 1.493 | 1.567 | 1.633 |  |
| Ethyl bromide | . 000 | . 121 | . 222 | . 387 | . 631 | . 854 | 1.043 | 1.223 | 1.400 | . 00368 |
|  | 9.806 | 9.959 | . 072 | . 235 | . 472 | . 653 | . 816 | . 978 | 1.123 |  |
|  | 1.567 | 1.452 | 1.413 | 1.419 | 1.442 | 1.589 | 1.687 | 1.758 | 1.892 |  |
| Ethyl iodide | . 000 | . 115 | . 218 | . 385 | . 656 | . 888 | 1.108 | 1.330 | 1.549 | . 00540 |
|  | 9.837 | 9.954 | . 057 | . 227 | . 467 | . 672 | . 854 | 1.030 | 1.200 |  |
|  | 1.455 | 1.449 | 1.445 | 1.439 | 1.545 | 1.644 | 1.795 | 1.995 | 2.234 |  |
| Acetone | . 000 | . 135 | . 226 | . 373 | . 605 | . 804 | . 987 | 1.160 |  | . 00285 |
|  | 9.895 1.274 | .017 1.312 | .113 1.297 | .245 1.343 | . 4.445 | . 610 1.563 | .762 1.679 | $\begin{array}{r} .898 \\ 1.828 \end{array}$ | 1.031 |  |
| Glycerine | . 000 | . 134 | . 260 | . 497 | . 936 | 1.346 | 1.741 | 2.133 |  | 3.8 |
|  | 8.810 | 8.920 | 9.023 | 9.204 | 9.529 | 9.818 | . 094 | . 369 | . 628 |  |
|  | 15.49 | 16.37 | 17.26 | 19.63 | 25.53 | 33.73 | 44.36 | 58.08 |  |  |
| CClı | . 000 | . 190 | . 351 | $\begin{array}{r} .493 \\ (1500) \end{array}$ | kg/cm |  |  |  |  | . 00845 |
|  | 9.760 | 9.949 | . 100 | . 349 | . 542 |  |  |  |  |  |
|  | 1.738 | 1.742 | 1.782 |  |  |  |  |  |  |  |
| Chloroform | . 000 | . 110 | . 211 | . 386 | . 660 | . 884 |  |  |  | . 00519 |
|  | 9.858 | 9.985 | . 094 | . 251 | . 480 | . 691 | . 914 | 1.141 |  |  |
|  | 1.387 | 1.334 | 1.309 | 1.365 | 1.514 | 1.560 |  |  |  |  |
| $\mathrm{CS}_{2}$ | . 000 | . 090 | . 160 | . 180 | . 309 | $\begin{array}{r} .674 \\ .527 \end{array}$ | $.840$ | $\begin{array}{r} 1.010 \\ .808 \end{array}$ | $\begin{array}{r} 1.189 \\ .946 \end{array}$ | . 00352 |
|  | 9.875 1.334 | 9.972 1.312 | .051 1.285 | .180 1.340 | . 1.371 | 1.403 | 1.476 | 1.592 | 1.750 |  |
| Ether | . 000 | . 189 | . 324 | . 514 | . 792 | 1.042 | 1.261 | 1.469 | 1.670 | . 00212 |
|  | 9.878 | . 024 | . 149 | . 344 | . 601 | . 806 | . 986 | 1.155 | 1.311 |  |
|  | 1.324 | 1.462 | 1.496 | 1.479 | 1.552 | 1.722 | 1.884 | 2.061 | 2.286 |  |
| Benzene | . 000 | . 173 | . 347 |  |  |  |  |  |  | . 00566 |
|  | 9.765 | 9.938 | . 081 | . 308 | $\left.\begin{array}{r} .498 \\ (3000) \end{array}\right\} \mathrm{kg} / \mathrm{cm}^{2}$ |  |  |  |  |  |
|  | 1.718 | 1.718 | 1.845 |  |  |  |  |  |  |  |
| Toluene |  | . 145 | . 274 | . 497 | . 897 | 1.285 | 1.699 | 2.177 | 1.832 | . 00523 |
|  | 9.796 | 9.939 | . 065 | . 267 | . 597 | . 896 | $1.186$ | 1.504 |  |  |
|  | 1.600 | 1.607 | 1.618 | 1.698 | 1.995 | 2.449 | 3.258 | 4.710 |  |  |
| Eugenol | . 000 | . 288 | . 541 | 1.081 | 2.273 | 3.007 |  |  |  |  |
|  |  | $\begin{aligned} & 9.616 \\ & 4.699 \end{aligned}$ | $\begin{aligned} & 9.810 \\ & 5.383 \end{aligned}$ | 1.65.1438.670 | $\begin{aligned} & (3000)(5000) \\ & .805 \\ & 29.38 \end{aligned} 1.520 \quad 2.343 \mathrm{~cm}^{2}$ |  |  |  |  |  |
|  | 9.429 |  |  |  |  |  |  |  |  |  |
|  |  |  |  | 8.670 |  |  |  |  |  |  |

[^151]The SAE viscosity numbers constitute a classification of crankcase lubricating oils in terms of viscosity only. Other facts of oil quality or character are not considered.

## Part 1.-Crankcase oil classification

SAE recommended practice


Part 2.-Automotive Manufacturers' viscosity classification
SAE general information

| Viscosity <br> number | $\overbrace{\text { Min. }}^{\text {Viscosity range at }} 0^{\circ} \mathrm{F}$, Saybolt univ., sec |  |
| :---: | :---: | :---: |
| 10W | 6,000 | 12,000 |
| 20 W | 12,000 | 48,000 |

${ }^{128}$ SAE Handbook, 1949 ed., p. 580, Soc. Automot. Eng., New York.

TABLE 336.-EFFECT OF PRESSURE UPON VISCOSITY ${ }^{120}$

| Substance | Temper-atureoreor | Absolute viscosity at 1 atmcentipoises centipois | Relative viscosity Pressure in $\mathrm{kg} / \mathrm{cm}^{2}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1 | 1000 | 4000 | 8000 | 12,000 |
| i-Pentane <br> Acetone | 30 | . 198 | 1.0 | 2.208 | 7.834 | 26.98 | 88.51 |
|  | 75 |  | . 662 | 1.560 | 5.188 | 15.10 | 38.55 |
|  | 30 | . 285 | 1.0 | 1.683 | 4.027 | 9.705 |  |
|  | 75 |  | . 785 | 1.297 | 2.786 | 5.781 | 10.74 |
| $\mathrm{CS}_{2}$ | 30 | . 352 | 1.0 | 1.445 | 3.228 | 6.918 | 15.45 |
|  | 75 |  | . 750 | 1.125 | 2.355 | 4.688 | 8.83 |
| Sulfuric ether | 30 | . 212 | 1.0 | 2.109 | 6.194 | 18.24 | 46.77 |
|  | 75 | - | . 755 | 1.409 | 3.990 | 9.683 | 20.46 |
| Petroleum ether | 30 | - | 1.0 | 1.995 | 8.51 | 38.9 | 151.4 |
| Kerosene | 80 30 | - |  |  | 3.63 | 11.5 | 30.9 |
|  | 80 | - | 1.0 | 2.88 | 8.13 | 75.9 | 631 |
| Water | 0 | 1.792 | 1.0 | . 921 | 1.111 | freezes | - |
|  | 10.3 | 1.297 | . 779 | . 743 | . 842 | 1.152 |  |
|  | 30 | . 801 | . 488 | . 514 | . 658 | . 923 | 1.206 |
|  | 75 | . 380 | . 222 | . 239 | . 302 | . 445 | -- |
|  | 100 | . 284 |  |  |  |  |  |
| Mercury | 30 | 1.516 | 1.0 | 1.023 | 1.097 | 1.202 | 1.324 |
|  | 75 | 1.340 | . 884 | . 883 | . 880 | . 877 | . 876 |

${ }^{129}$ Bridgman, P. W., The physics of high pressure. Macmillan, New York, 1931.

With very few exceptions present-day lubricants are petroleum products or blends of petroleum products with various compounding or addition agents such as fatty oils, diversified types of soap, and in rare instances solid materials such as graphite. Addition agents are more costly than petroleum derivatives; hence they are used as sparingly as possible. The addition agents are generally employed when conditions of use require greater "oiliness" (higher film strength) than is attainable with unblended petroleum oils. The latter usually deteriorate more slowly in service than blended products, which is an advantage supplementing that of low relative cost. There are a few jobs of lubrication for which fatty oils have never been entirely supplanted, as for example the use of porpoise-jaw oil in fine watches.

## Lubricants for Cutting Tools ${ }^{130}$

Various types of oils have been used as lubricants for cutting tools. These are fatty oils, kerosene, turpentine, mineral oils and various blends of these oils. Sulfur has been combined with some of these oils to increase the film strength. Such mixtures and blends are furnished by the various manufacturers under their trade names such as Pennex, Dortan, Fanox, and Kutwell by the Standard Oil Co. of New Jersey.

| Severity | Type of operation | $\begin{aligned} & \text { Ferrous } \\ & \text { (more than } \\ & 70 \% \text { ) } \end{aligned}$ $70 \%)$ | $\begin{gathered} \text { Ferrous } \\ (50-65 \%) \end{gathered}$ | Ferrous (less than $40 \%$ ) | Nonferrous (more than $100 \%$ ) | Nonferrous (less than $100 \%$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{1}{3}$ (greatest) | Broaching, internal | Em Sulf | Sulf Em | Sulf Em | MO Em | Sulf ML |
| 3 | Tapping, plain | Sulf | Sulf | Sulf | Em Dry | Sulf ML |
| 2 | Threading, pipe | Sulf | Sulf ML | Sulf |  | Sulf |
| 3 | Threading, plain | Sulf | Sulf | Sulf | Em Sulf | Sulf |
| 4 | Gear shaving | Sulf L | Sulf L | Sulf L |  |  |
| 4 | Gear cutting | Sulf ML Em | Sulf | Sulf ML |  | Sulf ML |
| 5 | Drilling, deep | Em ML | Sulf Em | Sulf | MO ML Em | Sulf ML |
| 8 | Boring, multiple head | Sulf Em | Sulf Em | Sulf Em | K Dry Em | Sulf Em |
| 8 | High-speed, lightfeed, automatic screw machines | Sulf Em ML | Sulf Em ML | Sulf ML Em | Em Dry ML | Sulf |
| 9 | Turning; singlepoint tool, form tools | Em Sulf ML | Em Sulf ML | Em Sulf ML | Em Dry ML | Em Sulf |

[^152]The required force $F$ necessary to just move an object along a horizontal plane $=f N$ where $N$ is the normal pressure on the plane and $f$ the "coefficient of friction." The angle of repose $\Phi(\tan \Phi=F / N)$ is the angle at which the plane must be tilted before the object will move from its own weight. The following table of coefficients was compiled by Rankine from the results of General Morin and other authorities and is sufficient for ordinary purposes.

| Material | $f$ | 1/f | ¢ |
| :---: | :---: | :---: | :---: |
| Wood on wood, dry.. | .25-.50 | 4.00-2.00 | 14.0-26.5 |
| Metals on oak, dry... | . .20 - 60 | $\xrightarrow{5.00} 2$ | ${ }_{26.5-31.0}^{11.5}$ |
| "، " "،, dry | .24-.26 | 4.17-3.85 | 13.5-14.5 |
| soapy | . 20 | 5.00 |  |
| " elm, dry. | .20-. 25 | 5.00-4.00 | 11.5-14.0 |
| Hemp on oak, dry | . 53 | 1.89 | 28.0 |
| " " wet | . 33 | 3.00 | 18.5 |
| Leather on oak. | .27-. 38 | 3.70-2.86 | 15.0-19.5 |
| "/ metals, dry. | . 56 | 1.79 | 29.5 |
| " | . 36 | 2.78 | 20.0 |
| " " greasy | . 23 | 4.35 | 13.0 |
| " " " oily | 15 | 6.67 | 8.5 |
| Metals on metals, dry. | .15-. 20 | 6.67-5.00 | 8.5-11.5 |
| "* " ${ }^{\text {" }}$ wet.............. |  | 3.33 | 16.5 |
| Smooth surfaces, occasionally greased | . $07-.08$ | 14.3-12.50 | 4.0-4.5 |
| ". continually greased. | . 05 | 20.00 | 3.0 |
| " best results. | .03-.036 | 33.3-27.6 | 1.75-2.0 |
| Steel on agate, dry | . 20 | 5.00 | 11.5 |
| " " ${ }^{\text {c }}$ oiled. | . 107 | 9.35 | 6.1 |
| Iron on stone. | . $30-.70$ | 3.33-1.43 | 16.7-35.0 |
| Wood on stone. | About 40 | 2.50 | 22.0 |
| Masonry on brick work, dry | .60-. 70 | 1.67-1.43 | 33.0-35.0 |
| "" " " damp mortar | . 74 | 1.35 | 36.5 |
| " dry clay | . 51 | 1.96 | 27.0 |
| " moist clay | . 33 | 3.00 | 18.25 |
| Earth on earth. | .25-1.00 | 4.00-1.00 | 14.0-45.0 |
| " " dry sand, clay, and mixed earth. | . $38-.75$ | 2.63-1.33 | 21.0-37.0 |
| " " damp clay | 1.00 | 1.00 | 45.0 |
| " " wet clay. | . 31 | 3.23 | 17.0 |
| " " " shingle and gravel | .81-1.11 | 1.23-. 9 | 39.0-48.0 |

## TABLE 339.-DYNAMIC PRESSURE AT DIFFERENT AIR SPEEDS

The force on a body moving through a fluid may be expressed in the form

$$
F=C_{F} q A
$$

where $F$ is the force, $C_{F}$ a nondimensionai force coefficient, $q$ the dynamic pressure ( $q=$ $\frac{1}{2} \rho V^{2}$, definition), and $A$ an area. In general, the value of the coefficient $C_{F}$ is dependent on several nondimensional parameters. When the medium is air, $C_{F}$ depends on the Reynolds number $\frac{V l p}{\eta}$, the Mach number $\frac{V}{a}$, the body shape and attitude to the relative wind, the relative surface roughness, and the degree of turbulence of the air stream. The quantity $\rho$ denotes the fluid density, $V$ the velocity of the body relative to the fluid, $\eta$ the coefficient of fluid viscosity, $l$ a linear dimension of the body fixing the scale, and $a$ the speed of sound in the ambient fluid.

The table gives values of dynamic pressure $q$ for a wide range of speeds. In conjunction with the values of the force coefficient in subsequent tables, this table can be used for computation of lift, drag, and moment under specified conditions. The values in the table are computed for standard air density: dry air, normal $\mathrm{CO}_{2}$ content, $15^{\circ} \mathrm{C}$, one atmosphere. Standard air density is $0.12497 \frac{\text { metric slugs }}{\mathrm{m}^{8}}$ or $0.002378 \frac{\mathrm{slugs}}{\mathrm{ft}^{3}}$. For standard gravity, the weight of one metric slug (MKS) is 9.807 kilograms and the weight of one slug is 32.174 pounds. For other densities the values must be multiplied by the ratio of the actual density to the standard density.

[^153]
## (continued)

TABLE 339.-DYNAMIC PRESSURE AT DIFFERENT AIR SPEEDS (concluded)

| Air speed $\mathrm{m} / \mathrm{sec}$ | Dynamic pressure, $q$ $\mathrm{kg} / \mathrm{m}^{2}$ | Air speed $\mathrm{m} / \mathrm{sec}$ | Dynamic pressure, $q$ $\mathrm{kg} / \mathrm{m}^{2}$ | Air speed $\mathrm{m} / \mathrm{sec}$ | Dynamic pressure, $q$ $\mathrm{kg} / \mathrm{m}^{2}$ | Air speed $\mathrm{m} / \mathrm{sec}$ | Dynamic pressure, $q$ $\mathrm{kg} / \mathrm{m}^{2}$ | Air speed $\mathrm{m} / \mathrm{sec}$ | Dynamic pressure, $q$ $\mathrm{kg} / \mathrm{m}^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | . 0625 | 12 | 8.998 | 35 | 76.54 | 85 | 451.4 | 170 | 1806 |
| 2 | . 2499 | 14 | 12.25 | 4 C | 99.98 | 90 | 506.1 | 180 | 2024 |
| 3 | . 5624 | 16 | 16.00 | 45 | 126.5 | 95 | 563.9 | 190 | 2256 |
| 4 | . 9998 | 18 | 20.24 | 50 | 156.2 | 100 | 624.8 | 200 | 2499 |
| 5 | 1.562 | 20 | 24.99 | 55 | 189.0 | 110 | 756.1 | 250 | 3905 |
| 6 | 2.249 | 22 | 30.24 | 60 | 224.9 | 120 | 899.8 | 300 | 5624 |
| 7 | 3.062 | 24 | 35.99 | 65 | 264.0 | 130 | 1056.0 | 350 | 7654 |
| 8 | 3.999 | 26 | 42.24 | 70 | 306.2 | 140 | 1225 | 400 | 9998 |
| 9 | 5.061 | 28 | 48.99 | 75 | 351.5 | 150 | 1406 | 450 | 12653 |
| 10 | 6.248 | 30 | 56.24 | 80 | 399.9 | 160 | 1600 | 500 | 15621 |
| Air speed $\mathrm{ft} / \mathrm{sec}$ | Dynamic pressure, $q$ $\mathrm{lb} / \mathrm{ft}^{2}$ | Air speed $\mathrm{ft} / \mathrm{sec}$ | Dynamic pressure, $q$ $\mathrm{lb} / \mathrm{ft}^{2}$ | $\begin{gathered} \text { Air } \\ \text { speed } \\ \mathrm{ft} / \mathrm{sec} \end{gathered}$ | Dvnamic pressure, $q$ $\mathrm{lb} / \mathrm{ft}^{2}$ | Air speed $\mathrm{ft} / \mathrm{sec}$ | Dynamic pressure, $q$ $\mathrm{lb} / \mathrm{ft}^{2}$ | Air speed $\mathrm{ft} / \mathrm{sec}$ | Dynamic pressure, $q$ $\mathrm{lb} / \mathrm{ft}^{2}$ |
| 1 | . 0012 | 20 | . 4756 | 120 | 17.12 | 220 | 57.55 | 600 | 428.0 |
| 2 | . 0048 | 30 | 1.0701 | 130 | 20.09 | 230 | 62.90 | 650 | 502.4 |
| 3 | . 0107 | 40 | 1.902 | 140 | 23.30 | 240 | 68.49 | 700 | 582.6 |
| 4 | . 0190 | 50 | 2.972 | 150 | 26.75 | 250 | 74.31 | 750 | 668.8 |
| 5 | . 0297 | 60 | 4.280 | 160 | 30.44 | 300 | 107.01 | 800 | 761.0 |
| 6 | . 0428 | 70 | 5.826 | 170 | 34.36 | 350 | 145.6 | 850 | 859.0 |
| 7 | . 0583 | 80 | 7.610 | 180 | 38.52 | 400 | 190.2 | 900 | 963.1 |
| 8 | . 0761 | 90 | 9.631 | 190 | 42.92 | 450 | 240.8 | 950 | 1073 |
| 8 | . 0963 | 100 | 11.890 | 200 | 47.56 | 500 | 297.2 | 1000 | 1189 |
| 10 | . 1189 | 110 | 14.39 | 210 | 52.43 | 550 | 359.7 | 1500 | 2675 |

TABLE 340.-FORCES ON THIN FLAT PLATES AT ANGLES TO THE WIND (FIG. 6)

For plates at angles to the wind (angle of attack, a) the force is usually resolved into components at right angles and parallel to the direction of the relative wind. The components, termed the lift and drag, respectively, are expressed in the form of coefficients, the forces being divided by the product of the dynamic pressure and the area of the plate (not the projected area on a plane normal to the wind). The ratio of the distance between the leading edge and the center of pressure to the chord length is called the center of pressure coefficient, $C P$. The center of pressure is defined as the intersection of the line of action of the resultant force, $F$, with the plate. The forces on a plate vary with "aspect ratio," a term defined for a rectangular plate as the ratio of the span to the chord length.

The lift ( $C_{L}$ ), drag ( $C_{D}$ ), and center of pressure coefficients ( $C P$ ) are given as functions of angle of attack a for thin plates of aspect ratio 1,3 , and 6.


Fig. 6.-The lift coefficient $\left(C_{L}\right)$, the drag coefficient $\left(C_{D}\right)$, and the center of pressure $(C P)$ for thin plates for aspect ratios 1,3 , and 6 , as a function of the angle $a$ with the wind. (See small figure in upper center.) $D=C_{D} A q, L=C_{L} A q, X=C P \times c$.
(continued) (FIG. 6) (concluded)

| Authority ${ }^{131}$ | Conditions of experiments |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Aspect ratio 1 |  |  |  | Aspect ratio 3 |  |  |  | Aspect ratio 6 |  |  |  |
|  | 1 | 2 | 3 | 4 | 1 | 3 | 5 | 1 | 3 | 6 | 6 a | 7 |
| Span, cm | 25 | 30.5 | 12 | 12 | 45 | 7.6 | 36 | 90 | . 72 | 30.5 | 30.5 | 45.7 to 91.4 |
| Chord, cm | 25 | 30.5 | 12 | 12 | 15 | 2.5 | 12 | 15 | 12 | 5.08 | 5.08 | 7.6 to 15.2 |
| Thickness, cm | . 3 | . 32 | . 17 |  | . 3 | . 025 | . 17 | . 3 | . 17 | . 117 | . 129 |  |
| Tunnel diam., cm | 150 | $\sim$ | 200 | 120 | 150 | 60 | 200 | 150 | 200 | 137 | 137 | 152.4 |
| Reynolds No. $\times 10^{-3}$ | 210 | 382 | 55 | 42 | 126 | 10 | 55 | 126 | 55 | 64 | 64 | 153 |

[^154]
## TABLE 340A.-VALUES OF DRAG COEFFICIENT $C_{D}$ FOR FLAT PLATES OF DIFFERENT ASPECT RATIO NORMAL TO THE WIND ( $\alpha=90^{\circ}$ )

Values of $C_{D}$ for circular disks are practically the same as for a square plate.

| Ispect ratio | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | $\infty$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $C_{D}$ | 1.12 | 1.18 | 1.22 | 1.24 | 1.26 | 1.28 | 1.30 | 1.32 | 2.00 |

## TABLE 340B.-FORCES ON NONROTATING CIRCULAR CYLINDERS (FIG. 7) ${ }^{132}$

The drag coefficient $C_{D}$ for cylinders whose axes are perpendicular to the relative wind, the area $A$ being taken as the product of the length $L$ and diameter $d$, depends to a marked degree on the aspect ratio $\frac{L}{d}$, the Reynolds number $R$, and the Mach number $M$. The figure shows the variation of the drag coefficient $C_{D}$ with $R$ for cylinders of infinite aspect ratio at very low Mach numbers. The drag coefficient $C_{D}$ varies with Mach number in a manner quite similar to that of the sphere on Table 340C (figures 8 and 10).


Fig. 7.-The drag coefficient $C_{D}$ as a function of the Reynolds number $R$ at low Mach numbers for cylinders of infinite aspect ratios with axes perpendicular to the wind.

Drag $=C_{D} A q$, Reynolds number, $R=\frac{V d \rho}{\eta}$, Mach number, $M=\frac{V}{a}$. For $q$ see Table 339, $V=$ air speed, $\rho=$ air density, $\eta=$ coefficient of air viscosity.

[^155]The variation of $C_{n}$ with aspect ratio for Reynolds number of 80,000 is as follows.

| Aspect ratio $\frac{L}{d}$ | 1 | 2 | 3 | 5 | 10 | 20 | 40 | $\infty$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $C_{D}$ |  | .63 | .69 | .75 | .75 | .83 | .92 | 1.00 | 1.20 |

If the axis of the cylinder is inclined to the wind direction, the force remains approximately at right angles to the axis of the cylinder, its magnitude falling off approximately as the square of the sine of the angle of the axis to the wind.

## TABLE 340C.-FORCES ON SPHERES (FIGS. 8-10) ${ }^{133}$

For spheres, the linear dimension $l$ is taken as the diameter of the sphere $d$ and the area $A$ as $\frac{\pi d^{2}}{4}$. For values of Reynolds number between 80,000 and 400,000 at low values of Mach number the value of the drag coefficient $C_{D}$, depends in large measure on the turbulence of the air stream. As the Reynolds number is increased in this range the drag coefficient of the sphere and the pressure coefficient at the rear of the sphere decreaserapidly. The pressure coefficient is equal to the ratio of the difference between frce stream stagnation pressure and local static pressure to the dynamic pressure $q$. The Reynolds number at which the pressure coefficient at the rear of the sphere is 1.22 is defined as the critical Reynolds number, $R_{c r}$. This value of pressure coefficient corresponds very nearly to $C_{D}=3$. The value of $R_{c r}$ represented by point $d$ in the figure is considered to be typical of turbulence-free air.


Fig. 8.-The drag coefficient $C_{D}$ on spheres as a function of the Reynolds number.

$$
\text { Drag, } D=C_{D} A q R=\frac{V d \rho}{\eta}
$$

Sphere tests in wind tunnels indicate different values of $R_{\text {cr }}$ for different sphere sizes. Correlation of the data may be obtained if values of $\frac{\sqrt{u^{2}}}{V}\left(\frac{d}{L}\right)^{t}=\left(K^{\circ}\right)$ are plotted as a function of $R_{c r}$. The value $\sqrt{u^{2}}$ is the root-mean-square of the fluctuation velocity in the direction of the relative wind, $l$ the velocity of the relative wind, $d$ the sphere diameter, and $L$ is the scale of the turbulence as defined in the reference. The figure shows a correlation $(K)$ obtained with two sizes of spheres and several values of $L$.

[^156]TABLE 340C.-FORCES ON SPHERES (FIGS. 8-10) (concluded)


Fig. 9.-The value of $\frac{\sqrt{\overline{u^{2}}}}{V}\left(\frac{d}{L}\right)^{\frac{1}{3}}=K$ plotted as a function of the critical Reynolds number, $R_{\text {cr }}$.

At Mach numbers greater than about 0.3 the drag coefficient $C_{D}$ depends on the values of both Reynolds number and Mach number.


Fig. 10.-The drag coefficient for a sphere as a function of the Reynolds number for several Mach numbers.

The values of the drag coefficients in this table are based on the area of the projection of the body on a plane normal to the wind direction. Where this projection is a circle, the diameter is used as the linear dimension $l$ in the Reynolds number. Where the projection is rectangular, the shortest side of the rectangle is taken as $l$.

| Body | $C_{D}$ | Reynolds number |
| :---: | :---: | :---: |
| Streamline bodies of revolution | .05-. 06 | 3,000,000 |
| Rectangular prism $1 \times 1 \times 5$ normal to $1 \times 5$ face | 1.56 | 180,000 |
| Rectangular prism $1 \times 1 \times 5$, long axis perpendicular to the relative wind and $1 \times 5$ face at $45^{\circ}$ | . 92 | 254,000 |
| Automobile | . 78 | $\left[\begin{array}{c} \text { about } \\ 300,000 \end{array}\right]$ |
| Cone, angle $60^{\circ}$, point to wind, solid. | . 51 | $\left[\begin{array}{l} \text { about } \\ 270,000 \end{array}\right]$ |
| Cone, angle $30^{\circ}$, point to wind, solid. | . 34 | 270,000 |
| Hemispherical cup, open back....... | . 41 | 100,000 |
| Hemispherical cup, open front | 1.40 | 100,000 |
| Sphero-conic body, cone $20^{\circ}$ point forward | . 16 | 135,000 |
| Sphero-conic body, cone $20^{\circ}$ point to rear. | . 09 | 135,000 |
| Cylinder 120 cm long, spherical ends with axis parallel to the relative wind. | . 19 | 100,000 |

## TABLE 341A.-SKIN FRICTION ON FLAT PLATES (FIGS. 11, 12) ${ }^{134}$

If the flat plate is in a uniform stream of fluid and the flow is parallel to the plate the skin friction coefficient, $C_{f}$, is dependent mainly on the Reynolds number, $R=\frac{V L \rho}{\eta}$. The skin friction coefficient $C_{t}=\frac{D_{t}}{q L}$ where $D_{t}$ is the friction drag per unit width of one side of the plate, $q$ the dynamic pressure (see Table 339), and $L$ the length from the leading edge of the plate.
For laminar flow

$$
\begin{equation*}
C_{t}=\frac{1.328}{\sqrt{R}} \tag{Blasius}
\end{equation*}
$$

For turbulent flow

$$
\begin{equation*}
C_{t}=\frac{0.455}{\left(\log _{10} R\right)^{2.58}} \tag{Schlichting}
\end{equation*}
$$

The Reynolds number for transition from laminar to turbulent flow depends on the roughness of the plate and the turbulence of the airstream.

The figure shows the variation of the skin friction $\left(C_{f}\right)$ with $R$ for laminar and turbulent flow.

[^157](continued)

TABLE 341A.-SKIN FRICTION ON FLAT PLATES (FIGS. 11, 12) (continued)


Fig. 11.-A $\log -\log$ plot of the skin-friction coefficient $C_{f}$ on a flat plate as a function of the Reynolds number for laminar and turbulent flow.

The local skin-friction coefficient $\frac{\tau_{0}}{2 q}$ may be approximated by a power function of the Reynolds number based on the momentum thickness, $R_{\ominus}=\frac{V \Theta \rho}{\eta}$. When the boundary layer is laminar

$$
\frac{\tau_{0}}{2 q}=\frac{0.2205}{R_{\ominus}}
$$

When the boundary layer is turbulent

$$
\frac{\tau_{0}}{2 q}=\frac{1}{\left[2.5 \log _{e} \frac{R_{\theta}}{2.5\left(1-5 \sqrt{\left.\tau_{0} / 2 q\right)}\right.}+5.5\right]^{2}},
$$

The momentum thickness

$$
\theta=\int_{0}^{\delta} \frac{u}{V}\left(1-\frac{u}{V}\right) \mathrm{dy}
$$

where $u$ is the local velocity inside the boundary layer, $V$ the local velocity outside the boundary layer, and $\delta$ the boundary-layer thickness. The local skin-friction coefficient is plotted against Reynolds number for the case of a turbulent boundary layer.

> (continued)

TABLE 341A.-SKIN FRICTION ON FLAT PLATES (FIGS. 11, 12) (concluded)


Fig. 12.-The local skin-friction coefficient on a flat plate plotted against the Reynolds number for a turbulent boundary layer.

## TABLE 342.-STANDARD ATMOSPHERE ${ }^{135}$

Standard atmospheric values are given up to altitudes of 65,000 feet, and quantities that have been found to be of use in the interpretation of airspeed and related factors are included (Table 343). These quantities are the pressure $p$ in pounds per square foot, the pressure $p$ in inches of water, the speed of sound $a$, the coefficient of viscosity $\eta$, and the kinematic viscosity $\nu$. The values for the coefficient of viscosity $\eta$ and the kinematic viscosity $\nu$ are not standard values since a standardization of air viscosity has not been agreed upon as yet. The values listed for $\eta$ and $\nu$ are believed to be sufficiently accurate, however, to be useful in calculations requiring viscosity of air. The coefficient of viscosity $\eta$ was computed from the formula

$$
\eta=\frac{2.318}{10^{8}} \frac{T^{3 / 2}}{T+216} .
$$

The kinematic viscosity of air $\nu$ was obtained from the definition $\nu=\frac{\eta}{\rho}$. The quantity $1 / \sqrt{\sigma}$ is given to facilitate the computation of the true airspeed $V$ from the equivalent airspeed $V_{0}$.

$$
V=\frac{1}{V_{\sigma}} V_{0}
$$

The speed of sound in miles per hour is computed from $a=33.42 \sqrt{T}$ where $T$ is the temperature in degrees Fahrenheit absolute. A value of $\gamma=1.4$ was assumed to hold throughout the temperature range.

The values of the standard atmosphere are based upon the following values:

$$
\text { Sea-level pressure } \begin{aligned}
\rho_{0} & =29.921 \mathrm{inHg} \\
& =407.1 \mathrm{inH}_{2} \mathrm{O} \\
& =2116.2 \mathrm{lb}^{\prime} / \mathrm{ft}^{2}
\end{aligned}
$$

Sea-level temperature $t_{0}=59^{\circ} \mathrm{F}$
Sea-level absolute temperature $T_{0}=518.4^{\circ} \mathrm{F}$ abs
Sea-level density $\rho_{0}=0.002378$ slug $/ \mathrm{ft}^{3}$
Gravity $g=32.1740 \mathrm{ft} / \mathrm{sec}^{2}$
Temperature gradient $\frac{d T}{d h}=0.00356617^{\circ} \mathrm{F} / \mathrm{ft}$
The altitude of the lower limit of the isothermal atmosphere $=35,332$ it Specific weight of mercury at $32^{\circ} \mathrm{F}=848.7149 \mathrm{lb} / \mathrm{ft}^{\mathrm{a}}$
Specific weight of water at $59^{\circ} \mathrm{F}=62.3724 \mathrm{lb} / \mathrm{ft}^{3}$

[^158]Up to the lower limit of the isothermal atmosphere ( $-67^{\circ} \mathrm{F}$ corresponding to $35,332 \mathrm{ft}$ ) the temperature is assumed to decrease linearly according to the equation

$$
T=T_{0}-\frac{d T}{d h} \mathrm{~h}
$$

Further, the atmosphere is assumed to be a dry perfect gas that obeys the laws of Charles and Boyle, so that the mass density corresponding to the pressure and temperature is

$$
\rho=\rho_{0} \frac{p}{p_{0}} \frac{T_{0}}{T}
$$

The pressure and altitude are related by

$$
\mathrm{h}=\frac{p_{0}}{\rho_{0} g} \frac{T_{m}}{T_{0}} \log e \frac{p_{0}}{p} .
$$

The harmonic mean temperature $T_{m}$ is given by

$$
T_{\mathrm{m}}=\frac{\Sigma \Delta h}{\sum \frac{\Delta h}{T_{a v}}}=\frac{\Delta h_{1}+\Delta h_{2}+\cdots}{\frac{\Delta h_{1}}{T_{a v 1}}+\frac{\Delta h_{2}}{T_{a v 2}}+\cdots}
$$

where $T_{a v 1}, T_{a v 2}, \ldots$ are the average temperatures for the altitude increments $\Delta h_{1}, \Delta h_{2}, \ldots$
The NACA Special Subcommittee on the Upper Atmosphere, at a meeting on June 24, 1946, resolved that a tentative extension of the standard atmosphere from 65,000 to 100,000 feet be based upon a constant composition of the atmosphere and an isothermal temperature which are the same as standard conditions at 65,000 feet. This tentative extended isothermal region (Table 344) ends at 32 kilometers (approximately $105,000 \mathrm{ft}$ ). It is possible that as results of higher altitude temperature soundings become available and the standard atmosphere is extended to very high altitudes the present recommendations may be modified.
The Subcommittee also recommended that the values of temperature given in the following table be considered as maximum and minimum values occurring for the given altitudes with the variations between the specified points to be linear:

| $\begin{aligned} & \text { Altitude } \\ & (\mathrm{km}) \end{aligned}$ | Temperature $\underbrace{\circ} \mathrm{C}$ abs) |  |
| :---: | :---: | :---: |
|  | Minimum | Maximum |
| 20 | 180 | 250 |
| 25 |  | 250 |
| 45 | 200 | 380 |

A tentative extension of the standard atmosphere computed from the equations using the recommended isothermal temperature and constant gravity altitudes from 65,000 to 100,000 feet are included in the table. Calculations have been made ${ }^{185}$ by assuming that the acceleration of gravity varies inversely as the square of the distance from the center of the earth. Up to 100,000 feet this assumption does not greatly affect the tabulated values.

| Altitude, h ft | Pressure, p |  |  | $\begin{gathered} \text { Density } \\ \rho \\ \text { slugs } / \mathrm{ft}^{3} \end{gathered}$ | Density ratio $\sigma=\frac{\rho}{\rho_{10}}$ | $\frac{1}{\overline{\sqrt{\sigma}}}$ | Tem-perature, <br> ${ }^{\circ} \mathrm{F}$ abs | Speed of sound $\mathrm{mi} / \mathrm{hr}$ | Coefficient of viscosity,$\frac{\operatorname{slugs}}{\mathrm{ft}-\mathrm{sec}}$ | Kinematic viscosity,$\mathrm{ft}^{2} / \mathrm{sec}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{lb} / \mathrm{ft}^{2}$ | in $\mathrm{H}_{2} \mathrm{O}$ | inHg |  |  |  |  |  |  |  |
| 0 | 2116 | 407.1 | 29.92 | . 002378 | 1.0000 | 1.000 | 518.4 | 760.9 | $3.725 \times 1$ | $0^{-7} 1.566 \times 10^{-4}$ |
| 2,000 | 1968 | 378.5 | 27.82 | . 002242 | . 9428 | 1.030 | 511.2 | 755.7 | 3.685 | 1.644 |
| 4,000 | 1828 | 351.6 | 25.84 | . 002112 | . 8881 | 1.061 | 504.1 | 750.4 | 3.644 | 1.725 |
| 6,000 | 1696 | 326.2 | 23.98 | . 001988 | . 8358 | 1.094 | 497.0 | 745.1 | 3.602 | 1.812 |
| 8,000 | 1572 | 302.4 | 22.22 | . 001869 | . 7859 | 1.128 | 489.9 | 739.7 | 3.561 | 1.905 |
| 10,000 | 1455 | 279.9 | 20.58 | . 001756 | . 7384 | 1.164 | 482.7 | 734.3 | 3.519 | 2.004 |
| 12,000 | 1346 | 258.9 | 19.03 | . 001648 | . 6931 | 1.201 | 475.6 | 728.8 | 3.476 | 2.109 |
| 14,000 | 1243 | 239.1 | 17.57 | . 001545 | . 6499 | 1.240 | 468.5 | 723.4 | 3.434 | 2.223 |
| 16,000 | 1146 | 220.6 | 16.21 | . 001448 | . 6088 | 1.282 | 461.3 | 718.7 | 3.391 | 2.342 |
| 18,000 | 1056 | 203.2 | 14.94 | . 001355 | . 5698 | 1.325 | 454.2 | 712.2 | 3.348 | 2.471 |
| 20,000 | 972.1 | 187.0 | 13.75 | . 001267 | . 5327 | 1.370 | 447.1 | 706.6 | 3.305 | 2.608 |
| 22,000 | 893.3 | 171.9 | 12.63 | . 001183 | . 4974 | 1.418 | 439.9 | 701.1 | 3.261 | 2.756 |
| 24,000 | 819.8 | 157.7 | 11.59 | . 001103 | . 4640 | 1.468 | 432.8 | 695.3 | 3.217 | 2.916 |
| 26,000 | 751.2 | 144.5 | 10.62 | . 001028 | . 4323 | 1.521 | 425.7 | 689.5 | 3.173 | 3.086 |
| 28,000 | 687.4 | 132.2 | 9.720 | . 000957 | . 4023 | 1.577 | 418.5 | 683.7 | 3.128 | 3.268 |
| 30,000 | 628.0 | 120.8 | 8.880 | . 000889 | . 3740 | 1.635 | 411.4 | 677.9 | 3.083 | 3.468 |
| 32,000 | 572.9 | 110.2 | 8.101 | . 000826 | . 3472 | 1.697 | 404.3 | 672.0 | 3.038 | 3.678 |
| 34,000 | 521.7 | 100.4 | 7.377 | . 000765 | . 3218 | 1.763 | 397.2 | 666.0 | 2.992 | 3.911 |
| 35,332 | 489.8 | 94.24 | 6.926 | . 000727 | . 3058 | 1.808 | 392.4 | 662.0 | 2.962 | 4.073 |
| 36,000 | 474.4 | 91.31 | 6.711 | . 000705 | . 2963 | 1.837 | 392.4 | 662.0 | 2.962 | 4.204 |
| 38,000 | 431.1 | 82.97 | 6.098 | .000640 | 2692 | 1.927 | 392.4 | 662.0 | 2.962 | 4.625 |
| 40,000 | 391.9 | 75.44 | 5.544 | . 000582 | . 2448 | 2.021 | 392.4 | 662.0 | 2.962 | 5.089 |
| 42,000 | 356.2 | 68.56 | 5.038 | . 000529 | . 2225 | 2.120 | 392.4 | 662.0 | 2.962 | 5.599 |
| 44,000 | 323.7 | 62.29 | 4.578 | . 000480 | . 2021 | 2.224 | 392.4 | 662.0 | 2.962 | 6.161 |
| 46,000 | 294.2 | 56.63 | 4.162 | . 000437 | . 1838 | 2.333 | 392.4 | 662.0 | 2.962 | 6.778 |
| 48,000 | 267.4 | 51.46 | 3.782 | . 000397 | . 1670 | 2.447 | 392.4 | 662.0 | 2.962 | 7.459 |
| 50,000 | 243.1 | 46.78 | 3.438 | . 000361 | . 1518 | 2.567 | 392.4 | 662.0 | 2.962 | 8.206 |
| 52,000 | 220.9 | 42.52 | 3.124 | . 000328 | . 1379 | 2.692 | 392.4 | 662.0 | 2.962 | 9.028 |
| 54,000 | 200.8 | 38.64 | 2.840 | . 000298 | 1.1254 | 2.824 | 392.4 | 662.0 | 2.962 | 9.933 |
| 56,000 | 182.5 | 35.12 | 2.581 | . 000271 | . 1140 | 2.962 | 392.4 | 662.0 | 2.962 | 10.93 |
| 58,000 | 165.9 | 31.92 | 2.346 | . 000246 | . 1036 | 3.107 | 392.4 | 662.0 | 2.962 | 12.02 |
| 60,000 | 150.8 | 29.01 | 2.132 | . 000224 | . 09415 | 3.259 | 392.4 | 662.0 | 2.962 | 13.23 |
| 62,000 | 137.1 | 26.37 | 1.938 | . 000203 | . 08557 | 3.419 | 392.4 | 662.0 | 2.962 | 14.56 |
| 64,000 | 124.6 | 23.96 | 1.761 | . 000185 | . 07777 | 3.586 | 392.4 | 662.0 | 2.962 | 16.02 |
| 65,000 | 118.7 | 22.85 | 1.679 | . 000176 | . 07414 | 3.672 | 392.4 | 662.0 | 2.962 | 16.80 |

[^159]TABLE 344.-PROPERTIES OF THE TENTATIVE STANDARD-ATMOSPHERE EXTENSION

| $\begin{gathered} \text { Altitude } \\ \mathrm{h} \\ \mathrm{ft} \end{gathered}$ | Pressure, p |  |  | $\begin{aligned} & \text { Density, } \\ & \rho \\ & \text { slugs } / \mathrm{ft}^{3} \end{aligned}$ | Density ratio. $\sigma=\frac{\rho}{\rho_{01}}$ | $\frac{1}{\sqrt{\sigma}}$ | Tem-perature, <br> ${ }^{\circ} \mathrm{F}$ abs | Speed of sound, $\mathrm{mi} / \mathrm{hr}$ | $\begin{gathered} \text { Coefficient } \\ \text { of } \\ \text { viscosity, } \\ \eta \\ \text { slugs } \\ \mathrm{ft}-\mathrm{sec} \end{gathered}$ | Kinematic viscosity, $\mathrm{ft}^{2} / \mathrm{sec}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | lb/ft ${ }^{2}$ | in $\mathrm{H}_{2} \mathrm{O}$ | inHg |  |  |  |  |  |  |  |
| 65,000 | 118.7 | 22.85 | 1.679 | . 000176 | . 07414 | 3.672 | 392.4 | 662.0 | $2.962 \times 10$ | $0^{-7} 16.80 \times 10^{-}$ |
| 70,000 | 93.53 | 17.99 | 1.322 | . 000139 | . 05839 | 4.138 | 392.4 | 662.0 | 2.962 | 21.33 |
| 75,000 | 73.66 | 14.17 | 1.042 | . 000109 | . 04599 | 4.663 | 392.4 | 662.0 | 2.962 | 27.09 |
| 80,000 | 58.01 | 11.16 | . 8202 | . 0000861 | . 03621 | 5.255 | 392.4 | 662.0 | 2.962 | 34.39 |
| 85,000 | 45.68 | 8.789 | . 6460 | . 0000678 | . 02852 | 5.921 | 392.4 | 662.0 | 2.962 | 43.67 |
| 90,000 | 35.97 | 6.921 | . 5086 | . 0000534 | . 02246 | 6.672 | 392.4 | 662.0 | 2.962 | 55.45 |
| 95,000 | 28.33 | 5.451 | . 4006 | . 0000421 | . 01769 | 7.519 | 392.4 | 662.0 | 2.962 | 70.41 |
| 100,000 | 22.31 | 4.293 | . 3156 | . 0000331 | . 01394 | 8.472 | 392.4 | 662.0 | 2.962 | 89.41 |

In high speed research, use is frequently made of the theoretical relationships existing between the Mach number and various flow parameters. Two types of flow are tabulated: isentropic flow and normal-shock flöw. Isentropic flow is generally valid for a subsonic or supersonic expanding flow and may be used for subsonic compression flow. Normal-shock How is valid for supersonic compression flow when the deviation of the flow through the shock is zero. Oblique-shock flow may be obtained from the normal-shock flow by superimposing a velocity tangential to the shock.
The assumption that air is a perfect gas with a value of $\gamma$ of 1.400 is valid for the conditions usually encountered in the subsonic and lower supersonic regions for normal stagnation conditions. For Mach numbers greater than about 4.0 or for unusual stagnation conditions, however, the behavior of air will depart appreciably from that of a perfect gas if the liquefaction condition is approached, and caution should be used in applying the results in the table at the higher Mach numbers.
The formulas for isentropic flow are:

$$
\begin{aligned}
\frac{p_{1}}{p_{0}} & =\left(1+\frac{\gamma-1}{2} M_{1}^{2}\right)^{\frac{\gamma}{1-\gamma}} \\
\frac{\rho_{1}}{\rho_{0}} & =\left(1+\frac{\gamma-1}{2} M_{1}^{2}\right)^{\frac{1}{1-\gamma}} \\
\frac{T_{1}}{T_{0}} & =\left(1+\frac{\gamma-1}{2} M_{1}^{2}\right)^{-1} \\
\frac{A_{c r}}{A_{1}} & =M_{1}\left(\frac{1+\frac{\gamma-1}{2}}{1+\frac{\gamma-1}{2} M_{1}^{2}}\right)^{\frac{\gamma+1}{2(\gamma-1)}} \\
\frac{c_{1}}{a_{0}} & =\left(1+\frac{\gamma-1}{2} M_{1}^{2}\right)^{-1} \\
V_{1} & =M_{1}\left(\frac{a_{1}}{a_{0}}\right) a_{0} \\
F_{c} & =\frac{2}{\gamma M_{1}^{2}}\left[\left(1+\frac{\gamma-1}{2} M_{1}^{2}\right)^{\frac{\gamma-1}{\gamma-1}}-1\right. \\
\phi & =\sin ^{-1}\left(\frac{1}{M_{1}}\right) \\
\nu & =\left(\frac{\gamma+1}{\gamma-1}\right)^{\frac{1}{2}} \cos ^{-1}\left[\frac{\gamma+1}{2\left(1+\frac{\gamma-1}{2} M_{1}^{2}\right)}\right]^{\frac{1}{2}}+\phi-90^{\circ},
\end{aligned}
$$

and the formulas for normal-shock flow are:

$$
\begin{aligned}
& \frac{p_{2}}{p_{1}}=\frac{2 \gamma}{\gamma+1} M_{1}^{2}-\frac{\gamma-1}{\gamma+1} \\
& \frac{p_{2}}{p_{0}}=\left(\frac{p_{2}}{p_{1}}\right)\left(\frac{p_{1}}{p_{0}}\right) \\
& \frac{p_{3}}{p_{2}}=\left(\frac{\gamma-1}{2} M_{2}{ }^{2}+1\right)^{\frac{\gamma}{\gamma-1}} \\
& \frac{p_{3}}{p_{0}}=\left(\frac{p_{3}}{p_{2}}\right)\left(\frac{p_{2}}{p_{0}}\right) \\
& M_{2}=\left[( \frac { \gamma + 1 } { 2 \gamma } ) ^ { 2 } \left(\frac{1}{\left.\left.M_{1}{ }^{2}-\frac{\gamma-1}{2 \gamma}\right)+\frac{\gamma-1}{2 \gamma}\right]^{3}} \$=\right.\right.\text {, }
\end{aligned}
$$

[^160]\[

$$
\begin{aligned}
& \frac{\rho_{2}}{\rho_{1}}=\left(\frac{M I_{1}}{M_{2}}\right)^{2}\left(\frac{p_{1}}{p_{2}}\right) \\
& \frac{V_{2}}{V_{1}}=\frac{\rho_{1}}{\rho_{2}}
\end{aligned}
$$
\]

where
$a=$ speed of sound in air.
$A=$ cross-sectional area of the stream tube.
$A_{\text {cr }}=$ cross-sectional area of the stream tube for $\mathrm{M}_{1}=1.0$.
$F_{c}=$ compressibility factor, increase in pressure above the static pressure set up in a tube whose open end is pointed into the relative wind divided by the dynamic pressure.
$M=$ Mach number $\left(\frac{V}{a}\right)$.
$\phi=$ Mach angle, degrees.
$p=$ absolute pressure.
$T=$ temperature, ${ }^{\circ} \mathrm{F}$ absolute.
$V=$ airspeed, feet per second, computed for $T_{0}=520^{\circ} \mathrm{F}$ absolute and $a_{0}=$ 1117.372 feet per second.
$\gamma=$ ratio of specific heats, taken as 1.400 .
$\nu=$ expansion angle required to change Mach number from 1.0 to $M_{1}$, degrees.
$\rho=$ mass density of air.
Subscripts:
$0=$ stagnation conditions before shock.
$1=$ air stream conditions before shock.
$2=$ air stream conditions behind shock.
$3=$ stagnation conditions behind shock.


Fig. 13.-Illustrating three types of flow.

$$
\begin{aligned}
& \text { 4 Goono } \\
& 4
\end{aligned}
$$

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\end{aligned}
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By suitably proportioning the thickness distribution over the chord of a plate, an airfoil may be derived around which the flow will adhere even when the angle of attack is large. Because the flow remains attached to the airfoil, high lift coefficients may be obtained with low drag coefficients.

The flow around a particular airfoil at a given angle of attack depends on the Reynolds number, $R$, the Mach number, $M$, and the degree of surface roughness. The main effect of increasing the Reynolds number is to change the maximum-lift coefficient and the minimum-drag coefficient. When the surface of the airfoil is made rough, simulating the surface of an actual airplane wing, the flow breaks away from the upper surface of the airfoil at a smaller angle of attack and therefore results in a considerably smaller value of maximum-lift coefficient. A rough surface increases the percentage of the chord over which the flow is turbulent and tends to make the drag coefficient much higher (see figure 11). As the Mach number is increased the variation of the local velocity from the stream velocity is increased.
On figure 14 are shown the force coefficients for two symmetrical NACA airfoils of infinite aspect ratio plotted against angle of attack, a, for a Reynolds number of $6 \times 10^{6}$. Methods exist (see Method for calculating wing characteristics by lifting-line theory using nonlinear section lift data, by James C. Sivells and Robert H. Neely, NACA TN No. 1269 , April 1947) for converting infinite aspect ratio data to finite wing characteristics. The force coefficients of a 21 -percent thick airfoil in the smooth condition and a 12 -percent thick airfoil in both the rough and smooth conditions are given.
Figure 15 shows the variation in the force coefficients with Mach number for a symmetrical 9 -percent thick airfoil at an angle of attack of $2^{\circ}$ and at Reynolds numbers from $.35 \times 10^{\text {a }}$ to $.75 \times 10^{\circ}$.

[^161]
## (continued)

TABLE 346A.-FORCES ON AIRFOILS AT ANGLES TO THE WIND (FIGS. 14, 15) (concluded)


Fig. 14.-Force coefficients for two symmetrical airfoils of infinite aspect ratio plotted against angle of attack, $a$, for Reynolds number $6 \times 10^{6}$.


Fig. 15.-The force coefficients, $C_{L}, C_{D}$, and $C P$, plotted against Mach number for a 9 -percent thick airfoil at an angle of attack of $2^{\circ}$ and Reynolds number from $.35 \times 10^{6}$ to $.75 \times 10^{6}$.

## TABLES 347-369.-DIFFFUSION, SOLUBILITY, SURFACE TENSION, AND VAPOR PRESSURE

## TABLE 347.-DIFFUSION OF AN AQUEOUS SOLUTION INTO PURE WATER

If $k$ is the coefficient of diffusion, $d S$ the amount of the substance which passes in the time $d t$, at the place $x$, through $q \mathrm{~cm}^{2}$ of a diffusion cylinder under the influence of a drop of concentration $d c / d x$, then

$$
d S=-k q \frac{d c}{d x} d t
$$

$k$ depends on the temperature and the concentration. $c$ gives the gram-molecules per liter. The unit of time is a day.

| Substance | $c$ | $\stackrel{t}{\circ}^{\circ} \mathrm{C}$ | $k$ |  | Substance | c | $\stackrel{t}{\circ}^{\circ} \mathrm{C}$ | $k$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bromine | . 1 | 12. | . 8 | Calcium | chloride | . 864 | 8.5 | . 70 |
| Chlorine | " | 12. | 1.22 |  |  | 1.22 | 9. | . 72 |
| Copper sulfate |  | 17. | . 39 | " | " | . 060 | 9. | . 64 |
| Glycerine | " | 10.14 | . 357 | " | " | . 047 | 9. | . 68 |
| Hydrochloric acid | " | 19.2 | 2.21 | Copper | sulfate | 1.95 | 17. | . 23 |
| Iodine | " | 12. | ( .5) |  |  | . 95 | 17. | . 26 |
| Nitric acid | " | 19.5 | 2.07 | " | " | . 30 | 17. | . 33 |
| Potassium chloride | " | 17.5 | 1.38 | " | " | . 005 | 17. | 47 |
| " hydroxide | " | 13.5 | 1.72 | Glycerin |  | 2/8 | 10.14 | . 354 |
| Silver nitrate |  | 12. | . 985 |  |  | 6/8 | 10.14 | . 345 |
| Sodium chloride | " | 15.0 | . 94 | " |  | 10/8 | 10.14 | . 329 |
| Urea | " | 14.8 | . 97 | " |  | 14/8 | 10.14 | . 30 C |
| Acetic acid | 2 | 13.5 | . 77 | Hydroc | hloric acid | 4.52 | 11.5 | 2.93 |
| Barium chloride | " | 8. | . 66 |  |  | 3.16 | 11. | 2.67 |
| Glycerine | " | 10.1 | 3.55 |  | " | . 945 | 11. | 2.12 |
| Sodium acetate | " | 12. | . 67 | " | " | . 387 | 11. | 2.02 |
| " chloride |  | 15.0 | . 94 |  | -" | . 250 | 11. | 1.84 |
| Urea . . ...... | " | 14.8 | . 969 | Magnes | ium sulfate | 2.18 | 5.5 | . 28 |
| Acetic acid | 1.0 | 12. | . 74 |  |  | . 541 | 5.5 | . 32 |
| Ammonia | " | 15.23 | 1.54 | " | ، | 3.23 | 10. | . 27 |
| Formic acid |  | 12. | . 97 | " | " | . 402 | 10. | . 34 |
| Glycerine - | " | 10.14 | . 339 | Potassi | um hydroxi | . 75 | 12. | 1.72 |
| Hydrochloric acid | " | 12. | 2.09 | " | " | . 49 | 12. | 1.70 |
| Magnesium sulfate | " | 7. | . 30 | " | " | . 375 | 12. | 1.70 |
| Potassium bromide | " | 10. | 1.13 | " | nitrate | 3.9 | 17.6 | . 89 |
| hydroxide | " | 12. | 1.72 | " | 仡 | 1.4 | 17.6 | 1.10 |
| Sodium chloride .... | " | 15.0 | . 94 | " | " | . 3 | 17.6 | 1.26 |
| " | " | 14.3 | . 964 | " | " | . 02 | 17.6 | 1.28 |
| hydroxide | " | 12. | 1.11 | " | sulfate | . 95 | 19.6 | . 79 |
| " iodide ... | " | 10. | . 80 | " | "، | . 28 | 19.6 | . 86 |
| Sugar ..... |  | 12. | . 254 | " | " | . 05 | 19.6 | . 97 |
| Sulfuric acid | " | 12. | 1.12 | Sil | . | . 02 | 19.6 | 1.01 |
| Zinc sulfate | " | 14.8 | . 236 | Silver | nitrate | 3.9 | 12. | . 535 |
| Acetic acid | 2.0 | 12. | . 69 | " |  | . 9 | 12. | . 88 |
| Calcium chloride |  | 10. | . 68 |  |  | . 02 | 12. | 1.035 |
| Cadmium sulfate |  | 19.04 | . 246 | Sodium | chloride | 2/8 | 14.33 | 1.013 |
| Hydrochloric acid |  | 12. | 2.21 | , | , | 4/8 | 14.33 | . 996 |
| Sodium iodide ... |  | 10. | . 90 | " | " | 6/8 | 14.33 | . 980 |
| Sulfuric acid | " | 12. | 1.16 | " | " | 10/8 | 14.33 | . 948 |
| Zinc acetate |  | 18.05 | . 210 |  | " | 14/8 | 14.33 | . 917 |
| "، " |  | . 04 | . 120 | Sulfuric | c acid | 9.85 | 18. | 2.36 |
| Acetic acid | 3.0 | 12. | . 68 |  | " | 4.85 | 18. | 1.90 |
| Potassium carbonate |  | 10. | . 60 | " | " | 2.85 | 18. | 1.60 |
| hydroxide | 4 | 12. | 1.89 | " | " | . 85 | 18. | 1.34 |
| Acetic acid . . . . . . . | 4.0 | 12. | . 66 | " | " | . 35 | 18. | 1.32 |
| Potassium chloride | " | 10. | 1.27 | " | " | . 005 | 18. | 1.30 |

Coefficients of diffusion of vapors in cgs units. The coefficients are for the temperatures given in the table and a pressure of 76 cmHg .

|  | Vapor | Temp. ${ }^{\circ} \mathrm{C}$ | $k$ for vapor diffusing into hydrogen | $\begin{gathered} k, \text { for vapor } \\ \text { diffusing into } \\ \text { air } \end{gathered}$ | $k$ : for vapor diffusing into carbon dioxide |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Acids: $\begin{array}{r}\text { F } \\ \text { A } \\ \text { I }\end{array}$ | Formic | . 0 | . 5131 | . 1315 | . 0879 |
|  |  | 65.4 | . 7873 | . 2035 | . 1343 |
|  | " | 84.9 | . 8830 | . 2244 | . 1519 |
|  | Acetic | . 0 | . 4040 | . 1061 | . 0713 |
|  | " | 65.5 | . 6211 | . 1578 | . 1048 |
|  | " . | 98.5 | . 7481 | . 1965 | . 1321 |
|  | Isovaleric | . 0 | . 2118 | . 0555 | . 0375 |
|  |  | 98.0 | . 3934 | . 1031 | . 0696 |
| Alcohols | : Methyl | . 0 | . 5001 | . 1325 | . 0880 |
|  |  | 25.6 | . 6015 | . 1620 | . 1046 |
|  | " | 49.6 | . 6738 | . 1809 | . 1234 |
|  | Ethyl | . 0 | . 3806 | . 0994 | . 0693 |
|  |  | 40.4 | . 5030 | . 1372 | . 0898 |
|  | " ${ }^{\text {c }}$ | 66.9 | . 5430 | . 1475 | . 1026 |
|  | Propyl | . 9 | . 3153 | . 0803 | . 0577 |
|  | " | 66.9 83.5 | . 48332 | . 1237 | . 0901 |
|  | Butyl | . 0 | . 2716 | . 0681 | . 0476 |
|  |  | 99.0 | . 5045 | . 1265 | . 0884 |
|  | Amyl | . 0 | . 2351 | . 0589 | . 0422 |
|  |  | 99.1 | . 4362 | . 1094 | . 0784 |
|  | Hexyl | . 0 | . 1998 | . 0499 | . 0351 |
|  |  | 99.0 | . 3712 | . 0927 | . 0651 |
| Benzene "، |  | . 0 | . 2940 | . 0751 | . 0527 |
|  |  | 19.9 | . 3409 | . 0877 | . 0609 |
|  |  | 45.0 | . 3993 | . 1011 | . 0715 |
| Carbon " | disulfide |  |  |  | . 0629 |
|  |  | . 19.9 | . 4255 | . 1015 | . 0726 |
| Esters: | Methyl acetate | . 0 | . 3277 | . 0840 | . 0557 |
|  |  | 20.3 | . 3928 | . 1013 | . 0679 |
|  | Ethyl " | . 0 | . 2373 | . 0630 | . 0450 |
|  |  | 46.1 | . 3729 | . 0970 | . 0666 |
|  | Methyl butyrate | ${ }^{0} 0$ | . 2422 | . 0640 | . 0438 |
|  |  | 92.1 | . 4308 | . 1139 | . 0809 |
|  | Ethyl |  | . 2238 | . 0573 | . 0406 |
|  | valerate | 96.5 | . 4112 | .1064 .0505 | . 0756 |
|  | " ، | 97.6 | . 3784 | . 0932 | . 0676 |
| Ether |  | . 0 | . 2960 | . 0775 | . 0552 |
|  |  | 19.9 | . 3410 | . 0893 | . 0636 |
| Water |  | . 0 | . 6870 | . 1980 | . 1310 |
|  |  | 49.5 | 1.0000 | . 2827 | . 1811 |
|  |  | 92.4 | 1.1794 | . 3451 | . 2384 |

## TABLE 349.-COEFFICIENTS OF DIFFUSION FOR VARIOUS GASES AND VAPORS



## TABLE 350.-DIFFUSION OF METALS INTO METALS

$\frac{d v}{d v}=k \frac{d^{2} v}{d v}$; where $x$ is the distance in direction of diffusion; $v$, the degree of concentration of the diffusing metal; $t$, the time; $k$, the diffusion constant $=$ the quantity of metal in grams diffusing through a $\mathrm{cm}^{2}$ in a day when unit difference of concentration $\left(\mathrm{g} / \mathrm{cm}^{8}\right)$ is maintained between two sides of a layer one cm thick.

| Diffusing metal | Dissolving metal | $\begin{aligned} & \text { Temper- } \\ & \text { ature } \end{aligned}{ }^{\circ} \mathrm{C}$ | ${ }^{k}$ | Diffusing metal | $\begin{aligned} & \text { Dis- } \\ & \text { solving } \\ & \text { metal } \end{aligned}$ | Temper- ature | k |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Gold | Lead | 555 | 3.19 | Platinum | Lead | 492 | 1.69 |
|  |  | . 492 | 3.00 | Lead | Tin | 555 | 3.18 |
| " . | " | .. 251 | . 03 | Rhodium | Lead | 550 | 3.04 |
| " . | " | 200 | . 008 | Tin | Mercury | y. 15 | 1.22 |
| " | " | 165 | . 004 | Lead |  | - 15 | 1.0 |
| " | . | . 100 | . 00002 | Zinc | " | - 15 | 1.0 |
| " | Bismut | . 555 | 4.52 | Sodium | " | . 15 | . 45 |
| , |  | . 5555 | 4.65 | Potassium | " | - 15 | . 40 |
| Silver |  | . 555 | 4.14 | Gold | " | . 15 | . 72 |

(Temperature variation)
The numbers give the number of grams of the anhydrous salt soluble in 1000 g of water at the given temperatures.

|  | Temperature ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Salt | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| $\mathrm{AgNO}_{3}$ | 1150 | 1600 | 2150 | 2700 | 3350 | 4000 | 4700 | 5500 | 6500 | 7600 | 9100 |
| $\mathrm{Al}_{2}\left(\mathrm{SO}_{4}\right)$ | 313 | 335 | 362 | 404 | 457 | 521 | 591 | 662 | 731 | 808 | 891 |
| $\mathrm{Al}_{2} \mathrm{~K}_{2}\left(\mathrm{SO}_{4}\right)_{4}$ | 30 |  |  | 84 |  |  | 248 |  |  |  | 1540 |
| $\mathrm{Al}_{2}\left(\mathrm{NH}_{4}\right)_{3}\left(\mathrm{SO}_{4}\right)_{4}$. | 26 | 45 | 66 | 91 | 124 | 159 | 211 | 270 | 352 |  |  |
| $\mathrm{B}_{2} \mathrm{O}_{3}$ | 11 | 15 | 22 |  | 40 |  | 62 |  | 95 |  | 157 |
| $\mathrm{BaCl}_{2}$ | 316 | 333 | 357 | 382 | 408 | 436 | 464 | 494 | 524 | 556 | 588 |
| $\mathrm{Ba}(\mathrm{NO}$ | 50 | 70 | 92 | 116 | 142 | 171 | 203 | 236 | 270 | 306 | 342 |
| $\mathrm{CaCl}_{3}$ | 595 | 650 | 745 | 1010 | 1153 |  | 1368 | 1417 | 1470 | 1527 | 1590 |
| $\mathrm{CoCl}_{2}$ | 405 | 450 | 500 | 565 | 650 | 935 | 940 | 950 | 960 |  | 1030 |
| CsCl | 1614 | 1747 | 1865 | 1973 | 2080 | 2185 | 2290 | 2395 | 2500 | 2601 | 2705 |
| $\mathrm{CsNO}_{3}$ | 93 | 149 | 230 | 339 | 472 | 644 | 838 | 1070 | 1340 | 1630 | 1970 |
| $\mathrm{Cs}_{2} \mathrm{SO}_{4}$ | 1671 | 1731 | 1787 | 1841 | 1899 | 1949 | 1999 | 2050 | 2103 | 2149 | 2203 |
| $\mathrm{Cu}\left(\mathrm{NO}_{3}\right)_{2}$ | 818 |  | 1250 |  | 1598 |  | 1791 |  | 2078 |  |  |
| $\mathrm{CuSO}_{4}$ | 149 |  |  | 255 | 295 | 336 | 390 | 457 | 535 | 627 | 735 |
| $\mathrm{FeCl}_{2}$ |  |  | 685 |  |  | 820 | - |  | 1040 | 1050 | 1060 |
| $\mathrm{Fe}_{2} \mathrm{Cl}_{8}$ | 744 | 819 | 918 |  |  | 3151 |  |  | 5258 |  | 5357 |
| $\mathrm{FeSO}_{4}$ | 156 | 208 | 264 | 330 | 402 | 486 | 550 | 560 | 506 | 430 |  |
| $\mathrm{HgCl}_{2}$ | 43 | 66 | 74 | 84 | 96 | 113 | 139 | 173 | 243 | 371 | 540 |
| KBr | 540 | - | 650 |  | 760 |  | 860 |  | 955 |  | 1050 |
| $\mathrm{K}_{2} \mathrm{CO}_{3}$ | 1050 |  |  | 1140 | 1170 | 1210 | 1270 | 1330 | 1400 | 1470 | 1560 |
| KCl | 285 | 312 | 343 | 373 | 401 | 429 | 455 | 483 | 510 | 538 | 566 |
| $\mathrm{KClO}_{3}$ | 33 | 50 | 71 | 101 | 145 | 197 | 260 | 325 | 396 | 475 | 560 |
| $\mathrm{K}_{2} \mathrm{CrO}_{4}$ | 589 | 609 | 629 | 650 | 670 | 690 | 710 | 730 | 751 | 771 | 791 |
| $\mathrm{K}_{2} \mathrm{Cr}_{2} \mathrm{O}_{7}$ | 50 | 85 | 131 |  | 292 |  | 505 |  | 730 |  | 1020 |
| $\mathrm{KHCO}_{3}$ | 225 | 277 | 332 | 390 | 453 | 522 | 600 |  |  |  |  |
| KI | 1279 | 1361 | 1442 | 1523 | 1600 | 1680 | 1760 | 1840 | 1920 | 2010 | 2090 |
| $\mathrm{KNO}_{3}$ | 133 | 209 | 316 | 458 | 639 | 855 | 1099 | 1380 | 1690 | 2040 | 2460 |
| KOH | 970 | 1030 | 1120 | 1260 | 1360 | 1400 | 1460 | 1510 | 1590 | 1680 | 1780 |
| $\mathrm{K}_{2} \mathrm{PtCl}_{8}$ | 7 | 9 | 11 | 14 | 18 | 22 | 26 | 32 | 38 | 45 | 52 |
| $\mathrm{K}_{2} \mathrm{SO}_{4}$ | 74 | 92 | 111 | 130 | 148 | 165 | 182 | 198 | 214 | 228 | 241 |
| LiOH | 127 | 127 | 128 | 129 | 130 | 133 | 138 | 144 | 153 |  | 175 |
| $\mathrm{MgCl}_{2}$ | 528 | 535 | 545 |  | 575 | -- | 610 | - - | 660 | - | 730 |
| MgSO4 .... (7aq) | 260 | 309 | 356 | 409 | 456 |  |  |  |  |  |  |
| " ${ }^{\text {c }}$....(6aq) | 408 | 422 | 439 | 453 |  | 504 | 550 | 596 | 642 | 689 | 738 |
| NH, Cl | 297 | 333 | 372 | 414 | 458 | 504 | 552 | 602 | 656 | 713 | 773 |
| $\mathrm{NH}_{4} \mathrm{HCO}_{3}$ | 119 1183 | 159 | 210 | 270 |  |  |  |  |  |  |  |
| $\mathrm{NH}_{4} \mathrm{NO}_{3}$ | 1183 |  |  | 2418 | 2970 | 3540? | 4300? | 5130? | 5800 | 7400 | 8710 |
| $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{SO}_{4}$ | 706 | 730 | 754 | 780 | 810 | 844 | 880 | 916 | 953 | 992 | 1033 |
| NaBr | 795 | 845 | 903 |  | 1058 | 1160 | 1170 |  | 1185 |  | 1205 |
| $\mathrm{Na}_{2} \mathrm{~B}_{4} \mathrm{O}_{7}$ |  | 16 |  | 39 | -- | 105 | 200 | 244 | 314 | 408 | 523 |
| $\mathrm{Na}_{2} \mathrm{CO}_{3} \ldots$ (10aq) | 71 | 126 | 214 | 409 | -- |  |  |  |  |  |  |
| " ${ }^{\text {c....(7aq) }}$ | 204 | 263 | 335 | 435 | (1aq) | 475 | 464 | 458 | 452 | 452 | 452 |
| NaCl | 356 | 357 | 358 | 360 | 363 | 367 | 371 | 375 | 380 | 385 | 391 |
| $\mathrm{NaClO}_{3}$ | 820 | 890 | 990 | - | 1235 |  | 1470 |  | 1750 |  | 2040 |
| $\mathrm{Na}_{2} \mathrm{CrO}$ | 317 | 502 | 900 |  | 960 | 1050 | 1150 |  | 1240 |  | 1260 |
| $\mathrm{Na}_{2} \mathrm{Cr}_{2} \mathrm{O}_{7}$ | 1630 | 1700 | 1800 | 1970 | 2200 | 2480 | 2830 | 3230 | 3860 |  | 4330 |
| $\mathrm{NaHCO}_{3}$ | 69 | 82 | 96 | 111 | 127 | 145 | 164 |  |  |  |  |
| $\mathrm{Na}_{2} \mathrm{HPO}_{4}$ | 25 | 39 | 93 | 241 | 639 |  |  | 949 |  |  | 988 |
| NaI | 1590 | 1690 | 1790 | 1900 | 2050 | 2280 | 2570 |  | 2950 |  | 3020 |
| $\mathrm{NaNO}_{3}$ | 730 | 805 | 880 | 962 | 1049 | 1140 | 1246 | 1360 | 1480 | 1610 | 1755 |
|  |  |  |  | (con | inued) |  |  |  |  |  |  |

TABLE 351.-SOLUBILITY OF INORGANIC SALTS IN WATER (concluded)
Temperature ${ }^{\circ} \mathrm{C}$


TABLE 352.-SOLUBILITY OF A FEW ORGANIC SALTS IN WATER
(Temperature variation ${ }^{\circ} \mathrm{C}$ )

| Salt |  | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $\mathrm{H}_{2}\left(\mathrm{CO}_{2}\right)_{2}$ | $\ldots$ | $\ldots$ | 36 | 53 | 102 | 159 | 228 | 321 | 445 | 635 | 978 | 1200 |
| $\mathrm{H}_{2}\left(\mathrm{CH}_{2} \cdot \mathrm{CO}_{2}\right)_{2}$ | $\ldots$ | 28 | 45 | 69 | 106 | 162 | 244 | 358 | 511 | 708 | - | 1209 |
| Tartaric acid | $\ldots$ | 1150 | 1260 | 1390 | 1560 | 1760 | 1950 | 2180 | 2440 | 2730 | 3070 | 3430 |
| Racemic | $\ldots$ | 92 | 140 | 206 | 291 | 433 | 595 | 783 | 999 | 1250 | 1530 | 1850 |
| $\mathrm{~K}\left(\mathrm{HCO}_{2}\right)$ | $\ldots$ | 2900 | - | 3350 | - | 3810 | - | 4550 | - | 5750 | - | 7900 |
| $\mathrm{KH}\left(\mathrm{C}_{4} \mathrm{H}_{4} \mathrm{O}_{6}\right)$ | $\ldots$ | 3 | 4 | 6 | 9 | 13 | 18 | 24 | 32 | 45 | 57 | 69 |

## TABLE 353.-SOLUBILITY OF GASES IN WATER

(Temperature variation ${ }^{\circ} \mathrm{C}$ )
The table gives the weight in grams of the gas which will be absorbed in 1000 g of water when the partial pressure of the gas plus the vapor pressure of the liquid at the given temperature equals 760 mmHg .

| Gas | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{O}_{2}$ | .0705 | .0551 | .0443 | .0368 | .0311 | .0263 | .0221 | .0181 | .0135 |
| $\mathrm{H}_{2}$ | .00192 | .00174 | .00160 | .00147 | .00138 | .00129 | .00118 | .00102 | .00079 |
| $\mathrm{~N}_{2}$ | .0293 | .0230 | .0189 | .0161 | .0139 | .0121 | .0105 | .0089 | .0069 |
| $\mathrm{Br}_{2}$ | 431. | 248. | 148. | 94.0 | 62. | 40. | 28. | 18. | 11. |
| $\mathrm{Cl}_{2}$ | - | 9.97 | 7.29 | 5.72 | 4.59 | 3.93 | 3.30 | 2.79 | 2.23 |
| $\mathrm{CO}_{2}$ | 3.35 | 2.32 | 1.69 | 1.26 | .97 | .76 | .58 | - | - |
| $\mathrm{H}_{2} \mathrm{~S}$ | 7.10 | 5.30 | 3.98 | - | - | - | - | - | - |
| $\mathrm{NH}_{3}$ | 987. | 689. | 535. | 422. | - | - | - | - | - |
| $\mathrm{SO}_{2}$ | 228. | 162. | 113. | 78. | 54. | - | - | - | - |

TABLE 354．－CHANGE OF SOLUBILITY PRODUCED BY UNIFORM PRESSURE

|  | $\underset{\text { at } 25^{\circ}{ }^{\circ} \mathrm{CH} \mathrm{H}_{2} \mathrm{O}}{ }$ |  | $\underset{\text { ans }}{\substack{\mathrm{ZnS}_{4} 5^{\circ} \\ \hline \mathrm{H}_{2} \mathrm{C}}}$ |  | Mannite at ${ }^{24.05^{\circ} \mathrm{C}}$ |  | $\mathrm{NaCl}_{\text {at }} 24.05^{\circ} \mathrm{C}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Percentage change |  |  |  |  |  |  |
| 1 | 76.80 | － | 57.95 | － | 20.66 | － | 35.90 | － |
| 500 | 78.01 | ＋1．57 | 57.87 | －． 14 | 21.14 | ＋2．32 | 36.55 | ＋1．81 |
| 1000 | 78.84 | ＋2．68 | 57.65 | －． 52 | 21.40 | $+3.57$ | 37.02 | $+3.12$ |
| 1500 | － | － | － | － | 21.64 | ＋4．72 | 37.36 | ＋4．07 |

TABLE 355．－COMMONLY USED ORGANIC SOLVENTS＊
Arranged in the order of their boiling points

| Name | $\begin{gathered} \text { Boiling } \\ \text { point } \\ \text { poic } \end{gathered}$ | Name | $\begin{gathered} \text { Roiling } \\ \text { point } \\ { }_{\text {ont }} \mathrm{C} \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| Ethyl ether | 34.54 | Xylene（0） | 144 |
| Carbon disulfide | 46.25 | Amyl acetate | 147.6 |
| Acetone | 56.08 | Ethyl lactate | 154 |
| Methyl acetate | 57.1 | Cellosolve acetate | 156 |
| Chloroform | 61.2 | Cyclohexanone | 156.7 |
| Methyl alcohol | 64.5 | Furfural | 158－162 |
| Carbon tetrachloride | 76.74 | Butyl cellosolve | 170.6 |
| Ethyl acetate | 77.15 | Ethyl acetoacetate | 180.0 |
| Ethyl alcohol | 78.32 | Diethyl oxalate | 186.1 |
| Benzol | 79.6 | Ethylene glycol | 197.2 |
| Isopropyl alcohol | 82.26 | Carbitol | 202 |
| Ethylene dichloride | 83.5 | Benzyl alcohol | 205.8 |
| Trichlorethylene | 87 | Ethyl benzoate | 213.2 |
| Ethyl propionate | 99.1 | Butyl stearate | （25mm） |
| Toluene ．．．．．．． | 110.7 | Butyl carbitol | ． 230 |
| Butyl alcohol（n） | 117.7 | Diethylene glycol | 245 |
| Ethyl butyrate | 121.3 | Triplienyl phosphate | （11mm） |
| Methyl cellosolve | 124.5 | Triacetin | ．． 259 |
| Diethyl carbonate | 125.8 | Diacetin | 261 |
| Butyl acetate | 126.5 | Dimethyl phthalate | 282 |
| Tetrachlorethane | 130 | Diethyl phthalate | 296 |
| Cellosolve | 135.1 | Dibutyl phthalate | 340 |
| Ethyl benzene | 136.1 | Diamyl phthalate | 344 |
| Amyl alcohol（n） | 137.9 |  |  |

[^162]TABLE 356.-ABSORPTION OF GASES AND VAPORS BY LIQUIDS*

|  | Absorption coefficient, at, for gases in water |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Temperature ${ }^{\circ} \mathrm{C}$ | Carbon dioxide $\mathrm{CO}_{2}$ | Carbon monoxide CO | $\underset{\mathrm{H}}{\text { Hydrogen }}$ | $\underset{\mathrm{N}}{\mathrm{Nitrogen}}$ | $\begin{aligned} & \text { Nitric } \\ & \text { oxide } \\ & \text { NO } \end{aligned}$ |  | Nitrous oxide $\mathrm{N}_{2} \mathrm{O}$ | $\begin{aligned} & \text { Oxygen } \\ & 0 \end{aligned}$ |
| 0 | 1.797 | . 0354 | . 02110 | . 02399 | . 0738 |  | 1.048 | . 04925 |
| 5 | 1.450 | . 0315 | . 02022 | . 02134 | . 0646 |  | . 8778 | . 04335 |
| 10 | 1.185 | . 0282 | . 01944 | . 01918 | . 0571 |  | . 7377 | . 03852 |
| 15 | 1.002 | . 0254 | . 01875 | . 01742 | . 0515 |  | . 6294 | . 03456 |
| 20 | . 901 | . 0232 | . 01809 | . 01599 | . 0471 |  | . 5443 | . 03137 |
| 25 | . 772 | . 0214 | . 01745 | . 01481 | . 0432 |  | . | . 02874 |
| 30 | - | . 0200 | . 01690 | . 01370 | . 0400 |  | - | . 02646 |
| 40 | . 506 | . 0177 | . 01644 | . 01195 | . 0351 |  | - | . 02316 |
| 50 | - | . 0161 | . 01608 | . 01074 | . 0315 |  | - | . 02080 |
| 100 | . 244 | . 0141 | . 01600 | . 01011 | . 0263 |  | - | . 01690 |
| Temperature ${ }^{\circ} \mathrm{C}$ | Air | $\underset{\mathrm{NH}_{3}}{\underset{\mathrm{Amman}}{2}}$ | Chlorine Cl | Ethylene $\mathrm{C}_{2} \mathrm{H}_{4}$ | Methane $\mathrm{CH}_{4}$ |  | Hydrogen sulfide $\mathrm{H}_{2} \mathrm{~S}$ | Sulfur dioxide $\mathrm{SO}_{2}$ |
| 0 | . 02471 | 1174.6 | 3.036 | . 2563 | . 05473 |  | 4.371 | 79.79 |
| 5 | . 02179 | 971.5 | 2.808 | . 2153 | . 04889 |  | 3.965 | 67.48 |
| 10 | . 01953 | 840.2 | 2.585 | . 1837 | . 04367 |  | 3.586 | 56.65 |
| 15 | . 01795 | 756.0 | 2.388 | . 1615 | . 03903 |  | 3.233 | 47.28 |
| 20 | . 01704 | 683.1 | 2.156 | . 1488 | . 03499 |  | 2.905 | 39.37 |
| 25 | - | 610.8 | 1.950 | - | . 02542 |  | 2.604 | 32.79 |
|  |  | Absorption | coefficients, | $a_{t, \text { for gase }}$ | s in alcohol | , $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{O}$ | ${ }_{5} \mathrm{OH}$ |  |
| Temperature ${ }^{\circ} \mathrm{C}$ | Carbon dioxide $\mathrm{CO}_{2}$ | Ethylene Methane <br> $\mathrm{C}_{2} \mathrm{H}_{4} \quad \mathrm{CH}_{4}$ | $\begin{gathered} \text { e Hydrogen } \\ \text { H } \end{gathered}$ | Nitrogen N | Nitric oxide NO | Nitrous oxide $\mathrm{N}_{2} \mathrm{O}$ | s Hydrogen sulfide $\mathrm{H}_{2} \mathrm{~S}$ | Sulfur dioxide $\mathrm{SO}_{2}$ |
| 0 5 | 4.329 3.891 | $3.595 \quad .5226$ | . 0692 | .1263 | . 3161 | 4.190 3.838 | 17.89 14.78 | 328.6 |
| 5 | 3.891 | $\begin{array}{ll}3.323 & .5086 \\ 3.086 & 4953\end{array}$ | . 0685 | . 1241 | . 2998 | 3.838 | 14.78 | 251.7 |
| 15 | 3.514 3.199 | $\begin{array}{ll}3.086 \\ 2.882 & .4953\end{array}$ | . 0679 | . 1228 | . 2861 | 5.525 3.215 | 11.99 9.54 | 190.3 |
| 20 | 2.946 | 2.713 . 4710 | . 0667 | . 1204 | . 2659 | 3.015 | 7.41 | 114.5 |
| 25 | 2.756 | 2.578 .4598 | . 0662 | . 1196 | . 2595 | 2.819 | 5.62 | 99.8 |

* This table contains the volumes of different gases, supposed measured at $0^{\circ} \mathrm{C}$ and 76 cmHg pressure. which unit volume of the liquid named will absorb at atmospheric pressure and the temperature stated in the first column. The numbers tabulated are commonly called the absorption coefficient for the gases in water, or in alcohol, at the temperature $t$ and under 1 atm of pressure.

TABLE 357.-VAPOR PRESSURE OF SOME ELEMENTS
(Over liquid unless otherwise noted.)


## TABLE 358.-SURFACE TENSION OF LIQUIDS

Part 1.-Water and alcohol in contact with moist air

Values represent means. See I.C.T. and L. and B. for more elaborate tables. Tension ( $\gamma$ ) in dynes/ cm .

| ${ }^{\circ} \mathrm{C}$ | $\mathrm{H}_{2} \mathrm{O} \mathrm{C}_{2} \mathrm{H}_{5} \mathrm{OH}$ | ${ }^{\circ} \mathrm{C}$ | $\mathrm{H}_{2} \mathrm{O} \mathrm{C}_{2} \mathrm{H}_{5} \mathrm{OH}$ | ${ }^{\circ} \mathrm{C}$ | $\mathrm{H}_{2} \mathrm{O}$ |  |
| ---: | :--- | :--- | :--- | :--- | :--- | :--- |
| -5 | 76.4 |  | 35 | 70.3 | 21.0 | 75 |

Part 2.-Miscellaneous liquids In contact with air

| Liquid $\quad{ }^{\circ} \mathrm{C}$ | $\begin{gathered} \text { Dynes } \\ \text { per cm } \end{gathered}$ | Formula |
| :---: | :---: | :---: |
| Actone ............ 20 | 23.7 | $\left(\mathrm{CH}_{3}\right)_{2} \mathrm{CO}$ |
| Acetic acid ......... 20 | 27.6 | $\mathrm{CH}_{3} \mathrm{CO}_{2} \mathrm{H}$ |
| Amyl alcohol ....... 20 | 24 | $\mathrm{C}_{5} \mathrm{H}_{12} \mathrm{O}$ |
| Aniline ............ 20 | 43 | $\mathrm{C}_{5} \mathrm{H}_{7} \mathrm{~N}$ |
| Benzene . . . . . . . . . . 0 | $27$ | $\mathrm{C}_{6} \mathrm{H}_{6}$ |
| Bromoform ........ 20 | 41.5 | $\mathrm{CHBr}_{3}$ |
| Butyric acid ....... 15 | 26.7 | $\mathrm{CH}_{3}\left(\mathrm{CH}_{2}\right)_{2} \mathrm{CO}_{2} \mathrm{H}$ |
| Carbon disulfide .... 20 | 32.3 | $\mathrm{CS}_{2}$ |
| Carbon tetrachloride. 20 | 26.8 | $\mathrm{CCl}_{4}$ |
| Chloroform ........ 20 | 27.2 | $\mathrm{CHCl}_{3}$ |
| Ether .............. 20 | 17.01 | $\mathrm{C}_{4} \mathrm{H}_{30} \mathrm{O}$ |
| Ethyl chloride ...... 20 | 16.2 | $\mathrm{CH}_{3} \mathrm{Cl}$ |
| Glycerine .......... 18 | 63 | $\mathrm{C}_{3} \mathrm{H}_{5}(\mathrm{OH})_{3}$ |
| Methyl alcohol ..... 20 | 22.6 | $\mathrm{CH}_{3} \mathrm{OH}$ |
| Olive oil ........... 18 | 33.1 |  |
| Petroleum ......... 25 | 26 |  |
| Phenol ............. 20 | 41.0 | $\mathrm{C}_{6} \mathrm{H}_{6} \mathrm{O}$ |
| Propyl alcohol ...... 20 | 23 | $\mathrm{CH}_{2}\left(\mathrm{CH}_{2}\right)_{1} \mathrm{OH}$ |
| Silicon tetrachloride . 19 | 17.0 | $\mathrm{SiCl}_{4}$ |
| Toluene ............ 20 | 28.4 | $\mathrm{C}_{7} \mathrm{H}_{8}$ |
| Turpentine ......... 20 | 27 |  |

TABLE 359.-SURFACE TENSION OF SOLUTIONS OF SALTS IN WATER

| $\begin{gathered} \text { Salt } \\ \mathrm{BaCl}_{2} \end{gathered}$ | Salt | ${ }^{\circ} \mathrm{C}$ | Dynes per cm |
| :---: | :---: | :---: | :---: |
|  | 0 | 30 | 71.1 |
|  | 24.6 | 30 | 75.6 |
| $\mathrm{CaCl}_{2}$ | 0 | 30 | 71.1 |
|  | 12.3 | 30 | 75.7 |
|  | 31.9 | 30 | 86.4 |
| HCl | 0 | 20 | 73.0 |
|  | 15 | 20 | 72.0 |
|  | 25 | 20 | 70.7 |
| KCl | 0 | 30 | 71.1 |
|  | 23.3 | 30 | 76.8 |
|  | 21.1 | 18 | 77.7 |
| NaCl | 0 | 18 | 72.4 |
|  | 7.6 | 18 | 74.8 |
|  | 13.7 | 18 | 76.9 |
| $\mathrm{NH}_{4} \mathrm{Cl}$ | 0 | 18 | 72.5 |
|  | 11 | 18 | 74.9 |
| $\mathrm{K}_{2} \mathrm{CO}_{3}$ | 0 | 30 | 71.1 |
|  | 39.4 | 30 | 89.4 |
|  | 53.6 | 30 | 107.2 |
| $\mathrm{Na}_{2} \mathrm{CO}_{3}$ | 0 | 30 | 71.1 |
|  | 10.5 | 30 | 73.9 |
|  | 24.4 | 30 | 76.5 |
|  | 63.1 | 30 | 80.6 |
| $\mathrm{KNO}_{3}$ | 0 | 18 | 72.6 |
|  | 15.2 | 18 | 74.5 |
|  | 21.5 | 18 | 75.4 |
| $\mathrm{NaNO}_{3}$ | 0 | 30 | 71.1 |
|  | 35.6 | 30 | 78.4 |
|  | 50.9 | 30 | 82.8 |
| CuSO. | 0 | 30 | 71.1 |
|  | 25.4 | 30 | 74.1 |
| $\mathrm{H}_{2} \mathrm{SO} 4$ | 0 | 18 | 72.8 |
|  | 12.7 | 18 | 73.5 |
|  | 47.6 | 18 | 76.7 |
|  | 80.3 | 18 | 71.2 |
|  | 90 | 18 | 63.6 |
| $\mathrm{K}_{2} \mathrm{SO} 4$ | 0 | 18 | 72.7 |
|  | 9.1 | 18 | 74.6 |
| $\mathrm{HNO}_{3}$ | 7.2 | 20 | 73.1 |
|  | 50 | 20 | 65.4 |
|  | 70 | 20 | 59.4 |
| NaOH | 0 | 20 | 72.8 |
|  | 10 | 20 | 77.3 |
|  | 20 | 20 | 85.8 |
|  | 30 | 20 | 95.1 |
| KOH | 0 | 18 | 72.8 |
|  | 3.8 | 18 | 74.1 |
|  | 7.8 | 18 | 75.5 |


| Liquid | Specific gravity | Surface tension in dynes per cm of liquid in contact with- |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Air | Water | Mercury |
| Water | 1.0 | 75.0 | . 0 | (392) |
| Mercury | 13.595 | 513.0 | 392.0 | 0 |
| Bisulfide of carbon. | 1.2687 | 30.5 | 41.7 | (387) |
| Chloroform | 1.498 | (31.8) | 26.8 | (415) |
| Ethyl alcohol | . 807 | (24.1) |  | 364 |
| Olive oil | . 918 | 34.6 | 18.6 | 317 |
| Turpentine | . 873 | 28.8 | 11.5 | 241 |
| Petroleum | . 870 | 29.7 | (28.9) | 271 |
| Hydrochloric acid | 1.10 | (72.9) | - | (392) |
| Hyposulfite of soda | 1.1248 | 69.9 | -- | 429 |

TABLE 361.-SURFACE TENSION OF LIQUIDS AT SOLIDIFYING POINT


## TABLE 362.-VAPOR PRESSURE AND RATE OF EVAPORATION

| ${ }^{\circ} \mathrm{K}$ | $\underset{\mathrm{mmHg}}{\mathrm{Mo}_{2}}$ | $\underset{\mathrm{mmHg}}{\mathrm{~W}}$ | Evaporation rate $\mathrm{g} \mathrm{cm}^{-2} \mathrm{sec}^{-1}$ |  | Platinum |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Mo | W | ${ }^{\circ} \mathrm{K}$ | mm | $\mathrm{g} \mathrm{cm}^{-2} \mathrm{sec}^{-1}$ |
| 1800 | . $0 \times 643$ | -- | . 010863 | -- | 1000 | . 017324 | . 018832 |
| 2000 | .08789 | . $0_{11} 645$ | . 07100 | . 012114 | 1200 | . 012111 | . 014260 |
| 2200 | . 0.396 | .09849 | . 0.480 | . 010144 | 1400 | . 018188 | (0.401 |
| 2400 | . 021027 | . 07492 | . 0,420 | . 08798 | 1600 | .07484 | .0096\% |
| 2600 | . 0160 | . 0.151 | . 013179 | .07236 | 1800 | . 0.350 | . 0,667 |
| 2800 | . 1679 | .04286 | . 02181 | .08429 | 2000 | . 03107 | . 0.195 |
| 3000 |  | . 03362 | - | . 0.523 | 4180 | 760 mm | - |
| 3200 | $3890^{\circ}$ \} | . 02333 | -- | . 0.467 |  |  |  |
| 3500 | 760 mm \} | . 0572 | -- | . 03769 |  |  |  |

[^163]For the range of pressures for which the corresponding values of $t^{\circ} \mathrm{C}$ are given in the table (Part 2), the pressure as a function of $T(=t+273)$ may be represented to a satisfactory degree of approximation by the relation

$$
\begin{equation*}
\log p=A-B / T \tag{1}
\end{equation*}
$$

Part 1 gives values of $A$ and $B$ used in calculating the values of $t^{\circ} \mathrm{C}$ in Part 2, where $p$ is expressed in microns of mercury. The symbols (s) and ( $l$ ) refer to the solid and liquid states, respectively.

The rate of evaporation is given by the relation

$$
\begin{align*}
\log W & =\overline{5} .7660+0.5 \log M+\log p-0.5 \log T  \tag{2}\\
& =c+\log p-0.5 \log T, \tag{3}
\end{align*}
$$

where $W$ is expressed in $\mathrm{g} \mathrm{cm}^{-2} \sec ^{-1}$, and $p$ in microns.
Explanation of data in Part 2.-The first row for each metal, which is designated $t$. gives the temperatures in ${ }^{\circ} \mathrm{C}$ corresponding to the pressures in microns at the head of each column. These were calculated by means of equation 1. The second row, designated II', gives the rates of evaporation (in a good vacuum) in grams per square centimeter per second $\left(\mathrm{g} \mathrm{cm}^{-2} \sec ^{-1}\right)$, at the values of $t$ immediately above in the same column. These were calculated by means of equation 3.

In addition to the values of $t$ given in the first row, which are to be regarded as, in the writer's opinion, the more reliable, there are also given, in the case of a number of the metals, a series of other values of $t$, which have been observed by some investigators: The fact that for the same value of the vapor pressure in microns two or more values of $t$ are quoted by different authorities indicates the degree of uncertainty that exists for some of the data given in the tables. For metals for which the data are very questionable, it has not heen considered worth while even to calculate values of $W$.

The column headed $t_{m}$ gives the melting point in degrees C , and $p_{m}$ gives the vapor pressure in microns at the melting point. For values of $t$ below $t_{m}$, the metal is obviously in the solid state, and for values of $t$ above $t_{m}$, the metal is in the liquid state.

[^164]Part 1.-Constants in relations for evaporation of metals

| Metal | $A$ | $10^{-3} \times B$ | $c+4$ | Metal | A | $10^{-3} \times B$ | $c+4$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Li | 10.50(1) | 7.480 | . 1867 | Si | 13.20(s) | 19.72 | . 4900 |
|  | 10.71 (1) | 5.480 | . 4468 |  | 12.55 (1) | 18.55 | . 4900 |
|  | 10.36(1) | 4.503 | . 5621 | Ti | 11.25(s) | 18.64 | . 6061 |
| Rb | 10.42(1) | 4.132 | . 7319 |  | 11.98 (1) | 20.11 |  |
|  | [10.53(1) | $4.291]$ |  | Zr | 12.38(s) | 25.87 | . 7460 |
| Cs | 9.86(1) | 3.774 | . 8278 |  | 13.04(1) | 27.43 |  |
|  | [10.02(1) | 3.883] |  | Th | 12.52 (1) | 28.44 | . 9488 |
| Cu | 12.81(s) | 18.06 | . 6678 | Ge | 10.94(1) | $13.11$ | . 6965 |
|  | 11.72 (1) | 16.58 |  | Sn | 9.97 (1) |  | . 8032 |
|  | 12.28(s) | 14.85 | . 7825 | Pb . | . . . . . . $10.69(1)$ | 9.60 | . 9242 |
|  | 11.66 (1) | 14.09 |  |  | 13.32 | 26.62 | . 6195 |
| Au | 11.65 (1) | 18.52 | . 9135 | Nb | 14.37(s) | 40.40 | . 7500 |
| Be | 12.99 (s) | 18.22 | . 2436 | Ta | 13.00 (s) | 40.21 | . 8947 |
|  | $11.95(1)$ | 16.59 | . 49590 |  |  |  |  |
| Mg | 11.82(s) | 7.741 |  | $\begin{aligned} & \mathrm{Sb}_{2} \\ & \mathrm{Bi} \end{aligned}$ | $\begin{aligned} & 11.42 \\ & 11.14(1) \end{aligned}$ | $\begin{aligned} & 9.913 \\ & 9.824 \end{aligned}$ | $\begin{aligned} & .9592 \\ & .9260 \end{aligned}$ |
| Ca | 11.30(s) | 9.055 | . 5675 | Cr | 12.88(s) | 17.56 | . 6240 |
| Sr | 11.13(s) | 8.324 | . 7373 | Mo | 11.80 (s) | 30.31 | . 7570 |
| Ba | 10.88 | 8.908 | . 8349 | W | 12.24(s) | 40.26 | . 8983 |
| Zn | 11.94 (s) | 6.744 | . 6737 |  |  | $\begin{aligned} & 25.80 \\ & 14.10 \end{aligned}$ | $\begin{array}{r} .9544 \\ .6359 \end{array}$ |
| Cd | 11.78(s) | 5.798 | . 7914 | $\begin{aligned} & \mathrm{U} \\ & \mathrm{Mn} \end{aligned}$ | $12.88(1)$ $12.25(\mathrm{~s})$ |  |  |
| B | 14.13(s) | 21.37 | . 2831 | Fe | 12.63(s) | 20.00 | . 6395 |
| A1 | 11.99 (1) | 15.63 | . 4814 |  | 13.41 (1) | 21.40 |  |
| Sc | 11.94 | 18.57 | . 5931 | Co | 12.43 | 21.96 | . 6512 |
| Y | 12.43 | 21.97 | . 7405 | Ni | 13.28(s) | 21.84 | . 6503 |
| La | 11.88(1) | 18.00 | . 8374 |  | 12.55(1) | 20.60 |  |
| Ce | 13.74 (1) | 20.10 | . 8392 | Ru | 13.50 | 33.80 | . 7696 |
| Ga | 10.79(1) | 13.36 | . 6877 | Rh | 13.55 | 30.40 | . 7722 |
| In . | 10.93(1) | 12.15 | . 7959 | Pd | 11.46 | 19.23 | . 7801 |
| T1. | 11.15 (1) | 8.92 | . 9212 | Os | 13.59 | 37.00 | . 9056 |
| C. | 14.06(s) | 38.57 | . 3056 | Ir | 13.06 | 34.11 | . 9089 |
|  |  |  |  | Pt | 12.633 | 27.50 | . 9112 |

Part 2.-Temperatures for given values $p$ in microns of mercury and rates of evaporation ( $\mathbf{W}, \mathrm{g} \mathrm{cm}^{-2} \mathbf{~ s e c}^{-1}$ )

| $\begin{gathered} t_{m} \\ 179 \end{gathered}$ | $9 \times 10_{m}^{p_{m}}$ |
| :---: | :---: |
| 98 | $8.2 \times 10^{-5}$ |
| 64 | $9.8 \times 10^{-4}$ |
| 38.5 | $1.5 \times 10^{-3}$ |
| 29 | $1.5 \times 10^{-3}$ |
| 1083 | . 31 |
| 961 | 1.78 |
| 1063 | $6 \times 10^{-3}$ |
| 1284 | 19.5 |
| 651 | $2.2 \times 10^{3}$ |
| 810 | $8.75 \times 10^{2}$ |
| 771 | $1.44 \times 10^{3}$ |




sN $\quad$ न
1000
858
$2.03 \times 10^{-2}$
861
$\ldots$
$\ldots$
$\cdots$
$\ldots$
$\ldots$
126
$4.14 \times 10^{-2}$
1648
$4.38 \times 10^{-3}$
1279
$7.69 \times 10^{-3}$
1.2765
1804
1804
$8.40 \times 10^{-3}$
2056
$1.14 \times 10^{-2}$
1754
$1.53 \times 10^{-2}$
1599
$1.60 \times 10^{-2}$
1443
$1.18 \times 10^{-2}$
1260
$1.60 \times 10^{-2}$
821
$2.52 \times 10^{-2}$





ョ
1000
3214
$3.42 \times 10^{-3}$
1670
$7.01 \times 10^{-3}$
1965
$8.53 \times 10^{-3}$
2459
$1.07 \times 10^{-2}$
2715
$1.63 \times 10^{-2}$
1635
$1.14 \times 10^{-2}$
1609
$1.47 \times 10^{-2}$
975
$2.38 \times 10^{-2}$
2207
$8.2 \times 10^{-3}$
9
TABLE 363.-EVAPORATION OF METALS (continued)







E N On
0
0

$$
8
$$

$$
\begin{gathered}
2338 \\
1.76 \times 10^{-2} \\
1251 \\
1.11 \times 10^{-2}
\end{gathered}
$$

$$
\begin{gathered}
2 \\
\underset{\infty}{0} \dot{x} \\
-0 \\
0
\end{gathered}
$$

TABLE 363.-EVAPORATION OF METALS (concluded)

 1
2295
$1.12 \times 10^{-5}$
3016
$1.45 \times 10^{-5}$
1730
$2.01 \times 10^{-5}$
878
$1.27 \times 10^{-5}$
1310
$1.10 \times 10^{-5}$
1494
$1.06 \times 10^{-8}$
1371
$1.10 \times 10^{-8}$
2230
$1.18 \times 10^{-5}$
1971
$1.25 \times 10^{-5}$
1405
$1.47 \times 10^{-5}$
2451
$1.54 \times 10^{-5}$
2340
$1.59 \times 10^{-8}$
1904
$1.75 \times 10^{-5}$ Mines Bull. 383, 1935 . b. Ditchhurn, R. W.,
the elements, Report for the Manhattan Project,


and Gilmour

$$
\begin{gathered}
2946 \\
1.04 \times 10^{-2} \\
2607 \\
1.10 \times 10^{-2} \\
2000 \\
1.26 \times 10^{-2} \\
3221 \\
1.36 \times 10^{-2}
\end{gathered}
$$

$$
\begin{gathered}
1.36 \times 10^{-2} \\
3118 \\
1.39 \times 10^{-2}
\end{gathered}
$$

TABLE

$$
\begin{aligned}
& 2582 \\
& 1.52 \times 10^{-2}
\end{aligned}
$$ H. A., Langmuir, I., and Mackay

$$
\begin{aligned}
& \\
& \\
& \\
&
\end{aligned}
$$

$$
\begin{aligned}
& 1.52 \times 10^{-2} \\
& \text { vol. } 13, \mathrm{p} .3
\end{aligned}
$$


Brewer, The the-
Taylor, J. B., and
$001 \times+0.6$
$0-01 \times+2 \cdot \varepsilon$

10
2533
$1.05 \times 10^{-4}$
3309
$1.43 \times 10^{-4}$
1898
$1.93 \times 10^{-4}$
980
$1.22 \times 10^{-4}$
1447
$1.02 \times 10^{-6}$
1649
$1.02 \times 10^{-4}$
1510
$1.06 \times 10^{-4}$
2431
$1.13 \times 10^{-4}$
2149
$1.20 \times 10^{-6}$
1566
$1.41 \times 10^{-4}$
2667
$1.48 \times 10^{-4}$
2556
$1.52 \times 10^{-4}$
2090
$1.68 \times 10^{-4}$
and Gilmour J. C., Rev. Mod. Phys.,





The vapor pressures on this page are in mmHg over a liquid phase unless distinguished by the subscript s. They are generally means from various determinations.


TABLE 364.-VAPOR PRESSURE OF ORGANIC LIQUIDS (concluded) 369

| ${ }^{\circ} \mathrm{C}$ |  | Carbon ${ }^{\text {dioxide }}$ $\mathrm{CO}_{2}$ | Ethyl $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{I}$ mm | Ethyl acetate mm | $\begin{gathered} \text { Hydrogen } \\ \text { sulfide } \\ \mathrm{H}_{2} \mathrm{~S} \\ \mathrm{~mm} \end{gathered}$ | Methyl chloride mm | Nap. $\mathrm{C}_{10} \mathrm{H}_{5}$ mm | $\begin{gathered} \text { Sulfur } \\ \text { dioxide } \\ \mathrm{SO}_{2} \\ \mathrm{~mm} \end{gathered}$ | $\underbrace{\substack{0 \\ \hline}}_{\mathbf{C}_{10} \mathrm{H}_{8}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  | mm |
| -50 | 403 | 6.74 |  |  | 1216 |  |  | $86-91.9$ | . 002 |
| -30 | 1.180 | 14.10 |  |  | 2840 | 579 |  | $286-81.7$ | . 005 |
| -25 | 1.496 | 16.61 |  |  |  | 718 |  | 379 -77.4 | . 007 |
| -20 | 1.877 | 19.44 |  | 6.5 | 4100 | 883 |  | $474-67.5$ | . 020 |
| -15 | 2.332 | 22.60 |  |  |  | 1079 | $\ldots$ | -57.7 | . 060 |
| -10 | 2.870 | 26.13 |  | 12.9 | 5720 | 1310 |  | $760-38.0$ | . 39 |
| - 5 | 3.502 | 30.05 |  |  |  | 1579 |  | -24.2 | 1.47 |
| 0 | 4.238 | 34.38 | 41.5 | 24.3 | 7750 | 1891 |  | $1155-2.9$ | 5.72 |
| + 5 | 5.090 | 39.16 | 53.5 |  |  | 2250 | $\cdots$ | ... 0 | 6.86 |
| 10 | 6.068 | 44.41 | 68.6 | 42.7 | 10300 | 2660 |  | $1714+15.0$ | 16.8 |
| 15 | 7.188 | 50.17 |  |  |  | 3134 | $\ldots$ | +25.8 | 28.7 |
| 20 | 8.458 | 56.50 | 108.5 | 72.8 | 14000 | 3667 | $\ldots$ | 2460 |  |
| 25 | 9.896 | 63.45 |  |  |  | 4267 |  |  |  |
| 30 | 11.512 | 71.4 | 167.6 | 119 | 17500 | 4940 |  | 3420 |  |
| 35 | 13.321 |  |  |  |  | 5700 |  |  |  |
| 40 | 15.339 | (I.C.T. | 250 | 186 | 22000 | 6650 | $\ldots$ | 4650 |  |
| 45 | 17.580 | 1928) |  |  |  |  |  |  |  |
| 50 | 20.060 |  | 362 | 282 | 27500 | 8510 | $\ldots$ | 6210 |  |
| 60 | 25.80 | . | 510 | 415 |  | 10900 |  | 8150 |  |
| 70 | 32.69 |  |  | 596 | 40400 | 14300 |  | 10540 |  |
| 80 | 40.90 |  | ... | 833 |  | 16800 | 9.6 |  |  |
| 90 | 50.56 |  |  | 1130 |  | 21000 | 13.0 |  |  |
| 100 | 61.82 |  |  | 1515 |  | 25800 | 19.7 | 27.8 atm |  |
|  | Cragoe |  |  | $200^{\circ}$ |  | $\left\{141^{\circ}\right.$ | $\left\{200^{\circ}\right.$ | $\left\{150^{\circ}\right.$ |  |
|  | 1920 |  |  | 5600 |  | \{53600 | $\{490$ | \{71.4" |  |

TABLE 365.-VAPOR PRESSURE AT LOW TEMPERATURES
Many of the following values are extrapolations made by Langmuir by means of plots of $\log p$ against $1 / T .1$ barye $=0.000000987 \mathrm{~atm}=0.000750 \mathrm{mmHg}$.

| Gas | ${ }^{\circ} \mathrm{C}$ | mmHg | Gas | ${ }^{\circ} \mathrm{C}$ | Baryes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{O}_{2}$ | -182.9 | 760 | $\mathrm{CO}_{2}$ | -148 | 100 |
|  | -211.2 | 7.75 |  | -168 |  |
| $\mathrm{N}_{2}$ | -195.8 | 760 |  | -182 | . 01 |
| CO | -210.5 | 86 |  | -193 | . 0001 |
|  | -200 | $\begin{aligned} & 863 \\ & 249 \end{aligned}$ | Ice | - 60 | 9.6 |
| CH. | -185.8 | 79.8 |  | - 89 | . 1 |
|  | -201.5 | 50.2 |  | -100 | . 01 |
| A | -186.2 | 760 |  | -110 | . 001 |
|  | -194.2 | 300 | Hg | + 30 | 3.7 |
| $\mathrm{C}_{2} \mathrm{H}_{4}$ | -175.7 | . 76 |  | + 20 | 1.6 |
|  | -188 | . 076 |  | + 10 | . 65 |
|  | -197 | . 0076 |  | 0 | . 25 |
|  | -205 | . 00076 |  | - 10 | . 087 |
| $\mathrm{C}_{2} \mathrm{H}_{6}$ | -150 | 7.6 |  | - 20 | . 029 |
|  | -180 | . 076 |  | - 40 | . 0023 |
|  | -190 | . 0076 |  | - 78 | $4.3 \times 10^{-8}$ |
|  | -198 | . 00076 |  | -180 | $2.3 \times 10^{-26}$ |


| $\bigcirc$ | 0 | 1 | 2 |  | 4 |  | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\bigcirc$ |  |  |  | 3 |  | 5 |  |  |  |  |
| E. | Vapor pressure in mmHg at $0^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |
| 0 | 12.24 | 13.18 | 14.15 | 15.16 | 16.21 | 17.31 | 18.46 | 19.68 | 20.98 | 22.34 |
| 10 | 23.78 | 25.31 | 27.94 | 28.67 | 30.50 | 32.44 | 34.49 | 36.67 | 38.97 | 41.40 |
| 20 | 44.00 | 46.66 | 49.47 | 52.44 | 55.56 | 58.86 | 62.33 | 65.97 | 69.80 | 73.83 |
| 30 | 78.06 | 82.50 | 87.17 | 92.07 | 97.21 | 102.60 | 108.24 | 114.15 | 120.35 | 126.86 |
| 40 | 133.70 | 140.75 | 148.10 | 155.80 | 163.80 | 172.20 | 181.00 | 190.10 | 199.65 | 209.60 |
| 50 | 220.00 | 230.80 | 242.50 | 253.80 | 265.90 | 278.60 | 291.85 | 305.65 | 319.95 | 334.85 |
| 60 | 350.30 | 366.40 | 383.10 | 400.40 | 418.35 | 437.00 | 456.45 | 476.45 | 497.25 | 518.85 |
| 70 | 541.20 | 564.35 | 588.35 | 613.20 | 638.95 | 665.55 | 693.10 | 721.55 | 751.00 | 781.45 |

From the formula $\log p=a+b a^{t}+c \beta^{t}$ Ramsay and Young obtain the following numbers:


TABLE 367.-VAPOR PRESSURE OF METHYL ALCOHOL

| 0 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| E | Vapor pressure in mmHg at $0^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |
| 0 | 29.97 | 31.6 | 33.6 | 35.6 | 37.8 | 40.2 | 42.6 | 45.2 | 47.9 | 50.8 |
| 10 | 53.8 | 57.0 | 60.3 | 63.8 | 67.5 | 71.4 | 75.5 | 79.8 | 84.3 | 89.0 |
| 20 | 94.0 | 99.2 | 104.7 | 110.4 | 116.5 | 122.7 | 129.3 | 136.2 | 143.4 | 151.0 |
| 30 | 158.9 | 167.1 | 175.7 | 184.7 | 194.1 | 203.9 | 214.1 | 224.7 | 235.8 | 247.4 |
| 40 | 259.4 | 271.9 | 285.0 | 298.5 | 312.6 | 327.3 | 342.5 | 358.3 | 374.7 | 391.7 |
| 50 | 409.4 | 427.7 | 446.6 | 466.3 | 486.6 | 507.7 | 529.5 | 552.0 | 575.3 | 599.4 |
| 60 | 624.3 | 650.0 | 676.5 | 703.8 | 732.0 | 761.1 | 791.1 | 822.0 | -- | -- |

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TABLE 368.-VAPOR PRESSURE OF A NUMBER OF LIQUIDS ( mm Hg )
Carbon disulfide, chlorobenzene, bromobenzene, and aniline

| Temp. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Carbon disulfide |  |  |  |  |  |  |  |  |  |  |
| 0 | 127.90 | 133.85 | 140.05 | 146.45 | 153.10 | 160.00 | 167.15 | 174.60 | 182.25 | 190.20 |
| 10 | 198.45 | 207.00 | 215.80 | 224.95 | 234.40 | 244.15 | 254.25 | 264.65 | 275.40 | 286.55 |
| 20 | 298.05 | 309.90 | 322.10 | 334.70 | 347.70 | 361.10 | 374.95 | 389.20 | 403.90 | 419.00 |
| 30 | 434.60 | 450.65 | 467.15 | 484.15 | 501.65 | 519.65 | 538.15 | 557.15 | 576.75 | 596.85 |
| 40 | 617.50 | 638.70 | 660.50 | 682.90 | 705.90 | 729.50 | 753.75 | 778.60 | 804.10 | 830.25 |
| Chlorobenzene |  |  |  |  |  |  |  |  |  |  |
| 20 | 8.65 | 9.14 | 9.66 | 10.21 | 10.79 | 11.40 | 12.04 | 12.71 | 13.42 | 14.17 |
| 30 | 14.95 | 15.77 | 16.63 | 17.53 | 18.47 | 19.45 | 20.48 | 21.56 | 22.69 | 23.87 |
| 40 | 25.10 | 26.38 | 27.72 | 29.12 | 30.58 | 32.10 | 33.69 | 35.35 | 37.08 | 38.88 |
| 50 | 40.75 | 42.69 | 44.72 | 46.84 | 49.05 | 51.35 | 53.74 | 56.22 | 58.79 | 61.45 |
| 60 | 64.20 | 67.06 | 70.03 | 73.11 | 76.30 | 79.60 | 83.02 | 86.56 | 90.22 | 94.00 |
| 70 | 97.90 | 101.95 | 106.10 | 110.41 | 114.85 | 119.45 | 124.20 | 129.10 | 134.15 | 139.40 |
| 80 | 144.80 | 150.30 | 156.05 | 161.95 | 168.00 | 174.25 | 181.70 | 187.30 | 194.10 | 201.15 |
| 90 | 208.35 | 215.80 | 223.45 | 231.30 | 239.35 | 247.70 | 256.20 | 265.00 | 274.00 | 283.25 |
| 100 | 292.75 | 302.50 | 312.50 | 322.80 | 333.35 | 344.15 | 355.15 | 366.65 | 378.30 | 390.25 |
| 110 | 402.55 | 415.10 | 427.95 | 441.15 | 454.65 | 468.50 | 482.65 | 497.20 | 512.05 | 527.25 |
| 120 | 542.80 | 558.70 | 575.05 | 591.70 | 608.75 | 626.15 | 643.95 | 662.15 | 680.75 | 699.65 |
| 130 | 718.95 | 738.65 | 758.80 | -_ | - - | - - | - - |  |  |  |

Bromobenzene

| 40 |  |  |  |  |  | 12.40 | 13.06 | 13.75 | 14.47 | 15.22 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 16.00 | 16.82 | 17.68 | 18.58 | 19.52 | 20.50 | 21.52 | 22.59 | 23.71 | 24.88 |
| 60 | 26.10 | 27.36 | 28.68 | 30.06 | 31.50 | 33.00 | 34.56 | 36.18 | 37.86 | 39.60 |
| 70 | 41.40 | 43.28 | 45.24 | 47.28 | 49.40 | 51.60 | 53.88 | 56.25 | 58.71 | 61.26 |
| 80 | 63.90 | 66.64 | 69.48 | 72.42 | 75.46 | 78.60 | 81.84 | 85.20 | 88.68 | 92.28 |
| 90 | 96.00 | 99.84 | 103.80 | 107.88 | 112.08 | 116.40 | 120.86 | 125.46 | 130.20 | 135.08 |
| 100 | 140.10 | 145.26 | 150.57 | 156.03 | 161.64 | 167.40 | 173.32 | 179.41 | 185.67 | 192.10 |
| 110 | 198.70 | 205.48 | 212.44 | 219.58 | 226.90 | 234.40 | 242.10 | 250.00 | 258.10 | 266.40 |
| 120 | 274.90 | 283.65 | 292.60 | 301.75 | 311.15 | 320.80 | 330.70 | 340.80 | 351.15 | 361.80 |
| 130 | 372.65 | 383.75 | 395.10 | 406.70 | 418.60 | 430.75 | 443.20 | 455.90 | 468.90 | 482.20 |
| 140 | 495.80 | 509.70 | 523.90 | 538.40 | 553.20 | 568.35 | 583.85 | 599.65 | 615.75 | 632.25 |
| 150 | 649.05 | 666.25 | 683.80 | 701.65 | 719.95 | 738.55 | 757.55 | 776.95 | 796.70 | 816.90 |
|  |  |  |  |  | Aniline |  |  |  |  |  |
| 80 | 18.80 | 19.78 | 20.79 | 21.83 | 22.90 | 24.00 | 25.14 | 26.32 | 27.54 | 28.80 |
| 90 | 30.10 | 31.44 | 32.83 | 34.27 | 35.76 | 37.30 | 38.90 | 40.56 | 42.28 | 44.06 |
| 100 | 45.90 | 47.80 | 49.78 | 51.84 | 53.98 | 56.20 | 58.50 | 60.88 | 63.34 | 65.88 |
| 110 | 68.50 | 71.22 | 74.04 | 76.96 | 79.98 | 83.10 | 86.32 | 89.66 | 93.12 | 96.70 |
| 120 | 100.40 | 104.22 | 108.17 | 112.25 | 116.46 | 120.80 | 125.28 | 129.91 | 134.69 | 139.62 |
| 130 | 144.70 | 149.94 | 155.34 | 160.90 | 166.62 | 172.50 | 178.56 | 184.80 | 191.22 | 197.82 |
| 140 | 204.60 | 211.58 | 218.76 | 226.14 | 233.72 | 241.50 | 249.50 | 257.72 | 266.16 | 274.82 |
| 150 | 283.70 | 292.80 | 302.15 | 311.75 | 321.60 | 331.70 | 342.05 | 352.65 | 363.50 | 374.60 |
| 160 | 386.00 | 397.65 | 409.60 | 421.80 | 434.30 | 447.10 | 460.20 | 473.60 | 487.25 | 501.25 |
| 170 | 515.60 | 530.20 | 545.20 | 560.45 | 576.10 | 592.05 | 608.35 | 625.05 | 642.05 | 659.45 |
| 180 | 677.15 | 695.30 | 713.75 | 732.65 | 751.90 | 771.50 | _- | - - | -_ |  |

(continued)

## TABLE 368.-VAPOR PRESSURE OF A NUMBER OF LIQUIDS ( mmHg ) (concluded)

Methyl salicylate, bromonaphthalene, and mercury
Methyl salicylate

| ${ }^{\text {Temp. }}$. | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 70 | 2.40 | 2.58 | 2.77 | 2.97 | 3.18 | 3.40 | 3.62 | 3.85 | 4.09 | 4.34 |
| 80 | 4.60 | 4.87 | 5.15 | 5.44 | 5.74 | 6.05 | 6.37 | 6.70 | 7.05 | 7.42 |
| 90 | 7.80 | 8.20 | 8.62 | 9.06 | 9.52 | 9.95 | 10.44 | 10.95 | 11.48 | 12.03 |
| 100 | 12.60 | 13.20 | 13.82 | 14.47 | 15.15 | 15.85 | 16.58 | 17.34 | 18.13 | 18.95 |
| 110 | 19.80 | 20.68 | 21.60 | 22.55 | 23.53 | 24.55 | 25.61 | 26.71 | 27.85 | 29.03 |
| 120 | 30.25 | 31.52 | 32.84 | 34.21 | 35.63 | 37.10 | 38.67 | 40.24 | 41.84 | 43.54 |
| 130 | 45.30 | 47.12 | 49.01 | 50.96 | 52.97 | 55.05 | 57.20 | 59.43 | 61.73 | 64.10 |
| 140 | 66.55 | 69.08 | 71.69 | 74.38 | 77.15 | 80.00 | 82.94 | 85.97 | 89.09 | 92.30 |
| 150 | 95.60 | 99.00 | 102.50 | 106.10 | 109.80 | 113.60 | 117.51 | 121.53 | 125.66 | 129.90 |
| 160 | 134.25 | 138.72 | 143.31 | 148.03 | 152.88 | 157.85 | 162.95 | 168.19 | 173.56 | 179.06 |
| 170 | 184.70 | 190.48 | 196.41 | 202.49 | 208.72 | 215.10 | 221.65 | 228.30 | 235.15 | 242.15 |
| 180 | 249.35 | 256.70 | 264.20 | 271.90 | 279.75 | 287.80 | 296.00 | 304.48 | 313.05 | 321.85 |
| 190 | 330.85 | 340.05 | 349.45 | 359.05 | 368.85 | 378.90 | 389.15 | 399.60 | 410.30 | 421.20 |
| 200 | 432.35 | 443.75 | 455.35 | 467.25 | 479.35 | 491.70 | 504.35 | 517.25 | 530.40 | 543.80 |
| 210 | 557.50 | 571.45 | 585.70 | 600.25 | 61505 | 630.15 | 645.55 | 661.25 | 677.25 | 693.60 |
| 220 | 710.10 | 727.05 | 744.35 | 761.90 | 779.85 | 798.10 |  |  |  |  |
| Bromonaphthalene |  |  |  |  |  |  |  |  |  |  |
| 110 | 3.60 | 3.74 | 3.89 | 4.05 | 4.22 | 4.40 | 4.59 | 4.79 | 5.00 | 5.22 |
| 120 | 5.45 | 5.70 | 5.96 | 6.23 | 6.51 | 6.80 | 7.10 | 7.42 | 7.76 | 8.12 |
| 130 | 8.50 | 8.89 | 9.29 | 9.71 | 10.15 | 10.60 | 11.07 | 11.56 | 12.07 | 12.60 |
| 140 | 13.15 | 13.72 | 14.31 | 14.92 | 15.55 | 16.20 | 16.87 | 17.56 | 18.28 | 19.03 |
| 150 | 19.80 | 20.59 | 21.41 | 22.25 | 23.11 | 24.00 | 24.92 | 25.86 | 26.83 | 27.83 |
| 160 | 28.85 | 29.90 | 30.98 | 32.09 | 33.23 | 34.40 | 35.60 | 36.83 | 38.10 | 39.41 |
| 170 | 40.75 | 42.12 | 43.53 | 44.99 | 46.50 | 48.05 | 49.64 | 51.28 | 52.96 | 54.68 |
| 180 | 56.45 | 58.27 | 60.14 | 62.04 | 64.06 | 66.10 | 68.19 | 70.34 | 72.55 | 74.82 |
| 190 | 77.15 | 79.54 | 81.99 | 84.51 | 87.10 | 89.75 | 92.47 | 95.26 | 98.12 | 101.05 |
| 200 | 104.05 | 107.12 | 110.27 | 113.50 | 116.81 | 120.20 | 123.67 | 127.22 | 130.86 | 134.59 |
| 210 | 138.40 | 142.30 | 146.29 | 150.38 | 154.57 | 158.85 | 163.25 | 167.70 | 172.30 | 176.95 |
| 220 | 181.75 | 186.65 | 191.65 | 196.75 | 202.00 | 207.35 | 212.80 | 218.40 | 224.15 | 230.00 |
| 230 | 235.95 | 242.05 | 248.30 | 254.65 | 261.20 | 267.85 | 274.65 | 281.60 | 288.70 | 295.95 |
| 240 | 303.35 | 310.90 | 318.65 | 326.50 | 334.55 | 342.75 | 351.10 | 359.65 | 368.40 | 377.30 |
| 250 | 386.35 | 395.60 | 405.05 | 414.65 | 424.45 | 434.45 | 444.65 | 455.00 | 465.60 | 476.35 |
| 260 | 487.35 | 498.55 | 509.90 | 521.50 | 533.35 | 545.35 | 557.60 | 570.05 | 582.70 | 595.60 |
| 270 | 608.75 | 622.10 | 635.70 | 649.50 | 663.55 | 677.85 | 692.40 | 707.15 | 722.15 | 737.45 |
| Mercury |  |  |  |  |  |  |  |  |  |  |
| 270 | 123.92 | 126.97 | 130.08 | 133.26 | 136.50 | 139.81 | 143.18 | 146.61 | 150.12 | 153.70 |
| 280 | 157.35 | 161.07 | 164.86 | 168.73 | 172.67 | 176.79 | 180.88 | 185.05 | 189.30 | 193.63 |
| 290 | 198.04 | 202.53 | 207.10 | 211.76 | 216.50 | 221.33 | 226.25 | 231.25 | 236.34 | 241.53 |
| 300 | 246.81 | 252.18 | 257.65 | 263.21 | 268.87 | 274.63 | 280.48 | 286.43 | 292.49 | 298.66 |
| 310 | 304.93 | 311.30 | 317.78 | 324.37 | 331.08 | 337.89 | 344.81 | 351.85 | 359.00 | 366.28 |
| 320 | 373.67 | 381.18 | 388.81 | 396.56 | 404.43 | 412.44 | 420.58 | 428.83 | 437.22 | 445.75 |
| 330 | 454.41 | 463.20 | 472.12 | 481.19 | 490.40 | 499.74 | 509.22 | 518.85 | 52863 | 538.56 |
| 340 | 548.64 | 558.87 | 569.25 | 579.78 | 590.48 | 601.33 | 612.34 | 623.51 | 634.85 | 646.36 |
| 350 | 658.03 | 669.86 | 681.86 | 694.04 | 706.40 | 718.94 | 731.65 | 744.54 | 757.61 | 770.87 |
| 360 | 784.31 |  |  |  |  |  |  |  |  |  |

## TABLE 369.-VAPOR PRESSURE OF SOLUTIONS OF SALTS IN WATER

The first column gives the chemical formula of the salt. The headings of the other columns give the number of gram-molecules of the salt in a liter of water. The numbers in these columns give the lowering of the vapor pressure produced by the salt at the temperature of boiling water under 76 cmHg .

| Subitance | 0.5 | 1.0 | 2.0 | 3.0 | 4.0 | 5.0 | 6.0 | 8.0 | 10.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Al}_{2}\left(\mathrm{SO}_{4}\right)_{3}$ | 12.8 | 36.5 |  |  |  |  |  |  |  |
| $\mathrm{AlCl}_{3}$ | 22.5 | 61.0 | 179.0 | 318.0 |  |  |  |  |  |
| $\mathrm{BaS}_{2} \mathrm{O}_{6}$ | 6.6 | 15.4 | 34.4 |  |  |  |  |  |  |
| $\mathrm{Ba}(\mathrm{OH})_{2}$ | 12.3 | 22.5 | 39.0 |  |  |  |  |  |  |
| $\mathrm{Ba}\left(\mathrm{NO}_{3}\right)_{2}$ | 13.5 | 27.0 |  |  |  |  |  |  |  |
| $\mathrm{Ba}\left(\mathrm{ClO}_{3}\right)_{2}$ | 15.8 | 33.3 | 70.5 | 108.2 |  |  |  |  |  |
| $\mathrm{BaCl}_{2}$ | 16.4 | 36.7 | 77.6 |  |  |  |  |  |  |
| $\mathrm{BaBr}_{2}$ | 16.8 | 38.8 | 91.4 | 150.0 | 204.7 |  |  |  |  |
| $\mathrm{CaS}_{2} \mathrm{O}_{3}$ | 9.9 | 23.0 | 56.0 | 106.0 |  |  |  |  |  |
| $\mathrm{Ca}\left(\mathrm{NO}_{3}\right)_{2}$ | 16.4 | 34.8 | 74.6 | 139.3 | 161.7 | 205.4 |  |  |  |
| $\mathrm{CaCl}_{2}$ | 17.0 | 39.8 | 95.3 | 166.6 | 241.5 | 319.5 |  |  |  |
| $\mathrm{CaBr}_{2}$ | 17.7 | 44.2 | 105.8 | 191.0 | 283.3 | 368.5 |  |  |  |
| $\mathrm{CdSO}_{4}$ | 4.1 | 8.9 | 18.1 |  |  |  |  |  |  |
| $\mathrm{CdI}_{2}$ | 7.6 | 14.8 | 33.5 | 52.7 |  |  |  |  |  |
| $\mathrm{CdBr}_{2}$ | 8.6 | 17.8 | 36.7 | 55.7 | 80.0 |  |  |  |  |
| $\mathrm{CdCl}_{2}$ | 9.6 | 18.8 | 36.7 | 57.0 | 77.3 | 99.0 |  |  |  |
| $\mathrm{Cd}\left(\mathrm{NO}_{3}\right)_{2}$ | 15.9 | 36.1 | 78.0 |  |  |  |  |  |  |
| $\mathrm{Cd}\left(\mathrm{ClO}_{3}\right)_{2}$ | 17.5 |  |  |  |  |  |  |  |  |
| $\mathrm{CoSO}_{4}$ | 5.5 | 10.7 | 22.9 | 45.5 |  |  |  |  |  |
| $\mathrm{CoCl}_{2}$ | 15.0 | 34.8 | 83.0 | 136.0 | 186.4 |  |  |  |  |
| $\mathrm{Co}\left(\mathrm{NO}_{3}\right)_{2}$ | 17.3 | 39.2 | 89.0 | 152.0 | 218.7 | 282.0 | 332.0 |  |  |
| $\mathrm{FeSO}_{4}$ | 5.8 | 10.7 | 24.0 | 42.4 |  |  |  |  |  |
| $\mathrm{H}_{3} \mathrm{BO}_{3}$ | 6.0 | 12.3 | 25.1 | 38.0 | 51.0 |  |  |  |  |
| $\mathrm{H}_{3} \mathrm{PO}_{4}$ | 6.6 | 14.0 | 28.6 | 45.2 | 62.0 | 81.5 | 103.0 | 146.9 | 189.5 |
| $\mathrm{H}_{3} \mathrm{AsO}_{4}$ | 7.3 | 15.0 | 30.2 | 46.4 | 64.9 |  |  |  |  |
| $\mathrm{H}_{2} \mathrm{SO}_{4}$ | 12.9 | 26.5 | 62.8 | 104.0 | 148.0 | 198.4 | 247.0 | 343.2 |  |
| $\mathrm{KH}_{2} \mathrm{PO}_{4}$ | 10.2 | 19.5 | 33.3 | 47.8 | 60.5 | 73.1 | 85.2 |  |  |
| $\mathrm{KNO}_{3}$ | 10.3 | 21.1 | 40.1 | 57.6 | 74.5 | 88.2 | 102.1 | 126.3 | 148.0 |
| $\mathrm{KClO}_{3}$ | 10.6 | 21.6 | 42.8 | 62.1 | 80.0 |  |  |  |  |
| $\mathrm{KBrO}_{3}$ | 10.9 | 22.4 | 45.0 |  |  |  |  |  |  |
| $\mathrm{KHSO}_{4}$ | 10.9 | 21.9 | 43.3 | 65.3 | 85.5 | 107.8 | 129.2 | 170.0 |  |
| $\mathrm{KNO}_{2}$ | 11.1 | 22.8 | 44.8 | 67.0 | 90.0 | 110.5 | 130.7 | 167.0 | 198.8 |
| $\mathrm{KClO}_{4}$ | 11.5 | 22.3 |  |  |  |  |  |  |  |
| KCl | 12.2 | 24.4 | 48.8 | 74.1 | 100.9 | 128.5 | 152.2 |  |  |
| $\mathrm{KHCO}_{3}$ | 11.6 | 23.6 | 59.0 | 77.6 | 104.2 | 132.0 | 160.0 | 210.0 | 255.0 |
|  | 12.5 | 25.3 | 52.2 | 82.6 | 112.2 | 141.5 | 171.8 | 225.5 | 278.5. |
| $\mathrm{K}_{2} \mathrm{C}_{2} \mathrm{O}_{4}$ | 13.9 | 28.3 | 59.8 | 94.2 | 131.0 |  |  |  |  |
| $\mathrm{K}_{2} \mathrm{WO}_{4}$ | 13.9 | 33.0 | 75.0 | 123.8 | 175.4 | 226.4 |  |  |  |
| $\mathrm{K}_{2} \mathrm{CO}_{3}$ | 14.4 | 31.0 | 68.3 | 105.5 | 152.0 | 209.0 | 258.8 | 350.0 |  |
| KOH | 15.0 | 29.5 | 64.0 | 99.2 | 140.0 | 181.8 | 223.0 | 309.5 | 387.8 |
| $\mathrm{K}_{2} \mathrm{CrO}_{4}$ | 16.2 | 29.5 | 60.0 |  |  |  |  |  |  |
| $\mathrm{LiNO}_{3}$ | 12.2 | 25.9 | 55.7 | 88.9 | 122.2 | 155.1 | 188.0 | 253.4 | 309.2 |
| LiCl | 12.1 | 25.5 | 57.1 | 95.0 | 132.5 | 175.5 | 219.5 | 311.5 | 393.5 |
| LiBr | 12.2 | 26.2 | 60.0 | 97.0 | 140.0 | 186.3 | 241.5 | 341.5 | 438.0 |
| $\mathrm{Li}_{2} \mathrm{SO} 4$ | 13.3 | 28.1 | 56.8 | 89.0 |  |  |  |  |  |
| LiHSO4 | 12.8 | 27.0 | 57.0 | 93.0 | 130.0 | 168.0 |  |  |  |
| LiI | 13.6 | 28.6 | 64.7 | 105.2 | 154.5 | 206.0 | 264.0 | 357.0 | 445.0 |
| $\mathrm{Li}_{2} \mathrm{SiF}_{8}$ | 15.4 | 34.0 | 70.0 | 106.0 |  |  |  |  |  |
| LiOH | 15.9 | 37.4 | 78.1 |  |  |  |  |  |  |
| $\mathrm{Li}_{2} \mathrm{CrO} 4$ | 16.4 | 32.6 | 74.0 | 120.0 | 171.0 |  |  |  |  |
|  |  |  |  | ntinued) |  |  |  |  |  |

TABLE 369.-VAPOR PRESSURE OF SOLUTIONS OF SALTS IN WATER
(concluded)

| Substance | 0.5 | 1.0 | 2.0 | 3.0 | 4.0 | 5.0 | 6.0 | 8.0 | 10.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{MgSO}_{4}$ | 6.5 | 12.0 | 24.5 | 47.5 |  |  |  |  |  |
| $\mathrm{MgCl}_{2}$ | 16.8 | 39.0 | 100.5 | 183.3 | 277.0 | 377.0 |  |  |  |
| $\mathrm{Mg}\left(\mathrm{NO}_{3}\right)_{2}$ | 17.6 | 42.0 | 101.0 | 174.8 |  |  |  |  |  |
| $\mathrm{MgBr}_{2}$ | 17.9 | 44.0 | 115.8 | 205.3 | 298.5 |  |  |  |  |
| $\mathrm{MgH}_{2}\left(\mathrm{SO}_{4}\right)_{2}$ | 18.3 | 46.0 | 116.0 |  |  |  |  |  |  |
| $\mathrm{MnSO}_{4}$ | 6.0 | 10.5 | 21.0 |  |  |  |  |  |  |
| $\mathrm{MnCl}_{2}$ | 15.0 | 34.0 | 76.0 | 122.3 | 167.0 | 209.0 |  |  |  |
| $\mathrm{NaH}_{2} \mathrm{PO} 4$ | 10.5 | 20.0 | 36.5 | 51.7 | 66.8 | 82.0 | 96.5 | 126.7 | 157.1 |
| $\mathrm{NaHSO}_{4}$ | 10.9 | 22.1 | 47.3 | 75.0 | 100.2 | 126.1 | 148.5 | 189.7 | 231.4 |
| $\mathrm{NaNO}_{3}$ | 10.6 | 22.5 | 46.2 | 68.1 | 90.3 | 111.5 | 131.7 | 167.8 | 198.8 |
| $\mathrm{NaClO}_{3}$ | 10.5 | 23.0 | 48.4 | 73.5 | 98.5 | 123.3 | 147.5 | 196.5 | 223.5 |
| $\left(\mathrm{NaPO}_{3}\right)_{8}$ | 11.6 |  |  |  |  |  |  |  |  |
| NaOH | 11.8 | 22.8 | 48.2 | 77.3 | 107.5 | 139.1 | 172.5 | 243.3 | 314.0 |
| $\mathrm{NaNO}_{2}$ | 11.6 | 24.4 | 50.0 | 75.0 | 98.2 | 122.5 | 146.5 | 189.0 | 226.2 |
| $\mathrm{Na}_{2} \mathrm{HPO}_{4}$ | 12.1 | 23.5 | 43.0 | 60.0 | 78.7 | 99.8 | 122.1 |  |  |
| $\mathrm{NaHCO}_{3}$ | 12.9 | 24.1 | 48.2 | 77.6 | 102.2 | 127.8 | 152.0 | 198.0 | 239.4 |
| $\mathrm{Na}_{2} \mathrm{SO}$ | 12.6 | 25.0 | 48.9 | 74.2 |  |  |  |  |  |
| NaCl | 12.3 | 25.2 | 52.1 | 80.0 | 111.0 | 143.0 | 176.5 |  |  |
| $\mathrm{NaBrO}_{3}$ | 12.1 | 25.0 | 54.1 | 81.3 | 108.8 | 136.0 |  |  |  |
| NaBr | 12.6 | 25.9 | 57.0 | 89.2 | 124.2 | 159.5 | 197.5 | 268.0 |  |
| NaI | 12.1 | 25.6 | 60.2 | 99.5 | 136.7 | 177.5 | 221.0 | 301.5 | 370.0 |
| $\mathrm{Na}_{4} \mathrm{P}_{2} \mathrm{O}_{7}$ | 13.2 | 22.0 |  |  |  |  |  |  |  |
| $\mathrm{Na}_{2} \mathrm{CO}_{3}$ | 14.3 | 27.3 | 53.5 | 80.2 | 111.0 |  |  |  |  |
| $\mathrm{Na}_{2} \mathrm{C}_{2} \mathrm{O}_{4}$ | 14.5 | 30.0 | 65.8 | 105.8 | 146.0 |  |  |  |  |
| $\mathrm{Na}_{2} \mathrm{WO}$, | 14.8 | 33.6 | 71.6 | 115.7 | 162.6 |  |  |  |  |
| $\mathrm{Na}_{3} \mathrm{PO}_{4}$ | 16.5 | 30.0 | 52.5 |  |  |  |  |  |  |
| $\left(\mathrm{NaPO}_{3}\right)_{3}$ | 17.1 | 36.5 |  |  |  |  |  |  |  |
| $\mathrm{NH}_{4} \mathrm{NO}_{3}$ | 12.8 | 22.0 | 42.1 | 62.7 | 82.9 | 103.8 | 121.0 | 152.2 | 180.0 |
| $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{SiF}_{8}$ | 11.5 | 25.0 | 44.5 |  |  |  |  |  |  |
| $\mathrm{NH}_{4} \mathrm{Cl}$ | 12.0 | 23.7 | 45.1 | 69.3 | 94.2 | 118.5 | 138.2 | 179.0 | 213.8 |
| $\mathrm{NH}_{4} \mathrm{HSO}_{4}$ | 11.5 | 22.0 | 46.8 | 71.0 | 94.5 | 118. | 139.0 | 181.2 | 218.0 |
| $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{SO}_{4}$ | 11.0 | 24.0 | 46.5 | 69.5 | 93.0 | 117.0 | 141.8 |  |  |
| $\mathrm{NH}_{4} \mathrm{Br}$ | 11.9 | 23.9 | 48.8 | 74.1 | 99.4 | 121.5 | 145.5 | 190.2 | 228.5 |
| $\mathrm{NH}_{4} \mathrm{I}$ | 12.9 | 25.1 | 49.8 | 78.5 | 104.5 | 132.3 | 156.0 | 200.0 | 243.5 |
| $\mathrm{NiSO}_{4}$ | 5.0 | 10.2 | 21.5 |  |  |  |  |  |  |
| $\mathrm{NiCl}_{2}$ | 16.1 | 37.0 | 86.7 | 147.0 | 212.8 |  |  |  |  |
| $\mathrm{Ni}\left(\mathrm{NO}_{3}\right)_{2}$ | 16.1 | 37.3 | 91.3 | 156.2 | 235.0 |  |  |  |  |
| $\mathrm{Pb}\left(\mathrm{NO}_{3}\right)_{2}$ | 12.3 | 23.5 | 45.0 | 63.0 |  |  |  |  |  |
| $\mathrm{Sr}\left(\mathrm{SO}_{3}\right)_{2}$ | 7.2 | 20.3 | 47.0 |  |  |  |  |  |  |
| $\mathrm{Sr}\left(\mathrm{NO}_{3}\right)_{2}$ | 15.8 | 31.0 | 64.0 | 97.4 | 131.4 |  |  |  |  |
| $\mathrm{SrCl}_{2}$ | 16.8 | 38.8 | 91.4 | 156.8 | 223.3 | 281.5 |  |  |  |
| $\mathrm{SrBr}_{2}$ | 17.8 | 42.0 | 101.1 | 179.0 | 267.0 |  |  |  |  |
| ZnSO | 4.9 | 10.4 | 21.5 | 42.1 | 66.2 |  |  |  |  |
| $\mathrm{ZnCl}_{2}$ | 9.2 | 18.7 | 46.2 | 75.0 | 107.0 | 153.0 | 195.0 |  |  |
| $\mathrm{Zn}\left(\mathrm{NO}_{3}\right)_{2}$ | 16.6 | 39.0 | 93.5 | 157.5 | 223.8 |  |  |  |  |

## TABLES 370-406.-VARIOUS ELECTRICAL CHARACTERISTICS ()F MATERIALS

The fundamental electrical and magnetic definitions and the values of the practical units of current, voltage, and other electrical quantities, have been given (Tables 2-5). Some data will now be presented on electrical characteristics of various materials.

## TABLE 370.-THE EFFECT OF ELECTRIC CURRENT ON THE HUMAN BODY ${ }^{188 \mathrm{~s}}$

Some thought must be given to the electrical characteristics of the human body, since careless handling of electric circuits is very dangerous. The regular 120 -volt circuit is dangerous, and any voltage above this increascs the hazard. No bare contacts should be permitted where anyone might come in contact with them.


Since the resistance of the human body for direct current (hand to foot or hand to hand), neglecting the contact resistance, is $5,000-10,000$ ohms, good contact with electric circuits must be avoided. For alternating current the resistance is much lower.

[^165]
## TABLE 371.-TRIBOELECTRICITY

## Part 1.-The tribo-electric series

The following table is so arranged that any material in the list becomes positively electrified when rubbed by one lower in the list. The phenomenom depends upon surface conditions and circumstances may alter the relative positions in the list.

| Asbestos (sheet). | 13 Silk. | 24 Amber. |
| :---: | :---: | :---: |
| 2 Rabbit's fur, hair ( Hg ). | $14 \mathrm{Al}, \mathrm{Mn}, \mathrm{Zn}, \mathrm{Cd}, \mathrm{Cr}, \mathrm{felt}$, | 25 Slate, chrome-alum. |
| ${ }^{3}$ Glass (combn. tubing). | hand, wash-leather. | 26 Shellac, resin, sealing-wax. |
| Vitreous silica, oppossum's | 15 Filter paper. | 27 Ebonite. |
| furs. (fusn) | 16 Vulcanized fiber. |  |
| Glass (fusn.). | 17 Cotton. | $\mathrm{S}_{\text {b, }} \mathrm{Ag}, \mathrm{Pd}, \mathrm{C}, \mathrm{Te}$, |
| Mica. | 18 Magnalium | Eureka, straw, copper |
| 7 Wool. | 19 K -alum, rock-salt, satin | sulfatc, brass. |
| Glass (pol.), quartz (pol.), glazed porcelain. | spar. 20 Woods, Fe. | 29 Para rubber, iron alum. 30 Guttapercha. |
| 9 Glass (broken edge), ivory. | 21 Unglazed porcelain, sal- | 31 Sulfur. |
| 10 Calcite. | ammoniac. | $32 \mathrm{Pt} \mathrm{Ag},$.Au . |
| 112 Cat 's fur. Pb , fluorspar | 22 K -bichromate, paraffin, | 33 Celluloid. |
| $12 \mathrm{Ca}, \mathrm{Mg}, \mathrm{Pb}$, fluorspar, borax. | tinned-Fe. <br> 23 Cork, ebony. | 34 Indiarubber. |

Part 2.-Triboelectric series in voltage of a number of metals as compared with silica (as $O$ ) ${ }^{139}$


Solids with liquids and liquids with liquids in air
Temperature of substances during experiment about $16^{\circ} \mathrm{C}$

|  | C | Cu | F e | Pb | Pt | Sn | Zn | $. ._{\mathrm{Zn}} \mathrm{malg} .$ | Brass | Distilled water |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | . 01 | . 269 |  |  | . 285 |  | $\int-.105$ |  |  |  |
| $\mathrm{H}_{2} \mathrm{O}$ | to to 17 | to .100 | . 148 | . 1712 | $\begin{gathered} \text { to } \\ .345 \end{gathered}$ |  | $\left\{\begin{array}{c} \text { to } \\ +.156 \end{array}\right.$ | . 100 | . 231 |  |
| Alum. sat.sol. |  | -. 127 | -. 653 | -. 139 | . 246 | -. 225 | -. 536 |  | . 014 |  |
| CuSO sol. ${ }^{\text {sun }}$. ${ }^{\text {a }}$ |  |  |  |  |  |  |  |  |  |  |
| sp.gr. 1.087 |  | . 103 |  |  |  |  |  |  |  |  |
| Sea salt sol. ${ }^{\text {a }}$.... 070 |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{NH}_{4} \mathrm{Cl}$, sat.sol. |  | -. 396 | -. 652 | -. 189 | . 059 | -. 364 | -. 637 |  | -. 348 |  |
| $\mathrm{ZnSO}_{4}$ sol. $1.125^{\circ}$ <br> at $4^{\circ} \mathrm{C}$ $-.238$ |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{ZnSO}_{4}$ sat.sol. ... |  |  |  |  |  |  | -. 430 | -. 284 |  | -. 200 |
| One part $\mathrm{H}_{2} \mathrm{O}+$ 3, sat. ZnSO |  |  |  |  |  |  | -. 444 |  |  |  |
| Strong $\mathrm{H}_{2} \mathrm{SO}_{4}$ in water: |  |  |  |  |  |  |  |  |  |  |
| 1 to 20 by wt. |  |  |  |  |  |  | -. 344 |  |  |  |
| 1 to 10 by vol. ....\{ $\left\{\begin{array}{c}\text { about } \\ -.035\end{array}\right.$ |  |  |  |  |  |  |  |  |  |  |
| 1to 5 by wt. ..... ... ... ... ... ... ... . 429 |  |  |  |  |  |  |  |  |  |  |
| 5 to 1 by wt. | .01 to 3.0 |  |  | -. 120 |  | -. 25 | ... |  | -. 016 |  |
| Con. $\mathrm{H}_{2} \mathrm{SO}_{4}$ | .55 to .85 | 1.113 |  | $\left\{\begin{array}{c} .72 \\ \text { to } \\ 1.252 \end{array}\right.$ | $\begin{aligned} & 1.3 \\ & \text { to } \\ & 1.6 \end{aligned}$ | $\ldots$ | $\ldots$ | . 848 |  | 1.298 |
| on. $\mathrm{HNO}_{3}$ |  |  |  |  | . 672 |  |  |  |  |  |

Mercurous sulfate paste, $\mathrm{Hg},+.475$. Sat.CuSO ${ }_{4}$ sol., $\mathrm{H}_{2} \mathrm{O},-.043$; sat. $\mathrm{ZnSO}_{4}$ sol., $+.095 ; 1$ pt. $\mathrm{H}_{2} \mathrm{O}, 3$ pt. $\mathrm{ZnSO}_{4}+.102$.
Concentrated $\mathrm{H}_{2} \mathrm{SO}_{4}, \mathrm{H}_{2} \mathrm{O},+1.298$; sat.alum.sol., $+1.456 ; \mathrm{CnSO}_{4}$ sat. $+1.269 ; \mathrm{ZnSO}_{4}$ sat.sol., +1.699 .

[^166]
## TABLE 373.-THERMAL ELECTROMOTIVE FORCE OF ALUMINUM VERSUS PLATINUM ${ }^{140}$

Temperature versus emf

| ${ }^{\circ} \mathrm{C}$ | mv | ${ }^{\circ} \mathrm{C}$ | mv | ${ }^{\circ} \mathrm{C}$ | mv |
| ---: | ---: | ---: | :---: | :---: | :---: |
| 0 | .000 | 240 | 1.374 | 480 | 3.703 |
| 20 | +.062 | 260 | 1.538 | 500 | 3.931 |
| 40 | .135 | 280 | 1.708 | 520 | 4.164 |
| 60 | .218 | 300 | 1.884 | 540 | 4.403 |
| 80 | .312 | 320 | 2.065 | 560 | 4.647 |
| 100 | .416 | 340 | 2.252 | 580 | 4.896 |
| 120 | .529 | 360 | 2.444 | 600 | 5.150 |
| 140 | .651 | 380 | 2.641 | 620 | 5.409 |
| 160 | .781 | 400 | 2.843 | 640 | 5.673 |
| 180 | .919 | 420 | 3.050 | 660 | 5.942 |
| 200 | 1.064 | 440 | 3.262 |  |  |
| 220 | 1.216 | 460 | 3.480 |  |  |

[^167]
## TABLE 374.-COMPOSITION AND ELECTROMOTIVE FORCE OF VOLTAIC CELLS

The electromotive forces given in this table approximately represent what may be expected from a cell in good working order, but, with the exception of the standard cells, all of them are subject to considerable variation.

Part 1.-Double fluid cells

| Name <br> of cell | Negative pole | Solution | Positive | Solution | $\underset{\text { in }}{\text { in volis }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Bunsen | Amalg. Z " | 1, $\mathrm{H}_{2} \mathrm{SO}_{4} ; 12, \mathrm{H}_{2} \mathrm{O}$ | C | Fuming $\mathrm{HNO}_{3}$ <br> $\mathrm{HNO}_{3}$; dens. 1.38 | $\begin{aligned} & 1.94 \\ & 1.86 \end{aligned}$ |
| Chromate | " " | $\begin{aligned} & \text { 12. } \mathrm{K}_{2} \mathrm{Cr}_{2} \mathrm{O}_{7} ; 25, \mathrm{H}_{2} \mathrm{SO}_{4} ; \\ & 100, \mathrm{H}_{2} \mathrm{O} \end{aligned}$ | " | $1, \mathrm{H}_{2} \mathrm{SO}_{4} ; 12, \mathrm{H}_{2} \mathrm{O}$ | 2.00 |
| " | " " | $1, \mathrm{H}_{2} \mathrm{SO}_{4} ; 12, \mathrm{H}_{2} \mathrm{O}$ | " | $12, \mathrm{~K}_{2} \mathrm{Cr}_{2} \mathrm{O}_{7} ; 100, \mathrm{H}_{2} \mathrm{O}$ | 2.03 |
| Daniell | " " ${ }^{\text {" }}$ | 1. $\mathrm{H}_{2} \mathrm{SO}_{4} ; 4, \mathrm{H}_{2} \mathrm{O}$ | Cu | Sat.sol. $\mathrm{CuSO}_{4} ; 5, \mathrm{H}_{2} \mathrm{O}$ | 1.06 |
|  |  | 1, $\mathrm{H}_{2} \mathrm{SO}_{4} ; 12, \mathrm{H}_{2} \mathrm{O}$ |  |  | 1.09 |
| " | "، "، | $5 \%$ sol. $\mathrm{ZnSO} ; 6 \mathrm{H}_{2} \mathrm{O}$ | " ${ }^{\text {P }}$ | " | 1.08 |
| Grove | " " | $1 \mathrm{H}_{2} \mathrm{SO}_{4} ; 12 \mathrm{H}_{2} \mathrm{O}$ | Pt | Fuming $\mathrm{HNO}_{3}$ | 1.05 1.93 |
|  | " " | Sol. $\mathrm{ZnSO} \mathrm{SO}_{4}$ |  | $\mathrm{HNO}_{3}$ : dens. 1.33 | 1.66 |
| " | " | $\mathrm{H}_{2} \mathrm{SO}_{4}$ sol. ; dens. 1.136 | " | Concent. $\mathrm{HNO}_{3}$ | 1.93 |
| " | " " | $\mathrm{H}_{2} \mathrm{SO}_{4}$; dens. 1.136 | " | $\mathrm{HNO}_{3}$ : dens. 1.33 | 1.79 |
| " | " " | $\mathrm{H}_{2} \mathrm{SO}_{4}$ sol. ; dens. 1.14 | " | $\mathrm{HNO}_{3}$; dens. 1.19 | 1.66 |
| " | "" " | $\mathrm{H}_{2} \mathrm{SO}_{4}$ sol. ; dens. 1.06 | ' |  | 1.61 |
| Partz | "، " | $\underset{\mathrm{NaCl}}{\mathrm{Nol} \text { sol. }}$ | " | $\mathrm{Sol}^{\prime} \mathrm{K}_{2} \mathrm{Cr}_{2} \mathrm{O}_{7}{ }^{\text {a }}$ | 1.88 2.06 |

Part 2.-Single fluid cells


Part 3.-Secondary cells


Part 4.-Standard cells

| Clark | $\mathrm{Zn}+\mathrm{Hg}$ | $\mathrm{ZnSO}_{4}$ | Paste <br> $\mathrm{H}_{2} \mathrm{SO}_{4}+\mathrm{Hg}$ <br> Weston \\| | $\mathrm{Cd}+\mathrm{Hg}$ |
| :--- | :---: | :---: | :---: | :---: |
|  | $\mathrm{CdSO}_{4}$ | Paste <br> CdSO4 +Hg | 1.434 |  |

|| Very low temperature coefficient.

## TABLE 375.-DIFFERENCE OF POTENTIAL BETWEEN METALS IN SOLUTIONS OF SALTS

The following numbers are given by G. Magnanini for the difference of potential in hundredths of a volt between zinc in a normal solution of sulfuric acid and the metals named at the head of the different columns when placed in the solution named in the first column. The solutions were contained in a U-tube, and the sign of the difference of potential is such that the current will flow from the more positive to the less positive through the external circuit.

| Stiength of the solution in gram molecules per liter |  | Zinc* | Cadmium* | Lead | Tin | Copper | Silver |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. of | Salt | Difference of potential in centivolts |  |  |  |  |  |
| . 5 | $\mathrm{H}_{2} \mathrm{SO}_{4}$ | . 0 | 36.6 | 51.3 | 51.3 | 100.7 | 121.3 |
| 1.0 | NaOH | $-32.1$ | 19.5 | 31.8 | . 2 | 80.2 | 95.8 |
| 1.0 | KOH | -42.5 | 15.5 | 32.0 | -1.2 | 77.0 | 104.0 |
| . 5 | $\mathrm{Na}_{2} \mathrm{SO}_{4}$ | 1.4 | 35.6 | 50.8 | 51.4 | 101.3 | 120.9 |
| 1.0 | $\mathrm{Na}_{2} \mathrm{~S}_{2} \mathrm{O}_{3}$ | - 5.9 | 24.1 | 45.3 | 45.7 | 38.8 | 64.8 |
| 1.0 | $\mathrm{KNO}_{3}$ | $11.8{ }^{\dagger}$ | 31.9 | 42.6 | 31.1 | 81.2 | 105.7 |
| 1.0 | $\mathrm{NaNO}_{3}$ | 11.5 | 32.3 | 51.0 | 40.9 | 95.7 | 114.8 |
| . 5 | $\mathrm{K}_{2} \mathrm{CrO}_{4}$ | $23.9 \dagger$ | 42.8 | 41.2 | 40.9 | 94.6 | 121.0 |
| . 5 | $\mathrm{K}_{2} \mathrm{Cr}_{2} \mathrm{O}_{7}$ | 72.8 | 61.1 | 78.4 | 68.1 | 123.6 | 132.4 |
| . 5 | $\mathrm{K}_{2} \mathrm{SO}{ }_{4}$ | 1.8 | 34.7 | 51.0 | 40.9 | 95.7 | 114.8 |
| . 5 | $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{SO}_{4}$ | $-.5$ | 37.1 | 53.2 | $57.6{ }^{\dagger}$ | 101.5 | 125.7 |
| . 25 | $\mathrm{K}_{4} \mathrm{FeC}_{6} \mathrm{~N}_{6}$ | $-6.1$ | 33.6 | 50.7 | 41.2 | - $\dagger$ | 87.8 |
| . 167 | $\mathrm{K}_{4} \mathrm{Fe}_{2}(\mathrm{CN})_{12}$ | $41.0 \ddagger$ | 80.8 | 81.2 | 130.9 | 110.7 | 124.9 |
| 1.0 | KCNS | - 1.2 | 32.5 | 52.8 | 52.7 | 52.5 | 72.5 |
| 1.0 | $\mathrm{NaNO}_{3}$ | 4.5 | 35.2 | 50.2 | 49.0 | 103.6 | $104.6{ }^{8}$ |
| . 5 | $\mathrm{Sr}\left(\mathrm{NO}_{3}\right)_{2}$ | 14.8 | 38.3 | 50.6 | 48.7 | 103.0 | 119.3 |
| . 125 | $\mathrm{Ba}\left(\mathrm{NO}_{3}\right)_{2}$ | 21.9 | 39.3 | 51.7 | 52.8 | 109.6 | 121.5 |
| 1.0 | $\mathrm{KNO}_{3}$ | - ${ }^{\dagger}$ | 35.6 | 47.5 | 49.9 | 104.8 | 115.0 |
| $.2$ | $\mathrm{KClO}_{3}$ | 15-10 ${ }^{\dagger}$ | 39.9 | 53.8 | 57.7 | 105.3 | 120.9 |
| . 167 | $\mathrm{KBrO}_{3}$ | 13-20 ${ }^{+}$ | 40.7 | 51.3 | 50.9 | 111.3 | 120.8 |
| 1.0 | $\mathrm{NH}_{4} \mathrm{Cl}$ | 2.9 | 32.4 | 51.3 | 50.9 | 81.2 | 101.7 |
| 1.0 | KF | 2.8 | 22.5 | 41.1 | 50.8 | 61.3 | 61.5 |
| 1.0 | NaCl |  | 31.9 | 51.2 | 50.3 | 80.9 | 101.3 |
| 1.0 | KBr | 2.3 | 31.7 | 47.2 | 52.5 | 73.6 | 82.4 |
| 1.0 | KCl | - | 32.1 | 51.6 | 52.6 | 81.6 | 107.6 |
| . 5 | $\mathrm{Na}_{2} \mathrm{SO}_{3}$ | $-8.2$ | 28.7 | 41.0 | 31.0 | 68.7 | 103.7 |
| -8 | NaOBr | 18.4 | 41.6 | 73.1 | $70.6{ }^{+}$ | 89.9 | 99.7 |
| 1.0 | $\mathrm{C}_{4} \mathrm{H}_{6} \mathrm{O}_{8}$ | 5.5 | 39.7 | 61.3 | $54.4 \ddagger$ | 104.6 | 123.4 |
| . 5 | $\mathrm{C}_{4} \mathrm{H}_{4} \mathrm{O}_{8}$ | 4.1 | 41.3 | 61.6 | 57.6 | 110.9 | 125.7 |
| . 5 | $\mathrm{C}_{6} \mathrm{H}_{4} \mathrm{KNaO}_{6}$ | - 7.9 | 31.5 | 51.5 | 42-47 | 100.8 | 119.7 |

[^168]The thermoelectric effect of a number of alloys is given in this table, the authority being Ed. Becquerel. They are relative to lead, and for a mean temperature of $50^{\circ} \mathrm{C}$. In reducing the results from copper as a reference metal, the thermoelectric effect of lead to copper was taken as -1.9 .

| Substance |  |  | Substance |  |  | Substance | 运 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Antimony | 806 |  | Antimony | $2)$ |  | Bismuth |  |  |
| Cadmium | 696 |  | Zinc | 1 | 43 | Antimony |  |  |
| Antimony | 4 |  | Tin | $1)$ |  | Bismuth |  |  |
| Cadmium | 2 1 1$\}$ | 146 | Antimony | 12 |  | Antimony |  |  |
| Zinc | 8067 |  | Cadmium | 10 | 35 | Bismuth |  |  |
| Cadmium | 696 | 137 | Zinc | 3 |  | Antimony |  |  |
| Bismuth | 121 |  | Antimony | $\left.\begin{array}{c}10 \\ 1\end{array}\right\}$ | 10.2 | Bismuth |  | -66.9 |
| Antimony Zinc | $\left.\begin{array}{l}806 \\ 406\end{array}\right\}$ | 95 | Antimony | 10 |  | Antimony |  | 66.9 |
| Antimony | 8067 |  | Bismuth | $1\}$ |  | Bismuth |  |  |
| Zinc | 406 | 8.1 | Antimony | 4) |  |  |  |  |
| Bismuth | 121 |  | Iron | $1\}$ | 2.5 | Bismuth |  | 24.5 |
| Antimony | 4 |  | Antimony | 8 ) |  | Selenium |  |  |
| Cadmium | 2 | 76 | Magnesium | $1\}$ |  | Bismuth |  |  |
| Lead | 11 |  | Antimony | 8 ) |  | Zinc |  | 1.1 |
| Antimony | 4) |  | Lead |  |  | Bismuth |  |  |
| Cadmium | 2 | 46 | Bismuth |  | -43.8 | Arsenic |  | 46.0 |
| Zinc | 1 1 |  | Bismuth | $2)$ |  | Bismuth | $1\}$ |  |
| Tin | $1)$ |  | Antimony |  | -33.4 | Bismuth s | $1\}$ | 68.1 |

## TABLE 377.-THERMOELECTRIC EFFECT

A measure of the thermoelectric effect of a circuit of two metals is the electromotive force produced by $1^{\circ} \mathrm{C}$ difference of temperature between the junctions. The thermoelectric effect varies with the temperature, thus: thermoclectric effect $=Q=d E / d t=A+B t$, where $A$ is the thermoelectric effect at $0^{\circ} \mathrm{C}, B$ is a constant, and $t$ is the mean temperature of the junctions. The neutral point is the temperature at which $d E / d t=0$, and its value is $-A / B$. When a current is caused to flow in a circuit of two metals originally at a uniform temperature, heat is liberated at one of the junctions and absorbed at the other. The rate of production or liberation of heat at each junction, or Peltier effect. is given in calories per second, by multiplying the current by the coefficient of the Peltier effect. This coefficient in calories per coulomb $=Q T / \mathcal{F}$, in which $Q$ is in volts per degree $C, T$ is the absolute temperature of the junction, and $\mathcal{F}=4.19$. Heat is also liberated or absorbed in each of the metals as the current flows through portions of varying temperature. The rate of production or liberation of heat in each metal, or the Thomson effect, is given in calories per second by multiplying the current by the coefficient of the Thomson effect. This coefficient, in calories per coulomb $=B T \theta / \dot{f}$, in which $B$ is in volts per degree C, $T$ is the mean absolute temperature of the junctions, and $\theta$ is the difference of temperature of the junctions. ( $B T$ ) is Sir W. Thomson's "Specific Heat of Electricity," The algebraic signs are so chosen in the following table that when $A$ is positive, the current flows in the metal considered from the hot junction to the cold. When $B$ is positive, $Q$ increases (algebraically) with the temperature. The values of $A, B$, and thermoelectric effect in the following table are zeith respect to lcad as the other metal of the thermoelectric circuit. The thermoelectric effect of a couple composed of two metals, 1 and 2 , is given by subtracting the value for 2 from that for 1 ; when this difference is positive, the current flows from the hot junction to the cold in 1. In the following table, $A$ is given in microvolts per degree, $B$ in microvolts per degree per degree, and the neutral point in degrees.

The table has been compiled from the resuits of Becquerel, Matthiessen and Tait; in reducing the results, the electromotive force of the Grove and Daniell cells has been taken as 1.95 and 1.07 volts. The value of constantan was reduced from results given in LandoltBörnstein's tables.

[^169]| Substance | $\underset{\text { Microvolts }}{A}$ | $\stackrel{B}{\text { Microvolts }}$ | Thermoelectric effect at mean temp. of junctions (microvolts) |  | $\begin{aligned} & \text { Neutral } \\ & \text { point } \\ & -\frac{A}{B} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $20^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ |  |
| Aluminum | - . 76 | +. 0039 | - . 68 |  | + 195 |
| Antimony, comm'l pressed wire. |  | - | + 6.0 |  |  |
| " axial |  | - | + 22.6 |  |  |
| equatorial |  |  | + 26.4 |  |  |
| Argentan | -11.94 | -. 0506 | - 12.95 | $-14.47$ | - 236 |
| Arsenic |  | - | - 13.56 | -12.7 |  |
| Bismuth, comm'l pressed wire. |  | - | - 97.0 | - |  |
| " pure " " |  |  | - 89.0 |  |  |
| " crystal, axial |  |  | - 65.0 |  |  |
| "" " equatorial | $+2.63$ | -. 0424 | -45.0 $+\quad 3.48$ | + 4.75 |  |
| Cadmium fused |  | -.0424 |  | + |  |
| Calcium |  |  | - | +8.9 |  |
| Cobalt | - | - | - 22 |  |  |
| Constantan |  |  |  | -19.3 |  |
| Copper | + 1.34 | +. 0094 | + 1.52 | +1.81 | $-143$ |
| ". commercial |  |  | + ${ }^{1} 10$ |  |  |
| Gallium galvanoplastic |  |  | + 3.8 |  |  |
| Gold | $+2.80$ | +. 0101 | + 3.0 | $+3.30$ | [-277] |
| Iron | +17.15 | $-.0482$ | + 16.2 | +14.74 | + 356 |
| " pianoforte wire |  |  | + 17.5 |  |  |
| ". commercial | - |  | - | +12.10 |  |
| Lead |  | . 0000 | $+\quad .00$ | + 9.10 +.00 |  |
| Magnesium | $+2.22$ | -. 0094 | + 2.03 | +1.75 | + 236 |
| Molybdenum |  | - | + 5.9 |  |  |
| Mercury |  |  | - . 413 | $-3.30$ |  |
| Nickel |  |  |  | -15.50 |  |
| " $\left(-18^{\circ}\right.$ to $\left.175^{\circ}\right)$ <br> " $\left(250^{\circ}-300^{\circ}\right)$ | $-21.8$ | $\begin{array}{r} -.0506 \\ +.2384 \end{array}$ | - 22.8 | -24.33 | [-431] |
| " (above $340^{\circ}$ ) . | -3.04 | +. 0506 |  |  |  |
| Palladium ... | - 6.18 | -. 0355 | - 6.9 | - 7.96 | - 174 |
| Phosphorus (red) |  | - | + 29.9 |  |  |
| Platinum |  |  | + . 5 |  |  |
| "، (hardened) | $+2.57$ | -. 0074 | $+\quad 2.42$ | + 2.20 | 347 |
| " (malleable) | - . 60 | -. 0109 | - .818 | - 1.15 | 55 |
| " wire |  |  |  | +. 94 |  |
| " another specimen |  | - | - | $-2.14$ |  |
| Platinum-iridium alloys: |  |  |  |  |  |
| $85 \% \mathrm{Pt}+15 \% \mathrm{Ir}$ | 7.90 | +. 0062 | + 8.03 | +8.21 | [-1274] |
| $90 \% \mathrm{Pt}+10 \% \mathrm{Ir}$ | + 5.90 | -. 0133 | + 5.63 | + 5.23 | 444 |
| $95 \% \mathrm{Pt}+5 \% \mathrm{Ir}$ | + 6.15 | +. 0055 | + 6.26 | + 6.42 | [-1118] |
| Selenium |  |  | $+807$. |  |  |
| Silver | + 2.12 | +. 0147 | + 2.41 | + 2.86 | - 144 |
| " (pure hard) |  | - | $+3.00$ |  |  |
| Steel wire | +11.27 | -. 0325 | + 10.62 | + + +9.18 | 347 |
| Tantalum |  | - | - 2.6 |  |  |
| Tellurium * $\beta$ | - | - | +500. | - |  |
| Thallium |  |  |  |  |  |
| Tin (commercial) |  | - |  | $+.33$ |  |
|  |  |  | + ${ }^{1}$ |  |  |
| T | - . 43 | +. 0055 | - . 33 | - . 16 | 78 |
| Tungsten Zinc |  |  | - 2.0 |  |  |
| Zinc .... | + 2.32 | +. 0238 | $+\quad 2.79$ | + 3.51 | 98 |
| pure pr |  |  |  |  |  |

[^170]TABLE 378.-THERMAL ELECTROMOTIVE FORCE OF METALS AND ALLOYS VERSUS PLATINUM
(millivolts)
One junction is supposed to be at $0^{\circ} \mathrm{C} ;+$ indicates that the current flows from the $0^{\circ}$ junction into the platinum. The rhodium and iridium were rolled, the other metals drawn.

| Temperature, ${ }^{\circ} \mathrm{C}$ | Au | Ag | $\begin{aligned} & 90 \% \mathrm{Pt}+ \\ & 10 \% \mathrm{Pd} \end{aligned}$ | $\begin{aligned} & 10 \% \mathrm{Pt}+ \\ & 90 \% \mathrm{Pd} \end{aligned}$ | Pd | $\begin{aligned} & 90 \% \mathrm{Pt}+ \\ & 10 \% \mathrm{Rh} \end{aligned}$ | $\begin{aligned} & 90 \% \mathrm{Pt}+ \\ & 10 \% \mathrm{Ru} \end{aligned}$ | Ir | Rh |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -185 | -. 15 | $-.16$ | -. 11 | $+.24$ | + . 77 | - | -. 53 | - . 28 | - . 24 |
| -80 | $-.31$ | -. 30 | -. 09 | +. 15 | + . 39 | - | $-.39$ | -. 32 | -. 31 |
| +100 | +. 74 | +. 72 | + . 26 | -. 19 | -. 56 | - | +. 73 | +. 65 | +. 65 |
| +200 | +1.8 | +1.7 | +. 62 | -. 31 | -1.20 |  | +1.6 | +1.5 | +1.5 |
| +300 | +3.0 | $+3.0$ | +1.0 | -. 37 | $-2.0$ | +2.3 | +2.6 | +2.5 | +2.6 |
| $+400$ | +4.5 | +4.5 | +1.5 | -. 35 | -2.8 | +3.2 | +3.6 | +3.6 | +3.7 |
| $+500$ | $+6.1$ | $+6.2$ | +1.9 | -. 18 | -3.8 | +4.1 | +4.6 | +4.8 | +5.1 |
| +600 | +7.9 | +8.2 | +2.4 | $+.12$ | -4.9 | +5.1 | $+5.7$ | +6.1 | +6.5 |
| +700 | +9.9 | +10.6 | +2.9 | +. 61 | -6.3 | +6.2 | +6.9 | +7.6 | +8.1 |
| +800 | +12.0 | +13.2 | +3.4 | +1.2 | -7.9 | +7.2 | +8.0 | -9.1 | +9.9 |
| +900 | +14.3 | +16.0 | +3.8 | +2.1 | -9.6 | +8.3 | +9.2 | +10.8 | +11.7 |
| +1000 | +16.8 |  | +4.3 | +3.1 | -11.5 | +9.5 | +10.4 | +12.6 | +13.7 |
| +1100 |  |  | +4.8 | +4.2 | -13.5 | +10.6 | $+11.6$ | +14.5 | +15.8 |
| +(1300) | - |  |  |  |  | +13.1 | +14.2 | +18.6 | +20.4 |
| +(1500) | - | - | - |  | - | +15.6 | +16.9 | +23.1 | +25.6 |

TABLE 379.-THERMOELECTRIC PROPERTIES AT LOW TEMPERATURES ${ }^{141}$
Thermoelectric emf per ${ }^{\circ} \mathrm{K}$ against silver alloy

| ${ }^{\circ} \mathrm{C}$ | Cu | Ag | Au | Pd | Pt | Fe | Pb |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| -255 | +.07 | -.10 | -1.20 | +.75 | +1.54 | +.05 | -1.06 |
| -240 | .45 | +.37 | .- .05 | 2.10 | 3.60 | 1.40 | -1.19 |
| -220 | .90 | .39 | .+ .24 | 3.40 | 5.24 | 4.80 | -1.25 |
| -200 | .89 | .31 | . .30 | 3.48 | 5.40 | 8.45 | -1.29 |
| -180 | .72 | .25 | .30 | 2.14 | 4.36 | 11.5 | -1.33 |
| -160 | .61 | .22 | .33 | .54 | 3.02 | 14.0 | -1.42 |
| -140 | .52 | .21 | .37 | -1.06 | 1.72 | 15.8 | -1.54 |
| -120 | .47 | .20 | .40 | -2.52 | .50 | 16.9 | -1.67 |
| -100 | .44 | .20 | .44 | -3.92 | -.70 | 17.5 | -1.79 |
| -80 | .45 | .20 | .47 | -5.27 | -1.76 | 17.5 | -1.92 |
| -60 | .47 | .20 | .51 | -6.52 | -2.80 | 17.3 | -2.05 |
| -40 | .49 | .20 | .55 | -7.80 | -3.80 | 16.9 | -2.17 |
| -20 | .51 | .20 | .58 | -9.05 | -4.72 | 16.2 | -2.29 |
| 0 | .53 | .21 | .62 | -10.32 | -5.62 | 15.8 | -2.42 |
| +20 | .56 | .22 | .65 | -11.6 | -6.56 | 15.3 | -2.54 |

${ }^{141}$ Borelius, Keesom, Johansson, Linde, Com. Phys. Lab. Leiden, No. 206, 1930.

TABLE 380.-PELTIER EFFECT, FE-CONSTANTAN, NI-CU, $0^{\circ}-560^{\circ} \mathrm{C}$

| Temperature |  | $0^{\circ}$ | $20^{\circ}$ | $130^{\circ}$ | $240^{\circ}$ | $320^{\circ}$ | $560^{\circ} \mathrm{C}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: |
| $\mathrm{Fe}-\mathrm{Constantan}$ | $\ldots \ldots \ldots$ | 3.1 | 3.6 | 4.5 | 6.2 | 8.2 | 12.5 |
| NiCu | $\ldots \ldots \ldots \ldots \ldots \ldots$ | 1.92 | 2.15 | 2.45 | 2.06 | 1.91 | 2.38 |


| ${ }^{\circ} \mathrm{K}$ | Cu | Ag | Au | Pd | Pt | Fe | Ni | Co | Pb |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | +. 59 | +1.40 | +2.83 | +1.9 | +3.2 | +1.3 |  |  | . |
| 25 | 1.04 | 1.23 | 2.09 | 2.6 | 3.6 | 2.7 |  |  |  |
| 30 | 1.22 | . 85 | 1.58 | 3.1 | 3.9 | 4.1 | -45 | -. 2 | . 00 |
| 40 | 1.03 | . 24 | . 88 | 3.2 | 3.8 | 6.7 | -5.4 | -. 3 | -. 04 |
| 50 | . 67 | -. 02 | . 45 | 2.5 | 2.7 | 9.0 | -5.0 | $-.8$ | -. 06 |
| 60 | . 18 | $-.17$ | . 19 | 1.0 | 1.0 | 10.8 | -4.5 | -2.0 | -. 09 |
| 70 | -. 29 | -. 24 | . 07 | -1.5 | -1.1 | 11.9 | -4.1 | -3.7 | -. 12 |
| 80 | -. 46 | -. 25 | . 05 | -4.6 | -3.3 | 12.6 | -4.0 | -5.5 | -. 15 |
| 90 | -. 48 | -. 17 | . 17 | -6.6 | -5.1 | 12.9 | -4.0 | -7.0 | -. 18 |
| 100 | -. 45 | -. 03 | . 32 | -7.8 | -6.5 | 13.0 | -4.5 | -8.4 | -. 20 |
| 110 | -. 37 | +. 12 | . 45 | -8.7 | -7.5 | 13.0 | -5.3 | -9.8 | -. 23 |
| 120 | -. 26 | . 25 | . 56 | -9.3 | -8.0 | 12.8 | -6.4 | -11.1 | -. 26 |
| 130 | -. 13 | . 35 | . 66 | -9.7 | -8.2 | 12.2 | -7.4 | -12.4 | -. 29 |
| 140 | +. 02 | . 44 | . 75 | -10.1 | -8.2 | 11.0 | -8.3 | -13.5 | -. 32 |
| 150 | . 17 | . 52 | . 83 | -10.3 | -8.3 | 8.9 | -9.0 | -14.6 | -. 34 |
| 160 | . 31 | . 59 | . 91 | -10.6 | -8.4 | 6.1 | -9.7 | -15.7 | -. 37 |
| 170 | . 46 | . 66 | . 99 | -10.9 | -8.5 | 2.6 | -10.3 | -16.7 | -. 40 |
| 180 | . 59 | . 72 | 1.06 | -11.2 | -8.7 | -. 2 | -10.9 | -17.6 | -. 42 |
| 200 | . 79 | . 84 | 1.19 | -12.1 | -9.1 | -3.5 | -12.1 | -19.6 | -. 46 |
| 220 | . 96 | . 96 | 1.31 | -13.3 | -9.8 | -4.5 | -13.3 | -21.5 | -. 49 |
| 240 | 1.10 | 1.08 | 1.43 | -146 | -10.6 | -4.8 | -14.5 | -23.4 | -. 52 |
| 260 | 1.24 | 1.20 | 1.54 | -15.8 | -11.4 | -5.2 | -15.7 | -25.4 | -. 54 |
| 280 | 1.38 | 1.32 | 1.66 | -17.0 | $-12.3$ | -56 |  |  | -. 55 |
| 300 | +1.52 | +1.44 | +1.77 | $-18.2$ | -13.2 | -5.9 |  |  | -. 57 |

## TABLE 382.-THERMOELECTRIC EFFECTS; PRESSURE EFFECTS

The following values of the thermoelectric effects under various pressures are taken from Bridgman. A positive emf means that the current at the hot junction flows from the uncompressed to the compressed metal. The cold junction is always at $0^{\circ} \mathrm{C}$. The last two columns give the constants in the equation $E=$ thermoelectric force against lead $\left(0^{\circ}\right.$ to $\left.100^{\circ} \mathrm{C}\right)=\left(A t+B t^{2}\right)$ $\times 10^{-8}$ volts; at atmospheric pressure, a positive emf meaning that the current flows from lead to the metal under consideration at the hot junction.


The following data indicate the magnitude of the effect of pressure on the Peltier and Thomson heats. They refer to the same samples as for the last table. The Peltier heat is considered positive if heat is absorbed by the positive current from the surroundings on flowing from uncompressed to compressed metal. A positive $d^{2} E / d t^{2}$ means a larger Thomson heat in the compressed metal, and the Thomson heat is itself considered positive if heat is absorbed by the positive current in flowing from cold to hot metal. Same reference as footnote 141, and notes as for preceding table.

| Metal |  |  |  |  |  |  | $\begin{gathered} 10^{8} \times \mathrm{J} \times \text { coulomb- heat, }{ }^{\text {Thoms }} \mathrm{C}^{-1} \\ \text { Pressure } \mathrm{kg} / \mathrm{cm}^{2} \end{gathered}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  | 6000 |  |  | 12,000 |  |
|  | Temperature ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  | Temperature ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |
|  | $0^{\circ}$ | $50^{\circ}$ | $100^{\circ}$ | $0^{\circ}$ | $50^{\circ}$ | $100^{\circ}$ | $0{ }^{\circ}$ | $50^{\circ}$ | $100^{\circ}$ | $0^{\circ}$ | $50^{\circ}$ | $100^{\circ}$ |
| Bi | $+1070$ | +1210 |  | +2580 | $+2810$ |  | +1150 | +650 |  | -520 | $-405$ |  |
| Zn | +98 | +140 | $+190$ | $+190$ | +278 | +412 | +41 | +48 | $+56$ | +63 | +133 | +220 |
| $\stackrel{\mathrm{Tl}}{\mathrm{Cd}}$ | +66 +19 | +95 +71 | +124 +118 | +112 +81 | +171 +148 | +229 +221 | +38 +109 | +28 +74 | +26 +63 | +79 +105 | +63 +92 | +50 +93 |
| Constantan | $+46$ | +57 | +70 +70 | +90 | +114 | +140 +103 | +5 | +6 | +6 | +13 | +14 | $+17$ |
| Pd | $+35$ | +43 | +52 | +68 | +86 | +103 | +3 | $+4$ | +4 | +9 | +9 | +8 |
|  | +23 | +37 | +35 | +45 | +76 | +65 | +49 | -6 | -18 | +96 | +17 | +59 |
| W | $+17$ | +25 | +32 | +36 | +49 | +65 | +8 | $+7$ | +6 | +9 | +14 | +20 |
| Ni | +11 | +17 | +23 | +24 | $+37$ | +50 | +9 | +7 | +8 | +16 | +15 | +10 |
| Ag |  |  |  | +25 | +34 | +44 | $+4$ | $+5$ | +6 | +7 | +8 | +10 |
|  | $-11$ | +18 | +15 | -38 | +38 | +36 | +79 | +58 | -121 | $-347$ | +120 | -194 |
|  | +7 | $+10$ | +16 | +14 | +20 | $+30$ | +2 | +6 | +10 | $+6$ | +8 | +20 |
| ${ }^{\text {Au }}$ | $+6$ | +10 | +14 | +13 | +18 | +25 | +4 | +4 | +5 | $+6$ | $+6$ | +7 |
| Cu | +4 | +6 | +8 | +8 | +11 | +16 | +4 | $+1$ | +4 | +6 | +3 +16 | +8 +20 |
| Al | -2 | $+2$ | +8 | -3 | $+7$ | +17 | +6 | +9 | +11 | +21 | +16 | +20 +2 |
| Mo | +1 | +2 | +0 | +2 | +4 | +1 | +1 | $-5$ | -1 | +2 | $-11$ | -2 |
| $\mathrm{Sn} \ldots .$. | -1 | +1 | +1 | -5 | +2 | +2 | $+6$ | +0 | -1 | +29 | +2 | - |
| Manganin | -2 | -2 | -2 | -4 | -4 | -4 | +1 | +1 | +0 | +2 | +1 | +1 |
| Mg ..... | -16 | -18 | -21 | -35 | -42 | -48 | 0 | 0 | 0 |  | 0 |  |
| Co | -23 | -33 | -44 | -46 | -67 | -90 | -14 | -11 | -10 | -20 | -24 | -28 |

## TABLE 384.-THERMAL ELECTROMOTIVE FORCE OF CADMIUM VERSUS PLATINUM

Temperature versus emf

| ${ }^{\circ} \mathrm{C}$ | mv | ${ }^{\circ} \mathrm{C}$ | mv | ${ }^{\circ} \mathrm{C}$ | mv |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 0 | .000 | 125 | 1.211 | 250 | 3.255 |
| 25 | +.171 | 150 | 1.559 | 275 | 3.740 |
| 50 | .378 | 175 | 1.940 | 300 | 4.238 |
| 75 | .620 | 200 | 2.351 | 315 | 4.539 |
| 100 | .898 | 225 | 2.790 |  |  |

## TABLE 385.-PELTIER EFFECT

The coefficient of Peltier effect may be calculated from the constants $A$ and $B$ of Table 377, as there shown. With $Q$ (see Table 377) in microvolts per ${ }^{\circ} \mathrm{C}$ and $T=$ absolute temperature $(K)$, the coefficient of Peltier effect $=\frac{Q T}{42}$ cal per coulomb $=0.00086$ QT cal per ampere-hour $=Q T / 1000$ millivolts ( $=$ millijoules per coulomb). Experimental results, expressed in slightly different units are here given. The figures are for the heat production at a junction of copper and the metal named in calories per ampere-hour. The current flowing from copper to the metal named, a positive sign indicates a warming of the junction.

| Calories per ampere-hour |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sb * | Sb com. mercial $\dagger$ | Bi pure $\qquad$ | $\begin{gathered} \mathrm{Bi} \dagger \\ - \end{gathered}$ | $\begin{array}{r} \mathrm{Cd} \\ -.62 \end{array}$ | German silver | $\begin{gathered} \mathrm{Fe} \\ -3.61 \end{gathered}$ | $\begin{gathered} \mathrm{Ni} \\ 4.36 \end{gathered}$ | $\begin{gathered} \mathrm{Pt} \\ .32 \end{gathered}$ | $\begin{array}{r} \mathrm{Ag} \\ -.41 \end{array}$ | $\begin{gathered} \mathrm{Zn} \\ -.58 \end{gathered}$ |
| 13.02 | 4.8 | 19.1 | 25.8 | . 46 | 2.47 | 2.5 | - | - | - | . 39 |
| *Becquerel's antimony is 806 parts $\mathrm{Sb}+406$ parts $\mathrm{Zn}+121$ parts Bi . <br> $\dagger$ Becquerel's bismuth is 10 parts $\mathrm{Bi}+1$ part Sb . |  |  |  |  |  |  |  |  |  |  |

The resistivities are the values of $\rho$ in the equation $R=\rho l / s$, where $R$ is the resistance in microhms of a length $l \mathrm{~cm}$ of uniform cross section $s \mathrm{~cm}^{2}$. The temperature coefficient is $a_{s}$ in the formula $R_{t}=R_{s}\left[1+a_{s}\left(t-t_{s}\right)\right]$. The information of column 2 does not necessarily apply to the temperature coefficient.

| Substance | Remarks | $\begin{gathered} \text { Tempera- } \\ \text { ture } \\ { }_{0} \mathrm{C} \end{gathered}$ | $\underset{\mathrm{cm}}{\text { Microhm. }}$ | Temperature coefficient |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $t$ 。 | $a_{0}$ |
| Advance | see constantan | - |  | - |  |
| Aluminum | -- | 20 | 2.828 | $18^{\circ}$ | +. 0039 |
| " | c. ${ }^{\text {p }}$. | -189 | . 64 | 25 | $+.0034$ |
| " | " | -100 | 1.53 | 100 | $+.0040$ |
| " | " | 0 | 2.62 | 500 | $+.0050$ |
| " | " | $+100$ | 3.86 | - | - |
| " | " | 400 | 8.0 |  |  |
| Antimony | - | 0 | 39.1 | 20 | +. 0036 |
|  |  | -190 | 10.5 | - |  |
| Arsenic | liquid | +860 | 120 |  |  |
| Arsenic Beryllium |  | 0 | 35 |  |  |
| Bismuth | - - | 18 | 119.0 | 20 | $+$. |
|  |  | 100 | 160.2 |  |  |
| Brass |  | 20 | 7 | 20 | +. 002 |
| Cadmium | drawn | -160 | 2.72 | 20 | $+.0038$ |
| " | " | 18 | 7.54 | - | - |
| " | liquid | 100 | 34.1 | - |  |
| Calcium | 99.57 pure | 20 | 4.59 | - | $+.0036$ |
| Calido | see nichrome | --187 |  | - | -- |
| Cesium | - | -187 | 5.25 | - | - |
|  | solid $\}$ | 0 | 19 |  |  |
| " |  | 27 | 22.2 | - | - |
|  | liquid $\}$ | 30 | 36.6 | - |  |
| Chromium |  | 0 | 13 | - |  |
| Climax | 99.8 pure | 20 | 87 | 20 | $+.0007$ |
| Constantan |  | 20 | 9.7 | -- |  |
|  | $60 \% \mathrm{Cu} .40 \% \mathrm{Ni}$ | 20 | 49 | 12 | $+.000008$ |
|  |  | - | - | 25 | $+.000002$ |
| " |  |  |  | 200 | -.000033 |
| " |  |  |  | 500 | $+.000027$ |
| Copper | annealed | 20 | 1.724 | 20 see col. 2 | +.00393 |
|  | hard-drawn | 20 | 1.77 | " " " " | +. 00382 |
| " . | electrolytic | -206 | . 144 | 100 | +. 0038 |
| " |  | +205 | 2.92 | 400 | +. 0042 |
| " . | pure | 400 | 4.10 | 1000 | +.0062 |
| Eureka | very pure, ann'ld | 20 | 1.692 | - |  |
| Excello | see constantan | 20 | 92 | 20 | $+.00016$ |
| Gallium | $18 \% \overline{\mathrm{Ni}}$ | 0 | 53 | - | - |
| German silver |  | 20 | 33 | 20 | $+.0004$ |
| Germanium | - | 0 | 89000. | - | -- |
| Gold |  | -183 | . 68 | 20 | $+.0034$ |
| " | 99.9 pure | 0 | 2.22 | 100 ann'ld | $+.0025$ |
|  | pure, drawn | 20 | 2.44 | 500 " | $+.0035$ |
| " . | 99.9 pure | 194.5 | 3.77 | 1000 | +. 0049 |
| Ia Ia | see constantan | - |  | - | - |
| Ideal |  |  |  |  |  |
|  | - | 0 | 8.37 |  |  |
| Iridium | - | -186 | 1.92 | - | - |
|  | - | 0 | 6.10 |  |  |
| Iron |  | $+100$ | 8.3 |  |  |
| Iron | 99.98\% pure | 20 | 10 | 20 | $+.0050$ |
|  | pure, soft | -205.3 | . 652 | 0 | $+.0062$ |
| " | ". " | - 78 | 5.32 | 25 | +. 0052 |
|  |  | 0 | 8.85 | 100 | +. 0068 |
|  |  | ntinued) |  |  |  |

(continued)

| Substance | Remarks | $\underset{\substack{\text { Tempera- } \\ \text { ture } \\ \text { ture }}}{ }$ | $\underset{\substack{\text { Microhm- } \\ \text { cm }}}{ }$ | Temperature coefficie |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ${ }^{\text {a }}$ | $a_{s}$ |
| Iron ...... | pure, soft | + 98.5 | 17.8 | 500 | +. 0147 |
| " ..... | " " |  |  |  | . 0050 |
|  | electrolytic | 0 | 10.0 | - |  |
| Lead | " | 100 | 14.41 |  |  |
|  |  | 20 | 22 | 20 | $+.0039$ |
|  | cold pressed | $-183$ | 6.02 | 18 | $+.0043$ |
| " | "، " | - 78 | 14.1 | - |  |
| " | " " | 0 | 19.8 |  |  |
| " | " " | + 90.4 | 28 |  |  |
| " |  | 196.1 | 36.9 |  |  |
| Lithium |  | 318 |  |  |  |
|  | solid | 187 0 | 1.35 |  |  |
| " | " | 99.3 | 127 |  |  |
| " | liquid | 230 | 45.2 |  |  |
| Magnesium |  | 20 | 4.6 | 20 | $+.004$ |
|  | free from $\mathrm{Zn}_{\text {n }}$ | $-183$ | 1.00 | 0 | +.0038 |
| " | " " | -78 | 2.97 | 25 | +.0050 |
| " | ". " ." | 0 | 4.35 | 100 | $+.0045$ |
| " | pure | +98.5 | 5.99 | 500 | $+.0036$ |
| Manganese | pure | 400 | ${ }_{50 \pm}$ | 600 | +.0100 |
| Manganin | $84 \mathrm{Cu}, 12 \mathrm{Mn}, 4 \mathrm{Ni}$ | 20 |  |  | $+.000006$ |
|  |  |  |  | 25 | . 000000 |
| " |  |  |  | 100 | -.000042 |
| " |  |  |  | 250 | -. 0000052 |
| " |  |  |  | 475 | -. 000000 |
| " |  |  |  | 500 | -. 000011 |
| Mercury | solid | ${ }^{20}$ | 95.783 | 20 | +.00089 |
|  |  | $-183.5$ | 6.97 | 0 | $+.00088$ |
| " | " |  | 15.04 |  |  |
| " |  | - 30.3 | 21.5 | $R_{t}=R_{0}(1+$ |  |
| " | liquid | - 36.1 | 80.6 | . $0000001 t^{2}$ ) |  |
| " |  | , | 94.07 |  |  |
|  | " | 50 | 98.50 |  |  |
| " | " | 100 | 103.25 |  |  |
| " . |  | 200. | 114.27 |  |  |
| Molybdenum |  | 350 | 135.5 |  |  |
|  | very pure | 0 | 5.14 | 25 | $+.0033$ |
| " |  |  |  | 1100 | ${ }^{+}+.0034$ |
| Monel metal | - | 20 | 42 | 20 | $+.0020$ |
| Nichrome |  | 20 | 100 | 20 | $+.0004$ |
| Nickel |  | 20 | 7.8 | 20 | +. 006 |
|  | ${ }_{\text {very }}^{\text {pure }}$ pure | ${ }_{-1825}$ | 7.236 |  |  |
| "، |  | -182.5 -78.2 | ${ }_{4}^{1.44}$ | 25 | +.0062 +.0043 |
| " | " | 0 | 6.93 | 100 | $+.0043$ |
| " | " ${ }^{\prime}$ | 94.9 | 11.1 | 500 | $+.0030$ |
|  |  | 20 | 9.5 |  | +.0037 |
| Palladium |  | 20 | 11 | 20 | $+.0033$ |
|  | very pure | -183 -78 | 2.78 |  | +.0035 |
| " | " " | - 88 |  |  |  |
| " |  | 98.5 | 13.79 |  |  |
| Platinum | wire |  | 9.83 | 20 | $+.003$ |
|  |  | -203.1 | 2.44 | 0 | +.0037 |
| " |  | - 97.5 | 6.87 |  |  |
| " | " |  | 10.96 |  |  |
|  | - | 400 |  |  |  |
|  |  | titued) |  |  |  |


| Substance | Remarks | $\begin{gathered} \text { Tempera- } \\ \begin{array}{c} \text { ture } \\ { }^{\circ} \mathrm{C} \end{array} \end{gathered}$ | $\underset{\substack{\text { Microhm } \\ \mathrm{cm}}}{ }$. | Temperature coefficient |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ${ }^{\text {t }}$ | $a_{a}$ |
| Potassium | _- | - 75 | 4 | 0 | +. 0057 |
|  |  | 0 | 6.1 |  |  |
| " |  | 55 | 8.4 |  |  |
| Rhodium | -- | $-186$ | . 70 |  | - |
|  |  | - 78.3 | 3.09 |  |  |
| " |  | 0 | 5.11 | 0 | $+.0043$ |
| " |  | 100 | 6.60 |  |  |
| Rubidium | solid | -190 | 2.5 | - |  |
|  |  | 0 | 11.6 |  |  |
| " | " | 35 | 13.4 | - |  |
| " | liquid | 40 | 19.6 |  |  |
| Silicium | -- | 20 | $58 \pm$ |  |  |
| Silver | 99.98 pure | 18 | 1.629 | 20 | +. 0038 |
|  | electrolytic | -183 | . 390 | 25 | +. 0030 |
| " . |  | - 78 | 1.021 | 100 | $+.0036$ |
| " | " | 0 | 1.468 | 500 | +. 0044 |
| " | " | 98.15 | 2.062 | - | - |
| " | " | 192.1 | 2.608 | - |  |
| " . . | " | 400 | 3.77 | -. |  |
| Sodium | solid | -180 | 1.0 | - |  |
|  |  | - 75 | 2.8 |  |  |
| " | " | 0 | 4.3 | 0 | $+.0054$ |
| " | " | 55 | 5.4 | - |  |
| Steel | liquid | 116 | 10.2 |  |  |
| Steel | E. B. B. | 20 | 10.4 | 20 see col. 2 | $+.005$ |
| " . ... | B. B. | 20 | 11.9 | " " " " | +. 004 |
| " . | Siemens-Martin | 20 | 18 | " " " " | $+.003$ |
| " | manganese | 20 | 70 | " " " " | $+.001$ |
| " | $35 \% \mathrm{Ni}$, "invar." | 20 | 81 |  |  |
| "، | piano wire | 0 | 11.8 | 0 see col. 2 | +. 0032 |
| " ${ }^{\text {c }}$ | temp. glass, hard | 0 | 45.7 |  | $+.0016$ |
| " ${ }^{\text {" }}$ | ", yellow | 0 | 27 |  |  |
| " | ", blue | 0 | 15.9 | 0 see col. 2 | $+.0033$ |
| Strontium | , | 20 | 24.8 |  |  |
| Tantalum | - | 20 | 15.5 | 20 | +. 0031 |
| Tellurium* | - | 19.6 | 200,000 | - |  |
| Thallium | pure | -183 | 4.08 | - | - |
|  | " | - 78 | 11.8 | - | - |
| " | " | 0 | 17.60 |  |  |
| Tin | " | 98.5 | 24.7 |  |  |
|  | - | 20 -184 | 11.5 3.40 | 20 | +.0042 |
| " | - | - 78 | 8.8 |  |  |
| " . | -- | 0 | 13 |  |  |
| " |  | 91.45 | 18.2 |  |  |
| Titanium | - | - | 55 |  |  |
| Tungsten | 000 ${ }^{\circ} \mathrm{K}$ | 20 | 5.51 | 18 | $+.0045$ |
|  | $1000^{\circ} \mathrm{K}$ | 727 | 25.3 | 500 | $+.0057$ |
| " | $1500^{\circ} \mathrm{K}$ | 1227 | 41.4 | 1000 | +. 0089 |
| " | $2000^{\circ} \mathrm{K}$ | 1727 | 59.4 | -- |  |
| " | $3000^{\circ} \mathrm{K}$ | 2727 | 98.9 | -- |  |
| " | $3500^{\circ} \mathrm{K}$ | 3227 | 118 |  |  |
| Zinc | trace Fe | -183 | 1.62 | 20 | $+.0037$ |
|  | " " | - 78 | 3.34 |  |  |
| " | " " | 0 | 5.75 |  |  |
| " | " " | 92.45 | 8 |  |  |
| " . | " " | 191.5 | 10.37 |  |  |
| " . | liquid | 440 | 37.2 | - | - |

[^171]TABLE 386.-RESISTIVITY OF METALS AND SOME ALLOYS (concluded)
Resistance temperature coefficient for a number of metals and alloys of high purity.


TABLE 387.-SOME ELEMENTS ARRANGED IN ORDER OF INCREASING
RESISTIVITY (Ohm-cm $\times 10^{-6}, 20^{\circ} \mathrm{C}$ )

| Ag | 1.468 | Mn | $5 . \pm$ | Pd | 10.21 | Ga | 53 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Cu | 1.59 | Mo | $(5.3)$ | Pt | 10.96 | Os | 56 |
| Au | 2.22 | Zn | 5.75 | Rb | 13 | Hg | 94.07 |
| Al | 2.6 | Ir | 6.10 | Sn | 13 | Bi | 110 |
| Cr | 2.6 | K | 6.1 | Ta | 14.6 | $\mathrm{Graphite} 8 \times 10^{2}$ |  |
| Ti | 3.2 | Ni | 6.93 | Tl | 17.6 | Carbon | $3 \times 10^{3}$ |
| Na | 4.3 | Cd | 7.04 | Cs | 19 | $2 \times 10^{5}$ |  |
| Ca | 4.3 | In | 8.37 | Pb | 20.4 | Te | $10^{12}$ |
| Mg | 4.35 | Li | 8.55 | Sr | $(23.5)$ | B | $8 \times 10^{12}$ |
| Rh | 4.69 | Fe | 8.8 | As | 35 | Se | $10^{13}$ |
| W | 5 | Co | 9 | Sb | 39 | S | $10^{17}$ |

TABLE 388.-THERMAL ELECTROMOTIVE FORCE OF PLATINUM-RHODIUM ALLOYS VERSUS PLATINUM
emf (mv)
Percent rhodium

| ${ }^{\text {Temp. }}{ }^{\circ}$ | . 5 | 1.0 | 5.0 | 10.0 | 20.0 | 40.0 | 80.0 | 100.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 |
| 100 | +. 10 | +. 18 | $+.54$ | +. 64 | +. 63 | $+.65$ | +. 62 | $+.70$ |
| 200 | . 20 | . 37 | 1.16 | 1.43 | 1.44 | 1.52 | 1.49 | 1.61 |
| 300 | . 29 | . 57 | 1.82 | 2.32 | 2.40 | 2.55 | 2.55 | 2.68 |
| 400 | . 39 | . 76 | 2.49 | 3.25 | 3.47 | 3.70 | 3.77 | 3.91 |
| 500 | . 48 | . 94 | 3.17 | 4.22 | 4.63 | 4.97 | 5.12 | 5.28 |
| 600 | . 58 | 1.12 | 3.86 | 5.22 | 5.87 | 6.36 | 6.60 | 6.77 |
| 700 | . 67 | 1.30 | 4.55 | 6.26 | 7.20 | 7.85 | 8.20 | 8.40 |
| 800 | . 76 | 1.48 | 5.25 | 7.33 | 8.59 | 9.45 | 9.92 | 10.16 |
| 900 | . 85 | 1.66 | 5.96 | 8.43 | 10.06 | 11.16 | 11.76 | 12.04 |
| 1000 | . 94 | 1.84 | 6.68 | 9.57 | 11.58 | 12.98 | 13.73 | 14.05 |
| 1100 | 1.03 | 2.02 | 7.42 | 10.74 | 13.17 | 14.90 | 15.81 | 16.18 |
| 1200 | 1.13 | 2.20 | 8.16 | 11.93 | 14.84 | 16.91 | 17.99 | 18.42 |

TABLE 389.-EFFECT OF TENSION ON THE RESISTANCE OF METALS

|  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Recip. Young's <br> mod. $\times 10^{6}$$\ldots \ldots$ | Li | Ca | Sr | Sb | Bi | Manganin | Co |
| Poisson ratio $\ldots \ldots$ | .42 | 4.75 | 7.5 | 1.25 | 4.2 | .72 | .5 |
| Tens. coef. spec. <br> resist. $\times 10^{6} \ldots \ldots+11$ | +.30 | .36 | .30 ? | .37 | .33 | .30 |  |

TABLE 390.-VARIATION OF THE ELECTRICAL RESISTANCE WITH PRESSURE FOR TWO TEMPERATURES OF A NUMBER OF METALS ${ }^{142}$

|  | Copper- $\Delta \mathrm{R} / \mathrm{R}_{0}$ |  | Silver- $\Delta \mathrm{R} / \mathrm{R}_{0}$ |  | Gold- $\Delta \mathrm{R} / \mathrm{R}_{6}$ |  | Iron- $\Delta \mathrm{R} / \mathrm{R}_{0}$ |  | Lead-- $\Delta \mathrm{R} / \mathrm{R}_{0}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pressure | $30^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $30^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $30^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $30^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ | $30^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ |
| 5,000 | . 0096 | . 0094 | . 0174 | . 0176 | . 0151 | . 0154 | . 0121 | . 0118 | . 0686 | . 0691 |
| 10,000 | . 0186 | . 0185 | . 0338 | . 0341 | . 0293 | . 0299 | . 0234 | . 0232 | . 1266 | . 1277 |
| 15,000 | . 0271 | . 0271 | . 0492 | . 0497 | . 0429 | . 0437 | . 0341 | . 0341 | . 1770 | . 1791 |
| 20,000 | . 0354 | . 0354 | . 0637 | . 0644 | . 0559 | . 0570 | . 0444 | . 0447 | . 2214 | . 2242 |
| 25,000 | . 0434 | . 0435 | . 0774 | . 0784 | . 0684 | . 0698 | . 0542 | . 0548 | . 2611 | . 2643 |
| 30,000 | . 0513 | . 0514 | . 0904 | . 0916 | . 0806 | . 0824 | . 0637 | . 0646 | . 2959 | . 2998 |

[^172]TABLE 391.-RELATIVE ELECTRICAL RESISTANCE WITH PRESSURE FOR TWO TEMPERATURES OF A NUMBER OF METALS*


[^173]Temperature versus emf

| ${ }^{\circ} \mathrm{C}$ | mv |  | ${ }^{\circ} \mathrm{C}$ | ${ }^{\mathrm{mv}}$ | ${ }^{\circ} \mathrm{C}$ |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 0 | .000 | 400 | 5.450 | 800 | 9.350 |
| 25 | -.350 | 425 | 5.580 | 825 | 9.675 |
| 50 | .710 | 450 | 5.745 | 850 | 10.010 |
| 75 | 1.090 | 475 | 5.960 | 875 | 10.350 |
| 100 | 1.485 | 500 | 6.165 | 900 | 10.695 |
| 125 | 1.880 | 525 | 6.360 | 925 | 11.045 |
| 150 | 2.285 | 550 | 6.585 | 950 | 11.400 |
| 175 | 2.695 | 575 | 6.800 | 975 | 11.765 |
| 200 | 3.105 | 600 | 7.040 | 1000 | 12.130 |
| 225 | 3.505 | 625 | 7.290 | 1025 | 12.500 |
| 250 | 3.850 | 650 | 7.550 | 1050 | 12.875 |
| 275 | 4.255 | 675 | 7.825 | 1075 | 13.250 |
| 300 | 4.590 | 700 | 8.105 | 1100 | 13.625 |
| 325 | 4.880 | 725 | 8.415 |  |  |
| 350 | 5.110 | 750 | 8.720 |  |  |
| 375 | 5.290 | 775 | 9.030 |  |  |

${ }^{143}$ Nat. Bur. Standards Journ. Res., vol. 5, p. 1291, 1930.

TABLE 393.-AVERAGE PRESSURE COEFFICIENTS* OF ELECTRICAL RESISTANCE UP TO $7000 \mathrm{~kg} / \mathrm{cm}^{2}$ AS A FUNCTION OF TEMPERATURE ${ }^{144}$

Temperatures

| Metal | $-182.0^{\circ} \mathrm{C}$ | $-78.4{ }^{\circ} \mathrm{C}$ | $0^{\circ} \mathrm{C}$ | $30^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lead | -12.76 | -12.88 | -12.99 | -9.3 | -9.2 |
| Magnesium | -5.89 | -4.49 | -4.39 |  |  |
| Aluminum | -9.16 | -4.71 | -4.28 |  |  |
| Silver | -4.09 | -3.46 | -3.45 | $-3.0$ | -3.0 |
| Gold | $-3.27 \dagger$ | -2.97 | -2.94 | -2.6 | -2.7 |
| Copper | -3.09 | -2.14 | -1.88 | $-1.7$ | -1.7 |
| Nickel | -1.88 | -2.00 | -1.85 |  |  |
| Iron | -2.44 | -2.27 | -2.34 |  |  |
| Palladium | -2.82 | -2.32 | -2.13 |  |  |
| Niobium | -. 80 | -. 98 | -1.18 |  |  |
| Platinum | -234 | -1.97 | -1.93 |  |  |
| Rhodium | -2.26 | -1.86 | $-1.64 \ddagger$ |  |  |
| Molybdenum | -1.91 | -1.29 | -1.30 |  |  |
| Tantalum | -1.17 | -1.42 | -1.45 |  |  |
| Tungsten | $-1.36$ | -1.42 | -1.37 |  |  |

${ }^{*} \times 10^{0}$
144 Bridgman, P. W., Proc. Amer. Icad. Arts and Sci., vol. 67, p. 342, 1932.
$\dagger$ Maximum pressure 4300 .
$\ddagger$ On a less pure sample.

TABLE 394.-RESISTIVITY OF MERCURY AND MANGANIN UNDER PRESSURE

| Pressure, $\mathrm{kg} / \mathrm{cm}^{2}$ |  | 500 | 1003 | 1500 | 2000 | 2500 | 3000 | 4000 | 5000 | 6000 | 6500 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $R\left(p,-75^{\circ}\right) \mathrm{Hg}$. | . 9186 | . 9055 | . 8930 | . 8818 | . 8714 | . 8582 | . 8478 | . 8268 | . 8076 | . 7896 | . 7807 |
| $R\left(p, 25^{\circ}\right) \mathrm{Hg}$. | 1.0000 | . 9836 | . 9682 | . 9535 | . 9394 | . 9258 | . 9128 | . 8882 | . 8652 | . 8438 | . 8335 |
| * Hg | 1.0090 | . 9854 | . 9716 | . 9588 | . 9462 | . 9342 | . 9228 | . 9010 | . 8806 | . 8616 | . 8527 |
| $R\left(p, 125^{\circ}\right) \mathrm{Hg}$. | 1.0970 | 1.0770 | 1.0583 | 1.0400 | 1.0230 | 1.0070 | . 9908 | . 9614 | . 9342 | . 9086 | . 8966 |

[^174]
## TABLE 395.-THERMAL ELECTROMOTIVE FORCE OF ZINC VERSUS PLATINUM

'Temperature versus emf

| ${ }^{\circ} \mathrm{C}$ | mv | ${ }^{\circ} \mathrm{C}$ | mv | ${ }^{\circ} \mathrm{C}$ | mv |
| ---: | ---: | ---: | ---: | ---: | :---: |
| 0 | .000 | 150 | 1.276 | 300 | 3.417 |
| 25 | +.153 | 175 | 1.572 | 325 | 3.853 |
| 50 | .331 | 200 | 1.894 | 350 | 4.310 |
| 75 | .533 | 225 | 2.240 | 475 | 4.786 |
| 100 | .758 | 250 | 2.610 | 400 | 5.290 |
| 125 | 1.005 | 3.002 | 415 | 5.604 |  |

TABLE 396.-CONDUCTIVITY AND RESISTIVITY OF MISCELLANEOUS ALLOYS
Temperature coefficients
Conductivity in mhos or $\frac{1}{\text { ohms-cm }}=\gamma^{t}=\gamma^{0}\left(1-a t+b t^{2}\right)$ and resistivity in microhm -cm $=\rho^{t}=\rho^{0}\left(1+a t-b t^{2}\right)$.


This table shows the conductivity of alloys and the variation of the conductivity with temperature. The conductivity is given as $C_{t}=C_{0}\left(1-a t+b t^{2}\right)$, and the range of tem: perature was from $0^{\circ}$ to $100^{\circ} \mathrm{C}$.
The table is arranged in three groups to show (1) that certain metals when melted together produce a solution which has a conductivity equal to the mean of the conductivities of the components, (2) the behavior of those metals alloyed with others, and (3) the behavior of the metals alloyed together.

Part 1

| Alloys | Weight | Volume \% |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | of first named |  | $\frac{C_{0}}{10^{4}}$ | $a \times 10^{6}$ | ${ }^{6} \times 10$ |
| $\mathrm{Sn}_{0} \mathrm{~Pb}$ | 77.04 | 83.96 | 7.57 | 3890 |  |
| $\mathrm{Sn} \mathrm{c}_{\text {Cd }}$ | 82.41 | 83.10 | 9.18 | 4080 | 11870 |
| SnZn | 78.06 | 77.71 | 10.56 | 3880 | 8720 |
| PbSn | 64.13 | 53.41 | 6.40 | 3780 | 8420 |
| ZnCd 2 | 24.76 | 26.06 | 16.16 | 3780 | 8000 |
| SnCd4 | 23.05 | 23.50 | 13.67 | 3850 | 9410 |
| CdPb ${ }_{8}$ | 7.37 | 10.57 | 5.78 | 3500 | 7270 |

Part 2

| Alloys | Volume | Weigh |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | of first named |  | $C_{0}$ | $a \times 10^{8}$ | $b \times 10$ |
| Lead-silver ( $\mathrm{Pb}_{20} \mathrm{Ag}$ ) | 95.05 | 94.64 | 5.60 | 3630 | 7960 |
| Lead-silver ( PbAg ) | 48.97 | 46.90 | 8.03 | 1960 | 3100 |
| Lead-silver ( $\mathrm{PbAg}_{2}$ ) | 32.44 | 30.64 | 13.80 | 1990 | 2600 |
| Tin-gold ( $\mathrm{Sn}_{12} \mathrm{Au}$ ) | 77.94 | 90.32 | 5.20 | 3080 | 6640 |
| " " (Sn ${ }_{0} \mathrm{Au}$ ) | 59.54 | 79.54 | 3.03 | 2920 | 6300 |
| Tin-copper | 92.24 | 93.57 | 7.59 | 3680 | 8130 |
|  | 80.58 | 83.60 | 8.05 | 3330 | 6840 |
| " " | 12.49 | 14.91 | 5.57 | 547 | 294 |
| " " | 10.30 | 12.35 | 6.41 | 666 | 1185 |
| " " | 9.67 | 11.61 | 7.64 | 691 | 304 |
| " " | 4.96 | 6.02 | 12.44 | 995 | 705 |
| " " | 1.15 | 1.41 | 39.41 | 2670 | 5070 |
| Tin-silyer | 91.30 | 96.52 | 7.81 | 3820 | 8190 |
|  | 53.85 | 75.51 | 8.65 | 3770 | 8550 |
| Zinc-copper | 36.70 | 42.06 | 13.75 | 1370 | 1340 |
|  | 25.00 | 29.45 | 13.70 | 1270 | 1240 |
| " " | 16.53 | 23.61 | 13.44 | 1880 | 1800 |
| " " | 8.89 | 10.88 | 29.61 | 2040 | 3030 |
| " " . | 4.06 | 5.03 | 38.09 | 2470 | 4100 |

Note.-Barus has pointed out that the temperature variation of platinum alloys containing less than $10 \%$ of the other metal can be nearly expressed by an equation $y=\frac{n}{x}-m$, where $y$ is the temperature coefficient and $x$ the specific resistance, $m$ and $n$ being constants. If $a$ be the temperature coefficient at $0^{\circ} \mathrm{C}$ and $s$ the corresponding specific resistance, $s(\alpha+m)=n$

For platinum alloys Barus's experiments gave $m=-.000194$ and $n=.0378$.
For steel $m=-.000303$ and $n=.0620$.
Matthiessen's experiments reduced by Barus gave for
Gold alloys $m=-.000045, n=.00721$.
Silver " $m=-.000112, n=.00538$.
Copper " $\quad m=-.000386, n=.00055$.
(continued)

Part 3

| Alloys | Weight \% | Volume\% |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | of first $\underbrace{\text { named }}$ |  | $C_{0}$ |  |  |
| Gold-copper | 99.23 | 98.36 | 35.42 | 2650 | 4650 |
|  | 90.55 | 81.66 | 10.16 | 749 | 81 |
| Gold-silver | 87.95 | 79.86 | 13.46 | 1090 | 793 |
|  | 87.95 | 79.86 | 13.61 | 1140 | 1160 |
| " " | 64.80 | 52.08 | 9.48 | 673 | 246 |
| " " | 64.80 | 52.08 | 9.51 | 721 | 495 |
| " " | 31.33 | 19.86 | 13.69 | 885 | 531 |
| " " | 31.33 | 19.86 | 13.73 | 908 | 641 |
| Gold-copper | 34.83 | 19.17 | 12.94 | 864 | 570 |
|  | 1.52 | . 71 | 53.02 | 3320 | 7300 |
| Platinum-silver | 33.33 | 19.65 | 4.22 | 330 | 208 |
|  | 9.81 | 5.05 | 11.38 | 774 | 656 |
| " " | 5.00 | 2.51 | 19.96 | 1240 | 1150 |
| Palladium-silver | 25.00 | 23.28 | 5.38 | 324 | 154 |
| Copper-silver | 98.08 | 98.35 | 56.49 | 3450 | 7990 |
|  | 94.40 | 95.17 | 51.93 | 3250 | 6940 |
| " " | 76.74 | 77.64 | 44.06 | 3030 | 6070 |
| " " | 42.75 | 46.67 | 47.29 | 2870 | 5280 |
| " " | 7.14 | 8.25 | 50.65 | 2750 | 4360 |
| " " | 1.31 | 1.53 | 50.30 | 4120 | 8740 |
| Iron-gold | 13.59 |  | 1.73 | 3490 | 7010 |
|  | 9.80 | 21.18 | 1.26 | 2970 | 1220 |
|  | 4.76 | 10.96 | 1.46 | 487 | 103 |
| Iron-copper | . 40 | . 46 | 24.51 | 1550 | 2090 |
| Phosphorus-copper | 2.50 | - | 4.62 | 476 | 145 |
|  |  | - | 14.91 | 1320 | 1640 |
| Arsenic-copper |  | - | 3.97 | 516 | 989 |
|  | 2.80 | - | 8.12 | 736 | 446 |
|  | trace | - | 38.52 | 2640 | 4830 |

The electrical resistivity ( $\rho$, ohm- cm ) of good conductors depends greatly on chemical purity, Slight contamination even with metals of lower $\rho$ may greatly increase $\rho$. Solid solutions of good conductors generally have higher $\rho$ than components. Reverse is true of bad conductors. In solid state allotropic and crystalline forms greatly modify $\rho$. For liquid metals this last cause of variability disappears. The + temperature coefficients of pure metals is of the same order as the coefficients of expansion of gases. For temperature resistance ( $t, \rho$ ) plot at low temperatures the graph is convex toward the axis of $t$ and probably approaches tangency to it. However for extremely low temperatures Onnes finds very sudden and great drops in $\rho$, e.g., for mercury, $\rho_{3 . \text { ok }}<4 \times 10^{-10} \rho_{o}$ and for $\mathrm{Sn}, \rho_{3 . \text { sk }}<10^{-7} \rho_{0}$. The $t, \rho$ graph for an alloy may be nearly parallel to the $t$ axis, cf. constantan; for poor conductors $\rho$ may decrease with increasing $t$. At the meltingpoints there are three types of behavior of good conductors; those about doubling $\rho$ and then possessing nearly linear $t, \rho$ graphs ( $\mathrm{Al}, \mathrm{Cu}, \mathrm{Sn}, \mathrm{Au}, \mathrm{Ag}, \mathrm{Pb}$ ) ; those where $\rho$ suddenly increases and then the + temp. coefficient is only approximately constant $(\mathrm{Hg}, \mathrm{Na}, \mathrm{K})$; those about doubling $\rho$ then having a - , slowly changing to a + temp. coef. ( $\mathrm{Zn}, \mathrm{Cd}$ ) ; those where $\rho$ suddenly decreases and thereafter steadily increases ( $\mathrm{Sb}, \mathrm{Bi}$ ). The values from different authorities do not necessarily fit because of different samples of metals. Resistivities are in microhm-cm unless otherwise stated. Italicized figures indicate liquid state.

| Gold |  |  | Copper |  |  | Silver |  |  | Zinc |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\rho_{t}$ |  |  | $\rho_{t}$ |  |  | $\rho_{8}$ | $\stackrel{ }{ }$ |  | $\rho_{1}$ |
| ${ }^{\circ} \mathrm{C}$ | $\rho_{t}$ | $\overline{\rho_{0}}$ | ${ }^{\circ} \mathrm{C}$ | $\rho_{1}$ | $\rho_{0}$ | ${ }^{\circ} \mathrm{C}$ | $\rho_{1}$ | $\rho_{0}$ | ${ }^{\circ} \mathrm{C}$ | $\rho_{t}$ | $\rho_{0}$ |
| -252.8 | . 018 | . 0081 | $-258.6$ | . 014 | . 0091 | -258.6 | . 009 | . 0057 | -252.9 | . 0511 | . 0089 |
| -200. | . 601 | . 267 | -252.8 | . 016 | . 0103 | -252.8 | . 014 | . 0090 | -200. | 1.39 | . 242 |
| -192.5 | . 520 | . 231 | -251.1 | . 028 | . 0178 | -189.5 | . 334 | . 222 | -191.1 | 1.23 | . 214 |
| -150. | .997 | . 444 | -206.6 | . 163 | . 1035 | $-200$. | . 357 | . 237 | $-150$. | 2.00 | . 348 |
| $-100$. | 1.400 | . 623 | -192.9 | . 249 | . 1580 | $-150$. | . 638 | . 424 | $-100$. | 2.90 | . 504 |
| - 77.6 | 1.564 | . 696 | -150. | . 567 | . 359 | $-100$. | . 916 | . 608 | - 77.8 | 3.97 | . 691 |
| - 50. | 1.813 | . 806 | $-100$. | . 904 | . 573 | $-76.8$ | 1.040 | .690 | -50 . | 4.04 | . 703 |
| 0. | 2.247 | 1.00 | - 50. | 1.240 | . 786 | - 50. | 1.212 | . 805 | 0. | 5.75 | 1.00 |
| 100. | 2.97 | 1.32 | 0. | 1.578 | 1.00 | 0. | 1.506 | 1.00 | 100. | 7.95 | 1.38 |
| 200. | 3.83 | 1.70 | 100. | 2.28 | 1.44 | 100. | 2.15 | 1.43 | 300. | 13.25 | 2.30 |
| 500. | 6.62 | 2.94 | 200. | 2.96 | 1.88 | 200. | 2.80 | 1.86 | 415. | 17.00 | 2.96 |
| 750. | 9.35 | 4.16 | 500. | 5.08 | 3.22 | 400. | 3.46 | 2.30 | 427. | 37.30 | 6.49 |
| 1000. | 12.54 | 5.58 | 750. | 7.03 | 4.46 | 750. | 6.65 | 4.42 | 450. | 37.08 | 6.46 |
| 1063. | 13.50 | 6.01 | 1000. | 9.42 | 5.97 | 960. | 8.4 | 5.58 | 500. | 36.60 | 6.36 |
| 1063. | 30.82 | 13.7 | 1083. | 10.20 | 6.47 | 960. | 16.6 | 11.0 | 600. | 35.90 | 6.25 |
| 1200. | 32.8 | 14.6 | 1083. | 21.30 | 13.5 | 1000. | 17.01 | 11.3 | 700. | 35.60 | 6.19 |
| 1400. | 35.6 | 15.8 | 1200. | 22.30 | 14.1 | 1200. | 19.36 | 12.9 | 800. | 35.60 | 6.19 |
| 1500. | 37.0 | 16.5 | 1400. | 23.86 | 15.1 | 1400. | 21.72 | 14.4 | 850. | 35.74 | 6.21 |
|  |  |  | 1500. | 24.62 | 15.6 | 1500. | 23.0 | 15.3 |  |  |  |
| Mercury |  |  | Potassium |  |  | Sodium |  |  | Iron |  |  |
| ${ }^{\circ} \mathrm{C}$ | $\mathrm{P}_{8}$ | $\rho_{t}$ | ${ }^{\circ} \mathrm{C}$ | $\rho_{t}$ |  | ${ }^{\circ} \mathrm{C}$ | $\rho_{t}$ |  | ${ }^{\circ} \mathrm{C}$ | $\rho_{1}$ | $\frac{\rho_{t}}{\rho_{0}}$ |
|  |  | $\rho_{0}$ |  | $\rho_{8}$ | $\rho_{0}$ |  | $\rho_{1}$ | $\rho_{0}$ |  |  |  |
| -200. | 5.38 | . 057 | -200. | 1.720 | . 246 | -200. | . 605 | . 137 | -252.7 | . 011 | . 0010 |
| $-150$. | 10.30 | . 109 | - 150. | 2.654 | . 379 | $-150$. | 1.455 | . 330 | $-200$. | . 57 | . 053 |
| -100. | 15.42 | . 164 | - 100. | 3.724 | . 532 | $-100$. | 2.380 | . 541 | -192.5 | . 844 | . 079 |
| - 50. | 21.4 | . 227 | $-50$. | 5.124 | . 732 | - 50. | 3.365 | . 764 | $-100$. | 5.92 | . 554 |
| - 30. | 91.7 | . 975 | 0. | 7.000 | 1.00 | 0. | 4.40 | 1.000 | $-75.1$ | 6.43 | . 602 |
| 0. | 94.1 | 1.000 | 20. | 7.116 | 1.016 | 20. | 4.873 | 1.107 | - 50. | 8.15 | . 763 |
| 50. | 98.3 | 1.045 | 60. | 8.790 | 1.256 | 93.5 | 6.290 | 1.429 | - 0. | 10.68 | 1.00 |
| 100. | 103.1 | 1.096 | 65. | 13.40 | 1.914 | 100. | 9.220 | 2.095 | 100. | 16.61 | 1.554 |
| 200. | 114.0 | 1.212 | 100. | 15.31 | 2.187 | 120. | 9.724 | 2.209 | 200. | 24.50 | 2.293 |
| 300. | 127.0 | 1.350 | 120. | 16.70 | 2.386 | 140. | 10.34 | 2.349 | 400. | 43.29 | 4.052 |
| Manganin |  |  | German silver |  |  | Constantan |  |  | 90\% | Pt 10\%\% | Rh |
|  |  | $\rho_{1}$ |  |  | $\rho_{i}$ |  |  | $\rho_{t}$ |  |  | $\rho_{t}$ |
| ${ }^{\circ} \mathrm{C}$ | $\rho_{1}$ | $\rho_{0}$ | ${ }^{\circ} \mathrm{C}$ | $\rho_{8}$ | $\rho_{0}$ | ${ }^{\circ} \mathrm{C}$ | $\rho_{t}$ | $\rho_{0}$ | ${ }^{\circ} \mathrm{C}$ | $\rho_{1}$ | $\rho_{0}$ |
| $-200$. | 37.8 | . 974 | $-200$. | 27.9 | . 930 | -200. | 42.4 | . 961 | -200. | 14.49 | . 685 |
| $-150$. | 38.2 | . 985 | $-150$. | 28.7 | . 957 | -150. | 43.0 | . 975 | $-150$. | 16.29 | . 770 |
| $-100$. | 38.5 | . 992 | $-108$. | 29.3 | . 977 | $-100$. | 43.5 | . 986 | $-100$. | 18.05 | . 854 |
| - 50. | 38.7 | . 997 | -- 50. | 29.7 | . 990 | - 50. | 43.9 | . 995 | - 50. | 19.66 | . 930 |
| $\theta$. | 38.8 | 1.000 | 0. | -30.0 | 1.000 | 0. | 44.1 | 1.000 | 0. | 21.14 | 1.000 |
| 100. | 38.9 | 1.003 | 100. | 33.1 | 1.103 | 100. | 44.6 | 1.012 | 100. | 24.20 | 1.145 |
| 400. | 38.3 | . 987 |  |  |  | 400. | 44.8 | 1.016 |  |  |  |

TABLE 398.-RESISTIVITIES AT HIGH AND LOW TEMPERATURES (concluded) (Ohm-cm unless stated otherwise.)

| Platinum |  |  | Lead |  |  | Bismuth |  |  | Cadmium |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\rho_{t}$ |  |  | $\rho_{i}$ |  |  | $\rho_{t}$ |  |  | $\rho_{i}$ |
| ${ }^{\circ} \mathrm{C}$ | $\rho_{8}$ | $\rho_{0}$ | ${ }^{\circ} \mathrm{C}$ | $\rho_{8}$ | $\rho_{0}$ | ${ }^{\circ} \mathrm{C}$ | $\rho_{t}$ | $\rho_{0}$ | ${ }^{\circ} \mathrm{C}$ | $\rho_{1}$ | $\rho_{0}$ |
| -265. | . 10 | . 0092 | -252.9 | . 59 | . 0298 | -200. | 34.8 | . 314 | -252.9 | . 17 | . 0218 |
| -25.3. | . 15 | . 014 | -203. | 4.42 | . 223 | -150 . | 55.3 | . 499 | --200. | 1.66 | . 214 |
| -233. | . 54 | . 049 | -192.8 | 5.22 | . 264 | $-100$. | 75.6 | . 683 | -190.2 | 2.00 | 2.58 |
| -153. | 4.18 | . 378 | $-103$. | 11.8 | . 598 | - 50. | 94.3 | . 852 | -183.1 | 2.22 | . 286 |
| - 73. | 7.83 | . 708 | - 75.8 | 13.95 | . 705 | 0. | 110.7 | 1.00 | -139.2 | 3.60 | . 464 |
| 0. | 11.05 | 1.00 | $-53$. | 15.7 | . 792 | 17. | 120.0 | 1.083 | -100 . | 4.80 | . 619 |
| 100. | 14.1 | 1.28 | 0. | 19.8 | 1.00 | 100. | 156.5 | 1.413 | 0. | 7.75 | 1.00 |
| 200. | 17.9 | 1.62 | 100. | 27.8 | 1.403 | 200. | 214.5 | 1.937 | 300. | 16.50 | 2.13 |
| 400. | 25.4 | 2.30 | 200. | 38.0 | 1.919 | 259. | 267.0 | 2.411 | 325. | 33.76 | 4.35 |
| 800. | 40.3 | 3.65 | 319. | 50.0 | 2.52 | 263. | 127.5 | 1.150 | 350. | 33.60 | 4.33 |
| 1000. | 47.0 | 4.25 | 333. | 95.9 | 4.80 | 300. | 128.9 | 1.164 | 400. | 33.70 | 4.35 |
| 1200. | 52.7 | 4.77 | 400. | 98.3 | 4.96 | 500. | 139.9 | 1.263 | 500. | 35.12 | 4.40 |
| 1400. | 58.0 | 5.25 | 600. | 107.2 | 5.41 | 700. | 150.8 | 1.361 | 700. | 35.78 | 4.62 |
| 1600. | 63.0 | 5.70 | 800. | 116.2 | 5.86 | 750. | 153.5 | 1.386 |  |  |  |
| Tin |  |  | Carbon, graphite * |  |  | Fused silica |  |  | Alundum cement |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | $\rho_{t}$ | ${ }^{\circ} \mathrm{C}$ | $\rho$ in ohms-cm |  |  |  |  | ${ }^{\circ} \mathrm{C}$ |  | $\rho$ in ohms. cm |
| ${ }^{\circ} \mathrm{C}$ | $\rho$ \% | $\rho_{0}$ |  |  |  | ${ }^{\circ} \mathrm{C} \quad \rho=$ megohms-cm |  |  |  |  |  |
| $-200$. | 2.60 | . 199 | Carbon Graphite |  |  | $\begin{array}{rr}15 . & >200,000,000 . \\ 230 .\end{array}$ |  |  | 20. |  | $>9 \times 10^{\circ}$ |
| $-100$. | 7.57 | . 580 | 0. | . 0035 | . 00080 |  |  |  | 800. |  | 30800. |
| 0. | 13.05 | 1.00 | 500. | . 0027 | . 00083 | $\begin{array}{lr}3300 . & 200.000 . \\ 350 . & 30,000 .\end{array}$ |  |  | 900. |  | 13600. |
| 200. | 20.30 | 1.55 | 1000. | . 0021 | . 00087 |  |  |  | 1000. |  | 7600. |
| 225. | 22.00 | 1.69 | 1500. | . 0015 | . 00090 | 450. |  | 80. |  |  | 6500.2300. |
| 235. | 47.60 | 3.65 | 2000. | . 0011 | . 00100 | 700. |  | 30. | 1200. |  |  |
| 750. | 61.22 | 4.69 | 2500. | . 0009 | . 0011 | 850. |  | bout 20. | 1600. |  | 190. |

TABLE 399.-SUPERCONDUCTIVITY OF SOME METALS ${ }^{145}$

| Metal | $\mathrm{T}^{\circ} \mathrm{K}$ | Metal | $\mathrm{T}^{\circ} \mathrm{K}$ | Metal | $\mathrm{T}^{\circ} \mathrm{K}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Nb | 9.22 | In | 3.38 | U | . 75 |
| Pb | 7.2 | Re | 2.57* | Os | . 71 |
| La | 5.2 | Tl | 2.4 | Zr | .54* |
| Ta | 4.4 | Th | 1.32 | Cd | . 54 |
| V | 4.3 | Al | 1.15 | Ti | . $53{ }^{\dagger}$ |
| Hg | 4.15 | Ga | 1.12 | Ru | . 47 |
| Sn | 3.71 | Zn | . $95^{\dagger}$ | Hf | . 35 |

145 Smith, Thomas S., Ohio State University, private communication.

* Daunt. J. G., and Smith, T. S. †Daunt, J. G., and Heer, C. V., Phys. Rev., vol. 76, pp. 719 and 1324, 1948.

TABLE 400.-SUPERCONDUCTIVITY OF SOME ALLOYS AND COMPOUNDS ${ }^{146}$

| NbC | $10.1{ }^{\circ} \mathrm{K}$ | $\mathrm{Pb}-\mathrm{As} \mathrm{alloy}$. | $8.4{ }^{\circ} \mathrm{K}$ | PbS | $4.1{ }^{\circ} \mathrm{K}$ | $\mathrm{W}_{2} \mathrm{C}$ | $2.05{ }^{\circ} \mathrm{K}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TaC | 9.2 | MoC | 7.7 | $\mathrm{Hg}_{5} \mathrm{Tl}_{7}$ |  | $\mathrm{Au}_{2} \mathrm{Bi}$ |  |
| $\mathrm{Pb}-\mathrm{As}-\mathrm{Bi}$ | 9.0 | $\mathrm{N}_{2} \mathrm{~Pb} 5$ | 7.2 | ZrB | 2.82 | CuS | 1.6 |
| $\mathrm{Pb}-\mathrm{Bi}-\mathrm{Sb}$ | 8.9 | $\mathrm{Bin}_{0} \mathrm{Tl}_{3}$ | 6.5 | WC | 2.8 | TiN | 1.4 |
| $\mathrm{Pb}-\mathrm{Sn}-\mathrm{Bi}$ | 8.5 | $\mathrm{Sb}_{2} \mathrm{Tl}_{7}$ | 5.5 | $\mathrm{Mo}_{2} \mathrm{C}$ | 2.4 | VN | 1.3 |
|  |  | TaSi .... | 4.2 |  |  | TiC | 1.1 |

[^175]
## TABLE 401.-VOLUME AND SURFACE RESISTANCE OF SOLID DIELECTRICS

The resistance between two conductors insulated by a solid dielectric depends both upon the surface resistance and the volume resistance of the insulator. The volume resistivity, $\rho$, is the resistance between two opposite faces of a centimeter cube. The surface resistivity, $\sigma$, is the resistance between two opposite edges of a centimeter square of the surface. The surface resistivity usually varies through a wide range with the humidity.

| Material |
| :--- | :--- | :--- |

## TABLE 402.-ELECTRICAL RESISTIVITY OF SOME OXIDES AND miscellaneous minerals *

| Material | Resistivity ohm-cm | Material | Resistivity |
| :---: | :---: | :---: | :---: |
| Graphite, commercial |  | Sulfur | $10^{14}$ |
| electrodes (density $=1.5$ ) | . $001-.0013$ | $\mathrm{PbO}_{2}$, synthetic | . 000092 |
| Hematite, $\mathrm{Fe}_{2} \mathrm{O}_{3}$, mineral. . | . $35-.7$ | $\mathrm{MnO}_{2}$, synthetic | 6 |
| Iron, metalic, meteoric ... | $2.4-3.2 \times 6^{-6}$ ? | $\mathrm{W}_{2} \mathrm{O}_{5}$ | . 00045 |
| Rock salt, pure impure | $\begin{aligned} & 10^{9}-10^{7} \\ & 10^{\circ} \end{aligned}$ | $\mathrm{WO}_{3}$ | $2 \times 10^{5}$ |

* For reference, see footnote 45, p. 136.

TABLE 403.-ELECTRICAL RESISTIVITY OF ROCKS AND SOILS*

| Igneous rocks | Resistivity ohm-cm | Sedimentary rocks | Resistivity |
| :---: | :---: | :---: | :---: |
| Granite | $10^{7}-10^{\circ}$ | Limestone | $10^{4}$ |
| Lava flow (basic) | $10^{8}-10^{7}$ | Limestone, Cambrian | $10^{4}-10^{5}$ |
| Lava, fresh | $3 \times 10^{5}-10^{6}$ | Sandstone, eastern | $3 \times 10^{3}-10^{4}$ |
| Quartz vein, massive | $>10^{\circ}$ | Sandstone |  |
| Metamorphic rocks | $\begin{aligned} & \text { Resistivity } \\ & \text { ohm-cm } \end{aligned}$ | Unconsolidated materials | Resistivity |
| Marble, white | $\begin{aligned} & 10^{10} \\ & 4 \times 10^{5} \end{aligned}$ | Clay, blue .............. | $\begin{gathered} \text { ohm-cm } \\ 2 \times 10^{4} \end{gathered}$ |
| Marble ${ }^{\text {Marble, }}$ yellow | ${ }_{10}^{4 \times 10^{10}}$ | Clay, blue earth | $10^{4}-4 \times 10^{4}$ |
| Schist, mica .. | $10^{7}$ | Clay, fire | $2 \times 10^{5}$ |
| Shale, Nonesuch | $10^{4}$ | Gravel |  |
| Shale, bed | $10^{5}$ | Sand, dry Sand, | $\begin{aligned} & 10^{5}-10^{6} \\ & 10^{5}-10^{6} \end{aligned}$ |

[^176]TABLE 404.-RESISTIVITY OF SOILS AND SEA WATER MEASURED WITH HIGH-FREQUENCY ALTERNATING CURRENT*

| Material | Frequency kilocycles/sec | Resistivity ohm/cm | Material | Frequency kilocycles/sec | Resistivity ohm/cm |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Soil, very dry Topsoil, dry | 1 to 10,000 | $10^{7}$ | Clay, dry | 37,000 | 60,000 |
|  | 37,000 | 7,000 | Chalk <br> (moisture, 24\%) | 100 | 33,000 |
|  |  |  |  | 1,200 | 22,000 |
|  |  |  |  | 10,000 | 14,000 |
| Loam, dark (moisture, $60 \%$ ) |  |  | Sea water | 100 | 21 |
|  | 100 | 2,600 |  | 1,200 | 21 |
|  | 1,200 | 2,300 |  | 10,000 | 16.5 |
|  | 10,000 | 1,500 |  |  |  |

* For reference, see footnote 45, p. 136.


## TABLE 405.-ELECTRICAL RESISTIVITY OF NATURAL WATERS*

| Material | Resistivity ohm-cm | Material | Resistivity ohm-cm |
| :---: | :---: | :---: | :---: |
| Very fresh distilled waters | $2 \times 10^{7}$ | Potable ground waters | $10^{3}-10^{5}$ |
| Mine waters | 500 | Surface waters. | $10^{5}$ |

* For reference, see footnote 45, p. 136.


## TABLE 406.-RESISTIVITY OF SOME GLASSES AT THREE TEMPERATURES ${ }^{147}$

| Glass | Principal use | Density | Log 10 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\overbrace{\substack{\text { Volume resistivity } \\ \text { (ohm }-\mathrm{cm})}}$ |  | $350{ }^{\circ} \mathrm{C}$ |
|  |  |  | $25^{\circ} \mathrm{C}$ | $250{ }^{\circ} \mathrm{C}$ |  |
| Potash soda lead | Lamp tubing | 2.85 | 17.+ | 8.9 | 7.0 |
| Soda lime ..... | Lamp bulbs | 2.47 | 12.4 | 6.4 | 5.1 |
| Potash soda lead | Lamp tubing | 3.05 | 17.+ | 10.1 | 8.0 |
| Hard Lime ..... | Cooking utensils | 2.53 | 17.+ | 11.4 | 9.4 |
| Borosilicate . | Kovar sealing | 2.28 | 17. | 9.2 | 7.4 |
| Borosilicate . | Low loss electrical | 2.13 | 17. + | 11.2 | 9.1 |
| Borosilicate . . | Baking ware | 2.24 | 15. | 8.2 | 6.7 |
| Pyrex ..... | General | 2.23 | 15. | 8.1 | 6.6 |
| Vycor | Low expansion ultraviolet transmission | 2.18 | 17.+ | 11.2 | 9.2 |
| Fused quartz |  | 2.20 |  |  | 10.48 |

[^177]
## TABLE 407.-CONDUCTIVITY OF ELECTROLYTIC SOLUTIONS

In these tables $m$ represents the number of gram molecules to the liter of water in the solution for which the conductivities are tabulated. The conductivities were obtained by measuring the resistance of a cell filled with the solution by means of a Wheatstone bridge alternating current and telephone arrangement. The results are for $18^{\circ} \mathrm{C}$, and relative to mercury at $0^{\circ} \mathrm{C}$, the cell having been standardized by filling with mercury and measuring the resistance. They are supposed to be accurate to within one percent of the true value.

The tabular numbers were obtained from the measurements in the following manner:
Let $K_{18}=$ conductivity of the solution at $18^{\circ} \mathrm{C}$ relative to mercury at $0^{\circ} \mathrm{C}$.
$K^{{ }^{*}}{ }_{18}=$ conductivity of the solvent water at $18^{\circ} \mathrm{C}$ relative to mercury at $0^{\circ} \mathrm{C}$.
Then $K_{18}-K^{{ }^{\star}}{ }_{18}=k_{18}=$ conductivity of the electrolyte in the solution measured.
$\frac{k_{18}}{m}=\mu=$ conductivity of the electrolyte in the solution per molecule, or the "specific molecular conductivity."

## Part 1.-Value of $k_{18}$ for a few electrolytes

This short table illustrates the apparent law that the conductivity in very dilute solutions is proportional to the amount of salt dissolved.

| $m$ | KCl | NaCl | $\mathrm{AgNO}_{3}$ | $\mathrm{KC}_{2} \mathrm{H}_{3} \mathrm{O}_{2}$ | $\mathrm{~K}_{2} \mathrm{SO}_{4}$ | $\mathrm{MgSO}_{4}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| .00001 | 1216 | 1.024 | 1080 | .939 | 1.275 | 1.056 |
| .00002 | 2.434 | 2.056 | 2.146 | 1.886 | 2.532 | 2.104 |
| .00006 | 7.272 | 6.162 | 6.462 | 5.610 | 7.524 | 6.216 |
| .0001 | 12.09 | 10.29 | 10.78 | 9.34 | 12.49 | 10.34 |

Part 2.-Electrochemical equivalents and normal solutions
The following table of the electrochemical equivalent numbers and the densities of approximately normal solutions of the salts quoted in Table 409 may be convenient. They represent g per $\mathrm{cm}^{3}$ of the solution at the temperature given.

| Salt dissolved | g per 1 | $m$ | ${ }^{\text {Temp. }}$ C. | Density | Salt disso.'ved | g per 1 | m |  | Density |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| KCl | 74.59 | 1.0 | 15.2 | 1.0457 | ${ }_{2}^{1} \mathrm{~K}_{2} \mathrm{SO}_{4}$ | 87.16 | 1.0 | 18.9 | 1.0658 |
| $\mathrm{NH}_{4} \mathrm{Cl}$ | 53.55 | 1.0009 | 18.6 | 1.0152 | $\frac{1}{2} \mathrm{Na}_{2} \mathrm{SO}_{4}$ | 71.09 | 1.0003 | 18.6 | 1.0602 |
| NaCl | 58.50 | 1.0 | 18.4 | 1.0391 | ${ }_{2} \mathrm{Li}_{2} \mathrm{SO}_{4}$ | 55.09 | 1.0007 | 186 | 1.0445 |
| LiCl | 42.48 | 1.0 | 18.4 | 1.0227 | ${ }_{2} \mathrm{MgSO}_{4}$ | 60.17 | 1.0023 | 186 | 1.0573 |
| $\frac{1}{2} \mathrm{BaCl}_{3}$ | 104.0 | 1.0 | 18.6 | 1.0888 | ${ }_{2} \mathrm{ZnSO}_{4}$ | 80.58 | 1.0 | 5.3 | 1.0794 |
| ${ }_{2} \mathrm{ZnCl}_{3}$ | 68.0 | 1.012 | 15.0 | 1.0592 | $\frac{1}{2} \mathrm{CuSO}_{4}$ | 79.9 | 1.001 | 18.2 | 1.0776 |
| KI | 165.9 | 1.0 | 18.6 | 1.1183 | ${ }_{2}^{1} \mathrm{~K}_{2} \mathrm{CO}_{3}$ | 69.17 | 1.0006 | 18.3 | 1.0576 |
| $\mathrm{KNO}_{3}$ | 101.17 | 1.0 | 18.6 | 1.0601 | $\frac{1}{2} \mathrm{Na}_{2} \mathrm{CO}_{3}$ | 53.04 | 1.0 | 17.9 | 1.0517 |
| $\mathrm{NaNO}_{3}$ | 85.08 | 1.0 | 18.7 | 1.0542 | KOH | 56.27 | 1.0025 | 18.8 | 1.0477 |
| $\mathrm{AgNO}_{3}$ | 169.9 | 1.0 | -- | - | HCl | 35.51 | 1.0041 | 18.6 | 1.0161 |
| ${ }_{2}^{1} \mathrm{Ba}\left(\mathrm{NO}_{3}\right)_{2}$ | 65.28 | . 5 |  |  | $\mathrm{HNO}_{3}$ | 6313 | 1.0014 | 18.6 | 1.0318 |
| $\mathrm{KClO}_{3}$ | 61.29 | . 5 | 18.3 | 1.0367 | $\frac{1}{2} \mathrm{H}_{2} \mathrm{SO} 4$ | 49.06 | 1.0006 | 18.9 | 1.0300 |
| $\mathrm{KC}_{3} \mathrm{H}_{3} \mathrm{O}_{2}$ | 98.18 | 1.0005 | 18.6 | 1.0467 |  |  |  |  |  |

## TABLE 408.-TEMPERATURE COEFFICIENTS OF CONDUCTIVITY

The temperature coefficient in general diminishes with dilution, and for very dilute solutions appears to approach a common value. The following table gives the temperature coefficient for solutions containing 0.01 gram molecule of the salt.


TABLE 409.-SPECIFIC MOLECULAR CONDUCTIVITY OF SOLUTIONS
Mercury $=10^{8} /($ ohm-cm $)$

| Salt dissolved | $m=10$ | 5 | 3 | 1 | . 5 | . 1 | . 05 | . 03 | . 01 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{1}{2} \mathrm{~K}_{2} \mathrm{SO}_{4}$ | - | - | - | - | 672 | 736 | 897 | 959 | 1098 |
| KCl | - | - | 827 | 919 | 958 | 1047 | 1083 | 1107 | 1147 |
| KI | - | 770 | 900 | 968 | 997 | 1069 | 1102 | 1123 | 1161 |
| $\mathrm{NH}_{4} \mathrm{Cl}$ | - | 752 | 825 | 907 | 948 | 1035 | 1078 | 1101 | 1142 |
| $\mathrm{KNO}_{3}$ | - | - | 572 | 752 | 839 | 983 | 1037 | 1067 | 1122 |
| $\frac{1}{2} \mathrm{BaCl}_{2}$ | - | - | 487 | 658 | 725 | 861 | 904 | 939 | 1006 |
| $\mathrm{KClO}_{3}$ | - | - | - | - | 799 | 927 | (976) | 1006 | 1053 |
| $\frac{1}{2} \mathrm{BaN}_{2} \mathrm{O}_{6}$ | - | - | - | - | 531 | 755 | 828 | (870) | 951 |
| $\frac{1}{2} \mathrm{CuSO}_{4}$ | - |  | 150 | 241 | 288 | 424 | 479 | 537 | 675 |
| $\mathrm{AgNO}_{3}$ | - | 351 | 448 | 635 | 728 | 886 | 936 | (966) | 1017 |
| $\frac{1}{2} \mathrm{ZnSO}_{4}$ | - | 82 | 146 | 249 | $30 ?$ | 431 | 500 | 556 | 685 |
| $\frac{1}{2} \mathrm{MgSO}_{4}$ | - | 82 | 151 | 270 | 330 | 474 | 532 | 587 | 715 |
| $\frac{1}{2} \mathrm{Na}_{2} \mathrm{SO}_{4}$ | - |  | - | 475 | 559 | 734 | 784 | 828 | 906 |
| $\frac{1}{2} \mathrm{ZnCl}_{2}$ | 60 | 180 | 280 | 514 | 601 | 768 | 817 | 851 | 915 |
| NaCl | - | 398 | 528 | 695 | 757 | 865 | 897 | (920) | 962 |
| $\mathrm{NaNO}_{3}$ | - | - | 430 | 617 | 694 | 817 | 855 | 877 | 907 |
| $\mathrm{KC}_{2} \mathrm{H}_{3} \mathrm{O}_{2}$ | 30 | 240 | 381 | 594 | 671 | 784 | 820 | 841 | 879 |
| $\frac{1}{2} \mathrm{Na}_{2} \mathrm{CO}_{3}$ | - | - | 254 | 427 | 510 | 682 | 751 | 799 | 899 |
| ${ }_{2}^{\frac{1}{2} \mathrm{H}_{2} \mathrm{SO}_{4}}$ | 660 | 1270 | 1560 | 1820 | 1899 | 2084 | 2343 | 2515 | 2855 |
| $\mathrm{C}_{2} \mathrm{H}_{4} \mathrm{O}$ | . 5 | 2.6 | 5.2 | 12 | 19 | 43 | 62 | 79 | 132 |
| HCl | 600 | 1420 | 2010 | 2780 | 3017 | 3244 | 3330 | 3369 | 3416 |
| $\mathrm{HNO}_{3}$ | 610 | 1470 | 2070 | 2770 | 2991 | 3225 | 3289 | 3328 | 3395 |
| ${ }_{\frac{1}{3} \mathrm{H}_{3} \mathrm{PO}_{4}}$ | 148 | 160 | 170 | 200 | 250 | 430 | 540 | 620 | 790 |
| KOH | 423 | 990 | 1314 | 1718 | 1841 | 1986 | 2045 | 2078 | 2124 |
| $\mathrm{NH}_{3}$ | . 5 | 2.4 | 3.3 | 8.4 | 12 | 31 | 43 | 50 | 92 |
| Salt dissolved | . 006 | . 002 | . 001 | . 0006 | . 0002 | . 0001 | . 00006 | . 00002 | . 00001 |
| ${ }_{2}^{1} \mathrm{~K}_{2} \mathrm{SO}_{4}$ | 1130 | 1181 | 1207 | 1220 | 1241 | 1249 | 1254 | 1266 | 1275 |
| KCl | 1162 | 1185 | 1193 | 1199 | 1209 | 1209 | 1212 | 1217 | 1216 |
| KI | 1176 | 1197 | 1203 | 1209 | 1214 | 1216 | 1216 | 1216 | 1207 |
| $\mathrm{NH}_{4} \mathrm{Cl}$ | 1157 | 1180 | 1190 | 1197 | 1204 | 1209 | 1215 | 1209 | 1205 |
| $\mathrm{KNO}_{3}$ | 1140 | 1173 | 1180 | 1190 | 1199 | 1207 | 1220 | 1198 | 1215 |
| ${ }_{2}^{\frac{1}{2}} \mathrm{BaCl}_{2}$ | 1031 | 1074 | 1092 | 1102 | 1118 | 1126 | 1133 | 1144 | 1142 |
| $\mathrm{KClO}_{3}$ | 1068 | 1091 | 1101 | 1109 | 1119 | 1122 | 1126 | 1135 | 1141 |
| $\frac{1}{2} \mathrm{BaN}_{2} \mathrm{O}_{6}$ | 982 | 1033 | 1054 | 1066 | 1084 | 1096 | 1100 | 1114 | 1114 |
| $\frac{1}{2} \mathrm{CuSO}_{4}$ | 740 | 873 | 950 | 987 | 1039 | 1062 | 1074 | 1084 | 1086 |
| $\mathrm{AgNO}_{3}$ | 1033 | 1057 | 1068 | 1069 | 1077 | 1078 | 1077 | 1073 | 1080 |
| $\frac{1}{2} \mathrm{ZnSO}_{4}$ | 744 | 861 | 919 | 953 | 1001 | 1023 | 1032 | 1047 | 1060 |
| $\frac{1}{3} \mathrm{MgSO}_{4}$ | 773 | 881 | 935 | 967 | 1015 | 1034 | 1036 | 1052 | 1056 |
| $\frac{1}{3} \mathrm{Na}_{2} \mathrm{SO}_{4}$ | 933 | 980 | 998 | 1009 | 1026 | 1034 | 1038 | 1056 | 1054 |
| ${ }_{3}^{1} \mathrm{ZnCl}_{2}$ | 939 | 979 | 994 | 1004 | 1020 | 1029 | 1031 | 1035 | 1036 |
| NaCl | 976 | 998 | 1008 | 1014 | 1018 | 1029 | 1027 | 1028 | 1024 |
| $\mathrm{NaNO}_{3}$ | 921 | 942 | 952 | 956 | 966 | 975 | 970 | 972 | 975 |
| $\mathrm{KC}_{2} \mathrm{H}_{3} \mathrm{O}_{2}$ | 891 | 913 | 919 | 923 | 933 | 934 | 935 | 943 | 939 |
| ${ }_{\frac{1}{2} \mathrm{Na}_{2} \mathrm{CO}_{3}}$ | 956 | 1010 | 1037 | 1046 | 988 | 874 | 790 | 715 | 697* |
| ${ }_{2}^{\frac{1}{2} \mathrm{H}_{2} \mathrm{SO}_{4}}$ | 3001 | 3240 | 3316 | 3342 | 3280 | 3118 | 2927 | 2077 | 1413* |
| $\mathrm{C}_{2} \mathrm{H}_{4} \mathrm{O}$ | 170 | 283 | 380 | 470 | 796 | 995 | 1133 | 1328 | 1304* |
| HCl | 3438 | 3455 | 3455 | 3440 | 3340 | 3170 | 2968 | 2057 | 1254* |
| $\mathrm{HNO}_{3}$ | 3421 | 3448 | 3427 | 3408 | 3285 | 3088 | 2863 | 1904 | 1144* |
| $\frac{1}{3} \mathrm{H}_{3} \mathrm{PO}_{4}$ | 858 | 945 | 968 | 977 | 920 | 837 | 746 | 497 | 402* |
| KOH | 2141 | 2140 | 2110 | 2074 | 1892 | 1689 | 1474 | 845 | 747* |
| $\mathrm{NH}_{3}$ | 116 | 190 | 260 | 330 | 500 | 610 | 690 | 700 | 560* |

[^178]
## TABLE 410.-LIMITING VALUES OF $\mu$, THE SPECIFIC MOLECULAR CONDUCTIVITY

This table shows limiting values of $\mu=\frac{k}{m} \cdot 10^{8}$ for infinite dilution for neutral salts, calculated from Table 409.

| Salt | ${ }^{\mu}$ | Salt | ${ }^{\mu}$ | Salt | ${ }^{\mu}$ | Salt | ${ }^{\mu}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{2}^{1} \mathrm{~K}_{2} \mathrm{SO}_{4}$ | 1280 | $\frac{1}{2} \mathrm{BaCl}_{2}$ | 1150 | $\frac{1}{2} \mathrm{MgSO}_{4}$ | 1080 | $\frac{1}{2} \mathrm{H}_{2} \mathrm{SO}_{4}$ | 3700 |
| KCl | 1220 | ${ }_{2}^{1} \mathrm{KClO}_{3}$ | 1150 | ${ }_{2}^{1} \mathrm{Na}_{2} \mathrm{SO}_{4}$ | 1060 | $\mathrm{HCl}^{\text {a }}$. | 3500 |
| KI | 1220 | ${ }_{2}^{1} \mathrm{BaN}_{2} \mathrm{O}_{6}$ | 1120 | $\frac{1}{2} \mathrm{ZnCl}_{2}$ | 1040 | $\mathrm{HNO}_{3}$ | 3500 |
| $\mathrm{NH}_{4} \mathrm{Cl}$ | 1210 | ${ }_{2}^{1} \mathrm{CuSO}_{4}$ | 1100 | NaCl | 1030 | ${ }_{3} \mathrm{H}_{3} \mathrm{PO} \mathrm{S}_{4}$ | 1100 |
| $\mathrm{KNO}_{3}$ | 1210 | $\mathrm{AgNO}_{3}$ | 1090 | $\mathrm{NaNO}_{3}$ | 980 | KOH | 2200 |
|  |  | $\frac{1}{2} \mathrm{ZnSO}_{4}$ | 1080 | $\mathrm{K}_{2} \mathrm{C}_{2} \mathrm{H}_{3} \mathrm{O}_{2}$ | 940 | $\frac{1}{2} \mathrm{Na}_{2} \mathrm{CO}_{3}$ | 1400 |

TABLE 411.-THE EQUIVALENT CONDUCTIVITY OF THE SEPARATE IONS

| Ion | $0^{\circ} \mathrm{C}$ | $18^{\circ}$ | $25^{\circ}$ | $50^{\circ}$ | $75^{\circ}$ | $100^{\circ}$ | $128^{\circ}$ | $156^{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| K | 40.4 | 64.6 | 74.5 | 115 | 159 | 206 | 263 | 317 |
| Na | 26 | 43.5 | 50.9 | 82 | 116 | 155 | 203 | 249 |
| $\mathrm{NH}_{4}$ | 40.2 | 64.5 | 74.5 | 115 | 159 | 207 | 264 | 319 |
| Ag | 32.9 | 54.3 | 63.5 | 101 | 143 | 188 | 245 | 299 |
| ${ }_{2}^{1} \mathrm{Ba}$ | 33 | $55^{2}$ | 65 | 104 | 149 | 200 | 262 | 322 |
| ${ }_{2}^{1} \mathrm{Ca}$ | 30 | $51^{2}$ | 60 | 98 | 142 | 191 | 252 | 312 |
| $\frac{1}{5} \mathrm{La}$ | 35 | 61 | 72 | 119 | 173 | 235 | 312 | 388 |
| Cl | 41.1 | 65.5 | 75.5 | 116 | 160 | 207 | 264 | 318 |
| $\mathrm{NO}_{3}$ | 40.4 | 61.7 | 70.6 | 104 | 140 | 178 | 222 | 263 |
| $\mathrm{C}_{2} \mathrm{H}_{3} \mathrm{O}_{2}$ | 20.3 | 34.6 | 40.8 | 67 | 96 | 130 | 171 | 211 |
| $\frac{1}{2} \mathrm{SO}_{4}$ | 41 | $68^{2}$ | 79 | 125 | 177 | 234 | 303 | 370 |
| ${ }_{\frac{1}{2}}^{1} \mathrm{C}_{2} \mathrm{O}_{4}$ | 39 | $63^{2}$ | 73 | 115 | 163 | 213 | 275 | 336 |
| $\frac{1}{3} \mathrm{C}_{6} \mathrm{H}_{5} \mathrm{O}_{7}$ | 36 | 60 | 70 | 113 | 161 | 214 |  |  |
| ${ }_{4}^{1} \mathrm{Fe}(\mathrm{CN})$ 。 | 58 | 95 | 111 | 173 | 244 | 321 |  |  |
| H | 240 | 314 | 350 | 465 | 565 | 644 | 722 | 777 |
| OH | 105 | 172 | 192 | 284 | 360 | 439 | 525 | 592 |

TABLE 412.-HYDROLYSIS OF AMMONIUM ACETATE AND IONIZATION OF WATER

| Temperature | Percentage hydrolysis | Ioniza. tion constant of water | Hydrogen-ion concentration in pure water Equivalents per liter | Temperature | Percentage hydrolysis | Ionization constant of water | Hydrogen-ion concentration in pure water Equivalents per liter |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $t$ | $100{ }_{\text {h }}$ | $\mathrm{K}_{\mathrm{w}} \times 10^{14}$ | $\mathrm{C}_{\mathrm{H}} \times 10^{7}$ | $t$ | $100{ }_{h}$ | $\mathrm{K}_{\mathrm{W}} \times 10^{14}$ | $\mathrm{C}_{\mathrm{H}} \times 10^{7}$ |
| $0^{\circ} \mathrm{C}$ | - | . 089 | . 30 | $100^{\circ} \mathrm{C}$ | 4.8 | 48. | 6.9 |
| 18 | (.35) | . 45 | . 68 | 156 | 18.6 | 223. | 14.9 |
| 25 | ) | . 82 | . 91 | 218 | 52.7 | 461. | 21.5 |
|  |  |  |  | 306 | 91.5 | 168. | 13.0 |

## TABLE 413.-THE EQUIVALENT CONDUCTIVITY OF SALTS, ACIDS, AND BASES IN AQUEOUS SOLUTIONS

In the following table the equivalent conductance is expressed in reciprocal ohms. The concentration is expressed in milli-equivalents of solute per liter of solution at the temperature to which the conductance refers. (In the cases of potassium hydrogen sulfate and phosphoric acid the concentration is expressed in milli-formula-weights of solute, $\mathrm{KHSO}_{4}$ or $\mathrm{H}_{3} \mathrm{PO}_{4}$, per liter of solution, and the values are correspondingly the modal, or "formal," conductances.) Except in the cases of the strong acids the conductance of the water was substracted, and for sodium acetate, ammonium acetate and ammonium chloride the values have been corrected for the hydrolysis of the salts.

$$
\begin{gathered}
\text { Concentration in } \frac{\mathrm{g} \text { equivalents }}{10001} \text {. } \\
\text { Equivalent conductance in } \frac{\text { reciprocal ohm }-\mathrm{cm}}{\mathrm{~g} \text { equivalents per } \mathrm{cm}^{\mathrm{x}}} \text {. }
\end{gathered}
$$



TABLE 413.-THE EQUIVALENT CONDUCTIVITY OF SALTS, ACIDS, AND BASES IN AQUEOUS SOLUTIONS (concluded)

| Substance | Concen tration |  | $25^{\circ}$ | $50^{\circ}$ | $75^{\circ}$ | $100^{\circ}$ | $128^{\circ}$ | $156^{\circ}$ | $218^{\circ}$ | $281^{\circ}$ | $300^{\text {a }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $18^{\circ}$ |  |  |  |  |  |  |  |  |  |
| Potassium sulfate. | 0 | 132.8 |  | - | - | 455 | - | 715 | 1065 | 1460 | 1725 |
|  | 2 | 124.8 |  |  | - | 402 | - | 605 | 806 | 893 | 867 |
| " " | 10 | 115.7 |  |  | - | 365 | - | 537 | 672 | 687 | 637 |
| " " | 40 | 104.2 |  | - | - | 320 | - | 455 | 545 | 519 | 466 |
| " " .... | 80 | 97.2 | - | - | - | 294 | - | 415 | 482 | 448 | 396 |
| " " .... | 100 | 95.0 |  |  |  | 286 |  |  |  |  |  |
| Hydrochloric | 0 | 379.0 |  |  |  | 850 | - | 1085 | 1265 | 1380 | 1424 |
|  | 2 | 373.6 |  |  | - | 826 |  | 1048 | 1217 | 1332 | 1337 |
| " " | 10 | 368.1 |  | - | - | 807 | - | 1016 | 1168 | 1226 | 1162 |
| " " | 80 | 353.0 |  |  |  | 762 | - | 946 | 1044 | 1046 | 862 |
| Nitric acid. | 100 | 350.6 |  |  |  | 754 |  | 929 | 1006 |  |  |
|  | 0 | 377.0 | 421.0 | 570 | 706 | 826 | 945 | 1047 | (1230) | - | (1380 |
|  | 2 | 371.2 | 413.7 | 559 | 690 | 806 | 919 | 1012 | 1166 | - | 1156 |
| " | 10 | 365.0 | 406.0 | 548 | 676 | 786 | 893 | 978 |  |  |  |
| " | 50 | 353.7 | 393.3 | 528 | 649 | 750 | 845 | 917 |  |  |  |
| " " | 100 | 346.4 | 385.0 | 516 | 632 | 728 | 817 | 880 |  | - | 454* |
| Sulfuric acid | 0 | 383.0 | (429) | (591) | (746) | 891 | (1041) | 1176 | 1505 | - | (2030) |
|  | 2 | 353.9 | 390.8 | 501 | 561 | 571 | 551 | 536 | 563 | - | 637 |
| " | 10 | 309.0 | 337.0 | 406 | 435 | 446 | 460 | 481 | 533 |  |  |
| " " | 50 | 253.5 | 273.0 | 323 | 356 | 384 | 417 | 448 | 502 |  |  |
| " "....... . | 100 | 233.3 | 251.2 | 300 | 336 | 369 | 404 | 435 | 483 | - | 474 |
| Postassium hydrogensulfate .................... | 2 | 455.3 | 506.0 | 661.0 | 754 | 784 | 773 | 754 |  |  |  |
|  | 50 | 295.5 | 318.3 | 374.4 | 403 | 422 | 446 | 477 |  |  |  |
|  | 100 | 263.7 | 283.1 | 329.1 | 354 | 375 | 402 | 435 |  |  |  |
| Phosphoric acid...... | 0 | 338.3 | 376 | 510 | 631 | 730 | 839 | 930 |  |  |  |
|  | 2 | 283.1 | 311.9 | 401 | 464 | 498 | 508 | 489 |  |  |  |
| "، "، ${ }^{\text {"..... }}$ | 10 | 203.0 | 222.0 | 273 | 300 | 308 | 298 | 274 |  |  |  |
| "، " ${ }^{\text {a }}$..... | 50 | 122.7 | 132.6 | 157.8 | 168.6 | 168 | 158 | 142 |  |  |  |
| " ${ }^{\text {" }}$ | 100 | 96.5 | 104.0 | 122.7 | 129.9 | 128 | 120 | 108 |  |  |  |
| Acetic acid. | 0 | (347.0) | - | - | - | (773) | - | (980) | (1165) |  | (1268) |
|  | 10 | 14.50 8.50 | - | - | - | 25.1 | - | 22.2 | 14.7 |  |  |
| " ${ }^{\text {" }}$ | 30 | 8.50 |  |  | - | 14.7 |  | 13.0 | 8.65 |  |  |
| , | 80 | 5.22 | - |  |  | 9.05 |  | 8.00 | 5.34 |  |  |
| Sodium | 100 | 216.5 | - | - | - | 8.10 594 | - | 835 | 4.82 1060 | - | 1.57 |
|  | 2 | 212.1 |  |  | - | 582 |  | 814 |  |  |  |
| "" "، | 20 | 205.8 |  |  |  | 559 | - | 771 | 930 |  |  |
| " " | 50 | 200.6 |  |  |  | 540 |  | 738 | 873 |  |  |
| Barium hydroxide. | 0 | 222 | 256 | 389 | (520) | 645 | (760) | 847 |  |  |  |
|  | 2 | 215 |  | 359 | 4 | 591 |  |  |  |  |  |
| "، " .... | 10 | 207 | 235 | 342 | 449 | 548 | 664 | 722 |  |  |  |
| "، " $\quad$.... | 50 | 191.1 | 215.1 | 308 | 399 | 478 | 549 | 593 |  |  |  |
|  | 10 | $\begin{gathered} 180.1 \\ (238) \end{gathered}$ | $\begin{gathered} 204.2 \\ (271) \end{gathered}$ | $\begin{gathered} 291 \\ (404) \end{gathered}$ | $\begin{gathered} 373 \\ (526) \end{gathered}$ | $\begin{gathered} 443 \\ (647) \end{gathered}$ | $\begin{gathered} 503 \\ (764) \end{gathered}$ | $\begin{gathered} 531 \\ (908) \end{gathered}$ | (1141) |  | (1406) |
| Ammonium hydroxide | 10 | 9.66 |  |  | (526) | 23.2 | - | 22.3 | 15.6 |  |  |
|  | 30 | 5.66 |  | - | 6.70 | 13.6 | - | 13.0 |  |  |  |
|  | 100 | 3.10 | 3.62 | 5.35 | 6.70 | 7.47 | - | 7.17 | 4.82 | - | 1.33 |

[^179]
# TABLE 414.-THE EQUIVALENT CONDUCTIVITY OF SOME ADDITIONAL SALTS IN AQUEOUS SOLUTION 

| Substance | Concentration | E'quivalent conductance at the following ${ }^{\circ} \mathrm{C}$ temperature |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $0^{\circ}$ | $18^{\circ}$ | $25^{\circ}$ | $50^{\circ}$ | $75^{\circ}$ | $100^{\circ}$ | $128^{\circ}$ | $156^{\circ}$ |
| Potassium nitrate. | 0 | 80.8 | 126.3 | 145.1 | 219 | 299 | 384 | 485 | 580 |
| 俍. | 2 | 78.6 | 122.5 | 140.7 | 212.7 | 289.9 | 370.3 | 460.7 | 551 |
| " " | 12.5 | 75.3 | 117.2 | 134.9 | 202.9 | 276.4 | 351.5 | 435.4 | 520.4 |
| " " | 50 | 70.7 | 109.7 | 126.3 | 189.5 | 257.4 | 326.1 | 402.9 | 476.1 |
| " " | 100 | 67.2 | 104.5 | 120.3 | 180.2 | 244.1 | 308.5 | 379.5 | 447.3 |
| Potassium oxalate | 0 | 79.4 | 127.6 | 147.5 | 230 | 322 | 419 | 538 | 653 |
| Potassium oxala | 2 | 74.9 | 119.9 | 139.2 | 215.9 | 300.2 | 389.3 | 489.1 | 587 |
| " " | 12.5 | 69.3 | 111.1 | 129.2 | 199,1 | 275.1 | 354.1 | 438.8 | 524.3 |
| " " | 50 | 63 | 101 | 116.5 | 178.6 | 244.9 | 312.2 | 383.8 | 449.5 |
| " " | 100 | 59.3 | 94.6 | 109.5 | 167 | 227.5 | 288.9 | 353.2 | 409.7 |
| " " | 200 | 55.8 | 88.4 | 102.3 | 155 | 210.9 | 265.1 | 321.9 | 372.1 |
| Calcium nitrate | 0 | 70.4 | 112.7 | 130.6 | 202 | 282 | 369 | 474 | 575 |
| Calum " | 2 | 66.5 | 107.1 | 123.7 | 191.9 | 266.7 | 346.5 | 438.4 | 529.8 |
| " " | 12.5 | 61.6 | 98.6 | 114.5 | 176.2 | 244 | 314.6 | 394.5 | 473.7 |
| " " | 50 | 55.6 | 88.6 | 102.6 | 157.2 | 216.2 | 276.8 | 343 | 405.1 |
| " " | 100 | 51.9 | 82.6 | 95.8 | 146.1 | 199.9 | 255.5 | 315.1 | 369.1 |
| " " | 200 | 48.3 | 76.7 | 88.8 | 135.4 | 184.7 | 234.4 | 288 | 334.7 |
| Potassium ferrocyani | 0 | 98.4 | 159.6 | 185.5 | 288 | 403 | 527 |  |  |
| " " | $2^{.5}$ | 91.6 84.8 | 137 | 171.1 158.9 | 243.8 | 335.2 | 427.6 |  |  |
| " " | 12.5 | 71 | 113.4 | 131.6 | 200.3 | 271 | 340 |  |  |
| " " | 50 | 58.2 | 93.7 | 108.6 | 163.3 | 219.5 | 272.4 |  |  |
| " " | 100 | 53 | 84.9 | 98.4 | 148.1 | 198.1 | 245 |  |  |
| " " | 200 | 48.8 | 77.8 | 90.1 | 135.7 | 180.6 | 222.3 |  |  |
| " " | 400 | 45.4 | 72.1 | 83.3 | 124.8 | 165.7 | 203.1 |  |  |
| Barium ferrocyanide |  | 91 | 150 | 176 | 277 | 393 | 521 |  |  |
|  | 2 | 46.9 | 75 | 86.2 | 127.5 | 166.2 | 202.3 |  |  |
| " " | 12.5 | 30.4 | 48.8 | 56.5 | 83.1 | 107 | 129.8 |  |  |
| Calcium ferrocyanide |  | 88 | 146 | 171 | 271 | 386 | 512 |  |  |
| Calcium ferrocyanide | 2 | 47.1 | 75.5 | 86.2 | 130 |  |  |  |  |
| " " | 12.5 | 31.2 | 49.9 | 57.4 |  |  |  |  |  |
| " " | 50 | 24.1 | 38.5 | 44.4 | 64.6 | 81.9 |  |  |  |
| " " | 100 | 21.9 | 35.1 | 40.2 | 58.4 | 73.7 | 84.3 |  |  |
| " " | 200 | 20.6 | 32.9 | 37.8 | 55 | 68.7 | 77.5 |  |  |
| " " | 400 | 20.2 | 32.2 | 37.1 | 54 | 67.5 | 76.2 |  |  |
| Potassium citrate |  | 76.4 | 124.6 | 144.5 | 228 | 320 | 420 |  |  |
|  | 0.5 |  | 120.1 | 139.4 |  |  |  |  |  |
| " " | 2 | 71 | 115.4 | 134.5 | 210.1 | 293.8 | 381.2 |  |  |
| " " | 5 | 67.6 | 109.9 | 128.2 | 198.7 | 276.5 | 357.2 |  |  |
| " " | 12.5 | 62.9 | 101.8 | 118.7 | 183.6 | 254.2 | 326 |  |  |
| " " | 50 | 54.4 | 87.8 | 102.1 | 157.5 | 215.5 | 273 |  |  |
| " " | 100 | 50.2 | 80.8 | 93.9 | 143.7 | 196.5 | 247.5 |  |  |
| " " | 300 | 43.5 | 69.8 | 81 | 123.5 | 167 | 209.5 |  |  |
| Lanthanum nitrate | 0 | 75.4 | 122.7 | 142.6 | 223 | 313 | 413 | 534 | 651 |
|  | 2 | 68.9 | 110.8 | 128.9 | 200.5 | 279.8 | 363.5 | 457.5 | 549 |
| " " | 12.5 | 61.4 | 98.5 | 114.4 | 176.7 | 243.4 | 311.2 | 383.4 | 447.8 |
| " " | 50 | 54 | 86.1 | 99.7 | 152.5 | 207.6 | 261.4 | 315.8 | 357.7 |
| " " | 100 | 49.9 | 79.4 | 91.8 | 139.5 | 189.1 | 236.7 | 282.5 | 316.3 |
| " " | 200 | 46 | 72.1 | 83.5 | 126.4 | 170.2 | 210.8 | 249.6 | 276.2 |

Every gram-atom involved in an electrolytic change requires the same number of coulombs, or ampere-hours of electricity, per unit change of valency. This constant is 96487.7 coulomb/g-atom, or 26.801 ampere-hours per g -atom hour, corresponding to an electrochemical equivalent of silver of $0.0011810 \mathrm{~g} \mathrm{sec}^{-1} \mathrm{amp}^{-1}$. It is to be noted that the change of valence of the element from its state before to that after the electrolytic action should be considered. The valence of a free, uncombined element is to be considered as 0 . The same current will electrolyze "chemically equivalent" quantities per unit time. The valence is then included in the "chemically equivalent" quantity.

| Element | Change of valency | Mg per coulomb | Coulombs per mg | $\begin{gathered} \text { G per } \\ \text { amp hour } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| Al | 3 | . 09317 | 10.733 | . 3354 |
| Cl |  | . 36749 | 2.7212 | 1.3230 |
|  | 3 | . 12250 | 8.1633 | . 4410 |
| " | . 5 | . 07350 | 13.605 | . 2646 |
| " | . 7 | . 05250 | 19.048 | . 1890 |
| Cu | . 1 | . 6585 | 1.5186 | 2.3706 |
|  | 2 | . 3293 | 3.0367 | 1.1855 |
| Au | . 1 | 2.044 | . 4892 | 7.358 |
|  | . 3 | . 6813 | 1.468 | 2.453 |
| H | . 1 | . 0104472 | 95.719 | . 0376099 |
| Pb | 1 | 2.1476 | . 46564 | 7.7314 |
| " |  | 1.07379 | . 93128 | 3.8656 |
| " | . 4 | . 53690 | 1.8625 | 1.9328 |
| Hg | . 1 | 2.0792 | . 48095 | 7.4851 |
|  | . 2 | 1.0396 | . 961908 | 3.7426 |
| Ni | . 1 | . 60828 | 1.6440 | 2.1898 |
|  | . 2 | . 3041 | 3.2884 | 1.0948 |
| " | . 3 | . 20276 | 4.9319 | . 7299 |
| O | . 2 | . 082914 | 12.0607 | . 298490 |
|  | 4 | . 041457 | 24.1214 | . 14945 |
| Pt | 2 | 1.01171 | . 98843 | 3.6422 |
| " | 4 | . 50585 | 1.97687 | 1.82107 |
| " |  | . 33724 | 2.9652 | 1.2140 |
| K | ... 1 | . 4052 | 2.4679 | 1.4587 |
| Ag | . 1 | 1.11810 | . 894374 | 4.02516 |
| Na | . 1 | . 23835 | 4.1955 | . 85806 |
| Sn | . 2 | . 61512 | 1.6257 | 2.2144 |
| " | . 4 | . 30756 | 3.2514 | 1.1072 |
| Zn | . 2 | . 33881 | 2.9515 | 1.21972 |

The electrochemical equivalent for silver is $0.00111810 \mathrm{~g} \mathrm{sec}^{-1} \mathrm{amp}^{-1}$. For other elements the electrochemical equivalent $=$ (atomic weight divided by change of valency) and this divided by 96487.7 coulomb/g-atom.

## TABLE 416.-INTRODUCTION TO WIRE TABLES; MASS AND VOLUME RESISTIVITY OF COPPER AND ALUMINUM

The following wire tables are abridged from those prepared by the Bureau of Standards at the request and with the cooperation of the Standards Committee of the American Institute of Electrical Engineers. The standard of copper resistance used is "The International Annealed Copper Standard" as adopted Scptember 5, 1913, by the International Electrotechnical Commission and represents the average commercial high-conductivity copper for the purpose of electric conductors. This standard corresponds to a conductivity of $58 \times 10^{-5} \mathrm{emu}$, and a density of 8.89 , at $20^{\circ} \mathrm{C}$. In the various units of mass resistivity and volume resistivity this may be stated as

> 0.15328 ohm $(\mathrm{m}, \mathrm{g})$ at $20^{\circ} \mathrm{C}$
> 875.20 ohms $(\mathrm{mil}, \mathrm{bt})$ at $20^{\circ} \mathrm{C}$
> 1.7241 microhm- cm at $20^{\circ} \mathrm{C}$
> 0.6779 microhm-in. at $20^{\circ} \mathrm{C}$
> 10.371 ohms (mil, ft) at $20^{\circ} \mathrm{C}$

The temperature coefficient for this particular resistivity is $\alpha_{29}=0.00393$, or $\alpha_{0}=0.00427$. The temperature coefficient of copper is proportional to the conductivity, so that where the conductivity is known the temperature coefficient may be calculated, and vice versa. Thus the next table shows the temperature coefficients of copper having various percentages of the standard conductivity. A consequence of this relation is that the change of resistivity per degree is constant, independent of the sample of copper and independent of the temperature of reference. This resistivity-temperature constant, for volume resistivity and Centigrade degrees, is 0.00681 microhm-cm, and for mass resistivity is 0.000597 ohm ( $\mathrm{m}, \mathrm{g}$ ).
The density of 8.89 g per $\mathrm{cm}^{3}$ at $20^{\circ} \mathrm{C}$, is equivalent to 0.32117 lb per in. ${ }^{3}$
The values in the following tables are for annealed copper of standard resistivity. The user of the tables must apply the proper correction for copper of other resistivity. Harddrawn copper may be taken as about 2.7 percent higher resistivity than annealed copper.

The following is a fair average of the chemical content of commercial high conductivity copper :

| Copper | 99.91\% | Sulfur | .002\% |
| :---: | :---: | :---: | :---: |
| Silver | . 03 | Iron | . 002 |
| Oxygen | . 052 | Nickel | trace |
| Arsenic | . 002 | Lead |  |
| Antimony | . 002 | Zinc |  |

The following values are consistent with the data above:

| R | $62.969 \times$ |
| :---: | :---: |
| Resistivity at $0^{\circ} \mathrm{C}$, in microhm-cm | 1.5881 |
| Density at $0^{\circ} \mathrm{C}$ | 8.90 |
| Coefficient of linear expansion per de | . 000017 |
| "Constant mass" temperature coefficient of resistance at $0^{\circ} \mathrm{C}$ | . 00427 |

The aluminum tables are based on a figure for the conductivity published by the National Bureau of Standards, which is the result of many thousands of determinations by the Aluminum Co. of America. A volume resistivity of 2.828 microhm- cm and a density of 2.70 may be considered to be good average values for commercial hard-drawn aluminum. These values give:

$$
\begin{aligned}
& \text { Conductivity at } 0^{\circ} \mathrm{C} \text { in emu.......................... } 38.36 \times 10^{-5} \\
& \text { Mass resistivity, in ohms ( } \mathrm{m}, \mathrm{~g} \text { ) at } 20^{\circ} \mathrm{C} \ldots \ldots . . . \\
& \text { Mass percent conductivity relative to copper......... } 200.7 \%
\end{aligned}
$$

The average chemical content of commercial aluminum wire is

| Aluminum | 99.57\% |
| :---: | :---: |
| Silicon |  |
| Iron | 14 |


| $\begin{aligned} & \text { Gage } \\ & \text { No. } \end{aligned}$ | American wire gage mils* | American (B. \& S.) mm * | Steel wire gage $\dagger$ til mils | $\underset{\text { Steel wire }}{\text { gage } \dagger}$ mm | Stubs' steel wire gage $\xrightarrow{\text { gage }}$ mils | (British) standard wire gage mils | Birminggage, (Stubs mils | Gage No. No |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7-0 |  |  | 490.0 | 12.4 |  | 500. |  | 7-0 |
| 6-0 |  |  | 461.5 | 11.7 |  | 464. |  | 6-0 |
| 5-0 |  |  | 430.5 | 10.9 |  | 432. |  | 5-0 |
| 4-0 | 460. | 11.7 | 393.8 | 10.0 |  | 400. | 454. | 40 |
| 3-0 | 410. | 10.4 | 362.5 | 9.2 |  | 372. | 425. | 3-0 |
| 2-0 | 365. | 9.3 | 331.0 | 8.4 |  | 348. | 380. | 2-0 |
| 0 | 325. | 8.3 | 306.5 | 7.8 |  | 324. | 340. | 0 |
|  | 289. | 7.3 | 283.0 | 7.2 | 227. | 300. | 300. | 1 |
| 2 | 258. | 6.5 | 262.5 | 6.7 | 219. | 276. | 284. | 2 |
| 3 | 229. | 5.8 | 243.7 | 6.2 | 212. | 252. | 259. | 3 |
| 4 | 204. | 5.2 | 225.3 | 5.7 | 207. | 232. | 238. | 4 |
| 5 | 182. | 4.6 | 207.0 | 5.3 | 204. | 212. | 220. | 5 |
| 6 | 162. | 4.1 | 192.0 | 4.9 | 201. | 192. | 203. | 6 |
| 7 | 144. | 3.7 | 177.0 | 4.5 | 199. | 176. | 180. | 7 |
| 8 | 128. | 3.3 | 162.0 | 4.1 | 197. | 160. | 165. | 8 |
| 9 | 114. | 2.91 | 148.3 | 3.77 | 194. | 144. | 148. | , |
| 10 | 102. | 2.59 | 135.0 | 3.43 | 191. | 128. | 134. | 10 |
| 11 | 91. | 2.30 | 120.5 | 3.06 | 188. | 116. | 120. | 11 |
| 12 | 81. | 2.05 | 105.5 | 268 | 185. | 104. | 109. | 12 |
| 13 | 72. | 1.83 | 91.5 | 2.32 | 182. | 92. | 95. | 13 |
| 14 | 64. | 1.63 | 80.0 | 2.03 | 180. | 80. | 83. | 14 |
| 15 | 57. | 1.45 | 72.0 | 1.83 | 178. | 72. | 72. | 15 |
| 16 | 51. | 1.29 | 62.5 | 1.59 | 175. | 64. | 65. | 16 |
| 17 | 45. | 1.15 | 54.0 | 1.37 | 172. | 56. | 58. | 17 |
| 18 | 40. | 1.02 | 47.5 | 1.21 | 168. | 48. | 49. | 18 |
| 19 | 36. | . 91 | 41.0 | 1.04 | 164. | 40. | 42. | 19 |
| 20 | 32. | . 81 | 34.8 | . 88 | 161. | 36. | 35. | 20 |
| 21 | 28.5 | . 72 | 31.7 | . 81 | 157. | 32. | 32. | 21 |
| 22 | 25.3 | . 62 | 28.6 | . 73 | 155. | 28. | 28. | 22 |
| 23 | 22.6 | . 57 | 25.8 | . 66 | 153. | 24. | 25. | 23 |
| 24 | 20.1 | . 51 | 23.0 | . 58 | 151. | 22. | 22. | 24 |
| 25 | 17.9 | . 45 | 20.4 | . 52 | 148. | 20. | 20. | 25 |
| 26 | 15.9 | . 40 | 18.1 | . 46 | 146. | 18. | 18. | 26 |
| 27 | 14.2 | . 36 | 17.3 | . 439 | 143. | 16.4 | 16. | 27 |
| 28 | 12.6 | . 32 | 16.2 | . 411 | 139. | 14.8 | 14. | 28 |
| 29 | 11.3 | . 29 | 15.0 | . 381 | 134. | 13.6 | 13. | 29 |
| 30 | 10.0 | . 25 | 14.0 | . 356 | 127. | 12.4 | 12. | 30 |
| 31 | 8.9 | . 227 | 13.2 | . 335 | 120. | 11.6 | 10. | 31 |
| 32 | 8.0 | . 202 | 12.8 | . 325 | 115. | 10.8 | 9. | 32 |
| 33 | 7.1 | . 180 | 11.8 | . 300 | 112. | 10.0 | 8. | 33 |
| 34 | 6.3 | . 160 | 10.4 | . 264 | 110. | 9.2 | 7. | 34 |
| 35 | 5.6 | . 143 | 9.5 | . 241 | 108. | 8.4 | 5. | 35 |
| 36 | 5.0 | . 127 | 9.0 | . 229 | 106. | 7.6 | 4. | 36 |
| 37 | 4.5 | . 113 | 8.5 | . 216 | 103. | 6.8 |  | 37 |
| 38 | 4.0 | . 101 | 8.0 | . 203 | 101. | 6.0 |  | 38 |

[^180](continued)

TABLE 417.-TABULAR COMPARISON OF WIRE GAGES (concluded)

| Gage | American wire gage (B. \& S.) mils * | American wire gage (B. \& S.) mm * | Steel wire gage † mils | Steel wire gage $\dagger$ mm | Stubs' steel wire gage mils | (British) standard wire gage mils | Birming. ham wire gage (Stubs') mils | Gage No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 39 | 3.5 | . 090 | 7.5 | . 191 | 99. | 5.2 |  | 39 |
| 40 | 3.1 | . 080 | 7.0 | . 178 | 97. | 4.8 |  | 40 |
| 41 |  |  | 6.6 | . 168 | 95. | 4.4 |  | 41 |
| 42 |  |  | 6.2 | . 157 | 92. | 4.0 |  | 42 |
| 43 |  |  | 6.0 | . 152 | 88. | 3.6 |  | 43 |
| 44 |  |  | 5.8 | . 147 | 85. | 3.2 |  | 44 |
| 45 |  |  | 5.5 | . 140 | 81. | 2.8 |  | 45 |
| 46 |  |  | 5.2 | . 132 | 79. | 2.4 |  | 46 |
| 47 |  |  | 5.0 | . 127 | 77. | 2.0 |  | 47 |
| 48 |  |  | 4.8 | . 122 | 75. | 1.6 |  | 48 |
| 49 |  |  | 4.6 | . 117 | 72. | 1.2 |  | 49 |
| 50 |  |  | 4.4 | . 112 | 69. | 1.0 |  | 50 |

## TABLE 418.-TEMPERATURE COEFFICIENTS OF COPPER FOR DIFFERENT INITIAL TEMPERATURES (CENTIGRADE) AND DIFFERENT CONDUCTIVITIES

| $\begin{aligned} & \text { Ohms } \\ & \text { (m, }{ }^{(\mathrm{m})} \text { ) } \mathrm{at} 20^{\circ} \mathrm{C} \end{aligned}$ | Percent conductivity | $a_{0}$ | $a_{15}$ | $a_{20}$ | $a_{25}$ | $a_{30}$ | $a_{50}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 16134 | 95\% | . 00403 | . 00380 | . 00373 | . 00367 | . 00360 | . 00336 |
| . 15966 | 96\% | . 00408 | . 00385 | . 00377 | . 00370 | . 00364 | . 00339 |
| . 15802 | 97\% | . 00413 | . 00389 | . 00381 | . 00374 | . 00367 | . 00342 |
| . 15753 | 97.3\% | . 00414 | . 00390 | . 00382 | . 00375 | . 00368 | . 00343 |
| . 15640 | 98\% | . 00417 | . 00393 | . 00385 | . 00378 | . 00371 | . 00345 |
| . 15482 | 99\% | . 00422 | . 00397 | . 00389 | . 00382 | . 00374 | . 00348 |
| . 15328 | 100\% | . 04427 | . 00401 | . 00393 | . 00385 | . 00378 | . 00352 |
| . 15176 | 101\% | . 00431 | . 00405 | . 00397 | . 00389 | . 00382 | . 00355 |

Note.-The fundamental relation between resistance and temperature is the following:

$$
R_{t}=R_{t_{1}}\left(1+a_{t_{1}}\left[t-t_{1}\right]\right),
$$

where $a_{t_{1}}$ is the "temperature coefficient," and $t_{1}$ is the "initial temperature" or "temperature of reference."

The values of $a$ in the above table exhibit the fact that the temperature coefficient of copper is proportional to the conductivity. The table was calculated by means of the following formula, which holds for any percent conductivity, $n$, within commercial ranges, and for centigrade temperatures. ( $n$ is considered to be expressed decimally: e.g., if percent conductivity $=99$ percent, $n=0.99$.)

$$
\alpha_{t_{1}}=\frac{1}{\frac{1}{n(0.00393)}+\left(t_{1}-20\right)} .
$$

TABLE 419.-REDUCTION OF OBSERVATIONS TO STANDARD TEMPERATURE (Copper)

| Temper${ }^{\circ} \mathrm{Cture}$ |  |  |  |  | Factors to reduce resistance to $20^{\circ} \mathrm{C}$ |  |  | Temper ${ }^{\text {ature, }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Corrections to reduce resistivity to $20^{\circ} \mathrm{C}$ |  |  |  | For 96 | For 98 | For 100 |  |
|  | Ohm (m, g) | $\underset{\substack{\text { Microhm- }}}{ }$ | $\underset{(\mathrm{mi}, \mathrm{lb})}{\mathrm{Ohm}}$ | $\begin{gathered} \text { Microhm- } \\ \text { in. } \end{gathered}$ | conductivity | conductivity | conductivity |  |
| 0 | +. 01194 | +. 1361 | + 68.20 | $+.05358$ | 1.0816 | 1.0834 | 1.0853 | 0 |
| 5 | +. 00896 | +. 1021 | + 51.15 | +. 04018 | 1.0600 | 1.0613 | 1.0626 | 5 |
| 10 | +. 00597 | +. 0681 | + 34.10 | +. 02679 | 1.0392 | 1.0401 | 1.0409 | 10 |
| 11 | $+.00537$ | +. 0612 | + 30.69 | +. 02411 | 1.0352 | 1.0359 | 1.0367 | 11 |
| 12 | +. 00478 | +. 0544 | + 27.28 | +. 02143 | 1.0311 | 1.0318 | 1.0325 | 12 |
| 13 | +. 00418 | $+.0476$ | + 23.87 | +. 01875 | 1.0271 | 1.0277 | 1.0283 | 13 |
| 14 | +. 00358 | $+.0408$ | + 20.46 | $+.01607$ | 1.0232 | 1.0237 | 1.0242 | 14 |
| 15 | +. 00299 | +. 0340 | + 17.05 | +. 01340 | 1.0192 | 1.0196 | 1.0200 | 15 |
| 16 | +. 00239 | +. 0272 | +13.64 | +. 01072 | 1.0153 | 1.0156 | 1.0160 | 16 |
| 17 | +. 00179 | +. 0204 | $+10.23$ | +. 00804 | 1.0114 | 1.0117 | 1.0119 | 17 |
| 18 | +. 00119 | +. 0136 | + 6.82 | +. 00536 | 1.0076 | 1.0078 | 1.0079 | 18 |
| 19 | +. 00060 | +. 0068 | + 3.41 | +. 00268 | 1.0038 | 1.0039 | 1.0039 | 19 |
| 20 | 0 | , |  | 0 | 1.0000 | 1.0000 | 1.0000 | 20 |
| 21 | -. 00060 | $-.0068$ | - 3.41 | -. 00268 | . 9962 | . 9962 | . 9961 | 21 |
| 22 | -. 00119 | -. 0136 | 6.82 | -. 00536 | . 9925 | . 9924 | . 9922 | 22 |
| 23 | -. 00179 | -. 0204 | - 10.23 | -. 00804 | . 8888 | . 9886 | . 9883 | 23 |
| 24 | -. 00239 | -. 0272 | $-13.64$ | $-.01072$ | . 9851 | . 9848 | . 9845 | 24 |
| 25 | -. 00299 | -. 0340 | - 17.05 | -. 01340 | . 9815 | . 9811 | . 9807 | 25 |
| 26 | -. 00358 | -. 0408 | - 20.46 | -. 01607 | . 9779 | . 9774 | . 9770 |  |
| 27 | -. 00418 | -. 0476 | - 23.87 | -. 01875 | . 9743 | . 9737 | . 9732 | 27 |
| 28 | -. 00478 | -. 0544 | - 27.28 | -. 02143 | ,9707 | . 9701 | . 9695 | 28 |
| 29 | -. 00537 | -. 0612 | - 30.69 | -. 02411 |  |  | . 9658 | 29 |
| 30 | -. 00597 | -. 0681 | - 34.10 | -. 02679 | . 9636 | . 9629 | . 9622 | 30 |
| 35 | -. 00896 | -. 1021 | - 51.15 | -. 04018 | . 9464 | . 9454 | . 9443 | 35 |
| 40 | -. 01194 | -. 1361 | - 68.20 | -. 05358 | . 9298 | . 9285 | . 9271 | 40 |
| 45 | -. 01493 | -. 1701 | -85.25 | -. 06698 | . 9138 | . 9122 | . 9105 | 45 |
| 50 | -. 01792 | -. 2042 | -102.30 | -. 08037 | . 8983 | . 8964 | . 8945 | 50 |
| 55 | -. 02090 | -. 2382 | -119.35 | $-.09376$ | . 8833 | . 8812 | . 8791 | 55 |
| 60 | -. 02389 | -. 2722 | -136.40 | -. 10716 | . 8689 | . 8665 | . 8642 | 60 |
| 65 | -. 02687 | -. 3062 | -153.45 | -. 12056 | . 8549 | . 8523 | . 8497 | 65 |
| 70 | -. 02986 | -. 3403 | -170.50 | -. 13395 | . 8413 | . 8385 | . 8358 | 70 |
| 75 | $-.03285$ | $-.3743$ | $-187.55$ | -. 14734 | 8281 | . 8252 | . 8223 | 75 |

## TABLE 420.-WIRE TABLE, STANDARD ANNEALED COPPER American wire gage (B. \& S.)

|  |  |  |  |  | Ohrns | er 1000 ft |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Diameter | Cross section | $20^{\circ} \mathrm{C}$ |  |  | $50^{\circ} \mathrm{C}$ |  |
| No. | at $20^{\circ} \mathrm{C}$ | Circular mils | in. ${ }^{2}$ | ( $=32^{\circ} \mathrm{F}$ ) | $=68^{\circ} \mathrm{F}$ ) | $\left(=122^{\circ} \mathrm{F}\right)$ | $\left(=167^{\circ} \mathrm{F}\right.$ ) |
| 0000 | 460.0 | 211600. | . 1662 | . 04516 | . 04901 | . 05479 | . 05961 |
| 000 | 409.6 | 167800. | . 1318 | . 05695 | . 06180 | . 06909 | . 07516 |
| 00 | 364.8 | 133100. | . 1045 | . 07181 | . 07793 | . 08712 | . 09478 |
| 0 | 324.9 | 105500. | . 08289 | . 09055 | . 09827 | . 1099 | . 1195 |
| 1 | 289.3 | 83690. | . 06573 | . 1142 | . 1239 | . 1385 | . 1507 |
| 2 | 257.6 | 66370. | . 05213 | . 1440 | . 1563 | . 1747 | . 1900 |
| 3 | 229.4 | 52640. | . 04134 | . 1816 | . 1970 | . 2203 | . 2396 |
| 4 | 204.3 | 41740. | . 03278 | . 2289 | . 2485 | . 2778 | . 3022 |
| 5 | 181.9 | 33100. | . 02600 | . 2887 | . 3133 | . 3502 | . 3810 |
| 6 | 162.0 | 26250. | . 02062 | . 3640 | . 3951 | . 4416 | . 4805 |
| 7 | 144.3 | 20820. | . 01635 | . 4590 | . 4982 | . 5569 | . 6059 |
| 8 | 128.5 | 16510. | . 01297 | . 5788 | . 6282 | . 7023 | . 7640 |
| 9 | 114.4 | 13090. | . 01028 | . 7299 | . 7921 | . 8855 | . 9633 |
| 10 | 101.9 | 10380. | . 008155 | . 9203 | . 9989 | 1.117 | 1.215 |
| 11 | 90.74 | 8234. | . 006467 | 1.161 | 1.260 | 1.408 | 1.532 |
| 12 | 80.81 | 6530. | . 005129 | 1.463 | 1.588 | 1.775 | 1.931 |
| 13 | 71.96 | 5178. | . 004067 | 1.845 | 2.003 | 2.239 | 2.436 |
| 14 | 64.08 | 4107. | . 003225 | 2.327 | 2.525 | 2.823 | 3.071 |
| 15 | 57.07 | 3257. | . 002558 | 2.934 | 3.184 | 3.560 | 3.873 |
| 16 | 50.82 | 2583. | . 002028 | 3.700 | 4.016 | 4.489 | 4.884 |
| 17 | 45.26 | 2048. | . 001609 | 4.666 | 5.064 | 5.660 | 6.158 |
| 18 | 40.30 | 1624. | . 001276 | 5.883 | 6.385 | 7.138 | 7.765 |
| 19 | 35.89 | 1288. | . 001012 | 7.418 | 8.051 | 9.001 | 9.702 |
| 20 | 31.96 | 1022. | . 0008023 | 9.355 | 10.15 | 11.35 | 12.35 |
| 21 | 28.45 | 810.1 | . 0006363 | 11.80 | 12.80 | 14.31 | 15.57 |
| 22 | 25.35 | 642.4 | . 0005046 | 14.87 | 16.14 | 18.05 | 19.63 |
| 23 | 22.57 | 509.5 | . 0004002 | 18.76 | 20.36 | 22.76 | 24.76 |
| 24 | 20.10 | 404.0 | . 0003173 | 23.65 | 25.67 | 28.70 | 31.22 |
| 25 | 17.90 | 320.4 | . 0002517 | 29.82 | 32.37 | 36.18 | 39.36 |
| 26 | 15.94 | 254.1 | . 0001996 | 37.61 | 40.81 | 45.63 | 49.64 |
| 27 | 14.20 | 201.5 | . 0001583 | 47.42 | 51.47 | 57.53 | 62.59 |
| 28 | 12.64 | 159.8 | . 0001255 | 59.80 | 64.90 | 72.55 | 78.93 |
| 29 | 11.26 | 126.7 | . 00009953 | 75.40 | 81.83 | 91.48 | 99.52 |
| 30 | 10.03 | 100.5 | . 00007894 | 95.08 | 103.2 | 115.4 | 125.5 |
| 31 | 8.928 | 79.70 | . 00006260 | 119.9 | 130.1 | 145.5 | 158.2 |
| 32 | 7.950 | 63.21 | . 00004964 | 151.2 | 164.1 | 183.4 | 199.5 |
| 33 | 7.080 | 50.13 | . 00003937 | 190.6 | 206.9 | 231.3 | 251.6 |
| 34 | 6.305 | 39.75 | . 00003122 | 240.4 | 260.9 | 291.7 | 317.3 |
| 35 | 5.615 | 31.52 | . 00002476 | 303.1 | 329.0 | 367.8 | 400.1 |
| 36 | 5.000 | 25.00 | . 00001964 | 382.2 | 414.8 | 463.7 | 504.5 |
| 37 | 4.453 | 19.83 | . 00001557 | 482.0 | 523.1 | 584.8 | 636.2 |
| 38 | 3.965 | 15.72 | . 00001235 | 607.8 | 659.6 | 737.4 | 802.2 |
| 39 | 3.531 | 12.47 | . 000009793 | 766.4 | 831.8 | 929.8 | 1012. |
| 40 | 3.145 | 9.888 | . 000007766 | 966.5 | 1049. | 1173. | 1276. |

(continued)

TABLE 420.-WIRE TABLE, STANDARD ANNEALED COPPER (continued) American wire gage (B. \& S.)

|  | Diameter in mils. at $20^{\circ} \mathrm{C}$ | lb/(1000 ft) | ft/lb | $\underbrace{\text { ft/ohm }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Gage No. |  |  |  | ${ }_{\left(=32^{\circ} \mathrm{C} \mathrm{~F}\right)}^{(=3}$ | $\left(\begin{array}{c} 20^{\circ} \mathrm{C} \\ \left.=68^{\circ} \mathrm{F}\right) \end{array}\right.$ | $\begin{gathered} 50^{\circ} \mathrm{C} \\ \left(=122^{\circ} \mathrm{F}\right) \end{gathered}$ | $\underset{\left(=167^{\circ} \mathrm{F}\right)}{\substack{7 \\\left({ }^{\circ}\right)}}$ |
| 0000 | 460.0 | 640.5 | 1.561 | 22140. | 20400. | 18250. | 16780. |
| 000 | 409.6 | 507.9 | 1.968 | 17560. | 16180. | 14470. | 13300. |
| 00 | 364.8 | 402.8 | 2.482 | 13930. | 12830. | 11480. | 10550. |
| 0 | 324.9 | 319.5 | 3.130 | 11040. | 10180. | 9103. | 8367. |
| 1 | 289.3 | 253.3 | 3.947 | 8758. | 8070. | 7219. | 6636. |
| 2 | 257.6 | 200.9 | 4.977 | 6946. | 6400. | 5725. | 5262. |
| 3 | 229.4 | 159.3 | 6.276 | 5508. | 5075. | 4540. | 4173. |
| 4 | 204.3 | 126.4 | 7.914 | 4368. | 4025. | 3600. | 3309. |
| 5 | 181.9 | 100.2 | 9.980 | 3464. | 3192. | 2855. | 2625. |
| 6 | 162.0 | 79.46 | 12.58 | 2747. | 2531. | 2264. | 2081. |
| 7 | 144.3 | 63.02 | 15.87 | 2179. | 2007. | 1796. | 1651. |
| 8 | 128.5 | 49.98 | 20.01 | 1728. | 1592. | 1424. | 1309. |
| 9 | 114.4 | 39.63 | 25.23 | 1370. | 1262. | 1129. | 1038. |
| 10 | 101.9 | 31.43 | 31.82 | 1087. | 1001. | 895.6 | 823.2 |
| 11 | 90.74 | 24.92 | 40.12 | 861.7 | 794.0 | 710.2 | 652.8 |
| 12 | 80.81 | 19.77 | 50.59 | 683.3 | 629.6 | 563.2 | 517.7 |
| 13 | 71.96 | 15.68 | 63.80 | 541.9 | 499.3 | 446.7 | 410.6 |
| 14 | 64.08 | 12.43 | 80.44 | 429.8 | 396.0 | 354.2 | 325.6 |
| 15 | 57.07 | 9.858 | 101.4 | 340.8 | 314.0 | 280.9 | 258.2 |
| 16 | 50.82 | 7.818 | 127.9 | 270.3 | 249.0 | 222.8 | 204.8 |
| 17 | 45.26 | 6.200 | 161.3 | 214.3 | 197.5 | 176.7 | 162.4 |
| 18 | 40.30 | 4.917 | 203.4 | 170.0 | 156.6 | 140.1 | 128.8 |
| 19 | 35.89 | 3.899 | 256.5 | 134.8 | 124.2 | 111.1 | 102.1 |
| 20 | 31.96 | 3.092 | 323.4 | 106.9 | 98.50 | 88.11 | 80.99 |
| 21 | 28.46 | 2.452 | 407.8 | 84.78 | 78.11 | 69.87 | 64.23 |
| 22 | 25.35 | 1.945 | 514.2 | 67.23 | 61.95 | 55.41 | 50.94 |
| 23 | 22.57 | 1.542 | 648.4 | 53.32 | 49.13 | 43.94 | 40.39 |
| 24 | 20.10 | 1.223 | 817.7 | 42.28 | 38.96 | 34.85 | 32.03 |
| 25 | 17.90 | . 9699 | 1031. | 33.53 | 30.90 | 27.64 | 25.40 |
| 26 | 15.94 | . 7692 | 1300. | 26.59 | 24.50 | 21.92 | 20.15 |
| 27 | 14.20 | . 6100 | 1639. | 21.09 | 19.43 | 17.38 | 15.98 |
| 28 | 12.64 | . 4837 | 2067. | 16.72 | 15.41 | 13.78 | 12.67 |
| 29 | 11.26 | . 3836 | 2607. | 13.26 | 12.22 | 10.93 | 10.05 |
| 30 | 10.03 | . 3042 | 3287. | 10.52 | 9.691 | 8.669 | 7.968 |
| 31 | 8.928 | . 2413 | 4145. | 8.341 | 7.685 | 6.875 | 6.319 |
| 32 | 7.950 | . 1913 | 5227. | 6.614 | 6.095 | 5.452 | 5.011 |
| 33 | 7.080 | . 1517 | 6591. | 5.245 | 4.833 | 4.323 | 3.974 |
| 34 | 6.305 | . 1203 | 8310 | 4.160 | 3.833 | 3.429 | 3.152 |
| 35 | 5.615 | . 09542 | 10480. | 3.299 | 3.040 | 2.719 | 2.499 |
| 36 | 5.000 | . 07568 | 13210. | 2.616 | 2.411 | 2.156 | 1.982 |
| 37 | 4.453 | . 06001 | 16660. | 2.075 | 1.912 | 1.710 | 1.572 |
| 38 | 3.965 | . 04759 | 21010. | 1.645 | 1.516 | 1.356 | 1.247 |
| 39 | 3.531 | . 03774 | 26500. | 1.305 | 1.202 | 1.075 | . 9886 |
| 40 | 3.145 | . 02993 | 33410. | 1.035 | . 9534 | . 8529 | . 7840 |

(continued)

TABLE 420.-WIRE TABLE, STANDARD ANNEALED COPPER (concluded)

|  |  | ohm/lb |  |  | lb/ohm |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Gage No. | Diameter in mils. at $20^{\circ} \mathrm{C}$ | $\left(=32^{\circ} \mathrm{C}\right. \text { F }$ | $(\overbrace{\left(=60^{\circ} \mathrm{F}\right)}^{2}$ | $\begin{gathered} 50^{\circ} \mathrm{C} \\ \left(=122^{\circ} \mathrm{F}\right) \end{gathered}$ | ${ }_{\left(=68^{\circ} \mathrm{F}\right)}^{20^{\circ} \mathrm{C}}$ |
| 0000 | 460.0 | . 00007051 | . 00007652 | . 00008554 | 13070. |
| 000 | 409.6 | . 0001121 | . 0001217 | . 0001360 | 8219. |
| 00 | 364.8 | . 0001783 | . 0001935 | . 0002163 | 5169. |
| 0 | 324.9 | . 0002835 | . 0003076 | . 0003439 | 3251. |
| 1 | 289.3 | . 0004507 | . 0004891 | . 0005468 | 2044. |
| 2 | 257.6 | . 0007166 | . 0007778 | . 0008695 | 1286. |
| 3 | 229.4 | . 001140 | . 001237 | . 001383 | 808.6 |
| 4 | 204.3 | . 001812 | . 001966 | . 002198 | 508.5 |
| 5 | 181.9 | . 002881 | . 003127 | . 003495 | 319.8 |
| 6 | 162.0 | . 004581 | . 004972 | . 005558 | 201.1 |
| 7 | 144.3 | . 007284 | . 007905 | . 008838 | 126.5 |
| 8 | 128.5 | . 01158 | . 01257 | . 01405 | 79.55 |
| 9 | 114.4 | . 01842 | . 01999 | . 02234 | 50.03 |
| 10 | 101.9 | . 02928 | . 03178 | . 03553 | 31.47 |
| 11 | 90.74 | . 04656 | . 05053 | . 05649 | 19.79 |
| 12 | 80.81 | . 07404 | . 08035 | . 08983 | 12.45 |
| 13 | 71.96 | . 1177 | . 1278 | . 1428 | 7.827 |
| 14 | 64.08 | . 1872 | . 2032 | .2271 | 4.922 |
| 15 | 57.07 | . 2976 | . 3230 | . 3611 | 3.096 |
| 16 | 50.82 | . 4733 | . 5136 | . 5742 | 1.947 |
| 17 | 45.26 | 7525 | . 8167 | . 9130 | 1.224 |
| 18 | 40.30 | 1.197 | 1.299 | 1.452 | . 7700 |
| 19 | 35.89 | 1.903 | 2.065 | 2.308 | . 4843 |
| 20 | 31.96 | 3.025 | 3.283 | 3.670 | . 3046 |
| 21 | 28.46 | 4.810 | 5.221 | 5.836 | . 1915 |
| 22 | 25.35 | 7.649 | 8.301 | 9.280 | . 1205 |
| 23 | 22.57 | 12.16 | 13.20 | 14.76 | . 07576 |
| 24 | 20.10 | 19.34 | 20.99 | 23.46 | . 04765 |
| 25 | 17.90 | 30.75 | 33.37 | 37.31 | . 02997 |
| 26 | 15.94 | 48.89 | 53.06 | 59.32 | . 01885 |
| 27 | 14.20 | 77.74 | 84.37 | 94.32 | .01185 |
| 28 | 12.64 | 123.6 | 134.2 | 150.0 | . 007454 |
| 29 | 11.26 | 196.6 | 213.3 | 238.5 | . 004688 |
| 30 | 10.03 | 312.5 | 339.2 | 379.2 | . 002948 |
| 31 | 8.928 | 497.0 | 539.3 | 602.9 | . 001854 |
| 32 | 7.950 | 790.2 | 857.6 | 958.7 | . 001166 |
| 33 | 7.080 | 1256. | 1364. | 1524. | . 0007333 |
| 34 | 6.305 | 1998. | 2168. | 2424. | . 0004612 |
| 35 | 5.615 | 3177. | 3448. | 3854. | . 0002901 |
| 36 | 5.000 | 5051. | 5482. | 6128. | . 0001824 |
| 37 | 4.453 | 8032. | 8717. | 9744. | . 0001147 |
| 38 | 3.965 | 12770. | 13860. | 15490. | . 00007215 |
| 39 | 3.531 | 20310. | 22040. | 24640. | . 00004538 |
| 40 | 3.145 | 32290. | 35040. | 39170. | . 00002854 |

American wire gage (B. \& S.). Metric units

|  | Diameter | Cross section | ${ }^{\text {ohm } / \mathrm{km}}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | at $20^{\circ} \mathrm{C}$ | at $20^{\circ} \mathrm{C}$ | $0^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ |
| 0000 | 11.68 | 107.2 | . 1482 | . 1608 | . 1798 | . 1956 |
| 000 | 10.40 | 85.03 | . 1868 | . 2028 | . 2267 | . 2466 |
| 00 | 9.266 | 67.43 | . 2356 | . 2557 | . 2858 | . 3110 |
| 0 | 8.252 | 53.48 | . 2971 | . 3224 | . 3604 | . 3921 |
| 1 | 7.348 | 42.41 | . 3746 | . 4066 | . 4545 | . 4944 |
| 2 | 6.544 | 33.63 | . 4724 | . 5127 | . 5731 | . 6235 |
| 3 | 5.827 | 26.67 | . 5956 | . 6465 | . 7227 | . 7862 |
| 4 | 5.189 | 21.15 | . 7511 | . 8152 | . 9113 | . 9914 |
| 5 | 4.621 | 16.77 | . 9471 | 1.028 | 1.149 | 1.250 |
| 6 | 4.115 | 13.30 | 1.194 | 1.296 | 1.449 | 1.576 |
| 7 | 3.665 | 10.55 | 1.506 | 1.634 | 1.827 | 1.988 |
| 8 | 3.264 | 8.366 | 1.899 | 2.061 | 2.304 | 2.506 |
| 9 | 2.906 | 6.634 | 2.395 | 2.599 | 2.905 | 3.161 |
| 10 | 2.588 | 5.261 | 3.020 | 3.277 | 3.663 | 3.985 |
| 11 | 2.305 | 4.172 | 3.807 | 4.132 | 4.619 | 5.025 |
| 12 | 2.053 | 3.309 | 4.801 | 5.211 | 5.825 | 6.337 |
| 13 | 1.828 | 2.624 | 6.054 | 6.571 | 7.345 | 7.991 |
| 14 | 1.628 | 2.081 | 7.634 | 8.285 | 9.262 | 10.08 |
| 15 | 1.450 | 1.650 | 9.627 | 10.45 | 11.68 | 12.71 |
| 16 | 1.291 | 1.309 | 12.14 | 13.17 | 14.73 | 16.02 |
| 17 | 1.150 | 1.038 | 15.31 | 16.61 | 18.57 | 20.20 |
| 18 | 1.024 | . 8231 | 19.30 | 20.95 | 23.42 | 25.48 |
| 19 | . 9116 | . 6527 | 24.34 | 26.42 | 29.53 | 32.12 |
| 20 | . 8118. | . 5176 | 30.69 | 33.31 | 37.24 | 40.51 |
| 21 | . 7230 | . 4105 | 38.70 | 42.00 | 46.95 | 51.08 |
| 22 | . 6438 | . 3255 | 48.80 | 52.96 | 59.21 | 64.41 |
| 23 | . 5733 | . 2582 | 61.54 | 66.79 | 74.66 | 81.22 |
| 24 | . 5106 | . 2047 | 77.60 | 84.21 | 94.14 | 102.4 |
| 25 | . 4547 | . 1624 | 97.85 | 106.2 | 118.7 | 129.1 |
| 26 | . 4049 | . 1288 | 123.4 | 133.9 | 149.7 | 162.9 |
| 27 | . 3606 | . 1021 | 155.6 | 168.9 | 188.8 | 205.4 |
| 28 | . 3211 | . 08098 | 196.2 | 212.9 | 238.0 | 258.9 |
| 29 | . 2859 | . 06422 | 247.4 | 268.5 | 300.1 | 326.5 |
| 30 | . 2546 | . 05093 | 311.9 | 338.6 | 378.5 | 411.7 |
| 31 | . 2268 | . 04039 | 393.4 | 426.9 | 477.2 | 519.2 |
| 32 | . 2019 | . 03203 | 496.0 | 538.3 | 601.8 | 654.7 |
| 33 | . 1798 | . 02540 | 625.5 | 678.8 | 758.8 | 825.5 |
| 34 | . 1601 | . 02014 | 788.7 | 856.0 | 956.9 | 1041. |
| 35 | . 1426 | . 01597 | 994.5 | 1079. | 1207. | 1313. |
| 36 | . 1270 | .01267 | 1254. | 1361. | 1522. | 1655. |
| 37 | . 1131 | . 01005 | 1581. | 1716. | 1919. | 2087. |
| 38 | . 1007 | . 007967 | 1994. | 2164. | 2419. | 2632. |
| 39 | . 08969 | . 006318 | 2514. | 2729. | 3051. | 3319. |
| 40 | . 07987 | . 005010 | 3171. | 3441. | 3847. | 4185. |
|  |  |  | (continued) |  |  |  |

TABLE 421.-WIRE TABLE, STANDARD ANNEALED COPPER (continued)
American wire gage (B. \& S.). Metric units

| $\begin{aligned} & \text { Gage } \\ & \text { No. } \end{aligned}$ | Diameter in mm at $20^{\circ} \mathrm{C}$ | $\mathrm{kg} / \mathrm{km}$ | $\mathrm{m} / \mathrm{g}$ | $\mathrm{m} / \mathrm{ohm}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $0^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $75^{\circ} \mathrm{C}$ |
| 0000 | 11.68 | 953.2 | . 001049 | 6749. | 6219. | 5563. | 5113. |
| 000 | 10.40 | 755.9 | . 001323 | 5352. | 4932. | 4412. | 4055. |
| 00 | 9.266 | 599.5 | . 001668 | 4245. | 3911. | 3499. | 3216. |
| 0 | 8.252 | 475.4 | . 002103 | 3366. | 3102. | 2774. | 2550. |
|  | 7.348 | 377.0 | . 002652 | 20669. | 2460. | 2200. | 2022. |
| 2 | 6.544 | 299.0 | . 003345 | 2117. | 1951. | 1745. | 1604. |
| 3 | 5.827 | 237.1 | . 004217 | 1679. | 1547. | 1384. | 1272. |
|  | 5.189 | 188.0 | . 005318 | 1331. | 1227. | 1097. | 1009. |
| 5 | 4.621 | 149.1 | . 006706 | 1056. | 972.9 | 870.2 | 799.9 |
| 6 | 4.114 | 118.2 | . 008457 | 837.3 | 771.5 | 690.1 | 634.4 |
| 7 | 3.665 | 93.78 | . 01066 | 664.0 | 611.8 | 547.3 | 503.1 |
| 8 | 3.264 | 74.37 | . 01345 | 526.6 | 485.2 | 434.0 | 399.0 |
| 9 | 2.906 | 58.98 | . 01696 | 417.6 | 384.8 | 344.2 | 316.4 |
| 10 | 2.588 | 46.77 | . 02138 | 331.2 | 305.1 | 273.0 | 250.9 |
| 11 | 2.305 | 37.09 | . 02696 | 262.6 | 242.0 | 216.5 | 199.0 |
| 12 | 2.053 | 29.42 | . 03400 | 208.3 | 191.9 | 171.7 | 157.8 |
| 13 | 1.828 | 23.33 | . 04287 | 165.2 | 152.2 | 136.1 | 125.1 |
| 14 | 1.628 | 18.50 | . 05406 | 131.0 | 120.7 | 108.0 | 99.24 |
| 15 | 1.450 | 14.67 | . 06816 | 103.9 | 95.71 | 85.62 | 78.70 |
| 16 | 1.291 | 11.63 | . 08595 | 82.38 | 75.90 | 67.90 | 62.41 |
| 17 | 1.150 | 9.226 | . 1084 | 65.33 | 60.20 | 53.85 | 49.50 |
| 18 | 1.024 | 7.317 | . 1367 | 51.81 | 47.74 | 42.70 | 39.25 |
| 19 | . 9116 | 5.803 | . 1723 | 41.09 | 37.86 | 33.86 | 31.13 |
| 20 | . 8118 | 4.602 | . 2173 | 32.58 | 30.02 | 26.86 | 24.69 |
| 21 | . 7230 | 3.649 | . 2740 | 25.84 | 23.81 | 21.30 | 19.58 |
| 22 | . 6438 | 2.894 | . 3455 | 20.49 | 18.88 | 16.89 | 15.53 |
| 23 | . 5733 | 2.295 | . 4357 | 16.25 | 14.97 | 13.39 | 12.31 |
| 24 | . 5106 | 1.820 | . 5494 | 12.89 | 11.87 | 10.62 | 9.764 |
| 25 | . 4547 | 1.443 | . 6928 | 10.22 | 9.417 | 8.424 | 7.743 |
| 26 | . 4049 | 1.145 | . 8736 | 8.105 | 7.468 | 6.680 | 6.141 |
| 27 | . 3606 | . 9078 | 1.102 | 6.428 | 5.922 | 5.298 | 4.870 |
| 28 | . 3211 | . 7199 | 1.389 | 5.097 | 4.697 | 4.201 | 3.862 |
| 29 | . 2859 | . 5709 | 1.752 | 4.042 | 3.725 | 3.332 | 3.063 |
| 30 | . 2546 | . 4527 | 2.209 | 3.206 | 2.954 | 2.642 | 2.429 |
| 31 | . 2268 | . 3590 | 2.785 | 2.542 | 2.342 | 2.095 | 1.926 |
| 32 | . 2019 | . 2847 | 3.512 | 2.016 | 1.858 | 1.662 | 1.527 |
| 33 | . 1798 | . 2258 | 4.429 | 1.599 | 1.473 | 1.318 | 1.211 |
| 34 | . 1601 | . 1791 | 5.584 | 1.268 | 1.168 | 1.045 | . 9606 |
| 35 | . 1426 | . 1420 | 7.042 | 1.006 | . 9265 | . 8288 | . 7618 |
| 36 | . 1270 | . 1126 | 8.879 | . 7974 | . 7347 | . 6572 | . 6041 |
| 37 | . 1131 | . 08931 | 11.20 | . 6324 | . 5827 | . 5212 | . 4791 |
| 38 | . 1007 | . 07083 | 14.12 | . 5015 | . 4621 | . 4133 | . 3799 |
| 39 | . 08969 | . 05617 | 17.80 | . 3977 | . 3654 | . 3278 | . 3013 |
| 40 | . 07987 | . 04454 | 22.45 | . 3154 | . 2906 | . 2600 | . 2390 |
|  |  |  |  | Hed) |  |  |  |

TABLE 421.-WIRE TABLE, STANDARD ANNEALED COPPER (concluded)
American wire gage (B. \& S.). Metric units

| Gage No. | Diameter in mm at $20^{\circ} \mathrm{C}$ | $\overbrace{}^{\text {ohm } / \mathrm{kg}}$ |  |  | g/ohm$20^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $0^{\circ} \mathrm{C}$ | $20^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ |  |
| 0000 | 11.68 | . 0001554 | . 0001687 | . 0001886 | 5928000. |
| 000 | 10.40 | . 0002472 | . 0002682 | . 0002999 | 3728000. |
| 00 | 9.266 | . 0003930 | . 0004265 | . 0004768 | 2344000. |
| 0 | 8.252 | . 0006249 | . 0006782 | . 0007582 | 1474000. |
| 1 | 7.348 | . 0009936 | . 001078 | . 001206 | 927300. |
| 2 | 6.544 | . 001580 | . 001715 | . 001917 | 583200. |
| 3 | 5.827 | . 002512 | . 002726 | . 003048 | 366800. |
| 4 | 5.189 | .003 995 | . 004335 | . 004846 | 230700. |
| 5 | 4.621 | . 006352 | . 006893 | . 007706 | 145100. |
| 6 | 4.115 | . 01010 | . 01096 | . 01225 | 91230. |
| 7 | 3.665 | . 01606 | . 01743 | . 01948 | 57380. |
| 8 | 3.264 | . 02553 | . 02771 | . 03098 | 36080. |
| 9 | 2.906 | . 04060 | . 04406 | . 04926 | 22690. |
| 10 | 2.588 | . 06456 | . 07007 | . 07833 | 14270. |
| 11 | 2.305 | . 1026 | . 1114 | . 1245 | 8976. |
| 12 | 2.053 | . 1632 | .1771 | . 1980 | 5645. |
| 13 | 1.828 | . 2595 | . 2817 | . 3149 | 3550. |
| 14 | 1.628 | . 4127 | . 4479 | . 5007 | 2233. |
| 15 | 1.450 | . 6562 | . 7122 | . 7961 | 1404. |
| 16 | 1.291 | 1.043 | 1.132 | 1.266 | 883.1 |
| 17 | 1.150 | 1.659 | 1.801 | 2.013 | 555.4 |
| 18 | 1.024 | 2.638 | 2.863 | 3.201 | 349.3 |
| 19 | . 9116 | 4.194 | 4.552 | 5.089 | 219.7 |
| 20 | . 8118 | 6.670 | 7.238 | 8.092 | 138.2 |
| 21 | . 7230 | 10.60 | 11.51 | 12.87 | 86.88 |
| 22 | . 6438 | 16.86 | 18.30 | 20.46 | 54.64 |
| 23 | . 5733 | 26.81 | 29.10 | 32.53 | 34.36 |
| 24 | . 5106 | 42.63 | 46.27 | 51.73 | 21.61 |
| 25 | . 4547 | 67.79 | 73.57 | 82.25 | 13.59 |
| 26 | . 4049 | 107.8 | 117.0 | 130.8 | 8.548 |
| 27 | . 3606 | 171.4 | 186.0 | 207.9 | 5.376 |
| 28 | . 3211 | 272.5 | 295.8 | 330.6 | 3.381 |
| 29 | . 2859 | 433.3 | 470.3 | 525.7 | 2.126 |
| 30 | . 2546 | 689.0 | 747.8 | 836.0 | 1.337 |
| 31 | . 2268 | 1096. | 1189. | 1329. | . 8410 |
| 32 | . 2019 | 1742. | 1891. | 2114. | . 5289 |
| 33 | . 1798 | 2770. | 3006. | 3361. | . 3326 |
| 34 | . 1601 | 4404. | 4780. | 5344. | . 2092 |
| 35 | . 1426 | 7003. | 7601. | 8497. | . 1316 |
| 36 | .1270 | 11140. | 12090. | 13510. | . 08274 |
| 37 | . 1131 | 17710. | 19320. | 21480. | . 05204 |
| 38 | . 1007 | 28150. | 30560. | 34160. | . 03273 |
| 39 | . 08969 | 44770. | 48590. | 54310. | . 02058 |
| 40 | . 07987 | 71180. | 77260. | 86360. | . 01294 |

TABLE 422.-WIRE TABLE, ALUMINUM
Hard-drawn aluminum wire at $20^{\circ} \mathrm{C}\left(68^{\circ} \mathrm{F}\right)$
American wire gage (B. \& S.). Engiish units

| $\begin{aligned} & \text { Gage } \\ & \text { No. } \end{aligned}$ | Diameter in mils | Cross section |  | $\frac{\text { ohm }}{1000 \mathrm{ft}}$ | 1 b | lb/ohm | $\mathrm{ft} / \mathrm{ohm}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\overbrace{\text { Circular mils }}$ | . ${ }^{2}$ |  | $\overline{1000 \mathrm{ft}}$ |  |  |
| 0000 | 460. | 212000. | . 166 | . 0804 | 195. | 2420. | 12400. |
| 000 | 410. | 168000. | . 132 | . 101 | 154. | 1520. | 9860. |
| 00 | 365. | 133000. | . 105 | . 128 | 122. | 957. | 7820. |
| 0 | 325. | 106000. | . 0829 | . 161 | 97.0 | 602. | 6200. |
| 1 | 289. | 83700. | . 0657 | . 203 | 76.9 | 379. | 4920. |
| 2 | 258. | 66400. | . 0521 | . 256 | 61.0 | 238. | 3900. |
| 3 | 229. | 52600. | . 0413 | . 323 | 48.4 | 150. | 3090. |
| 4 | 204. | 41700. | . 0328 | . 408 | 38.4 | 94.2 | 2450. |
| 5 | 182. | 33100. | . 0260 | . 514 | 30.4 | 59.2 | 1950. |
| 6 | 162. | 26300. | . 0206 | . 648 | 24.1 | 37.2 | 1540. |
| 7 | 144. | 20800. | . 0164 | . 817 | 19.1 | 23.4 | 1220. |
| 8 | 128. | 16500. | . 0130 | 1.03 | 15.2 | 14.7 | 970. |
| 9 | 114. | 13100. | . 0103 | 1.30 | 12.0 | 9.26 | 770. |
| 10 | 102. | 10400. | . 00815 | 1.64 | 9.55 | 5.83 | 610. |
| 11 | 91. | 8230. | . 00647 | 2.07 | 7.57 | 3.66 | 484. |
| 12 | 81. | 6530. | . 00513 | 2.61 | 6.00 | 2.30 | 384. |
| 13 | 72. | 5180. | . 00407 | 3.29 | 4.76 | 1.45 | 304. |
| 14 | 64. | 4110. | . 00323 | 4.14 | 3.78 | . 911 | 241. |
| 15 | 57. | 3260. | . 00256 | 5.22 | 2.99 | . 573 | 191. |
| 16 | 51. | 2580. | . 00203 | 6.59 | 2.37 | . 360 | 152. |
| 17 | 45. | 2050. | . 00161 | 8.31 | 1.88 | . 227 | 120. |
| 18 | 40. | 1620. | . 00128 | 10.5 | 1.49 | . 143 | 95.5 |
| 19 | 36. | 1290. | . 00101 | 13.2 | 1.18 | . 0897 | 75.7 |
| 20 | 32. | 1020. | . 000802 | 16.7 | . 939 | . 0564 | 60.0 |
| 21 | 28.5 | 810. | . 000636 | 21.0 | . 745 | . 0355 | 47.6 |
| 22 | 25.3 | 642. | . 000505 | 26.5 | . 591 | . 0223 | 37.8 |
| 23 | 22.6 | 509. | . 000400 | 33.4 | . 468 | . 0140 | 29.9 |
| 24 | 20.1 | 404. | . 000317 | 42.1 | . 371 | . 00882 | 23.7 |
| 25 | 17.9 | 320. | . 000252 | 53.1 | . 295 | . 00555 | 18.8 |
| 26 | 15.9 | 254. | . 000200 | 67.0 | . 234 | . 00349 | 14.9 |
| 27 | 14.2 | 202. | . 000158 | 84.4 | . 185 | . 00219 | 11.8 |
| 28 | 12.6 | 160. | . 000126 | 106. | . 147 | . 00138 | 9.39 |
| 29 | 11.3 | 127. | . 0000995 | 134. | . 117 | . 000868 | 7.45 |
| 30 | 10.0 | 101. | . 0000789 | 169. | . 0924 | . 000546 | 5.91 |
| 31 | 8.9 | 79.7 | . 0000626 | 213. | . 0733 | . 000343 | 4.68 |
| 32 | 8.0 | 63.2 | . 0000496 | 269. | . 0581 | . 000216 | 3.72 |
| 33 | 7.1 | 50.1 | . 0000394 | 339. | . 0461 | . 000136 | 2.95 |
| 34 | 6.3 | 39.8 | . 0000312 | 428. | . 0365 | . 0000854 | 2.34 |
| 35 | 5.6 | 31.5 | . 0000248 | 540. | . 0290 | . 0000537 | 1.85 |
| 36 | 5.0 | 25.0 | . 0000196 | 681. | . 0230 | . 0000338 | 1.47 |
| 37 | 4.5 | 19.8 | . 0000156 | 858. | . 0182 | . 0000212 | 1.17 |
| 38 | 4.0 | 15.7 | . 0000123 | 1080. | . 0145 | . 0000134 | . 924 |
| 39 | 3.5 | 12.5 | . 00000979 | 1360. | . 0115 | . 00000840 | . 733 |
| 40 | 3.1 | 9.9 | . 00000777 | 1720. | . 0091 | . 00000528 | . 581 |

TABLE 423.-WIRE TABLE, ALUMINUM
Hard-drawn aluminum wire at $20^{\circ} \mathrm{C}\left(68^{\circ} \mathrm{F}\right)$
American wire gage (B. \& S.). Metric units

| $\begin{gathered} \text { Gage } \\ \text { No. } \end{gathered}$ | Diameter in mm | Cross section in $\mathrm{mm}^{2}$ | ohm/km | kg/km | g/ohm | $\mathrm{m} / \mathrm{ohm}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0000 | 11.7 | 107. | . 264 | 289. | 1100000. | 3790. |
| 000 | 10.4 | 85.0 | . 333 | 230. | 69000. | 3010. |
| 00 | 9.3 | 67.4 | . 419 | 182. | 434000. | 2380. |
| 0 | 8.3 | 53.5 | . 529 | 144. | 273000. | 1890. |
| 1 | 7.3 | 42.4 | . 667 | 114. | 172000. | 1500. |
| 2 | 6.5 | 33.6 | . 841 | 90.8 | 108000. | 1190. |
| 3 | 5.8 | 26.7 | 1.06 | 72.0 | 67900. | 943. |
|  | 5.2 | 21.2 | 1.34 | 57.1 | 42700. | 748. |
| 5 | 4.6 | 16.8 | 1.69 | 45.3 | 26900. | 593. |
| 6 | 4.1 | 13.3 | 2.13 | 35.9 | 16900. | 470. |
| 7 | 3.7 | 10.5 | 2.68 | 28.5 | 10600. | 373. |
| 8 | 3.3 | 8.37 | 3.38 | 22.6 | 6680. | 296. |
|  | 2.91 | 6.63 | 4.26 | 17.9 | 4200. | 235. |
| 10 | 2.59 | 5.26 | 5.38 | 14.2 | 2640. | 186. |
| 11 | 2.30 | 4.17 | 6.78 | 11.3 | 1660. | 148. |
| 12 | 2.05 | 3.31 | 8.55 | 8.93 | 1050. | 117. |
| 13 | 1.83 | 2.62 | 10.8 | 7.08 | 657. | 92.8 |
| 14 | 1.63 | 2.08 | 13.6 | 5.62 | 413. | 73.6 |
| 15 | 1.45 | 1.65 | 17.1 | 4.46 | 260. | 58.4 |
| 16 | 1.29 | 1.31 | 21.6 | 3.53 | 164. | 46.3 |
| 17 | 1.15 | 1.04 | 27.3 | 2.80 | 103. | 36.7 |
| 18 | 1.02 | . 823 | 34.4 | 2.22 | 64.7 | 29.1 |
| 19 | . 91 | . 653 | 43.3 | 1.76 | 40.7 | 23.1 |
| 20 | . 81 | . 518 | 54.6 | 1.40 | 25.6 | 18.3 |
| 21 | . 72 | . 411 | 68.9 | 1.11 | 16.1 | 14.5 |
| 22 | . 64 | . 326 | 86.9 | . 879 | 10.1 | 11.5 |
| 23 | . 57 | . 258 | 110. | . 697 | 6.36 | 9.13 |
| 24 | . 51 | . 205 | 138. | . 553 | 4.00 | 7.24 |
| 25 | . 45 | . 162 | 174. | . 438 | 2.52 | 5.74 |
| 26 | . 40 | . 129 | 220. | . 348 | 1.58 | 4.55 |
| 27 | . 36 | . 102 | 277. | . 276 | . 995 | 3.61 |
| 28 | . 32 | . 0810 | 349. | . 219 | . 626 | 2.86 |
| 29 | . 29 | . 0642 | 440. | . 173 | . 394 | 2.27 |
| 30 | . 25 | . 0509 | 555. | . 138 | . 248 | 1.80 |
| 31 | . 227 | . 0404 | 700. | . 109 | . 156 | 1.43 |
| 32 | . 202 | . 0320 | 883. | . 0865 | . 0979 | 1.13 |
| 33 | . 180 | . 0254 | 1110. | . 0686 | . 0616 | . 899 |
| 34 | . 160 | . 0201 | 1400. | . 0544 | . 0387 | . 712 |
| 35 | . 143 | . 0160 | 1770. | . 0431 | . 0244 | . 565 |
| 36 | . 127 | . 0127 | 2230. |  | . 0153 | . 448 |
| 37 | . 113 | . 0100 | 2820. | . 0271 | . 00963 | . 355 |
| 38 | . 101 | . 0080 | 3550. | . 0215 | . 00606 | . 282 |
| 39 | . 090 | . 0063 | 4480. | . 0171 | . 00381 | . 223 |
| 40 | . 080 | . 0050 | 5640. | . 0135 | . 00240 | . 177 |

TABLE 424.-AUXILIARY TABLE FOR COMPUTING WIRE RESISTANCES
For computing resistances in ohms per meter from resistivity, $\rho$, in microhm-cm (see Table 386, etc.). e.g., to compute for No. 23 copper wire when $\rho=1.724$ : $1 \mathrm{~m}=0.0387+.0271+$ $.0008+.0002=0.0668$ ohms ; for No. 11 lead wire when $\rho=20.4: 1 \mathrm{~m}=0.0479+.0010=$ 0.0489 ohms. The following relation allows computation for wires of other gage numbers: resistance in ohms per m of No. $n$ wire $=2 \times$ resistance of wire No. $(n-3)$ within 1 percent: e.g., resistance of $m$ of No. $18=2 \times$ No. 15 .

| Gage No. | Diam. in mm | Section$\mathrm{mm}^{2}$ | $\rho$ in microhm-cm |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|  |  |  | Resistance of wire 1 m , long in ohms |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0000 | 11.7 | 107.2 | .04933 | .$_{0} 187$ | . 02280 | . 03373 | .03466 | . 03560 | .03653 | . 03746 | . 03840 | .03933 |
| 00 | 9.27 | 67.43 | . 03148 | .03297 | . 03445 | . 03593 | . 03742 | . 03890 | . 02104 | .02119 | . $0_{2} 133$ | . 02148 |
| 1 | 7.35 | 42.41 | . 03236 | . 03472 | . 03707 | . 03943 | . 02118 | . 02141 | . 02165 | . $\mathrm{O}_{2} 189$ | . $0_{2} 212$ | . 02236 |
| 3 | 5.83 | 26.67 | . 03375 | . 03750 | . 02112 | . 02150 | . 02187 | . 02225 | . 02262 | . 02300 | . 02337 | . 02375 |
| 5 | 4.62 | 16.77 | . 03596 | . 02119 | . 02179 | . 02239 | . 02298 | . 02358 | . 02417 | . 02477 | . 02537 | . 02596 |
| 7 | 3.66 | 10.55 | . 03948 | . 02190 | . 02284 | . 02379 | . 02474 | . 02569 | . 02664 | . 02758 | . 02853 | . 02948 |
| 9 | 2.91 | 6.634 | . 0.151 | . 02301 | . 02452 | . 02603 | . 02754 | . 02904 | . 0106 | . 0121 | . 0136 | . 0151 |
| 11 | 2.30 | 4.172 | . 02240 | . 02479 | . 02719 | . 02959 | . 0120 | . 0144 | . 0168 | . 0192 | . 0216 | . 0240 |
| 13 | 1.83 | 2.624 | . 02381 | . 02762 | . 0114 | . 0152 | . 0191 | . 0229 | . 0267 | . 0305 | . 0343 | . 0381 |
| 15 | 1.45 | 1.650 | . 02606 | . 0121 | . 0182 | . 0242 | . 0303 | . 0364 | . 0424 | . 0485 | . 0545 | . 0606 |
| 17 | 1.15 | 1.038 | . 02963 | . 0193 | . 0289 | . 0385 | . 0482 | . 0578 | . 0674 | . 0771 | . 0867 | . 0963 |
| 19 | . 912 | . 6527 | . 0153 | . 0306 | . 0460 | . 0613 | . 0766 | . 0919 | . 1072 | . 1226 | . 1379 | . 1532 |
| 21 | . 723 | . 4105 | . 0244 | . 0487 | . 0731 | . 0974 | . 1218 | . 1462 | . 1705 | . 1949 | . 2192 | . 2436 |
| 23 | . 573 | . 2582 | . 0387 | . 0775 | . 1162 | . 1549 | . 1936 | . 2324 | . 2711 | . 3098 | . 3486 | . 3873 |
| 25 | . 455 | . 1624 | . 0616 | . 1232 | . 1847 | . 2463 | . 3079 | . 3695 | . 4310 | . 4926 | . 5542 | . 6158 |
| 27 | . 361 | . 1021 | . 0979 | . 1959 | . 2938 | . 3918 | . 4897 | . 5877 | . 6856 | . 7835 | . 8815 | . 9794 |
| 29 | . 286 | . 0642 | . 1557 | . 3114 | . 4671 | . 6228 | . 7786 | . 9343 | 1.090 | 1.246 | 1.401 | 1.557 |
| 31 | . 227 | . 0404 | . 2476 | . 4952 | . 7428 | . 9904 | 1.238 | 1.486 | 1.733 | 1.981 | 2.228 | 2.476 |
| 33 | . 180 | . 0254 | . 3937 | . 7874 | 1.181 | 1.575 | 1.968 | 2.362 | 2.756 | 3.150 | 3.543 | 3.937 |
| 35 | . 143 | . 0160 | . 6262 | 1.252 | 1.879 | 2.505 | 3.131 | 3.757 | 4.383 | 5.009 | 5.636 | 6.262 |
| 37 | . 113 | . 0100 | . 9950 | 1.990 | 2.985 | 3.980 | 4.975 | 5.970 | 6.965 | 7.960 | 8.955 | 9.950 |
| 39 | . 090 | . 0063 | 1.583 | 3.166 | 4.748 | 6.331 | 7.914 | 9.497 | 11.08 | 12.66 | 14.25 | 15.83 |
| 40 | . 080 | . 0050 | 1.996 | 3.992 | 5.988 | 7.984 | 9.980 | 11.98 | 13.97 | 15.97 | 17.96 | 19.96 |

TABLE 425.-SAFE CURRENT-CARRYING CAPACITY OF COPPER WIRE, FOR DIFFERENT CONDITIONS, IN AMPERES PER CONDUCTOR*

| $\begin{aligned} & \text { Wire } \\ & \text { size } \\ & \text { AWG } \end{aligned}$ | $\overbrace{}^{\text {Varnish cambric insuiators }}$ |  |  |  | $\overbrace{}^{\text {Impregnated }}$ paper insulation |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Not more than three conductors in raceway or cable | Rubber insulators <br> in enclosed and exposed conduit |  |  |  |
|  | Single wire in free air |  |  |  |  | Three con- |
|  |  |  | Single | Three | conductor | in under- |
|  |  |  | conductor | conductor. | cable in air | ground duct |
| 14 | 30 | 23 | 23 | 19 |  |  |
| 10 | 54 | 38 | 40 | 33 |  |  |
| 6 | 99 | 68 | 71 | 57 | 98 | 78 |
| 3 | 155 | 104 |  |  |  |  |
| 2 | 179 | 118 | 127 | 101 | 173 | 134 |
| 0 | 245 | 157 | 167 | 133 | 234 | 177 |
| 0000 | 383 | 237 | 256 | 203 | 352 | 264 |

[^181]TABLE 426.-THE CALCULATION OF THE HIGH-FREQUENCY RESISTANCE OF CONDUCTORS*

The resistance of a conductor to high-frequency alternating currents is not the same as it offers to direct or low-frequency currents. The linkages of flux with the inner portions of the conductor are more numerous than with the outer portions. That is, the reactances of the inner filaments are greater than those of the outer filaments. Consequently, the current density decreases from the outside toward the center of the conductor.

This tendency of the current to crowd toward the outer portions of the cross section becomes more pronounced the higher the frequency, and at very high frequencies the current density is sensibly zero everywhere except in the surface layer of the conductor. This phenomenon is called the "skin effect." It causes an increase in the effective resistance of the conductor over its resistance to a direct current.

What is of interest in the calculation of the high-frequency resistance is the resistance ratio, the quotient of the resistance at the given frequency by the direct-current resistance. The resistance ratio depends upon the distribution of current density in the cross section, and this is a function of the frequency and the shape of the cross section. In general, however, the resistance ratio is a function of the parameter $\sqrt{\frac{f}{R_{0}}}$, in which $f$ is the frequency, and $R_{0}$ is the direct-current resistance per unit length. In what follows $R_{0}$ will be taken as the direct-current resistance per 1000 ft of conductor.

The distribution of current in the cross section is affected by a neighboring conductor carrying high-frequency currents. This proximity effect finds an explanation in that the value of the mutual inductance of any filament $A$ of one conductor on a filament $B$ of the other conductor depends upon the positions of $A$ and $B$ in their respective cross sections. The proximity effect may be very appreciable for conductors nearly in contact; falling off rapidly as their distance increased, it is negligible for moderate ratios of distance apart to cross sectional dimensions. In such cases the resistance is sensibly the same as for an isolated conductor.
Besides the spacing factor of the conductors, the proximity effect depends upon the frequency, and in lesser degree upon the shape of the cross sections. Quantitatively, the proximity effect may be expressed by the proximity factor, which is the quotient of actual resistance of the conductor by the resistance which it would have if removed to a great distance from the disturbing conductor, both values of resistance being referred to the same frequency.

That is, if
$R_{0}=$ the direct current resistance
$R_{1}=$ the resistance of the conductor when isolated, frequency $f$
$R_{2}=$ the resistance in the presence of the disturbing conductor at frequency $f$
then the proximity factor is $P=\frac{R_{2}}{R_{1}}$, and the resistance ratio $\frac{R_{2}}{R_{0}}$, in the presence of the disturbing conductor, is obtained from the resistance ratio $\frac{R_{1}}{R_{0}}$ when isolated by the relation $\frac{R_{2}}{R_{0}}=P \frac{R_{1}}{R_{0}}$. Resistance ratio may be obtained in any case if the resistance ratio when isolated is known, together with the value of the proximity factor.

Formulas for the high-frequency resistance ratio have been developed in only a few simple (but important) cases, and even then very complicated formulas result. For practical work, tables are necessary for simplifying the calculations. The following tables cover the most important cases.

Formulas have been derived for the high-frequency resistance ratio of single-layer coils wound with round wire. Generally, these differ from one another and from measured values, because simplifying assumptions are made which are not sufficiently realized in practice. No tables of values for coils such as are met in practical radio work are available As a rough guide, the high-frequency resistance ratio for a single-layer coil is often from two to five times as great as the resistance ratio of the same wire stretched out straight and carrying current of the given frequency. The experimental work available indicates that this factor is due to the coiling of the wire, that is, the total proximity effect of the turns of the coil is largely dependent upon the frequency and the ratio of wire diameter to pitch of winding, and in lesser degree to the ratio of length to diameter.

[^182](continued)

TABLE 426.-THE CALCULATION OF THE HIGH-FREQUENCY RESISTANCE OF CONDUCTORS (continued)

## Part 1.-Resistance ratio "F" for isolated round wires

Resistance ratio $F$ of isolated round wire, as a function of the square root of the frequency divided by the direct current resistance per 1000 ft of conductor.

| $v \overline{f / R_{0}}$ | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $F$ | 1.000 | 1.000 | 1.0005 | 1.0025 | 1.008 | 1.019 | 1.038 | 1.069 | 1.114 | 1.173 | 1.247 |
| $V \overline{f / R_{0}}$ | 100 | 120 | 140 | 160 | 180 | 200 | 250 | 300 | 350 | 400 | 500 |
| $F$ | 1.247 | 1.427 | 1.631 | 1.836 | 2.036 | 2.231 | 2.715 | 3.201 | 3.688 | 4.176 | 5.152 |

Part 2.-Values of resistance ratio for isolated tubular conductors
$t$, thickness of wall of tube; $d$, outer diameter of tube

| $\sqrt{\frac{f}{R_{0}}}$ | $\frac{t}{d}=0.01$ | 0.02 | 0.03 | 0.04 | 0.05 | 0.06 | 0.07 | 0.08 | 0.09 | 0.10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 50 | 1.000 | 1.000 | 1.000 | 1.001 | 1.001 | 1.001 | 1.001 | 1.001 | 1.001 | 1.001 |
| 100 | 1.001 | 1.001 | 1.002 | 1.002 | 1.004 | 1.008 | 1.007 | 1.009 |  | 1.014 |
| 150 | 1.001 | 1.003 | 1.006 | 1.011 | 1.017 | 1.024 | 1.033 | 1.044 | 1.056 | 1.070 |
| 200 | 1.002 | 1.008 | 1.019 | 1.034 | 1.053 | 1.076 | 1.104 | 1.134 | 1.167 | 1.204 |
| 250 | 1.005 | 1.020 | 1.046 | 1.081 | 1.125 | 1.176 | 1.233 | 1.296 | 1.365 | 1.440 |
| 300 | 1.011 | 1.042 | 1.095 | 1.163 | 1.25 | 1.34 | 1.44 | 1.55 | 1.65 | 1.75 |
| 350 | 1.020 | 1.076 | 1.167 | 1.285 | 1.42 | 1.56 | 1.70 | 1.83 | 1.97 | 2.09 |
| 400 | 1.032 | 1.127 | 1.27 | 1.44 | 1.66 | 1.81 | 1.99 | 2.13 | 2.28 | 2.42 |
| 450 | 1.051 | 1.198 | 1.41 | 1.63 | 1.87 | 2.08 | 2.28 | 2.44 | 2.60 | 2.74 |
| 500 | 1.079 | 1.30 | 1.57 | 1.86 | 2.14 | 2.34 | 2.56 | 2.73 | 2.88 | 3.03 |
| $\sqrt{\frac{f}{R_{0}}}$ | $\frac{t}{d}=0.10$ | 0.12 | 0.15 | 0.20 | 0.25 | 0.30 | 0.35 | 0.40 | 0.45 | ${ }_{\text {Solid }}$ |
| 0 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 50 | 1.001 | 1.001 | 1.002 | 1.004 | 1.006 | 1.008 | 1.012 | 1.015 | 1.017 | 1.019 |
| 100 | 1.014 | 1.021 | 1.032 | 1.063 | 1.094 | 1.132 | 1.175 | 1.202 | 1.224 | 1.247 |
| 150 | 1.070 | 1.102 | 1.155 | 1.266 | 1.39 | 1.51 | 1.60 | 1.68 | 1.71 | 1.733 |
| 200 | 1.204 | 1.294 | 1.42 | 1.65 | 1.845 | 1.995 | 2.095 | 2.15 | 2.20 | 2.231 |
| 250 | 1.44 | 1.585 | 1.79 | 2.11 | 2.32 | 2.45 | 2.536 | 2.64 | 2.68 | 2.715 |
| 300 | 1.75 | 1.94 | 2.19 | 2.51 | 2.735 | 2.90 | 3.03 | 3.12 | 3.17 | 3.201 |
| 350 | 2.09 | 2.33 | 2.57 | 2.90 | 3.15 | 3.35 | 3.495 | 3.59 | 3.66 | 3.688 |
| 400 | 2.42 | 2.66 | 2.92 | 3.27 | 3.58 | 3.80 | 3.96 | 4.07 | 4.14 | 4.176 |
| 450 | 2.74 | 3.00 | 3.27 | 3.66 | 4.00 | 4.25 | 4.43 | 4.55 | 4.63 | 4.664 |
| 500 | 3.03 | 3.33 | 3.62 | 4.07 | 4.42 | 4.69 | 4.90 | 5.03 | 5.12 | 5.152 |
| (continued) |  |  |  |  |  |  |  |  |  |  |

# TABLE 426.-THE CALCULATION OF THE HIGH-FREQUENCY RESISTANCE OF CONDUCTORS (concluded) 

## Part 3.-Coefficients in formula for proximity factor of equal parallel round wires

The proximity factor of two equal parallel conductors may be calculated by the formula

$$
P=1+\left[G \cdot d^{2} / s^{2}\right] /\left[F\left(1-H d^{2} / s^{2}\right)\right]
$$

in which the coefficient $F$ is to be obtained from Part 1 for the given value of $\sqrt{f / R_{0}}$ and the coefficients $G$ and $H$ are to be taken from the table below for the given value of $\sqrt{f / R_{0}}$. In the table below the values of $H$ apply to currents in the same direction; in the case of currents in opposite directions $H^{\prime}$ is to be used. In the above formula $d$ is the diameter of the wires and $s$ their axial spacing. The proximity factor for two equal parallel tubular conductors does not differ much from the value for two solid wires with the same axial spacing and a value of $\overline{f / R_{0}}$ one-half the value for two solid wires of the same diameter, except for conductors very close together.

| $\sqrt{f / R_{0}}$ | $G$ | $H$ | $H^{\prime}$ | $\sqrt{f / R_{0}}$ | $G$ | $H$ | $H^{\prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | +.0417 | +.0417 | 200 | .8491 | -.1904 | .5530 |
| 25 | .0036 | .0395 | .0443 | 250 | 1.0959 | -.2017 | .5932 |
| 50 | .0519 | +.0109 | .0798 | 300 | 1.340 | -.2093 | .6200 |
| 75 | .1903 | -.0659 | .1838 | 350 | 1.585 | -.2149 | .6389 |
| 100 | .3562 | -.1379 | .3112 | 400 | 1.830 | -.2191 | .6530 |
| 125 | .4914 | -.1685 | .4114 | 450 | 2.073 | -.2224 | .6639 |
| 150 | .6096 | -.1776 | .4787 | 500 | 2.319 | -.2231 | .6722 |
| 175 | .7277 | -.1839 | .5228 |  |  |  |  |

## TABLE 427.-RATIO OF ALTERNATING TO DIRECT CURRENT RESISTANCES FOR COPPER WIRES

This table gives the ratio of the resistance of straight copper wires with alternating currents of different frequencies to the value of the resistance with direct currents.

| Diameter of wire in mm | Frequency $f=$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 60 | 100 | 1000 | 10,000 | 100,000 | 1,000,000 |
| . 05 | _ | -- | - | -_ | -- | *1.001 |
| . 1 | -- | -- | - | - | *1.001 | 1.008 |
| . 25 | -- | -- | - | -- | 1.003 | 1.247 |
| . 5 | - | - | -- | *1.001 | 1.047 | 2.240 |
| 1.0 | -- | -- | - | 1.008 | 1.503 | 4.19 |
| 2.0 | -- | -- | 1.001 | 1.120 | 2.756 | 8.10 |
| 3. | -- | -- | 1.006 | 1.437 | 4.00 | 12.0 |
| 4. | -- | -- | 1.021 | 1.842 | 5.24 | 17.4 |
| 5. | -- | *1.001 | 1.047 | 2.240 | 6.49 | 19.7 |
| 7.5 | 1.001 | 1.002 | 1.210 | 3.22 | 7.50 | 29.7 |
| 10. | 1.003 | 1.008 | 1.503 | 4.19 | 12.7 | 39.1 |
| 15. | 1.016 | 1.038 | 2.136 | 6.14 | 18.8 | - |
| 20. | 1.044 | 1.120 | 2.756 | 8.10 | 25.2 | - |
| 25. | 1.105 | 1.247 | 3.38 | 10.1 | 28.3 | - |
| 40. | 1.474 | 1.842 | 5.24 | 17.4 | - | - |
| 100. | 3.31 | 4.19 | 13.7 | 39.1 | - | - |

Values between 1.000 and 1.001 are indicated by $* 1.001$.
The values are for wires having an assumed conductivity of 1.60 microhm- cm ; for copper wires at room temperatures the values are slightly less than as given in table.
The change of resistance of wire other than copper (iron wires excepted) may be calculated from the above table by taking it as proportional to $d \sqrt{f / \rho}$ where $d=$ diameter, $f$ the frequency (cycles $/ \mathrm{sec}$ ) and $\rho$ the resistivity.

If a given wire be wound into a solenoid, its resistance, at a given frequency, will be greater than the values in the table, which apply to straight wires only. The resistance in this case is a complicated function of the pitch and radius of the winding, the frequency, and the diameter of the wire, and is found by experiment to be sometimes as much as twice the value for a straight wire.

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TABLE 428.-MAXIMUM DIAMETER OF WIRES FOR HIGH-FREQUENCY RESISTANCE RATIO OF 1.01

| Frequency $\div 10^{00}$ | 0.1 | 0.2 | 0.4 | 0.6 | 0.8 | 1.0 | 1.2 | 1.5 | 2.0 | 3.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wavelength, m | 3003 | 1500 | 750 | 500 | 375 | 300 | 250 | 200 | 150 | 100 |
|  | Diameter in cm |  |  |  |  |  |  |  |  |  |
| Copper . | . 0356 | . 0251 | . 0177 | . 0145 | . 0125 | . 0112 | . 0102 | . 0092 | . 0079 | . 0065 |
| Silver | . 0345 | . 0244 | . 0172 | . 0141 | . 0122 | . 0109 | . 0099 | . 0089 | . 0077 | . 0063 |
| Gold | . 0420 | . 0297 | . 0210 | . 0172 | . 0149 | . 0133 | . 0121 | . 0108 | . 0094 | . 0077 |
| Platinum | . 1120 | . 0793 | . 0560 | . 0457 | . 0396 | . 0354 | . 0323 | . 0290 | . 0250 | . 0205 |
| Mercury | . 264 | . 187 | . 132 | . 1080 | . 0936 | . 0836 | . 0763 | . 0683 | . 0591 | . 0483 |
| Manganin | . 1784 | . 1261 | . 0892 | . 0729 | . 0631 | . 0564 | . 0515 | . 0461 | . 0399 | . 0325 |
| Constantan | . 1892 | . 1337 | . 0946 | . 0772 | . 0664 | . 0598 | . 0546 | . 0488 | . 0423 | . 0345 |
| German silver | . 1942 | . 1372 | . 0970 | . 0792 | . 0692 | . 0614 | . 0560 | . 0500 | . 0434 | . 0354 |
| Graphite . . . | . 765 | . 541 | . 383 | . 312 | . 271 | . 242 | . 221 | . 197 | . 171 | . 140 |
| Carbon | 1.60 | 1.13 | . 801 | . 654 | . 566 | . 506 | . 462 | . 414 | . 358 | . 292 |
| Iron $\mu=1000$. | . 00263 | . 00186 | . 00131 | . 00108 | . 00094 | . 00083 | . 00076 | . 00068 | . 00059 | . 00048 |
| $\mu=500$. | . 00373 | . 00264 | . 00187 | . 00152 | . 00132 | . 00118 | . 00108 | . 00096 | . 00084 | . 00068 |
| $\mu=100$. | . 00838 | . 00590 | . 00418 | . 00340 | . 00295 | . 00264 | . 00241 | . 00215 | . 00186 | . 00152 |

TABLES 429-452.--SOME CHARACTERISTICS OF DIELECTRICS

TABLE 429.-STEADY POTENTIAL DIFFERENCE IN VOLTS REQUIRED TO PRODUCE A SPARK IN AIR WITH BALL ELECTRODES (RADIUS R)

| Spark <br> length, <br> cm | $R=0$ <br> Points | $R=0.25$ <br> cm | $R=0.5$ <br> cm | $R=1 \mathrm{~cm}$ | $R=2 \mathrm{~cm}$ | $R=3 \mathrm{~cm}$ | $R=\infty$ <br> Plates |
| :---: | ---: | :---: | :---: | :---: | :---: | :---: | ---: |
| .02 | - | - | 1560 | 1530 |  |  |  |
| .04 | - | - | 2460 | 2430 | 2340 |  |  |
| .06 | - | - | 3300 | 3240 | 3060 |  |  |
| .08 | 3720 | 5010 | 4050 | 3990 | 3810 |  |  |
| .1 | 47680 | 8610 | 8490 | 4560 | 4560 | 4500 | 4350 |
| .2 | 43490 | 8370 | 7770 | 7590 |  |  |  |
| .3 | 5310 | 11140 | 11460 | 11340 | 11190 | 10560 | 10650 |
| .4 | 5970 | 14040 | 14310 | 14340 | 14250 | 13140 | 13560 |
| .5 | 6300 | 15990 | 16950 | 17220 | 16650 | 16470 | 16320 |
| .6 | 6840 | 17130 | 19740 | 20070 | 20070 | 19380 | 19110 |
| .8 | 8070 | 18960 | 23790 | 24780 | 25830 | 26220 | 24960 |
| 1.0 | 8670 | 20670 | 26190 | 27810 | 29850 | 32760 | 30840 |
| 1.5 | 9960 | 22770 | 29970 | 33260 |  |  |  |
| 2.0 | 10140 | 24570 | 33060 | 45480 |  |  |  |
| 3.0 | 11250 | 28380 |  |  |  |  |  |
| 4.0 | 12210 | 29580 |  |  |  |  |  |
| 5.0 | 13050 |  |  |  |  |  |  |

TABLE 430.-ALTERNATING-CURRENT POTENTIAL REQUIRED TO PRO. DUCE A SPARK IN AIR WITH VARIOUS BALL ELECTRODES

The potentials given are the maxima of the alternating waves used. Frequency, 33 cycles per second.

| Spark length <br> cm | $R=1 \mathrm{~cm}$ | $R=1.92$ | $R=5$ | $R=7.5$ | $R=10$ | $R=15$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| .08 | 3770 |  |  |  |  |  |
| .10 | 4400 | 4380 | 4330 | 4290 | 4245 | 4230 |
| .15 | 5990 | 5940 | 5830 | 5790 | 5800 | 5780 |
| .20 | 7510 | 7440 | 7340 | 7250 | 7320 | 7330 |
| .25 | 9045 | 8970 | 8850 | 8710 | 8760 | 8760 |
|  |  |  |  |  |  |  |
| .30 | 10480 | 10400 | 10270 | 10130 | 10180 | 10150 |
| .35 | 11980 | 11890 | 11670 | 11570 | 11610 | 11590 |
| .40 | 13360 | 13300 | 13100 | 12930 | 12980 | 12970 |
| .45 | 14770 | 14700 | 14400 | 14290 | 14330 | 14320 |
| .50 | 16140 | 16070 | 15890 | 15640 | 15690 | 15690 |
|  |  |  |  |  |  |  |
| .6 | 18700 | 18730 | 18550 | 18300 | 18350 | 18400 |
| .7 | 21350 | 21380 | 21140 | 20980 | 20990 | 21000 |
| .8 | 23820 | 24070 | 23740 | 23490 | 23540 | 23550 |
| .9 | 26190 | 26640 | 26400 | 26130 | 26110 | 26090 |
| 1.0 | 28380 | 29170 | 28950 | 28770 | 28680 | 28610 |
| 1.2 | 32400 | 34100 | 33790 | 33660 | 33640 | 33620 |
| 1.4 | 35850 | 38850 | 38850 | 38580 | 38620 | 38580 |
| 1.6 | 38750 | 43400 | 43570 | 43250 | 43520 |  |
| 1.8 | 40900 | - | 48300 | 47900 |  |  |
| 2.0 | 42950 | - | - | 52400 |  |  |

TABLE 431.-POTENTIAL NECESSARY TO PRODUCE A SPARK IN AIR BETWEEN MORE WIDELY SEPARATED ELECTRODES

|  |  | Steady $\underbrace{\text { potentials }}$ |  |  |  |  |  | Steady potentials <br> Ball electrodes |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Ball electrodes |  | Cup electrodes Projection |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  | $\begin{aligned} & R= \\ & 1 \mathrm{~cm} \end{aligned}$ | $\begin{gathered} R=\bar{c}= \\ 2.5 \mathrm{~cm} \end{gathered}$ | 4.5 mm | 1.5 mm |  |  | $R=$ | $R=$ |
|  |  |  |  |  |  |  |  | 1 cm | 2.5 cm |
| . 3 | - | - | - | - | 11280 | 6.0 | 61000 | - | 86830 |
| . 5 | - | 17610 | 17620 | - | 17420 | 7.0 | - | 52000 | - |
| . 7 | - | - | 23050 | - | 22950 | 8.0 | 67000 | 52400 | 90200 |
| 1.0 | 12000 | 30240 | 31390 | 31400 | 31260 | 10.0 | 73000 | 74300 | 91930 |
| 1.2 | - | 33800 | 36810 | - | 36700 | 12.0 | 82600 | - | 93300 |
| 1.5 | - | 37930 | 44310 | - | 44510 | 14.0 | 92000 | - | 94400 |
| 2.0 | 29200 | 42320 | 56000 | 56500 | 56530 | 15.0 |  | - | 94700 |
| 2.5 |  | 45000 | 65180 | - | 68720 | 16.0 | 101000 | - | 101000 |
| 3.0 | 40000 | 46710 | 71200 | 80400 | 81140 | 20.0 | 119000 |  |  |
| 3.5 | - | - | 75300 | - | 92400 | 25.0 | 140600 |  |  |
| 4.0 | 48500 | 49100 | 78600 | 101700 | 103800 | 30.0 | 165700 |  |  |
| 4.5 | - | - | 81540 | - | 114600 | 35.0 | 190900 |  |  |
| 5.0 | 56500 | 50310 | 83800 | - | 126500 |  |  |  |  |
| 5.5 | - | - | - | - | 135700 |  |  |  |  |



The specially constructed electrodes for the columns headed "cup electrodes" had the form of a projecting knob 3 cm in diameter and having a height of 4.5 mm and 1.5 mm respectively, attached to the plane face of the electrodes. These electrodes give a very satisfactory linear relation between the spark lengths and the voltage throughout the range studied.

TABLE 432.-EFFECT OF THE PRESSURE OF THE AIR ON THE DIELECTRIC STRENGTH

Voltages are given for different spark lengths $l$.

| Pressure, <br> cmHg | $l=0.04$ | $l=0.06$ | $l=0.08$ | $i=0.10$ | $l=0.20$ | $l=0.30$ | $i=0.40$ | $l=0.50$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | - | - | $\overline{-}$ | - | 744 | 939 | 1110 | 1266 |
| 4 | - | 483 | 567 | 648 | 1015 | 1350 | 1645 | 1915 |
| 6 | - | 582 | 690 | 795 | 1290 | 1740 | 2140 | 2505 |
| 10 | - | 771 | 933 | 1090 | 1840 | 2450 | 3015 | 3580 |
| 15 | - | 1060 | 1280 | 1490 | 2460 | 3300 | 4080 | 4850 |
| 25 | 1110 | 1420 | 1725 | 2040 | 3500 | 4800 | 6000 | 7120 |
| 35 | 1375 | 1820 | 2220 | 2615 | 4505 | 6270 | 7870 | 9340 |
| 45 | 1640 | 2150 | 2660 | 3120 | 5475 | 7650 | 9620 | 11420 |
| 55 | 1820 | 2420 | 3025 | 3610 | 6375 | 8950 | 11290 | 13455 |
| 65 | 2040 | 2720 | 3400 | 4060 | 7245 | 10210 | 12950 | 15470 |
| 75 | 2255 | 3035 | 3805 | 4565 | 8200 | 11570 | 14650 | 17450 |

TABLE 433.-POTENTIALS IN VOLTS TO PRODUCE A SPARK IN KEROSENE

| Spark <br> length cm | Electrodes balls of diam. $d$ |  |  |  | Spark length cm | Electrodes balls of diam. $d$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.5 cm | 1 cm | 2 cm | 3 cm |  | 0.5 cm | 1 cm | 2 cm | 3 cm |
| . 1 | 3800 | 3400 | 2750 | 2200 | . 5 | 13050 | 12400 | 11000 | 6900 |
| . 2 | 7503 | 6450 | 4800 | 3500 | . 6 | 14000 | 13550 | 12250 | 8250 |
| . 3 | 10250 | 9450 | 7450 | 4600 | . 8 | 15500 | 15100 | 13850 | 10450 |
| . 4 | 11750 | 10750 | 9100 | 5600 | 1.0 | 16750 | 16400 | 15250 | 12350 |

## TABLE 434.-DIELECTRIC STRENGTH OF MATERIALS

Potential necessary for puncture expressed in kilovolts per centimeter thickness of the dielectric

| Substance | Kilovolts per cm | Substance |  | ilovolts | Substance | Kilovolts per cm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ebonite | 300-1100 | Oils : | Thickness |  | Papers : |  |
| Empire cloth | 80-300 | Castor | . 2 mm | 190 | Beeswaxed | 770 |
| "" paper | 450 |  |  | 130 | Blotting | 150 |
|  | 20 | Cottonseed |  | 70 | Manilla | 25 |
| Fuller board | 200-300 | Lard | . 2 " | 140 | Paraffined | 500 |
| Glass | 300-1500 |  | 1.0 " | 40 | Varnished | 100-250 |
| Granite (fused)... | 90 | Linseed, raw | . 2 " | 185 | Paraffin: |  |
| Guttapercha ..... | 80-200 |  | 1.0 | 90 | Melted | 75 |
| Impregnated jute | ${ }_{30} 20$ | boiled | . 2 " | 190 80 | Solid ${ }^{\text {Melt. }} 43{ }^{\text {point }}$ |  |
| Leatheroid ....... | $30-60$ $100-200$ | Lubricating |  | 80 50 |  | 400 |
| Linen, varnished.. | $100-200$ $40-90$ | Lubricating Neatsfoot |  | 200 | $\begin{array}{ll}  & 47^{\circ} \\ & 52^{\circ} \end{array}$ | 230 |
| Liquid air ....... | 40-90 | Neatsfoot | $\begin{aligned} .2 \\ 1.0 \end{aligned}$ | 200 | " $70^{\circ}$ | 450 |
| Mica: ${ }_{\text {Madras }} \begin{aligned} & \text { Thickness } \\ & \\ & 1.1 \mathrm{~mm}\end{aligned}$ | 1600 | Olive | . 2 | 170 | Presspaper | 45-75 |
| " 1.0 " | 300 |  | 1.0 | 75 | Rubber | 160-500 |
| Bengal . 1 " | 2200 | Paraffin |  | 215 | Vaseline | 90-130 |
| " 1.0 " | 700 |  | 1.0 " | 160 | Xylene $\begin{gathered}\text { Thickness } \\ 2 \mathrm{~mm}\end{gathered}$ |  |
| Canada . 1 " | 1500 | Sperm, mineral | . 2 " | 180 |  | 80 |
| " 1.0 " | 500 |  | 1.0 " | 85 |  |  |
| South America. | 1500 | natural | . 2 " | 195 |  |  |
| Micanite | 400 | " " | 1.0 " | 90 |  |  |
|  |  | Turpentine | . 2 " | 160 |  |  |

TABLE 435.-DIELECTRIC CONSTANT (SPECIFIC INDUCTIVE CAPACITY) OF GASES

Atmospheric pressure
Wavelengths of the measuring current greater than 10000 cm

| Gas |  | Dielectric constant |  | Gas | ${ }^{\circ} \mathrm{C}$ | Dielectric constant |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ${ }^{\circ} \mathrm{C}$ | Vacuum = 1 | Air $=1$ |  |  | ${ }_{\text {Vacuum }}=1$ | Air $=1$ |
| Air | 0 | 1.000588 | 1.000000 | HCl | 100 | 1.00258 | 1.00199 |
| $\mathrm{NH}_{3}$ | 20 | 1.00718 | 1.00659 | $\mathrm{H}_{2}$ | 0 | 1.000264 | . 999676 |
| $\mathrm{CS}_{2}$ | 0 | 1.00290 | 1.00231 | CH 4 | 0 | 1.000948 | 1.000360 |
|  | 100 | 1.00239 | 1.00180 | $\mathrm{N}_{2} \mathrm{O}$ | 0 | 1.00108 | 1.00050 |
| $\mathrm{CO}_{2}$ | 0 | 1.000966 | 1.000377 | $\mathrm{SO}_{2}$ | 0 | 1.00993 | 1.00934 |
| CO | 0 | 1.000692 | 1.000104 | $\mathrm{H}_{2} \mathrm{O}, 4 \mathrm{~atm}$ | 145 | 1.00705 | 1.00646 |
| $\mathrm{C}_{2} \mathrm{H}_{4}$ | 0 | 1.00138 | 1.00079 |  |  |  |  |

## TABLE 436.-VARIATION OF THE DIELECTRIC CONSTANT WITH THE TEMPERATURE

If $\mathrm{K}_{0}=$ the dielectric constant at the temperature $\theta^{\circ} \mathrm{C}$ of the above table, $\mathrm{K}_{1}$ at the temperature $t^{\circ} \mathrm{C}$, and $\alpha$ and $\beta$ are quantities in the following table, then $\mathrm{K}_{t}=\mathrm{K}_{\theta}-a(t-\theta)$ $+\beta(t-\theta)^{2}$.

| Ammonia $\ldots \ldots \ldots \ldots \ldots . \ldots$ | $a=5.45 \times 10^{-8}$ | $\beta=2.59 \times 10^{-7}$ | Range, $15-110^{\circ} \mathrm{C}$ |
| :--- | :---: | :---: | :---: |
| Sulfur dioxide $\ldots \ldots \ldots \ldots \ldots$ | $6.19 \times 10^{-5}$ | $1.86 \times 10^{-7}$ | $0-110$ |
| Water vapor $\ldots \ldots \ldots \ldots \ldots$ | $1.4 \times 10^{-6}$ | $\cdots$ | 145 |

The dielectric constant of air at 76 cmHg and varying temperature may be calculated since $K-1$ is approximately proportional to the density. See Table 437.

TABLE 437.-VARIATION OF THE DIELECTRIC CONSTANT OF GASES WITH THE PRESSURE

|  | ${ }^{\circ} \mathrm{C}$ | Pressure atm |  |  | ${ }^{\circ} \mathrm{C}$ | Pressure atm |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Air | 19 | 20 | 1.0108 | Air | 11 | 120 | 1.0579 |
| " | , | 40 | 1.0218 |  | " | 140 | 1.0674 |
| " | " | 60 | 1.0330 | " | " | 160 | 1.0760 |
| " | " | 80 | 1.0439 | " |  | 180 | 1.0845 |
| " | " | 100 | 1.0548 | $\mathrm{CO}_{2}$ | 15 | 10 | 1.008 |
| " | 11 | 20 | 1.0101 | " | " | 20 | 1.020 |
| " | " | 40 | 1.0196 | " |  | 40 | 1.060 |
| " | " | 60 | 1.0294 | $\mathrm{N}_{2} \mathrm{O}$ | 15 | 10 | 1.010 |
| " | " | 80 | 1.0387 | " | 碞 | 20 | 1.025 |
| " | " | 100 | 1.0482 | " | " | 40 | 1.070 |

TABLE 438.-DIELECTRIC CONSTANT OF LIQUIDS (K). PRESSURE EFFECT ${ }^{148}$


[^183]A wavelength greater than 10000 cm is designated by $\infty$.

| Substance | ${ }^{\text {Temp. }} \mathrm{C}$. | Wave. length, cm | Dielectric constant | Substance | ${ }^{\text {Temp }}{ }_{\text {c }}{ }^{\text {cos }}$ | Wave. lengtb, cm | Dielectric constant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alcohol: |  |  |  | Ethyl ether | 100 | " | 3.12 |
| Amyl . | frozen | $\infty$ | 2.4 |  | 140 | " | 2.66 |
|  | -100 | " | 30.1 | " " | 180 | " | 2.12 |
| " | -50 | " | 23.0 |  |  |  |  |
| " | 0 | " | 17.4 |  | ${ }_{\text {crite }}^{\text {Crit. }}$ |  |  |
| " | +20 | " | 16.0 | " " | 192 | " | 1.53 |
| " | 18 | 200 | 10.8 | " ${ }^{\text {c }}$ | 18 | 83 | 4.35 |
| " | 18 | 73 | 4.7 | Formic acid | +2 | 73 | 19.0 |
| Ethyl | frozen | $\infty$ | 2.7 |  | (frozen) |  |  |
|  | -120 | " | 54.6 | " " | 15 | 1200 | 62.0 |
| " | -80 | " | 44.3 | " " | 16 | 73 | 58.5 |
| " | -40 | " | 35.3 | Glycerine | 15 | 1200 | 56.2 |
| " | 0 | " | 28.4 |  | 15 | 200 | 39.1 |
| " | +20 | " | 25.8 | " | 15 | 75 | 25.4 |
| " | 17 | 200 | 24.4 |  | - | 8.5 | 4.4 |
| " |  | 75 | 23.0 | " |  | . 4 | 2.6 |
| " | " | 53 | 20.6 | Hexane | 17 | $\infty$ | 1.880 |
| " | " | 4 | 8.8 | Hydrogen p | 18 | 75 | 84.7 |
| Methyi | frozen | $\infty$ | 3.07 | Kerosene |  | $\bar{\infty}$ | . 2 |
|  | -100 | " | 58.0 | Meta-xylene | 18 | $\infty$ | 237 |
| " | -50 | $\cdots$ | 45.3 |  | 17 | 73 | 2.37 |
| " | 0 | " | 35.0 |  | (rozen) |  |  |
| " | $+20$ | " | 31.2 | Nitrobenzol | -10 | ¢ | 9.9 |
| " | 17 | 75 | 33.2 |  | -5 |  | 42.0 |
| Propyl | -120 | \% | 46.2 | " | 15 |  | 41.0 |
|  | -60 | " | 33.7 | " | +15 | " | 37.8 |
| " | 0 | " | 24.8 | " | 30 | " | 35.1 |
| " ${ }^{\prime}$ | $+20$ | 7 | 22.2 | " | 18 |  | 36.45 |
| Aceton | 15 | 75 | 12.3 | " | 17 | 73 | 34.0 |
| Acetone | -80 | $\infty$ | 33.8 | Octane | 17 | $\infty$ | 1.949 |
|  | 0 | " | 26.6 | Oils: |  |  |  |
| " | 15 | 1200 | 21.85 | Almond | 20 | $\infty$ | 2.83 |
| Actic acid | 17 | 73 | 20.7 | Castor | 11 | " | 4.67 |
| Acetic acid | 18 | $\infty$ | 9.7 | Colza | 20 | " | 3.11 |
|  | 15 | 1200 | 10.3 | Cottonseed | 14 | " | 3.10 |
| "" " | 17 | 200 | 7.07 | Lemon | 21 | " | 2.25 |
| " " . | 19 | 75 | 6.29 | Linseed | 13 | " | 3.35 |
| Amyl acetate | 19 | $\infty$ | 4.81 | Neatsfoot |  | " | 3.02 |
| Amylene ... | 16 | " | 2.20 | Olive | 20 | " | 3.11 |
| Aniline | 18 | $\infty$ | 7.316 | Peanut | 11.4 | " | 3.03 |
| Benzol (benzene) | 18 | " | 2.288 | Petroleum | - | 2000 | 2.13 |
|  | 19 | 73 | 2.26 | Petroleum | 20 | $\infty$ | 1.92 |
| Bromine | 23 | 84 | 3.18 | Rape seed | 16 | " | 2.85 |
| Carbon bisulfide | 20 | - | 2.626 | Sesame | 13.4 | " | 3.02 |
| " " | 17 | 73 | 2.64 | Sperm | 20 | " | 3.17 |
| Chloroform | 18 | $\infty$ | 5.2 | Turpentine | 20 | " | 2.23 |
| Decane | 17 | 73 | 4.95 | Vaseline |  |  | 2.17 |
| Decylene | 14 | - | 2.24 | Phenol | -83 | $\infty$ | 2.68 |
| Ethyl ether | -80 | $\infty$ | 7.05 | " | +16 | " | 2.33 |
| " ${ }^{\text {c }}$ | -40 | " | 5.67 | " | 19 | 73 | 2.31 |
| " " | 0 | " | 4.68 | Water | 18 | $\infty$ | 81.07 |
| " " | 18 | " | 4.368 | (for temp. | 17 | 200 | 80.6 |
| " " | 20 | " | 4.30 | see Table | 17 | 74 | 81.7 |
| " " . | 60 | " | 3.65 |  | 17 | 38 | 83.6 |

Temperature coefficients of the formula ： $\mathrm{K}_{\theta}=\mathrm{K}_{t}\left[1-a(t-\theta)+\beta(t-\theta)^{2}\right]$

| Substance | a | $\beta$ | $\begin{aligned} & \text { Temp. } \\ & \text { range, }{ }^{\circ} \mathrm{C} \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Amyl acetate | ． 0024 | － | － |
| Aniline ．．．．． | ． 00351 |  |  |
| Benzene | ． 00106 | ． 0000087 | 10－40 |
| Carbon bisulfide | ． 0000966 | ． 00000060 | 20－181 |
| Chloroform | ． 00410 | ． 000015 | 22－181 |
| Ethyl ether | ． 00459 | － |  |
| Methyl alcohol | ． 0057 |  |  |
| Oils：Almond | ． 00163 | ． 000026 |  |
| Castor | ． 01067 | － | － |
| Olive．．． | ． 00364 |  | － |
| Paraffin | ． 000738 | ． 0000072 |  |
| Toluene | ． 000921 |  | $\begin{gathered} 0-13 \\ 20-181 \end{gathered}$ |
| Water | ． 004474 |  | 5－20 |
| ＂ | ． 004583 | ． 0000117 | 0－76 |
| ＂Meta－xylene | ． 004366 | －－ | $4-25$ $20-181$ |

TABLE 441．－DIELECTRIC CONSTANT OF LIQUEFIED GASES
A wavelength greater than 10000 cm is designated by $\infty$ ．

|  |  | 5 |  |  |  |  | $E$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Substance | ${ }^{\text {Temp．}}{ }^{\text {C }}$ ． |  | Dielectric constant | Substance |  | ${ }^{\text {Temp．}}{ }^{\text {c }}$ |  | Dielectric constant |
| Air | －191 | $\begin{aligned} & \infty \\ & 75 \end{aligned}$ | $\begin{gathered} 1.43_{2} \\ 1.47-1.50 \end{gathered}$ | Nitrous oxide |  |  |  |  |
| Ammonia | －34 | 75 | 21－23 |  | $\mathrm{N}_{2} \mathrm{O}$ | －88 | $\infty$ | $1.93{ }^{3}$ |
|  | 14 | 130 | 16.2 | ＂＂ |  | －5 | ＂ | 1.63. |
| Carbon dioxide | －5 | $\infty$ | 1.608 | ＂ |  | ＋5 | ＂ | $1.57{ }^{3}$ |
|  | 0 | ＂ | 1.58 | －＂ |  | ＋15 | ＂ | 1.520 |
| ＂ | +10 +15 | ＂ | $1.54{ }^{\circ}$ | Oxygen |  | －182 | ＂ | $1.49{ }_{1}$ $1.46{ }^{\text {a }}$ |
| Chlorine | ＋60 | ＂ | 2.15 。 | Sulfur dioxide |  | 14.5 | 120 | 13.75 |
|  | －20 | ＂＂ | 2.03 。 |  |  | 20 | $\stackrel{\infty}{ }$ | 14.0 |
| ＂ | 0 | ＂ | 1.97 。 | ＂＂ |  | 40 | ＂ | 12.5 |
| ＂ | ＋10 | ＂ | $1.94{ }^{\circ}$ | ＂＂＂ |  | 60 | ＂ | 10.8 |
| ＂ | 0 | ＂ | 2.08 | ＂＂ |  | 80 | ＂ | 9.2 |
| ＂． | ＋14 | 100 | 1.88 | ＂＂ |  | 100 | ＂ | 7.8 |
| Cyanogen | 23 | 84 | 2.52 | ＂＂ |  | 120 | ＂ | 6.4 |
| Hydrocyanic acid | 21 | ＂ | about 95 | ＂＂ |  | 140 | ＂ | 4.8 |
| Hydrogen sulfide | 10 | $\cdots$ | 5.93 | Critical |  | 154.2 | ＂ | 2.1 |
| ＂＂ | 50 | ＂، | 4.92 |  |  |  |  |  |
|  | 90 | ＂ | 3.76 |  |  |  |  |  |

TABLE 442．－DIELECTRIC CONSTANT OF ROCKS＊

| Material | Wave length， m | Dielectric constant， range | Material |  | Wave． length， cm | Dielectric constant， range |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Chalk， middle Devonian |  |  | Limestone |  |  | 8．0－12．0 |
|  |  | 8．0－9．0 | Marmorized | limestone | $3 \times 10$ | 15.2 |
| Coral dolomite |  | 8．0－9．0 | Mica schist |  |  | 16．0－17．0 |
| Granite |  | 7．0－9．0 | Sandstone， | variegated |  | $9.0-11.0$ |

[^184]

## TABLE 444.-ELECTROSTRICTION*

Electrostriction is a change in the dimensions of a dielectric proportional to the square of an applied electric field. The effect is very small except for bodies of very high dielectric constant or high mechanical compliance.n,

> Typical values for-

| Glasses | Rubber | Barium titanate <br> polycrystalline |
| :---: | :---: | :---: |
| 0.1 to $0.7 \times 10^{-12}$ | $7 \times 10^{-0}$ | $100 \times 10^{-9} \mathrm{~cm}^{2} /$ statvolt |
| transverse | longitudinal | longitudinal |

[^185]TABLE 445.-STANDARD SOLUTIONS FOR THE CALIBRATION OF APPARATUS FOR THE MEASURING OF DIELECTRIC CONSTANT


TABLE 446.-DIELECTRIC CONSTANT OF MINERALS *

| Material | Wavelength, cm | Range | Dielectric constant |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | - axis | \|| axis |
| Asphalt |  | 2.7 |  |  |
| Beryl | $\infty$ |  | 7.85 | 6.05 |
| Coal, anthracite | . | 5.6-6.3 | ... | ... |
| Fluorite . ... |  | 6.8 | . . | $\ldots$ |
| Glass, flint ex. heavy |  | 9.9 | ... |  |
| Glass, hard crown . |  | 7.0 | ... | ... |
| Glass, Jena barium |  | 7.8-8.5 | ... | ... |
| Glass, lead (Powell) |  | 5.4-8.0 | . . . | ... |
| Gypsum ${ }^{\circ}$. |  | 6.3 | . . | ... |
| Ice $\left(-2^{\circ} \mathrm{C}\right)$ |  | 93.9 |  |  |
| Iceland spar .... | . 75 |  | 8.50 | 8.00 |
| Quartz, fused ... |  | 3.5-3.6 | . . . | . . . |
| Sulfur, amorphous | . . . . . | 3.9 |  |  |

*For reference, see footnote 45, p. 136.

## TABLE 447.-THE DIELECTRIC PROPERTIES OF NONCONDUCTORS

Results of tests at unit area and unit thickness of dielectric

| At 1000 cycles | Mica | Paper | Celluloid | Ice |
| :---: | :---: | :---: | :---: | :---: |
| Max. breakdown volts per cm. | $1.06 \times 10^{6}$ | $.71 \times 10^{6}$ | $1.05 \times 10^{8}$ | . $001 \times 10^{3}$ |
| Specific induc. capacity. | 4.00 | 4.90 | 13.26 | 86.40 |
| Max. absorbable energy, watts-sec/ $\mathrm{cm}^{8}$. | . 198 | . 108 | . 640 | . 00040 |
| $90^{\circ}$-angle of lead. . . . . . . . | $0^{\circ} 57^{\prime}$ | $2^{\circ} 10^{\prime}$ | $3^{\circ} 40^{\prime}$ | $13^{\circ} 39^{\prime}$ |
| Equiv. resistance (ohm-cm) $\times 10^{11}$ | 3.91 | 9.84 | 48.3 | 1400 |
| Conductivity, $1 /(\mathrm{ohm}-\mathrm{cm}) \times 10^{-10}$ | 2.56 | 1.02 | . 207 | . 00722 |
| Percent change in cap. per cycle $\times 10^{4}$. | 2.18 | 14.31 | 30.7 | 70.0 |
| Percent change in resistance per cycle.. | . 258 | . 146 | . 106 | . 127 |
| At 15 cycles |  |  |  |  |
| Specific inductive capacity | 4.09 | 5.77 | 18.60 | 429.0 |
| Max. absorbable energy, watt-sec/ $\mathrm{cm}^{8}$. . | . 203 | . 126 | . 90 | . 002 |
| Percent change in capacity per cycle... | . 00 | . 306 | 1.74 | 1.59 |
| On direct current Conductivity, $1 /($ ohm -cm$)$ | $2.42 \times 10^{-17}$ | $2.27 \times 10^{-14}$ | $71.5 \times 10^{-14}$ | $163.10^{-11}$ |

TABLE 448.-VALUES OF DIELECTRIC CONSTANT FOR SEVERAL ELECTRIC INSULATING MATERIALS AT RADIO FREQUENCIES

| Material | $\begin{gathered} \text { Frequency } \\ \mathrm{kc} \end{gathered}$ | Dielectric constant | Material | $\begin{aligned} & \text { Frequency } \\ & \text { kc } \end{aligned}$ | Dielectric constant |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Glass | 30 | 5.1-7.9 | Phenolic insulation: |  |  |
| cobalt | 500 | 7.3 | laminated ..... | 190 | 5.0-7.4 |
| crown | 230 | 6.3 |  | 1000 | 4.7-7.0 |
|  | 800 | 6.2 | molded | 190 | 4.3-7.6 |
| flint | 500 | 7.0 |  | 1000 | 4.9-7.0 |
|  | 890 | 7.0 | Rubber, hard ...... | 135 | 3.7 |
| photographic | 100 | 7.5 |  | 210 |  |
|  | 1700 | 7.4 |  | 1126 | 3.0-3.7 |
| plate | 500 | 6.8-7.6 | Wood: |  |  |
| Pyrex | 30 | 4.8 | bay | 870 | 3.8 |
|  | 500 | 4.9-5.8 | birch ......... | 500 | 5.2 |
| Marble | 44 | 8.4 | maple ........ | 500 | 4.4 |
|  | 80-650 | 9.2-11.7* | oak . | 300 | 3.1 t-6.7 |
|  | 1400 | 7.3 |  | 425 |  |
| Mica | 100-1000 | 5.8-8.7 |  | 635 | $3.0{ }^{\dagger}-6.5$ |
|  |  |  |  | 1060 | 3.3 |

* Range of 10 samples of various kinds of marble.
$\dagger$ After drying sample for 48 hours at $80^{\circ} \mathrm{C}$.


## TABLE 449.-COMPARISON OF ELECTRICAL PROPERTIES OF INSULATING MATERIALS AT ROOM TEMPERATURE **

| Material | Intrinsic dielectric strength |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { Thickness } \\ (\mathrm{mm}) \end{gathered}$ | ( $\mathrm{Kv} / \mathrm{cm}$ ) | Dielectric constant | resistivity <br> (ohm-cm) |
| Cellulose acetate | .025-. 12 | $2300 \dagger$ | 5.5 | $10^{18}$ |
| Glass : |  |  |  |  |
| borosilicate No. 7740 (Pyrex) | . 10 | 4800* | 4.8 | $10^{18}$ |
| soda lead ............ | . 10 | 3100** | 8.2 | $10^{14}$ |
| soda lime |  | 4500* | 7.0 | $10^{18}$ |
| Mica, muscovite clear ruby | .020-. 10 | 3000-8200† | 7.3 | $10^{17}$ |
| Phenolic resin | .012-. 04 | 2600-3300 $\dagger$ | 7.5 | $10^{11}$ |
| Porcelain, electrical | - | $380 \dagger$ | 4.4-6.8 | $10^{24}$ |
| Porcelain, steatite-low loss |  | $500 \dagger$ | 6.0-6.5 | $10^{15}$ |
| Silica, fused |  | 5000* | 3.5 | $10^{18}$ |
| Rubber, hard | . $10-.30$ | $2150 \dagger$ | 2.8 | $10^{18}$ |

[^186]Intrinsic dielectric strength can be realized only under test conditions and is very much higher than the working dielectric strength attainable in ordinary service. These data are listed for purposes of comparison.

```
cgs system, \(K_{\text {vacuum }}=1\)
```

The dielectric constants, $\dagger K$, given here have usually been determined at low field strength (order of $1 \mathrm{volt} / \mathrm{cm}$ ). Unless specifically noted, the frequency is between 60 cycles $/ \mathrm{sec}$ and 5 megacycles/sec. Homogeneous crystals show little dispersion in this frequency range unless they are strongly piezoelectric or have very high dielectric constant. For some strongly piezoelectric crystals, the notation "free" appears in the frequency column. Dielectric constants so noted hold for the mechanically unconstrained condition which is usually fulfilled for frequencies below the principal mechanical resonances of the test body. The dielectric constants for the "clamped" crystal are smaller than for the "free" crystal. The difference does not exceed 10 percent except for $K_{a}$ of Rochelle salt (see fig. 16) and $K \|$ of barium titanate.
$K_{a}, K_{b}$, and $K_{0}$ for orthorhombic crystals refer to electric field parallel to the crystallographic $a, b$, and $c$ axes.

For monoclinic crystals, $K_{b}$ refers to electric field parallel to the $b$ axis which is the symmetry axis; $K_{c}$ to field parallel to the $c$ axis accepted by crystallographic convention; and $K_{z}$ to an electric field perpendicular to the $b$ and $c$ axes.

[^187]
## Cubic crystals

| Name | Composition | K | Author. ity ${ }^{148}$ | Name | Composition | K | Author ity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Silver chloride | AgCl | 12.3 | g | Sphalerite | ZnS | 8.8 | e |
| Silver bromide | AgBr | 13.1 | g | Sodium chlorate | $\mathrm{NaClO}_{3}$ | 5.7 | h |
| Lithium fluoride .. | LiF | 9.00 | f | Sodium bromate | $\mathrm{NaBrO}_{3}$ | 5.7 | h |
| Sodium chloride .. | NaCl | 5.90 |  | Magnesium oxide | MgO | 9.65 | f |
| Potassium chloride | KCl | 4.68 | g | Potassium bromide | KBr | 4.90 | f |
| Barium oxide .... | BaO | 34. | 0 | Thallium chloride. | TlCl | 31.1 | $g$ |

Uniaxial crystals

| Name | Composition | $K \perp$ | K \\| | Frequency | Authority |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Quartz | . $\mathrm{SiO}_{2}$ | 4.5 | 4.6 |  | b |
| Calcite | $\mathrm{CaCO}_{3}$ | 8.78 | 8.29 |  | g |
| Sapphire | .. $\mathrm{Al}_{2} \mathrm{O}_{3} \ddagger$ | 8.6 | 10.5 | $10^{2}-10^{7}$ | f |
| Rutile | . $\mathrm{TiO}_{2} \ddagger$ | 86 | 170 | $10^{5}-10^{\text {a }}$ | f |
| Barium titanate | . $\mathrm{BaTiO}_{3}$ | 4400 | 200 | ? $-10^{7}$ | i |
| Tourmaline |  | 8.2 | 7.5 |  | h |
| Magnesite | . $\mathrm{MgCO}_{3}$ | 6.91 | 8.1 |  | g |
| Dihydrogen phosphates and arsenates: |  |  |  |  |  |
| "ADP" ... | $\mathrm{NH}_{4} \mathrm{H}_{2} \mathrm{P}$ | 56 | 15.4 | free |  |
| "KDP" | . $\mathrm{KH}_{2} \mathrm{PO}_{4}$ | 46 | 22 | free | h |
| "ADA" | . $\mathrm{NH}_{4} \mathrm{H}_{2} \mathrm{~A}$ | 75 | 14 | free | d |
| "KDA" | $\mathrm{KH}_{2} \mathrm{AsO}$ | 52 | 22 | free | d |

Orthorhombic crystals


[^188](continued)

TABLE 450.-DIELECTRIC CONSTANT OF CRYSTALS (concluded)

| Name | Composition $\mathrm{Ka}_{\mathrm{a}}$ | Kı | $K_{\text {c }}$ | Frequency | Authority |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Tartrates: |  |  |  |  |  |
| Rochelle salt | $\mathrm{NaKC} \mathrm{H}_{4} \mathrm{O}_{6} \cdot 4 \mathrm{H}_{2} \mathrm{O} \quad 8.0$ |  |  | $2.5 \times 10^{10}$ | h |
| " " $30^{\circ} \mathrm{C}{ }^{8}$. | 300 | 9.4 | 9.6 | free | c, j |
|  | $\mathrm{NaNH}_{4} \mathrm{C}_{4} \mathrm{H}_{4} \mathrm{O}_{6} \cdot 4 \mathrm{H}_{2} \mathrm{O} 9.0$ | 8.9 | 10.0 | free | h |
|  | $\mathrm{LiKC}_{4} \mathrm{H}_{4} \mathrm{O}_{8} \cdot \mathrm{H}_{2} \mathrm{O} \quad 5.84$ | 7.32 | 7.4 | free | h |
|  | $\mathrm{LiNH}_{4} \mathrm{C}_{4} \mathrm{H}_{4} \mathrm{O}_{6} \cdot \mathrm{H}_{2} \mathrm{O} \quad 7.2$ | 8.0 | 6.9 | free | h |

Monoclinic crystals

| Lithium sulfate | $\mathrm{Li}_{2} \mathrm{SO}_{4} \cdot \mathrm{H}_{2} \mathrm{O}$ | 5.6 | 10.3 | 6.5 | free | h |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tartaric acid | $\mathrm{C}_{4} \mathrm{H}_{4} \mathrm{O}_{8}$ | 4.3 | 4.3 | 4.5 | free |  |
| Potassium tartrate | $\mathrm{K}_{2} \mathrm{C}_{4} \mathrm{H}_{4} \mathrm{O}_{6} \cdot \frac{1}{2} \mathrm{H}_{2} \mathrm{O}$ | 6.44 | 5.80 | 6.49 | free |  |
| Ammonium tartrate | $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{C}_{4} \mathrm{H}_{4} \mathrm{O}_{6}$ | 6.45 | 8.2 | 6.0 | free | h |
| Ethylene diamine tartrate (EDT) | $\mathrm{C}_{2} \mathrm{~N}_{2} \mathrm{H}_{8} \cdot \mathrm{C}_{4} \mathrm{H}_{8} \mathrm{O}_{8}$ | 5.0 | 8.22 | 6.0 | free | h |

References: a, Bechmann, K., and Lynch, A. C., Nature, vol. 163, p. 915, 1949. b, Cady, W. G., Piezoelectricity, McGraw-Hill, New York, 1946. c, Hablüzel, J., Helvet. Phys. Acta, vol. 12, p. 489, 1939. d, Jaffe, H., The Brush Development Co. Report to U.S. Signal Corps on synthetic watersoluble piezoelectric crystals, April 1, 1948 . e, Jaffe, H., personal communication. f, Laboratory for Insulation Research, Massachusetts Inst. Techn. Tables of Dielectric Materials III, 1948; and personal communication. g, Landolt Börnstein Tables, 5th ed. h, Mason, W. P., Piezoelectric crýstals and their application to ultrasonics, Van Nostrand Co., New York, 1950 . i, Merz, W. J., Phys. Rev., vol. 75, p. 687, $1949 .{ }^{2}$, Mueller, H., Phys. Rev., vol. 47, p. 175, 1935 ; vol. 58, p. $5655^{\prime}, 1940$. k, Naval Research Laboratory, Crystal Section. 1,' Spitzer,' F., Dissertation, Göttingen, 1938. m, Standards on piezoelectric crystals, Proc. Inst. Radio Eng., vol. 37, p. 1378, 1949. n, International Critical Tables, vol. $6 . \quad$ o, Bever and Sproul, Phys. Rev., vol. 53, p. 801, 1951.


Fig. 16.-Dielectric constant $K_{a}$ of Rochelle salt. Curve A: free condition (audio frequency); curve B: clamped condition (radio frequency).

In this table are listed piczoelectric strain coefficients $* d_{n m}$ which are ratios of piezoelectric polarization components to components of applied stress at constant electric field (direct piezoelectric effect) and also ratios between piezoelectric strain components to applied electric field components at constant mechanical stress (converse effect). The subscripts $\mathrm{n}=1$ to 3 indicate electric field components, $\mathrm{m}=1$ to 6 mechanical stress or strain components. These components are referred to orthogonal coordinate axes. For correlation of these to crystallographic axes, we follow Standards on Piezoelectric Crystals. ${ }^{\text {m }}$
In the monoclinic system, indices 2 and 5 refer to the symmetry (b) axis, in distinction from the older convention ${ }^{\circ}$ relating indices 3 and 6 to the symmetry axis. Crystal classes are designated by international (Hermanr-Mauguin) symbols. A dot in place of a coefficient indicates that it is equal by symmetry from another listed coefficient; a blank space indicates that the coefficient is zero by symmetry. If the sign of a coefficient is not given it is unknown, not necessarily positive.

$$
\begin{aligned}
\text { Unit for } \begin{aligned}
d_{n m} & =10^{-8} \text { statcoulomb } / \text { dyne }=\frac{1}{3} \times 10^{-12} \text { coulomb } / \text { newton } \\
& =10^{-8} \mathrm{~cm} / \text { statvolt }=\frac{1}{3} \times 10^{-12} \text { meter } / \mathrm{volt}
\end{aligned}
\end{aligned}
$$

[^189]
## Cubic and tetragonal crystals

| Name | Composition | Class | $d_{14}$ | $d_{38}$ | Authority ${ }^{149}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Sphalerite | ZnS | 43 m | 9.7 | . | b |
| Sodium chlorate | $\mathrm{NaClO}_{3}$ | 23 | 5.2 | - | 1 |
| Sodium bromate | $\mathrm{NaBrO}_{3}$ | 23 | 7.3 | - | 1 |
| "ADP" | $\mathrm{NH}_{4} \mathrm{H}_{2} \mathrm{PO}$ | 42m | $-1.5$ | $+48.0$ | d |
| "KDP" | $\mathrm{K} \mathrm{H}_{2} \mathrm{PO}_{4}$ | 42 m | $+1.3$ | $+21$ | e |
| "ADA" | $\mathrm{NH}_{4} \mathrm{H}_{2} \mathrm{AsO}_{4}$ | $\overline{42} \mathrm{~m}$ | +41 | $+31$ | d |
| "KDA" . | $\mathrm{K} \mathrm{H}_{2} \mathrm{AsO}_{4}$ | $\overline{42} \mathrm{~m}$ | $+23.5$ | $+22$ | d |

Trigonal crystals

| Name | Class | $d_{11}$ | $d_{14}$ | $d_{15}$ | $d_{22}$ | $d_{31}$ | $d_{33}$ | Authority |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Quartz | 32 | +6.9 | -2.0 |  |  |  |  | b |
| Tourmaline | 3 m |  |  | +11.0 | -. 94 | +. 96 | +5.4 | b |

Orthorhombic crystals


Monoclinic crystals (Class 2)


Polarized polycrystalline substance


## TABLE 452.-VALUES FOR POWER FACTOR IN PERCENT FOR SEVERAL ELECTRICAL INSULATING MATERIALS AT RADIO FREQUENCIES

From the range of values given, an approximate figure can be taken for a particular material and its relative position with respect to other materials seen. Data of this kind are much affected by the condition and past treatment of the samples and by the conditions of the tests. The power factor and dielectric constant of dry air may be taken as 0 and 1.00 . Fused quartz has the lowest power factor among the solid insulating materials, and is used for supporting the insulated plates of standard air condensers.

| Material | Frequency | Power factor | Material | Frequency | Power factor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Amber | 187.5 | . 459 | Paraffin | 14 | . 042 |
|  | 300 | . 476 |  | 100 | .017- . 031 |
|  | 600 | . 495 |  | 500 | . 026 |
|  | 1000 | . 514 |  | 1070 | . 034 |
| Glass .... | 30 | . $35-2.98 *$ | Phenolic |  |  |
|  | 600 | . $040-.653^{\dagger}$ | insulation : |  |  |
|  | 500 | . 70 | laminated $\\|$. | 190 | $2.62-8.0$ |
|  | 500 | . 42 |  | 1000 | $3.85-6.65$ |
|  | 890 | . 40 | molded II | 190 | $1.64-10.9$ |
| photographic | 100 | . 95 |  | 1000 | 1.56-8.4 |
|  | 235 | . 86 | Rubber, hard | 135 | . 68 |
|  | 1700 | . 77 |  | 315 | . 70 |
| plate | 14 | . 97 |  | 600 | . 62 |
|  | 100 | . $77-.93$ |  | 625 | . 70 |
|  | 500 | . $66-.70$ |  | 710 | . 88 |
|  | 635 | . 82 |  | 1000 | . 68 |
|  | 1000 | . 62 |  | 1085 | . 74 |
| Pyrex | 14 | . 88 |  | 1126 | 1.05 |
|  | 30 | . $26-.56$ | Wood: |  |  |
|  | 100 | . $58-.74$ | bay ....... | 870 | 3.76 |
|  | 420 | . 50 | birch | 500 | 6.48 |
|  | 500 | . 42 - . 67 | maple | 500 | $3.33-3.63$ |
|  | 750 | . 68 | oak | 300 | 2.94โ-13.8 |
| Marble | 80-650 | . $35-4.72 \ddagger$ |  | 635 | 3.241-10.1 |
| Mica .......... | 600 | .007-. 938 |  | 1060 | 4.20 |

[^190]Antenna arrays (figs. 17-19).-The basis for all directivity control in antenna arrays is wave interference. By providing a large number of sources of radiation, it is possible with a fixed amount of power greatly to reinforce radiation in a desired direction by suppressing the radiation in undesired directions. The individual sources may be any type of antenna.

The radiation patterns of several common types of individual elements are shown in figure 17. The expressions hold for linear radiators, rhombics, vees, horn radiators, or other complex antennas when combined into arrays, provided a suitable expression is used for $A$, the radiation pattern of the individual

| type of rodialor | current distribution | $\qquad$ <br> horizontd $F(\theta)$ | verical |
| :---: | :---: | :---: | :---: |
| Hall-wave dipole |  | $\begin{aligned} & F(\theta)= \\ & K \frac{\cos \left(\frac{\pi}{2} \sin 0\right)}{\cos \theta} \\ & \cong K \cos \theta \end{aligned}$ | $F(\beta)=K(1)$ |
| Shortened dipole |  | $F(\theta) \cong K \cos \theta$ | $F(\beta)=K(1)$ |
| Lengthened dipole |  | $\begin{aligned} & F(\theta)= \\ & K\left[\frac{\cos \left(\frac{\pi i}{\lambda} \sin \theta\right)-\cos \frac{\pi}{\lambda}}{\cos \theta}\right] \end{aligned}$ | $F(\beta)=K(1)$ |
| Horizontal loop |  | $F(\theta) \cong K(1)$ | $F(\beta)=K \cos \beta$ |
| Horizontal turnstile | $i_{1}$ and $i_{2}$ phosed $90^{\circ}$ | $F(\theta) \cong K^{\prime}(1)$ | $F(\beta) \cong K^{\prime}(1)$ |
| $\theta=$ horizontol angle measured from perpendicular bisecting plone |  |  |  |
| $\beta=$ vertical ongle measured from horizon |  |  |  |
| $K$ and $K^{\prime}$ ore constonts and $K^{\prime} \cong 0.7 K$ |  |  |  |

Fig. 17.-Radiation patterns of several common types of antennas.
antenna. The array expressions are multiplying factors. Starting with an individual antenna having a radiation pattern given by $A$, the result of combining it with similar antennas is obtained by multiplying $A$ by a suitable array factor, thus obtaining an $A^{\prime}$ for the group. The group may then be treated as a single source of radiation. The result of combining the group with similar groups, or, for instance, of placing the group above ground, is obtained by multiplying $A^{\prime}$ by another of the array factors given.

The expressions given here assume negligible mutual coupling between individual antennas. When coupling is not negligible, the expressions apply only if the feeding is adjusted to overcome the coupling and thus produce resultant currents that are of the amplitude and relative phases indicated.

[^191]One of the most important arrays is the linear multielement array where a large number of equally spaced antenna elements are fed equal currents in phase to obtain maximum directivity in the forward direction. Figure 18 gives expressions for the radiation pattern of several particular cases and the general case of any number of broadside elements.

In this type of array a great deal of directivity may be obtained. A large number of minor lobes, however, are apt to be present, and they may be undesirable under some conditions, in which case a type called the binomial array may be used. Here again all the radiators are fed in phase but the current is not distributed equally among the array elements, the center radiators in the array


Fig. 18.-Linear multielement array broadside directivity.
being fed more current than the outer ones. Figure 19 shows the configuration and general expression for such an array. In this case the configuration is made for a vertical stack of loop antennas in order to obtain single-lobe directivity in the vertical plane. If such an array were desired in the horizontal plane, say $n$ dipoles end to end, with the specified current distribution the expression would be

$$
\mathrm{F}(\theta)=2^{\mathrm{n}-1}\left[\frac{\cos \pi / 2 \sin \theta}{\cos \theta}\right] \cos ^{\mathrm{n}-1}\left(1 / 2 \mathrm{~S}^{\circ} \sin \theta\right)
$$

The term binomial results from the fact that the current intensity in the successive array elements is in accordance with the binomial expansion $(1+1)^{\mathrm{n}-1}$, where $n$ is the number of elements.
cos $\beta[1]$

Fig. 19.-Development of binomial array.

TABLE 453.-DIELECTRIC CONSTANT OF NONPOLAR GASES ${ }^{150}$
at $0^{\circ} \mathrm{C}$ and 76 cmHg

| Gas | $(\mathrm{K}-1) \times 10^{8}$ | Gas | $(\mathrm{K}-1) \times 10^{6}$ | Gas $\quad(\mathrm{K}-1) \times 10^{0}$ |
| :---: | :---: | :---: | :---: | :---: |
| Helium | 69.2 | Hydrogen | 272 | Carbon dioxide. . 988 |
| Neon | 134.1 | Oxygen | 532.5 | Air ( $\mathrm{CO}_{2}$ free). . 570 |
| Argon | 554.2 | Nitrogen | . 580 |  |

[^192]TABLE 454.-DIELECTRIC CONSTANT AND LOSS TANGENT OF DIELECTRIC MATERIALS ${ }^{131}$
The following table presents values of dielectric constant, ${ }^{2} \epsilon^{\prime}$ (relative to that vacuum $\epsilon_{0}$ ) and loss tangent, $\tan \delta$, for various substances at the frequencies and temperatures indicated. The loss tangent, $\tan \delta$, is identical with the power factor, $\cos \theta$ (or $\sin \delta$ ), for low loss substances. The table shows it multiplied by $10^{4}$.

Part 1.—Solids

| Materials <br> A. Inorganic | ${ }^{\text {Temp }}$ C | Frequency, cycles per second |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $1 \times 10^{2}$ |  | $1 \times 10^{3}$ | $1 \times 10^{0}$ | $1 \times 10^{8}$ | $1 \times 10^{10}$ |
| 1. Crystals $-12 \epsilon^{\prime} / \epsilon_{0}{ }^{\text {IT* }}$ |  |  |  |  |  |  |  |
|  | -12 | $\begin{gathered} \epsilon^{\prime} / \epsilon_{0} \\ \tan \delta \end{gathered}$ |  |  |  | $\begin{aligned} & 4.15 \\ & 1200 \end{aligned}$ |  | $\begin{array}{r} 3.17 \\ 7 \end{array}$ |
| Sodium chloride ${ }^{2}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 5.90 | 5.90 | 5.90 |  | 5.90 |
|  |  | $\tan \delta$ | <1 | <1 | <2 |  | 5 |
| 2. Ceramics |  |  |  |  |  |  |  |
| a. Steatite bodies AlSiMag $211^{3}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 6.00 | 5.98 | 5.97 | 5.96 | 5.90 |
|  |  | $\tan \delta$ | 92 | 34 | 5 | 4 | 14 |
| b. Miscellaneous Ruby mica ${ }^{4}$ | 26 | $\begin{aligned} & \epsilon^{\prime} / \epsilon_{0} \\ & \tan \delta \end{aligned}$ | $\begin{aligned} & 5.4 \\ & 25 \end{aligned}$ | $5.4$ | $5.4$ | 5.4 |  |
| Mycalex K $10{ }^{5}$ | 24 | $\epsilon^{\prime} / \epsilon_{0}$ | 9.5 | 9.3 | 9.0 |  | 11.3** |
|  |  | $\tan \delta$ | 170 | 125 | 26 |  | 40 |
| Porcelain, dry process ${ }^{6}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 5.50 | 5.36 | 5.08 | 5.04 | 4.74 |
|  |  | $\tan \delta$ | 220 | 140 | 75 | 78 | 156 |
| 3. Glasses |  |  |  |  |  |  |  |
|  |  | $\tan \delta$ | 6 | 6 | 6 |  | 9.4 |
| Corning No. $1990{ }^{8}$ | 24 | $\epsilon^{\prime} / \epsilon_{0}$ | 8.40 | 8.38 | 8.30 | 8.20 | 7.94 |
|  |  | $\tan \delta$ | 00 | 82.5 | 5 | 9 | 42 |
| Foamglas ${ }^{\circ}$ | 23 | $\epsilon^{\prime} / \epsilon_{0}$ | 90.0 | 82.5 | 17.5 |  | 5.49 |
| Fused quartz ${ }^{10}$ | 25 | ${ }_{\text {tan }} \tan _{\epsilon^{\prime} / \epsilon_{0}}$ | 1500 3.78 | 1600 3.78 | 3180 3.78 | 3.78 | 455 |
| Fused quartz |  | $\tan \delta$ | 8.5 | 7.5 | 2 |  | 1 |

B. Organic, with or without inorganic components

1. Crystals

2. Plastics
a. Phenol-formaldehyde Bakelite BM-16981 ${ }^{12}$

25

| Formica $\mathrm{XX}^{13}$ (field $\perp$ to laminate) | 26 |
| :---: | :---: |
|  |  |

(field $\frac{1}{}$ to laminate) ...
b. Phenol-aniline-formaldehyde

Resinox $7013^{14}$
25 (preformed and preheated)

| $\epsilon^{\prime} / \epsilon_{0}$ | 5.05 | 4.87 | 4.72 | 4.62 | 4.52 |
| ---: | ---: | ---: | ---: | ---: | ---: |
| $\tan \delta$ | 190 | 160 | 72 | 56 | 82 |
| $\epsilon^{\prime} / \epsilon_{0}$ | 5.23 | 5.15 | 4.60 | 4.04 | $3.55 \dagger$ |
| $\tan \delta$ | 230 | 165 | 340 | 570 | $700^{\dagger}$ |
| $\epsilon^{\prime} / \epsilon_{0}$ | 4.64 | 4.55 | 4.37 | 4.30 | 4.25 |
| $\tan \delta$ | 160 | 137 | 62 | 77 | 124 |

c. Melamine-formaldehyde

Formica grade FF-41 ${ }^{15}$ (sheet stock) ..............
Melmac resin 592 ${ }^{18} \ldots . .$.
d. Urea-formaldehyde
$\begin{array}{lllllllll}\text { Plaskon urea, natura }{ }^{17} \ldots \ldots & 24 & \epsilon^{\prime} / \epsilon_{0} & 7.1 & 6.7 & 6.0 & 5.2 & 4.65\end{array}$
e. Hexamethylene-adipamide

| Nylon $610^{18}$. | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 3.60 | 3.50 | 3.14 | 3.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\tan \delta$ | 155 | 186 | 218 | 200 |
| Nylon $610^{18}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 4.5 | 4.2 | 3.2 | 3.0 |
| 90\% humidit |  | $\tan \delta$ | 650 | 640 | 380 | 220 |

[^193]
## TABLE 454.-DIELECTRIC CONSTANT AND LOSS TANGENT OF DIELECTRIC MATERIALS (continued)

|  | ${ }^{\text {Temp. }}{ }^{\text {c }}$. | Frequency, cycles per second |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| f. Cellulose derivatives |  | $1 \times 10^{2}$ |  | $1 \times 10^{3}$ | $1 \times 10^{6}$ | $1 \times 10^{8}$ | $1 \times 10^{10}$ |
| (1) Acetates |  |  |  |  |  |  |  |
| Tenite II 205A $\mathrm{H}^{18}$ (cellulose acetate) (butyrate) | 26 | $\begin{gathered} \epsilon^{\prime} / \epsilon_{0} \\ \tan \delta \end{gathered}$ | $\begin{array}{r} 354 \\ 78 \end{array}$ | $\begin{array}{r} 3.50 \\ 107 \end{array}$ | $\begin{array}{r} 3.28 \\ 178 \end{array}$ | $\begin{array}{r} 3.05 \\ 190 \end{array}$ |  |
| (2) Nitrate Pyralin ${ }^{20}$ | 27 | $\begin{aligned} & \epsilon^{\prime} / \epsilon_{n} \\ & \tan \delta \end{aligned}$ | $\begin{aligned} & 10.8 \\ & 6400 \end{aligned}$ | $\begin{aligned} & 8.4 \\ & 1000 \end{aligned}$ | $\begin{gathered} 6.6 \\ 640 \end{gathered}$ | $5.2$ | $\begin{array}{r} 332 \\ 1310 \end{array}$ |
| (3) Ethyl cellulose Ethocel No. 2 | 25 | $\begin{gathered} \epsilon^{\prime} / \epsilon_{0} \\ \tan \delta \end{gathered}$ | $\begin{array}{r} 3.90 \\ 75 \end{array}$ | $\begin{array}{r} 3.80 \\ 210 \end{array}$ | $\begin{aligned} & 3.40 \\ & 275 \end{aligned}$ | $\begin{aligned} & 3.20 \\ & 240 \end{aligned}$ |  |
| g. Silicone resins DC $2101^{22}$ | 25 | $\begin{gathered} \epsilon^{\prime} / \epsilon_{0} \\ \tan \delta \end{gathered}$ | 2.970 | 2.9 | 2.9 | 2.9 |  |
| h. Polyvinyl resins <br> Polyethylene DE-3401 ${ }^{23}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ $\tan \delta$ | $\stackrel{2.26}{<2}$ | $\stackrel{2.26}{<2}$ | $\stackrel{2.26}{ }$ |  | ${ }_{3.6} 2.26$ |
| Vinylite QYNA ${ }^{24}$ | 20 | $\epsilon^{\prime} / \epsilon_{0}$ | 3.18 | 3.10 | 2.88 | 2.85 |  |
|  |  | $\tan \delta$ | 130 | 185 | 160 | 81 |  |
| Saran B-115 ${ }^{25}$ | 23 | $\epsilon^{\prime} / \epsilon_{0}$ | 4.88 | 4.65 | 3.18 | 2.82 | 2.70 |
| Lucite HM-119 ${ }^{28}$ |  | $\tan \delta$ | 800 | 630 284 | 570 | 180 | 21 |
|  | 23 | $\begin{aligned} & \epsilon^{\prime} / \epsilon_{0} \\ & \tan \delta \end{aligned}$ | 3.20 620 | 2.84 440 | 2.63 145 | 2.58 | 2.57 49 |
| Polystyrene ${ }^{27}$ (commercially molded) <br> Sheet stock | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.56 | 2.56 | 2.56 | 2.55 | 2.54 |
|  |  | $\tan \delta$ | <. 5 | <. 5 | . 7 | <1 | 4.3 |
| 3. Elastomers |  |  |  |  |  |  |  |
| Hevea rubber ${ }^{28}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | $2.4$ | $2.4$ | $2.4$ | $2.4$ |  |
| Gutta-percha ${ }^{\text {ap }}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.61 | 2.60 | 2.53 | 2.47 | 2.38 |
|  |  | $\tan \delta$ | 5 | 4 | 42 | 120 | 50 |
| GR-S (Buna S) ${ }^{30}$ | 26 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.66 | 2.66 | 2.56 | 2.52 | 2.44 |
| compound ${ }_{\text {c }}$ |  | $\tan \delta$ | 7 | 9 | 120 | 95 | 50 |
| GR-I (Butyl rubber) ${ }^{31}$ | 25 | $\epsilon^{\prime} / \varepsilon_{0}$ | 2.39 | 2.38 | 2.35 | 2.35 | 2.35 |
|  |  | $\tan \delta$ | 34 | 35 | 10 | 10 | 8 |
| Neoprene GR-M ${ }^{32}$ | 26 | $\begin{gathered} \epsilon^{\prime} / \epsilon_{0} \\ \tan \delta \end{gathered}$ | $\begin{gathered} 7.5 \\ 800 \end{gathered}$ | $\begin{aligned} & 6.5 \\ & 860 \end{aligned}$ | $\begin{aligned} & 5.7 \\ & 950 \end{aligned}$ | $\begin{gathered} 3.4 \\ 1600 \end{gathered}$ |  |
| 4. Natural resins |  |  |  |  |  |  |  |
| Amber ${ }^{33}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.7 | 2.7 | 2.65 |  |  |
|  |  | $\tan \delta$ | 12.5 | 18 | 56 |  |  |
| Shellac, natural $\mathrm{XL}^{34}$ | 28 | $\epsilon^{\prime} / \epsilon_{0}$ | 3.86 | 3.81 | 3.47 | 3.10 |  |
|  |  | $\tan \delta$ | 65 | 74 | 310 | 300 |  |
| 5. Asphalts and Cement <br> Plicene cement ${ }^{35}$. | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.48 | 2.48 | 2.48 | 2.47 | 2.35 |
|  |  | $\tan \delta$ | 43.9 | 35.5 | 25.5 | 15 | 6.8 |
| 6. Waxes |  |  |  |  |  |  |  |
|  |  | $\tan \delta$ | 186 | 120 | 25 |  |  |
| Beeswax, white ${ }^{37}$ | 23 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.65 | 2.63 | 2.43 | 2.39 | 2.35 |
|  |  | $\tan \delta$ | 140 | 118 | 84 | 60 | 48 |
| Ceresin, white ${ }^{\text {88 }}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.3 | 2.3 | 2.3 | 2.3 | 2.24 |
|  |  | $\tan \delta$ | 8 | 6 | 4 | 4 | 6.5 |
| Paraffin wax ${ }^{39}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.25 | 2.25 | 2.25 | 2.25 | 2.24 |
| $132^{\circ}$ ASTM |  | $\tan \delta$ | <2 | <2 | <2 | <2 | 2.1 |
| Sealing wax ${ }^{10}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 3.68 | 3.52 | 3.29 | 3.2 |  |
| Red express |  | $\tan \delta$ | 249 | 150 | 80 | 120 |  |
| 7. Woods |  |  |  |  |  |  |  |
| Balsa | 26 | $\epsilon^{\prime} / \epsilon_{0}$ | 1.4 | 1.4 | 1.37 | 1.30 | 1.20 |
|  |  | $\tan \delta$ | 50 | 40 | 120 | 135 | 83 |
| Fir, Douglas, plywood $\ddagger$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.1 | 2.1 | 1.90 |  |  |
| Mahogany $\ddagger$ | 25 | $\tan _{\epsilon^{\prime} / \epsilon_{0}}$ | 115 | 105 | 230 | 207 |  |
|  |  | $\boldsymbol{\epsilon} / \epsilon_{\delta}$ $\tan \delta$ | 8.86 | + 120 | 250 | 320 | 210 |

TABLE 454.-DIELECTRIC CONSTANT AND LOSS TANGENT OF DIELECTRIC MATERIALS (continued)

Part 2.-Liquids

| A. $\begin{gathered}\text { Materials } \\ \text { Inorganic } \\ \text { Water, conductivity }{ }^{\text {a/ }}\end{gathered}$ | ${ }^{\text {Temp. }}$ ¢ ${ }^{\text {c }}$ | Frequency, cycles per second |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $1 \times 10^{5}$ | $1 \times 10^{6}$ | $3 \times 10^{8}$ | $3 \times 10^{6}$ | $1 \times 10^{10}$ |
|  | 1.5 | $\epsilon^{\prime} / \varepsilon_{0}$ | 87.0 | 87.0 | 86.5 | 80.5 | 38 |
|  |  | $\boldsymbol{\operatorname { t a n }} \delta$ | 1,900 | 190 | 320 | 3,100 | 10,300 |
|  | 25 | $\epsilon^{\prime} / \varepsilon_{0}$ | 78.2 | 78.2 | 77.5 | 76.7 | 55 |
|  |  | $\tan \delta$ | 4,000 | 400 | 160 | 1,570 | 5,400 |
|  | 45 | $\epsilon^{\prime} / \epsilon_{0}$ |  | 71.5 | 71.0 | 70.7 | 59 |
|  |  | $\tan \delta$ |  | 590 | 105 | 1,060 | 4,000 |
|  | 65 | $\epsilon^{\prime \prime} / \epsilon_{0}$ |  | 64.8 | 64.5 | 64.0 | 59 |
|  |  | $\boldsymbol{\operatorname { t a n }} \delta$ |  | 865 | 84 | 765 | 3,200 |
|  | 85 | $\epsilon^{\prime} / \epsilon_{0}$ |  | 58 | 57 | 56.5 | , 54 |
|  |  | $\boldsymbol{\operatorname { t a n }} \delta$ | 12,400 | 1.240 | 73 | 547 | 2,600 |
| B. Organic |  |  |  |  |  |  |  |
| 1. Aliphatic Methyl alcohol ${ }^{42}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | $1 \times 10^{2}$ | $1 \times 10^{3}$ | $\begin{array}{r} 1 \times 10^{8} \\ 31 \end{array}$ | $1 \times 10^{8}$ 31 | 8.9 |
|  |  | $\boldsymbol{\operatorname { t a n }} \delta$ |  |  | 2,000 | 380 | 8,100 |
| Ethyl alcohol ${ }^{48}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ |  |  | 24.5 | 23.7 | 1.7 |
|  |  | $\tan \delta$ |  |  | 900 | 620 | 680 |
| n-Propyl alcohol ${ }^{\text {4/ }}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ |  |  | 20.1 | 19.0 | 2.3 |
|  |  | $\tan \delta$ |  |  | 180 | 2000 | 900 |
| Carbon tetrachloride ${ }^{45}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.17 | 2.17 | 2.17 | 2.17 | 2.17 |
| 2. Aromatic |  |  |  | 8 | <. 4 | <2 | 16 |
|  |  |  |  |  |  |  |  |
|  |  | $\tan \delta$ |  |  | 80 |  |  |
| Styrene N-100 ${ }^{18}$ | 22 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.40 | 2.40 | 2.40 |  | 2.36 |
|  |  | $\tan \delta$ | 38 | 5 | <3 |  | 58 |
| 3. Insulating oils |  |  |  |  |  |  |  |
|  |  | $\tan \delta$ | 12.6 | 2 |  |  | 18 |
| Fractol ${ }^{48}$ | 26 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.17 | 2.17 |  |  | 2.16 |
|  |  | $\tan \delta$ | $<1$ | <1 |  |  | 11.3 |
| Marcol ${ }^{48}$ | 24 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.14 | 2.14 | 2.14 |  | 2.14 |
| Primol-D ${ }^{50}$ | 24 | $\tan _{\epsilon^{\prime} / \epsilon_{0}}$ | 2.17 | ${ }_{2} 2.17$ | ${ }_{2}<^{17}$ |  | 11.2 2.16 |
| Cable oil $5314^{51}$ |  | $\boldsymbol{\operatorname { t a n }} \delta$ | $<1$ | $<1$ | <2 |  | 10.6 |
|  | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.25 | 2.25 |  |  | 2.22 |
|  |  | $\tan \delta$ | 3 | <. 4 |  |  | 22 |
|  | 80 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.18 | 2.18 |  |  |  |
|  |  | $\tan \delta$ | 38 | 4 |  |  |  |
| Pyranol $1467{ }^{62}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 4.40 36 | 4.40 3 | $\begin{array}{r} 4.40 \\ 190 \end{array}$ | $\begin{aligned} & 4.04 \\ & 1300 \end{aligned}$ | 2.65 750 |
| Halowax oil $1000^{53}$ | 25 | $\epsilon^{\prime} / \epsilon_{0}$ | 4.80 | 4.77 | 4.77 |  | 2.99 |
|  |  | $\tan \delta$ | 490 | 50 | <2 |  | 1850 |
| 4. Lubricants |  |  |  |  |  |  |  |
|  |  | $\tan \delta$ | 3 | 2 | <1 | <4 | 10 |
| Silicone fluid No. 500, ${ }^{\text {s4 }}$ | 22 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.76 | 2.76 |  |  | 2.72 |
| 100 cs . at $25^{\circ} \mathrm{C} \ldots$ |  | $\tan \delta$ | . 4 | <. 4 |  |  | 240 |
| Silicone fluid No. $200,{ }^{\text {s4 }}$ 100 cs . at $25^{\circ} \mathrm{C} \ldots \ldots$. | 23 | $\epsilon^{\prime} / \epsilon_{0}$ | 2.76 | 2.76 |  |  | 2.70 |
| 100 cs . at $25^{\circ} \mathrm{C} \ldots$. |  | $\tan \delta$ | . 8 | . 4 |  |  | 320 |

[^194]
## (continued)

## TABLE 454.-DIELECTRIC CONSTANT AND LOSS TANGENT OF DIELECTRIC MATERIALS (concluded)

$1 \%$ antioxidant (Bakelite) 24, $100 \%$ polyvinyl chloride (Bakelite). 25 , Polyvinylidene and vinyl chlorides (Dow). 26, Polymethyl methacrylate (DuPont). 27, For sheet stock, various samples used for different frequencies; for rod stock, $\epsilon^{\prime} / \epsilon_{0}$ is the same as for sheet stock. (Plax). 28, Pale crepe (Rubber Research Corp.). 29, Palaquium Oblongifolium (Hermann Weber). 30, 100 pts GR-S, 1 pt stearic acid, 5 pts Kadox, 5 pts Captax, 3 pts sulfur (Rubber Research Corp). 31, Copolymer of $98.99 \%$ isobutylene, $1-2 \%$ isoprene (Rubbe: Research Corp.). 32, Poly-2-chlorobutadiene-1, 3 stabilized with Methyl Tuads (DuPont). 33, Fossil resin (Amber Mines). 34, Contains ca. $3.5 \%$ wax (Zinsser). 35, Central Scientific. 36, Shell Oil. 37, Bromund. 38, Vegetable and mineral waxes (Kuhne-Libby). 39, Mainly $\mathrm{C}_{22}$ to $\mathrm{C}_{29}$ aliphatic, saturated hydrocarbons (Standard Oil New Jerscy). 40, Dennison. 41, Research Laboratory of Physical Chemistry, Massachusetts Inst. Techn. 42, Absolute, Analytical Grade (Mallinckrodt). 43, Absolute (U. S. Industrial Chemicals). 44, Eastman Kodak. Dried and refractionated, Lab. Ins. Res. 45, Purified Lab. Ins. Res. 46, Dow. 47, $72.0 \%$ paraffins, $28.0 \%$ naphthenes (Stanco). $48,57.4 \%$ paraffins, $42.6 \%$ naphthenes (Stanco). 49, $72.4 \%$ paraffins, $27.6 \%$ naphthenes (Stanco). $50,49.4 \%$ paraffins, $50.6 \%$ naphthenes (Stanco). 51, Aliphatic and aromatic hydrocarbons (General Electric). 52, Chlorinated benzenes and diphenyls (General Electric). $53,60 \%$ mono-, $40 \%$ di- and trichloronaphthalenes (Bakelite). 54, Methyl or ethyl siloxane polymer (Dow Corning).
cs., centistoke.

TABLE 455.-DIELECTRIC CONSTANT AND CONDUCTIVITY OF SOILS ${ }^{152}$
Measurements of samples of soil taken from different depths at various sites in England

| Geological classification | $\underset{\mathrm{ft}}{\text { Depth }}$ | Description of sample |  | uctivity (i | n esu) a | 20 ${ }^{\circ} \mathrm{C}$ | Dielectric constant |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\%_{1 \mathrm{kc}}$ | 100 kc | 1.2 Mc | 10 Mc | $\begin{aligned} & 1.2 \\ & \mathrm{Mc} \end{aligned}$ | ${ }_{10}^{10}$ |
| Lower lias |  |  |  |  |  |  |  |  |
|  | Surface | Dark fibrous loam... 60 | $3.0 \times 10^{8}$ | $3.4 \times 10^{8}$ | $3.9 \times 10$ | $0^{8} 6.0 \times 1$ | 100 | 55 |
|  | 1 | Loam and clay...... 33 | 6.5 | 7.0 | 7.0 | 9.0 | 95 | 43 |
|  | 2 | Clay and sand...... 26 | 7.5 | 8.0 | 8.0 | 12.0 | 105 | 48 |
|  | 3 | Blue clay ......... 25 | 8.0 | 9.0 | 9.5 | 11.0 | 95 | 46 |
| Chalk. .... | Surface | Fibrous loam . ...... 21 | . 85 | . 90 | . 95 | 1.4 | 39 | 23 |
|  | 1 | Chalky loam ....... 21 | . 55 | . 55 | . 85 | . 95 | 41 | 25 |
|  | 2 | Chalk ............. 24 | . 28 | . 26 | . 38 | . 61 | 28 | 21 |
| Upper greensand |  |  |  |  |  |  |  |  |
|  | Surface | Fibrous loam ...... 37 | 2.7 | 3.4 | 4.0 | 5.0 | 80 | 49 |
|  | 1 | Brown, sandy clay.. 19 | 2.2 | 2.4 | 2.4 | 3.8 | 39 | 19 |
|  | 2 | Brown sand ........ 15 | 1.8 | 2.0 | 2.1 | 3.3 | 33 | 19 |
| Upper lias |  |  |  |  |  |  |  |  |
|  | Surface | Fibrous loam ...... 28 | . 85 | . 95 | 1.1 | 1.6 | 48 | 30 |
|  | 1 | Sandy loam ........ 16 | . 34 | . 34 | . 40 | . 61 | 20 | 17 |
|  | 2 | Brown sand ........ 14 | . 29 | . 29 | . 33 | . 46 | 20 | 14 |
|  | 5 | Sand and sandstone.. 8.5 | . 075 | . 090 | . 12 | . 22 | 14 | 9 |
| Red marls. | Surface | Reddish-brown loam. 23 | 1.5 | 1.7 | 1.8 | 2.3 | 46 | 32 |
|  | 1 | Reddish-brown clay. 20 | 1.5 | 1.7 | 1.8 | 2.5 | 50 | 33 |
|  | 2 | Reddish-brown clay. 18 | 2.6 | 2.8 | 3.1 | 3.6 | 80 | 45 |
| Devonian | Surface | Black fibrous loam. . 21 | 1.3 | 1.5 | 1.8 | 2.5 | 90 | 65 |
|  | 1 | Loam and slate..... 9.0 | . 026 | . 030 | . 040 | . 060 | 12 | 10 |
|  | 10 | Slate ............ - | . 00026 | . 0025 | . 0092 | . 046 | 9.5 | 8.0 |
| Granite | $1$ | Gritty loam ........ 18 | . 12 | . 12 | . 16 | . 18 | 22 | 15 |
|  | $3 \text { to } 10$ | Granite . . . . . . . . . . - | . 00090 | . 0070 | . 028 | . 11 | 12 | 8.5 |
|  | 3 to 10 | Granite | . 00070 | . 0050 | . 019 | . 095 | 10.0 | 7.5 |
| Boulder clay | $\begin{gathered} \text { Surface } \\ 2 \\ 3 \end{gathered}$ | Fibrous loam ....... 38 <br> Clay and loam ..... 19 <br> Dark grit and clay.. 18 | $\begin{gathered} .55 \\ 1.1 \\ .60 \end{gathered}$ | $\begin{gathered} .65 \\ 1.1 \\ .70 \end{gathered}$ | $\begin{gathered} .75 \\ 1.2 \\ .80 \end{gathered}$ | $\begin{aligned} & 1.1 \\ & 1.7 \\ & 1.2 \end{aligned}$ | $\begin{aligned} & 50 \\ & 60 \\ & 50 \end{aligned}$ | $\begin{aligned} & 20 \\ & 21 \\ & 19 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |

[^195]The dipole moments are given in Debye units (1 Debye unit $=1 \times 10^{-18}$ esu). The moments listed were obtained from gaseous measurements. The data are taken from Tables of Electric Dipole Moments, April 1947, compiled by L. G. Wesson, Laboratory for Insulation Research, Massachusetts Inst. Techn., Cambridge, Mass. Where several sources were given, a study was made to select the best value. Reference to original sources can be made from the above tables.

Part 1.-Inorganic substances

| Substance | $\begin{gathered} \text { Electric } \\ \text { dipole } \\ \text { moment } \\ 1 \times 10^{-18} \\ \text { esu } \end{gathered}$ | Substance | $\begin{gathered} \text { Electric } \\ \text { dipole } \\ \text { moment } \\ \text { momplo } \\ \text { esu } \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| Ammonia | 1.46 | Nitric oxide | . 1 |
| Argon | . 0 | Nitrogen | . 0 |
| Arsine | . 16 | Nitrogen dioxide | 3 |
| Boron fluoride | . 0 | Oxygen | 0 |
| Deuterium chloride | 1.089 | Phosphine | . 55 |
| Helium | . 0 | Potassium chloride | 6.3 |
| Hydrogen | . 0 | Silane, $\mathrm{SiH}_{4}$ | . |
| Hydrogen fluoride | 1.91 | Sodium iodide | 4.9 |
| Hydrogen iodide | . 38 | Sulfur dioxide | 1.7 |
| Krypton . ... |  | Water | 1.84 |
| Neon | . 0 | Xenon | . 0 |

Part 2.-Organic substances

| Substance | $\begin{aligned} & \text { Electric } \\ & \text { dipole } \\ & \text { moment } \\ & 1 \times 10^{-1 s} \\ & \text { esu } \end{aligned}$ | Substance | $\begin{aligned} & \text { Electric } \\ & \text { dipole } \\ & \text { moment } \\ & 1 \times 10^{-1.15} \\ & \text { esu } \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Phosgene $\mathrm{CCl}_{2} \mathrm{O}$ |  | Ethyl chloride $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Cl}$ | 2.00 |
| (carbonyl chloride) | 1.18 | Ethyl fluoride $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{~F}$ | 1.92 |
| Thiophosgene $\mathrm{CCl}_{2} \mathrm{~S}$ | . 28 | Ethyl iodide $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{I}$ | 1.87 |
| Carbon tetrachloride $\mathrm{CCl}^{\text {c }}$ | . 0 | Nitroethane $\mathrm{C}_{2} \mathrm{H}_{3} \mathrm{NO}_{2}$ | 3.70 |
| Chloroform $\mathrm{CHCl}_{3}$ | 1.02 | Ethane $\mathrm{C}_{2} \mathrm{H}_{6}$ | . 0 |
| Hydrogen cyanide CHN | 2.94 | Ethyl alcohol $\mathrm{C}_{2} \mathrm{H}_{6} \mathrm{O}$ | 1.68 |
| Formaldehyde $\mathrm{CH}_{2} \mathrm{O}$ | 2.27 | Methyl sulfone $\mathrm{C}_{2} \mathrm{H}_{6} \mathrm{O}_{2} \mathrm{~S}$ | 4.41 |
| Formic acid $\mathrm{CH}_{2} \mathrm{O}_{2}$ | 1.51 | Dimethylamine $\mathrm{C}_{2} \mathrm{H}_{7} \mathrm{~N}$ | . 99 |
| Methyl bromide $\mathrm{CH}_{3} \mathrm{Br}$ | 1.79 | Cyanogen $\mathrm{C}_{2} \mathrm{~N}_{3}$ | . 0 |
| Methyl chloride $\mathrm{CH}_{3} \mathrm{Cl}$ | 1.86 | Propene (propylene) $\mathrm{C}_{3} \mathrm{H}_{6}$ | . 35 |
| Methyl iodide $\mathrm{CH}_{3} \mathrm{I}$ | 1.64 | Acetone $\mathrm{C}_{3} \mathrm{H}_{6} \mathrm{O} \ldots \ldots .$. | 2.85 |
| Formamide $\mathrm{CH}_{3} \mathrm{NO}$ | 3.22 | Methyl acetate $\mathrm{C}_{3} \mathrm{H}_{0} \mathrm{O}_{2}$ | 1.67 |
| Nitromethane $\mathrm{CH}_{3} \mathrm{NO}_{2}$ | 3.49 | Ethyl ether $\mathrm{C}_{4} \mathrm{H}_{10} \mathrm{O}$ | 1.14 |
| Methane $\mathrm{CH}_{4}$ |  | Ethyl sulfide $\mathrm{C}_{4} \mathrm{H}_{10} \mathrm{~S}$ | 1.51 |
| Methyl alcohol $\mathrm{CH}_{4} \mathrm{O}$ | 1.69 | Diethyl carbonate $\mathrm{C}_{5} \mathrm{H}_{10} \mathrm{O}_{3}$ | 1.06 |
| Carbon monoxide CO |  | Bromobenzene $\mathrm{C}_{6} \mathrm{H}_{5} \mathrm{Br}$ | 1.74 |
| Carbon dioxide $\mathrm{CO}_{2}$ | . 0 | Chlorobenzene $\mathrm{C}_{6} \mathrm{H}_{5} \mathrm{Cl}$ | 1.69 |
| Carbon disulfide $\mathrm{CS}_{2}$ | . 0 | Fluorobenzene $\mathrm{C}_{0} \mathrm{H}_{5} \mathrm{~F}$ | 1.57 |
| Acetylene $\mathrm{C}_{2} \mathrm{H}_{2}$ | . 0 | Nitrobenzene $\mathrm{C}_{6} \mathrm{H}_{5} \mathrm{NO}_{2}$ | 4.23 |
| Ethylene $\mathrm{C}_{2} \mathrm{H}_{4}$ | . 0 | Benzene $\mathrm{C}_{8} \mathrm{H}_{8}$ | . 0 |
| Acetaldehyde $\mathrm{C}_{2} \mathrm{H}_{4} \mathrm{O}$ | 2.71 | Phenol $\mathrm{C}_{6} \mathrm{H}_{8} \mathrm{O}$ | 1.40 |
| Acetic acid $\mathrm{C}_{2} \mathrm{H}_{4} \mathrm{O}_{2}$. | 1.73 | Aniline $\mathrm{C}_{6} \mathrm{H}_{7} \mathrm{~N}$ | 1.48 |
| Ethyl bromide $\mathrm{C}_{2} \mathrm{H}_{3} \mathrm{Br}$ | 1.96 | Toluene $\mathrm{C}_{7} \mathrm{H}_{3}$ | . 37 |

For very low frequencies ( 100 kc and under), an empirical transmission formula of the form

$$
F=\frac{377 h I}{\lambda d} \sqrt{\frac{\theta}{\sin \theta}} \times e^{\frac{-a d}{\lambda^{x}}}
$$

has been found useful (Austin-Cohen; Austin; Espenschied, Anderson, and Bailey), where
$F=$ received field intensity, in $\mu \nu / m$
$h=$ effective height of transmitting antenna, in km
$I=$ transmitting antenna current, in amp
$\theta=$ transmission distance, in radians
$d=$ transmission distance, in km
$\lambda=$ wavelength, in km
Values of $a$ and $x$ were found to vary somewhat.
Since theoretical justification for the Austin-Cohen value of $x=\frac{1}{2}$ has been given by Watson (Proc. Roy. Soc. London, A, vol. 95, p. 546, 1919), data furnished by the above observers have been reevaluated, assuming validity of the relationship

$$
F=\frac{377 h I}{\lambda d} \sqrt{\frac{\theta}{\sin \theta}} \times e^{\frac{-a d}{\sqrt{\lambda}}}
$$

and the resulting values of $\alpha$ presented in the accompanying table, together with their relative weights estimated from the number of observations used in their determination.
a yaries notably with frequency, time of day, and the type of ground along the transmission path, and less definitely with season, solar activity, and the location of the transmission path. The values presented here are for conditions where the entire transmission path, at the height of the ionospheric reflecting layer, lies in daylight or in darkness. For conditions of sunrise or sunset on the transmission path, a has generally been found to lie between day and night values, but under certain circumstances, to far exceed these values.

| $\begin{array}{r} \mathrm{f}, \mathrm{kc} \\ 12.8 \end{array}$ | a .59 | Day weight $10^{-3} 97$ | $a$ | Night weight | Transmission path |  |  | Observations by |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Ground | Transmitter location | Receiver location |  |
|  |  |  |  |  | Sea water | Bordeaux, France | Washington, D. C. | Austin |
| 17.13 | . 66 | 112 | . $32 \times$ | $10^{-8} 48$ | " | Rocky Point, N. Y. | New Southport, England | Espenchied, Anderson, Bailey |
| 22.9 | 1.49 | 59 |  |  | Land | San Diego, Calif. | Washington, D. C. | Austin |
| 23.4 | 1.01 | 97 |  |  | Sea water | Nauen, Germany | Washington, D. C. | Austin |
| 24.05 | . 61 | 93 | . 25 | 7 | " | Leafield, England | Belfast, Maine | Espenchied, Anderson, Bailey |
| 24.05 | . 80 | 42 | . 46 | 2 | " | " | Riverhead, L. I., N. Y. | ، |
| 24.05 | . 81 | 52 | . 44 | 1 | " | " | Greenharbor, Mass. | " |
| 25.7 | . 76 | 104 | . 29 | 42 | " | Marion, Mass. | New Southgate, England | " |
| 52 | 1.45 | 29 | . 60 | 15 | " | Northolt, England | Riverhead, L. I., N. Y. | " |
| 52 | 1.40 | 75 | . 84 | 21 | " | " | Belfast, Maine | " |
| 54.5 | 1.49 | 45 | . 89 | 30 | " | " | Green Harbor, Mass. | " |
| 57 | 1.48 | 112 | . 55 | 48 | " | Rocky Point, N. Y. | Nrw Southgate, England | " |

At high frequencies and distances where the radiation is chiefly received by means of sky-wave transmission, reference is given to the methods for calculation of received field intensities presented in Chapter 7, National Bureau of Standards Circular 462, "Ionospheric Radio Propagation."

For long transmission paths (over 4000 km ),
where

$$
F=F_{0}+\frac{1}{2} \log P-S_{0} J Q \bar{K} d
$$

$F=\log$ of the received field intensity, in $\frac{\mu v}{m}$
$F_{0}=\log$ of the ionospherically unabsorbed field intensity, in $\frac{\mu v}{m}$, for 1 kw effective radiated power
$=1.6-1.44[\log d-3.60]$
$d=$ transmission distance, in units of 1000 km
$P=$ effective radiated power, in kw
$\log S_{0}=0.502-1.916(\log f-0.477)$
$f=$ frequency, in Mc
$Q=1+0.005 R$
$R=$ sunspot number
$\bar{K}=$ average $K$ for the transmission path
$K=0.142+0.858 \cos \psi$
$\psi=$ solar zenith angle
$\bar{K} d=0.142 D^{\prime}+\left(K_{1}+K_{2}-0.284\right) \tan \frac{D^{\prime}}{2 R}$
where $\quad D^{\prime}=$ the length of the path in the region where $K$ is not equal to zero, in units of 1000 km
$K_{1}$ and $K_{2}=$ values of $K$ at transmitting and receiving stations
$R=$ radius of the earth in units of 1000 km
$J=$ seasonal variation factor. $J$ has the values $1.0,1.3,1.15$, respectively, if both terminals of the transmission path lie in summer, winter, or equinoctial regions. If one terminal lies in a summer region, the other in winter, $J=1.15$.

## TABLE 458.-E-LAYER MAXIMUM USABLE FREQUENCIES IN Mc FOR 2,000 $\cdot \mathrm{km}$ TRANSMISSION DISTANCE

| June * |  |  |  |  |  | Equinox |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| of day: | $00 \quad 04$ | 08 | 12 | 16 | 20 |  | 08 | 12 | 16 | 20 |
|  | Sunspot number $=0$ |  |  |  |  | Sunspot number $=0$ |  |  |  |  |
| Latitude <br> N. $80^{\circ}$ | $\begin{array}{ll}7.5 & 9.7\end{array}$ | 11.3 | 11.8 | 11.3 | 9.7 |  | $\begin{array}{llll}8.2 & 10.0 & 8.6\end{array}$ |  |  |  |
| 40 |  | 13.6 | 16.2 | 13.6 |  |  | 11.7 | 14.4 | 12.2 |  |
| 0 |  | 12.3 | 15.6 | 12.3 |  |  | 13.2 | 16.8 | 13.0 |  |
| 40 |  | 8.3 | 12.0 | 8.3 |  |  | 11.4 | 14.2 | 11.9 |  |
| S. 80 |  |  |  |  |  |  | 7.3 | 8.7 | 7.5 |  |
|  | Sunspot number $=125$ |  |  |  |  | Sunspot number $=125$ |  |  |  |  |
| N. $80^{\circ}$ | 9.811 .2 | 13.4 | 14.0 | 13.4 | 11.2 |  | 8.9 | 10.3 | 8.7 |  |
| 40 |  | 17.4 | 20.2 | 17.4 |  |  | 15.1 | 18.6 | 14.7 |  |
| 0 |  | 16.3 | 20.8 | 16.3 |  |  | 17.0 | 21.3 | 16.4 |  |
| 40 |  | 10.7 | 15.4 | 10.7 |  |  | 13.5 | 16.8 | 13.3 |  |
| S. 80 |  |  |  |  |  |  | 8.3 | 9.6 | 8.1 |  |

* For December, use reversed latitudes.

Norton calculated from Van der Pol's and Bremmer's theory and checked at broadcast frequencies the following results for vertically polarized ground-wave propagation. In many cases ionospheric waves will be much stronger than is indicated for ground-wave propagation in these tables. Some indication of when ionospheric waves may be expected is given.

Factor A for transmission over sea water
$\epsilon=80,(\sigma=5 \times \mathrm{mhos} / \mathrm{m})$

| Freq. |  |  |  |
| :---: | :--- | :--- | :---: |
| Mc |  |  |  |
| .5 | 50 km | 100 km | 150 km |
| 2 | 1.0 | .96 | .90 |
| 10 | 1.0 | .77 | .72 |
| 50 | .71 | .0050 | .33 |
| 200 | .025 | - | .0016 |

Factor A for transmission over good ground

$$
\epsilon=15, \sigma=10^{-2} \mathrm{mhos} / \mathrm{m}
$$

| $\begin{aligned} & \text { Freq. } \\ & \text { Mc. } \end{aligned}$ | 5 km | 10 km | 15 km | 25 km | 50 km | 100 km | 150 km |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 1 | 1.00 | 1.00 | 1.0 | 1.0 | 1.0 | . 90 | . 87 |
| . 5 | . 98 | . 93 | . 90 | . 73 | . 68 | . 48 | . 35 |
| 2.0 | . 50 | . 30 | . 21 | . 095 | . 049 | . 018 | . 0092 |
| 10 | . 026 | . 011 | . 0072 | . 0036 | . 0018 | . 00054 | . 00020 |
| 50 | . 0030 | . 0015 | . 0096 | . 00040 | . 00017 |  |  |
| 300 | . 00046 | . 00021 | . 00013 |  |  |  |  |

Factor A for transmission over poor ground $\epsilon=5, \sigma=10^{-3} \mathrm{mhos} / \mathrm{m}$

| $\begin{aligned} & \text { Freq. } \\ & \text { Mc. } \end{aligned}$ | 5 km | 10 km | 15 km | 25 km | 50 km | 100 km | 150 km |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 1 | 1.0 | . 99 | . 95 | . 92 | . 85 | . 73 | . 64 |
| . 5 | . 64 | . 45 | . 35 | . 22 | . 096 | . 038 | . 022 |
| 2.0 | . 056 | . 027 | . 018 | . 010 | . 0050 | . 0018 | . 00093 |
| 10 | . 0059 | . 0030 | . 0019 | . 0011 | . 00048 | . 00013 |  |
| 50 | . 0012 | . 00055 | . 00036 | . 00022 | -_- |  |  |
| 100 | . 00080 | . 00026 | . 00016 |  | -- | -- | - |

## CRITICAL FREQUENCIES AND MAXIMUM USABLE FREQUENCIES FOR RADIO TRANSMISSION BY REFLECTION FROM THE E AND F 2 LAYERS OF THE IONOSPHERE

Values of ionospheric critical frequencies and virtual reflection heights for all ionospheric layers ( $E, F_{1}, F_{2}, E_{s}$ ) observed at a large number of stations are regularly distributed by the Central Radio Propagation Laboratory of the National Bureau of Standards to laboratories cooperating in ionospheric research. The values presented in Tables 458 and 461 are synthesized from the trends of these data. Values are not given here for the $F_{1}$ and $E_{s}$ layers since their trends are much less accurately established than those of the $E$ and $F_{2}$ layers.
Table 458 presents $E$-layer maximum usable frequencies for a transmission distance of $2,000 \mathrm{~km}$, the maximum practical distance for 1 -hop transmission by means of $E$-layer reflection.
Table 461 presents $F_{2}$-layer ordinary-wave critical frequencies, and maximum usable frequencies for a transmission distance of 4.000 km , the maximum practical distance for 1-hop transmission by means of $F_{2}$-layer reflection.

[^196](continued)

Latitudes and local times are those of the ionospheric reflection points. The $F_{2}$-layer zones ( $W, I$, and $E$ ) are those chosen for practical description of longitude effect by the International Radio Conference of April-May 1944. The IV 'and $E$ zones are centered on $70^{\circ} \mathrm{W}$. and $110^{\circ} \mathrm{E}$. longitude, respectively; the two $I$ zones are intermediate between these.
Values are presented for sunspot numbers of 0 and 125. Since both critical frequencies and maximum usable frequencics show approximately linear variation with sunspot number, values for any other sunspot number, $X$, may be obtained by interpolation.
[World-wide charts of predicted $M U F$, three months in advance, for both $E$ and $F_{2}$ layers, are regularly published in Central Radio Propagation Laboratory Series D reports, "Basic Radio Propagation Prediction."]
$E$-Layer ordinary-wave critical frequencies.-These may be obtained by dividing the E-layer $2,000 \mathrm{~km}$ MUF by 4.78 , since the minimum virtual height of reflection is nearly constant for this layer.

Extraordinary-wave critical frequencies, $f^{x}$ (or zero-distance $M U F$ ). -The or-dinary-wave critical frequency $f^{\circ}$, the extraordinary-wave critical frequency $f^{x}$, and the gyrofrequency $f_{n}$ are related by the equation

$$
\left(f^{0}\right)^{2}=\left(f^{x} \pm f_{n}\right) f^{x}
$$

The gyrofrequency, $f_{n}$, varies with the intensity of the earth's magnetic field, $H$, and is given by

$$
f_{n}=\frac{e H}{2 \pi m c},
$$

where $c$ and $m$ are, respectively, the electronic (or ionic) charge and mass, $c$ the velocity of light in free space, and $H$ is given in gauss.

Ion density.-The number of ions per $\mathrm{cm}^{3}$ at the reflection point may be obtained from the value of the ordinary-wave critical frequency, $f^{\circ}$, by the equation

$$
N=\frac{\pi m}{e^{2}\left(f^{\circ}\right)^{2}},
$$

where $m$ and $c$ are, respectively, the ionic mass and charge.
Minimum virtual heights of reflection.-The maximum usable frequency at any transmission (except for those nearly equal to zero) is equal to

$$
M U F=f^{\circ} \sec \phi
$$

where $\phi$ is the angle of incidcnce of the wave upon the ionospheric reflecting layer.
$\phi$ is approximately given by

$$
\phi=\tan ^{-1} \frac{\sin \frac{1}{2} \theta}{1+(h / R)-\cos \frac{1}{2} \theta},
$$

where $\theta$ is the angular distance of the transmission path, $h$ the virtual height of reflection, and $R$ the radius of the earth. (Cf. Smith, N., Proc. Inst. Radio Eng., May 1939, p. 232.)
Maximum usable frequencies for other transmission distances.-These may be obtained from the MUF of Table 461 by using the factors and procedure presented in Table 462.

Skip distances.-The MUF for a given distance is the frequency for which that distance is the skip distance.

TABLE 460.-ATTENUATION OF MICROWAVES BY WATER VAPOR IN THE ATMOSPHERE (in $\mathrm{db} / \mathrm{km}$ ) ${ }^{154}$
Measured at $45^{\circ} \mathrm{C}$ at atmospheric pressure

| Wavelength (cm) | .75 cm | .96 | 1.16 | 1.28 | 1.37 | 1.69 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Frequency (kmc) | 40.2 | 31.2 | 25.8 | 23.5 | 21.9 | 17.8 |
| Water vapor density |  |  |  |  |  |  |
| $\left(\mathrm{g} / \mathrm{m}^{8}\right)$ | $.103 \mathrm{db} / \mathrm{km}$ | .081 | .149 | .230 | .224 | .049 |
| 10 | .408 | .321 | .495 | .69 | .672 | .18 |
| 30 | .84 | .665 | .90 | 1.15 | 1.12 | .355 |
| 50 |  |  |  |  |  |  |

[^197]
# TABLE 461.- $\mathrm{F}_{2}$-LAYER CRITICAL FREQUENCIES AND MAXIMUM USABLE FREQUENCIES FOR $4,000-\mathrm{km}$ TRANSMISSION DISTANCE IN Mc 

E zone

|  | June |  | Sept. |  | Dec. |  | June |  | Sept. |  | Dec. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lati- tude | $f^{\circ} F_{2}$ | $\begin{aligned} & 2-4000 \\ & M U F \end{aligned}$ | $f^{\circ} F_{2}$ | $F_{F_{2: 4}^{2-400}}^{M U F}$ | $f^{\circ} F_{2}$ | $\begin{aligned} & F_{2}-4000 \\ & M U F \end{aligned}$ | $f^{\circ} \mathrm{F}_{2}$ | ${ }_{2}^{24000}$ | $f^{\circ} F_{2}$ | $\begin{aligned} & F_{M}-4000 \\ & M U F \end{aligned}$ |  | $\begin{aligned} & 2-4000 \\ & M U F \end{aligned}$ |
| Local time of day : 00 |  |  |  | Sunspot number $=0$ |  |  | Time: 12 |  | Sunspot number $=0$ |  |  |  |
| N. $80^{\circ}$ | 4.1 | 14.2 | 3.9 | 13.9 | 3.4 | 12.6 | 4.2 | 13.9 | 4.4 | 15.4 | 3.7 | 13.4 |
| 40 | 4.18 | 13.9 | 3.8 | 12.9 | 2.9 | 9.6 | 5.8 | 19.0 | 6.1 | 21.4 | 6.8 | 24.7 |
| 0 | 3.5 | 11.4 | 4.0 | 14.7 | 4.9 | 16.5 | 9.0 | 25.6 | 8.6 | 24.7 | 8.2 | 24.5 |
| 40 | 2.7 | 9.2 | 3.0 | 10.3 | 4.3 | 14.7 | 5.0 | 18.8 | 5.6 | 19.5 | 5.9 | 19.4 |
| S. 80 | 2.4 | 8.8 | 2.8 | 9.9 | 3.9 | 13.5 | 3.3 | 11.9 | 3.6 | 12.9 | 4.5 | 14.9 |


|  |  | Sunspot |  |  |  |  |  | number $=125$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | :---: | :---: |
| N. $80^{\circ}$ | 5.2 | 16.3 | 6.1 | 18.8 | 5.6 | 17.8 |  |  |
| 40 | 8.6 | 24.9 | 7.0 | 21.3 | 3.5 | 10.8 |  |  |
| 0 | 8.8 | 27.0 | 10.9 | 38.8 | 8.2 | 25.9 |  |  |
| 40 | 4.1 | 12.8 | 5.9 | 18.2 | 8.2 | 24.7 |  |  |
| S. 80 | 4.4 | 13.8 | 5.4 | 17.5 | 5.4 | 16.5 |  |  |

Local time of day : $04 \quad$ Sunspot number $=0$

| $\mathrm{N} .80^{\circ}$ | 3.9 | 13.0 | 3.6 | 12.9 | 3.0 | 10.8 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 40 | 3.7 | 11.8 | 3.7 | 12.3 | 2.9 | 9.9 |
| 0 | 2.3 | 8.1 | 2.3 | 8.5 | 3.0 | 9.9 |
| 40 | 2.9 | 10.1 | 2.0 | 6.9 | 2.6 | 8.9 |
| S .80 | 2.4 | 8.5 | 2.5 | 8.7 | 3.8 | 13.3 |

Sunspot number $=125$

| N. $80^{\circ}$ | 5.2 | 15.4 | 5.5 | 17.5 | 4.4 | 14.0 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 40 | 8.0 | 23.3 | 6.3 | 18.8 | 3.6 | 10.9 |
| 0 | 4.9 | 15.3 | 7.2 | 23.5 | 6.2 | 20.0 |
| 40 | 4.1 | 12.8 | 4.6 | 14.1 | 6.0 | 17.8 |
| S. 80 | 4.1 | 12.9 | 5.2 | 16.5 | 5.6 | 16.5 |


| Local time of day: 08 |  |  |  |  |  |  |  | Sunspot number $=0$ |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N. $80^{\circ}$ | 4.0 | 13.0 | 4.0 | 14.3 | 3.4 | 12.5 |  |  |  |  |  |  |
| 40 | 5.8 | 19.4 | 5.7 | 20.9 | 5.2 | 19.4 |  |  |  |  |  |  |
| 0 | 7.4 | 22.5 | 7.8 | 25.3 | 6.7 | 20.6 |  |  |  |  |  |  |
| 40 | 3.9 | 14.1 | 4.3 | 15.9 | 5.0 | 17.4 |  |  |  |  |  |  |
| S. 80 | 2.4 | 8.8 | 3.4 | 11.8 | 4.3 | 14.7 |  |  |  |  |  |  |


| 5.4 | 16.0 |
| ---: | ---: |
| 9.0 | 25.6 |
| 14.0 | 32.7 |
| 10.8 | 36.4 |
| 6.0 | 19.8 |


| 6.7 | 21.2 | 5.4 | 17.6 |
| ---: | ---: | ---: | ---: |
| 11.4 | 35.3 | 11.1 | 36.4 |
| 15.5 | 38.8 | 12.7 | 30.2 |
| 10.5 | 34.1 | 8.3 | 22.7 |
| 6.2 | 19.8 | 6.2 | 17.6 |

Time: 16
$4.5 \quad 14.8$
$\begin{array}{ll}5.6 & 18.2 \\ 8.4 & 24.2\end{array}$
$5.0 \quad 18.2$
$3.0 \quad 10.9$

| 5.6 | 16.3 |
| ---: | ---: |
| 9.0 | 26.5 |
| 14.0 | 34.0 |
| 10.4 | 35.3 |
| 5.4 | 17.4 |

Time: 20
$4.2 \quad 14.3$
$5.5 \quad 18.8$
$4.5 \quad 14.7$
$2.7 \quad 9.6$
$2.5 \quad 9.3$

Sunspot number $=0$

| 4.5 | 15.9 | 3.9 | 14.2 |
| :--- | :--- | :--- | :--- |


| 5.6 | 20.0 | 5.0 | 18.3 |
| :--- | :--- | :--- | :--- |
| 9.0 | 27.0 | 8.6 | 28.1 |


| 5.1 | 18.3 | 5.9 | 19.9 |
| :--- | :--- | :--- | :--- |

$\begin{array}{llll}3.7 & 12.7 & 4.3 & 14.3\end{array}$
Sunspot number $=125$

| 6.5 | 20.0 | 5.4 | 17.3 |
| ---: | ---: | ---: | ---: |
| 10.9 | 33.2 | 8.8 | 28.8 |
| 16.2 | 41.2 | 12.2 | 29.6 |
| 9.8 | 32.3 | 8.2 | 25.9 |
| 6.7 | 21.9 | 6.0 | 17.3 |

Sunspot number $=0$ $\begin{array}{llll}4.4 & 15.8 & 3.7 & 13.3\end{array}$

| 5.1 | 18.2 | 2.7 | 9.6 |
| ---: | ---: | ---: | ---: |
| 8.2 | 25.9 | 7.2 | 23.5 |
| 4.0 | 13.9 | 5.4 | 19.4 |

$\begin{array}{llll}3.3 & 11.4 & 4.4 & 14.9\end{array}$
Sunspot number $=125$

| N. $80^{\circ}$ | 5.3 | 15.4 | 6.7 | 21.2 | 5.0 | 15.8 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 40 | 9.4 | 28.2 | 10.0 | 33.2 | 8.2 | 29.4 |
| 0 | 12.7 | 35.5 | 13.5 | 38.2 | 12.0 | 34.7 |
| 40 | 7.5 | 26.0 | 8.1 | 28.1 | 7.4 | 21.4 |
| S. 80 | 4.3 | 13.6 | 5.9 | 19.3 | 6.2 | 17.6 |


| 5.5 | 16.7 |
| ---: | ---: |
| 8.6 | 26.0 |
| 11.0 | 28.2 |
| 5.5 | 17.6 |
| 4.4 | 13.9 |

Sunspot number $=125$

I zone

| Local time of day : 00 |  |  |  | Sunspot number $=0$ |  |  | Time : 12 |  | Sunspot number $=0$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N. $80^{\circ}$ | 3.9 | 13.6 | 3.6 | 12.9 | 2.7 | 9.8 | 4.0 | 13.5 | 3.7 | 13.2 | 3.4 | 12.5 |
| 40 | 3.8 | 12.9 | 3.0 | 10.1 | 3.0 | 9.8 | 5.2 | 17.2 | 5.5 | 19.4 | 6.8 | 25.9 |
| 0 | 5.2 | 16.9 | 6.3 | 23.3 | 5.0 | 16.5 | 6.2 | 17.6 | 6.5 | 18.8 | 7.8 | 22.9 |
| 40 | 2.9 | 9.8 | 2.6 | 8.9 | 5.4 | 17.9 | 4.7 | 17.9 | 5.2 | 18.3 | 6.6 | 21.9 |
| S. 80 | 2.4 | 8.8 | 2.8 | 9.9 | 3.9 | 13.5 | 3.3 | 11.9 | 3.6 | 12.9 | 4.5 | 14.9 |
| Sunspot number $=125 \quad$ Sunspot number $=125$ |  |  |  |  |  |  |  |  |  |  |  |  |
| N. $80^{\circ}$ | 5.2 | 16.9 | 5.8 | 18.2 | 4.8 | 15.3 | 5.3 | 15.6 | 5.9 | 18.7 | 5.4 | 17.3 |
| 40 | 6.4 | 18.6 | 5.0 | 15.3 | 3.3 | 10.3 | 7.9 | 21.9 | 10.2 | 31.9 | 11.0 | 37.7 |
| 0 | 9.0 | 28.2 | 10.0 | 32.8 | 10.0 | 31.8 | 10.4 | 24.8 | 11.0 | 28.6 | 10.9 | 25.6 |
| 40 | 4.1 | 12.7 | 5.8 | 18.2 | 8.4 | 24.7 | 11.5 | 38.7 | 10.8 | 34.7 | 9.4 | 26.5 |
| S. 80 | 4.4 | 13.8 | 5.4 | 17.5 | 5.4 | 16.5 | 6.0 | 19.8 | 6.2 | 19.8 | 6.2 | 17.6 | (continued)

TABLE 461.- $F_{2}$-LAYER CRITICAL FREQUENCIES AND MAXIMUM USABLE
FREQUENCIES FOR $4,000-\mathrm{km}$ TRANSMISSION DISTANCE IN Mc (continued)

|  | June |  | $\underbrace{\text { Sept. }}$ |  |  |  | June |  | Sept. |  | Dec. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Lati- } \\ & \text { tude } \end{aligned}$ |  | ${ }_{\text {rex }}^{4000}$ | $f^{\circ} F_{2}$ | $\underbrace{M U F}_{F_{2}+4000}$ |  | $\begin{aligned} & F_{2}-4000 \\ & M U F \end{aligned}$ |  | $\underbrace{4000}$ | $f^{\circ} F_{2}$ | $\underbrace{M U F}_{F_{2}-4000}$ |  | $\begin{aligned} & 2-4000 \\ & M U F \end{aligned}$ |
| Local time of day : 04 |  |  |  | Sunspot number $=0$ |  |  | Time: 16 |  | Sunspot |  | number $=0$ |  |
| N. $80^{\circ}$ | 3.7 | 12.8 | 3.4 | 12.2 | 2.7 | 9.9 | 4.0 | 13.2 | 3.6 | 12.6 | 3.4 | 12.1 |
| 40 | 3.1 | 10.7 | 2.9 | 9.9 | 2.9 | 10.0 | 5.2 | 17.0 | 5.5 | 19.8 | 5.6 | 20.6 |
| 0 | 3.2 | 11.0 | 3.0 | 11.6 | 3.3 | 10.3 | 6.8 | 19.8 | 8.2 | 24.6 | 9.4 | 30.0 |
| 40 | 2.8 | 9.6 | 2.2 | 7.5 | 3.5 | 11.9 | 4.6 | 17.2 | 4.8 | 17.0 | 6.4 | 21.8 |
| S. 80 | 2.4 | 8.5 | 2.5 | 8.7 | 3.8 | 13.3 | 3.0 | 10.9 | 3.7 | 12.7 | 4.3 | 14.3 |
|  |  |  | Sunspot number $=125$ |  |  |  |  |  | Sunspot number $=125$ |  |  |  |
| N. $80^{\circ}$ | 4.8 | 15.4 | 5.7 | 17.4 | 3.9 | 12.2 | 5.2 | 15.6 | 5.9 | 18.8 | 5.2 | 16.6 |
| 40 | 5.3 | 15.3 | 4.6 | 14.2 | 3.4 | 10.6 | 7.8 | 22.6 | 9.7 | 30.6 | 9.8 | 33.9 |
| 0 | 6.9 | 21.8 | 5.4 | 17.6 | 7.2 | 22.9 | 10.8 | 26.8 | 12.5 | 31.8 | 12.4 | 35.0 |
| 40 | 4.0 | 12.5 | 4.2 | 12.6 | 6.2 | 18.5 | 10.0 | 33.5 | 10.4 | 33.5 | 9.2 | 27.3 |
| S. 80 | 4.1 | 12.9 | 5.2 | 16.5 | 5.6 | 16.5 | 5.4 | 17.4 | 6.7 | 21.9 | 6.0 | 17.3 |
| Local time of day : 08 |  |  |  | Sunspot number $=0$ |  |  | Time : 20 |  | Sunspot number $=0$ |  |  |  |
| N. $80^{\circ}$ | 3.9 | 12.8 | 3.6 | 13.2 | 3.0 | 10.9 | 3.8 | 13.2 | 3.6 | 12.8 | 3.1 | 11.5 |
| 40 | 4.8 | 16.5 | 5.0 | 18.8 | 5.0 | 18.8 | 5.2 | 17.9 | 3.6 | 12.9 | 2.7 | 8.8 |
| 0 | 6.2 | 18.6 | 5.6 | 17.9 | 7.4 | 22.9 | 6.0 | 20.8 | 7.0 | 21.6 | 7.6 | 24.9 |
| 40 | 3.5 | 12.9 | 4.3 | 15.9 | 5.6 | 19.4 | 2.7 | 9.5 | 3.4 | 11.8 | 6.7 | 22.2 |
| S. 80 | 2.4 | 8.8 | 3.4 | 11.8 | 4.3 | 14.7 | 2.5 | 9.3 | 3.3 | 11.4 | 4.4 | 14.9 |
|  |  |  | Sunspot number $=125$ |  |  |  |  |  | Sunspot number $=125$ |  |  |  |
| N. $80^{\circ}$ | 5.1 | 15.0 | 5.9 | 18.8 | 4.3 | 13.5 | 5.1 | 16.0 | 5.8 | 18.3 | 4.9 | 15.5 |
| 40 | 7.6 | 21.2 | 8.6 | 28.8 | 7.8 | 29.4 | 7.5 | 21.4 | 6.7 | 21.6 | 3.7 | 12.7 |
| 0 | 8.9 | 24.9 | 11.6 | 33.0 | 10.3 | 29.3 | 9.4 | 23.4 | 10.2 | 25.9 | 10.5 | 27.0 |
| 40 | 7.7 | 26.5 | 8.6 | 29.4 | 8.8 | 25.6 | 5.4 | 17.6 | 7.4 | 24.3 | 9.2 | 26.8 |
| S. 80 | 4.3 | 13.6 | 5.9 | 19.3 | 6.2 | 17.6 | 4.4 | 13.9 | 6.3 | 20.6 | 6.0 | 17.6 |

W zone

| Local time of day: 00 |  |  |  |  |  | Sunspot number $=0$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | ---: | :---: | :---: | :---: |
| N. $80^{\circ}$ | 3.9 | 13.6 | 3.6 | 12.9 | 2.7 | 9.8 |  |  |  |
| 40 | 3.0 | 10.5 | 2.0 | 6.8 | 2.3 | 7.8 |  |  |  |
| 0 | 4.4 | 14.6 | 5.5 | 20.6 | 3.6 | 12.0 |  |  |  |
| 40 | 2.3 | 7.9 | 3.4 | 11.8 | 5.0 | 16.5 |  |  |  |
| S. 80 | 3.0 | 10.8 | 3.2 | 11.3 | 4.2 | 14.8 |  |  |  |


| Time : 12 | Sunspot number $=0$ |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| 4.0 | 13.5 | 3.7 | 13.2 | 3.4 | 12.5 |
| 5.2 | 16.8 | 5.2 | 18.6 | 6.5 | 24.5 |
| 7.6 | 21.8 | 10.6 | 30.3 | 8.6 | 26.5 |
| 5.0 | 18.9 | 6.7 | 24.1 | 8.4 | 28.1 |
| 3.4 | 12.5 | 3.6 | 12.8 | 4.6 | 15.0 |


|  |  |  | Sunspot number $=125$ |  |  |  |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | :---: |
| N. $80^{\circ}$ | 5.2 | 16.9 | 5.8 | 18.2 | 4.8 | 15.3 |  |
| 40 | 6.6 | 20.6 | 5.6 | 17.0 | 4.6 | 14.5 |  |
| 0 | 10.5 | 31.8 | 12.2 | 39.2 | 9.0 | 28.3 |  |
| 40 | 3.4 | 10.6 | 7.2 | 22.6 | 9.9 | 29.3 |  |
| S. 80 | 5.1 | 16.3 | 6.2 | 20.0 | 5.9 | 17.5 |  |


| Local time of day : 04 |  |  |  | Sunspot number $=0$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N. $80^{\circ}$ | 3.7 | 12.8 | 3.4 | 12.2 | 2.7 | 9.9 |
| 40 | 2.1 | 6.8 | 1.7 | 5.8 | 2.6 | 8.9 |
| 0 | 3.2 | 11.0 | 3.5 | 12.8 | 2.3 | 7.8 |
| 40 | 2.0 | 6.8 | 2.9 | 10.0 | 4.7 | 15. |
| S. 80 | 2.9 | 10.5 | 2.5 | 8.9 | 4.2 | 14. |

1.6
8.8
3.6
8.3

Sunspot number $=125$

| 5.3 | 15.6 | 5.9 | 18.7 | 5.4 | 17.3 |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 7.1 | 20.8 | 9.3 | 29.3 | 12.3 | 40.3 |
| 11.7 | 28.2 | 14.9 | 37.0 | 14.1 | 33.3 |
| 11.0 | 37.6 | 13.9 | 44.7 | 12.1 | 33.9 |
| 5.7 | 18.3 | 7.6 | 24.7 | 7.0 | 19.8 |

Sunspot number $=125$

| N. $80^{\circ}$ | 4.8 | 15.4 | 5.7 | 17.4 | 3.9 | 12.2 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 40 | 4.9 | 15.6 | 4.1 | 12.5 | 4.4 | 13.6 |
| 0 | 7.0 | 22.1 | 6.2 | 21.5 | 4.9 | 14.5 |
| 40 | 3.2 | 9.9 | 5.8 | 17.6 | 9.4 | 27.6 |
| S .80 | 4.6 | 14.7 | 5.2 | 16.7 | 5.6 | 16.7 |

Time: 16
$4.0 \quad 13.2$
$\begin{array}{ll}5.2 & 17.2 \\ 9.2 & 26.9 \\ 4.4 & 16.5\end{array}$
$\begin{array}{ll}3.2 & 11.8\end{array}$
Sunspot number $=0$

| 3.6 | 12.6 | 3.4 | 12.1 |
| ---: | ---: | ---: | ---: |
| 5.3 | 19.0 | 5.7 | 21.0 |
| 10.2 | 31.5 | 8.6 | 27.3 |
| 5.0 | 18.5 | 7.2 | 24.5 |
| 3.8 | 13.3 | 4.5 | 14.9 |

Sunspot number $=125$

| 5.2 | 15.6 | 5.9 | 18.8 | 5.2 | 16.6 |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 7.4 | 21.8 | 9.3 | 28.8 | 11.2 | 36.3 |
| 11.8 | 29.4 | 14.0 | 37.5 | 13.8 | 34.3 |
| 8.5 | 30.0 | 11.4 | 37.4 | 11.0 | 32.9 |
| 5.2 | 16.6 | 6.9 | 22.2 | 6.5 | 18.7 |

TABLE 461.- F $_{2}$-LAYER CRITICAL FREQUENCIES AND MAXIMUM USABLE
FREQUENCIES FOR $4,000 \cdot \mathrm{~km}$ TRANSMISSION DISTANCE IN Mc (concluded)


## TABLE 462.-FACTORS FOR OBTAINING F ${ }_{2}$-LAYER MUF, AND COMBINED E, $F_{1}$-LAYER MUF AT OTHER DISTANCES, FROM $F_{2}-4,000 \mathrm{~km}$ MUF AND E-2,000 km MUF

The accompanying table presents (a) factors, $F_{2000} E-E, F_{1}$, by which the 2,000 $E$-layer maximum usable frequencies may be multiplied in order to obtain values of maximum usable frequencies by combined $E$ - and $F_{1}$-layer transmission for other distances, and (b) factors, $F_{4000 F_{2-F}}$, by which $4,000-\mathrm{km} F_{2}$-layer maximum usable frequencies may be multiplied in order to obtain values of $F_{2}$-layer maximum usable frequencies at other transmission distances. These factors become less accurate with decreasing transmission distance.

For obtaining the maximum usable frequency for practical radio transmission, the following procedures may be used:

1. One-hop transmission:-Obtain both the combined $E$-, $F_{1}$-layer, and $F_{2}$-layer maximum usable frequencies pertinent to the midpoint of the transmission path. The higher of the two will be the $M U F$ for the path, neglecting possible transmission by sporadic- $E$ ionization.
2. Long-path transmission:-For transmission paths exceeding $4,000 \mathrm{~km}$, the following procedure generally affords a sufficiently good value for practical use:
(a) Determine the $2,000-\mathrm{km} E$-layer $M U F$ for a point $1,000 \mathrm{~km}$ along the transmission path from the transmitting station. Determine the $4,000-\mathrm{km} F_{2}$-layer $M U F$ for a point $2,000 \mathrm{~km}$ along the transmission path from the transmitting station. Select the higher of two values, for comparison with a value to be later obtained in procedure (b).
(b) Determine the $2,000-\mathrm{km} E$-layer $M U F$ for a point $1,000 \mathrm{~km}$ along the transmission path from the receiving station. Determine the $4,000-\mathrm{km} F_{2}$-layer $M U F$ for a point 2,000 km along the transmission path from the receiving station. Select the higher of these two values, for comparison with the value obtained in procedure (a).
(c) Compare the values obtained in procedures (a) and (b) above. The lower of the two will be the MUF for the transmission path, neglecting possible transmission by sporadic- $E$ ionization.
For more detailed and accurate procedures, and for inclusion of sporadic- $E$ layer effects, reference is given to National Bureau of Standards Circular 462, "Ionospheric Radio Propagation," and to reports of the Central Radio Propagation Laboratory, Series D, "Basic Radio Propagation Prediction."

| $\begin{gathered} \text { Distance } \\ \mathrm{km} \end{gathered}$ |  | $F_{4000} F_{5}-F_{2}$ | $\begin{gathered} \text { Distance } \\ \mathrm{km} \end{gathered}$ | $F_{2000 \mathrm{E}-\mathrm{E}, \mathrm{F}_{1}}$ | $F_{40000} \mathrm{~F}_{2}-\mathrm{F}_{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 200 | . 25 | . 35 | 2200 |  | . 79 |
| 400 | . 36 | . 36 | 2400 |  | . 83 |
| 600 | . 48 | . 38 | 2600 | ... | . 86 |
| 800 | . 62 | . 41 | 2800 | $\ldots$ | . 90 |
| 1000 | . 72 | . 46 | 3000 | $\ldots$ | . 92 |
| 1200 | . 82 | . 51 | 3200 | $\ldots$ | . 95 |
| 1400 | . 88 | . 57 | 3400 | $\ldots$ | . 97 |
| 1600 | . 95 | . 63 | 3600 |  | . 98 |
| 1800 | . 98 | . 69 | 3800 |  | . 99 |
| 2000 | 1.00 | . 74 | 4000 |  | 1.00 |

TABLE 463.-CALCULATED ATTENUATION OF MICROWAVES BY RAIN
(db/km) ${ }^{1205}$

| Rate of rainfall ( $\mathrm{mm} / \mathrm{hr}$ ) | Wavelength (cm) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 1.25 | 3 | 5 | 10 |
| 2.46 | . $193 \mathrm{db} / \mathrm{km}$ | . 049 | . 004 | . 0007 |
| 6.0 (moderate) | . 615 | . 192 | . 012 | . 0017 |
| 22.6 (heavy) .. | 2.40 | . 728 | . 053 | . 0070 |
| 43.1 (cloudburst) | 6.17 | 1.64 | . 165 | . 016 |

${ }^{155}$ Adapted from article by L. Goldstein in Summary Technical Report of the National Defense Research Committee, Committee on Propagation, vol. 2, p. 164, published by Academic Press.

## TABLE 464.-ATTENUATION OF MILLIMETER WAVES BY ATMOSPHERIC OXYGEN ( $\mathrm{db} / \mathrm{km}$ ) ${ }^{158}$

| Wave length ( mm ) | Attentration coeff. cient ( $\mathrm{db} / \mathrm{km}$ ) | Wave length (mm) | Attenuation coefficient ( $\mathrm{db} / \mathrm{km}$ ) | Wave length (mm) | Attenua- tion coeff- cient $(\mathrm{db} / \mathrm{km})$ | Wavelength (mm) | Attenua tion coeff. cient <br> ( $\mathrm{db} / \mathrm{km}$ ) | Wavelength (mm) | Attenua- tion coefficient <br> ( $\mathrm{db} / \mathrm{km}$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6.34 | . 05 | 5.60 | 1.8 | 5.19 | 12.7 | 5.10 | 13.9 | 4.96 | 14.7 |
| 5.76 | 1.0 | 5.28 | 10.2 | 5.13 | 15.7 | 5.04 | 14.5 | 4.48 | . 4 |

${ }^{156}$ Lamont, H. R., Proc. Phys. Soc. London, vol. 61, p. 562, 1948.

# TABLE 465.-EXTRATERRESTRIAL RADIO FREQUENCY RADIATION* <br> Part 1.-Discrete sources 

| Source | - ${ }^{\text {a }}$ | $\delta$ | Reported by ${ }^{157}$ | Remarks |
| :---: | :---: | :---: | :---: | :---: |
| Cygnus | $20^{\text {h }} 00^{\text {m }}$ | $+43^{\circ}$ | Hey, Parsons, Phillips ${ }^{\text {c }}$ | Approx. position; $\lambda \approx 5 \mathrm{~m}$. |
| Cygnus A | 1959 | +41 ${ }^{\circ} 41^{\prime}$ | Bolton ${ }^{\text {a }}$ | Uncertainty of position about $1^{\circ}$. Observed on $100 \mathrm{Mc} / \mathrm{s}$. |
| Cygnus | $19^{\mathrm{h}} 58^{\mathrm{m}} 47^{\mathrm{g}} \pm 10^{\text {s }}$ | $+41^{\circ} 41^{\prime} \pm 7^{\prime}$ | Bolton and Stanley ${ }^{\text {P }}$ | Observed on $100,60,85,200$ $\mathrm{Mc} / \mathrm{s}$. |
| Cygnus | $19^{\mathrm{h}} 56^{\mathrm{m}} .5$ | $+39^{\circ} 50^{\prime}$ | Ryle and Smith ${ }^{\text {d }}$ | Observed on $80 \mathrm{Mc} / \mathrm{s}$. |
| Cygnus ......... | 2030 | $+38^{\circ}$ | Hey, Parsons, Phillips ${ }^{\text {g }}$ | Observed on $64 \mathrm{Mc} / \mathrm{s}$; position very uncertain. |
| Ursa Major | 1218.2 | $+58^{\circ} 00$ | Ryle and Smith ${ }^{\text {d }}$ | Observed on $80 \mathrm{Mc} / \mathrm{s}$. |
| Taurus A ....... | 513 | $+28^{\circ}$ | Bolton ${ }^{\text {a }}$ | Angular width $<30^{\circ}$; uncertainty of position about $1^{\circ}$. Observed on $100 \mathrm{Mc} / \mathrm{s}$. |
| Taurus A | $5^{\prime \prime} 31^{\prime \prime \prime} 00^{s} \pm 30^{\text {s }}$ | $+22^{\circ} 01^{\prime}$ | Bolton, Stanley, Slee ${ }^{\text {b }}$ | Intensity measured at $100 \mathrm{Mc} / \mathrm{s}$. |
| Taurus A | $53120 \pm 30$ | $+22^{\circ} 02^{\prime} \pm 8^{\prime}$ | Bolton, Stanley ${ }^{\text {h }}$ | Observed on $100 \mathrm{Mc} / \mathrm{s}$. |
| Cassiopeia ....... | $23^{\mathrm{h}} 17^{\mathrm{m}} .5$ | $+58^{\circ} 10^{\prime}$ | Ryle and Smith ${ }^{\text {d }}$ | Observed on $80 \mathrm{Mc} / \mathrm{s}$. |
| Possible sources .. |  | $\begin{aligned} & +46^{\circ} 11^{\prime} \\ & +5714 \\ & +48 \\ & +24 \\ & +2 \end{aligned}$ | $\left.\begin{array}{l} \text { Ryle } \\ \text { Ryle } \\ \text { Ryle } \\ \text { Ryle } \\ \text { Ryle } \end{array}\right\}$ | Obsered on $80 \mathrm{Mc} / \mathrm{s}$. |
| Coma Berenices A. | 1204 | $+20^{\circ} 30^{\prime}$ | Bolton ${ }^{\text {a }}$ | Angular width $<15^{\prime}$; uncertainty of position about $1^{\circ}$. Observed on $100 \mathrm{Mc} / \mathrm{s}$. |
| Hercules A | 1621 | +15 | Bolton ${ }^{\text {a }}$ | Angular width $<1^{\circ}$; uncertainty of position about $1^{\circ}$. Observed on $100 \mathrm{Mc} / \mathrm{s}$. |
| Virgo A | $12^{\text {h }} 28^{1 / 10} 06^{\text {a }} \pm 37^{\text {s }}$ | $+12^{\circ}+11^{\prime} \pm 10^{\prime}$ | Bolton, Stanley, Slee ${ }^{\text {b }}$ | Intensity measured at $100 \mathrm{Mc} / \mathrm{s}$. |
| Centaurus A ..... | $132220 \pm 60$ | $-42^{\circ} 37^{\prime} \pm 8^{\prime}$ | Bolton, Stanley, Slee ${ }^{\text {b }}$ | Intensity measured at $100 \mathrm{Mc} / \mathrm{s}$. |

[^198]Part 2.-Galactic noise from direction of Sagittarius '

| L 己 0 0 0 |  | $\begin{aligned} & \text { 淢 } \\ & \text { E } \\ & \text { U } \\ & \text { IE } \\ & \text { IE } \end{aligned}$ |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\Delta} \\ & \text { 2 } \\ & 0.0 \\ & 0 . \end{aligned}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Moxon | 40 | 750.0 | 30,000 | $35 \times 70$ | Reber | 480 | 62.5 | $2302 \times 3$ |
| Hey, Parsons, and Phillips | 65 | 462.5 | 10,500 | $12 \times 30$ | Reber | 900 | 33.3 |  |
| Moxon | 90 | 333.3 | 3,000 | $35 \times 35$ | Southworth | 3000 | 10.0 | Negative results but due to low |
| Reber | 160 | 187.5 | 5,300 | $6 \times 8$ | Reber | 3300 | 9.1 | sensitivity can only say |
| Moxon | 200 | 150.0 | 300 |  | Southworth | 30,000 | 1.0 | $T_{\nu} \ll 20,000$ |

Part 3.-Constant component of solar noise '

|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Piddington and Minnett ... | 24,000 | 1.25 | $1.0 \times 10^{4} \pm 10 \%$ | Lehany and Yabsley.. 600 |  | $.5 \times 10^{6} \pm 20 \%$ |
| Dicke and Beringer | 24,000 | 1.25 | $1.0 \times 10^{4}$ | Reber .............. 480 | 62.5 | $1.0 \times 10^{6}$ |
| Southworth ...... | 10,000 | 3 | $1.8 \times 10^{4}$ | McCready, Pawsey and Payne-Scott ........ 200 | 150. | $1.2 \times 10^{6}$ |
| Sander | 9,375 | 3.2 | $2.2 \times 10^{4}$ | Pawsey and Yabsley.. 200 | 150. | . $7 \times 10^{6}$ |
| Southworth | 3,000 | 10 | $1.8 \times 10^{4}$ | Lehany and Yabsley.. 200 | 150. | $1.0 \times 10^{6}$ |
| Covington | 2,804 | 10.7 | $5.6 \times 10^{4}$ | Ryle and Vonberg.... 175.4 | 171. | . $6 \times 10^{8}$ |
| Covington | 2,804 | 10.7 | $6.5 \times 10^{4}$ | Reber ............. 160 | 187. | $1.8 \times 10^{6}$ |
| Lehany and Yabsley. | 1,200 | 25 | $1.0 \times 10^{5} \pm 20 \%$ | Ryle and Vonberg.... 80 | 375. | $1.3 \times 10^{6}$ |

[^199]TABLES 466-494.-MAGNETIC PROPERTIES OF MATERIALS

## TABLE 466.-DEFINITIONS*, BASIC EQUATIONS, AND GENERAL DISCUSSION

$B$, flux density (magnetic) induction, $=\phi / A=4 \pi I+H$; unit the gauss, maxwell per cm .
Diamagnetic substances, $\mu<1$, $\kappa$ negative. Most diamagnetic substance known is $\mathrm{Bi}, \mu=$ $.9998 \kappa=-14 \times 10^{-6}$.
Ferromagnetic substances, $\mu$ very large, $\kappa$ very large: $\mathrm{Fe}, \mathrm{Ni}, \mathrm{Co}$, Heusler's alloy (see Table 476), magnetite and a few alloys of Mn. $\mu$ for Heusler's alloy, 90 to 100 for $B=$ 2,200; for Si sheet steel 350 to 5,300 .
$H$, field strength, $=$ No. of lines of force crossing unit area in normal direction; unit $=$ gauss $=$ one line per unit area.
Hall effect (galvanomagnetic difference of potential), Ettinghausen effect (galvanomagnetic difference of temperature), Nernst effect (thermomagnetic difference of potential) and the Leduc effect (thermomagnetic difference of temperature), see Tables 519 and 521.
Hysteresis is work done in taking a $\mathrm{cm}^{3}$ of the magnetic material through a magnetic cycle $=\int H d I=(1 / 4 \pi) \int H d B$. Steinmetz's empirical formula gives a close approximation to the hysteresis loss; it is $a B^{1.6}$ where $B$ is the max. induction and $a$ is a constant (see Table 482). The retentivity ( $B_{r}$ ) is the value of $B$ when the magnetizing force is reduced to zero. The reversed field necessary to reduce the magnetism to zero is called the coercive force ( $H_{e}$ ).
$I$, intensity of magnetization or pole strength per unit area, $=\mathbf{M} / V=m / A$ where $A$ is cross section of uniformly magnetized pole face, and $V$ is the volume of the magnet. $4 \pi m / A=4 \pi I=$ No. of lines of force leaving unit area of pole.
$J$, specific intensity of magnetism, $=I / \rho$ where $\rho=$ density, $\mathrm{g} / \mathrm{cm}^{3}$.
$J_{A}, J_{M}$, similarly atomic and molecular intensity of magnetization.
$\kappa$, susceptibility; permeability relates to effect of iron core on magnetic field strength of coil; if effect be considered on iron core, which becomes a magnet of pole strength $m$ and intensity of magnetism $I$, then the ratio $I / H=(\mu-1) ; 4 \pi$ is the magnetic susceptibility per unit volume and is a measure of the magnetizing effect of a magnetic field on the material placed in the field. $\mu=4 \pi \kappa+1$.
$\mathbf{M}$, magnetic moment $=m l$, where $l$ is length between poles of magnet.
Magneto-strictive phenomena:
Joule effect: Mechanical change in length when specimen is subjected to a magnetic field. With increasing field strength, iron and some iron alloys show first a small increment $\Delta l / l=(7$ to 35$) \times 10^{-7}$, then a decrement, and for $H=1600$. $\Delta l / l$ may amount to $-(6$ to 8$) \times 10^{-6}$. Cast cobalt with increasing field first decreases, $\Delta l / l=-8 \times 10^{-6}, H=$ 150 , then increases in length, $\Delta l / l=+5 \times 10^{-6}, H=2,000$; annealed cobalt steadily contracts, $\Delta l / l=-25 \times 10^{-6}, H=2000$. Ni rapidly then slowly contracts, $\Delta l / l=-30 \times$ $10^{-6}, H=100 ;-35 \times 10^{-6}, H=300 ;-36 \times 10^{-6}, H=2,000$. A transverse field generally gives a reciprocal effect.

Villari effect; really a reciprocal Joule effect. The susceptibility of an iron wire is increased by stretching when the magnetism is below a certain value, but diminished when above that value.

Wiedemann effect: The lower end of a vertical wire, magnetized longitudinally, when a current is passed through it, if free, twists in a certain direction, depending upon circumstances. A reciprocal effect is observed in that when a rod of soft iron, exposed to longitudinal magnetizing force, is twisted, its magnetism is reduced.
$\mu$, magnetic permeability, $=B / H$. Strength of field in air-filled solenoid $=H=(4 \pi / 10)$ $n i$ in gausses, $i$ in amperes, $n$, number of turns per cm length. If iron filled, induction increased, i.e., No. of lines of force per unit area, $B$, passing through coil is greater than $H ; \mu=B / H$.

Paramagnetic substances, $\mu>1$, very small but positive, $\kappa=10^{-3}$ to $10^{-6}$ : oxygen, especially at low temperatures, salts of $\mathrm{Fe}, \mathrm{Ni}, \mathrm{Mn}$, many metallic elements. (See Table 486.)

Paramagnetic substances show no retentivity or hysteresis effect. Susceptibility independent of field strength. The specific susceptibility for both para- and diamagnetic substances is independent of field strength.
$\phi$, magnetic flux, $=4 \pi m+H A$ for magnet placed in field of strength $H$ (axis parallel to field). Unit, the maxwell.

Unit pole is of such strength that it will repel another unit pole with a force of one dyne; at unit distance in free space, $4 \pi$ lines of force radiate from it. $m$, pole strength; $4 \pi m$ lines of force radiate from pole of strength $m$.

$$
\chi \text {, specific susceptibility (per unit mass) }=\kappa / \rho=J / H .
$$

$\chi_{A}$, atomic susceptibility, $=\chi \times$ (atomic weight) ; $\chi_{M}=$ molecular susceptibility.

[^200]
## TABLE 467.-MAGNETIC PROPERTIES OF VARIOUS TYPES OF IRON AND STEEL

From tests made at the National Bureau of Standards. $B$ and $H$ are measured in cgs units.

| lues of | 2000 | 4000 | 6000 | - 8000 | 10,00 |  |  | 16,000 | 8,000 | 20,000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Annealed Norway iron..H | . 81 | 1.15 | 1.60 | 2.18 | 3.06 | 4.45 | 7.25 | 23.5 | 116. |  |
|  | 2470 | 3480 | 3750 | 3670 | 3270 | 2700 | 1930 | 680 |  |  |
| Cast semi-steel |  | 2.90 | 4.3 | 6.46 |  | 15.1 | . 9 | . 5 |  | 325. |
|  | 000 | 1380 |  |  | 102 | 795 | 563 | 317 |  | 62. |
| Machinery steel | 5.0 | 8.8 | 13.1 | 18.6 | 25.8 | 35.8 | 50.5 | 76.0 | 142. |  |
|  | 400 | 455 | 460 | 430 | 390 | 340 | 280 | 210 |  |  |
|  | 3.30 | 4.48 | 6.35 | 9.10 | 13.0 | 18.9 | 28.8 | 47.0 | 103. | 240. |
|  | 606 | 893 | 945 | 880 | 770 | 635 | 486 | 340 |  | 83 |
| $\left.\begin{array}{l}\text { Annealed in vacuo } \\ \text { from } 900^{\circ} \mathrm{C}\end{array}\right\}$ | . 46 | . 60 | . 80 | 1.02 | 1.38 | 2.00 | 3.20 | 11.3 | 72.0 | 194. |
|  | 4350 | 6670 | 7500 | 7840 | 7250 | 6000 | 4380 | 1420 | 250 | 103 |
| As received................. $H_{\text {max }}$ After annealing............. $H_{\max }$ |  |  |  |  |  |  |  |  |  | - 2.8 |
|  |  | 150 |  | $B_{\text {max }}$ | 19,500, |  | 。 | .53 |  |  |

## TABLE 468.-MAGNETIC PROPERTIES OF ELECTRICAL SHEETS

From tests made at the National Bureau of Standards. $B$ and $H$ are measured in cgs units.

| Values of $B$ |  | 2000 | 4000 | 6000 | 8000 | 10,000 | 12,00 | 14,0 | 16,00 | 18,000 | 20,000 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dynamo steel | H | 1.00 | 1.10 | 1.43 | 2.00 | 3.10 | 4.95 | 9.20 | 34.0 | 114. |  |
|  | $\mu$ | 2000 | 3640 | 4200 | 4000 | 3220 | 2420 | 1520 | 470 | 158 |  |
| $\left.\begin{array}{l} \text { Ordinary trans- } \\ \text { former steel } \end{array}\right\}$ | H | . 60 | . 87 | 1.10 | 1.48 | 2.28 | 3.85 | 10.9 | 43.0 | 149. | - |
|  | $\mu$ | 3340 | 4600 | 5450 | 5400 | 4380 | 3120 | 1280 | 372 | 121 | - |
| $\left.\begin{array}{l} \text { High silicon trans- } \\ \text { former steel } \end{array}\right\}$ | H | . 50 | . 70 | . 90 | 1.28 | 1.99 | 3.60 | 9.80 | 47.4 | 165. | - |
|  | $\mu$ | 4000 | 5720 | 6670 | 6250 | 5020 | 3340 | 1430 | 338 | 109 |  |

## TABLE 469.-MAGNETIC PROPERTIES OF IRON IN VERY WEAK FIELDS

The effect of very small magnetizing forces has been studied by C. Baur and by Lord Rayleigh. The following short table is taken from Baur's paper, and is taken by him to indicate that the susceptibility is finite for zero values of $H$ and for a finite range increases in simple proportion to $H$. He gives the formula $k=15+100 \mathrm{H}$, or $I=15 \mathrm{H}+$ $100 \mathrm{H}^{2}$. The experiments were made on an annealed ring of round bar 1.013 cm radius, the ring having a radius of 9.432 cm . Lord Rayleigh's results for an iron wire not annealed give $k=6.4+5.1 H$, or $I=6.4 H+5.1 H^{2}$. The forces were reduced as low as 0.00004 cgs, the relation of $k$ to $H$ remaining constant.

| First experiment |  |  | Second experiment |  |
| :---: | :---: | :---: | :---: | :---: |
| H | $k$ | I | H | $k$ |
| . 01580 | 16.46 | 2.63 | . 0130 | 15.50 |
| . 03081 | 17.65 | 5.47 | . 0847 | 18.38 |
| . 07083 | 23.00 | 16.33 | . 0946 | 20.49 |
| . 13188 | 28.90 | 38.15 | . 1864 | 25.07 |
| . 23011 | 39.81 | 91.56 | . 2903 | 32.40 |
| . 38422 | 58.56 | 224.87 | . 3397 | 35.20 |

TABLE 470.-TYPICAL DATA FOR MAGNETIC MATERIALS ${ }^{157 \pi}$
Part 1.-High-permeability materials


[^201]TABLE 470.-TYPICAL DATA FOR MAGNETIC MATERIALS (concluded)

| Material | Percent composition (remainder Fe ) | Heat treatment * (temperature, ${ }^{\circ} \mathrm{C}$ ) | Magnetizing force Hmax. oersteds | Coercive force $H_{e}$ oersteds | Residual induction $B_{r}$ gatusses | Energy product BHmax. $\times 10^{-8}$ | Method of fabrication $\dagger$ | Mechanical Properties $\ddagger$ | Weight lb/in. ${ }^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Carbon steel | $1 \mathrm{Mn}, 0.9 \mathrm{C}$ | Q 800 | 300 | 50 | 10,000 | . 20 | HR, M, P | H, S | . 280 |
| Tungsten steel | $5 \mathrm{~W}, 0.3 \mathrm{Mn}, 0.7 \mathrm{C}$ | Q 850 | 300 | 70 | 10,300 | . 32 | HR, M, P | H, S | . 292 |
| Chromium steel | $3.5 \mathrm{Cr}, 0.9 \mathrm{C}, 0.3 \mathrm{Mn}$ | Q 830 | 300 | 65 | 9,700 | . 30 | HR, M, P | H, S | . 280 |
| 17\% Cobalt steel | $17 \mathrm{Co}, 0.75 \mathrm{C}, 2.5 \mathrm{Cr}, 8 \mathrm{~W}$ | Q | 1,000 | 150 | 9,500 | . 65 | HR, M, P | H, S | - |
| $36 \%$ Cobalt steel | $36 \mathrm{Co}, 0.7 \mathrm{C}, 4 \mathrm{Cr}, 5 \mathrm{~W}$ | Q 950 | 1,000 | 240 | 9,500 | . 97 | HR, M, P | H, S | . 296 |
| Remalloy or Comol | $17 \mathrm{Mo}, 12 \mathrm{Co}$ | Q 1200, В 700 | 1,000 | 250 | 10,500 | 1.1 | HR, M, P | H | . 295 |
| Indalloy (sintered) | - Mo, - Co |  | 1,000 | 240 | 9,000 | . 9 | HR, M, P | H | . 290 |
| Alnico I ....... | $12 \mathrm{Al}, 20 \mathrm{Ni}, 5 \mathrm{Co}$ | A 1200, B 700 | 2,000 | 440 | 7,200 | 1.4 | C, G | H, B | . 249 |
| Alnico II | $10 \mathrm{Al}, 17 \mathrm{Ni}, 2.5 \mathrm{Co}, 6 \mathrm{Cu}$ | A 1200, В 600 | 2,000 | 550 | 7,200 | 1.6 | C, G | H, B | .256 |
| Alnico II (sintered) | $10 \mathrm{Al}, 17 \mathrm{Ni}, 2.5 \mathrm{Co}, 6 \mathrm{Cu}$ | A 1300 | 2,000 | 520 | 6,900 | 1.4 | Sn, G | H | . 249 |
| Alnico IV ........ | $12 \mathrm{Al}, 28 \mathrm{Ni}, 5 \mathrm{Co}$ | Q 1200, B 650 | 3,000 | 700 | 5,500 | 1.3 | Sn, C, G | H | . 253 |
| Alnico V | $8 \mathrm{Al}, 14 \mathrm{Ni}, 24 \mathrm{Co}, 3 \mathrm{Cu}$ | AF 1300, B 600 | 2,000 | 550 | 12,500 | 4.5 | C, G | H, B | . 264 |
| Alnico VI | $8 \mathrm{Al}, 15 \mathrm{Ni}, 24 \mathrm{Co}, 3 \mathrm{Cu}, 1 \mathrm{Ti}$ | AF 1300, B600 | 3,000 | 750 | 10,000 | 3.5 | C, G | H, B | .268 |
| Alnico XII | $6 \mathrm{Al}, 18 \mathrm{Ni}, 35 \mathrm{Co}, 8 \mathrm{Ti}$ | - - | 3,000 | 950 | 5,800 | 1.5 | C, G | H, B | . 26 |
| Vicalloy I | $52 \mathrm{Co}, 10 \mathrm{~V}$ | B 600 | 1,000 | 300 | 8,800 | 1.0 | C, CR, M, P | D | . 295 |
| Vicalloy II (wire) | $52 \mathrm{Co}, 14 \mathrm{~V}$ | CW + B 600 | 2,000 | 510 | 10,000 | 3.5 | C, CR, M, P | D | . 292 |
| Cunife (wire) ... | $60 \mathrm{Cu}, 20 \mathrm{Ni}$ | $C W+B 600$ | 2,400 | 550 | 5,400 | 1.5 | C, CR, M, P | D, M | . 311 |
| Cunico . . . . . . | $50 \mathrm{Cu}, 21 \mathrm{Ni}, 29 \mathrm{Co}$ | CW + B600 | 3,200 | 660 | 3,400 | . 80 | C, CR, M, P | D, M | . 300 |
| Vectolite | $30 \mathrm{Fe}_{2} \mathrm{O}_{3}, 44 \mathrm{Fe}_{3} \mathrm{O}_{4}, 26 \mathrm{C}_{2} \mathrm{O}_{3}$ | - - | 3,000 | 1,000 | 1,600 | . 60 | Sn, G | W | . 113 |
| Silmanal | 86.8 Ag, 8.8 Mn, 4.4 Al |  | 20,000 | 6,000 ${ }^{2}$ | 550 | . 075 | C, CR, M, P | D, M | . 325 |
| Platinum-cobalt | $77 \mathrm{Pt}, 23 \mathrm{Co}$ | Q 1200, B 650 | 15,000 | 3,600 | 5,900 | 6.5 | C, CR, M | D | - |
| Hyflux . . . . . . . | Fine powder | - - | 2,000 | 390 | 6,600 | . 97 | - | - | 176 |

[^202]| Induction data |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Values of B 2 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 |
| Carbon steel $\ldots$...........H | 33 | 50 | 61 | 72 | 93 | 155 | 290 | 600 | - |
| . $9 \mathrm{C}, .5 \mathrm{Mn}, .2 \mathrm{Si}, \mathrm{Bal} \mathrm{Fe} . . \mu$ | 60 | 80 | 98 | 111 | 108 | 77 | 48 | 27 |  |
| Chrome ..................H | 32 | 48 | 61 | 75 | 100 | 175 | - | - | - |
| Bar, 3.5 Cr, 0.9 C.......... $\mu$ | 63 | 83 | 98 | 107 | 100 | 69 | - | - | - |
| Chrome ................. H | 30 | 44 | 52.5 | 62 | 75 | 155 | 235 | - | - |
| Sheet, 5.75 Cr, 1.25 C...... $\mu$ | 67 | 91 | 114 | 129 | 133 | 104 | 60 | - | - |
| Chrome $\ldots$................ H | 36 | 47.5 | 64 | 80 | 122 | - | - | - |  |
| Sheet, 5.75 Cr, $10 \mathrm{C} . . . . . . . . \mu$ | 56 | 84 | 94 | 100 | 82 | - | - | - | - |
| Tungsten steel $\ldots \ldots \ldots . . . \mathrm{H}$ | 35 | 52.5 | 63 | 70 | 81.5 | 115 | 195 | 195 | 500 |
| 0.6 C, $5 \mathrm{~W}, 0.5 \mathrm{Mn}, 0.2 \mathrm{Si} . . \mu$ | 57 | 76 | 95 | 114 | 123 | 104 | 72 | 72 | 32 |
| Cobalt .................... H | 140 | 203 | 240 | 269 | 313 | 413 | 649 | - | - |
| Bar, $36 \mathrm{Co}, 3.5 \mathrm{Cr}, 3.0 \mathrm{~W} . . . \mu$ | 14 | 20 | 25 | 30 | 32 | 29 | 22 | - | - |
|  | 134 | 201 19.9 | $\stackrel{237}{25.3}$ | 258 31 | 290 34.5 | 369 32.5 | $\stackrel{651}{21.5}$ | 1355 11.8 | 2571 |
| $12 \mathrm{Co}, 17 \mathrm{Mo}$, Bal Fe...... ${ }^{\mu}$ | 14.9 | 19.9 | 25.3 | 31 | 34.5 | 32.5 | 21.5 | 11.8 | 7 |
| Alnico $1 \ldots \ldots . . . . . . . . . . . \mathrm{H}$ | 280 | 400 | 478 | 582 | 910 | 1820 | - | - | - |
| $12 \mathrm{Al}, 20 \mathrm{Ni}, 5 \mathrm{Co}$, Bal Fe.. $\mu$ | 7.1 | 10.0 | 12.6 | 13.8 | 11.0 | 6.6 | - | - | - |
|  | 360 | 560 | 668 | 785 | 1020 | 1680 | - | - | - |
| Cast, $10 \mathrm{Al}, 17 \mathrm{Ni}, 12.5 \mathrm{Co.}. \mu$ | 5.6 | 7.1 | 9.0 | 10.2 | 9.8 | 7.1 | - | - |  |
| Alnico $2 \ldots . . . . . . . . . . . . . . H$ | 340 | 515 | 605 | 760 | 1200 | 1800 | - | - |  |
| Sintered, $10 \mathrm{Al}, 17 \mathrm{Ni} . . . . . . \mu$ | 5.9 | 7.8 | 9.9 | 10.5 | 8.3 | 6.7 | - | - |  |
| Alnico $3 \ldots \ldots \ldots . . . . . .$. H | 305 | 473 | 565 | 698 | 1035 | 2000 | - | - | - |
| $12 \mathrm{Al}, 2.5 \mathrm{Ni}$, Bal Fe....... $\mu$ Up to $5 / 8 \times 5 / 8^{\prime \prime}$ cross section | 6.6 | 8.5 | 10.6 | 11.5 | 9.7 | 6.0 | - | - | - |
|  | 279 | 395 | 478 | 575 | 940 | 1910 |  |  |  |
| Cast, $12 \mathrm{Al}, 25 \mathrm{Ni}$, Bal Fe. . $\mu$ $5 / 8 \times 5 / 8^{\prime \prime}$ cross section and over | 7.2 | 10.1 | 12.5 | 13.9 | 10.6 | 6.3 | - | - | - |
| Alnico 4 .................. H | 500 | 850 | 1075 | 1350 | 1890 | - | - | - |  |
| Cast, and sintered .......... $\mu$ $12 \mathrm{Al}, 28 \mathrm{Ni}, 5 \mathrm{Co}$, Bal Fe | 4.0 | 4.7 | 5.6 | 5.9 | 5.3 | - | - | - | - |
| Alnico 5 ................. H | 468 | 560 | 580 | 580 | 598 | 640 | 945 | - | - |
| Cast, $8 \mathrm{Al}, 14 \mathrm{Ni}, 24 \mathrm{Co}$, $3 \mathrm{Cu}, \mathrm{Bal} \mathrm{Fe}$. | 4.3 | 7.1 | 10.3 | 13.8 | 16.7 | 18.8 | 148 | - | - |
| Alnico 6 .................. H | 430 | 675 | 770 | 845 | 940 | 1110 | 1700 | - | - |
| Cast, $8 \mathrm{Al}, 15 \mathrm{Ni}, 24 \mathrm{Co}$, $3 \mathrm{Cu}, 1.25 \mathrm{Ti}$, Bal Fe .. | 4.7 | 5.9 | 7.8 | 9.5 | 10.6 | 10.8 | 8.2 | - | - |
| Alnico $12 \ldots . . . . . . . . . . . . . H$ | 610 | 1000 | 1300 | 1600 | 2000 | 3000 | - | - | - |
| Cast, $6 \mathrm{Al}, 18 \mathrm{Ni}, 35 \mathrm{Co}$, $8 \mathrm{Ti}, \mathrm{Bal} \mathrm{Fe}$. | 3.3 | 4.0 | 4.6 | 5.0 | 5.0 | 4.8 | - | - | - |
| Cunife ................... ${ }^{\text {H }}$ | 530 | 645 | 845 | - | - | - | - | - | - |
| Under $.155^{\prime \prime}$ dia. 60 Cu , 20 Ni, Bal Fe.......... $\mu$ | 3.8 | 6.2 | 7.1 | - | - | - | - | - | - |
| Cunico .................. H | 590 | 1000 | 1630 | 3200 | - | - |  |  |  |
| $50 \mathrm{Cu}, 21 \mathrm{Ni}, 29 \mathrm{Co} . . . . . . . . \mu$ | 3.4 | 4.0 | 3.7 | 2.5 | - | - |  | - | - |
| Vectolite ................H | 1110 | 2050 | 3700 | - | - | - | - | - | - |
| $\begin{aligned} & 30 \mathrm{Fe}_{2} \mathrm{O}_{3}, 44 \mathrm{Fe}_{3} \mathrm{O}_{4} \\ & 26 \mathrm{Co}_{2} \mathrm{O}_{3} \ldots \ldots \ldots \ldots \ldots \ldots . . \end{aligned}$ | 1.8 | 2.0 | 1.7 | _ | - | - | - | - | - |
| Silmanal |  |  |  | Max | mum $\mu$ | 1.111 |  |  |  |

[^203]

TABLE 473.-MAXIMUM CORE LOSSES IN ELECTRICAL STEEL SHEETS

| Designation Thickness, in.: | Watts per lb for 60 cycles |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | . 0140 | . 0155 | . 0170 | . 0185 | . 0220 | . 0250 | . 0280 | . 0310 |
|  | At 10,000 gausses |  |  |  |  |  |  |  |
| Armature AISI M-43. | 1.30 | 1.38 | 1.46 | 1.55 | 1.75 | 1.98 | 2.23 | 2.50 |
| Electrical AISI M-36 | 1.17 | 1.23 | 1.29 | 1.35 | 1.50 | 1.70 | 1.94 | 2.17 |
| Motor AISI M-27. | 1.01 | 1.05 | 1.09 | 1.14 | 1.22 | 1.30 | 1.44 | 1.60 |
| Dynamo AISI M-22 | . 82 | . 86 | . 90 | . 94 | 1.02 | 1.10 |  |  |
| Transformer 72 AISI M-19.. | . 72 | . 76 | . 80 | . 83 | . 90 | . 97 |  |  |
| Transformer 65 AISI M-17.. | . 65 | . 68 | . 72 | . 75 |  |  |  |  |
| Transformer 58 AISI M-15.. | . 58 | . 61 | . 65 | . 68 |  |  |  |  |
| Transformer 52 AISI M-14.. | . 52 |  |  |  |  |  |  |  |
| Transformer 100 AISI M-10.. |  |  |  |  |  |  |  |  |
| Transformer 90 A IS $\mathrm{M}-9 .$. |  |  |  |  |  |  |  |  |
| At 15,000 gausses |  |  |  |  |  |  |  |  |
| Armature AISI M-43. | 4.30 | 4.37 | 4.44 | 4.50 | 4.80 | 5.30 | 5.85 | 6.50 |
| Electrical AISI M-36. | 3.60 | 3.67 | 3.74 | 3.80 | 4.10 | 4.40 | 4.95 | 5.50 |
| Motor AISI M-27. | 2.65 | 2.75 | 2.85 | 2.95 | 3.20 | 3.40 | 3.70 | 4.10 |
| Dynamo AISI M-22. | 1.85 | 2.23 | 2.31 | 2.40 | 2.60 | 2.80 |  |  |
| Transformer 72 AISI M-19.. | 1.65 | 1.93 | 2.02 | 2.10 | 2.25 | 2.40 |  |  |
| Transformer 65 AISI M-17.. | 1.50 | 1.72 | 1.80 | 1.88 |  |  |  |  |
| Transformer 58 AISI M-15.. | 1.40 | 1.57 | 1.65 | 1.73 |  |  |  |  |
| Transformer 52 AISI M-14.. |  |  |  |  |  |  |  |  |
| Transformer 100 AISI M-10.. |  |  |  |  |  |  |  |  |
| Transformer 90 AISI M-9... |  |  |  |  |  |  |  |  |


| Nickel at $0^{\circ}$ and $100^{\circ} \mathrm{C}$ |  |  |  |  | Cobalt at $0^{\circ}$ and $100^{\circ} \mathrm{C}$ |  |  |  |  | Magnetite * |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| H | $s$ | $I$ | $B$ | $\mu$ |  | $S$ | I | B | $\mu$ |  | I | B | ${ }^{\mu}$ |
| 100 | 35.0 | 309 | 3980 | 39.8 | 200 | 106 | 848 | 10850 | 54.2 | 500 | 325 | 4580 | 9.16 |
| 200 | 43.0 | 380 | 4966 | 24.8 | 300 | 116 | 928 | 11960 | 39.9 | 1000 | 345 | 5340 | 5.34 |
| 300 | 46.0 | 406 | 5399 | 18.0 | 500 | 127 | 1016 | 13260 | 26.5 | 2000 | 350 | 6400 | 3.20 |
| 500 | 50.0 | 441 | 6043 | 12.1 | 700 | 131 | 1048 | 13870 | 19.8 | 12000 | 350 | 16400 | 1.37 |
| 700 | 51.5 | 454 | 6409 | 9.1 | 1000 | 134 | 1076 | 14520 | 14.5 |  |  |  |  |
| 1000 | 53.0 | 468 | 6875 | 6.9 | 1500 | 138 | 1104 | 15380 | 10.3 |  |  |  |  |
| 1500 | 56.0 | 494 | 7707 | 5.1 | 2500 | 143 | 1144 | 16870 | 6.7 |  |  |  |  |
| 2500 | 58.4 | 515 | 8973 | 3.6 | 4000 | 145 | 1164 | 18630 | 4.7 |  |  |  |  |
| 4000 | 59.0 | 520 | 10540 | 2.6 | 6000 | 147 | 1176 | 20780 | 3.5 |  |  |  |  |
| 6000 | 59.2 | 522 | 12561 | 2.1 | 9000 | 149 | 1192 | 23980 | 2.6 |  |  |  |  |
| 9000 | 59.4 | 524 | 15585 | 1.7 | At $0^{\circ} \mathrm{C}$ this specimen gave the following results: |  |  |  |  |  |  |  |  |
| 12000 | 59.6 | 526 | 18606 | 1.5 |  |  |  |  |  |  |  |  |  |
| At $0^{\circ}$ | C this | s spe | cimen | gave | 7900 | 154 | 1232 | 23380 | 3.0 |  |  |  |  |

the following results: $\begin{array}{llllllll}12300 & 67.5 & 595 & 19782 & 1.6\end{array}$
*These results are given by Du Bois for a specimen of magnetite.
$S=$ Magnetic moment per gram. $I=$ Magnetic moment per $\mathrm{cm}^{3}$.

Professor Ewing has investigated the effects of very intense fields on the induction in iron and others metals. The results show that the intensity of magnetization does not increase much in iron after the field has reached an intensity of 1000 cgs units, the increase of induction above this being almost the same as if the iron were not there, that is to say, $d B / d H$ is practically unity. For hard steels, and particularly mangapese steels, much higher forces are required to produce saturation. Hadfield's manganese steel seems to have nearly constant susceptibility up to a magnetizing force of 10,000 . The following tables, taken from Ewing's papers, illustrate the effects of strong fields on iron and steel. The results for nickel and cobalt do not differ greatly from those given above.

| Lowmoor wrought iron |  |  |  | Vicker's tool steei |  |  |  | Hadfield's manganese steel |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| H | I | $B$ | $\mu$ | H | I | B | $\mu$ | H | I | $B$ | ${ }^{\mu}$ |
| 3080 | 1680 | 24130 | 7.83 | 6210 | 1530 | 25480 | 4.10 | 1930 | 55 | 2620 | 1.36 |
| 6450 | 1740 | 28300 | 4.39 | 9970 | 1570 | 29650 | 2.97 | 2380 | 84 | 3430 | 1.44 |
| 10450 | 1730 | 32250 | 3.09 | 12120 | 1550 | 31620 | 2.60 | 3350 | 84 | 4400 | 1.31 |
| 13600 | 1720 | 35200 | 2.59 | 14660 | 1580 | 34550 | 2.36 | 5920 | 111 | 7310 | 1.24 |
| 16390 | 1630 | 36810 | 2.25 | 15530 | 1610 | 35820 | 2.31 | 6620 | 187 | 8970 | 1.35 |
| 18760 | 1680 | 39900 | 2.13 |  |  |  |  | 7890 | 191 | 10290 | 1.30 |
| 18980 | 1730 | 40730 | 2.15 |  |  |  |  | 8390 | 263 | 11690 | 1.39 |
|  |  |  |  |  |  |  |  | 9810 | 396 | 14790 | 1.51 |

## TABLE 475.-EFFECT OF TEMPERATURE ON PERMEABILITY OF NICKEL-IRON ALLOY (47-50 Ni) ${ }^{158}$

| $\stackrel{\text { Test }}{\text { Temp. }}{ }^{\circ} \mathrm{F}$ | $B$ (gausses) at $30 H$ (oersteds) | $\begin{gathered} \text { Maximum } \\ \text { permeability } \\ (B / H) \end{gathered}$ | $B \underset{\substack{\text { maximum } \\ \text { permeability } \\(B / H)}}{\text { (gauses) }}$ | Permeability ( $B / H$ ) at 100 gausses |
| :---: | :---: | :---: | :---: | :---: |
| 390 | 11500 | 79000 | 4600 | 8000 |
| 190 | 11850 | 59000 | 4400 | 7000 |
| 80 | 12000 | 49000 | 4700 | 6100 |
| 32 | 12000 | 44000 | 5200 | 5600 |
| - 42 | 12200 | 34000 | 6000 | 4500 |
| -100 | 12300 | 30000 | 7000 | 4200 |

[^204]Several alloys have been experimented with that, although all the constitutents are nonmagnetic or very weakly magnetic materials, have quite definite magnetic properties. Among these are Nos. 1-3 below, Heusler magnetic alloys. Some alloys made up for the most part of magnetic elements are nonmagnetic or very weakly magnetic, i.e., No. 4 below.

1. $61 \mathrm{Cu}, 25 \mathrm{Mg}, 14 \mathrm{Al}$
magnetic with a permeability $\mu$ of 33.
2. $75.6 \mathrm{Cu}, \mathrm{Mn} 14.3, \mathrm{Al} 10.1, \mathrm{~Pb}$
magnetic $B_{r}=480, \quad H_{0}=3.8, \mu$ $\max =80$.
3. $\mathrm{Cu} 61.5, \mathrm{Mn} 23.5, \mathrm{Al} 15$
$B_{r}=2550, \quad H_{c}=7.3, \mu \max =$ 236.
4. $\mathrm{Cu} 78, \mathrm{Fe} 12, \mathrm{Mg}$ nonmagnetic.

TABLE 477.-PERMEABILITY OF SOME SPECIMENS OF IRON AND STEEL
This table gives the induction and the permeability for different values of the magnetizing force of some of the specimens in Table 493. The specimen numbers refer to the same table. The numbers have been taken from the curves given by Hopkinson and may therefore be slightly in error; they are the mean values for rising and falling magnetizations.

| Magnetizing force | Specimen 1 (iron) |  | Specimen 8 (annealed steel) |  | Specimen 9 (same as 8 tempered) |  | $\begin{gathered} \text { Specimen } \\ \text { (cast iron) } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $B$ | ${ }_{\mu}$ | $B$ | $\mu$ | B | $\stackrel{\mu}{\mu}$ | B | $\stackrel{4}{4}$ |
| 1 |  | - | - | - | - |  | 265 | 265 |
| 2 | 200 | 100 | - | - | - | - | 700 | 350 |
| 3 |  |  |  |  |  |  | 1625 | 542 |
| 5 | 10050 | 2010 | 1525 | 300 | 750 | 150 | 3000 | 600 |
| 10 | 12550 | 1255 | 9000 | 900 | 1650 | 165 | 5000 | 500 |
| 20 | 14550 | 727 | 11500 | 575 | 5875 | 294 | 6000 | 300 |
| 30 | 15200 | 507 | 12650 | 422 | 9875 | 329 | 6500 | 217 |
| 40 | 15800 | 395 | 13300 | 332 | 11600 | 290 | 7100 | 177 |
| 50 | 16000 | 320 | 13800 | 276 | 12000 | 240 | 7350 | 149 |
| 70 | 16360 | 234 | 14350 | 205 | 13400 | 191 | 7900 | 113 |
| 100 | 16800 | 168 | 14900 | 149 | 14500 | 145 | 8500 | 85 |
| 150 | 17400 | 116 | 15700 | 105 | 15800 | 105 | 9500 | 63 |
| 200 | 17950 | 90 | 16100 | 80 | 16100 | 80 | 10190 | 51 |
| Magnetiz- <br> ing force | $\underset{(\mathrm{a}}{\mathrm{ASTM}}$ | $\begin{aligned} & 20 \text { medium } \\ & \mathrm{s} \text { cast) } \end{aligned}$ |  | ASTM | $\begin{aligned} & 0 \text { medium } \\ & \text { cast) } \end{aligned}$ |  | ASTM 40 furnace | $\begin{aligned} & \text { lectric } \\ & \text { cast) } \end{aligned}$ |
| H | B | ${ }_{\mu}$ |  | B | $\mu$ |  | B | $\mu$ |
| 5 | 1300 | 260 |  | 600 | 120 |  | 1750 | 350 |
| 10 | 3400 | 340 |  | 2550 | 255 |  | 4100 | 410 |
| 20 | 5250 | 262 |  | 4450 | 222 |  | 5950 | 297 |
| 30 | 6200 | 206 |  | 5450 | 181 |  | 6950 | 231 |
| 40 | 6950 | 173 |  | 6100 | 152 |  | 7600 | 190 |
| 50 | 7500 | 150 |  | 6700 | 134 |  | 8250 | 165 |
| 70 | 8300 | 118 |  | 7600 | 108 |  | 9100 | 130 |
| 100 | 9100 | 91 |  | 8600 | 86 |  | 10050 | 100 |
| 150 | 10150 | 67 |  | 9800 | 65 |  | 11100 | 74 |
| 200 | 11050 | 55 |  | 10650 | 53 |  | 11900 | 59 |

TABLE 478.-MAGNETIC PROPERTIES OF SOFT IRON AT $0^{\circ}$ and $100^{\circ} \mathrm{C}$

| Soft iron at $0^{\circ} \mathrm{C}$ |  |  |  |  | Soft iron at $100^{\circ} \mathrm{C}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| H | s* | ${ }_{\text {I }}+$ | B | ${ }^{\mu}$ | H | $s$ | 1 | B | $\mu$ |
| 100 | 180.0 | 1408 | 17790 | 177.9 | 100 | 180.0 | 1402 | 17720 | 177.2 |
| 200 | 194.5 | 1521 | 19310 | 96.5 | 200 | 194.0 | 1511 | 19190 | 96.0 |
| 400 | 208.0 | 1627 | 20830 | 52.1 | 400 | 207.0 | 1613 | 20660 | 51.6 |
| 700 | 215.5 | 1685 | 21870 | 31.2 | 700 | 213.4 | 1663 | 21590 | 29.8 |
| 1000 | 218.0 | 1705 | 22420 | 22.4 | 1000 | 215.0 | 1674 | 22040 | 21.0 |
| 1200 | 218.5 | 1709 | 22670 | 18.9 | 1200 | 215.5 | 1679 | 22300 | 18.6 |

TABLE 479.-MAGNETIC PROPERTIES OF STEEL AT $0^{\circ}$ and $100^{\circ} \mathrm{C}$

| Steel at $0^{\circ} \mathrm{C}$ |  |  |  |  | Steel at $100^{\circ} \mathrm{C}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| H | $S \dagger$ | I | B | $\mu$ | H | $S$ | I | B | $\mu$ |
| 100 | 165.0 | 1283 | 16240 | 162.4 | 100 | 165.0 | 1278 | 16170 | 161.7 |
| 200 | 181.0 | 1408 | 17900 | 89.5 | 200 | 180.0 | 1395 | 17730 | 88.6 |
| 400 | 193.0 | 1500 | 19250 | 48.1 | 400 | 191.0 | 1480 | 19000 | 47.5 |
| 700 | 199.5 | 1552 | 20210 | 28.9 | 700 | 197.0 | 1527 | 19890 | 28.4 |
| 1000 | 203.5 | 1583 | 20900 | 20.9 | 1000 | 199.0 | 1543 | 20380 | 20.4 |
| 1200 | 205.0 | 1595 | 21240 | 17.7 | 1500 | 203.0 | 1573 | 21270 | 14.2 |
| 3750* | 212.0 | 1650 | 24470 | 6.5 | 3000 | 205.0 | 1593 | 23020 | 7.7 |
|  |  |  |  |  | 5000 | 208.0 | 1612 | 25260 | 5.1 |

* The results in this and other tables for forces above 1200 were obtained from a small piece of the metal provided with a polished mirror surface and placed, with its polished face normal to the lines of force, between the poles of a powerful electromagnet. The induction was then inferred from the rotation of the plane of a polarized ray of red light reflected normally from the surface. (See Kerr's Constants, Tables 516, 517, 520.)
$\dagger$ Magnetic moment per grain. $\$$ Magnetic moment per $\mathrm{cm}^{2}$.

TABLE 480.-ENERGY LOSSES IN TRANSFORMER STEELS
D. C. Hysteresis data

From $B_{\max }=10,000$ gausses

| Grade | Thickness in. | $\underset{\text { oersteds }}{H_{c}}$ | $\begin{gathered} B_{r} \\ \text { gausses } \end{gathered}$ | $H_{\max }$ oersteds | $H_{c} \times{ }^{\text {r }}$ r |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Transformer 52 | . 0140 | -. 20 | 4800 | 2.03 | 960 |
| Transformer 58 | . 0140 | -. 24 | 5050 | 1.94 | 1210 |
| Transformer 65 | . 0140 | -. 31 | 5200 | 2.16 | 1610 |
| Transformer 72 | . . 0140 | -. 42 | 6200 | 2.19 | 2610 |
| Transformer 72 | . 0185 | -. 43 | 5050 | 2.58 | 2170 |
| Transformer 72 | . . 0250 | -. 50 | 5300 | 2.72 | 2650 |
| Dynamo | . 0140 | -. 51 | 6650 | 2.30 | 3400 |
| Dynamo | . . 0185 | -. 53 | 5500 | 2.85 | 2920 |
| Dynamo | . . 0250 | $-.59$ | 5750 | 2.87 | 3400 |
| Motor | . . 0140 | -. 55 | 6350 | 3.33 | 3500 |
| Motor | . . 0185 | -. 58 | 6700 | 2.80 | 3890 |
| Motor | . . 0250 | -. 63 | 6900 | 2.99 | 4350 |
| Electrical | . . 0140 | -. 62 | 7700 | 2.52 | 4770 |
| Electrical | . . 0285 | -. 61 | 8100 | 2.16 | 4950 |
| Electrical | . . 0250 | -. 68 | 8250 | 2.26 | 5610 |
| Armature | . . 0140 | -. 64 | 8350 | 2.30 | 5350 |
| Armature | . . 0185 | -. 68 | 8300 | 2.20 | 5650 |
| Armature | . . 0250 | $-.72$ | 8230 | 2.26 | 5940 |

## TABLE 481.-ENERGY LOSSES IN TRANSFORMER STEELS

a c core losses
Watts/lb for 60 cycle at 10,000 gausses

| Designation | Thickness in. | Gage | Eddy current loss | Hysteresis | Total |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Transformer 52 | . 0134 | 29 | . 149 | . 345 | 494 |
| Transformer 58 | . 0137 | 29 | . 163 | . 385 | . 548 |
| Transformer 65 | . 0136 | 29 | . 193 | . 426 | . 619 |
| Transformer 72 | . . 0136 | 29 | . 205 | . 450 | . 675 |
| Dynamo | . 0137 | 29 | . 218 | . 572 | . 790 |
| Motor | . . 0140 | 29 | . 245 | . 709 | . 954 |
| Electrical | . . 0137 | 29 | . 262 | . 852 | 1.114 |
| Armature | . . 0139 | 29 | . 486 | . 741 | 1.227 |
| Oriented C. R. st | . 0140 | 29 | . 164 | . 236 | . 40 |

C. P. Steinmetz concludes from his experiments that the dissipation of energy due to hysteresis in magnetic metals can be expressed by the formula $c=a B^{1.6}$, where $e$ is the energy dissipated and $a$ a constant. He also concludes that the dissipation is the same for the same range of induction, no matter what the absolute value of the terminal inductions may be. His experiments show this to be nearly true when the induction does not exceed $\pm 15000 \mathrm{cgs}$ units per $\mathrm{cm}^{2}$. It is possible that, if metallic induction only be taken, this may be true up to saturation; but it is not likely to be found to hold for total inductions much above the saturation value of the metal. The law of variation of dissipation with induction range in the cycle, stated in the above formula, is also subject to verification.
The following table gives the values of the constant $a$ as found by Steinmetz for a number of different specimens. The data are taken from his second paper.

| Kind of material | Description of specimen | $\underset{a}{\text { Value of }}$ |
| :---: | :---: | :---: |
| Iron | Norway iron | . 00227 |
|  | Wrought bar | . 00326 |
| " . | Commercial ferrotype plate | . 00548 |
| " | Annealed | . 00458 |
| " | Thin tin plate | . 00286 |
| " | Medium-thickness tin plate | . 00425 |
| Steel | Soft galvanized wire | . 00349 |
|  | Annealed cast steel | . 00848 |
| " | Soft annealed cast steel | . 00457 |
| " | Very soft annealed cast steel | . 00318 |
| " | Same as 8 tempered in cold water | . 02792 |
| " | Tool steel glass hard-tempered in water | . 07476 |
| " | ". ". tempered in oil | . 02670 |
| " | " " annealed $14 . \ldots$...................... | . 01899 |
| " | $\left\{\begin{array}{l}\text { Same as 12, 13, and 14, after having been subjected } \\ \text { to an alternating } \mathrm{m} . \mathrm{m} . \text { f. of from } 4000 \text { to } 6000\end{array}\right\}$ | $\left\{\begin{array}{l}.06130 \\ .02700\end{array}\right.$ |
| " $\quad$... |  | . 01445 |
| Cast iron | Gray cast iron ................ | . 01300 |
|  | "" " " containing $\frac{1}{8} \%$ aluminum | . 01365 |
|  | " " " " $\frac{1}{2} \%$ | . 01459 |
| Magnetite | A square rod $6 \mathrm{~cm}^{2}$ section and 6.5 cm long, from \{the Tilly Foster mines, Brewsters, Putnam County, | . 02348 |
| Nickel | New York, stated to be a very pure sample. Soft wire |  |
|  | \{Annealed wire, calculated by Steinmetz from | . 0156 |
| " | Ewing's experiments <br> Hardened, also from Ewing's experiments ....... | . 0385 |
| Cobalt .... | \{Rod containing about $2 \%$ of iron, also calculated $\}$ | . 0120 |
|  | \{from Ewing's experiments by Steinmetz ..........\} Consisted of thin needle-like chips obtained by milling grooves about 8 mm wide across a pile of |  |
|  | thin sheets clamped together. About $30 \%$ by volume of the specimen was iron. |  |
| Iron filings | 1 st experiment, continuous cyclic variation of $\mathrm{m} . \mathrm{m}$.\} <br> f. 180 cycles per second | . 0457 |
|  | 2d experiment, 114 cycles per second | . 0396 |
|  | 3d "1 79-91 cycles per second | . 0373 |
| Nickel alloy | Permalloy | . 00001 |
| Electrical sheet | Hipernik | . 000015 |
|  | Silicon steel $4.5 \%$ Si <br> Silicon steel $4.5 \% \mathrm{Si}$ | . 000045 |
|  | Silicon steel 4.4\% Si | . 00056 |
|  | Silicon steel $3.5 \%$ Si | . 00065 |
|  | Silicon steel $2.5 \% \mathrm{Si}$ | . 00081 |
|  | Silicon steel $1.0 \%$ Si | . 00088 |
|  | Silicon steel $0.5 \%$ Si | . 001 |
|  | Low carbon sheet | . 003 |
|  | Cast steel annealed | . 005 |
|  | Cast iron annealed | . 012 |

The relation deduced by Curie that $\chi=C / T$, where $C$ is a constant and $T$ the absolute temperature, holds for some paramagnetic substances over the ranges given in the following table. Many paramagnetic substances do not obey the law. See the following table.

| Substance | $\times 10^{\circ}$ | nge ${ }^{\circ} \mathrm{C}$ | Substance | $C \times 10^{8}$ | Range ${ }^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Oxygen | 33,700 | $20^{\circ}$ to $450^{\circ} \mathrm{C}$ | Gadolinium sulfate. | 21,000 | $-259^{\circ}$ to 17 |
| Air | 7,830 | - - - | Ferrous sulfate | 11,000 | -259 " 17 |
| Palladium | 1,520 | 20 to 1370 | Ferric sulfate | 17,000 | -208"17 |
| Magnetite | 28,000 | 850 " 1360 | Manganese chloride. | 30,000 | -258 " 17 |
| Cast iron | 38,500 | 850 " 1267 |  |  |  |

## TABLE 484.-TEMPERATURE EFFECT ( ${ }^{\circ} \mathrm{C}$ ) ON SUSCEPTIBILITY OF DIAMAGNETIC ELEMENTS *

## No effect:

B Cryst. 400 to $1200^{\circ}$
P white
S Crvst. ; ppt.
$\mathrm{Zn}-170$ to $300^{\circ}$
As
C Diamond, +170 to $200^{\circ}$
C "Sugar" carbon
Si Cryst.
-
$\mathrm{Se} \quad-$
Br
Zr
Zr
$\mathrm{Cryst}-$.170
Cd
Cd
-170 to $300^{\circ}$
$\mathrm{Sb}-170$ to $50^{\circ}$
Cd -170 to $300^{\circ}$
Cs and Au
ncrease with rise in temperature:
Be $\quad$ C Diamond, 200 to $1200^{\circ}$
B Cryst. +170 to $400^{\circ}$
Ag
I -170 to $114^{\circ}$
Decrease with rise in temperature:

| C Amorphous | Gd -179 to $30^{\circ}$ | In -170 to $150^{\circ}$ | T1 |
| :---: | :---: | :---: | :---: |
| C Ceylon graphite | $\mathrm{Ge}-170$ to $900^{\circ}$ | $\mathrm{Sb}+50$ to $+631^{\circ}$ | $\mathrm{Pb}-170$ to $327^{\circ}$ |
| Cu | Zr 500 to $1200^{\circ}$ | Te - | Bi - 170 to $268^{\circ}$ |
| $\mathrm{Zn}+300$ to $700^{\circ}$ | Cd 300 to $700^{\circ}$ | I +114 to $+200^{\circ}$ |  |

*Tables 484 and 485 are from Honda and Owen.

## TABLE 485.-TEMPERATURE EFFECT ( ${ }^{\circ} \mathrm{C}$ ) ON SUSCEPTIBILITY OF PARAMAGNETIC ELEMENTS

## No effect:

| Li | - | $\mathrm{K}-170$ to $150^{\circ}$ | $\mathrm{Cr}-170$ to $500^{\circ}$ | W |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Na}-170$ to $97^{\circ}$ | $\mathrm{Ca}-170$ to $18^{\circ}$ | $\mathrm{Mn}-170$ to $250^{\circ}$ | Os | - |
| Al 657 to $1100^{\circ}$ | $\mathrm{V}-170$ to $500^{\circ}$ | Rb | - |  |

## Increase with rise in temperature:

| $\mathrm{Ti}-40$ to $1100^{\circ}$ | $\mathrm{Cr} \mathrm{500} \mathrm{to} 1100^{\circ}$ | $\mathrm{Ru}+550$ to $1200^{\circ}$ | $\mathrm{Ba}-170$ to $18^{\circ}$ |
| :---: | :---: | :---: | :---: |
| V 500 to $1100^{\circ}$ | $\mathrm{Mo}-170$ to $1200^{\circ}$ | Rh | - |

Decrease with rise in temperature:

| (O) | - | $\mathrm{Ti}-180$ to $-40^{\circ}$ | Ni 350 to $800^{\circ}$ | Pd and Ta |
| :---: | :---: | :---: | :--- | :--- |
| $\mathrm{As}-170$ to $657^{\circ}$ | Mn | 250 to $1015^{\circ}$ | Co above $1150^{\circ}$ | Pt and U |
| Mg | - | $(\mathrm{Fe})$ | - | $\mathrm{Nb}-170$ to $400^{\circ}$ |

If $I$ is the intensity of magnetization produced in a substance by a field strength $H$ then the magnetic susceptibility $\kappa=I / H$. This is generally referred to the unit mass; italicized figures refer to the unit volume. The susceptibility depends greatly upon the purity of the substance, especially its freedom from iron. The mass susceptibility of a solution containing $p$ percent by weight of a water-free substance (susceptibility $\kappa$ ) is $\kappa_{x}=(p / 100) \kappa+(1-p / 100) \kappa_{0}$. ( $\kappa_{0}=$ susceptibility of water.)


TABLE 487.-TEMPERATURE VARIATION OF RESISTANCE OF BISMUTH IN TRANSVERSE MAGNETIC FIELD ( ${ }^{\circ} \mathrm{C}$ )

Proportional values of resistance

| $H$ | $-192^{\circ}$ | $-135^{\circ}$ | $-100^{\circ}$ | $-37^{\circ}$ | $0^{\circ}$ | $+18^{\circ}$ | $+60^{\circ}$ | $+100^{\circ}$ | $+183^{\circ}$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 0 | .40 | .60 | .70 | .88 | 1.00 | 1.08 | 1.25 | 1.42 | 1.79 |
| 2000 | 1.16 | .87 | .86 | .96 | 1.08 | 1.11 | 1.26 | 1.43 | 1.80 |
| 4000 | 2.32 | 1.35 | 1.20 | 1.10 | 1.18 | 1.21 | 1.31 | 1.46 | 1.82 |
| 6000 | 4.00 | 2.06 | 1.60 | 1.29 | 1.30 | 1.32 | 1.39 | 1.51 | 1.85 |
| 8000 | 5.90 | 2.88 | 2.00 | 1.50 | 1.43 | 1.42 | 1.46 | 1.57 | 1.87 |
| 10000 | 8.60 | 3.80 | 2.43 | 1.72 | 1.57 | 1.54 | 1.54 | 1.62 | 1.89 |
| 12000 | 10.8 | 4.76 | 2.93 | 1.94 | 1.71 | 1.67 | 1.62 | 1.67 | 1.92 |
| 14000 | 12.9 | 5.82 | 3.50 | 2.16 | 1.87 | 1.80 | 1.70 | 1.73 | 1.94 |
| 16000 | 15.2 | 6.95 | 4.11 | 2.38 | 2.02 | 1.93 | 1.79 | 1.80 | 1.96 |
| 18000 | 17.5 | 8.15 | 4.76 | 2.60 | 2.18 | 2.06 | 1.88 | 1.87 | 1.99 |
| 20000 | 19.8 | 9.50 | 5.40 | 2.81 | 2.33 | 2.20 | 1.97 | 1.95 | 2.03 |
| 25000 | 25.5 | 13.3 | 7.30 | 3.50 | 2.73 | 2.52 | 2.22 | 2.10 | 2.09 |
| 30000 | 30.7 | 18.2 | 9.8 | 4.20 | 3.17 | 2.86 | 2.46 | 2.28 | 2.17 |
| 35000 | 35.5 | 20.35 | 12.2 | 4.95 | 3.62 | 3.25 | 2.69 | 2.45 | 2.25 |

TABLE 488.-INCREASE OF RESISTANCE OF NICKEL DUE TO A TRANSVERSE MAGNETIC FIELD, EXPRESSED AS \% OF RESISTANCE AT $0^{\circ} \mathrm{C}$ AND $H=0$

| $H_{0}$ | $-190^{\circ}$ | $-75^{\circ}$ |  | $0^{\circ}$ | $+18^{\circ}$ | $+100^{\circ}$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | +0 | 0 | 0 | 0 | $+182^{\circ}$ |  |
| 1000 | +.20 | +.23 | +.07 | +.07 | +.96 | +.04 |
| 2000 | +.17 | +.16 | $\pm .03$ | $\pm .03$ | +.72 | -.07 |
| 3000 | .00 | -.05 | -.34 | -.36 | -.14 | -.60 |
| 4000 | -.17 | -.15 | -.60 | -.72 | -.70 | -1.15 |
| 6000 | -.19 | -.20 | -.70 | -.83 | -1.02 | -1.53 |
| 8000 | -.19 | -.23 | -.76 | -.90 | -1.15 | -1.66 |
| 10000 | -.18 | -.27 | -.82 | -.95 | -1.23 | -1.76 |
| 12000 | -.18 | -.30 | -.87 | -1.00 | -1.30 | -1.85 |
| 14000 | -.18 | -.32 | -.91 | -1.04 | -1.37 | -1.95 |
| 16000 | -.17 | -.35 | -.94 | -1.09 | -1.44 | -2.05 |
| 18000 | -.17 | -.38 | -.98 | -1.13 | -1.51 | -2.15 |
| 20000 | -.16 | -.41 | -1.03 | -1.17 | -1.59 | -2.25 |
| 25000 | -.14 | -.49 | -.12 | -1.29 | -1.76 | -2.50 |
| 30000 | -.12 | -.56 | -1.22 | -1.40 | -1.95 | -2.73 |
| 35000 | -.10 | -.63 | -1.32 | -1.50 | -2.13 | -2.98 |

TABLE 489.-CHANGE OF RESISTANCE OF VARIOUS METALS IN A
TRANSVERSE MAGNETIC FIELD
(Room temperature)



Brackets indicate annealing at $800^{\circ} \mathrm{C}$ in vacuum.
Parentheses indicate hardening by quenching from cherry-red.

TABLE 491.-CAST IRON IN INTENSE FIELDS

| Soft cast iron |  |  |  | Hard cast iron |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| H | $B$ | I | $\mu$ | II | B | $I$ | $\mu$ |
| 114 | 9950 | 782 | 87.3 | 142 | 7860 | 614 | 55.4 |
| 172 | 10800 | 846 | 62.8 | 254 | 9700 | 752 | 38.2 |
| 433 | 13900 | 1070 | 32.1 | 339 | 10850 | 836 | 30.6 |
| 744 | 15750 | 1200 | 21.2 | 684 | 13050 | 983 | 19.1 |
| 1234 | 17300 | 1280 | 14.0 | 915 | 14050 | 1044 | 15.4 |
| 1820 | 18170 | 1300 | 10.0 | 1570 | 15900 | 1138 | 10.1 |
| 12700 | 31100 | 1465 | 2.5 | 2020 | 16800 | 1176 | 8.3 |
| 13550 | 32100 | 1475 | 2.4 | 10900 | 26540 | 1245 | 2.4 |
| 13800 | 32500 | 1488 | 2.4 | 13200 | 28600 | 1226 | 2.2 |
| 15100 | 33650 | 1472 | 2.2 | 14800 | 30200 | 1226 | 2.0 |

## TABLE 492.-CORRECTIONS FOR RING SPECIMENS

In the case of ring specimens, the average magnetizing force is not the value at the mean radius, the ratio of the two being given in the table. The flux density consequently is not uniform, and the measured hysteresis is less than it would be for a uniform distribution. This ratio is also given for the case of constant permeability, the values being applicable for magnetizations in the neighborhood of the maximum permeability. For higher magnetizations the flux density is more uniform, for lower it is less, and the correction greater.

| Ratio of radial width to diameter of rings | Ratio of average $H$ to $H$ at mean radius |  | Ratio of hysteresis for uniform distribution to actual hysteresis |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Rectangular cross section | Circular cross section | Rectangular cross section | Circular cross section |
| 1/2 | 1.0986 | 1.0718 | 1.112 | 1.084 |
| 1/3 | 1.0397 | 1.0294 | 1.045 | 1.033 |
| 1/4 | 1.0216 | 1.0162 | 1.024 | 1.018 |
| 1/5 | 1.0137 | 1.0102 | 1.015 | 1.011 |
| 1/6 | 1.0094 | 1.0070 | 1.010 | 1.008 |
| 1/7 | 1.0069 | 1.0052 | 1.008 | 1.006 |
| 1/8 | 1.0052 | 1.0040 | 1.006 | 1.004 |
| 1/10 | 1.0033 | 1.0025 | 1.003 | 1.002 |
| 1/19 | 1.0009 | 1.0007 | 1.001 | 1.001 |

## TABLE 493.-COMPOSITION AND MAGNETIC PROPERTIES OF IRON AND STEEL

This table and Table 477 are from a paper by Dr. Hopkinson on the magnetic propertics of iron and steel. The numbers in the columns headed "magnetic properties" give results for the highest magnetizing force used, which is stated in the paper to have been 240. The maximum magnetization is not tabulated; but as stated by Hopkinson it may be obtained by subtracting the magnetizing force (240) from "the maximum induction and then dividing by $4 \pi$. "Coercive force" is the magnetizing force required to reduce the magnetization to zero. The "demagnetizing irct is the "maximum induction" stated in the table. The "energy dissipated" was calculated from the formula: Energy dissipated $=$ coercive force $\times$ maximum induction divided by $\pi$, which however, was only found to agree roughly with the the results of the experiment.

TABLE 493.-COMPOSITION AND MAGNETIC PROPERTIES OF IRON AND STEEL

$H=$ true intensity of magnetizing field, $H^{\prime}=$ intensity of applied field, $I=$ intensity of magnetization, $H=H^{\prime}-N I$.

Shuddemagen says: The demagnetizing factor is not a constant, falling for highest values of $I$ to about $1 / 7$ the value when unsaturated; for values of $B(=H+4 \pi I)$ less than $1000, N$ is approximately constant; using a solenoid wound on an insulating tube, or a tube of split brass, the reversal method gives values for $N$ which are considerably lower than those given by the step-by-step method; if the solenoid is wound on a thick brass tube, the two methods practically agree.

Values of $K \times 10^{4}$ are given where $B$ is determined by the step method and $H=H^{\prime}-K B$.

| Values of $N \times 10^{4}$ |  |  |  |  |  |  |  | Values of $K \times 10^{4}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Ratio } \\ \text { of } \\ \text { length } \\ \text { to } \\ \text { diameter } \end{gathered}$ | Ellipsoid | Cylinder |  |  |  |  |  |  |  |
|  |  | Uniform Magneto- <br> metric <br> magneti- <br> zation <br> method  <br> (Mann)  |  | Ballistic step method |  |  |  |  |  |
|  |  |  |  | Shuddemagen for range of <br> Dubois practical constancy |  |  |  |  |  |
|  |  |  |  | Diameter |  |  |  | Diameter 0.3175 cm | Diameter 1.1 to 2.0 cm |
| 5 | 7015 | 2 | 6800 | 0.158 cm | cm | 1 | , |  |  |
| 10 | 2549 | 630 | 2550 | 2160 | - | - | 1960 |  |  |
| 15 | 1350 | 280 | 1400 | 1206 | - | - | 1075 | - | 85.2 |
| 20 | 848 | 160 | 898 | 775 | - | - | 671 | - | 53.3 |
| 30 | 432 | 70 | 460 | 393 | 388 | 350 | 343 | 30.9 | 27.3 |
| 40 | 266 | 39 | 274 | 238 | 234 | 212 | 209 | 18.6 | 16.6 |
| 50 | 181 | 25 | 182 | 162 | 160 | 145 | 149 | 12.7 | 11.6 |
| 60 | 132 | 18 | 131 | 118 | 116 | 106 | 106 | 9.25 | 8.45 |
| 70 | 101 | 13 | 99 | 89 | 88 |  |  | - | - |
| 80 | 80 | 9.8 | 78 | 69 | 69 | 66 | 63 | 5.5 | 5.05 |
| 90 | 65 | 7.8 | 63 | 55 | 56 |  |  | - | - |
| 100 | 54 | 6.3 | 51.8 | 45 | 46 | 41 | 41 | 3.66 | 3.26 |
| 150 | 26 | 2.8 | 25.1 | 20 | 23 | 21 | 21 | 1.83 | 1.67 |
| 200 | 16 | 1.57 | 15.2 | 11 | 12.5 | 11 | 11 |  |  |
| 300 | 7.5 | . 70 | 7.5 | 5.0 |  |  |  |  |  |
| 400 | 4.5 | . 39 | - | 2.8 |  |  |  |  |  |

TABLE 495.-ELEMENTS OF THE EARTH'S MAGNETIC FIELD
The elements commonly used to describe the natural geomagnetic field are:

| Symbol <br> $D$ | Name <br>  <br>  <br> $I$ |
| :---: | :--- |
| $H$ | Magnetic declination |
| $X$ | Magnetic dip or inclination |
| $Y$ | North intensity |
| $Z$ | East intensity |
| $F$ | Vertical intensity |
| Total intensity |  |

## Remarks

Bearing of magnetic north with respect to geographic north, counted positive from north around by east
Positive when $Z$ has downward direction Positive regardless of direction
Referred to geographic north
Referred to geographic east
Positive when downward
Positive regardless of direction

For a given time and place, the field is completely described by specifying the values of three magnetic elements, provided they include one from the group $D, X, Y$, and one from the group, $I, Z, F$. The ways in which the magnetic elements are interrelated may be seen from figure 20 and the formulas below. The formulas in the right-hand group are


Fig. 20.-Interrelation of the magnetic elements.
obtained from the others by differentiation ; they are useful when dealing with small increments, such as those which describe annual and daily changes and minor local anomalies of the geomagnetic field. The formulas pertaining to values of $\Delta D$ and $\Delta I$ are expressed in minutes of arc.

$$
\begin{array}{ll}
X=H \cos D & \Delta X=\cos D \Delta H-H \sin D \sin 1^{\prime} \Delta D \\
Y=H \sin D & \Delta Y=\sin D \Delta H+H \cos D \sin 1^{\prime} \Delta D \\
Y=X \tan D & \Delta F=\cos I \Delta H+\sin I \Delta Z \\
H & =\sqrt{X^{2}+Y^{2}} \\
H & =F \cos I
\end{array}
$$

[^205]TABLE 495.-ELEMENTS OF THE EARTH'S MAGNETIC FIELD (concluded)
For purposes of mathematical analysis, it is convenient to recognize that the magnetic intensity or field strength (like other vector fields) is derivable from a scalar function or potential. If $V$ be the potential corresponding to the geomagnetic field, we may write

$$
F=-\operatorname{grad} V,
$$

whence any of the magnetic elements may be expressed as functions of the potential.
In polar coordinates ( $r, \theta, \lambda$ ) with origin at the earth's center, we have

$$
V=a \sum_{n=1}^{\infty}\left\{(r / a)^{\mathrm{n}} T_{\mathrm{n}}{ }^{\mathrm{e}}+(a / r)^{\mathrm{n}+1} T_{\mathrm{n}}{ }^{1}\right\}=V^{\mathrm{e}}+V^{\mathrm{L}},
$$

where $a$ denotes the earth's mean radius ( $6.37 \times 10^{8} \mathrm{~cm}$ ) (see Table 827).

$$
T_{\mathrm{n}} \equiv \sum_{m=0}^{m}\left(g_{\mathrm{n}}^{\mathrm{nm}} \cos m \lambda+h_{\mathrm{n}}^{\mathrm{m}} \sin m \lambda\right) p_{\mathrm{n}}^{\mathrm{m}}(\theta)
$$

Here $\theta$ is the colatitude and $\lambda$ the east longitude, and the affixes $e$ and $i$ refer to portions respectively of external and internal origin. The function

$$
\begin{aligned}
P_{\mathrm{n}}^{\mathrm{m}}(\theta) & =\left\{2 \frac{(n-m)!}{(n+m)!}\right\}^{3} P_{\mathrm{n}, \mathrm{~m}}(\theta) \text { when } m>0 \\
& =P_{\mathrm{n}, \mathrm{~m}}(\theta) \text { when } m=0,
\end{aligned}
$$

where

$$
\begin{aligned}
P_{\mathrm{n}, \mathrm{~m}}(\theta) & =\frac{(2 n)!}{2^{\mathrm{n}} n!(n-m)!} \sin ^{\mathrm{m}} \theta\left\{\cos ^{\mathrm{n}-\mathrm{m}} \theta\right. \\
& \left.-\frac{(n-m)(n-m-1)}{2(2 n-1)} \cos ^{\mathrm{n}-\mathrm{m}-2} \theta+\ldots\right\}
\end{aligned}
$$

Magnetic surveys of portions of the earth have been made by means of observations at many thousands of stations, the elements usually observed being $D, H$, and $I$. Such surveys are repeated in part every few years in populated areas, and at intervals of one or more decades in most areas, because of a substantial and usually unpredictable change in the earth's field known as geomagnetic secular change. These changes are most accurately measured at fixed magnetic observatories to the number of about one hundred. The U. S. Coast and Geodetic Survey operates magnetic observatories at Cheltenham, Md.; Tucson, Ariz.; Sitka, Alaska; Honolulu, T. H.; and San Juan, P. R. Other nations conduct similar measurements.
Magnetic surveys by airplane will no doubt be commonplace in future years.
The part of the earth's field having external origin does not exceed a few percent, and its existence has never been indiciated with much certainty hy the spherical harmonic analyses. If the distinction between contributions of external and internal origin in the first formula is disregarded, the accompanying tables give the values of the principal harmonic terms at various epochs.
The magnetic moment of the earth as given by the centered dipole approximation for 1922 was $8.04 \times 10^{25} \mathrm{cgs}$. The axis of this dipole intersects the earth's surface at points called the geomagnetic (axis) poles, located in 1922 at latitude $78: 5 \mathrm{~N}$., and longitude 270.0 E .; and at latitude 78.5 S ., and longitude $111^{\circ} \mathrm{E}$. In comparison with these currently adopted values, the analysis of Vestine and Lange for 1945 shows only slight change that may have taken place since 1922.
The dipole part of the earth's field diminishes with height $h$ approximately as $(1-3 h / a)$. Values for 1945 have been estimated in tabulation to heights as great as $h=5000 \mathrm{~km}$ for spherical harmonic terms up to degree six. ${ }^{\dagger}$

The magnetic north and south poles of popular interest are those defined by $H=0$, or by $I= \pm 90^{\circ}$. As $H$ changes with time, owing to secular change, these poles must move with time, except in the unlikely event that the lines of zero change of $X$ and $Y$ both happen to pass through the poles. There are a principal north magnetic pole and a principal south magnetic pole, which undergo substantial change in position with time. In addition there are undoubtedly local (secondary) magnetic poles near each principal pole. These secondary poles occur only in pairs. Of each pair, one pole has the character of a potential focus (like the corresponding principal pole), while the other is a "false pole" or node of the equipotential lines. The secondary poles do not individually undergo large-scale migration, since they are associated with localized magnetic materials in the earth's crust. These occur when such materials succeed in reducing the changing value of $H$ to zero, as the principal migrates.

The principal north and south magnetic poles are not diametrically opposite, each being about $2,300 \mathrm{~km}$ from the antipodes of the other.

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TABLE 496.-THE FIRST EIGHT GAUSS COEFFICIENTS OF THE EARTH'S MAGNETIC POTENTIAL (V) EXPRESSED IN UNITS OF $10^{-4}$ cgs

| Sour | poch |  | 1 | $h_{1}$ | , |  | $h_{2}{ }^{1}$ | $g_{2}{ }^{2}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Gauss | 1835 | $-3235$ | -311 | +625 | + 51 | +292 | + 12 | - 2 | +157 |
| Erman-Pe | 1829 | -3201 | -284 | +601 | - 8 | +257 | - 4 | - 14 | +146 |
| Adams | 1845 | -3219 | -278 | +578 | + 9 | +284 | $-10$ | + 4 | +135 |
| Adams | 1880 | -3168 | -243 | +603 | - 49 | +297 | -75 | + 61 | +149 |
| Fritsche | 1885 | -3164 | -241 | +591 | - 35 | +286 | -75 | +68 | +142 |
| Schmidt | 1885 | -3168 | -222 | $+595$ | - 50 | +278 | -71 | + 65 | +149 |
| Dyson and Fu | 1922 | -3095 | -226 | +592 | -89 | +299 | -124 | +144 | + 84 |
| Afanasieva |  | $-3032$ | -229 | +590 | -125 | +288 | -146 | +150 | + 48 |
| Vestine and | 1945 | -3057 | -211 | +581 | -127 | +296 | -166 | +164 | + 54 |

TABLE 497.-SPHERICAL HARMONIC COEFFICIENTS OF THE AVERAGE ANNUAL SECULAR VARIATION EXPRESSED IN UNITS OF $10^{-5}$ cgs

| Source | Epoch | $g_{1}{ }^{0}$ | $g_{1}{ }^{1}$ | $h_{1}{ }^{1}$ | $g_{2}{ }^{0}$ | $g_{2}{ }^{1}$ | $h_{2}{ }^{1}$ | $g_{2}{ }^{2}$ | $h_{2}{ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dyson-Schmidt | 1922-1885 | $+20$ | - | -1 | -10 | +6 | -14 | +21 | -18 |
| Bartels | 1920-1902 | +42 | -9 | $+12$ | - 7 | +8 | -25 | +13 | -8 |
| Carlheim-Gyllensköld | 1920-1902 | 0 | $+13$ | + 4 | 0 | -4 | -12 | $+13$ | -17 |
| Vestine and Lange. | ( 1912.5 | $+25$ | $+1$ | -7 | $-7$ | -1 | -9 | +24 | -17 |
|  | 1922.5 | +28 | + 4 | $-7$ | -10 | $+1$ | -14 | $+17$ | -17 |
|  | 1932.5 | $+23$ |  | $-5$ | -14 | +1 | -18 | $+10$ | -14 |
|  | 1942.5 | $+9$ | $+2$ | $+1$ | -18 | 0 | -20 | $+2$ | -14 |

The magnetic moment of the earth (epoch 1922) $=8.06 \times 10^{25} \mathrm{cgs}$.

|  | S Latitude 78.6 N. |
| :---: | :---: |
| Geomagnetic north pole.......... | \{ Longitude 289.9 E. |
| omagnetic south | S Latitude 78.6 S. |

$\{$ Longitude 109.9 E.

TABLE 498.-COORDINATES OF NORTH MAGNETIC POLE


| Date or <br> epoch | South <br> lati- <br> tude, <br> $\circ$ | East <br> longi- <br> tude <br> $\circ$ | Observer |
| :---: | :---: | :---: | :--- | :--- |$\quad$ Authority *

* For authorities, see bibliography, p. 501.
$\dagger$ Based on the above position for 1912.5 with reduction for secular change.


## TABLE 500.-DIP OR INCLINATION, UNITED STATES

This table gives for the epoch January 1, 1950, smoothed values of the magnetic dip, I, corresponding to the longitudes, $\lambda$, west of Greenwich in the heading and the north latitudes, $\boldsymbol{\Phi}$, in the first column. The remarks about smoothing, in Table 502, apply to this table as well.

| $\left.{ }_{\Phi}\right\|^{\lambda}$ | $65^{\circ}$ | $70^{\circ}$ | $75^{\circ}$ | $80^{\circ}$ | $85^{\circ}$ | $90^{\circ}$ | $95^{\circ}$ | $100^{\circ}$ | $105^{\circ}$ | $110^{\circ}$ | $115^{\circ}$ | $120^{\circ}$ | $125^{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 21 |  |  | 54.7 |  |  |  |  |  |  |  |  |  |  |
| 23 |  |  | 57.0 | 56.3 | 55.0 | 54.1 | 52.7 | 51.4 | 50.1 |  |  |  |  |
| 25 |  |  | 59.2 | 58.5 | 57.6 | 56.6 | 55.2 | 53.9 | 52.6 | 51.4 | 50.3 |  |  |
| 27 |  |  | 61.1 | 60.8 | 59.9 | 58.8 | 57.6 | 56.3 | 55.0 | 53.7 | 52.6 | 51.6 |  |
| 29 |  | 62.9 | 63.0 | 62.8 | 62.0 | 61.0 | 59.8 | 58.5 | 57.2 | 56.0 | 54.8 | 53.8 |  |
| 31 |  | 64.5 | 64.8 | 64.7 | 63.9 | 63.0 | 61.8 | 60.6 | 59.4 | 58.2 | 57.0 | 55.9 |  |
| 33 |  | 66.2 | 66.5 | 66.5 | 65.9 | 64.9 | 63.8 | 62.6 | 61.5 | 60.4 | 59.0 | 58.0 |  |
| 35 |  | 67.8 | 68.2 | 68.2 | 67.7 | 66.8 | 65.8 | 64.7 | 63.6 | 62.4 | 61.1 | 60.0 |  |
| 37 |  | 69.4 | 69.9 | 69.9 | 69.5 | 68.6 | 67.6 | 66.6 | 65.5 | 64.4 | 63.0 | 61.8 |  |
| 39 | .. | 70.7 | 71.3 | 71.4 | 71.1 | 70.4 | 69.4 | 68.5 | 67.4 | 66.2 | 64.9 | 63.6 | 62.7 |
| 41 |  | 72.0 | 72.6 | 72.8 | 72.6 | 72.0 | 71.2 | 70.2 | 69.2 | 68.0 | 66.7 | 65.4 | 64.3 |
| 43 | 72.3 | 73.2 | 73.9 | 74.2 | 74.0 | 73.6 | 72.5 | 71.9 | 70.9 | 69.6 | 68.4 | 67.1 | 65.9 |
| 45 | 73.4 | 74.4 | 75.2 | 75.6 | 75.5 | 75.0 | 74.4 | 73.6 | 72.6 | 71.3 | 70.0 | 68.8 | 67.5 |
| 47 | 74.4 | 75.6 | 76.3 | 76.8 | 76.9 | 76.6 | 75.9 | 75.1 | 74.1 | 72.8 | 71.6 | 70.4 | 69.2 |
| 49 | 75.5 | 76.6 | 77.4 | 78.0 | 78.4 | 78.1 | 77.3 | 76.5 | 75.5 | 74.4 | 73.0 | 71.9 | 70.7 |

## TABLE 501.-SECULAR CHANGE OF DIP, UNITED STATES

Smoothed values of the magnetic dip for the indicated places for January 1 of the years stated. The degrees are given in the third column and in the succeeding column. The remarks about smoothing, in Table 502, apply to this table as well.

| Lat. | Long. |  | 1930 | 1935 | 1940 | 1945 | 1950 | Lat. | Lon |  | 1930 | 1935 | 1940 | 1945 | 1950 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $25^{\circ}$ | $80^{\circ}$ | 55' | 179' | 202' | 214' | 213' | 210 | $43^{\circ}$ | $70^{\circ}$ | $73^{\prime}$ | 17' | 19' | $24^{\prime}$ | $19^{\prime}$ | 12 |
| 25 | 90 | 53 | 188 | 210 | 218 | 216 | 215 | 43 | 80 | 73 | 76 | 80 | 85 | 80 | 74 |
| 25 | 100 | 51 | 162 | 176 | 178 | 176 | 173 | 43 | 90 | 73 | 39 | 43 | 46 | 40 | 33 |
| 31 | 80 | 62 | 137 | 154 | 166 | 164 | 161 | 43 | 100 | 71 | 67 | 69 | 70 | 63 | 56 |
| 31 | 90 | 60 | 163 | 178 | 185 | 181 | 178 | 43 | 110 | 69 | 50 | 50 | 51 | 45 | 39 |
| 31 | 100 | 58 | 153 | 162 | 165 | 161 | 157 | 43 | 120 | 67 | 20 | 16 | 18 | 14 | 7 |
| 31 | 110 | 57 | 72 | 77 | 77 | 75 | 71 | 47 | 70 | 75 | 49 | 46 | 49 | 44 | 36 |
| 37 | 80 | 68 | 102 | 113 | 122 | 118 | 114 | 47 | 80 | 76 | 61 | 60 | 62 | 57 | 50 |
| 37 | 90 | 67 | 92 | 101 | 108 | 102 | 97 | 49 | 90 | 78 | 23 | 22 | 21 | 15 | 7 |
| 37 | 100 | 65 | 98 | 104 | 107 | 101 | 96 | 49 | 100 | 76 | 46 | 45 | 43 | 37 | 31 |
| 37 | 110 | 63 | 89 | 91 | 93 | 88 | 82 | 49 | 110 | 74 | 35 | 32 | 31 | 26 | 21 |
| 37 | 120 | 61 | 61 | 59 | 62 | 57 | 51 | 49 | 120 | 71 | 68 | 62 | 62 | 58 | 53 |




Fig. 23.-World isodynamic lines, epoch 1945 (lines of equal horizontal intensity, H, in cgs).



FIG. 25.-World isodynamic lines, epoch 1945 (lines of equal total intensity, F , in cgs).

# TABLE 502.-SECULAR CHANGE OF MAGNETIC DECLINATION IN THE UNITED STATES 

Smoothed values of the magnetic declination for the indicated places for January 1 of the years stated. The degrees are given in the fourth column, together with the indication E (east) or W (west) ; the minutes are given in the succeeding columns. The pattern depicted by this table for any date is highly smoothed and corresponds with that shown on "datum charts" discussed in current publications of the U. S. Coast and Geodetic Survey, such as those cited.** The latter contain more detailed secular-change tables, as well as current magnetic charts which may be consulted for values reflecting a greater amount of local information than it is possible to show in tabular form.
** See bibliography, references d, e, p. 501.

| Locality | Lat. | Long. |  | 1920 |  |  |  | Locality <br> Mexico | $\begin{aligned} & \text { Lat. } \\ & 28^{\circ} \end{aligned}$ | Long. |  |  | 1920 |  | 1940 | 1950 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| At sea | $44^{\circ}$ | $68^{\circ}$ | $13^{\circ} \mathrm{W}$ | 319' | 357' | $377{ }^{\prime}$ |  |  |  | $100^{\circ}$ | 8 | E | 112 ' | 127' | 142' | 135' |
| Maine | 46 | 68 | 16 W | 269 | 299 | 312 | 307 | Tex. | 30 | 100 | 9 | E | 75 | 85 | 98 | 92 |
| Canada | 48 | 68 | 19 W | 241 | 263 | 269 | 258 | Tex. | 32 | 100 | 9 | E | 98 | 103 | 114 | 108 |
| At sea | 40 | 72 | 6 W | 311 | 356 | 382 | 387 |  |  |  |  |  |  |  |  |  |
| Conn. | 42 | 72 | 7 W | 355 | 400 | 425 | 426 | Tex. | 34 | 100 | 10 | E | 63 | 63 | 69 | 63 |
| N. H. | 44 | 72 | 9 W | 349 | 392 | 413 | 410 | Okla. | 36 | 100 | 10 | E | 89 | 82 | 83 | 76 |
|  |  |  |  |  |  |  |  | Kans. | 38 | 100 | 11 | E | 52 | 38 | 35 | 25 |
| Canada | 46 | 72 | 11 W | 357 | 393 | 409 | 401 | Kans. | 40 | 100 | 11 | E | 74 | 52 | 47 | 34 |
| At sea | 34 | 76 |  | 260 | 283 | 298 | 306 | Nehr. | 42 | 100 | 11 | E | 99 | 71 | 62 | 46 |
| N. C. | 36 | 76 | 0 W | 324 | 351 | 366 | 372 | S. Dak. | 44 | 100 | 11 | E | 129 | 94 | 79 | 59 |
| Md. | 38 | 76 | 1 W | 333 | 367 | 382 | 385 |  |  |  |  |  |  |  |  |  |
| Pa . | 40 | 76 | 2 W | 350 | 389 | 403 | 404 | N. Dak. | 46 | 100 | 12 | E | 105 | 63 | 40 | 16 |
| Pa. | 42 | 76 | 3 W | 376 | 420 | 434 | 432 | N. Dak. | 48 | 100 | 12 | E | 143 | 94 | 64 | 34 |
|  |  |  |  |  |  |  |  | Tex. | 30 | 104 | 10 | E | 91 | 100 | 110 | 100 |
| N. Y. | 44 | 76 | 5 W | 357 | 402 | 415 | 409 | Tex. | 32 | 104 | 11 | E | 65 | 69 | 76 | 66 |
| At sea | 26 | 80 | 0 E | 72 | 77 | 75 | 59 | N. Mex. | 34 | 104 | 11 | E | 98 | 97 | 100 | 90 |
| At sea | 28 | 80 | 0 E | 39 | 40 | 37 | 25 | N. Mex. | 36 | 104 | 12 | E | 72 | 66 | 65 | 52 |
| At sea | 30 | 80 | $0 \dagger$ | 4* | 0 | 3 | 11 |  |  |  |  |  |  |  |  |  |
| At sea | 32 | 80 | $0 \dagger$ | 33 | 43 | 46 | 51 | Colo. | 38 | 104 | 13 | E | 45 | 33 | 26 | 12 |
| S. C. | 34 | 80 | $0 \dagger$ | 81 | 96 | 98 | 101 | Colo. | 40 | 104 | 13 | E | 78 118 | 60 | 49 | 31 |
|  |  |  |  |  |  |  |  | Nebr. | 42 | 104 | 13 | E | 118 | 94 | 79 | 58 |
| N. C. | 36 | 80 | $0 \dagger$ | 132 | 153 | 157 | 157 | S. Dak. | 44 | 104 | 14 | E | 107 | 76 | 57 | 31 |
| Va . | 38 | 80 | $0 \dagger$ | 191 | 218 | 221 | 219 | N. Dak. | 46 | 104 | 15 | E | 98 | 61 | 37 | 6 |
| Pa. | 40 | 80 | ${ }^{0} \dagger$ | 255 | 289 | 293 | 288 | N. Dak. | 48 | 104 | 15 | E | 154 | 110 | 79 | 44 |
| Pa . | 42 | 80 | 0 W | 326 | 365 | 371 | 365 |  |  |  |  |  |  |  |  |  |
| Canada | 44 | 80 | 1 W | 352 | 396 | 403 | 394 | Mexico | 30 | 108 | 11 | E | 95 | 100 | 108 | 95 |
| Fla. | 30 | 84 | 2 E | 28 | 31 | 39 | 35 | N. Mex. | 32 | 108 | 12 | E | 74 | 75 | 79 | 65 |
|  |  |  |  |  |  |  |  | N. Mex. | 34 | 108 | 12 | E | 111 | 109 | 109 | 95 |
| Ga. | 32 | 84 | 1 E | 62 | 59 | 66 | 66 | N. Mex. | 36 | 108 | 13 | E | 90 | 84 | 80 | 63 |
| Ga. | 34 | 84 | 1 E | 32 | 23 | 30 | 32 | Colo. | 38 | 108 | 14 | $\underset{\text { E }}{\text { E }}$ | 69 | 59 | 51 | 32 |
| Tenn. | 36 | 84 | ${ }_{0} \mathrm{E}$ | 59 | 44 | 50 | 54 | Colo. | 40 | 108 | 15 | E | 56 | 40 | 26 | 5 |
| Ky. | 38 | 84 | $0 \dagger$ | 18* | 5 | 0 | 6* |  |  |  |  |  |  |  |  |  |
| Ohio | 40 | 84 | ${ }^{0+}$ | 24 | 55 | 52 | 44 | Wyo. | 42 | 108 | 15 | E | 111 | 90 | 73 | 47 |
| Mich. | 42 | 84 | $0 \dagger$ | 77 | 114 | 113 | 105 | Wyo. | 44 | 108 | 16 | E | 113 | 86 | 66 | 35 |
|  |  |  |  |  |  |  |  | Mont. | 46 | 108 | 17 | E | 114 | 81 | 56 | 21 |
| Mich. | 44 | 84 | $0 \dagger$ | 141 | 183 | 187 | 178 | Mont. | 48 | 108 | 18 | E | 117 | 78 | 47 | 8 |
| Mich. | 46 | 84 | $0 \dagger$ | 212 | 260 | 270 | 263 | Ariz. | 32 | 112 | 12 | E | 125 | 125 | 126 | 112 |
| Ala. | 30 | 88 | 4 E | 42 | 50 | 64 | 64 | Ariz. | 34 | 112 | 13 | E | 107 | 104 | 103 | 86 |
| Ala. | 32 | 88 | 4 E | 28 | 30 | 42 | 44 |  |  |  |  |  |  |  |  |  |
| Ala. | 34 | 88 | 4 E | 12 | 7 | 18 | 22 | Ariz. | 36 | 112 | 14 | E | 91 | 84 | 78 | 60 |
| Tenn. | 36 | 88 | 3 E | 54 | 42 | 53 | 58 | Utah | 38 | 112 | 15 | E | 80 | 70 | 60 | 39 |
|  |  |  |  |  |  |  |  | Utah | 40 | 112 | 16 | E | 76 | 62 | 49 | 25 |
| Ind. | 38 | 88 |  | 34 | 14 | 23 | 29 | Utah | 42 | 112 | 17 | E | 79 | 61 | 44 | 16 |
| II1. | 40 | 88 | $2{ }_{2} \mathrm{E}$ | 70 | 41 | 47 | 52 | Idaho | 44 | 112 | 18 | E | 84 | 61 | 41 | 9 |
| 111. | 42 | 88 |  | 41 | 6 | 8 | 12 | Mont. | 46 | 112 | 19 | E | 96 | 67 | 41 | 5 |
| Wis. | 44 | 88 | ${ }^{1} \mathrm{E}$ | 70 | 28 | 25 | 27 |  |  |  |  |  |  |  |  |  |
| Mich. | 46 48 | 88 88 | ${ }_{0}{ }^{+} \mathrm{E}$ | 37** | 37 20 | 28 | 42 | Mont. | 48 32 | 112 |  | $\underset{\text { E }}{ }$ | 163 | 129 | 99 163 | 59 148 |
| Mich. | 48 | 88 | $0 \dagger$ | 35* | 20 | 35 | 42 | Mexico | 32 | 116 | 12 | E | 164 | 162 | 163 | 148 |
| La. | 30 | 92 |  | 47 | 57 | 74 | 74 | Calif. Calif. | 34 36 | 116 116 | 13 | $\stackrel{\text { E }}{\text { E }}$ | 151 | 146 | 144 | 128 |
| La. | 32 | 92 | 6 E | 44 | 49 | 64 | 66 | Nev. | 38 | 116 | 15 | E | 137 | 127 | 118 | 97 |
| Ark. | 34 | 92 | 6 E | 39 | 37 | 51 | 55 | Nev. | 40 | 116 | 16 | E | 138 | 126 | 113 | 89 |
| Ark. | 36 | 92 | 6 E | 40 | 29 | 38 | 42 |  |  |  |  |  |  |  |  |  |
| Mo. | 38 | 92 | 6 E | 39 | 20 | 27 | 29 | Nev. | 42 | 116 | 17 | E | 140 | 124 | 109 | 81 |
| Mo. | 40 | 92 | 6 E | 34 | 8 | 12 | 12 | Idaho | 44 | 116 | 18 | E | 152 | 133 | 114 | 83 |
|  |  |  |  |  |  |  |  | Idaho | 46 | 116 | 19 | E | 168 | 143 | 120 | 85 |
| Iowa | 42 | 92 | E | 87 | 52 | 50 | 49 | Mont. | 48 | 116 | 21 | E | 119 | 90 | 61 | 23 |
| Minn. | 44 | 92 | 5 E | 76 | 34 | 28 | 22 | At sea | 34 | 120 | 13 | E | 189 | 184 | 180 | 163 |
| Minn. | 46 | 92 |  | 128 | 79 | 64 | 53 | Calif. | 36 | 120 | 14 | E | 184 | 177 | 171 | 152 |
| Mlinn. | 48 | 92 | 4 E | 116 | 60 | 37 | 21 |  |  |  |  |  |  |  |  |  |
| At sea | 28 | 96 | 7 E | 85 | 101 | 119 | 115 | Calif. | 38 | 120 | 15 | E | 182 | 1/2 | 163 | 143 |
| Tex. | 30 | 96 | 7 E | 96 | 107 | 123 | 121 | Calif. | 40 |  | $16$ | $\underset{\mathrm{F}}{\mathrm{E}}$ |  |  | 156 |  |
|  |  |  |  |  |  |  |  | Calif. | 42 | 120 | 17 | E | 184 | 169 | 154 | 129 |
| Tex. Okla. dex. | 32 34 3 | 96 96 | 8 8 8 E | 48 61 | 54 61 | 67 | 66 69 | Oreg. | 44 46 | 120 | 18 | $\stackrel{\text { E }}{\text { E }}$ | 200 | 181 | 163 | 135 |
| Okla. | 36 | 96 | 8 E | 75 | 66 | 71 | 69 | Wash. | 48 | 120 | 21 | E | 168 | 142 | 116 | 80 |
| Kans. | 38 | 96 |  | 27 | 10 | 12 | 9 |  |  |  |  |  |  |  |  |  |
| Kans. | 40 | 96 | 9 E | 38 | 13 | 12 | 6 | At sea | 38 | 124 | 15 | E | 212 | 202 | 194 | 175 |
| lowa | 42 | 96 | 9 E | 48 | 16 | 11 | 2 | Calif. | 40 | 124 | 16 | E | 211 | 199 | 187 | 167 |
|  |  |  |  |  |  |  |  | Calif. | 42 | 124 | 17 | E | 215 | 201 | 187 | 164 |
| Minn. | 44 | 96 | 8 E | 120 | 81 | 70 | 57 | Oreg. | 44 | 124 | 18 | E* | 239 | 212 | 194 | 170 |
| Minn. | 46 | 96 | 8 E | 134 | 88 | 69 | 50 | Oreg. | 46 | 124 | 19 | F | 241 | 222 | 203 | 175 |
| Minn. | 48 | 96 | 8 E | 154 | 100 | 71 | 48 | Wash. | 48 | 124 | 20 | E | 256 | 234 | 210 | 179 |

[^206]The daily variation is not predictable in detail since it fluctuates in form and amplitude from day to day. However, the variations shown in this table appear with considerable regularity when the data are averaged over several months or years. Values are based on the 10 leastdisturbed days of each month of the interval 1918-1928, using photographic registrations obtained at three of the magnetic observatories listed in Table 510. A plus sign signifies that east declination is greater, or west declination less, than the mean for the day.

| Hour, local mean time | January, February, November, December |  |  | March, April, September, October |  |  | $\begin{gathered} \text { May, June, } \\ \text { July, August } \end{gathered}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Sitka, Alaska | Cheltenham, Md. | Tucson, Ariz. | Sitka, Alaska | Cheltenham, Md. | Tucson, Ariz. | Sitka, Alaska | Cheltenbam, Md. | Tucson, Ariz. |
| 2 a.m. | . 0 | - . 2 | -. 3 | . 0 | $+.4$ | $+.1$ | - . 9 | $+.3$ | $+.1$ |
| $4 \mathrm{a} . \mathrm{m}$. | $+.2$ | $+.2$ | -. 2 | $+.5$ | $+1.0$ | +.3 | $+.6$ | +1.0 | $+.6$ |
| 6 a. m. | $+.7$ | +.8 | +. 2 | +2.4 | +2.3 | +1.5 | +4.9 | +4.1 | +2.6 |
| 8 a.m. | +1.8 | +2.5 | +1.9 | +4.8 | +4.7 | +4.0 | +7.7 | $+5.9$ | +4.7 |
| $10 \mathrm{a} . \mathrm{m}$. | +1.7 | +2.5 | +2.3 | +3.6 | +2.2 | +1.4 | +4.8 | +1.3 | $+.4$ |
| Noon | $-.2$ | -2.0 | -1.1 | -. 6 | -3.7 | -2.3 | -1.8 | -4.7 | -3.2 |
| $2 \mathrm{p} . \mathrm{m}$. | -1.5 | -3.2 | -2.2 | -2.9 | -4.7 | -2.8 | -5.2 | -5.4 | -3.2 |
| 4 p.m. | -1.6 | -1.5 | -1.0 | -3.2 | -2.2 | -1.4 | -5.1 | -2.5 | -1.4 |
| 6 p.m. | -. 9 | -. 2 | . 0 | -2.3 | -. 6 | -. 6 | -2.5 | -. 2 | -. 3 |
| 8 p.m. | $-.3$ | $+.5$ | $+.3$ | -1.3 | . 0 | -. 2 | -1.0 | -. 4 | -. 4 |
| $10 \mathrm{p} . \mathrm{m}$. | . 0 | +. 6 | $+.2$ | -. 8 | $+.3$ | $-.1$ | $-1.0$ | . 0 | -. 2 |
| Midnight | $-.1$ | $+.2$ | -. 1 | $-.3$ | $+.4$ | . 0 | $-1.1$ | $+.2$ | -. 1 |

* Expressed in minutes.


## TABLE 504.-HORIZONTAL MAGNETIC INTENSITY, UNITED STATES

This table gives for the epoch January 1, 1950, the smoothed horizontal intensity, $H$, expressed in cgs units, corresponding to the longitudes west of Greenwich in the heading and the north latitudes in the first column. The remarks about smoothing, in Table 502, apply to this table as well.

| ${ }^{1}{ }^{\lambda}$ | $65^{\circ}$ | $70^{\circ}$ | $75^{\circ}$ | $80^{\circ}$ | $85^{\circ}$ | $90^{\circ}$ | 95 | $100^{\circ}$ | 105 | $110^{\circ}$ | $115^{\circ}$ | 120 | 125 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $21^{\circ}$ |  |  | . 267 |  |  |  |  |  |  |  |  |  |  |
| 23 |  |  | . 262 | . 267 | . 274 | . 282 | . 288 | . 293 | . 296 |  |  |  |  |
| 25 |  |  | . 254 | . 259 | . 266 | . 273 | . 278 | . 284 | . 288 | . 290 | . 290 |  |  |
| 27 |  |  | . 246 | . 251 | . 257 | . 264 | . 270 | . 276 | . 280 | . 282 | . 282 | 282 |  |
| 29 |  | . 232 | . 236 | . 241 | . 247 | . 254 | . 260 | . 266 | . 271 | . 273 | . 274 | . 276 |  |
| 31 |  | . 222 | . 226 | . 231 | . 237 | . 244 | . 250 | . 257 | . 262 | . 265 | . 267 | . 269 |  |
| 33 |  | . 212 | . 215 | . 220 | . 225 | . 232 | . 239 | . 246 | . 252 | . 256 | . 259 | . 261 |  |
| 35 |  | . 202 | . 204 | . 208 | . 213 | . 220 | . 227 | . 234 | . 241 | . 246 | . 250 | . 253 |  |
| 37 |  | . 192 | . 193 | . 196 | . 201 | .207 | . 214 | . 222 | . 229 | . 236 | . 240 | . 244 |  |
| 39 |  | . 181 | . 181 | . 184 | . 188 | . 194 | . 201 | . 210 | . 217 | . 224 | . 230 | . 234 | 238 |
| 41 |  | . 171 | . 170 | . 171 | . 176 | . 181 | . 188 | . 196 | . 204 | . 212 | . 219 | . 224 | 230 |
| 43 | . 165 | . 161 | . 160 | . 160 | . 162 | . 167 | . 174 | . 182 | . 191 | . 200 | . 207 | . 214 | 219 |
| 45 | . 156 | . 151 | . 148 | . 148 | . 149 | . 153 | . 160 | . 168 | . 177 | . 186 | . 195 | . 202 | 208 |
| 47 | . 145 | . 140 | . 137 | . 135 | . 135 | . 140 | . 146 | . 154 | . 164 | . 174 | . 182 | . 190 | 197 |
| 49 | . 134 | . 129 | . 126 | . 123 | . 122 | . 126 | . 133 | . 140 | . 150 | . 160 | . 170 | . 178 | 185 |

TABLE 505.-SECULAR CHANGE OF HORIZONTAL INTENSITY, UNITED STATES
Smoothed values of horizontal intensity in cgs units at the indicated places for January 1 of the years stated. The remarks about smoothing, in Table 502, apply to this table as well.

| Lat. | Long. | 1930 | 1935 | 1940 | 1945 | 1950 | Lat. | Long. | 1930 | 1935 | 1940 | 1945 | 1950 |
| ---: | ---: | ---: | ---: | ---: | ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $25^{\circ}$ | $80^{\circ}$ | .2653 | .2612 | .2589 | .2586 | .2587 | $43^{\circ}$ | $70^{\circ}$ | .1627 | .1613 | .1601 | .1608 | .1613 |
| 25 | 90 | .2801 | .2761 | .2741 | .2735 | .2731 | 43 | 80 | .1621 | .1604 | .1589 | .1595 | .1598 |
| 25 | 100 | .2908 | .2878 | .2861 | .2851 | .2843 | 43 | 90 | .1693 | .1675 | .1664 | .1671 | .1671 |
| 31 | 80 | .2361 | .2325 | .2303 | .2304 | .2306 | 43 | 100 | .1838 | .1822 | .1814 | .1820 | .1820 |
| 31 | 90 | .2464 | .2461 | .2442 | .241 | .2438 | 43 | 110 | .2015 | .2002 | .1994 | .1997 | .1996 |
| 31 | 100 | .2622 | .2595 | 2578 | .2573 | .2567 | 43 | 120 | .2154 | .2143 | .2135 | .2136 | .2136 |
| 31 | 110 | .2698 | .2677 | .2662 | .2656 | .2648 | 47 | 70 | .1405 | .1398 | .1389 | .1398 | .1403 |
| 37 | 80 | .2003 | .1974 | .1954 | .1958 | .1960 | 47 | 80 | .1362 | .1352 | .1342 | .1350 | .1353 |
| 37 | 90 | .211 | .2084 | .2068 | .2071 | .2070 | 49 | 90 | .1256 | .1249 | .1243 | .1253 | .1255 |
| 37 | 100 | .2262 | .2239 | .2226 | .2227 | .2223 | 49 | 100 | .1406 | .1398 | .1394 | .1103 | .1405 |
| 37 | 110 | .2389 | .2372 | .2361 | .2359 | .2355 | 49 | 110 | .1601 | .1592 | 1587 | .1594 | .1597 |
| 37 | 120 | .2473 | .2460 | .2449 | .2446 | .2442 | 49 | 120 | .1783 | .1775 | .1771 | .1775 | .1777 |

## TABLE 506.-VERTICAL MAGNETIC INTENSITY, UNITED STATES

This table gives for the epoch January 1, 1950, the smoothed vertical intensity, $Z$, expressed in cgs units, corresponding to the longitudes west of Greenwich in the heading and the north latitudes in the first column. The remarks about smoothing, in Table 502, apply to this table as well.

| ${ }^{1}{ }^{\lambda}$ | $65^{\circ}$ | $70^{\circ}$ | $75^{\circ}$ | $80^{\circ}$ | $85^{\circ}$ | $90^{\circ}$ | $95^{\circ}$ | $100^{\circ}$ | 10 | 110 | $115^{\circ}$ | $120^{\circ}$ | 125 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $21^{\circ}$ |  |  | . 378 |  |  |  |  |  |  |  |  |  |  |
| 23 |  |  | . 402 | . 399 | . 391 | . 389 | . 378 | . 367 | . 354 |  |  |  |  |
| 25 |  |  | . 425 | . 422 | . 419 | . 414 | . 401 | . 390 | . 376 | . 362 | . 348 |  |  |
| 27 |  |  | . 445 | . 448 | . 442 | . 435 | . 426 | . 413 | . 399 | . 383 | . 368 | . 356 |  |
| 29 |  | 454 | . 463 | . 468 | . 465 | . 458 | . 447 | . 434 | . 421 | . 404 | . 389 | . 376 |  |
| 31 |  | . 465 | . 480 | . 488 | . 484 | . 478 | . 467 | . 456 | . 442 | . 427 | . 411 | . 398 |  |
| 33 |  | . 480 | . 494 | . 505 | . 503 | . 495 | . 487 | . 477 | . 464 | . 449 | . 432 | . 418 |  |
| 35 |  | . 493 | . 511 | . 552 | . 520 | . 513 | . 505 | . 505 | . 485 | . 471 | . 453 | . 437 |  |
| 37 |  | . 509 | . 526 | . 536 | . 536 | . 529 | . 521 | . 514 | . 502 | . 491 | . 473 | . 456 |  |
| 39 |  | . 518 | . 536 | . 545 | . 548 | . 545 | . 536 | . 531 | . 521 | . 509 | . 491 | . 473 | 461 |
| 41 |  | . 527 | . 544 | . 557 | . 559 | . 558 | . 551 | . 546 | . 536 | . 524 | . 509 | . 490 | 476 |
| 43 | . 517 | . 534 | . 554 | . 566 | . 569 | . 566 | . 563 | . 558 | . 551 | . 538 | . 523 | . 506 | 490 |
| 45 | . 521 | . 541 | . 561 | . 573 | . 575 | . 576 | . 572 | . 571 | . 564 | . 550 | . 536 | . 521 | 503 |
| 47 | . 521 | . 546 | . 563 | . 578 | . 583 | . 585 | . 583 | . 581 | . 576 | . 559 | . 548 | . 533 | 518 |
| 49 | . 518 | . 542 | . 565 | . 581 | . 595 | . 596 | . 591 | . 586 | . 581 | . 570 | . 556 | . 543 | 527 |

## TABLE 507.-SECULAR CHANGE OF VERTICAL INTENSITY, UNITED STATES

Smoothed values of vertical intensity in cgs units at the indicated places for January 1 of the years stated. The remarks about smoothing, in Table 502, apply to this table as well.

| Lat. | Long. | 30 | 1935 | 1940 | 1945 | 1950 | Lat. | Long. | 930 | 1935 | 1940 | 1945 | 1950 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $25^{\circ}$ | $80^{\circ}$ | . 4243 | . 4240 | . 4236 | . 4228 | . 4222 | $43^{\circ}$ | $70^{\circ}$ | . 5417 | . 5382 | . 5370 | . 5365 | . 5343 |
| 25 | 90 | . 4174 | . 4171 | . 4162 | . 4148 | . 4139 | 43 | 80 | . 5754 | . 5719 | . 5698 | . 5687 | . 5660 |
| 25 | 100 | . 3959 | . 3952 | . 3933 | . 3914 | . 3896 | 43 | 90 | . 5771 | . 5734 | . 5715 | . 5702 | . 5659 |
| 31 | 80 | . 4902 | . 4889 | . 4887 | . 4881 | . 4875 | 43 | 100 | . 5696 | . 5658 | . 5639 | . 5618 | . 5579 |
| 31 | 90 | . 4835 | . 4823 | . 4810 | . 4794 | . 4778 | 43 | 110 | . 5486 | . 5451 | . 5434 | . 5413 | . 5381 |
| 31 | 100 | . 4644 | . 4624 | . 4603 | . 4582 | . 4559 | 43 | 120 | . 5158 | . 5115 | . 5104 | . 5085 | . 506 |
| 31 | 110 | . 4351 | . 4332 | . 4307 | . 4292 | . 4268 | 47 | 70 | . 5559 | . 5511 | . 5496 | . 5498 | . 546 |
| 37 | 80 | . 5415 | . 5389 | . 5378 | . 5370 | . 5356 | 47 | 80 | . 5907 | . 5856 | . 5828 | . 5824 | . 578 |
| 37 | 90 | . 5368 | . 5341 | . 5332 | . 5312 | . 5287 | 49 | 90 | . 6110 | . 6067 | . 6029 | . 6024 | . 596 |
| 37 | 100 | . 5236 | . 5207 | . 5189 | . 5167 | . 5137 | 49 | 100 | . 5979 | . 5937 | . 5905 | . 5897 | . 5860 |
| 37 | 110 | . 5005 | . 4977 | . 4961 | . 4938 | . 4908 | 49 | 110 | . 5806 | . 5754 | . 5729 | . 5722 | . 570 |
| 37 | 120 | . 4654 | . 4623 | . 4612 | . 4591 | . 4564 | 49 | 120 | . 5531 | . 5474 | . 5461 | . 5452 | . 543 |

## TABLE 508.-TOTAL MAGNETIC INTENSITY, UNITED STATES

This table gives for the epoch January 1, 1950, the smoothed total intensity, $F$, expressed in cgs units, corresponding to the longitudes west of Greenwich in the heading and the north latitudes in the first column. The remarks about smoothing, in Table 502, apply to this table as well.

| ${ }^{1}{ }^{\lambda}$ | $65^{\circ}$ | $70^{\circ}$ | $75^{\circ}$ | $80^{\circ}$ | $85^{\circ}$ | $90^{\circ}$ | $95^{\circ}$ | $100^{\circ}$ | $105^{\circ}$ | $110^{\circ}$ | $115^{\circ}$ | $120^{\circ}$ | $125^{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $21^{\circ}$ |  |  | . 463 |  |  |  |  |  |  |  |  |  |  |
| 23 |  |  | . 480 | . 480 | . 477 | . 481 | . 475 | . 469 | . 461 |  |  |  |  |
| 25 |  |  | . 495 | . 495 | . 496 | . 496 | . 489 | . 482 | . 473 | . 464 | . 453 |  |  |
| 27 |  |  | . 508 | . 514 | . 512 | . 509 | . 504 | . 497 | . 487 | . 476 | . 464 | . 454 |  |
| 29 |  | . 510 | . 520 | . 526 | . 526 | . 524 | . 518 | . 509 | . 501 | . 488 | . 476 | . 466 |  |
| 31 | $\ldots$ | . 515 | . 530 | . 539 | . 539 | . 536 | . 530 | . 523 | . 514 | . 502 | . 490 | . 480 |  |
| 33 |  | . 525 | . 539 | . 550 | . 552 | . 547 | . 543 | . 536 | . 528 | . 517 | . 503 | . 493 |  |
| 35 |  | . 533 | . 550 | . 562 | . 562 | . 558 | . 535 | . 549 | . 541 | . 531 | . 518 | . 505 |  |
| 37 |  | . 544 | . 561 | . 570 | . 572 | . 568 | . 564 | . 560 | . 552 | . 544 | . 530 | . 518 |  |
| 39 |  | . 549 | . 566 | . 575 | . 579 | . 578 | . 572 | . 571 | . 564 | . 556 | . 542 | . 528 | . 519 |
| 41 |  | . 554 | . 570 | . 582 | . 586 | . 586 | . 582 | . 580 | . 574 | . 566 | . 554 | . 539 | . 529 |
| 43 | . 543 | . 558 | . 576 | . 588 | . 591 | . 590 | . 589 | . 587 | . 583 | . 574 | . 563 | . 549 | . 537 |
| 45 | . 543 | . 562 | . 581 | . 592 | . 594 | . 596 | . 594 | . 595 | . 591 | . 581 | . 571 | . 559 | . 545 |
| 47 | . 541 | . 564 | . 580 | . 594 | . 599 | . 601 | . 601 | . 602 | . 599 | . 585 | . 577 | . 565 | . 554 |
| 49 | . 535 | . 557 | . 579 | . 594 | . 607 | . 609 | . 606 | . 603 | . 600 | . 592 | . 581 | . 572 | . 559 |

## TABLE 509.-_SECULAR CHANGE OF TOTAL INTENSITY, UNITED STATES

Smoothed values of total intensity in cgs units at the indicated places for January 1 of the years stated. The remarks about smoothing, in Table 502, apply to this table as well.

| Lat. | Long. | 1930 | 1935 | 1940 | 1945 | 195 | Lat. | Long. | 1930 | 1935 | 1940 | 45 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $25^{\circ}$ | $80^{\circ}$ | . 5004 | . 4980 | . 4964 | . 4956 | . 4951 | $43^{\circ}$ | $70^{\circ}$ | . 5656 | . 5619 | . 5604 | . 5601 | . 5581 |
| 25 | 90 | . 5026 | . 5002 | . 4984 | . 4968 | . 4959 | 43 | 80 | . 5978 | . 5940 | . 5915 | . 5907 | . 5881 |
| 25 | 100 | . 4912 | . 4889 | . 4864 | . 4843 | . 4823 | 43 | 90 | . 6014 | . 5974 | . 5952 | . 5942 | . 5901 |
| 31 | 80 | . 5441 | . 5414 | . 5402 | . 5398 | . 5393 | 43 | 100 | . 5985 | . 5944 | . 5923 | . 5906 | . 5869 |
| 31 | 90 | . 5441 | . 5415 | . 5394 | . 5380 | . 5364 | 43 | 110 | . 5845 | . 5807 | . 5788 | . 5770 | . 5740 |
| 31 | 100 | . 5332 | . 5303 | . 5276 | . 5255 | . 5232 | 43 | 120 | . 5589 | . 5545 | . 5532 | . 5516 | . 5493 |
| 31 | 110 | . 5120 | . 5092 | . 5064 | . 5047 | . 5023 | 47 | 70 | . 5734 | . 5686 | . 5669 | . 5673 | . 5642 |
| 37 | 80 | . 5773 | . 5739 | . 5722 | . 5716 | . 5703 | 47 | 80 | . 6062 | . 6010 | . 5981 | . 5979 | . 5940 |
| 37 | 90 | . 5768 | . 5733 | . 5719 | . 5701 | . 5677 | 49 | 90 | . 6237 | . 6194 | . 6156 | . 6153 | . 6095 |
| 37 | 100 | . 5703 | . 5668 | . 5647 | . 5626 | . 5597 | 49 | 100 | . 6142 | . 6099 | . 6067 | . 6061 | . 6026 |
| 37 | 110 | . 5546 | . 5513 | . 5494 | . 5473 | . 5444 | 49 | 110 | . 6022 | . 5970 | . 5945 | . 5940 | . 5920 |
| 37 | 120 | . 5271 | . 5237 | . 5222 | . 5202 | . 5176 | 49 | 120 | . 5812 | . 5754 | . 5741 | . 5734 | . 5715 |

The usual conventions are followed as explained in connection with Table 502.
In addition to permanent geomagnetic observatories, there are given the numerous series of magnetic records obtained for the better part of a
year by special expeditions, as, for example, those obtained during the two International Polar Years of $1882-83$ and $1932-33$; all are listed in decreas-
ing order of north latitude.
Generally, values are from continuous magnetograph records for all days, and are for mean of year.
The many special notes applying to individual observatories have been omitted in the tabulation; these may be obtained from the references cited
below if desired. However, the following general types of notes should be taken cognizance of:

\[

=\)|  Observatory so marked is in a region of local magnetic disturbance.  |
| :--- |

\]

\[\)|  a break occurred between the preceding and following years due to change in procedure, method, standard, or site.  |
| :--- |

\]

\[\)|  Means quoted here are for all days, and may differ slightly from previously published means for  10  quiet days, given in offi-  |
| :--- |
|  cial publication of U.S. Coast and Geodetic Survey.  |

\]





$* *$ For references, see bibliography, p. 501.
$\dagger \gamma=10^{-5} \mathrm{cgs}$.
Observatory
Teplitz Bay (Ca Teplitz Bay (Camp Abruzzi).
Alger Island ................... Bay Tikhaya (Calm Bay) . Refuge Harbor (Greenland) Cape Thordsen (Spitsbergen) Sveagruvan (Spitsbergen) Chelyuskin

Jekman Island.
Point Barrow

| $\underset{D}{\text { Declination }}$ | $\underset{I}{\text { Inclination }}$ | $\begin{gathered} \text { Horizontal } \\ H \\ \gamma \end{gathered}$ | North X $\gamma$ | $\underset{Y}{\text { East }}$ <br> $\gamma$ | $\begin{gathered} \text { Vertical } \\ Z \\ \gamma \end{gathered}$ | $\begin{gathered} \text { Total } \\ F \\ \gamma \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |
| $-21^{\circ} 43^{\prime} 8$ | $+76{ }^{\circ} 53.5$ | 11726 | 10890 | -4340 | $+50352$ | 51699 |
| $-3433.2$ | +78 17.9 | 10576 | 8710 | -5998 | $+51063$ | 52147 |
| - 407.7 |  | 11567 | 11537 | - 833 |  |  |
| - 210.6 | +77 25.8 | 11244 | 11236 | -427 | $+50424$ | 51662 |
| $-154.3$ | +7728.4 | 11213 | 11207 | - 373 | $+50647$ | 51698 |
| + 546.2 | +7725.5 | 11341 | 11284 | $+1140$ | $+50838$ | 52088 |
| - 542 | +7608 | 12233 | 12172 | -1215 | +49555 | 51042 |
| -57 41.1 | +8134.7 | 8227 | 4398 | -6953 | $+55564$ | 56170 |
| -55 28.0 | +8134.5 | 8174 | 4634 | -6734 | $+55193$ | 55795 |
| +4225 | +8151.6 | 8448 | 6237 | +5698 | $+59061$ | 59662 |
| - 606 | +89 17.3 | 750 | 746 | - 80 | +60434 | 60439 |
| + 236.5 | +7604.0 | 12207 | 12194 | +556 | +49202 | 50693 |
| + 425.1 | +76 32.2 | 11882 | 11847 | $+915$ | $+49630$ | 51033 |
| + 644.0 | +76 11.7 | 12318 | 12233 | $+1444$ | $+50118$ | 51609 |
| +15 41.2 | +75 37.2 | 13707 | 13196 | $+3706$ | $+53460$ | 55189 |
| $(+1537.5$ | +75 36.7 | 13720 | 13213 | +3695 | +53478 | 55210) |
| -39 52.9 | +78 18.1 | 10705 | 8215 | -6864 | $+51699$ | 52796 |
| $(+2952.4$ | +7711.2 | 12582 | 10910 | $+6267$ | $+55323$ | 56736) |
| ( +29 46.1 | +7711.9 | 12587 | 10926 | +6249 | +55395 | 56807) |
| -52 12.1 | +85 29.2 | 4722 | 2894 | -3731 | +59824 | 60010 |
| -12 36.1 | +86 23.4 | 3834 | 3742 | -836 | +60762 | 60883 |
| +3730.7 | +8239.0 | 7734 | 6135 | +4709 | +59956 | 60453 |
| - 904.1 | +7324.1 | 16147 | 15945 | -2545 | +54169 | 56524 |
| $(-914.8$ | +7309.9 | 16393 | 16180 | -2634 | +54179 | 56605) |
| (-708 | +73 36.4 | 13900 | 13792 | -1726 | $+47250$ | 49252) |
| (-6 16 | +73 44.6 | 13837 | 13754 | -1510 | $+47450$ | 49426) |
| -17 08.0 |  | 14500 | 13857 | -4272 |  |  |
| (-17 36.4 |  | 14524 | 13844 | -4393 |  |  |
| -43 20.8 | +7738.1 | 11616. | 8447 | -7973 | $+52989$ | 54247 |
| (continued) |  |  |  |  |  |  |



|  |  | $\begin{aligned} & \text { No } \\ & \text { NO } \\ & \text { NON } \end{aligned}$ | $\begin{array}{ll} \sim & 0 \\ \sim & \\ \sim & 8 \end{array}$ | $\begin{aligned} & \text { NO } \\ & \text { NN } \\ & \text { NN } \end{aligned}$ | $\infty$ O N N | $\begin{aligned} & \infty \\ & \stackrel{\infty}{0} \\ & \stackrel{0}{\mathrm{o}} \end{aligned}$ | $\stackrel{\circ}{\circ}$ 국 | $\bigcirc$ | 3 - - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NoJ | ऽलN | 옹 윽 | ल⿵冂 | N | 아 | $\bigcirc$ | 2 | 5 |
|  | $\begin{aligned} & \text { gag } \\ & ++1 \end{aligned}$ | 잉 $+t+$ | ¢ + + | 20 + | + | 3 + + | O O + | O + + | O + |


TABLE 510.-MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES (continued)

| Observatory | $\begin{aligned} & \text { Latitude } \\ & ( \pm 三 N, \\ & (=S) \end{aligned}$ | Longitude east | Year | $\underset{D}{\text { Declination }}$ | $\underset{I}{\text { Inclination }}$ | Components of intensity |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Horizontal H | $\begin{gathered} \text { North } \\ X \end{gathered}$ | ${ }_{Y} \text { East }$ | $\underset{Z}{\text { Vertical }}$ | Total F |
|  |  |  |  |  |  | $\stackrel{\gamma}{\gamma}$ | ${ }^{\gamma}$ | $\gamma$ 3561 | $\gamma$ +46624 | $\gamma$ 48835 |
|  | $+60^{\circ} 08^{\prime}$ | $358^{\circ} 49^{\prime}$ | 1930 | $-14^{\circ} 11.2$ | +72 ${ }^{\circ} 41.6$ | 14527 | 14084 | -3561 | $\underline{+46624}$ | $\underline{48835}$ |
| Lerwick |  |  | 1944 | -1139.3 | +7258.0 | 14381 | 14084 | -2905 | $+46937$ | 49091 |
|  |  |  | 1946 | -11 21.3 | +7300.2 | 14364 | 14083 | -2828 | +46990 | 49136 |
| Oslo (Christiania) | +59 55 | 1043 | 1929 | - 807.0 |  | 15934 | 15774 | -2250 |  |  |
|  |  |  | 1930 | - 758.9 |  | 15929 | 15775 | -2212 |  |  |
| Slutsk (Pavlovsk, succeed Leningrad) | $+5941$ | 3029 | 1939 | + 504.9 | +72 14.1 | 15260 | 15200 | +1352 | $+47631$ | 50016 |
|  |  |  | 1941 | + 516.8 | +72 18.2 | 15228 | 15163 | +1401 | $+47725$ | 50096 |
| Lovö | +5921 | 1750 | 1940 | - 128.1 | +7152.6 | 15317 | 15312 | - 393 | $+46979$ | 49241 |
|  |  |  | 1946 | - 042.4 | +72 03.2 | 15231 | 15230 | - 188 | +47024 | 49429 |
| Sitka ${ }^{\text {a }}$ | +5703 | 22440 | 1920 | +30 28.5 | +7422.3 | 15568 | 13417 | +7896 | +55655 | 57791 |
|  |  |  | 1930 | +30 15.6 | +74 22.8 | 15449 | 13344 | +7785 | +55256 | 57375 |
|  |  |  | 1945 | +29 30.2 | +74 15.4 | 15513 | 13501 | $+7640$ | +55029 | 57174 |
|  |  |  | 1947 | $(+2922.6$ | +7415.8 | 15503 | 13510 | $+7605$ | +55016 | 57159) |
| Sverdlovsk (Katharinenburg) | $+5650$ | 6038 | 1899 | + 959.6 | +7042.0 <br> +7220.3 | 17795 | 17525 | +3088 | $\underline{+50815}$ | 53840 |
|  |  |  | 1929 | +10 57.2 | +72 20.3 | 16285 | 15988 | +3094 | $+51145$ | 53676 |
|  |  |  | 1931 | +1054.6 | +7226.9 | 16200 | 15907 | +3066 | +51220 | 53721 |
| Vyssokaya Dubrava (succeeding Sverd |  |  |  |  |  |  |  |  |  |  |
|  | +56 44 | 6104 | 1940 | +1257.2 +1303.0 | +7231.9 +7240.0 | 16085 | 15676 | +3606 +3620 | +51116 +51360 | 53587 52803 |
| Rude Skov (succeeding Copenhagen) | $+5551$ | 1227 | 1934 | +1203.0 +600.4 | +721.9 +6919.0 | 16893 | 16800 | +3620 -1768 | +51360 +44747 | 52803 47829 |
|  |  |  | 1944 | - 351.0 | +69 45.6 | 16710 | 16672 | -1122 | +45318 | 48301 |
|  |  |  | 1946 | - 334.8 | +69 49.3 | 16680 | 16647 | -1041 | +45386 | 48354 |
| Zaimishche (new site of Kasan)..... | +55 50 | 4851 | 1940 | +927.5 | +7110.5 | 16651 | 16425 | $+2736$ | +48441 | 51601 |
|  |  |  | 1945 | $\left(\begin{array}{l}+940.9\end{array}\right.$ | +7121.7 | 16560 | 16324 | +2785 | $+49096$ | 51814) |
| Kasan | +5547 | 4908 | 1909 | + 805.1 | +69 09.1 | 18118 | 17938 | $+2548$ | $+47575$ | 50908 |
|  |  |  | 1913 | + 810.9 | +69 18.2 | 17959 | 17776 | $+2556$ | $+47535$ | 50815 |
| Kutchino | +55 46 | 3758 | 1927 | + 636.1 | +68 59.5 | 17875 | 17756 | +2055 | $+46545$ | 59859 |
| Copenhagen | +55 41 +5519 | 1234 35648 | 1900 | -10 12.2 | +6839.0 +69432 | 17513 | 17236 16036 | -3102 | +44803 +44881 | 48104 |
| Eskdalemuir | +5519 | 35648 | 1930 | -1447.1 -1205.9 | +6839.2 +6954.0 | 16585 | 16036 | -4232 | +44881 +45134 | 47847 48061 |
| Gross Raum | +5450 | 2030 | 1925 | - 218.3 | +68 01.9 | 17771 | 17757 | -715 | $+44055$ | 47504 |
|  |  |  | 1935 | - 043.1 | +68 33.5 | 17530 | 17529 | - 221 | +44636 | 47955 |
| Flensburg | $+5447$ | 926 | 1903 | -11 28.0 | .... | . . . | .... | .... | . . . | .... |
|  |  |  |  | (continued) |  |  |  |  |  |  |

TABLE 510.-MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES (continued)

| $\begin{aligned} & \text { Latitude } \\ & ( \pm 三 N) \\ & (=S) \end{aligned}$ | Longitudeeast | Year | $\underset{D}{\text { Declination }}$ | $\underset{I}{\text { Inclination }}$ | Components of intensity |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Horizontal H | North $X$ | $\underset{Y}{\text { East }}$ | ${ }_{Z}^{\text {Vertical }}$ | Total $F$ |
|  |  |  |  |  | $\gamma$ | $\gamma$ | $\gamma$ | ${ }^{\gamma}$ | $\gamma$ |
| $54^{\circ} 37^{\prime}$ | $246^{\circ} 40^{\prime}$ | 1920 | $+27^{\circ} 38.6$ | $+77^{\circ} 53.6$ | 12923 | 11445 | +5996 | $+60246$ | 61617 |
|  |  | 1942 | +25 33.6 | +7751.8 | 12729 | 11482 | +5492 | $+59188$ | 60541 |
| +54 36 | 1848 | 1934 | - 235.5 | +68 25.2 | 17553 | 17535 | - 794 | +44384 | 47729 |
| +54 25 | 1839 | 1903 | - 713 |  |  |  |  |  |  |
| +5422 | 1245 | 1903 | - 952.9 | +67 37.6 | 18261 | 17990 | -3134 | $+44363$ | 47974 |
| + 5421 | 1224 | 1903 | -1008 |  |  | . . . . | .... |  |  |
| +5406 | 1208 | 1903 | -10 08 |  |  |  |  |  |  |
| +5351 | 35732 | 1920 | -15 52.9 | $+6843.5$ | 17303 | 16640 | -4734 | +44429 | 47679 |
|  |  | 1943 | -11 30.5 | +68 54.5 | 17166 | 16820 | -3425 | +44504 | 47699 |
| +53 45 | 904 | 1939 | - 559.1 | +68 12.0 | 17636 | 17540 | -1839 | +44092 | 47488 |
|  |  | 1946 | - 459.7 | +68 21.2 | 17601 | 17534 | -1532 | +44347 | 47712 |
| +53 27 | 1434 | 1901 | -843 |  |  |  |  |  |  |
| +52 49 | 640 | 1940 | - 709.2 | $+6739.2$ | 17959 | 17820 | -2236 | $+43686$ | 47233 |
|  |  | 1946 | -614.7 | +67 45.0 | 17946 | 17840 | -1952 | $+43867$ | 47396 |
| +5228 | 10402 | 1899 | +208.8 | +70 27.8 | 19948 | 19934 | P +747 | +56220 | 59654 |
|  |  | 1930 | $(+017.7$ | $+7121.5$ | 19019 | 19019 | + 98 | $+56380$ | 59500) |
|  |  | 1945 | (-0 47.7 | +71 34.4 | 19028 | 19026 | - 264 | +57109 | $60196)$ |
| +52 23 | 1304 | 1899 | $-1000.7$ | +66 25.7 | 18818 | 18531 | -3271 | $+43133$ | 47060 |
|  |  | 1920 | - 729.4 | +66 33.5 | 18606 | 18447 | -2425 | +42912 | 46772 |
|  |  | 1927 | - 609.1 | +66 44.0 | 18489 | 18383 | -1981 | +43002 | 46809 |


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 (continued)

$\begin{array}{ll}+42899 & 46776 \\ +43106 & 46888 \\ +56293 & 59682 \\ +56081 & 59360 \\ +43565 & 47310 \\ +43084 & 46801 \\ +43263 & 46945 \\ +43431 & 47182\end{array}$




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TABLE 510.-MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES (continued)





TABLE 510.-MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES (continued)

| $\underset{H}{\text { Horizontal }}$ | $\begin{gathered} \text { North } \\ X \end{gathered}$ | ${ }_{Y}^{\text {East }}$ | $\underset{Z}{\text { Vertical }}$ | Total F |
| :---: | :---: | :---: | :---: | :---: |
| $\gamma$ | $\gamma$ | $\gamma$ | $\gamma$ | $\boldsymbol{\gamma}$ |
| 20314 | 20168 | -2432 | $+40813$ | 45593 |
| 20299 | 20188 | -2118 | $+41005$ | 45754 |
| 20314 | 20259 | -1497 | +41578 | 46275 |
| 20638 | 20353 | -3415 | $+40750$ | 45678 |
|  |  |  |  |  |
| 20730 | 20475 | -3257 | $+40752$ | 45721 |
| 20011 | 19737 | -3296 | +41374 | 45959 |
| 20085 | 19889 | -2801 | +41658 | 46247 |
| 21076 | 20937 | -2413 | +40521 | 45674 |
| 20917 | 20826 | -1951 |  |  |
| 20299 | 19963 | -3677 | $+41058$ | 45802 |
| 20383 | 20108 | -3337 | $+41250$ | 46011 |
| 25067 | 24737 | -4052 | $+44643$ | 51199 |
| 25191 | 24846 | -4154 | +44764 | 51365 |
| 21413 | 21412 | + 220 | +41875 | 47032 |
| 21267 | 21256 | - 6988 | +42099 | 47105 |
| 21213 | 21205 | - 595 | +42206 | 47237 |
| 22120 | 21815 | -3662 | +38899 | 44748 |
| 22049 | 21911 | -2466 | +38690 | 44532 |
| 22137 | 22011 | -2360 | +38818 | 44686 |
| 22196 | 22086 | -2212 |  |  |
| 15290 | 15158 | -2006 | $+56503$ | 5853 |
| 15303 | 15171 | -2004 | $+56460$ | 58497 |
| 22390 | 21895 | -4681 | +39087 | 45046 |
| 21913 | 21235 | -5411 | +39408 | 45091 |
| 22013 | 21360 | -5324 | +39498 | 45218 |
| 26826 | 26519 | -4049 | +44579 | 52028 |
| 16913 | 26601 | -4086 | +44662 | 52144 |
| 22418 | 21779 | $-5313$ | +38829 | 44836 |






|  | 응 | 3 | 5 | in | N- | cinfovis | N |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $10 \infty$ | $\stackrel{\infty}{+\infty}+$ | $\stackrel{\infty}{+}$ | $\stackrel{\infty}{+}$ | $\stackrel{+}{+}$ | $\begin{aligned} & \text { + } \\ & +\underset{+}{+} \end{aligned}$ | 눈안안 <br> $+++++$ |  |  |  |  |  |





| $\begin{aligned} & \text { Latitude } \\ & (+\equiv N \end{aligned}$ | Longitude east |
| :---: | :---: |
| $+42^{\circ} 05^{\prime}$ | $44^{\circ} 42^{\prime}$ |
| +4150 | 4442 |
| +4143 | 4448 |
| +4125 | 6912 |
| $+4120$ | 6918 |
| +4052 | 1415 |
| +40 49 | 030 |
| $+4012$ | 35135 |
| $+3847$ | 26450 |
| +38 44 | 28310 |
| +38 43 | 35051 |
| +3759 | 2342 |
| +3746 | 33421 |
| +3730 | 12638 |
| +36 28 | 35348 |
| +3614 | 14011 |


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| Observatory | $\begin{aligned} & \text { Latitude } \\ & ( \pm \equiv N) \\ & \stackrel{=}{=}) \end{aligned}$ | Longitude east |
| :---: | :---: | :---: |
| Tsingtao | $+36^{\circ} 04^{\prime}$ | $120^{\circ} 19^{\prime}$ |
| Tokyo | +35 41 | 13945 |
| Ksara | +33 49 | 3553 |
| Tuscon ${ }^{\text {a }}$ | +32 15 | 24910 |
| Lukiapang (succeeding Zikawei). | +31 19 | 12102 |
| Zikawei | +31 12 | 12126 |
| Zô-sè | +3106 | 12111 |
| Dehra Dun | +30 19 | 7803 |
| Helwan | +29 52 | 3120 |
| Taihoku | +2502 | 12131 |
| Minamitori Shima | +24 17 | 15358 |
| Tamarasset | +22 48 | 532 |
| Barrackpore | +22 46 | 822 |
| Au Tau (succeeding Hongkong). | +22 27 | 11403 |
| Hongkong (superseded by Au Tau | +22 18 | 11410 |



| Horizontal H | $\begin{gathered} \text { North } \\ X \end{gathered}$ | $\underset{Y}{\text { East }}$ | $\stackrel{\text { Vertical }}{Z}$ | $\underset{F}{\text { Total }}$ |
| :---: | :---: | :---: | :---: | :---: |
| $\gamma$ | $\boldsymbol{\gamma}$ | $\boldsymbol{\gamma}$ | $\gamma$ | $\gamma$ |
| 29254 | 28868 | $+4737$ | +24758 | 38324 |
| 28838 | 28410 | +4951 | $+23712$ | 37335 |
| 28459 | 27995 | $+5117$ | +23158 | $36691)$ |
| 28346 | 27874 | $+5151$ | $+23146$ | $36596)$ |
| 28659 | 28075 | $+5757$ | $+22935$ | $36706)$ |
| 32160 | 31749 | $+5122$ | +33903 | 46730 |
| 30825 | 30385 | +5192 | +33235 | 45329 |
| 30622 | . 30192 | $+5116$ | +32884 | 44934 |
| 38675 | 38671 | $+544$ | +16394 | 42006 |
| 39207 | 39205 | - 364 | +16725 | 42625 |
| 37441 | 37440 | $+290$ | +14558 | 40172 |
| 37393 | 37393 | $+144$ | +15150 | 40345 |
| 36861 | 36853 | + 744 | +15578 | 40018 |
| 37253 | 37253 | - 87 | +17777 | 41277 |
| 37652 | 37651 | - 239 | +17906 | 41693 |
| (27494 | 27398 | -2321) | +35872 | 45197 |
| 27397 | 27238 | -2948 | $+35827$ | 45102 |
| 27430 | 27264 | -3012 | +35704 | 45024 |
| 28828 | 28804 | $-1177$ | +34203 | 44731 |
| 27566 | 27490 | -2043 | +34908 | 44480 |
| 38253 | 38252 | + 298 | $+10813$ | 39752 |
| 38356 | 38354 | + 404 | +10844 | 39859 |
| 38029 | 38025 | + 576 | $+11095$ | 39614 |
| 38215 | 38211 | + 571 | +10960 | 39756 |
| 37485 | 37480 | - 600 | + 2459 | 37566 |
| 37950 | 37927 | -1332 | + 3112 | 38077 |
|  | ... | . |  |  |
| 33142 | 33138 | - 538 | - 9904 | 34590 |




(continued)
TABLE 510.-MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES (continued)

| Observatory <br> Honolulu ${ }^{\text {a }}$ | Latitude $\begin{gathered} (+\equiv N \\ \pm=S) \\ +21^{\circ} 19^{\prime} \end{gathered}$ | $\begin{gathered} \text { Longitude } \\ \text { east } \\ 201^{\circ} 56^{\prime} \end{gathered}$ |
| :---: | :---: | :---: |
| Honolulu (new site) | +21 18 | 20154 |
| Teoloyucan ....... | +1945 | 26049 |
| Toungoo | +1856 | 9627 |
| Colaba (superseded Alibag) | +1854 | 7249 |
| Alibag (succeeding Colaba) | $+1838$ | 7252 |
| San Juan ${ }^{\text {a }}$ (superseding Vieques). | +1823 | 29353 |
| Vieques ${ }^{\text {" }}$ (succeeded San Juan). | +1809 | 29433 |
| Antipolo (superseding Manila) | +1436 | 12110 |
| Manila (succeeded by Antipolo).... | +1435 | 12058 |
| Kodakanai | $+1014$ | 7728 |
| Palau (Parao) | $+720$ | 13429 |
| Yaluit | + 555 | 16939 |
| Mogadiscio ......................... | $+202$ | 4521 |

TABLE 510.-MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES (continued)

|  | $\begin{aligned} & \text { Latitude } \\ & ( \pm \pm N) \end{aligned}$ | Longitude east | Year | $\underset{D}{\text { Declination }}$ | Inclination | Components of intensity |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | $\begin{gathered} \text { Horizontal } \\ H \\ \gamma \end{gathered}$ | $\begin{gathered} \text { North } \\ X \\ \gamma \end{gathered}$ | $\begin{gathered} \text { East } \\ \underset{\gamma}{\gamma} \end{gathered}$ | $\begin{gathered} \text { Vertical } \\ \underset{\gamma}{\gamma} \end{gathered}$ | $\begin{gathered} \text { Total } \\ F \\ \gamma \end{gathered}$ |
| Batavia-Buitenzorg | From magnetograph records at Batavia discontinued April |  |  | t Buitenzorg <br> 1,1899 , becau | (Latitude se of electri | longitude $106^{\circ} 47^{\prime}$ ) disturbances. |  | reduced to Batavia; recording |  |  |
|  | $-6^{\circ} 11^{\prime}$ | $106^{\circ} 49^{\prime}$ | $\begin{aligned} & 1902 \\ & 1926 \end{aligned}$ | $\begin{aligned} & +1^{\circ} 02.4 \\ & +051.6 \end{aligned}$ | $\begin{aligned} & -30^{\circ} 20^{\prime} 2 \\ & -3209.6 \end{aligned}$ | $\begin{aligned} & 36717 \\ & 36826 \end{aligned}$ | $\begin{aligned} & 36711 \\ & 36822 \end{aligned}$ | $\begin{aligned} & +666 \\ & +553 \end{aligned}$ | $\begin{aligned} & -21487 \\ & -23154 \end{aligned}$ | $\begin{aligned} & 42542 \\ & 43500 \end{aligned}$ |
| Batavia-Kuyper | From magnetograph records at Kuyper (Latitude $-6^{\circ} 02^{\prime}$, longitude $106^{\circ} 44^{\prime}$ ) reduced to Batavia; in dated November 15, 1941, the Director of the Observatory stated that the published values of 1928 Preface of "Report on magnetic observations in Batavia," 58B, 1935) are subject to correction becaus vious errors in the scale-values and that revised values will be supplied later. |  |  |  |  |  |  |  |  |  |
|  | $-611$ | 10649 | $\begin{aligned} & 1940 \\ & 1944 \end{aligned}$ | $\begin{array}{r} + \\ + \\ + \\ + \\ \hline \end{array}$ | $\begin{aligned} & -3232.0 \\ & -3231.6 \end{aligned}$ | $\begin{aligned} & 37035 \\ & 37145 \end{aligned}$ | $\begin{aligned} & 37025 \\ & 37133 \end{aligned}$ | $\begin{array}{r} +865 \\ +984 \end{array}$ | $\begin{aligned} & -23624 \\ & -23689 \end{aligned}$ | $\begin{aligned} & 43928 \\ & 44055) \end{aligned}$ |
| Dar-es-Salaam | -6 49 | 3918 | 1898 | $-818.1$ | -36 56.8 | 28966 | 28662 | -4182 | -21875 | 36244 |
| St. Paul de Loanda | - 849 | 1313 | 1910 | -16 12.3 | -35 32.2 | 20125 | 19325 | -5616 | -14374 | 24732 |
|  |  |  | 1918 | -15 03.5 | -36 04.2 | 19917 |  |  |  |  |
| Elisabethville | -1140 | 2728 | 1933 | - 932.1 | -46 01.3 | 23801 | 23472 | -3943 | -24665 | 34276 |
|  |  |  | 1945 | - 855.4 | -46 53.9 | 23286 | 23004 | $-3612$ | -24883 | 34079 |
| Huancayo | $-1203$ | 28440 | 1922 | + 807.6 | + 037.5 | 29735 | 29436 | +4203 | + 324 | 29737 |
|  |  |  | 1944 | + 634.8 | + 210.3 | 29367 | 29174 | $+3365$ | + 1114 | 29388 |
|  |  |  | 1946 | + 626.7 | + 206.6 | 29259 | 29074 | +3284 | + 1078 | 29279 |
| Samoa, Apia | -13 48 | 18814 | 1930 | +10 34.2 | -30 07.9 | 35195 | 34598 | +6456 | -20428 | 40694 |
|  |  |  | 1940 | +10 54.5 | $-3038.1$ | 34868 | 34238 | $+6598$ | -20650 | 40524 |
|  |  |  | 1946 | +1114.0 | $-3038.5$ | 34839 | 34172 | $+6787$ | -20683 | 40493 |
| Tanarive | $-1855$ | 4732 | 1910 | - 901.3 | -53 58.9 | 22585 | 22306 | -3542 | -31065 | 38407 |
|  |  |  | 1941 | - 938.5 | -53 54.3 | 21082 | 20784 | -3531 | -28916 | 35785 |
| Mauritius* | -20 06 | 5733 | 1899 | - 932.9 | -54 16.8 | 23854 | 23524 | -3957 | -33171 | 40857 |
|  |  |  | 1930 | -12 05.5 | -52 39.6. | 22697 | 22193 | -4753 | -29750 | 37420 |
|  |  |  | 1940 | -13 58.9 | -53 06.9 | 22419 | 21755 | $-5417$ | -29876 | 37352 |
|  |  |  | 1945 | -14 51.5 | -53 23.1 | 22389 | 21640 | $-5741$ | -30131 | 37539 |
| La Quiaca | -23 07 | 29425 | 1920 | + 603.3 | -12 39.6 | 26621 | 26472 | +2808 | - 5979 | 27284 |
|  |  |  | 1933 | + 416.7 | -12 21.2 | 26223 | 26150 | +1956 | - 5743 | 26845 |
| Vassouras (succeeding Rio de Janeiro) | -22 24 | 31621 | 1915 | -10 28.1 | -14 44.1 | 24700 | 24289 | -4488 | - 6496 | 25540 |
|  |  |  | 1942 | $-1358.8$ | $-1857.8$ | $23683$ | $22982$ | -5721 | $-8138$ | $25042$ |
|  |  |  | 1944 | -14 12.7 | -19 22.2 | 23563 | 22842 | -5785 | - 8284 | 24977 |

TABLE 510.-MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES (continued)

| $\underset{D}{\text { Declination }}$ | Inclination | $\begin{gathered} \text { Horizontal } \\ H \\ \gamma \end{gathered}$ | North X $\gamma$ | $\begin{gathered} \text { East } \\ Y \\ \gamma \end{gathered}$ | $\begin{gathered} \text { Vertical } \\ Z \\ \gamma \end{gathered}$ | Total F $\gamma$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $-7^{\circ} 55.7$ | $-13^{\circ} 17.1$ | 25040 | 24801 | -3454 | - 5912 | 25729 |
| - 855.3 | -13 57.2 | 24772 | 24472 | -3842 | - 6169 | 25529 |
| - 422.8 | -63 51.4 | 24925 | 24852 | -1904 | -50780 | 56567 |
| - 408.0 | -64 17.7 | 24623 | 24559 | -1775 | -51151 | 56769 |
| - 257.9 | -64 25.4 | 24767 | 24734 | -1281 | -51746 | 57368 |
| + 951.7 | -26 03.0 | 25894 | 25511 | +4435 | -12657 | 28822 |
| + 524.9 | -26 30.0 | 24137 | 24029 | +2278 | -12034 | 26971 |
| + 459.3 | -26 48.1 | 23884 | 23794 | +2077 | -12066 | 26759 |
| +14 59.5 |  |  |  |  |  |  |
| +1357.9 | $-2957.2$ |  |  |  |  |  |
| -24 39.9 | -63 09.2 | 15050 | 13677 | -6281 | -29733 | 33325 |
| -24 13.1 | -63 42.6 | 14357 | 13094 | -5889 | -29061 | 32413 |
| -23 54.5 | -63 59.0 | 14328 | 13098 | -5807 | -29352 | 32663 |
| -23 46.4 | -64 17.5 | 13875 | 12697 | -5594 | -28819 | 31985 |
| + 812.7 | -67 36.0 | 23071 | 22834 | +3295 | -55974 | 60542 |
| + 820.8 | -67 51.5 | 22872 | 22630 | $+3320$ | -56208 | 60683 |
| + 907.4 | $-6751.0$ | 22884 | 22594 | $+3628$ | -56215 | 60694 |
| + 825.1 | -67 23.1 | 23323 | 23072 | $+3414$ | -55989 | 60653 |
| + 800.8 | $-6755.1$ | 22874 | 22651 | +3189 | -56384 | 60847 |
| +1745.0 | -67 57.8 | 22365 | 21301 | +6819 | -55252 | 59607 |
| +1830.2 | -68 03.4 | 22248 | 21098 | $+7060$ | $-55220$ | 59533 |
| $(+1901.7$ | -68 04.8 | 22215 | 21001 | $+7243$ | -55203 | 59506) |
| $+1615.1$ | -67 40.8 | 22694 | 21787 | $+6351$ | -55277 | 59754 |
| +1748.3 | -68 18.3 | 22108 | 21049 | $+6760$ | -55570 | 59806 |
| -36 58.0 | $-7025.3$ | 16243 | 12978 | -9768 | -45672 | 48474 |
| +15 57.3 | -50 13.8 | 27306 | 26254 | $+7505$ | -32808 | 43685 |
| +15 10.3 | -49 43.4 | 26878 | 25941 | +7034 | -31719 | 41575 |
| +1502.4 | -49 39.4 | 26771 | 25854 | $+6947$ | -31520 | 41355 |
| + 516.6 | $-5431.0$ | 25667 | 25558 | $+2360$ |  |  |
| + 307.8 |  | 23928 | 23892 | +1307 |  |  |


| $\begin{array}{ll} & \text { Latitude } \\ \text { Observatory } \\ ( \pm \text { ( } \\ \text { O }\end{array}$ | $\underset{\text { east }}{\text { Longitude }}$ | Year | $\underset{D}{\text { Declination }}$ | I <br> Inclination |
| :---: | :---: | :---: | :---: | :---: |
| Rio de Janeiro |  |  |  |  |
| (superseded by Vassouras)....... $-22^{\circ} 55^{\prime}$ | $316^{\circ} 49^{\prime}$ | 1900 | - $7^{\circ} 55.7$ | $-13^{\circ} 17.1$ |
| Watheroo |  | 1906 | - 855.3 | -13 57.2 |
| Watheroo | 1552 | 1919 | - 422.8 | -6351.4 -6417.7 |
|  |  | 1945 | -257.9 | -64 25.4 |
| Pilar | 29607 | 1905 | + 951.7 | -26 03.0 |
|  |  | 1940 | + 524.9 | -26 30.0 |
|  |  | 1944 | + 459.3 | -26 48.1 |
| Santiago (new station) ............ -33 27 | 28918 | 1899 | +1459.5 |  |
|  |  | 1909 | +13 57.9 | -29 57.2 |
| Cape Town |  |  |  |  |
|  |  | 1941 | -24 13.1 | -63 42.6 |
| Hermanus (succeeding Cape Town). -34 25 | 1914 | 1940 | -23 54.5 | -63 59.0 |
|  |  | 1946 | -23 46.4 | -64 17.5 |
| Toolangi (succeeding Melbourne)... -37 32 | 14528 | 1919 | + 812.7 | -67 36.0 |
|  |  | 1930 | + 820.8 | -67 51.5 |
|  |  | 1944 | +907.4 | -67 51.0 |
| Melbourne (superseded by Toolangi). -37 50 | 14458 | 1899 | + 825.1 | -67 23.1 |
|  |  | 1920 | + 800.8 | -67 55.1 |
| Amberley (succeeding Christchurch) -43 10 | 17244 | 1929 | +1745.0 | -67 57.8 |
|  |  | 1940 | +18 30.2 | -68 03.4 |
|  |  | 1945 | $(+1901.7$ | -68 04.8 |
| Christchurch |  |  |  |  |
|  |  | 1930 | +1748.3 | -68 18.3 |
| Kerguelen , ....................... -49 25 | 6953 | 1902 | $-3658.0$ | -70 25.3 |
| New Year's Island (Staten Island).. -54 39 | 29551 | 1902 | +15 57.3 | -50 13.8 |
|  |  | 1914 | $+1510.3$ | -49 43.4 |
|  |  | 1916 | +1502.4 | -49 39.4 |
| Laurie Island . . . . . . . . . . . . . . . . . -60 43 | 31513 | 1905 | + 516.6 | $-5431.0$ |

(continued)
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Components of intensit
TABLE 510.-MEAN ANNUAL VALUES OF MAGNETIC ELEMENTS AT OBSERVATORIES (concluded)

| Components of intensity |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Horizontal } \\ H \end{gathered}$ | $\begin{gathered} \text { North } \\ X \end{gathered}$ | ${ }_{Y}{ }_{Y}$ | $\begin{gathered} \text { Vertical } \\ Z \end{gathered}$ | $\underset{F}{\text { Total }}$ |
| $\boldsymbol{\gamma}$ | $\gamma$ | $\boldsymbol{\gamma}$ | $\boldsymbol{\gamma}$ | $\boldsymbol{\gamma}$ |
| 13309 | 6171 | -11792 | -58206 | 59708 |
| 3112 | 3091 | - 358 | -67349 | 67421 |
| 4227 | -1802 | +3824 | -68146 | 68277 |
| 10038 | -2581 | +9700 | -66166 | 66923 |
| 9445 | -2695 | $+9053$ | -66296 | 66966 |
| 8983 | -2599 | $+8599$ | -66541 | 67145 |


| Longitude east | Year | Declination | $\underset{I}{\text { Inclination }}$ |
| :---: | :---: | :---: | :---: |
| $89^{\circ} 38^{\prime}$ | 1902 | $-62^{\circ} 22^{\prime} 6$ | $-77^{\circ} 07.2$ |
| 14240 | 1912 | 636.8 | -87 21.3 |
| 16624 | 1911 \} | +154 46.4 | -86 27.0 |
| 19609 | $1912\}$ | +104 54.0 |  |
| 19609 | $1941\}$ | +10454.0 | -81 22.4 |
| 19604 | $\left.\begin{array}{l} 1934 \\ 1935 \end{array}\right\}$ | +106 34.7 | -81 53.5 |
| 19612 | $1929\}$ | +106 49.1 | -82 18.7 |
|  | 1930 \} | +106 49.1 | -82 18.7 |


| Observatory | Latitude $( \pm 三 N)$ |
| :---: | :---: |
| Winter Station, Gauss. | $-66^{\circ} 02^{\prime}$ |
| Cape Denison | 6700 |
| Cape Evans . | -77 38 |
| Little America (III) | $-7829$ |
| Little America (II) | -78 34 |
| Little America (I) | -78 35 | OF 1922, FOR POINTS IN VARIOUS GEOGRAPHICAL LOCATIONS

















 $\underset{\substack{\text { Geo- } \\ \text { graphic } \\ \text { latitude }}}{\text {. }}$ $\stackrel{\circ}{\infty}$ 똥ํㅅ
엉응N

| 山 |  | $\left\lvert\, \begin{gathered} \text { B ANONA } \\ \hline \text { \| } \end{gathered}\right.$ | $\begin{aligned} & 0 \infty 0 \approx \pm \\ & 11111 \end{aligned}$ | №刃NNT |  <br> 11111 | 今～inco | 우ำnio | a |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{0}{x}$ |  |  |  | 제NN <br> ｜｜｜｜ | స్లిల్సべけ | gnipioti | oorinina |  |
| $\stackrel{0}{6}$ |  | $\begin{gathered} 8 \text { ONO } O \infty \\ 11 \mid 1 \end{gathered}$ | のニッツッ | のシ̃̃̃̃ |  | ーinco ㄲㅇㅇ <br> ｜11｜｜ |  |  |
| $\sum_{0}^{2}$ |  | $\stackrel{\circ}{\circ}-\operatorname{mon} a$ | Mnへの | స̃నNAN |  | ～요か | Ninoom | － |
| $\begin{aligned} & \text { 山 O } \\ & \text { U } \\ & \text { U } \end{aligned}$ |  | $\begin{aligned} & \text { ON }+\infty \infty 0 \\ & =1\|1\| l \mid \end{aligned}$ | $\because \approx 0 \infty \pi$ | NતNowo <br> 11।1। | Nopion | Nㅡㅇㄴㅇㅇ | Aicios | $\infty \times$ |
| ㅇ |  | $\begin{gathered} \text { minna = } \\ =1111 \mid \end{gathered}$ |  | iస |  | $3$ |  | \＃ |
|  |  | $\begin{aligned} & \text { minnag } \\ & =11111 \end{aligned}$ | Mッへのデ | సָ৷ |  | $8$ | ${\underset{i l}{\infty}}_{\infty}^{\infty}$ |  |
| $\underset{\sim}{x}$ | 范 | $\begin{aligned} & -m \operatorname{mon}= \\ & 1111 \end{aligned}$ | $\underset{1}{m \rightarrow n}$ | ふNતN |  |  | \|il |  |
|  | 들 |  |  |  |  | nion | か®® | \＃® |
|  | $\stackrel{\text { E．}}{\substack{\text { ¢ }}}$ | $\left\{\begin{array}{c} \text { gmina }= \\ 1\|1\| 1 \end{array}\right.$ |  |  |  | 80 | ¢1｜ | ¢ |
| ${ }^{2} 0$ | \| | $\begin{gathered} \infty N+\infty \infty \\ 1\|1\| \mid \end{gathered}$ | 궈ำ® | NTNo№ ｜｜｜｜｜ | $1$ |  | $\infty \infty$ |  |
| $\frac{\bar{E}}{\infty} \stackrel{\bar{x}}{5}$ | － | $\begin{gathered} \text { R-minna } \\ \|\|\|\|\mid \end{gathered}$ | $11$ | NiN | $\pm \underset{f}{\infty}$ | $0$ | ！ |  |
| $0 \geq$ |  | $\begin{array}{r} 8-\operatorname{ran} n \\ \|\|\|\mid \end{array}$ | $1111$ | －ิกึึN <br> ｜｜｜｜｜ | $1$ | $1$ | $i i$ |  |
|  |  |  | $111$ |  |  | $11$ | Nir |  |
|  |  | $\begin{array}{r} \text { tanont } \\ 11 \end{array}$ | $6 \infty$ <br> 1111 | ショ9テ̃ | \|cur | 운 | BNin |  |
| $0$ |  | $\begin{array}{r} \text { OATON } \\ 1 \end{array}$ | $\begin{aligned} & +0 \infty 007 \\ & 1\|1\| 1 \end{aligned}$ | キ゚へべデ | Nme | ج | 요윤 |  |
| $\mathrm{Z}_{\mathbf{U}}^{\infty}$ |  | かのでNo | $\begin{gathered} N+6 \infty 0 \\ 1\|\|\|\mid \end{gathered}$ |  | imen | 品芯 | Coinin |  |
|  |  | $\bigcirc 000 \mathrm{mon}$ | $\begin{aligned} & N+\infty \infty \\ & \|\|\|\|\mid \end{aligned}$ | 워サーニ | సimp | \|io | 介in |  |
| $\stackrel{\ddot{-}}{\stackrel{1}{n}}$ |  | $0 \simeq 0 \infty 0 \mathrm{o}$ | $\begin{gathered} \text { NONJO } \\ 1\|\mid \end{gathered}$ | かoำた | ふNિMల |  ｜1 1｜ | NㅓㅇㅇㅇN 11111 | へャ |
| $\begin{aligned} & \stackrel{\rightharpoonup}{山} \\ & \stackrel{\rightharpoonup}{\otimes} \\ & \stackrel{1}{2} \end{aligned}$ |  | O．ODONO <br>  | $\begin{gathered} N+\infty \infty \\ 1\|1\| l \end{gathered}$ |  | ㅍNN్లి | 寸NNㅇㅇㅇ ｜111｜ | प్ర NN요 <br> ｜11｜ | \＄0 |


| Geographic | Geographic east longitude in degrees |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| latitude * | 190 | 200 | 210 | 220 | 230 | 240 | 250 | 260 | 270 | 280 | 290 | 300 | 310 | 320 | 330 | 340 | 350 | 360 |
| $+88^{\circ}$ | 78 | 78 | 79 | 79 | 79 | 80 | 80 | 80 | 80 | 80 | 80 | 80 | 80 | 80 | 80 | 80 | 79 | 79 |
| +84 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 84 | 84 | 84 | 84 | 83 | 82 | 81 | 80 | 79 |
| +80 | 73 | 75 | 76 | 77 | 79 | 81 | 82 | 84 | 86 | 87 | 88 | 88 | 86 | 85 | 83 | 81 | 79 | 78 |
| +76 | 70 | 72 | 73 | 75 | 77 | 79 | 81 | 83 | 85 | 86 | 87 | 87 | 85 | 83 | 81 | 79 | 77 | 75 |
| $+72$ | 67 | 69 | 70 | 72 | 74 | 76 | 79 | 80 | 82 | 83 | 83 | 83 | 82 | 80 | 78 | 76 | 75 | 73 |
| +68 | 63 | 65 | 67 | 69 | 71 | 73 | 75 | 77 | 78 | 79 | 79 | 79 | 78 | 77 | 75 | 73 | 71 | 69 |
| +64 | 60 | 62 | 63 | 65 | 67 | 69 | 71 | 73 | 74 | 75 | 75 | 75 | 74 | 73 | 72 | 70 | 68 | 66 |
| +60 | 56 | 58 | 60 | 62 | 64 | 66 | 67 | 69 | 70 | 71 | 71 | 71 | 71 | 69 | 68 | 66 | 64 | 62 |
| $+56$ | 52 | 54 | 56 | 58 | 60 | 62 | 64 | 65 | 66 | 67 | 67 | 67 | 67 | 65 | 64 | 62 | 60 | 58 |
| $+52$ | 48 | 50 | 52 | 54 | 56 | 58 | 60 | 61 | 62 | 63 | 63 | 63 | 63 | 62 | 60 | 58 | 57 | 55 |
| $+48$ | 45 | 47 | 49 | 50 | 52 | 54 | 56 | 57 | 58 | 59 | 59 | 59 | 59 | 58 | 56 | 55 | 53 | 51 |
| +46 | 43 | 45 | 47 | 49 | 51 | 52 | 54 | 55 | 57 | 57 | 57 | 57 | 57 | 56 | 54 | 53 | 51 | 49 |
| +44 | 41 | 43 | 45 | 47 | 49 | 50 | 52 | 53 | 55 | 55 | 55 | 55 | 55 | 54 | 52 | 51 | 49 | 47 |
| $+42$ | 39 | 41 | 43 | 45 | 47 | 48 | 50 | 51 | 53 | 53 | 53 | 53 | 53 | 52 | 50 | 49 | 47 | 45 |
| $+40$ | 37 | 39 | 41 | 43 | 45 | 47 | 48 | 50 | 51 | 51 | 51 | 51 | 51 | 50 | 48 | 47 | 45 | 43 |
| $+38$ | 35 | 37 | 39 | 41 | 43 | 45 | 46 | 48 | 49 | 49 | 49 | 49 | 49 | 48 | 46 | 45 | 43 | 41 |
| +36 | 33 | 35 | 37 | 39 | 41 | 43 | 44 | 46 | 47 | 47 | 47 | 47 | 47 | 46 | 45 | 43 | 41 | 39 |
| +34 | 31 | 33 | 35 | 37 | 39 | 41 | 42 | 44 | 45 | 45 | 45 | 45 | 45 | 44 | 43 | 41 | 39 | 37 |
| +32 | 29 | 31 | 33 | 35 | 37 | 39 | 40 | 42 | 43 | 43 | 43 | 43 | 43 | 42 | 41 | 39 | 37 | 35 |
| $+30$ | 27 | 29 | 31 | 33 | 35 | 37 | 38 | 40 | 41 | 41 | 41 | 41 | 41 | 40 | 39 | 37 | 35 | 33 |
| $+28$ | 25 | 27 | 29 | 31 | 33 | 35 | 36 | 38 | 39 | 39 | 39 | 39 | 39 | 38 | 37 | 35 | 33 | 32 |
| $+26$ | 23 | 25 | 27 | 29 | 31 | 33 | 34 | 36 | 37 | 37 | 37 | 37 | 37 | 36 | 35 | 33 | 31 | 30 |
| +24 | 21 | 23 | 25 | 27 | 29 | 31 | 32 | 34 | 35 | 35 | 35 | 35 | 35 | 34 | 33 | 31 | 29 | 28 |
| $+22$ | 19 | 21 | 23 | 25 | 27 | 29 | 30 | 32 | 33 | 33 | 33 | 33 | 33 | 32 | 31 | 29 | 28 | 26 |
| +20 | 17 | 19 | 21 | 23 | 25 | 27 | 28 | 30 | 31 | 31 | 31 | 31 | 31 | 30 | 29 | 27 | 26 | 24 |
| +18 | 15 | 17 | 19 | 21 | 23 | 25 | 26 | 28 | 29 | 29 | 29 | 29 | 29 | 28 | 27 | 25 | 24 | 22 |
| +16 | 14 | 15 | 17 | 19 | 21 | 23 | 24 | 26 | 27 | 27 | 27 | 27 | 27 | 26 | 25 | 23 | 22 | 20 |
| $+14$ | 12 | 14 | 16 | 17 | 19 | 21 | 23 | 24 | 25 | 25 | 25 | 25 | 25 | 24 | 23 | 21 | 20 | 18 |
| +12 | 10 | 12 | 14 | 15 | 17 | 19 | 21 | 22 | 23 | 23 | 23 | 23 | 23 | 22 | 21 | 19 | 18 | 16 |
| +10 | 8 | 10 | 12 | 14 | 15 | 17 | 19 | 20 | 21 | 21 | 21 | 21 | 21 | 20 | 19 | 17 | 16 | 14 |











TABLE 511．－GEOMAGNETIC COORDINATES OF POSITION ON THE EARTH REFERRED TO THE GEOMAGNETIC AXIS POLE OF 1922，FOR POINTS IN VARIOUS GEOGRAPHICAL LOCATIONS（continued）

| : |  | añ\|l| |  | $\begin{gathered} \text { Nong } \\ \text { inion } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| $\text { 육 } \forall \mathrm{NO}_{\infty}$ | $\begin{array}{r} \text { TNONA } 0 \infty \text { ONT } \\ 1 \mid 1111 \end{array}$ | NNતNTM |  | $\begin{aligned} & \text { ngon } \\ & \text { ilitin } \end{aligned}$ |
|  | $\begin{array}{r} \text { OANON } F O \infty O N \\ 111111 \end{array}$ | NNNNN |  | $\begin{aligned} & \text { na } 2000 \\ & 11111 \end{aligned}$ |
| $\underset{m}{0} \pm \underset{\sim}{2}=a$ | $\begin{array}{r} \text { Nom- monä } \\ \|1\|\|\mid \end{array}$ |  |  | $\begin{gathered} \text { Wo Nosion } \\ 11111 \end{gathered}$ |
| $\stackrel{\sim}{\sim} \infty$ |  | TMNN |  | 5incio |
| 응ํํックニ | $\begin{array}{r} \text { anmmerna } \\ \|\|\|\|\mid \end{array}$ | MANNI |  | $\begin{aligned} & \text { mencou } \\ & 11111 \end{aligned}$ |
|  | $\begin{array}{r} \text { anmm-muna } \\ \|\|\|\|\mid \end{array}$ | TANN |  | mingion |
| 이으コニ | $\begin{array}{r} \text { anmemana } \\ \|\|\|\|\mid \end{array}$ | MANNI |  | minciog |
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TABLE 511．－GEOMAGNETIC COORDINATES OF POSITION ON THE EARTH REFERRED TO THE GEOMAGNETIC AXIS POLE OF 1922，FOR POINTS IN VARIOUS GEOGRAPHICAL LOCATIONS（concluded）

are given
alues，see
b，Fleming，J．A．，ed．，Terrestrial magnetism and electricity，Physics ．Serial 664， $1946 . \quad e$, Deel，Samuel A．，and Herbert Howe，H． H．，Laporte，L．Lange，İ，Cooper，C．，and Hendrix，W．C．，Descrip No． 580,1947 h，Macht，H．G．，Das erdmagnetisch Feld der
60, p． 876,$1941 ;$ vol． 69, p． 106,$1946 ;$ vol． 70, p． 202 ， 1946 1949．k，Blackett，P．M．S．，Nature，vol．159，p．658，1947．（Gives no．Wasserfall，Terr．Mag．，vol．44，p．263，1939．${ }^{\text {o．}}$ ．Aus－
vol．4，p．1，Adelaide，1944． p ，Terr．Mag．，vol．48，pp． $97-108$ ， States and possessions，by U．S．Coast and Geodetic Survey．
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$\begin{array}{llll}332 & 339 & 346 & 353 \\ 334 & 340 & 347 & 353\end{array}$
மo $\stackrel{\infty}{n}$ Chapman，S．i．and Bartels，J．，Geomagnetism，vols． 1 and 2，Oxford， 1940,
8，McGraw－Hill，New York， 1939 c，Ludy，Albert K．，and Herbert How

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ol． 197, p． 433,1
56, p． 283,195
 5，idem，Serial Carnegie Inst． ge analysis，Carnegie W．M．，
i，Elsasser，W． Bıbliography：a，C，McGraw－Ḧ ill，New York， 1939. 663，Washington，1945．tables and magnetic charts for 1945 tion of the earth＇s main magnetic field and its secular chan Scott，W．E．，The geomagnetic field，its description a
Polargebiete．Zeitschr．Meteorol．，vol．1．pp．289－297， j ，Bullard，E．C．，The nagnetic，field within the earth， recent review，theories of earth＇s field．）1，Journal of Geophysical Research，vol．
Bericht über die Tätigkeit des Preuss．Met．Inst．im Jahre 1929：Veroffentlichungen Bericht uber dic Tatigkeit des Preus．Met．Inst．im Jahre 1929：Veröoffentlichungen
tralian Antartic Research（B．A．N．Z．A．R．）Expedition 1929－3i（D．Mawson，ed．）， 1.182 ，and 23 ． in Hee．Fohnston，W．W．Scott，and Ella Balsam，Internat．Union Geod．and Geophys．， n H．F．Johnston，W．E．Scott，and Ella Balsam，Internat．Union Geod．and Geophys．
（1），Forecasts of geomagnetic activity，National Bureau of Standards．
World isomagnetic charts are issued by U．S．Hydrographic Office；for the United

## 502

TABLE 512.-MAGNETIC AND ELECTRIC DATA FOR SUN AND EARTH
(Chapman, Cosmical magnetic phenomena, Nature, vol. 124, p. 19, 1929.)
Sun's magnetic field too small to be measured by direct effects on earth; measured by Zeeman effect on spectrum lines.
Earth's magnetic axis inclined $12^{\circ}$ to rotation axis.
Earth's field rotates at same speed as nearly rigid earth.
Earth: Polar intensity of field $\frac{3}{3}$ gauss.
Sun: Intense local fields frequent, 3000 gauss. The magnetic field of spots reverses each cycle (Proc. Astron. Soc. Pacific, vol. 41, p. 136, 1929). The polarity of leading spot in a bipolar group in the Northern Hemisphere is opposite that in the Southern Hemisphererelationship reverses each new sunspot cycle $\therefore$ complete magnetic cycle is double sunspot cycle.


Further characteristics of spots: (Milne, Monthly Notices, Roy. Astron. Soc., vol. 90, p. 487,1930 .) Umbra (dark center), 800 (very small) to $80,000 \mathrm{~km}$ across: penumbra may reach $240,000 \mathrm{~km}$. Generally short-lived. A few last several (3) rotations, very rarely 6; one in 1840, 18 months. Most occur in 2 belts $5^{\circ}$ to $40^{\circ} \mathrm{N}$. and S. latitudes, often occur in pairs (see above). Umbra temperature $4000^{\circ} \mathrm{K}$. Evershed gives velocity of outburst from spot $2 \mathrm{~km} / \mathrm{sec}$.

Faraday discovered that, when a piece of heavy glass is placed in magnetic field and a beam of plane polarized light passed through it in a direction parallel to the lines of magnetic force, the plane of polarization of the beam is rotated. This was subsequently found to be the case with a large number of substances, but the amount of the rotation was found to depend on the kind of matter and its physical condition, and on the strength of the magnetic field and the wavelength of the polarized light. Verdet's experiments agree fairly well with the formula

$$
\theta=c l H\left(r-\lambda \frac{d r}{d \lambda}\right) \frac{r^{2}}{\lambda^{2}}
$$

where $c$ is a constant depending on the substance used, $l$ the length of the path through the substance, $H$ the intensity of the component of the magnetic field in the direction of the path of the beam, $r$ the index of refraction, and $\lambda$ the wavelength of the light in air. If $H$ be different, at different parts of the path, $l H$ is to be taken as the integral of the variation of magnetic potential between the two ends of the medium. Calling this difference of potential $v$, we may write $\theta=A v$, where $A$ is constant for the same substance, kept under the same physical conditions, when the one kind of light is used. The constant $A$ has been called "Verdet's constant," and a number of values of it are given in Tables 514-517. For variation with temperature the following formula is given by Bichat:

$$
R=R_{0}\left(1-0.00104 t-0.000014 t^{2}\right)
$$

which has been used to reduce some of the results given in the table to the temperature corresponding to a given measured density. For change of wavelength the following approximate formula, given by Verdet and Becquerel, may be used :

$$
\frac{\theta_{1}}{\theta_{2}}=\frac{\mu_{1}^{2}\left(\mu_{1}^{2}-1\right) \lambda_{2}^{2}}{\mu_{2}^{2}\left(\mu_{2}^{2}-1\right) \lambda_{1}^{2}}
$$

where $\mu$ is index of refraction and $\lambda$ wavelength of light.
A large number of measurements of what has been called molecular rotation have been made, particularly for organic substances. These numbers are not given in the table, but numbers proportional to molecular rotation may be derived from Verdet's constant by multiplying in the ratio of the molecular weight to the density. The densities and chemical formulas are given in the table. In the case of solutions, it has been usual to assume that the total rotation is simply the algebraic sum of the rotations which would be given by the solvent and dissolved substance, or substances, separately; and hence that determinations of the rotary power of the solvent medium and of the solution enable the rotary power of the dissolved substance to be calculated. Experiments by Quincke and others do not support this view, as very different results are obtained from different degrees of saturation and from different solvent media. No results thus calculated have been given in the table, but the qualitative result, as to the sign of the rotation produced by a salt, may be inferred from the table. For example, if a solution of a salt in water gives Verdet's constant less than 0.0130 at $20^{\circ} \mathrm{C}$, Verdet's constant for the salt is negative.

As a basis for calculation, Verdet's constant for carbon disulfide and the sodium line $D$ has been taken as 0.0130 at $20^{\circ} \mathrm{C}$.

| Wavelength | $.5 \mu$ | $1.0 \mu$ | $1.5 \mu$ | $2.0 \mu$ | $2.5 \mu$ |
| :--- | ---: | :--- | :---: | :---: | :---: |
| Steel $\ldots \ldots \ldots \ldots \ldots$ | $-11^{\prime}$ | $-16^{\prime}$ | $-14^{\prime}$ | $-11^{\prime}$. | -9.0 |
| Cobalt $\ldots \ldots \ldots \ldots \ldots$ | -9.5 | -11.5 | -9.5 | -11. | -6.5 |
| Nickel $\ldots \ldots \ldots \ldots \ldots$ | -5.5 | -4.0 | 0 | +1.75 | +3.0 |

Field intensity $=10,000$ cgs units. (Intensity of magnetization $=$ about 800 in steel, 700 to 800 in cobalt, about 400 in nickel.)

## TABLE 514.—VERDET'S CONSTANT

Part 1.-Solids

| Substance | Formula | Wavelength | Verdet's constan in min |
| :---: | :---: | :---: | :---: |
|  |  | $\stackrel{\mu}{58}$ |  |
| Amber | ZnS | . ${ }^{\prime \prime}$ | . 22334 |
| Diamond | C | " | . 0127 |
| Lead borate | $\mathrm{PbBr}_{2} \mathrm{O}_{4}$ | " | . 0600 |
| Selenium | Se | . 687 | . 4625 |
| Sodium borate | $\mathrm{Na}_{2} \mathrm{~B}_{4} \mathrm{O}_{7}$ | . 589 | . 0170 |
| Ziqueline (Cuprite) | $\mathrm{Cu}_{2} \mathrm{O}$ | . 687 | . 5908 |
| Fluorite .. | $\mathrm{CaF}_{2}$ | . 2534 | . 05989 |
|  |  | . 3655 | . 02526 |
|  |  | . 4358 | . 01717 |
|  |  | . 4916 | . 01329 |
|  |  | . 589 | . 00897 |
|  |  | 1.00 | . 00300 |
|  |  | 2.50 | . 00049 |
|  |  | 3.00 | . 00030 |
| Glass : |  |  |  |
|  |  | . 589 | . 0161 |
|  |  |  | . 0220 |
|  |  | " | . 0317 |
|  |  | " | . 0608 |
|  |  | " | . 0888 |
| Zeiss, ultraviolet |  | .313 .405 | . 06364 |
| " $\ldots . . . . . . . . . . . . . . . . .$. |  | . 436 | . 0311 |
| Quartz, along axis, i.e., plate cut $\perp$ to axis | $\dddot{S i O}_{2}$ | . 2194 | . 1587 |
|  |  | . 2573 | . 1079 |
|  |  | . 3609 | . 04617 |
|  |  | . 4800 | . 02574 |
|  |  | . 5892 | . 01664 |
|  |  | . 6439 | . 01368 |
| Rock salt | NaCl | . 2599 | . 2708 |
|  |  | . 3100 | . 1561 |
|  |  | . 4046 | . 0775 |
|  |  | . 4916 | . 0483 |
|  |  | . 6708 | . 0245 |
|  |  | 1.00 | . 01050 |
|  |  | 2.00 | . 00262 |
|  |  | 4.00 | . 00069 |
| Sugar, cane: along axis IIA. | $\mathrm{C}_{12} \mathrm{H}_{22} \mathrm{O}_{11}$ | . 451 | . 0122 |
|  |  | . 540 | . 0076 |
|  |  | . 626 | . 0066 |
| axis IIA ${ }^{1}$ | - | . 540 | . 0084 |
|  | KCl | . 626 | . 0075 |
| Sylvite |  | . 4358 | . 0534 |
|  |  | . 5461 | . 0316 |
|  |  | . 6708 | . 02012 |
|  |  | . 90 | . 01051 |
|  |  | 1.20 | . 00608 |
|  |  | 2.00 | . 00207 |
|  |  | 4.00 | . 00054 |

Part 2.-Liquids (for $\lambda=0.589 \mu$ )

| Substance | Chemical formula | $\begin{aligned} & \text { Density } \\ & \text { in } g \text { per } \\ & \mathrm{cm}^{3} \end{aligned}$ | Verdet's constant in min | ${ }^{\text {Temp. }}{ }^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: |
| Acetone | $\mathrm{C}_{3} \mathrm{H}_{8} \mathrm{O}$ | . 7947 | . 0113 | $20^{\circ}$ |
| Acids: Formic | $\mathrm{CH}_{2} \mathrm{O}_{2}$ | 1.2273 | . 0105 | 15 |
| Acetic | $\mathrm{C}_{2} \mathrm{H}_{4} \mathrm{O}_{2}$ | 1.0561 | . 0105 | 21 |
| Hydrochloric | HCl | 1.2072 | . 0224 | 15 |
| Hydrobromic | HBr | 1.7859 | . 0343 |  |
| Hydroiodic . | HI | 1.9473 | . 0515 | " |
| Nitric .... | $\mathrm{HNO}_{3}$ | 1.5190 | . 0070 | 13 |
| Alcohols: Methyl | $\mathrm{CH}_{3} \mathrm{OH}$ | . 7920 | . 0093 | 20 |
| Ethyl | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{OH}$ | . 7900 | . 0112 |  |
| Benzene ....... | $\mathrm{C}_{8} \mathrm{H}_{8}$ | . 8786 | . 0297 | " |
| Bromides : Methyl | $\mathrm{CH}_{3} \mathrm{Br}$ | 1.7331 | . 0205 | 0 |
| Ethyl | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Br}$ | 1.4486 | . 0183 | 15 |
| Carbon bisulfide | $\mathrm{CS}_{2}$ | 1.26 | . 0420 | 18 |
| Chlorides: Carbon | $\mathrm{CCl}_{4}$ | 1.60 | . 0321 | 15 |
| Chloroform | $\mathrm{CHCl}_{3}$ | 1.4823 | . 0164 | 20 |
| Ethyl .. | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Cl}$ | . 9169 | . 0138 | 6 |
| Iodides: Methyl . | $\mathrm{CH}_{3} \mathrm{I}$ | 2.2832 | . 0336 | 15 |
| Ethyl. | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{I}$ | 1.9417 | . 0296 |  |
| Nitrates: Methyl | $\mathrm{CH}_{3} \mathrm{O} \cdot \mathrm{NO}_{2}$ | 1.2157 | . 0078 |  |
| Ethyl . | $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{O} \cdot \mathrm{NO}_{2}$ | 1.1149 | . 0091 | " |
| Paraffins: Pentane | $\mathrm{C}_{5} \mathrm{H}_{12}$ | . 6332 | . 0118 | " |
| Hexane | $\mathrm{C}_{6} \mathrm{H}_{14}$ | . 6743 | . 0125 |  |
| Toluene ......... | $\mathrm{C}_{7} \mathrm{H}_{8}$ | 8581 | . 0269 | 28 |
| Water $=.2496 \mu$ | $\mathrm{H}_{2} \mathrm{O}$ 。 | .... | . 1042 | . |
| . 275 |  | .... | . 0776 |  |
| . 4046 |  | ... | . 0293 | $\cdots$ |
| . 589 |  |  | . 0131 |  |
| 1.000 |  | $\ldots$ | . 00410 |  |
| 1.300 |  |  | . 00264 |  |
| Xylene | $\mathrm{C}_{8} \mathrm{H}_{10}$ | . 8746 | . 0263 | 27 |

TABLE 515.-VERDET'S CONSTANT FOR SOLUTIONS OF ACIDS AND SALTS IN WATER $(\lambda=0.589 \mu)$

| Chemical formula | Density g per $\mathrm{cm}^{3}$ | Verdet's constant in min | $\underset{{ }^{\mathrm{T}} \mathrm{C} \mathrm{C} \text {. }}{ }$ | Chemical formula | $\begin{aligned} & \text { Density } \\ & \mathrm{g} \text { per } \\ & \mathrm{cm}^{3} \end{aligned}$ | Verdet's constant in min | $\underset{{ }^{\circ} \mathrm{C}}{\text { Temp. }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HBr | 1.3775 | . 0244 | $20^{\circ}$ | $\mathrm{Fe}_{2} \mathrm{Cl}_{\text {e }}$ | 1.6933 | -. 2026 | $15^{\circ}$ |
| HCl | 1.1573 | . 0204 | ، |  | 1.5315 | -. 1140 |  |
| * | 1.0762 | . 0168 | " | " | 1.1681 | -. 0015 | " |
| HI | 1.9057 | . 0499 | " | " | 1.0864 | . 0081 | " |
| [ | 1.1760 | . 0205 | " | " | 1.0232 | . 0122 | " |
| $\mathrm{HNO}_{3}$ | 1.3560 | . 0105 | " | $\mathrm{HgCl}_{2}$ | 1.0381 | . 0137 | 16 |
| $\mathrm{NH}_{3}$ | . 8918 | . 0153 | 15 | $\mathrm{NiCl}_{2}$ | 1.4685 | . 0270 | 15 |
| $\mathrm{NH}_{4} \mathrm{Br}$ | 1.2805 | . 0226 | " | " | 1.2432 | . 0196 | " |
| $\mathrm{BaBr}_{2}$ | 1.5399 | . 0215 | 20 | KCl | 1.6000 | . 0163 | " |
| $\mathrm{CdBr}_{2}$ | 1.3291 | . 0192 | " | NaCl | 1.0418 | . 0144 | " |
| $\mathrm{CaBr}_{2}$ | 1.2491 | . 0189 | " | $\mathrm{SrCl}_{2}$ | 1.1921 | . 0162 | " |
| KBr | 1.1424 | . 0163 | " | $\mathrm{SnCl}_{2}$ | 1.3280 | . 0265 | " |
| " | 1.0876 | . 0151 | " | $\mathrm{ZnCl}_{2}$ | 1.2851 | . 0196 | " |
| NaBr | 1.1351 | . 0165 | " | $\mathrm{NH}_{4} \mathrm{I}$ | 1.5948 | . 0396 | " |
|  | 1.0824 | . 0152 | " | " | 1.2341 | . 0235 | " |
| $\mathrm{K}_{2} \mathrm{CO}_{3}$ | 1.1906 | . 0140 | " | KI | 1.6743 | . 0338 | " |
| $\mathrm{Na}_{2} \mathrm{CO}_{3}$ | 1.1006 | . 0140 | * | " . | 1.1705 | . 0182 | " |
| $\mathrm{NH}_{4} \mathrm{Cl}$ | 1.0718 | . 0178 | 15 | $\mathrm{KNO}_{3}$ | 1.0634 | . 0130 | 20 |
| $\mathrm{BaCl}_{2}$ | 1.2897 | . 0168 | 20 | $\mathrm{NaNO}_{3}$ | 1.1112 | . 0131 | " |
| $\mathrm{CdCl}_{2}$ | 1.3179 | . 0185 | " | $\mathrm{U}_{2} \mathrm{O}_{3} \mathrm{~N}_{2} \mathrm{O}_{5}$ | 2.0267 | . 0053 | " |
|  | 1.1732 | . 0160 | " |  | 1.1963 | . 0115 | " |
| $\mathrm{CaCl}_{2}$ | 1.1504 | . 0165 | " | $\mathrm{BaSo}_{4}$ | 1.1788 | . 0134 | " |
| " | 1.0832 | . 0152 | " | $\mathrm{K}_{2} \mathrm{SO}_{4}$ | 1.0475 | . 0133 | " |
| $\mathrm{FeCl}_{2}$ | 1.4331 | . 0025 | 15 | $\mathrm{Na}_{2} \mathrm{SO}_{4}$ | 1.0661 | . 0135 | " |
| " | 1.1093 | . 0118 | " |  |  |  |  |

Du Bois shows that in the case of substances like iron, nickel, and cobalt which have a variable magnetic susceptibility the expression in Verdet's equation, which is constant for substances of constant susceptibility, requires to be divided by the susceptibility to obtain a constant. For this expression he proposes the name "Kundt's constant." These experiments of Kundt and $\mathrm{Du}_{\mathrm{u}}$ Bois show that it is not the difference of magnetic potential between the two ends of the medium, but the product of the length of the medium and the induction per unit arca, which controls the amount of rotation of the beam.
Some data on the Verdet constant of gases by Ingersol (*) and by de Mallemann ( ${ }^{\dagger}$ ) for wavelength 5780 A , pressure 760 mmHg , and at temperature $0^{\circ} \mathrm{C}$ :

| Substance | Verdet constant in min | Substance | Verdet constant in min | Substance | Verdet constant in $\min$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Hydrogen ${ }^{\dagger}$ | $6.29 \times 10^{-8}$ | Helium* | . $51 \times 10^{-9}$ | Methane ${ }^{\dagger}$ | $17.4 \times 10^{-6}$ |
| Hydrogen * | 6.26 | Oxygen* | 5.55 | Ethylene $\dagger$ | 34.4 |
| Deuterium * | 6.21 | Oxygen ${ }^{\dagger}$ | 5.69 | Ethylene* | 34.6 |
| Nitrogen* | 6.30 | Argon $\dagger$ | 9.36 | Carbon dioxide * | 9.25 |

The de Mallemann values are from numerous papers in Comptes Rendus, 1929 to date (See in particular R. de Mallemann, F. Suhner, and J. Grange, C. R., vol. 232, p. 1094, 1915. See also P. Gabiano Ann. d. Physique, vol. 10, p. 68, 1933.). The Ingersoll values are from an ONR preliminary report (October 1952). The probable error of the de Mallemann and the Ingersoll values is of the order of 1 percent. The dispersion of the rotation for most gases, except oxygen, is roughly as the inverse square of the wavelength.

| Substance | Pressure | Temp. | Verdet's constant in min |  |
| :---: | :---: | :---: | :---: | :---: |
| Atmospheric air | Atmospheric | Ordinary | $6.83 \times$ |  |
| Carbon dioxide . |  |  | 13.00 |  |
| Carbon disulfide | 74 cmHg | $70^{\circ} \mathrm{C}$ | 23.49 | " |
| Ethylene | Atmospheric | Ordinary | 34.48 | " |
| Nitrogen |  |  | 6.92 | " |
| Nitrous oxide | " | " | 16.90 | " |
| Oxygen |  | " | 6.28 | " |
| Sulfur dioxide |  | $20^{\circ}$ | 31.39 | " |
|  | 246 cmHg | $20^{\circ} \mathrm{C}$ | 38.40 |  |

TABLE 517.-VERDET'S AND KUNDT'S CONSTANTS FOR SOME MATERIALS
The following short table is quoted from Du Bois's paper. The quantities are stated in cgs measure. circular measure (radians) being used in the expression of "Verdet's constant" and "Kundt's constant."

| Name of substance | Magnetic susceptibility | $\overbrace{\text { Number }}^{\text {Verdet's constant }}$ | Wavelength of light in cm |  | Knudt's constant |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Cobalt | - | - | 6.44 |  | 3.99 |
| Nickel | - | - |  |  | 3.15 |
| Iron |  | - | 6.56 | " | 2.63 |
| Oxygen: 1 atm . | $+.0126 \times 10^{-5}$ | . $000179 \times 10^{-5}$ | 5.89 | " | . 014 |
| Sulfur dioxide | -. 0751 | . 302 |  |  | $-4.00$ |
| Water | -. 0694 | . 377 |  | " | - 5.4 |
| Nitric acid | -. 0633 | . 356 |  | " | - 5.6 |
| Alcohol | -. 0566 | . 330 |  | " | - 5.8 |
| Ether | -. 0541 | . 315 |  | " | - 5.8 |
| Arsenic chloride | -. 0876 | 1.222 |  | " | -14.9 |
| Carbon disulfide | -. 0716 | 1.222 |  | " | -17.1 |
| Faraday's glass | -. 0982 | 1.738 |  | " | -17.7 |

Du Bois has shown that the rotation of the major axis of vibration of radiations normally reflected from a magnet is algebraically equal to the normal component of magnetization multiplied into a constant $K$. He calls this constant $K$, Kerr's constant for the magnetized substance forming the magnet.

| Color of light | Spectrum line | Wavelength | Kerr's constant in minutes per cgs unit of magnetization |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Cobalt | Nickel | Iron | Magnetite |
| Red | $\mathrm{Li} a$ | . $677 \mu$ | -. 0208 | -. 0173 | -. 0154 | +. 0096 |
| Red | - | . 620 | -. 0198 | -. 0160 | -. 0138 | $+.0120$ |
| Yellow | D | . 589 | -. 0193 | -. 0154 | -. 0130 | +. 0133 |
| Green | $b$ | . 517 | -. 0179 | -. 0159 | -. 0111 | +. 0072 |
| Blue | F | . 486 | -. 0180 | -. 0163 | -. 0101 | $+.0026$ |
| Violet | G | . 431 | $-.0182$ | -. 0175 | -. 0089 | - |

## TABLE 519.-TRANSVERSE GALVANOMAGNETIC AND THERMOMAGNETIC EFFECTS

Effects are considered positive when, the magnetic field being directed away from the observer, and the primary current of heat or electricity directed from left to right, the upper edge of the specimen has the higher potential or higher temperature.
$E=$ difference of potential produced $; T=$ difference of temperature produced $; I=$ primary current ; $\frac{d t}{d x}=$ primary temperature gradient ; $B=$ breadth, and $D=$ thickness, of specimen; $H=$ intensity of field, cgs units.

Hall effect (galvanomagnetic difference of potential), $E=R \frac{H I}{D}$
Ettingshausen effect ("
Nernst effect (thermomagnetic " "
Leduc effect ( " " potential), $E=Q H B \frac{d t}{d x}$

| Substance | Values of $R$ | $P \times 10^{6}$ | $Q \times 10^{8}$ | $5 \times 10^{8}$ |
| :---: | :---: | :---: | :---: | :---: |
| Tellurium | + 400 to 800 | +200 | +360000 | +400 |
| Antimony | +. 9 " ". 22 | +2 | +9000 to 18000 | +200 |
| Steel | +.012".033 | -. 07 | -700 " 1700 | +69 |
| Heusler alloy | +. 010 ". 026 | - | +1600" 7000 |  |
| Iron | +. 0007 ". 011 | -. 06 | -1000" 1500 | +39 |
| Cobalt | +.0016".0046 | +. 01 | +1800" 2240 | +13 |
| Zinc | - | - | -54 " 240 | +13 |
| Cadmium | $+.00055$ |  |  |  |
| Iridium | $+.00040$ | - | up to - 50 | + 5 |
| Lead | +. 00009 | - | -5.0 (?) |  |
| Tin | -. 00003 | - | -4.0 (?) |  |
| Platinum | -. 0002 | - |  | -2 |
| Copper | -. 00052 | - | -90 to 270 | -18 |
| German silver | -. 00054 |  |  |  |
| Gold | -. 00057 to . 00071 |  |  |  |
| Constantin | -. 0009 |  |  |  |
| Manganese | -. 00093 |  |  |  |
| Palladium | -. 0007 to .0012 | - | - 50 to 130 | - 3 |
| Silver | -. 0008 ". 0015 | - | -46" 430 | -41 |
| Sodium | -. 0023 |  |  |  |
| Magnesium | 一. 00094 to . 0035 |  |  |  |
| Aluminum | -. 00036 " . 0037 |  |  |  |
| Nickel | -. 0045 " . 024 | +.04 to 19 | +2000" 9000 | -45 |
| Carbon | -. 017 |  | +100 |  |
| Bismuth | - up to 16. | +3 to 40 | + up to 132000 | -200 |


| Mirror | $\underset{\substack{\text { Field } \\ \text { cgs }}}{ }$ | . $41 \mu$ | . $44 \mu$ | $48 \mu$ | . $52 \mu$ | .56ر | . $60 \mu$ | . $64 \mu$ | . $66 \mu$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Iron | 21,500 | -. 25 | -. 26 | -. 28 | -. 31 | -. 36 | -. 42 | -. 44 | -. 45 |
| Cobalt | 20,000 | -. 36 | -. 35 | -. 34 | -. 35 | -. 35 | -. 35 | -. 35 | -. 36 |
| Nickel | 19,000 | -. 16 | -. 15 | -. 13 | -. 13 | -. 14 | -. 14 | -. 14 | -. 14 |
| Steel | 19,200 | -. 27 | -. 28 | -. 31 | -. 35 | -. 38 | $-.40$ | -. 44 | -. 45 |
| Invar | 19,800 | -. 22 | -. 23 | -. 24 | -. 23 | $-.23$ | -. 22 | -. 23 | -. 23 |
| Magnetite | 16,400 | -. 07 | -. 02 | $+.04$ | +. 06 | +. 08 | +. 06 | $+.04$ | +. 03 |

table 521.-VARIATION OF HALL CONSTANT WITH THE TEMPERATURE

| Bismuth |  |  |  |  |  | Antimony |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| H | $-182^{\circ} \mathrm{C}$ | $-90^{\circ}$ | -23 ${ }^{\circ}$ | +11.5 ${ }^{\circ}$ | $+100^{\circ}$ | H | $-186^{\circ} \mathrm{C}$ | -79 ${ }^{\circ}$ | $+21.5^{\circ}$ | $+58^{\circ}$ |
| 1000 | 62.2 | 28.0 | 17.0 | 13.3 | 7.28 | 1750 | . 263 | . 249 | . 217 |  |
| 2000 | 55.0 | 25.0 | 16.0 | 12.7 | 7.17 | 3960 | . 252 | . 243 | . 211 |  |
| 3000 | 49.7 | 22.9 | 15.1 | 12.1 | 7.06 | 6160 | . 245 | 235 | . 209 | . 203 |
| 4000 | 45.8 | 21.5 | 14.3 | 11.5 | 6.95 |  |  |  |  |  |
| 5000 | 42.6 | 20.2 | 13.6 | 11.0 | 6.84 |  |  |  |  |  |
| 6000 | 40.1 | 18.9 | 12.9 | 10.6 | 6.72 |  |  |  |  |  |


|  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\overbrace{H}$ | $+14.5^{\circ} \mathrm{C}$ | $+104^{\circ}$ | $125^{\circ}$ | $189^{\circ}$ | $212^{\circ}$ | $239^{\circ}$ | $259^{\circ}$ | $269^{\circ}$ | $270^{\circ}$ |  |
| 890 | 5.28 | 2.57 | 2.12 | 1.42 | 1.24 | 1.11 | .97 | .83 | $.77^{*}$ |  |

[^207]
## TABLES 522-555.-OPTICAL GLASS AND OPTICAL CRYSTALS

Optical glass and optical crystals are in general described by giving their indices of refraction for standard wavelengths, such as the $D, A, C, F$, etc., lines and their $v$ values $=\left(n_{D}-1\right) /\left(n_{F}-n_{C}\right)$. Also, the spectral transmission and some other physical constants may be given. In addition, many crystals have different optical properties in different directions which require some consideration of their optical axes. For glasses used as filters the spectral transmission is an important item. A table of wavelength units and some data on various types of optical glass and crystals follow.

TABLE 522.-RADIATION WAVELENGTH UNITS
Radio

meter $\quad$\begin{tabular}{c}
Radiation <br>
micron

$\quad$

Colorimetry <br>
millimicron

$\quad$

Spectroscopy <br>
angstrom

$\quad$

X-rays <br>
X-ray units

$\quad$

$\gamma$ rays <br>
microangstrom
\end{tabular}

| $\underbrace{\text { Units }}$ |  | Powers-of-10 equivalent of units listed in column 1 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | cgs |  |  |
| Name | Symbol | $\mu$ | $m \mu$ | A | $X U$ | $\mu$ A | ${ }_{\text {cmit }}$ | mm | $m$ |
| Micron | $\mu$ | 1 | $10^{3}$ | $10^{4}$ | $10^{7}$ | $10^{10}$ | $10^{-4}$ | $10^{-3}$ | $10^{-8}$ |
| Millimicron | $m \mu$ | $10^{-3}$ | 1 | 10 | $10^{4}$ | $10^{7}$ | $10^{-7}$ | $10^{-6}$ | $10^{-9}$ |
| Angstrom | A | $10^{-4}$ | $10^{-1}$ | 1 | $10^{3}$ | $10^{6}$ | $10^{-8}$ | $10^{-7}$ | $10^{-10}$ |
| X-ray unit | $X \mu$ | $10^{-7}$ | $10^{-4}$ | $10^{-3}$ | 1 | $10^{3}$ | $10^{-11}$ | $10^{-10}$ | $10^{-13}$ |
| Microangstrom | $\mu A$ | $10^{-10}$ | $10^{-7}$ | $10^{-8}$ | $10^{-3}$ | 1 | $10^{-14}$ | $10^{-13}$ | $10^{-16}$ |

The X-ray unit as originally used referred to the measurement of $x$-wavelengths using a calcite crystal. Such results are in error by a factor of 1.00203 .

OPTICAL GLASS
TABLE 523.-CHARACTERISTICS OF AMERICAN-MADE OPTICAL GLASSES ${ }^{180}$

Crown glasses-crown (CO), light barium crown (LBC), dense barium crown (DBC). extra dense barium crown (EDBC)

| Name | $C-B L$ |  | $D B C-C G$ | $D B C-C G$ | DBC - CG | DBC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Type | $518 / 596$ | 573/568 | 612/595 | 620/603 | ${ }^{638 / 555}$ | $617 / 5$ |
| $n_{D}$ | 1.51780 | 1.57250 | 1.61160 | 1.62030 | 1.63840 | 1.61700 |
| $n_{G}{ }^{\prime}$ | 1.52886 | 1.58538 | 1.6246 | 1.6332 | 1.6532 | 1.63171 |
| $n_{F}$ | 1.52393 | 1.57962 | 1.61880 | 1.62750 | 1.64650 | 1.62511 |
| $n c$ | 1.51524 | 1.56954 | 1.60852 | 1.61722 | 1.63500 | 1.61367 |
|  |  | 56.8 | 59.5 | 60.3 | 55.5 |  |

Flint glasses-crown flint (CF), light flint (LF), short flint (SF), extra light flint (ELF), light barium flint (LBF), barium flint (BF), dense barium flint (DBF), dense flint (DF), extra dense flint (EDF)

| Name | $C F-B L$ | LBF-BL | $B F-B L$ | DBF-BL | DBF-CG | ELF -bL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Type | 526/546 | 548/537 | 570/481 | 617/385 | 670/472 | 541/475 |
| $n_{D}$ | 1.52560 | 1.54770 | 1.57040 | 1.61700 | 1.66990 | 1.54140 |
| $n{ }^{\prime}{ }^{\prime}$ | 1.53793 | 1.56081 | 1.58575 | 1.63811 | 1.6882 | 1.55618 |
| $n_{F}$ | 1.53239 | 1.55491 | 1.57880 | 1.62843 | 1.67990 | 1.54949 |
| $n_{C}$ | 1.52277 | 1.54471 | 1.56695 | 1.61242 | 1.66572 | 1.53809 |
| $\nu$ | 54.6 | 53.7 | 48.1 | 38.5 | 47.2 | 47.5 |
| Name | ELF-BL | SF-CG | $L F-B L$ | DF - ${ }^{\text {BL }}$ | EDF - BL $^{\text {c }}$ |  |
| Type | 559/455 | 613/442 | 575/429 | 596/397 | 751/277 |  |
| $n_{D}$ | 1.55850 | 1.61300 | 1.57510 | 1.59560 | 1.75060 |  |
| $n{ }^{\prime}$ | 1.57447 | 1.6308 | 1.59263 | 1.61538 | 1.78716 |  |
| $n_{F}$ | 1.56722 | 1.62280 | 1.58464 | 1.60632 | 1.77009 |  |
| $n c$ | 1.55495 | 1.60893 | 1.57122 | 1.59130 | 1.74302 |  |
| $\nu$ | 45.5 | 44.2 | 42.9 | 39.7 | 27.7 |  |

[^208]
(concluded)
TABLE 524.-CHARACTERISTICS OF SOME OPTICAL GLASSES MADE AT THE NATIONAL BUREAU OF STANDARDS

| Name | $\underset{572 / 425}{F}$ | $\underset{5795 / 410}{F}$ | $\stackrel{F}{605 / 381}$ | $\underset{617 / 366}{F}$ | $\underset{620 / 362}{F}$ | $\stackrel{F}{F} \underset{649 / 338}{ }$ | $\underset{666 / 324}{F}$ | $\begin{gathered} F \\ 672 / 322 \end{gathered}$ | $\begin{gathered} F \\ 689 / 309 \end{gathered}$ | $\begin{gathered} F \\ 720 / 295 \end{gathered}$ | $\begin{gathered} F \\ 754 / 277 \end{gathered}$ | $\begin{gathered} B F \\ 584 / 460 \end{gathered}$ | $\begin{gathered} B F \\ 588 / 534 \end{gathered}$ | $\begin{gathered} B F \\ 604 / 435 \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nominal |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $n^{n}$ | ${ }_{42.5}^{1.5725}$ | $\begin{aligned} & 1.5795 \\ & 41.0 \end{aligned}$ | $\begin{aligned} & 1.605 \\ & 38.1 \end{aligned}$ | $\begin{aligned} & 1.617 \\ & 36.6 \end{aligned}$ | $\begin{aligned} & 1.620 \\ & 36.2 \end{aligned}$ | $\begin{gathered} 1.649 \\ 33.8 \end{gathered}$ | $\begin{aligned} & 1.666 \\ & 32.4 \end{aligned}$ | ${ }_{32.2}^{1.6725}$ | $\begin{gathered} 1.689 \\ 30.9 \end{gathered}$ | $\begin{gathered} 1.720 \\ 29.5 \end{gathered}$ | $\begin{gathered} 1.754 \\ 27.7 \end{gathered}$ | $\begin{gathered} 1.584 \\ 46.0 \end{gathered}$ | ${ }_{53.4}^{1.588}$ | $\begin{aligned} & 1.604 \\ & 43.5 \end{aligned}$ |
| Typical glass |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $n{ }^{\prime}{ }^{\prime}$ | 1.58950 | 1.59800 | 1.62590 | 1.63936 | 1.64311 | 1.67470 | 1.69335 | 1.70003 | 31.71851 | 1.75349 | 1.79106 | 1.60030 | 1.60249 | 1.62240 |
| $n_{P}$ | 1.58146 | 1.58951 | 1.61630 | 1.62907 | 1.63268 | 1.66285 | 1.68069 | 1.68710 | 1.70475 | 1.73808 | 1.77380 | 1.59283 | 31.59614 | 1.61410 |
| $n_{0}$. | 1.56796 | 1.56536 | 1.60030 | 1.61217 | 1.61556 | 1.64356 | 1.66021 | 1.66619 | 1.68259 | 1.71345 | 1.74644 | 1.58019 | 1.58513 | 1.60020 |
| ${ }_{\nu}$. | 42.4 | 40.9 | 37.9 | 36.5 | 36.2 | 33.7 | 32.5 | 32.1 | 31.1 | 29.2 | 27.5 | 46.2 | 53.4 | 43.4 |
| Composition (batch) | Percent | Percent | Percent | Percent | Percent | Percent | Percent | Percent | Percent | Percent | Percent | Percent | Percent | Percent |
| $\mathrm{SiO}_{2}$ | 55.1 | 53.1 | 47.6 | 45.6 | 45.6 | 41.2 | 39.3 | 38.8 | 37.0 | 34.1 | 31.2 | 49.8 | 45.8 | 45.7 |
| PbO | 31.7 | 35.5 | 40.9 | 43.2 | 45.2 | 51.1 | 54.4 | 55.4 | 58.1 | 62.4 | 66.2 | 18.8 | 10.0 | 23.3 |
| BaO | 1.0 | . 6 |  |  |  |  |  |  |  |  |  | 13.4 | 25.9 | 14.3 |
| $\mathrm{B}_{2} \mathrm{O}_{3}$ |  |  |  |  |  |  |  |  |  |  |  |  | 8.8 |  |
| $\mathrm{Na}_{2} \mathrm{O}$ | 5.0 | . 4 | 2.2 | 4.6 | 3.0 | . 7 |  |  |  |  |  | 1.5 | . 8 |  |
| $\mathrm{K}_{2} \mathrm{O}$ | 6.9 | 9.6 | 8.8 | 6.1 | 5.7 | 6.5 | 6.0 | 5.5 | 4.6 | 3.2 | 2.3 | 8.2 | 6.7 | 8.2 |
| $\mathrm{As}_{2} \mathrm{O}_{3}$ | . 3 | . 3 | . 5 | . 5 | . 5 | . 5 | . 3 | . 3 | . 3 | . 3 | . 3 | . 5 | . 5 | . 4 |
| $\mathrm{Sb}_{2} \mathrm{O}_{3}$ |  | . 5 |  |  |  |  |  |  |  |  |  | 7.8 |  | 8.1 |
| ZnO BeO |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| SrO |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\xrightarrow{\mathrm{Li}_{2} \mathrm{O}}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{Cl}_{\mathrm{CaO}}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{SO}_{2} \ldots \ldots \ldots \ldots \ldots$. 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{Al}_{2} \mathrm{O}_{3}$$\begin{array}{lll} \mathrm{ArO}_{2} \mathrm{H}_{2} & \ldots & \ldots \end{array}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

TABLE 525.-INDEX OF REFRACTION OF EASTMAN KODAK CO. NONSILICA GLASSES (1949)

Part 1

| Type | $\begin{aligned} & E K-110 \\ & (E K-110 \\ & -5328) \end{aligned}$ | EK-210 | EK-310 | $\begin{aligned} & E K-325 \\ & (E K-32 \\ & -2641) \end{aligned}$ | $\begin{aligned} & E K-330 \\ & (E K-33 \\ & -2734 s) \end{aligned}$ | $\begin{aligned} & E K-450 \\ & (E K-45 \\ & -29) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Index |  |  |  |  |  |  |
| $n_{n}$ | 1.71786 | 1.75861 | 1.77301 | 1.77288 | 1.78280 | 1.83767 |
| $n n_{0}$ | 1.71227 | 1.75201 | 1.76538 | 1.76518 | 1.77532 | 1.82832 |
| $n_{F}$ | 1.70554 | 1.74413 | 1.75638 | 1.75607 | 1.76643 | 1.81738 |
| $n_{n}$ | 1.69680 | 1.73400 | 1.74500 | 1.74450 | 1.75510 | 1.80370 |
|  | (1.6973) |  |  | (1.7442) | (1.7555) | (1.8016) |
| $n \mathrm{C}$ | 1.69313 | 1.72979 | 1.74033 | 1.73973 | 1.75043 | 1.79814 |
| $n A^{\prime}$ | 1.68877 | 1.72484 | 1.73491 | 1.73417 | 1.74499 | 1.79180 |

Type numbers and $n_{D}$ values in parentheses are 1947 descriptions of $E K$ glasses for which expansion data appear in Table 550.

Part 2.-Dispersion of glasses

| Index |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $n_{D}$ | 1.69680 | 1.73400 | 1.74500 | 1.74450 | 1.75510 | 1.80370 |
|  | (1.6973) |  |  | (1.7442) | (1.7555) | (1.8016) |
| $\nu=\frac{n_{D}-1}{n_{F}-n_{C}}$ | 56.15 | 51.18 | 46.42 | 45.56 | 47.19 | 41.8 |
|  | (56.0) |  |  | (45.8) | (47.2) | (40.9) |
| $n_{F}-n_{C} \ldots$. | . 01241 | . 01434 | . 01605 | . 01634 | . 01600 | . 01924 |
|  | (.01246) |  |  | (.01624) | (.01602) | (.01959) |
| $n_{F}-n_{D}$ | . 00874 | . 01013 | . 01138 | . 01157 | . 01133 | . 01368 |
|  | (.00877) |  |  | (.01153) | (.01133) | (.01394) |
| $n_{g}-n_{F}$ | . 00673 | . 00788 | . 00900 | . 00911 | . 00889 | . 01094 |
|  | (.00677) |  |  | (.00913) | (.00890) | (.01118) |
| $n_{h}-n_{0}$ | . 00559 | . 00660 | . 00763 | . 00770 | . 00748 | . 00935 |
|  | (.00562) |  |  | (.00776) | (.00750) | (.00959) |
| $n_{D}-n_{A}{ }^{\prime}$ | . 00803 | . 00916 | . 01009 | . 01033 | . 01011 | . 01190 |
|  | (.00806) |  |  | (.01018) | (.01014) | (.0-) |

TABLE 526.-TRANSMISSION OF OPTICAL GLASS
Thickness 10 mm , reflection deducted *

|  | $\begin{gathered} B S C \\ -1 \end{gathered}$ | $\begin{gathered} B S C \\ -2 \end{gathered}$ | ${ }_{-1}^{C}$ | $\begin{gathered} L B C \\ -2 \end{gathered}$ | $\begin{gathered} D B C \\ -1 \end{gathered}$ | $\begin{gathered} D B C \\ -3 \end{gathered}$ | $\begin{gathered} C F \\ -1 \end{gathered}$ | BF | DF | ${ }_{-3}{ }_{-}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cut-off in $m \mu$ | 300 | 296 | 301 | 306 | 328 | 320 | 310 | 316 | 326 | 350 |
| $T$ at 360 m $\mu$ | 900 | 76.0 | 84.0 | 47.5 | 22.0 | 82.5 | 97.0 | 94.0 | 72.5 | 6.5 |
| $380 \mathrm{~m} \mathrm{\mu}$. | 98.0 | 95.0 | 97.2 | 92.5 | 96.8 | 98.5 | 99.0 | 98.0 | 84.5 | 47.0 |
| 400 m $\mu$. | 99.5 | 99.5 | 99.3 | 99.5 | 99.5 | 99.4 | 99.5 | 99.5 | 90.5 | 70.0 |
| $460 \mathrm{~m} \mathrm{\mu}$. | 99.5 | 99.5 | 99.3 | 99.5 | 99.5 | 99.4 | 99.5 | 99.5 | 97.0 | 96.2 |
| $500 \mathrm{~m} \mathrm{\mu}$ | 99.5 | 99.5 | 99.3 | 99.5 | 99.5 | 99.4 | 99.5 | 99.5 | 98.9 | 99.3 |
| $800 m \mu$. | 99.5 | 98.5 | 99.3 | 99.2 | 99.4 | 99.4 | 99.5 | 99.5 | 99.5 | 99.5 |
| 1000 m $\mu$. | 99.5 | 94.5 | 99.3 | 97.2 | 96.6 | 99.4 | 99.5 | 99.5 | 99.5 | 99.5 |
| 2000 m | 88.8 | 85.0 | 95.0 | 90.5 | 65.0 | 80.5 | 70.0 | 88.5 | 99.5 | 99.5 |
| 3000 m $\mu$. | . 5 | . 0 | 17.5 | . 6 | . 0 | . 0 | . 9 | . 9 | 6.0 | 3.0 |
| Cut-off in $m \mu$. | 3200 | 3000 | 4000 | 3200 | 2900 | 2850 | 3350 | 3250 | 3500 | 4100 |

[^209]TABLE 527.-CHANGES WITH TEMPERATURE IN ABSOLUTE INDEX OF REFRACTION (n) AT $20^{\circ} \mathrm{C}$ FOR A NUMBER OF GLASSES * $\dagger$

| $n{ }^{\text {d }}$ | Boro- silicate crown <br> BSC- 1 | $\stackrel{\text { Crown }}{C-1}$ | Light $\stackrel{\text { crown }}{ }$ | Dense crown DBC- 3 | $\begin{gathered} \text { Crown } \\ \text { fint } \\ \text { fint } \end{gathered}$ | $\begin{gathered} \text { Barium } \\ \text { fint } \\ B F-1 \end{gathered}$ | $\begin{gathered} \text { Dense } \\ \text { finint } \\ D F-2 \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\Delta n /{ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |
| 4360A | 101 | 199 | 085 | 305 | 261 | 246 | . 586 |
| 5087 A . | . 087 | . 171 | . 087 | . 276 | . 244 | . 218 | . 450 |
| 5462A. |  | . 159 |  |  |  |  | . 405 |
| 5894A. | . 059 | . 150 | . 036 | . 256 | . 205 | . 162 | . 370 |
| 6440A. | . 050 | . 131 | . 025 | . 237 | . 184 | . 140 | . 334 |

* For references, see footnote 160 , p. 509.
$\dagger$ In units of the fifth decimal place.

TABLE 528.-INDEX OF REFRACTION OF GLASSES MADE BY SCHOTT AND GENOESSEN, JENA

The following constants are for glasses made by Schott and Genoessen, Jena: $n_{A}, n_{c}, n_{D}, n_{F}, n_{G}$, are the indices of refraction in air for $A=0.7682 \mu, C=0.6563 \mu, D=0.5893, F=0.4861, G^{\prime}=$ $0.4341, \nu=\left(n_{D}-1\right) /\left(n_{F}-n_{C}\right)$.

| Catalogue type $=$ Designation $=$ |  |  | $\begin{aligned} & \text { O } 546 \\ & \text { Zinc. } \end{aligned}$ | O 381 <br> Higher dis- | $\begin{aligned} & \text { O. } 184 \\ & \text { Light } \end{aligned}$ | $\begin{aligned} & \mathrm{O} 102 \\ & \text { Heavy } \end{aligned}$ | $\begin{gathered} \text { O } 165 \\ \text { Heavy } \end{gathered}$ | $\underset{\text { Heaviest }}{\text { S } 57}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | ${ }_{\substack{\text { crown } \\ 1092}}$ | persion crown | silicate fint | silicate fint | silicate fint | silicate fint |
| Melting |  | ${ }_{\nu}^{\text {number }}$ 三 | 1092 60.7 | 1151 51.8 | ${ }_{41.1}^{451}$ | ${ }_{33.7}^{469}$ | 500 27.6 | ${ }_{22.2}^{163}$ |
| 5 | Cd | . $2763 \mu$ | 1.56759 | - | - | - | - |  |
|  | Cd | . 2837 | 1.56372 |  |  |  | - |  |
|  | Cd | . 2980 | 1.55723 | 1.57093 | 1.65397 | - | - | - |
|  | Cd | . 3403 | 1.54369 | 1.55262 | 1.63320 | 1.71968 | 1.85487 | - |
|  | Cd | . 3610 | 1.53897 | 1.54664 | 1.61388 | 1.70536 | 1.83263 | - |
|  | H | . $4340 \mu$ | 1.52788 | 1.53312 | 1.59355 | 1.67561 | 1.78800 | 1.94493 |
| $\square$ | H | . 4861 | 1.52299 | 1.52715 | 1.58515 | 1.66367 | 1.77091 | 1.91890 |
|  | Na | . 5893 | 1.51698 | 1.52002 | 1.57524 | 1.64985 | 1.75130 | 1.88995 |
|  | H | . 6563 | 1.51446 | 1.51712 | 1.57119 | 1.64440 | 1.74368 | 1.87893 |
| - | K | . 7682 | 1.51143 | 1.51368 | 1.56669 | 1.63820 | 1.73530 | 1.86702 |
| $\begin{aligned} & \text { U } \\ & \vec{B} \\ & \vec{y} \end{aligned}$ |  | . $800 \mu$ | 1.5103 | 1.5131 | 1.5659 | 1.6373 | 1.7338 | 1.8650 |
|  |  | 1.200 | 1.5048 | 1.5069 | 1.5585 | 1.6277 | 1.7215 | 1.8481 |
|  |  | 1.600 | 1.5008 | 1.5024 | 1.5535 | 1.6217 | 1.7151 | 1.8396 |
|  |  | 2.000 | 1.4967 | 1.4973 | 1.5487 | 1.6171 | 1.7104 | 1.8316 |
|  |  | 2.400 | - | - | 1.5440 | 1.6131 | - | 1.8286 |

Percentage composition of the above glasses:
$\mathrm{O} 546, \mathrm{SiO}_{2}, 65.4 ; \mathrm{K} 2 \mathrm{O}, 15.0 ; \mathrm{Na}_{2} \mathrm{O}, 5.0 ; \mathrm{BaO}, 9.6 ; \mathrm{ZnO}, 2.0 ; \mathrm{Mn}_{2} \mathrm{O}_{3}, 0.1 ; \mathrm{As}_{2} \mathrm{O}_{3}, 0.4 ; \mathrm{B}_{2} \mathrm{O}_{3}, 2.5$.
O 381, $\mathrm{SiO}_{2}, 68.7 ; \mathrm{PbO}, 13.3 ; \mathrm{Na}_{2} \mathrm{O}, 15.7 ; \mathrm{ZnO}, 2.0 ; \mathrm{MnO}_{2}, 0.1 ; \mathrm{As}_{2} \mathrm{O}_{5}, 0.2$.
O 184, $\mathrm{SiO}_{2}, 53.7 ; \mathrm{PbO}, 36.0 ; \mathrm{K}_{2} \mathrm{O}, 8.3 ; \mathrm{Na}_{2} \mathrm{O}, 1.0 ; \mathrm{Mn}_{2} \mathrm{O}_{3}, 0.06 ; \mathrm{As}_{2} \mathrm{O}_{2}, 0.3$.
O 102, $\mathrm{SiO}_{2}, 40.0 ; \mathrm{PbO}, 52.6 ; \mathrm{K} 2 \mathrm{O}, 6.5 ; \mathrm{Na}_{2} \mathrm{O}, 0.5 ; \mathrm{Mn}_{2} \mathrm{O}_{3}, 0.09 ; \mathrm{As}_{2} \mathrm{O}_{5}, 0.3$.
$\mathrm{O} 165, \mathrm{SiO}_{2}, 29.26 ; \mathrm{PbO}, 67.5 ; \mathrm{K}_{2} \mathrm{O}, 3.0 ; \mathrm{Mn}_{2} \mathrm{O}_{3}, 0.04 ; \mathrm{As}_{2} \mathrm{O}_{3}, 0.2$.
S $57, \mathrm{SiO}_{2}, 21.9 ; \mathrm{PbO}, 78.0 ; \mathrm{As}_{2} \mathrm{O}_{5}, 0.1$.

TABLE 529.-CHANGE OF INDICES OF REFRACTION FOR $1^{\circ} \mathrm{C}$ IN UNITS OF THE FIFTH DECIMAL PLACE


Coefficients, $a$, in the formula $I_{t}=I_{0} a^{t}$, where $I_{0}$ is the intensity before, and $I_{t}$ after, transmission through the thickness $t$.

| Unit $t=1 \mathrm{dm}$ | Coefficient of transmission, a |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | . $375 \mu$ | 390ر | .400 | . 434 |  | . $436 \mu$ | . $455 \mu$. $477 \mu .503 \mu \quad .580 \mu .677 \mu$ |  |  |  |  |
| O 340, Ordinary light flint | . 388 | . 456 | . 614 | . 569 |  | . 680 | . 834 | . 880 | . 880 | . 878 | . 939 |
| O 102, Heavy silicate flint | - | . 025 | . 463 | . 502 |  | . 566 | . 683 | . 700 | . 782 | . 828 | . 794 |
| O 93, Ordinary " |  |  |  |  |  |  | . 807 | . 899 | . 871 | . 903 | . 943 |
| O 203, " " crow | . 583 | . 583 | . 695 | . 667 |  |  | . 822 | . 860 | . 872 | . 872 | . 903 |
| O 598, (Crown) |  |  |  |  |  |  |  | . 771 | . 776 | . 818 | . 860 |
| Unit $t=1 \mathrm{~cm}$ | 0.7 ${ }^{\text {m }}$ | 0.95 $\mu$ | $1.1 \mu$ | 1.4 $\mu$ | $1.7 \mu$ | 2.0 | 0ر $2.3 \mu$ | $2.5 \mu$ | $2.7 \mu$ | $2.9 \mu$ | $3.1 \mu$ |
| S 204, Borate crown | 1.00 | . 99 | . 94 | . 90 | . 85 |  | . 81.69 | . 43 | . 29 | . 18 | - |
| S 179, Medium phosphate crown. |  | . 98 | . 95 |  | . 84 |  | . 67.49 | . 87 | . 18 |  |  |
| O 1143, Dense borosilicate crown.. | . 98 |  | . 97 |  | . 95 |  | 93.90 | . 84 | . 71 | . 47 | . 27 |
| O 1092, Crown | . 99 | . 96 | . 95 | . 99 | . 99 | . 9 | 91.82 | . 71 | . 60 | . 48 | . 29 |
| O 1151, " | . 98 |  | . 99 |  | . 98 |  | 94.90 | . 79 | . 75 | . 45 | . 32 |
| O 451, Light flint | 1.00 | - | . 99 |  | . 98 |  | 95.92 | . 84 | . 78 | . 54 | . 34 |
| O 469, Heavy " | 1.00 | - | . 98 |  | . 99 |  | 98.98 | . 97 | . 90 | . 66 | . 50 |
| O 500, | 1.00 | - | 1.00 | - | 1.00 |  | - 1.00 | . 99 | . 92 | . 74 | . 53 |
| S 163, " | 1.00 | - | . 98 | - | . 99 |  | 9 | -- | . 94 | . 78 | . 60 |

## Part 2

$R$ is reflection factor yellow light for two surfaces. Values of transmission are for 1 mm thickness. Ordinary figures refer to wavelengths in $\mu, .281$ to .775 , black-faced infrared.

| Glass durability | $\underset{R}{\text { Density }}$ | . 2851 | . 302 | .334 1.15 | 366 1.30 |  | .480 2.00 | .546 $\mathbf{2 . 2 0}$ | .578 2.40 | .644 $\mathbf{2 . 6 0}$ | .700 2.80 | .775 3.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| U G 1 | 2.77 | . 00 | . 17 | . 69 | . 85 | . 00 | . 00 | . 00 | . 00 | . 00 | . 01 | . 34 |
| 2/3 | . 911 | . 22 | . 11 | . 05 | . 04 | . 03 | . 04 | . 06 | . 11 | . 15 | . 19 | . 17 |
| B G 1 | 2.50 | . 04 | . 40 | . 93 | . 97 | . 86 | . 44 | . 04 | . 05 | . 01 | . 51 | . 94 |
|  | . 915 | . 97 | . 93 | . 76 | . 58 | . 40 | . 50 | . 59 | . 69 | . 74 | . 75 | . 55 |
| B G 4 | 2.41 | . 00 | . 00 | . 04 | . 74 | . 87 | . 53 | . 01 | . 01 | . 00 | . 07 | . 13 |
| 5 | . 921 | . 12 | . 11 | . 13 | . 12 | . 14 | . 21 | . 45 | . 59 | . 63 | . 45 | . 40 |
| B G 10 | 2.60 | . 00 | . 00 | . 14 | . 64 | . 93 | . 95 | . 94 | . 88 | . 75 | . 62 | . 42 |
|  | . 916 | . 31 | . 25 | . 26 | . 31 | . 47 | . 55 | . 56 | . 58 | . 55 | . 47 | . 46 |
| V G 1 | 2.93 | . 00 | . 00 | . 00 | . 00 | . 02 | . 47 | . 77 | . 56 | . 12 | . 06 | . 04 |
| 2 | . 905 | . 05 | . 09 | . 18 | . 27 | . 47 | . 65 | . 71 | . 76 | . 77 | . 69 | . 55 |
| G G 2 | 2.58 | . 00 | . 00 | . 00 | . 64 | . 99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
|  | . 916 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | . 99 | . 99 | . 98 | . 94 | . 84 | . 70 |
| G G 4 | 2.73 | . 00 | . 00 | . 03 | . 01 | . 67 | . 92 | . 97 | . 96 | . 94 | . 96 | . 99 |
| 2 | . 913 | . 99 | . 99 | . 99 | . 99 | . 99 | .99 | . 99 | . 98 | . 94 | . 85 | . 64 |
| G G 11 | 2.54 | . 00 | . 00 | . 00 | . 00 | . 01 | . 24 | . 99 | . 99 | . 99 | . 99 | . 98 |
| ${ }^{2}$ | . 913 | . 97 | . 96 | . 96 | . 99 | . 96 | . 97 | . 97 | . 95 | . 91 | . 82 | . 68 |
| R G 2 | 2.74 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 92 | . 98 | . 98 |
| 2 | . 913 | . 98 | . 98 | . 98 | . 98 | . 98 | . 98 | . 97 | . 95 | . 92 | . 81 | . 65 |
| R G 5 | 2.74 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 00 | . 02 | . 96 | . 98 |
| 2 | . 913 | . 98 | . 98 | . 99 | . 99 | . 99 | . 99 | . 98 | . 97 | . 92 | . 79 | . 58 |
| N G 5 | 2.42 | . 00 | . 00 | . 00 | . 29 | . 59 | . 63 | . 66 | . 68 | . 70 | . 70 | . 65 |
| 1 | . 919 | . 61 | . 59 | . 61 | . 65 | . 73 | . 78 | . 78 | . 76 | . 69 | . 58 | . 40 |

U G 1 dark purple (uv., extreme red). B G 1 blue (uv.. extreme red). B G 4 blue (ir.). B G 10, light blue green, ir. absorption. V G 1 yellow.green. G G 2 colorless, uv. absorption. G G 4 almost colorless, strong uv. absorption, G G 11 dark yellow for contract filters. R G 2 pure red. R G 5 dark red. N G 5 light neutral.

## OPTICAL CRYSTALS

Not so many years ago physicists had to depend upon natural crystals for their various optical instruments. Now, owing to a great deal of work in this field, it has been found possible to grow artificial crystals of various materials for this purpose. Data on some of these artificial crystals are given in the following tables and the spectral transmission of some of them is shown in figure 26.
TABLE 531.-SOME ARTIFICIAL OPTICAL CRYSTALS*
Part 1

|  | Size grown |  |  | Transmission range | Uses | ence ${ }^{16}$ <br> Refer- |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Diameter | Length | Weight |  |  |  |
|  | 190 mm | 125 mm | 13 kg | $\begin{aligned} & .2 \text { to } 15 \mu, \text { practical, } \\ & 8.5 \text { to } 15 \mu \end{aligned}$ | Ultraviolet, visible, and infrared spectroscopy, as lens elements for uv. and ir. | a, b |
| Potassium chloride ( KCl ) $\ddagger \ldots$. cubic | 190 | 125 | 16 | . 38 to $21 \mu$ | About the same as NaCl | c, d |
| Silver chloride ( AgCl )......... cubic (optical)s | 95 | 125 | 4.5 | Infrared to $30 \mu$ | Windows and prisms for uv. and ir. spectroscopy | e |
| Calcium fluoride ( $\mathrm{CaF}_{2}$ ) $\\|$... .. cubic | 125 | 100 | 5.0 | . 125 to $9.0 \mu$ | Windows and prisms uv., v., and ir. Lens parts | c, f |
| Potassium bromide ( KBr ) $\mathrm{T}_{\text {\% }} \ldots$. . cubic | 190 | 125 | 16 | Practical, 15 to $25 \mu$ | Prisms and lenses for far infrared | b, c, e |
| Potassium iodide (KI) $1 . . . .$. . cubic | 190 | 125 | 16 | Long wavelength infrared, trans. 2 cm thickness, $50 \%$ at $32.8 \mu$ | Prisms and windows for far infrared | d, h |
| Lithium fluoride (LiF) ${ }^{\text {r }}$....... cubic | 150 | 120 | 6 | Practical, 1 to $5.0 \mu$ | Windows and prisms for uv. and ir., and as lens components | b, g |
| Thallium bromide-iodide ...... cubic (KRS-5) ${ }^{4}$ | 125 | 87.5 | 6.8 | 20 to $37 \mu$ | Prisms and windows, ir., lens parts | e, i |
| Barium fluoride ( $\mathrm{BaF}_{3}$ ) ...... cubic | 125 | 100 | ${ }_{35}^{6.0}$ | up to $12 \mu$ | Infrared windows, prisms | j |
| Cesium bromide ( CsBr ) . ...... cubic | 190 | 125 126 | 35 16 | to $42 \mu$ | Windows, prisms Scintillation | j |
| Potassium iodide (KI)......... cubic (thallium activated) | 190 | 126 | 16 |  | Scintillation counters | j |
| Sodium iodide (Na I).......... cubic (thallium activated) | 190 | 125 | 16 |  | Scintillation counters | j |

 tion 181 References: a, Gore, R. C., et al., Journ. Opt. Soc. Amer., vol. 37, p. 23, 1947. b, Kremers, H. C., Journ. Ind. Eng. Chem., vol. 32, p. 1478, 1940, and Journ. Opt.



TABLE 531.-SOME ARTIFICIAL OPTICAL CRYSTALS (concluded)

## Part 2



TABLE 532.-nd, DISPERSION AND DENSITY OF JENA GLASSES

| No. and type of Jena glass | $n_{\text {d }}$ for $D$ | $n_{F}-n_{C}{ }^{\nu}$ |  | $n_{D}-n_{A}$ | $n_{F}-n_{D}$ | $n_{G}{ }^{\prime}-n_{F}$ | Specifi gravity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| O 225 Light phosphate crown. | 1.5159 | . 00737 | 70.0 | . 00485 | . 00515 | . 00407 | 2.58 |
| O 802 Borosilicate crown | 1.4967 | 0765 | 64.9 | 0504 | 0534 | 0423 | 2.38 |
| UV 3109 Ultraviolet crown | 1.5035 | 0781 | 64.4 | 0514 | 0546 | 0432 | 2.41 |
| O 227 Barium-silicate crown | 1.5399 | 0909 | 59.4 | 0582 | 0639 | 0514 | 2.73 |
| O 114 Soft silicate crown... | 1.5151 | 0910 | 56.6 | 0577 | 0642 | 0521 | 2.55 |
| O 608 High-dispersion crown | 1.5149 | 0943 | 54.6 | 0595 | 0666 | 0543 | 2.60 |
| UV 3248 Ultraviolet flint | 1.5332 | 0964 | 55.4 | 0611 | 0680 | 0553 | 2.75 |
| O 381 High-dispersion crown | 1.5262 | 1026 | 51.3 | 0644 | 0727 | 0596 | 2.70 |
| O 602 Baryt light flint. | 1.5676 | 1072 | 53.0 | 0675 | 0759 | 0618 | 3.12 |
| S 389 Borate flint | 1.5686 | 1102 | 51.6 | 0712 | 0775 | 0629 | 2.83 |
| O 726 Extra light flint | 1.5398 | 1142 | 47.3 | 0711 | 0810 | 0669 | 2.87 |
| O 154 Ordinary light flint | 1.5710 | 1327 | 43.0 | 0819 | 0943 | 0791 | 3.16 |
| O 184 " " " | 1.5900 | 1438 | 41.1 | 0882 | 1022 | 0861 | 3.28 |
| O 748 Baryt flint | 1.6235 | 1599 | 39.1 | 0965 | 1142 | 0965 | 3.67 |
| O 102 Heavy flint | 1.6489 | 1919 | 33.8 | 1152 | 1372 | 1180 | 3.87 |
| O 41 " " | 1.7174 | 2434 | 29.5 | 1439 | 1749 | 1521 | 4.49 |
| O 165 " " | 1.7541 | 2743 | 27.5 | 1607 | 1974 | 1730 | 4.78 |
| S 386 Heavy flint | 1.9170 | 4289 | 21.4 | 2451 | 3109 | 2808 | 6.01 |
| S 57 Heaviest flint | 1.9626 | 4882 | 19.7 | 2767 | 3547 | 3252 | 6.33 |



[^210]TABLE 533.-INDEX OF REFRACTION OF QUARTZ $\left(\mathrm{SiO}_{2}\right), 15^{\circ} \mathrm{C}{ }^{1014}$

| Wavelength $m \mu$ | Quartz | Quartz | Vitreous | Wavelength in air at $m$ | Quartz ${ }_{\text {nor }}$ | Quartz | Vitreous |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 185.467 | 1.67578 | 1.68997 | 1.57436 | 533.85 | 1.546799 | 1.555996 | 1.46067 |
| 193.583 | 1.65999 | 1.67343 | 1.55999 | 579.066 | 1.544667 | 1.553791 |  |
| 202.55 | 1.64557 | 1.65842 | 1.54727 | 589.29 | 1.544246 | 1.553355 | 1.45845 |
| 214.439 | 1.63039 | 1.64262 | 1.53386 | 643.847 | 1.542288 | 1.551332 | 1.45674 |
| 226.503 | 1.61818 | 1.62992 | 1.52308 | 667.815 | 1.541553 | 1.550573 |  |
| 250.329 | 1.60032 | 1.61139 | 1.50745 | 706.520 | 1.540488 | 1.549472 | 1.45517 |
| 274.867 | 1.58752 | 1.59813 | 1.49617 | 794.763 | 1.538478 | 1.547392 | 1.45340 |
| 303.412 | 1.576955 | 1.58720 | 1.48594 | 1000.00 | 1.53503 | 1.54381 | $\ldots$ |
| 340.365 | 1.56747 | 1.577385 | 1.47867 | 1200.00 | 1.53232 | 1.54098 |  |
| 396.848 | 1.55813 | 1.56772 | 1.47061 | 1400.00 | 1.52972 | 1.53826 | $\ldots$ |
| 434.047 | 1.553963 | 1.563405 | 1.46690 | 1600.00 | 1.52703 | 1.53545 | $\ldots$ |
| 467.815 | 1.551027 | 1.560368 | 1.46435 | 2058.20 | 1.51998 | 1.52814 | $\ldots$ |
| 508.582 | 1.548229 | 1.557475 | 1.46191 | 2500.00 | 1.51156 | 1.5195 |  |
|  |  |  |  | 3000.00 | 1.49962 | 1.5070 |  |

101a Sosman, Robt. B., The properties of silica, p. 591, Chemical Catalog Co., NewYork, 1927.

TABLE 534.-INDEX OF REFRACTION OF ROCK SALT IN AIR


[^211]| $\lambda(\mu)$ | $n$ | $\lambda(\mu)$ | n | $\lambda(\mu)$ | ${ }^{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| . 185409 | 1.82710 | 1.1786 | 1.478311 | 8.2505 | 1.462726 |
| . 200090 | 1.71870 |  | 1.47824 |  | 1.46276 |
| . 21946 | 1.64745 | 1.7680 | 1.475890 | 8.8398 | 1.460858 |
| . 257317 | 1.58125 |  | 1.47589 |  | 1.46092 |
| . 281640 | 1.55836 | 2.35728 | 1.474751 | 10.0184 | 1.45672 |
| . 308227 | 1.54136 | 2.9466 | 1.473834 |  | 1.45673 |
| . 358702 | 1.52115 |  | 1.47394 | 11.786 | 1.44919 |
| . 394415 | 1.51219 | 3.5359 | 1.473049 |  | 1.44941 |
| . 467832 | 1.50044 |  | 1.47304 | 12.965 | 1.44346 |
| . 508606 | 1.49620 | 4.7146 | 1.471122 |  | 1.44385 |
| . 58933 | 1.49044 |  | 1.47129 | 14.144 | 1.43722 |
| . 67082 | 1.48669 | 5.3039 | 1.470013 | 15.912 | 1.42617 |
| . 78576 | 1.483282 | 5.303 | 1.47001 | 17.680 | 1.41403 |
| . 88398 | 1.481422 | 5.8932 | 1.468804 | 20.60 | 1.3882 |
| . 98220 | 1.480084 |  | 1.46880 | 22.5 | 1.369 |
| At $18^{\circ} \mathrm{C}^{162}$ |  |  |  |  |  |
| $\lambda(\mu)$ | $n$ | $\lambda(\mu)$ | ${ }^{n}$ | $\lambda(\mu)$ | $\stackrel{n}{ }$ |
| 18.2 | 1.409 | 22.2 | . 1.374 | 26.7 | 1.300 |
| 18.8 | 1.401 | 23.1 . | . 1.363 | 27.2 | 1.275 |
| 19.7 ... | . 1.398 | 24.1 . | . 1.352 | 28.2 | 1.254 |
| 20.4 | . 1.389 | 24.9 . | 1.336 | 28.8 | 1.226 |
| 21.1 . | 1.379 | 25.7 | 1.317 |  |  |
| $n^{2}=a^{2}+\frac{M_{1}}{\lambda^{2}-\lambda_{1}{ }^{2}}+\frac{M_{2}}{\lambda^{2}-\lambda_{2}{ }^{2}}-k \lambda^{2}-h \lambda^{4}$ or $=b^{2}+\frac{M_{1}}{\lambda^{2}-\lambda_{1}{ }^{2}}+\frac{M_{2}}{\lambda^{2}-\lambda_{2}{ }^{2}}+\frac{M_{3}}{\lambda_{2}{ }^{2}-\lambda^{2}}$ |  |  |  |  |  |
| $\begin{aligned} a^{2} & =2.174967 \\ M_{1} & =.008344206 \\ \lambda_{1}{ }^{2} & =.0119082 \\ M_{2} & =.00698382 \end{aligned}$ |  | $\begin{aligned} \lambda_{2}{ }^{2} & =.0255550 \\ k & =.000513495 \\ h & =.000000167587 \end{aligned}$ |  | $\begin{aligned} b^{2} & =3.866619 \\ M_{3} & =5569.715 \\ \lambda_{3}^{2} & =3292.47 \end{aligned}$ |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

TABLE 536.-INDEX OF REFRACTION OF POTASSIUM BROMIDE* ( $22^{\circ} \mathrm{C}$ )

| Wavelength | Index | Wavelength | Index | Wavelength | Index |
| :---: | :---: | :---: | :---: | :---: | :---: |
| . 4047 | 1.589752 | 1.7011 | 1.53901 | 14.29 | 1.51505 |
| . 4358 | 1.581479 | 2.440 | 1.53733 | 14.98 | 1.51280 |
| . 4861 | 1.571789 | 2.730 | 1.53693 | 17.40 | 1.50390 |
| . 5086 | 1.568475 | 3.419 | 1.53614 | 18.16 | 1.50076 |
| . 5461 | 1.563928 | 4.258 | 1.53523 | 19.01 | 1.49705 |
| . 5876 | 1.559965 | 6.238 | 1.53288 | 19.91 | 1.49288 |
| . 6438 | 1.555858 | 6.692 | 1.53225 | 21.18 | 1.48655 |
| . 7065 | 1.552447 | 8.662 | 1.52903 | 21.83 | 1.48311 |
| 1.2140 | 1.54408 | 9.724 | 1.52695 | 23.86 | 1.47140 |
| 1.1287 | 1.54258 | 11.035 | 1.52404 | 25.14 | 1.46324 |
| 1.3621 | 1.54061 | 11.862 | 1.52200 |  |  |

* Prepared by Stephens, Plyler, Rodney, and Spindler, National Bureau of Standards, March 1952.

TABLE 537.-INDEX OF REFRACTION OF NITROSO-DIMETHYL-ANILINE (WOOD)

| $\lambda$ | $n$ | $\lambda$ | $n$ | $\lambda$ | $n$ | $\lambda$ | $n$ | $\lambda$ | $n$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| .497 | 2.140 | .525 | 1.945 | .584 | 1.815 | .636 | 1.647 | .713 | 1.718 |
| .500 | 2.114 | .536 | 1.909 | .602 | 1.796 | .647 | 1.758 | .730 | 1.713 |
| .506 | 2.074 | .546 | 1.879 | .611 | 1.783 | .659 | 1.750 | .749 | 1.709 |
| .508 | 2.025 | .557 | 1.857 | .620 | 1.778 | .669 | 1.743 | .763 | 1.697 |
| .516 | 1.985 | .569 | 1.834 | .627 | 1.769 | .696 | 1.723 |  |  |

Nitroso-dimethyl-aniline has enormous dispersion in yellow and green, metallic absorption in violet.

TABLE 538.-REFRACTIVE INDEX OF SILVER CHLORIDE (AgCI) AT $23.9^{\circ} \mathrm{C}$ *
Tenths of microns


* Prepared by Leroy W. Tilton, Earle K. Plyler, and Robert E. Stephens, National Bureau of Standards.

TABLE 539.-INDEX OF REFRACTION OF FLUORITE (CaF $\mathbf{2}^{2}$ ) IN AIR
Part 1

| $\lambda(\mu)$ | $n$ | $\lambda(\mu)$ | $n$ | $\lambda(\mu)$ | $n$ | $\lambda(\mu)$ | $n$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| .1856 | 1.50940 | .76040 | 1.43101 | 2.2100 | 1.42288 | 5.0092 | 1.39898 |
| .19881 | 1.49629 | .8840 | 1.42982 | 2.3573 | 1.42199 | 5.3036 | 1.39529 |
| .21441 | 1.48462 | 1.1786 | 1.42787 | 2.5537 | 1.42088 | 5.5985 | 1.39142 |
| .22645 | 1.47762 | 1.3756 | 1.42690 | 2.6519 | 1.42016 | 5.8932 | 1.38719 |
| .25713 | 1.46476 | 1.4733 | 1.42641 | 2.7502 | 1.41971 | 6.4825 | 1.37819 |
| .32525 | 1.44987 | 1.5715 | 1.42596 | 2.9466 | 1.41826 | 7.0718 | 1.36805 |
| .34555 | 1.44697 | 1.6206 | 1.42582 | 3.1430 | 1.41707 | 7.6612 | 1.35680 |
| .39681 | 1.44214 | 1.7680 | 1.42507 | 3.2413 | 1.41612 | 8.2505 | 1.34444 |
| .48607 | 1.43713 | 1.9153 | 1.42437 | 3.5359 | 1.41379 | 8.8398 | 1.33079 |
| .58930 | 1.43393 | 1.9644 | 1.42413 | 3.8306 | 1.41120 | 9.4291 | 1.31612 |
| .65618 | 1.43257 | 2.0626 | 1.42359 | 4.1252 | 1.40855 | 51.2 | 3.47 |
| .68671 | 1.43200 | 2.1608 | 1.42308 | 4.4199 | 1.40559 | 61.1 | 2.66 |
| .71836 | 1.43157 |  |  | 4.7146 | 1.40238 | $\infty$ | 2.63 |

Part $2^{163}$

| $\lambda(\mu)$ | n | $\lambda(\mu)$ | $n$ | $\lambda(\mu)$ | $n$ | $\lambda(\mu)$ | $n$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 404658 | 1.4415099 | . 508585 | 1.4361735 | . 770688 | 1.4308799 | 1.734047 | 1.4252000 |
| . 407785 | 1.4412890 | . 546077 | 1.4359584 | . 819115 | 1.4303704 | 1.767893 | 1.4250359 |
| . 435836 | 1.4394944 | . 579016 | 1.4341020 | . 961049 | 1.4291954 | 2.034339 | 1.4237262 |
| . 447150 | 1.4388656 | . 589298 | 1.4338304 | 1.092154 | 1.4283523 | 2.184308 | 1.4229318 |
| . 472219 | 1.4376377 | . 636238 | 1.4328439 | 1.156031 | 1.4279924 | 2.312063 | 1.4222226 |
| . 480525 | 1.4372742 | . 643850 | 1.4327050 | 1.178596 | 1.4278658 | 2.357191 | 1.4219705 |
| . 486138 | 1.4370381 | . 656286 | 1.4324825 | 1.441574 | 1.4265842 | 2.544951 | 1.4208398 |
| . 501570 | 1.4364325 | . 706523 | 1.4316947 | 1.638231 | 1.4256500 | 2.575402 | 1.4206797 |
| $n^{2}=a^{2}+\frac{M_{1}}{\lambda^{2}-\lambda_{1}{ }^{2}}-e \lambda^{2}-f \lambda^{4} \text { or }=b^{2}+\frac{M_{2}}{\lambda^{2}-\lambda_{v}{ }^{2}}+\frac{M_{3}}{\lambda^{2}-\lambda_{r}{ }^{2}}$ |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| $M_{1}=.0062183 \quad b^{2}=6.09651$ |  |  |  |  |  |  |  |
| $\begin{aligned} \lambda_{1}{ }^{2} & =.007706 \\ e & =.0031999 \end{aligned}$ |  |  | $M_{2}=.0061386$ |  |  | . $0940 \mu$ |  |
|  |  |  | $\lambda_{v}{ }^{2}=.00884-\lambda_{r}=35.5 \mu$ |  |  |  |  |

Change of index of refraction of fluorite for $1^{\circ} \mathrm{C}$ in units of the 5 th decimal place C line, $-1.220 ; \mathrm{D},-1.206 ; \mathrm{F},-1.170 ; \mathrm{G},-1.142$.

[^212]TABLE 540.—REFRACTIVE INDICES OF LITHIUM FLUORIDE AT $23.6^{\circ} \mathrm{C}$ *
Tenths of microns

| Wave length $\mu$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0. |  |  |  |  |  | 1.39430 | 1.39181 | 1.39017 | 1.38896 | 1.38797 |
|  | 1.38711 | 1.38631 | 1.38554 | 1.38477 | 1.38400 | 1.38320 | 1.38238 | 1.38153 | 1.38064 | 1.37971 |
| 2. | 1.37875 | 1.37774 | 1.37669 | 1.37560 | 1.37446 | 1.37327 | 1.37203 | 1.37075 | 1.36942 | 1.36804 |
| 3. | 1.36660 | 1.36512 | 1.36359 | 1.36201 | 1.36037 | 1.35868 | 1.35693 | 1.35514 | 1.35329 | 1.35138 |
| 4. . | 1.34942 | 1.34740 | 1.34533 | 1.34319 | 1.34100 | 1.33875 | 1.33645 | 1.33408 | 1.33165 | 1.32916 |
| 5.. | 1.32661 | 1.32399 | 1.32131 | 1.31856 | 1.31575 | 1.31287 | 1.30993 | 1.30692 | 1.30384 | 1.30068 |
| 6. | 1.29745 |  |  |  |  |  |  |  |  |  |

* Prepared by Leroy W. Tilton and Earle K. Plyler, National Bureau of Standards.

TABLE 541.-INDEX OF REFRACTION OF ICELAND SPAR $\left(\mathrm{CaCO}_{3}\right)$ IN AIR

| $\lambda(\mu)$ | no | ne | $\lambda(\mu)$ | nn | $n$. | $\lambda(\mu)$ | no | $n$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 198 | - | 1.5780 | . 508 | 1.6653 | 1.4896 | . 991 | 1.6438 | 1.4802 |
| . 200 | 1.9028 | 1.5765 | . 533 | 1.6628 | 1.4884 | 1.229 | 1.6393 | 1.4787 |
| . 208 | 1.8673 | 1.5664 | . 589 | 1.6584 | 1.4864 | 1.307 | 1.6379 | 1.4783 |
| . 226 | 1.8130 | 1.5492 | . 643 | 1.6550 | 1.4849 | 1.497 | 1.6346 | 1.4774 |
| . 298 | 1.7230 | 1.5151 | . 656 | 1.6544 | 1.4846 | 1.682 | 1.6313 | - |
| . 340 | 1.7008 | 1.5056 | . 670 | 1.6537 | 1.4843 | 1.749 | - | 1.4764 |
| . 361 | 1.6932 | 1.5022 | . 760 | 1.6500 | 1.4826 | 1.849 | 1.6280 |  |
| . 410 | 1.6802 | 1.4964 | . 768 | 1.6497 | 1.4826 | 1.908 | - | 1.4757 |
| . 434 | 1.6755 | 1.4943 | . 801 | 1.6487 | 1.4822 | 2.172 | 1.6210 |  |
| . 486 | 1.6678 | 1.4907 | . 905 | 1.6458 | 1.4810 | 2.324 | - | 1.4739 |

TABLE 542.-INDEX OF REFRACTION FOR VARIOUS ALUMS

| $R$ | $\begin{aligned} & \stackrel{\vdots}{\hat{W}} \\ & \stackrel{5}{5} \end{aligned}$ | $\begin{aligned} & \text { ㅂ } \\ & \stackrel{0}{E} \\ & H \end{aligned}$ | Index of refraction for the Fraunhofer lines |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | a | B | c | D | E | b | F | G |
|  |  |  | Aluminum alums $\mathrm{RAl}\left(\mathrm{SO}_{4}\right)_{2}+12 \mathrm{H}_{2} \mathrm{O}$ * |  |  |  |  |  |  |  |
| Na | 1.667 | 17-28 | 1.43492 | 1.43563 | 1.43653 | 1.43884 | 1.44185 | 1.44231 | 1.44412 | 1.44804 |
| $\mathrm{NH}_{3}\left(\mathrm{CH}_{3}\right)$ | 1.568 | 7-17 | . 45013 | . 45062 | . 45177 | . 45410 | . 45691 | . 45749 | . 45941 | . 46363 |
| K | 1.735 | 14-15 | . 45226 | . 45303 | . 45398 | . 45645 | . 45934 | . 45996 | . 46181 | . 46609 |
| Rb | 1.852 | 7-21 | . 45232 | . 45328 | . 45417 | . 45660 | . 45955 | .45999 | . 46192 | . 46618 |
| Cs | 1.961 | 15-25 | . 45437 | . 45517 | . 45618 | . 45856 | . 46141 | . 46203 | . 46386 | . 46821 |
| $\mathrm{NH}_{4}$ | 1.631 | 15-20 | . 45509 | . 45599 | . 45693 | . 45939 | . 46234 | . 46288 | . 46481 | . 46923 |
| Tl | 2.329 | 10-23 | . 49226 | . 49317 | . 49443 | . 49748 | . 50128 | . 50209 | . 50463 | . 51076 |
| Chrome alums $\mathrm{RCr}\left(\mathrm{SO}_{4}\right)_{2}+12 \mathrm{H}_{2} \mathrm{O}$ * |  |  |  |  |  |  |  |  |  |  |
| Cs | 2.043 | 6-12 | 1.47627 | 1.47732 | 1.47836 | 1.48100 | 1.48434 | 1.48491 | 1.48723 | 1.49280 |
| K | 1.817 | 6-17 | . 47642 | . 47738 | . 47865 | . 48137 | . 48459 | . 48513 | . 48753 | . 49309 |
| Rb | 1.946 | 12-17 | . 47660 | . 47756 | . 47868 | . 48151 | . 48486 | . 48522 | . 48775 | . 49323 |
| $\mathrm{NH}_{4}$ | 1.719 | 7-18 | . 47911 | . 48014 | . 48125 | . 48418 | . 48744 | . 48794 | . 49040 | . 49594 |
| T1 | 2.386 | 9-25 | . 51692 | . 51798 | . 51923 | . 52280 | . 52704 | . 52787 | . 53082 | . 53808 |
| Iron alums $R \mathrm{Fe}\left(\mathrm{SO}_{4}\right)_{2}+12 \mathrm{H}_{2} \mathrm{O}$ * |  |  |  |  |  |  |  |  |  |  |
| K | 1.806 | 7-11 | 1.47639 | 1.47706 | 1.47837 | 1.48169 | 1.48580 | 1.48670 | 1.48939 | 1.49605 |
| Rb | 1.916 | 7-20 | . 47700 | . 47770 | . 47894 | . 48234 | . 48654 | . 48712 | . 49003 | . 49700 |
| Cs | 2.061 | 20-24 | . 47825 | . 47921 | . 48042 | . 48378 | . 48797 | . 48867 | . 49136 | . 49838 |
| $\mathrm{NH}_{4}$ | 1.713 | 7-20 | . 47927 | . 48029 | . 48150 | . 48482 | . 48921 | . 48993 | . 49286 | . 49980 |
| Tl | 2.385 | 15-17 | . 51674 | . 51790 | . 51943 | . 52365 | . 52859 | . 52946 | . 53284 | . 54112 |

The values are for the sodium $D$ line unless otherwise stated and are arranged in the order of increasing indices. Selected by Edgar T. Wherry from a private compilation of E. S. Larsen, of the U. S. Geological Survey.

|  | Mineral | Formula | Index of refraction $\lambda \stackrel{\text { refraction }}{=}$ |
| :---: | :---: | :---: | :---: |
| Villiaumite |  | NaF | 1.328 |
| Cryolithionite |  | $3 \mathrm{NaF} \cdot 3 \mathrm{LiF} \cdot 2 \mathrm{AlF}_{3}$ | 1.339 |
| Opal ...... |  | $\mathrm{SiO}_{2} \cdot \mathrm{nH}_{2} \mathrm{O}$ | 1.406 |
| Fluorite |  | $\mathrm{CaF}_{2}$ | 1.434 |
| Alum |  | $\mathrm{K}_{2} \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 4 \mathrm{SO}_{3} \cdot 24 \mathrm{H}_{2} \mathrm{O}$ | 1.456 |
| Sodalite |  | $3 \mathrm{Na}_{2} \mathrm{O} \cdot 3 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2} \cdot 2 \mathrm{NaCl}$ | 1.483 |
| Cristobalite |  | $\mathrm{SiO}_{2}$ | 1.486 |
| Analcite |  | $\mathrm{Na}_{2} \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 4 \mathrm{SiO}_{2} \cdot 2 \mathrm{H}_{2} \mathrm{O}$ | 1.487 |
| Sylvite |  | KCl | 1.490 |
| Noselite |  | $5 \mathrm{Na} 2 \mathrm{O} \cdot 3 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2} \cdot 2 \mathrm{SO}_{3}$ | 1.495 |
| Hauynite |  | Like preceding +CaO | 1.496 |
| Lazurite |  | $4 \mathrm{Na}_{2} \mathrm{O} \cdot 3 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2} \cdot \mathrm{Na}_{2} \mathrm{~S}_{6}$ | $1.500 \pm$ |
| Leucite |  | $\mathrm{K} 2 \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 4 \mathrm{SiO}_{3}$ | 1.509 |
| Pollucite |  | $2 \mathrm{Cs} 2 \mathrm{O} \cdot 2 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 9 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.525 |
| Halite |  | NaCl | 1.544 |
| Bauxite |  | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{nH}_{2} \mathrm{O}$ | $1.570 \pm$ |
| Pharmacosider |  | $3 \mathrm{Fe}_{3} \mathrm{O}_{3} \cdot 2 \mathrm{As}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{~K}_{2} \mathrm{O} \cdot 5 \mathrm{H}_{2} \mathrm{O}$ | 1.676 |
| Spinel |  | $\mathrm{MgO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3}$ | $1.720 \pm$ |
| Berzeliite |  | $3(\mathrm{Ca}, \mathrm{Mg}, \mathrm{Mn}) \mathrm{O} \cdot \mathrm{As}_{2} \mathrm{O}_{0}$ | 1.727 |
| Periclasite |  | MgO | 1.736 |
| Grossularite |  | $3 \mathrm{CaO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2}$ | 1.736 |
| Helvite |  | $3(\mathrm{Mn}, \mathrm{Fe}) \mathrm{O} \cdot 3 \mathrm{BeO} \cdot 3 \mathrm{SiO}_{2} \cdot \mathrm{MnS}$ | 1.739 |
| Pyrope |  | $3 \mathrm{MgO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2}$ | 1.745 |
| Arsenolite |  | $\mathrm{As}_{2} \mathrm{O}_{3}$ | 1.754 |
| Hessonite |  | $3 \mathrm{CaO} \cdot(\mathrm{Al}, \mathrm{Fe})_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2}$ | 1.763 |
| Pleonaste |  | $(\mathrm{Mg}, \mathrm{Fe}) \mathrm{O} \cdot \mathrm{Al}_{3} \mathrm{O}_{3}$ | $1.770 \pm$ |
| Almandite |  | $3 \mathrm{FeO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2}$ | 1.778 |
| Hercynite |  | $\mathrm{FeO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3}$ | $1.800 \pm$ |
| Gahnite |  | $\mathrm{ZnO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3}$ | $1.805 \pm$ |
| Spessartite |  | $3 \mathrm{MnO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2}$ | 1.811 |
| Lime |  | CaO | 1.838 |
| Uvarovite |  | $3 \mathrm{CaO} \cdot \mathrm{Cr}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2}$ | 1.838 |
| Andradite |  | $3 \mathrm{CaO} \cdot \mathrm{Fe}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2}$ | 1857 |
| Microlite |  | $6 \mathrm{CaO} \cdot 3 \mathrm{Ta}_{2} \mathrm{O}_{0} \cdot \mathrm{NbOF}_{3}$ | 1.925 |
| Nantokite |  | CuCl | 1.930 |
| Pyrochlore |  | Contains $\mathrm{CaO}, \mathrm{Ce}_{2} \mathrm{O}_{2}, \mathrm{TiO}_{2}$, etc. | 1.960 |
| Schorlomite |  | $3 \mathrm{CaO} \cdot(\mathrm{Fe}, \mathrm{Ti})_{2} \mathrm{O}_{3} \cdot 3(\mathrm{Si}, \mathrm{Ti}) \mathrm{O}_{2}$ | 1.980 - |
| Percylite |  | $\mathrm{PbO} \cdot \mathrm{CuCl}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 2.050 |
| Picotite |  | $(\mathrm{Mg}, \mathrm{Fe}) \mathrm{O} \cdot(\mathrm{Al}, \mathrm{Cr})_{2} \mathrm{O}_{3}$ | $2.050 \pm$ |
| Eulytite |  | $2 \mathrm{Bi}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2}$ | 2.050 |
| Cerargyrite |  | AgCl | 2.061 |
| Mosesite |  | Contains $\mathrm{Hg}, \mathrm{NH}_{4}, \mathrm{Cl}$, etc. | 2.065 |
| Chromite |  | $\mathrm{FeO} \cdot \mathrm{Cr}_{2} \mathrm{O}_{3}$ | 2.070 |
| Senarmontite |  | $\mathrm{Sb}_{2} \mathrm{O}_{3}$ | 2.087 |
| Embolite |  | $\mathrm{Ag}(\mathrm{Br}, \mathrm{Cl})$ | $2.150 \pm$ |
| Manganosite |  | MnO | 2.160 |
| Bunsenite |  | NiO | 2.18 * |
| Lewisite |  | $5 \mathrm{CaO} \cdot 2 \mathrm{TiO}_{2} \cdot 3 \mathrm{Sb}_{2} \mathrm{O}_{5}$ | 2.200 |
| Miersite |  | $\mathrm{CuI} \cdot 4 \mathrm{AgI}$ | 2.200 |
| Bromyrite |  | AgBr | 2.253 |
| Dysanalite |  | Contains $\mathrm{CaO}, \mathrm{FeO}, \mathrm{TiO}_{2}$, etc. | 2.330 |
| Marshite |  | CuI | 2.346 |
| Franklinite |  | $(\mathrm{Zn}, \mathrm{Fe}, \mathrm{Mn}) \mathrm{O} \cdot(\mathrm{Fe}, \mathrm{Mn})_{2} \mathrm{O}_{3}$ | 2.360* |
| Sphalerite |  | $(\mathrm{Zn}, \mathrm{Fe}) \mathrm{S}$ | 2.370 |
| Perovskite |  | $\mathrm{CaO} \cdot \mathrm{TiO}$, | 2.380 |
| Diamond |  | C | 2.419 |

(continued)

# TABLE 543.-INDEX OF REFRACTION OF SELECTED MONOREFRINGENT OR ISOTROPIC MINERALS (concluded) 

| Mineral | Formula | Index of refraction $\lambda=0.589 \mu$ |
| :---: | :---: | :---: |
|  | $\mathrm{HgO} \cdot 2 \mathrm{HgCl}$ | 2.490* |
|  | $\mathrm{MnS}_{2}$ | 2.690* |
|  | MnS | 2.700* |
|  | $\mathrm{Cu}_{2} \mathrm{O}$ | 2.849 |

- Li line.

TABLE 544.—INDEX OF REFRACTION OF MISCELLANEOUS MONOREFRINGENT OR ISOTROPIC SOLIDS

| Substance | Spectrum line | Index of refraction | Substance | Spectrum line | Index of refraction |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Albite glass | D | 1.4890 | Gelatin, Nelson no. 1 | D | 1.530 |
| Amber . . . . | D | 1.546 | " various .... | D | 1.516-1.534 |
| Ammonium chloride | D | 1.6422 | Gum Arabic | . red | 1.480 |
| Anorthite glass .... | D | 1.5755 | " " | . red | 1.514 |
| Asphalt ...... | - D | 1.635 | Obsidian ..... | . D | 1.482-1.496 |
| "، | . $670 \mu$ | 1.621 | Phosphorus | - D | 2.1442 |
| Bell metal | D | 1.0052 | Pitch .... | . red | 1.531 |
| Boric acid, melted. | C | 1.4623 | Potassium bromide | . D | 1.5593 |
| " " " | D | 1.4637 | " chlorstanna | e. D | 1.6574 |
| " " | F | 1.4694 | " iodide | . D | 1.6666 |
| Borax, melted | C | 1.4624 | Resins: Aloes ... | . red | 1.619 |
| " ${ }^{\text {c }}$ | . D | 1.4630 | Canada balsam | . red | 1.528 |
| " | F | 1.4702 | Colophony . | . red | 1.548 |
| Camphor | . D | 1.532 | Copal ... | . red | 1.528 |
| " | D | 1.5462 | Mastic | . red | 1.535 |
| Canada balsam | . D | 1.530 | Peru balsam | . . D | 1.593 |
| Ebonite | . red | 1.66 | Selenium | - A | 2.61 |
| Fuchsin |  | 2.03 | " | . B | 2.68 |
| " | - B | 2.19 | " | - C | 2.73 |
| " | . C | 2.33 | " .......... | . D | 2.93 |
| " | . G | 1.97 | Sodium chlorate | . D | 1.5150 |
| " | H | 1.32 | Strontium nitrate ... | . D | 1.5667 |

TABLE 545.-INDEX OF REFRACTION OF MISCELLANEOUS UNIAXIAL CRYSTALS

|  |  | Index of refraction |  |
| :---: | :---: | :---: | :---: |
| Crystal | Spectrum line | Ordinary ray | Extraordinary ray |
| Ammonium arseniate $\mathrm{NH}_{4} \mathrm{H}_{2} \mathrm{AsO}_{4}$ | D | 1.5766 | 1.5217 |
| Benzil ( $\left.\mathrm{C}_{7} \mathrm{H}_{6} \mathrm{CO}\right)_{2}$ | D | 1.6588 | 1.6784 |
| Corundum, $\mathrm{Al}_{2} \mathrm{O}_{3}$, sapphire, ruby | D | 1.769 | 1.760 |
| Ice at $-8^{\circ} \mathrm{C}$. | D | 1.308 | 1.313 |
| " " | Li | 1.297 | 1.304 |
| Ivory | D | 1.539 | 1.541 |
| Potassium arseniate $\mathrm{KH}_{2} \mathrm{AsO}_{4}$ | F | 1.5762 | 1.5252 |
| " " | D | 1.5674 | 1.5179 |
| " " ${ }^{\text {".. }}$ | C | 1.5632 | 1.5146 |
| Sodium arseniate $\mathrm{Na}_{3} \mathrm{AsO}_{4} \cdot 12 \mathrm{H}_{2} \mathrm{O}$ | D | 1.457 | 1.466 |
| " nitrate $\mathrm{NaNO}_{3} \ldots \ldots$. | D | 1.586 | 1.336 |
| " phosphate $\mathrm{Na}_{3} \mathrm{PO}_{4} \cdot 12 \mathrm{H}_{2} \mathrm{O}$ | D | 1.447 | 1.453 |
| Nickel sulfate $\mathrm{NiSO}_{4} \cdot 6 \mathrm{H}_{2} \mathrm{O} \ldots$ | F | 1.5173 | 1.4930 |
|  | D | 1.5109 | 1.4873 |
| " " ${ }^{\text {" }}$ | C | 1.5078 | 1.4844 |
| Strychnine sulfate | D | 1.614 | 1.599 |

## TABLE 546.-INDEX OF REFRACTION OF SELECTED UNIAXIAL MINERALS

The values are arranged in the order of increasing indices for the ordinary ray and are for the sodium $D$ line unless otherwise indicated. Selected by Edgar T. Wherry from a private compilation of Esper S. Larsen, of the U. S. Geological Survey.

| Ice Mineral | Uniaxial positive mineralsFormula | Index of $\underbrace{\text { refraction }}$ |  |
| :---: | :---: | :---: | :---: |
|  |  | $\overbrace{\substack{\text { Ordinary } \\ \text { ray }}}$ | $\underbrace{}_{\substack{\text { Extraordinary } \\ \text { ray }}}$ |
|  | $\mathrm{H}_{2} \mathrm{O}$ | 1.309 | 1.313 |
| Sellaite | $\mathrm{MgF}_{2}$ | 1.378 | 1.390 |
| Chrysocolla | $\mathrm{CuO} \cdot \mathrm{SiO}_{2} \cdot 2 \mathrm{H}_{2} \mathrm{O}$ | $1.460 \pm$ | $1.570 \pm$ |
| Laubanite . | $2 \mathrm{CaO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 5 \mathrm{SiO}_{2} \cdot 6 \mathrm{H}_{2} \mathrm{O}$ | 1.475 | 1.486 |
| Chabazite | $\left(\mathrm{Ca}, \mathrm{Na}_{2}\right) \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 4 \mathrm{SiO}_{2} \cdot 6 \mathrm{H}_{2} \mathrm{O}$ | $1.480 \pm$ | $1.482 \pm$ |
| Douglasite | $2 \mathrm{KCl} \cdot \mathrm{FeCl}_{3} \cdot 2 \mathrm{H}_{2} \mathrm{O}$ | 1.488 | 1.500 |
| Hydronephelite | $2 \mathrm{Na}_{2} \mathrm{O} \cdot 3 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2} \cdot 7 \mathrm{H}_{2} \mathrm{O}$ | $1.490{ }^{\text {1 }}$ | ${ }_{1.502}^{1.537}$ |
| Apophyllite | $\mathrm{K}_{2} \mathrm{O} \cdot 8 \mathrm{CaO} \cdot 16 \mathrm{SiO}_{2} \cdot 16 \mathrm{H}_{2} \mathrm{O}$ | $1.535 \pm$ | $1.537 \pm$ |
| Quartz | $\mathrm{SiO}_{2} \mathrm{H}^{\text {cen }}$ | 1.544 | 1.553 |
| Coquimbite | $\mathrm{Fe}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SO}_{3} \cdot 9 \mathrm{H}_{2} \mathrm{O}$ | 1.550 | 1.556 |
| Brucite Alunite . | $\mathrm{MgO} \cdot \mathrm{H}_{2} \mathrm{O}$ K 2 O $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot 4 \mathrm{SO}_{3} \cdot 6 \mathrm{H}_{2} \mathrm{O}$ | 1.559 1.572 | 1.580 1.592 |
| Penninite | $5(\mathrm{Mg}, \mathrm{Fe}) \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2} \cdot 4 \mathrm{H}_{2} \mathrm{O}$ | 1.576 | 1.579 |
| Cacoxenite | $2 \mathrm{Fe}_{2} \mathrm{O}_{3} \cdot \mathrm{P}_{2} \mathrm{O}_{5} \cdot 12 \mathrm{H}_{2} \mathrm{O}$ | 1.582 | 1.645 |
| Eudialite | $6 \mathrm{Na}_{2} \mathrm{O} \cdot 6(\mathrm{Ca}, \mathrm{Fe}) \mathrm{O} \cdot 20(\mathrm{Si}, \mathrm{Zr}) \mathrm{O}_{2} \cdot \mathrm{NaCl}$ | 1.606 | 1.611 |
| Dioptase | $\mathrm{CuO} \cdot \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.654 | 1.707 |
| Phenacite | $2 \mathrm{BeO} \cdot \mathrm{SiO}_{2}$ | 1.654 | 1.670 |
| Parisite | $2 \mathrm{CeOF} \cdot \mathrm{CaO} \cdot 3 \mathrm{CO}_{2}$ | $1.676 \pm$ | 1.757 |
| Willemite | $2 \mathrm{ZnO} \cdot \mathrm{SiO}_{2}$ | 1.691 | 1.719 |
| Vesuvianite | $2(\mathrm{Ca}, \mathrm{Mn}, \mathrm{Fe}) \mathrm{O} \cdot(\mathrm{Al}, \mathrm{Fe})(\mathrm{OH}, \mathrm{F}) \mathrm{O} \cdot 2 \mathrm{SiO}_{2}$ | $1.716 \pm$ | 1.721 |
| Xenotime | $\mathrm{Y}_{2} \mathrm{O}_{3} \cdot \mathrm{P}_{2} \mathrm{O}_{5}$ | . 721 | 1.816 |
| Connellite | $20 \mathrm{CuO} \cdot \mathrm{SO}_{3} \cdot 2 \mathrm{CuCl}_{2} \cdot 20 \mathrm{H}_{2} \mathrm{O}$ | 1.724 | 1.746 |
| Benitoite | $\mathrm{BaO} \cdot \mathrm{TiO}_{2} \cdot 3 \mathrm{SiO}_{2}$ | 1.757 | 1.804 |
| Ganomalite | $6 \mathrm{PbO} \cdot 4(\mathrm{Ca}, \mathrm{Mn}) \mathrm{O} \cdot 6 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.910 | 1.945 |
| Scheelite | $\mathrm{CaO} \cdot \mathrm{WO}_{3}$ | 1.918 | 1.934 |
| Zircon | $\mathrm{ZrO} \cdot \mathrm{SiO}_{2}$ | $1.923 \pm$ | $1.968 \pm$ |
| Powellite | $\mathrm{CaO} \cdot \mathrm{MoO}_{3}$ | 1.974 | 1.978 |
| Calomel | HgCl | 1.973 | 2.650 |
| Cassiterite | $\mathrm{SnO}_{2}$ | 1.997 | 2.093 |
| Zincite | ZnO | 2.013 | 2.029 |
| Phosgenite | $\mathrm{PbO} \cdot \mathrm{PbCl}_{2} \cdot \mathrm{CO}_{2}$ | 2.114 | 2.140 |
| Penfieldite | $\mathrm{PbO} \cdot \mathrm{PbCl}_{2}$ | 2.130 | 2.210 |
| Iodyrite | AgI | 2.210 | 2.220 |
| Tapiolite | $\mathrm{FeO} \cdot(\mathrm{Ta}, \mathrm{Nb})_{2} \mathrm{O}_{5}$ | 2.270 | 2.420 (Li line) |
| Wurtzite | ZnS | 2.356 | 2.378 |
| Derbylite | $6 \mathrm{FeO} \cdot \mathrm{Sb}_{2} \mathrm{O}_{3} \cdot 5 \mathrm{TiO}_{2}$ | 2.450 | 2.510 (Li line) |
| Greenockite | CdS | 2.506 | 2.529 |
| Rutile | $\mathrm{TiO}_{2}$ | 2.616 | 2.903 |
| Moissanite | CSi | 2.654 | 2.697 |
| Cinnabar | HgS | 2.854 | 3.201 |

Uniaxial negative minerals

| Chiolite | $2 \mathrm{NaF} \cdot \mathrm{AlF}_{3}$ | 1.349 | 1.342 |
| :---: | :---: | :---: | :---: |
| Hanksite | $11 \mathrm{Na}_{2} \mathrm{O} \cdot 9 \mathrm{SO}_{3} \cdot 2 \mathrm{CO}_{2} \cdot \mathrm{KCl}$ | 1.481 | 1.461 |
| Thaumasite | $3 \mathrm{CaO} \cdot \mathrm{CO}_{2} \cdot \mathrm{SiO}_{2} \cdot \mathrm{SO}_{3} \cdot 15 \mathrm{H}_{2} \mathrm{O}$ | 1.507 | 1.468 |
| Hydrotalcite | $6 \mathrm{MgO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{CO}_{2} \cdot 15 \mathrm{H}_{2} \mathrm{O}$ | 1.512 | 1.498 |
| Cancrinite | $4 \mathrm{Na} 2 \mathrm{O} \cdot \mathrm{CaO} \cdot 4 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 2 \mathrm{CO}_{2} \cdot 9 \mathrm{SiO}_{2} \cdot 3 \mathrm{H}_{2} \mathrm{O}$ | 1.524 | 1.496 |
| Milarite | $\mathrm{K}_{2} \mathrm{O} \cdot 4 \mathrm{CaO} \cdot 2 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 24 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.532 | 1.529 |
| Kaliophilite | $\mathrm{K}_{2} \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 2 \mathrm{SiO}_{2}$ | 1.537 | 1.533 |
| Mellite | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{C}_{12} \mathrm{O}_{8} \cdot 18 \mathrm{H}_{2} \mathrm{O}$ | 1.539 | 1.511 |
| Marialite | "Ma" $=3 \mathrm{Na}_{2} \mathrm{O} \cdot 3 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 18 \mathrm{SiO}_{2} \cdot 2 \mathrm{NaCl}$ | 1.539 | 1.537 |
| Nephelite | $\mathrm{Na}_{2} \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 2 \mathrm{SiO}_{2}$ | 1.542 | 1.538 |
| Wernerite | $\mathrm{Me}_{1} \mathrm{Ma}_{1} \pm$ | 1.578 | 1.551 |
| Beryl | $3 \mathrm{BeO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2}$ | $1.581 \pm$ | $1.575 \pm$ |
| Torbernite | $\mathrm{CuO} \cdot 2 \mathrm{UO}_{3} \cdot \mathrm{P}_{2} \mathrm{O}_{5} \cdot 8 \mathrm{H}_{2} \mathrm{O}$ | 1.592 | 1.582 |
| Meionite | $" \mathrm{Me} "=4 \mathrm{CaO} \cdot 3 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2}$ | 1.597 | 1.560 |
| Melilite | Contains $\mathrm{Na}_{2} \mathrm{O}, \mathrm{CaO}, \mathrm{Al}_{2} \mathrm{O}_{3}, \mathrm{SiO}_{2}$, etc. | 1.634 | 1.629 |

## TABLE 546.-INDEX OF REFRACTION OF SELECTED UNIAXIAL MINERALS (concluded)

Uniaxial negative minerals (continued)

| Mineral | Uniaxial ngative minal (contined) | Index of refraction |  |
| :---: | :---: | :---: | :---: |
|  | Formula | $\overbrace{\substack{\text { Ordinary } \\ \text { ray }}}$ | $\underbrace{}_{\substack{\text { Extraordinary } \\ \text { ray }}}$ |
| Apatite | $9 \mathrm{CaO} \cdot 3 \mathrm{P}_{2} \mathrm{O}_{5} \cdot \mathrm{Ca}(\mathrm{F}, \mathrm{Cl})_{2}$ | 1.634 | 1.631 |
| Calcite | $\mathrm{CaO} \cdot \mathrm{CO}_{2}$ | 1.658 | 1.486 |
| Gehlenite | $2 \mathrm{CaO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{SiO}_{2}$ | 1.669 | 1.658 |
| Tourmaline | Contains $\mathrm{Na}_{2} \mathrm{O}, \mathrm{FeO}, \mathrm{Al}_{2} \mathrm{O}_{3}, \mathrm{~B}_{2} \mathrm{O}_{3}, \mathrm{SiO}_{2}$, etc. | $1.669 \pm$ | $1.638 \pm$ |
| Dolomite | $\mathrm{CaO} \cdot \mathrm{MgO} \cdot 2 \mathrm{CO}_{2}$ | 1.681 | 1.500 |
| Magnesite | $\mathrm{MgO} \cdot \mathrm{CO}_{2}$ | 1.700 | 1.509 |
| Pyrochroite | $\mathrm{MnO} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.723 | 1.681 |
| Corundum | $\mathrm{Al}_{2} \mathrm{O}_{3}$ | 1.768 | 1.760 |
| Smithsonite | $\mathrm{ZnO} \cdot \mathrm{CO}_{2}$ | 1.818 | 1.618 |
| Rhodochrosite | $\mathrm{MnO} \cdot \mathrm{CO}_{2}$ | 1.818 | 1.595 |
| Jarosite | $\mathrm{K}_{2} \mathrm{O} \cdot 3 \mathrm{Fe}_{2} \mathrm{O}_{3} \cdot 4 \mathrm{SO}_{3} \cdot 6 \mathrm{H}_{2} \mathrm{O}$ | 1.820 | 1.715 |
| Siderite | $\mathrm{FeO} \cdot \mathrm{CO}_{2}$ | 1.875 | 1.635 |
| Pyromorphite | $9 \mathrm{PbO} \cdot 3 \mathrm{P}_{2} \mathrm{O}_{5} \cdot \mathrm{PbCl}_{2}$ | 2.050 | 2.042 |
| Barysilite .... | $3 \mathrm{PbO} \cdot 2 \mathrm{SiO}_{2}$ | 2.070 | 2.050 |
| Mimetite | $9 \mathrm{PbO} \cdot 3 \mathrm{As}_{2} \mathrm{O}_{5} \cdot \mathrm{PbCl}_{2}$ | 2.135 | 2.118 |
| Matlockite | $\mathrm{PbO} \cdot \mathrm{PbCl}_{2}$ | 2.150 | 2.040 |
| Stolzite | $\mathrm{PbO} \cdot \mathrm{WO}_{3}$ | 2.269 | 2.182 |
| Geikielite | $(\mathrm{Mg}, \mathrm{Fe}) \mathrm{O} \cdot \mathrm{TiO}_{2}$ | 2.310 | 1.950 |
| Vanadinite | $9 \mathrm{PbO} \cdot 3 \mathrm{~V}_{2} \mathrm{O}_{5} \cdot \mathrm{PbCl}_{2}$ | 2.354 | 2.299 |
| Wulfenite | $\mathrm{PbO} \cdot \mathrm{MoO}_{3}$ | 2.402 | 2.304 (Li line) |
| Octahedrite | $\mathrm{TiO}_{2}$ | 2.554 | 2.493 |
| Massicotite | PbO | 2.665 | 2.535 (Li line) |
| Proustite | $3 \mathrm{Ag}_{2} \mathrm{~S} \cdot \mathrm{As}_{2} \mathrm{~S}_{3}$ | 2.979 | 2.711 " " |
| Pryargyrite | $3 \mathrm{Ag}_{2} \mathrm{~S} \cdot \mathrm{Sb}_{2} \mathrm{~S}_{3}$ | 3.084 | 2.881 " |
| Hematite . | $\mathrm{Fe}_{2} \mathrm{O}_{3}$ | 3.220 | 2.940 " |

TABLE 547.-INDEX OF REFRACTION OF MISCELLANEOUS LIQUIDS
(see also Table 551), LIQUEFIED GASES, OILS, FATS, AND WAXES

| Substance | ${ }_{\text {Temp }}^{\text {e }}$ | $\begin{aligned} & \text { Index for } D \\ & 0.589 \mu \end{aligned}$ | Substance | ${ }_{\text {Temp }}{ }^{\text {C }}$ | $\begin{aligned} & \text { Index for } D \\ & 0.589 \mu \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Liquefied gases: |  |  | Oils: |  |  |
| $\mathrm{Br}_{2}$ | 15 | 1.659 | Lavender | 20 | $1.464-1.466$ |
| $\mathrm{Cl}_{2}$ | 14 | 1.367 | Linseed | 15 | 1.4820-1.4852 |
| $\mathrm{CO}_{2}$ | 15 | 1.195 | Maize | 15.5 | 1.4757-1.4768 |
| $\mathrm{C}_{2} \mathrm{~N}_{2}$ | 18 | 1.325 | Mustard seed | 15.5 | 1.4750-1.4762 |
| $\mathrm{C}_{2} \mathrm{H}_{4}$ | 6 | 1.180 | Neat's foot | 15 | 1.4695-1.4708 |
| $\mathrm{H}_{2} \mathrm{~S}$ | 18.5 | 1.384 | Olive | 15.5 | 1.4703-1.4718 |
| $\mathrm{N}_{2}$ | -190 | 1.205 | Palm | 60 | 1.4510 |
| $\mathrm{NH}_{3}$ | 16.5 | 1.325 | Peanut | 15.5 | 1.4723-1.4731 |
| NO | 90 | 1.330 | Peppermint | 20 | 1.464-1.468 |
| $\mathrm{N}_{2} \mathrm{O}$ | 15 | 1.194 | Poppy | 15.5 | 1.4770 |
| $\mathrm{O}_{2}$ | -181 | 1.221 | Porpoise | 25 | 1.4677 |
| $\mathrm{SO}_{2}$ | 15 | 1.350 | Rape (Colza) | 15.5 | 1.4748-1.4752 |
| HCl | 16.5 | 1.252 | Seal | 25 | 1.4741 |
| HBr | 10 | 1.325 | Sesame | 15.5 | 1.4742 |
| HI | 16.5 | 1.466 | Soya bean | 15.5 | 1.4760-1.4775 |
| Oils: |  |  | Sperm | 15.5 | 1.4665-1.4672 |
| Almond | 15.5 | 1.4728-1.4753 | Sunflower | 15.5 | 1.4739 |
| Castor | 15 | 1.4799-1.4803 | Tung | 19 | 1.503 |
| Citronella | 20 | $1.47-1.48$ | Whale | 40 | 1.4649 |
| Clove | 20 | 1.5301-1.5360 | Fats and Waxes: |  |  |
| Cocoanut | 15.5 | 1.4587 | Beef tallow .... | 40 | 1.4552-1.4587 |
| Cod liver | 15 | 1.4790-1.4833 | Beeswax | 75 | 1.4398-1.4451 |
| Cotton seed | 15.5 | 1.4737-1.4757 | Carnauba wax. | 84 | 1.4520-1.4541 |
| Croton | 27 | 1.4757-1.4768 | Cocoa butter | 40 | 1.4560-1.4518 |
| Eucalyptus | 20 | $1.460-1.467$ | Lard | 40 | 1.4584-1.4601 |
| Lard | 15.5 | 1.4702-1.4720 | Mutton tallow.. | 60 | 1.4510 |

## TABLE 548.-INDEX OF REFRACTION OF SELECTED BIAXIAL MINERALS

The values are arranged in the order of increasing $\beta$ index of refraction and are for the sodium $D$ line except where noted. Selected by Edgar T. Wherry from private compilation of Esper S. Larsen, of the U. S. Geological Survey.

| Mineral | Biaxial positive minerals | Index of $\underbrace{\text { refraction }}$ |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Formula | $n_{a}$ | $n \beta$ | m |
| Stercorite | $\mathrm{Na}_{2} \mathrm{O} \cdot\left(\mathrm{NH}_{4}\right)_{2} \mathrm{O} \cdot \mathrm{P}_{2} \mathrm{O}_{6} \cdot 9 \mathrm{H}_{2} \mathrm{O}$ | 1.439 | 1.441 | 1.469 |
| Aluminite | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{SO}_{2} \cdot 9 \mathrm{H}_{3} \mathrm{O}$ | 1.459 | 1.464 | 1.470 |
| Tridymite | $\mathrm{SiO}_{2}$ | 1.469 | 1.470 | 1.473 |
| Thenardite | $\mathrm{Na}_{2} \mathrm{O} \cdot \mathrm{SO}_{3}$ | 1.464 | 1.474 | 1.485 |
| Carnallite | $\mathrm{KCl} \cdot \mathrm{MgCl}_{2} \cdot 6 \mathrm{H}_{2} \mathrm{O}$ | 1.466 | 1.475 | 1.494 |
| Alunogen | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SO}_{3} \cdot 16 \mathrm{H}_{2} \mathrm{O}$ | 1.474 | 1.476 | 1.483 |
| Melanterite | $\mathrm{FeO} \cdot \mathrm{SO}_{3} \cdot 7 \mathrm{H}_{2} \mathrm{O}$ | 1.471 | 1.478 | 1.486 |
| Natrolite | $\mathrm{Na}_{2} \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2} \cdot 2 \mathrm{H}_{2} \mathrm{O}$ | 1.480 | 1.482 | 1.493 |
| Arcanite | $\mathrm{K}_{2} \mathrm{O} \cdot \mathrm{SO}_{3}$ | 1.494 | 1.495 | 1.497 |
| Struvite | $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{O} \cdot 2 \mathrm{MgO} \cdot \mathrm{P}_{2} \mathrm{O}_{5} \cdot 12 \mathrm{H}_{2} \mathrm{O}$ | 1.495 | 1.496 | 1.500 |
| Heulandite | $\mathrm{CaO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2} \cdot 3 \mathrm{H}_{2} \mathrm{O}$ | 1.498 | 1.499 | 1.505 |
| Thomsonite | $\left(\mathrm{Na}_{2}, \mathrm{Ca}\right) \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 2 \mathrm{SiO}_{2} \cdot 3 \mathrm{H}_{2} \mathrm{O}$ | 1.497 | 1.503 | 1.525 |
| Harmotome | $(\mathrm{K} 2, \mathrm{Ba}) \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{8} \cdot 5 \mathrm{SiO}_{2} \cdot 5 \mathrm{H}_{2} \mathrm{O}$ | 1.503 | 1.505 | 1.508 |
| Petalite | $\mathrm{Li}_{2} \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 8 \mathrm{SiO}_{2}$ | 1.504 | 1.510 | 1.516 |
| Monetite | $2 \mathrm{CaO} \cdot \mathrm{P}_{2} \mathrm{O}_{5} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.515 | 1.518 | 1.525 |
| Newberyite | $2 \mathrm{MgO} \cdot \mathrm{P}_{2} \mathrm{O}_{5} \cdot 7 \mathrm{H}_{2} \mathrm{O}$ | 1.514 | 1.519 | 1.533 |
| Gypsum | $\mathrm{CaO} \cdot \mathrm{SO}_{3} \cdot 2 \mathrm{H}_{2} \mathrm{O}$ | 1.520 | 1.523 | 1.530 |
| Mascagnite | $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{O} \cdot \mathrm{SO}_{3}$ | 1.521 | 1.523 | 1.533 |
| Albite .... | " $\mathrm{Ab}^{\prime \prime}=\mathrm{Na}_{2} \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{3}$ | 1.525 | 1.529 | 1.536 |
| Hydromagnesit | $4 \mathrm{MgO} \cdot 3 \mathrm{CO}_{2} \cdot 4 \mathrm{H}_{2} \mathrm{O}$ | 1.527 | 1.530 | 1.540 |
| Wavellite | $3 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 2 \mathrm{P}_{2} \mathrm{O}_{5} \cdot 12\left(\mathrm{H}_{2} \mathrm{O}, 2 \mathrm{HF}\right)$ | 1.525 | 1.534 | 1.552 |
| Kieserite | $\mathrm{MgO} \cdot \mathrm{SO}_{3} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.523 | 1.535 | 1.586 |
| Copiapite | $2 \mathrm{Fe}_{2} \mathrm{O}_{3} \cdot 5 \mathrm{SO}_{3} \cdot 18 \mathrm{H}_{2} \mathrm{O}$ | 1.530 | 1.550 | 1.592 |
| Whewellite | $\mathrm{CaO} \cdot \mathrm{C}_{2} \mathrm{O}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.491 | 1.555 | 1.650 |
| Variscite | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{P}_{2} \mathrm{O}_{8} \cdot 4 \mathrm{H}_{2} \mathrm{O}$ | 1.551 | 1.558 | 1.582 |
| Labradorite | $\mathrm{Ab}_{2} \mathrm{An}_{3}$ | 1.559 | 1.563 | 1.568 |
| Gibbsite | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{H}_{2} \mathrm{O}$ | 1.566 | 1.566 | 1.587 |
| Wagnerite | $3 \mathrm{MgO} \cdot \mathrm{P}_{2} \mathrm{O}_{5} \cdot \mathrm{MgF}_{2}$ | 1.569 | 1.570 | 1.582 |
| Anhydrite | $\mathrm{CaO} \cdot \mathrm{SO}_{3}$ | 1.571 | 1.576 | 1.614 |
| Colemanite | $2 \mathrm{CaO} \cdot 3 \mathrm{~B}_{2} \mathrm{O}_{3} \cdot 5 \mathrm{H}_{2} \mathrm{O}$ | 1.586 | 1.592 | 1.614 |
| Fremontite | $\mathrm{Na}_{2} \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{8} \cdot \mathrm{P}_{2} \mathrm{O}_{5} \cdot\left(\mathrm{H}_{2} \mathrm{O}, 2 \mathrm{HF}\right)$ | 1.594 | 1.603 | 1.615 |
| Vivianite | $3 \mathrm{FeO} \cdot \mathrm{P}_{2} \mathrm{O}_{5} \cdot 8 \mathrm{H}_{2} \mathrm{O}$ | 1.579 | 1.603 | 1.633 |
| Pectolite | $\mathrm{Na} 2 \mathrm{O} \cdot 4 \mathrm{CaO} \cdot 6 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.595 | 1.604 | 1.633 |
| Calamine | $2 \mathrm{ZnO} \cdot \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.614 | 1.617 | 1.636 |
| Chondrodite | $4 \mathrm{MgO} \cdot \mathrm{SiO}_{2} \cdot \mathrm{Mg}(\mathrm{F}, \mathrm{OH})_{2}$ | 1.604 | 1.617 | 1.636 |
| Turquoise | $\mathrm{CuO} \cdot 3 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 2 \mathrm{P}_{2} \mathrm{O}_{6} \cdot 9 \mathrm{H}_{2} \mathrm{O}$ | 1.610 | 1.620 | 1.650 |
| Topaz | $2 \mathrm{AlOF} \cdot \mathrm{SiO}_{2}$ | 1.619 | 1.620 | 1.627 |
| Celestite | $\mathrm{SrO} \cdot \mathrm{SO}_{3}$ | 1.622 | 1.624 | 1.631 |
| Prehnite | $2 \mathrm{CaO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.616 | 1.626 | 1.649 |
| Barite | $\mathrm{BaO} \cdot \mathrm{SO}_{3}$ | 1.636 | 1.637 | 1.648 |
| Anthophyllite | $\mathrm{MgO} \cdot \mathrm{SiO}_{2}$ | 1.633 | 1.642 | 1.657 |
| Sillimanite . | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{SiO}_{2}$ | 1.638 | 1.642 | 1.653 |
| Forsterite | $2 \mathrm{MgO} \cdot \mathrm{SiO}_{2}$ | 1.635 | 1.651 | 1.669 |
| Enstatite | $\mathrm{MgO} \cdot \mathrm{SiO}_{2}$ | 1.650 | 1.653 | 1.658 |
| Euclase | $2 \mathrm{BeO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 2 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.653 | 1.656 | 1.673 |
| Triplite | $3 \mathrm{MnO} \cdot \mathrm{P}_{2} \mathrm{O}_{8} \cdot \mathrm{MnF}_{2}$ | 1.650 | 1.660 | 1.672 |
| Spodumene | $\mathrm{Li}_{2} \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 4 \mathrm{SiO}_{2}$ | 1.660 | 1.666 | 1.676 |
| Diopside | $\mathrm{CaO} \cdot \mathrm{MgO} \cdot 2 \mathrm{SiO}_{2}$ | 1.664 | 1.671 | 1.694 |
| Olivine | $2(\mathrm{Mg}, \mathrm{Fe}) \mathrm{O} \cdot \mathrm{SiO}_{2}$ | 1.662 | 1.680 | 1.699 |
| Triphylite | $\mathrm{Li}_{2} \mathrm{O} \cdot 2(\mathrm{Fe}, \mathrm{Mn}) \mathrm{O} \cdot \mathrm{P}_{2} \mathrm{O}_{5}$ | 1.688 | 1.688 | 1.692 |
| Zoisite. | $4 \mathrm{CaO} \cdot 3 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.700 | 1.702 | 1.706 |
| Strengite | $\mathrm{Fe}_{2} \mathrm{O}^{2} \cdot \mathrm{P}_{2} \mathrm{O}_{8} \cdot 4 \mathrm{H}_{2} \mathrm{O}$ | 1.708 | 1.708 | 1.745 |
| Diaspore | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.702 | 1.722 | 1.750 |
| Staurolite | $2 \mathrm{FeO} \cdot 5 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 4 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.736 | 1.741 | 1.746 |
| Chrysoberyl | $\mathrm{BeO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3}$ | 1.747 | 1.748 | 1.757 |
| Azurite | $3 \mathrm{CuO} \cdot 2 \mathrm{CO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.730 | 1.758 | 1.838 |
| Scorodite | $\mathrm{Fe}_{2} \mathrm{O}_{3} \cdot \mathrm{As}_{2} \mathrm{O}_{5} \cdot 4 \mathrm{H}_{2} \mathrm{O}$ | 1.765 | 1.774 | 1.797 |

(continued)

TABLE 548.-INDEX OF REFRACTION OF SELECTED BIAXIAL MINERALS (continued)

Biaxial positive minerals (continued)

| Mineral | Formula | Index of $\underbrace{\text { refraction }}$ |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | na | ${ }^{n} \beta$ | ${ }^{7}$ |
| Olivenite | $4 \mathrm{CuO} \cdot \mathrm{As}_{2} \mathrm{O}_{6} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.772 | 1.810 | 1.863 |
| Anglesite | $\mathrm{PbO} \cdot \mathrm{SO}_{3}$ | 1.877 | 1.882 | 1.894 |
| Titanite | $\mathrm{CaO} \cdot \mathrm{TiO}_{2} \cdot \mathrm{SiO}_{2}$ | 1.900 | 1.907 | 2.034 |
| Claudetite | $\mathrm{As}_{2} \mathrm{O}{ }_{3}$ | 1.871 | 1.920 | 2.010 |
| Sulfur | S | 1.950 | 2.043 | 2.240 |
| Cotunnite | $\mathrm{PbCl}_{2}$ | 2.200 | 2.217 | 2.260 |
| Huebnerite | $\mathrm{MnO} \cdot \mathrm{WO}_{3}$ | 2.170 | 2.220 | 2.320 |
| Manganite | $\mathrm{Mn}_{2} \mathrm{O}_{3} \cdot \mathrm{H}_{2} \mathrm{O}$ | 2.240 | 2.240 | 2.530 (Li) |
| Raspite | $\mathrm{PbO} \cdot \mathrm{WO}_{3}$ | 2.270 | 2.270 | 2.300 |
| Mendipite | $2 \mathrm{PbO} \cdot \mathrm{PbCl} 2_{2}$ | 2.240 | 2.270 | 2.310 |
| Tantalite | $(\mathrm{Fe}, \mathrm{Mn}) \mathrm{O} \cdot \mathrm{Ta}_{2} \mathrm{O}_{3}$ | 2.260 | 2.320 | 2.430 (Li) |
| Wolframite | $(\mathrm{Fe}, \mathrm{Mn}) \mathrm{O} \cdot \mathrm{WO}_{3}$ | 2.310 | 2.360 | 2.460 (Li) |
| Crocoite | $\mathrm{PbO} \cdot \mathrm{CrO}_{3}$ | 2.310 | 2.370 | 2.660 (Li) |
| Pseudobrookite | $2 \mathrm{Fe}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{TiO}_{2}$ | 2.380 | 2.390 | 2.420 (Li) |
| Stibiotantalite | $\mathrm{Sb}_{2} \mathrm{O}_{3} \cdot \mathrm{Ta}_{2} \mathrm{O}_{3}$ | 2.374 | 2.404 | 2.457 |
| Montroydite | HgO | 2.370 | 2.500 | 2.650 (Li) |
| Brookite ... | $\mathrm{TiO}_{2}$ | 2.583 | 2.586 | 2.741 |
| Massicot | PbO | 2.510 | 2.610 | 2.710 |

Biaxial negative minerals

| Mirabilite | $\mathrm{Na}_{2} \mathrm{O} \cdot \mathrm{SO}_{3} \cdot 10 \mathrm{H}_{2} \mathrm{O}$ | 1.394 | 1.396 | 1.398 |
| :---: | :---: | :---: | :---: | :---: |
| Thomsenolite | $\mathrm{NaF} \cdot \mathrm{CaF}_{2} \cdot \mathrm{AlF}_{3} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.407 | 1.414 | 1.415 |
| Natron | $\mathrm{Na}_{2} \mathrm{O} \cdot \mathrm{CO}_{2} \cdot 10 \mathrm{H}_{2} \mathrm{O}$ | 1.405 | 1.425 | 1.440 |
| Kalinite | $\mathrm{K}_{2} \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 4 \mathrm{SO}_{3} \cdot 24 \mathrm{H}_{2} \mathrm{O}$ | 1.430 | 1.452 | 1.458 |
| Epsomite | $\mathrm{MgO} \cdot \mathrm{SO}_{3} \cdot 7 \mathrm{H}_{2} \mathrm{O}$ | 1.433 | 1.455 | 1.461 |
| Sassolite | $\mathrm{B}_{2} \mathrm{O}_{3} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.340 | 1.456 | 1.459 |
| Borax | $\mathrm{Na}_{2} \mathrm{O} \cdot 2 \mathrm{~B}_{2} \mathrm{O}_{3} \cdot 10 \mathrm{H}_{2} \mathrm{O}$ | 1.447 | 1.470 | 1.472 |
| Goslarite | $\mathrm{ZnO} \cdot \mathrm{SO}_{3} \cdot 7 \mathrm{H}_{2} \mathrm{O}$ | 1.457 | 1.480 | 1.484 |
| Pickeringite | $\mathrm{MgO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 4 \mathrm{SO}_{3} \cdot 22 \mathrm{H}_{2} \mathrm{O}$ | 1.476 | 1.480 | 1.483 |
| Bloedite | $\mathrm{Na}_{2} \mathrm{O} \cdot \mathrm{MgO} \cdot 2 \mathrm{SO}_{3} \cdot 4 \mathrm{H}_{2} \mathrm{O}$ | 1.483 | 1.487 | 1.486 |
| Trona | $3 \mathrm{Na}_{2} \mathrm{O} \cdot 4 \mathrm{CO}_{2} \cdot 5 \mathrm{H}_{2} \mathrm{O}$ | 1.410 | 1.492 | 1.542 |
| Thermonatrite | $\mathrm{Na}_{2} \mathrm{O} \cdot \mathrm{CO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.420 | 1.495 | 1.518 |
| Stilbite | $\left(\mathrm{Ca}, \mathrm{Na}_{2}\right) \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2} \cdot 5 \mathrm{H}_{2} \mathrm{O}$ | 1.494 | 1.498 | 1.500 |
| Niter | $\mathrm{K}_{2} \mathrm{O} \cdot \mathrm{N}_{2} \mathrm{O}_{3}$ | 1.334 | 1.505 | 1.506 |
| Kainite | $\mathrm{MgO} \cdot \mathrm{SO}_{3} \cdot \mathrm{KCl} \cdot 3 \mathrm{H}_{2} \mathrm{O}$ | 1.494 | 1.505 | 1.516 |
| Gaylussite | $\mathrm{Na} 2 \mathrm{O} \cdot \mathrm{CaO} \cdot 2 \mathrm{CO}_{2} \cdot 5 \mathrm{H}_{2} \mathrm{O}$ | 1.444 | 1.516 | 1.523 |
| Scolecite | $\mathrm{CaO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2} \cdot 3 \mathrm{H}_{2} \mathrm{O}$ | 1.512 | 1.519 | 1.519 |
| Laumontite | $\mathrm{CaO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 4 \mathrm{SiO}_{2} \cdot \mathrm{H}_{3} \mathrm{O}$ | 1.513 | 1.524 | 1.525 |
| Orthoclase | $\mathrm{K} 2 \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2}$ | 1.518 | 1.524 | 1.526 |
| Microcline | Same as preceding | 1.522 | 1.526 | 1.530 |
| Anorthoclase | ( $\mathrm{Na}, \mathrm{K})_{2} \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2}$ | 1.523 | 1.529 | 1.531 |
| Glauberite | $\mathrm{Na}_{2} \mathrm{O} \cdot \mathrm{CaO} \cdot 2 \mathrm{SO}_{3}$ | 1.515 | 1.532 | 1.536 |
| Cordierite | $4(\mathrm{Mg}, \mathrm{Fe}) \mathrm{O} \cdot 4 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 10 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.534 | 1.538 | 1.540 |
| Chalcanthite | $\mathrm{CuO} \cdot \mathrm{SO}_{3} \cdot 5 \mathrm{H}_{2} \mathrm{O}$ | 1.516 | 1.539 | 1.546 |
| Oligoclase | $\mathrm{Ab}_{4} \mathrm{An}$ | 1.539 | 1.543 | 1.547 |
| Beryllonite | $\mathrm{Na}_{2} \mathrm{O} \cdot 2 \mathrm{BeO} \cdot \mathrm{P}_{2} \mathrm{O}_{3}$ | 1.552 | 1.558 | 1.561 |
| Kaolinite | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot 2 \mathrm{SiO}_{2} \cdot 2 \mathrm{H}_{2} \mathrm{O}$ | 1.561 | 1.563 | 1.565 |
| Biotite.. | $\mathrm{K}_{2} \mathrm{O} \cdot 4(\mathrm{Mg}, \mathrm{Fe}) \mathrm{O} \cdot 2 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.541 | 1.574 | 1.574 |
| Autunite | $\mathrm{CaO} \cdot 2 \mathrm{UO}_{3} \cdot \mathrm{P}_{2} \mathrm{O}_{5} \cdot 8 \mathrm{H}_{2} \mathrm{O}$ | 1.553 | 1.575 | 1.577 |
| Anorthite | $" \mathrm{An} "=\mathrm{CaO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 2 \mathrm{SiO}_{2}$ | 1.576 | 1.584 | 1.588 |
| Lanthanite | $\mathrm{La}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{CO}_{2} \cdot 9 \mathrm{H}_{2} \mathrm{O}$ | 1.520 | 1.587 | 1.613 |
| Pyrophyllite | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot 4 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.552 | 1.588 | 1.600 |
| Talc | $3 \mathrm{MgO} \cdot 4 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.539 | 1.589 | 1.589 |
| Hopeite | $3 \mathrm{ZnO} \cdot \mathrm{P}_{2} \mathrm{O}_{5} \cdot 4 \mathrm{H}_{2} \mathrm{O}$ | 1.572 | 1.590 | 1.590 |
| Muscovite | $\mathrm{K}_{2} \mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2} \cdot 2 \mathrm{H}_{2} \mathrm{O}$ | 1.561 | 1.590 | 1.594 |
| Amblygonite | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{P}_{2} \mathrm{O}_{5} \cdot 2 \mathrm{LiF}$ | 1.579 | 1.593 | 1.597 |
| Lepidolite | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{SiO}_{2} \cdot 2(\mathrm{~K}, \mathrm{Li}) \mathrm{F}$ | 1.560 | 1.598 | 1.605 |
| Phlogopite | $\mathrm{K} 2 \mathrm{O} \cdot 6 \mathrm{MgO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2} \cdot 2 \mathrm{H}_{2} \mathrm{O}$ | 1.562 | 1.606 | 1.606 |
| Tremolite | $\mathrm{CaO} \cdot 3 \mathrm{MgO} \cdot 4 \mathrm{SiO}_{2}$ | 1.600 | 1.616 | 1.627 |

Biaxial negative minerals (continued)

|  |  | Index of ${ }^{\text {refraction }}$ |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Mineral | Formula | na | n $\beta$ | ny |
| Actinolite | $\mathrm{CaO} \cdot 3(\mathrm{Mg}, \mathrm{Fe}) \mathrm{O} \cdot 4 \mathrm{SiO}_{2}$ | 1.614 | 1.630 | 1.641 |
| Wollastonite | $\mathrm{CaO} \cdot \mathrm{SiO}_{2}$ | 1.620 | 1.632 | 1.634 |
| Lazulite | ( $\mathrm{Fe}, \mathrm{Mg}$ ) $\mathrm{O} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{P}_{2} \mathrm{O}_{5} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.612 | 1.634 | 1.643 |
| Danburite | $\mathrm{CaO} \cdot \mathrm{B}_{2} \mathrm{O}_{3} \cdot 2 \mathrm{SiO}_{2}$ | 1.632 | 1.634 | 1.636 |
| Glaucophane | $\mathrm{Na}_{2} \mathrm{O} \cdot 2 \mathrm{FeO} \cdot \mathrm{Al}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2}$ | 1.621 | 1.638 | 1.638 |
| Andalusite | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{SiO}_{2}$ | 1.632 | 1.638 | 1.643 |
| Hornblende | Contains $\mathrm{Na}_{2} \mathrm{O}, \mathrm{MgO}, \mathrm{FeO}, \mathrm{SiO}_{2}$, etc. | 1.634 | 1.647 | 1.652 |
| Datolite | $2 \mathrm{CaO} \cdot 2 \mathrm{SiO}_{2} \cdot \mathrm{~B}_{2} \mathrm{O}_{3} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.625 | 1.653 | 1.669 |
| Erythrite | $3 \mathrm{CoO} \cdot \mathrm{As}_{2} \mathrm{O}_{5} \cdot 8 \mathrm{H}_{2} \mathrm{O}$ | 1.626 | 1.661 | 1.699 |
| Monticellite | $\mathrm{CaO} \cdot \mathrm{MgO} \cdot \mathrm{SiO}_{2}$ | 1.651 | 1.662 | 1.668 |
| Strontianite | $\mathrm{SrO} \cdot \mathrm{CO}_{2}$ | 1.520 | 1.667 | 1.667 |
| Witherite | $\mathrm{BaO} \cdot \mathrm{CO}_{2}$ | 1.529 | 1.676 | 1.677 |
| Aragonite | $\mathrm{CaO} \cdot \mathrm{CO}_{2}$ | 1.531 | 1.682 | 1.686 |
| Axinite . | $6(\mathrm{Ca}, \mathrm{Mn}) \mathrm{O} \cdot 2 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{~B}_{2} \mathrm{O}_{3} \cdot 8 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.678 | 1.685 | 1.688 |
| Dumortierite | $8 \mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{~B}_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.678 | 1.686 | 1.689 |
| Cyanite | $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot \mathrm{SiO}_{2}$ | 1.712 | 1.720 | 1.728 |
| Epidote | $4 \mathrm{CaO} \cdot 3(\mathrm{Al}, \mathrm{Fe})_{2} \mathrm{O}_{3} \cdot 6 \mathrm{SiO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.729 | 1.763 | 1.780 |
| Atacamite | $3 \mathrm{CuO} \cdot \mathrm{CuCl}_{2} \cdot 3 \mathrm{H}_{2} \mathrm{O}$ | 1.831 | 1.861 | 1.880 |
| Fayalite | $2 \mathrm{FeO} \cdot \mathrm{SiO}_{2}$ | 1.824 | 1.864 | 1.874 |
| Caledonite | $2(\mathrm{~Pb}, \mathrm{Cu}) \mathrm{O} \cdot \mathrm{SO}_{3} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.818 | 1.866 | 1.909 |
| Malachite | $2 \mathrm{CuO} \cdot \mathrm{CO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.655 | 1.875 | 1.909 |
| Lanarkite | $2 \mathrm{PbO} \cdot \mathrm{SO}_{3}$ | 1.930 | 1.990 | 2.020 |
| Leadhillite | $4 \mathrm{PbO} \cdot \mathrm{SO}_{3} \cdot 2 \mathrm{CO}_{2} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.870 | 2.000 | 2.010 |
| Cerusite | $\mathrm{PbO} \cdot \mathrm{CO}_{2}$ | 1.804 | 2.076 | 2.078 |
| Laurionite | $\mathrm{PbCl}_{2} \cdot \mathrm{PbO} \cdot \mathrm{H}_{2} \mathrm{O}$ | 2.077 | 2.116 | 2.158 |
| Matlockite | $\mathrm{PbO} \cdot \mathrm{PbCl}_{2}$ | 2.040 | 2.150 | 2.150 |
| Baddeleyite | $\mathrm{ZrO}_{2}$ | 2.130 | 2.190 | 2.200 |
| Lepidocrocite | $\mathrm{Fe}_{2} \mathrm{O}_{3} \cdot \mathrm{H}_{2} \mathrm{O}$ | 1.930 | 2.210 | 2.510 |
| Limonite ... | $2 \mathrm{Fe}_{2} \mathrm{O}_{3} \cdot 3 \mathrm{H}_{2} \mathrm{O}$ in part | 2.170 | 2.290 | 2.310 |
| Goethite | $\mathrm{Fe}_{2} \mathrm{O}_{3} \cdot \mathrm{H}_{2} \mathrm{O}$ | 2.210 | 2.350 | $2.350(\mathrm{Li})$ |
| Valentinite | $\mathrm{Sb}_{2} \mathrm{O}_{3}$ | 2.180 | 2.350 | 2.350 |
| Turgite | $2 \mathrm{Fe}_{2} \mathrm{O}_{3} \cdot \mathrm{H}_{2} \mathrm{O}$ in part | 2.450 | 2.550 | $2.550(\mathrm{Li})$ |
| Realgar | AsS | 2.460 | 2.590 | 2.610 (Li) |
| Terlinguaite | $\mathrm{Hg}_{2} \mathrm{OCl}$ | 2.350 | 2.640 | 2.660 (Li) |
| Hutchinsonite | $(\mathrm{Tl}, \mathrm{Ag})_{2} \mathrm{~S} \cdot \mathrm{PbS} \cdot 2 \mathrm{As}_{2} \mathrm{~S}_{3}$ | 3.078 | 3.176 | 3.188 |
| Stibnite | $\mathrm{Sb}_{2} \mathrm{~S}_{3}$ | 3.194 | 4.303 | 4.460 |


| Crystal | Spectrum line | Index of refraction |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | $n^{2}$ | $n \beta$ | ${ }^{n} \gamma$ |
| Ammonium oxalate, $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{C}_{2} \mathrm{O}_{4} \cdot \mathrm{H}_{2} \mathrm{O}$. | D | 1.4381 | 1.5475 | 1.5950 |
| Ammonium acid tartrate, $\left(\mathrm{NH}_{4}\right) \mathrm{H}\left(\mathrm{C}_{4} \mathrm{H}_{4} \mathrm{O}_{6}\right)$ | D | 1.5188 | 1.5614 | 1.5910 |
| Ammonium tartrate, $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{C}_{4} \mathrm{H}_{4} \mathrm{O}_{6}$ | D | - | 1.581 | - |
| Antipyrin, $\mathrm{CuH}_{12} \mathrm{NO}_{2}$ | D | 1.5697 | 1.6935 | 1.7324 |
| Citric acid, $\mathrm{C}_{6} \mathrm{H}_{8} \mathrm{O}_{7} \cdot \mathrm{H}_{2} \mathrm{O}$ | D | 1.4932 | 1.4977 | 1.5089 |
| Codein, $\mathrm{C}_{18} \mathrm{H}_{21} \mathrm{NO}_{3} \cdot \mathrm{H}_{2} \mathrm{O}$ | D | 1.5390 | 1.5435 | - |
| Magnesium carbonate, $\mathrm{MgCO}_{3} \cdot 3 \mathrm{H}_{2} \mathrm{O}$. | D | 1.495 | 1.501 | 1.526 |
| " sulfate, $\mathrm{MgSO}_{4} \cdot 7 \mathrm{H}_{2} \mathrm{O} \ldots$ | D | 1.432 | 1.455 | 1.461 |
| "، " | Cd, . $226 \mu$ | 1.4990 | 1.5266 | 1.5326 |
| " " ........... | H, . $656 \mu$ | 1.4307 | 1.4532 | 1.4584 |
| Potassium bichromate, $\mathrm{K}_{2} \mathrm{Cr}_{2} \mathrm{O}_{7}$ | D | 1.7202 | 1.7380 | 1.8197 |
| " chromate, $\mathrm{K}_{2} \mathrm{CrO}_{4}$ | D | 1.683 | 1.7254 | - |
| " " | red | 1.6873 | 1.722 | 1.7305 |
| " nitrate, $\mathrm{KNO}_{3}$ | D | 1.3346 | 1.5056 | 1.5064 |
| " sulfate, $\mathrm{K}_{2} \mathrm{SO}_{4}$ | F | 1.4976 | 1.4992 | 1.5029 |
| " ${ }^{\text {de, }}$ | D | 1.4932 | 1.4946 | 1.4980 |
| " " $\ldots$...... | C | 1.4911 | 1.4928 | 1.4959 |
| Racemic acid, $\mathrm{C}_{4} \mathrm{H}_{6} \mathrm{O}_{6} \cdot \mathrm{H}_{2} \mathrm{O}$ | yellow | - | 1.526 | - |
| Resorcin, $\mathrm{C}_{6} \mathrm{H}_{8} \mathrm{O}_{2}$ | D | 661 | 1.555 | - |
| Sodium bichromate, $\mathrm{Na}_{2} \mathrm{Cr}_{2} \mathrm{O}_{7} \cdot 2 \mathrm{H}_{2} \mathrm{O}$.. | D | 1.6610 | 1.6994 | 1.7510 |
| " acid tartrate, $\mathrm{NaH}\left(\mathrm{C}_{4} \mathrm{H}_{4} \mathrm{O}_{6}\right) \cdot 2 \mathrm{H}$ | red | 1.5122 | 1.5332 | - |
| Sugar (cane), $\mathrm{C}_{12} \mathrm{H}_{22} \mathrm{O}_{11}$. | T1 | 1.5422 | 1.5685 | 1.5734 |
|  | D | 1.5397 | 1.5667 | 1.5716 |
| - | Li | 1.5379 | 1.5639 | 1.5693 |
| Tartaric acid, $\mathrm{C}_{4} \mathrm{H}_{4} \mathrm{O}_{6}$ (right-) | D | 1.4953 | 1.5353 | 1.6046 |
| Zinc sulfate, $\mathrm{ZnSO}_{4} \cdot 7 \mathrm{H}_{2} \mathrm{O}$. | F | 1.4620 | 1.4860 | 1.4897 |
| " " | D | 1.4568 | 1.4801 | 1.4836 |
| " | C | 1.4544 | 1.4776 | 1.4812 |

TABLE 550.-SPECIFIC GRAVITY, COEFFICIENT OF EXPANSION, AND STAIN CLASS OF OPTICAL GLASS *

| Glass type | Specific gravity |  | Cofficient of expansion mean values $\times 10^{7}$ |  |  |  | Stain class for $B L$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $B L$ | $C G$ | $-40^{\circ}$ to $0^{\circ}$ | $0^{\circ}$ to $40^{\circ}$ | $0^{\circ}$ to $100^{\circ}$ | $0^{\circ}$ to $300^{\circ}$ |  |
|  |  |  | BL | $B L$ | BL | $C G$ |  |
| 511635 | 2.48 |  | 73.0 | 77.0 | 79.6 |  | 1 |
| 517645 | 2.53 | 2.53 | 62.0 | 65.2 | 67.5 | 80 | 1 |
| 523586 | 2.53 | ... | 75.8 | 80.2 | 83.0 | . . | 1 |
| 529516 | 2.73 | . . | 70.2 | 73.0 | 74.5 | . | 1 |
| 573574 | 3.21 |  | 74.2 | 78.0 | 80.0 |  | 3 |
| 580410 | 3.27 | 3.21 |  |  |  | 99 | 1 |
| 584460 | 3.31 |  | 76.2 | 80.0 | 81.9 |  | 1 |
| 605381 | 3.49 | 3.47 |  |  |  | 86 | 1 |
| 611572 | 3.57 | 3.56 | 57.8 | 61.2 | 64.1 | 70 | 5 |
| 611588 | 3.58 | 3.40 | 60.8 | 64.0 | 66.9 | 71 | 5 |
| 617366 | 3.64 | 3.58 | 70.8 | 73.0 | 74.2 | 89 | 1 |
| 617550 | 3.66 | 3.50 | ... | . | . . . | 72 | 5 |
| 620362 | 3.67 | 3.61 | ... | . . | . . | 87 | 1 |
| 649338 | 3.91 | 3.89 |  |  |  | 85 | 2 |
| 720293 | 4.51 |  | 73.5 | 75.2 | 77.3 |  | 3 |
| Melt No. |  |  |  |  |  |  |  |
| EK-110-5328 |  | 4.1 | 58.0 | 61.2 | 63.5 |  |  |
| EK-32-2641 |  | 4.5 | 57.8 | 61.2 | 63.9 | $\ldots$ |  |
| EK-33-2734s |  | 4.7 | 53.5 | 57.0 | 59.4 | . . |  |
| EK-45-29 |  | 4.6 | 57.0 | 60.5 | 63.4 | . . |  |

$B L$, Bausch \& Lomb Optical glass. EK, Eastman Kodak glass. $C G$ Corning glass.
The first 15 glass types in column I are described in Table 524 of NBS glasses.

[^213]SMITHSONIAN PHYSICAL TABLES

TABLE 551.-INDEX OF REFRACTION OF SOME LIQUIDS RELATIVE TO AIR

| Substance | Density | ${ }^{\text {Temp }} \mathrm{C}$ | Indices of refraction |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | ${ }_{H}^{0.397 \mu}$ | $\stackrel{0.434 \mu}{G^{\prime}}$ | $\underset{F}{0.486 \mu}$ | $0.589 \mu$ | ${ }^{0.656 \mu}$ |
| Acetaldehyde, $\mathrm{CH}_{3} \mathrm{CHO}$ | . 780 | 20 | - | 1.3394 | 1.3359 | 1.3316 | 1.3298 |
| Acetone, $\mathrm{CH}_{3} \mathrm{COCH}_{3}$ | . 791 | 20 | - | 1.3678 | 1.3639 | 1.3593 | 1.3573 |
| Aniline, $\mathrm{C}_{6} \mathrm{H}_{5} \cdot \mathrm{NH}_{2}$ | 1.022 | 20 |  | 1.6204 | 1.6041 | 1.5863 | 1.5793 |
| Alcohol, methyl, $\mathrm{CH}_{3} \cdot \mathrm{OH}$ | . 794 | 20 | 1.3399 | 1.3362 | 1.3331 | 1.3290 | 1.3277 |
| ". ethyl, $\mathrm{C}_{2} \mathrm{H}_{6} \cdot \mathrm{OH}$ | . 808 | 0 |  | 1.3773 | 1.3739 | 1.3695 | 1.3677 |
|  | . 800 | 20 |  | 1.3700 | 1.3666 | 1.3618 | 1.3605 |
| " $d n / d t$ |  | 20 | - | -. 0004 | -. 0004 | -. 0004 | -. 0004 |
| " n-propyl $\mathrm{C}_{3} \mathrm{H}_{7} \cdot \mathrm{OH}$ | . 804 | 20 | - | 1.3938 | 1.3901 | 1.3854 | 1.3834 |
| Benzene, $\mathrm{C}_{0} \mathrm{H}_{0}$ | . 880 | 20 |  | 1.5236 | 1.5132 | 1.5012 | 1.4965 |
| " $\mathrm{C}_{6} \mathrm{H}_{6} d n / d t$ |  | 20 |  | -. 0007 | -. 00006 | -. 0006 | -. 0006 |
| Bromnaphthalene, $\mathrm{C}_{10} \mathrm{H}_{7} \mathrm{Br}$ | 1.487 | 20 | 1.7289 | 1.7041 | 1.6819 | 1.6582 | 1.6495 |
| Carbon disulfide, $\mathrm{CS}_{2}$ | 1.293 | 0 | 1.7175 | 1.6920 | 1.6688 | 1.6433 | 1.6336 |
| " " $\quad$........ | 1.263 | 20 | 1.6994 | 1.6748 | 1.6523 | 1.6276 | 1.6182 |
| " tetrachloride, CC | 1.591 | 20 |  | 1.4729 | 1.4676 | 1.4607 | 1.4579 |
| Chinolin, $\mathrm{C}_{5} \mathrm{H}_{7} \mathrm{~N}$ | 1.090 | 20 | - | 1.6679 | 1.6470 | 1.6245 | 1.6161 |
| Chloral, $\mathrm{CCl}_{3} \cdot \mathrm{CHO}$ | 1.512 | 20 | - | 1.4679 | 1.4624 | 1.4557 | 1.4530 |
| Chloroform, $\mathrm{CHCl}_{3}$ | 1.489 | 20 | 1.463 | 1.458 | 1.4530 | 1.4467 | 1.4443 |
| Decane, $\mathrm{C}_{10} \mathrm{H}_{22}$ | . 728 | 14.9 | - | 1.4200 | 1.4160 | 1.4108 | 1.4088 |
| Ether, ethyl, $\mathrm{C}_{2} \mathrm{H}_{5} \cdot \mathrm{O}$ | . 715 | 20 | - | 1.3607 | 1.3576 | 1.3538 | 1.3515 |
| " " ${ }^{\text {c }} d n / d t$ |  | 20 |  | -. 0006 | -. 0000 | -. 0006 | -. 0006 |
| Ethyl nitrate, $\mathrm{C}_{2} \mathrm{H}_{5} \cdot \mathrm{O} \cdot \mathrm{NO}_{3}$ | 1.109 | 20 | - | 1.395 | 1.392 | 1.3853 | 1.3830 |
| Formic acid, $\mathrm{H} \cdot \mathrm{CO}_{2} \mathrm{H}$ | 1.219 | 20 | - | 1.3804 | 1.3764 | 1.3714 | 1.3693 |
| Glycerine, $\mathrm{C}_{3} \mathrm{H}_{8} \mathrm{O}_{3}$ | 1.260 | 20 | - | 1.4828 | 1.4784 | 1.4730 | 1.4706 |
| Hexane, $\mathrm{CH}_{3}\left(\mathrm{CH}_{2}\right) 4 \mathrm{CH}$ | . 660 | 20 | - | 1.3836 | 1.3799 | 1.3754 | 1.3734 |
| Hexylene, $\mathrm{CH}_{3}\left(\mathrm{CH}_{2}\right)_{3} \mathrm{CH} \cdot \mathrm{C}$ | . 679 | 23.3 |  | 1.4059 | 1.4007 | 1.3945 | 1.3920 |
| Methylene iodide $\mathrm{CH}_{2} \mathrm{I}_{2}$. | 3.318 | 20 | 1.8027 |  | 1.7692 | 1.7417 | 1.7320 |
| " " dn/dt |  | 20 |  |  | $-.0007$ | -. 0007 | -. 0006 |
| Naphthalene, $\mathrm{C}_{10} \mathrm{H}_{8}$ | . 962 | 98.4 | - | - | 1.6031 | 1.5823 | 1.5746 |
| Nicotine, $\mathrm{C}_{10} \mathrm{H}_{14} \mathrm{~N}_{2}$ | 1.012 | 22.4 | - | 1.5439 |  | 1.5239 | 1.5198 |
| Octane, $\mathrm{CH}_{3}\left(\mathrm{CH}_{2}\right)_{6} \mathrm{CH}_{3}$ | . 707 | 15.1 | - | 1.4097 | 1.4046 | 1.4007 | 1.3987 |
| Oil, almond | . 92 | 0 |  | - | 1.4847 | 1.4782 | 1.4755 |
| anise seed | . 99 | 15.1 | 1.6084 | - | 1.5743 | 1.5572 | 1.5508 |
|  | . 99 | 21.4 |  |  | 1.5647 | 1.5475 | 1.5410 |
| bitter almond | 1.05 | 20 | - | 1.5775 | 1.5623 | - | 1.5391 |
| cassia |  | 10 | 1.7039 | - | 1.6389 | 1.6104 | 1.6007 |
|  |  | 22.5 | 1.6985 | - | 1.6314 | 1.6026 | 1.5930 |
| cinnamon | 1.05 | 23.5 | - | - | 1.6508 | 1.6188 | 1.6077 |
| olive | . 92 | 0 |  |  | 1.4825 | 1.4763 | 1.4738 |
| rock |  | 0 |  | - | 1.4644 | 1.4573 | 1.4545 |
| turpentine | . 87 | 10.6 | 1.4939 | - | 1.4817 | 1.4744 | 1.4715 |
|  | . 87 | 20.7 | 1.4913 |  | 1.4793 | 1.4721 | 1.4692 |
| Pentane, $\mathrm{CH}_{3}\left(\mathrm{CH}_{2}\right)_{3} \mathrm{CH}_{3}$ | . 625 | 15.7 | - | 1.3645 | 1.3610 | 1.3581 | 1.3570 |
| Phenol, $\mathrm{C}_{6} \mathrm{H}_{5} \mathrm{OH}$ | 1.060 | 40.6 | - | 1.5684 | 1.5558 | 1.5425 | 1.5369 |
|  | 1.021 | 82.7 |  |  | 1.5356 | 5 | 1.5174 |
| Styrene, $\mathrm{C}_{6} \mathrm{H}_{5} \mathrm{CH} \cdot \mathrm{CH}_{2}$ | . 982 | 16.6 |  | 1.5816 | 1.5659 | 1.5485 | 1.5419 |
| $\stackrel{\text { Thymol, } \mathrm{C}_{10} \mathrm{H}_{14} \mathrm{O}}{\text { Toluene, } \mathrm{CH}_{3}{ }^{\text {C }} \mathrm{C}_{6} \mathrm{H}_{6}}$ | . 88 |  |  |  | 1.5386 |  | 1.5228 |
| Toluene, $\mathrm{CH}_{3} \cdot \mathrm{C}_{6} \mathrm{H}_{6}$ | . 86 | 20 |  | 1.5170 | 1.5070 | 1.4955 | 1.4911 |
| Water, $\mathrm{H}_{2} \mathrm{O}$ | - | 20 | 1.3435 | 1.3404 | 1.3372 | 1.3330 | 1.3312 |
|  | - | 0 | 1.3444 | 1.3413 | 1.3380 | 1.3338 | 1.3319 |
| " |  | 40 | 1.3411 | 1.3380 | 1.3349 | 1.3307 | 1.3290 |
| " | - | 80 | 1.3332 | 1.3302 | 1.3270 | 1.3230 | 1.3213 |

TABLE 552.-INDICES OF REFRACTION FOR SOLUTIONS OF SALTS AND ACIDS RELATIVE TO AIR

| Substance | Density | ${ }^{\text {Temp }}{ }^{\circ} \mathrm{C}$ | Indices of refraction for spectrum lines |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | C | D | F | $\mathbf{H}_{\gamma}$ | H |
| Solutions in water |  |  |  |  |  |  |  |
| Ammonium chloride | 1.067 | 27.05 | 1.37703 | 1.37936 | 1.38473 | - | 1.39336 |
|  | . 025 | 29.75 | . 34850 | . 35050 | . 35515 | - | . 36243 |
| Calcium chloride | . 398 | 25.65 | . 44000 | . 44279 | . 44938 | - | . 46001 |
| " ${ }^{\text {" }}$ | . 215 | 22.9 | . 39411 | . 39652 | . 40206 | - | . 41078 |
| " | . 143 | 25.8 | . 37152 | . 37369 | . 37876 | - | . 38666 |
| Hydrochloric acid | 1.166 | 20.75 | 1.40817 | 1.41109 | 1.41774 | - | 1.42816 |
| Nitric acid | . 359 | 18.75 | . 39893 | . 40181 | . 40857 | - | . 41961 |
| Potash (caustic) | . 416 | 11.0 | . 40052 | . 40281 | . 40808 | - | . 41637 |
| Potassium chloride | normal | lution | . 34087 | . 34278 | . 34719 | 1.35049 | - |
| " ${ }^{\text {c }}$ | double | ormal | . 34982 | . 35179 | . 35645 | . 35994 | - |
| " | triple | rmal | . 35831 | . 36029 | . 36512 | . 36890 | - |
| Soda (caustic) | 1.376 | 21.6 | 1.41071 | 1.41334 | 1.41936 | - | 1.42872 |
| Sodium chloride | . 189 | 18.07 | . 37562 | . 37789 | . 38322 | 1.38746 | - |
| " ${ }^{\text {a }}$ | . 109 | 18.07 | . 35751 | . 35959 | . 36442 | . 36823 | - |
| " " | . 035 | 18.07 | . 34000 | . 34191 | . 34628 | . 34969 | - |
| Sodium nitrate | 1.358 | 22.8 | 1.38283 | 1.38535 | 1.39134 | - | 1.40121 |
| Sulfuric acid | . 811 | 18.3 | . 43444 | . 43669 | . 44168 | - | . 44883 |
| " ${ }^{\text {" }}$ | . 632 | 18.3 | . 42227 | . 42466 | . 42967 | - | . 43694 |
| " " | . 221 | 18.3 | . 36793 | . 37009 | . 37468 | - | . 38158 |
| " " | . 028 | 18.3 | . 33663 | . 33862 | . 34285 | - | . 34938 |
| Zinc chloride | 1.359 | 26.6 | 1.39977 | 1.40222 | 1.40797 | - | 1.41738 |
| " ${ }^{\text {a }}$ | . 209 | 26.4 | . 37292 | . 37515 | . 38026 | - | . 38845 |
| Solutions in ethyl alcohol |  |  |  |  |  |  |  |
| Ethyl alcohol | . 789 | 25.5 | 1.35971 | 1.35971 | 1.36395 | - | 1.37094 |
|  | . 932 | 27.6 | . 35372 | . 35556 | . 35986 | - | . 36662 |
| Fuchsin (nearly satur | - | 16.0 | . 3918 | . 398 | . 361 | - | . 3759 |
| Cyanin (saturated) . | - | 16.0 | . 3831 | - | . 3705 | - | . 3821 |

Note.-Cyanin in chloroform also acts anomalously; for example, Sieben gives for a 4.5 percent solution $\mu_{A}=1.4593, \mu_{B}=1.4695, \mu_{F}$ (green) $=1.4514, \mu_{G}$ (blue) $=1.4554$. For a 9.9 percent solution he gives $\mu_{A}=1.4902, \mu_{F}$ (green) $=1.4497, \mu_{G}($ blue $)=1.4597$.

Solutions of potassium permanganate in water

| $\begin{aligned} & \stackrel{5}{5} \\ & \stackrel{0}{0} 5 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ |  |  |  |  |  | $\begin{aligned} & \stackrel{y}{5} \\ & \text { E } \\ & \stackrel{1}{0} \\ & \stackrel{y}{0} \\ & 3 \end{aligned}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . $687 \mu$ | B | 1.3328 | 1.3342 | - | 1.3382 | . $516 \mu$ | - | 1.3368 | 1.3385 | - | - |
| . 656 | C | . 3335 | . 3348 | 1.3365 | . 3391 | . 500 | - | . 3374 | . 3383 | 1.3386 | 1.3404 |
| . 617 | - | . 3343 | . 3365 | . 3381 | . 3410 | . 486 | F | . 3377 | - | - | . 3408 |
| . 594 | - | . 3354 | . 3373 | . 3393 | . 3426 | . 480 | - | . 3381 | . 3395 | . 3398 | . 3413 |
| . 589 | D | . 3353 | . 3372 | - | . 3426 | . 464 | - | . 3397 | . 3402 | . 3414 | . 3423 |
| . 568 | - | . 3362 | . 3387 | . 3412 | . 3445 | . 447 | - | . 3407 | . 3421 | . 3426 | . 3439 |
| . 553 | - | . 3366 | . 3395 | . 3417 | . 3438 | . 434 | - | . 3417 | - | - | . 3452 |
| . 527 | E | . 3363 | - | - | - | . 423 | - | . 3431 | . 3442 | . 3457 | . 3468 |
| . 522 | - | . 3362 | . 3377 | . 3388 |  | - | - | - | - | - | $\rightarrow$ |

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 TABLE 553.-INDEX OF REFRACTION OF AIR $\left(15^{\circ} \mathrm{C}, 76 \mathrm{cmHg}\right)$Corrections for reducing wavelengths and frequencies in air ( $15^{\circ} \mathrm{C}, 76 \mathrm{cmHg}$ ) to vacuo
The indices were computed from the Cauchy formula $(n-1) 10^{7}=2726.43+12.288 /\left(\lambda^{2} \times\right.$ $\left.10^{-8}\right)+0.3555 /\left(\lambda^{4} \times 10^{-16}\right)$. For $0^{\circ} \mathrm{C}$ and 76 cmHg the constants of the equation become 2875.66, 13.412 and 0.3777 respectively, and for $30^{\circ} \mathrm{C}$ and $76 \mathrm{cmHg} 2589.72,12.259$ and 0.2576 . Sellmeier's formula for but one absorption band closely fits the observations: $n^{2}=1+0.00057378 \lambda^{2} /\left(\lambda^{2}-\right.$ 595260). If $n-1$ were strictly proportional to the density, then $(n-1)_{0} /(n-1) t$ would equal $1+$ at where a should be 0.00367 . The following values of $a$ were found to hold:

$$
\begin{array}{llllllll}
\lambda & 0.85 \mu & 0.75 \mu & 0.65 \mu & 0.55 \mu & 0.45 \mu & 0.35 \mu & 0.25 \mu \\
\alpha & 0.003672 & 0.003674 & 0.003678 & 0.003685 & 0.003700 & 0.003738 & 0.003872
\end{array}
$$

The indices are for dry air $\left(0.05 \pm \% \mathrm{CO}_{2}\right)$. Corrections to reduce to dry air the indices for moist air may be made for any wavelength by Lorenz's formula, $+0.000041(m / 760)$, where $m$ is the vapor pressure in mm. The corresponding frequencies in waves per cm and the corrections to reduce wavelengths and frequencies in air at $15^{\circ} \mathrm{C}$ and 76 cmHg pressure to vacuo are given. E.g., a light wave of 5000 angstroms in dry air at $15^{\circ} \mathrm{C}, 76 \mathrm{cmHg}$ becomes 5001.391 A in vacuo ; a frequency of 20,000 waves per cm correspondingly becomes 19994.44.

| $\begin{gathered} \text { Wave- } \\ \text { length, } \\ \text { ang- } \\ \text { antroms } \end{gathered}$ | $\begin{aligned} & \text { Dry air } \\ & (n-1) \\ & \left(x-10^{7}\right. \\ & 15^{\circ} \mathrm{C} \\ & 76^{\mathrm{cmHg}} \end{aligned}$ | $\begin{gathered} \text { Vacuo } \\ \text { correction } \\ \text { for in air } \\ (n \lambda-\lambda) \\ \text { add } \end{gathered}$ | $\begin{gathered} \text { Fre- } \\ \text { quency } \\ \text { waves per } \\ \text { cm } \\ \frac{1}{\lambda} \\ \text { in air } \end{gathered}$ | Vacuo correction for $\frac{1}{\lambda}$ in air $\left(\frac{1}{n \lambda}-\frac{1}{\lambda}\right)$ | Wave- length, ang. | $\begin{gathered} \text { Dry air } \\ (n-1) \\ \times 10^{7} \\ \times 15^{\circ} \mathrm{C} \\ 76 \mathrm{cmHg} \end{gathered}$ | $\begin{gathered} \text { Vacuo } \\ \text { correction } \\ \text { for } \lambda \text { in a arir } \\ (n \lambda-\lambda) \end{gathered}$ | $\begin{gathered} \begin{array}{c} \text { Fre- } \\ \text { quency } \\ \text { waves per } \\ \text { cm } \end{array} \\ \frac{1}{\lambda} \\ \text { in air } \end{gathered}$ | Vacuo correction for $\frac{1}{\lambda}$ in air $\left(\frac{1}{n \lambda}-\frac{1}{\lambda}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2000 | 3256 | . 651 | 50,000 | 16.27 | 5500 | 2771 | 1.524 | 18,181 | 5.04 |
| 2100 | 3188 | . 670 | 47,619 | 15.18 | 5600 | 2769 | 1.551 | 17,857 | 4.94 |
| 2200 | 3132 | . 689 | 45,454 | 14.23 | 5700 | 2768 | 1.578 | 17,543 | 4.85 |
| 2300 | 3086 | . 710 | 43,478 | 13.41 | 5800 | 2766 | 1.604 | 17,241 | 4.77 |
| 2400 | 3047 | . 731 | 41,666 | 12.69 | 5900 | 2765 | 1.631 | 16,949 | 4.68 |
| 2500 | 3014 | . 754 | 40,000 | 12.05 | 6000 | 2763 | 1.658 | 16,666 | 4.60 |
| 2600 | 2986 | . 776 | 38,461 | 11.48 | 6100 | 2762 | 1.685 | 16,393 | 4.53 |
| 2700 | 2962 | . 800 | 37,037 | 10.97 | 6200 | 2761 | 1.712 | 16,129 | 4.45 |
| 2800 | 2941 | . 824 | 35,714 | 10.50 | 6300 | 2760 | 1.739 | 15,873 | 4.38 |
| 2900 | 2923 | . 848 | 34,482 | 10.08 | 6400 | 2759 | 1.766 | 15,625 | 4.31 |
| 3000 | 2907 | . 872 | 33,333 | 9.69 | 6500 | 2758 | 1.792 | 15,384 | 4.24 |
| 3100 | 2893 | . 897 | 32,258 | 9.33 | 6600 | 2757 | 1.819 | 15,151 | 4.18 |
| 3200 | 2880 | . 922 | 31,250 | 9.00 | 6700 | 2756 | 1.846 | 14,925 | 4.11 |
| 3300 | 2869 | . 947 | 30,303 | 8.69 | 6800 | 2755 | 1.873 | 14,705 | 4.05 |
| 3400 | 2859 | . 972 | 29,411 | 8.41 | 6900 | 2754 | 1.900 | 14,492 | 3.99 |
| 3500 | 2850 | 998 | 28,571 | 8.14 | 7000 | 2753 | 1.927 | 14,285 | 3.93 |
| 3600 | 2842 | 1.023 | 27,777 | 7.89 | 7100 | 2752 | 1.954 | 14,084 | 3.88 |
| 3700 | 2835 | 1.049 | 27,027 | 7.66 | 7200 | 2751 | 1.981 | 13,888 | 3.82 |
| 3800 | 2829 | 1.075 | 26,315 | 7.44 | 7300 | 2751 | 2.008 | 13,698 | 3.77 |
| 3900 | 2823 | 1.101 | 25,641 | 7.24 | 7400 | 2750 | 2.035 | 13,513 | 3.72 |
| 4000 | 2817 | 1.127 | 25,000 | 7.04 | 7500 | 2749 | 2.062 | 13,333 | 3.66 |
| 4100 | 2812 | 1.153 | 24,390 | 6.86 | 7600 | 2749 | 2.089 | 13,157 | 3.62 |
| 4200 | 2808 | 1.179 | 23,809 | 6.68 | 7700 | 2748 | 2.116 | 12,987 | 3.57 |
| 4300 | 2803 | 1.205 | 23,255 | 6.52 | 7800 | 2748 | 2.143 | 12,820 | 3.52 |
| 4400 | 2799 | 1.232 | 22,727 | 6.36 | 7900 | 2747 | 2.170 | 12,658 | 3.48 |
| 4500 | 2796 | 1.258 | 22,222 | 6.21 | 8000 | 2746 | 2.197 | 12,500 | 3.43 |
| 4600 | 2792 | 1.284 | 21,739 | 6.07 | 8100 | 2746 | 2.224 | 12,345 | 3.39 |
| 4700 | 2789 | 1.311 | 21,276 | 5.93 | 8250 | 2745 | 2.265 | 12,121 | 3.33 |
| 4800 | 2786 | 1.338 | 20,833 | 5.80 | 8500 | 2744 | 2.332 | 11,764 | 3.23 |
| 4900 | 2784 | 1.364 | 20,406 | 5.68 | 8750 | 2743 | 2.400 | 11,428 | 3.13 |
| 5000 | 2781 | 1.391 | 20,000 | 5.56 | 9000 | 2742 | 2.468 | 11,111 | 3.05 |
| 5100 | 2779 | 1.417 | 19,607 | 5.45 | 9250 | 2741 | 2.536 | 10,810 | 2.96 |
| 5200 | 2777 | 1.444 | 19,230 | 5.34 | 9500 | 2740 | 2.604 | 10,526 | 2.88 |
| 5300 | 2775 | 1.471 | 18,867 | 5.23 | 9750 | 2740 | 2.671 | 10,256 | 2.81 |
| 5400 | 2773 | 1.497 | 18,518 | 5.13 | 10000 | 2739 | 2.739 | 10,000 | 2.74 |

A formula was given by Biot and Arago expressing the dependence of the index of refraction of a gas on pressure and temperature. More recent experiments confirm their conclusions. The formula is $n_{t}-1=\frac{n_{0}-1}{1+a t} \cdot \frac{p}{760}$, where $n_{t}$ is the index of refraction for temperature $t, n_{0}$ for temperature zero, a the coefficient of expansion of the gas with temperature, and $p$ the pressure of the gas in millimeters of mercury. For air see Table 553.

Indices of refraction

| Wave-length | $(n-1)^{10^{3}}$ |  |  |  | Wave-length $\mu$ | $(n-1)^{10^{3}}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Air | 0 | $N$ | H |  | Air | 0 | $N$ | H |
| $\mu$ |  |  |  |  |  |  |  |  |  |
| . 4861 | . 2951 | . 2734 | . 3012 | . 1406 | . 4360 | . 2971 | . 2743 | $\mathrm{CO}_{2}$ | . 1418 |
| . 5461 | . 2936 | . 2717 | . 2998 | . 1397 | . 5462 | . 2937 | . 2704 | .4506 | . 1397 |
| . 5790 | . 2930 | . 2710 |  | . 1393 | . 6709 | . 2918 | . 2683 | . 4471 | . 1385 |
| . 6563 | . 2919 | . 2698 | . 2982 | . 1387 | 6.709 | . 2881 | . 2643 | . 4804 | . 1361 |
|  |  |  |  |  | 8.678 | . 2888 | . 2650 | . 4579 | . 1361 |

The values are for $0^{\circ} \mathrm{C}$ and 760 mmHg

| Substance $\underset{\substack{\text { Kind of } \\ \text { light }}}{\text { d }}$ | Indices of refraction | Substance | Kind of light | Indices of refraction |
| :---: | :---: | :---: | :---: | :---: |
| Acetone ......... D | 1.001079-1.001100 | Hydrogen | white | 1.000138-1.000143 |
| Ammonia ........ white | $1.000381-1.000385$ |  | D | 1.000132 |
| D | 1.000373-1.000379 | en | D | 1.000644 |
| Argon ........... D | 1.000281 | gen | D | 1.000623 |
| Benzene ......... D | 1.001700-1.001823 | Methane | white | 1.000443 |
| Bromine . ....... D | 1.001132 |  | D | 1.000444 |
| Carbon dioxide ... white | 1.000449-1.000450 | Methyl alcohol | D | $1.000549-1.000623$ |
| D | 1.000448-1.000454 | Methyl ether | D | 1.000891 |
| Carbon disulfide. $\left\{\begin{array}{c}\text { white } \\ D\end{array}\right.$ | $\begin{aligned} & 1.001500 \\ & 1.001478-1.001485 \end{aligned}$ | Nitric oxide | white | $\begin{aligned} & 1.000303 \\ & 1.000297 \end{aligned}$ |
| Carbon monoxide $\left\{\begin{array}{l}\text { white } \\ \text { white }\end{array}\right.$ | 1.000340 | Nitrogen | white | 1.000295-1.000300 |
| Chlorine ......... white | 1.000772 | Nitrous | white | 1.000296-1.000298 |
| " | 1.000773 |  | D | 1.000516 |
| Chloroform ...... D | 1.001436-1.001464 | Oxygen | white | 1.000272-1.000280 |
| Cyanogen ........ white | 1.000834 | " . | D | 1.000271-1.000272 |
| D | 1.000784-1.000825 | Pentane | D | 1.001711 |
| Ethyl alcohol .... D | 1.000871-1.000885 | Sulfur dioxide | white | 1.000665 |
| Ethyl ether ...... D | 1.001521-1.001544 |  | D | 1.000686 |
| Helium .......... D | 1.000036 | Water | white | 1.000261 |
| $\begin{gathered} \text { Hydrochloric } \\ \text { acid } \ldots \ldots \ldots . \end{gathered}\left\{\begin{array}{c} \text { white } \\ \mathrm{D} \end{array}\right.$ | $\begin{aligned} & 1.000449 \\ & 1.000447 \end{aligned}$ | " | D | 1.000249-1.000259 |

TABLE 555.-PHYSICAL PROPERTIES OF SOME SPECIAL GLASSES

| Glass | Composition * | $\begin{aligned} & \text { Density } \\ & \mathrm{g} / \mathrm{cm}^{8} \end{aligned}$ | Young's modulus $\mathrm{kg} / \mathrm{mm}^{2}$ | Coefficient of thermal expansion cgs |  | Specific heat | $\begin{gathered} \text { Softening } \\ \text { points } \\ { }^{\circ} \mathrm{C} \end{gathered}$ | Electric resistance $\dagger$ | Dielectric constant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fused quartz | $\mathrm{SiO}_{2}$ | 2.20 | 7100 | $5.5 \times 10^{-7}$ | . 0033 | . 18 | 1660 | 10.48 | 4.1 |
| Pyrex (7740) | $\begin{aligned} & \mathrm{SiO}_{2}, 80: \mathrm{B}_{2} \mathrm{O}_{3}, 14 \\ & \mathrm{Na}_{2} \mathrm{O}, 4: \mathrm{Al}_{2} \mathrm{O}_{3}, 2 \end{aligned}$ | 2.35 | 6900 | $32 \times 10^{-7}$ | . 0027 | . 25 | 775 | 6.6 | 4.5 |
| Vycor (7900) | $\mathrm{SiO}_{2}, 96: \mathrm{B}_{2} \mathrm{O}_{3}, 3:$ other oxides | 2.18 | 6800 | $8 \times 10^{-7}$ | . 0022 | $\ldots$ | 1500 | 8.1 | 3.8 |
| Lead glass | $\begin{aligned} & \mathrm{SiO}_{2}, 68: \mathrm{PbO}, 15: \\ & \mathrm{Na}_{2} \mathrm{O}_{3}, 10: \mathrm{K}_{2} \mathrm{O}, 6: \\ & \mathrm{CaO}, 1 \end{aligned}$ | 4.26 | 5400 | $91 \times 10^{-7}$ | $\ldots$ | $\ldots$ | 580 | 9.7 | 9.5 |
| Soda lime glass. | $\begin{aligned} & \mathrm{SiO}_{2}, 72: \mathrm{Na}_{2} \mathrm{O}, 15: \\ & \mathrm{CaO}, 9: \mathrm{MgO}, 3: \\ & \mathrm{Al}_{2} \mathrm{O}_{3}, 1 \end{aligned}$ | 2.47 | 6900 | $92 \times 10^{-7}$ | $\cdots$ | $\ldots$ | 695 | 5.1 | 7.2 |
|  | $\underset{\mu}{\text { Diameter }}$ | Breaking strength |  | Young's modulus |  | Torsion coefficient |  |  | $\Delta l / l$ <br> for failure |
| Quartz fibers $\ddagger$ | 1.5 | $.90 \times 10^{11}$ |  | $11.1 \times 10^{11}$ |  |  |  |  |  |
|  | 3.0 | . 65 |  |  |  | $6.6 \times 10^{11}$ |  |  | . 059 |
|  | 5.0 | . 48 |  | 9.8 |  | 5.8 |  |  | . 049 |
|  | 10.0 | . 30 |  | 8.5 |  | 4.8 |  |  | . 035 |
|  | 30.0 | . 145 |  | 7.1 |  | 3.5 |  |  | . 020 |

## TABLE 556.-COLOR SCREENS

Although only the potassium salt does not keep well, it is perhaps safer to use freshly prepared solutions.


The following list is condensed from Wood's Physical Optics:
Methyl violet, $4 R \cdot$ (Berlin Anilin Fabrik) very dilute, and nitroso-dimethyl-aniline transmits $0.365 \mu$. Methyl violet + chinin-sulfate (separate solutions), the violet solution made strong enough to blot out $0.4359 \mu$, transinits 0.4047 and 0.4048 , also faintly 0.3984 .

Cobalt glass + aesculin solution transmits $0.4359 \mu$.
Guinea green B extra (Berlin) + chinin sulfate transmits $0.4916 \mu$.
Neptune green (Bayer, Elberfeld) + chrysoidine. Dilute the latter enough to just transmit 0.5790 and 0.5461 ; then add the Neptune green until the yellow lines disappear.

Chrysoidine + eosine transmits $0.5790 \mu$. The former should be dilute and the eosine added until the green line disappears.

Silver chemically deposited on a quartz plate is practically opaque except to the ultraviolet region $0.3160-0.3260$ where 90 percent of the energy passes through. The film should be of such thickness that a window backed by a brilliantly lighted sky is barely visible.
In the following those marked with a * are transparent to a more or less degree to the ultraviolet.

* Cobalt chloride: solution in water, absorbs $0.50-.53 \mu$; addition of $\mathrm{CaCl}_{2}$ widens the band to $0.47-.50$. It is exceedingly transparent to the ultraviolet down to 0.20 . If dissolved in methyl alcohol + water, absorbs $0.50-.53$ and everything below 0.35 . In methyl alcohol alone $0.485-0.555$ and below $0.40 \mu$.

Copper chloride : in ethyl alcohol absorbs above 0.585 and below 0.535 ; in alcohol +50 percent water, above 0.595 and below $0.37 \mu$.

Neodymium salts are useful combined with other media, sharpening the edges of the absorption bands. In solution with bichromate of potash, transmits $0.535-.565$ and above $0.60 \mu$, the bands very sharp (a useful screen for photographing with a visually corrected objective).

Praseodymium salts: three strong bands at $0.482, .468, .444$. In strong solutions they fuse into a sharp band at $0.435-.485 \mu$. Absorption below 0.34 .

Picric acid absorbs $0.36-.42 \mu$, depending on the concentration.
Potassium chromate absorbs $0.40-.35,0.30-.24$, transmits $0.23 \mu$.

* Potassium permanganate : absorbs $0.555-.50$, transmits all the ultraviolet.

Chromium chloride: absorbs above 0.57 , between 0.50 and .39 , and below $0.33 \mu$. These limits vary with the concentration.

Aesculin: absorbs below $0.363 \mu$, very useful for removing the ultraviolet.

* Nitroso-dimethyl-aniline: very dilute aqueous solution absorbs $0.49-.37$ and transmits all the ultraviolet.

Very dense cobalt glass + dense ruby glass or a strong potassium bichromate solution cuts off everything below 0.70 and transmits freely the red.

Iodine : saturated solution in $\mathrm{CS}_{2}$ is opaque to the visible and transparent to the infrared.

Filters from the following components: Distilled $\mathrm{H}_{2} \mathrm{O}$; Aq. sol. $\mathrm{CuSO}_{4} \cdot 5 \mathrm{H}_{2} \mathrm{O}$; $\mathrm{NiSO}_{4}$. $7 \mathrm{H}_{2} \mathrm{O}$; Glasses, Corning G 986A, G 586, G 980A ; dyed gelatin, Wratten filters 88A, 25, 61, 49.

| Filter and absorbent | ${ }^{\text {Solution }}$ |  | Wavelengthslimits | Max | Transmission at max |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Concentration | Thick ness |  |  |  |
| 88A |  |  | .720-1.400 |  | . 80 |
| 88A, $\mathrm{H}_{2} \mathrm{O}$ |  | 2 cm | .720-1.380 | . 800 | . 72 |
| 88A, G 986A* |  |  | .720-1.020 | . 770 | . 35 |
| $25, \mathrm{CuSO}_{4} \cdot 5 \mathrm{H}_{2} \mathrm{O}$ | 5\% | 2 cm | .590-. 690 | . 630 | . 26 |
| 61, "، | 5\% | 2 cm | .490-. 690 | . 530 | . 52 |
| 49, " | 5\% | 2 cm | . $380-.500$ | . 460 | . 26 |
| G 586,* | 10\% | 2 cm | . $330-.430$ | . 380 | . 69 |
| $\mathrm{G} 986 \mathrm{~A}, \mathrm{NiSO} \cdot{ }^{\prime} \cdot 7 \mathrm{H}_{2} \mathrm{O}$ | 50\% | 1 cm | .260-. 360 | . 310 | . 50 |

${ }^{184}$ Tones, L. A., Journ. Opt. Soc. Amer., vol. 16, p. 259, 1928.

* Thickness .32 cm .

TABLE 558.-NARROW BAND PASS FILTERS*

| Filter | Thickness range | Wavelength limits | Max | Transmission at max |
| :---: | :---: | :---: | :---: | :---: |
| C.S. 5-74 | 5. -7.5 mm | . $402-.480 \mu$ | . $430 \mu$ | 14.5 percent |
| 5-76 | 5. -5.8 | . $400-.483$ | . 430 | 27.5 |
| 5-75 | 3.2-5.7 | . $395-.495$ | . 460 | 12.5 |
| 4-104 | 6. -8.5 | . $467-.530$ | . 485 | 5.3 |
| 4-117 | 7. -12 . | .466-. 580 | . 495 | 34.0 |
| 4-105 | 9. -12.5 | .483-.570 | . 515 | 11.0 |
| 4-102 | 9. -13.5 | .528-.573 | . 550 | 10.6 |
| 4-115 $\dagger$ | 10. -14. | .530-. 575 | . 555 | 35.5 |
| 3-110 | 5. -9. | . $561-.620$ | . 580 | 3.0 |
| 3-120 | 6. -10 . | .565-. 670 | . 590 | 19.5 |
| 2-77 | $6.5-9.5$ | .585-. 705 | . 610 | 11.5 |
| 2-78 | 4. -7. | .612-. 760 | . 640 | 16.0 |
| 2-79 | 8.8-12. | .665-.780 | . 715 | 9.5 |
| 7-84 | 10. -13. | . $710-.900$ | . 750 | 15.0 |
| $7-85 \ddagger$ | 5. -6. | .800-1.101 | . 960 | 25.0 |
| 7-86 | 7. -8 . | 1.200-2.800 | 2.100 | 45.0 |
| 4-17 | 5.5-10. | 1.700-2.800 | 2.400 | 21.0 |

[^214]
## TABLE 559.-TRANSPARENCY OF WATER ${ }^{165}$

Values of $a$ in $I=I_{0} e^{-a t} ; t$ in $\mathrm{cm} ; I_{0}, I$, intensity before and after transmission through distilled water at $20^{\circ} \mathrm{C}$; wavelength $\lambda$ in $\mu$.

| $b$ |  | $c$ |  | ${ }^{\text {d }}$ |  | ${ }^{d}$ |  | $e$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\lambda$ | a | $\lambda$ | $a$ | $\lambda$ | $a$ | $\lambda$ | $a$ | $\lambda$ | $a$ |
| . 1829 | 4.7 | . 20 | . 08 | . 40 | . 00080 | . 54 | . 00044 | . 70 | . 0058 |
| . 1854 | 1.11 | . 24 | . 0135 | . 42 | . 00061 | . 58 | . 00084 | . 75 | 028 |
| . 1862 | . 86 | . 28 | . 0077 | . 44 | . 00046 | . 60 | . 00197 | . 80 | . 024 |
| . 1878 | . 48 | . 30 | . 0064 | . 48 | . 00037 | . 62 | . 00265 | . 85 | . 027 |
| . 1916 | . 20 | . 34 | . 0028 | . 50 | . 00038 | . 64 | . 00292 | . 90 | . 06 |
| . 1935 | . 12 | . 38 | . 0013 | . 52 | . 00040 | . 68 | . 00406 | . 95 | . 3 |

[^215]Percent transmission for a number of wavelengths. All values are for a thickness of 3.5 mm unless otherwise noted. The values given include surface reflection losses. All glasses except the sharp cutting reds and yellows will meet the standard value at 3.5 mm within a thickness range of 3.0 to 4.0 mm . The sharp cutting reds and yellows will meet the standard value at 3.5 within a thickness range of 2.0 to 6.0 mm .

| Filter | . $40 \mu$ | . 45 | . 50 | . 55 | . 60 | . 65 | . 70 | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N-1 | 80 | 64 | 69 | 69 | 68 | 68 | 79 |  |
| N-2 | 58 | 25 | 33 | 36 | 35 | 38 | 76 |  |
| N-3 | 36 | 7 | 12 | 13 | 12 | 13 | 52 |  |
| $\mathrm{N}-6$ † |  | . 02 | . 15 | . 11 | . 08 | . 16 |  | 0 at $.43 \mu ; 9.8$ at $.68 \mu$ |
| R-1 | . | . . | . |  | 28 | 86 | 87 | 0 at. $58 \mu$ |
| R-2 | . | . | . | 1 | 69 | 85 | 84 | 0 at $.54 \mu ; 35$ at $.59 \mu$ |
| R-5 | . | . | . | . . | 2 | 87 | 89 | 0 at. $59 \mu$ |
| R-6 | . | . | . | . | 84 | 86 | 83 | $54 \%$ at $.58 \mu$ |
| R-7 | - | $\ldots$ | $\cdots$ |  |  |  | 81 | $44 \%$ at $.67 \mu$ |
| Y-4 |  |  |  | 68 | 89 | 89 | 89 | 0 at $.51 \mu$ |
| Y-9 | 27 | 56 | 74 | 82 | 84 | 85 | 86 |  |
| Y-10 |  | 1 | 73 | 87 | 90 | 89 | 87 | 0 at . $44 \mu$ |
| G-1 |  | 3 | 7 | 1 |  |  |  | 0 at. 41 and $.56 \mu$ |
| G-9 |  | 1 | 23 | 54 | 22 | 6 | 8 | 0 at $.43 \mu$ |
| BG-1 | 36 | 64 | 68 | 41 | 11 | 2 |  | 0 at $.69 \mu$ |
| B-1 | 87 | 82 | 46 | 33 | 14 | 15 | 68 |  |
| B-2 | 82 | 59 | 7 | 2 | . | . . | 39 | 0 at .58 and $.66 \mu$ |
| B-4 | 42 | 11 |  |  |  |  |  | 0 at $.48 \mu$ |
| B-8 | 91 | 86 | 63 | 53 | 35 | 38 | 81 |  |
| B-10 | 84 | 84 | 59 | 44 | 23 | 19 | 36 |  |

[^216]TABLE 561.-SPECTRAL TRANSMISSION OF SOME RED PYROMETER GLASSES


## TABLE 562.-THE EFFECTIVE WAVELENGTH $\lambda_{e}$ OF CORNING 50-PERCENT RED PYROMETER GLASS* 5 mm THICK FOR SOME TEMPERATURE INTERVALS ${ }^{188}$

$\left.\begin{array}{cccc}\hline \text { Temperature } \\ \text { interval }\end{array} \quad \lambda_{e} \quad \begin{array}{c}\text { Temperature } \\ \text { interval }\end{array}\right]$

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TABLE 563.-ULTRAVIOLET TRANSPARENCY OF ATMOSPHERIC COMPONENTS
$I=I_{0} 10^{-a d}, d$ in $\mathrm{cm} 0^{\circ} \mathrm{C}, 760 \mathrm{mmHg}$.

| Oxygen |  | Oxygen |  | $\underbrace{\text { Ozone }}$ |  | $\underbrace{\text { Ozone }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 1900 M | $a=.0014$ | . $186 \mu$ | $a=.0089$ | . $2378 \mu$ | 100.5 | . $230 \mu$ |  | . $290 \mu$ | 16.6 |
| . 1920 | . 0007 | . 193 | . 0015 | . 2482 | 141 | . 240 | 95 | . 300 | 4.6 |
| . 1929 | . 0022 |  |  | . 2537 | 148.8 | . 250 | 120 | . 310 | 1.23 |
| . 1947 | . 0007 |  | $\mathrm{O}_{2}$, air | . 2652 | 123 | . 260 | 120 | . 320 | . 35 |
| . 1950 | . 0021 |  |  | . 2804 | 45.6 | . 270 | 91 | . 330 | . 093 |
| . 1955 | . 00075 | Air |  | . 2967 | 6.9 | . 280 | 46 | . 340 | . 024 |
| . 1962 | . 0020 | .186 $\mu$ | $a=.0019$ | . 3125 | . 96 |  |  |  |  |
| . 1970 | . 0007 | Water |  | . 3341 | . 07 | $\begin{aligned} & \text { Nitrogen } \\ & .186=.000478 \end{aligned}$ |  |  |  |
| . 2000 | . 00043 |  |  |  |  |  |  |  |  |
| . 2050 | . 0003 |  |  |  |  |  |  |  |  |
| . 2100 | . 0002 |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |

Air at sea level (Washington), 400 m practically no absorption $\lambda>.3 \mu ;<.28 \mu$ about that due to molecular scattering. Air transmission reduced by $1 / 100: 22 \mathrm{~km}$ at $.28 \mu$; 5 at $25 \mu$; 0.57 at $.22 \mu ; 20 \mathrm{~km}$ at $.205 \mu$.

## Atmospheric transparency for ultraviolet

| Wavelength, $\mu \ldots \ldots$ | .29 | .30 | .31 | .32 | .33 | .34 | .35 | .37 | .39 | .41 | .43 | .45 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Percent transmitted .. | 0 | .9 | 9. | 20. | 27. | 33. | 38. | 46. | 51. | 56. | 60. | 64. |

## TABLE 564.-TRANSMISSION OF DYESTUFF SOLUTIONS OF "ADJUSTED" CONCENTRATIONS *

The table gives the percentage transmittances (column 5) at various wavelengths, of the dye solutions, dissolved or buffered as indicated in the third column. All solutions are adjusted to that concentration which gives unit density ( 10 -percent transmittance) at the wavelength of maximum absorption, except for those solutions (marked * in column 4) that have the maximum absorption in the ultraviolet range. The wavelength of maximum absorption is given in column 2. In column 3 is given the serial number of the dye as listed and described in the Colour Index of the British Society of Dyers and Colorists (1924). Dyes having no Colour Index number are listed by the "prototype number" (abbreviated Pr.) of the 1949 Technical Manual and Year Book of the American Association of Textile Chemists and Colorists, p. 147. The names assigned to the dyes are not the names used by the individual American manufacturers but are older names assigned by the Year Book to each Colour Index number, p. 237; or to the "foreign prototype," p. 261.

In column 4, $A$ stands for acid buffer ( $p H=4.6$ ), $K$ for alkaline buffer ( $p H=9.3$ ). In this column, $E$ stands for ethanol (ethyl alcohol) used as solvent, and $B z$ for benzene. Where $A$ or $K$ are used, the solvent was water. $N$ stands for "no buffer," with water as solvent.
In some cases two or more sets of transmissions correspond to a given Colour Index number and name. For example, C.I. No. 326 corresponds to 62 dyestuffs listed as on the American market in 1939, and these may be classified as of several distinct types of Benzo Fast Scarlets and Benzo Fast Oranges. In less striking cases, the different types result from uncontrollable variations in manufacture. In such cases, the transmissions should be considered as representative rather than as specifications of the dye. No manufacturer would guarantee the transmissions within a narrow range, though all data are accurate measurements on actual representatives of at least one manufacturer's products. Transmissions vary somewhat with the exact $p H$ of the buffer and with the characteristics of the instrument used for measurement, especially with the slit width. The present data obtained with the General Electric recording spectrophotometer, which has a 10 -micron slit width.
From the data of the table, approximate data for stronger solutions, whose transmission at the wavelength of maximum absorption is only 1 percent, may be readily obtained by means of a table of squares. Such solutions are twice as concentrated as those of the table. Their transmissions at any given wavelength are approximately the squares of the tabulated transmissions. These relations depend on the validity of Beer's Law for the solution in question.

[^218]TABLE 564.-TRANSMISSION OF DYESTUFF SOLUTIONS OF "ADJUSTED" CONCENTRATIONS (continued)

| Name | $\lambda$ Max. | $\begin{aligned} & \text { C.I. No. } \\ & \text { or or } \\ & \text { Pr. No. } \end{aligned}$ |  | Buffer or solvent | Wavelength (microns) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | . 40 | . 42 | . 44 | . 46 | . 48 | . 50 | . 52 | . 54 | . 56 | . 58 | . 60 | . 62 | . 64 | . 66 | . 68 | . 70 |
|  |  |  |  | Transmittances (percent) |
| Primuline . . . . . | $343$ |  |  |  |  | 0 | 4 | 21 | 49 | 73 | 87 | 92 | 95 | 96 | 97 | 97 | 98 | 98 | 99 | 99 | 99 |
| Celliton Fast Yellow G | 356 | Pr. | 242 |  | E* | 3 | 7 | 15 | 36 | 70 | 90 | 96 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 |
| Milling Yellow O. | 373 | Pr. | 139 | A* | 2 | 7 | 14 | 29 | 56 | 78 | 91 | 96 | 97 | 98 | 98 | 98 | 99 | 99 | 99 | 99 |
| Amido Azo Toluol | 379 |  | 17 | $\mathrm{Bz}{ }^{*}$ | 0 | 3 | 18 | 35 | 53 | 72 | 88 | 96 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Milling Orange | 380 |  | 274 | $A^{*}$ | 2 | 7 | 14 | 24 | 40 | 61 | 80 | 92 | 97 | 98 | 99 | 99 | 99 | 99 | 99 | 99 |
| Diamine Green G | 383 |  | 594 | K | 4 | 8 | 12 | 18 | 29 | 40 | 44 | 39 | 29 | 19 | 12 | 10 | 10 | 12 | 29 | 65 |
|  | $\begin{array}{r} (615 \\ 647) \end{array}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Diamine Catechine G. | 389 | Pr. | 69 | K* | 6 | 8 | 13 | 20 | 30 | 41 | 51 | 60 | 68 | 76 | 84 | 89 | 93 | 95 | 96 | 97 |
| Naphthol Yellow S . | 391 |  | 10 | $A^{*}$ | 11 | 10 | 12 | 30 | 70 | 94 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
|  | (418) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 10 | 100 | 100 |
| Supramine Yellow 3GL | 390 | Pr. | 474 | ${ }^{\text {* }}$ | 3 | 6 | 18 | 49 | 82 | 96 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Mikado Yellow | 392 |  | 622 | K* | 3 | 6 | 18 | 50 | 82 | 94 | 98 | 98 | 99 | 99 | 99 | 99 | 99 | 100 | 100 | 100 |
| Chrysophenine . $\because \because$ | 392 |  | 365 | K* | 5 | 8 | 12 | 20 | 37 | 62 | 79 | 86 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 88 |
| Fastusol Yellow L5G | 394 | Pr. | 99 | K* | 1 | 4 | 20 | 57 | 90 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 99 | 99 |
| Mikado Yellow | 397 |  | 622 | K* | 4 | 6 | 17 | 47 | 78 | 92 | 97 | 98 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 99 |
| Diamine Fast Orange EG | 408 | Pr. | 72 | K | 10 | 11 | 16 | 24 | 36 | 53 | 71 | 86 | 94 | 98 | 99 | 99 | 99 | 99 | 100 | 100 |
| Benzo Chrome Brown G | 408 | Pr. | 365 | K | 10 | 11 | 13 | 17 | 24 | 32 | 42 | 53 | 65 | 77 | 87 | 92 | 95 | 97 | 98 | 99 |
| Thioflavine T | 410 |  | 815 | N | 11 | 12 | 35 | 82 | 98 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Sun Yellow | 410 |  | 620 | N | 11 | 11 | 20 | 41 | 70 | 89 | 96 | 98 | 99 | 99 | 99 | 99 | 100 | 100 | 100 | 100 |
| Sun Yellow | 413 |  | 620 | K | 11 | 10 | 17 | 33 | 57 | 75 | 86 | 93 | 97 | 99 | 99 | 100 | 100 | 100 | 100 | 100 |
| Sulphon Orange G. | 414 | Pr. | 186 | A | 11 | 10 | 13 | 16 | 15 | 17 | 24 | 40 | 74 | 94 | 99 | 100 | 100 | 100 | 100 | 100 |
| Fastusol Orange LGGL | 415 | Pr. | 276 | K | 11 | 10 | 13 | 19 | 29 | 46 | 68 | 86 | 95 | 98 | 98 | 99 | 99 | 99 | 99 | 99 |
| Azosol Fast Yellow CGG | 426 | Pr. | 215 | E | 17 | 10 | 12 | 30 | 69 | 95 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Resorcin Brown . . . . . | 428 |  | 234 | A | 13 | 10 | 10 | 14 | 24 | 39 | 59 | 79 | 91 | 96 | 99 | 99 | 100 | 100 | 100 | 100 |
| Benzo Fast Brown 3GL | 430 | Pr. | 28 | K | 12 | 10 | 10 | 13 | 18 | 26 | 38 | 53 | 68 | 79 | 87 | 92 | 94 | 95 | 96 | 97 |
| Auramine . | 431 |  | 655 | A | 29 | 12 | 12 | 35 | 80 | 97 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Euchrysine 2G | 434 |  | 797 | A | 30 | 14 | 11 | 28 | 72 | 94 | 98 | 99 | 99 | 99 | 100 | 100 | 100 | 100 | 100 | 100 |
| Pryazol Orange | 443 |  | 653 | K | 15 | 12 | 10 | 12 | 22 | 45 | 73 | 91 | 97 | 99 | 99 | 100 | 100 | 100 | 100 | 100 |
| Celliton Fast Brown 3R | 445 | Pr. | 230 | E | 23 | 13 | 10 | 11 | 16 | 24 | 37 | 55 | 72 | 85 | 93 | 97 | 99 | 99 | 99 | 100 |
| Benzamine Brown 3GO. | 447 |  | 596 | K | 10 | 10 | 10 | 10 | 15 | 24 | 39 | 58 | 74 | 84 | 90 | 94 | 96 | 97 | 98 | 98 |
| Trisulfon Brown B. | 450 |  | 561 | K | 12 | 11 | 10 | 10 | 11 | 13 | 17 | 22 | 28 | 32 | 38 | 46 | 56 | 68 | 78 | 86 |





| $\begin{aligned} & \text { C.I. No. } \\ & \text { Pr. } \begin{array}{l} \text { or } \end{array} . \end{aligned}$ | $\begin{gathered} \text { Buffer } \\ \text { or } \\ \text { solvent } \end{gathered}$ | Wavelength (microns) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | . 40 | . 42 | . 44 | . 46 | . 48 | . 50 |  |  | . 56 |  | . 60 | . 62 | . 64 | . 66 | . 68 | . 70 |
|  |  | Transmittances (percent) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 768 | A | 93 | 92 | 88 | 74 | 46 | 27 | 11 | 74 | 99 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| 88 | A | 61 | 59 | 53 | 39 | 22 | 13 | 10 | 15 | 26 | 46 | 74 | 92 | 98 | 100 | 100 | 100 |
| Pr. 393 | K | 47 | 44 | 41 | 32 | 20 | 12 | 10 | 15 | 34 | 66 | 86 | 95 | 98 | 99 | 100 | 100 |
| Pr. 182 | Bz | 46 | 45 | 39 | 31 | 20 | 13 | 10 | 13 | 28 | 70 | 94 | 98 | 99 | 99 | 100 | 100 |
| 382 | K | 26 | 34 | 43 | 37 | 23 | 13 | 10 | 13 | 25 | 54 | 84 | 96 | 98 | 100 | 100 | 100 |
| 184 | A | 63 | 59 | 52 | 40 | 23 | 13 | 10 | 13 | 25 | 56 | 89 | 98 | 100 | 100 | 100 | 100 |
| Pr. 188 | A | 57 | 59 | 56 | 46 | 29 | 16 | 10 | 14 | 22 | 43 | 72 | 91 | 97 | 99 | 99 | 99 |
| 773 | A | 92 | 90 | 88 | 79 | 57 | 36 | 13 | 28 | 80 | 97 | 99 | 99 | 99 | 99 | 99 | 99 |
| Pr. 363 | E | 58 | 50 | 40 | 33 | 31 | 31 | 16 | 15 | 42 | 70 | 95 | 99 | 100 | 100 | 100 | 100 |
| Pr. 234 | E | 88 | 83 | 71 | 51 | 33 | 20 | 12 | 12 | 15 | 29 | 79 | 96 | 98 | 99 | 99 | 99 |
| 778 | N | 95 | 94 | 93 | 85 | 68 | 42 | 25 | 12 | 67 | 99 | 100 | 100 | 100 | 100 | 100 | 100 |
| Pr. 394 | A | 53 | 48 | 43 | 40 | 30 | 19 | 13 | 10 | 12 | 23 | 69 | 92 | 96 | 96 | 96 | 96 |
| 677 | A | 92 | 83 | 65 | 47 | 34 | 28 | 18 | 10 | 35 | 78 | 94 | 98 | 99 | 99 | 99 | 99 |
| 698 | N | 95 | 97 | 96 | 93 | 82 | 58 | 25 | 10 | 15 | 26 | 35 | 58 | 81 | 95 | 99 | 100 |
| Pr. 35 | K | 69 | 71 | 71 | 62 | 46 | 29 | 17 | 10 | 12 | 21 | 32 | 51 | 72 | 87 | 95 | 98 |
| 779 | A | 93 | 91 | 90 | 84 | 69 | 45 | 28 | 14 | 30 | 93 | 100 | 100 | 100 | 100 | 100 | 100 |
| Pr. 213 | E | 84 | 86 | 87 | 84 | 70 | 47 | 26 | 12 | 18 | 66 | 92 | 97 | 99 | 100 | 100 | 100 |
| 842 | N | 92 | 85 | 75 | 65 | 51 | 33 | 18 | 11 | 11 | 27 | 66 | 91 | 98 | 99 | 99 | 100 |
| 1080 | A | 79 | 74 | 60 | 45 | 32 | 22 | 15 | 11 | 10 | 14 | 24 | 44 | 68 | 85 | 95 | 98 |
| 749 | A | 92 | 93 | 96 | 95 | 84 | 63 | 40 | 19 | 15 | 75 | 98 | 99 | 99 | 100 | 100 | 100 |
| 748 | A | 92 | 93 | 96 | 94 | 84 | 66 | 40 | 24 | 10 | 41 | 93 | 99 | 100 | 100 | 100 | 100 |
| 710 | A | 82 | 85 | 84 | 77 | 62 | 41 | 23 | 13 | 10 | 11 | 16 | 26 | 38 | 51 | 63 | 72 |




Benzo Azurine G




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TABLE 564.-TRANSMISSION OF DYESTUFF SOLUTIONS OF "ADJUSTED" CONCENTRATIONS (concluded)

|  | $\begin{gathered} \lambda \text { Max. } \\ 637 \\ (<400 \\ 443) \end{gathered}$ | $\begin{gathered} \text { C.I. No. } \\ \text { Pr. No. } \\ 737 \end{gathered}$ | Buffer solvent A |  |  |  |  |  |  | W | eng | (m |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | . 40 | Transmittances (percent) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Wool Green S.... |  |  |  | 85 | 86 | 86 | 88 | 90 | 92 | 89 | 80 | 65 | 47 | 34 | 17 | 11 | 41 | 82 | 96 |
| Xylene Blue VS | $\begin{gathered} 637 \\ (414) \end{gathered}$ | 672 | A | 81 | 82 | 96 | 99 | 99 | 97 | 93 | 86 | 72 | 52 | 38 | 20 | 10 | 38 | 80 | 95 |
| Nile Blue A. | $\begin{gathered} 638 \\ (605, \\ 428) \end{gathered}$ | 913 | A | 87 | 86 | 87 | 89 | 91 | 87 | 76 | 57 | 36 | 18 | 10 | 11 | 10 | 18 | 52 | 78 |
| Alizarine Cyanine Green. | $\begin{gathered} 641 \\ (610 \\ 413) \end{gathered}$ | 1078 | A | 24 | 23 | 35 | 55 | 69 | 68 | 57 | 41 | 28 | 18 | 11 | 10 | 10 | 13 | 30 | 59 |
| Alizarine Astrol B. | $\begin{array}{r} 642 \\ (607 \\ <400) \end{array}$ | 1075 | A | 51 | 56 | 74 | 87 | 86 | 75 | 61 | 42 | 28 | 17 | 11 | 11 | 10 | 17 | 43 | 75 |
| Alkali Fast Green 10G. | $\begin{gathered} 662 \\ (437) \end{gathered}$ | Pr. 13 | A | 72 | 64 | 60 | 74 | 89 | 93 | 92 | 86 | 76 | 61 | 42 | 26 | 15 | 10 | 15 | 38 |
| Methylene Blue | $\begin{array}{r} 664 \\ (<400) \end{array}$ | 922 | A | 97 | 98 | 97 | 96 | 93 | 92 | 91 | 86 | 75 | 59 | 36 | 28 | 20 | 11 | 29 | 80 |
| Naphthol Green B. | $\begin{array}{r} 723 \\ (<400) \end{array}$ | 5 | A | 12 | 18 | 25 | 40 | 56 | 64 | 70 | 74 | 71 | 59 | 42 | 28 | 18 | 14 | 11 | 10 |

Alum: Ordinary alum (crystal) absorbs the infrared.
Metallic reflection at $9.05 \mu$ and 30 to $40 \mu$.
Rock salt: Rubens and Trowbridge give the following transparencies for a 1 cm thick plate in percent :

| $\lambda$ | 9 | 10 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20.7 | $23.7 \mu$ |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\%$ | 99.5 | 99.5 | 99.3 | 97.6 | 93.1 | 84.6 | 66.1 | 51.6 | 27.5 | 9.6 | .6 | 0. |

Pflüger gives the following for the ultraviolet, same thickness : $280 \mu \mu, 95.5$ percent ; 231. 86 percent; 210, 77 percent ; 186, 70 percent.
Metallic reflection at $0.110 \mu, 0.156,51.2$, and $87 \mu$.
Sylvite: Transparency of a 1 cm thick plate:

| $\lambda$ | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20.7 | $23.7 \mu$ |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\%$ | 100. | 98.8 | 99.0 | 99.5 | 99.5 | 97.5 | 95.4 | 93.6 | 92. | 86. | 76. | 58. | 15. |

Metallic reflection at $0.114 \mu, 0.161,61.1,100$.
Fluorite: Very transparent for the ultraviolet nearly to $0.1 \mu$.
Rubens and Trowbridge give the following for a 1 cm plate:

$$
\begin{array}{lcclcc}
\lambda & 8 \mu & 9 & 10 & 11 & 12 \mu \\
\% & 84.4 & 54.3 & 16.4 & 1.0 & 0
\end{array}
$$

Metallic reflection at $24 \mu, 31.6,40 \mu$.
Iceland spar: Merritt gives the following values of $k$ in the formula $i=i_{o} e^{-k d}(\mathrm{~d}$ in cm$)$ :
For the ordinary ray :

| $\lambda$ | 1.02 | 1.45 | 1.72 | 2.07 | 2.11 | 2.30 | 2.44 | 2.53 | 2.60 | 2.65 | $2.74 \mu$ |
| ---: | :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| $k$ | .0 | .0 | .03 | .13 | .74 | 1.92 | 3.00 | 1.92 | 1.21 | 1.74 | 2.36 |


| $\lambda$ | 2.83 | 2.90 | 2.95 | 3.04 | 3.30 | 3.47 | 3.62 | 3.80 | 3.98 | 4.35 | 4.52 | $4.83 \mu$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
| $k$ | 1.32 | .70 | 1.80 | 4.71 | 22.7 | 19.4 | 9.6 | 18.6 | $\infty$ | 6.6 | 14.3 | 6.1 |

For the extraordinary ray :

| $\lambda$ | 2.49 | 2.87 | 3.00 | 3.28 | 3.38 | 3.59 | 3.76 | 3.90 | 4.02 | 4.41 | $4.67 \mu$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :--- | :--- |
| $k$ | .14 | .08 | .43 | 1.32 | .89 | 1.79 | 2.04 | 1.17 | .89 | 1.07 | 2.40 |
|  |  |  | $\lambda$ | 4.91 | 5.04 | 5.34 | $5.50 \mu$ |  |  |  |  |
|  |  |  | $k$ | 1.25 | 2.13 | 4.41 | 12.8 |  |  |  |  |

Quartz: Very transparent to the ultraviolet; Pfüger gets the.following transmission values for a plate 1 cm thick: at $0.222 \mu, 94.2$ percent $; 0.214,92 ; 0.203,83.6 ; 0.186,67.2$ percent.
Merritt gives the following values for $k$ (see formula under Iceland spar):
For the ordinary ray:

| $\lambda$ | 2.72 | 2.83 | 2.95 | 3.07 | 3.17 | 3.38 | 3.67 | 3.82 | 3.96 | 4.12 | $4.50 \mu$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| $k$ | .20 | .47 | .57 | .31 | .20 | .15 | 1.26 | 1.61 | 2.04 | 3.41 | 7.30 |

For the extraordinary ray :

| $\lambda$ | 2.74 | 2.89 | 3.00 | 3.08 | 3.26 | 3.43 | 3.52 | 3.59 | 3.64 | 3.74 | 3.91 | 4.19 | $4.36 \mu$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :--- | :--- |
| $k$ | .0 | .11 | .33 | .26 | .11 | .51 | .76 | 1.88 | 1.83 | 1.62 | 2.22 | 3.35 | 8.0 |

For $\lambda>7 \mu$, becomes opaque, metallic reflection at $8.50 \mu, 9.02,20.75-24.4 \mu$, then transparent again.

TABLE 566.-TRANSPARENCY OF WATER VAPOR (steam)

| Wave. <br> length | Steam | Absorp. <br> tion | Wave- <br> length | Steam | Absorp- <br> tion | Wave- <br> length | Steam | Absorp. <br> tion |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $.95 \mu$ | 109 cm | $7 \%$ | $6.5 \mu$ | 32.4 cm | $80 \%$ | $20 \mu$ | 32.4 | $80 \%$ |
| 1.13 | $"$ | 14 | 11 | 104 | 15 | 22 | $"$ | 22 |
| 1.36 | $"$ | 75 | 13 | 104 | 35 | 26 | $" 6$ | 30 |
| 1.84 | $"$ | 84 | 15 | 104 | 55 | 30 | 4 | 80 |
| 2.64 | $"$ | 100 | 18 | 32.4 | 55 | 34 | $"$ | 80 |

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## TABLE 567.-TRANSMISSION OF RADIATION THROUGH MOIST AIR (percent)

The values of this table are of use for finding the transmission of energy through air containing a known amount of water vapor. An approximate value for the transmission may be had if the amount of energy from the source between the wavelengths of the first column is multiplied by the corresponding transmission coefficients of the subsequent columns. The values for the wavelengths greater than $18 \mu$ are tentative and doubtful.

*These places require multiplication by the following factors to allow for losses in $\mathrm{CO}_{2}$ gas. Under average sea-level outdoor conditions the $\mathrm{CO}_{2}$ (partial pressure $=0.003 \mathrm{~atm}$ ) amounts to about $0.6 \mathrm{~g} / \mathrm{cm}^{8}$. Paschen gives 3 times as much for indoor conditions.
$2 \mu$ to $3 \mu$, for 2 g in $m^{2}$ path (95); for 140 g in $m^{2}$ path ( 93 );
4 " 5 " "، "، "" (93); " " "، " "" (70); more $\mathrm{CO}_{2}$ no further effect;
13 " 14, slight allowance to be made;
14 "، $15,80 \mathrm{gg}$ in $\mathrm{m}^{2}$ path reduces energy to zero;
$\dagger$ These places require multiplication by 0.90 and 0.70 respectively for one air mass and 0.85 and 0.65 for two air masses to allow for ozone absorption when the radiation comes from a celestial body.

## TABLE 568.-INFRARED TRANSMISSION OF VARIOUS SUBSTANCES (percent) ${ }^{107}$

|  |  | $20 \mu$ | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | 120 | $130 \mu$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fused quartz | .2 mm | 0 | 0 | 2 | 20 | 35 | 51 | 53 | 52 |  |  |  |  |
| " | 1.0 " | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 6 | 18 | 30 | 22 | 27 |
| Crystal | 1.0 " | 0 | 1 | 7 | 42 | 57 | 62 | 59 | 72 | 71 | 78 | 70 | 72 |
| Sulfur, rhombic | . 9 " | 30 | 40 | 10 | 6 | 39 | 37 | 52 | 58 | 51 | 56 | 58 | 38 |
| Paraffin ...... | 2.0 " | 19 | 35 | 42 | 51 | 58 | 64 | 65 | 75 | 85 | 79 | 76 | 70 |
| Mica | $6 \mu$ | 6 | 18 | 50 | 53 | 46 | 57 | 50 | 21 | 27 | 50 | (55) | (55) |
| Cellophane | $40 \mu$ | 0 | 16 | 22 | 23 | 24 | 24 | 23 | 23 | 29 | 30 | 30 | 42 |
| Celluloid | $1 \mu$ | 92 | 93 | 95 | 96 | 96 | 97 | 97 | 98 | 98 | 99 | 99 | 99 |
| Black paper | . 1 mm |  |  |  | 2 | 5 | 13 | 19 | 22 | 23 | 26 | 28 | 30 |
| Camphor soot | * | 60 | 76 | 79 | 80 | 81 | 82 | 84 | 85 | 86 | 87 | 89 | 90 |
| Pfund Bi black. | * | 30 | 40 | 44 | 48 | 50 | 40 | 45 | 58 | 60 | 57 | 60 | 63 |
| Lampblack, water glass | . 8 | 0 | (1) | (3) | 7 | 12 | 21 | 20 | 26 | 30 | 25 | 30 | 30 |

[^219]TABLE 569.-INFRARED TRANSMISSION, IN PERCENT, OF A NUMBER OF MATERIALS ${ }^{188}$

| Thick- | Lead chloride | Magneoxide oxid | $\begin{gathered} \text { Potas- } \\ \text { sium } \\ \text { chloride } \end{gathered}$ | Silver chloride | Thallium bromide |  | Thallium chloride | Sapphire | Cesium bromide |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { in mess } \\ & \lambda(\mu) \end{aligned}$ | 6 | . 47 | 6 | 6 | 6 | 8 | 6 | 1.17 | 7 |
| . 40 | . | . | . | $\cdots$ | . | . | . | . | 71.5 |
| . 60 | . | . | . | . | . |  | . | . | 77.8 |
| 1 | . |  | $\cdots$ |  | $\cdots$ | . | . |  | 79.8 |
| 2 | $\cdots$ | 88 | . | 73 | . | . | . | 86.5 | 82.0 |
| 3 | . | 87 | . | 76 | . | . | . | 89.0 | 82.0 |
| 4 | . | 89 | $\cdots$ | 77 | $\cdots$ | . | $\cdots$ | 89.2 | 82.0 |
| 5 | $\cdots$ | 90 | . | 79 | . | . | . | 82.5 | 82.0 |
| 6 | $\cdots$ | 89 | $\cdots$ | 80 | $\cdots$ | . |  | 50.0 | 82.0 |
| 7 | . | 84 | . | 80 | . | . | . | 4.0 | 83.0 |
| 8 | $\ldots$ | 78 | $\cdots$ | 80 | . | . | . | .. | 83.0 |
| 10 | . | 11 | . | 80 | . | $\cdots$ | . | . | 83.5 |
| 12 |  |  | . | 80 | $\cdots$ | . | $\cdots$ | . | 84.0 |
| 14 | 82 | . | . | 80 | $\ldots$ | .. | .. | . | 84.5 |
| 16 | 82 | . |  | 82 | $\cdots$ | . | . | . | 85.0 |
| 18 | 80 | . | 87 | 82 | . | . | . | . | 85.0 |
| 20 | 77 | . | 72 | 78 |  | . |  | . | 85.0 |
| 22 | 69 | . | 37 | 62 | 61 | . | 57 | . | 85.0 |
| 24 | 52 | . | 12 | 46 | 61 |  | 38 | . | 84.0 |
| 26 | 19 | $\cdots$ | . | 27 | 60 | 66 | 18 | . | 84.0 |
| 28 | . | $\cdots$ | $\cdots$ | . | 57 | 62 | 6 | . | 83.0 |
| 30 | . | $\cdots$ | . | $\cdots$ | 50 | 61 |  | . | 83.0 |
| 32 | $\cdots$ | . | . | . | 39 | 58 | . | . | 83.0 |
| 34 | $\ldots$ | . | $\ldots$ | $\ldots$ | 33 | 54 | . | . | 82.0 |
| 36 | . | $\cdots$ | $\cdots$ | . | 26 | 51 | . | . | 80.0 |
| 38 |  | . | . |  | . | . | . | . | 76.0 |

${ }^{108}$ Data from E. K. Plyler, Nat. Bur. Standards Journ. Res., vol. 41, p. 125, 1948, and E. K. Plyler, National Bureau of Standards, private communication. Cesium bromide data by E. K. Plyler and F. A. Phelps.

TABLE 570.-INFRARED TRANSMISSION OF GASES (percent) ${ }^{180}$

| Length of cell, 4 inches. |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Material | Pressure | $6.7 \mu$ | $8.7 \mu$ | $20.75 \mu$ | $22.9 \mu$ | $27.3 \mu$ | $29.4 \mu$ | $32.8 \mu$ |
| $\mathrm{NH}_{2}$ | 760 mmHg | 24 | 26 | 79 | 93 | 83 | 82 | 62 |
| $\mathrm{C}_{2} \mathrm{H}_{3}$ | 760 | 95 | 92 | 99 | 101 | 101 | 100 | 98 |
| $\mathrm{H}_{2} \mathrm{~S}$ | 760 | 97 | 98 | 98 | 97 | 92 | 90 | 83 |
| $\mathrm{SO}_{2}$ | 760 | 98 | 5 | 7 | 58 | 100 | 100 | 96 |
| $\mathrm{C}_{6} \mathrm{H}_{4}$ | 96 | 65 | 97 | 102 | 99 | 100 | 98 | 95 |
| $\mathrm{CCl}_{4}$ | 114 | 95 | 99 | 97 | 99 | 99 | 99 | 91 |
| $\mathrm{CS}_{3}$ | 361 | 30 | 98 | 100 | 86 | 98 | 99 | 96 |
| $\mathrm{CHCl}_{2}$ | 200 | 93 | 90 | 99 | 98 | 98 | 97 | 97 |
| $\left(\mathrm{C}_{2} \mathrm{H}_{6}\right)_{2} \mathrm{O}$ | 526 | 17 | 6 | 61 | 45 | 69 | 71 | 61 |

100 Strong, Phys. Rev., vol. 37, p. 1565, 1931, Restrahlung.

TABLE 571.-INFRARED TRANSMISSION OF SOLIDS (percent)

| Material | Description | $6.7 \mu$ | $8.7 \mu$ | $20.75 \mu$ | 22.94 | $27.3 \mu$ | $29.4 \mu$ | $32.8 \mu$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lacquer film | $\pm .55 \mu$ thickness | 96 | 93 | 97 | 98 | 99 | 99 | 100 |
| Mica . . . . . | $10 \mu$ thickness | 83 | 22 | 19 | 00 | 35 | 42 | 44 |
| Soot on lacquer | Opaque to visible | 25 | 22 | 67 | 53 | 60 | 67 | 60 |
| Quartz, fused. | $10 \mu$ thickness | 86 | 02 | 01 | 03 | 51 | 55 | 68 |
| Glass ....... | $3 \mu$ thickness | 93 | 07 | 12 | 14 | 48 | 51 | 56 |
| Cellophane | $25 \mu$ thickness | 33 | 04 | 04 | 01 | 20 | 25 | 26 |
| $\mathrm{MgO} \ldots$ | Deposit from burning <br> Mg ribbon | 88 | 86 | 04 | 02 | 90 | 93 | 87 |
| ZnO | Deposit from Zn arc | 99 | 80 | 15 | 05 | 93 | 79 | 80 |


| Description of reflector | $22.9 \mu$ | $32.8 \mu$ |
| :---: | :---: | :---: |
| Deposit of MgO from burning Mg ribbon. | 0 | 0 |
| Reflection $\beta$ - MgO | 80 | 33 |
| Mica | 32 | . . |
| Paraffin | 04 | . |
| Pencil mark on paper | 09 |  |
| Soot coating | 43 | 48 |
| Silver covered with MgO coating | 08 | 91 |
| Silver covered with ZnO coating | 01 | 52 |
| Uptical black | 31 | . . |
| Gold foil blackened with bismuth. | $>19$ | . |
| $\mathrm{KBr}+1.5 \mu \mathrm{CaF}_{2}$ deposited by evaporation | 10 |  |
| $\mathrm{KI}+1.5 \mu \mathrm{CaF}_{2}$ deposited by evaporation. | 13 | . |

## TABLE 573.-ABSORPTION OF VARIOUS MATERIALS USED FOR BLACKENING RECEIVERS FOR MEASURING RADIATION OF DIFFERENT WAVELENGTHS ${ }^{170}$

Soot from a candle, acetylene, or camphor flame has been used and was found by Pfund to be very good to wavelengths about $1.2 \mu$; beyond this to longer wavelengths the soot becomes transparent until at about $11 \mu$, for a film about as thick as will work satisfactorily, it transmits about 50 percent of the incident radiation.

Very finely powdered metal such as zinc ( 4 parts Zn and 1 part Sb ) and platinum were found to be very good. Even for wavelengths of about $14 \mu$ the Zn powder absorbed over 98 percent of the radiation and out to $51 \mu$ the absorption was about 85 percent.

For longer wavelengths powdered $\mathrm{NaCl}, \mathrm{KBr}, \mathrm{TlCs}$, and some other salts were found to be very good, as shown in the table.

The figures given in the table for radiation absorption are relative, those with the highest values being the blackest. For instance, India ink and tellurium powder are the best absorbers for radiation shorter than $5 \mu$ while for longer wavelengths than $50 \mu$ powdered glasses and CuSO، are probably the more nearly black.

The absorptive power is an integrated effect over the entire far infrared. Litharge, powdered glass, white lead, copper sulfide, celestite, and red phosphorus were the best absorbers beyond $50 \mu$. A very thin coat of the absorbing material in most cases was an inefficient absorber of the extreme infrared waves. A very poor absorbing material in most cases such as copper or platinum will absorb if the surface is sufficiently rough

For radiometers, the absorbing material is better when mixed with turpentine and alcohol and painted on the vanes. For thermocouples, the absorbing material is better if it is mixed with lacquer. Sixty-fold sensitiveness and better steadiness comes from evacuation.

The high absorption of glass in the near infrared suggests its use as a source of radiation. Two Pt wires separated by 4 mm and covered with glass were heated by an electric current; the hot portion of the glass between the wires served as a source of extreme infrared radiation. A convenient method of filtering out the near infrared is to grind the windows with emery so that the pits are about $4 \mu$ deep. The apparatus may be adjusted with visible light by covering the rough surface with turpentine.

| Substance | Radiation absorbed for |  | Substance | Radiation absorbed for$\lambda<5 \mu \quad \lambda>50 \mu$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\lambda<5 \mu$ | $\lambda>50 \mu$ |  |  |  |
| Litharge | 10.8 | 4.3 | Silver sulfide | 12.8 | 4.4 |
| Ground glass | 11.9 | 4.7 | Copper sulfate crystals |  |  |
| Powdered glass | 11.7 | 5.0 | from solution ...... | 15.0 | 4.1 |
| White lead 2 Pb |  |  | Wellsbach mantle |  |  |
| $\mathrm{CO}_{3} \cdot \mathrm{~Pb}(\mathrm{OH})_{2}$ | 14.9 | 4.9 | material | 8.9 | 31 |
| White lead in lacquer | 14.3 | 4.4 | Platinum black | 18.2 | 4.4 |
| Red phosphorus | 18.3 | 5.0 | Tartaric acid and |  |  |
| Red phosphorus from |  |  | sugar | 16.0 | 3.9 |
| a match box..... | 17.7 | 5.1 | Talc | 12.5 | 3.8 |
| Celestite, powdered |  |  | Water glass | 12.1 | 3.7 |
| $\mathrm{SrSO}_{4}$ | 14.7 | 4.6 | Tellurium, powdered | 19.2 | 3.3 |
| Brucite, powdered |  |  | India ink . . . . . . . . | 18.8 | 3.8 |
| $\mathrm{Mg}(\mathrm{OH})_{2} \ldots \ldots$ | 11.4 | 4.2 | Lacquer | 8.6 | 3.0 |
| Angelsite, powdered |  |  | Castor oil | 8.8 | 28 |
| PbSO4, ....... |  | 4.2 | Glycerine | 11.2 | 3.1 |
| Copper sulfide | 17.1 | 5.2 | Turpentine | 8.1 | . 2 |
| Copper oxide | 13.8 | 4.4 | Clean receiver | 2.9 | . 2 |

[^220]
## TABLES 574-592.-REFLECTION AND ABSORPTION OF RADIATION

According to Fresnel, the amount of light reflected by the surface of a transparent medium $=\frac{1}{2}(A+B)=\frac{1}{2}\left\{\frac{\sin ^{2}(i-r)}{\sin ^{2}(i+r)}+\frac{\tan ^{2}(i-r)}{\tan ^{2}(i+r)}\right\} ; A$ is the amount polarized in the plane of incidence; $B$ is that polarized perpendicular to this ; $i$ and $r$ are the angles of incidence and refraction.

TABLE 574.-RADIATION REFLECTED WHEN $i=0^{\circ}$ OR INCIDENT LIGHT IS NORMAL TO SURFACE $=(n-1)^{2} /(n+1)^{2}$
(percent)

| $n$ | $1(A+B)$ | $n$ | $\frac{1}{2}(A+B)$ | $n$ | $1(A+B)$ | $n$ | $\frac{1}{2(A+B)}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.00 | .00 | 1.4 | 2.78 | 2.0 | 11.11 | 5. | 44.44 |
| 1.02 | .01 | 1.5 | 4.00 | 2.25 | 14.06 | 5.83 | 50.00 |
| 1.05 | .06 | 1.6 | 5.33 | 2.5 | 18.37 | 10. | 66.67 |
| 1.1 | .23 | 1.7 | 6.72 | 2.75 | 22.89 | 100. | 96.08 |
| 1.2 | .83 | 1.8 | 8.16 | 3. | 25.00 | $\infty$ | 100.00 |
| 1.3 | 1.70 | 1.9 | 9.63 | 4. | 36.00 |  |  |

TABLE 575.-RADIATION REFLECTED WHEN $n=1.55$


[^221]
# TABLE 576.-REFLECTING FACTOR OF POWDERS (WHITE LIGHT) (percent) 

Various pure chemicals, very finely powdered and surface formed by pressing down with glass plate. White (noon sunlight) light. Reflection in percent.


[^222]
## TABLE 577.-VARIATION OF REFLECTING FACTOR OF SURFACES WITH ANGLE (RELATIVE VALUES)

Illumination at normal incidence, $1 \frac{1}{4}$-watt tungsten lamp, reflection at angles indicated with normal.

| Angle of observation | $0^{\circ}$ | $1^{\circ}$ | $3^{\circ}$ | $5^{\circ}$ | $10^{\circ}$ | $15^{\circ}$ | $30^{\circ}$ | $45^{\circ}$ | $60^{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Magnesium carbonate block. | . 88 | - | - | . 88 | . 88 | . 87 | . 83 | . 72 | . 68 |
| Magnesium oxide | . 80 | - | - | . 80 | . 80 | . 80 | . 77 | . 75 | . 66 |
| Matt photographic paper | . 78 | - | - | . 78 | . 78 | . 78 | . 78 | . 76 | . 72 |
| White blotter ........ | . 76 | - | - | . 76 | . 76 | . 76 | . 73 | . 70 | . 67 |
| Pot opal, ground | . 69 | . 69 | . 69 | . 69 | . 69 | . 69 | . 68 | . 66 | . 64 |
| Flashed opal, not ground | 11.3 | 11.3 | 11.3 | . 31 | . 22 | . 21 | . 20 | . 20 | . 18 |
| Glass, fine ground...... | . 29 | . 29 | . 29 | . 29 | . 27 | . 20 | . 14 | . 13 | . 12 |
| Glass, coarse ground | . 23 | . 22 | . 21 | . 20 | . 19 | . 16 | . 11 | . 11 | . 12 |
| Matt varnish on foil | . 83 | - | . 78 | . 72 | . 62 | . 49 | . 28 | . 21 | . 16 |
| Mirror with ground face | 4.9 | - | - | 4.55 | 3.86 | 3.03 | . 78 | . 42 | . 35 |

The following figures, taken from Fowle, Smithsonian Misc. Coll., vol. 58, No. 8, indicate the amount of energy scattered on each side of the directly reflected beam from a silvered mirror; the energy at the center of the reflected beam was taken as 100,000 , and the angle of incidence was about $3^{\circ}$.


Wavelength of max. energy of Nernst lamp used as source about $2 \mu$.

TABLE 578.—ULTRAVIOLET REFLECTING FACTOR OF SOME METALS ${ }^{17}$

| Aluminum,castrolled | . $250 \mu$ | . 300 | . 350 | . 400 | . 450 | . 500 | . 550 | . 600 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | . 43 | . 45 | . 54 | . 62 | . 68 | . 72 | . 73 | . 74 |
|  | . 21 | . 28 | . 34 | . 41 | . 46 | . 50 | . 53 | . 56 |
| Rhodium | . 30 | . 37 | . 44 | . 50 | . 53 | . 57 | . 58 | . 59 |
| Tin, polished | . 33 | . 38 | . 45 | . 52 | . 60 | . 67 | . 72 | . 73 |
| Duralumin | . 24 | . 31 | . 44 | . 46 | . 46 | . 46 | . 46 | . 46 |
| tarnished to. | . 20 | . 26 | . 32 |  |  |  |  |  |

[^223]TABLE 579．－PERCENTAGE REFLECTION FROM METALS，VIOLET END OF SPECTRUM ${ }^{172}$

| Wavelength in | ． 10 | ． 15 | ． 20 | ． 25 | ． 30 | ． 35 | ． 40 | ． 50 | ． 60 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ni electroplated |  | ． |  | 40 | 44 | 51 | 53 | 56 | （60） |
| ＂vac．fused． |  |  |  | 48 | 42 | 45 | 52 | 62 | 64 |
| Ag（min． $7 \%, 33 \mu$ ） |  | ． |  | 30 | 16 | 71 | 88 | 92 | （94） |
| Stellite（ $\mathrm{Co}, \mathrm{Cr}, \mathrm{Mo}$ ） | ． | ． | ． | 46 | 49 | 55 | 60 | 64 | （68） |
| Stainless steel，13\％Cr |  | ． |  | 40 | 47 | 52 | 56 | 59 | （60） |
| Cobalt ．．．．．．．． |  |  | ． | 43 | 46 | 52 | 58 | 62 | （67） |
| Speculum |  |  |  | 31 | 41 | 50 | 56 | 60 | （62） |
| Beryllium（98．7\％） | 53 | 67 | 79 | 84 | 87 |  |  | ．． | ．． |
| Chromium on steel． | 63 | 65 | 71 | 78 | 82 | 86 | 88 |  |  |

${ }^{172}$ Coblentz，Stair，Nat．Bur．Standards Journ．Res．，vol．2，p．343， 1929.

## TABLE 580．－PERCENTAGE REFLECTING FACTOR OF DRY POWDERED PIGMENTS

The total reflecting power depends on the distribution of energy in the illuminant and is given in the last three columns for noon sun，blue sky，and for a 7.9 lumens／watt tungsten filament．

| Spectrum color | Vio－ <br> let <br> .44 | Blue |  | Green |  |  | Yellow |  | Orange |  |  | Red |  |  | $E$50888 | $\begin{aligned} & \stackrel{\rightharpoonup}{s} \\ & \stackrel{\infty}{=} \\ & \text { 㐫 } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wavelength in $\mu$ |  | ． 46 | ． 48 | ． 50 | ． 52 | ． 54 | ． 56 | ． 58 | ． 60 | ． 62 | ． 64 | ． 66 | ． 68 | ． 70 |  |  |  |
| American vermilion | 8 | 6 | 5 | 5 | 6 | 6 | 9 | 11 | 24 | 39 | 53 | 61 | 66 | 65 | 14 | 12 | 12 |
| Venetian red | 5 | 5 | 5 | 5 | 5 | 6 | 7 | 12 | 19 | 24 | 28 | 30 | 32 | 32 | 11 | 10 | 13 |
| Tuscan red | 7 | 7 | 7 | 8 | 8 | 8 | 8 | 12 | 16 | 18 | 20 | 22 | 23 | 24 | 11 | 10 | 12 |
| Indian red | 8 | 7 | 7 | 7 | 7 | 7 | 7 | 11 | 15 | 18 | 20 | 22 | 23 | 24 | 10 | 9 | 11 |
| Burnt sienna | 4 | 4 | 4 | 4 | 5 | 6 | 9 | 14 | 18 | 20 | 21 | 23 | 24 | 25 | 11 | 9 | 13 |
| Raw sienna | 12 | 13 | 13 | 13 | 18 | 26 | 35 | 43 | 46 | 46 | 45 | 44 | 45 | 43 | 33 | 30 | 37 |
| Golden ochre | 22 | 22 | 23 | 27 | 40 | 53 | 63 | 71 | 75 | 74 | 73 | 73 | 73 | 72 | 58 | 55 | 63 |
| Chrome yellow ochre | 8 | 9 | 7 | 7 | 10 | 19 | 30 | 46 | 60 | 62 | 66 | 82 | 81 | 80 | 33 | 29 | 40 |
| Yellow ochre ．．．．．．． | 20 | 20 | 21 | 24 | 32 | 42 | 53 | 63 | 64 | 61 | 60 | 59 | 59 | 59 | 49 | 46 | 53 |
| Chrome yellow medium | 5 | 5 | 6 | 8 | 18 | 48 | 66 | 75 | 78 | 79 | 81 | 81 | 81 | 81 | 54 | 50 | 63 |
| Chrome yellow light．． | 13 | 13 | 18 | 30 | 56 | 82 | 88 | 89 | 90 | 89 | 88 | 87 | 85 | 84 | 76 | 70 | 82 |
| Chrome green light．．． |  | 10 | 14 | 23 | 26 | 23 | 20 | 17 | 14 | 11 | 9 | 8 | 7 | 6 | 19 | 19 | 18 |
| Chrome green medium | 7 | 7 | 10 | 21 | 21 | 17 | 13 | 11 | 9 | 7 | 6 | 6 | 6 | 5 | 14 | 14 | 12 |
| Cobalt blue ．．．．．．．．．．． | 59 | 58 | 49 | 35 | 23 | 15 | 11 | 10 | 10 | 10 | 11 | 15 | 20 | 25 | 16 | 18 | 13 |
| Ultramarine blue | 67 | 54 | 38 | 21 | 10 | 6 | 4 | 3 | 3 | 4 | 5 | 7 | 10 | 17 | 7 | 10 | 6 |

## TABLE 581．—INFRARED DIFFUSE PERCENTAGE REFLECTING FACTORS OF DRY PIGMENTS

| Wavelength in $\mu$ | Ois | $\begin{aligned} & 0 \\ & 3 \\ & \hline \end{aligned}$ | O. © | O | $\begin{aligned} & \infty \\ & \mathbb{N}_{4}^{\infty} \\ & \text { in } \end{aligned}$ | $\stackrel{N}{\infty}_{\infty}^{\infty}$ | $\begin{aligned} & 0 . \\ & \text { O } \\ & \text { L } \end{aligned}$ | $\begin{aligned} & 0_{4}^{\infty} \\ & < \end{aligned}$ | $\begin{aligned} & \text { O゙ } \\ & \underset{F}{\circ} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & 0 \\ & \sum_{\infty}^{\infty} \end{aligned}$ | $\begin{aligned} & 0 \\ & \text { Ũ } \end{aligned}$ | $\begin{aligned} & \text { O゙ } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0_{0}^{\infty} \\ & \sum_{2}^{\infty} \\ & \hline \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ．60＊ | 3 | － | 27 | 52 | 26 | 74 | 70 | 84 | 86 | 82 | 86 | 85 | 86 | 88 | 85 | 76 | 68 |
| ． 95 ＊ | 4 | 24 | 45 | － | 41 | － | － | 88 | － | 86 | － | － | 84 | 93 | 89 | 79 | 72 |
| 4.4 | 14 | 15 | 33 | 51 | 30 | 34 | 41 | 21 | 47 | 8 | 16 | 22 | 23 | 29 | 11 | － | － |
| 8.8 | 13 | － | 5 | 26 | 4 | 11 | 5 | 20 | 7 | 3 | 2 | 4 | 5 | 10 | 4 | － | － |
| 24.0 | 6 | 4 | 8 | 10 | 9 | 10 | 7 | 6 | 10 | 5 | 9 | 6 | 5 | 7 | 9 | － | － |

[^224]Perpendicular incidence and reflection (See also Tables 578, 579, 589)
The numbers give the percents of the incident radiation reflected.

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 251 | - | - | 67.0 | 35.8 | 29.9 | 37.8 | - | 32.9 | 25.9 | 33.8 | 38.8 | - | 34.1 |
| . 288 | - | - | 70.6 | 37.1 | 37.7 | 42.7 | - | 35.0 | 24.3 | 38.8 | 34.0 |  | 21.2 |
| . 305 | - |  | 72.2 | 37.2 | 41.7 | 44.2 | - | 37.2 | 25.3 | 39.8 | 31.8 |  | 9.1 |
| . 316 | - |  |  |  |  |  |  |  |  |  |  |  | 4.2 |
| . 326 | - | - | 75.5 | 39.3 | - | 45.2 | - | 40.3 | 24.9 | 41.4 | 28.6 | - | 14.6 |
| . 338 | - | - | 81. | T3 | 51 | 46.5 | - | - | - | 43.4 | - | - | 55.5 |
| . 357 | - | - | 81.2 | 43.3 | 51.0 | 48.8 | - | 45.0 | 27.3 | 43.4 | 27.9 |  | 74.5 |
| . 385 | - | - | 83.9 | 44.3 | 53.1 | 49.6 | - | 47.8 | 28.6 | 45.4 | 27.1 | - | 81.4 |
| . 420 | - | - | 83.3 | 47.2 | 56.4 | 56.6 | - | 51.9 | 32.7 | 51.8 | 29.3 | - | 86.6 |
| . 450 | 85.7 | 72.8 | 83.4 | 49.2 | 60.0 | 59.4 | 48.8 | 54.4 | 37.0 | 54.7 | 33.1 | - | 90.5 |
| . 500 | 86.6 | 70.9 | 83.3 | 49.3 | 63.2 | 60.8 | 53.3 | 54.8 | 43.7 | 58.4 | 47.0 | - | 91.3 |
| . 550 | 88.2 | 71.2 | 82.7 | 48.3 | 64.0 | 62.6 | 59.5 | 54.9 | 47.7 | 61.1 | 74.0 |  | 92.7 |
| . 600 | 88.1 | 69.9 | 83.0 | 47.5 | 64.3 | 64.9 | 83.5 | 55.4 | 71.8 | 64.2 | 84.4 |  | 92.6 |
| . 650 | 89.1 | 71.5 | 82.7 | 51.5 | 65.4 | 66.6 | 89.0 | 56.4 | 80.0 | 66.5 | 88.9 | - | 94.7 |
| . 700 | 89.6 | 72.8 | 83.3 | 54.9 | 66.8 | 68.8 | 90.7 | 57.6 | 83.1 | 69.0 | 92.3 | - | 95.4 |
| 800 | - | - | 84.3 | 63.1 |  | 69.6 | - | 58.0 | 88.6 | 70.3 | 94.9 |  | 96.8 |
| 1.0 | - | - | 84.1 | 69.8 | 70.5 | 72.0 | - | 63.1 | 90.1 | 72.9 |  | - | 97.0 |
| 1.5 | - | - | 85.1 | 79.1 | 75.0 | 78.6 | - | 70.8 | 93.8 | 77.7 | 97.3 | - | 98.2 |
| 2.0 | - | - | 86.7 | 82.3 | 80.4 | 83.5 | - | 76.7 | 95.5 | 80.6 | 96.8 | 91.0 | 97.8 |
| 3.0 |  | - | 87.4 | 85.4 | 86.2 | 88.7 | - | 83.0 | 97.1 | 88.8 |  | 93.7 | 98.1 |
| 4.0 | - |  | 88.7 | 87.1 | 88.5 | 91.1 | - | 87.8 | 97.3 | 91.5 | 96.9 | 95.7 | 98.5 |
| 5.0 | - | - | 89.0 | 87.3 | 89.1 | 94.4 | - | 89.0 | 97.9 | 93.5 | 97.0 | 95.9 | 98.1 |
| 7.0 | - | - | 90.0 | 88.6 | 90.1 | 94.3 | - | 92.9 | 98.3 | 95.5 | 98.3 | 97.0 | 98.5 |
| 9.0 | - | - | 90.6 | 90.3 | 92.2 | 95.6 | - | 92.9 | 98.4 | 95.4 | 98.0 | 97.8 | 98.7 |
| 11.0 |  |  | 90.7 | 90.2 | 92.9 | 95.9 | - | 94.0 | 98.4 | 95.6 | 98.3 | 96.6 | 98.8 |
| 14.0 | - | - | 92.2 | 90.3 | 93.6 | 97.2 | - | 96.0 | 97.9 | 96.4 | 97.9 |  | 98.3 |

TABLE 583.-LONG-WAVE ABSORPTION BY GASES
Unless otherwise noted, gases were contained in a $20-\mathrm{cm}$ long tube.


The radiation used to measure the reflecting factors for the wavelengths given was obtained from the sun's radiation transmitted through selected filters. The radiation from a "pointalight" transmitted through a thin gold filter may be used in place of the sun.

| Description | (1.78ر) | (.84 $\mu$ ) | (.61 $\mu$ ) | (.50ر) | Gold film | Com. puted |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Magnesium carbonate | . 63 | . 99 | . 98 | . 96 | . 96 |  |

Clay tiles

| Dutch: light red. | . 68 | . 66 | . 56 | . 21 | . 57 | . 52 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Machine-made : red | . 72 | . 42 | . 34 | . 11 | . 38 | . 38 |
| red | . 55 | . 38 | . 31 | . 11 | . 34 | . 33 |
| lighter red | . 52 | . 40 | . 32 | . 13 | . 34 | . 33 |
| dark purple | . 22 | . 22 | . 19 | . 13 | . 19 | . 18 |
| Hand-made : red |  | . 47 | . 37 | . 12 | . 40 | . 39 |
| red | 55 | . 33 | . 28 | . 13 | . 31 | 31 |

Concrete tiles

| Uncolored | . 37 | . 38 | . 36 | . 27 | . 35 | 33 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Brown | . 13 | . 17 | . 15 | . 09 | . 15 | . 13 |
| Brown: very rough | . 08 | . 13 | . 13 | . 10 | . 12 | . 11 |
| Black ..... | . 06 | . 09 | . 09 | . 09 | . 09 | . 8 |

Slates

| rk gray: smooth | . 09 | . 11 | . 11 | . 11 | . 11 | . 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| fairly rough | . 10 | . 11 | . 10 | . 09 | . 10 | . 10 |
| rough ...... | . 09 | . 10 | . 11 | . 11 | . 10 | . 10 |
| Greenish gray: rough | . 16 | . 11 | . 12 | . 13 | . 12 | . 13 |
| Mauve ......... | . 14 | . 16 | . 13 | . 10 | . 14 | . 13 |
| Blue gray | . 20 | . 16 | . 13 | . 12 | . 13 | . 15 |
| Silver gray (Norwegian) | . 22 | . 21 | . 21 | . 19 | . 21 | . 20 |

Other roofing materials

| Asbestos cement: white | . 35 | . 42 | . 41 | . 36 | . 41 | . 39 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| red | . 33 | . 33 | . 29 | . 14 | . 31 | . 26 |
| Enamelled steel : white | . 35 | . 53 | . 53 | . 57 | . 52 | . 52 |
| green | . 26 | . 34 | . 17 | . 13 | . 24 | . 25 |
| red | . 24 | . 26 | . 18 | . 08 | . 19 | . 19 |
| blue | . 23 | . 27 | . 17 | . 18 | . 20 | . 23 |
| Galvanized iron : new. | . 58 | . 30 | . 34 | . 34 | . 35 | . 35 |
| very dirty | . 10 | . 09 | . 09 | . 09 | . 09 | . 09 |
| whitewashed | . 63 | . 79 | . 79 | . 76 | . 78 | . 74 |
| Special roofing sheet: brown. | . 20 | . 15 | . 12 | . 07 | . 13 | . 13 |
| green | . 13 | . 20 | . 12 | . 12 | . 14 | . 15 |
| Bituminous felt | . 10 | . 12 | . 11 | . 11 | . 12 | . 11 |
| Aluminized felt | . 67 | . 60 | . 61 | . 57 | . 62 | . 60 |
| Weathered asphalt | . 12 | . 12 | . 11 | . 09 | . 11 | . 11 |
| Roofing lead: old. . | . 46 | . 20 | . 19 | . 15 | . 21 | . 23 |

## Bricks

| Gault : cream | . 74 | . 69 | . 64 | . 43 | . 64 | . 61 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Stock: light fawn | . 56 | . 47 | . 38 | . 19 | . 44 | . 39 |
| Fletton: light portion | . 67 | . 61 | . 57 | . 35 | . 58 | . 52 |
| dark portion | . 54 | . 46 | . 37 | . 15 | . 41 | . 37 |
| Wire cut : red | . 56 | . 48 | . 41 | . 15 | . 44 | . 39 |
| Sand-lime: red | . 41 | . 37 | . 30 | . 11 | . 32 | . 30 |
| Mottled purple | . 33 | . 26 | . 22 | . 15 | . 23 | . 23 |
| Stafford: blue |  | . 12 | . 11 | . 08 | . 11 | . 12 |
| Lime-clay (French) | . 57 | . 63 | . 52 | . 29 | . 54 | 49 |

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TABLE 585.-REFLECTION AND TRANSMISSION OF VARIOUS MATERIALS FOR VERY LONG WAVELENGTHS

With quartz, 1.7 cm thick : 60 to $80 \mu$, absorption very great; $63 \mu$, 99 percent ; $82 \mu, 97.5$; $97 \mu, 83$.

| Percentage reflection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wavelength | Iceland spar Marble | Rock salt | Sylvite | KBr | KI | Fluorite | Glass | Water | Alcohol |
| $\lambda=82 \mu$ * | - - | 25.8 | 36.0 | 82.6 | 29.6 | 19.7 | - | 9.6 | - |
| $\lambda=108 \mu \dagger$ | $47.1 \quad 43.8$ | 20.3 | 19.3 | 31.1 | 35.5 | 20.2 | 19.2 | 11.6 | 1.6 |
| Percentage transparency Uncorrected for reflections |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| Solid | Thickness | Transparency |  |  |  |  |  | hickness precipitable liquid | Trans. parency |
| Paraffin | 3.03 | 57.0 |  | Benzene |  | 1.00 |  | - | 56.8 |
| Mica | . 055 | 16.6 |  | Ethyl alcohol |  | . 158 |  | - | 7.9 |
| Hard rubber | . 40 | 39.0 |  | Ethyl ether |  | . 158 |  | - | 37.1 |
| Quartz \|| axis... | - 2.00 | 62.6 |  | Water ... |  | . 029 |  | - | 25.8 |
| Quartz, amorph | - 3.85 | 0 |  | Water |  | . 044 |  | - | 13.6 |
| Rock salt . . . . . | - . 21 | 21.5 |  |  |  |  |  |  |  |
| Fluorite | . 59 | 5.3 |  | Vapors: |  |  |  |  |  |
| Diamond | 1.26 | 45.3 |  | Alco | ol | . 2.00 |  | . 023 | 88 |
| Quartz ${ }_{\text {" }}$ axis | - 2.00 | 81.3 |  | Ethe | ... | . 2.0 |  | . 350 | 33.5 |
| " " | 4.03 | 66.4 |  | Benz | ne | . 2.00 |  | . 063 | 100 |
| " " " | . 7.26 | 49.8 |  | Wat | r | . . 4.0 |  | . 21 | 19.6 |
| " " " . | . 11.74 | 35.5 |  | $\mathrm{CO}_{2}$ |  | . 2.00 |  | - | 100 |
| " " | . 14.66 | 29.0 |  |  |  |  |  |  |  |

[^225]
## TABLE 586.-TRANSPARENCY OF BLACK ABSORBERS (percent)

| Method and wavelength |  | Black silk paper, .025 mm thick | Opaque black paper, .11 mm thick | Black cardboard .4 mm thick | $\begin{gathered} \text { Candle } \\ \text { ampplack, } \\ 10 \mathrm{~cm}^{2}=1.8 \\ \mathrm{mg} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Spectrometer |  | 0 | 0 | 0 | . 5 |
|  | 4 | . 9 | 0 | 0 | 8.6 |
|  | 6 | 1.7 | 0 | 0 | 16.0 |
|  | 12 | 8.2 | 1.4 | 0 | 37.6 |
| Fluorite "reststrahlen" | 26 | 24.2 | 32 | 0 | 76.7 |
| Rock salt "reststrahlen" . | 52 | 46.0 | 15.1 | 0 | 91.3 |
| Quartz lens isolation..... |  | 61.5 | 33.5 | 1.6 | 91.5 |

## TABLE 587.-RELATIVE REFLECTIVITY OF SNOW, SAND, AND OTHER MATERIALS ${ }^{173}$

|  | Maine sand | Florida sand $\dagger$ | Crushed quartz | Snow | Plaster of paris | White paper | Sodium $\ddagger$ carbonate | Sodium chloride | White cotton cloth § |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 3 to $.4 \mu$ | . 8 | 15 | 40 | 35 | 40 | 8 | 14 | 38 | 26 |
| .4 to $.8 \mu$ | . 25 | 40 | 50 | 40 | 53 | 30 | 28 | 49 | 42 |
| . 8 to $2.6 \mu$ | . 33 | 50 | 53 | 15 | 60 | 30 | 35 | 54 | 40 |
| 2.6 to $7 \mu$ | . 31 | 30 | 28 | 18 | 63 | 15 | 18 | 55 | 20 |
| $7 \mu \ldots$ | . 48 | . . | . . | 26 |  | . |  | . . |  |

[^226] SUBSTANCES

|  | Lamp-blacks |  |  |  |  |  |  |  | $\begin{aligned} & \stackrel{y}{x} \\ & \frac{0}{4} \\ & \frac{1}{4} \end{aligned}$ |  | $\begin{aligned} & \stackrel{\bigsqcup}{0} \\ & \text { a } \\ & \stackrel{y}{*} \\ & \stackrel{y y}{3} \end{aligned}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Wave- length $\mu$ | 薜 | $\begin{aligned} & \stackrel{g}{\ddot{W}} \\ & \stackrel{\circ}{\circ} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| . 60 | 3.2 |  |  |  |  |  |  | 52. | 84. | 82. |  | 89. | 15. | 1.8 | 14. | 30. |
| . 95 | 3.4 | 1.3 | 1.1 | . 6 | 1.3 | 1.1 |  |  | 88. | 86. | 75. | 93. |  |  | 21. |  |
| 4.4 | 3.2 | 1.3 | . 9 | . 8 | 1.2 | 1.4 |  | 51. | 21. | 8. | 18. | 29. |  | 3.7 |  |  |
| 8.8 | 3.8 |  | 1.3 | 1.2 | 1.6 | 2.1 |  | 26. | 2. | 3. | 5. | 11. |  | 2.7 |  | 12. |
| 24.0 | 4.4 | 3.0 | 4.0 | 2.1 | 5.7 | 4.2 |  | 10. | 6. | 5. |  | 7. |  |  |  |  |

## TABLE 589.-INFRARED REFLECTIVITY OF TUNGSTEN (Temperature variation)

Three tungsten mirrors were used-a polished Coolidge X-ray target and two polished flattened wires mounted in evacuated soft-glass bulbs with terminals for heating electrically. Weniger and Pfund, Journ. Franklin Inst.

| Wavelength in $\mu$ | Absolute reflectivity at room temperature in percent | Percent increase in reflectivity in going from room temperature to |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $1377^{\circ} \mathrm{K}$ | $1628^{\circ} \mathrm{K}$ | $1853^{\circ} \mathrm{K}$ | $2056^{\circ} \mathrm{K}$ |
| . 67 | 51 | $+6.0$ | +7.4 | + 8.7 | + 9.8 |
| . 80 | 55 | - | - | - | +8.2 |
| 1.27 | 70 | . 0 | . 0 | . 0 | . 0 |
| 1.90 | 83 | -6.6 | -8.2 | -9.6 | -11.0 |
| 2.00 | 85 | -7.5 | -9.3 | -10.9 | -12.3 |
| 2.90 | 92 | -7.7 | -9.4 | -11.1 | -12.5 |
| 4.00 | 93 | - | - | - | $-12.5$ |

TABLE 590.-RESTRAHLUNG BANDS FROM VARIOUS MATERIALS ${ }^{176}$ (percent)
(p)

| Number ofreflections $\quad$Crystal <br> mirrors | $\begin{gathered} \text { Filter } \\ \text { (3 mm paraffin } \\ \text { in each case) } \end{gathered}$ | Wavelength in $\mu$ | Frequency in $\sim / \mathrm{cm}$ |
| :---: | :---: | :---: | :---: |
| 4 ...... Quartz | 1 cm KCl | 20.7 | 483 |
| 3 ....... Fluorite | 5 mm KCl | 23 | 435 |
| 1 ....... Metal. |  |  |  |
| 2 ....... Fluorite | 3 mm KBr | 27.3 | 366 |
| 4 ...... Calcite |  | 29.4 | 340 |
| 3 ...... Fluorite | .4 mm quartz | 32.8 | 305 |
| 1 ....... Metal | 1.2 mm KBr |  |  |
| 3 ...... Aragonite | . 4 mm quartz | 41* | 244 |
| ${ }_{4}^{1} \ldots \ldots . . \begin{gathered}\text { Metal } \\ \end{gathered}$ |  |  |  |
| $4{ }_{4} \ldots \ldots . \cdot \mathrm{KaCl}^{\text {N }}$ | 2 mm ، quartz | 52 | 192 |
| $4 \ldots \ldots$ KBr | " | 83 | 120 |
| 4 ....... KI | " | 94 | 106 |
| $4 \ldots . . . \mathrm{TlBr}$ | " | 117 | 85 |
| 4 ...... Tli | " | 152 | 66 |
| Magnesium oxide | " | 22.5 | 444 |

[^227]556
TABLE 591.-INFRARED REFLECTING FACTOR OF VARIOUS MATERIALS* (percent)

|  | $\begin{aligned} \lambda & =20 \mu \\ \sim / \mathrm{cm} & =500 \end{aligned}$ | 25 400 | 333 <br> 300 | 50 200 | 668 150 150 | 100 100 | ${ }_{669}^{150 \mu}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rough brass | 67 | 70 | 78 | 83 | 92 | 96 | 100 |
| ough bras | 24 | 33 | 42 | 58 | 68 | 81 | 99 |
| " " | 12 | 14 | 17 | 21 | 25 | 40 | 82 |
| Galena | . 31 | 30 | 21 | 51 | 73 | 76 | 76 |
| Zincite | . 50 | 35 | 18 | 21 | 18 | 20 | 15 |
| $\beta$ magnesia, | .. 80 | 60 | 34 | 30 | 30 | 30 | 30 |
| Stibnite | .. 21 | 20 | 4 | 39 | 48 | 52 | 39 |
| Sphalerite | 10 | 15 | 29 | 20 | 19 | 18 | 17 |
| Corundum | ... (30) | 41 | 26 | 31 | 29 | 24 | 22 |
| Cuprite .. | ... 45 | 47 | 47 | 42 | 41 | 42 | 46 |

*For reference, see footnote 174, p. 555.

TABLE 592.-INFRARED TRANSMISSION OF VARIOUS MATERIALS*

|  | $\begin{aligned} \lambda & =20 \mu \\ \sim / \mathrm{cm} & =500 \end{aligned}$ | 25 400 | 335 300 | 50 200 | 663 150 | 100 100 | ${ }_{663} 150 \mu$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| KBr |  | 61 | 46 | 3 | .. | .. | .. |
| K l |  | 83 | 76 | 12 |  |  |  |
| Amorphous $\mathrm{SiO}_{2}$ | . 3 | 27 | 64 | 63 | 62 | 70 | 87 |
| CCl , liquid ...... | ... (57) | 63 | 50 | 74 | 74 | (72) | . |
| $\mathrm{KCl} \ldots$ | .... 97 | 97 | 96 | 93 | 80 | 98 |  |

* For reference, see footnote 174, p. 555.

TABLES 593-597.-ROTATION OF PLANE OF POLARIZED LIGHT

## TABLE 593.-TARTARIC ACID, CAMPHOR, SANTONIN, SANTONIC ACID, CANE SUGAR

A few examples are here given showing the effect of wavelength on the rotation of the plane of polarization. The rotations are for a thickness of one decimeter of the solution. The following symbols are used:

| $p=$ | number grams of the active substance in | 100 g of the solution. |
| :--- | :--- | :--- |
| $c=$ | solvent |  |
| $q=$ | $"$ | $"$ |

Right-handed rotation is marked + , left-handed - .

| Line of spectrum | Wavelength | Tartaric acid, $\mathrm{C}_{4} \mathrm{H}_{8} \mathrm{O}_{6}$, dissolved in water. $\begin{aligned} & q=50 \text { to } 95 . \\ & \text { temp }=24^{\circ} \dot{\mathrm{C}} \end{aligned}$ | Camphor, $\mathrm{C}_{10} \mathrm{H}_{16} \mathrm{O}$, dissolved in alcohol.$\begin{gathered} q=50 \text { to } 95 \\ \text { temp }=22.9^{\circ} \mathrm{C} \end{gathered}$ |  | Santonin, $\mathrm{C}_{13} \mathrm{H}_{18} \mathrm{O}_{3}$, dissolved in chloroform $\begin{aligned} & q=75 \text { to } 96.5, \\ & \text { temp }=20^{\circ} \mathrm{C} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| B | 6867 A |  |  |  | $-140: 1+.2085 q$ |
| C | 6562 | $+2: 748+.09446 q$ | 38:549 | 852 q | $-149.3+.1555 q$ |
| D | 5892 | $+1.950+.13030 q$ | 51.945 | 964 q | $-202.7+.3086 q$ |
| E | 5269 | $+.153+.17514 q$ | 74.331 | 343 q | $-285.6+.5820 q$ |
| $\mathrm{b}_{1}$ | 5183 |  |  |  | $-302.38+.6557 q$ |
| $\mathrm{b}_{2}$ | 5172 | $-.832+.19147 q$ | 79.348 | $451 q$ |  |
| F | 4861 | $-3.598+.23977 q$ | 99.601 | 912 q | $-365.55+.8284 q$ |
| e | 4383 | $-9.657+.31437 q$ | 149.696 | $346 q$ | $-534.98+1.5240 q$ |
|  |  |  | Santoni | ${ }_{15} \mathrm{H}_{18} \mathrm{O}_{3}$ | Santonic acid, |
|  |  | $\begin{aligned} & \text { Santonin, } \mathrm{C}_{15} \mathrm{H}_{18} \mathrm{O}_{3}, \\ & \text { dissolved in alco. } \\ & c=1.782 \\ & \text { temp }=20^{\circ} \mathrm{C} \end{aligned}$ | dissolved in alcohol. $c=4.046$ $\text { temp }=20^{\circ} \mathrm{C}$ | dissolved in chloroform. $c=3.1-30.5$ temp $=20^{\circ} \mathrm{C}$ | dissolved in chloroform. $c=27.192$ temp $=20^{\circ} \mathrm{C}$ |
| B | 6867 | $-110.4{ }^{\circ}$ | $442^{\circ}$ | $484^{\circ}$ | - $49^{\circ}$ |
| C | 6562 | -118.8 | 504 | 549 | - 57 |
| D | 5892 | -161.0 | 693 | 754 | - 74 |
| E | 5269 | -222.6 | 991 | 1088 | -105 |
| $\mathrm{b}_{1}$ | 5183 | -237.1 | 1053 | 1148 | -112 |
| $\mathrm{b}_{2}$ | 5172 | 1 | - | - | 13 |
| F | 4861 | -261.7 | 1323 | 1444 | -137 |
| e | 4383 | -380.0 | 2011 | 2201 | -197 |
| G | 4307 | - | - | - |  |
| g | 4226 | - | 2381 | 2610 | -230 |

Values obtained at the National Bureau of Standards for the rotation of sucrose are given below.

| Light source | $\frac{\operatorname{Rot} \lambda}{\operatorname{Rot} \lambda=5461 \mathrm{~A}}$ | $[a]^{20}{ }^{*}$ | Light source | $\frac{\operatorname{Rot} \lambda}{\operatorname{Rot} \lambda=5461}$ | $[\alpha]_{\lambda}^{20}{ }^{\text {* }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Li 6708 | . 644 | 50.45 | Cd 4678 | 1.403 | 109.9 |
| Cd 6438 | . 711 | 55.70 | Hg 4358 | 1.644 | 128.8 |
| Na 5892.5 | . 84922 | 66.529 | Ag 4208 | 1.786 | 139.9 |
| Hg 5780 | . 8854 | 69.36 | Hg 4047 | 1.95 | 152.8 |
| Hg 5461 | 1.0000 | 78.342 |  |  |  |
| Ag 5209 | 1.108 | 86.80 |  |  |  |
| Cd 5086 | 1.167 | 91.43 |  |  |  |
| Cd 4800 | 1.323 | 103.65 |  |  |  |

[^228]TABLE 594.-SODIUM CHLORATE; QUARTZ

| Sodium chlorate |  |  |  | Quartz |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Spec- } \\ & \text { trum } \\ & \text { line } \end{aligned}$ | $\begin{gathered} \text { Wave. } \\ \text { length } \end{gathered}$ | ${ }^{\text {Temp }}{ }^{\text {C }}$ | Rotation per mm | $\begin{aligned} & \text { Spec- } \\ & \text { trum } \\ & \text { Sine } \end{aligned}$ | Wave. length | Rotation per mm | $\begin{gathered} \text { Spec- } \\ \text { trum } \\ \text { line } \end{gathered}$ | Wave- | Rotation per mm |
| a | 7164 A | 15.0 | 2:068 | A | 7604 | 12:668 | $\mathrm{Cd}_{9}$ | 3609 | 63:628 |
| B | 6870 | 17.4 | 2.318 | a | 7164 | 14.304 | N | 3582 | 64.459 |
| C | 6563 | 20.6 | 2.599 | B | 6870 | 15.746 | $\mathrm{Cd}_{10}$ | 3465 | 69.454 |
| D | 5892 | 18.3 | 3.104 |  |  |  | 0 | 3441 | 70.587 |
| E | 5270 | 16.0 | 3.841 | C | 6563 | 17.318 |  |  |  |
| F | 4861 | 11.9 | 4.587 | $\mathrm{D}_{1}$ | 5896 | 21.684 | $\mathrm{Cd}_{11}$ | 3401 | 72.448 |
| $\mathrm{G}^{\prime}$ | 4340 | 10.1 | 5.331 | $\mathrm{D}_{2}$ | 5890 | 21.727 | P | 3360 | 74.571 |
| G | 4308 | 14.5 | 6.005 |  |  |  | Q | 3285 | 78.579 |
| H | 4101 | 13.3 | 6.754 | E | 5270 | 27.543 | $\mathrm{Cd}_{12}$ | 3247 | 80.459 |
| L | 3820 | 14.0 | 7.654 | F | 4862 | 32.773 |  |  |  |
| M | 3728 | 10.7 | 8.100 | G | 4308 | 42.604 | R | 3180 | 84.972 |
| N | 3581 | 12.9 | 8.861 |  |  |  | $\mathrm{Cd}_{17}$ | 2747 | 121.052 |
| P | 3361 | 12.1 | 9.801 | h | 4102 | 47.481 | $\mathrm{Cd}_{18}$ | 2571 | 143.266 |
| Q | 3287 | 11.9 | 10.787 | H | 3969 | 51.193 | $\mathrm{Cd}_{23}$ | 2312 | 190.426 |
| R | 3180 | 13.1 | 11.921 | K | 3934 | 52.155 |  |  |  |
| T | 3021 | 12.8 | 12.424 |  |  |  | $\mathrm{Cd}_{24}$ | 2264 | 201.824 |
| $\mathrm{Cd}_{17}$ | 2747 | 12.2 | 13.426 | L | 3820 | 55.625 | $\mathrm{Cd}_{25}$ | 2193 | 220.731 |
| $\mathrm{Cd}_{18}$ | 2571 | 11.6 | 14.965 | M | 3728 | 58.894 | $\mathrm{Cd}_{28}$ | 2143 | 235.972 |

TABLE 595.-REFLECTING FACTOR OF METALS (See Table 584)

| Wavelength | A1 | Sb | Cd | Co | Graphite | Ir | Mg | Mo | Pd | Rh | Si | Ta | Te | Sn | W | Va | Zn |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mu$ |  | Percents |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| . 5 | - | - | - | - | 22 | - | 72 | 46 | - | 76 | 34 | 38 | - | - | 49 | 57 | - |
| . 6 | - | 53 | - | - | 24 | - | 73 | 48 | - | 77 | 32 | 45 | 49 | - | 51 | 58 | - |
| . 8 | - | 54 | - | - | 25 | - | 74 | 52 | - | 81 | 29 | 64 | 48 | - | 56 | 60 | - |
| 1.0 | 71 | 55 | 72 | 67 | 27 | 78 | 74 | 58 | 72 | 84 | 28 | 78 | 50 | 54 | 62 | 61 | 80 |
| 2.0 | 82 | 60 | 87 | 72 | 35 | 87 | 77 | 82 | 81 | 91 | 28 | 90 | 52 | 61 | 85 | 69 | 92 |
| 4.0 | 92 | 68 | 96 | 81 | 48 | 94 | 84 | 90 | 88 | 92 | 28 | 93 | 57 | 72 | 93 | 79 | 97 |
| 7.0 | 96 | 71 | 98 | 93 | 54 | 95 | 91 | 93 | 94 | 94 | 28 | 94 | 68 | 81 | 95 | 88 | 98 |
| 10.0 | 98 | 72 | 98 | 97 | 59 | 96 | - | 94 | 97 | 95 | 28 | - | - | 84 | 96 | - | 98 |
| 12.0 | 98 | - | 99 | 97 | - | 96 | - | 95 | 97 | - | - | 95 | - | 85 | 96 | - | 99 |

The surfaces of some of the samples were not perfect so that the corresponding values have less weight. The following more recent values are given for tungsten and stellite, an exceedingly hard and untarnishable alloy of $\mathrm{Co}, \mathrm{Cr}, \mathrm{Mo}, \mathrm{Mn}$, and $\mathrm{Fe}(\mathrm{C}, \mathrm{Si}, \mathrm{S}, \mathrm{P}$ ).

| Wa | $\mu$, | . 15 | . 20 | . 30 | . 50 | . 75 | 1.00 | 2.00 | 3.00 | 4.00 | 5.00 | 9.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tungsten |  |  |  |  | . 50 | . 52 | . 576 | . 900 | . 943 | . 948 | . 953 | - |
| Stellite, |  | 32 | 42 | 50 | . 64 | . 67 | . 689 | 747 | 792 | . 825 | 848 | 880 |

## TABLE 596.—OPTICAL CONSTANTS OF METALS

Two constants are required to characterize a metal optically, the refractive index, $n$, and the absorption index, $k$, the latter of which has the following significance: the amplitude of a wave after traveling one wavelength, $\lambda^{1}$ measured in the metal, is reduced in the ratio 1: $\exp (-2 \pi k)^{*}$ or for any distance $d 1: \exp \left(-2 \pi d k / \lambda^{1}\right)$, for the same wavelength measured in air this ratio becomes $1: \exp \left(-2 \pi d n k / \lambda^{1}\right), n k$ is sometimes called the extinction coefficient. Plane polarized light reflected from a polished metal surface is in general elliptically polarized because of the relative change in phase between the two rectangular components vibrating in and perpendicular to the plane of incidence. For a certain angle, $\bar{\phi}$ (principal incidence) the change is $90^{\circ}$ and if the plane polarized incident beam has a certain azimuth $\bar{\psi}$ (principal azimuth) circularly polarized light results.

$$
k=\tan 2 \bar{\psi}\left(1-\cot ^{2} \bar{\phi}\right) \text { and } n=\frac{\sin \bar{\phi} \tan \bar{\phi}}{\left(1+k^{2}\right)^{1}}\left(1+\frac{1}{2} \cot ^{2} \bar{\phi}\right) .
$$

(continued)

For rougher approximations the factor in parentheses may be omitted. $R=$ computed percentage reflection.
(The points have been so selected that a smooth curve drawn through them closely indicates the characteristics of the metal.)

| Metal | $\lambda$ | $\bar{\phi}$ | $\bar{\downarrow}$ | Computed |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $n$ | $k$ | $n k$ | $R$ |
| Cobalt | $\stackrel{\mu}{\mu}$ | $64^{\circ} 31^{\prime}$ | $29^{\circ} 39$ | 1.10 | 1.30 | 1.43 | \% 32. |
|  | . 275 | 7022 | 2959 | 1.41 | 1.52 | 2.14 | 46. |
|  | . 500 | 775 | 3153 | 1.93 | 1.93 | 3.72 | 66. |
|  | . 650 | 790 | 3125 | 2.35 | 1.87 | 4.40 | 69. |
|  | 1.00 | 8145 | 296 | 3.63 | 1.58 | 5.73 | 73. |
|  | 1.50 | 8321 | 2618 | 5.22 | 1.29 | 6.73 | 75. |
|  | 2.25 | 8348 | 265 | 5.65 | 1.27 | 7.18 | 76. |
| Copper | . 231 | 6557 | 2614 | 1.39 | 1.05 | 1.45 | 29. |
|  | . 347 | 656 | 2816 | 1.19 | 1.23 | 1.47 | 32. |
|  | . 500 | 7044 | 3346 | 1.10 | 2.13 | 2.34 | 56. |
|  | . 650 | 7416 | 4130 | . 44 | 7.4 | 3.26 | 86. |
|  | . 870 | 7840 | 4230 | . 35 | 11.0 | 3.85 | 91. |
|  | 1.75 | 844 | 4230 | . 83 | 11.4 | 9.46 | 96. |
|  | 2.25 | 8513 | 4230 | 1.03 | 11.4 | 11.7 | 97. |
|  | 4.00 | 8720 | 4230 | 1.87 | 11.4 | 21.3 |  |
|  | 5.50 | 8800 | 4150 | 3.16 | 9.0 | 28.4 |  |
| Gold | 1.00 | 8145 | 4400 | . 24 | 28.0 | 6.7 |  |
|  | 2.00 | 8530 | 4356 | . 47 | 26.7 | 12.5 |  |
|  | 3.00 | 8705 | 4350 | . 80 | 24.5 | 19.6 |  |
|  | 5.00 | 8815 | 4325 | 1.81 | 18.1 | 33. |  |
| Iridium | 1.00 | 8210 | 2920 | 3.6 | 1.60 | 5.8 |  |
|  | 2.00 | 8440 | 2810 | 6.0 | 1.48 | 8.9 |  |
|  | 3.00 | 8540 | 2640 | 8.0 | 1.37 | 11.0 |  |
|  | 5.00 | 8720 | 2400 | 12.5 | 1.13 | 14.1 |  |
| Nickel | . 420 | 7220 | 3142 | 1.41 | 1.79 | 2.53 | 54. |
|  | . 789 | 761 | 3141 | 1.79 | 1.86 | 3.33 | 62. |
|  | . 750 | 7845 | 326 | 2.19 | 1.99 | 4.36 | 70. |
|  | 1.00 | 8033 | 322 | 2.63 | 2.00 | 5.26 | 74. |
|  | 2.25 | 8421 | 3330 | 3.95 | 2.33 | 9.20 | 85. |
| Platinum | 1.00 | 8200 | 3030 | 3.4 | 1.82 | 6.2 |  |
|  | 2.00 | 8445 | 2940 | 5.7 | 1.70 | 9.7 |  |
|  | 3.00 | 8600 | 2850 | 7.7 | 1.59 | 12.3 |  |
|  | 5.00 | 8715 | 2700 | 11.5 | 1.37 | 15.7 |  |
| Silver | . 226 | 6241 | 2216 | 1.41 | . 75 | 1.11 | 18. |
|  | . 293 | 6314 | 1856 | 1.57 | . 62 | . 97 | 17. |
|  | . 316 | 5228 | 1538 | 1.13 | . 38 | . 43 | 4. |
|  | . 332 | 521 | 372 | . 41 | 1.61 | . 65 | 32. |
|  | . 395 | 6636 | 436 | . 16 | 12.32 | 1.91 | 87. |
|  | . 500 | 7231 | 4329 | . 17 | 17.1 | 2.94 | 93. |
|  | . 759 | 7535 | 4347 | . 18 | 20.6 | 3.64 | 95. |
|  | . 750 | 7926 | 446 | . 17 | 30.7 | 5.16 | 97. |
|  |  | 820 | 442 | . 24 | 29.0 | 6.96 | 98. |
|  | 1.50 | 8442 | 4348 | . 45 | 23.7 | 10.7 | 98. |
|  | 2.25 | 8618 | 4334 | . 77 | 19.9 | 15.4 | 99. |
|  | 3.00 | 8710 | 4240 | 1.65 | 12.2 | 20.1 |  |
|  | 4.50 | 8820 | 4110 | 4.49 | 7.42 | 33.3 |  |
| Steel | . 226 | 6651 | 2817 | 1.30 | 1.26 | 1.64 | 35. |
|  | . 257 | 6835 | 2845 | 1.38 | 1.35 | 1.86 | 40. |
|  | . 325 | 6957 | 309 | 1.37 | 1.53 | 2.09 | 45. |
|  | . 500 | 7547 | 292 | 2.09 | 1.50 | 3.14 | 57. |
|  | . 650 | 7748 | $27 \quad 9$ | 2.70 | 1.33 | 3.59 | 59. |
|  | 1.50 | 8148 | 2851 | 3.71 | 1.55 | 5.75 | 73. |
|  | 2.25 | 8322 | 3036 | 4.14 | 1.79 | 7.41 | 80. |

[^229]TABLE 597.-OPTICAL CONSTANTS OF METALS (additional data)

| Metal | $\lambda$ | $n$ | $k$ | $R$ | Metal | $\lambda$ | $n$ | $k$ | $R$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mu$ |  |  |  |  | $\mu$ |  |  |  |
| Al * | . 589 | 1.44 | 5.32 | 83 | Ni * | . 275 | 1.09 | 1.16 | 24 |
| Sb* | . 589 | 3.04 | 4.94 | 70 |  | . 441 | 1.16 | 1.23 | 25 |
| Bit ${ }^{\text {t }}$ | white | 2.26 | - | - |  | . 589 | 1.30 | 1.97 | 43 |
| Cd* | . 589 | 1.13 | 5.01 | 85 | Rh * | . 579 | 1.54 | 4.67 | 78 |
| Cr* | . 579 | 2.97 | 4.85 | 70 | Se $\ddagger$ | . 400 | 2.94 | 2.31 | 44 |
| Nb * | . 579 | 1.80 | 2.11 | 41 |  | . 490 | 3.12 | 1.49 | 35 |
| $\mathrm{Au}^{\dagger}$ | . 257 | . 92 | 1.14 | 28 |  | . 589 | 2.93 | . 45 | 25 |
|  | . 441 | 1.18 | 1.85 | 42 |  | . 760 | 2.60 | . 06 | 20 |
|  | . 589 | . 47 | 2.83 | 82 | Si* | . 589 | 4.18 | . 09 | 38 |
| I crys | . 589 | 3.34 | . 57 | 30 |  | 1.25 | 3.67 | . 08 | 33 |
| Ir* | . 579 | 2.13 | 4.87 | 75 |  | 2.25 | 3.53 | . 08 | 31 |
| Fe § | . 257 | 1.01 | . 88 | 16 | Na (liq) | . 589 | . 004 | 2.61 | 99 |
|  | . 441 | 1.28 | 1.37 | 28 | Ta** | . 579 | 2.05 | 2.31 | 44 |
|  | . 589 | 1.51 | 1.63 | 33 | Sn* | . 589 | 1.48 | 5.25 | 82 |
| Pb * | . 589 | 2.01 | 3.48 | 62 | W * | . 579 | 2.76 | 2.71 | 49 |
| Mg* | . 589 | . 37 | 4.42 | 93 | $\mathrm{V}^{*}$ | . 579 | 3.03 | 3.51 | 58 |
| Mn* | . 579 | 2.49 | 3.89 | 64 | Zn* | . 257 | . 55 | . 61 | 20 |
| Hg (liq) | . 326 | . 68 | 2.26 | 66 |  | . 441 | . 93 | 3.19 | 73 |
|  | . 441 | 1.01 | 3.42 | 74 |  | . 589 | 1.93 | 4.66 | 74 |
|  | . 589 | 1.62 | 4.41 | 75 |  | . 668 | 2.62 | 5.08 | 73 |
|  | . 668 | 1.72 | 4.70 | 77 |  |  |  |  |  |
| Pd* | . 579 | 1.62 | 3.41 | 65 37 | $\begin{aligned} & \lambda 三 \text { wavel } \\ & k \equiv \text { absor } \end{aligned}$ | ion ind | $\begin{aligned} \text { refrac } \\ R= \end{aligned}$ | $\begin{aligned} & \text { index } \\ & \text { ction. } \end{aligned}$ | cent. |
| $\mathrm{Pt} \dagger$ | . 257 | 1.17 | 1.65 | 37 |  |  |  |  |  |
|  | . 441 | 1.94 | 3.16 | 58 |  |  |  |  |  |
|  | . 589 | 2.63 | 3.54 | 59 |  |  |  |  |  |
|  | . 668 | 2.91 | 3.66 | 59 |  |  |  |  |  |

* Solid. † Electrolytic. $\ddagger$ Prism. § Deposited as film in vacuo.


## TABLES 598-601.-MEDIA FOR DETERMINATIONS OF REFRACTIVE INDICES WITH THE MICROSCOPE

TABLE 598.-LIQUIDS, $n_{D}(0.589 \mu)=1.74$ to 1.78
In 100 parts of methylene iodide at $20^{\circ} \mathrm{C}$ the number of parts of the various substances indicated in the following table form saturated solutions having the refractive indices specified. When ready for use the liquids can be mixed to give intermediate refractions. Commercial iodoform $\left(\mathrm{CHI}_{3}\right)$ powder is not suitable, but crystals from a solution of the powder in ether may be used, or the crystallized product may be bought. A fragment of tin in the liquids containing the $\mathrm{SnI}_{4}$ will prevent discoloration.

| $\mathrm{CHI}_{3}$ | $\mathrm{SnI}_{4}$ | $\mathrm{AsI}_{3}$ | $\mathrm{SbI}_{3}$ | $S$ | $\eta_{\text {na }}$ at $20^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 25 |  | 12 |  | 1.764 |
|  | 25 |  | 12 |  | 1.783 |
|  | 30 |  |  | 6 | 1.806 |
|  | 27 | 13 | 7 |  | 1.820 |
| 40 | 27 | 16 |  | 1.826 |  |
| 35 | 31 | 14 | 8 | 10 | 1.842 |
|  | 31 | 16 | 8 | 10 | 1.853 |

TABLE 599.-RESINLIKE SUBSTANCES, $n_{D}(0.589 \mu)=1.68$ to 2.10
Piperine, an inexpensive alkaloid, comes in very pure straw-colored crystals. Melted, it dissolves the tri-iodides of Sb and As very freely. The solutions are fluid at slightly above $100^{\circ}$ and when cold, resinlike. Three parts antimony iodide to one part of arsenic iodide with varying proportions of piperine are easier to manipulate than one containing either iodide alone. In preparing, the constituents, in powder of about 1 mm grain, should be weighed out and then fused over, not in, a low flame. Three-inch test tubes are suitable.

| Percent iodides | 00 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Index of refraction. . . 1.683 | 1.700 | 1.725 | 1.756 | 1.794 | 1.840 | 1.897 | 1.968 | 2.050 |  |

## TABLE 600.-PERMANENT STANDARD RESINOUS MEDIA, $n_{\mathrm{D}}(0.589 \mu)=1.546$ to 1.682

Any proportions of piperine rosin form a homogeneous fusion which cools to a transparent resinous mass. On account of the strong dispersion of piperine the refractive indices of minerals apparently matched with those of mixtures rich in this constituent are 0.005 to 0.01 too low. To correct this error a screen made of a thin film of 7 percent antimony iodide and 93 percent piperine should be used over the eyepiece. Any amber-colored rosin in lumps is suitable.

| Percent rosin <br> Index of <br> refraction$\ldots \ldots$ | 00 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

TABLE 601.-SUBSTANCES, $n_{\mathrm{p}}=1.39$ to 1.75

|  | $n$ |  |  | $n$ | $n$ |
| :--- | :---: | :--- | :---: | :--- | :---: |
| n-Heptane | 1.39 | Eugenol | 1.54 | Quinaldine | 1.61 |
| Octylene | 1.41 | Nitrobenzene | 1.55 | Iodobenzene | 1.62 |
| Cyclohexane | 1.44 | Anethole | 1.56 | a-Chloronaphthalene | 1.63 |
| d-Limonene | 1.47 | o-Toluidine | 1.57 | a-Bromonaphthalene | 1.66 |
| p-Xylene | 1.50 | o-Bromophenol | 1.58 | a-Iodonaphthalene | 1.69 |
| Chlorobenzene | 1.53 | Bromoform | 1.59 | Methylene iodide | 1.75 |

## TABLE 602.-SENSITOMETRIC CONSTANTS OF TYPE PLATES AND FILMS, DEFINITIONS

Density ( $D$ ).-Density is a measure of the degree of blackening of an exposed film or plate after development. Density is defined in general terms as the logarithm of the ratio of the radiant flux, $P_{0}$, incident on the sample to the radiant flux, $P_{t}$, transmitted by the sample.


Fig. 27.-Typical characteristic curve. Ordinates are diffuse transmission density ( $D$ ) : abscissae, $\log$ s of exposure $(\log E) . A-C=$ toe, $C-E=$ straight line, $E-F=$ shoulder, $B=$ speed point, $B-D=\Delta \log E=1.50$. Tan $a=\gamma$, Tan $b=\beta$, Tan $a=0.3 \beta$.

$$
D=\log \left(\frac{P_{0}}{P_{\mathrm{t}}}\right)
$$

Exposure ( $E$ ). $-E=I t$ (expressed in meter-candle seconds). $I=$ illumination (metercandles, mc ) incident on the photographic material during exposure, $t=$ exposure time in seconds.

Gamma ( $\gamma$ ).-Gamma is defined as the tangent of the angle alpha (a) (fig. 27) which the straight-line part of the characteristic curve makes with the log-exposure axis.

Gamma infinity $\left(\gamma_{\infty}\right) .-\gamma_{\infty}$ is defined as the limiting value to which gamma approaches as development time is increased.

Time of development for the half gamma infinity ( $t_{\gamma}=\gamma_{\infty} / 2$ ). A convenient practical specification of development rate of significance in comparing developers.

Time of development for gamma of unity ( $t_{\gamma}=1.0$ ). - A convenient practical specification of development rate of significance in comparing photographic materials. Comparisons must be confined to materials in the same developer.

Inertia ( $i$ ). $-i=$ the value of exposure where the straight-line portion of the characteristic curve (fig. 27) extended cuts the $\log E$ axis.

Speed $\left(S_{c}\right)-S_{0}=1 / E$, where $E$ is the exposure corresponding to point $B$ on the $D-\log E$ curve in figure 27. This point is located in the following manner: A $\log$ exposure range of 1.50 , represented in the figure by the distance along the log exposure axis between $B$ and $D$, is selected in a region where the slope of the curve at the low end of the range is 0.30 of the average slope over the entire range. When the slope, or tangent of angle $a$, is 0.30 of the tangent of angle $b$, the point $B$, at the low end of the exposure range, represents the exposure value $(E)$ from which the speed of the material is derived.

[^230]In the determination of the values given in Table 604, developing solutions made up according to the following formulas were used (temperature, $20^{\circ} \mathrm{C}$ ):
Developer A:
Monomethyl para-aminophenol sulfate *.............................. 2.0 grams
Sodium sulfite (anhydrous)
Hydroquinone .......................................................... 4.0 "
Sodium carbonate (anhydrous).............................................. 6.0 "
Potassium bromide .............................................................. . 75 "
Air-free distilled water to make........................................ 1.0 liter
Developer B:
Monomethyl para-aminophenol sulfate *.............................. $\quad 2.0$ grams
Sodium sulfite (anhydrous)
80.0 "

Hydroquinone ............................................................. 4.0
Borax.................................................................. 4.0 "
Potassium bromide ....................................................... . . . 5 "
Air-free distilled water to make................................................ 1.0 liter
Developer C:

Monomethyl para-aminophenol sulfate *................................... 2.2 grams
Sodium sulfite (anhydrous).............................................. . . . . . 96.0
Hydroquinone .................................................................. 8.8
Sodium carbonate, monohydrated....................................... 56.0 "
Potassium bromide .................................................... 5.0 " "
Air-free distilled water to make............................................... 1.0 liter

- Sold under such trade names as Metol, Elon, Rhodol, and Pictol.

TABLE 604.-SENSITOMETRIC CONSTANTS OF TYPE PLATES AND FILM


## Sheet films and plates

| Fast panchromatic | A | 1.45 | 2.6 | 5.2 | 2500 | 500 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fast orthochromatic | A | 1.50 | 2.0 | 4.2 | 1700 | 400 |
| Medium-speed panchromatic .. | A | 1.50 | 3.6 | 6.3 | 840 | 200 |
| Medium-speed orthochromatic. . | A | 1.25 | 2.7 | 9.9 | 850 | 200 |
| Blue-sensitive | A | 1.35 | 2.7 | 5.7 | 430 | 100 |
| Amateur roll films |  |  |  |  |  |  |
| Fast panchromatic | A | 1.28 | 2.9 | 6.6 | 2500 | 400 |
| Fast orthochromatic | A | 1.25 | 2.2 | 5.7 | 1300 | 200 |
| Fine-grain panchromatic | A | 2.50 | 5.5 | 4.2 | 400 | 100 |
| Process films and plates |  |  |  |  |  |  |
| Panchromatic | C | 6.90 | 3.3 | 8 | 60 | $\ldots$ |
| Orthochromatic .............. |  | 5.00 | 2.00 | . 7 | 60 |  |
| Blue-sensitive ................. | C | 4.00 | 2.7 | 1.7 | 35 | $\ldots$ |

[^231]
## TABLE 605.-COMPARISON OF NUCLEAR AND OPTICAL EMULSIONS

Nuclear track plates differ markedly in physical composition and general characteristics from the ordinary photographic materials (optical type) as shown in the table, where a number of properties of optica! and nuclear emulsions are compared.

| Property | Optical type | Nuclear type |
| :---: | :---: | :---: |
| AgBr : gelatin ( wt ) | . 47 :53 | 80:20 |
| AgBr : gelatin (vol) | . 15:85 | 45:55 |
| Grain diameter | . 5 to $3 \mu$. | . 1 to $.4 \mu$ |
| Emulsion thickness | . $10 \mu$ | $25-300 \mu$ |
| Emulsion wt mg/ $\mathrm{cm}^{2}$. | .2-4 | 10-80 |
| Sensitivity to light. | . Very high | Low |
| Response to $\alpha$-particles | . High | Individual tracks |
| Response to $\beta$-particles | . Moderate | Individual tracks |
| Response to $\boldsymbol{\gamma}$-rays. | . Low | Very low |

TABLE 606.-RESOLVING POWER AND EDGE GRADIENT VALUES ${ }^{175}$

## Part 1.-Definitions

Resolving power ( $R$ ).-The resolving power of a photographic material is broadly defined as the ability to record fine detail distinguishably. Any quantitative evaluation depends on the type of detail, and for convenience parallel lines separated by spaces whose width is equal to the common width of the lines are almost universally used. ${ }^{179}$ Values are usually given as the number of lines per millimeter that can be resolved visually under adequate magnification.

Resolving power increases with increasing exposure to a maximum and then decreases, It is relatively unaffected by the type of developer, although developers that markedly reduce the grain size improve resolution. As the development time increases from zero, resolving power rises rapidly to a maximum, decreases slightly, and then remains sensibly constant for all practical development times. It increases in a roughly exponential manner as the contrast in the test object increases from zero, becoming substantially constant for contrasts exceeding about $100: 1$. Its dependence on wavelength is less well known, but in general it increases as wavelength decreases because of the increasing opacity of the emulsion. Although resolving power tends to increase as granularity decreases, this is by no means always the case. The values given in Table 608 apply when the ratio of brightness of the light to the dark lines is $1000: 1$ and the test object is photographed with an especially well-corrected $f / 5$ lens in tungsten light with the optimum exposure; the materials were developed for practical times in the developer for which the data are given in Table 604.

As thus specified, resolving power is a threshold phenomenon and is not a criterion of the clearness with which gross details will be reproduced. Furthermore, it is of questionable value when the image is to be scanned with a physical photometer because the effect of granularity depends upon the design of the instrument.

Edge gradient $(G)$.-The appearance of sharpness produced by a photographic image probably depends, among other factors, upon the rate of change of density across the edge of the image with distance measured normal to the boundary. The curve of density vs distance resembles the $H$ and $D$ curve, and its gradient, called edge gradient to distinguish it from the gradient of the $H$ and $D$ curve, passes through a maximum with respect to distance. The values of this maximum for the respective materials in density units per micron are given in Table 608. These values were determined with a test object consisting of an extremely sharp, clear line in an opaque background on a high-resolution plate. This test object was pressed firmly against the sample with a contact liquid between and the combination was exposed to light from an $f / 5$ lens. The resulting image was scanned with a physical microphotometer having a comparatively narrow slit.

The determinants of edge gradient have been less studied than have the determinants of resolving power, but it is known that the maximum gradient has a maximum with respect to exposure. It would be expected that the maximum gradient would increase in gamma, but present knowledge indicates that it increases less rapidly. The dependence on wavelength has not been studied with modern techniques, but older studies indicate that gradient increases with decreasing wavelength. The values in Table 608 are for $\gamma \infty / 2$ and tungsten light at the optimum exposure.

Both resolving power and edge gradient are inherent properties of the emulsion and are relatively inflexible. It is possible to improve them by bathing the material in dye that absorbs the light to which the emulsion is sensitive, but this is rarely practical because of the concomitant reduction in speed.

[^232]
# TABLE 606.-RESOLVING POWER AND EDGE GRADIENT VALUES (concluded) <br> Part 2.-Values 

| Material | Resolving power | $\begin{gathered} \text { Edge } \\ \text { gradient } \\ \left(\times 10^{-2}\right) \end{gathered}$ |
| :---: | :---: | :---: |
| Motion-picture films : |  |  |
| Fast panchromatic | 95 | 8 |
| Medium-speed panchromatic | 100 | 9 |
| Fine-grain panchromatic | 100 | 10 |
| Positive (regular) | 105 | 18 |
| Positive (fine-grain) | 130 | 22 |
| Professional sheet films: |  |  |
| Fast panchromatic | 85 | 11 |
| Fast orthochromatic | 100 | 10 |
| Medium-speed panchromatic | 75 | 10 |
| Medium-speed orthochromatic | 75 | 11 |
| Blue-sensitive . .............. | 90 | 10 |
| Amateur roll films : |  |  |
| Fast panchromatic | 95 | 10 |
| Fast orthochromatic | 100 | 11 |
| Fine-grain panchromatic | 105 | 12 |
| Process films and plates: |  |  |
| Panchromatic film. | 125 | 22 |
| Orthochromate film | 130 | 23 |
| Blue-sensitive plates | 110 | 18 |
| High resolution plates:. | 2,500 * |  |

[^233]TABLE 607.-RELATIVE PHOTOGRAPHIC EFFICIENCY OF ILLUMINANTS


## TABLE 608.-SPECTRAL SENSITIVITY OF PHOTOGRAPHIC MATERIALS

Spectral sensitivity is normally expressed in terms of the reciprocal of the energy (ergs $/ \mathrm{cm}^{2}$ ) at various wavelengths required to produce a given density under given conditions of development. The curves in figure 28 are shown for a scale of relative sensitivity values, with a value of 10 assigned to the point of maximum sensitivity. The curves should be regarded only as representative of the type of sensitizing for which they were determined and are not suitable for quantitative use. In figure 29 spectral sensitivity data are presented in a different form. Here the wavelengths to which classes of spectroscopic plates are sensitive are shown in a block diagram. No indications are given of the way in which sensitivity varies with wavelength. A solid portion of the block diagram indicates the spectral region for which the class is especially valuable, i.e., where the sensitizing is most effective.


Fig. 28.-Spectral sensitivity curves for typical films: 1, blue sensitive; 2, orthochromatic; 3, panchromatic; 4, infrared sensitive.


Fig. 29.-The range of spectral sensitivity of kodak spectroscopic plates.

## TABLE 609.-NUCLEAR TRACK PLATE SPECIFICATIONS



## TABLES 610-625A.-STANDARD WAVELENGTHS ${ }^{177-102}$ AND SERIES RELATIONS IN ATOMIC SPECTRA*

Primary standard of wavelength.-The red radiation, $6438.4696 A$, emitted by a cadmium lamp of Michelson type was first chosen in 1907 by the International Union for Cooperation in Solar Research ${ }^{177}$ as a primary standard of wavelength and definition of the angstrom as a unit of wavelength measurement. This primary standard was adopted in 1922 by the International Astronomical Union ${ }^{178}$ and in 1927 by the International Committee on Weights and Measures ${ }^{179}$ with the statement that the wavelength of this radiation is $6438.4696 \times 10^{-10}$ meters when the light is propagated in dry air at $15^{\circ} \mathrm{C}$ (hydrogen thermometer) at a pressure of 760 mmHg , gravity being 980.665 $\mathrm{cm} / \mathrm{sec}^{2}$.

Specifications for the standard cadmium lamp were last revised in 1935; ${ }^{180}$ they designate that the lamp must be Michelson H-type with internal electrodes, excited with continuous or alternating current of industrial frequency, maintained at a temperature near $300^{\circ} \mathrm{C}$ (never exceeding $320^{\circ} \mathrm{C}$ ) and contain air under a pressure between 0.7 and 1.0 mmHg at that temperature. The constriction must not be less than 2 mm diameter and the current must not exceed 7 milliamps/ $\mathrm{mm}^{2}$.

A summary of nine directly measured values of the wavelength of the red radiation of cadmium in terms of the meter has been given by H . Barrell ${ }^{181}$ as in Table 612.
${ }^{177-102}$ For footnotes 177-192, see p. 578.

* Data furnished and arranged by W. F. Meggers, National Bureau of Standards.


## TABLE 610.-PRELIMINARY VALUES OF Hg ${ }^{188}$ WAVELENGTHS IN ANGSTROMS

| N.B.S. (U.S.A.) | N.P.L. (England) | I.B.W.M. (France) | Mean |
| :---: | :---: | :---: | :---: |
| 5790.6628 | 5790.6628 | 5790.6630 | 5790.6629 |
| 5769.5983 | 5769.5985 | 5769.5986 | 5769.5985 |
| 5460.7532 | 5460.7531 | 5460.7533 | 5460.7532 |

International secondary standards of wavelength from neon, krypton, and iron spectra.-Spectroscopic secondary standards of wavelength are derived from the primary standard (Cd 6438.4696 A ) by means of the Fabry-Perot interferometer. The existing international secondary standards represent the mean of three or more independent, concordant values adopted by the International Astronomical Union. All values of secondary standards of wavelength are valid for normal air ( $15^{\circ} \mathrm{C}$ and 760 mmHg ). The most precisely determined secondary standards of wavelength have been obtained from discharge tubes of the Geissler type containing neon or krypton gas at a pressure not exceeding 15 mmHg . In 1935 the International Astronomical Union ${ }^{183}$ adopted 8 -figure values of 20 neon wavelengths with the reservation that they apply only to the conditions under which they were determined, viz, with interferometers of high resolving power but plate separations not exceeding 40 mm .
${ }^{129}$ For reference, see p. 578.

TABLE 611.-NEON SECONDARY STANDARD WAVELENGTHS IN ANGSTROMS

| 5852.4878 | 6074.3377 | 6266.4950 | 6532.8824 |
| :--- | :--- | :--- | :--- |
| 5881.8950 | 6096.1630 | 6304.7892 | 6598.9529 |
| 5944.8342 | 6143.0623 | 6334.4279 | 6678.2764 |
| 5975.5340 | 6163.5939 | 6382.9914 | 6717.0428 |
| 6029.9971 | 6217.2813 | 6506.5279 | 7032.4127 |

[^234][^235]TABLE 612.-VALUES OF THE WAVELENGTH OF THE CADMIUM RED LINE IN TERMS OF THE INTERNATIONAL METER (Unit $=1 \times 10^{-10} \mathrm{~m}$ )

|  |  |  |  | Diffe | rences mean |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Date of determination | bservers | Original values | $\begin{gathered} \text { and adjusted } \\ \text { values in } \\ \text { normal air } \end{gathered}$ | $10^{-10} \mathrm{~m}$ | $\begin{aligned} & \text { Parts } \\ & 10^{\circ} \end{aligned}$ |
| 1892-93 | Michelson and Benoit (B.I.P.M.) | 6438.4722 | 6438.4691 | -. 0005 | $-.08$ |
| 1905-06 | Benoit, Fabry and Perot | 6438.4696 | 6438.4703 | $+.0007$ | +. 11 |
| 1927 | Watanabe and Imaizumi | 6438.4685 | 6438.4682 | -. 0014 | -. 22 |
|  | (Tokyo) Sears and Barrell |  |  |  |  |
| 1933 | Sears and Barrell (N.P.L.) | 6438.4711 | 6438.4713 | $+.0017$ | +. 26 |
| 1933 | Kösters and Lampe <br> (P.T.R.) | 6438.4672 | 6438.4689 | -. 0007 | -. 11 |
| 1934-35 | Sears and Barrell | 6438.4709 | 6438.4709 | +.0013 | +. 20 |
| 1934-35 | Kösters and Lampe | 6438.4685 | 6438.4690 | -. 0006 | -. 09 |
|  | (P.T.R.) |  |  |  |  |
| 1937 | Kösters and Lampe <br> (P.T.R.) | 6438.4700 | 6438.4700 | $+.0004$ |  |
| 1940 | Romanova, Varlich, Kartashev, and Batarchukova (Leningrad) | 6438.4677 | 6438.4687 | -. 0009 | -. 14 |
|  |  | Mean | 6438.4696 | $\pm .0009$ | $\pm .14$ |

The values originally reported (column 3) are corrected (column 4) to take account of subsequent conclusions (a) regarding the values to be attributed to the standards of length employed, and adjusted (b), so far as the available information permits, to uniform standard conditions of dry air at $15^{\circ} \mathrm{C}$ and 760 mmHg pressure, containing 0.03 percent $\mathrm{CO}_{2}$. The statistical mean deviation associated with the average value of $6438.4696 \times 10^{-10} \mathrm{~m}$ derived from these nine determinations amounts to $\pm 0.0010 \times 10^{-10} \mathrm{~m}$.

The recent production of purer monochromatic radiation (than the cadmium red line) suggests that eventually another wavelength from a single heavy isotype of even mass number may be adopted as the primary standard of length. Thus, since 1945 many milligrams of $\mathrm{Hg}^{108}$ have been made by transmutation of gold in chain-reacting uranium piles. Electrodeless lamps containing $\mathrm{Hg}^{188}$ have been made and distributed by the National Bureau of Standards. When excited by ultra-high frequency ( $>100$ megacycles) and water cooled these lamps emit with high intensity ideally sharp mercury lines. Preliminary measurements, relative to Cd 6438.4696 A , of the yellow and green lines of $\mathrm{Hg}^{198}$ have been reported ${ }^{182}$ by the National Bureau of Standards, by the National Physical Laboratory, and by the International Bureau of Weights and Measures, as in Table 610.

[^236]TABLE 613.-RESULTANT S VALUES AND TERM MULTIPLICITIES

| Number of <br> electrons | $s$ | Term multiplicities |
| :---: | :--- | :--- |
| 1 | $1 / 2$ | Doublets |
| 2 | $0,1,3 / 2$ | Singlets, triplets |
| 3 | $1 / 2,32$ | Doublets, quartets |
| 4 | $0,1,2$ | Singlets, triplets, quintets |
| 5 | $1 / 2,3 / 2,5 / 2$ | Doublets, quartets, sextets |
| 6 | $0,1,2,3,5 / 2,7 / 2$ | Singlets, triplets, quintets, septets |
| 7 | $1 / 2,3 / 2,5 / 2,7 / 2$ | Doublets, quartets, sextets, octets |
| etc. |  |  |


| 4273.9700 | 4319.5797 | 4453.9179 | 5649.5629 |
| :--- | :--- | :--- | :--- |
| 4282.9683 | 4351.3607 | 4463.6902 | 5870.9158 |
| 4286.4873 | 4332.6423 | 4502.3547 | 5939.8503 |
| 4300.4877 | 4376.1220 | 5562.2257 | 6421.029 |
| 4318.5525 | 4399.9670 | 5570.2895 | 6456.291 |

Neon and krypton secondary standards are used extensively for interference measurements in metrology and spectroscopy, but their spectral range and distribution does not make them generally suitable for wavelength measurements by interpolation in prismatic or in grating spectra. For the latter purpose a system of secondary standards should consist of lines of comparable intensity distributed as uniformly as possible throughout the entire range of wavelengths commonly observed in optical spectra. An approach to such a system is found in the internationally adopted secondary standards derived from the spectrum of the iron arc. The source for iron secondary standards is specified ${ }^{188}$ as the "Pfund arc operated between 110 and 250 volts, with 5 amperes or less, at a length of 12-15 millimeters used over a central zone at right angles to the axis of the arc, not to exceed 1.0-1.5 millimeters in width, and with an iron rod 6-7 millimeters diameter as the upper pole and a bead of oxide of iron as the lower pole. As the secondary standards to the red of 6000 A are all stable lines, and as the exposures with the above-mentioned arc may be rather long, it is recommended that the $6 \mathrm{~mm}, 6$ ampere arc be retained for this region."

The list of iron secondary standards adopted by the International Astronomical Union ${ }^{198}$ consists of 3067 -figure values ranging from 2447.708 to 6677.933 A , thus covering a little more than one octave.

Internal evidence from the combination principle as well as the agreement between independent observers indicates that the average probable error in these standards is $\pm 0.001 \mathrm{~A}$. Preliminary values of long-wave iron lines ( 6750.158 to 10216.351 A) have been suggested. ${ }^{157}$

Additional ultraviolet iron lines ( 2100.794 to 3383.980 A ) have been suggested ${ }^{188}$ and only one or two confirmatory observations arc required to extend the secondary standards over a range of more than two octaves.

185-188 For references, see p. 578.

TABLE 615.-J VALUES FOR LEVELS IN TERMS HAVING ODD AND EVEN
MULTIPLICITIES

|  | Values of $J$ for - |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Terms | Singlets | Doublets | Triplets | Quartets | Quintets | Sextets |
| S | 0 | 1/2 | 1 | 3/2 | 2 | 5/2 |
| $P$ | 1 | 1/2, 3/2 | 012 | 1/2, 3/2, $5 / 2$ | 123 | 3/2,5/2, 7/2 |
| D | 2 | 3/2, 5/2 | 123 | 1/2, 3/2, 5/2, 7/2 | 01234 | 1/2,3/2,5/2, 7/2, 9/2 |
| F | 3 | 5/2,7/2 | 234 | 3/2, 5/2, 7/2, 9/2 | 12345 | 1/2,3/2, 5/2, 7/2, 9/2,11/2 |
| G | 4 | 7/2, 9/2 | 345 | 5/2, 7/2, 9/2,11/2 | 23456 | 3/2, 5/2, 7/2, 9/2, 11/2, 13/2 |

TABLE 616.-TERMS FROM NONEQUIVALENT ELECTRONS

| Electrons | Terms (omitting $J$ values) |
| :---: | :---: |
| sS | ${ }^{1} S,{ }^{8} S$ |
| $s p$ | ${ }^{1} P$, ${ }^{8} P$ |
| sd | ${ }^{1} D,{ }^{3} D$ |
| $p p$ | ${ }^{1} S,{ }^{1} P,{ }^{1} D,{ }^{8} S,{ }^{8} P,{ }^{8} D$ |
| $p d$ | ${ }^{1} P,{ }^{1} D,{ }^{1} F,{ }^{8} P,{ }^{8} D,{ }^{8} F$ |
| dd | ${ }^{1} S,{ }^{1} P,{ }^{1} D,{ }^{1} F,{ }^{1} G,{ }^{8} S,{ }^{8} P,{ }^{8} D,{ }^{9} F,{ }^{8} G$ |
| $d f$ |  |
| ff | ${ }^{1} S,{ }^{1} P,{ }^{1} D,{ }^{1} \mathrm{~F},{ }^{1} \mathrm{G},{ }^{1} \mathrm{H},{ }^{1} \mathrm{I},{ }^{8} S,{ }^{8} P,{ }^{8} \mathrm{D},{ }^{8} \mathrm{~F},{ }^{8} \mathrm{G},{ }^{8} \mathrm{H},{ }^{8} \mathrm{I}$ |

TABLE 617.-IRON SECONDARY STANDARDS OF WAVELENGTH IN ANGSTROMS

| 2447.708 | 3175.447 | 3565.381 | 3767.194 | 3922.914 | 42 | 4647.437 | 5270.360 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2584.536 | 3178.015 | 3576.760 | 3787.883 | 3927.922 | 4271.764 | 4667.459 | 5307.365 |
| 2635.808 | 3184.896 | 3581.195 | 3790.095 | 3930.299 | 4282.406 | 4678.852 | 5328.534 |
| 2679.062 | 3191.659 | 3584.663 | 3795.004 | 3935.815 | 4285.44 | 4691.414 | 5341.026 |
| 2689.212 | 3196.930 | 3585.320 | 3797.517 | 3940.882 | 4294.128 | 4707.281 | 5371.493 |
| 2699.107 | 3200.475 | 3586.114 | 3798.513 | 3942.443 | 4298.040 | 4710.286 | 5397.131 |
| 2723.577 | 3205.400 | 3589.107 | 3799.549 | 3948.779 | 4305.455 | 4733.596 | 5405.778 |
| 2735.475 | 3215.940 | 3608.861 | 3805.345 | 3956.681 | 4307.906 | 4641.533 | 5429.699 |
| 2767.523 | 3217.380 | 3617.788 | 3815.842 | 3966.066 | 4315.087 | 4745.806 | 5434.527 |
| 2778.221 | 3222.069 | 3618.769 | 3824.444 | 3967.423 | 4325.765 | 4772.817 | 5446.920 |
| 2804.521 | 3225.789 | 3621.463 | 3825.884 | 3969.261 | 4337.049 | 4786.810 | 5455.613 |
| 2813.288 | 3226.223 | 3631.464 | 3827.825 | 4005.246 | 4352.737 | 4789.654 | 5497.519 |
| 2823.276 | 3239.436 | 3647.844 | 3834.225 | 4014.534 | 4358.505 | 4859.748 | 5501.469 |
| 2832.436 | 3244.190 | 3649.508 | 3839.259 | 4045.815 | 4369.774 | 4878.218 | 5506.782 |
| 2838.120 | 3257.594 | 3651.469 | 3840.439 | 4063.597 | 4375.932 | 4903.317 | 5569.625 |
| 2851.798 | 3271.002 | 3669.523 | 3841.051 | 4066.979 | 4383.547 | 4918.999 | 5572.849 |
| 2869.308 | 3284.588 | 3676.314 | 3843.259 | 4067.275 | 4390.954 | 4924.776 | 586.763 |
| 2912.158 | 3286.755 | 3677.630 | 3846.803 | 4071.740 | 4404.752 | 4939.690 | 5615.652 |
| 2929.008 | 3298.133 | 3679.915 | 3849.969 | 4107.492 | 4408.419 | 4966.096 | 5624.549 |
| 2941.343 | 3340.566 | 3687.458 | 3850.820 | 4114.449 | 4415.125 | 4994.133 | 5658.826 |
| 2953.940 | 3347.927 | 3695.054 | 3856.373 | 4118.549 | 4422.570 | 5001.871 | 662.525 |
| 2957.365 | 3370.786 | 3704.463 | 3859.913 | 4121.806 | 4427.312 | 5012.071 | 027.057 |
| 2965.255 | 3396.978 | 3705.567 | 3865.526 | 4127.612 | 4430.618 | 5041.759 | 6075.487 |
| 2981.446 | 3399.336 | 3719.935 | 3867.219 | 4132.060 | 4442.343 | 5049.825 | 6136.620 |
| 2987.292 | 3401.521 | 3722.564 | 3872.504 | 4134.681 | 4443.197 | 5051.636 | 137.696 |
| 2999.512 | 3407.461 | 3724.380 | 3873.763 | 4143.871 | 4447.722 | 5083.342 | 6191.562 |
| 3037.388 | 3413.135 | 3727.621 | 3878.021 | 4147.673 | 4454.383 | 5110.414 | 6230.728 |
| 3047.605 | 3427.121 | 3732.399 | 3878.575 | 4156.803 | 4459.121 | 5123.723 | 6252.561 |
| 3057.446 | 3443.878 | 3733.319 | 3886.284 | 4170.906 | 4461.65 | 5127.363 | 6265.140 |
| 3059.086 | 3445.151 | 3734.867 | 3887.051 | 4175.640 | 4466.554 | 5150.843 | 6318.022 |
| 3067.244 | 3465.863 | 3737.133 | 3888.517 | 4184.895 | 4489.741 | 5167.491 | 6335.335 |
| 3075.721 | 3476.704 | 3738.308 | 3895.658 | 4202.031 | 4494.568 | 5168.901 | 5393.605 |
| 3083.742 | 3485.342 | 3748.264 | 3899.709 | 4203.987 | 4517.530 | 5171.599 | 6421.355 |
| 3091.578 | 3490.575 | 3749.487 | 3902.948 | 4213.650 | 4528.619 | 5198.714 | 430.851 |
| 3116.633 | 3497.843 | 3758.235 | 3906.482 | 4216.186 | 4531.152 | 5202.339 | 6494.985 |
| 3134.111 | 3513.820 | 3760.052 | 3907.937 | 4219.364 | 4547.851 | 5216.278 | 6546.245 |
| 3157.040 | 3521.264 | 3763.790 | 3917.185 | 4250.790 | 4592.655 | 5227.192 | 6592.919 |
| 3160.658 | 3558.518 | 3765.542 | 3920.260 | 4260.479 | 4602.944 | $5242.495$ | 6663.446 |

Iron tertiary standards of wavelength. - The iron tertiary standards derived from diffraction-grating interpolation between secondary standards, and formerly adopted, ${ }^{189}$ have all been superseded by interferometer, or grating interpolated, values published in the M.I.T. Wavelength Tables (John Wiley \& Sons, New York, 1939).

Extreme ultraviolet standards of wavelength. - Provisional standards of wavelength in the extreme ultraviolet, measured relative to secondary and tertiary iron standards in overlapping spectral orders, have been published; ${ }^{100}$ they include 57 carbon lines ( 1930.900 to 858.091 A ), 23 nitrogen lines ( 1745.246 to 775.966 A ), 25 oxygen lines ( 1306.038 to 580.974 A ), and 10 argon lines ( 1066.660 to 871.099 A).

Standard solar wavelengths.-The International Astronomical Union ${ }^{101}$ has adopted 7 -figure standards of wavelength in the solar spectrum when two or more accordant values have been reported. These values have resulted mainly from interferometer measurements of solar-absorption wavelengths relative to neon or to iron secondary standards. The standards represent integrated solar light, are corrected for Doppler-Fizeau displacement, and are valid for standard air at $15^{\circ} \mathrm{C}$ and 760 mmHg pressure. In the long-wave region many of the solar spectrum standards originate in the terrestrial atmosphere as absorption by oxvgen or water vapor.
In Table 618 the + sign following the symbol of an element indicates ionization; a symbol like Fe -, solar line too strong to be due to iron alone; $\mathrm{Fe}, \mathrm{Co}$, coincidences of like order; Fe Co , coincidence closer for preceding element; $\mathrm{Fe}-\mathrm{Co}, \mathrm{Fe}$ wavelength smaller, Co larger than solar line; an italicized element indicates a more prominent contribution and boldface a decidedly predominant element.

[^237]TABLE 618.-STANDARD SOLAR WAVELENGTHS MEASURED IN AIR AT $15^{\circ} \mathrm{C}$ AND 1 ATMOSPHERE PRESSURE

| $\lambda$ Solar | Origin Intensity | $\lambda$ Solar | Origin | Intensity | $\lambda$ Solar | Origin | Intensity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3592.027 | $\mathrm{V}+2$ | 4348.947 | Fe | 2 | 4832.719 | $\mathrm{Ni}-\mathrm{Fe}$ | 仡 |
| 3635.469 | Ti 4 | 4365.904 | Fe | 2 | 4839.551 | Fe | 3 |
| 3650.538 | 2 | 4389.253 | Fe | 2 | 4939.694 | Fe | 3 |
| 3672.712 | $\mathrm{Fe} \quad 3$ | 4398.020 | Y + | 1 | 4983.260 | Fe | 3 |
| 3695.056 | $\mathrm{Fe} \quad 5$ | 4416.828 | $\mathrm{Fe}+$ | 2 | 4994.138 | Fe | 4 |
| 3710.292 | $\mathrm{Y}+3$ | 4425.444 | Ca | 4 | 5002.798 | Fe | 2 |
| 3725.496 | Fe 3 | 4430.622 | Fe | 3 | 5014.951 | Fe | 3 |
| 3741.065 | Ti 4 | 4439.888 | Fe | 1 | 5028.133 | Fe | 2 |
| 3752.418 | Fe 3 | 4451.588 | Mn | 3 | 5079.745 | Fe | 4 |
| 3760.537 | $\mathrm{Fe} \quad 4$ | 4454.388 | Fe | 3 | 5090.782 | Fe | 5 |
| 3769.994 | $\mathrm{Fe} \quad 4$ | 4459.755 | $\mathrm{Cr}-\mathrm{V}$ | 1 | 5109.657 | Fe | 2 |
| 3781.190 | Fe 3 | 4470485 | Ni | 2 | 5150.852 | Fe | 4 |
| 3793.876 | CrFe 2 | 4481.616 | Fe | 1 | 5159.065 | Fe | 2 |
| 3804.015 | Fe 3 | 4502.221 | Mn | 2 | 5198.718 | Fe | 3 |
| 3821.187 | $\mathrm{Fe}{ }^{4}$ | 4508.289 | $\mathrm{Fe}+$ | 4 | 5225.534 | Fe | 2 |
| 3836.090 | $\mathrm{Ti}+\mathrm{CrV}$ ? 2 | 4512.741 | Ti | 3 | 5242.500 | Fe | 3 |
| 3843.264 | $\mathrm{Fe}^{4}$ | 4517.534 | Fe | 3 | 5253.468 | Fe | 2 |
| 3897.458 | $\mathrm{Fe}-\quad 4$ | 4525.146 | Fe | 5 | 5273.389 | Fe | 3 |
| 3906.752 | $\mathrm{Fe} \quad 3$ | 4531.631 | Fe | 2 | 5288.533 | Fe | 2 |
| 3916.737 | $\mathrm{Fe} \quad 4$ | 4534.785 | Ti | 4 | 5300.751 | Cr | 2 |
| 3937.336 | Fe 3 | 4541.523 | $\mathrm{Fe}+$ | 2 | 5307.369 | Fe | 3 |
| 3949.959 | $\mathrm{Fe} \quad 5$ | 4547.853 | Fe Ti | 3 | 5322.049 | Fe | 3 |
| 3953.861 | $\mathrm{Fe}-3$ | 4548.770 | Ti | 2 | 5332.908 | Fe | 4 |
| 3960.284 | $\mathrm{Fe}-3$ | 4550.773 | Fe | 2 | 5348.326 | Cr | 4 |
| 3963.691 | Cr 3 | 4563.766 | $\mathrm{Ti}+$ | 4 | 5365.407 | Fe | 4 |
| 3977.747 | $\mathrm{Fe}{ }^{6}$ | 4571.102 | Mg | 5 | 5379.581 | Fe | 3 |
| 3991.121 | $\mathrm{Cr}-\mathrm{Zr}+3$ | 4571.982 | $\mathrm{Ti}+$ | 6 | 5389.486 | Fe | 3 |
| 4003.769 | $\mathrm{Fe}-\mathrm{Ti} 3$ | 4576.339 | $\mathrm{Fe}+$ | 2 | 5398.287 | Fe - | 3 |
| 4016.423 | $\mathrm{Fe} \quad 2$ | 4578.559 | Ca | 3 | 5409.799 | Cr | 5 |
| 4029.642 | $\mathrm{Fe}-\mathrm{Zr}+5$ | 4587.134 | Fe | 2 | 5415.210 | Fe | 5 |
| 4030.190 | $\mathrm{Fe}^{2}$ | 4589.953 | Ti + | 3 | 5432.955 | Fe - | 2 |
| 4037.121 | 2 | 4598.125 | Fe | 3 | 5445.053 | Fe | 4 |
| 4053.824 | $\mathrm{Ti}+\mathrm{Fe} \quad 2$ | 4602.008 | Fe | 3 | 5462.970 | Fe | 3 |
| 4062.447 | $\mathrm{Fe} \quad 5$ | 4602.949 | Fe | 6 | 5473.910 | Fe | 3 |
| 4073.767 | Fe 4 | 4607.654 | Fe | 4 | 5487.755 | Fe | 3 |
| 4079.843 | Fe 3 | 4617.276 | Ti | 3 | 5501.477 | Fe | 5 |
| 4082.943 | Mn 4 | 4625.052 | Fe | 5 | 5512.989 | Ca | 4 |
| 4091.557 | Fe 3 | 4630.128 | Fe | 4 | 5525.552 | Fe | 2 |
| 4094.938 | Ca 4 | 4635.853 | Fe | 2 | 5534.848 | $\mathrm{Fe}+$ | 2 |
| 4107.492 | Fe 5 | 4637.510 | Fe | 5 | 5546.514 | Fe | 2 |
| 4120.212 | $\mathrm{Fe} \quad 4$ | 4638017 | Fe | 4 | 5590.126 | Ca | 3 |
| 4136.527 | $\mathrm{Fe} \quad 3$ | 4643.470 | Fe | 4 | 5601.286 | Ca | 3 |
| 4139.936 | Fe 4 | 4647.442 | Fe | 4 | 5624.558 | Fe V | 4 |
| 4154.814 | Fe 4 | 4656.474 | Ti | 3 | 5641.448 | Fe | 2 |
| 4163.654 | $\mathrm{Ti}+\mathrm{Cr}-\mathrm{Fe} 5$ | 4664.794 | Cr Na | 3 | 5655.500 | Fe | 2 |
| 4168.620 | $\mathrm{FeFe}+$ ? 2 | 4678.172 |  | 3 N | 5667.524 | Fe | 2 |
| 4178.859 | $\mathrm{Fe}+3$ | 4678.854 | Fe | 6 | 5679.032 | Fe | 3 |
| 4184.900 | $\mathrm{Fe}, \mathrm{Cr} 4$ | 4683.567 | Fe | 3 | 5690.433 | Si | 3 |
| 4191.683 | $\mathrm{Fe}^{3}$ | 4690.144 | Fe | 4 | 5701.557 | Fe | 4 |
| 4198.638 | $\mathrm{Fe} \quad 3$ | 4700.162 | Fe | 3 | 5731.772 | Fe | 4 |
| 4208.608 | $\mathrm{Fe} \quad 3$ | 4704.954 | Fe | 3 | 5741.856 | Fe | 2 |
| 4220.347 | Fe 3 | 4720.999 | Fe | 2 | 5752.042 | Fe | 4 |
| 4233.612 | $\mathrm{Fe} \quad 6$ | 4728.552 | Fe | 4 | 5760.841 | Ni | 2 |
| 4241.123 | Fe 2 | 4733.598 | Fe | 4 | 5805.226 | Ni | 4 |
| 4246.837 | $\mathrm{Sc}+5$ | 4735.848 | Fe | 3 | 5809.224 | Fe | 4 |
| 4257.661 | $\mathrm{Mn} \quad 2$ | 4736.783 | Fe | 6 | 5816.380 | Fe | 5 |
| 4266.968 | $\mathrm{Fe} \quad 3$ | 4741.535 | Fe | 4 | 5853.688 | $\mathrm{Ba}+$ | 5 |
| 4276.680 | $\mathrm{FeTi}{ }_{2}$ | 4745.807 | Fe | 4 | 5857.459 | Ca | 8 |
| 4282.412 | Fe 5 | 4772.823 | Fe | 4 | 5859.596 | Fe | 5 |
| 4291.472 | $\mathrm{Fe} \quad 2$ | 4788.765 | Fe | 3 | 5862.368 | Fe | 6 |
| 4318.659 | Ca Ti 4 | 4789.658 | Fe | 3 | 5866.461 | Ti | 3 |
| 4331.651 | $\mathrm{Ni} \quad 2$ | 4802.887 | Fe | 2 | 5867.572 | Ca | 2 |
| 4337.925 | Ti +4 | 4824.143 | $\mathrm{Cr}+-\mathrm{Fe}$ | e 3 | 5892.883 | Ni | 4 |

(continued)

## TABLE 618.-STANDARD SOLAR WAVELENGTHS MEASURED IN AIR AT $15^{\circ} \mathrm{C}$ AND 1 ATMOSPHERE PRESSURE (continued)

| $\lambda$ Solar | Origin Intensity | $\lambda$ Solar | Origin | Intensity | $\lambda$ Solar | Origin | Intensity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5898.166 | Atm 4 | 6213.437 | Fe | 6 | 6455.605 | Ca | 2 |
| 5905.680 | $\mathrm{Fe} \quad 4$ | 6215.149 | Fe | 3 | 6456.391 | $\mathrm{Fe}+$ | 3 |
| 5916.257 | $\mathrm{Fe}-3$ | 6216.358 | V | 1 | 6471.668 | Ca | 5 |
| 5919.054 | Atm 5 | 6219.287 | Fe | 6 | 6475.632 | Fe | 2 |
| 5919.644 | Atm 7 | 6226.740 | Fe | 1 | 6482.809 | Ni | 1 |
| 5927.797 | Fe 3 | 6229.232 | Fe | 1 | 6493.788 | Ca | 6 |
| 5930.191 | Fe 6 | 6230.736 | $\mathrm{Fe}-\mathrm{V}$ | 8 | 6494.994 | Fe | 8 |
| 5932.092 | Atm 5 | 6232.648 | Fe | 4 | 6498.945 | Fe | 1 |
| 5934.665 | Fe 5 | 6240.653 | Fe | 3 | 6499.654 | Ca | 4 |
| 5946.006 | Atm 3 | 6244.476 | Si | 2 | 6516.083 | $\mathrm{Fe}+$ | 2 |
| 5952.726 | $\mathrm{Fe} \quad 4$ | 6245.620 | $\mathrm{Sc}+$ | 1 | 6518.373 | Fe | 2 |
| 5956.706 | $\mathrm{Fe} \quad 4$ | 6246.327 | Fe | 7 | 6569.224 | Fe | 4 |
| 5975.353 | $\mathrm{Fe} \quad 3$ | 6247.562 | $\mathrm{Fe}+$ | 2 | 6592.926 | Fe | 6 |
| 5976.787 | $\mathrm{Fe} \quad 4$ | 6252.565 | Fe | 7 | 6609.118 | Fe | 5 |
| 5983.688 | $\mathrm{Fe} \quad 5$ | 6254.253 | SiFe | 5 | 6643.638 | Ni | 6 |
| 5984.826 | Fe 6 | 6256.367 | FeNi | 6 | 6677.997 | Fe | 8 |
| 6003.022 | $\mathrm{Fe} \quad 6$ | 6258.110 | Ti | 3 | 6717.687 | Ca | 6 |
| 6008.566 | $\mathrm{Fe} \quad 6$ | 6258.713 | Ti | 3 | 6810.267 | Fe | 2 |
| 6013.497 | Mn 6 | 6265.141 | Fe | 5 | 6858.155 | Fe | 4 |
| 6016.647 | Mn 6 | 6270.231 | Fe | 2 | 6870.946 | Atm O | 13 |
| 6024.068 | $\mathrm{Fe} \quad 7$ | 6279.101 | Atm O | 3 | 6879.928 | Atm O | 10 |
| 6027.059 | Fe 4 | 6279.896 | Atm O | 2 | 6918.122 | Atm O | 8 |
| 6042.104 | Fe 3 | 6280.393 | Atm O | 2 | 6919.002 | Atm O | 8 |
| 6065.494 | $\mathrm{Fe} \quad 7$ | 6280.622 | Fe | 3 | 6923.302 | Atm O | 6 |
| 6078.499 | $\mathrm{Fe} \quad 5$ | 6281.178 | Atm O | 1 | 6924.172 | Atm O | 6 |
| 6079.016 | $\mathrm{Fe} \quad 3$ | 6281.956 | Atm O | 2 | 6928.728 | Atm O | 5 |
| 6082.718 | $\mathrm{Fe} \quad 1$ | 6283.796 | Atm O | 1 | 6934.422 | Atm O | 3 |
| 6085.257 | $\mathrm{Ti}-\mathrm{Fe} \quad 2$ | 6289.398 | Atm O | 1 | 6959.452 | Atm | 9 |
| 6086.288 | $\mathrm{Ni} \quad 2$ | 6290.221 | Atm O | 2 | 6961.260 | Atm | 11 |
| 6089.574 | Fe 2 | 6292.162 | Atm O | 2 | 6978.862 | Fe | 6 |
| 6090.216 | V 2 | 6292.958 | Atm O | 3 | 6986.579 | Atm | 8 |
| 6093:649 | $\mathrm{Fe} \quad 2$ | 6295.178 | Atm O | 3 | 6988.986 | Atm | 8 |
| 6096.671 | Fe 3 | 6295.960 | Atm O | 3 | 7022.957 | Fe | 4 |
| 6102.183 | $\mathrm{Fe} \quad 6$ | 6297.799 | Fe | 5 | 7023.504 | Atm | 5 |
| 6102.727 | Ca 9 | 6299.228 | Atm O | 3 | 7027.478 | Atm | 5 |
| 6111.078 | $\mathrm{Ni} \quad 2$ | 6301.508 | Fe | 7 | 7034.910 | Si | 5 |
| 6116.198 | Ni 3 | 6302.499 | Fe | 5 | 7122.206 | Ni | 7 |
| 6122.226 | Ca 10 | 6302.764 | Atm O | 2 | 7568.906 | Fe | 5 |
| 6127.912 | Fe 3 | 6305.810 | Atm O | 2 | 7574.048 | Ni | 5 |
| 6128.984 | $\mathrm{Ni} \quad 1$ | 6306.565 | Atm O | 2 | 7586.027 | Fe | 8 |
| 6136.624 | Fe 8 | 6309.886 | Atm 0 | 2 | 7595.770 | Atm $\mathrm{O}_{2}$ | 12 |
| 6137.002 | $\mathrm{Fe} \quad 3$ | 6315.314 | Fe | 3 | 7599.462 | Atm $\mathrm{O}_{2}$ | 0 |
| 6137.702 | Fe 7 | 6315.814 | Fe | 2 | 7602.995 | Atm $\mathrm{O}_{2}$ | 0 |
| 6141.727 | $B a+-\mathrm{Fe} 7$ | 6318.027 | Fe | 6 | 7611.194 | $\mathrm{Atm} \mathrm{O}_{2}$ | 0 |
| 6145.020 | $\mathrm{Si} \quad 2$ | 6322.694 | Fe | 5 | 7616.980 | Ni | 8 |
| 6149.249 | $\mathrm{Fe}+2$ | 6327.604 | Ni | 2 | 7619.214 | Ni | 4 |
| 6151.623 | Fe 4 | 6330.852 | Fe | 2 | 7621.802 | Atm $\mathrm{O}_{2}$ | 0 |
| 6154.230 | Na 2 | 6335.337 | Fe | 7 | 7625.354 | Atm $\mathrm{O}_{2}$ | 1 |
| 6157.733 | Fe 5 | 6336.830 | Fe | 7 | 7638.306 | Atm $\mathrm{O}_{2}$ | 3 |
| 6161.295 | Ca 4 | 6344.155 | Fe | 4 | 7647.202 | Atm $\mathrm{O}_{2}$ | 1 |
| 6162.180 | Ca 15 | 6355.035 | Fe | 4 | 7649.553 | Atm $\mathrm{O}_{2}$ | -1 |
| 6165.363 | Fe 2 | 6358.687 | Fe | 6 | 7651.963 | Atm $\mathrm{O}_{2}$ | 0 |
| 6166.440 | Ca 5 | 6378.256 | Ni | 2 | 7657.606 | Mg | 9 N |
| 6169.564 | Ca 7 | 6380.750 | Fe | 4 | 7665.944 | Atm $\mathrm{O}_{2}$ | 10 |
| 6170.516 | $\mathrm{Fe}-\mathrm{Ni} 4$ | 6393.612 | Fe | 7 | 7671.669 | Atm $\mathrm{O}_{2}$ | 10 |
| 6173.341 | $\mathrm{Fe} \quad 5$ | 6400.009 | Fe | 8 | 7676.565 | Atm $\mathrm{O}_{2}$ | 9 |
| 6175.370 | $\mathrm{Ni} \quad 3$ | 6400.323 | Fe | 2 | 7677.619 | Atm $\mathrm{O}_{2}$ | 9 |
| 6176.816 | Ni 5 | 6408.026 | Fe | 5 | 7682.758 | Atm $\mathrm{O}_{2}$ | 8 |
| 6180.209 | $\mathrm{Fe} \quad 5$ | 6411.658 | Fe | 7 | 7683.802 | Atm $\mathrm{O}_{2}$ | 8 |
| 5186.717 | Ni 2 | 6419.956 | Fe | 4 | 7690.218 | Atm $\mathrm{O}_{2}$ | 6 |
| 6187.995 | $-\mathrm{Fe} 4$ | 6421.360 | Fe | 7 | 7695.838 | Atm $\mathrm{O}_{2}$ | 4 |
| 6191.571 | Fe 9 | 6430.856 | Fe | 7 | 7696.869 | Atm $\mathrm{O}_{2}$ | 4 |
| 6200.321 | Fe 6 | 6449.820 | Ca | 6 | 7714.310 | Ni | 6 |

TABLE 618.-STANDARD SOLAR WAVELENGTHS MEASURED IN AIR AT $15^{\circ} \mathrm{C}$ AND 1 ATMOSPHERE PRESSURE (continued)

| $\lambda$ Solar | Origin | Intensity | $\lambda$ Solar | Origin | Intensity | $\lambda$ Solar | Origin | Intensity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7727.616 | Ni | 5 | 8259.692 | Atm | 8 | 9073.134 | Atm | 1 |
| 7748.284 | Fe | 6 | 8263.445 | Atm | 7 | 9074.306 | Atm | 7 |
| 7751.116 | Fe | 2 | 8272.042 | Atm | 8 | 9092.482 | Atm | 5 |
| 7780.568 | Fe | 8 | 8279.600 | Atm | 9 | 9105.399 | Atm | 7 |
| 7788.933 | Ni | 5 | 8300.408 | Atm | 10 | 9118.009 | Atm | 5 |
| 7797.588 | Ni | 5 | 8304.300 | Atm | 6 | 9132.443 | Atm | 3 |
| 7807.916 | $\mathrm{Fe} ?-\mathrm{Fe}$ | e 4 | 8311.956 | Atm | 6 | 9140.457 | Atm | 1 |
| 7832.208 | Fe | 9 | 8316.224 | Atm | 5 | 9150.800 | Atm | 1 |
| 7836.130 | Al | 4 N | 8327.061 | Fe | 10 | 9175.249 | Atm | 5 |
| 7864.437 | Atm | 2 | 8329.682 | Atm | 8 | 9178.534 | Atm | 3 |
| 7885.014 | Atm Ti | 1 | 8333.584 | Atm | 5 | 9181.203 | Atm | 3 |
| 7887.117 | Atm | 3 | 8342.290 | Atm | 3 | 9190.208 | Atm | 3 |
| 7893.512 | Atm | 4 | 8349.162 | Atm | 4 | 9192.568 | Atm | 5 |
| 7912.870 | Fe | 2 | 8357.040 | Atm | 6 | 9205.584 | Atm | 3 |
| 7915.634 | Atm | 3 | 8362.302 | Atm | 5 | 9225.006 | Atm | 6 |
| 7920.666 | Atm | 7 | 8367.331 | Atm | 6 | 9232.750 | Atm | 3 |
| 7928.618 | Atm | 7 | 8376.381 | Atm | 4 | 9251.100 | Atm | 6 |
| 7937.150 | Fe | 7 | 8394.020 | Atm | 3 | 9254.347 | Atm | 1 |
| 7941.096 | Fe | 2 | 8397.152 | Atm | 2 | 9275.072 | Atm | 2 |
| 7945.858 | Fe | 7 | 8426.514 | Ti | 2 | 9289.856 | Atm | 2 |
| 7958.492 | Atm | 7 | 8434.968 | Ti | 4 | 9301.910 | Atm | 5 |
| 7971.522 | Atm | 4 | 8439.581 | Fe | 5 | 9311.734 | Atm | 6 |
| 7984.342 | Atm | 4 | 8468.418 | Fe | 9 | 9314.006 | Atm | 4 |
| 7994.488 | Fe | 3 | 8471.744 | Fe | 2 | 9320.768 | Atm | 7 |
| 8000.300 | Atm | 6 | 8514.082 | Fe | 7 | 9321.650 | Atm | 0 |
| 8012.940 | Atm | 4 | 8515.122 | Fe | 5 | 9348.382 | Atm | 2 |
| 8036.460 | Atm | 3 | 8526.676 | Fe | 3 | 9361.227 | Atm | 6 |
| 8039.600 | Atm | 3 | 8556.797 | Si | 8 N | 9363.334 | Atm | 3 |
| 8045.530 | Atm | 3 | 8571.807 | Fe | 2 | 9374.280 | Atm | 1 |
| 8046.058 | Fe | 8 | 8582.271 | Fe | 6 | 9400.094 | Atm | 7 |
| 8047.625 | Fe | 4 | 8595.968 | Si | 3 N | 9406.904 | Atm | 6 |
| 8063.286 | Atm | 2 | 8598.836 | Fe | 3 | 9444.412 | Atm | 5 |
| 8075.158 | Fe | 2 | 8611.812 | Fe | 7 | 9463.992 | Atm | 3 |
| 8096.580 | Atm | 3 | 8613.946 | Fe | 1 | 9472.418 | Atm | 1 |
| 8103.165 | Atm | 1 | 8616.284 | Fe | 2 | 9476.754 | Atm | 4 |
| 8107.842 | Atm | 4 | 8648.472 | Si | 10 N | 9478.884 | Atm | 0 |
| 8118.910 | Atm | 2 | 8674.756 | Fe | 7 | 9483.970 | Atm | 1 |
| 8125.445 | Atm | 3 | 8699.461 | Fe | 4 | 9486.042 | Atm | 7 |
| 8133.209 | Atm | 2 | 8713.208 | Fe | 3 | 9504.434 | Atm | 3 |
| 8139.718 | Atm | 3 | 8717.833 | Mg ? | 7 N | 9507.742 | Atm | 1 |
| 8146.213 | Atm | 5 | 8747.438 | Fe | 0 | 9512.630 | Atm | 5 |
| 8147.188 | Atm | 5 | 8773.906 | A1 | 6 | 9533.411 | Atm | 4 |
| 8165.337 | Atm | 3 | 8784.444 | Fe | 1 | 9549.958 | Atm | 2 |
| 8169.386 | Atm | 6 | 8790.454 | Fe Si | 6 | 9550.962 | Atm | 2 |
| 8177.932 | Atm | 7 | 8793.350 | Fe | 6 | 9558.836 | Atm | 2 |
| 8178.491 | Atm | 4 | 8824.234 | Fe | 10 | 9575.680 | Atm | 3 |
| 8181.848 | Atm | 9 | 8866.943 | Fe | 9 | 9587.126 | Atm | 5 |
| 8194.836 | Na | 12 N | 8868.444 | Fe | 3 | 9598.870 | Atm | 7 |
| 8200.694 | Atm | 6 | 8876.030 | Fe | 1 | 9601.170 | Atm | 3 |
| 8207.749 | Fe | 4 | 8879.316 | Atm | 4 | 9624.496 | Atm | 3 |
| 8212.132 | Atm | 5 | 8917.506 | Atm | 1 | 9629.997 | Atm | 1 |
| 8218.114 | Atm | 10 | 8927.392 | $\mathrm{Ca}+$ | 7 | 9643.105 | Atm | 3 |
| 8221.553 | Atm | 6 | 8930.270 | Atm | 4 | 9651.932 | Atm | 2 |
| 8225.688 | Atm | 5 | 8946.878 | Atm | 4 | 9664.646 | Atm | 6 |
| 8229.762 | Atm | 8 | 8950.744 | Atm | 1 | 9686.386 | Atm | 3 |
| 8233.906 | Atm | 8 | 8958.402 | Atm | 4 | 9694.588 | Atm | 0 |
| 8234.628 | Atm | 3 | 8963.492 | Atm | 4 | 9700.139 | Atm | 2 |
| 8237.341 | Atm | 5 | 8969.030 | Atm | 0 | 9708.922 | Atm | 6 |
| 8239.132 | Fe | 2 | 8976.424 | Atm | 1 | 9730.638 | Atm | 4 |
| 8239.924 | Atm | 4 | 8993.043 | Atm | 0 | 9755.979 | Atm | 0 |
| 8248.137 | Fe | 4 | 9047.412 | Atm | 2 | 9765.495 | Atm | 4 |
| 8248.802 | $\bigcirc$ | 4 | 9052.974 | Atm | 7 | 9768.637 | Atm | 2 |
| 8252.727 | Atm | 6 | 9060.434 | Atm | 6 | 9776.818 | Atm | 3 |

# TABLE 618.-STANDARD SOLAR WAVELENGTHS MEASURED IN AIR AT $15^{\circ} \mathrm{C}$ AND 1 ATMOSPHERE PRESSURE (concluded) 

| $\lambda$ Solar | Origin | Intensity | $\lambda$ Solar | Origin | Intensity | $\lambda$ Solar | Origin | Intensity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9779.406 | Atm | 5 | 9803.241 | Atm | 3 | 9843.978 | Atm | 2 |
| 9787.146 | Atm | 3 | 9821.754 | Atm | 3 | 9850.524 | Atm | -1 |
| 9791.006 | Atm | 7 | 981.690 | $\mathrm{Atm}-\mathrm{Ti}$ | 4 | 9873.638 | Atm | 4 |
| 9795.288 | Atm | 1 | 9835.758 | Atm | 1 | 9878.200 | Atm | Fe |
| 1 | 1 |  |  |  |  |  |  |  |
| 9799.476 | Atm | 7 | 9840.092 | Atm | -1 | 9889.050 | Fe | 5 |

Prominent lines in simple spectra of elements.-The more prominent lines, in simple spectra, easily excited with high intensity, are universally employed in spectroscopy, refractometry, polarimetry, spectrophotometry, interferometry, and metrology either to calibrate the wavelength scales of dispersing instruments or to make optical measurements at various wavelengths. A brief tabulation of the wavelengths most commonly used for these purposes is given in Table 619, where numerical values of wavelengths and approximate relative intensities by elements are followed by graphical presentation (fig. 30). The spectral range is restricted to that easily observed photographically in air (2000 to 10000 A). Values of wavelengths are quoted from the M.I.T. Wavelength Tables (John Wiley \& Sons, New York, 1939) and relative intensities in individual spectra are estimated from arc spectrograms made at the National Bureau of Standards.

TABLE 619.-WAVELENGTHS (IN ANGSTROMS) AND RELATIVE INTENSITIES OF PROMINENT LINES IN SIMPLE SPECTRA

| Wavelength | Intensity |  | Wavelength | Intensity |  | Wavelength | Intensity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| H 6562.849 | 200 | Mg | 5183.618 | 75 | Cu | 5782.132 | 30 |
| 6562.725 | 100 |  | 5172.699 | 45 |  | 5218.202 | 100 |
| 4861.327 | 40 |  | 5167.343 | 15 |  | 5153.235 | 30 |
| 4340.465 | 15 |  | 3838.258 | 75 |  | 5105.541 | 15 |
| 4101.735 | 5 |  | 3832.306 | 50 |  | 4651.134 | 10 |
| 3970.074 | 1 |  | 3829.350 | 20 |  | 4586.954 | 8 |
|  |  |  | 2852.129 | 500 |  | 4062.698 | 25 |
| He 7065.188 | 40 |  | 2802.695 | 400 |  | 4022.657 | 20 |
| 6678.149 | 75 |  | 2795.53 | 800 |  | 3273.962 | 400 |
| 5875.618 | 500 |  |  |  |  | 3247.540 | 800 |
| 5015.675 | 45 | AI | 3961.527 | 500 |  | 2961.165 | 4 |
| 4921.929 | 25 |  | 3944.032 | 250 |  | 2824.369 | 8 |
| 4713.143 | 25 |  | 3092.713 | 100 |  | 2766.371 | 15 |
| 4471.477 | 40 |  | 3082.155 | 50 |  | 2618.366 | 30 |
| 4026.189 | 20 |  | 2660.393 | 5 |  | 2492.146 | 5 |
| 3888.646 | 500 |  | 2652.489 | 4 |  | 2406.665 | 5 |
| 3203.14 | 25 |  | 2575.100 | 10 |  | 2392.627 | 20 |
| 3187.743 | 50 |  | 2567.987 | 5 |  | 2293.842 | 15 |
| 2945.104 | 25 |  |  |  |  | 2263.079 | 10 |
| 2733.32 | 25 | A | 8521.441 | 200 |  | 2246.995 | 8 |
| 2511.22 | 10 |  | 8424.647 | 250 |  | 2230.084 | 4 |
| 2385.42 | 5 |  | 8408.208 | 300 |  | 2225.697 | 6 |
|  |  |  | 8264.521 | 150 |  | 2199.583 | 5 |
| Li 8126.52 | 30 |  | 8115.311 | 400 |  | 2192.260 | 4 |
| 6707.844 | 900 |  | 8103.692 | 200 |  | 2135.976 | 4 |
| 6103.642 | 60 |  | 8014.786 | 80 |  |  |  |
| 4971.990 | 5 |  | 8006.156 | 60 | Zn | 4810.534 | 100 |
| 4602.863 | 10 |  | 7503.867 | 150 |  | 4722.159 | 60 |
| 4132.29 | 3 |  | 7067.217 | 300 |  | 4680.138 | 20 |
| 3232.61 | 4 |  | 6965.430 | 500 |  | 3345.572 | 15 |
| 2741.31 | 2 |  | 6871.290 | 100 |  | 3345.020 | 80 |
|  |  |  | 6752.832 | 100 |  | 3302.941 | 15 |
| Na 8194.811 | 30 |  | 6677.282 | 80 |  | 3302.588 | 40 |
| 8183.270 | 15 |  | 4200.675 | 50 |  | 3282.333 | 20 |
| 5895.923 | 500 |  | 4158.590 | 50 |  | 3075.901 | 10 |
| 5889.953 | 900 |  | 4044.418 | 20 |  | 2138.56 | 950 |
| 5688.224 | 10 |  | 3948.979 | 20 |  | 2061.91 | 15 |
| 5682.657 | 6 |  |  |  |  | 2025.51 | 30 |
| 3302.988 | 10 | Cu | 8092.634 | 30 |  |  |  |
| 3302.323 | 20 |  | 7933.130 | 15 |  |  |  |
|  |  |  | (continued) |  |  |  |  |

TABLE 619.-WAVELENGTHS (IN ANGSTROMS) AND RELATIVE INTENSITIES OF PROMINENT LINES IN SIMPLE SPECTRA (concluded)


## TABLE 620.-WAVELENGTHS OF FRAUNHOFER LINES

For convenience of reference the values of the wavelengths corresponding to the Fraunhofer lines usually designated by the letters in the column headed "Index letter," are here tabulated separately. The letters $. x, y$, and $Z$ were assigned by Abney. ${ }^{192}$ Except for $D_{3}$, the rest have been taken from Higg's map of the normal solar spectrum. The data in columns 2, 3, and 4 are from the following sources:
For $\lambda>6600$, Babcock, H. D., and Moore, C. E., Carnegie Inst. Washington Publ. 579, 1947.

For $\lambda$ 3062-6600, Revised Rowland Table, St. John, C. E., et al., Carnegie Inst. Washington Publ. 396, 1928, with additions and corrections by C. E. Moore, unpublished (1949).

For $\lambda<3062$, Babcock, H. D., Moore, C. E., and Coffeen, M. F., Astrophys. Journ., vol. 107, p. 287, 1948 (Mount W'ilson Contr. No. 745).

[^238](continued)

TABLE 620.-WAVELENGTHS OF FRAUNHOFER LINES (concluded)

| Index letter | Identification | Solar wavelength | Solar intensity | Index letter | Identification | Solar wavelength | Solar intensity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $y$ | Atm | 8987.65 | 10 | G | $\{\mathrm{Fe} \mathrm{Ti}+$ | 4307.912 | 6 |
| $x_{4}$ | Mg | 8806.775 | 14 | $G$ | $\{\mathrm{Ca}$ | 4307.747 | 3 |
| $x_{2}$ | $\mathrm{Ca}+$ | 8662.170 | 23 |  | Ca | $4226.740 \ddagger$ | 20d |
| $x_{2}$ | $\mathrm{Ca}+$ | 8542.144 | 25 | $h$ | $\mathrm{H}_{0}$ | 4101.748 | 40N |
| $x_{1}$ | $\mathrm{Ca}+$ | 8498.062 | 20 | H | $\mathrm{Ca}+$ | $3968.49 ?$ | 700 |
| Z | Atm | 8226.962 | (20) | K | $\mathrm{Ca}+$ | 3933.682 | 1000 |
| A | Atm $\mathrm{O}_{2}$ | 7593.695* | 10 | $L$ | $\mathrm{Fe}_{\mathrm{Fe}}$ | 3820.436 3727 | 25 |
| $a$ | Atm | 7184.526 | 8 | $\stackrel{M}{1}$ | Fe Fe | 3727.634 3581.209 | 30 |
| $B$ | Atm $\mathrm{O}_{2}$ | 6867.187 * | 4 | $\bigcirc$ | $\stackrel{\mathrm{Fe}}{ }$ | 3441.019 | 15 |
| C | $\mathrm{H}_{0}$ | 6562.808 | 40 | P | $\stackrel{\mathrm{Fe}}{\mathrm{Ti}}+$ | 3361.193 | 8 |
| a | Atm $\mathrm{O}_{2}$ | 6276.607 * | 2 d | $Q$ | Fe | 3286.772 | 7N |
| $D_{2}$ | Na | 5895.940 | 20 | Q | $\{\mathrm{Ca}+$ | 3181.276 | 3 |
| $D_{2}$ | Na | 5889.973 | 30 | $R$ | $\left\{\begin{array}{l}\text { Ca }+ \\ \end{array}\right.$ | 3179.342 | 5 d ? |
| $D_{\text {i }}$ | $\left\{\begin{array}{l}\mathrm{He} \\ \hline\end{array}\right.$ | $5875.650{ }^{\dagger}$ |  |  |  | 3143.996 | 2 |
| $\mathrm{D}_{2}$ | $\{\mathrm{He}$ | $5875.618{ }^{\dagger}$ |  | $r$ | $\{\mathrm{Ti}+$ | 3143.764 | 4 |
|  | Fe | 5270.388 | 4 |  |  | 3101.895 | 3 |
| $E$ | $\{\mathrm{Ca}$ | 5270.268 | 3 | $S_{2}$ | $\{\mathrm{Ni}$ | 3101.574 | 4N |
|  | Fe | 5269.550 | 8D |  | Fe | 3100.682 | 3 |
| $b_{2}$ | Mg | 5183.619 | 30 |  | Fe | 3100.325 | 4N |
| $b_{2}$ | Mg | 5172.698 | 20 | $S_{2}$ | $\{\mathrm{Fe}$ | 3099.987 | 3 |
| $b_{3}$ | $\{\mathrm{Fe}+$ | 5169.050 | 4 |  | Fe | 3099.896 | 3 |
| $b_{3}$ | , Fe | 5168.908 | 3 | $s$ | Fe | 3047.614 | 35 |
| $b_{4}$ | $\{\mathrm{Fe}$ | 5167.508 | 5 |  | $(\mathrm{Fe}$ | 3021.077 | 30 |
| b4 | $\{\mathrm{Mg}$ | 5167.328 | 15 | $T$ | $\{\mathrm{Fe}$ | 3020.656 | 40 |
| $F$ | $\mathrm{H}_{8}$ | 4861.342 | 30 |  | Fe | 3020.490 | 20 |
| . 9 | $\mathrm{H}_{7}$ | 4340.475 | 20N | $t$ | FeNi | 2994.436 | 40 |

[^239]
## REFERENCES FOR STAND.ARD WAVELENGTHS

177 Trans Int. Union Coop. Solar Res., vol. 2, p. 142, 1907.
${ }^{178}$ Trans. Int. Astron. Union, vol. 1, p. 35, 1922.
${ }_{179}$ Procès Verbaux Comité Int. Poids et Mesures, Ser. 2, vol. 12, p. 67, 1927.
150 Ihid., vol. 17. p. 91, 1935.
${ }^{181}$ Proc. Roy. Soc. London, vol. A186, p. 164, 1946.
182 Journ. Opt. Soc. Amer., vol. 38, p. 7, 1948 ; vol. 40, p. 545,1950 . Comptes Rendus, vol. 228, p. 964, 1949.
${ }_{183}$ Trans. Int. Astron. Union, vol. 5, p. 86, 1935.
154 Ibid., vol. 5, p. 87, 1935.
iss Ihid., vol. 1, p. 36, 1922.
${ }^{158}$ Ihid., vol. 3, p. 86, 1928 ; vol. 4, p. 234,1932 ; vol. 6, p. 79, 1938.
${ }^{157}$ Ihid., vol. 5, p. 84, 1935 ; vol. 7, p. $146,1949$.
158 Ibid., vol. 6, p. 80, 1938.
${ }^{18}$ Ibid., vol. 1, p. 41, 1922 ; vol. 2, p. 42, 1925.
${ }^{2} 0$ Phys. Rev., vol. 47, f. 653, 1935.
${ }^{101}$ Trans. Int. Astron. 'tnion, vol. 3, p. 93, 1928 ; vol. 6, p. 90, 1938.
192 Philos. Trans., vol. 177, p. $457,1886$.

Series relations in atomic spectra.-The analysis of atomic spectra began in 1889 when J. R. Rydberg first found that the wave number (number of waves per cm ) of a spectral line could be represented as the difference between two numerical quantities that he called spectral terms. From the data of alkali and alkaline-earth spectra Rydberg sorted singlet, doublet, and triplet terms that formed sequences of the form $\frac{R}{(n+\mu)^{2}}$, where $R$ is Rydberg's constant, $n$ is an integer, and $\mu$ a fraction. Rydberg also distinguished between sharp, principal, and diffuse terms; the initial letters $s, p$, and $d$ survive in spectroscopic notation today. To distinguish between successive terms of a series, cardinal numbers ( $n$ ) were prefixed to the literal symbols, and to distinguish between the components of doublet and triplet terms numerical subscripts were arbitrarily attached.

Thus the wave numbers of the yellow doublet of sodium were represented symbolically: $\sigma=1 s-2 p_{1,2}$. More than 30 years passed before these arbitrary symbols could be given any atomic interpretation.
The concept of atomic energy levels was first clearly stated in 1913 by N. Bohr who postulated (1) that stationary atomic states exist, and (2) that the frequency of atomic radiation is proportional to the difference between two atomic energy states, $h v=\left(E_{1}-\right.$ $E_{2}$ ), the proportionality factor being Planck's constant, h. By 1919 the accumulation of singlet, doublet, and triplet terms found in arc and spark spectra barely sufficed to suggest two general laws of spectral structures: (1) the alternation law which states that even and odd multiplicities alternate in successive columns of the periodic chart of the atoms, and (2) the displacement law which states that the spectrum of an ionized atom resembles that of the preceding atom but the analogous lines are displaced toward higher frequencies. Term multiplicities of atoms or ions are thus determined solely by the number of electrons in the atoms, whereas the atomic charge controls the position of the spectrum. These two facts suggested that electrons and protons were involved in the exegesis of atomic spectra.
The more complex spectra resisted all attempts at interpretation until 1922 when M. A. Catalán deliberately set out to discover a new or more general principle in spectral structure. He found in the arc spectra of chromium and manganese terms having five or six levels which combined to produce groups of lines that he called multiplets. In a few years thousands of terms were found in atomic and ionic spectra, and contemporaneously the present quantum theory of atomic encrgy levels was developed. As a result of these developments the arbitrary symbols that empirical spectroscopy devised for the yellow doublet of sodium were replaced by the following:

$$
\sigma=3{ }^{2} S_{1 / 2}-3^{2} P^{\circ}{ }_{14,11 / 2}
$$

Each and every item of this spectroscopic notation now has definite physical meaning in terms of a vector model of the Rutherford-Bohr atom which is assumed to consist of a minute but massive nucleus (composed of protons and neutrons) with one or more electrons circulating about it. The normal number of electrons in any atom is equal to the atomic number, $Z$ : identical with the number of protons in its nucleus.

Spectral lines result from changes in atomic energies defined by the positions of one or more optical electrons in successive shells and by their orbital and axial momenta, each of which is associated with an appropriate quantum number. In general, the first large change in atomic energy occurs when an clectron jumps from its normal shell, represented by the principal quantum number $n$, to another shell. These principal quantum numbers identify the successive shells of the periodic system and serve as coefficients to the spectral term symbols $S, P, D, F$, etc. If an electron is moved from its lowest value of $n$ to $n=\infty$ the atom is ionized, and the voltage necessary to remove this electron is called the ionization potential. This ionization energy is expressed in wave number $\left(\mathrm{cm}^{-1}\right)$ or in electron volts (ev) as in Tables 623 and 624. Increasing atomic energies are exhibited in absorption spectra, decreasing energies in emission spectra.

After that due to a change in $n$, the next largest change in atomic energy is usually one associated with orbital angular momentum symbolized by an azimuthal quantum number $l$ having integral values $0,1,2,3,---$ corresponding respectively to the empirical term symbols $S, P, D, F,--$. Electrons with $l=0$ are called $s$-electrons, those with $l=1, p$-electrons, etc. These four $l$ values and the first seven $n$ values suffice to describe the normal electron configurations of all possible atoms and ions. When two or more optical electrons are present, their individual orbital momenta $l_{1} . l_{2}---$ are added vectorially to form a resultant $L$ which is restricted by quanturn theory to integral values ranging in the case of two electrons from $l_{1}+l_{2}$ to $\left|l_{1}-l_{2}\right|$. The types of spectral terms resulting from various simple configurations of electrons are shown in Table 621.

## TABLE 621.-L VALUES AND SPECTRAL TERMS RESULTING FROM TWO ELECTRONS

| Electrons | $L$ | Terms |
| :---: | :---: | :---: |
| ss | 0 | $S$ |
| $s p$ | 1 | $P$ |
| $p p$ | 012 | $S P D$ |
| $p d$ | 123 | $P D F$ |
| dd | $\begin{array}{lllll}0 & 1 & 234\end{array}$ | $S P D F G$ |
| $\stackrel{d f}{\text { ff }}$ | 1 0 0 1234456 |  |
|  | (continued) |  |

## TABLE 621.-L VALUES AND SPECTRAL TERMS RESULTING FROM TWO ELECTRONS (concluded)

A third contribution to the total energy of an atom or ion comes from the rotation of each electron about its own axis. This axial angular momentum is the same for all electrons ; it is represented by the spin quantum number $s=1 / 2$. When two or more electrons are present the individual spin vectors $s_{1}, s_{2}, \ldots$ combine with each other to yield a resultant $S$, but (like $L$ ) the resultant spin $S$ can take only certain discrete values, the maximum being obtained when all the individual spins are parallel, and the minimum being either one-half or zero according as the number of electrons is odd or even. Electron spins account for the splitting of most spectral terms into two or more components (called levels) and give a physical meaning to the subscripts attached to these levels. These subscripts are called inner quantum numbers: they are symbolized by $J$ to represent the vector sum of $L$ and $S$. The largest and smallest values of $J$ result from simple addition and subtraction of $L$ and $S$ and all intermediate values of $J$ that differ by integral amounts are allowed:

$$
J=(L+S),(L+S-1)
$$

when $L>S$ the number of permitted $J$ values is $2 S+1$, which fixes the term multiplicity $R$ and underlies the alternation law, since the maximum multiplicity will be even or odd according as the number of electrons is odd or even. The $S$ values and spectral-term multiplicities associated with numbers of optical electrons are displayed in Table 613.

Because $s=1 / 2$ for each electron the total angular momentum $J$ of an atom or ion will have integral values for levels belonging to odd multiplicities, and half-integral values for levels if the term multiplicities are even, as shown in Table 615.

TABLE 622.-TERMS FROM EQUIVALENT ELECTRONS

| Electrons | Terms (omitting $J$ values) |
| :---: | :---: |
| $s^{2}$ | ${ }^{1} S$ |
| $p^{2}$ | ${ }^{1} S,{ }^{1} D,{ }^{3} P$ |
| $p^{8}$ | ${ }^{2} P,{ }^{2} D,{ }^{4} S$ |
| $d^{2}$ | ${ }^{1} S,{ }^{1} D,{ }^{1} G,{ }^{8} P,{ }^{8} \mathrm{~F}$ |
| $d^{3}$ | ${ }^{2} P,{ }^{2} D,{ }^{2} D,{ }^{2} F,{ }^{2} G,{ }^{2} H,{ }^{4} P,{ }^{4} F$ |
| $f^{2}$ | ${ }^{1} S,{ }^{1} D,{ }^{1} G,{ }^{1} I,{ }^{3} P,{ }^{3} F,{ }^{8} \mathrm{H}$ |

The actual types and multiplicities of terms arising from various configurations of optical electrons depend on whether the electrons are equivalent or nonequivalent, that is, have the same or different values of $n$ and $l$. In any atom the maximum number of equivalent electrons is $2(2 l+1)$, and no shell can contain more than two $s$ electrons $\left(s^{2}\right)$, six $p$ electrons ( $p^{6}$ ), ten $d$ electrons ( $d^{\text {10 }}$ ) or fourteen $f$ electrons ( $f^{14}$ ). In simple cases the spectral terms arising from nonequivalent electrons may be obtained from the $L$ values of Table 621 and the $S$ values of Table 613, as shown in Table 616.

When the optical electrons are equivalent, the Pauli exclusion principle introduces simplifications, some of which are evident by comparing Tables 616 and 622.

An important consequence of the Pauli principle is that closed shells, in which the maximum number of equivalent electrons is present, have $L=O$ and $S=O$ and therefore may be ignored in deriving the terms given by any electron configuration. Furthermore, any subgroup that lacks one or more electrons to fill the group behaves spectroscopically as if the lacking electrons were present, except that the terms are, in general, regular (smallest $J$ level has least energy) when the group is less than half filled but inverted when more than half filled.

Each configuration (excluding single eiectrons and closed shells) yields many energy states, and the object of spectrum analysis is to determine (1) the numerical values of the energy levels, (2) the quantum numbers that characterize them, and (3) the electron configurations from which they arise. The wave number of each obscrved spectral line measures the energy difference between two quantized states of an atom or ion, but, because the same level can in general combine with many others, the number of levels is usually much smaller than the number of classified lines. The combining properties of atomic energy levels are governed by simple rules. Thus all terms or levels of a given atom fall into two groups of different parity called even and odd according as the arithmetical sum of the $l$ values of the optical electrons is even or odd (distinguished by the sign ${ }^{\circ}$ and by
level value in italics), and normally spectral lines are permitted only when terms of different parity combine. Furthermore, an overwhelning majority of the transitions between atomic energy levels obey the following rules:

$$
\begin{aligned}
& \Delta R=0 \\
& \Delta L= \pm 1 \\
& \Delta J=0, \pm 1, \text { excepting } 0 \text { to } 0
\end{aligned}
$$

In complex spectra, especially of heavy elements, intersystem combinations are observed for $\Delta R= \pm 2, \pm 4$. Likewise, transitions for $\Delta L=0$ give strong multiplets, and transitions for which $\Delta L= \pm 2, \pm 3$ are observed but usually only faintly. Violations of the $\Delta J$ rule are extremely rare. Assignment of $L$ values and electron configurations to energy levels implicitly assumes that $L S$ coupling or interaction exists among the individual vectors. This means that the individual $l$ vectors are strongly coupled to produce resultant $L$ values of different energies, and the individual $s$ vectors are also strongly coupled to produce resultant $S$ values. These $L$ and $S$ resultants are then less strongly coupled with each other to produce resultant $J$ values. Other types of coupling such as $J J$ or $J L$ are sometimes met with and in such cases $L$ loses all or most of its significance. Also when the levels of two like-parity configurations overlap or dovetail, it is practically impossible to distinguish the two configurations or choose the levels that belong to each. However, because $L S$ coupling holds for all the higher elements, predominates in many others, and is either accurately or approximately valid for the ground states of all atoms and ions, it is basic for the standardized notation for spectral terms. Thus, any atomic energy level or spectral term is symbolically represented by four quantities. (1) its principal quantum number $n$ written as a coefficient of the term-type symbol; (2) its type- $S, P, D, F$, etc.where the capital letters stand for azimuthal quantum numbers or orbital angular momenta $L=0,1,2,3$, etc., respectively ; (3) its inner quantum number or total angular momentum $J=L+S$, written as a subscript to the term-type symbol; and (4) its multiplicity number, $R=2 S+1$, written as a superior prefix to the term-type symbol. In addition the parity, if the sum of $p$ and $f$ electrons is odd, is indicated by the sign ${ }^{\circ}$ attached like an exponent to the term-type symbol.

For any given spectrum in which energy levels have been established, and in which $L S$ coupling exists, it is possible to assign notation as well as electron configuration without ambiguity. Relative values of $J$ are readily determined from the combining properties of the levels and the selection rule, $\Delta J=0 \pm 1$. In terms of odd multiplicity the absolute value of $J$ is fixed by the absence of the transition 0 to 0 which is forbidden. In other cases the absolute value of $J$ can often be deduced from the sum rule (the sum of the intensities of all the lines of a multiplet that belong to the same initial or final state is proportional to the statistical weight $2 J+1$ of the initial or final state respectively), or from the interval rule (the interval between two successive components, $J$ and $J+1$, of a polyfold term is proportional to $J+1$ ). The most decisive determination of $J$ and $L$ (excepting singlet terms) results from the observation of completely resolved Zeeman patterns since an external magnetic field causes each energy level to be split into $2 J+1$ sublevels and the splitting factors indicate $L$ values.

It is a consequence of atomic structure that long series of spectral terms of the same parity, $L, S, J$, but increasing $n$, are observed only in one-electron spectra, as for example to $n=79$ in the first spectrum of sodium. Five- six- or seven-electrons provide so many configurations and competing levels that it is often exceedingly difficult to detect the second or any higher members of a spectral series.

Quantum principles having thus specified the various spectral terms arising from certain electrons, it became possible in 1925 to determine from identified terms the electron configurations of all atoms and ions. By 1950 the ground states of 82 species of neutral atoms and 75 singly ionized atoms had been uniquely determined from spectral structure. Besides disclosing the ground level and normal electron configuration of each atom or ion, the discovery of series relations in atomic spectra has given exact values for many ionization potentials which measure the forces with which the optical electrons are bound to atoms and ions. Furthermore, since the most intense radiations are usually associated with the largest $L$ and $J$ values of low-lying levels, the analysis of spectra has aided in selecting the strongest spectral lines characteristic of atoms and ions. In general, the strongest lines result from $s \longleftrightarrow p$ electron transitions, but do not necessarily end on the ground state. Because these data are of great importance in spectroscopy, atomic physics, chemistry, and astrophysics, they are collected for neutral atoms in Table 623 and for singly ionized atoms in Table 624. ${ }^{193}$

[^240]TABLE 623．－SPECTROSCOPIC PROPERTIES OF NEUTRAL ATOMS
The wavelengths of strongest lines exceeding 2000 A are valid for standard air，the remainder for vacuum．

| $\underset{n}{\text { Period }}$ | $\begin{aligned} & \text { Neutral } \\ & \text { atom } \end{aligned}$ | Normal electron configuration | Ground | Spectral multiplicities | Ionization potential volts | Strongest line，$A$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 H | $1 s^{1}$ | ${ }^{2} \mathrm{~S}_{01 /}$ | 2 | 13.595 | 1215.66 |
|  | 2 He | $1 s^{2}$ | ${ }^{1} \mathrm{~S}$ 。 | 1， 3 | 24.580 | 584.33 |
| 2 | 3 Li | $2 s^{1}$ | ${ }^{2} \mathrm{~S}_{01 / 4}$ | 2 | 5.390 | 6707.85 |
|  | 4 Be | $2 s^{2}$ | ${ }^{1} \mathrm{~S}^{2}$ | 1，3 | 9.320 | 2348.61 |
|  | 5 B | $2 s^{2} 2 p^{1}$ | ${ }^{2} \mathrm{P}^{\circ}{ }^{0}{ }^{1 / 2}$ | 2 | 8.296 | 2497.73 |
|  | 6 C | $2 s^{2} 2 p^{2}$ | ${ }^{3} \mathrm{P}$ 。 | 1， 3 | 11.264 | 1657.01 |
|  | 7 N | $2 s^{2} 2 p^{3}$ | ${ }^{4} \mathrm{~S}^{\circ}{ }^{1 / 2}$ | 2，4 | 14.54 | 1134.98 |
|  | 8 O | $2 s^{2} 2 p^{4}$ | ${ }^{3} \mathrm{P} \mathrm{P}_{2}$ | 1，3，5 | 13.614 | 1302.19 |
|  | 9 F | $2 s^{2} 2 p^{5}$ | ${ }^{2} \mathrm{P}^{\circ}{ }^{1 / 1 / 8}$ | 2，4 | 17.418 | 954.80 |
|  | 10 Ne | $2 s^{2} 2 p^{6}$ | ${ }^{1} \mathrm{~S}$ 。 | 1，3 | 21.559 | 735.89 |
| 3 | 11 Na | $3 s^{1}$ | ${ }^{2} \mathrm{~S}_{01 / 8}$ | 2 | 5.138 | 5889.95 |
|  | 12 Mg | $3 s^{2}$ | ${ }^{1} \mathrm{~S}_{0} \mathrm{P}_{0}$ | 1，3 | 7.644 | 2852.13 |
|  | 13 Al | $3 s^{2} 3 p^{1}$ | ${ }^{2} \mathrm{P}^{0}{ }_{0}{ }^{1 / 2}$ | 2 | 5.984 | 3961.53 |
|  | 14 Si | $3 s^{2} 3 p^{2}$ | ${ }^{8} \mathrm{P}$ 。 | 1，3 | 8.149 | 2516.12 |
|  | 15 P | $3 s^{2} 3 p^{3}$ | ${ }^{4} \mathrm{~S}^{\circ}{ }^{1 / 1 / 8}$ | 2，4 | 10.55 | 1774.94 |
|  | 16 S | $3 s^{2} 3 p^{4}$ | ${ }^{8} \mathrm{P}_{2}$ | 3， 5 | 10.357 | 1807.31 |
|  | 17 Cl | $3 s^{2} 3 p^{5}$ | ${ }^{2} \mathrm{P}^{0}{ }^{0}{ }_{1 / 2}$ | 2， 4 | 13.01 | 1347.2 |
|  | 18 A | $3 s^{2} 3 p^{8}$ | ${ }^{1} \mathrm{~S}$ 。 | 1， 3 | 15.755 | 1048.22 |
| 4 | 19 K | $4 s^{1}$ | ${ }^{2} \mathrm{~S}_{01 / 8}$ | 2 | 4.339 | 7664.91 |
|  | 20 Ca | $4 s^{2}$ | ${ }^{2} \mathrm{~S}_{0}$ | 1，3 | 6.111 | 4226.73 |
|  | 21 Sc | $3 d^{1} 4 s^{2}$ | ${ }^{2} \mathrm{D}_{11 /}$ | 2，4 | 6.538 | 5671.80 |
|  | 22 Ti | $3 d^{2} 4 s^{2}$ | ${ }^{3} \mathrm{~F}_{2}$ | 1，3，5 | 6：818 | 4981.73 |
|  | 23 V | $3 d^{3} 4 s^{2}$ | ${ }^{4} \mathrm{~F}_{1} 1 / 4$ | 2，4， 6 | 6.743 | 4379.24 |
|  | 24 Cr | $3 d^{6} 4 s^{1}$ | ${ }^{7} \mathrm{~S}_{3}$ | 1，3，5， 7 | 6.74 | 4254.35 |
|  | 25 Mn | $3 d^{5} 4 s^{2}$ | ${ }^{8} \mathrm{~S}_{21 / 4}$ | 2，4，6， 8 | 7.432 | 4030.76 |
|  | 26 Fe | $3 d^{6} 4 s^{2}$ | ${ }^{6} \mathrm{D}$ 4 | 1，3，5， 7 | 7.868 | 3581.20 |
|  | 27 Co | $3 d^{7} 4 s^{2}$ | ${ }^{4} \mathrm{~F}_{44 / 8}$ | 2，4， 6 | 7.862 | 3453.50 |
|  | 28 Ni | $3 d^{88} 4 s^{2}$ | ${ }^{3} \mathrm{~F}$ ； | 1，3， 5 | 7.633 | 3414.76 |
|  | 29 Cu | $3 d^{10} 4 s^{1}$ | ${ }^{2} \mathrm{~S}^{\circ}{ }_{01 / 9}$ | 2，4 | 7.724 | 3247.54 |
|  | 30 Zn | $4 s^{2}$ | ${ }^{1} \mathrm{~S}$ 。 | 1，3 | 9.931 | 2138.56 |
|  | 31 Ga | $4 s^{2} 4 p^{1}$ | ${ }^{2} \mathrm{P}^{0}{ }_{01 / 2}$ | 2，4 | 6.00 | 4172.06 |
|  | 32 Ge | $4 s^{2} 4 p^{2}$ | ${ }^{3} \mathrm{P}_{0}$ | 1，3 | 7.88 | 2651.18 |
|  | 33 As | $4 s^{2} 4 p^{3}$ | ${ }^{4} S^{\circ}{ }^{1}{ }_{1 / 2}$ | 2，4 | 9.81 | 1890.43 |
|  | 34 Se | $4 s^{2} 4 p^{4}$ | ${ }_{3}^{3} \mathrm{P}_{2}$ | 3，5 | 9.750 | 1960.91 |
|  | 35 Br | $4 s^{2} 4 p^{5}$ | ${ }^{2} \mathrm{P}^{\circ}{ }^{\circ}{ }_{1 / 8}$ | 2， 4 | 11.84 | 1488.4 |
|  | 36 Kr | $4 s^{2} 4 p^{6}$ | ${ }^{1} \mathrm{~S}_{0}{ }^{1 / 2}$ | 1， 3 | 13.996 | 1235.82 |
| 5 | 37 Rb | $5 s^{1}$ | ${ }^{2} \mathrm{~S}_{01 / 8}$ | 2 | 4.176 | 7800.23 |
|  | ． 38 Sr | $5 s^{2}$ | ${ }^{1} \mathrm{~S}$ o | 1，3 | 5.692 | 4607.33 |
|  | 39 Y | $4 d^{1} 5 s^{2}$ | ${ }^{2} \mathrm{D}_{1 / 2}$ | 2，4 | 6.377 | 5466.47 |
|  | 40 Zr | $4 d^{2} 5 s^{2}$ | ${ }^{3} \mathrm{~F}_{2}$ | 1，3，5 | 6.835 | 4687.80 |
|  | 41 Nb | $4 d^{4} 5 s^{1}$ | ${ }^{6} \mathrm{D}_{0} 1 / 4$ | 2，4， 6 | 6.881 | 4058.94 |
|  | 42 Mo | $4 d^{5} 5 s^{1}$ | ${ }^{7} \mathrm{~S}_{3} \mathrm{~S}_{3}$ | 3，5， 7 | 7.131 | 3798.25 |
|  | 43 Tc | $4 d^{8} 5 s^{2}$ | ${ }^{8} \mathrm{~S}^{5} \mathrm{~F}_{21 / 2}$ | 4，6， 8 | 7.23 | 3636.10 349894 |
|  | ${ }_{45}^{44 \mathrm{Ru}}$ | $4 d^{7} 5 s^{1}$ $4 d^{8} 5 s^{1}$ | ${ }^{5}{ }^{5} \mathrm{~F}_{5} \mathrm{~F}_{5}$ | 3，5， 7 | 7.365 7.461 | 3498.94 3434.89 |
|  | 46 Pd | $4 d^{10}$ | ${ }^{1} \mathrm{~S}_{0}{ }^{1 / 2}$ | 1，3， 5 | 8.33 | 3404.58 |
|  | 47 Ag | $5 s^{1}$ | ${ }^{2} \mathrm{~S}_{01 / 8}$ | 2，4 | 7.574 | 3280.68 |
|  | 48 Cd | $5 s^{2}$ | ${ }^{1} \mathrm{~S}$ 。 | 1，3 | 8.991 | 2288.02 |
|  | （continued） |  |  |  |  |  |

TABLE 623.-SPECTROSCOPIC PROPERTIES OF NEUTRAL ATOMS (concluded)


TABLE 624．－SPECTROSCOPIC PROPERTIES OF SINGLY－IONIZED ATOMS
The wavelengths of strongest lines exceeding 2000 A are valid for standard air，the remainder for vacuum．

| $\underset{n}{\text { Period }}$ | Ionized | $\begin{gathered} \text { Normal } \\ \text { electron } \\ \text { configuration } \end{gathered}$ | $\begin{gathered} \text { Ground } \\ \text { level } \end{gathered}$ | Spectral multiplicities | Ionization potential volts | Strongest line，$A$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $1 \mathrm{H}^{+}$ |  |  |  |  |  |
|  | $2 \mathrm{He}^{+}$ | $1 \mathrm{~s}^{1}$ | ${ }^{2} \widetilde{S}_{0}{ }_{0}$ | $\dddot{2}$ | 54.403 | 303.78 |
| 2 | $3 \mathrm{Li}^{+}$ | $1 s^{2}$ | ${ }^{1} \mathrm{~S}_{0}$ | 1，3 | 75.6193 | 1．99．26 |
|  | $4 \mathrm{Be}^{+}$ | $2 s^{1}$ | ${ }^{2} \mathrm{~S}_{01 / 4}$ | 2 | 18.206 | 3130.42 |
|  | $5 \mathrm{~B}^{+}$ | $2 s^{2}$ | ${ }^{2} \mathrm{~S}^{2}$ | 1， 3 | 25.149 | 1362.46 |
|  | $6 \mathrm{C}^{+}$ | $2 s^{2} 2 p^{1}$ | ${ }^{2} \mathrm{P}^{\circ}{ }_{0}{ }^{1 / 2}$ | 2，4 | 24.376 | 1335.71 |
|  | 7 N ＋ | $2 s^{2} 2 p^{2}$ | ${ }^{3} \mathrm{P}_{0}$ | 1，3，5 | 29.605 | 1085.74 |
|  | $8 \mathrm{O}^{+}$ | $2 s^{2} 2 p^{3}$ | ${ }^{1} \mathrm{~S}^{\circ}{ }_{1}{ }^{1 / 1}$ | 2，4 | 35.146 | 834.47 |
|  | $9 \mathrm{~F}+$ | $2 s^{2} 2 p^{4}$ | ${ }^{3} \mathrm{P}_{2}$ | 1，3，5 | 34.98 | 606.81 |
|  | $10 \mathrm{Ne}+$ | $2 s^{2} 2 p^{5}$ | ${ }^{2} \mathrm{P}^{2}{ }^{1} 1 / 4$ | 2，4 | 41.07 | 460.73 |
| 3 | $11 \mathrm{Na}+$ | $2 s^{2} 2 p^{8}$ | ${ }^{1} \mathrm{~S}_{0}$ | 1， 3 | 47.29 | 372.07 |
|  | $12 \mathrm{Mg}{ }^{+}$ | $3 s^{1}$ | ${ }^{2} \mathrm{~S}_{0} \mathrm{~S}_{4}$ | 2 | 15.03 | 2795.53 |
|  | $13 \mathrm{Al}^{+}$ | $3 s^{2}$ | ${ }^{1} \mathrm{~S}$ 。 | 1，3 | 18.823 | 1670.81 |
|  | $14 \mathrm{Si}+$ | $3 s^{2} 3 p^{1}$ | ${ }^{2} \mathrm{P}^{\circ}{ }_{0} 1 / 2$ | 2，4 | 16.34 | 1817.0 |
|  | $15 \mathrm{P}+$ | $3 s^{2} 3 p^{2}$ | ${ }^{3} \mathrm{P}$ 。 | 1，3，5 | 19.65 | 1542.32 |
|  | 16 S ＋ | $3 s^{2} 3 p^{3}$ | ${ }^{4} \mathrm{~S}^{\circ}{ }_{1 / 1}$ | 2，4 | 23.4 | 1259.53 |
|  | $17 \mathrm{Cl}+$ | $3 s^{2} 3 p^{4}$ | ${ }^{3} \mathrm{P}_{2}$ | 1，3， 5 | 23.80 | 1071.05 |
|  | $18 \mathrm{~A}+$ | $3 s^{2} 3 p^{5}$ | ${ }^{2} \mathrm{P}^{\circ}{ }_{1 / 2}$ | 2，4 | 27.62 | 919.78 |
| 4 | $19 \mathrm{~K}+$ | $3 s^{2} 3 p^{0}$ | ${ }^{1} \mathrm{~S}_{0}{ }^{1 / 2}$ | 1，3 | 31.81 | 600.77 |
|  | $20 \mathrm{Ca}+$ | $4 s^{1}$ | ${ }^{2} \mathrm{~S}_{014}$ | 2 | 11.87 | 3933.67 |
|  | ${ }_{21} \mathrm{Sc}^{+}$ | $3 d^{1} 4 s^{1}$ | ${ }^{3} \mathrm{D}_{1}$ | 1，3 | 12.80 | 3613.84 |
|  | $22 \mathrm{Ti}+$ | $3 d^{2} 4 s^{1}$ | ${ }^{4} \mathrm{~F}_{1}{ }^{1 / 2}$ | 2，4 | 13.57 | 3349.41 |
|  | $23 \mathrm{~V}+$ | $3 d^{4}$ | ${ }^{5} \mathrm{D}$ 。 | 1，3，5 | 14.65 | 3093.11 |
|  | ${ }_{24} \mathrm{Cr}+$ | $3 d^{5}$ | ${ }^{8} \mathrm{~S}_{2 \%}$ | 2，4， 6 | 16.49 | 2835.63 |
|  | 25 Mn ＋ | $3 d^{5} 4 s^{1}$ | ${ }^{7} \mathrm{~S}_{3}$ | 3，5， 7 | 15.64 | 2576.10 |
|  | ${ }^{26} \mathrm{Fe}{ }^{+}$ | $3 d^{6} 4 s^{2}$ | ${ }^{6} \mathrm{D}_{4}{ }_{4} / 4$ | 2，4，6， 8 | 16.18 | 2382.04 |
|  | ${ }^{27} \mathrm{Co}^{+}$ | $3 d^{8}$ | ${ }^{9} \mathrm{~F}_{4}{ }^{\text {d }}$ | 3，5 | 17.05 | 2286.14 |
|  | $28 \mathrm{Ni}^{+}$ | $3 d^{\text {b }}$ | ${ }^{2} \mathrm{D}_{2 / 2}$ | 2， 4 | 18.15 | 2216.47 |
|  | ${ }_{29} \mathrm{Cu}^{+}$ | $3 d^{10}$ | ${ }^{1} \mathrm{~S}^{2}$ | 1，3，5 | 20.29 | 2135.98 |
|  | ${ }_{30} \mathrm{Zn}^{+}$ | $4 s^{1}$ | ${ }^{2} \mathrm{~S}_{0} \mathrm{~S}_{1 / 8}$ | 2，4 | 17.96 | 202551 |
|  | ${ }_{31} \mathrm{Ga}{ }^{+}$ | $4 s^{2}$ | ${ }^{1} \mathrm{~T}^{1} \mathrm{~S}$ 。 | 1，3 | 20.51 | 1414.44 |
|  | $32 \mathrm{Ge}+$ | $4 s^{2} 4 p$ | ${ }^{2} \mathrm{P}^{\circ}{ }_{0 \%}$ | 2 | 15.93 | 1649.26 |
|  | $33 \mathrm{As}+$ | $4 s^{2} 4 p^{2}$ | ${ }^{8} \mathrm{P}_{0}{ }^{\text {a }}$ | 1，3 | 20.2 | 1266.36 |
|  | $34 \mathrm{Se}+$ | $4 s^{2} 4 p^{8}$ | ${ }^{6} \mathrm{~S}{ }^{\circ}{ }_{1 / 1}$ | 2，4 | 21.5 | 1192.29 |
|  | ${ }^{35} \mathrm{Br}^{+}$ | $4 s^{2} 4 p^{4}$ | ${ }^{3} \mathrm{~S}_{2}{ }^{2}$ | 1，3，5 | 21.6 | 1015.42 |
|  | ${ }_{36} \mathrm{Kr}^{+}$ | $4 s^{2} 4 p^{5}$ | ${ }^{2} \mathrm{P}^{0}{ }_{1 \%}$ | 2，4 | 24.56 | 917.43 |
| 5 | $37 \mathrm{Rb}+$ | $4 s^{2} 4 p^{6}$ | ${ }^{1} \mathrm{~S}_{0}{ }^{1 /}$ | 1， 3 | 27.5 | 741.4 |
|  | $38 \mathrm{Sr}{ }^{+}$ | $5 s^{1}$ |  | 2 | 11.026 | 4077.71 |
|  | $39 \mathrm{Y}+$ | $5 s^{2}$ | ${ }^{1} \mathrm{~S}_{0}{ }^{\text {a }}$ | 1，3 | 12.233 | 3710.29 |
|  | $40 \mathrm{Zr}+$ | $4 d^{2} 5 s^{1}$ | ${ }^{4} \mathrm{~F}_{12 / 4}$ | 2，4 | 12.916 | 3391.98 |
|  | $41 \mathrm{Nb}{ }^{+}$ | $4 d^{4}$ | ${ }^{5} \mathrm{D}$ 。 | 1，3，5 | 13.895 | 3094.18 |
|  | $42 \mathrm{Mo}+$ | $4 d^{5}$ | ${ }^{6} \mathrm{~S}_{21 / 2}$ | 4， 6 | ．．． | 2816.15 |
|  | $43 \mathrm{Tc}{ }^{+}$ | $4 d^{5} 5 s^{1}$ | ${ }^{7} \mathrm{~S}_{3}$ | 5，7 | ．．． | 2543.24 |
|  | $44 \mathrm{Ru}+$ | $4 d^{7}$ | ${ }^{4} \mathrm{~F}_{44}{ }^{\text {a }}$ | 2，4，6 |  | 2402.72 |
|  | $45 \mathrm{Rh}{ }^{+}$ | $4 d^{8}$ | ${ }^{3} \mathrm{~F}$ | 3，5 |  | 2334.77 |
|  | $46 \mathrm{Pd}+$ | $4 d^{\circ}$ | ${ }^{2} \mathrm{D}_{2 / 8}$ | 2，4 | 19.9 | 2296.53 |
|  | $47 \mathrm{Ag}+$ | $4 d^{10}$ | ${ }^{1} \mathrm{~S}^{2}{ }^{2}$ | 1，3 | 21.5 | 2246.41 |
|  | $48 \mathrm{Cd}^{+}$ | $5 s^{1}$ | ${ }^{2} \mathrm{~S}^{151 / 2}$ | 2，4 | 16.90 | 2144.38 |
|  | $49 \mathrm{In}{ }^{+}$ | 5s ${ }^{2}$ | ${ }^{1} \mathrm{~S}$ ， | 1,3 | 18.86 | 1586.4 |
|  | $50 \mathrm{Sn}^{+}$ | $5 s^{2} 5 p^{1}$ | ${ }^{2} \mathrm{P}^{\circ}{ }^{01 / 2}$ | 2， 4 | 14.6 | 2152.22 |
|  | ${ }_{52} \mathrm{Sb}^{+}$ | $5 s^{2} 5 p^{2}$ | ${ }^{3} \mathrm{P}$ ． | 1，3 | 19 | 1606.98 |
|  | ${ }_{53} \mathrm{TE}^{+}$ | 5s ${ }^{2} 5 p^{2} 5 p^{1}$ | ${ }^{3} \mathrm{~S}_{12}{ }^{3} \mathrm{P}^{2}$ | 1，3，5 | 21.5 19.0 | 1161.52 |
|  | $54 \mathrm{Xe}{ }^{+}$ | $5 s^{2} 5 p^{5}$ | ${ }^{2} \mathrm{P}^{2}{ }_{1 / 4}$ | 1，4 | 21.2 | 1100.42 |


| $\underset{n}{\text { Period }}$ | Ionized atom | $\begin{gathered} \text { Normal } \\ \text { electron } \\ \text { configuration } \end{gathered}$ | Ground level | Spectral multiplicities | Ionization potential volts | Strongest line，$A$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 55 Cs ＋ | $5 s^{2} 5 p^{\circ}$ | ${ }^{1} \mathrm{~S}^{2}$ ， | 1，3 | 23.5 | 926.75 |
|  | $56 \mathrm{Ba}+$ | $6 s^{1}$ | ${ }^{2} \mathrm{Sa}_{3}{ }_{3}$ | 2 | 10.00 | 4554.04 |
|  | $57 \mathrm{La}{ }^{+}$ | $5 d^{2}$ | ${ }^{3} \mathrm{~F}$ ， | 1，3 | 11.43 | 3949.10 |
|  | ${ }_{58} \mathrm{Ce}^{+}$ | $4 f^{2} 6 s^{1}$ | ${ }^{4} \mathrm{H}_{3}{ }^{1 / 4}$ | 2，4 | ．．． | 4186.60 |
|  | $59 \mathrm{Pr}{ }^{+}$ | $4 f^{\circ} 6 s^{1}$ | ${ }^{\circ} \mathrm{I}^{\circ}$ ． | 3，5 |  | 4179.42 |
|  | $60 \mathrm{Nd}^{+}$ | $4 f^{6} 6 s^{1}$ | ${ }^{\circ} \mathrm{I}_{31 / 4}$ | 4，6，8 |  | 4303.57 |
|  | $61 \mathrm{Pm}{ }^{+}$ | $4 f^{6} 6 s^{1}$ | $\stackrel{\square}{8}$ |  |  |  |
|  | $62 \mathrm{Sm}{ }^{+}$ | $4 f^{8} 6 s^{1}$ | ${ }^{8} \mathrm{~F}_{0}{ }^{\text {a }}$ | 6，8 | 11.2 | 3568.27 |
|  | $63 \mathrm{Eu}{ }^{+}$ | $4 f^{\prime} 6 s^{1}$ | ${ }^{9} \mathrm{~S}$ ， | 7，9 | 11.24 | 4205.05 |
|  | $64 \mathrm{Gd}^{+}$ | $4 f^{7} 6 s^{1} 5 d^{1}$ | ${ }^{10} \mathrm{D}^{\circ}{ }_{23 /}$ | 6，8， 10 | $12 \pm$ | 3422.47 |
|  | $65 \mathrm{~Tb}^{+}$ |  | ．．． | ．．． |  | ．．． |
|  | $66 \mathrm{Dy}{ }^{+}$ | ．．． | ．．． | $\ldots$ | ．．． | ．．． |
|  | $67 \mathrm{Ho}{ }^{+}$ |  | $\ldots$ | $\ldots$ | $\ldots$ |  |
|  | ${ }_{69} 68 \mathrm{Tm}^{+}$ | $4{ }^{1 \mathrm{f}^{\mathrm{is}} \dot{6} s^{2}}$ | ${ }^{3} \stackrel{1}{5}^{\circ}$ 。 | 1， 3 |  | 3848.02 |
|  | $70 \mathrm{Yb}^{+}$ | $4 f^{4} 6 s^{1}$ | ${ }^{2} \mathrm{~S}_{0}{ }^{3}$ | 2 | 12.10 | 3694.20 |
|  | $71 \mathrm{Lu}{ }^{+}$ | $6 s^{2}$ | ${ }^{1} \mathrm{~S}_{0}$ | 1，3 | 14.7 | 2615.43 |
|  | $72 \mathrm{Hf}+$ | $5 d^{1} 6 s^{2}$ | ${ }^{2} \mathrm{D}_{13}{ }^{\text {a }}$ | 2，4 | 14.9 | 2641.41 |
|  | $73 \mathrm{Ta}+$ | $5 d^{3} 6 s^{1}$ | ${ }^{6} \mathrm{~F}_{3}$ | 1，3， 5 | ．．． | 2685.17 |
|  | $74 \mathrm{~W}^{+}$ | $5 d^{4} 6 s^{1}$ | ${ }^{6} \mathrm{D}_{014}$ | 4，6 | $\ldots$ | 2204.49 |
|  | $75^{+} \mathrm{Re}$＋ | $5 d^{5} 6 s^{1}$ | ${ }^{7} \mathrm{~S}_{3}$ | 5，7 | $\ldots$ | ．．． |
|  | $76 \mathrm{Os}{ }^{+}$ |  | ．．． | $\ldots$ | ．．． |  |
|  | $77 \mathrm{Ir}{ }^{+}$ |  |  |  |  |  |
|  | $78 \mathrm{Pt}{ }^{+}$ | $5 d^{\text {b }}$ | ${ }^{2} \mathrm{D}_{2}{ }^{1 / 4}$ | 2，4 | 18.54 | 1777.09 |
|  | $79 \mathrm{Au}+$ | $5 d^{10}$ | ${ }^{1} \mathrm{~S}^{2}{ }^{\text {a }}$ | 1 | 20.5 | 1740.47 |
|  | $80 \mathrm{Hg}^{+}$ | $6 s^{2}$ | ${ }^{2} \mathrm{~S}_{0} \mathrm{~S}_{0}$ | 2，4 | 18.751 | 1649.96 |
|  | ${ }_{82}^{81 ~} \mathrm{Tl}^{+}+$ | $6 s^{2}$ | ${ }_{2}^{1} \mathrm{~S}_{2} \mathrm{p}_{0}$ | 1， 3 | 20.42 | 1908.64 |
| 8 | $82 \mathrm{~Pb}{ }^{+}$ | $6 s^{2} 6 p^{1}$ | ${ }^{2} \mathrm{P}^{\circ}{ }^{\text {anh }}$ | 2，4 | 15.03 | 1726.75 |
|  | $83 \mathrm{Bi}^{+}$ | $6 s^{2} 6 p^{2}$ | ${ }^{3} \mathrm{P}$ 。 | 3 | 16.7 | 1902.41 |
|  | $84 \mathrm{Po}^{+}$ | $\ldots$ | ．．． | $\cdots$ | $\cdots$ | ．．． |
|  | $86 \mathrm{Rn}{ }^{+}$ |  |  | $\ldots$ |  |  |
|  | $87 \mathrm{Fr}{ }^{+}$ |  |  |  |  |  |
| 7 | 88 Ra ＋ | $7 \mathrm{~s}^{1}$ | ${ }^{2} \mathrm{~S}_{04}$ | 2 | 10.14 | 3814.42 |
|  | $89 \mathrm{Ac}+$ | $7 s^{2}$ | ${ }^{1} \mathrm{~S}$ 。 | 1，3 | ．．． |  |
|  | $90 \mathrm{Th}{ }^{+}$ | $6 d^{2} 7 s^{1}$ | ${ }^{4} \mathrm{~F}_{14}{ }^{\text {a }}$ | 2，4 | $\ldots$ | 4019.14 |
|  | ${ }_{92} 91 \mathrm{~Pa}^{+}+$ | $5 \mathrm{f}^{9} 7 s^{2}$ | ${ }^{\circ} \mathrm{I}{ }^{\circ}{ }^{\circ}{ }^{\text {a }}$ | 4，6 |  | 3719.29 |
|  | $93 \mathrm{~Np}+$ |  | ［1／2 | 4，6 |  | ．．． |
|  | $94 \mathrm{Pu}{ }^{+}$ |  | ．．． | ．．． | ．．． | $\ldots$ |
|  | $95 \mathrm{Am}+$ | $\ldots$ | $\ldots$ | ．．． |  |  |
|  | $96 \mathrm{Cm}{ }^{+}$ | $\ldots$ | $\ldots$ | $\ldots$ |  | $\ldots$ |
|  | $97 \mathrm{Bk}{ }^{+}$ | ．．． | ． | $\cdots$ |  | $\ldots$ |
|  | 98 Cf | ．．． | $\ldots$ | ．．． | $\cdots$ | ．．． |

References for series relations in atomic spectra：Meggers，W．F．，Journ．Opt．Soc．Amer．，vol．31， p．44，1941；vol．31．p．606，1941．Pauling，L．，and Goudsmit，S．，The structure of line spectra， McGraw－Hill Book Co．，New York， 1930 ．White，H．E．，Introduction to atomic spectra，McGraw－ Hill Book Co．，New York，1934．Herzberg，G．，Atomic spectra and atomic structure，Dover Publica－ tions，New York，1944．Condon，E．U．，and Shortley，G．H．，The theory of atomic spectra，Macmillan Co．，New York，1935．Bacher，R．F．，and Goudsmit，S．，Atomic energy states，McGraw－Hill Book Co．，New York．1932．Moore，C．E．，Atomic energy levels，Nat．Bur．Standards Circ．467，vol．1， 1949；vol．2， 1952.

## TABLE 625.-MOLECULAR CONSTANTS OF DIATOMIC MOLECULES *

The energy, $E$, of a molecule is the sum of three contributions, the electronic energy, $E_{e}$, the vibrational energy, $E_{v}$, and the rotational energy, $E_{r}$, i.e.,

$$
\begin{equation*}
E=E_{0}+E_{v}+E_{r} \tag{1}
\end{equation*}
$$

The electronic energy, $E_{e}$, gives the largest contribution and is entirely similar to the energy of atoms. Similar to $S, P, D$ states of atoms, one distinguishes $\Sigma, \Pi, \Delta, \ldots$ states of diatomic molecules depending on whether the electronic orbital angular momentum about the intes nuclear axis is $0,1,2 \ldots$ in units of $h / 2 \pi$. Just as for atoms the resultant electron spin $S$ determines the multiplicity $(2 S+1)$ of the electronic state which is added to the term symbol as a left superscript. $\Sigma$ states are designated $\Sigma^{+}$or $\Sigma^{-}$depending on whether their eigenfunctions remain unchanged or change sign upon reflection at a plane through the internuclear axis. For molecules with identical nuclei (such as $\mathrm{N}_{2}, \mathrm{H}_{2}$, $\mathrm{O}_{2}, \ldots$ ) a subscript $g$ or $u$ indicates whether the eigenfunction upon reflection at the center remains unchanged or changes sign (e.g. ${ }^{1} \Sigma_{0}{ }^{+},{ }^{1} \Sigma_{u}{ }^{+},{ }^{1} \Pi_{g}, \ldots$. . .
In each electronic state the molecule may have various amounts of vibrational energy. Quantum mechanics shows that for diatomic molecules the vibrational energy is given by

$$
\begin{equation*}
\frac{E_{v}}{h c}=G(v)=\omega_{e}\left(v+\frac{1}{2}\right)-\omega_{e} x_{e}\left(v+\frac{1}{2}\right)^{2}+\ldots \tag{2}
\end{equation*}
$$

where $v$ is the vibrational quantum number which can assume the values $0,1,2, \ldots$ and where $\omega_{e}$ is the (classical) vibrational frequency (in $\mathrm{cm}^{-1}$ ) for infinitesimal amplitudes. The constant $\omega_{e} x_{e}$ is small compared to $\omega_{e}$ and is due to the anharmonicity of the vibration.
If the vibrational energy is increased more and more, a point is reached at which the two atoms fly apart, that is, the molecule is dissociated. The dissociation energy, $D_{0}$, corresponds to the maximum of the function $G(v)$ and can in many cases be determined from the spectrum.

In each vibrational level the molecule may have various amounts of rotational energy. For diatomic molecules, in the simplest case ( ${ }^{1} \Sigma$ state), the rotational energy is given by

$$
\begin{equation*}
\frac{E_{r}}{h c}=F(J)=B_{v} J(J+1)-\ldots \tag{3}
\end{equation*}
$$

where $J$ is the rotational quantum number which may take the values $0,1,2, \ldots$ and where $B_{v}$ is the so-called rotational constant which is slightly different for different vibrational levels of a given electronic state: one has

$$
\begin{equation*}
B_{v}=B_{e}-a_{e}\left(v+\frac{1}{2}\right)+\ldots \tag{4}
\end{equation*}
$$

Here $a_{0}$ is small compared to the rotational constant $B_{e}$ which refers to the equilibrium position. For $B_{e}$ one finds

$$
\begin{equation*}
B_{0}=\frac{h}{8 \pi^{2} c \mu r_{\mathrm{e}}{ }^{2}} \tag{5}
\end{equation*}
$$

Here $\mu=\frac{m_{1} m_{2}}{m_{1}+m_{2}}$ is the reduced mass of the molecule with $m_{1}$ and $m_{2}$ the masses of the two atoms, and $r_{e}$ is the internuclear distance in the equilibrium position. The product $\mu r_{e}{ }^{2}$ is the moment of inertia of the molecule; in other words, $B_{e}$, apart from universal constants, is the reciprocal moment of inertia.

Each electronic state of a diatomic molecule is characterized by a certain set of values for the vibrational and rotational constants $\omega_{e}, \omega_{e} x_{e}, \ldots, D_{0}, r_{e}, B_{e}, a_{e}, \ldots$ These constants have been determined for a large number of diatomic molecules in various electronic states from the analysis of band spectra. A comprehensive and up-to-date table may be found in "Molecular Spectra and Molecular Structure. I. Spectra of Diatomic Molecules," by G. Herzberg (Van Nostrand. New York, 1950). The following table is an excerpt from the compilation just mentioned, but brought up to date, 1953. Here only the constants $\omega_{e}, D_{0}{ }^{\circ}$, and $r_{e}$ for the ground states are listed and the type of the ground state is given. From $r_{e}$ the rotational constant $B_{e}$ can be obtained according to the formula (5) given above. $D_{0}{ }^{\circ}$ corresponds to dissociation into normal atoms. The values are given in ev (electron-volts) where 1 ev corresponds to $8068.3 \mathrm{~cm}^{-1}$. The numbers on the element symbols give the mass numbers of the isotopic species to which the constants refer. When no mass number is given the data refer to the ordinary isotopic mixture. With the exception of the hydrogen molecule in each case only the data for one isotopic species are listed.

More detailed explanation of the underlying theory, the methods of determination of these constants and references for each individual molecule may be found in the book already quoted.

[^241]TABLE 625A.-MOLECULAR CONSTANTS FOR THE GROUND STATES OF DIATOMIC MOLECULES

The following symbols are used: ( ) Constants and symbols in parentheses are uncertain or of low accuracy. [ ] Constants in brackets refer to the lowest vibrational levels rather than to the equilibrium position. Such a value under $\omega_{e}$ is the first vibrational quantum $\Delta G_{1} / 2=G(1)-G(0)=\omega_{e}$ $2 \omega_{\text {exe }}{ }^{+} \ldots$; under $r_{e}$ it is the effective value $r_{0}$ in the lowest vibrational level ( $v=0$ ), that is, it has been obtained from $B_{0}$ rather than $B_{e}$. "An asterisk in the column "Type of state" indicates that it is doubtful whether the state whose constants are given is the ground state of the molecule. $\dagger$ A dagger after a value under $r_{e}$ indicates that it has been obtained from electron diffraction rather than from the spectrum of the molecule. \{In a few cases several values of the dissociation energy are compatible with the available data. These values are grouped together by braces.

| Molecule | Type of state | $\omega_{e}\left(\mathrm{~cm}^{-1}\right)$ | $D_{0}{ }^{\circ}(\mathrm{ev})$ | $r$ ( ${ }^{( }$) |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Ag}^{109} \mathrm{Br}^{81}$ | ( $\left.{ }^{1} \Sigma\right)$ | 247.72 | 2.6 |  |
| $\mathrm{Ag}^{107} \mathrm{Cl}^{25}$ | $\left({ }^{1} \Sigma\right)$ | 343.6 | 3.1 |  |
| $\mathrm{AgH}^{1}$ | ${ }^{1} \Sigma^{+}$ | 1760.0 | 2.5 | 1.617 |
| $\mathrm{Ag}^{107} \mathrm{I}^{127}$ | $\left({ }^{1} \Sigma\right)$ | 206.18 | 2.98 |  |
| $\mathrm{AgO}^{18}$ | ${ }^{2} \Sigma^{-}$ | 493.2 | (1.8) |  |
| $\mathrm{Al}^{77} \mathrm{Br}^{78}$ | ${ }^{1} \Sigma^{+}$ | 378.0 | (2.4) | 2.295 |
| $\mathrm{Al}^{27} \mathrm{Cl}^{19}$ | ${ }^{1} \Sigma^{+}$ | 481.30 | (3.1) | 2.14 |
| $\mathrm{Al}^{27} \mathrm{~F}^{18}$ | ${ }^{1} \mathrm{\Sigma}$ + | 814.5 | (2.5) |  |
| $\mathrm{Al}^{2} \mathrm{H}^{1}$ | ${ }^{1} \mathrm{\Sigma}$ + | 1682.57 | <3.06 | 1.6459 |
| $\left(\mathrm{Al}^{27} \mathrm{H}^{1}\right)^{+}$ | ${ }^{2} \Sigma^{+}$ | (1610) |  | 1.602 |
| $\mathrm{Al}^{27} \mathrm{I}^{127}$ | ${ }^{1} \Sigma^{+}$ | 316.1 | (2.9) |  |
| $\mathrm{Al}^{27} \mathrm{O}^{18}$ | ${ }^{2} \Sigma{ }^{+}$ | 978.2 | (<3.75) | 1.6176 |
| $\mathrm{As}_{2}{ }^{75}$ | ${ }^{1} \Sigma_{0}^{+}$ | 429.44 | $\leq 3.96$ |  |
| $\left(\mathrm{As}^{75}\right)^{7}{ }^{+}$ | $\left({ }^{2} \Sigma^{+}\right.$) | 314.8 | (2.4) |  |
| $\mathrm{As}^{775} \mathrm{~N}^{16}$ | ${ }_{2}^{1} \Sigma^{+}$ | 1068.0 | (6.5) |  |
| $\mathrm{As}^{78} \mathrm{O}^{16}$ | ${ }^{2} \Pi$ | 967.4 | $\leq 5.0$ |  |
| $\mathrm{Au}^{107} \mathrm{Cl}^{108}$ | $\left({ }^{1} \Sigma^{+}\right.$) | 382.8 | (3.5) |  |
| $\mathrm{Au}^{189} \mathrm{H}^{1}$ | ${ }^{1} \Sigma^{+}$ | 2305.01 | 3.1 | 1.5237 |
| $\mathrm{B}_{2}{ }^{11}$ | ${ }^{8} \Sigma^{8} 0^{-}$ | 1051.3 | (3.6) | 1.589 |
| $\mathrm{BaBr}^{79}$ | ${ }^{2} \Sigma^{+}$ | 193.8 | (2.8) |  |
| $\mathrm{Ba}^{138} \mathrm{Cl}^{38}$ | ${ }^{2} \mathrm{\Sigma}$ | 279.3 | (2.7) |  |
| $\mathrm{BaF}^{19}$ | ${ }^{2} \Sigma$ | 468.9 | (3.8) |  |
| $\mathrm{BaH}^{1}$ | ${ }^{2} \Sigma^{*}$ | 1172 | $\leq 1.82$ | 2.2318 |
| $\mathrm{BaO}^{19}$ | ${ }^{1} \Sigma$ | 669.8 | 4.7 | 1.940 |
| BaS |  |  | (2.3) |  |
| $\mathrm{B}^{11} \mathrm{Br}^{79}$ | ${ }^{1} \Sigma^{+}$ | 684.31 | (4.1) | 1.89 |
| $\mathrm{B}^{12} \mathrm{Cl}^{25}$ | ${ }^{1} \Sigma$ + | 839.12 | (4.2) | 1.716 |
| $\mathrm{Be}^{9} \mathrm{Cl}^{19}$ | ${ }^{2} \Sigma{ }^{2}+$ | 846.58 | (4.3) | (1.7) |
| $\mathrm{Be}^{9} \mathrm{~F}^{19}$ | ${ }^{2} \Sigma^{+}$ | 1265.6 | (5.4) | 1.3614 |
| $\mathrm{Be}^{9} \mathrm{H}^{1}$ | ${ }^{2} \Sigma^{+}$ | 2058.6 | (2.2) | 1.3431 |
| $\left(\mathrm{Be}^{9} \mathrm{H}^{1}\right)^{+}$ | ${ }^{1} \Sigma^{+}$ | 2221.7 | (3.2) | 1.3122 |
| $\mathrm{Be}^{9} \mathrm{O}^{18}$ | ${ }^{1} \Sigma^{+}$ | 1487.32 | $\left\{\begin{array}{l}(3.7) \\ (3.0)\end{array}\right.$ | 1.3308 |
| $\mathrm{B}^{11} \mathrm{~F}^{19}$ | ${ }^{1} \Sigma{ }^{\text {L }}$ | 1400.6 | (4.3) | 1.262 |
| ${ }^{111} \mathrm{H}^{1}$ | ${ }^{1} \Sigma^{+}$ | (2366) | <3.51 | 1.2325 |
| $\left(\mathrm{B}^{11} \mathrm{H}^{1}\right)^{+}$ | ${ }^{2} \Sigma^{+}$ | (2435) |  | [1.2146] |
| ${ }^{\mathrm{Bi}_{2}{ }^{200}}{ }^{200}{ }^{\text {cem }}$ | ${ }^{1} \Sigma_{0}{ }^{+}$ | 172.71 | 1.70 |  |
| $\mathrm{Bi}^{200} \mathrm{Br}^{79}$ |  | 209.34 | 2.74 |  |
| ${ }^{\mathrm{Bi}^{205} \mathrm{C} \mathrm{Cl}^{28}} \mathrm{Bi}^{200} \mathrm{~F}^{18}$ |  | 308.0 510.7 | (3.0) |  |
| ${ }^{\mathrm{Bi}^{200} \mathrm{~F}^{20} \mathrm{~F}^{20}} \mathrm{Bi}^{\text {a }} \mathrm{H}^{1}$ |  | 510.7 1698.9 | (2.7) | 1.809 |
| $\mathrm{Bi}^{200} \mathrm{I}^{127}$ | (0) | 163.9 163.1 | (2.7) | 1.809 |
| $\mathrm{Bi}^{200} \mathrm{O}^{16}$ |  | 702.1 | (2.9) |  |
| $\mathrm{B}^{11} \mathrm{~N}^{14}$ | ${ }^{8} \mathrm{II}$ * | 1514.6 | (5.0) | 1.281 |
| $\mathrm{B}^{11} \mathrm{O}^{16}$ | ${ }^{2} \Sigma+$ | 1885.44 | (9.1) | 1.2049 |
| $\mathrm{Br}^{87} \mathrm{BrCl}^{81}$ | ${ }^{1} \Sigma_{0}{ }^{+}{ }^{+}$ | [430] ${ }^{3}$ | 1.971 2.138 | 2.284 |
| $\mathrm{Br}^{7 \mathrm{~F}^{18}}$ | ${ }^{1} \Sigma$ | 673 | 2.16 | 1.75555 |
| $\mathrm{BrO}^{16}$ | * | 713 | (2.2) |  |
| $\mathrm{C}_{2}^{12}$ | ${ }^{8} \Pi_{4}$ | 1641.35 | (3.6) | 1.3117 |
| $\mathrm{CaBr}^{78}$ | ${ }^{2} \Sigma+$ | 285.3 | (2.9) |  |
| $\mathrm{CaCl}^{\text {s5 }}$ | ${ }^{2} \Sigma+$ | 369.8 | $\leq 2.76$ | (1.866) |
| $\mathrm{Ca}^{10} \mathrm{~F}^{10}$ | ${ }^{2} \Sigma^{2}+$ | 587.1 | $\leq 3.15$ | ([2.02]) |
| $\mathrm{Ca}^{40} \mathrm{H}^{1}$ | ${ }^{2} \Sigma$ | 1299 | $\leq 1.70$ | 2.0020 |
| (continued) |  |  |  |  |

TABLE 625A.-MOLECULAR CONSTANTS FOR THE GROUND STATES OF DIATOMIC MOLECULES (continued)

| Molecule | Type of state | $\omega_{0}\left(\mathrm{~cm}^{-1}\right)$ | $D_{0}{ }^{\circ}(\mathrm{ev})$ | re( $(\underset{A}{ })$ |
| :---: | :---: | :---: | :---: | :---: |
| $\left(\mathrm{Ca}^{\text {0 }} \mathrm{H}^{1}\right)^{+}$ |  |  |  | [1.73] |
| $\mathrm{CaI}^{127}$ | $\left({ }^{2} \Sigma\right)$ | 242.0 | (2.8) |  |
| $\mathrm{Ca}^{10} \mathrm{O}^{16}$ | ${ }^{2}$ * | 732.1 | 5.0 | 1.822 |
| CaS |  |  | $\leq 5.2$ |  |
| $\mathrm{C}^{12} \mathrm{Cl}^{185}$ | ${ }^{2} \mathrm{II}$ | 846 |  |  |
| $\mathrm{Cd}_{2}$ |  |  | . 087 |  |
| CdBr | * | 230.0 | (3.3) |  |
| $\mathrm{CdCl}^{25}$ | ${ }^{2} \Sigma$ | 330.5 | (2.8) |  |
| $\mathrm{CdF}^{19}$ | $\left({ }^{2} \Sigma\right)$ | (535) |  |  |
| $\mathrm{CdH}^{1}$ | ${ }^{2} \Sigma^{+}$ | 1430.7 | . 678 | 1.762 |
| $\left(\mathrm{CdH}^{1}\right)^{+}$ | ${ }^{1} \Sigma^{+}$ | 1775.4 | (2.0) | 1.667 |
| CdI ${ }^{127}$ | ${ }^{2} \Sigma$ | 178.5 | (1.6) |  |
| CdS |  |  | $\leq 3.9$ |  |
| CdSe |  |  | $\leq 3.2$ |  |
| $\mathrm{CeO}^{16}$ | * | 865.0 | (77) |  |
| CF | ${ }^{2} 1$ | 1308.4 | (4.8) | 1.27 |
| $\mathrm{C}^{12} \mathrm{H}^{1}$ | ${ }^{2} I I$ | 2861.6 | 3.47 | 1.1198 |
| $\left(\mathrm{C}^{12} \mathrm{H}^{1}\right)^{+}$ | ${ }^{1} \Sigma^{+}$ | [2739.54] | 3.6 | 1.13083 |
| $\mathrm{Cl}_{2}{ }^{28}$ | ${ }^{1} \Sigma_{0}{ }^{+}$ | 564.9 | 2.475 | 1.988 |
| $\left(\mathrm{Cl}_{2}{ }^{38}\right)^{+}$ | ${ }^{2} \Pi$ | 645.3 | (4.4) | 1.891 |
| $\mathrm{Cl}^{28} \mathrm{~F}^{18}$ | ${ }^{1} \Sigma$ | 786.3 | 2.616 | 1.62813 |
| $\mathrm{ClO}^{16}$ | * | (780) | 1.9 |  |
| $\mathrm{C}^{12} \mathrm{~N}^{16}$ | ${ }^{2} \Sigma{ }^{+}$ | 2068.70 |  | 1.1718 |
| $\mathrm{C}^{12} \mathrm{O}^{16}$ | ${ }^{1} \Sigma^{+}$ | 2170.21 | $\left\{\begin{array}{r}11.108 \\ 9.844\end{array}\right.$ | 1.1282 |
|  | 2 | 2170.21 | 9.605 | 1.1282 |
| $\left(\mathrm{C}^{12} \mathrm{O}^{16}\right)^{+}$ | ${ }^{2} \Sigma^{+}$ | 2214.24 | (9.9) | 1.1151 |
| CoCl | * | 421.2 |  |  |
| $\mathrm{CoH}^{1}$ | $\Omega=4$ | (1890) |  | [1.542] |
| $\mathrm{CoO}^{16}$ | * | (850) |  |  |
| $\mathrm{C}^{12} \mathrm{P}^{81}$ | ${ }^{2} \Sigma$ | 1239.67 | (6.9) | 1.562 |
| $\mathrm{CrO}^{12} \mathrm{~S}^{18}$ | * | 898.8 | 4.4 |  |
| $\mathrm{C}^{12} \mathrm{CS}_{2} \mathrm{~S}^{188}$ | ${ }^{1} \Sigma^{+}{ }^{+}$ | 1285.1 | (7.8) | 1.534 |
| $\mathrm{Cs}^{188} \mathrm{Br}$ | ${ }^{1} \mathrm{\Sigma}^{\text {\% }}$ | (194) | $\geq 3.9$ | [3.14] † |
| $\mathrm{Cs}^{183} \mathrm{Cl}$ | ${ }^{1} \Sigma^{+}$ | 299 |  | 2.88 |
| $\mathrm{C}^{12} \mathrm{Se}$ | ${ }^{1} \Sigma^{+}$ | 1036.0 | (6.8) |  |
| $\mathrm{CsF}{ }^{19}$ | ${ }^{1} \Sigma^{+}$ | (270) | 5.67 | 2.34 |
| $\mathrm{Cs}^{128} \mathrm{H}^{1}$ | ${ }^{1} \Sigma^{+}$ | 890.7 | (1.9) | 2.494 |
| $\mathrm{Cs}^{128} \mathrm{I}^{127}$ | ${ }^{1} \mathrm{\Sigma}$ + | 142 | $3.37{ }^{7}$ | [3.41] $\dagger$ |
| CsRb |  | 49.4 |  |  |
| $\mathrm{Cu}_{2}$ | ( ${ }^{1} \Sigma_{0}^{+}$) | 160 | ( .17) |  |
| $\mathrm{Cu}^{\mathbf{x s}} \mathrm{Br}^{78}$ | ${ }^{12}{ }^{+}$ | 314.10 | (2.5) |  |
| $\mathrm{Cu}^{48 \mathrm{Cl}^{125}}$ | ${ }^{1} \Sigma^{+}$ | 416.9 | (3.0) |  |
| $\mathrm{Cu}^{\text {es }} \mathrm{F}^{19}$ | ${ }^{1} \mathrm{E}+$ | 622.7 | (3.0) | 1.743 |
| $\mathrm{Cu}^{088} \mathrm{H}^{1}$ | ${ }^{1} \Sigma^{+}$ | 1940.4 | $<2.89$ | 1.463 |
| $\left(\mathrm{Cu}^{\text {as }} \mathrm{H}^{1}\right)^{+}$ | ${ }^{2} \mathrm{\Sigma}$ | [1874] |  | [2.27] |
| $\mathrm{Cu}^{281} \mathrm{I}^{127}$ | ${ }^{1} \Sigma^{+}$ | 264.8 | (3.0) |  |
| $\mathrm{CuO}^{16}$ | $\left({ }^{2} \Sigma^{+}\right)$ | 628 | 4.9 |  |
| $\mathrm{F}_{2}{ }^{10}{ }^{\text {a }}$ | ${ }^{1} \Sigma^{\circ} \Sigma^{+}{ }^{+}$ | [892.1] | $<1.63$ | $1.418 \dagger$ |
| $\mathrm{FeCl}^{\text {2s }}$ | ${ }^{6} \Sigma^{\text {\% }}$ | 406.6 |  |  |
| $\mathrm{FeO}^{16}$ |  | 880 | $\leq 4.24$ |  |
| $\mathrm{Ga}^{\infty} \mathrm{Br}^{81}$ | ${ }^{1} \Sigma^{+}$ | 263.0 | (2.7) |  |
| $\mathrm{Ga}^{* \infty} \mathrm{Cl}^{15}$ | ${ }^{1} \Sigma{ }^{+}$ | 365.3 | $\leq 5.0$ | [2.21] |
| $\mathrm{Ga}^{20} \mathrm{~F}^{10}$ | ${ }^{1} \Sigma^{+}$ | 623.2 | (6.3) |  |
| $\mathrm{Ga}^{\infty} \mathrm{I}^{18}$ | ${ }^{1} \Sigma^{+}$ | 216.4 | $\leq 2.88$ |  |
| $\mathrm{GaO}^{10}$ | ${ }^{2} \Sigma$ | 767.69 | (2.9) |  |
| $\mathrm{GdO}^{16}$ | * | 841.0 | (5.9) |  |
| GeBr | ${ }^{2} 1$ | 296.6 | (3.0) |  |
| $\mathrm{Ge}^{74} \mathrm{Cl}^{15}$ | ${ }^{2} 11$ | 406.6 | (4.0) |  |
| GeF ${ }^{19}$ | ${ }^{2} 11$ | 665.2 | (4.9) |  |
| ${ }_{\text {Ge }} \mathrm{Ge}^{7{ }^{78} \mathrm{O}^{16} \mathrm{~S}^{16}}$ | ${ }^{1} \Sigma^{1} \Sigma^{+}$ | 985.7 575.8 | (6.9) | 1.651 |
| $\mathrm{Ge}^{74} \mathrm{~S}^{81}$ | ${ }^{1} \Sigma^{*}$ | 575.8 | (5.6) |  |
|  |  | (continued) |  |  |

TABLE 625A.-MOLECULAR CONSTANTS FOR THE GROUND STATES OF DIATOMIC MOLECULES (continued)

| Molecule | Type of state | $\omega_{e}\left(\mathrm{~cm}^{-1}\right)$ | $D_{0}{ }^{\circ}(\mathrm{ev})$ | $r$ ( ${ }^{\text {a }}$ ) |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Ge}^{74} \mathrm{Se}^{80}$ | ${ }^{1} \Sigma^{+}$ | 406.8 | (4.1) |  |
| $\mathrm{Ge}^{74} \mathrm{Te} \mathrm{e}^{130}$ | ${ }^{1} \Sigma^{+}$ | 323.4 | (3.2) |  |
| $\mathrm{H}_{2}{ }^{1}$ | ${ }^{1} \Sigma_{g}{ }^{+}$ | 4395.2 | 4.476 | .7416 |
| $\mathrm{H}^{1} \mathrm{H}^{2}$ | ${ }^{1} \Sigma_{0}+$ | 3809.7 | 4.511 | .7414* |
| $\mathrm{H}^{2} \mathrm{H}^{3}$ | ${ }^{1} \Sigma_{0}{ }^{+}$ | 2853.8 | 4.570 | (0.7416 ${ }^{\text {a }}$ ) |
| $\mathrm{H}_{2}{ }^{2}$ | ${ }^{1} \Sigma_{0}{ }^{+}$ | 3118.5 | 4.554 | (.74166) |
| $\mathrm{H}^{1} \mathrm{H}^{8}$ | ${ }^{1} \Sigma_{0}{ }^{+}$ | 3608.3 | 4.524 | (.74169) |
| $\mathrm{H}_{2}{ }^{\text {a }}$ | ${ }^{1} \Sigma_{0}{ }^{+}$ | 2553.8 | 4.588 | (.74166) |
| $\left(\mathrm{H}_{2}{ }^{1}\right)^{+}$ | ${ }^{2} \Sigma_{\square}{ }^{+}$ | 2297 | 2.648 | 1.06 |
| $\mathrm{H}^{1} \mathrm{Br}$ | ${ }^{1} \Sigma^{+}$ | 2649.67 | 3.75 | 1.414 |
| $\left(\mathrm{H}^{1} \mathrm{Br}\right)^{+}$ | ${ }^{2} \Pi_{1}$ |  | 3.5 | [1.459] |
| $\mathrm{H}^{1} \mathrm{Cl}^{25}$ | ${ }^{1} \Sigma^{+}$ | 2989.74 | 4.430 | 1.27460 |
| $\left(\mathrm{H}^{1} \mathrm{Cl}^{35}\right)^{+}$ | ${ }^{2} \mathrm{II}_{4}$ | 2675.4 | 4.48 | 1.3153 |
| $\mathrm{He}_{2}{ }^{4}$ | ${ }^{1} \Sigma_{0}{ }^{+}$ | unstable |  |  |
| $\left(\mathrm{He}_{2}{ }^{4}\right)^{+}$ | ${ }^{2} \Sigma_{u}{ }^{+}$ | [1627.2] | (3.1) | 1.08 |
| $\mathrm{H}^{1} \mathrm{~F}^{10}$ | ${ }^{1} \Sigma^{+}$ | 4138.52 | 5.8 | . 9171 |
| $\mathrm{Hg}_{2}$ | ${ }^{1} \Sigma_{0}+$ | (36) | . 060 | 3.3 |
| $\mathrm{Hg}^{202} \mathrm{Br}^{81}$ | $\left({ }^{2} \Sigma\right)$ | 186.2 | . 7 |  |
| $\mathrm{HgCl}^{25}$ | ${ }^{2} \Sigma^{+}$ | 292.61 | 1.0 | [2.23] † |
| $\mathrm{HgF}^{18}$ | $\left({ }^{2} \Sigma\right)$ | 490.8 | (1.8) |  |
| $\mathrm{HgH}{ }^{1}$ | ${ }^{2} \Sigma^{+}$ | 1387.09 | . 376 | 1.7404 |
| $\left(\mathrm{HgH}^{1}\right)^{+}$ | ${ }^{1} \Sigma^{+}$ | 2033.87 | (2.3) | 1.594 |
| $\mathrm{HgI}^{127}$ | $\left({ }^{2} \Sigma\right)$ | 125.6 | . 36 |  |
| HgS |  |  | $\leq 2.8$ |  |
| HgSe |  |  | $\leq 2.7$ |  |
| HgTl |  | 26.9 | (.031) |  |
| $\mathrm{H}^{1} \mathrm{I}^{127}$ | ${ }^{1} \Sigma^{+}$ | 2309.5 | 3.056 | 1.604 |
| $\left(\mathrm{H}^{1} \mathrm{I}^{127}\right)^{+}$ |  |  | 3.11 |  |
| $\mathrm{H}^{1} \mathrm{~S}^{32}$ | ${ }^{2} \mathrm{II}_{4}$ |  | $<3.8$ | [1.35] |
| $\mathrm{I}_{2}{ }^{127}$ | ${ }^{1} \Sigma^{+}{ }^{+}$ | 214.25 | 1.5417 | 2.667 |
| $\mathrm{I}^{187} \mathrm{Br}^{78}$ | ${ }^{1} \Sigma^{+}$ | 268.4 | 1.817 |  |
| $\mathrm{I}^{129} \mathrm{Cl}^{28}$ | ${ }^{1} \Sigma^{+}$ | 384.18 | 2.152 | 2.32070 |
| $\mathrm{I}^{127} \mathrm{~F}^{10}$ | ${ }^{1} \Sigma^{+}$ | 610 | 1.98 |  |
| $\mathrm{In}^{115} \mathrm{Br}^{81}$ | ${ }^{1} \Sigma^{+}$ | 221.0 | $\leq 3.3$ | [2.57] † |
| $\mathrm{In}^{115} \mathrm{Cl}^{95}$ | ${ }^{1} \Sigma^{+}$ | 317.4 | $\leq 4.54$ | 2.32 |
| In ${ }^{115} \mathrm{~F}^{18}$ | ${ }^{1} \Sigma+$ | 534.7 | (5.7) |  |
| In ${ }^{115} \mathrm{H}^{1}$ | ${ }^{1} \Sigma^{+}$ | 1474.7 | $\leq 2.48$ | 1.8376 |
| $\mathrm{In}^{116} \mathrm{I}^{129}$ | ${ }^{1} \Sigma^{+}$ | 177.1 | $\leq 2.7$ | [2.86] † |
| $\mathrm{InO}{ }^{18}$ | $\left({ }^{2} \Sigma\right)^{*}$ | 703.09 | (1.3) |  |
| $\mathrm{I}^{177} \mathrm{O}^{16}$ | * | 687 | (1.9) |  |
| $\mathrm{K}_{2}{ }^{80}$ | ${ }^{1} \Sigma_{0}{ }^{+}$ | 92.64 | . 514 |  |
| KBr | ${ }^{1} \Sigma^{+}+$ | 231 | 3.96 | [2.94] † |
| KCl | ${ }^{1} \Sigma^{+}$ | 280 | 4.42 | [2.79] ${ }^{\dagger}$ |
| $\mathrm{KF}^{19}$ | ${ }^{1} \Sigma+$ | (390) | $\leq 5.9$ | [2.55] |
| $\mathrm{K}^{89} \mathrm{H}^{1}$ | ${ }^{1} \Sigma^{+}$ | 985.0 | 1.88 | 2.244 |
| KI ${ }^{127}$ | ${ }^{1} \Sigma^{2}+$ | 212 | 3.33 | [3.23] † |
| $\mathrm{La}^{189} \mathrm{O}^{18}$ | ${ }^{2} \Sigma$ | 811.6 | (9) |  |
| $\mathrm{Li}_{2}{ }^{7}$ | ${ }^{1} \Sigma_{0}+$ | 351.43 | 1.03 | 2672 |
| LiBr | ${ }^{1} \Sigma^{+}$ |  | 4.5 |  |
| LiCl | ${ }^{1} \Sigma^{+}$ |  | 5.1 |  |
| $\mathrm{Li}^{7} \mathrm{Cs}^{138}$ | ${ }^{1} \Sigma^{+}$ | (167) |  |  |
| $\mathrm{LiF}^{19}$ |  |  |  |  |
| $\mathrm{Li}^{7} \mathrm{H}^{1}$ | ${ }^{1} \Sigma^{+}$ | 1405.65 | (2.5) | 1.5953 |
| $\mathrm{LiI}^{127}$ | ${ }^{1} \Sigma^{+}$ | 450 | 3.6 |  |
| LiK | ${ }^{1} \Sigma^{+}$ | (207) |  |  |
| LiRb | ${ }^{1} \Sigma^{+}$ | (185) |  |  |
| $\mathrm{LuO}^{16}$ |  | 841.66 | (5.3) |  |
| $\mathrm{Mg}^{24} \mathrm{Br}^{79}$ | ${ }^{2} \Sigma{ }^{2}$ ) | 373.8 | $\leq 3.35$ |  |
| $\mathrm{Mg}^{24} \mathrm{Cl}^{25}$ | ${ }^{2} \mathrm{\Sigma}+$ | 465.4 | (3.2) |  |
| Mg ${ }^{24} \mathrm{~F}^{19}$ | ${ }^{2} \Sigma \Sigma^{+}$ | 717.6 | (4.2) | [1.75] |
| $\mathrm{Mg}^{24} \mathrm{H}^{1}$ | ${ }^{2} \Sigma+$ | 1495.7 | $\leq 2.49$ | 1.7306 |
| $\left(\mathrm{Mg}^{24} \mathrm{H}^{1}\right)^{+}$ | ${ }^{1} \Sigma^{+}$ | 1695.3 | (2.1) | 1.649 |
| MgI ${ }^{127}$ | $\left({ }^{2} \Sigma^{+}\right)$ | [312] |  |  |

(continued)

TABLE 625A.—MOLECULAR CONSTANTS FOR THE GROUND STATES OF DIATOMIC MOLECULES (continued)

| Molecule | Type of state | $\omega_{0}\left(\mathrm{~cm}^{-1}\right)$ | $D_{0}{ }^{\circ}(\mathrm{ev})$ | re(A) |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Mg}^{24} \mathrm{O}^{16}$ | ${ }^{1} \Sigma$ * | 785.1 | 5.2 | 1.749 |
| MgS | * | 525.2 | (2.9) |  |
| $\mathrm{Mn}^{\text {55 }} \mathrm{Br}$ | ${ }^{7} \mathrm{\Sigma}$ | 289.7 | (2.9) |  |
| $\mathrm{Mn}^{\text {55 }} \mathrm{Cl} \mathrm{C}^{(8)}$ | ${ }^{7} \Sigma$ ) | 384.9 | (3.3) |  |
| $\mathrm{Mn}^{55} \mathrm{~F}^{19}$ | $\left({ }^{7} \Sigma\right)$ | 618.8 | (3.9) |  |
| $\mathrm{Mn}^{585} \mathrm{H}^{1}$ | ${ }^{7} \Sigma$ | [1490.58] | < (2.4) | 1.73075 |
| $\mathrm{Mn}^{555} \mathrm{I}^{127}$ | ( ${ }^{\text {² }}$ ) | (240) |  |  |
| $\mathrm{Mn}^{65} \mathrm{O}^{16}$ | * | 840.7 | (4.4) |  |
| $\mathrm{N}^{14}$ | ${ }^{1} \Sigma_{0}{ }^{+}$ | 2359.61 | 9.756 | 1.094 |
| $\left(\mathrm{N}_{2}{ }^{24}\right)^{+}$ | ${ }^{2} \Sigma_{0}{ }^{+}$ | 2207.19 | 8.724 | 1.116 |
| $\mathrm{Na}_{2}{ }^{23}$ | ${ }^{1} \Sigma_{0}{ }^{+}$ | 159.23 | . 73 | 3.079 |
| $\mathrm{Na}^{23} \mathrm{Br}$ | ${ }^{1} \Sigma^{+}$ | 315 | 3.85 | [2.64] $\dagger$ |
| $\mathrm{Na}^{23} \mathrm{Cl}$ | ${ }^{1} \Sigma^{+}$ | 380 | 3.58 | [2.51] † |
| $\mathrm{Na}^{23} \mathrm{C} \mathrm{C}^{138}$ | ${ }^{1} \Sigma^{+}$ | (98) |  |  |
| $\mathrm{Na}{ }^{23} \mathrm{~F}^{18}$ |  |  | $\leq 5.3$ |  |
| $\mathrm{Na}^{29} \mathrm{H}^{1}$ | ${ }^{1} \Sigma^{+}$ | 1172.2 | (2.2) | 1.8873 |
| $\mathrm{Na}^{23} \mathrm{I}^{127}$ | ${ }^{1} \Sigma^{+}$ | 286 | 3.16 | [2.90] $\dagger$ |
| $\mathrm{Na}^{23} \mathrm{~K}$ | ${ }^{1} \Sigma^{+}$ | 123.29 | . 62 |  |
| $\mathrm{Na}^{23} \mathrm{Rb}$ | ${ }^{1} \Sigma^{+}$ | 106.64 | (.57) |  |
| $\mathrm{N}^{14} \mathrm{Br}$ | * | 693 | (3.0) |  |
| $\mathrm{N}^{43} \mathrm{H}^{2}$ | ${ }^{3} \Sigma^{-}$ | (3300) | (3.8) | 1.038 |
| NiBr | * | 334 |  |  |
| NiCl | $\left({ }^{2} \Pi\right)$ * | 419.2 | (7.3) |  |
| $\mathrm{NiH}^{1}$ | ${ }^{2} \Delta_{5} / 2$ | [1926.6] | $\leq 3.1$ | 1.475 |
| $\mathrm{NiO}^{18}$ | ** | (615) | $\leq 4.27$ |  |
|  | ${ }^{2} \mathrm{II}$ | 1903.85 | 6.49 | 1.1508 |
| $\left({ }_{\left(\mathrm{N}^{14} \mathrm{~N}^{14} \mathrm{O}^{18}\right)^{18}}{ }^{\text {a }}\right.$ |  |  | 10.6 |  |
| $\mathrm{N}^{14} \mathrm{~S}^{82}$ | ${ }^{2} \Pi_{r}$ | 1220.0 | (5.9) |  |
| $\mathrm{O}_{2}{ }^{\text {10 }}$ | ${ }^{3} \Sigma_{0}{ }^{2}$ | 1580.36 | 5.080 | 1.20740 |
| $\mathrm{O}_{2+}^{+{ }^{+18}{ }^{\text {a }}}$ | ${ }^{2} \Pi^{2} \Pi_{0}$ | 1876.4 | 6.48 | 1.1227 |
| $\mathrm{O}^{19} \mathrm{H}^{19}$ | ${ }^{2} \Pi_{4}$ | 3735.21 | 4.35 | . 9706 |
| $\left(\mathrm{O}^{16} \mathrm{H}^{1}\right)^{+}$ | ${ }^{9} \Sigma^{-}$ | [2955] | $\geq 4.4$ | 1.0289 |
| $\mathrm{P}_{2}{ }_{2}{ }^{31}$ | ${ }^{1} \Sigma_{0}{ }^{+}$ | 780.43 | 5.031 | 1.894 |
| $\mathrm{Pb}_{2} \mathrm{PbBr}^{\text {º }}$ |  | 256.5 | (.7) |  |
| $\stackrel{\mathrm{PbBr}}{ } \mathrm{PbCl}^{\text {as }}$ | $\left.{ }^{2}{ }^{2} \Pi_{1} / 2\right)$ | 207.5 | 3.0 |  |
| $\mathrm{PbF}^{19}$ | ${ }_{2}{ }^{2} \Pi_{1} / 2$ | 303.8 507.2 | 3.1 |  |
| $\mathrm{PbH}^{1}$ | $\left.{ }^{2}{ }^{2} \Pi_{1} / 2 / 2\right)$ | 1564.1 | $\leq 1.59$ | 1.839 |
| $\mathrm{PbI}^{127}$ | $\left({ }^{2} \Pi_{1} / 2\right)$ | 160.5 | 2.8 |  |
| $\mathrm{PbO}^{18}$ | ${ }^{1} \Sigma^{+}$ | 721.8 | (4.2) | 1.922 |
| $\mathrm{Pb}^{209} \mathrm{~S}^{32}$ | $1 \Sigma$ ${ }^{1} \Sigma+$ $1^{2}+$ | 428.14 | (4.7) | 2.395 |
| PbSe | ${ }^{1} \Sigma^{+}$ | 277.6 | (4.7) |  |
| $\mathrm{PbTe}^{81}$ | ${ }^{1} \Sigma$ | 211.8 | (3.5) |  |
| ${ }_{\mathrm{P}^{31}}^{\mathrm{P}^{31} \mathrm{H}^{14}}$ | ${ }^{3} \Sigma^{3} \Sigma^{+}$ | ${ }^{(2380)}$ |  | [1.433] |
| $\mathrm{P}^{81} \mathrm{O}^{19}$ | ${ }^{1} \Sigma^{+}{ }_{r}$ | 1337.24 1230.6 | (6.3) | 1.4470 |
| $\mathrm{Pr}^{141} \mathrm{O}^{16}$ | * | 818.9 |  |  |
| $\mathrm{Rb}_{2}{ }^{\text {ab }}$ | ${ }^{1} \Sigma_{0}+$ | 57.28 | . 49 |  |
| RbBr | (15) |  | 3.9 |  |
| $\mathrm{RbCl}^{18}$ | ${ }_{1}^{15}$ | (253) | $>3.96$ | [2.89] † |
| $\mathrm{RbCs}^{183}$ | ${ }^{1} \Sigma^{1}+$ | 49.41 |  |  |
| $\mathrm{RbF}^{19}$ | $\left({ }_{1}^{1} \Sigma\right)$ | 340 | 5.48 |  |
| $\mathrm{RbH}^{1}$ | ${ }^{1} \Sigma^{1} \Sigma^{+}$ | 936.77 | (1.9) | ${ }_{[3.267}^{2.367} \dagger$ |
| $\mathrm{S}_{2}{ }^{82}$ | ${ }^{3} \Sigma_{\square}-$ | 725.68 | $\leq 4.4$ | 1.889 |
|  | ${ }^{1} \Sigma_{0}{ }^{+}$ | 269.85 | (3.7) |  |
| $\mathrm{SbBi}^{209}$ | ${ }^{1} \Sigma^{+}$ | 220.0 | (3.0) |  |
| $\mathrm{SbCl}^{\text {58 }}$ |  | 369.0 | (4.6) |  |
| $\mathrm{SbF}^{18}$ |  | 614.2 | (4.2) |  |
| $\mathrm{SbN}^{19}$ | ${ }_{2}^{1 / 2}$ | 942.0 | (4.8) |  |
| $\mathrm{Sc}^{45} \mathrm{O}^{16}$ | ${ }^{2} \mathrm{I}$ | 817.2 | (7) |  |
|  |  | continued) |  |  |

TABLE 625A.-MOLECULAR CONSTANTS FOR THE GROUND STATES OF DIATOMIC MOLECULES (concluded)

| Molecule | Type of state | $\omega_{e}\left(\mathrm{~cm}^{-1}\right)$ | $D_{0}{ }^{\circ}(\mathrm{ev})$ | $r$ ( ${ }_{\text {( }}$ ) |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Se}_{2}{ }^{80}$ | $\left({ }^{1} \Sigma_{0}{ }^{+}\right)$ | 391.77 | $\leq 3.55$ | 2.16 |
| $\mathrm{SeO}^{18}$ |  | 907.1 | (5.4) |  |
| $\mathrm{Si}_{2}$ | * | (750) |  |  |
| $\mathrm{SiBr}^{\text {r }}$ | ${ }^{2}$ II | 425.4 | (3.7) |  |
| $\mathrm{Si}^{28} \mathrm{C} 1^{35}$ | ${ }^{2} \mathrm{II}_{r}$ | 535.4 | (4.0) |  |
| $\mathrm{Si}^{28} \mathrm{~F}^{18}$ | ${ }^{2} \Pi_{r}$ | 856.7 | (4.8) | [1.603] |
| $\mathrm{Si}^{28} \mathrm{H}^{1}$ | ${ }^{2} \Pi_{r}$ | (2080) |  | 1.520 |
| $\mathrm{Si}^{29} \mathrm{~N}^{14}$ | ${ }^{2} \Sigma^{+}$ | 1151.68 | (4.5) | 1.572 |
| $\mathrm{Si}^{28} \mathrm{O}^{18}$ | ${ }^{1} \Sigma^{+}$ | 1242.03 | 7.2 | 1.510 |
| $\left(\mathrm{Si}^{28} \mathrm{O}^{18}\right)^{+}$ | ${ }^{2} \Sigma+$ | (851) |  | 1.504 |
| $\mathrm{Si}^{28} \mathrm{~S}^{32}$ | ${ }^{1} \Sigma^{+}$ | 749.5 | (6.6) | 1.929 |
| $\mathrm{Si}^{28} \mathrm{Se}$ | ${ }^{1} \Sigma \Sigma^{+}$ | 580.0 | (5.8) |  |
| $\mathrm{Si}^{28} \mathrm{Te}$ | ${ }^{1} \Sigma^{\prime}+$ | 481.2 | (5.5) |  |
| SnBr | ${ }^{2} \Pi_{r}$ | 247.7 | (3.0) |  |
| $\mathrm{SnCl}{ }^{35}$ | ${ }^{2} \mathrm{II}$ | 352.5 | (3.6) |  |
| $\mathrm{SnF}{ }^{18}$ | ${ }^{2} \mathrm{IH}_{1} / 2$ | 582.9 | (3.9) |  |
| $\mathrm{SnH}{ }^{1}$ | ${ }^{2} \mathrm{II}_{r}$ | (1580) | $<3.2$ | [1.782] |
| $\mathrm{SnO}^{16}$ | ${ }^{1} \Sigma+$ | 822.4 | 5.7 | 1.838 |
| SnS | ${ }^{1} \Sigma^{+}$ | 487.68 | $\leq 3.0$ | (2.06) |
| SnSe | ${ }^{1} \Sigma^{+}$ | 331.2 | (4.6) |  |
| SnTe | ${ }^{1} \Sigma^{+}$ | 259.5 | (4.2) |  |
| $\mathrm{S}^{32} \mathrm{O}^{16}$ | ${ }^{3} \Sigma^{-}$ | 1123.7 | $\left\{\begin{array}{l}4.001 \\ 5.146\end{array}\right.$ | 1.4933 |
| $\mathrm{SrBr}{ }^{70}$ | ${ }^{2} \boldsymbol{\Sigma}+$ | 216.5 | (2.8) |  |
| $\mathrm{SrCl}^{35}$ | ${ }^{2} \Sigma+$ | 302.3 | (3.0) |  |
| $\mathrm{SrF}{ }^{19}$ | ${ }^{2} \Sigma^{+}$ | 500.1 | (3.5) |  |
| SrH ${ }^{1}$ | ${ }^{2} \Sigma \Sigma^{+}$ | 1206.2 | $\leq 1.68$ | 2.1455 |
| SrI ${ }^{127}$ | $\left({ }^{2} \Sigma\right)$ | 173.9 | (2.2) |  |
| $\mathrm{SrO}^{18}$ | ${ }^{1} \Sigma^{*}$ | 653.5 | (4.5) | 1.921 |
| SrS |  |  | $\leq 2.7$ |  |
| $\mathrm{Te}_{2}$ |  | 251 | $\leq 3.18$ | [2.59] † |
| $\mathrm{TeO}^{16}$ |  | 796.0 | $\left\{\begin{array}{l}2.728 \\ 3.453\end{array}\right.$ |  |
| $\mathrm{Ti}^{48} \mathrm{Cl}^{\text {85 }}$ | * | 456.4 | (1.0) |  |
| $\mathrm{Ti}^{48} \mathrm{O}^{16}$ | ${ }^{8} \mathrm{II}{ }_{r}$ | 1008.26 | (6.9) | 1.620 |
| T1Br ${ }^{81}$ | ${ }^{1} \Sigma^{+}$ | 192.1 | $\leq 3.19$ | [2.68] $\dagger$ |
| $\mathrm{TlCl}^{36}$ | ${ }^{1} \Sigma^{+}$ | 287.47 | 3.75 | [2.55] $\dagger$ |
| T1F ${ }^{18}$ | ${ }^{1} \Sigma^{+}$ | 475.00 | <4.72 |  |
| T1H ${ }^{1}$ | ${ }^{1} \Sigma^{+}$ | 1390.7 | $\leq 2.18$ | 1.870 |
| T11 ${ }^{177}$ | ${ }^{1} \Sigma^{+}$ | 150 | $\leq 2.64$ | [2.87] $\dagger$ |
| $\mathrm{V}^{51} \mathrm{O}^{16}$ | $\left.{ }^{2} \Delta\right)^{*}$ | 1012.7 | (6.4) | 1.890 |
| YbCl | $\left({ }^{2} \Sigma\right)^{*}$ | 293.6 | (1.2) |  |
| $\mathrm{Y}^{89} \mathrm{O}^{16}$ | ${ }^{2} \Sigma$ | 852.5 | (9) |  |
| $\mathrm{Zn}_{2}$ | ${ }^{1} \Sigma$ ) |  | (.25) |  |
| ZnBr | $\left({ }^{2} \Sigma\right)^{*}$ | (220) |  |  |
| $\mathrm{ZnCl}^{35}$ | ${ }^{2} \Sigma$ | 390.5 | (3.0) |  |
| $\mathrm{ZnF}{ }^{19}$ | ${ }^{2} \Sigma$ | (630) |  |  |
| $\mathrm{ZnH}{ }^{1}$ | ${ }^{2} \Sigma+$ | 1607.6 | . 851 | 1.5945 |
| $\left(\mathrm{ZnH}^{1}\right)^{+}$ | ${ }^{1} \Sigma^{2}+$ | 1916 | (2.5) | 1.515 |
| $\mathrm{Zn}^{84} \mathrm{I}^{127}$ | $\left({ }^{2} \Sigma\right)^{*}$ | 223.4 | (2.0) |  |
| ZnO |  |  | $\leq 4.0$ |  |
| ZnS |  |  | $\leq 4.4$ |  |
| ZnTe |  |  | $\leq 2.2$ |  |
| $\mathrm{Zr}^{\text {00 }} \mathrm{O}^{16}$ | ${ }^{8} \mathrm{II}$ | 937.2 | (7.8) | (1.416) |

The atmosphere, with a total mass of about $5.3 \times 10^{21} \mathrm{~g}$ (about one-millionth the mass of the earth), extends $7,000-60,000$ miles above sea level (depending upon the definition of the top) and for purposes of discussion may be divided into several regions or layers. From sea level up to about 10-15 km (the troposphere), about the next 30 km above this (the stratosphere), and the entire region above this (i.e., above about 40 km ) is spoken of as the upper atmosphere. At heights above 80 km in the upper atmosphere strong ionization is found and thus this region is called the ionosphere. Again the ionosphere may be divided into three or four layers ; first, the $E$ layer (about 100 km ) moderately ionized; next the $F_{1}$ layer (at about 200 km ) more strongly ionized ; the $F_{2}$ layer (about 300 km ) much more strongly ionized. Above this, there is some recent evidence indicating an additional ionized region, the $G$ layer ( $400-700 \mathrm{~km}$ ).
The following tables give some characteristics of the atmosphere as a function of the height above sea level.

TABLE 626.-COMPOSITION OF THE AIR NEAR GROUND LEVEL ${ }^{196}$

| Gas | Molecular weight | Percent per volume |
| :---: | :---: | :---: |
| Nitrogen | 28 | 78.09 |
| Oxygen | 32 | 20.95 |
| Argon | 40 | .93 100.00 |
| Carbon dioxide | 44 | . $02-.04$ |
| Neon | 20.2 | $18 \times 10^{-4}$ |
| Helium |  | $5.3 \times 10^{-4}$ |
| Krypton | 83 | $1.1 \times 10^{-4}$ |
| Hydrogen | 2 | $.5 \times 10^{-4}$ |
| Xenon | 130 | . $08 \times 10^{-4}$ |
| Ozone | 48 | $.02 \times 10^{-4}$, increasing with altitude |
| Radon . |  | $7 \times 10^{-18}$, decreasing with altitude |
| Water vapor | 18 | . $2-4$, variable |

104 Regener, E., The structure and composition of the stratosphere, No. 509, Headquarters Air Materiel Command, Wright Field, Dayton, Ohio, April 1946.

TABLE 627.-COMPOSITION OF THE ATMOSPHERE UP TO THE F LAYER, LATITUDE $45^{\circ} 195$

| $\underset{\mathrm{km}}{\text { Altitude }}$ | Composition, <br> 1 percent volume | Molecular weight of mixture, $M$ | $\begin{gathered} \text { Altitude } \\ \mathrm{km} \end{gathered}$ | Composition <br> 1 percent volume | Molecular weight of mixture, $M$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | $21 \mathrm{O}_{2}, 78 \mathrm{~N}_{2}, .93 \mathrm{~A}$ | 28.9 | 120 | $30.5 \mathrm{O}, 69.5 \mathrm{~N}_{2}$ | 24.35 |
| 50 | $18 \mathrm{O}_{2}, 82 \mathrm{~N}_{2}$ | 28.66 | 300 | $30.5 \mathrm{O}, 69.5 \mathrm{~N}_{2}$ | 24.35 |
| 83 | $18 \mathrm{O}_{2}, 82 \mathrm{~N}_{2}$ | 28.66 | ( $F_{2}$ layer) |  |  |

[^242]A standard atmosphere is defined by an altitude-temperature-pressure relation. It is an aeronautic necessity in valuating the performance of airplanes and for the calibration of instruments. The following standard has been officially adopted by the Army Air Corps, National Bureau of Standards, National Advisory Committee for Aeronautics, and the Weather Bureau. See Table 343.

| Altitude Meters | Pressure |  | Density |  | Temperature |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{mmHg}^{\text {m }}$ | in Hg | $\mathrm{kg} / \mathrm{m}^{8}$ | $\underline{1 b / f t^{8}}$ |  |
| 0 | 760.0 | 29.921 | 1.2255 | . 07650 | 15.0 |
| 1000 | 674.1 | 26.54 | 1.1120 | . 06942 | 8.5 |
| 2000 | 596.2 | 23.47 | 1.0068 | . 06286 | + 2.0 |
| 3000 | 525.8 | 20.70 | . 9094 | . 05678 | -4.5 |
| 4000 | 462.3 | 18.20 | . 8193 | . 05115 | -11.0 |
| 5000 | 405.1 | 15.95 | . 7363 | . 04597 | -17.5 |
| 6000 | 353.8 | 13.93 | . 6598 | . 04119 | -24.0 |
| 7000 | 307.9 | 12.12 | . 5896 | . 03681 | -30.5 |
| 8000 | 266.9 | 10.51 | . 5252 | . 03279 | -37.0 |
| 9000 | 230.4 | 9.07 | . 4664 | . 02912 | -43.5 |
| 10000 | 198.2 | 7.80 | . 4127 | . 02577 | -50.0 |
| 11000 | 169.7 | 6.68 | . 3614 | . 02256 | -55.0 |
| 12000 | 145.0 | 5.71 | . 3090 | . 01929 | -55.0 |
| 13000 | 124.0 | 4.88 | . 2642 | . 01649 | -55.0 |
| 14000 | 106.0 | 4.17 | . 2259 | . 01410 | $-55.0$ |
| 15000 | 90.6 | 3.57 | . 1931 | . 01206 | -55.0 |

table 629.-VALUES OF ATMOSPHERIC TEMPERATURE, PRESSURE, AND DENSITY UP TO THE F LAYER*

| Heigbt, $h$ |  | Apparent gravity, $g^{\prime}$ $\mathrm{cm} / \mathrm{sec}^{3}$ | ${ }_{\text {Temp }}{ }_{\mathbf{K}}$ | Pressure, $p$ <br> millibars | Density, $\rho$ | $\begin{gathered} \text { Number } \\ \text { density, } \\ \text { particles } / \mathrm{cm}^{2} \end{gathered}$ | Mean particle speed, $v$ $\mathrm{cm} / \mathrm{sec}$ | Mean free path, $L$ cm | Mean collision freq, $\nu$ $1 / \mathrm{sec}$ | Speed of sound, $c$ $\mathrm{cm} / \mathrm{sec}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| km | mi |  |  |  |  |  |  |  |  |  |
| 0 | 0 | 980.69 | 288.0 | 1014 | $1.223 \times 10^{-2}$ | $2.568 \times 10^{18}$ | $4.590 \times 10^{4}$ | $9.744 \times 10^{-6}$ | $4.712 \times 10^{0}$ | $3.410 \times 10^{4}$ |
| 1.524 | . 947 | 980.22 | 278.1 | 843.5 | $1.055 \times 10^{-6}$ | $2.213 \times 10^{19}$ | 4.511 | $1.130 \times 10^{-8}$ | $3.991 \times 10^{0}$ | 3.351 |
| 3.048 | 1.894 | 979.74 | 268.2 | 697.5 | $9.047 \times 10^{-4}$ | $1.898 \times 10^{10}$ | 4.432 | $1.318 \times 10^{-5}$ | $3.362 \times 10^{\circ}$ | 3.291 |
| 6.096 | 3.788 | 978.80 | 248.4 | 466.8 | $6.537 \times 10^{-4}$ | $1.371 \times 10^{10}$ | 4.264 | $1.825 \times 10^{-8}$ | $2.337 \times 10^{\circ}$ | 3.167 |
| 9.144 | 5.682 | 977.87 | 226.6 | 302.3 | $4.601 \times 10^{-4}$ | $9.652 \times 10^{18}$ | 4.090 | $2.592 \times 10^{-5}$ | $1.578 \times 10^{0}$ | 3.038 |
| 10.769 | 6.629 | 977.37 | 218.0 | 236.2 | $3.768 \times 10^{-6}$ | $7.905 \times 10^{18}$ | 3.996 | $3.165 \times 10^{-8}$ | $1.262 \times 10^{\circ}$ | 2.967 |
| 13.716 | 8.523 | 976.46 | 218.0 | 149.2 | $2.381 \times 10^{-4}$ | $4.995 \times 10^{18}$ | 3.996 | $5.010 \times 10^{-5}$ | $7.976 \times 10^{8}$ | 2.967 |
| 16.764 | 10.417 | 975.52 | 218.0 | 92.88 | $1.482 \times 10^{-6}$ | $3.109 \times 10^{28}$ | 3.996 | $8.048 \times 10^{-5}$ | $4.965 \times 10^{8}$ | 2.967 |
| 22.860 | 14.205 | 973.66 | 218.0 | 36.14 | $5.761 \times 10^{-5}$ | $1.210 \times 10^{18}$ | 3.996 | $2.069 \times 10^{-6}$ | $1.931 \times 10^{8}$ | 2.968 |
| 27.432 | 17.045 | 972.26 | 218.0 | 17.89 | $2.849 \times 10^{-8}$ | $5.989 \times 10^{17}$ | 3.999 | $4.178 \times 10^{-6}$ | $9.572 \times 10^{7}$ | 2.970 |
| 32.000 | 19.884 | 970.87 | 218.0 | 8.901 | $1.415 \times 10^{-5}$ | $2.979 \times 10^{17}$ | 4.002 | $8.399 \times 10^{-6}$ | $4.765 \times 10^{7}$ | 2.972 |
| 39.624 | 24.621 | 968.54 | 276.0 | 3.148 | $3.946 \times 10^{-6}$ | $8.323 \times 10^{18}$ | 4.508 | $3.006 \times 10^{-6}$ | $1.499 \times 10^{7}$ | 3.348 |
| 50.000 | 31.068 | 965.40 | 355.0 | 1.054 | $1.024 \times 10^{-6}$ | $2.166 \times 10^{18}$ | 5.118 | $1.155 \times 10^{-2}$ | $4.430 \times 10^{6}$ | 3.802 |
| 60.000 | 37.282 | 962.39 | 355.0 | $4.136 \times 10^{-1}$ | $4.019 \times 10^{-7}$ | $8.501 \times 10^{18}$ | 5.118 | $2.943 \times 10^{-2}$ | $1.739 \times 10^{6}$ | 3.802 |
| 68.581 | 42.614 | 959.81 | 300.2 | $1.740 \times 10^{-1}$ | $2.000 \times 10^{-7}$ | $4: 230 \times 10^{18}$ | 4.706 | $5.915 \times 10^{-2}$ | $7.956 \times 10^{5}$ | 3.496 |
| 78.000 | 48.466 | 957.00 | 240.0 | $5.469 \times 10^{-2}$ | $7.860 \times 10^{-8}$ | $1.663 \times 10^{15}$ | 4.209 | $1.505 \times 10^{-1}$ | $2.797 \times 10^{5}$ | 3.126 |
| 83.000 | 51.573 | 955.51 | 240.0 | $2.752 \times 10^{-8}$ | $3.956 \times 10^{-8}$ | $8.367 \times 10^{14}$ | 4.209 | $2.990 \times 10^{-1}$ | $1.408 \times 10^{5}$ | 3.126 |
| 92.965 | 57.765 | 952.55 | 276.4 | $7.938 \times 10^{-8}$ | $9.507 \times 10^{-9}$ | $2.096 \times 10^{14}$ | 4.612 | 1.194 | $3.862 \times 10^{4}$ | 3.443 |
| 100.58 | 62.500 | 950.30 | 304.2 | $3.526 \times 10^{-4}$ | $3.713 \times 10^{-0}$ | $8.459 \times 10^{18}$ | 4.916 | 2.958 | $1.662 \times 10^{4}$ | 3.686 |
| 120.00 | 74.564 | 944.60 | 375.0 | $6.677 \times 10^{-4}$ | $5.218 \times 10^{-10}$ | $1.299 \times 10^{13}$ | 5.708 | $1.926 \times 10$ | $2.964 \times 10^{8}$ | 4.322 |
| 152.40 | 94.697 | 935.20 | 505.5 | $8.67 \times 10^{-5}$ | $5.02 \times 10^{-11}$ | $1.25 \times 10^{12}$ | 6.63 | $2.00 \times 10^{2}$ | $3.32 \times 10^{2}$ | 5.02 |
| 213.36 | 132.58 | 917.88 | 751.0 | $5.99 \times 10^{-6}$ | $2.33 \times 10^{-12}$ | $5.83 \times 10^{10}$ | 8.07 | $4.29 \times 10^{3}$ | $1.88 \times 10$ |  |
| 259.08 | 160.98 | 905.21 | 935.2 | $1.40 \times 10^{-8}$ | $4.38 \times 10^{-18}$ | $1.09 \times 10^{10}$ | 9.01 | $2.29 \times 10^{4}$ | $3.93 \times 10$ |  |
| 300.00 | 186.41 | 894.09 | 1100 | $4.84 \times 10^{-7}$ | $1.29 \times 10^{-18}$ | $3.21 \times 10^{0}$ | 9.78 | $7.79 \times 10^{4}$ | $1.25 \times 10$ |  |

[^243]* For reference, see footnote 195, p. 592.
$\dagger d=$ diameter of particle.

| Mean mol wt M | Pressure, p millibars | $\underset{\mathrm{g} / \mathrm{cm}^{3}}{\substack{\text { Density, }}}$ | Number density, $n$ particles $/ \mathrm{cm}^{3}$ | $\dagger=2 \times 10^{-8} \mathrm{~cm}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Mean particle speed $v$ $\mathrm{~cm} / \mathrm{sec}$ | Mean free path, $L$ cm | Mean collision freq, $\nu$ $1 / \mathrm{sec}$ |
| 24.35 | $4.84 \times 10^{-7}$ | $1.29 \times 10^{-13}$ | $3.21 \times 10^{9}$ | $9.78 \times 10^{4}$ | $1.76 \times 10^{5}$ | $5.56 \times 10^{-1}$ |
| 14.40 | $9.70 \times 10^{-8}$ | $1.12 \times 10^{-14}$ | $4.72 \times 10^{8}$ | $1.48 \times 10^{5}$ | $1.20 \times 10^{6}$ | $1.24 \times 10^{-1}$ |
| 14.36 | $4.06 \times 10^{-8}$ | $3.69 \times 10^{-15}$ | $1.56 \times 10^{8}$ | $1.67 \times 10^{5}$ | $3.63 \times 10^{9}$ | $4.62 \times 10^{-2}$ |
| 14.33 | $2.05 \times 10^{-8}$ | $1.54 \times 10^{-15}$ | $6.49 \times 10^{7}$ | $1.84 \times 10^{5}$ | $8.69 \times 10^{6}$ | $2.12 \times 10^{-2}$ |
| 14.31 | $1.16 \times 10^{-8}$ | $8.00 \times 10^{-10}$ | $3.39 \times 10^{7}$ | $1.92 \times 10^{5}$ | $1.66 \times 10^{7}$ | $1.16 \times 10^{-2}$ |
| 14.28 | $4.01 \times 10^{-0}$ | $2.75 \times 10^{-16}$ | $1.17 \times 10^{7}$ | $1.93 \times 10^{5}$ | $4.81 \times 10^{7}$ | $4.00 \times 10^{-8}$ |
| 14.26 | $2.41 \times 10^{-0}$ | $1.65 \times 10^{-16}$ | $7.03 \times 10^{0}$ | $1.93 \times 10^{5}$ | $8.01 \times 10^{7}$ | $2.41 \times 10^{-8}$ |
| 14.19 | $2.31 \times 10^{-10}$ | $1.58 \times 10^{-17}$ | $6.73 \times 10^{5}$ | $1.93 \times 10^{5}$ | $8.36 \times 10^{8}$ | $2.31 \times 10^{-4}$ |
| 14.11 | $2.96 \times 10^{-11}$ | $2.01 \times 10^{-19}$ | $8.62 \times 10^{4}$ | $1.94 \times 10^{5}$ | $6.52 \times 10^{0}$ | $2.97 \times 10^{-5}$ |
| 9.14 | $9.75 \times 10^{-14}$ | $4.29 \times 10^{-21}$ | $2.84 \times 10^{2}$ | $2.41 \times 10^{5}$ | $1.98 \times 10^{12}$ | $1.22 \times 10^{-7}$ |
| 1.76 | $2.58 \times 10^{-14}$ | $2.18 \times 10^{-22}$ | $7.52 \times 10$ | $5.48 \times 10^{5}$ | $7.49 \times 10^{12}$ | $7.32 \times 10^{-8}$ |
| 1.12 | $1.58 \times 10^{-14}$ | $8.52 \times 10{ }^{23}$ | $4.61 \times 10$ | $6.87 \times 10^{5}$ | $122 \times 10^{13}$ | $562 \times 10^{-8}$ |
| 1.04 | $9.82 \times 10^{-15}$ | $4.90 \times 10^{-23}$ | $2.86 \times 10$ | $7.14 \times 10^{5}$ | $1.96 \times 10^{18}$ | $3.64 \times 10^{-8}$ |
| 1.02 | $7.90 \times 10^{-15}$ | $3.94 \times 10^{-23}$ | $2.33 \times 10$ | $7.19 \times 10^{5}$ | $2.41 \times 10^{13}$ | $2.98 \times 10^{-8}$ |
| 1.02 | $7.11 \times 10^{-15}$ | $3.49 \times 10^{-23}$ | $2.08 \times 10$ | $7.20 \times 10^{5}$ | $2.71 \times 10^{13}$ | $2.66 \times 10^{-8}$ |
| 1.02 | $6.60 \times 10^{-15}$ | $3.23 \times 10^{-20}$ | $1.93 \times 10$ | $7.21 \times 10^{5}$ | $2.92 \times 10^{13}$ | $2.47 \times 10^{-8}$ |
| 1.02 | $6.27 \times 10^{-15}$ | $3.06 \times 10^{-29}$ | $1.83 \times 10$ | $7.22 \times 10^{5}$ | $3.08 \times 10^{13}$ | $2.34 \times 10^{-8}$ |
| 1.02 | $6.03 \times 10^{-15}$ | $2.94 \times 10^{-23}$ | $1.76 \times 10$ | $7.22 \times 10^{5}$ | $3.20 \times 10^{13}$ | $2.26 \times 10^{-8}$ |

# Percentage composition by mass 

|  |  |
| :---: | :---: |
|  |  |
|  |  |
|  |  <br>  |




| $=$ |  |
| :---: | :---: |
| 䄔 |  |

# TABLE 631.-RELATIVE DENSITY OF MOIST AIR FOR DIFFERENT PRESSURES AND HUMIDITIES 

Part 1.-Values of $\frac{h}{760}$, from $h=1$ to $h=9$, for the computation of different values of the ratio of actual to normal barometric pressure

This gives the density of moist air at pressure $h$ in terms of the same air at normal atmosphere pressure. When air contains moisture, as is usually the case with the atmossphere, we have the following equation for pressure term: $h=B-0.378 p$, where $p$ is the vapor pressure, and $B$ the corrected barometric pressure. When the necessary psychrometric observations are made the values of $p$ may be taken from Table 640 and then $0.378 p$ from Table 632, or the dew point may be found and the value of $0.378 p$ taken from Table 632.

| h | $\frac{h}{760}$ | Examples of use of the table To find the value of $\frac{h}{760}$ when $h=754.3$ $h=700$ gives .92105 |
| :---: | :---: | :---: |
| 1 | . 0013158 | 50 " 0.065789 |
| 2 | . 0026316 | 4 " . 005263 |
| 3 | . 0039474 | . 3 " . 000395 |
| 4 | . 0052632 | 754.3 . 992497 |
| 5 | . 0065789 |  |
| 6 | . 0078947 | To find the value of $\frac{h}{760}$ when $h=5.73$ |
| 7 | . 0092105 | $h=5$ gives . 0065789 |
| 8 | . 0105263 | - . 7 " . 0009210 |
| 9 | . 0118421 | . 03 " . 0000395 |
|  |  | 5.73 . 0075394 |

Part 2.-Values of the logarithms of $\frac{h}{760}$ for values of $h$ between 80 and 800
Values from 8 to 80 may be got by subtracting 1 from the characteristic, and from 0.8 to 8 by subtracting 2 from the charactcristic, and sc on.

| Values of $\log \frac{h}{760}$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| h | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 80 | $\overline{1} .02228$ | $\overline{1} .02767$ | $\overline{1} .03300$ | $\overline{1} .03826$ | $\overline{1} .04347$ | $\overline{1} .04861$ | 1. 05368 | $\overline{1} .05871$ | $\overline{1} .06367$ | 1.06858 |
| 90 | . 07343 | . 07823 | . 08297 | . 08767 | . 09231 | . 09691 | . 10146 | . 10596 | . 11041 | . 11482 |
| 100 | $\overline{1} .11919$ | $\overline{1} .12351$ | $\overline{1.12779 ~}$ | $\overline{1} .13202$ | $\overline{1} .13622$ | $\overline{1} .14038$ | $\overline{1} .14449$ | 1.14857 | 1. 15261 | $\overline{1.15661}$ |
| 110 | . 16058 | . 16451 | . 16840 | . 17226 | . 17609 | . 17988 | . 18364 | . 18737 | . 19107 | . 19473 |
| 120 | . 19837 | . 20197 | . 20555 | . 20909 | . 21261 | 21611 | . 21956 | . 22299 | . 22640 | . 22978 |
| 130 | . 23313 | . 23646 | . 23976 | . 24304 | . 24629 | . 24952 | . 25273 | . 25591 | . 25907 | . 26220 |
| 140 | . 26531 | . 26841 | . 27147 | . 27452 | . 27755 | . 28055 | . 28354 | . 28650 | . 28945 | . 29237 |
| 150 | $\overline{1} .29528$ | $\overline{1} .29816$ | $\overline{1} .30103$ | $\overline{1} .30388$ | 1. 30671 | 1. 30952 | $\overline{1} .31231$ | $\overline{1} .31509$ | $\overline{1} .31784$ | -1.32058 |
| 160 | . 32331 | . 32601 | . 32870 | . 33137 | . 33403 | . 33667 | . 33929 | . 34190 | . 34450 | . 34707 |
| 170 | . 34964 | . 35218 | . 35471 | . 35723 | . 35974 | . 36222 | . 36470 | . 36716 | . 36961 | . 37204 |
| 180 | . 37446 | . 37686 | . 37926 | . 38164 | . 38400 | . 38636 | . 38870 | . 39128 | . 39334 | . 39565 |
| 190 | . 39794 | . 40022 | . 40249 | . 40474 | . 40699 | . 40922 | . 41144 | . 41365 | . 41585 | . 41804 |
| 200 | $\overline{1.42022 ~}$ | 1. 42238 | $\overline{1} .42454$ | $\overline{1} .42668$ | 1. 42882 | 1. 43094 | $\overline{1.43305}$ | 1. 43516 | - 1.43725 | 1. 43933 |
| 210 | . 44141 | . 44347 | . 44552 | . 44757 | . 44960 | . 45162 | . 45364 | . 45565 | . 45764 | . 45963 |
| 220 | . 46161 | . 46358 | . 46554 | . 46749 | . 46943 | . 47137 | . 47329 | . 47521 | . 47712 | . 47902 |
| 230 | . 48091 | . 48280 | . 48467 | . 48654 | . 48840 | . 49025 | . 49210 | . 49393 | . 49576 | . 49758 |
| 240 | . 49940 | . 50120 | . 50300 | . 50479 | . 50658 | . 50835 | . 51012 | . 51188 | . 51364 | . 51539 |

[^244]TABLE 631.-RELATIVE DENSITY OF MOIST AIR FOR DIFFERENT PRESSURES AND HUMIDITIES (continued)
Part 2.-Values of the logarithms of $\frac{h}{760}$ for values of $h$ between 80 and 800 (continued)
Values of $\operatorname{Iog} \frac{h}{760}$
$h$
250
260
270
280
290

| 0 | 1 | 2 | 3 | 4 |
| :---: | :---: | :---: | :---: | :---: |


| $\overline{1} .51713$ | $\overline{1} .51886$ | $\overline{1} .52059$ | $\overline{1} .52231$ | $\overline{1} .5$ |
| ---: | ---: | ---: | ---: | ---: |
| .53416 | .53583 | .53749 | .53914 | .5 |
| .55055 | .55216 | .55376 | .55535 | .55 |
| .56634 | .56789 | .56944 | .57097 | .57 |
| .58158 | .58308 | .58457 | .58605 | .58 |

$\overline{1} .5$$\overline{1} .59631 \overline{1} .5$ .59775 $\overline{1} .59919$ 1.
.62434
.63770
.

6506 $\begin{array}{rrrrr}.59631 & \overline{1} .59775 & \overline{1} .59919 & \overline{1} .60063 & \overline{1} .60 \\ .61055 & .61195 & .61334 & .61473 & .6161 \\ .62434 & .62569 & .62704 & .62839 & .629 \\ .63770 & .63901 & .64332 & .64163 & .64 \\ .65067 & .65194 & .65321 & .65448 & .6557 \\ .66325 & \overline{1} .66449 & \overline{1} .66573 & \overline{1} .66696 & \overline{1} .668\end{array}$ 1. $\begin{array}{rr}\overline{1} .66325 & \overline{1} \\ .67549 & .67\end{array}$ .52402

.54079
.55694
.57250

.58753 .69897 . .71025 . 7 67669 . 67790 | 6 | $\overline{1} .66$ |
| :--- | :--- | 0206 ̄̄

| $\overline{1} .52573$ | $\overline{1} .5$ |
| ---: | ---: |
| .54243 | .54 |
| .55852 | -.5 |
| .57403 | .5 |
| .58901 | .5 |

$\square$$1.51713 \quad \overline{1} .51886 \quad \overline{1} .52059 \quad \overline{1} .52231$
1.527
.5
.560
.5
.5
43
10 . $.52912 \overline{1}$.
.54570 1.53081
54732 54732
.56323 1.53249
.54894
.56479
.58008
.59486 $.59048 \quad .59194 \quad .59340$ $\begin{array}{lr}.60774 & \overline{1} .60914 \\ .62161 & .62298\end{array}$

## $\qquad$

.61887 .
$\begin{array}{rr}\overline{1} .60632 & \overline{1} .6 \\ .62025 & .61 \\ .63373 & \end{array}$ 62973 . 63107 . 63240 . 63373 . 63506 . 63638 .64293 . 64423 . 64553 . 64682 . 64810 . 64939 .65574 . 65701.65826 . 65952 . 66077 . 66201

$$
9 \overline{1} .66941 \overline{1} .
$$

$\overline{1} .67064 \overline{1}$$7 \overline{1} .67428$688191| .66941 | 1. |  |
| :--- | :--- | :--- |
| .69322 | . |  |
|  | .70465 |  |
| .71578 | . |  |$\begin{array}{llllll}.68029 & .68148 & .68267 & .68385 & .68503 & .68621 \\ .69206 & .69322 & .69437 & .69553 & .69668 & .69783\end{array}$.68385

.69553

.70690.68503170352.70577.70690| 70802 | .70978 |
| :--- | :--- |.71688.71798.71907.71

-.71578
1.72125 1.72233 72233 1.72341 $\overline{1}$ . 1.72449 $\overline{1} .7$ $\begin{array}{rr}\overline{1} .72557 & \overline{1} . \\ .73619 & .\end{array}$ 1.72664

.73723 $\overline{1.7277}$ | 1 | $\overline{1} .7$ |
| :--- | ---: |
|  | .7 |

.73828
.74860
.75867 72878 1. 1.72985 $\overline{1.73091}$ .74244 .75265 .76264 $\overline{1}$. 1.77240

- 1.7 .74347 $75366 \quad .75467 \quad .75567$ .74655
.75668
.76657
.74758
.75768 .7586 .76755
- 1.7
4 1.
20 1. .76852
74961 74036 4140 .75967 . 76066 . 76165 77336 1.77 $32 \overline{1.77}$ .77528

1.7762 1.77720 | .78664 | 1.77815 | $\overline{1} .779$ |
| ---: | ---: | ---: |
| .78757 | .788 |  |

[^245]78005
$\overline{1.78100}$
.78194
.78570
.79496
.80403
.80043
.79221 . 79313 . 79405
.80938 . 81027 . 81115 . 81203
$\overline{1} 818$

$3 \overline{1} .8$
$81902 \overline{1} .819$


| 1.82075 | 1 |
| :--- | :--- |
| .82930 |  |
| .83769 |  |
| 8 |  |

$\overline{1} .8$
-.80493.79679$78770 \quad .78943$79770 . 79861 . 7995280672 . 80761.80850.81554 .8164281729

- 
- 1.82
$\overline{1}$. 1.82590580 . 88261590
600 ī189734
. $90452 \quad .90523 \quad .90594$

| 620 | .91158 | .91228 | .91298 |
| :--- | :--- | :--- | :--- |
| 630 | .91853 | .91922 | .91990 |


| 640 | .92537 | .92604 | .92672 |
| :--- | :--- | :--- | :--- |

# TABLE 631.-RELATIVE DENSITY OF MOIST AIR FOR DIFFERENT 

 PRESSURES AND HUMIDITIES (concluded)
## Part 2.-Values of the logarithms of $\frac{h}{760}$ for values of $h$ between 80 and 800 (concluded)

| h | Values of $\log \frac{h}{760}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 1 | 2 | 3 | 4 | 5 | B | 7 | 8 | 9 |
| 750 | $\overline{1} .99425$ | $\overline{1} .99483$ | $\overline{1} .99540$ | 1.99598 | $\overline{1} .99656$ | $\overline{1} .99713$ | $\overline{1} .99771$ | $\overline{1} .99828$ | $\overline{1} .99886$ | 1.99942 |
| 760 | . 00000 | . 00057 | . 00114 | . 00171 | . 00228 | . 00285 | . 00342 | . 00398 | . 00455 | . 00511 |
| 770 | . 00568 | . 00624 | . 00680 | . 00737 | . 00793 | . 00849 | . 00905 | . 00961 | . 01017 | . 01072 |
| 780 | . 01128 | . 01184 | . 01239 | . 01295 | . 01350 | . 01406 | . 01461 | . 01516 | . 01571 | . 01626 |
| 790 | . 01681 | . 01736 | . 01791 | . 01846 | . 01901 | . 01955 | . 02010 | . 02064 | . 02119 | . 02173 |

## TABLE 632.-DENSITY OF MOIST AIR, VALUES OF 0.378p

This table gives the humidity term $0.378 p$, which occurs in the equation $\delta=\delta_{0} \frac{h}{760}=$ $\delta_{0} \frac{B-0.378 p}{760}$ for the calculation of the density of air containing aqueous vapor at pressure $p ; \delta_{0}$ is the density of dry air at normal temperature and barometric pressure, $B$ the observed barometric pressure, and $h=B-0.378 p$, the pressure corrected for humidity. For values of $\frac{h}{760}$, see Table 631. Temperatures are in degrees centigrade, and pressures in mmHg .

| Dew point | $\stackrel{p}{p}$ pressure (ice) | 0.378p | $\begin{aligned} & \text { Dew } \\ & \text { point } \end{aligned}$ | $\underset{\substack{\text { Vapor } \\ \text { nessure }}}{p}$ $\begin{aligned} & \text { pressure } \\ & \text { (water) } \end{aligned}$ (water) | 0.378p | $\begin{aligned} & \text { Dew } \\ & \text { point } \end{aligned}$ | $\begin{gathered} \text { papor } \\ \text { pressure } \\ \text { (water) } \end{gathered}$ | 0.378p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{C}$ | mmHg | mmHg | ${ }^{\circ} \mathrm{C}$ | mmHg | mmHg | ${ }^{\circ} \mathrm{C}$ | mmHg | mmHg |
| -50 | . 029 | . 01 | 0 | 4.58 | 1.73 | 30 | 31.86 | 12.0 |
| -45 | . 054 | . 02 | 1 | 4.92 | 1.86 | 31 | 33.74 | 12.8 |
| -40 | . 096 | . 04 | 2 | 5.29 | 2.00 | 32 | 35.70 | 13.5 |
| -35 | . 169 | . 06 | 3 | 5.68 | 2.15 | 33 | 37.78 | 14.3 |
| -30 | . 288 | . 11 | 4 | 6.10 | 2.31 | 34 | 39.95 | 15.1 |
| -25 | . 480 | . 18 | 5 | 6.54 | 2.47 | 35 | 42.23 | 16.0 |
| 24 | . 530 | . 20 | 5 | 7.01 | 2.66 | 36 | 44.62 | 16.9 |
| 23 | . 585 | . 22 | 7 | 7.51 | 2.84 | 37 | 47.13 | 17.8 |
| 22 | . 646 | . 24 | 8 | 8.04 | 3.04 | 38 | 49.76 | 18.8 |
| 21 | . 712 | . 27 | 9 | 8.61 | 3.25 | 39 | 52.51 | 19.8 |
| -20 | . 783 | . 30 | 10 | 9.21 | 348 | 40 | 55.40 | 20.9 |
| 19 | . 862 | . 33 | 11 | 9.85 | 3.72 | 41 | 58.42 | 22.1 |
| 18 | . 947 | . 36 | 12 | 10.52 | 3.98 | 42 | 61.58 | 23.3 |
| 17 | 1.041 | . 39 | 13 | 11.24 | 4.25 | 43 | 64.89 | 24.5 |
| 16 | 1.142 | . 43 | 14 | 11.99 | 4.53 | 44 | 68.35 | 25.8 |
| -15 | 1.252 | . 47 | 15 | 12.79 | 4.84 | 45 | 71.97 | 27.2 |
| 14 | 1.373 | . 52 | 16 | 13.64 | 5.16 | 46 | 75.75 | 28.6 |
| 13 | 1.503 | . 57 | 17 | 14.54 | 5.50 | 47 | 79.70 | 30.1 |
| 12 | 1.644 | . 62 | 18 | 15.49 | 5.85 | 48 | 83.83 | 31.7 |
| 11 | 1.798 | . 68 | 19 | 16.49 | 6.23 | 49 | 88.14 | 33.3 |
| -10 | 1.964 | . 74 | 20 | 17.55 | 6.63 | 50 | 92.6 | 35.0 |
| 9 | 2.144 | . 81 | 21 | 18.66 | 7.06 | 51 | 97.3 | 36.8 |
| 8 | 2.340 | . 88 | 22 | 19.84 | 7.50 | 52 | 102.3 | 38.6 |
| 7 | 2.550 | . 96 | 23 | 21.09 | 7.97 | 53 | 107.3 | 40.6 |
| 6 | 2.778 | 1.05 | 24 | 22.40 | 8.47 | 54 | 112.7 | 42.6 |
| - 5 | 3.025 | 1.14 | 25 | 23.78 | 8.99 | 55 | 118.2 | 44.7 |
| 4 | 3.291 | 1.24 | 26 | 25.24 | 9.54 | 56 | 124.0 | 46.9 |
| 3 | 3.578 | 1.35 | 27 | 26.77 | 10.12 | 57 | 130.0 | 49.1 |
| 2 | 3.887 | 1.47 | 28 | 28.38 | 10.73 | 58 | 136.3 | 51.5 |
| 1 | 4.220 | 1.60 | 29 | 30.08 | 11.37 | 59 | 142.8 | 54.0 |
| 0 | 4.580 | 1.73 | 30 | 31.86 | 12.04 | 60 | 149.6 | 56.5 |

TABLE 633.-MAINTENANCE OF AIR AT DEFINITE HUMIDITIES
The relative humidity and vapor pressure of aqueous vapor of moist air in equilibrium conditions above aqueous solutions of sulfuric acid are given below.

| Density of acid sol | Relativehumidity | Vapor pressure |  | Density ofacid sol | Relativehumidity | Vapor pressure |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\overparen{\substack{20^{\circ} \mathrm{C} \\ \mathrm{~mm}}}$ | $\begin{gathered} 30^{\circ} \mathrm{C} \\ \mathrm{~mm} \end{gathered}$ |  |  | $20^{\circ} \mathrm{C}$ | $\begin{aligned} & 30^{\circ} \mathrm{C} \\ & \mathrm{~mm} \end{aligned}$ |
| 1.00 | 100.0 | 17.4 | 31.6 | 1.30 | 58.3 | 10.1 | 18.4 |
| 1.05 | 97.5 | 17.0 | 30.7 | 1.35 | 47.2 | 8.3 | 15.0 |
| 1.10 | 93.9 | 16.3 | 29.6 | 1.40 | 37.1 | 6.5 | 11.9 |
| 1.15 | 88.8 | 15.4 | 28.0 | 1.50 | 18.8 | 3.3 | 6.0 |
| 1.20 | 80.5 | 14.0 | 25.4 | 1.60 | 8.5 | 1.5 | 2.7 |
| 1.25 | 70.4 | 12.2 | 22.2 | 1.70 | 3.2 | . 6 | 1.0 |

## TABLE 634.-PRESSURE OF AQUEOUS VAPOR IN THE ATMOSPHERE

For various altitudes (barometric readings)
The amount of water vapor in the atmosphere may be determined by the use of the wet-bulb-dry-bulb hygrometer.
The first column gives the depression of the wet-bulb temperature $t_{1}$ below the air temperature $t$. The value corresponding to the barometric height at the altitude of observation is to be subtracted from the vapor pressure corresponding to the wet-bulb temperature taken from Part 3, Table 635. The temperature corresponding to this vapor pressure taken from Part 3, Table 635 is the dew point. The wet bulb should be ventilated about 3 meters per second. For sea-level use Table 640. Example : $t=35^{\circ}, t_{1}=30^{\circ}$, barometer 74 cmHg . Then $31.83-2.46=29.37 \mathrm{~mm}=$ aqueous vapor pressure; the dew point is $28.6^{\circ} \mathrm{C}$.

| ${ }^{t}{ }^{\circ} \mathrm{C}{ }^{t_{1}}$ | Barometric pressure in cmHg |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 74 | 72 | 70 | 68 | 86 | 64 | 62 | 60 | 58 | 56 | 54 | 52 | 50 | 48 |
|  | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm |
| $1{ }^{\circ}$ | . 50 | . 48 | . 47 | . 46 | . 44 | . 43 | . 42 | . 40 | . 39 | . 38 | . 36 | . 35 | . 34 | . 32 |
| 2 | . 98 | . 96 | . 93 | . 90 | 88 | . 85 | . 82 | . 80 | . 77 | . 75 | . 72 | . 69 | . 67 | . 64 |
| 3 | 1.47 | 1.43 | 1.39 | 1.35 | 1.32 | 1.28 | 1.24 | 1.20 | 1.15 | 1.12 | 1.08 | 1.04 | 1.00 | . 96 |
| 4 | 1.97 | 1.91 | 1.86 | 1.81 | 1.75 | 1.70 | 1.65 | 1.60 | 1.54 | 1.49 | 1.44 | 1.38 | 1.33 | 1.28 |
| 5 | 2.46 | 2.39 | 2.32 | 2.26 | 2.19 | 2.13 | 2.06 | 1.99 | 1.93 | 1.86 | 1.80 | 1.73 | 1.66 | 1.60 |
| 6 | 2.95 | 2.87 | 2.79 | 2.71 | 2.63 | 2.55 | 2.47 | 2.39 | 2.32 | 2.24 | 2.16 | 2.08 | 2.00 | 1.92 |
| 7 | 3.45 | 3.36 | 3.26 | 3.17 | 3.08 | 2.99 | 289 | 2.80 | 2.71 | 2.61 | 2.52 | 2.43 | 2.33 | 2.24 |
| 8 | 3.95 | 3.84 | 3.73 | 3.63 | 3.53 | 3.42 | 3.31 | 3.20 | 3.10 | 2.99 | 2.88 | 2.78 | 2.67 | 2.56 |
| 9 | 4.44 | 4.32 | 4.21 | 4.09 | 3.97 | 3.85 | 3.73 | 3.61 | 3.49 | 3.37 | 3.25 | 3.13 | 3.00 | 2.88 |
| 10 | 4.94 | 4.81 | 4.68 | 4.54 | 4.41 | 4.28 | 4.14 | 4.01 | 3.88 | 3.74 | 3.61 | 3.48 | 3.34 | 3.21 |
| 11 | 5.44 | 5.30 | 5.15 | 5.00 | 4.86 | 4.71 | 4.56 | 4.42 | 4.27 | 4.12 | 3.97 | 3.83 | 3.68 | 3.53 |
| 12 | 5.94 | 5.78 | 5.62 | 5.46 | 5.30 | 5.14 | 4.98 | 4.82 | 4.66 | 4.50 | 4.34 | 4.18 | 4.02 | 3.85 |
| 13 | 6.45 | 6.27 | 6.10 | 5.92 | 5.75 | 5.57 | 5.40 | 5.23 | 5.05 | 4.88 | 4.70 | 4.53 | 4.36 | 4.18 |
| 14 | 6.95 | 6.76 | 6.58 | 6.39 | 6.20 | 6.01 | 5.83 | 5.64 | 5.45 | 5.26 | 5.07 | 4.88 | 4.70 | 4.51 |
| 15 | 7.46 | 7.26 | 7.06 | 6.85 | 6.65 | 6.45 | 6.25 | 6.05 | 5.85 | 5.64 | 5.44 | 5.24 | 5.04 | 4.84 |
| 16 | 7.96 | 7.75 | 7.54 | 7.32 | 7.11 | 6.89 | 6.68 | 6.46 | 6.24 | 6.03 | 5.81 | 5.60 | 5.38 | 5.17 |
| 17 | 8.47 | 8.24 | 8.02 | 7.79 | 7.56 | 7.33 | 7.10 | 6.87 | 6.64 | 6.41 | 6.18 | 5.95 | 5.72 | 5.50 |

## TABLE 635.-PRESSURE OF SATURATED WATER VAPOR FOR VARIOUS CONDITIONS OF TEMPERATURE AND SURROUNDINGS

Pressure in mmHg , temperature in ${ }^{\circ} \mathrm{C}$
Part 1.-At low temperatures over ice

| Temp | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -60 | .0081 | .0371 | .0062 | .0054 | .0047 | .0041 | .0035 | .0030 | .0026 | .0023 |
| -50 | .0295 | .0261 | .0222 | .0203 | .0178 | .0157 | .0138 | .0121 | .0106 | .0094 |
| -40 | .0962 | .0858 | .0766 | .0681 | .0607 | .0540 | .0479 | .0425 | .0377 | .0333 |
| -30 | .2855 | .2560 | .2308 | .2075 | .1865 | .1675 | .1502 | .1337 | .1205 | .1078 |
| -20 | .7740 | .7030 | .6380 | .5780 | .5240 | .4790 | .4290 | .3880 | .3500 | .3160 |
| -10 | 1.945 | 1.782 | 1.630 | 1.486 | 1.359 | 1.239 | 1.130 | 1.029 | .9360 | .8510 |
| 0 | 4.580 | 4.219 | 3.880 | 3.565 | 3.280 | 3.010 | 2.765 | 2.531 | 2.322 | 2.128 |

Part 2.-At low temperatures over water

| Temp | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -10 | 2.148 | 1.983 | 1.832 | 1.690 | 1.556 | 1.434 | 1.319 | 1.215 | 1.109 | 1025 |
| 0 | 4.580 | 4.260 | 3.968 | 3.672 | 3.410 | 3.160 | 2.930 | 2.712 | 2.510 | 2.321 |

Part 3.-Fcr temperatures $0^{\circ}$ to $374^{\circ}$ over water

| Temp | 0 | . 1 | . 2 | . 3 | . 4 | . 5 | . 6 | . 7 | . 8 | . 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 4.580 | 4.615 | 4.648 | 4.685 | 4.712 | 4.750 | 4.784 | 4.820 | 4.855 | 4.888 |
| 1 | 4.922 | 4.960 | 4.998 | 5.030 | 5.065 | 5.105 | 5.140 | 5.175 | 5.212 | 5.250 |
| 2 | 5.289 | 5.328 | 5.365 | 5.404 | 5.442 | 5.482 | 4.525 | 5.566 | 5.602 | 5.642 |
| 3 | 5.680 | 5.720 | 5.761 | 5.801 | 5.842 | 5.885 | 5.930 | 5.972 | 6.014 | 6.055 |
| 4 | 6.095 | 6.139 | 6.182 | 6.125 | 6.270 | 6.314 | 6.358 | 6.401 | 6.445 | 6.490 |
| 5 | 6.535 | 6.582 | 6.535 | 6.679 | 6.724 | 6.770 | 6.816 | 6.862 | 6.910 | 6.960 |
| 6 | 7.010 | 7.058 | 7.106 | 7.155 | 7.204 | 7.254 | 7.306 | 7.356 | 7.408 | 7.460 |
| 7 | 7.509 | 7.560 | 7.613 | 7.666 | 7.720 | 7.772 | 7.823 | 7.875 | 7.929 | 7.984 |
| 8 | 8.039 | 8.095 | 8.149 | 8.205 | 8.260 | 8.315 | 8.370 | 8.425 | 8.482 | 8.542 |
| 9 | 8.605 | 8.670 | 8.726 | 8.782 | 8.838 | 8.900 | 8.960 | 9.020 | 9.080 | 9.140 |
| 10 | 9.200 | 9.263 | 9.325 | 9.390 | 9.455 | 9.520 | 9.580 | 9.645 | 9.707 | 9.770 |
| 11 | 9.835 | 9.901 | 9.965 | 10.032 | 10.100 | 10.170 | 10.240 | 10.308 | 10.375 | 10.445 |
| 12 | 10.518 | 10.580 | 10.655 | 10.718 | 10.790 | 10.858 | 10.928 | 11.000 | 11.075 | 11.150 |
| 13 | 11.225 | 11.300 | 11.375 | 11.750 | 11.525 | 11.600 | 11.677 | 11.755 | 11.829 | 11.905 |
| 14 | 11.980 | 12.060 | 12.140 | 12.217 | 12.295 | 12.375 | 12.455 | 12.538 | 12.620 | 12.698 |
| 15 | 12.776 | 12.860 | 12.945 | 13.025 | 13.110 | 13.195 | 13.280 | 13.365 | 13.450 | 13.540 |
| 16 | 13.625 | 13.710 | 13.801 | 13.895 | 13.985 | 14.075 | 14.165 | 14.255 | 14.345 | 14.440 |
| 17 | 14.530 | 14.620 | 14.710 | 14.800 | 14.895 | 14.990 | 15.085 | 15.172 | 15.270 | 15.375 |
| 18 | 15.460 | 15.560 | 15.660 | 15.760 | 15.960 | 15.960 | 16.060 | 16.160 | 16.260 | 16.360 |
| 19 | 16.460 | 16.570 | 16.680 | 16.790 | 16.900 | 17.000 | 17.100 | 17.210 | 17.315 | 17.425 |
| 20 | 17.525 | 17.635 | 17.745 | 17.855 | 17.965 | 18.080 | 18.195 | 18.310 | 18.425 | 18.540 |
| 21 | 18.650 | 18.765 | 18.880 | 19.000 | 19.110 | 19.225 | 19.345 | 19.460 | 19.580 | 19.700 |
| 22 | 19.820 | 19.940 | 20.060 | 20.185 | 20.310 | 20.430 | 20.580 | 20.690 | 20.800 | 20.930 |
| 23 | 21.050 | 21.190 | 21.320 | 21.450 | 21.580 | 21.710 | 21.840 | 21.970 | 22.100 | 22.230 |
| 24 | 22.365 | 22.500 | 22.630 | 22.763 | 22.905 | 23.050 | 23.190 | 23.310 | 23.450 | 23.600 |
| 25 | 23.750 | 23.900 | 24.030 | 24.200 | 24.345 | 24.490 | 24.640 | 24.790 | 24.935 | 25.080 |
| Temp | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 20 | 17.53 | 18.65 | 19.82 | 21.05 | 22.37 | 23.75 | 25.21 | 26.74 | 28.32 | 30.03 |
| 30 | 31.82 | 33.70 | 35.69 | 37.71 | 39.15 | 42.20 | 44.60 | 47.04 | 49.70 | 52.45 |
| 40 | 55.30 | 58.35 | 61.50 | 64.85 | 68.30 | 71.90 | 75.65 | 79.55 | 83:00 | 88.00 |
| 50 | 92.50 | 97.25 | 102.1 | 107.1 | 113.0 | 118.0 | 123.9 | 129.9 | 136.2 | 142.6 |
| 60 | 149.4 | 156.3 | 163.9 | 171.7 | 179.4 | 187.6 | 196.1 | 205.0 | 214.1 | 223.8 |
| 70 | 308.5 | 243.2 | 252.2 | 265.9 | 275.2 | 289.1 | 301.5 | 314.2 | 327.3 | 340.9 |
| 80 | 355.2 | 369.7 | 384.8 | 400.6 | 416.5 | 439.8 | 450.8 | 468.6 | 487.0 | 506.0 |
| 90 | 525.5 | 546.5 | 567.0 | 588.5 | 610.8 | 634.0 | 658.0 | 682.0 | 707.0 | 733.0 |
| 100 | 767.0 | 786.5 | 815.5 | 845.0 | 875.1 | 906.0 | 937.8 | 970.5 | 1004.2 | 1038.8 |
| (continued) |  |  |  |  |  |  |  |  |  |  |

TABLE 635.-PRESSURE OF SATURATED WATER VAPOR FOR VARIOUS CONDITIONS OF TEMPERATURE AND SURROUNDINGS (concluded)

| Temp | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 110 | 1074 | 1111 | 1149 | 1187 | 1227 | 1268 | 1310 | 1353 | 1397 | 1442 |
| 120 | 1489 | 1536 | 1585 | 1636 | 1687 | 1740 | 1794 | 1850 | 1907 | 1965 |
| 130 | 2025 | 2086 | 2149 | 2214 | 2280 | 2347 | 2416 | 2487 | 2559 | 2633 |
| 140 | 2709 | 2786 | 2866 | 2947 | 3030 | 3115 | 3201 | 3290 | 3381 | 3473 |
| 150 | 3568 | 3665 | 3763 | 3864 | 3967 | 4072 | 4180 | 4290 | 4402 | 4516 |
| 160 | 4632 | 4751 | 4873 | 4997 | 5123 | 5252 | 5383 | 5518 | 5654 | 5794 |
| 170 | 5936 | 6080 | 6228 | 6378 | 6532 | 6688 | 6847 | 7009 | 7174 | 7342 |
| 180 | 7513 | 7688 | 7865 | 8046 | 8230 | 8417 | 8608 | 8802 | 8999 | 9200 |
| 190 | 9404 | 9612 | 9823 | 10040 | 10260 | 10480 | 10700 | 10940 | 11170 | 11410 |
| 200 | 11650 | 11890 | 12140 | 12400 | 12650 | 12920 | 13180 | 13450 | 13730 | 14010 |
| 210 | 14290 | 14580 | 14870 | 15160 | 15470 | 15770 | 16080 | 16400 | 16720 | 17040 |
| 220 | 17370 | 17710 | 18050 | 18390 | 18740 | 19100 | 19450 | 19820 | 20190 | 20560 |
| 230 | 20950 | 21330 | 21720 | 22120 | 22520 | 22930 | 23350 | 23770 | 24190 | 24620 |
| 240 | 25060 | 25500 | 25950 | 26410 | 26870 | 27340 | 27810 | 28290 | 28780 | 29270 |
| 250 | 29770 | 30280 | 30790 | 31310 | 31830 | 32360 | 32900 | 33450 | 34000 | 34560 |
| 260 | 35130 | 35700 | 36280 | 36870 | 37470 | 38070 | 38680 | 39300 | 39920 | 40560 |
| 270 | 41200 | 41840 | 42500 | 43160 | 43840 | 44520 | 45200 | 45900 | 46600 | 47320 |
| 280 | 48040 | 48760 | 49500 | 50250 | 51000 | 51770 | 52540 | 53320 | 54110 | 54910 |
| 290 | 55710 | 56530 | 57360 | 58190 | 59040 | 59890 | 60750 | 61620 | 62510 | 63400 |
| 300 | 64300 | 65210 | 66130 | 67060 | 68000 | 68960 | 69920 | 70890 | 71870 | 72860 |
| 310 | 73870 | 74880 | 75910 | 76940 | 77990 | 79050 | 80120 | 81200 | 82290 | 83390 |
| 320 | 84500 | 85630 | 86760 | 87910 | 89070 | 90250 | 91430 | 92630 | 93840 | 95060 |
| 330 | 96290 | 97530 | 98790 | 100060 | 101350 | 102640 | 103950 | 105280 | 106600 | 108000 |
| 340 | 109300 | 110700 | 112100 | 113500 | 114900 | 116300 | 117800 | 119200 | 120700 | 122200 |
| 350 | 123700 | 125200 | 126800 | 128300 | 129900 | 131400 | 133000 | 134600 | 136300 | 137900 |
| 360 | 139600 | 141200 | 142900 | 144600 | 146300 | 148100 | 149800 | 151600 | 153400 | 155200 |
| 370 | 157000 | 158800 | 160700 | 162600 | 164400 | - | - | - | - | - |

## TABLE 636.-WEIGHT IN GRAMS OF A CUBIC METER OF SATURATED AQUEOUS VAPOR

| $\mathrm{Temp}^{\circ} \mathrm{C}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -20 | 1.074 | . 988 | . 909 | . 836 | . 768 | . 705 | 646 | . 592 | . 542 | . 496 |
| -10 | 2.358 | 2.186 | 2.026 | 1.876 | 1.736 | 1.605 | 1.483 | 1.369 | 1.264 | 1.165 |
| -0 | 4.847 | 4.523 | 4.217 | 3.930 | 3.660 | 3.407 | 3.169 | 2.946 | 2.737 | 2.541 |
| $+0$ | 4.847 | 5.192 | 5.559 | 5.947 | 6.360 | 6.797 | 7.260 | 7.750 | 8.270 | 8.819 |
| +10 | 9.399 | 10.01 | 10.66 | 11.35 | 12.07 | 12.83 | 13.63 | 14.84 | 15.37 | 16.21 |
| $+20$ | 17.30 | 18.34 | 19.43 | 20.58 | 21.78 | 23.05 | 24.38 | 25.78 | 27.24 | 28.78 |
| $+30$ | 30.38 | 32.07 | 33.83 | 35.68 | 37.61 | 39.63 | 41.75 | 43.96 | 46.26 | 48.67 |

For higher temperatures see Table 166.

## TABLE 637.-WEIGHT IN GRAINS OF A CUBIC FOOT OF SATURATED AQUEOUS VAPOR

| ${ }_{\mathrm{T}_{\mathrm{O}} \mathrm{~F}}^{\mathrm{T}}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -20 | . 219 | . 208 | . 198 | . 188 | . 179 | . 170 | . 161 | . 153 | . 146 | . 138 |
| $-10$ | . 355 | . 339 | . 323 | . 308 | . 293 | . 280 | . 266 | . 254 | . 242 | . 230 |
| -0 | . 563 | . 540 | . 517 | . 492 | . 469 | . 448 | . 428 | . 408 | . 390 | . 372 |
| $+0$ | . 563 | . 587 | . 614 | . 642 | . 671 | . 701 | . 732 | . 768 | . 799 | . 834 |
| +10 | . 870 | . 908 | . 947 | . 988 | 1.030 | 1.074 | 1.119 | 1.166 | 1.215 | 1.265 |
| +20 | 1.318 | 1.375 | 1.431 | 1.488 | 1.548 | 1.612 | 1.676 | 1.746 | 1.815 | 1.886 |
| $+30$ | 1.961 | 2.038 | 2.118 | 2.200 | 2.285 | 2.375 | 2.466 | 2.558 | 2.656 | 2.755 |
| $+40$ | 2.862 | 2.970 | 3.081 | 3.195 | 3.315 | 3.438 | 3.563 | 3.691 | 3.822 | 3.965 |
| $+50$ | 4.105 | 4.256 | 4.410 | 4.565 | 4.722 | 4.890 | 5.060 | 5.235 | 5.420 | 5.608 |
| $+60$ | 5.805 | 6.000 | 6.195 | 6.410 | 6.628 | 6.855 | 7.080 | 7.317 | 7.560 | 7.810 |
| +70 | 8.060 | 8.325 | 8.600 | 8.880 | 9.165 | 9.460 | 9.765 | 10.075 | 10.390 | 10.720 |
| +80 | 11.06 | 11.40 | 11.76 | 12.12 | 12.50 | 12.87 | 13.27 | 13.70 | 14.09 | 14.52 |
| +90 | 14.96 | 15.41 | 15.98 | 16.34 | 16.84 | 17.32 | 17.82 | 18.34 | 18.90 | 19.39 |
| +100 | 19.96 | 20.55 | 21.15 | 21.75 | 22.35 | 23.05 | 23.65 | 24.32 | 24.98 | 25.68 |
| +110 | 26.35 | 27.12 | 27.90 | 28.62 | 29.40 | 30.20 | 31.00 | 31.85 | 32.68 | 33.55 |

## TABLE 638.-RELATIVE HUMIDITY FOR VARIOUS PRESSURES AND DRY-BULB TEMPERATURES

Vertical argument is the observed vapor pressure which may be computed from the wet-bulb and dry-bulb readings through Tables 634 or 640 . The horizontal argument is the observed air temperature (dry-bulb reading).

| Vapor pressure mmHg | Air temperatures, dry bulb, ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | -1 | -2 | -3 | -4 | -5 | -6 | -7 | -8 | -9 | -10 | -11 | -12 |  |  |  | 20 |
| . 25 | 6 | 7 | 7 | 8 | 8 | 9 | 10 | 10 | 11 | 13 | 15 | 15 | 15 | 16 | 17 | 18 | 28 |
| . 50 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 21 | 23 | 26 | 28 | 29 | 31 | 34 | 37 | 55 |
| . 75 | 17 | 19 | 20 | 22 | 24 | 25 | 27 | 29 | 32 | 34 | 37 | 40 | 43 | 46 | 50 | 54 | 81 |
| 1.00 | 23 | 25 | 27 | 29 | 32 | 34 | 36 | 39 | 42 | 45 | 49 | 53 | 57 | 61 | 67 | 72 |  |
| 1.25 | 29 | 31 | 33 | 36 | 39 | 42 | 45 | 48 | 52 | 56 | 60 | 65 | 70 | 76 | 82 | 87 |  |
| 1.50 | 35 | 37 | 40 | 43 | 46 | 49 | 53 | 57 | 61 | 67 | 71 | 77 | 83 | 90 | 97 |  |  |
| 1.75 | 40 | 43 | 46 | 48 | 53 | 57 | 62 | 66 | 71 | 77 | 82 | 87 | 92 | 98 |  |  |  |
| 2.00 | 45 | 48 | 52 | 56 | 60 | 65 | 70 | 75 | 81 | 87 | 94 | 97 |  |  |  |  |  |
| 2.25 | 51 | 54 | 59 | 63 | 68 | 73 | 79 | 84 | 91 | 98 |  |  | mmHg |  |  | -2 | $-3^{\circ}$ |
| 2.50 | 56 | 60 | 65 | 70 | 75 | 81 | 88 | 94 | 100 |  |  |  | 3.50 | 78 | 84 | 90 | 97 |
| 2.75 | 61 | 66 | 71 | 76 | 81 | 87 | 94 |  |  |  |  |  | 3.75 | 84 | 90 | 96 |  |
| 3.00 | 67 | 72 | 78 | 83 | 88 | 94 | 99 |  | . | . | . |  | 4.00 | 90 | 96 |  |  |
| 3.25 | 72 | 78 | 84 | 90 | 96 | . | . |  |  |  | . |  | 4.25 | 96 |  |  |  |
| 3.50 | 78 | 84 | 90 | 97 | . | . | . | $\cdots$ | $\cdots$ | .. | . | .. | 4.50 | 100 | . | . |  |


| $\begin{aligned} & \text { Vapor } \\ & \text { pressure } \\ & \mathrm{mmHg} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| . 5 | 12 | 11 | 11 | 10 | 9 | 9 | 8 | 8 | 7 | 7 | 6 | 6 | 6 | 5 | 5 | 5 | 4 | 4 | 4 | 3 | 3 |
| 1.0 | 24 | 23 | 21 | 20 | 18 | 17 | 16 | 15 | 14 | 13 | 13 | 12 | 11 | 10 | 10 | 9 | 9 | 8 | 8 | 7 | 7 |
| 1.5 | 35 | 33 | 31 | 29 | 27 | 25 | 23 | 21 | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 11 | 10 | 10 |
| 2.0 | 46 | 43 | 40 | 37 | 35 | 32 | 30 | 28 | 27 | 25 | 23 | 22 | 21 | 20 | 18 | 17 | 16 | 15 | 14 | 13 | 12 |
| 2.5 | 56 | 52 | 48 | 45 | 42 | 39 | 36 | 34 | 32 | 30 | 28 | 26 | 25 | 23 | 22 | 21 | 19 | 18 | 17 | 16 | 15 |
| 3.0 | 67 | 63 | 58 | 54 | 50 | 47 | 44 | 41 | 38 | 36 | 34 | 32 | 30 | 28 | 26 | 25 | 23 | 22 | 20 | 19 | 18 |
| 3.5 | 78 | 73 | 68 | 63 | 59 | 55 | 52 | 48 | 45 | 43 | 40 | 38 | 35 | 33 | 31 | 29 | 28 | 26 | 24 | 23 | 22 |
| 4.0 | 91 | 85 | 79 | 74 | 69 | 65 | 61 | 57 | 53 | 50 | 47 | 44 | 41 | 39 | 37 | 35 | 32 | 30 | 29 | 27 | 25 |
| 4.5 | 99 | 93 | 87 | 81 | 76 | 71 | 67 | 62 | 58 | 55 | 52 | 49 | 46 | 43 | 40 | 38 | 36 | 33 | 31 | 29 | 28 |
| 5.0 |  |  | 95 | 89 | 83 | 78 | 73 | 68 | 64 | 60 | 56 | 53 | 50 | 47 | 44 | 41 | 39 | 36 | 34 | 32 | 31 |
| 5.5 |  |  |  | 96 | S1 | 86 | 81 | 75 | 70 | 66 | 62 | 58 | 55 | 51 | 48 | 45 | 42 | 40 | 37 | 35 | 33 |
| 6.0 |  |  |  |  | 100 | 94 | 88 | 82 | 76 | 72 | 68 | 64 | 60 | 56 | 53 | 50 | 46 | 43 | 40 | 38 | 36 |
| 6.5 |  |  |  |  | $\ldots$ | 99 | 93 | 89 | 83 | 78 | 72 | 68 | 64 | 60 | 56 | 52 | 49 | 46 | 44 | 41 | 39 |
| 7.0 | $\cdots$ |  |  |  |  |  | 200 | 94 | 88 | 82 | 77 | 72 | 68 | 64 | 60 | 56 | 52 | 49 | 47 | 44 | 42 |
| 7.5 | .. | $\cdots$ | . | . | .. | . | . | 100 | 94 | 88 | 83 | 77 | 73 | 68 | 65 | 61 | 57 | 54 | 51 | 48 | 46 |
| 8.0 |  |  |  | . | . | . |  | . | 100 | 94 | 88 | 83 | 77 | 73 | 68 | 65 | 61 | 57 | 54 | 51 | 48 |
| 8.5 |  |  |  |  |  |  |  |  |  | 98 | 92 | 86 | 81 | 76 | 72 | 68 | 63 | 60 | 57 | 53 | 51 |
| 9.0 |  |  |  |  |  |  |  |  |  |  | 97 | 91 | 86 | 81 | 76 | 72 | 67 | 64 | 60 | 56 | 53 |
| 9.5 |  |  |  |  |  |  |  |  |  |  |  | 97 | 91 | 85 | 80 | 75 | 71 | 67 | 63 | 59 | 56 |
| 10.0 |  |  |  |  |  |  |  |  |  |  |  |  | 95 | 89 | 84 | 7 | 7 | 70 | 66 | 62 | 59 |
| 11.0 |  |  |  |  |  |  |  |  |  |  |  |  |  | 96 | 92 | 87 | 82 | 77 | 72 | 67 | 64 |
| 12.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 94 | 89 | 84 | 79 | 74 | 70 |
| 13.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 96 | 90 | 85 | 80 | 76 |
| 14.0 |  |  |  | . |  |  |  |  |  |  |  |  |  |  |  |  |  | 98 | 93 | 88 | 84 |
| 15.0 |  |  |  | . | . | . |  |  |  |  |  |  | $\cdots$ | . |  |  | . |  | 97 |  | 86 |
| 16.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 17.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Vapor |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 |
| 1 | 7 | 6 | 6 | 6 | 5 | 5 | 5 | 5 | 4 | 4 | 4 | 4 | 3 | 3 | 3 | 3 | 3 | 2 | 2 | 2 | 2 |
| 2 | 12 | 11 | 11 | 10 | 10 | 9 | 9 | 8 | 8 | 7 | 7 | 7 | 6 | 6 | 6 | 5 | 5 | 5 | 5 | 4 |  |
| 3 | 18 | 17 | 16 | 15 | 15 | 14 | 13 | 12 | 12 | 11 | 11 | 10 | 9 | 9 | 8 | 8 | 7 | 7 | 7 | 6 | 6 |
| 4 | 25 | 23 | 22 | 20 | 19 | 18 | 17 | 16 | 15 | 15 | 14 | 13 | 12 | 12 | 11 | 11 | 10 | 10 | 9 | 9 | 8 |
| 5 | 30 | 28 | 27 | 25 | 24 | 23 | 22 | 20 | 19 | 18 | 17 | 16 | 15 | 15 | 14 | 14 | 13 | 12 | 11 | 11 | 10 |
| 6 | 36 | 34 | 32 | 30 | 29 | 27 | 26 | 24 | 23 | 21 | 20 | 19 | 18 | 17 | 17 | 16 | 15 | 14 | 13 | 12 | 12 |
| 7 | 42 | 39 | 37 | 35 | 34 | 32 | 30 | 28 | 26 | 25 | 23 | 22 | 21 | 20 | 19 | 18 | 17 | 16 | 16 | 15 | 14 |
| 8 | 48 | 45 | 42 | 40 | 38 | 36 | 34 | 32 | 30 | 29 | 27 | 26 | 24 | 23 | 22 | 21 | 20 | 19 | 18 | 17 |  |

(continucd)

TABLE 638.-RELATIVE HUMIDITY FOR VARIOUS PRESSURES AND DRY-BULB TEMPERATURES (continued)

| $\begin{gathered} \text { Vapor } \\ \text { pressure } \\ \text { mmHg } \end{gathered}$ | Air temperatures, dry bulb, ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 233 | 3334 | 35 | 36 | 37 | 38 | 3940 | 40 |
| 9 | 53 | 50 | 47 | 44 | 41 | 39 | 37 | 35 | 33 | 31 | 29 | 27 | 26 | 25 | 524 | 23 | 22 | 21 | 20 | 1918 | 18 |
| 10 | 59 | 56 | 52 | 50 | 47 | 44 | 42 | 40 | 37 | 35 | 34 | 32 | 30 | 20 28 | 827 | 26 | 24 | 23 | 22 | 2120 | 20 |
| 11 | 64 | 61 | 57 | 53 | 50 | 48 | 45 | 43 | 41 | 38 | 36 | 35 | 33 | 331 | 129 | 28 | 26 | 25 | 24 | 2322 | 2 |
| 12 | 70 | 66 | 62 | 59 | 56 | 53 | 50 | 47 | 44 | 42 | 40 | 38 | 36 | 34 | 3432 | 31 | 29 | 28 | 26 | 2524 | 24 |
| 13 | 75 | 71 | 67 | 63 | 60 | 57 | 53 | 50 | 48 | 45 | 43 | 31 | 38 | 86 | 3635 | 33 | 32 | 30 | 28 | $27 \quad 26$ | 6 |
| 14 | 81 | 76 | 72 | 68 | 64 | 61 | 57 | 54 | 51 | 49 | 46 | 44 | 41 | 139 | 3937 | 35 | 33 | 32 | 30 | 2927 | 27 |
| 15 | 86 | 82 | 77 | 72 | 68 | 65 | 61 | 56 | 54 | 52 | 49 | 46 | 44 | 442 | 240 | 38 | 36 | 34 | 32 | 3129 | 29 |
| 16 | 92 | 87 | 82 | 77 | 73 | 69 | 65 | 62 | 58 | 55 | 52 | 249 | 47 | 75 | 542 | 40 | 38 | 36 | 34 | 3331 | 31 |
| 17 |  | 92 | 86 | 82 | 77 | 73 | 69 | 65 | 62 | 58 | 55 | 52 | 49 | 47 | 745 | 42 | 40 | 38 | 36 | 3433 | 33 |
| 18 | $\ldots$ | 100 | 91 | 86 | 82 | 77 | 73 | 69 | 65 | 62 | 58 | 55 | 52 | 250 | 047 | 45 | 42 | 40 | 38 | $36 \quad 35$ | 35 |
| 19 |  | . | 99 | 93 | 86 | 81 | 77 | 73 | 69 | 65 | 61 | 158 | 55 | 52 | 250 | 47 | 45 | 42 | 40 | 3836 | 36 |
| 20 |  |  |  | 96 | 90 | 85 | 80 | 76 | 72 | 68 | 65 | 51 | 58 | 85 | 55 | 50 | 47 | 45 | 42 | 4038 | 38 |
| 21 |  |  |  | 99 | 94 | 89 | 84 | 79 | 75 | 72 | 68 |  | 61 | 158 | 585 | 52 | 49 | 47 | 44 | 4240 |  |
| 22 |  |  |  |  | 98 | 93 | 88 | 83 | 79 | 75 | 71 | 167 | 63 | 360 | 057 | 54 | 51 | 49 | 46 | 4442 | 42 |
| 23 |  |  |  |  |  | 97 | 92 | 87 | 82 | 78 | 74 | 470 | 66 | 66 | 259 | 57 | 54 | 51 | 48 | 4644 | 44 |
| 24 |  |  |  |  |  |  | 96 | 90 | 85 | 81 | 77 | 73 | 69 | 65 | 65 | 59 | 56 | 53 | 50 | 4846 | 46 |
| 25 |  |  |  |  |  |  | 100 | - 94 | 89 | 84 | 79 | 975 | 71 | 168 | 68 | 61 | 58 | 55 | 51 | 5048 |  |
| 26 |  |  | . | . |  |  |  | 97 | 92 | 87 | 83 | 378 | 74 | 470 | 067 | 63 | 60 | 57 | 54 | 5249 |  |
| 27 |  |  |  |  |  |  |  |  | 96 | 91 | 86 | 82 | 78 | 873 | 369 | 65 | 62 | 59 | 56 | 5351 | 51 |
| 28 |  |  |  |  |  |  |  |  | 99 | 94 | 89 | 85 | 82 | 277 | 771 | 68 | 64 | 61 | 58 | 5553 | 53 |
| 29 |  |  |  |  |  |  |  |  |  | 97 | 92 | 87 | 83 | 378 | 874 | 70 |  | 63 | 60 | 5754 | 54 |
| 30 |  |  |  |  |  |  |  | . |  |  | 95 | 90 | 85 | 581 | 8177 | 73 | 70 | 66 | 62 | 5956 |  |
| 31 |  |  |  |  |  |  |  | . | . |  | 98 | 83 | 88 | 883 | 8379 | 75 | 71 | 68 | 64 | 6158 | 58 |
| 32 |  |  |  |  |  | . |  |  |  | . |  | 95 | 90 | 086 | 8681 | 77 | 73 | 69 | 66 | 6360 |  |
| 33 |  | . | .. |  |  |  |  |  |  | . | .. | 98 | 95 | 589 | 8985 | 80 | 76 | 72 | 69 | 6562 |  |
| 34 |  | . | . |  |  |  | . | . .. | .. | . | .. |  | 98 | 893 | 388 | 84 |  |  | 72 | 6865 |  |
| 35 |  | . | . | . |  |  | . | . . | .. | . | .. | . .. | 100 | - 95 | 99 | 85 | 81 |  | 73 | 6966 |  |
| 36 |  |  |  |  |  |  | . | - | . | . | - | . .. |  | 97 | 791 | 86 | 82 | 78 | 74 | 7067 |  |
| 37 |  | ... |  |  |  |  |  | . |  | . | -. |  |  | 98 | 8894 | 89 | 84 | 80 | 76 | 7269 |  |
| 38 |  | .. |  |  |  |  |  | $\cdots$ | . | . | . | . . |  | . .. | 96 | 91 | 86 | 82 | 78 | 7470 |  |
| 39 |  | . |  |  | . |  | . | . . | . . | . | . | . . |  |  | 98 | 93 | 88 | 84 | 80 | 7672 |  |
| 40 |  |  | . |  |  |  |  | . | . . | . | . | . . |  |  | 100 | 95 | 90 | 86 | 82 | 7874 |  |
| 41 |  |  |  |  |  |  |  | . | . | . |  | . . |  |  | . .. | 97 | 92 | 88 | 83 | 8076 |  |
| 42 |  |  |  |  |  |  |  |  | . | . |  | . . | . | . . | . $\cdot$ |  |  | 90 | 85 | 8177 |  |
| 43 |  |  |  |  |  |  |  | . $\cdot$ | . | . |  | - . | . | . .. | . . |  |  | 92 |  | 83 85 81 |  |
| 44 |  |  |  | . | .. |  |  | . . | . . | . | . | . . |  |  | . .. |  | 99 |  | 90 | 8581 |  |
| 45 |  |  | . | . |  |  |  | . | $\cdots$ | $\cdots$ | $\cdots$ | . $\cdot$ | $\cdots$ | - . | . |  |  | 96 |  |  |  |
| 46 |  |  |  |  |  |  |  | . | . |  |  |  |  |  | . .. |  |  | 98 |  |  |  |
| 47 |  |  |  |  |  |  |  |  | . | $\cdots$ |  | . - |  |  | . .. |  |  |  | 95 |  |  |
| 48 |  |  |  |  |  |  |  | . | .. | $\cdots$ |  | . . |  | - . | . ${ }^{\text {. }}$ | . |  |  | 99 | $\begin{array}{ll} 92 & 88 \\ 94 & 89 \end{array}$ |  |
| 49 |  |  | . |  |  |  |  |  |  |  |  |  |  | . .. | . .. |  |  |  |  | $96 \quad 91$ |  |
| 50 |  | . | . |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 9892 |  |
| 52 |  |  |  |  |  |  |  |  | .- | . |  | . .. |  |  | . .. | . | . |  |  | 9994 |  |
| 53 |  |  | . |  |  |  |  | . | . | .. |  | . . |  | . .. | . .. |  |  |  |  |  |  |
| 54 |  |  | . |  |  |  |  |  | . | . |  | . .. |  |  | . . |  | . |  |  |  | 98 |
| 55 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | . |  |  |  |  |  | 100 |
| $\begin{gathered} \text { Vapor } \\ \text { pressure } \\ \mathrm{mmHg} \end{gathered}-$ | Air temperatures, dry bulb, ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 253 | 5354 | 55 | 56 | 57 | 58 | 5960 | 60 |
| 5 | 10 |  | 9 | 9 | 8 | 8 |  |  | 7 | ' | 6 | 66 | 6 | 66 | 65 | 5 | 5 | 5 | 5 | 44 | 4 |
| 10 | 20 | 19 | 18 | 17 | 16 | 15 | 14 |  | 13 | 13 | 12 | 12 | 11 | 111 | 1110 | 10 | 9 | 9 | - | 87 | 7 |
| 15 | 29 | 28 | 26 | 25 | 24 | 23 | 22 | 21 | 20 | 19 | 18 | 17 | 16 | 16 | 1615 | 14 | 14 | 13 | 12 | $12 \quad 11$ | 11 |
| 20 | 38 | 37 | 35 | 33 | 31 | 30 | 29 | 27 | 26 | 25 | 24 | 423 | 22 | 220 | 2019 | 18 | 18 | 17 | 16 | 1515 | 15 |
| 25 | 47 | 45 | 43 | 41 | 39 | 37 | 35 | 33 | 32 | 31 | 29 | 528 | 27 | 25 | 24 | 23 | 22 | 21 | 20 | 1919 | 19 |
| 30 | 56 | 53 | 51 | 49 | 46 | 44 | 42 | 40 | 38 | 36 | 35 | 533 | 32 | 2730 | 3029 | 28 | 27 | 25 | 24 | $22 \quad 21$ | 21 |
| 35 | 66 | 62 | 59 | 57 | 53 | 51 | 48 | 46 | 44 | 42 | 40 | 038 | 37 | 735 | 3533 | 32 | 30 |  |  | 26 |  |
| 40 | 74 | 70 | 67 | 64 | 60 | 58 | 55 | 52 | 50 | 48 | 45 | 543 | 41 | 139 | 3938 | 36 | 35 | 33 | 32 | 3028 |  |
| 45 | 82 | 78 | 75 | 71 | 68 | 65 | 61 | 58 | 56 | 53 | 51 | 148 | 46 | 644 | 44 | 40 | 39 | 37 | 35 | $34 \quad 32$ |  |
| 50 |  | 87 | 82 | 79 | 75 | 71 | 68 | 65 | 62 | 59 | 56 | 53 | 51 | 149 | 4947 | 45 | 43 | 41 | 39 | 3735 |  |

(continued)

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## TABLE 638.-RELATIVE HUMIDITY FOR VARIOUS PRESSURES AND DRY-BULB TEMPERATURES (concluded)

| $\underset{\substack{\text { Vapors } \\ \text { presure }}}{ }$ | Air temperatures, dry bulb, ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 40 | 41 | 42 | 43 | 44 | 45 |  | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 |
| 55 | 100 | 95 | 90 | 86 | 82 | 78 | 74 | 71 | 68 | 65 | 62 | 59 | 56 | 54 | 51 | 49 | 47 | 45 | 43 | 4139 |
| 60 |  |  | 97 | 93 | 88 | 84 | 80 | 77 | 73 | 70 | 67 | 64 | 61 | 58 | 55 | 53 | 51 | 49 | 47 | 4543 |
| 65 |  |  |  |  | 96 | 91 | 87 | 83 | 79 | 75 | 72 | 69 | 65 | 62 | 60 | 57 | 55 | 52 | 50 | 4846 |
| 70 |  |  |  |  |  |  | 93 | 89 | 85 | 81 | 77 | 74 | 70 | 67 | 64 | 461 | 59 | 56 | 54 | 5249 |
| 75 |  |  |  | . |  |  | 100 | 95 | 91 | 86 | 83 | 79 | 75 | 72 | 69 | 66 | 63 | 60 |  | 5553 |
| 80 |  |  |  |  |  |  |  |  | 96 | 91 | 87 | 83 | 80 | 76 | 73 | 369 | 66 | 63 | 61 | 5856 |
| 85 |  |  |  |  |  |  |  | $\cdots$ |  | 97 | 92 | 88 | 84 | 81 | 77 | 74 | 70 | 67 | 64 | 6259 |
| 90 |  |  |  |  |  |  |  | .- |  |  | 96 | 92 | 89 | 85 | 81 | 178 | 74 | 71 | 68 | $65 \quad 62$ |
| 95 |  |  | 5 | 58 | 59 | 0 |  |  |  |  |  | 97 | 93 | 89 | 85 | 582 | 78 | 75 | 71 | 6865 |
| 100 |  | 125 | 96 | 92 | 88 | 84 |  |  |  |  |  |  | 99 | 94 | 89 | 986 | 82 | 78 | 75 | 7269 |
| 105 |  | 130 |  | 96 | 92 | 88 |  |  |  |  |  |  |  | 98 | 94 | 490 | 86 | 82 | 78 | 7572 |
| 110 |  | 135 |  | 99 | 95 | 91 |  |  |  |  |  |  |  |  | 98 | 894 | 89 | 85 |  | 7875 |
| 115 |  | 140 |  |  | 99 | 94 |  |  |  |  |  |  |  |  |  | 97 | 93 | 89 | 85 | 8278 |
| 125 |  | 145 |  |  |  | 97 |  |  |  |  |  |  |  |  |  |  | 97 |  |  | 8582 |
| 125 |  | 150 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 8884 |

## TABLE 639.-RELATIVE HUMIDITY, WET AND DRY THERMOMETERS

This table gives the relative humidity direct from the difference between the reading of the dry ( $t^{\circ} \mathrm{C}$ ) and the wet ( $t_{1}{ }^{\circ} \mathrm{C}$ ) thermometer. It is computed for a barometer reading of 1000 mb . The wet thermometers should be ventilated about 3 meters per second. Changes due to different pressure can be calculated from the data given in Tables 634 and 640.

Temperatures of dry thermometer, $t^{\circ}$

| $\left(t^{\circ}-t_{1}{ }^{\circ}\right)$ | -15 | -10 | -5 | 0 | 5 | $\left(t^{\circ}-t_{1}{ }^{\circ}\right)$ | 10 | 15 | 20 | 25 | 30 | 35 | 40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 2 | 92 | 94 | 95 | 96 | 97 | . 5 | 94 | 95 | 96 | 96 | 97 | 97 | 97 |
| . 4 | 84 | 89 | 91 | 92 | 95 | 1.0 | 89 | 90 | 92 | 93 | 93 | 94 | 94 |
| . 5 | 80 | 86 | 89 | 91 | 93 | 1.5 | 83 | 86 | 88 | 89 | 90 | 91 | 91 |
| . 6 | 76 | 82 | 88 | 90 | 92 | 2.0 | 77 | 81 | 83 | 85 | 86 | 88 | 89 |
| . 8 | 68 | 77 | 83 | 87 | 89 | 2.5 | 72 | 76 | 80 | 82 | 83 | 85 | 86 |
| 1.0 | 60 | 71 | 78 | 83 | 86 | 3.0 | 67 | 72 | 75 | 78 | 80 | 82 | 83 |
| 1.2 | 52 | 65 | 74 | 80 | 84 | 3.5 | 61 | 67 | 72 | 75 | 77 | 79 | 81 |
| 1.4 | 43 | 59 | 72 | 76 | 81 | 4.0 | 56 | 63 | 68 | 71 | 74 | 76 | 78 |
| 1.5 | 39 | 56 | 67 | 74 | 80 | 4.5 | 51 | 58 | 64 | 68 | 71 | 73 | 76 |
| 1.6 | 35 | 53 | 65 | 73 | 78 | 5.0 | 46 | 54 | 60 | 65 | 68 | 71 | 73 |
| 1.8 | 27 | 49 | 61 | 69 | 75 | 6 | 36 | 46 | 53 | 58 | 62 | 65 | 68 |
| 2.0 | 18 | 41 | 56 | 65 | 73 | 7 | 26 | 38 | 46 | 52 | 57 | 60 | 63 |
| 2.5 | . | 27 | 46 | 58 | 66 | 8 | 15 | 29 | 39 | 46 | 51 | 55 | 59 |
| 3.0 | . | 10 | 35 | 50 | 60 | 9 | 5 | 21 | 32 | 40 | 46 | 51 | 54 |
| 3.5 | . | . | 24 | 41 | 53 | 10 | . | 13 | 25 | 34 | 41 | 46 | 50 |
| 4.0 |  | . | 12 | 33 | 47 | 11 | . | 5 | 19 | 30 | 36 | 42 | 46 |
| 4.5 |  | $\cdots$ |  | 25 | 40 | 12 |  | . | 13 | 23 | 31 | 37 | 43 |
| 5 |  | $\cdots$ | $\cdots$ | 16 | 34 | 13 |  | $\cdots$ | . | 18 | 28 | 33 | 38 |
| 6 | . | $\cdots$ | $\cdots$ | , | 21 | 14 | $\because$ | $\cdots$ | $\cdots$ | 13 | 25 | 29 | 34 |
| 7 | $\ldots$ | $\ldots$ | $\ldots$ |  | 8 | 15 | $\ldots$ | $\ldots$ | $\cdots$ | 8 | 19 | 25 | 31 |
|  |  |  |  |  |  | 16 |  |  | $\ldots$ |  | 13 | 21 | 28 |
|  |  |  |  |  |  | 17 |  | $\cdots$ | $\cdots$ | . | 9 | 18 | 24 |
|  |  |  |  |  |  | 18 | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 5 | 14 | 21 |
|  |  |  |  |  |  | 19 | $\ldots$ | $\cdots$ | $\cdots$ | . | 3 | 10 | 18 |
|  |  |  |  |  |  | 20 | . |  | . | . | 2 | 7 | 14 |
|  |  |  |  |  |  | 22 |  |  | . | . | .. |  | 11 |
|  |  |  |  |  |  | 24 | . | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | . | 9 |

TABLE 640.-PRESSURE OF AQUEOUS VAPOR IN THE ATMOSPHERE: SEA LEVEL

This table gives the vapor pressure corresponding to various values of the difference $t-t_{1}$ between the readings of dry-bulb and wet-bulb thermometers and the temperature $t_{1}$ of the wet-bulb thermometer. The difference $t-t_{1}$ is given by two-degree steps in the top line, and $t_{1}$ by degrees in the first column. Temperatures in Centigrade degrees, vapor pressures in millimeters of mercury are used throughout the table. The table was calculated for barometric pressure $B$ equal to 76 cmHg . A correction is given for each centimeter at the top of the columns. Ventilating velocity of wet thermometer about 3 meters per second.

| $t_{1}$ | $\begin{aligned} & t-t_{1} \\ & =0^{\circ} \end{aligned}$ | $2^{\circ}$ | $4^{\circ}$ | $6^{\circ}$ | $8^{\circ}$ | $10^{\circ}$ | $12^{\circ}$ | $14^{\circ}$ | $16^{\circ}$ | $18^{\circ}$ | $20^{\circ}$ | Differ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Corrections for $B$ per $\mathrm{cmH}_{8}$ |  | . 013 | . 026 | . 040 | 053 | . 966 | . 079 | . 09 | . 106 | . 119 | . 132 | $\begin{aligned} & \text { ence } \\ & \text { for } \\ & 0.1^{\circ} \text { in } \\ & t-t_{1} \end{aligned}$ |
| -10 | 1.96 | . 97 |  | - | - |  |  |  |  |  |  | . 050 |
| -9 | 2.14 | 1.15 | . 16 |  |  |  |  | Exar | nple |  |  | . 050 |
| -8 | 2.34 | 1.35 | . 35 |  |  |  |  |  |  |  |  | 050 |
| -7 | 255 | 1.56 | . 66 |  |  |  | $=$ | 10.0 |  | 74.5 | Hg | . 050 |
| - 6 | 2.78 | 1.78 | . 79 |  |  | From | table: |  | $12 \times$ | $0.050=$ |  | . 050 |
| - 5 | 3.02 | 2.03 | 1.03 | . 03 |  |  | , $1.5 \times$ |  |  |  |  | . 050 |
| -4 -3 | 3.29 3.58 | 2.29 | 1.29 1.58 | . 29 |  | Henc |  |  |  |  | 5.64 | . 050 |
| -2 | 3.89 | 2.89 | 1.89 | . 88 | - | - | - | - | - | - | - | . 050 |
| -1 | 4.22 | 3.22 | 2.22 | 1.21 | . 21 | - | - |  | - |  |  | . 050 |
| 0 | 4.58 | 3.58 | 2.57 | 1.57 | . 57 | - | - | - | - |  |  | . 050 |
| 1 | 4.92 | 3.92 | 2.92 | 1.91 | . 91 | - |  |  |  |  |  | . 050 |
| 2 | 5.29 | 4.29 | 3.28 | 2.27 | 1.27 | 26 | - |  |  |  |  | . 050 |
| 3 | 5.68 | 4.68 | 3.67 | 2.66 | 1.66 | . 65 | - | - | - |  |  | . 050 |
| 4 | 6.10 | 5.09 | 4.08 | 3.07 | 2.07 | 1.06 | . 05 | - | - | - |  | . 050 |
| 5 | 6.54 | 5.53 | 4.52 | 3.51 | 2.51 | 1.50 | . 49 | - |  | - |  | . 050 |
| 6 | 7.01 | 6.00 | 4.99 | 3.98 | 2.97 | 1.96 | . 95 | - | - |  |  | . 050 |
| 7 | 7.51 | 6.50 | 5.49 | 4.48 | 3.47 | 2.46 | 1.45 | . 43 | - |  |  | . 050 |
| 8 | 8.04 | 7.03 | 6.02 | 5.01 | 400 | 2.98 | 1.97 | 96 | - |  |  | . 050 |
| 9 | 8.61 | 7.60 | 6.58 | 5.57 | 4.56 | 3.54 | 2.53 | 1.52 | . 50 | - | - | . 050 |
| 10 | 9.21 | 8.20 | 7.18 | 6.17 | 5.15 | 4.14 | 3.12 | 2.11 | 1.09 | . 08 | - | . 050 |
| 11 | 9.85 | 8.83 | 7.81 | 6.80 | 5.78 | 4.77 | 3.75 | 2.73 | 1.72 | . 70 |  | . 051 |
| 12 | 10.52 | 9.50 | 8.49 | 7.47 | 6.45 | 5.44 | 4.42 | 3.40 | 2.38 | 1.37 | . 35 | . 051 |
| 13 | 11.24 | 10.22 | 9.20 | 8.18 | 7.16 | 6.14 | 5.13 | 4.11 | 3.09 | 2.07 | 1.05 | . 051 |
| 14 | 11.99 | 10.97 | 9.95 | 8.93 | 7.91 | 6.90 | 5.88 | 4.86 | 3.84 | 2.82 | 1.80 | . 051 |
| 15 | 12.79 | 11.77 | 10.75 | 9.73 | 8.71 | 7.69 | 6.67 | 5.65 | 4.63 | 3.61 | 2.59 | . 051 |
| 16 | 13.64 | 12.62 | 11.60 | 10.58 | 9.95 | 8.53 | 7.51 | 6.49 | 5.47 | 4.45 | 3.43 | . 051 |
| 17 | 14.54 | 13.52 | 12.49 | 11.47 | 10.45 | 9.42 | 8.40 | 7.38 | 6.36 | 5.33 | 4.31 | . 051 |
| 18 | 15.49 | 14.46 | 13.44 | 12.42 | 11.39 | 10.37 | 9.34 | 8.32 | 7.30 | 6.27 | 5.25 | . 051 |
| 19 | 16.49 | 15.46 | 14.44 | 13.41 | 12.39 | 11.36 | 10.34 | 9.31 | 8.29 | 7.26 | 6.24 | . 051 |
| 20 | 17.55 | 16.52 | 15.50 | 14.47 | 13.44 | 12.42 | 11.39 | 10.36 | 9.34 | 8.31 | 7.29 | . 051 |
| 21 | 18.66 | 17.64 | 16.61 | 15.58 | 14.56 | 13.53 | 12.50 | 11.47 | 10.45 | 9.42 | 8.39 | . 051 |
| 22 | 19.84 | 18.82 | 17.79 | 16.76 | 15.73 | 14.70 | 13.67 | 12.64 | 11.62 | 10.59 | 10.57 | . 051 |
| 23 | 21.09 | 20.06 | 19.03 | 18.00 | 16.97 | 15.94 | 14.91 | 13.88 | 12.85 | 11.82 | 10.79 | . 051 |
| 24 | 22.40 | 21.37 | 20.34 | 19.31 | 18.27 | 17.24 | 16.21 | 15.18 | 14.15 | 13.12 | 12.09 | . 051 |
| 25 | 23.78 | 22.75 | 21.71 | 20.68 | 19.65 | 18.62 | 17.59 | 16.56 | 15.52 | 14.49 | 13.46 | . 052 |
| 26 | 25.24 | 24.20 | 23.17 | 22.14 | 21.10 | 20.07 | 19.04 | 18.00 | 16.97 | 15.94 | 14.90 | . 052 |
| 27 | 26.77 | 25.73 | 24.70 | 23.66 | 22.63 | 21.60 | 20.56 | 19.53 | 18.49 | 17.46 | 16.42 | . 052 |
| 28 | 28.38 | 27.34 | 26.31 | 25.27 | 24.24 | 23.20 | 22.17 | 21.13 | 20.10 | 19.06 | 18.02 | . 052 |
| 29 | 30.08 | 29.04 | 28.00 | 26.97 | 25.93 | 24.89 | 23.86 | 22.82 | 21.78 | 20.75 | 19.71 | . 052 |
| 30 | 31.86 | 30.82 | 29.78 | 28.75 | 27.71 | 26.67 | 25.63 | 24.60 | 23.56 | 22.52 | 21.48 | . 052 |
| 31 | 33.74 | 32.70 | 31.66 | 30.62 | 29.58 | 28.54 | 27.50 | 26.46 | 25.42 | 24.38 | 23.34 | . 052 |
| 32 | 35.70 | 34.66 | 33.62 | 32.58 | 31.54 | 30.50 | 29.46 | 28.42 | 27.38 | 26.34 | 25.30 | . 052 |
| 33 | 37.78 | 36.73 | 35.69 | 34.65 | 33.61 | 32.57 | 31.53 | 30.49 | 29.44 | 28.40 | 27.36 | .052 |
| 34 | 39.95 | 38.90 | 37.86 | 36.82 | 35.78 | 34.73 | 33.69 | 32.65 | 31.61 | 30.57 | 29.52 | . 052 |
| 35 | 42.23 | 41.18 | 40.14 | 39.10 | 3805 | 37.01 | 35.97 | 34.92 | 33.88 | 32.83 | 31.79 | . 052 |
| 36 | 44.62 | 43.57 | 42.53 | 41.48 | 40.44 | 39.40 | 38.35 | 37.31 | 36.26 | 35.22 | 34.17 | .052 |
| 37 | 47.13 | 46.08 | 45.04 | 43.99 | 42.94 | 41.90 | 40.85 | 39.81 | 38.76 | 37.71 | 36.67 | . 052 |
| 38 | 49.76 | 48.71 | 47.66 | 46.61 | 45.57 | 44.52 | 43.47 | 42.43 | 41.38 | 40.33 | 39.29 | .052 |
| 39 | 52.51 | 51.46 | 50.41 | 49.37 | 48.32 | 47.27 | 46.22 | 45.17 | 44.12 | 43.08 | 42.03 | . 052 |
| 40 | 55.40 | 54.35 | 53.30 | 52.25 | 51.20 | 50.15 | 49.10 | 48.05 | 47.00 | 45.95 | 44.00 | . 052 |

TABLE 641.-PRESSURE OF COLUMNS OF MERCURY AND WATER
British and metric measures. Correct at $0^{\circ} \mathrm{C}$ for mercury and at $4^{\circ} \mathrm{C}$ for water.

| Metric $\underbrace{\text { measure }}$ |  |  | British measure |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| cmHg | Pressure $\mathrm{g} / \mathrm{cm}^{2}$ | Pressure 1b/in. ${ }^{2}$ | inHg | Pressure <br> $\mathrm{g} / \mathrm{cm}^{2}$ | Pressure 1b/in. ${ }^{2}$ |
| 1 | 13.5954 | . 193367 | 1 | 34.532 | . 491152 |
| 2 | 27.1908 | . 386734 | 2 | 69.065 | . 982304 |
| 3 | 40.7862 | . 580101 | 3 | 103.597 | 1.473457 |
| 4 | 54.3816 | . 773468 | 4 | 138.129 | 1.964609 |
| 5 | 67.9770 | . 966835 | 5 | 172.662 | 2.455761 |
| 6 | 81.5724 | 1.160204 | 6 | 207.194 | 2.946918 |
| 7 | 95.1678 | 1.353566 | 7 | 241.726 | 3.438058 |
| 8 | 108.7632 | 1.546936 | 8 | 276.259 | 3.929286 |
| 9 | 122.3586 | 1.740303 | 9 | 310.791 | 4.420370 |
| 10 | 135.9540 | 1.933670 | 10 | 345.323 | 4.911522 |
| $\begin{gathered} \mathrm{cm}_{2} \text { of } \\ \mathrm{H}_{2} \mathrm{O} \end{gathered}$ | Pressure $\mathrm{g} / \mathrm{cm}^{2}$ | Pressure <br> lb/in. ${ }^{2}$ | $\underset{\mathrm{H}_{2} \mathrm{O}}{\text { Inches of }}$ | Pressure $\mathrm{g} / \mathrm{cm}^{2}$ | Pressure lb/in. ${ }^{2}$ |
| 1 | 1 | . 0142234 | 1 | 2.54 | . 036127 |
| 2 | 2 | . 0284468 | 2 | 5.08 | . 072255 |
| 3 | 3 | . 0426702 | 3 | 7.62 | . 108382 |
| 4 | 4 | . 0568936 | 4 | 10.16 | . 144510 |
| 5 | 5 | . 0711170 | 5 | 12.70 | . 180637 |
| 6 | 6 | . 0853404 | 6 | 15.24 | . 216764 |
| 7 | 7 | . 0995638 | 7 | 17.78 | . 252892 |
| 8 | 8 | . 1137872 | 8 | 20.32 | . 289019 |
| 9 | 9 | . 1280106 | 9 | 22.86 | . 325147 |
| 10 | 10 | . 1422340 | 10 | 25.40 | . 361274 |

107 The tables on the barometer have been adapted from the Smithsonian Meteorological Tables, sixth edition.

TABLE 642.-CORRECTION OF THE BAROMETER FOR CAPILLARITY * Metric measure

| Diameter of tube in mm | Height of meniscus in millimeters |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | . 4 | . 6 | . 8 | 1.0 | 1.2 | 1.4 | 1.6 | 1.8 |
| 4 | 1.1 | 1.7 | 2.1 | 2.4 | 2.6 |  |  |  |
| 5 | . 73 | 1.06 | 1.34 | 1.55 | 1.76 |  |  |  |
| 6 | . 47 | . 71 | . 91 | 1.08 | 1.21 | 1.30 | 1.37 | 1.43 |
| 7 | . 33 | . 48 | . 63 | . 76 | . 86 | . 96 | 1.03 | 1.08 |
| 8 | . 24 | . 35 | . 46 | . 55 | . 63 | . 70 | . 77 | . 82 |
| 9 | . 18 | . 27 | . 35 | . 41 | . 47 | . 53 | . 57 | . 61 |
| 10 | . 12 | . 18 | . 24 | . 30 | . 35 | . 40 | . 44 | . 47 |
| 12 | . 07 | . 10 | . 13 | . 16 | . 20 | . 22 | . 25 | . 27 |
| 14 | . 04 | . 06 | . 08 | . 10 | . 11 | . 13 | . 15 | . 17 |
| 16 | . 02 | . 04 | . 05 | . 06 | . 07 | . 09 | . 10 | . 11 |

* Corrections to be added in millimeters.

TABLE 643.—VOLUME OF MERCURY MENISCUS IN mm ${ }^{3}$

| Height of meniscus | Diameter of tube in mm |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| mm |  |  |  |  |  |  |  |  |  |  |  |
| 1.6 | 157 | 185 | 214 | 245 | 280 | 318 | 356 | 398 | 444 | 492 | 541 |
| 1.8 | 181 | 211 | 244 | 281 | 320 | 362 | 407 | 455 | 507 | 560 | 616 |
| 2.0 | 206 | 240 | 278 | 319 | 362 | 409 | 460 | 513 | 571 | 631 | 694 |
| 2.2 | 233 | 271 | 313 | 358 | 406 | 459 | 515 | 574 | 63, | 704 | 776 |
| 2.4 | 262 | 303 | 350 | 400 | 454 | 511 | 573 | 639 | 708 | 781 | 859 |
| 2.6 | 291 | 338 | 388 | 444 | 503 | 565 | 633 | 706 | 782 | 862 | 948 |

TABLE 644.-CONSTANT a FOR REDUCTION OF BAROMETRIC HEIGHT TO STANDARD TEMPERATURE *

| Brass scale and English measure |  | Brass scale and metric measure |  | Glass scale and metric measure |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Height of barometer in inches | $\begin{gathered} \text { in inches for } \\ \text { temp }{ }^{\circ} \mathrm{F} \end{gathered}$ | Height of barometer in mmHg | $\underset{\substack{a \\ \text { in mm for } \\ \text { temp } \\{ }^{\circ} \mathrm{C}}}{\text { 俍 }}$ | Height of barometer in mmHg | $\begin{gathered} a \\ \text { in mm } \\ \text { temp }{ }^{\circ} \mathrm{C} \mathrm{C} \end{gathered}$ |
| 15.0 | . 00135 | 400 | . 0651 | 50 | . 0086 |
| 16.0 | . 00145 | 410 | . 0668 | 100 | . 0172 |
| 17.0 | . 00154 | 420 | . 0684 | 150 | . 0258 |
| 17.5 | . 00158 | 430 | . 0700 | 200 | . 0345 |
| 18.0 | . 00163 | 440 | . 0716 | 250 | . 0431 |
| 18.5 | . 00167 | 450 | . 0732 | 300 | . 0517 |
| 19.0 | . 00172 | 460 | . 0749 | 350 | . 0603 |
| 19.5 | . 00176 | 470 | . 0765 |  |  |
|  |  | 480 | . 0781 | 400 | . 0689 |
| 20.0 | . 00181 | 490 | . 0797 | 450 | . 0775 |
| 20.5 | . 00185 |  |  | 500 | . 0861 |
| 21.0 | . 00190 | 500 | . 0813 | 520 | . 0895 |
| 21.5 | . 00194 | 510 | . 0830 | 540 | . 0930 |
| 22.0 | . 00199 | 520 | . 0846 | 560 | . 0965 |
| 22.5 | . 00203 | 530 | . 0862 | 580 | . 0999 |
| 23.0 | . 00208 | 540 | . 0878 |  |  |
| 23.5 | . 00212 | 550 | . 0894 | 600 | . 1034 |
|  |  | 560 | . 0911 | 610 | . 1051 |
| 24.0 | . 00217 | 570 | . 0927 | 620 | . 1068 |
| 24.5 | . 00221 | 580 | . 0943 | 630 | . 1085 |
| 25.0 | . 00226 | 590 | . 0959 | 640 | . 1103 |
| 25.5 | . 00231 |  |  | 650 | . 1120 |
| 26.0 | . 00236 | 600 | . 0975 | 660 | . 1137 |
| 26.5 | . 00240 | 610 | . 0992 |  |  |
| 27.0 | . 00245 | 620 | . 1008 | 670 | . 1154 |
| 27.5 | . 00249 | 630 | . 1024 | 680 | . 1172 |
|  |  | 640 | . 1040 | 690 | . 1189 |
| 28.0 | . 00254 | 650 | . 1056 | 700 | . 1206 |
| 28.5 | . 00258 | 660 | . 1073 | 710 | . 1223 |
| 29.0 | . 00263 | 670 | . 1089 | 720 | . 1240 |
| 29.2 | . 00265 | 680 | . 1105 | 730 | . 1258 |
| 29.4 | . 00267 | 690 | . 1121 |  |  |
| 29.6 | . 00268 |  |  | 740 | . 1275 |
| 29.8 | . 00270 | 700 | . 1137 | 750 | . 1292 |
| 30.0 | . 00272 | 710 | . 1154 | 760 | . 1309 |
|  |  | 720 | . 1170 | 770 | . 1327 |
| 30.2 | . 00274 | 730 | . 1186 | 780 | . 1344 |
| 30.4 | . 00276 | 740 | . 1202 | 790 | . 1361 |
| 30.6 | . 00277 | 750 | . 1218 | 800 | . 1378 |
| 30.8 | . 00279 | 760 | . 1235 |  |  |
| 31.0 | . 00281 | 770 | . 1251 | 850 | . 1464 |
| 31.2 | . 00283 | 780 | . 1267 | 900 | . 1551 |
| 31.4 | . 00285 | 790 | . 1283 | 950 | . 1639 |
| 31.6 | . 00287 | 800 | . 1299 | 1000 | . 1723 |

[^246]
## Free-air altitude term. Correction to be subtracted.

The correction to reduce the barometer to sea level is $\left[\left(g_{1}-g\right) / g\right] \times B$ where $B$ is the barometer reading and $g$ and $g_{1}$ the value of gravity at sea level and the place of observation respectively. The following values were computed for free-air values of gravity $g_{1}$ (Table 802). It has been customary to assume for mountain stations that the value of $g_{1}=$ say about $\frac{子}{}{ }^{3}$ the free-air value, but a comparison of modern determinations of $g_{1}$ in this country shows that little reliance can be placed on such an assumption. Where $g_{1}$ is known its value should be used in the above correction term. (See Tables 803-805.) Similarly for the latitude term, see succeeding tables; the true value of $g$ should be used if known; the succeeding tables are based on the theoretical values, Table 802.)

| Height |  | Observed height of barometer in mmHg |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| sea level | $g_{1}-g$ | 400 | 450 | 500 | 550 | 600 | 650 | 700 | 750 | 800 |  |  |
| meters 100 | . 031 | Correction in mmHg to be subtracted for height above sea level |  |  |  |  |  | . 02 | . 02 | . 02 | - | - |
| 200 | . 062 |  |  |  |  |  |  | . 04 | . 05 | . 05 | - |  |
| 300 | . 093 | in first column and barometer read- |  |  |  |  |  | . 07 | . 07 | . 07 |  |  |
| 400 | . 123 | ing in the top line. |  |  |  |  |  | . 09 | . 10 | . 10 | - |  |
| 500 | . 154 |  | - |  | - | - |  | . 11 | . 12 | . 13 | - |  |
| 600 | . 185 | - | - | - | - | - | . 12 | . 13 | . 14 | - | - |  |
| 700 | . 216 | - | - | - | - | - | . 14 | . 15 | . 16 | - | - |  |
| 800 | . 247 |  | - |  |  | - | . 16 | . 18 | . 19 | - | - |  |
| 900 | . 278 | - | - |  |  | - | . 18 | . 20 | . 22 | - |  |  |
| 1000 | . 309 | - | - | - | . 18 | . 19 | . 20 | . 22 | . 24 | - | - |  |
| 1100 | . 339 | - | - | - | . 19 | . 21 | . 22 | . 24 | - | - | - |  |
| 1200 | . 370 | - | - |  | . 21 | . 23 | . 24 | . 26 | - | - | - |  |
| 1300 | . 401 |  |  |  | . 22 | . 24 | . 26 | . 29 | - | - | - |  |
| 1400 | . 432 |  |  |  | . 24 | . 26 | . 28 | . 31 | - | - |  |  |
| 1500 | . 463 | - | - | . 24 | . 26 | . 28 | . 30 | . 33 | - | - | - |  |
| 1600 | . 494 | - | - | . 25 | . 28 | . 30 | . 32 | - | - | - | - |  |
| 1700 | . 525 | - | - | . 27 | . 30 | . 32 | . 34 | - | - | - |  |  |
| 1800 | . 555 | - | - | . 28 | . 31 | . 34 | . 36 | - | - | . 020 | . 0463 | 15000 |
| 1900 | . 586 | - | - | . 30 | . 33 | . 36 | . 39 | - | - | . 019 | . 0447 | 14500 |
| 2000 | . 617 | - | . 28 | . 31 | . 34 | . 38 | . 41 | - | . 021 | . 019 | . 0432 | 14000 |
| 2100 | . 648 | - | . 30 | . 33 | . 36 | . 40 | - | - | . 021 | . 018 | . 0416 | 13500 |
| 2200 | . 679 | - | . 31 | . 35 | . 38 | . 41 | - | - | . 020 | . 017 | . 0401 | 13000 |
| 2300 | . 710 | - | . 32 | . 36 | . 40 | . 43 | - | . 021 | . 019 | . 017 | . 0386 | 12500 |
| 2400 | . 740 |  | . 34 | . 38 | . 42 | . 45 | - | . 021 | . 018 | . 016 | . 0370 | 12000 |
| 2500 | . 771 | . 31 | . 35 | . 39 | . 43 | . 47 |  | . 020 | . 018 | . 015 | . 0355 | 11500 |
| 2600 | 802 | . 33 | . 37 | . 41 | - | - | . 021 | . 019 | . 017 | . 015 | . 0339 | 11000 |
| 2700 | . 833 | . 34 | . 38 | . 42 | - | - | . 020 | . 018 | . 016 | . 014 | . 0324 | 10500 |
| 2800 | . 864 | . 35 | . 40 | . 44 | - | - | . 019 | . 017 | . 015 | . 013 | . 0308 | 10000 |
| 2900 | . 895 | . 36 | . 41 | . 46 | - | . 020 | . 018 | . 016 | . 015 | . 013 | . 0293 | 9500 |
| 3000 | . 926 | . 38 | . 42 | . 47 | - | . 019 | . 017 | . 016 | . 014 | . 012 | . 0278 | 9000 |
| 3100 | . 957 | . 39 | . 44 |  | - | . 018 | . 016 | . 015 | . 013 | - | . 0262 | 8500 |
| 3200 | . 988 | . 40 | . 46 | - | - | . 017 | . 015 | . 014 | . 012 | - | . 0247 | 8000 |
| 3300 | 1.019 | . 42 | . 47 | - | . 017 | . 016 | . 014 | . 013 | - | - | . 0231 | 7500 |
| 3400 | 1.049 | . 43 | . 48 |  | . 016 | . 015 | . 013 | . 012 | - | - | . 0216 | 7000 |
| 3500 | 1.080 | . 44 | . 49 | - | . 015 | . 014 | . 012 | . 011 | - | - | . 0200 | 6500 |
| 3600 | 1.111 | . 45 | - | - | . 014 | . 013 | . 011 | - | - | - | . 0185 | 6000 |
| 3700 | 1.142 | . 46 | - | - | . 013 | . 012 | . 011 | - | - | - | . 0170 | 5500 |
| 3800 | 1.173 | . 48 |  | . 012 | . 011 | . 011 | . 010 | - | - |  | . 0154 | 5000 |
| 3900 | 1.204 | . 49 | - | . 011 | . 010 | . 010 |  | - |  |  | . 0139 | 4500 |
| 4000 | 1.235 | . 50 | - | . 010 | . 009 | . 009 |  | - | - |  | . 0123 | 4000 |
| - | - | - | . 008 | . 008 | . 007 | . 007 | Cor | ectio | in | n. to | . 0092 | 3000 |
|  | - | . 006 | . 005 | . 005 | . 004 | - | be sub | ract | for | eight | . 0062 | 2000 |
|  | - | . 003 | . 003 | . 003 | - |  | above colum | $\begin{gathered} \text { sea } 1 \\ 1 \text { and } \end{gathered}$ | vel i bas |  | . 0031 | 1000 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | $\underbrace{30}$ | 28 | 26 |  |  | 20 | 18 | 16 |  | $g_{1}-g$ | Height |
|  |  | Observed height of barometer in inches |  |  |  |  |  |  |  |  |  | abo sea level |

TABLE 646.-REDUCTION OF BAROMETER TO STANDARD GRAVITY*
METRIC MEASURES
From latitude $0^{\circ}$ to $45^{\circ}$, the correction is to be added algebraically.

| $\begin{aligned} & \text { Liti- } \\ & \text { tude } \end{aligned}$ | 520 | 540 | 560 | 580 |  | 620 | 640 | 660 | 680 | 00 | 720 |  |  | 780 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $-1.37-1.42-1.48-1.53-1.58-1.64-1.69-1.74-1.79-1.85-1.90-1.95-2.00-2.06$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | 1.36 | 1.42 | 1.47 | 1.52 | 1.57 | 1.63 | 1.68 | 1.73 | 1.78 | 1.83 | 1.89 | 1.94 | 1.99 | 2.04 |
| 7 | 1.35 | 1.40 | 1.46 | 1.51 | 1.56 | 1.61 | 1.66 | 1.72 | 1.77 | 1.82 | 1.87 | 1.92 | 1.98 | 2.03 |
| 8 | 1.34 | 1.39 | 1.44 | 1.49 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 | 1.85 | 1.91 | 1.96 | 2.01 |
| 9 | 1.33 | 1.38 | 1.43 | 1.48 | . 53 | 1.58 | 1.63 | 1.68 | 1.73 | 1.78 | 1.84 | 1. | 19 | 1.99 |
| $-1.31-1.36-1.41-1.46-1.51-1.56-1.61-1.66-1.71-1.76-1.81-1.86-1.92-1.97$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | 1.29 | 1.34 | 1.39 | 1.44 | 1.49 | 1.54 | 1.59 | 1.64 | 1.69 | 1.74 | 1.79 | 1.84 | 1.89 | 1.94 |
| 12 | 1.27 | 1.32 | 1.37 | 1.42 | 1.47 | 1.52 | 1.57 | 1.62 | 1.67 | 1.72 | 1.76 | 1.81 | 1.86 | 1.91 |
| 13 | 1.25 | 1.30 | 1.35 | 1.40 | . 45 | 1.50 | 1.54 | 1.59 | 1.6 | 1.69 | 1.74 | 1.78 | 1.83 | 1.88 |
| 14 | 1.23 | 1.28 | 1.33 | 1.38 | 1.42 | 1.47 | 1.52 | 1.56 | 1.6 | 1.66 | 1.71 | 1.75 | 1.80 | 85 |
| $15-1.21-1.26-1.30-1.35-1.40-1.44-1.49-1.54-1.58-1.63-1.67-1.72-1.77-1.81$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16 | 1.19 | 1.23 | 1.28 | 1.32 | 1.37 | 1.41 | 1.46 | . 50 | 1.55 | 1.60 | 1.64 | 1.69 | 1.73 | 1.78 |
| 17 | 1.16 | 1.20 | 1.25 | 1.29 | 1.34 | 1.38 | 1.43 | 1.47 | 1.5 | 1.56 | 1.60 | 1.65 | 1.69 | 1.74 |
| 18 | 1.13 | 1.18 | 1.22 | 126 | 1.31 | 1.35 | 1.39 | 1.44 | 1.48 | 1.52 | 1.57 | 1.61 | 1.65 | 1.70 |
| 19 | 1.10 | 1.15 | 1.19 | 1.23 | 1.27 | 1.32 | 1.36 | 1.40 | 1.44 | 1.48 | 1.53 | 1.57 | 16 | 1.65 |
| $20-1.07-1.11-1.16-1.20-1.24-1.28-1.32-1.36-1.40-1.44-1.49-1.53-1.57-1.61$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 21 | 1.04 | 1.08 | 1.12 | 116 | 1.20 | 1.24 | 1.28 | 1.32 | 1.36 | 1.40 | 1.44 | 1.48 | 1.52 | 1.56 |
|  | 1.01 | 1.05 | 1.09 | 13 | . 16 | 1.20 | 1.24 | 1.28 | 1.3 | 1.36 | 1.40 | 1.44 | 1.48 | 1.51 |
| 23 |  | 1.01 | 1.05 | 1.09 | 1.13 | 1.16 | 1.20 | 1.24 | 1.28 | 1.31 | 1.35 | 1.39 | 1.43 | 1.46 |
| 24 |  | . 98 | 1.01 | 1.05 | 1.08 | 1.12 | 1.16 | 1.19 | 1.23 | 1.27 | 1.30 | 1.3 | . 3 |  |
| $25-.90-.94-.97-1.01-1.04-1.08-1.11-1.15-1.18-1.22-1.25-1.29-1.32-1.36$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 26 |  | . 90 | . 93 | . 97 | 1.00 | 1.03 | 1.07 | 1.10 | 1.13 | 1.17 | 1.20 | 1.23 | 1.27 | 1.30 |
| $27$ | . 83 | . 86 | . 89 | . 92 | . 96 | . 99 | 1.02 | 1.05 | 1.08 | 1.12 | 1.15 | 1.18 | 1.21 | 1.24 |
| 28 | 79 | . 82 | . 85 | 88 | . 91 | . 94 | . 97 | 1.00 | 1.03 | 1.06 | 1.09 | 1.12 | 1.15 | 1.18 |
| 29 | . 75 | 78 | 81 |  | . 86 | 89 | . 92 | . 95 | . 98 | 1.01 | 1.04 | 1.07 | 1.10 | 112 |
| $30-.71-.74-.76-.79-.82-.85-.87-.90-.93-.95-.98-1.01-1.04-1.06$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 31 | . 67 | . 69 | . 72 | . 74 | . 77 | . 80 | . 82 | . 85 |  | . 90 |  | . 95 |  | 1.00 |
| $32$ | . 62 | . 65 | . 67 | . 70 | . 72 | . 74 | . 77 | . 79 | . 82 | . 84 | . 86 | :89 | . 91 | . 94 |
| 33 | . 58 | . 60 | . 63 | . 65 |  | . 69 | . 72 | . 74 |  | . 78 | . 80 | . 83 |  | 87 |
| 34 |  | . 56 | . 58 |  |  |  | . 66 | . 68 |  |  | . 74 | . 76 |  |  |
|  | - . $49-.51-.53-.55-.57-.59-.61-.63-.64-.66-.68-.70-.72$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 36 | . 45 | . 46 | . 48 | . 50 | . 52 | . 53 | . 55 | . 57 |  | . 60 | . 6 | . 64 |  | 67 |
| $37$ | . 40 | . 42 | . 43 | 4 | . 46 | . 48 | 49 | . 51 | . 52 | . 54 | . 56 | . 57 | . 59 |  |
| 38 | . 36 | 37 | . 38 |  |  | . 42 | . 44 | . 45 | . 46 | 48 | . 49 | . 51 |  | 3 |
| 39 |  | . 32 | . 33 |  |  |  | . 38 |  |  | . 42 | . 43 |  |  |  |
| $40-.26-.27-.28-.29-.30-.31-.32-.33-.34-.35-.36-.37-.38-.39$ | - $.26-.27-.28-.29-.30-.31-.32-.33-.34-.35-.36-.37-.38-.39$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 41 | . 21 | . 22 | . 23 | . 24 | . 25 | . 26 | . 26 | 27 |  | . 29 | . 30 | . 30 |  |  |
| 42 | . 17 | . 17 | 18 |  |  | 20 |  | . 21 | 22 | . 22 | . 23 | . 24 | . 24 |  |
| 43 | . 12 | 12 | 13 |  |  | . 14 |  |  |  | . 16 | . 16 | . 17 |  | . 18 |
| 44 | . 07 | . 07 |  |  |  |  |  |  |  | . 10 |  |  |  |  |
|  | - . $02-.02-.03-.03-.03-.03-.03-.03-.03-.03-.03-.03-.03-.04$ |  |  |  |  |  |  |  |  |  |  |  |  |  |

[^247]
## (continued)

From latitude $46^{\circ}$ to $90^{\circ}$, the correction is to be added algebraically.


TABLE 647.-REDUCTION OF BAROMETER TO STANDARD GRAVITY*
ENGLISH MEASURES
From latitude $0^{\circ}$ to $45^{\circ}$, the correction is to be added algebraically.

| Lati- | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | $\begin{array}{r} \text { Inch } \\ -.051 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.054 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.056 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.059 \end{array}$ | $\begin{array}{r} \mathrm{In}-\mathrm{h} \\ -.062 \end{array}$ | $\begin{array}{r} \text { Incl } \\ -.064 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.067 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.070 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.072 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.075 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.078 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.080 \end{array}$ |
| 5 | -. 050 | -. 053 | -. 055 | -. 058 | -. 061 | -. 063 | -. 066 | -. 069 | -. 071 | -. 074 | -. 077 | 79 |
| 6 | . 050 | . 052 | . 055 | . 058 | . 060 | . 063 | . 066 | . 068 | . 071 | . 073 | . 076 | 079 |
| 7 | . 049 | . 052 | . 055 | . 057 | . 060 | . 062 | . 065 | . 068 | . 070 | . 073 | . 075 | . 078 |
| 8 | . 049 | . 052 | . 054 | . 057 | . 059 | . 062 | . 064 | . 067 | . 070 | . 072 | . 075 | 077 |
| 9 | . 048 | . 051 | . 054 | . 056 | . 059 | . 061 | . 064 | . 066 | . 069 | . 071 | . 074 | . 076 |
| 10 | -. 048 | -. 050 | -. 053 | -. 055 | -. 058 | -. 060 | -. 063 | -. 066 | -. 068 | $-.071$ | -. 073 | -. 076 |
| 11 | . 047 | . 050 | . 052 | . 055 | . 057 | . 060 | . 062 | . 065 | . 067 | . 070 | . 072 | . 075 |
| 12 | . 047 | . 049 | . 051 | . 054 | . 056 | . 059 | . 061 | . 064 | . 066 | . 069 | . 071 | 074 |
| 13 | . 046 | . 048 | . 051 | . 053 | . 055 | . 058 | . 060 | . 063 | . 065 | . 068 | . 070 | 07 |
| 14 | . 045 | . 047 | . 050 | . 052 | . 055 | . 057 | . 059 | . 062 | . 06 | . 06 | . 069 | 071 |
| 15 | -. 044 | $-.047$ | -. 049 | -. 051 | -. 053 | -. 056 | -. 058 | -. 060 | -. 063 | -. 065 | -. 067 | -. 070 |
| 16 | . 043 | . 046 | . 048 | . 050 | . 052 | . 055 | . 057 | . 059 | . 062 | . 064 | . 066 | . 068 |
| 17 | . 042 | . 045 | . 047 | . 049 | . 051 | . 053 | . 056 | . 058 | . 060 | . 062 | . 065 | . 067 |
| 18 | . 041 | . 044 | . 046 | . 048 | . 050 | . 052 | . 054 | . 057 | . 059 | . 061 | . 063 | 65 |
| 19 | . 040 | . 042 | . 045 | . 047 | . 049 | . 051 | . 053 | . 055 | . 057 | . 059 | . 062 | . 064 |
| 20 | $-.039$ | -. 041 | $-.043$ | -. 045 | -. 047 | $-.050$ | -. 052 | -. 054 | -. 056 | -. 058 | -. 060 | -. 062 |
| 21 | . 038 | . 040 | . 042 | . 044 | . 046 | . 048 | . 050 | . 052 | . 054 | . 056 | . 058 | . 060 |
| 22 | . 037 | . 039 | . 041 | . 043 | . 045 | . 047 | . 049 | . 050 | . 052 | . 054 | . 056 | 05 |
| 23 | . 036 | . 038 | . 039 | . 041 | . 043 | . 045 | 047 | . 049 | . 051 | . 053 | . 054 | . 56 |
| 24 | . 034 | . 036 | . 038 | . 040 | . 042 | . 043 | 045 | . 047 | . 049 | . 051 | . 052 | 054 |
| 25 | -. 033 | -. 035 | -. 037 | -. 038 | -. 040 | -. 042 | -. 043 | -. 045 | -. 047 | -. 049 | -. 050 | -. 052 |
| 26 | . 032 | . 033 | . 035 | . 037 | . 038 | . 040 | . 042 | . 043 | . 045 | . 047 | . 048 | . 05 |
| 27 | . 030 | . 032 | . 033 | . 035 | . 037 | . 038 | . 040 | . 041 | . 043 | . 045 | . 046 | . 04 |
| 28 | . 029 | . 030 | . 032 | . 033 | . 035 | . 036 | . 038 | . 039 | . 041 | . 043 | . 044 | 46 |
| 29 | . 027 | . 029 | . 030 | . 032 | . 033 | . 035 | . 036 | . 037 | . 039 | 040 | 042 |  |
| 30 | -. 026 | -. 027 | -. 029 | -. 030 | -. 031 | -. 033 | -. 034 | -. 035 | -. 037 | -. 038 | -. 040 | -. 041 |
| 31 | . 024 | . 026 | . 027 | . 028 | . 030 | . 031 | . 032 | . 033 | . 035 | . 036 | . 037 | . 038 |
| 32 | . 023 | . 024 | . 025 | . 026 | . 028 | . 029 | . 030 | . 031 | . 032 | . 034 | . 035 | . 036 |
| 33 | . 021 | . 022 | . 023 | . 025 | . 026 | . 027 | . 028 | . 029 | . 030 | . 031 | . 032 | . 034 |
| 34 | . 020 | . 021 | . 022 | . 023 | . 024 | . 025 | . 02 | . 027 | . 028 | 1020 |  |  |
| 35 | -. 018 | -. 019 | -. 020 | -. 021 | -. 022 | -. 023 | -. 024 | -. 025 | -. 026 | -. 027 | -. 027 | -. 028 |
| 36 | . 016 | . 017 | . 018 | . 019 | . 020 | . 021 | . 022 | . 022 | . 023 | . 024 | . 025 | . 026 |
| 37 | . 015 | . 015 | . 016 | . 017 | . 018 | . 019 | . 019 | . 020 | . 021 | . 022 | . 022 | . 023 |
| 38 | . 013 | . 014 | . 014 | . 015 | . 016 | . 016 | . 017 | . 018 | . 018 | . 019 | . 020 | . 020 |
| 39 | . 011 | . 012 | . 012 | . 013 | . 014 | . 014 | . 0 | . 015 | . 016 | . 017 | . 017 | . 018 |
| 40 | -. 010 | -. 010 | -. 011 | -. 011 | -. 012 | -. 012 | -. 013 | -. 013 | -. 014 | -. 014 | -. 015 | -. 015 |
| 41 | . 008 | . 008 | . 009 | . 009 | . 009 | . 010 | . 010 | . 011 | . 011 | . 012 | . 012 | . 012 |
| 42 | . 006 | . 006 | . 007 | . 007 | . 007 | . 008 | . 008 | . 008 | . 009 | . 009 | . 009 | . 010 |
| 43 | . 004 | . 005 | . 005 | . 005 | . 005 | . 005 | . 006 | . 006 | . 006 | . 006 | . 007 | . 007 |
| 44 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 004 | . 00 | . 004 | 4 | 004 |
| 45 | -. 001 | -. 001 | -. 001 | -. 001 | -. 001 | -. 001 | $-.001$ | -. 001 | -. 001 | -. 00 | -. 001 | -. 001 |

[^248](continued)

## ENGLISH MEASURES

From latitude $46^{\circ}$ to $90^{\circ}$, the correction is to be added algebraically.

| Latitude | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 45 | $\begin{array}{r} \text { Inch } \\ -.001 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.001 \end{array}$ | $-.001$ | $\begin{array}{r} \text { Inch } \\ -.001 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.001 \end{array}$ |  |  | $\begin{array}{r} \text { Inch } \\ -.001 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.001 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.001 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.001 \end{array}$ | $\begin{array}{r} \text { Inch } \\ -.001 \end{array}$ |
| 46 | $+.001$ | $+.001$ | $+.001$ | $+.001$ | $+.001$ | $+.001$ | $+.001$ | $+.001$ | $+.001$ | $+.001$ | $+.001$ | . 001 |
| 47 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 003 | . 004 | . 004 | . 004 | . 004 | . 004 |
| 48 | . 004 | . 005 | . 005 | . 005 | . 005 | . 006 | . 006 | . 006 | . 006 | . 006 | . 007 | . 007 |
| 49 | . 006 | . 006 | . 007 | . 007 | . 007 | . 008 | . 008 | . 008 | . 009 | . 009 | . 009 | . 010 |
| 50 | . 008 | . 008 | . 009 | . 009 | . 010 | . 010 | . 010 | . 011 | . 012 | . 012 | . 012 | 12 |
| 51 | $+.010$ | $+.010$ | $+.011$ | +. 011 | +. 012 | $+.012$ | +. 013 | $+.013$ | $+.014$ | +. 014 | $+.015$ | +. 015 |
| 52 | . 011 | . 012 | . 012 | . 013 | . 014 | . 014 | . 015 | . 015 | . 016 | . 016 | . 017 | 18 |
| 53 | . 013 | . 014 | . 014 | . 015 | . 016 | . 016 | . 017 | . 018 | . 018 | . 019 | . 020 | . 020 |
| 54 | . 015 | . 015 | . 016 | . 017 | . 018 | . 019 | . 019 | . 020 | . 021 | . 022 | . 022 | . 023 |
| 55 | . 016 | . 017 | . 018 | . 019 | . 020 | . 021 | . 021 | . 022 | . 023 | . 024 | . 025 | . 026 |
| 56 | $+.018$ | $+.019$ | $+.020$ | $+.021$ | +. 022 | $+.023$ | +. 024 | $+.024$ | $+.026$ | +. 026 | $+.027$ | +. 028 |
| 57 | . 020 | . 021 | . 022 | . 023 | . 024 | . 025 | . 026 | . 027 | . 028 | . 029 | . 030 | . 031 |
| 58 | . 021 | . 022 | . 023 | . 025 | . 026 | . 027 | . 028 | . 029 | . 030 | . 031 | . 032 | . 033 |
| 59 | . 023 | . 024 | . 025 | . 026 | . 028 | . 029 | . 030 | . 031 | . 032 | . 033 | . 035 | 36 |
| 60 | . 024 | . 026 | . 027 | . 028 | . 029 | . 031 | . 032 | . 033 | . 034 | . 036 | . 037 | . 038 |
| 61 | $+.026$ | $+.027$ | +. 028 | $+.030$ | $+.031$ | $+.033$ | +. 034 | +. 035 | $+.037$ | +. 038 | +. 039 | +. 041 |
| 62 | . 027 | . 029 | . 030 | . 032 | . 033 | . 034 | . 036 | . 037 | . 039 | . 040 | . 042 | . 043 |
| 63 | . 029 | . 030 | . 032 | . 033 | . 035 | . 036 | . 038 | . 039 | . 041 | . 042 | . 044 | . 045 |
| 64 | . 030 | . 032 | . 033 | . 035 | . 036 | . 038 | . 040 | 041 | . 043 | . 044 | . 046 | . 047 |
| 65 | . 031 | . 033 | . 035 | . 036 | . 038 | 040 | . 041 | . 043 | . 045 | . 046 | . 048 | . 050 |
| 66 | +.033 | +. 034 | $+.036$ | +. 038 | $+.040$ | $+.041$ | $+.043$ | +. 045 | $+.047$ | +. 048 | $+.050$ | +. 052 |
| 67 | . 034 | . 036 | . 038 | . 039 | . 041 | . 043 | . 045 | . 047 | . 048 | . 050 | . 052 | . 054 |
| 68 | . 035 | . 037 | . 039 | . 041 | . 043 | . 045 | . 046 | . 048 | . 050 | . 052 | . 054 | . 056 |
| 69 | . 036 | . 038 | . 040 | . 042 | 044 | . 046 | . 048 | . 050 | . 052 | . 054 | . 056 | . 05 |
| 70 | . 038 | . 040 | . 042 | . 044 | . 046 | . 048 | . 050 | . 052 | . 053 | . 055 | . 057 | . 059 |
| 71 | +. 039 | $+.041$ | $+.043$ | +. 045 | +. 047 | +. 049 | $+.051$ | +. 053 | +. 055 | $+.057$ | +. 059 | $+.061$ |
| 72 | . 040 | . 042 | . 044 | . 046 | . 048 | . 050 | . 052 | . 054 | . 057 | . 059 | . 061 | 063 |
| 73 | . 041 | . 043 | . 045 | . 047 | . 049 | . 052 | . 054 | . 056 | . 058 | . 060 | . 062 | . 064 |
| 74 | . 042 | . 044 | . 046 | . 048 | . 051 | . 053 | . 055 | . 057 | . 059 | . 062 | . 064 | . 066 |
| 75 | . 043 | . 045 | . 047 | . 049 | . 052 | . 05 | . 056 | . 058 | . 061 | . 063 | 065 |  |
| 76 | +. 044 | +. 046 | $+.048$ | $+.050$ | $+.053$ | $+.055$ | +. 057 | $+.060$ | +. 062 | +. 064 | 066 | 069 |
| 77 | . 044 | . 047 | . 049 | . 051 | . 054 | . 056 | . 058 | . 061 | . 063 | . 065 | . 068 | . 070 |
| 78 | . 045 | . 047 | . 050 | . 052 | . 055 | . 057 | . 059 | . 062 | . 064 | . 066 | . 069 | . 071 |
| 79 | . 046 | . 048 | . 051 | . 053 | . 055 | . 058 | . 060 | . 063 | . 065 | . 067 | . 070 | . 072 |
| 80 | . 046 | . 049 | . 051 | . 054 | . 056 | . 059 | . 06 | . 063 | . 06 | . 06 | . 07 | . 073 |
| 81 | $+.047$ | +. 049 | +. 052 | +. 054 | $+.057$ | $+.059$ | +. 062 | +. 064 | $+.067$ | +. 069 | $+.072$ | $+.074$ |
| 82 | . 047 | . 050 | . 052 | . 055 | . 057 | . 060 | . 062 | . 065 | . 067 | . 070 | . 072 | . 075 |
| 83 | . 048 | . 050 | . 053 | . 056 | . 058 | . 061 | . 063 | . 066 | . 068 | . 071 | . 073 | . 076 |
| 84 | . 048 | . 051 | . 053 | . 056 | . 059 | . 061 | . 064 | . 066 | . 069 | . 071 | . 074 | . 076 |
| 85 | . 049 | . 051 | . 054 | . 056 | . 059 | . 061 | . 064 | . 067 | . 069 | . 072 | . 074 | . 07 |
| 90 | +. 049 | +. 052 | +. 055 | +. 057 | $+.060$ | +. 062 | +. 065 | +. 068 | +. 070 | +. 073 | +. 075 | +. 078 |

TABLE 648.-DETERMINATION OF HEIGHTS BY THE BAROMETER

> Formula of Babinet : $Z=C \frac{B_{0}-B}{B_{0}+B}$
> $C$ (in feet) $=52494\left[1+\frac{t_{0}+t-64}{900}\right]$ English measures.
> $C$ (in meters) $=16000\left[1+\frac{2\left(t_{0}+t\right)}{1000}\right]$ metric measures.

In which $Z=$ difference of height of two stations in feet or meters.
$B_{0}, B=$ barometric readings at the lower and upper stations respectively, corrected for all sources of instrumental error.
$t_{0}, t=$ air temperatures at the lower and upper stations respectively.
values of $C$

| English measures |  |  | Metric measures |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \frac{1}{2}\left(t_{0}+t\right) \\ & 0 \mathrm{~F} \end{aligned}$ | $C$ Feet | Log C | $\frac{1}{\frac{1}{2}\left(t_{0}+t\right)}$ | $\stackrel{C}{C}$ | Log C |
| 10 | 49928 | 4.69834 | -10 | 15360 | 4.18639 |
| 15 | 50511 | . 70339 | -8 | 15488 | . 19000 |
|  |  |  | - 6 | 15616 | . 19357 |
| 20 | 51094 | 4.70837 | -4 | 15744 | . 19712 |
| 25 | 51677 | . 71330 | -2 | 15872 | . 20063 |
| 30 | 52261 | 4.71818 | 0 | 16000 | 4.20412 |
| 35 | 52844 | . 72300 | + 2 | 16128 | . 20758 |
|  |  |  | 4 | 16256 | . 21101 |
| 40 | 53428 | 4.72777 |  | 16384 | . 21442 |
| 45 | 54011 | . 73248 | 8 | 16512 | . 21780 |
| 50 | 54595 | 4.73715 | 10 | 16640 | 4.22115 |
| 55 | 55178 | . 74177 | 12 | 16768 | . 22448 |
|  |  |  | 14 | 16896 | . 22778 |
| 60 | 55761 | 4.74633 | 16 | 17024 | . 23106 |
| 65 | 56344 | . 75085 | 18 | 17152 | . 23431 |
| 70 | 56927 | 4.75532 | 20 | 17280 | 4.23754 |
| 75 | 57511 | . 75975 | 22 | 17408 | . 24075 |
|  |  |  | 24 | 17536 | . 24393 |
| 80 | 58094 | 4.76413 | 26 | 17664 | . 24709 |
| 85 | 58677 | . 76847 | 28 | 17792 | . 25022 |
| 90 | 59260 | 4.77276 | 30 | 17920 | 4.25334 |
| 95 | 59844 | . 77702 | 32 | 18048 | . 25643 |
|  |  |  | 34 | 18176 | . 25950 |
| 100 | 60427 | 4.78123 | 36 | 18304 | . 26255 |

TABLE 649.-THUNDERSTORM ELECTRICITY ${ }^{198}$
(Lightning strokes consist of current peaks and continuing currents.)

Cloud-to-ground stroke characteristics.-First discharge in a stroke progresses from cloud to ground as stepped leaders (average velocity, 1 foot per microsecond). After contacting earth a return stroke progresses toward the cloud (velocity, $65-450$ feet $/ \mu$ sec; average, 100 feet $/ \mu$ sec). Subsequent discharges progress from the cloud as continuous leaders (average velocity, 10 feet $/ \mu \mathrm{sec}$ ) and again a return stroke is formed. is hear case of tall objects (skyscrapers) stroke leaders may start from the building toward the cloud. In such a case no thunder or very little thunder is heard unless initial discharge is followed by current peaks.
${ }^{198}$ McEachron, K. B., "Lightning and Lightning Protection," Encycl. Brit., vol. 14, June 1948. Used by permission.

The elements of atmospheric electricity show variations, both regular and irregular. Over land the irregular variations are very pronounced and the regular variations differ notably from place to place, in marked contrast to the corresponding characteristics over the ocean. Therefore, and because of the wider and more uniform geographical distribution of ocean observations, it seems best to give the greater weight to the ocean data when attempting to arrive at values characterizing world-wide conditions. Because of the wide variation from place to place in the means from land stations, due to local factors, a general mean of these is of questionable significance. Hence it seems better to indicate the extremes of station means in the case of elements for which the data are sufficiently abundant.

Certain disparities, which will be found between published tables of ocean data, arise largely from the inclusion of more recent data.

Of the atmospheric-electric clements the potential gradient has been the most extensively observed. The sign of the average gradient is everywhere such as to drive positive ions toward the earth. The periodic variations in this element are of great interest because of their apparent relation with cosmic phenomena. Thus the potential gradient apparently increases with increase in sunspot numbers and varies throughout the year. The maxima in monthly means occur everywhere, with few exceptions, at the time of northern winter, and the corresponding minima occur at the time of northern summer. The diurnal variation observed over the oceans is cverywhere in phase when considered on a common-time basis, except for a minor phase-shift that depends upon the season. This diurnal variation derived from observatories made on the Carnegie during 1915 to 1921, given by the Fourier expression $\Delta P / P=0.15 \sin \left(\theta+186^{\circ}\right)+0.03 \sin \left(2 \theta+237^{\circ}\right)$ where $\theta$ is reckoned at $15^{\circ}$ per hour beginning at $0^{\text {h }}$ Greenwich mean civil time, is in close agreement with that obtained from 1928-1929 observations.

No general expression that will approximately characterize the diurnal variation over land can be given. These variations determined by local factors are apparently superimposed upon a variation of the same world-wide character as that found to prevail over the oceans.

* Tables 650-653 prepared by G. R. Wait, Department of Terrestrial Magnestism, Carnegie Institution of Washington.


## TABLE 651.-IONIC EQUILIBRIUM IN THE ATMOSPHERE

Equilibrium for atmospheric ionization occurs when $q=a n^{2}+\eta_{1} N_{0} n+\eta_{2} N n$, where $n$ and $N$ are the number of pairs of small and large ions of one sign and $N_{0}$ the number of uncharged nuclei ; $a, \eta_{1}, \eta_{2}$, are coefficients of recombination of small ions with small ions, with uncharged nuclei, and with large ions. If for both small and large ions the positive and negative are equally abundant, then $N_{0} / N=\eta_{2} / \eta_{1}$. When $n / N \ll 2 \eta_{2} / a$, the equilib-rium-condition is expressed by $q=\beta n ; \beta$ is designated the diminution-constant; $1 / \beta=\ominus$ is the "average life" of a small ion in air which contains an abundance of large ions; $\Theta$ varies inversely as $N$.

| $\begin{aligned} & a: 1.6 \times 10^{-8} \mathrm{~cm}^{3} / \mathrm{sec} \\ & \eta_{1}: 5 \times 10^{-6} " \\ & \eta_{2}: 6 \times 10^{-8} \quad " \\ & \Theta \text { Over land, } \\ & \text { Average, } 30 \mathrm{sec} \end{aligned}$ |
| :---: |
|  |  |
|  |  |
|  |  |
|  |  |

Extremes, 10 to 60 sec
Over sea, 230 sec
$N$ : Over land, 500 to 50,000 ions $/ \mathrm{cm}^{3}$
Aitken nuclei, number per $\mathrm{cm}^{3}$ :
Over open country, up to $10^{5}$
Over midocean, about 800
In free air,
Altitude $1 \mathrm{~km} 6,000 \quad 5 \mathrm{~km} 50$
$3 \mathrm{~km} \quad 200 \quad 8.5 \mathrm{~km}$ about 5

TABLE 652.-CHARGE ON RAIN AND SNOW
Specific net charge on precipitation:
Average, $0.5 \mathrm{esu} / \mathrm{g}$
Maximum observed, $20 \mathrm{esu} / \mathrm{g}$
Specific charge on individual raindrops or snowflakes:
Rain, +2.7 to $-3.2 \mathrm{esu} / \mathrm{g}$
Snow, +11.6 to $-8.1 \mathrm{esu} / \mathrm{g}$

| Element | Symbol | Means | Units | Variations |
| :---: | :---: | :---: | :---: | :---: |
| Potential gradient. |  | Land: 64 to 317 |  | $\begin{array}{ll} \text { Range } & \text { Percent of mean } \\ \text { Annual } & 22 \text { to } 145 \end{array}$ |
|  |  |  |  | Diurnal 35 to 120 |
|  |  | Sea: 128 |  | Annual 13 |
|  |  |  |  | Diurnal 35 |
|  |  | Free air |  | Percentage of surface values at various altitudes |
|  |  |  |  | $\begin{array}{lllll} 0 & \mathrm{~km} & 100 & 6 & 6 \mathrm{~km} \\ 3 & 8 & 17 & 9 & 4 \end{array}$ |
| Air-conductivity total | $\lambda=\lambda_{+}+\lambda_{-}$ |  |  |  |
|  |  | Land: 1 to 5 | esu $\times 10^{-4}$ | Variations determined chiefly by local factors |
|  |  | Sea: $\quad 2.6$ |  | Variations small and chiefly ir regular |
|  |  | Free air |  | Ratio of value at various altitudes to that at surface $\begin{array}{lll} 0 \mathrm{~km} \\ 3 \times 8 & 6 \mathrm{~km} 20 \\ 3 & " & 38 \end{array}$ |
| Ratio of positive <br> to negative <br> conductivity $\ldots$.$\lambda_{+} / \lambda_{-}$ Land: 1.12  <br>   Sea: 1.26 |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Air-earth current density | $i=\lambda P / 30000$ | Land: 7.0 | esu $\times 10^{-7}$ |  |
|  |  | Sea: 11.0 |  |  |
| Density of small ions: Positive .. | $n_{+}$ <br> $n-$ $\left(n_{+}+n_{-}\right) / 2$ | Land: 750 | ions/ $\mathrm{cm}^{3}$ |  |
|  |  | Sea: 600 |  |  |
| Negative . |  | Land: 650 | " |  |
|  |  | Sea: 500 | " |  |
|  |  | Free air |  | . Values at various altitudes <br> 2 km 1300 <br> 4 " 1900 |
| Ratio of positive to negative ionic density |  |  |  | 5 " 2300 |
|  | $p=n_{+} / n_{-}$ | Land: 1.23 |  |  |
|  |  | Sea: 1.23 |  |  |
|  |  | (continue ${ }^{\text {d }}$ |  |  |

Element
Space-charge, over land. .

| Space-charge, over land.. | $\rho$ |
| :--- | :---: |
|  | $\rho=-\left(\frac{d P}{d h} / 1.2 \pi\right) \times$ |
|  | $($ For $h=$ height in |
| Mobility of small ions: |  |
| Positive $\ldots \ldots \ldots \ldots \ldots$ | $k_{+}=\lambda_{+} / 300 \mathrm{en}$ |
| $k_{+}$ |  |
| Negative $\ldots \ldots \ldots \ldots$. | $k_{-}$ |

Rate of formation of ion-pairs $\qquad$
Symbol
$\rho$

Means
At surface: * -2000 to +1900
Free air :

| 0 to 3 km | $\stackrel{\rho}{9.0}$ | " |
| :---: | :---: | :---: |
| 3 to 6 | 0.9 | " |
| 6 to 9 | 0.4 | " |
| Land: | 0.9 | $\mathrm{cm} \mathrm{sec}{ }^{-1}$ volt $^{-1} \mathrm{~cm}^{-1}$ |
| Sea: | 1.6 |  |
| Land : | 1.0 | " |
| Sea : | 1.7 | " |
| Over land: <br> Ra and Th products in air |  |  |
|  |  |  |
|  |  |  |
| a rays | 4.6 | ions $\mathrm{cm}^{-8} \mathrm{sec}^{-1}$ |
| $\beta$ rays | 0.2 |  |
|  |  | " |
| Radioac |  |  |
| matter in the |  |  |
| earth's |  |  |
| $\beta$ rays | 0.1 | " |
| $\gamma$ rays | 3.0 | " |
| Penetrating |  |  |
| Total | 9.55 | " |
| At sea : |  |  |
| Penetrating |  |  |
| radiat |  | " |
| (? |  | " |
| Total | 2.2 | " |

*The sign and magnitude of surface values are exceedingly variable from place to place.

Just a few years ago it was held that the universe was made up of 92 elements and that probably these elements were made of two elementary particles. While most of these 92 elements had been identified and their properties studied, there were several that had not been identified and thus very little was known directly about their properties.

As a result of a great amount of study and investigation, during the past few years the number of known elementary particles has been extended to seven or eight (see Table 720), and all the elements missing from the periodic table (see Table 658) have been identified and some of their properties studied. ${ }^{199}$ In addition to this, the number of elements has been extended to five or six beyond uranium and some of the properties of these elements have been studied. (See Table 658.)

It is now generally considered that the elements are made up of electrons, protons, and neutrons. Each element now has three designations: the name; the atomic number, $Z$, i.e., the charge on the atomic nucleus and the mass number, $A$, which is the number of protons and neutrons that make up the nucleus of the atom and extends from 1 for hydrogen (or the neutron) to 246 for the isotope of californium. This mass number is not too definite since, in many cases, several atoms have isotopes of the same mass number.

Atoms of number greater than 83 and certain isotopes of eight atoms of lower atomic number, are unstable in that they break down into other isotopes, i.e., they are radioactive. (See Table 732.) There are in all about 1,220 different isotopes ${ }^{199}$ that have been identified and have had some of their properties studied. Of these only 274 are stable. A number of atoms ${ }^{200}$ $(Z=43,61,85,93,94,95,96)$ are so unstable that they are not now found on the earth. Two of the isotopes, $A=5$, and 8 , have so short a life that it is almost impossible to detect them. A radioactive material with a life shorter than about $10^{-20} \mathrm{sec}$ and longer than about $10^{14}$ years will be unobservable as such.

The values given for certain physical dimensions of molecules, atoms, or nuclei depend upon the definition of the particular dimension and the method used in its calculation. Diameters may be calculated from Van der Waal's equation, from viscosity, and from certain force relations. Some values are the results of assuming the atom or nucleus to be a sphere. While these various methods give results that do not differ too much, neither are the results in good enough agreement for one to feel that the answer is final. The following tables give some results of physical dimension obtained by various means of calculation.

[^249]TABLE 654.-CONVERSION FACTORS FOR UNITS OF MOLECULAR ENERGY*


[^250]| Element | Symbol | At | Atomic weight * | Element | Symbol | At | Atomic weight * |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actinium | Ac | 89 | 227 | Molybdenum | Mo | 42 | 95.95 |
| Aluminum | . Al | 13 | 26.98 | Neodymium | Nd | 60 | 144.27 |
| Americium | Am | 95 | [243] | Neon | Ne | 10 | 20.183 |
| Antimony | . Sb | 51 | 121.76 | Neptunium | Np | 93 | [237] |
| Argon ... | . A | 18 | 39.944 | Nickel .... | Ni | 28 | 58.69 |
| Arsenic | . As | 33 | 74.91 | Niobium | Nb | 41 | 92.91 |
| Astatine | . At | 85 | [210] | Nitrogen | N | 7 | 14.008 |
| Barium | Ba | 56 | 137.36 | Osmium | Os | 76 | 190.2 |
| Berkelium | . Br | 97 | [245] | Oxygen | . O | 8 | 16 |
| Beryllium | Be | 4 | 9.013 | Palladium | Pd | 46 | 10.5 .7 |
| Bismuth . | Bi | 83 | 209.00 | Phosphorus | . P | 15 | 30.975 |
| Boron | B | 5 | 10.82 | Platinum . | Pt | 78 | 195.23 |
| Bromine | . Br | 35 | 79.916 | Plutonium | Pu | 94 | [242] |
| Cadmium | . Cd | 48 | 112.41 | Polonium | Po | 84 | 210 |
| Calcium | . Ca | 20 | 40.08 | Potassium | K | 19 | 39.100 |
| Californium | . $\mathrm{C} f$ | 98 | [246] | Praseodymium | Pr | 59 | 140.92 |
| Carbon . . | . C | 6 | 12.010 | Promethium | Pm | 61 | [145] |
| Cerium | . Ce | 58 | 140.13 | Protactinium | Pa | 91 | 231 |
| Cesium . | . Cs | 55 | 132.91 | Radium . | Ra | 88 | 226.05 |
| Chlorine | . Cl | 17 | 35.457 | Radon | Rn | 86 | 222 |
| Chromium | . Cr | 24 | 52.01 | Rhenium | Re | 75 | 186.31 |
| Cobalt . | . Co | 27 | 58.94 | Rhodium | R h | 45 | 102.91 |
| Copper | . Cu | 29 | 63.54 | Rubidium | Rb | 37 | 85.48 |
| Curium | . Cm | 96 | [243] | Ruthenium | Ru | 44 | 101.7 |
| Dysprosium | . Dy | 66 | 162.46 | Samarium | Sm | 62 | 150.43 |
| Erbium . . . | . Er | 68 | 167.2 | Scandium |  | 21 | 44.96 |
| Europium | . Eu | 63 | 152.0 | Selenium | Se | 34 | 78.96 |
| Fluorine . |  | 9 | 19.00 | Silicon | Si | 14 | 28.06 |
| Francium | Fr | 87 | [223] | Silver | Ag | 47 | 107.880 |
| Gadolinium | . Gd | 64 | 156.9 | Sodium | Na | 11 | 22.997 |
| Gallium | . Ga | 31 | 69.72 | Strontium | Sr | 38 | 87.63 |
| Germanium | . Ge | 32 | 72.60 | Sulfur | S | 16 | $32.066 \dagger$ |
| Gold | . Au | 79 | 197.2 | Tantalum | Ta | 73 | 180.88 |
| Hafnium | . Hf | 72 | 178.6 | Technetium | Tc | 43 | [99] |
| Helium . | . He | 2 | 4.003 | Tellurium | Te | 52 | 127.61 |
| Holmium | . Ho | 67 | 164.94 | Terbium | Tb | 65 | 1592 |
| Hydrogen |  | 1 | 1.0080 | Thallium | Tl | 81 | 204.39 |
| Indium . . | . In | 49 | 114.76 | Thorium | Th | 90 | 232.12 |
| Iodine | . I | 53 | 126.91 | Thulium | Tm | 69 | 169.4 |
| Iridium |  | 77 | 193.1 | Tin | Sn | 50 | 118.70 |
| Iron . . . | . Fe | 26 | 55.85 | Titanium | Ti | 22 | 47.90 |
| Krypton | Kr | 36 | 83.80 | Tungsten |  | 74 | 183.92 |
| Lanthanum | La | 57 | 138.92 | Uranium | U | 92 | 238.07 |
| Lead . . . | Pb | 82 | 207.21 | Vanadium | V | 23 | 50.95 |
| Lithium | . Li | 3 | 6.940 | Xenon | Xe | 54 | 131.3 |
| Lutetium | Lu | 71 | 174.99 | Ytterbium | Yb | 70 | 17304 |
| Magnesium | Mg | 12 | 24.32 | Yttrium . | Y | 39 | 88.92 |
| Manganese | . Mn | 25 | 54.93 | Zinc | Zn | 30 | 65.38 |
| Mercury . . | . Hg | 80 | 200.61 | Zirconium | Zr | 40 | 91.22 |

[^251]| 1 Hydrogen | H | 34 Selenium | Se | 67 Holmium | Ho |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2 Helium | He | 35 Bromine | Br | 68 Erbium | Er |
| 3 Lithium | Li | 36 Krypton | Kr | 69 Thulium | Tm |
| 4 Beryllium | Be | 37 Rubidium | Rb | 70 Ytterbium | Yb |
| 5 Boron | B | 38 Strontium | Sr | 71 Lutetium | Lu |
| 6 Carbon | C | 39 Yttrium | Y | 72 Hafnium | Hf |
| 7 Nitrogen | N | 40 Zirconium | Zr | 73 Tantalum | Ta |
| 8 Oxygen | O | 41 Niobium | Nb | 74 Tungsten | W |
| 9 Fluorine | F | 42 Molybdenum | Mo | 75 Rhenium | Re |
| 10 Neon | Ne | 43 Technetium | Tc | 76 Osmium | Os |
| 11 Sodium | Na | 44 Ruthenium | Ru | 77 Iridium | Ir |
| 12 Magnesium | Mg | 45 Rhodium | Rh | 78 Platinum | Pt |
| 13 Aluminum | A1 | 46 Palladium | Pd | 79 Gold | Au |
| 14 Silicon | Si | 47 Silver | Ag | 80 Mercury | Hg |
| 15 Phosphorus | P | 48 Cadmium | Cd | 81 Thallium | Tl |
| 16 Sulfur | S | 49 Indium | In | 82 Lead | Pb |
| 17 Chlorine | Cl | 50 Tin | Sn | 83 Bismuth | Bi |
| 18 Argon | A | 51 Antimony | Sb | 84 Polonium | Po |
| 19 Potassium | K | 52 Tellurium | Te | 85 Astatine | At |
| 20 Calcium | Ca | 53 Iodine | I | 86 Radon | Rn |
| 21 Scandium | Sc | 54 Xenon | Xe | 87 Francium | Fr |
| 22 Titanium | Ti | 55 Cesium | Cs | 88 Radium | Ra |
| 23 Vanadium | V | 56 Barium | Ba | 89 Actinium | Ac |
| 24 Chromium | Cr | 57 Lanthanum | La | 90 Thorium | Th |
| 25 Manganese | Mn | 58 Cerium | Ce | 91 Protactinium | Pa |
| 26 Iron | Fe | 59 Praesodymium | Pr | 92 Uranium | U |
| 27 Cobalt | Co | 60 Neodymium | Nd | 93 Neptunium | Np |
| 28 Nickel | Ni | 61 Promethium | Pm | 94 Plutonium | Pu |
| 29 Copper | Cu | 62 Samarium | Sm | 95 Americium | Am |
| 30 Zinc | Zn | 63 Europium | Eu | 96 Curium | Cm |
| 31 Gallium | Ga | 64 Gadolinium | Gd | 97 Berkelium | Bk |
| 32 Germanium | Ge | 65 Terbium | Tb | 98 Californium | Cf |
| 33 Arsenic | As | 66 Dysprosium | Dy |  |  |

Given below by atomic numbers are some foreign or obsolete names for certain of the elements.

4 Glucinium, Gl
11 Natrium
13 Aluminium
19 Kalium
26 Ferrum

41 Columbium, Cb
43 Masurium, Ma
47 Argentum
50 Stannum
51 Stibium

61 Illinium, Il
71 Cassiopeium
72 Celtium
75 Bohemium
79 Aurum

80 Hydragyrum
82 Plumbum
85 Alabamine, Ab
86 Emanation, niton
87 Virginium, Vi
TABLE 657.-PERIODIC SYSTEM OF THE ELEMENTS ${ }^{20}$

|  | $\overbrace{0}^{\text {I }}$ |  | II |  | $\underbrace{\text { III }}$ | $\mathrm{I}^{\text {IV }}$ |  | v |  | VI |  | VII |  | $\underbrace{\text { VIII }}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I | $\begin{gathered} a \\ 1 \mathrm{H} \\ 1.0080 \end{gathered}$ | $b$ | a | $b$ | ${ }_{a} \quad{ }^{\text {b }}$ | a | $b$ | $a$ | b | $a$ | $b$ | a | $b$ |  | $a$ |  | $\begin{aligned} & b \\ & 2 \mathrm{He} \\ & 4.003 \end{aligned}$ |
| II | $\begin{aligned} & 3 \mathrm{Li} \\ & 6.940 \end{aligned}$ |  |  | $\begin{aligned} & 4 \mathrm{Be} \\ & 9.013 \end{aligned}$ | $\begin{array}{r} 5 \mathrm{~B} \\ 10.82 \end{array}$ |  | $\underset{12.010}{6 \mathrm{C}}$ |  | $\begin{gathered} 7 \mathrm{~N} \\ 14.008 \end{gathered}$ |  | ${ }_{16}^{80}$ |  | $\begin{gathered} 9 \mathrm{~F} \\ 19.00 \end{gathered}$ |  |  |  | $\begin{aligned} & 10 \mathrm{Ne} \\ & 20.183 \end{aligned}$ |
| III | $\begin{aligned} & 11 \mathrm{Na} \\ & 22.997 \end{aligned}$ |  | $\underset{24.32}{12 \mathrm{Mg}}$ |  | $\begin{aligned} & 13 \mathrm{Al} \\ & 26.98 \end{aligned}$ |  | $\begin{aligned} & 14 \mathrm{Si} \\ & 28.06 \end{aligned}$ |  | $\begin{aligned} & 15 \mathrm{P} \\ & 30.975 \end{aligned}$ |  | $\begin{aligned} & 16 \mathrm{~S} \\ & 32.066 \end{aligned}$ |  | $\begin{aligned} & 17 \mathrm{Cl} \\ & 35.457 \end{aligned}$ |  |  |  | $\begin{aligned} & 18 \mathrm{~A} \\ & 39.944 \end{aligned}$ |
| IV | $\begin{aligned} & 19 \mathrm{~K} \\ & 39.100 \end{aligned}$ | $\underset{63.54}{29 \mathrm{Cu}}$ | $\begin{aligned} & 20 \mathrm{Ca} \\ & 40.08 \end{aligned}$ | $\begin{aligned} & 30 \mathrm{Zn} \\ & 65.38 \end{aligned}$ | $\begin{array}{ll} \begin{array}{l} 21 \mathrm{Sc} \\ 44.96 \end{array} & \\ & \\ & 31 . \mathrm{Ga} \end{array}$ | $\begin{aligned} & 22 \mathrm{Ti} \\ & 47.90 \end{aligned}$ | $\begin{aligned} & 32 \mathrm{Ge} \\ & 72.60 \end{aligned}$ | $\begin{aligned} & 23 \mathrm{~V} \\ & 50.95 \end{aligned}$ | $\begin{aligned} & 33 \mathrm{As} \\ & 74.91 \end{aligned}$ | $\begin{aligned} & 24 \mathrm{Cr} \\ & 52.01 \end{aligned}$ | $\begin{aligned} & 34 \mathrm{Se} \\ & 78.96 \end{aligned}$ | $\begin{aligned} & 25 \mathrm{Mn} \\ & 54.93 \end{aligned}$ | $\begin{aligned} & 35 \mathrm{Br} \\ & 79.916 \end{aligned}$ | $\begin{aligned} & 26 \mathrm{Fe} \\ & 55.85 \end{aligned}$ | $\begin{aligned} & 27 \mathrm{Co} \\ & 58.94 \end{aligned}$ | $\begin{aligned} & 28 \mathrm{Ni} \\ & 58.69 \end{aligned}$ | $\begin{aligned} & 36 \mathrm{Kr} \\ & 83.80 \end{aligned}$ |
| v | $\begin{aligned} & 37 \mathrm{Rb} \\ & 85.48 \end{aligned}$ | $\begin{gathered} 47 \mathrm{Ag} \\ 107.880 \end{gathered}$ | $\begin{aligned} & 38.63 \end{aligned}$ | ${ }_{112.41}^{48 \mathrm{Cd}}$ | $\begin{array}{lr} 39 \mathrm{Y} & \\ 88.92 & 49 \mathrm{In} \\ & 114.76 \end{array}$ | $\begin{aligned} & 40 \mathrm{Zr} \\ & 91.22 \end{aligned}$ | $\begin{array}{r} 50 \mathrm{Sn} \\ 118.70 \end{array}$ | $\begin{aligned} & 41 \mathrm{Nb} \\ & 92.91 \end{aligned}$ | $\begin{array}{r} 51 \mathrm{Sb} \\ 121.61 \end{array}$ | $\begin{aligned} & 42 \mathrm{Mo} \\ & 95.95 \end{aligned}$ | $\begin{gathered} 52 \mathrm{Te} \\ 127.61 \end{gathered}$ | ${ }^{43} \mathbf{~} 99 \mathrm{Tc}$ | $\begin{array}{r} 531 \\ 126.91 \end{array}$ | $\begin{gathered} 44 \mathrm{Ru} \\ 101.7 \end{gathered}$ | $\begin{gathered} 45 \mathrm{Rh} \\ 102.91 \end{gathered}$ | ${ }_{106.7}^{46 \mathrm{Pd}}$ | $\underset{131.3}{54 \mathrm{Xe}}$ |
| VI | $\begin{array}{r} 55 \mathrm{Cs} \\ 132.91 \end{array}$ |  | $\begin{array}{r} 56 \mathrm{Ba} \\ 137.36 \end{array}$ |  | $\begin{aligned} & 57 \mathrm{La} \\ & 138.92 \\ & 58 \text { to } 71 \\ & \text { Rare carths * } \end{aligned}$ | $\begin{gathered} 72 \mathrm{Hf} \\ 178.6 \end{gathered}$ |  | $\begin{gathered} 73 \mathrm{Ta} \\ 180.88 \end{gathered}$ |  | $\begin{array}{r} 74 \mathrm{~W} \\ 183.92 \end{array}$ |  | $\begin{gathered} 75 \mathrm{Re} \\ 186.31 \end{gathered}$ |  | $\begin{array}{r} 76 \mathrm{Os} \\ 190.2 \end{array}$ | $\begin{gathered} 77 \mathrm{Ir} \\ 193.1 \end{gathered}$ | $\begin{gathered} 78 \mathrm{Pt} \\ 195.23 \end{gathered}$ |  |
|  |  | $\begin{gathered} \text { 79. Au } \\ 197.2 \end{gathered}$ |  | $\begin{gathered} 80 \mathrm{Hg} \\ 200.61 \end{gathered}$ | $\begin{array}{r} 81 \mathrm{Tl} \\ 204.39 \end{array}$ |  | $\begin{gathered} 82 \mathrm{~Pb} \\ 207.21 \end{gathered}$ |  | $\begin{array}{r} 83 \mathrm{Bi} \\ 209.00 \end{array}$ |  | ${ }_{210}^{84} \mathrm{Po}$ |  | $\begin{aligned} & 85 \mathrm{At} \\ & {[210]} \end{aligned}$ |  |  |  | ${ }_{222}^{86} \mathbf{R n}$ |
| VII | ${ }_{223}^{87 \mathrm{Fr}}$ |  | $\begin{gathered} 88 \mathrm{Ra} \\ 226.05 \end{gathered}$ |  | $\begin{aligned} & 89 \mathrm{Ac} \\ & 227 \\ & 90.103 \\ & \text { Actinide rare } \\ & \text { earths } \dagger \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |

[^252]TABLE 658.-ELECTRON CONFIGURATIONS OF THE ELEMENTS, NORMAL STATES *

|  | $K$ |  | $L$ |  | M |  |  | $N$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Js | $2 s$ | $2 p$ | $3 s$ | $3 p$ | $3 d$ | $4 s$ | 4p | $4 d$ | $\overline{5 s}$ |
| 1 H | 1 |  |  |  |  |  |  |  |  |  |
| 2 He | 2 |  |  |  |  |  |  |  |  |  |
| 3 Li | 2 | 1 |  |  |  |  |  |  |  |  |
| 4 Be | 2 | 2 |  |  |  |  |  |  |  |  |
| 5 B | 2 | 2 | 1 |  |  |  |  |  |  |  |
| 6 C | 2 | 2 | 2 |  |  |  |  |  |  |  |
| 7 N | 2 | 2 | 3 |  |  |  |  |  |  |  |
| 8 O | 2 | 2 | 4 |  |  |  |  |  |  |  |
| 9 F | 2 | 2 | 5 |  |  |  |  |  |  |  |
| 10 Ne | 2 | 2 | 6 |  |  |  |  |  |  |  |
| 11 Na | 2 | 2 | 6 | 1 |  |  |  |  |  |  |
| 12 Mg | 2 | 2 | 6 | 2 |  |  |  |  |  |  |
| 13 Al | 2 | 2 | 6 | 2 | 1 |  |  |  |  |  |
| 14 Si | 2 | 2 | 6 | 2 | 2 |  |  |  |  |  |
| 15 P | 2 | 2 | 6 | 2 | 3 |  |  |  |  |  |
| 16 S | 2 | 2 | 6 | 2 | 4 |  |  |  |  |  |
| 17 Cl | 2 | 2 | 6 | 2 | 5 |  |  |  |  |  |
| 18 A | 2 | 2 | 6 | 2 | 6 |  |  |  |  |  |
| 19 K | 2 | 2 | 6 | 2 | 6 |  | 1 |  |  |  |
| 20 Ca | 2 | 2 | 6 | 2 | 6 |  | 2 |  |  |  |
| 21 Sc | 2 | 2 | 6 | 2 | 6 | 1 | 2 |  |  |  |
| 22 Ti | 2 | 2 | 6 | 2 | 6 | 2 | 2 |  |  |  |
| 23 V | 2 | 2 | 6 | 2 | 6 | 3 | 2 |  |  |  |
| 24 Cr | 2 | 2 | 6 | 2 | 6 | 5 | 1 |  |  |  |
| 25 Mn | 2 | 2 | 6 | 2 | 6 | 5 | 2 |  |  |  |
| 26 Fe | 2 | 2 | 6 | 2 | 6 | 6 | 2 |  |  |  |
| 27 Co | 2 | 2 | 6 | 2 | 6 | 7 | 2 |  |  |  |
| 28 Ni | 2 | 2 | 6 | 2 | 6 | 8 | 2 |  |  |  |
| 29 Cu | 2 | 2 | 6 | 2 | 6 | 10 | 1 |  |  |  |
| 30 Zn | 2 | 2 | 6 | 2 | 6 | 10 | 2 |  |  |  |
| 31 Ga | 2 | 2 | 6 | 2 | 6 | 10 | 2 |  |  |  |
| 32 Ge | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 2 |  |  |
| 33 As | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 3 |  |  |
| 34 Se | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 4 |  |  |
| 35 Br | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 5 |  |  |
| 36 Kr | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 |  |  |
| 37 Rb | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 |  | 1 |
| 38 Sr | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 |  | 2 |
| 39 Y | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | , | 2 |
| 40 Zr | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 2 | 2 |
| 41 Nb | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 4 | 1 |
| 42 Mo | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 5 | 1 |
| 43 Tc | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 5 |  |
| 44 Ru | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 7 | 1 |
| 45 Rh | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 8 | 1 |
| 46 Pd | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 |  |

[^253](continued)

TABLE 658.-ELECTRON CONFIGURATIONS OF THE ELEMENTS, NORMAL STATES (concluded)

|  | K | $L$ |  |  | ${ }^{M}$ |  |  |  | $N$ |  |  | 0 |  |  |  | $P$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $1 s$ | $2 s$ | $2 p$ | 35 | 3p | $3 d$ | 4s | $4 p$ | $4 d$ | $4 f$ | $5 s$ | 5p | $5 d$ | $5 f$ | $6 s$ | 6p | $6 d$ | 7s |
| 47 Ag | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 |  | 1 |  |  |  |  |  |  |  |
| 48 Cd | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 |  | 2 |  |  |  |  |  |  |  |
| 49 In | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 |  | 2 | 1 |  |  |  |  |  |  |
| 50 Sn | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 |  | 2 | 2 |  |  |  |  |  |  |
| 51 Sb | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 |  | 2 | 3 |  |  |  |  |  |  |
| 52 Te | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 |  | 2 | 4 |  |  |  |  |  |  |
| 53 I | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 |  | 2 | 5 |  |  |  |  |  |  |
| 54 Xe | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 |  | 2 | 6 |  |  |  |  |  |  |
| 55 Cs | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 |  | 2 | 6 |  |  | 1 |  |  |  |
| 56 Ba | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 |  | 2 | 6 |  |  | 2 |  |  |  |
| 57 La | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 |  | 2 | 6 | 1 |  | 2 |  |  |  |
| 58 Ce | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 2 | 2 | 6 |  |  | 2 |  |  |  |
| 59 Pr | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 3 | 2 | 6 |  |  | 2 |  |  |  |
| 60 Nd | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 4 | 2 | 6 |  |  | 2 |  |  |  |
| 61 Pm | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 5 | 2 | 6 |  |  | 2 |  |  |  |
| 62 Sm | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 6 | 2 | 6 |  |  | 2 |  |  |  |
| 63 Eu | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 7 | 2 | 6 |  |  | 2 |  |  |  |
| 64 Gd | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 7 | 2 | 6 | 1 |  | 2 |  |  |  |
| 65 Tb | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 9 | 2 | 6 |  |  | 2 |  |  |  |
| 66 Dy | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 10 | 2 | 6 |  |  | 2 |  |  |  |
| 67 Ho | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 11 | 2 | 6 |  |  | 2 |  |  |  |
| 68 Er | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 12 | 2 | 6 |  |  | 2 |  |  |  |
| 69 Tm | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 13 | 2 | 6 |  |  | 2 |  |  |  |
| 70 Yb | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 |  |  | 2 |  |  |  |
| 71 Lu | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 1 |  | 2 |  |  |  |
| 72 Hf | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 2 |  | 2 |  |  |  |
| 73 Ta | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 3 |  | 2 |  |  |  |
| 74 W | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 4 |  | 2 |  |  |  |
| 75 Re | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 5 |  | 2 |  |  |  |
| 76 Os | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 6 |  | 2 |  |  |  |
| 77 Ir | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 7 |  | 2 |  |  |  |
| 78 Pt | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 9 |  | 1 |  |  |  |
| 79 Au | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 |  | 1 |  |  |  |
| 80 Hg | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 |  | 2 |  |  |  |
| 81 Tl | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 |  | 2 | 1 |  |  |
| 82 Pb | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 |  | 2 | 2 |  |  |
| 83 Bi | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 |  | 2 | 3 |  |  |
| 84 Po | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 |  | 2 | 4 |  |  |
| 85 At | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 |  | 2 | 5 |  |  |
| 86 Rn | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 |  | 2 | 6 |  |  |
| 87 Fr | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 |  | 2 | 6 |  | 1 |
| 88 Ra | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 |  | 2 | 6 |  | 2 |
| 89 Ac | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 |  | 2 | 6 | 1 | 2 |
| 90 Th | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 |  | 2 | 6 | 2 | 2 |
| 91 Pa | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 | 2 | 2 | 6 | 1 | 2 |
| 92 U | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 | 3 | 2 | 6 | 1 | 2 |
| 93 Np | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 | 4 | 2 | 6 | 1 | 2 |
| 94 Pu | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 | 5 | 2 | 6 | 1 | 2 |
| 95 Am | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 | 6 | 2 | 6 | 1 | 2 |
| 96 Cm | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 | 7 | 2 | 6 | 1 | 2 |
| 97 Bk | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 | 8 | 2 | 6 | 1 | 2 |
| 98 Cf | 2 | 2 | 6 | 2 | 6 | 10 | 2 | 6 | 10 | 14 | 2 | 6 | 10 | 9 | 2 | 6 | 1 | 2 |

TABLE 659.-RADII, IN ANGSTROM UNITS, OF THE ELECTRONIC ORBITS OF LIGHTER ELEMENTS ${ }^{203}$

|  | K | $L$ |  | M |  |  | $N$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Element | $1 s$ | $2 s$ | $2 p$ | $3 s$ | $3 p$ | ${ }^{3 d}$ | $4 s$ | $4 p$ |
| H | . 53 |  |  |  |  |  |  |  |
| He | . 30 |  |  |  |  |  |  |  |
| Li | . 20 | 1.50 |  |  |  |  |  |  |
| Be | . 143 | 1.19 |  |  |  |  |  |  |
| B | . 112 | . 88 | . 85 |  |  |  |  |  |
| C | . 090 | . 67 | . 66 |  |  |  |  |  |
| N | . 080 | . 56 | . 53 |  |  |  |  |  |
| O | . 069 | . 48 | . 45 |  |  |  |  |  |
| F | . 061 | . 41 | . 38 |  |  |  |  |  |
| Ne | . 055 | . 37 | . 32 |  |  |  |  |  |
| Na | . 050 | . 32 | . 28 | 1.55 |  |  |  |  |
| Mg | . 046 | . 30 | . 25 | 1.32 |  |  |  |  |
| A1 | . 042 | . 27 | . 23 | 1.16 | 1.21 |  |  |  |
| Si | . 040 | . 24 | . 21 | . 98 | 1.06 |  |  |  |
| P | . 037 | . 23 | . 19 | . 88 | . 92 |  |  |  |
| S | . 035 | . 21 | . 18 | . 78 | . 82 |  |  |  |
| Cl | . 032 | . 20 | . 16 | . 72 | . 75 |  |  |  |
| A | . 031 | . 19 | . 155 | . 66 | . 67 |  |  |  |
| K | . 029 | . 18 | . 145 | . 60 | . 63 |  | 2.02 |  |
| Ca | . 028 | . 16 | . 133 | . 55 | . 58 |  | 2.03 |  |
| Sc | . 026 | . 16 | . 127 | . 52 | . 54 | . 61 | 1.80 |  |
| Ti | . 025 | . 150 | . 122 | . 48 | . 50 | . 55 | 1.66 |  |
| V | . 024 | . 143 | . 117 | . 46 | . 47 | . 49 | 1.52 |  |
| Cr | . 023 | . 138 | . 112 | . 43 | . 44 | . 45 | 1.41 |  |
| Mn | . 022 | . 133 | . 106 | . 40 | . 41 | . 42 | 1.31 |  |
| Fe | . 021 | . 127 | . 101 | . 39 | . 39 | . 39 | 1.22 |  |
| Co | . 020 | . 122 | . 096 | . 37 | . 37 | . 36 | 1.14 |  |
| Ni | . 019 | . 117 | . 090 | . 35 | . 36 | . 34 | 1.07 |  |
| Cu | . 019 | . 112 | . 085 | . 34 | . 34 | . 32 | 1.03 |  |
| Zn | . 018 | . 106 | . 081 | . 32 | . 32 | . 30 | . 97 |  |
| Ga | . 017 | . 103 | . 078 | . 31 | . 31 | . 28 | . 92 | 1.13 |
| Ge | . 017 | . 100 | . 076 | . 30 | . 30 | . 27 | . 88 | 1.06 |
| As | . 016 | . 097 | . 073 | . 29 | . 29 | . 25 | . 84 | 1.01 |
| Se | . 016 | . 095 | . 071 | . 28 | . 28 | . 24 | . 81 | . 95 |
| Br | . 015 | . 092 | . 069 | . 27 | . 27 | . 23 | . 76 | . 90 |
| Kr | . 015 | . 090 | . 067 | . 25 | . 25 | . 22 | . 74 | . 86 |

${ }^{208}$ Slater, J. C., Introduction to chemical physics, 1939. Courtesy of McGraw-Hill Book Co.

TABLE 660.-ELEMENTAL ABUNDANCES IN THE UNIVERSE ${ }^{204}$
(Atoms per 10,000 atoms of $\mathrm{Si}^{*}$ )

| $Z$ | Element | Abundance | Source II | $z$ | Element | Abun. dance | Source | $Z$ | Element | Abundance | Source |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | H $\dagger$ | $3.5 \times 10^{8}$ | S | 29 | Cu | 4.6 | M | 58 | Ce | . 023 | M |
| 2 | $\mathrm{He}^{+}$ | $3.5 \times 10^{7}$ | S | 30 | Zn | 1.6 | M | 59 | Pr | . 0096 | M |
| 3 | Li | 1. |  | 31 | Ga | . 65 | M | 60 | Nd | . 033 | M |
| 4 | Be | . 2 |  | 32 | Ge | 2.5 | M | 61 | Pm |  |  |
| 5 | B | . 2 |  | 33 | As | 4.8 | M | 62 | Sm | . 012 | $\ddot{M}$ |
| 6 | C | 80,000 | S | 34 | Se | . 25 | M | 63 | Eu | . 0028 | M |
| 7 | N | 160,000 | S | 35 | Br | . 42 | M | 64 | Gd | . 017 | M |
| 8 | O | 220,000 | S | 36 | Kr $\ddagger$ |  |  | 65 | Tb | . 0052 | M |
| 9 | F | 90 | P | 37 | Rb | . 071 | M | 66 | Dy | . 020 | M |
| 10 | $\mathrm{Ne} \ddagger$ | 9,000-24,000 | $\mathrm{P}, \mathrm{Sc}$ | 38 | Sr | . 41 | M | 67 | Ho | . 0057 | M |
| 11 | Na | $462 \pm 36$ | M | 39 | Y | . 10 | M | 68 | Er | . 016 | M |
| 12 | Mg | $8,870 \pm 250$ | M | 40 | Zr | 1.5 | M | 69 | Tm | . 0029 | M |
| 13 | Al | $882 \pm 81$ | M | 41 | Nb | . 009 | M | 70 | Yb | . 015 | M |
| 14 | Si | 10,000 | M | 42 | Mo | . 19 | M | 71 | Lu | . 0048 | M |
| 15 | P | 130 | M | 43 | Tc |  |  | 72 | Hf | . 007 | M |
| 16 | S | 3500 | S | 44 | Ru | . 093 | M | 73 | Ta | . 0031 | M |
| 17 | Cl | 170 | P | 45 | R h | . 035 | M | 74 | W | . 17 | M |
| 18 | A $\ddagger$ | 130-2,200 | $\mathrm{P}, \mathrm{Pe}$ | 46 | Pd | . 032 | M | 75 | Re | . 0041 | M |
| 19 | K | $69.3 \pm 7.5$ | M | 47 | Ag | . 027 | M | 76 | Os | . 035 | M |
| 20 | Cas | $670 \pm 74$ | M, S | 48 | Cd | . 026 | M | 77 | Ir | . 014 | M |
| 21 | Sc | . 18 | M | 49 | In | . 01 | M | 78 | Pt | . 087 | M |
| 22 | Ti | $26.0 \pm 9.0$ | M | 50 | Sn | . 62 | M | 79 | Au | . 0082 | M |
| 23 | V | 2.5 | M | 51 | Sb | . 017 | M | 80 | Hg | ? | M |
| 24 | Cr | 95 | M | 52 | Te | ? | . | 81 | T1 | ? | M |
| 25 | Mn | 77 | M | 53 | I | . 02 |  | 82 | Pb | . 27 | M |
| 26 | Fe | 18,300 | M | 54 | Xe $\ddagger$ |  | M | 83 | Bi | . 0021 | M |
| 27 | Co | + 99 | M | 55 | Cs | . 001 | M | 90 | Th | . 012 | M |
| 28 | Ni | 1,340 | M | 56 | Ba | . 039 | M | 92 | U | . 0026 | M |
|  |  |  |  | 57 | La | . 021 | M |  |  |  |  |

${ }^{204}$ Brown and Harrison, Rev. Mod. Phys., vol. 21, p. 625, 1949.

* Silicon is 12.3 percent by weight in meteorites. p. $\dagger$ The hydrogen-helium ratio and the ratio of hydrogen and helium to the "oxygen group" elements ( $\mathrm{C}, \mathrm{N}, \mathrm{O}, \mathrm{Ne}, \mathrm{Fe}$ ) are those computed by J. Greenstein and reported by M. Harrison, Astrophys. Journ., vol. 108, p. 310, 1940. $\ddagger$ See Table 663. \& Stellar and meteoritic values have been combined by equalizing the calcium abundances. I| The letters $\mathrm{S}, \mathrm{P}, \mathrm{Sc}, \mathrm{Pe}$, and M desig. nate the sources chosen (solar, planetary nebulae, $\tau$-Scorpii, $\gamma$ Pegasi, or meteoritic).

TABLE 661.-ABUNDANCE OF ELEMENTS IN OUR PLANET GIVEN IN PERCENTAGE BY WEIGHT*

| Element | $\begin{gathered} \text { Earth } \\ \text { crust } \end{gathered}$ | Earth | Lithosphere, $\dagger$ <br> hydrosphere, atmosphere | Element | $\begin{gathered} \text { Earth } \\ \text { crust } \end{gathered}$ | Earth | Lithosphere, $\dagger$ hydrosphere, atmosphere |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| O | 46.6 | 24.4 | 49.38 | P | ... | . 17 | . 12 |
| Si | 27.7 | 12.2 | 25.8 | C | ... | . 07 | . 17 |
| Al | 8.1 | 1.0 | 7.5 | Cl | ... | . 05 | . 19 |
| Fe | 5.0 | 45.6 | 4.66 | H | $\ldots$ | . 04 | . 87 |
| Ca | 3.63 | 1.2 | 3.34 | Cu | $\ldots$ | . 01 | . 01 |
| Na | 2.8 | . 47 | 2.55 | Zn | ... | . 0005 | . 03 |
| K | 2.16 | . 12 | 2.38 | As | $\cdots$ | . 01 |  |
| Mg | 2.1 | 9.4 | 2.07 | $\stackrel{\mathrm{Ba}}{ }$ |  | ... | . 04 |
| Ti | . 4 | . 06 | . 61 | F | ... | ... | . 04 |
| Mn | . 1 | . 19 | . 09 | N | $\cdots$ | ... | . 03 |
| Ni |  | 3.41 | . 01 | Zr | ... | ... | . 02 |
| S |  | 1.08 | . 07 | V | ... | ... | . 02 |
| Co |  | . 26 | . 002 | Sr | $\ldots$ | ... | . 02 |
| Cr |  | . 22 | . 03 |  |  |  |  |

[^254]TABLE 662.-CHEMICAL COMPOSITION OF EARTH—METEORITES AND SOLAR ATMOSPHERE * 205

The table gives $\log N H$, where $N H=$ the number of atoms, neutral and ionized, per $\mathrm{cm}^{3}$. Constants added to data of Russell and Brown to give order of magnitude agreement with Unsöld. : indicates less accuracy; ? origin doubtful.

H and He are about 97 percent of the total solar mass, the oxygen group 2.7 percent, the metals 0.3 percent ; and by numbers of atoms 99 percent, 0.9 percent, and 0.1 percent respectively.

The level of ionization in the solar atmosphere is such that atoms of $I P=8.33 \mathrm{ev}$ are 50 percent ionized; ionization temperature $=5676^{\circ} \mathrm{K}$; electron pressure $\approx 32 \mathrm{bar}$; 85 percent of free electrons come from $\mathrm{Mg}, \mathrm{Si}, \mathrm{Fe}$, according to Unsöld.

| Element | Earth. meteorite $\dagger$ | Sun $\ddagger$ | Sun 8 | Element | Earth meteorite $\dagger$ | Sun $\ddagger$ | Sun § |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 H | 18.04 | 22.1 | 24.13 | 41 Nb | 13.05 | 12.6: |  |
| 2 He | ... | 20.6? |  | 42 Mo | 14.38 | 13.0 | 13.40 |
| 3 Li | 14.91 | 13.6: |  | 44 Ru | 14.07 | 13.3 |  |
| 4 Be | 14.23 | 13.4 | . . . . | 45 Rh | 13.64 | 12.1 |  |
| 5 B | 14.72 | 16.6: |  | 46 Pd | 13.61 | 12.7 |  |
| 6 C | 17.22 | 19.1 | 19.91 | 47 Ag | 13.53 | 126 |  |
| 7 N | 15.01 | 19.6: | 20.23 | 48 Cd | 13.52 | 13.8 : |  |
| 8 O | 19.64 | 20.6 | 20.35 | 49 In | 13.10 | 11.6: |  |
| 9 F | 15.48 | 17.6: | . . . | 50 Sn | 14.89 | 12.8? |  |
| 10 Ne |  |  |  | 51 Sb | 13.33 | 12.4 : |  |
| 11 Na | 17.76 | 18.8 | 17.90 | 53 I | 13.35 |  |  |
| 12 Mg | 19.05 | 18.9 | 19.13 | 55 Cs | 12.10 | ? |  |
| 13 Al | 18.04 | 18.0 | 17.95 | 56 Ba | 13.69 | 14.9 | 14.57 |
| 14 Si | 19.10 | 19.1 | 18.91 | 57 La | 13.42 | 13.4 |  |
| 15 P | 17.21 | 15.6: |  | 58 Ce | 13.46 | 14.0 |  |
| 16 S | 17.98 | 17.3 : | 18.54 | 59 Pr | 13.08 | 12.2 : |  |
| 17 Cl | 16.63 |  |  | 60 Nd | 13.62 | 13.6 |  |
| 18 A |  |  |  | 62 Sm | 13.18 | 13.1 |  |
| 19 K | 16.94 | 18.4 : | 16.82 | 63 Eu | 12.55 | 13.0 : |  |
| 20 Ca | 17.93 | 183 | 17.85 | 64 Gd | 13.33 | 12.7 : |  |
| 21 Sc | 14.36 | 15.2 | 14.95 | 65 Tb | 12.82 |  |  |
| 22 Ti | 16.52 | 16.8 | 16.58 | 66 Dy | 13.40 | 13.2 : |  |
| 23 V | 15.50 | 16.6 | 15.67 | 67 Ho | 12.85 |  |  |
| 24 Cr | 17.80 | 17.3 | 17.20 | 68 Er | 13.30 | 11.7: |  |
| 25 Mn | 16.99 | 17.5 | 17.08 | 69 Tm | 12.56 | 12.1: |  |
| 26 Fe | 19.37 | 18.8 | 19.34 | 70 Yb | 13.28 | 12.6: |  |
| 27 Co | 17.10 | 17.2 | 16.65 | 71 Lu | 12.78 | 12.6 : |  |
| 28 Ni | 18.23 | 17.6 | 17.57 | 72 Hf | 12.94 | 12.0 |  |
| 29 Cu | 15.76 | 16.6 | 15.85 | 73 Ta | 12.59 | 11.6 : |  |
| 30 Zn | 15.30 | 16.5 | 16.40 | 74 W | 14.33 | 11.8 |  |
| 31 Ga | 14.91 | 13.6 : |  | 75 Re | 12.71 |  |  |
| 32 Ge | 15.50 | 14.6 |  | 76 Os | 13.64 | 12.1 : |  |
| 33 As | 15.78 |  |  | 77 Ir | 13.25 | 11.4? |  |
| 34 Se | 14.50 |  |  | 78 Pt | 14.04 | 13.2 |  |
| 35 Br | 14.72 |  |  | 79 Au | 13.01 |  |  |
| 37 Rb | 13.95 | 13.3 : |  | 82 Pb | 14.53 | 12.8 | 14.2 |
| 38 Sr | 14.71 | 14.9 | 14.97 | 83 Bi | 12.42 |  |  |
| 39 Y | 14.10 | 14.2 | 14.83 | 90 Th | 13.18 |  |  |
| 40 Zr | 15.28 | 14.1 | 13.99 | 92 U | 12.51 |  |  |

[^255]
## TABLE 663.-COSMIC ABUNDANCES OF THE RARE GASES*

As estimated by interpolation of the abundance curves (abundances in atoms per 10,000 atoms of silicon).

|  | Isotope used <br> for inter- <br> polation | Estimated <br> ahundance <br> of isotope | Estimated <br> abundance <br> of element | Gas | Isotone used <br> for inter- <br> polation | Estimated <br> abundance <br> of isotope |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Ne | $\mathrm{Ne}^{21}$ | 100 | 37,000 | Kr | $\mathrm{Kr}^{\text {Estimated }}$ahundance <br> of element |  |
| A | $\mathrm{A}^{36}$ | 1000 | 1,000 | Xe | $\mathrm{Xe}^{181}$ | .004 |

[^256]Part 1.-Approximate counts of atomic lines identified in solar and sunspot spectra ${ }^{200}$

| $\underbrace{\text { Neutral }}$ atoms |  |  |  |  |  |  |  | Singly ionized atoms |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Disk |  |  |  | $\underbrace{\text { Spot }}$ |  |  |  | ${ }^{\text {Disk }}$ |  |  |
|  |  | $\overbrace{}^{\text {No. lines ** }}$ |  |  | No. $\overbrace{\text { lines }}$ |  |  |  | No. lines |  |  |
| $\begin{aligned} & \text { ® } \\ & \stackrel{4}{4} \end{aligned}$ |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{y y} \\ & \stackrel{E}{E} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\underline{x}} \\ & \stackrel{x}{\mu} \end{aligned}$ |  |  | $\begin{aligned} & . \vec{B} \\ & \times \\ & \stackrel{x}{\approx} \end{aligned}$ | $\stackrel{\stackrel{\rightharpoonup}{5}}{\stackrel{y}{E}}$ |  |  |  |
| 1 | $\mathrm{H}^{\dagger}$ | 9 |  | 40 |  |  | 25 ? |  |  |  |  |
| 2 | Hei ${ }^{\dagger}$ | 1 |  | 5 |  |  | 5 |  |  |  |  |
| 3 | LiI | 2 |  | -3 |  |  | 3 |  |  |  |  |
| 4 | Bei | 2 |  | -3 |  |  |  |  |  |  |  |
| 5 | B $\ddagger$ |  |  |  |  |  |  | Beir | 2 |  | 1 |
| 6 | $\mathrm{C}_{1}$ | 41 | 7 | 12 |  |  | 10 |  |  |  |  |
| 7 | N I | 8 | 6 | -1 |  |  | -2 |  |  |  |  |
| 8 | OI | 12 | 1 | 5 |  |  | 1 |  |  |  |  |
| 9 | F |  |  |  |  |  |  |  |  |  |  |
| 11 | Na 1 | 21 | 6 | 30 |  |  | 70? |  |  |  |  |
| 12 | Mg I | 55 | 4 | (200) |  |  | 30 | Mg II | 12 | 2 | (1000) |
| 13 | Ali | 22 | 5 | 20 |  |  | 25 |  |  |  |  |
| 14 | Sil | 156 | 29 | (80) |  |  | 12 |  |  |  |  |
| 15 | P I | 6 | 1 | 1 |  |  |  | Si II | 4 | 2 | 2 |
| 16 | SI | 31 | 10 | 8 |  |  | 2 |  |  |  |  |
| 19 | K I | 4 | 3 | 12 |  |  | 20 |  |  |  |  |
| 20 | CaI | 108 | 21 | 20 |  |  | 40 |  |  |  |  |
| 21 | Sci | 43 | 14 | 2 | 15 | 1 | 7 | Ca II | 25 |  | 1000 |
| 22 | Til | 687 | 264 | 7 | 134 | 2 | 10 | Scin | 57 | 26 | 6 |
| 23 | V I | 272 | 133 | 4 | 53 | 2 | 8 | Ti II | 255 | 119 | 12 |
| 24 | $\mathrm{Cr}{ }^{\text {I }}$ | 776 | 305 | 10 | 23 |  | 12 | V II | 160 | 103 | 5 |
| 25 | Mn I | 185 | 73 | 7 | 1 |  | 12 | Crif | 216 | 133 | 6 |
| 26 | Fe 1 | 4164 | 877 | 40 | 2 |  | 35 | Mnil | 16 | 11 | 6 |
| 27 | Cor | 501 | 209 | 6 | 7 |  | 6 | Feil | 371 | 140 | 6 |
| 28 | Nir | 617 | 180 | 25 |  |  | 9 | Coir | 6 | 7 | 0 |
| 29 | Cu | 14 | 3 | 10 |  |  | 7 | Ni ir | 13 | 8 | 3 |
| 30 | Zn I | 9 | 3 | 3 |  |  | 1 |  |  |  |  |
| 31 | Ga I | 1 | 1 | 1 |  |  | 2 |  |  |  |  |
| 32 | Ge I | 5 |  | 3 |  |  |  |  |  |  |  |
| 37 | RbI | 1 |  | -3 | 1 |  | 4 |  |  |  |  |
| 38 | Sri | 13 | 2 | 1 | 6 |  | 3 | Sr ${ }^{11}$ | 8 | 2 | 9 |
| 39 | Y I | 17 | 10 | 0 | 12 | 1 | 3 | Y II | 53 | 18 | 3 |
| 40 | Zri | 59 | 41 | 0 | 41 |  | 3 | Zrin | 148 | 93 | 3 |
| 41 | Nb I | 4 | 2 | -1 |  |  |  | Nb II | 13 | 8 | -1 |
| 42 | Moi | 8 | 6 | -2 |  |  |  | Moir | 7 | 5 | 0 |
| 44 | Ru 1 | 15 | 5 | -1 |  |  |  |  |  |  |  |
| 45 | Rhi | 8 | 3 | -2 |  |  |  | Rhin? | 3 | 2 | -2 |
| 46 | Pd | 8 | 7 | 0 |  |  |  |  |  |  |  |
| 47 | Ag I | 3 |  | 0 |  |  |  |  |  |  |  |
| 48 | Cdi | 1 |  | -1 |  |  |  |  |  |  |  |
| 49 | In I | 1 |  | -2 |  |  | -1 |  |  |  |  |
| 50 | Sn I | 2 | 2 | -2 |  |  |  |  |  |  |  |
| 51 | Sb I | 1 | 1 | $-3 \mathrm{~N}$ |  |  |  |  |  |  |  |
| 56 | BaI |  |  |  | 1 |  | 1 | Ba II | 6 | 3 | 8 |

[^257](continued)

TABLE 664.-66 KNOWN ELEMENTS IN THE SUN'S ATMOSPHERE (concluded)

| Neutral atoms |  |  |  |  |  |  |  | Singly ionized atoms |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Disk |  |  | $\underbrace{\text { Spot }}$ |  |  |  | $\underbrace{\text { Disk }}$ |  |  |
|  |  | No. lines |  |  | $\overbrace{}^{\text {No. }}$ lines |  |  |  | $\underbrace{\text { No. lines }}$ |  |  |
| $\begin{aligned} & \text { 艺 } \\ & \text { 4 } \end{aligned}$ | $\begin{aligned} & \text { 号 } \\ & \text { E } \\ & \underline{y} \end{aligned}$ | تِ $\stackrel{\rightharpoonup}{E}$ $\stackrel{0}{0}$ $\stackrel{0}{5}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{E} \\ & \stackrel{\rightharpoonup}{x} \\ & \text { añ } \end{aligned}$ |  |  | $\begin{aligned} & \ddot{E} \\ & \times \\ & \stackrel{x}{\pi} \end{aligned}$ |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\tilde{E}} \\ & \stackrel{ت}{E} \end{aligned}$ |  |
| 57 | La I |  |  |  | 1 |  | -2 N | La in | 44 | 20 | 1 |
| 58 |  |  |  |  |  |  |  | Ceir | 106 | 81 | 0 |
| 59 |  |  |  |  |  |  |  | PriI | 11 | 16 | -1 |
| 60 |  |  |  |  |  |  |  | Nd ii | 74 | 72 | 1 |
| 62 |  |  |  |  |  |  |  | Smil | 82 | 63 | 0 |
| 63 | EuI |  |  | 2 |  |  | -1 | Eu II | 10 | 4 | 1 |
| 64 |  |  |  |  |  |  |  | Gd II | 29 | 20 | 0 |
| 65 |  |  |  |  |  |  |  | Tbir? | 2 | 2 | -1 |
| 66 |  |  |  |  |  |  |  | Dy 11 | 29 | 25 | 1 |
| 68 |  |  |  |  |  |  |  | EriI | 2 |  | -1 |
| 69 |  |  |  |  |  |  |  | Tm Ii? | 6 | 5 | -1 |
| 70 | Yb I | 2 |  | 0 |  |  | 1 | Ybil |  | 2 | 3 ? |
| 71 |  |  |  |  |  |  |  | Luil? | 1 | 4 | $-3$ |
| 72 | Hf I |  | 1 | -3 |  |  |  | Hf in | 13 | 5 | -1 |
| 73 | Ta I? | 3 |  | -2 |  |  |  |  |  |  |  |
| 74 | W i | 13 | 8 | -1 |  |  | -1 |  |  |  |  |
| 76 | Os I | 2 | 4 ? | 0 |  | 1 | -1 |  |  |  |  |
| 77 | Ir I | 2 | 4 | -2 |  |  |  |  |  |  |  |
| 78 | Pt I | 3 |  | 2 |  |  |  |  |  |  |  |
| 79 | Aul | 1 |  | -3 |  |  | -2 |  |  |  |  |
| 82 | Pb 1 | 2 |  | -2 |  |  |  |  |  |  |  |
| 90 | Thi | 1 |  | -1 |  |  |  |  |  |  |  |

Part 2.—Molecules in the sun-18 present (either disk or spot spectrum, or both) ${ }^{207}$

| OH | Mg H | Sc O | CH | Mg O | Y O |
| :--- | :--- | :--- | :--- | :--- | :--- |
| NH | $\mathrm{C}_{2}$ | $\mathrm{A1} \mathrm{O}$ | Cn | CaH | MgF |
| $\mathrm{O}_{2}$ | Ti O | ZrO | Si H | BH | SrF |

[^258]
## TABLE 665.-ABUNDANCES OF LIGHT ELEMENTS IN EARLY TYPE STARS

The table gives the number of atoms per 1000 atoms oxygen for $\tau$ Scorpii, spectrum $d B o^{208} ; 10$ Lacertae, $O ;{ }^{209} ; \gamma$ Pegasi, $B 2.5$ IV ${ }^{200}$; mean for $8 B$-stars, weighted mean by Aller, ${ }^{200}$ the last 3 columns from letters to the editor, 1950. : less certain.

| Element | $\tau$ Sco | 10 Lac | $\gamma \mathrm{Peg}$ | 8 B-stars | Mean |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 H | $10 \times 10^{5}$ | $20 \times 10^{5}$ | $87 \times 10^{5}$ | .... | $20 \times 10^{5}$ |
| 2 He | $1.8 \times 10^{5}$ | $1.68 \times 10^{5}$ | $5.5 \times 10^{5}$ : |  | $1.7 \times 10^{5}$ |
| 6 C | 170 | 200 | 120 | 150 | 160 |
| 7 N | 380 | 220 | 200 | 230 | 250 |
| 80 | 1000 | 1000 | 1000 | 1000 | 1000 |
| 10 Ne | 1100 | 880 |  |  | 1000 |
| 12 Mg | 59 | 62 | 310 | 93 | 120 |
| 13 Al | 3.7 |  | 11 | 4.2 | 6 |
| 14 Si | 64 | 82 | 90 | 38 | 60 |
| 15 P |  |  | 1.1 |  | 1.1 |
| 16 S | ..... |  | 40 | 22 | 30 |
| 17 Cl |  |  | 20 : |  | 20 : |
| 18 A | $\ldots$ | .... | $100:$ |  | 100 : |

[^259]The gases that have been detected are listed together with the means of detection and approximate abundances. Both the observations and the application of ionization theory introduce considerable uncertainty in the determination of abundances. Values given are the best current estimates. In general, the composition of the interstellar gas appears to be the same as for the stars.

| Gas | Density in clouds atoms $/ \mathrm{cm}$ | Detection | Gas | $\begin{gathered} \text { Density } \\ \text { in clouds } \\ \text { atoms } / \mathrm{cm}^{3} \end{gathered}$ | Detection |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Hydrogen | 10 | Emission lines | Titanium | $10^{-8} \dagger$ | Absorption lines |
| Oxygen | . 01 | Emission lines | Nitrogen |  | N emission, CN ab- |
| Carbon | . 003 | Molecular absorption lines | Potassium | $10^{-5} \dagger$ | sorption lines Absorption lines |
| Calcium | $2 \times 10^{-8}$ | Absorption lines | Sulfur |  | Emission lines |
| Sodium | $4 \times 10^{-5}$ | Absorption lines | CH | $10^{-6} \dagger$ | Absorption lines |
| Iron |  | Absorption lines | CN | $10^{-8} \dagger$ | Absorption lines |

The interstellar gas is strongly concentrated in clouds as evidenced by the multiplicity of interstellar absorption lines. Stromgren suggests density between clouds is about $1 \%$ of that in clouds.

[^260]TABLE 667.-THE ABUNDANCE OF CERTAIN ELEMENTS IN THE NEBULAE ${ }^{211}$
(Given as the exponent of 10 )

| Element | Abundance | Element | Abundance | Element | Abundance | Element | Abundance | Element | Abundance |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| H | 11- | C | 9 | Na | . $27+$ | S | 8 | Sc | . $<6+$ |
| He | 10 | N | 9- | Mg | $7+$ | Cl | $7+$ | Ti | 7 - |
| Li | . $<8$ - | O | 9 | Al | . <8- | A | 7 | V |  |
| Be | . $<8$ - | F | 6 | Si | . $<9$ | K | 6+ | Cr | 7 |
| B | $<9$ | Ne | 8 | P | . $<8$ - | Ca | 7- | Mn |  |

${ }^{211}$ Bowen and Wyse, Lick Obs. Bull., vol. 19. p. 1. 1939.

## TABLE 668.-MATTER IN INTERSTELLAR SPACE * 212

The interpretation of the interstellar absorption curve and of absorption by dark clouds requires the presence of small grains with radii ranging around $10^{-5} \mathrm{~cm}$. Polarization of starlight indicates that some, if not all, grains are elongated. Composition, from absorption curve and scattering appears to be mainly dielectric.

## Density of matter

| Solid grains: |  |
| :---: | :---: |
| Uniform region, abs $0.5 \mathrm{~m} / \mathrm{kpc}$ | $10^{-28} \mathrm{~g} / \mathrm{cm}^{3}$ |
| Large cloud, abs 1 mag ( $10 \mathrm{~m} / \mathrm{kpc}$ ) | $10^{-25} \mathrm{~g} / \mathrm{cm}^{3}$ |
| Dense condensation, abs 5-10 m ( $1000 \mathrm{~m} / \mathrm{kpc}$ ) | $10^{-28} \mathrm{~g} / \mathrm{cm}^{3}$ |
| Mean density, gas and grains. | $3 \times 10^{-24} \mathrm{~g} / \mathrm{cm}^{3}$ |
| Oort limit (Max density, stars plus diffuse matter) | $6 \times 10^{-24} \mathrm{~g} / \mathrm{cm}^{3}$ |
| Mean space density of stellar matter. | $3 \times 10^{-24} \mathrm{~g} / \mathrm{cm}^{3}$ |

[^261]Colloidal science originally dealt with that large field of small particles, but now it has been extended to cover also those materials that are small in one or two of the three dimensions. Thus, this field now includes chain molecules and films as well as the fine particles.

The diameters of atoms range from 2 to $3 A$ (angstroms) while diameters of ordinary inorganic molecules extend from about 7 to $10 A$. Organic molecules are much larger and their dimensions may extend to $20 A$ or larger. It is sometimes stated that colloid particles range in diameter from $20 A$ to a much larger value but it must be remembered that it is difficult to fix such dimensions.

Many of the properties of colloids are due to their relatively very great surface as compared with their volumes. Some of the newer experimental tools, i.e., ultracentrifuges, X-rays, and the electron microscopes, have been a great help in studying these particles and their reactions. Several tables follow that give properties and characteristics of colloids and colloidal particles.

## TABLE 669.-BROWNIAN MOVEMENT

The Brownian movement is a microscopically observed agitation of colloidal particles. It is caused by the bombardment of them by the molecules of the medium and may be used to determine the value of Avogadro's number. Perrin, Chaudesaignes, Ehrenhaft, and De Broglie found, respectively, 70, 64,63 and $64 \times 10^{22}$ as the value of this constant. The following table indicates the size and the dependence of this movement on the magnitude of the particles.

| Material | Diameter $\times 10^{5} \mathrm{~cm}$ | Medium | ${ }^{\text {Temp }}{ }^{\text {C }}$ | $\begin{aligned} & \text { Velocity } \\ & \times 10^{\circ} \mathrm{cm} / \mathrm{sec} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| Dust particles | 2.0 | Water |  | none |
| Gold | . 35 |  | 20 ? | 200. |
| Gold | . 1 | " |  | 280. |
| Gold | . 06 | " | " | 700. |
| Platinum | . 4 to .5 | Acetone | 18 | 3900. |
| Platinum | . to . 5 | Water | 20 | 3200. |
| Rubber emuls | 10. |  | 17 | 124. |
| Mastic | 10. | " | 20? | 1.55 |
| Gamboge | 4.5 | " | 20 | 2.4 |
|  | 2.13 | " | " | 3.4 |

The movement varies inversely as the size of the particles; in water, particles of diameter greater than $4 \mu$ show no perceptible movement; when smaller than $.1 \mu$, lively movement begins, while at $10 m \mu$ the trajectories amount to up to $20 m \mu$.

TABLE 670.-PARTICLE SIZES OF SOME INDIVIDUAL DUSTS ${ }^{212 a}$

| Dust | Diameter, cm |
| :---: | :---: |
| Milk powder (by evaporation of fine spray) | $1.4 \times 10^{-2}-.7 \times 10^{-2}$ |
| Fine powder ( 300 mesh) e.g., cement...... | $1 \times 10^{-2}-.7 \times 10^{-2}$ |
| Smelter fumes | $1 \times 10^{-2}-1 \times 10^{-5}$ |
| Atmosphere, fog particles | $1.4 \times 10^{-3}-3.5 \times 10^{-3}$ |
| Cement kiln flue dust.. | $6 \times 10^{-3}-.8 \times 10^{-8}$ |
| $\mathrm{H}_{2} \mathrm{SO}_{4}$ mist from concentrators | $1.1 \times 10^{-3}-1.6 \times 10^{-4}$ |
| $\mathrm{NH}_{4} \mathrm{Cl}$ fumes | $1 \times 10^{-4}-1 \times 10^{-5}$ |
| Oil sinoke | $1 \times 10^{-4}-5 \times 10^{-8}$ |
| Resin smoke | $1 \times 10^{-4}-1 \times 10^{-6}$ |
| Tobacco smoke | $1.5 \times 10^{-5}-1 \times 10^{-6}$ |

[^262]$M$, molecular weight; $f / f_{0}$, dissymmetry constant ; $a$, short diameter; $b$, long diameter.

| Substance | M | $f / f_{0}$ | $b / a$ | a (A) | $b$ (A) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Zein | 35000 | 2.0 | 20.1 | 16 | 322 |
| Cytochromec C | 15600 | 1.3 | 5.8 | 18 | 98 |
| Gliadin | 26000 | 1.6 | 11.1 | 18 | 196 |
| Hordein | 27500 | 1.6 | 11.1 | 18 | 196 |
| Erythrocruorin (chironimus) | 31400 | 1.6 | 11.1 | 19 | 208 |
| Serum albumin, urea denatured. | 67100 | 1.98 | 19.4 | 20 | 356 |
| Lactalbumin a | 17500 | 1.2 | 4.3 | 21 | 91 |
| Erythrocruorin (lampetra) | 17100 | 1.2 | 4.3 | 22 | 94 |
| Bence-Jones $\beta$......... | 37700 | 1.3 | 5.8 | 25 | 144 |
| Myoglobin | 17200 | 1.1 | 2.9 | 24 | 70 |
| Crotoxin | 30000 | 1.2 | 4.3 | 25 | 109 |
| Concanavalin B | 42000 | 1.3 | 5.8 | 26 | 149 |
| Tuberculin protein | 32000 | 1.2 | 4.3 | 26 | 112 |
| Lactoglobulin .... | 41800 | 1.2 | 4.3 | 28 | 122 |
| Pepsin . . | 35500 | 1.08 | 2.7 | 31 | 84 |
| Insulin | 40900 | 1.13 | 3.3 | 31 | 102 |
| Egg albumin | 40500 | 1.1 | 2.9 | 32 | 91 |
| Hemoglobin (horse) | 69000 | 1.24 | 4.8 | 32 | 155 |
| Serum albumin (horse) | 67100 | 1.2 | 4.3 | 34 | 145 |
| Yellow ferment | 82800 | 1.2 | 4.3 | 36 | 152 |
| Canavalin | 113000 | 1.3 | 5.8 | 36 | 207 |
| Serum globulin | 167000 | 1.4 | 7.5 | 37 | 280 |
| Diphtheria toxin | 72000 | 1.2 | 4.3 | 34 | 145 |
| Antipneumococcus serum globulin (rabbit) | 157000 | 1.4 | 7.5 | 37 | 274 |
| Antipneumococcus serum globulin (man). | 195000 | 1.5 | 9.2 | 37 | 338 |
| Concanavalin A . . . . . . . . . . . . . . . . . . . | 96000 | 1.1 | 2.9 | 43 | 124 |
| Erythrocruorin (arc a) | 33600 | 1.0 | 1. | 43 | 43 |
| Bence-Jones a ........ | 35000 | 1.0 | 1. | 43 | 43 |
| Catalase .... | 248000 | 1.3 | 5.8 | 46 | 297 |
| Antipneumococcus serum globulin (horse) | 920000 | 2.0 | 20.1 | 47 | 950 |
| Phycoerythrin (seramium) ............... | 290000 | 1.2 | 4.3 | 54 | 232 |
| Amandin ............... | 329000 | 1.3 | 5.8 | 51 | 291 |
| Tyroglobulin | 628000 | 1.5 | 9.2 | 54 | 498 |
| Edestin .... | 309000 | 1.2 | 4.3 | 55 | 237 |
| Excelsin | 294000 | 1.1 | 2.9 | 62 | 179 |
| Urease | 483000 | 1.2 | 4.3 | 64 | 274 |
| Hemocyanin (palinurus) | 446000 | 1.2 | 4.3 | 62 | 268 |
| Tobacco mosaic virus.. | 60000000 | 3.0 |  |  |  |
| Legumin | 208000 | 1.02 |  |  |  |

[^263]TABLE 672.-INFLUENCE OF PARTICLE SIZE UPON SOLUBILITY ${ }^{214}$

| Material | Size of particles ${ }^{\mu}$ | Solubility at $25^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: |
| CaSO | 2.0 | 2.085 g per liter* |
|  | . 3 | 2.476 g per liter |
| BaSO4 | 1.8 | 2.29 mg per liter * |
|  | . 1 | 4.15 mg per liter |
| HgO | Coars | 50 mg per liter * |

[^264](In small calories)

| Substance | Fuller's earth | Bone charcoal | Kaolin | Dispersive power percent |
| :---: | :---: | :---: | :---: | :---: |
| Amylene | 57.1 |  | 78.8 | 1.54 |
| Water . | 30.2 | 18.5 |  | 2.82 |
| Acetone | 27.3 | 19.3 |  | 1.72 |
| Methyl alcohol | 21.8 | 17.6 | 27.6 | 1.60 |
| Ethyl acetate | 18.5 | 16.5 |  | 1.05 |
| Ethyl alcohol | 17.2 | 16.5 | 24.5 | ... |
| Aniline | 13.4 |  |  | . . |
| Amyl alcohol | 10.9 | 10.6 | 20.4 |  |
| Ethyl ether | 10.5 |  |  | . 90 |
| Chloroform | 8.4 | 14.0 | 15.7 | . 86 |
| Benzene | 4.6 | 11.1 | 9.9 | . 39 |
| Carbon disulfide | 4.6 | 8.4 | 9.9 |  |
| Carbon tetrachloride | 4.2 | 13.9 | 9.4 | . 27 |
| Hexane | 3.9 | 8.9 | 7.2 | . 22 |

* For reference, see footnote 214 , p. 631.


# TABLE 674.-EFFECT OF ACTIVATION ON THE ADSORBING POWER OF CHARCOAL ${ }^{215}$ 

| Substance tested | Adsorption $\mathrm{mg} \mathrm{CCl} 4 /(\mathrm{g} \mathrm{C})$ | Granular density | Physical character |
| :---: | :---: | :---: | :---: |
| Ironwood | 22 | . 96 | Fibrous, hard |
| Primary ironwood charcoal | 30 | . 89 | Hard |
| Activated ironwood charcoal | 1160 | . 72 | Hard, friable, granular |
| Commercial wood charcoal | 11 | . 46 | Firm, fibrous |
| Highest activated wood charcoal * | . 1480 | . 30 | Soft, friable |
| Cocoanut shell .... | 18 | 1.20 | Hard |
| Primary cocoanut charcoal | 47 | . 96 | Hard |
| Activated cocoanut charcoal. | . 630 | . 84 | Hard |
| Lignite semi-coke | 30 | 1.09 | Firm |
| Good activated lignite charcoal | 640 | . 89 | Firm |
| Highest activated lignite charcoal * | . 2715 | . 31 | Friable, granular |

[^265]TABLE 675. -HEATS OF ADSORPTION OF VAPORS ON CHARCOAL*

|  | Vapor | Integral heat of adsorption, $\stackrel{h}{\text { cal/mole }}$ | Heat of liquefaction, cal/mole | Net heat of adsorption, h-Q cal/mole | $\begin{gathered} h \cdot Q / \mathrm{ml} \\ \mathrm{cal} / \mathrm{mole} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Cl}$ |  | 12330 | 6220 | 6110 | 86.4 |
| $\mathrm{CS}_{2}$ |  | 12630 | 6830 | 5800 | 99.1 |
| $\mathrm{CH}_{3} \mathrm{OH}$ |  | . 12950 | 9330 | 3620 | 90.8 |
| $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Br}$ |  | . 14330 | 6850 | 7480 | 102.0 |
| $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{I}$ |  | . 14250 | 7810 | 6440 | 81.5 |
| $\mathrm{CHCl}_{3}$ |  | . 14930 | 8000 | 6930 | 87.5 |
| $\mathrm{HCOOC}_{2} \mathrm{H}_{5}$ |  | 15420 | 8380 | 7040 | 90.1 |
| $\mathrm{C}_{6} \mathrm{H}_{8} \ldots . .$. |  | . 15170 | 7810 | 7360 | 85.0 |
| $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{OH}$ |  | . 14980 | 10650 | 4330 | 76.8 |
| $\mathrm{CCl}_{4}$ |  | 16090 | 8000 | 8090 | 85.6 |
| $\left(\mathrm{C}_{2} \mathrm{H}_{5}\right)_{2} \mathrm{O}$ |  | . 16090 | 6900 | 9190 | 80.3 |

[^266]TABLE 676.-SPREADING COEFFICIENTS, $S$, OF ORGANIC LIQUIDS ON WATER AT $20^{\circ} \mathrm{C}$ *

| Spreading liquids | $S=W_{a}-W_{c} \dagger$ | Spreading liquids | $S=W_{a}-W_{c}$ |
| :---: | :---: | :---: | :---: |
| Butyric acid | 45.66 | Heptane | 22.40 |
| Ethyl ether | . 45.50 | Ethyl bromide | 17.44 |
| Isoamyl chloride | 33.88 | Chloroform | 13.04 |
| Heptaldehyde | 32.22 | Anisole | 11.76 |
| Nitromethane | 26.32 | Phenetole | 10.66 |
| Mercaptan | 24.86 | p-Cymene | 10.10 |
| Oleic acid | . 24.62 | Isopentane | 9.44 |
|  | Liquids which form lenses $\quad S=W_{a}-W_{0}$ <br> Ethylene dibromide .......... -3.19 <br> Carbon disulfide ............... -6.94 <br> Monoiodobenzene ............. -8.74 <br> Bromoform .................... 9.58 <br> Liquid petrolatum .............-13.64 |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |

*For reference, see footnote 215, p. 632 . $\dagger W_{a}$, work adhesion; $W_{c}$, work of cohesion.

TABLE 677.-HEATS OF ADSORPTION OF GASES BY CHARCOAL ${ }^{216}$

| Gas |  |  |  | Gas |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Argon | 3636 | 1504 | 4180 | Carbon dioxide | 7300 | 2540 | 6100 |
| Nitrogen | 3686 | 1250 |  | Ammonia | 7200 | 5000 | 7120 |
| Carbon monoxide. . | 3416 | 1410 | 3715 |  |  |  |  |

[^267]TABLE 678.-BOND ENERGIES* IN KILOCALORIES PER MOL ${ }^{217}$


[^268]TABLE 679.-IGNITION AND PROPAGATION TEMPERATURES OF DUSTS IN AIR*

Degrees Centigrade

| Dust | Ignition temperature | Propagation temperature | Dust | Ignition temperature | Propagation temper ature |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Sugar | . 540 | 805 | Cork | 630 | 1000 |
| Dextrin | . 540 | 940 | Rice | . 630 | 970 |
| Starch | . . 640 | 1035 | Mustard | . 680 | 1050 |
| Cocoa | . 620 | 970 | Wheat elev |  | (1295) |
|  |  | 995 | Oat and co |  | (995) |
| Flour | 630 | (1265) | Oat hull |  | (1020) |

* For reference, see footnote 214, p. 631.

TABLE 680.-LOWER EXPLOSIVE LIMITS *
Milligrams per liter of air

| Dust | Glowing Pt wire | Arc | Induc. tion spark | Dust | Glowing Pt wire | Arc | Induction spark |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Starch | 7.0 | 10.3 | 13.7 | Sugar | 10.3 | 17.2 | 34.4 |
| Corn elevator | 10.3 | 10.3 | 13.7 | Aluminum | 7.0 | 7.0 | 13.7 |
| Wheat elevator | 10.3 | 10.3 |  | Coal | 17.2 | 24.1 | No |
| Sulfur | 7.0 | 13.7 | 13.7 |  |  |  | ignition |

* For reference, see footnote 214, p. 631.

TABLE 681.-SOME MEASUREMENTS OF EXPLOSION PRESSURES*

| Dust | Pressure generated, lb/in. ${ }^{2}$ | Dust | Pressure generated, lb/in. ${ }^{2}$ | Dust | Pressure generated, 1b/in. ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lycopodium | 17.5 | Cornstarch | 12.7 | Cocoa | 9.9 |
| Dextrin ... | 14.6 | Wheat elevator | . 12.5 | Sulfur flour | 8.8 |
| Wheat starch | . 14.0 | Sugar . . . . . . | . 12.2 | Rice-bran dust | 8.7 |
| Tanbark dust | . 13.3 | Linseed meal .. | . 11.7 | Ground-cork dust | t. 7.4 |
| Wood dust . | . 12.8 | Pittsburgh coal | . 10.1 |  |  |

* For reference, see foot note 214, p. 631.


## TABLE 682.-pH STABILITY RANGE OF SOME PROTEINS*

| Protein | Source | Stable in the pH range of |
| :---: | :---: | :---: |
| Amandin | Almonds | 4.3 to 10.0 |
| Bence-Jones | Pathological urine | 3.5 to 7.5 |
| Edestin | Hempseed | 5.5 to 9.7 |
| Egg albumin | Hens' eggs | 4.0 to 9.0 |
| Erythrocruorin | Blood of Arenicola marina | 2.6 to 8.0 |
| Erythrocruorin | Blood of Lumbricus terrestris | 2.6 to 10.0 |
| Excelsin ..... | Brazil nuts | 5.5 to 10.0 |
| Hemocyanin | Blood of Helix pomatia | 4.5 to 7.4 |
| CO-hemoglobin | Horse blood hemoglobin plus | 6.0 to 9.05 |
| Insulin ...... | Beef pancreas | 4.5 to 7.0 |
| Legumin | Vetch .. | 5.0 to 9.0 |
| Phycocyan | Ceramium rubrum | 1.5 to 8.0 |
| Serum albumin | Horse blood | 4.0 to 9.0 |
| Serum globulin | Horse blood | 4.0 to 8.0 |

[^269]
## TABLE 683.-ELECTRON EMISSION FOR HOT SOLIDS

The electron emission from a solid varies with the temperature $T\left({ }^{\circ} \mathrm{K}\right)$ in accordance with the Richardson-Laue-Dushman equation

$$
\begin{equation*}
I=A T^{2}\left[\exp \left(-b_{0} / T\right)\right] \tag{1}
\end{equation*}
$$

where $I=$ current in amps $\mathrm{cm}^{-2}$, and $A$ and $b_{\circ}$ are constants, characteristic of the material.
The constant $b_{0}$ is ordinarily expressed in terms of electron volts ( $\Phi_{0}$ ) where

$$
\begin{align*}
& \Phi_{o}=8.620 \times 10^{-5} b_{0} \\
& b_{0}=1.160 \times 10^{4} \theta_{o} \tag{2}
\end{align*}
$$

The values of $A$ and $b_{0}$ (or $\boldsymbol{\Phi}_{o}$ ) are customarily derived from a plot of $\log \left(I / T^{2}\right)$ versus $1 / T$, where

$$
\begin{equation*}
\log I=\log A+2 \log T-\frac{b_{0}}{2.303 T} \tag{3}
\end{equation*}
$$

and

$$
\log =\log \text { to base } 10
$$

Hence,

$$
\begin{equation*}
\Phi_{o}=1.986 \times 10^{-4}\left(b_{0} / 2.303\right) \tag{4}
\end{equation*}
$$

Theoretically, $\boldsymbol{\Phi}_{o}$, as determined from thermionic emission data, should be identical with $\boldsymbol{\Phi}_{e}$, the "work function" from contact potential measurements, and $\Phi_{e}$, the work function determined by means of Einstein's equation

$$
V e=h \nu-\Phi
$$

where $\nu=$ frequency for photoelectric emission, $V=$ retarding potential, $e=$ charge on the electron, and $h=$ quantum constant.

[^270]
## TABLE 684.-ELECTRON EMISSION CONSTANTS FOR METALS AND CARBON

The table gives emission constants (see preceding equations) for metals and carbon. For other values and comprehensive data on this topic see references in footnote 218.

| Element | A | $10^{-4} b_{0}$ | $\phi$ 。 | $I_{T}$ | $T^{\circ} \mathrm{K}$ | $\phi$ e |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Barium | 60 | 2.47 | 2.10 | $1.5 \times 10^{-8}$ | 800 | 2.48-2.51 |
| Calcium | 60 | 2.60 | 2.24 | $2.9 \times 10^{-7}$ | 800 | 2.71 |
| Carbon | 30 | 5.03 | 4.34 | $1.4 \times 10^{-3}$ | 2000 | 4.82 |
| Cesium | 162 | 2.10 | 1.81 | $2.5 \times 10^{-11}$ | 500 | 1.91 |
| Chromium | 48 | 5.34 | 4.60 | $3.8 \times 10^{-8}$ | 1500 | 4.37 |
| Cobalt | 41 | 5.12 | 4.41 | $1.3 \times 10^{-7}$ | 1500 |  |
| Copper | 65 | 5.08 | 4.38 | $5.6 \times 10^{-15}$ | 1000 | 4.46 |
| Hafnium | 15 | 4.10 | 3.53 | $2.8 \times 10^{-4}$ | 1600 |  |
| Iron | 26 | 5.20 | 4.48 | $6.8 \times 10^{-16}$ | 1000 | 4.63 |
| Molybdenum | 60 | 5.07 | 4.37 | $2.4 \times 10^{-3}$ | 2000 | 4.12 |
| Nickel .... | 30 | 5.35 | 4.61 | $2.2 \times 10^{-8}$ | 1500 |  |
| Niobium | 37 | 4.65 | 4.01 | $1.2 \times 10^{-3}$ | 2000 |  |
| Palladium | 60 | 5.79 | 4.99 | $3.0 \times 10^{-8}$ | 1600 | 4.92 |
| Platinum | 32 | 6.17 | 5.32 | $1.8 \times 10^{-9}$ | 1600 |  |
| Rhenium | 200 | 5.92 | 5.1 | $1.0 \times 10^{-4}$ | 2000 |  |
| Rhodium | 33 | 5.57 | 4.80 | $1.1 \times 10^{-4}$ | 2000 | 4.92 |
| Tantalum | 55 | 4.86 | 4.19 | $6.2 \times 10^{-9}$ | 2000 | 4.05 |
| Thorium | 60 | 3.89 | 3.35 | $4.3 \times 10^{-9}$ | 1600 | 3.3-3.6 |
| Tungsten | 60 | 5.24 | 4.52 | $1.00 \times 10^{-3}$ | 2000 | 4.3-4.5 |
| Zirconium | 330 | 4.79 | 4.13 | $8.5 \times 10^{-5}$ | 1600 |  |

[^271]The table gives emission data for a range of temperature, for the most frequently used metals and for thoriated tungsten (ThW). Values of $A$ and $b_{0}$ oused in calculation of $I$ (amp $/ \mathrm{cm}^{2}$ ) are those given in Table 684. For ThW, the values used are $A=3.0$ and $\phi_{0}=2.72, b_{0}=3.15 \times 10^{4}$.

| $T{ }^{\circ} \mathrm{K}$ | Tungsten |  | Molybdenum |  | Tantalum |  | ${ }^{\text {Niobium }}$ |  | ThW ${ }_{\text {c }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | I | $w$ | I | W | I | $w$ | I | W |  |
| 1000 |  |  |  |  |  |  |  |  | $1.73 \times 10^{-7}$ |
| 1200 |  |  |  |  |  |  |  |  | $3.95 \times 10^{-5}$ |
| 1400 |  |  |  |  |  |  |  |  | $2.03 \times 10^{-3}$ |
| 1600 | $9.27 \times 10^{-7}$ | 7.74 | $2.39 \times 10^{-6}$ | 6.30 | $9.1 \times 10^{-8}$ | 7.36 | $2.19 \times 10^{-5}$ | 6.40 | $4.06 \times 10^{-2}$ |
| 1800 | $4.47 \times 10^{-5}$ | 14.2 | $1.05 \times 10^{-6}$ | 11.3 | $3.32 \times 10^{-6}$ | 13.3 | $6.95 \times 10^{-6}$ | 11.4 | . 428 |
| 2000 | $1.00 \times 10^{-3}$ | 24.0 | $2.15 \times 10^{-8}$ | 19.2 | $6.21 \times 10^{-8}$ | 21.6 | $1.16 \times 10^{-2}$ | 18.5 | 2.864 |
| 2200 | $1.33 \times 10^{-2}$ | 38.2 | $2.59 \times 10^{-2}$ | 30.7 | $6.78 \times 10^{-2}$ | 34.2 | . 115 | 29.9 |  |
| 2400 | . 116 | 57.7 | . 215 | 47.0 | . 509 | 51.3 | . 800 | 45.3 |  |
| 2600 | . 716 | 83.8 | 1.29 | 69.5 | 2.25 | 75.4 | 5.20 | 67.0 |  |
| 2800 | 3.54 | 117.6 | 6.04 | 98.0 | 12.53 | 105.5 | 60.67 | 130.6 |  |
| 3000 | 14.15 | 160.5 | 23.28 | 116.0 | 45.60 | 144.4 |  |  |  |

[^272]
## TABLE 686.-PHOTOELECTRIC EFFECT

A negative charged body loses its charge under the influence of ultraviolet radiation because of the escape of negative electrons freed by the absorption of the energy of the radiation. The radiation must have a wavelength shorter than some limiting value $\lambda_{0}$ characteristic of the metal. The emission of these electrons, unlike that from hot bodies, is independent of the temperature. The relation between the maximum velocity $v$ of the expelled electron and the frequency $\nu$ of the radiation is $\left(\frac{1}{2}\right) m v^{2}=h \nu-P$ (Einstein's equation) where $h$ is Planck's constant ( $6.62 \times 10^{-27} \mathrm{erg} \mathrm{sec}$ ), $h \nu$, the energy of a "quanta," $P$, the work which must be done by the electron in overcoming surface forces. ( $\frac{1}{2}$ ) $m v^{2}$ is the maximum kinetic energy the electron may have after escape. Richardson identifies the $P$ of Einstein's formula with the $\phi_{e}$ of electron emission of Table 683. The minimum frequency $\nu_{0}$ (corresponding to maximum wavelength $\lambda_{0}$ ) at which the photoelectric effect can be observed is determined by $h \nu=P . P$ applies to a single electron, whereas $w$ applies to 96,500 coulombs ( $6.02 \times 10^{23}$ electrons) ; therefore $w=N P=.00399 \nu_{0}$ ergs. $\phi=(12.4$ $\left.\times 10^{-5}\right) \lambda_{0}$ volts.

TABLE 687.-THE ELECTRON AFFINITY OF THE ELEMENTS, IN VOLTS

| Metal | Contact (Henning) | Thermionic (Langmuir) | Photo- electric and contact (Millikan) | Photo- electric Richardson | Miscellaneous | $\begin{gathered} \text { Single- } \\ \text { inne- } \\ \text { spectra } \end{gathered}$ | Adjusted mean |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tungsten | . - | 4.52 | - | - | - | - | 4.52 |
| Platinum | - |  | - | 4.3 | 4.45 | - | 4.4? |
| Tantalum | - | 4.31 | - | - | - |  | 4.3 |
| Molybdenum | - | 4.31 | - |  |  |  | 4.3 |
| Carbon .... |  | 4.14 | - | - | - |  | 4.1 |
| Silver | 4.05 | - | - | - | - |  | 4.1 |
| Copper | (4.0) | - | - | 4.1 | - | - | 4.0 |
| Bismuth |  | - | - | 3.7 | - | - | 3.7 |
| Tin | 3.78 |  |  | 3.5 |  |  | 3.8 |
| Iron | 3.86 | 3.2? |  |  |  |  | 3.7 |
| Zinc | 3.46 |  | - | 3.4 | - | 4.04 | 3.4 |
| Thorium | - | 3.36 | - |  |  |  | 3.4 |
| Aluminum | 3.06 | - | - | 2.8 |  |  | 3.0 |
| Magnesium | 2.63 |  |  | 3.2 |  | 4.35 | 2.7 |
| Titanium |  | 2.4? |  |  |  |  | 2.4 |
| Lithium | - | - | 2.35 |  | - | 1.85 | 2.35 |
| Sodium | - | - | 1.82 | 2.1 | - | 2.11 | 1.82 |

There has been considerable controversy over the reality and nature of the contact differences of potential between two metals. At present, owing to the studies of Langmuir, there is a decided tendency to believe that this Volta difference of potential is an intrinsic property of metals closely allied to the phenomena given in Tables 684 to 688 and that the discrepancies among different observers have been caused by the same disturbing surface conditions. The values are for freshly cut surfaces in vacuo. Freshly cut surfaces are more electropositive and grow more electronegative with age. That the observed initial velocities of emission of electrons from freshly cut surfaces are nearly the same for all metals suggests that the more electropositive a metal is the greater the actual velocity of emission of electrons from its surface.


From the equation $w=R T \log \left(N_{A} / N_{B}\right)$, where $w$ is the work necessary per grammolecule when electrons pass through a surface barrier separating concentrations $N_{A}$ and $N_{B}$ of electrons, it can be shown that the Volta potential difference between two metals should be

$$
v_{1}-v_{2}=\frac{1}{F}\left\{w_{2}-w_{1}+R T \log \left(N_{A} / N_{B}\right)\right\}=\frac{w_{2}-w_{1}}{F}=\phi_{2}-\phi_{1}
$$

(see Table 686 for significance of symbols), since the number of free electrons in different metals per unit volume is so nearly the same that $R T \log \left(N_{A} / N_{B}\right)$ may be neglected. The contact potentials may thus be calculated from photoelectric phenomena. They are independent of the temperature. The following table gives a summary of values of $\phi$ in volts obtained from the various phenomena where an electron is torn from the attraction of some surface. In the case of ionization potentials the work necessary to take an electron from an atom of metal vapor is only approximately equal to that needed to separate it from a solid metal surface.

## TABLE 689.-ELECTRODE POTENTIALS

It should not be assumed that all the emf of an electrolytic cell is contact emf. Its emf varies with the electrolyte, whereas the contact emf is an intrinsic property of a metal. There must be an emf between the two electrodes of such a cell dependent upon the concentration of the electrolyte used. The following table gives in its first line the electrode potential $e_{n}$ of the corresponding metals (in solutions of their salts containing normal ion concentration) on assumption of no contact emf at the junction of the metals. The second line, $\phi-e_{n}-3.7$ volts, gives an idea of the electrode potentials (arbitrary zero) exclusive of contact emf.

| Metal | g | Cu | Bi | Sn | Fe | Zn | Mg | Li | Na |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $e_{\text {A }}$ | $+.80$ | $+.34$ | $+.20$ | -. 10 | -. 43 | -. 76 | $-1.55$ | $-3.03$ | -2.73 |
| $\phi-e_{n}-3.7$ | -. 40 | $+.04$ | +. 20 | $-.20$ | $-.43$ | -. 46 | $-.55$ | $-1.65$ | $-.85$ |

## TABLE 690-PRESSURE AND NUMBER OF MOLECULES

1. Units of Pressure
```
            \(A_{n}=\) normal atmosphere
                        \(=760 \mathrm{mmHg}\) at \(0^{\circ} \mathrm{C}\) and \(45^{\circ}\) latitude
            \(=1.01325 \times 10^{8}\) microbars
1 dyne \(\mathrm{cm}^{-2}=1\) microbar \(=0.75\) micron
    1 micron \(=10^{-3} \mathrm{mmHg}=1.333\) microbars
            \(=1 \mu\)
            \(P_{m m}=\) pressure in mmHg
                            \(P_{\mu}=\) pressure in microns \(=10^{-3} P_{m m}\)
            \(P \mu b=\) pressure in microbars \(=1.333 \times 10^{-3} P_{m m}\)
```

2. Number of molecules per unit volume

For ideal gas,

$$
\begin{aligned}
P V & =R_{\circ} T \\
\text { Where } & =\text { volume per gram-molecular weight } \\
P & \equiv \text { pressure } \\
T & \equiv \text { absolute temperature in degrees Absolute }\left({ }^{\circ} \mathrm{K}\right) \\
& \equiv \text { degrees Centigrade }+273.16
\end{aligned}
$$

For ideal gas at $0^{\circ} \mathrm{C}$ and $A_{n}=1$,

$$
\begin{aligned}
& V=V_{o}=22,414.6 \mathrm{~cm}^{3} \\
& \text { Hence } R_{0}=62.364 \mathrm{~mm} \text { liter, } \mathrm{deg}^{-1} \mathrm{~K} \mathrm{~g} \mathrm{~mole}^{-1} \\
& =8.3146 \times 10^{7} \mathrm{erg} \mathrm{deg}^{-1} \mathrm{~K} \mathrm{~g} \mathrm{~mole}^{-1} \\
& \rho=\text { density of gas } / \mathrm{g} / \mathrm{cm}^{3} \\
& =1.2027 \times 10^{-8} M P \mu b / T^{-1} \mathrm{~g} \mathrm{~cm}^{-8} \\
& =1.6035 \times 10^{-5} M P_{m m} / T^{-1} \mathrm{~g} \mathrm{~cm}^{-8} \\
& \text { Where } M=\text { molecular weight in grams } \\
& n=\text { number of molecules per } \mathrm{cm}^{3} \\
& =7.244 \times 10^{15} P \mu b / T \\
& =9.656 \times 10^{18} P_{m m} / T
\end{aligned}
$$

3. The number of molecules per $\mathrm{cm}^{8}$ for different temperatures and pressures

| $T\left({ }^{\circ} \mathrm{K}\right)$ | $P_{\mu \mathrm{t}}$ | $P_{m m}$ | $n$ | T. | $P_{\mu \nu}$ | $P_{m m}$ | $n$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 273.16 | $1.0133 \times 10^{8}$ | 760 | $2.687 \times 10^{19}$ | 298.16 | $1.333 \times 10^{3}$ |  | $3.240 \times 10^{10}$ |
| 298.16 |  | " | $2.462 \times 10^{10}$ | 273.16 | 1.000 | $7.50 \times 10^{-4}$ | $2.653 \times 10^{13}$ |
| 273.16 | $1.333 \times 10^{3}$ | 1 | $3.536 \times 10^{18}$ | 298.16 |  |  | $2.430 \times 10^{18}$ |

[^273]TABLE 691.-MEAN FREE PATHS, L, MOLECULAR DIAMETERS, $\delta$, AND RELATED DATA FOR WATER AND MERCURY VAPORS*

|  | $t^{\circ} \mathrm{C}$ | $P_{m m * *}{ }^{*}$ | $10^{5} \eta_{0}$ | $10^{9} L^{1}{ }^{1}$ | $L_{1}{ }^{\text {P }}$ | $10^{8} \delta_{6}$ | $10^{-14} \mathrm{~N}$ ¢ $\dagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{H}_{2} \mathrm{O}$ | 0 | 4.58 | 8.69 | 2.90 | $6.34 \times 10^{-4}$ | 4.68 | 5.27 |
|  | 15 | 12.79 | 9.26 |  |  |  |  |
| - | 25 | 23.76 | 9.64 | 3.37 | $1.42 \times 10^{-4}$ |  |  |
| Hg | 219.4 | 31.57 | 46.66 | 6.28 | $1.99 \times 10^{-4}$ | 4.27 | 6.32 |
|  | 1500 | 2.807 | 39.04 | 4.87 | $1.74 \times 10^{-8}$ | 4.50 | 5.70 |
|  | 100.0 | . 2729 | 33.56 | 3.93 | $1.44 \times 10^{-2}$ | 4.70 | 5.22 |
|  | 25.0 | . 0018 | 25.40 | 2.66 | 1.45 | 5.11 | 4.42 |
|  | . 0 |  | 16.2(J) |  |  | $6.26(J)$ |  |

[^274]Part 1.-Discussion
Let a denote the most probable velocity, $v_{a}$, the average velocity and $v_{\mathrm{r}}$, the mean velocity (the square root of the mean square). Then

$$
\begin{aligned}
\alpha & =\sqrt{2 R_{n} T / M}=12,895 \sqrt{T / M} \mathrm{~cm} \mathrm{sec} \\
v_{a} & =(2 / \sqrt{\pi}) \quad a=1.1284 a=14,551 \sqrt{T / M} \mathrm{~cm} \mathrm{sec}^{-1} \\
v_{r} & =\sqrt{3 / 2} a=1.225 a=15,794 \sqrt{\Gamma / M} \mathrm{~cm} \mathrm{sec}^{-1}
\end{aligned}
$$

The probability of a random velocity $v=c a$ is

$$
f_{c}=(r / \sqrt{\pi}) c^{2}\left[\exp -c^{2}\right]
$$

The fraction of the total number of molecules, $N$, which have a random velocity equal to or less than $v=c a$ is

$$
y=\frac{N_{c}}{N}=\int_{0}^{0} f_{c} d c
$$

Part 2 of this table gives values of $f_{c}$ and of $y$ for a series of values of $c$. The third column gives values of $\Delta y$, which is the fraction of the total number that have values of $c$ between that given in the same horizontal row and that in the preceding row.
From the relation for $f_{c}$ we obtain the relation for the probability that a molecule possesses the translational energy $E$. Let $x=E /(k T)$ where $x$ is a dimensionless quantity. Then

$$
f_{x}=2 \sqrt{x / \pi}(\exp -x)
$$

and the average kinetic energy is $E_{a v}=(3 / 2) k T$
where

$$
\begin{aligned}
k & =\text { Boltzmann constant } \\
& =1.3805 \times 10^{-10} \mathrm{erg} \mathrm{deg}^{-1} \mathrm{~K}
\end{aligned}
$$

The last two columns in Part 2, below, give values of $f_{x}$ for a series of values of $x$.
Part 2.-Values of functions for application of distribution laws

| c | $f$ c | $y$ | $\Delta y$ | $x$ | $f_{x}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 0 |  | 0 |  |
| . 2 | . 0867 | . 0059 | . 0059 | . 1 | . 3229 |
| . 3 | . 1856 | . 0193 | . 0134 | . 2 | . 4131 |
| . 5 | . 4393 | . 0812 | . 0619 | . 5 | . 4839 |
| . 7 | . 6775 | . 1939 | . 1127 | . 7 | . 4688 |
| 1.0 | . 8302 | . 4276 | . 2337 | 1.0 | . 4152 |
| 1.3 | . 7036 | . 6634 | . 2358 | 1.4 | . 3294 |
| 1.6 | . 4464 | . 8369 | . 1735 | 1.8 | . 2502 |
| 1.8 | . 2862 | . 9096 | . 0727 | 2.2 | . 1855 |
| 2.0 | . 1652 | . 9540 | . 0444 | 2.5 | . 1464 |
| 2.2 | . 0867 | . 9784 | . 0244 | 3.0 | . 0973 |
| 2.5 | . 0275 | . 9941 | . 0157 | 3.5 | . 0637 |
| 3.0 | . 0025 | $1-4.2 \times 10^{-8}$ |  | 4.0 | . 0413 |
| 4.0 | $4.1 \times 10^{-6}$ | $1-5.1 \times 10^{-7}$ |  | 5.0 | . 0170 |
| 5.0 | $\% .8 \times 10^{-10}$ | $1-7.9 \times 10^{-11}$ |  | 6.0 | . 0069 |

Part 3.-Rates of incidence and of evaporation of molecules
The rate at which molecules strike a surface is given by

$$
\begin{aligned}
\nu & =(1 / 4) n v_{a} \mathrm{~cm}^{-2} \mathrm{sec}^{-1} \\
& =2.635 \times 10^{10}\left(P_{\mu b}\right) /(\sqrt{M T}) \mathrm{cm}^{-2} \mathrm{sec}^{-1} \\
& =3.513 \times 10^{22} P_{m m} / \sqrt{M T} \mathrm{~cm}^{-2} \mathrm{sec}^{-1} \\
G & =\text { mass of gas of molecular wt, } M, \\
& =1.6604 \times 10^{-24} M \nu \\
& =4.375 \times 10^{-5}\left(P_{\mu b}\right)(\sqrt{M / T}) \mathrm{g} \mathrm{~cm}^{-2} \mathrm{sec}^{-1} \\
& =5.833 \times 10^{-2}\left(P_{m m}\right)(\sqrt{M / T}) \mathrm{g} \mathrm{~cm}^{-2} \mathrm{sec}^{-1}
\end{aligned}
$$

If we assume that the accommodation coefficient for condensation is unity, then the rate of evaporation is equal to the rate of condensation and the vapor pressure, $P_{m m}$, is given by the relation

$$
P_{m m}=17.14 G \sqrt{T / M}
$$

# TABLE 693.-MASSES, VELOCITIES, AND RATES OF INCIDENCE OF MOLECULES* 

$\nu_{1}=$ rate of incidence of molecules per $\mathrm{cm}^{2}$ per sec, at $0^{\circ} \mathrm{C}$ and 1 microbar.
$\nu_{1}=$ rate of incidence of molecules per $\mathrm{cm}^{2}$ per sec, at $0^{\circ} \mathrm{C}$ and 1 mm .
$G_{1}=$ mass of gas corresponding to $\nu_{1}\left(\mathrm{~g} \mathrm{~cm}^{-2} \mathrm{sec}^{-1}\right)$.
$G_{1^{\prime}}=$ mass of gas corresponding to $\nu_{1^{1}}\left(\mathrm{~g} \mathrm{~cm}^{-2} \sec ^{-1}\right)$.
$m=$ mass of molecule in grams $=1.66035 \times 10^{-24} M ; M=$ molecular weight ; $\rho_{1}{ }^{\circ}$ $=$ density $\left(\mathrm{g} \mathrm{cm}^{-3}\right)$ of gas at $0^{\circ} \mathrm{C}$ and 1 microbar.
$v_{a}=$ average velocity ( $\mathrm{cm} \mathrm{sec}^{-1}$ ).

| $\begin{gathered} \text { Gas or } \\ \text { vapor } \end{gathered}$ | M | $10^{29} \mathrm{~m}$ | $10^{-4} \times v_{\text {a }}$ |  |  | $10^{-17 \nu_{1}}$ | $10^{-20} \nu_{1}{ }^{\prime}$ | $10^{5} G_{1}$ | $10^{2} G_{1}{ }^{\prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $10^{10} \rho_{1} 0$ | $0^{\circ} \mathrm{C}$ | $25^{\circ} \mathrm{C}$ |  |  |  |  |
| $\mathrm{H}_{2}$ | 2.016 | . 3347 | . 8878 | 16.93 | 17.70 | 11.23 | 14.97 | . 3759 | . 5012 |
| He | 4.003 | . 6646 | 1.7631 | 12.01 | 12.56 | 7.969 | 10.63 | . 5297 | . 7062 |
| CH4 | 16.04 | 2.663 | 7.063 | 6.005 | 6.273 | 3.981 | 5.308 | 1.060 | 1.414 |
| $\mathrm{NH}_{3}$ | 17.03 | 2.827 | 7.498 | 5.829 | 6.089 | 3.865 | 5.152 | 1.092 | 1.456 |
| $\mathrm{H}_{2} \mathrm{O}$ | 18.02 | 2.992 | 7.936 | 5.665 | 5.919 | 3.756 | 5.007 | 1.124 | 1.498 |
| Ne | 20.18 | 3.351 | 8.886 | 5.355 | 5.594 | 3.550 | 4.733 | 1.190 | 1.586 |
| CO | 28.01 | 4.651 | 12.34 | 4.543 | 4.746 | 3.012 | 4.016 | 1.402 | 1.868 |
| $\mathrm{N}_{2}$ | 28.02 | 4.652 | 12.34 | 4.542 | 4.745 | 3.011 | 4.015 | 1.402 | 1.868 |
| Air | 28.98** | 4.811 | 12.77 | 4.468 | 4.668 | 2.962 | 3.950 | 1.425 | 1.900 |
| $\mathrm{O}_{2}$ | 32.00 | 5.313 | 14.09 | 4.252 | 4.442 | 2.819 | 3.758 | 1.497 | 1.996 |
| A | 39.94 | 6.631 | 17.59 | 3.805 | 3.976 | 2.523 | 3.363 | 1.675 | 2.230 |
| $\mathrm{CO}_{2}$ | 44.01 | 7.308 | 19.38 | 3.624 | 3.787 | 2.403 | 3.204 | 1.756 | 2.342 |
| $\mathrm{CH}_{3} \mathrm{Cl}$ | 50.49 | 8.383 | 22.23 | 3.385 | 3.356 | 2.244 | 2.991 | 1.881 | 2.508 |
| $\mathrm{SO}_{2}$ | 64.06 | 10.64 | 28.21 | 3.004 | 3.139 | 1.992 | 2.656 | 2.118 | 2.825 |
| $\mathrm{Cl}_{2}$ | 70.91 | 11.77 | 31.23 | 2.856 | 2.984 | 1.893 | 2.524 | 2.229 | 2.973 |
| Kr | 83.7 | 13.90 | 36.85 | 2.629 | 2.747 | 1.743 | 2.324 | 2.422 | 3.229 |
| $\mathrm{C}_{7} \mathrm{H}_{10}$ | 100.2 | 16.63 | 44.12 | 2.403 | 2.510 | 1.593 | 2.123 | 2.650 | 3.533 |
| Xe | 131.3 | 21.80 | 57.82 | 2.099 | 2.193 | 1.392 | 1.856 | 3.034 | 4.044 |
| $\mathrm{CCl}_{4}$ | 153.8 | 25.54 | 67.72 | 1.939 | 2.026 | 1.286 | 1.714 | 3.283 | 4.377 |
| $\mathrm{Hg}{ }^{\dagger}$ | 200.6 | 33.31 | (88.33) | 1.698 | 1.774 | (1.126 | 1.501 | 3.750 | 4.998) |

* For reference, see footnote 219 , p. 636.
** Calculated from the value $\rho$ (density) $=1.293 \times 10^{-8}$ at $0^{\circ} \mathrm{C}$ and 760 mmHg .
$\dagger$ Since the vapor pressure of mercury at $0^{\circ} \mathrm{C}$ is $1.85 \times 10^{-4} \mathrm{mmHg}(=0.247 \mu b)$, the values given in parentheses have no physical significance. Actual values at $0^{\circ} \mathrm{C}$, corresponding to saturation pressure, are as follows: $\rho=21.79 \times 10^{-10} ; \nu=2.777 \times 10^{16} ; G=9.249 \times 10^{-6}$.

TABLE 694.-MOLECULAR VELOCITIES ${ }^{220}$

| Gas | Root mean square velocities, NTP | Average velocities, NTP |
| :---: | :---: | :---: |
| Hydrogen | $18.38 \times 10^{4} \mathrm{~cm} / \mathrm{sec}$ | $16.93 \times 10^{4} \mathrm{~cm} / \mathrm{sec}$ |
| Helium . | 13.11 | 12.08 |
| Water vapor | 6.15 | 5.65 |
| Neon | 5.84 | 5.38 |
| Carbon monoxide | 4.93 | 4.54 |
| Nitrogen | 4.93 | 4.54 |
| Ethylene | 4.93 | 4.54 |
| Nitric oxide | 4.76 | 4.38 |
| Oxygen . | 4.61 | 4.25 |
| Argon | 4.13 | 3.80 |
| Carbon dioxide | 3.93 | 3.62 |
| Nitrous oxide | 3.93 | 3.62 |
| Krypton | 2.86 | 2.63 |
| Xenon | 2.28 | 2.10 |
| Mercury vapor | 1.84 | 1.70 |
| Air ........ | 4.85 | 4.47 |
| Ammonia | 6.33 | 5.82 |

[^275]Let $L=$ mean free path, $\delta=$ molecular diameter. Then

$$
\begin{array}{ll} 
& L=\frac{1}{\sqrt{2} \pi n \delta^{2}} \\
\text { and } & \eta=0.499 \rho v_{o} L  \tag{2}\\
\text { when } & \eta=\text { coefficient of viscosity } \\
& \rho=\text { density of gas at given pressure and temperature }
\end{array}
$$

Unit of $\eta$ is the poise $=\mathrm{g} \mathrm{cm}^{-1} \mathrm{sec}^{-1}$
Hence

$$
\begin{align*}
L & =1.1451 \times 10^{4} \frac{\eta}{P_{\mu b}} \sqrt{\frac{T}{M}} \mathrm{~cm}  \tag{3}\\
& =8.589 \frac{\eta}{P_{m m}} \sqrt{\frac{T}{M}} \mathrm{~cm}  \tag{4}\\
\delta^{2} & =\frac{2.714 \times 10^{-21}}{\eta} \sqrt{M T} \mathrm{~cm}^{2} \tag{5}
\end{align*}
$$

and
$\eta$, as a function of $T$, is given by the relation

$$
\begin{equation*}
\eta_{T}=\left(\frac{T}{T_{0}}\right)^{3 / 2}\left(\frac{C+T_{0}}{C+T}\right) \tag{6}
\end{equation*}
$$

where $\eta_{o}=$ value at $T_{0 .} \eta=$ value at $T$ and $C$ is known as the Sutherland constant. For short ranges of temperature, the exponential relation is used, of the form

$$
\begin{equation*}
\left(\eta_{r} / \eta_{0}\right)=\left(T / T_{\theta}\right)^{x} \tag{7}
\end{equation*}
$$

In Tables 691 and 696, which give values of $L, \delta$ and related data for a number of gases and vapors,

$$
\begin{aligned}
& \eta_{15}=\text { coefficient of viscosity at } 15^{\circ} \mathrm{C} \\
& \eta_{0}=\text { " " " " } 0^{\circ} \mathrm{C} \\
& \text { and } \eta_{25}=\text { " " " " } 25^{\circ} \mathrm{C} \\
& x=\text { valuc of exponent in equation (7) } \\
& L_{0}{ }^{1}=\text { value of mean free path (in } \mathrm{cm} \text { ) at } 0^{\circ} \mathrm{C} \text { and } \\
& 1 \mathrm{mmHg} \\
& L_{0}{ }^{280}=\text { value of mean free path (in } \mathrm{cm} \text { ) at } 0^{\circ} \mathrm{C} \text { and } \\
& 760 \mathrm{mmHg} \\
& L_{25}{ }^{1}=\text { value of mean free path (in } \mathrm{cm} \text { ) at } 25^{\circ} \mathrm{C} \text { and } \\
& 1 \mathrm{mmHg} \\
& L_{25}{ }^{750}=\text { value of mean frce path (in } \mathrm{cm} \text { ) at } 25^{\circ} \mathrm{C} \text { and } \\
& 760 \mathrm{mmHg} \\
& \delta=\text { value of molecular diameter (in cm) at } 0^{\circ} \mathrm{C} \\
& N_{s}=1.154 / \delta^{2}=\text { of molecules per } \mathrm{cm}^{2} \text { to form a mono- } \\
& \text { layer (assuming that the spacing is that of } \\
& \text { close-packed or face-centered lattice) } \\
& \omega=\text { collision-frequency at } 25^{\circ} \mathrm{C} \text { and } 760 \mathrm{mmHg} \\
& =\tau^{\prime} / L_{25}{ }^{\text {sico}}
\end{aligned}
$$

For the vapors of $\mathrm{H}_{2} \mathrm{O}$ and Hg (Table 691), $P=$ vapor pressure in mmHg at the ten1perature $t$, and $L_{t}$ and $\delta_{t}$ denote the values of the mean free path and diameter, respectively, at this temperature. For $\mathrm{H}_{2} \mathrm{O}$ vapor, $C=650$ and $\eta_{15}=9.26 \times 10^{-5}$. For $\mathrm{Hg}, C=$ 942.2 and value of $\eta$ at $t=219.4^{\circ} \mathrm{C}$ was used. The values of $\eta_{0}$ and $\delta_{0}$ for Hg at $0^{\circ} \mathrm{C}$ are those given by Jeans.

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TABLE 696.-VISCOSITY, $\eta$, MEAN FREE PATHS, L, MOLECULAR DIAMETERS, $\delta$, AND RELATED DATA FOR A NUMBER OF GASES *

| Gas: <br> Characteristic | $\mathrm{H}_{2}$ | He | Ne 67 | Air 79 | $\begin{aligned} & \mathrm{O}_{2} \\ & 81 \end{aligned}$ | A $.86$ | $\mathrm{CO}_{2}$ | Kr 85 | Xe 92 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $x^{* *}$ | .$^{.} 69$ |  |  |  |  |  |  |  | . 92 |
| $10^{*} \times \eta_{15}{ }^{\circ} \dagger$ | 871 | 1943 | 3095 | 1796 | 2003 | 2196 | 1448 | 2431 | 2236 |
| $10^{7} \times \eta_{0}{ }^{\circ}$ | 839 | 1878 | 2986 | 1722 | 1918 | 2097 | 1377 | 2372 | 2129 |
| $10^{7} \times \eta_{25}{ }^{\circ}$ | 892 | 1986 | 3166 | 1845 | 2059 | 2261 | 1496 | 2502 | 2308 |
| $10^{3} \times L_{0}{ }^{10} \ddagger$ | 8.39 | 13.32 | 9.44 | 4.54 | 4.81 | 4.71 | 2.95 | 3.69 | 2.64 |
| $10^{\text {n }} \times L_{0^{0}}{ }^{\text {780 }}$ | 11.04 | 17.53 | 12.42 | 5.98 | 6.33 | 6.20 | 3.88 | 4.85 | 3.47 |
| $10^{3} \times L_{20^{0}}{ }^{1}$ | 9.31 | 14.72 | 10.45 | 5.09 | 5.40 | 5.31 | 3.34 | 4.06 | 2.98 |
| $10^{6} \times L_{25}{ }^{0700}$ | 12.26 | 19.36 | 13.75 | 6.69 | 7.10 | 6.67 | 4.40 | 5.34 | 3.93 |
| $10^{8} \times \delta$ | 2.75 | 2.18 | 2.60 | 3.74 | 3.64 | 3.67 | 4.65 | 4.15 | 4.91 |
| C | 84.4 | 80 | 56 | 112 | 125 | 142 | 254 | 188 | 252 |
| $10^{-14} \times N_{8}$ § | 15.22 | 24.16 | 17.12 | 8.24 | 8.71 | 8.54 | 5.34 | 6.69 | 4.78 |
| $10^{-0} \times \omega$ i | 14.45 | 7.16 | 1.68 | 6.98 | 6.26 | 5.70 | 8.61 | 6.48 | 5.71 |

* For reference, see footnote 219, p. 636.
** ${ }_{x}$ from relations $\eta_{T}=a T^{x} . \quad \stackrel{\dagger}{\dagger} \stackrel{6}{=}$ a measure of strength of the attraction forces (in dynes) between molecules. $\ddagger L_{o 0^{1}}=$ mean free path at $0^{\circ} \mathrm{C}$ and .1 mmHg , etc. $\delta N_{s}=$ number of molecules $/ \mathrm{cm}^{2}$ for monomolecular layer. If $\omega=$ collision frequency ( $\mathrm{sec}^{-1}$ ) at $25^{\circ} \mathrm{C}$ and 760 mmHg .


## TABLES 697-712.-ATOMIC AND MOLECULAR DIMENSIONS

## TABLE 697.-EFFECTIVE ATOMIC RADII

Goldschmidt, on the basis of reasonable though empirical assumptions, has calculated effective radii of atoms in various charged conditions; Pauling, on the basis of wave mechanics, has presented theoretical values for most of the elements, the two series agreeing well in many cases. The latter values are printed in boldface type ; the values considered nontypical are in parentheses ; e.g., for silicon we have : $\mathrm{Si}^{+4}(0.22-) 0.39-\mathbf{0 . 4 1}, \mathrm{Si}^{\circ}\left(1.12-\right.$ ) $1.18, \mathrm{Si}^{-4}$ (1.98); 2.71, signifying silicon, carrying $4+$ charges, has apparent radius between 0.22 and 0.41 ; but the lower values relate to compounds where the atoms appear to be deformed ; so Goldschmidt gives 0.39 as most significant. Wave mechanics yields 0.41. Neutral, the radius ranges from 1.2, in abnormal compounds, to 1.18 in those typical ; when carrying 4 - charges, the value is 1.98 , according to calculations deemed faulty, 2.71 according to theory.

In applying the data to replacements, halides and oxides are usually ionized, and the values in the outer columns apply. Thus in fluorite the value for $\mathrm{Ca}^{+2}$ should be added to that for $\mathrm{F}^{-1}$, giving between 2.32 and 2.42 , or 2.37 as a mean; and the observed $\mathrm{Ca}-\mathrm{F}$ distance in the crystal is 2.36 angstrom units. In the remaining types of compounds the atoms appear to be largely neutral and the first column should be used.


TABLE 698*.-DIFFUSION COEFFICIENTS OF GASEOUS IONS AT NTP ${ }^{221}$

| Gas | Dry gas |  | Moist gas |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $D^{+}$ | $D^{-}$ | D+ | D- |
| Air | . 028 | . 043 | . 032 | . 035 |
| Oxygen | . 025 | . 0396 | . 0288 | . 0358 |
| Carbon dioxide | . 023 | . 026 | . 0245 | . 0255 |
| Nitrogen | . 029 | . 0414 |  |  |
| Hydrogen | . 123 | . 190 | . 128 | . 142 |

[^276]TABLE 699.-DIFFUSION COEFFICIENTS OF NEUTRAL GASES AT $0^{\circ} \mathrm{C}$ AND 760 mmHg *

| Gases | $D^{* *}$ | $m \dagger$ | Gases | $D^{* *}$ | $m \dagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A - He | . 706 |  | $\mathrm{H}_{2}-\mathrm{CO}$ | . 651 | 1.75 |
| $\mathrm{Air}-\mathrm{CO}_{2}$ | . 134 |  | $\mathrm{H}_{2}-\mathrm{CO}_{2}$ | . 534 | 1.75 |
| Air - $\mathrm{O}_{2}$ | . 178 |  | $\mathrm{H}_{2}-\mathrm{N}_{2}$ | . 674 | 1.75 |
| $\mathrm{CO}-\mathrm{CO}_{2}$ | . 136 | 2.00 | $\mathrm{H}_{2}-\mathrm{N}_{2} \mathrm{O}$ | . 535 | 1.75 |
| $\mathrm{CO}-\mathrm{H}_{2} \mathrm{O}$ | . 642 |  | $\mathrm{H}_{2}-\mathrm{O}_{2}$ | . 679 | 1.75 |
| $\mathrm{CO}-\mathrm{O}_{2}$ | . 183 | 1.75 | $\mathrm{H}_{2} \mathrm{O}-\mathrm{Air}$ | . 220 | 1.75 |
| $\mathrm{CO}_{2}-\mathrm{Air}$ | . 134 |  | $\mathrm{Hg}-\mathrm{Air}$ | . 112 |  |
| $\mathrm{CO}_{2}-\mathrm{H}_{2} \mathrm{O}$ | . 528 |  | $\mathrm{O}_{2}-\mathrm{Air}$ | . 178 | 1.75 |
| $\mathrm{He}-\mathrm{A}$ | . 641 | 1.75 | $\mathrm{O}_{2}-\mathrm{H}_{2}$ | . 722 |  |
| $\mathrm{H}_{2}-$ Air | . 661 | 1.75 | $\mathrm{O}_{2}-\mathrm{CO}$ | . 185 | 1.75 |
|  |  |  | $\mathrm{O}_{2}-\mathrm{CO}_{2}$ | . 136 | 2.00 |

[^277]
## TABLE 700.-MOBILITIES OF POSITIVE IONS IN NOBLE GASES AT 760 mmHg AND $0^{\circ} \mathrm{C}$ *

( $\mathrm{cm} / \mathrm{sec}$ per volt $/ \mathrm{cm}$ )

| Ion | He | Ne | A | Kr | Xe |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Gas ${ }^{\dagger}$ | 20.1 | 5.85 | 1.81 | . 88 | . 61 |
| Li | 24.2 | 11.87 | 4.68 | 3.72 | 2.84 |
| Na | 22.7 | 8.16 | 3.03 | 2.20 | 1.69 |
| K | 21.5 | 7.51 | 2.64 | 1.86 | 1.35 |
| Rb | 20.1 | 6.75 | 2.24 | 1.49 | 1.03 |
| Cs | 18.4 | 6.10 | 2.10 | 1.33 | . 91 |

* For reference, see footnote 221 , above.
$\dagger$ Ions same as gas.

TABLE 701.-MOLECULAR DIAMETERS, $\delta$, FOR ATTRACTIVE SPHERES *

| Gas | From $\eta$ † | From $b \ddagger$ | Gas | From $\eta$ † | From $b \ddagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Argon | $2.87 \times 10^{-8} \mathrm{~cm}$ | $2.87 \times 10^{-8} \mathrm{~cm}$ | Hydrogen | $2.38 \times 10^{-8} \mathrm{~cm}$ | $2.53 \times 10^{-8} \mathrm{~cm}$ |
| Krypton | 3.15 | 3.16 | Nitrogen | 3.13 | 3.56-3.10 |
| Xenon | 3.50 | 3.45 | Air .... | 3.11 | 3.32 |
| Helium | 1.91 | 1.97 | Carbon |  |  |
| Oxygen | 2.96 | 2.91 | dioxide | 3.23 | 3.22 |
|  |  |  | . . | 3.30 | 3.42 |

[^278]
## TABLE 702.-MOBILITY* OF SINGLY-CHARGED GASEOUS IONS AT 760 mmHg AND $0^{\circ} \mathrm{C}$ **

( $\mathrm{cm} / \mathrm{sec}$ per volt $/ \mathrm{cm}$ )

| Gas | $(\epsilon-1) \dagger$ | $K_{0}{ }^{-}$ | $K{ }^{+}$ |
| :---: | :---: | :---: | :---: |
| Air (dry) | . 000585 | 2.2 | 1.6 |
| A (pure) | . 00056 | 206.0 | 1.81 |
| $\mathrm{Cl}_{2}$ |  | . 74 | . 74 |
| $\mathrm{CCl}_{4}$ | . 0030 | . 31 | . 30 |
| CO | . 00070 | 1.14 | 1.10 |
| $\mathrm{CO}_{2}$ (dry) | . 00098 | . 98 | . 84 |
| $\mathrm{H}_{2}$ | . 00028 | 8.15 | 5.9 |
| $\mathrm{H}_{2}$ (pure) |  | 7900.0 | 13.8 |
| HCl ..... | . 0046 | . 62 | . 53 |
| $\mathrm{H}_{2} \mathrm{O}$ (at $100^{\circ} \mathrm{C}$ ) |  | . 95 | 1.1 |
| $\mathrm{H}_{2} \mathrm{~S} \ldots . . . . .$. | . 0040 | . 56 | . 62 |
| He | . 000074 | 6.3 | 5.09 |
| He (pure) |  | 500.0 | 21.4 |
| Hg in He . | .... | ... | 13.4 |
| Hg in $\mathrm{N}_{2}$. |  | . . | 2.02 |
| $\mathrm{Kr} \ldots .$. | . 0007685 |  | . 94 |
| $\mathrm{N}_{2}$ | . 00058 | 1.84 | 1.27 |
| $\mathrm{N}_{2}$ (pure) |  | 145.0 | 2.51 |
| $\mathrm{NH}_{3}$ | . 0072 | . 66 | . 56 |
| $\mathrm{NH}_{3}$ in $\mathrm{N}_{2}$. |  |  | 3.06 |
| $\mathrm{N}_{2} \mathrm{O}$ | . 00113 | . 90 | . 82 |
| Ne | . 0001231 |  | 5.64 |
| $\mathrm{O}_{2}$ | . 00051 | 1.8 | 1.31 |
| $\mathrm{SO}_{2}$ | . 0095 | . 41 | . 41 |

* $K=K_{o \rho_{0}} / \rho$, where $\rho_{0}$ is the gas density at $N T P$ and $\rho$ is the density at which $K$ is desired.

$$
K=\frac{0.235\left(\frac{m_{1}+m_{2}}{m_{1}}\right)^{1}}{\left(\rho / \rho_{o}\right)(\epsilon-1)_{o} M_{o}}
$$

where $m_{1}=$ mass of ion, $m_{2}=$ mass of gas particle, $\epsilon=$ dielectric constant, $(\epsilon-1) o$ is calculated for NTP. $M_{0}=$ molecular weight of gas. Values of mobility in this table may not be absolute, but are of orienting value.
** For reference, see footnote 221, p. 644.
$\dagger$ International Critical Tables; Tables Annuelles Internationales de Constants.

TABLE 703.-MOLECULAR DIAMETER (BRAGG)*

| Gas | From crystal measured in $2 d$ | From viscosity 7 | Ratio, $2 d / \eta$ |
| :---: | :---: | :---: | :---: |
| Neon | $1.30 \times 10^{-8} \mathrm{~cm}$ | $2.35 \times 10^{-8} \mathrm{~cm}$ | . 553 |
| Argon | 2.05 | 2.87 | . 714 |
| Krypton | 2.35 | 3.15 | . 746 |
| Xenon . | 2.70 | 3.50 | . 771 |

* For reference, see foot note 220, p. 640.

TABLE 704.-NUMBER OF MOLECULES (PER $\mathrm{cm}^{2}$ AT $0^{\circ} \mathrm{C}$ ) OF MONOLAYER AND EQUIVALENT VOLUME ( $\left.\mathrm{cm}^{\mathrm{s}}\right)^{*}$

| Gas | $\begin{aligned} & \text { No molecules } \\ & \times 10^{-14} \end{aligned}$ | $\begin{aligned} & \text { Vol gas } \\ & \text { at } 760 \mathrm{~mm} \mathrm{mg} \\ & \text { and } 20^{\circ} \mathrm{C} \\ & \times 10^{5} \end{aligned}$ | Gas | $\begin{gathered} \text { No molecules } \\ \times 10^{-14} \end{gathered}$ | $\begin{aligned} & \text { Vol gas } \\ & \text { at } 760 \mathrm{~mm} \mathrm{mg} \\ & \text { and } 20^{\circ} \mathrm{C} \\ & \times 10^{5} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{H}_{2}$ | . 15.22 | 6.08 | CO | 8.07 | 3.23 |
| He | . 24.16 | 9.65 | $\mathrm{CO}_{2}$ | 5.34 | 2.13 |
| A | . 8.54 | 3.41 | $\mathrm{CH}_{4}$ | 5.23 | 2.09 |
| $\mathrm{N}_{2}$ | 8.10 | 3.24 | $\mathrm{NH}_{3}$ | 4.56 | 1.82 |
| O | . 8.71 | 3.48 | $\mathrm{H}_{2} \mathrm{O}$ | 5.27 | 2.11 |

[^279]According to Langmuir, in solids and liquids every atom is chemically combined to adjacent atoms. In most inorganic substances the identity of the molecule is generally lost, but in organic compounds a more permanent existence of the molecule probably occurs. When oil spreads over water evidence points to a layer a molecule thick and that the molecules are not spheres. Were they spheres and an attraction existed between them and the water, they would be dissolved instead of spreading over the surface. The presence of the $-\mathrm{COOH},-\mathrm{CO}$ or -OH groups generally renders an organic substance soluble in water, whereas the hydrocarbon chain decreases the solubility. When an oil is placed on water the -COOH groups are attracted to the water and the hydrocarbon chains repelled but attracted to each other. The process leads the oil over the surface until all the -COOH groups are in contact if possible. Pure hydrocarbon oils will not spread over water. Benzene will not mix with water. When a limited amount of oil is present the spreading ceases when all the water-attracted groups are in contact with water. If weight $w$ of oil spreads over water surface $A$, the area covered by each molecule is $A M / w N$ where $M$ is the molecular weight of the oil $(\mathrm{O}=16), N$, Avogadro's constant. The vertical length of a molecule $l=M / a \rho N=W / \rho A$ where $\rho$ is the oil density and $a$ the horizontal area of the molecule.

| Substance | Cross section in $\mathrm{cm}^{2} \times 10^{16}$ | $\begin{aligned} & l \text { in } \mathrm{cm} \\ & \left(\text { lengtb) } \times 10^{8}\right. \end{aligned}$ |
| :---: | :---: | :---: |
| Palmitic acid $\mathrm{C}_{13} \mathrm{H}_{31} \mathrm{COOH}$ | 24 | 19.6 |
| Stearic acid $\mathrm{C}_{17} \mathrm{H}_{35} \mathrm{COOH}$. | 24 | 21.8 |
| Cerotic acid $\mathrm{C}_{25} \mathrm{H}_{51} \mathrm{COOH}$ | 25 | 29.0 |
| Oleic acid $\mathrm{C}_{1}: \mathrm{H}_{33} \mathrm{COOH}$. | 48 | 10.8 |
| Linoleic acid $\mathrm{C}_{17} \mathrm{H}_{31} \mathrm{COOH}$ | 47 | 10.7 |
| Linolenic acid $\mathrm{C}_{17} \mathrm{H}_{22} \mathrm{COOH}$ | 66 | 7.6 |
| Ricinoleic acid $\mathrm{C}_{17} \mathrm{H}_{32}(\mathrm{OH}) \mathrm{COOH}$ | 90 | 5.8 |
| Cetyl alcohol $\mathrm{C}_{18} \mathrm{H}_{33} \mathrm{OH} \ldots . . . . . .$. . | 21 | 21.9 |
| Myricyl alcohol $\mathrm{C}_{30} \mathrm{H}_{61} \mathrm{OH}$. | 29 | 35.2 |
| Cetyl palmitate $\mathrm{C}_{15} \mathrm{H}_{31} \mathrm{COOC}_{10} \mathrm{H}_{33}$ | 21 | 44.0 |
| Tristearin ( $\left.\mathrm{C}_{18} \mathrm{H}_{35} \mathrm{O}_{2}\right)_{3} \mathrm{C}_{3} \mathrm{H}_{5} \ldots \ldots$. | 69 | 23.7 |
| Trielaidin $\left(\mathrm{C}_{18} \mathrm{H}_{33} \mathrm{O}_{2}\right)_{3} \mathrm{C}_{3} \mathrm{H}_{5}$ | 137 | 11.9 |
| Triolein $\left(\mathrm{C}_{18} \mathrm{H}_{33} \mathrm{O}_{2}\right)_{3} \mathrm{C}_{3} \mathrm{H}_{5}$. | 145 | 11.2 |
| Castor oil ( $\left.\mathrm{C}_{77} \mathrm{H}_{32}(\mathrm{OH}) \mathrm{COO}\right)_{3} \mathrm{C}_{3} \mathrm{H}_{5}$ | 280 | 5.7 |
| Linseed oil ( $\left.\mathrm{C}_{12} \mathrm{H}_{31} \mathrm{COO}\right)_{3} \mathrm{C}_{3} \mathrm{H}_{5} \ldots$ | 143 | 11.0 |

TABLE 706.-VOLUMES OF INERT GAS ATOMS *

| Gas | Vo'ume from radius | $b$ | $\frac{b}{\text { volume }}$ | $\begin{gathered} \text { Volume } \\ \text { of } \\ \text { liquid } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| Neon | 3.33 | 17.1 | 5.1 | 16.7 |
| Argon | 8.6 | 32.2 | 3.8 | 28.1 |
| Krypton | 12.5 | 39.7 | 3.2 | 38.9 |
| Xenon | 18.8 | 50.8 | 2.7 | 47.5 |

[^280]| Material | $\begin{gathered} \text { ro } \\ \text { observed } \\ A \end{gathered}$ | $\stackrel{r_{0}}{\text { calculated }}$ | Melting ${ }^{\circ} \mathrm{C}$ ( C , | Material | $\stackrel{\text { ro }}{\text { observed }}$ |  | Melting ${ }^{\text {point, }} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sodium chloride structure |  |  |  |  |  |  |  |
| LiF | 2.01 | 2.10 | 870 | NH4 | 3.62 | 3.65 |  |
| LiCl | 2.57 | 2.60 | 613 | AgF | 2.46 | 2.30 | 435 |
| LiBr | 2.75 | 2.75 | 547 | AgCl | 2.77 | 2.80 | 455 |
| LiI | 3.00 | 3.00 | 446 | AgBr | 2.88 | 2.95 | 434 |
| NaF | 2.31 | 2.35 | 980 | MgO | 2.10 | 2.15 | 2800 |
| NaCl | 2.81 | 2.85 | 804 | MgS | 2.60 | 2.60 |  |
| NaBr | 2.98 | 3.00 | 755 | MgSe | 2.73 | 2.70 |  |
| NaI | 3.23 | 3.25 | 651 | CaO | 2.40 | 2.40 | 2572 |
| KF | 2.67 | 2.65 | 880 | CaS. | 2.84 | 2.85 |  |
| KCl | 3.14 | 3.15 | 776 | CaSe | 2.96 | 2.95 |  |
| KBr | 3.29 | 3.30 | 730 | CaTe | 2.97 | 3.15 |  |
| KI | 3.53 | 3.55 | 773 | SrO | 2.58 | 2.60 | 2430 |
| RbF | 2.82 | 2.80 | 760 | SrS . | 3.01 | 3.05 | 882 |
| RbCl | 3.27 | 3.30 | 715 | SrSe | 3.12 | 3.15 |  |
| RbBr | 3.43 | 3.45 | 682 | SrTe. | 3.33 | 3.35 |  |
| RbI | 3.66 | 3.70 | 642 | BaO. | 2.77 | 2.75 | 1923 |
|  | 3.00 | 3.05 | 684 | BaS . | 3.19 | 3.20 |  |
| $\mathrm{NH}, \mathrm{Cl}$ | 3.27 | 3.25 |  | BaSe | 3.30 | 3.30 |  |
| $\mathrm{NH}_{4} \mathrm{Br}$ | 3.45 | 3.40 |  | BaTe | 3.50 | 3.50 |  |
| Cesium chloride structure |  |  |  |  |  |  |  |
| CsCl | 3.56 | 3.55 | 646 | $\mathrm{NH}_{4} \mathrm{Br}$ | 3.51 | 3.40 |  |
| CsBr | 3.71 | 3.70 | 636 | $\mathrm{NH}_{4} \mathrm{I}$ | 3.78 | 3.65 |  |
|  |  | 3.95 | 621 | TICl | 3.33 |  | 430 |
| $\mathrm{NH}_{4} \mathrm{Cl}$ | 3.34 | 3.25 |  | TlBr | 3.44 |  | 460 |
| Zincblende structure |  |  |  |  |  |  |  |
| CuCl | 2.34 | 2.30 | 422 | ZnTe | 2.64 | 2.65 |  |
| CuBr | 2.46 | 2.45 | 504 | CdS | 2.52 | 2.50 | 1750 |
| CuI | 2.62 | 2.70 | 605 | CdSe | 2.62 | 2.60 |  |
| BeS | 2.10 | 2.10 |  | CdTe |  | 2.80 |  |
| BeSe | 2.18 | 2.20 |  | HgS | 2.53 | 2.50 |  |
| BeTe | 2.43 | 2.40 |  | HgSe | 2.62 | 2.60 |  |
| ZnS | 2.35 | 2.35 | 1800 | HgTe | 2.79 | 2.80 |  |
| ZnSe | 2.45 | 2.45 |  |  |  |  |  |

Wurtzite structure (first distance is that to neighbor along axis, second to three neighbors in same layer)

| $\mathrm{NH}_{4} \mathrm{~F}$ | 2.63, 2.76 | 2.75 |  | ZnS | 2.36, 2.36 | 2.35 | 1850 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BeO | 1.64, 1.60 | 1.65 | 2570 | CdS | 2.52, 2.56 | 2.50 | 1750 |
| Z 11 O | 1.94, 2.04 | 1.90 |  | CdSe | 2.63, 2.64 | 2.60 |  |

[^281](Angstroms)

| $\begin{gathered} \mathrm{Be}^{++} \\ .20 \end{gathered}$ | $\begin{gathered} \mathrm{Li}^{+} \\ .80 \end{gathered}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Mg}^{++}$ | $\mathrm{Na}^{+}$ | $\mathrm{F}^{-}$ | $\mathrm{O}^{--}$ |  |  |
| . 70 | 1.05 | 1.30 | 1.45 |  |  |
| $\mathrm{Ca}^{++}$ | $\mathrm{K}^{+}$ | $\mathrm{Cl}^{-}$ | $\mathrm{S}^{--}$ | $\mathrm{Zn}^{++}$ | $\mathrm{Cu}^{+}$ |
| . 95 | 1.35 | 1.80 | 1.90 |  | . 50 |
| Sr ${ }^{++}$ | $\mathrm{Rb}^{+}$ | $\mathrm{Br}^{-}$ | Se-- | $\mathrm{Cd}^{++}$ | $\mathrm{Ag}^{+}$ |
| 1.15 | 1.50 | 1.95 | 2.00 | . 60 | 1.00 |
| $\mathrm{Ba}^{++}$ |  |  | Te ${ }^{-}$ | $\mathrm{Hg}^{+}$ |  |
| 1.30 | $1.75$ | 2.20 | 2.20 | . 60 |  |
|  | $\begin{aligned} & \mathrm{NH}_{4}^{+} \\ & 1.45 \end{aligned}$ |  |  |  |  |

*For reference, see footnote 203, p. 624.

TABLE 703.-CRYSTAL STRUCTURE AND INTERATOMIC DISTANCES FOR METALS (Angstroms) ${ }^{*}$

Abbreviations: b.c., body-centered cubic; f.c., face-centered cubic ; hex, hexagonal ; di, diamond; *, other structures.

| $\begin{aligned} & \mathrm{Li} \text { b.c. } \\ & 3.03 \end{aligned}$ | Na b.c. 3.72 | $\begin{aligned} & \text { K b.c. } \\ & 4.50 \end{aligned}$ | $\begin{aligned} & \mathrm{Rb} \text { b.c. } \\ & 4.86 \end{aligned}$ | $\begin{aligned} & \text { Cs b.c. } \\ & 5.25 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Be hex } \\ & 2.28 \\ & 2.24 \end{aligned}$ | Mg hex <br> 3.20 <br> 3.19 | $\begin{aligned} & \text { Ca f.c. } \\ & 3.93 \end{aligned}$ | $\begin{aligned} & \mathrm{Sr} \text { f.c. } \\ & 4.29 \end{aligned}$ | $\begin{aligned} & \text { Ba b.c. } \\ & 4.35 \end{aligned}$ |
| B | $\begin{aligned} & \mathrm{Al} \text { f.c. } \\ & 2.85 \end{aligned}$ | Sc | $\begin{aligned} & \mathrm{Y} \\ & 3.58 \end{aligned}$ | La hex, f.c. 3.72, 3.73 |
|  |  | Ti hex 2.95 | $\begin{aligned} & \mathrm{Zr} \text { hex } \\ & 3.23 \end{aligned}$ | ${ }_{3.32}$ Hex |
|  |  | 2.90 | 3.18 | 3.33 |
|  |  | $\begin{aligned} & \text { V b.c. } \\ & 2.63 \end{aligned}$ | Nb | $\begin{aligned} & \text { Ta b.c. } \\ & 2.88 \end{aligned}$ |
|  |  | $\begin{aligned} & \mathrm{Cr} \text { b.c. } \\ & 2.49 \end{aligned}$ | $\underset{2.72}{\text { Mo b.c. }}$ | $\begin{aligned} & \mathrm{W} \text { b.c. } \\ & 2.73 \end{aligned}$ |
|  |  | $\mathrm{Mn}_{2.50}{ }^{*}$ |  |  |
|  |  | Fe f.c. $2.57,2.48$ | $\begin{aligned} & \text { Ru hex } \\ & 2.69 \\ & 2.65 \end{aligned}$ | $\begin{aligned} & \text { Os hex } \\ & 2.71 \\ & 2.67 \end{aligned}$ |
|  |  | $\begin{aligned} & \text { Co hex, f.c. } \\ & 2.71 \end{aligned}$ | $\begin{aligned} & \mathrm{Rh} \text { f.c. } \\ & 2.69 \end{aligned}$ | $\begin{aligned} & \text { Ir f.c. } \\ & 2.70 \end{aligned}$ |
|  |  | $\begin{aligned} & \mathrm{Ni} \text { f.c. } \\ & 2.49 \end{aligned}$ | Pd f.c. 2.74 | $\begin{aligned} & \mathrm{Pt} \text { f.c. } \\ & 2.76 \end{aligned}$ |
|  |  | ${\underset{2.55}{\mathrm{Cu}} \text { f.c. } . ~}_{\text {. }}$ | $\begin{aligned} & \mathrm{Ag} \text { f.c. } \end{aligned}$ | Au f.c. 2.87 |
|  |  | $\begin{aligned} & \mathrm{Zn} \text { hex } \\ & 2.65 \\ & 2.94 \end{aligned}$ | $\begin{aligned} & \text { Cd hex } \\ & 2.97 \\ & 3.30 \end{aligned}$ | ${\underset{2 g}{ } \mathrm{Hg}^{*}}^{*}$ |
|  |  | $\begin{gathered} \mathrm{Ga}_{2.56}^{*} \end{gathered}$ | $\begin{aligned} & \text { In * } \\ & 3.24,3.33 \end{aligned}$ | Tl hex, f.c. 3.45, 3.43 |
|  | $\underset{2.35}{\mathrm{Si} \mathrm{di}}$ | $\begin{aligned} & \mathrm{Ge} \text { di } \\ & 2.43 \end{aligned}$ | $\underset{2.80}{\mathrm{Sn}^{\mathrm{di}}}$ | $\mathrm{Pb} \text { f.c. }$ $3.49$ |
|  |  | $\begin{aligned} & \text { As * } \\ & 2.50 \end{aligned}$ | $\mathrm{Sb}_{2.88}{ }^{*}$ | $\begin{aligned} & \mathrm{Bi}^{\mathrm{Bi}}{ }^{*} \end{aligned}$ |
|  |  | $\begin{aligned} & \mathrm{Se}^{*} .32 \end{aligned}$ | $\begin{aligned} & \mathrm{Te}^{*} \\ & 2.88 \end{aligned}$ |  |

[^282]The binding energy has been calculated by multiplying the absolute value of the appropriate energy level (in $\mathrm{cm}^{-1}$ ), referred to its proper limit,
by the factor 0.00012395 , to express it in electron volts. A dash indicates that no such term exists. Brackets denote an estimated value.

| Element | $1 s$ | 2 s | $2 p$ | 3 s | 3p | $3 d$ |  | $4 s$ |  | 4p |  | $4 d$ |  | 5s |  | 5p |  | 5d |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HI | 13.59 | 3.40 | 3.40 | 1.51 | 1.51 |  |  | . 85 |  | . 85 |  | . 85 |  | . 54 |  | . 54 |  | . 54 |  |
| He 1 | 24.58 | 4.77 | 3.62 | 1.87 | 1.58 |  |  | $.99$ |  | . 88 |  | . 85 |  |  |  | . 56 |  | . 54 |  |
| Li 1 | . . . | 5.39 | 3.54 | 2.02 | 1.56 |  |  |  |  | [1.87 |  | . 85 |  | . 62 |  | . 55 |  | . 54 |  |
| Be I | . . | 9.32 | 6.60 | 2.86 | 2.03 |  |  |  |  | [1.15] |  | . 90 |  | . 77 |  | [.69] |  | . 57 |  |
| $\mathrm{B}_{1}$ | - | ... | 8.30 | 3.33 |  |  |  |  |  |  |  |  |  | . 84 |  | [.69] |  | . 55 |  |
| $\mathrm{C}_{\mathrm{N}} \mathrm{I}$ | ... | . . | 11.26 | 3.79 | 2.73 |  |  |  |  | 1.33 |  | . 91 |  | . 87 |  | . 75 |  | . 58 |  |
| N O I | $\ldots$ | . . | 11.54 13.61 | 4.22 4.47 | 2.95 |  |  |  |  |  |  |  |  | . 93 |  | . |  | . 57 |  |
| $\mathrm{F}_{\mathrm{F}}^{1}$ | $\ldots$ | $\ldots$ | 13.61 $17.42^{*}$ | 4.47 4.72 | 2.88 3.05 |  |  |  |  |  |  | . 86 |  | . 96 |  | . 74 |  | . 55 |  |
| $\mathrm{Ne} \mathrm{I}^{\text {I }}$ | ... | ... | 21.56 | 4.94 | 3.18 |  |  |  |  |  |  | . 86 |  | . 98 |  | . 78 |  | . 55 |  |
| Na 1 | ... | . . | . . . | 5.14 | 3.04 |  |  |  |  |  |  | . 86 |  | 1.02 |  | . 79 |  | . 55 |  |
| Mg 1 | . . . | . . | . . . | 7.64 | 4.94 |  |  |  |  |  |  |  |  | 1.21 |  | . 92 |  | . 66 |  |
| Al 1 | . . | . . | . . | . . | 5.98 |  |  |  |  |  |  | 1.16 |  |  |  | . 99 |  | . 75 |  |
| Si 1 | ... | ... | . . |  | 8.15 |  |  |  |  | $\begin{array}{ll}2.29 & 1.45\end{array}$ |  |  |  | 1.43 |  | 1.15 |  | . 83 |  |
| ${ }^{P} 1$ | ... | ... | ... | . . | [10.55] ${ }^{\text {b }}$ |  |  |  |  |  |  |  |  | [1.59] |  |  |  |  |  |
| $\mathrm{S}_{1}$ | ... |  | ... | . . | 10.36 |  |  |  |  | 2.49 |  | 1.06 |  |  |  | 1.201.30 |  | . 66 |  |
| $\mathrm{Cl}_{1}$ |  |  |  |  | 13.01 |  |  |  |  |  |  |  |  | 1.69 |  |  |  |  |  |
| $A_{1}$ | - . | - . | - . | - . | 15.76 | 1.91 |  | 4.21 |  | 2.85 |  | 1.07 |  |  |  | 1.30 |  | . 66 |  |
|  |  |  |  |  |  | $A \dagger$ | $B \ddagger$ | A | $B$ | A | $B$ | A | $B$ | A | $B$ | A | $B$ | A | $B$ |
| $\mathrm{K}_{1}$ |  | ... | ... |  | . . | 1.67 | 5 | 4.34 | . | 2.73 |  | . 94 |  | 1.73 |  | 1.28 | - | . 60 |  |
| Ca I | ... | $\ldots$ | . . |  | . . |  | 3.59 | 5.28 | 6.11 | 3.37 | 4.23 | 1.44 | 1.49 | 1.92 | 2.20 | 1.45 | 1.58 | . 81 | . 81 |
| Sci | . . |  |  |  |  | 2.97 | 5.13 | 5.73 | 6.56 | 3.56 | 4.62 |  | 1.96 | 1.96 | 2.30 |  |  |  |  |
| Ti 1 | ... | ... | $\ldots$ | . . . |  | 3.38 | 6.02 | 6.13 | 6.83 | 3.66 | 4.87 | 1.51 | 1.73 | 2.10 | 2.38 |  | 1.65 |  | . 90 |
| V I | . $\cdot$ | $\ldots$ | ... | $\cdots$ | . $\cdot$ | 4.23 | 6.80 | 6.48 | 7.06 | 3.68 | 5.03 | 1.53 | 1.65 | 2.14 | 2.43 |  |  |  | . 90 |
| $\mathrm{CrI}^{\text {r }}$ | ... | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 2.38 | 8.25 | 6.76 | 7.29 | 3.87 | 5.15 | 1.53 | 1.66 | 2.19 | 2.49 | 1.53 |  | . 85 |  |
| Mn I | $\cdots$ | $\cdots$ | . $\cdot$ | ... | $\ldots$ |  | 5.32 | 7.09 | 7.43 | 4.03 | 5.15 | 1.55 | 1.64 | 2.24 | 2.54 |  | 1.73 |  | . 90 |
| Fe 1 | ... | ... | ... |  | . . . | 4.05 | 7.04 | 7.27 | 7.90 | 4.03 | 5.50 | 1.55 | 1.66 | 2.30 | 2.59 |  |  |  | . 9 |
| Cor |  |  | $\cdots$ |  |  | 4.45 | 7.85 | 7.43 | 8.28 | 3.89 | 5.35 | 1.54 | 1.65 | 2.31 | 2.62 |  |  |  |  |
| Ni 1 |  |  |  |  |  | 5.81 | 8.65 | 7.61 | 8.67 | 4.09 | 5.48 | 1.56 | 1.65 | 2.35 | 2.67 | 1.59 |  | . 87 | . 89 |
| Cu I |  | $\ldots$ |  |  |  |  | 10.44 | 7.72 | 9.05 | 3.94 | 5.61 | 1.53 | 1.66 | 2.38 | 2.71 | 1.60 | 1.73 | . 86 | . 92 |
| Zn 1 |  | . . |  |  |  | - |  |  | 9.39 |  | 5.39 |  | 1.65 |  | 2.74 |  | 1.80 |  | . 92 |
| Ga 1 | ... | . . | . . . | . . | $\cdots$ |  |  |  |  |  |  |  |  |  |  |  |  |  | 4 |
| Ge 1 | . . . | $\ldots$ | $\cdots$ |  | ... |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| As 1 | . . | $\ldots$ | . . | $\ldots$ | ... |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Se I | . . | ... |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\stackrel{\mathrm{Br}}{1}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Kr 1 | - . |  | $\cdots$ |  | $\cdots$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  | $A$ | $B$ | A | $B$ | A | $B$ | A | $B$ |
| Rb i |  |  |  |  |  |  |  |  |  |  |  | 1.78 |  | 4.18 |  | 2.62 |  | . 99 | - |
| Sri |  | $\ldots$ | . $\cdot$ | $\ldots$ | ... |  |  |  |  |  |  |  | 3.44 |  | 5.69 | 3.37 | 3.92 |  | 1.39 |
|  | $\ldots$ | $\ldots$ | $\ldots$ | . . | $\ldots$ |  |  |  |  |  |  | 3.89 4.58 | 5.27 6.35 | 6.16 6.67 | 6.63 695 | 3.96 4.34 | 4.78 |  | 1.86 |
| $\stackrel{\mathrm{Nr}_{1}}{ }$ | $\cdots$ | $\ldots$ | $\ldots$ | $\ldots$ | . |  |  |  |  |  |  | 4.58 5.36 | 6.35 | 6.67 6.77 | 6.63 6.92 | 4.34 4.04 | 5.12 4.99 |  | 2.00 |

[^283] SINGLY-IONIZED ATOMS* $\dagger$

| Element | is | $2 s$ | $2 p$ | $3 s$ | 3p | $3 d$ | $4 s$ | $4 p$ | $4 d$ | $5 s$ | 5p | 5d |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| He II | 54.40 | 13.60 | 13.60 | 6.04 | 6.04 | 6.04 | 3.40 | 3.40 | 3.40 | 2.18 | 2.18 | 2.18 |
| Li ir | 75.62 | 16.61 | 14.35 | 6.86 | 6.27 | 6.05 | 3.73 | 3.49 | 3.40 | 2.34 | 2.22 | 2.18 |
| Be II |  | 18.21 | 14.25 | 7.27 | 6.25 | 6.05 | 3.89 | 3.49 | 3.40 | 2.42 | 2.22 | 2.18 |
| B II |  | 25.15 | 20.52 | 9.06 | 7.30 | 6.48 | 4.53 | 3.89 | 3.57 | 2.73 |  | 2.26 |
| C II |  |  | 24.38 | 9.93 | 8.05 | 6.33 | 4.89 | 4.23 | 3.54 | 2.89 | 2.65 | 2.25 |
| N II |  |  | 29.61 | 11.15 | 9.20 | 6.49 | 5.24 | 4.55 | 3.62 | 3.05 |  | 2.25 |
| O II |  |  | 35.15 | 12.19 | 9.87 | 6.48 | 5.57 | 4.68 | 3.60 | 3.20 | 2.80 | 2.27 |
| $\mathrm{F}_{\text {II }}$ |  |  | 34.98 | 13.08 | 9.86 | 6.33 | 5.81 | 4.40 | 3.49 |  |  |  |
| Ne II |  |  | 41.07 | 13.91 | 10.55 | 6.47 | 6.12 |  | 3.60 |  |  |  |
| Na II |  |  | 47.29 | 14.45 | 10.95 | 6.32 | 6.20 |  | 3.47 | 3.50 |  |  |
| Mg II |  |  |  | 15.03 | 10.61 | 6.17 | 6.38 | 5.04 | 3.47 | 3.53 | 2.95 | 2.21 |
| Al II |  |  |  | 18.82 | 14.19 | 6.98 | 7.51 | 5.76 | 3.77 | 3.94 | 3.24 | 2.36 |
| Si II |  |  |  |  | 16.34 | 6.51 | 8.22 | 6.28 | 3.82 | 4.20 | 3.47 | 2.41 |
| P II |  |  |  |  | 19.65 | 6.81 | 8.92 | 6.86 | 4.16 | 4.36 |  | 2.41 |
| S II |  |  |  |  | 23.4 | 9.75 | 9.82 | 7.85 | 4.57 | 4.78 | 3.06 |  |
| Cl II |  |  |  |  | 23.80 | 10.13 | 10.43 | 7.86 | 4.63 | 4.93 |  | 2.75 |
| A II |  |  |  |  | 27.62 | 11.22 | 10.98 | 8.40 | 4.85 | 5.11 | 4.05 | 2.28 |
| K II |  |  |  |  | 31.81 | 11.55 | 11.67 | 9.10 | 5.11 | 5.46 |  |  |
| Ca II |  |  |  |  |  | 10.18 | 11.87 | 8.75 | 4.82 | 5.40 | 4.36 | 2.85 |
| Sc II |  |  |  |  |  | 12.20 | 12.80 | 9.56 | 5.42 | 5.66 |  |  |
| Ti II |  |  |  |  |  | 13.46 | 13.57 | 9.91 | 5.53 | 5.87 |  |  |
| V II |  |  |  |  |  | 14.65 | 14.33 | 10.36 | 5.67 |  |  |  |
| Cr II |  |  |  |  |  | 16.49 | 15.01 | 10.69 | 5.76 | 6.24 |  |  |
| Mn II |  |  |  |  |  | 13.86 | 15.64 | 10.88 | 5.78 | 6.39 | 4.99? | 3.25 |
| Fe II |  |  |  |  |  | 15.95 | 16.18 | 11.41 | 5.91 | 6.53 | 5.35 |  |
| Co II |  |  |  |  |  | 17.05 | 16.64 | 11.45 |  | 6.64 |  |  |
| Ni II |  |  |  |  |  | 18.15 | 17.11 | 11.76 |  | 6.77 |  |  |
| Cu II |  |  |  |  |  | 20.29 | 17.57 | 12.05 | 6.09 | 6.90 | 5.40 | 3.39 |
| Zn II |  |  |  |  |  |  | 17.96 | 11.95 | 5.95 | 7.00 | 5.39 | 3.34 |
| Ga II |  |  |  |  |  |  | 20.51 | 14.64 | 7.16 | 7.75 | 5.83 | 3.51 |
| Ge II |  |  |  |  |  |  |  | 15.93 | 5.91 | 8.20 | 6.14 | 3.52 |
| As II |  |  |  |  |  |  |  | 20.2 | 9.2 | 10.4 | 8.4 |  |
| Se II |  |  |  |  |  |  |  | 21.5 |  | 9.70 | 7.50 | 4.36 |
| Br II |  |  |  |  |  |  |  | 21.6 | 7.65 | 9.94 | 7.37 | 4.32 |
| Kr ${ }_{11}$ |  |  |  |  |  |  |  | 24.56 | 8.95 | 10.58 | 7.96 | 4.63 |
| Rb II |  |  |  |  |  |  |  | 27.50 |  | 10.97 | 8.38 | 4.67 |
| Sr II |  |  |  |  |  |  |  |  | 9.22 | 11.03 | 8.09 | 4.42 |
| Y 11 |  |  |  |  |  |  |  |  | 11.40 | 12.29 | 9.15 | 5.14 |
| Zr II |  |  |  |  |  |  |  |  | 13.71 | 14.03 | 10.56 | 4.87 |
| Nb II |  |  | . . . |  | .... | .... | .... |  |  |  |  |  |

* See column 6, Table 623.
$\dagger$ For reference, see footnote 222, p. 649.


## TABLE 712.-CONSTANTS OF DIATOMIC MOLECULES *

The attractive force between atoms varies with the distance between centers. When this distance $=r_{e}$, the sum of the two radii, the force changes from an attraction to a repulsion. The force, $D$, at this distance, $r_{e}$, is thus the force necessary to pull the two atoms apart. The energy of separation is generally given.

| Substance | $\underset{\substack{\text { kgcal } \\ \text { mole }}}{D}$ | electron volts | $\stackrel{r}{\text { a }}$ | Substance | $\underset{\substack{\text { kgcal } \\ \text { mole }}}{\text { and }}$ | $\underset{\substack{D \\ \text { electron } \\ \text { volts }}}{ }$ | ${ }^{\text {r }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{H}_{2}$ | 103 | 4.454 | . 75 | CO | 223 | 9.6 | 1.13 |
| CH | 81 | 3.5 | 1.12 | $\mathrm{C}_{2}$ | 128 | 5.6 | 1.31 |
| NH | 97 | 4.2 | 1.08 | $\mathrm{Cl}_{2}$ | 57 | 2.47 | 1.98 |
| OH | 102 | 4.4 | . 96 | $\mathrm{Br}_{2}$ | 46 | 1.96 | 2.28 |
| HCl | 102 | 4.40 | 1.27 | $\mathrm{I}_{2}$ | 36 | 1.53 | 2.66 |
| NO | 123 | 5.3 | 1.15 | $\mathrm{Li}_{2}$ | 26 | 1.14 | 2.67 |
| $\mathrm{O}_{2}$ | 117 | 5.09 | 1.20 | $\mathrm{Na}_{2}$ | 18 | . 76 | 3.07 |
| $\mathrm{N}_{2}$ | 170 | 7.35 | 1.09 | $\mathrm{K}_{2}$ | 12 | . 51 | 3.91 |

[^284]Nuclear physics may be divided into three fields: radioactivity, cosmic rays, and artificial disintegration. The third division-artificial disintegration-is today the most active single experimental (and theoretical) problem of the physicist. This new branch of physics has introduced a number of terms, some of which are defined in Table 716. There is hardly a major physical laboratory that does not have at least one of the devices listed in Table 718 for producing high-energy particles of one kind or another.

The study of nuclear physics started more than 50 years ago with the discovery of radioactivity. This was a study of natural disintegration up to about 1919 when Rutherford produced and studied artificial disintegration by bombarding nitrogen with swift $a$-particles from $\mathrm{RaC}^{\prime}$. However, he had to depend upon nature for the high-speed particles that he used. The value of the speed and energy of the $\alpha$-rays from natural radioactive materials (Table 732) shows the nature of the particles then available. It was not until about 10 years later that a start was made on the development of the various devices for producing the regulated high-speed and high-energy particles listed in Table 718.
By bombarding different materials with one of the high-speed particles produced by various devices it has been found possible to produce one or more radioactive isotopes of each of the 92 elements and, in addition, to produce 6 elements beyond uranium-each with a number of isotopes.* There are now 9 or 10 known fundamental particles (Table 720), 5 or 6 of which are used in the bombardment of isotopes for the production of new reactions. Some examples of reactions thus brought about by the use of different ones of these high-speed particles together with the minimum energy of the particles necessary to produce the reactions are given in Table 726.

The relative masses of the isotopes vary from 1.0081374 for $\mathrm{H}^{1}$ to about 242.14152 for $\mathrm{Cm}^{242}$. The actual mass in grams for $\mathrm{H}^{1}$ is $1.67339 \times 10^{-24}$ grams, and thus the mass, in grams, of any atom may be determined from its atomic weight. The mass of the neutron is $1.67473 \times 10^{-24} \mathrm{~g}$. The radius of a nucleus, $r$, is given approximately by $1.4 \times 10^{-13} A^{1 / 3} \mathrm{~cm}, A$ being the atomic mass number. These values give for the density of the nucleus about $10^{14}$ $\mathrm{g} / \mathrm{cm}^{3}$ (see Table 872). The atomic weight, the magnetic moment, and the spin of a number of isotopes are given in Table 719.

* For reference, see footnote 199, p. 618.

TABLE 713.-MASS, ENERGY, AND VELOCITY RELATIONS FOR THE ELECTRON

| Energy <br> Mev <br> very small | g <br> $9.1066 \times 10^{-28}$ | $m_{0}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |

The neutrons and protons are held together in a nucleus by attractive forces (nuclear force) which have a range of only about $2 \times 10^{-13} \mathrm{~cm}$ but are stronger than the electric Coulomb forces at distances less than this range. The energy which would be required to separate a nucleus into its constituent protons and neutrons (collectively denoted by nucleons) is called the nuclear binding energy. According to Einstein's mass-energy relation this binding energy is equal to $c^{2}$ times the difference between the nuclear mass and the mass in the free state of the nucleons contained in the nucleus. The binding energy per nucleon is of the order of magnitude of a few Mev, its actual amount depending on various factors. Starting at about 1 Mev for the deuteron (nucleus of heavy hydrogen) the binding energy per nucleon increases on the average with increasing atomic weight $A$ reaching a maximum of about 10 Mev for $A$ about 50 ; as $A$ increases further the Coulomb repulsion between the constituent protons becomes more and more important and the binding energy per particle decreases again. In addition to this general trend there are individual variations in stability, a notable example being the great stability of the $a$-particle (nucleus of $\mathrm{He}^{4}$ ) with a binding energy of more than 7 Mev per nucleon.

The theory of relativity shows that energy and mass are related and that mass may be converted into energy, giving an amount of energy in ergs $=m c^{2}$, where $c$ is the velocity of light expressed in $\mathrm{cm} / \mathrm{sec}$ and $m$ the mass in grams. This theory also shows that the velocity of light is the upper limit for the velocity for any particle. It is to be noted that this theory tells us nothing as to the method of converting mass to energy!

The mass $m$ of a fast-moving particle depends upon its velocity $v$, thus, $m$ (at velocity $v$ ) $=\frac{m_{o}}{\sqrt{1-\beta^{2}}}$ where $\beta=v / c$. The kinetic energy of a particle moving with a velocity near that of light

$$
K E \doteq m_{0} c^{2}\left(\frac{1}{\sqrt{1-\beta^{2}}}-1\right)
$$

or

$$
m \doteq m_{o}+\frac{K E}{c^{2}}
$$

Some calculated results of the above relations are shown in Table 713. This theory, together with nuclear physics, shows that each moving particle has a wavelength that is given thus: the wavelength, $\lambda=h / m v$ for a particle of mass $m$ with a velocity $v$. (See Table 722.)

## TABLE 715.-TWO INTERESTING RESULTS OF ARTIFICIAL DISINTEGRATION *

| Different results from the same material ${ }_{13} \mathrm{Al}^{27}+{ }_{2} \mathrm{He}^{4} \rightarrow{ }_{15} \mathrm{P}^{20}+{ }^{20}{ }^{1}$ ${ }_{13} \mathrm{Al}^{27}+{ }_{2} \mathrm{He}^{4} \rightarrow{ }_{14} \mathrm{Si}^{30}+{ }_{1} \mathrm{H}^{1}$ ${ }_{13} \mathrm{Al}^{27}+{ }_{1} \mathrm{H}^{2} \rightarrow{ }_{12} \mathrm{Mg}^{25}+{ }_{6} \mathrm{He}^{4}$ ${ }_{13} \mathrm{Al}^{27}+{ }_{1} \mathrm{H}^{2} \rightarrow{ }_{13} \mathrm{Al}^{24}+{ }_{1} \mathrm{H}^{2}$ ${ }_{13} \mathrm{Al}^{27}+{ }_{1} \mathrm{H}^{1} \rightarrow{ }_{14} \mathrm{Si}^{27}+{ }_{\mathrm{on}}{ }^{1}$ ${ }_{13} \mathrm{Al}^{27}+{ }_{0 n^{1}} \rightarrow{ }_{13} \mathrm{Al}^{28}+h \nu$ ${ }_{13} \mathrm{Al}^{27}+{ }_{0 n^{1}} \rightarrow{ }_{12} \mathrm{Mg}^{27}+{ }_{1} \mathrm{H}^{1}$ ${ }_{13} \mathrm{Al}^{27}+{ }_{o n}{ }^{1} \rightarrow{ }_{11} \mathrm{Na}^{24}+{ }_{2} \mathrm{He}^{6}$ |
| :---: |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |

Different results from the same material ${ }_{13} \mathrm{Al}^{27}+{ }_{2} \mathrm{He}^{4} \rightarrow{ }_{15} \mathrm{P}^{30}+{ }_{0} n^{1}$ ${ }_{13} \mathrm{Al}^{27}+{ }_{2} \mathrm{He}^{4} \rightarrow{ }_{44} \mathrm{Si}^{30}+{ }_{1} \mathrm{H}^{1}$ ${ }_{13} \mathrm{Al}^{27}+{ }_{1} \mathrm{H}^{2} \rightarrow{ }_{12} \mathrm{Mg}^{25}+{ }_{8} \mathrm{He}^{4}$ ${ }_{13} \mathrm{Al}^{27}+\mathrm{H}^{1} \rightarrow{ }_{13} \mathrm{~S}^{27}+\mathrm{H}_{12}$ ${ }_{13} \mathrm{Al}^{27}+{ }_{o n^{1}} \rightarrow{ }_{18} \mathrm{Al}^{28}+h \nu$ ${ }_{13} \mathrm{Al}^{27}+{ }_{\mathrm{on}}{ }^{1} \rightarrow{ }_{12} \mathrm{Mg}^{27}+{ }_{1} \mathrm{H}^{1}$ ${ }_{13} \mathrm{Al}^{27}+{ }_{o n}{ }^{1} \rightarrow{ }_{11} \mathrm{Na}^{24}+{ }_{2} \mathrm{He}^{4}$
Different ways of
producing the same materials
${ }_{12} \mathrm{Mg}^{25}+{ }_{2} \mathrm{He}^{4} \rightarrow{ }_{13} \mathrm{Al}^{28}+{ }_{1} \mathrm{H}^{1}$
${ }_{33} \mathrm{Al}^{28}+{ }_{1} \mathrm{H}^{2} \rightarrow{ }_{13} \mathrm{Al}^{28}+{ }_{1} \mathrm{H}^{1}$
${ }_{18} \mathrm{Al}^{27}+{ }^{29}{ }^{2} \rightarrow{ }_{13} \mathrm{Al}^{28}+h \nu$
${ }_{14} \mathrm{Si}^{28}+{ }_{0 n^{1}} \rightarrow{ }_{18} \mathrm{Al}^{28}+{ }_{1} \mathrm{H}^{1}$
${ }_{15} \mathrm{P}^{31}+{ }_{o n^{1}} \rightarrow{ }_{13} \mathrm{Al}^{28}+{ }_{2} \mathrm{He}^{4}$

[^285]Alpha-particle.-A helium atom, stripped of its outer electrons, that is expelled from a radioactive material.

Artificial disintegration.-Breaking down of an atom by a controlled experiment.
Atom.-The smallest particle of any material substance that can exist as such.
Atomic bomb.-A bomb depending upon atomic energy. ( U or Pu fission.)
Atomic energy.-Energy due to some breaking down of an atom.
Atomic mass unit, amu.-(1) The mass of a unit atomic weight (see Dalton). (2) An energy unit equal to the mass energy ( $m c^{2}$ ) of a unit atomic mass ( $1 / 16$ mass $0^{16}$ ) $=$ $1.4921 \times 10^{-4} \mathrm{ergs}=931.3 \mathrm{Mev}$.

Atomic number.-The value of the positive charge of the atom. This determines the chemical properties.

Atomic weight.-Chemical: The relative weight of an atom taking the oxygen atom, found in nature, as having a weight of 16 . Physical: The relative weight of an atom taking the oxygen isotope 16 as having a weight of 16 . This makes the ratio of physical to chemical scale $=1.000272 \pm .000005$.

Barn.-Unit area cross section of nucleus $=10^{-24} \mathrm{~cm}^{2}$.
Baryton.-See Table 720. See meson.
Beta-ray.-An electron expelled from a radioactive material.
Betatron.-See Table 718.
Binding energy.-The energy due to the packing of an element assuming that the element is made up of protons, electrons, and neutrons.

Bursts (cosmic ray).-A very great output of particles due to a cosmic-ray encounter with an atom.

Cathode rays.-Electrons that are driven from the negative electrode (the cathode) of a discharge tube. (See Table 758.)

Chain reaction.-A reaction in which one or more of the products of the reaction keeps it going, i.e., such as the fission of $92 \mathrm{U}^{235}$.

Compton effect.-The change in wavelength due to the scattering of radiation by a material substance.

Cosmic rays.-A radiation that falls upon the outer atmosphere, generally thought to come from outer space. (See page 710.)

Cosmos.-The entire universe.
Cross section, $\sigma$.-The proportionality constant between the beam intensity and the number of particles, considered, that strike a target. It has the dimension of an area. See Barn.

Cyclotron.-See Table 718.
De Broglie wavelength.-For a particle of mass $m$ and velocity $v$, the De Broglie wavelength $\lambda=h / m v$.

Delta-rays.-Electrons that are emitted from certain materials due to a-ray bombardment.

Deuterium.-See deuteron.
Deuteron.-This isotope of hydrogen that has twice the atomic weight of the proton.
Electron 士.-The smallest particle of electricity that can exist.
Positron, + electron. (Charge $+4.8025 \times 10^{-10}$ esu.)
Negatron, - electron. (Charge $-4.8025 \times 10^{-17}$ esu.)
Electron shell.-The shell that is used to describe the location of the outer electrons of an atom. These are $K, L, M, N, O$. (See Table 658.)

Energy units.-See Table 654. Erg:
ev-The energy equal to that of an electron moving under an emf of 1 volt $=1.602 \times$ $10^{-12}$ ergs.
Mev-The energy equal to that of an electron moving under an emf of $10^{6}$ volts.
amu-The mass-energy of a unit mass of atomic weight $=1.492 \times 10^{-3} \mathrm{ergs}$.
Mass unit-Energy value of one gram $=8.987 \times 10^{20} \mathrm{ergs}$.
Fission. -The breaking down of a heavy atom into two parts of about equal mass. (See page 706.)

Gamma-rays.-Radiation of very short wavelength that results from some radioactive breakdown. (See Tables 747-752.)

H-rays.-Hydrogen atoms that are emitted from certain materials due to a-ray bombardment.
h.-Planck constant. See quantum.
h or $\mathrm{h}=h / 2 \pi$.
Isobar.-One of two or more nuclei that have the same weight but different atomic numbers.

Isomer.-As applied to an isotope, it is one of two or more that have the same atomic number and weight but different radioactive properties.

Isotope.-One of two or more atomic nuclei that differ in weight but have the same atomic number, thus the same chemical characteristics.
Magnetic moment.-Nuclear unit of $=\frac{e h}{4 \pi M_{c}}=5.05 \times 10^{-24} \mathrm{erg} /$ oersted where $M=$ mass of proton.

Magneton (Bohr).-The magnetic moment of the electron $=\frac{c h}{M_{e} 2 \pi c}=9.27 \times 10^{-21}$ erg/oersted.

Mass-energy ratio.-The relativistic relation between mass and energy, i.e., $E=m c^{2}$.
Mass, rest.-The mass of a particle $M_{0}$ when at rest. See Table 714.
Mass-velocity ratio.-The variation of mass with velocity, $v=$ velocity, then
$M_{v}=\frac{M_{0}}{\sqrt{1-\frac{v^{2}}{c^{2}}}}, c=$ velocity of light. (See Table 714.)
Meson (Mesotron).—See Table 720.
Maximum velocity.-The highest velocity for any material substance, i.e., the velocity of light.

Mev.-A unit of energy; an electron moving under an emf of $10^{8} \mathrm{v}$. ( $1.603 \times 10^{-6} \mathrm{ergs}$ ). See energy units (Table 654).
Molecule. - An aggregate of two or more atoms of a substance that exists as a unit.
Momentum, angular of nucleus, measured in units $\hbar=\hbar=h / 2 \pi$.
Negatron.-See negative electron. (Sometimes spelled negaton.)
Neutrino.-See Table 720.
Neutron.-A neutral particle with a mass about the same as the proton. See Table 720.
Nucleon.-General name for protons and neutrons.
Nucleus.-The central part of an atom, i.e., what is left of an atom after all the outer electrons are stripped off.
Packing fraction.-Related to the mass lost when the atom was formed $=\frac{M_{1}-A}{A}$ where $M$ is the atomic weight of the atom and $A$ the atomic number.
Photon.-The quantum of radiation $=h \nu$.
Proton.-The nucleus of the smallest unit mass, the smallest isotope of the hydrogen atom.

Positron.-See electron. (Sometimes written positon.)
Quantum $=h \nu$, a so-called atom of energy. $h=$ Planck constant. See photon.
Radioactivity.-Natural breakdown of atoms. (See page 672.)
Range of a particle. -The distance it can move through different media.
Rest mass.-The mass of any particle at rest.
Shower.-(Cosmic rays.) See Bursts. Showers may extend a very great distance, i.e., several hundred meters, and have about $10^{15} \mathrm{ev}$ energy.
Spin.-Unit of nuclear spin $=\hbar=\hbar=h / 2 \pi$.
Synchrotron.-See Table 718.
Tritium.-See Triton.
Triton.-The isotpe of hydrogen that has three times the atomic weight of the proton.
Ultimate particle.-See Table 720.
Valence electrons.-The electrons of an atom, in the outer shell that determines its chemical valency.
Van de Graaff generator.-See Table 718.
Volt-electron, ve.-A unit of energy equal to that of an electron moving under an e:nf of 1 volt $=1.602 \times 10^{-12}$ ergs.
X-rays.-A radiation of very short wavelengths that results when an electron is stopped (or started) very quickly, as when striking a metal target. (See page 692.)

| Atomic number | Element | Isotopes (total number) | Naturally radioactive isotopes (number) | Artificially radioactive isotopes (number) $\qquad$ | Relative abundance of natural isotopes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Hydrogen | 3 |  | 1 | $\mathrm{H}^{1} \dagger: \mathrm{H}^{2}=99.9844$ : 0156 |
| 2 | Helium | 3 |  | 1 | $\mathrm{He}^{8}: \mathrm{He}^{4}=1.3 \times 10^{-4}: 99.9999$ |
| 3 | Lithium | 3 |  | 1 | $\mathrm{Li}^{9}: \mathrm{Li}^{\text {² }}=7.39: 92.61$ |
|  | Beryllium | 4 |  | 3 | $\mathrm{Be}^{9}=100.00$ |
| 5 | Boron | 3 |  | 1 | $\mathrm{B}^{10}: \mathrm{B}^{11}=18.83: 81.17$ |
| 6 | Carbon | 5 |  | 3 | $\mathrm{C}^{12}: \mathrm{C}^{18}=98.9: 1.1$ |
| 7 | Nitrogen | 5 |  | 3 | $\mathrm{N}^{14}: \mathrm{N}^{15}=99.62: .38$ |
| 8 | Oxygen | 6 |  | 3 | $\mathrm{O}^{18}: \mathrm{O}^{17}: \mathrm{O}^{18}=99.757: .039:$ |
| 9 | Fluorine | 4 |  | 3 | $\mathrm{F}^{19}=100.00$ |
| 10 | Neon | 5 |  | 2 | $\begin{aligned} & \mathrm{Ne}^{20}: \mathrm{Ne}^{21}: \mathrm{Ne}^{22}=90.51: .28: \end{aligned}$ |
| 11 | Sodium | 5 |  | 4 | $\mathrm{Na}^{23}=100.00$ |
| 12 | Magnesium | 5 |  | 2 | $\begin{aligned} & \mathrm{Mg}^{24}: \mathrm{Mg}^{25}: \mathrm{Mg}^{26}=78.60: \\ & 10.11: 11.29 \end{aligned}$ |
| 13 | Aluminum | 5 |  | 4 | $\mathrm{Al}^{27}=100.00$ |
| 14 | Silicon | 5 |  | 2 | $\mathrm{Si}_{3.05}^{\mathrm{Si}^{88}} \mathrm{Si}^{20}: \mathrm{Si}^{30}=92.28: \quad 4.67:$ |
| 15 | Phosphorus | 5 |  | 4 | $\mathrm{P}^{31}=100.00$ |
| 16 | Sulfur | 7 |  | 3 | $\mathrm{S}^{: 2}: \mathrm{S}^{18}: \mathrm{S}^{3 .}: \mathrm{S}^{30}=95.06: .74:$ |
| 17 | Chlorine | 7 |  | 5 | $\mathrm{Cl}^{35}: \mathrm{Cl}^{38}=75.4: 24.6$ |
| 18 | Argon | 7 |  | 4 | $\begin{gathered} \mathrm{A}^{38}: \mathrm{A}^{58}: \mathrm{A}^{40}=.307: .060: \\ 99.633 \end{gathered}$ |
| 19 | Potassium | 9 | $\mathrm{K}^{40}$ | 6 | $\mathrm{K}^{39}: \mathrm{K}^{40}: \mathrm{K}^{41}=93.3: 011: 6.7$ |
| 20 | Calcium | 10 |  | 4 | $\begin{aligned} & \mathrm{Ca}^{40}: \mathrm{Ca}^{42}: \mathrm{Ca}^{43}: \mathrm{Ca}^{44}: \mathrm{Ca}^{40} \\ & \mathrm{Ca}^{45}=96=96: .64: .15: 206: \\ & .0033: 19 \end{aligned}$ |
| 21 | Scandium | 10 |  | 9 | $\mathrm{Sc}^{15}=100.00$ |
| 22 | Titanium | 9 |  | 4 |  |
| 23 | Vanadium | 5 |  | 4 | $\mathrm{V}^{81}=100.00$ |
| 24 | Chromium | 7 |  | 3 | $\begin{aligned} & \mathrm{Cr}^{50}: \mathrm{Cr}^{52}: \mathrm{Cr}^{53}: \mathrm{Cr}^{54}=4.49: \\ & \quad 83.78: 9.43: 2.30 \end{aligned}$ |
| 25 | Manganese | 6 |  | 5 | $\mathrm{Mn}^{555}=100.00$ |
| 26 | Iron | 8 |  | 4 | $\begin{aligned} & \mathrm{Fe}^{54}: \mathrm{Fe}^{58}: \mathrm{Fe}^{57}: \mathrm{Fe}^{58}=5.81: \\ & 91.64: 2.21: .34 \end{aligned}$ |
| 27 | Cobalt | 9 |  | 8 | $\mathrm{Co}^{59}{ }^{59}=100.00$ |
| 28 | Nickel | 10 |  | 5 |  |
| 29 | Copper | 10 |  | 8 |  |
| 30 | Zinc | 12 |  | 7 | $\begin{gathered} \mathrm{Zn}^{84}: \mathrm{Zn}^{88}: \mathrm{Zn}^{67}: \mathrm{Zn}^{98}: \mathrm{Zn}^{\mathrm{nop}} \\ 48.89: 27.81: 4.07: 18.61: .6 \end{gathered}$ |
| 31 | Gallium | 10 |  | 8 | $\mathrm{Ga}^{\mathrm{m}_{98}}: \mathrm{Ga}^{71}{ }^{71}=60.2: 39.8$ |
| 32 | Germanium | 14 |  | 9 | $\begin{aligned} & \mathrm{Ge}^{70}: \mathrm{Ge}^{72}: \mathrm{Ge}^{73} \cdot \mathrm{Ge}^{74}: \mathrm{Ge}^{79} \\ & 20.55: 27.37: 7.61: 36.74: 7.6 \overline{{ }^{7}} \end{aligned}$ |
| 33 | Arsenic | 9 |  | 8 | ${ }^{\mathrm{As}^{75}{ }^{75} 5}=100.00$ |
| 34 | Selenium | 16 |  | 10 |  |
| 35 | Bromine | 14 |  | 12 |  |
| 36 | Krypton | 22 |  | 16 | $\mathrm{Kr}^{78}:{ }^{50}:^{62}:{ }^{63}:^{84}:^{88}=.342: 2.223:$ 11.50: 11.48: 57.02: 17.43 |
| 37 | Rubidium | 16 | $\mathrm{Rb}^{87}$ | 14 |  |
| 38 | Strontium | 14 |  | 10 |  |
| 39 | Yttrium | 11 |  | 10 | $\mathrm{Y}^{88}=100.00$ |
| 40 | Zirconium | 12 |  | 7 |  |
| 41 | Niobium | 15 |  | 14 | $N \mathrm{~b}^{93}=100.00$ |

* For reference, see foot note 199, p. 618.
$\dagger$ Numbers following symbol indicate names of isotopes of that element.

[^286]| $\begin{aligned} & \text { Atomic } \\ & \text { number } \\ & Z \end{aligned}$ | Element | Isotopes number) number | $\begin{gathered} \text { Naturally } \\ \text { radioactive } \\ \text { isotopes } \\ \text { (number) } \end{gathered}$ | Artificially radioactive isotopes (number) (number) | Relative abundance of natural isotopes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 42 | Molybdenum | 12 |  | 5 |  |
| 43 | Technetium | 19 |  | 19 |  |
| 44 | Ruthenium | 13 |  | 6 |  |
| 45 | Rhodium | 11 |  | 10 | $\mathrm{Rh}^{103}=100.00$ |
| 46 | Palladium | 12 |  | 6 | $\mathrm{Pd}^{102}::^{104}::^{105}:{ }^{100}:{ }^{108}:{ }^{110}=.8: 9.3$ $\quad 22.6: 27.2: 26.8: 13.5$ |
| 47 | Silver | 14 |  | 12 | $\mathrm{Ag}^{107}: \mathrm{Ag}^{109}=51.35: 48.65$ |
| 48 | Cadmium | 16 |  | 8 |  |
| 49 | Indium | 15 |  | 13 | $\mathrm{In}^{113}: \mathrm{In}^{115}=4.23: 95.77$ |
| 50 | Tin | 27 |  | 17 |  |
| 51 | Antimony | 19 |  | 17 | $\mathrm{Sb}^{121}: \mathrm{Sb}^{123}=53.25: 42.75$ |
| 52 | Tellurium | 26 |  | 18 | $\begin{aligned} & \mathrm{Te}^{120}: 122: 123: 124: 125: 128: 128: 130= \\ & .091: 2.49: 89: 4.63: 7.01: \\ & 18.72: 31.72: 34.46 \end{aligned}$ |
| 53 | Iodine | 17 |  | 16 | $\mathrm{I}^{127}=100.00$ |
| 54 | Xenon | 22 |  | 13 |  <br> $.094: .088: 1.90: 26.23: 4.07$ <br> 21.17: 26.96: 10.54: 8.95 |
| 55 | Cesium | 16 |  | 15 |  |
| 56 | Barium | 19 |  | 12 | $\mathrm{Ba}^{180}:^{132}::^{184}:^{155}:{ }^{138}:{ }^{187}:{ }^{138}=.101$ $.097: 2.42: 6.59: 7.81: 11.32:$ $71.66$ |
| 57 | Lanthanum | 12 |  | 10 | $\mathrm{La}^{138}: \mathrm{La}^{130}=.089: 99.911$ |
| 58 | Cerium | 12 |  | 8 | $\begin{gathered} \mathrm{Ce}^{198}: 188 \text { : } 1400 . \overline{142} \\ 88.48: 11.07 \end{gathered}=.193: .250:$ |
| 59 | Praseodymium | 7 |  | 6 |  |
| 60 | Neodymium | 12 | $N d^{180}$ | 4 |  |
| 61 | Promethium | 8 |  | 8 |  |
| 62 | Samarium | 13 | $\mathrm{Sm}^{152}$ | 6 |  |
| 63 | Europium | 11 |  | 9 |  |
| 64 | Gadolinium | 11 |  | 4 |  |
| 65 | Terbium | 7 |  | 6 | $\mathrm{Tb}^{159}=100.00$ |
| 66 | Dysprosium | 10 |  | 3 |  |
| 67 | Holmium | 7 |  | 6 | $\mathrm{Ho}^{105}=100.00$ |
| 68 | Erbium | 10 |  | 4 | $\operatorname{Er}^{182}: \overline{164}: 108::^{107}: 188: 170=.1: 1.5$ 32.9: 24.4: 26.9: 14.2 |
| 69 | Thulium | 8 |  | 7 | $\mathrm{Tm}^{1209}=100.00$ |
| 70 | Ytterbium | 10 |  | 3 | $\begin{array}{r} \mathrm{Y}^{108,} 1770: 171_{: 172}^{: 173}: 174: 178 \\ 4.21: 14.26: \quad 21.49: \quad 17.02: \\ 29.58: 13.38: \end{array}$ |
| 71 | Lutetium |  | $\mathrm{Lu}^{178}$ | 5 | $\mathrm{Lu}^{175}: \mathrm{Lu}^{178}=97.5: 2.5$ |
| 72 | Hafnium | 9 |  | 3 | $\mathrm{Hf}^{174}: \mathrm{inf}^{177}:^{1778}:{ }^{178}: 150=.18: 5.30$ : <br> 18.47: 27.10: 13.84: 35.11 |
| 73 | Tantalum | 9 |  | 8 | $\mathrm{Ta}^{281}=100.00$ |
|  |  |  | (conti |  |  |


| Atomic number Z | Element | Isctopes (total number) | Naturally radioactive isotopes (number) | Artificially radioactive isotopes (number) | Relative abundance of natural isotopes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 74 | Tungsten | 10 |  | 5 | $W^{180}:^{182}:^{188}:^{184}:^{188}=.122: 25.77$ : |
|  |  |  |  |  | 14.24: 30.68:29.17 |
| 75 | Rhenium | 11 | $\mathrm{Re}^{187}$ | 9 | $\mathrm{Re}^{185}: \mathrm{Re}^{187}=37.07: 62.93$ |
| 76 | Osmium | 10 |  | 3 | Os ${ }^{184}:^{188}:{ }^{187}:^{188}:^{189}:^{180}:{ }^{182}=.018$ : |
|  |  |  |  |  | $1.59: 1.64: 13.3: 16.1: 26.4:$ |
| 77 | Iridium | 6 |  | 4 | $\mathrm{Ir}^{191}: \mathrm{Ir}^{199}=38.5: 61.5$ |
| 78 | Platinum | 11 |  | 6 | $\mathrm{Pt}^{182}:{ }^{184}:^{196}:^{108}:{ }^{188}=.78: 32.8$ : |
| 79 | Gold | 13 |  | 12 | $\begin{array}{rl}33.7 & 25.4: 7.23 \\ \mathrm{uu}^{187}=100.00\end{array}$ |
| 80 | Mercury | 13 |  | 6 |  |
|  | Mercury |  |  | 6 | $\begin{aligned} & \mathrm{Hg}^{100}: i^{108}::^{100}::^{200}:{ }^{201}::^{202}:{ }^{204}=.15: \\ & \quad 6.7 \end{aligned}$ |
| 81 | Thallium | 15 | $\mathrm{Tl}^{2017}\left(\mathrm{AcC}^{\prime \prime}\right)$ | 10 | $\mathrm{Tl}^{203}: \mathrm{Tl}^{205}=29.1: 70.9$ |
|  |  |  | $\mathrm{Tl}^{2088}\left(\mathrm{ThC}^{\prime \prime}\right)$ |  |  |
|  |  |  | $\mathrm{Tl}^{210}\left(\mathrm{RaC}^{\prime \prime}\right)$ |  |  |
| 82 | Lead | 14 | $\mathrm{Pb}^{210}(\mathrm{RaD})$ | 6 | $\mathrm{Pb}^{204}:{ }^{208}:{ }^{207}:{ }^{208}=1.5: 23.6: 22.6$ : |
|  |  |  | $\mathrm{Pb}^{211}$ ( AcB ) |  | $52.3$ |
|  |  |  | $\mathrm{Pb}^{212}$ (ThB) |  |  |
|  |  |  | $\mathrm{Pb}^{214}(\mathrm{RaB})$ |  |  |
| 83 | Bismuth | 13 | $\mathrm{Bi}^{210}(\mathrm{RaE})$ | 8 | $\mathrm{Bi}^{209}=100.00$ |
|  |  |  | $\mathrm{Bi}^{211}$ ( AcC ) |  |  |
|  |  |  | $\mathrm{Bi}^{212}$ ( ThC ) |  |  |
|  |  |  | $\mathrm{Bi}^{214}(\mathrm{RaC})$ |  |  |

## TABLE 718.-DEVICES FOR PRODUCING HIGH.ENERGY PARTICLES* $\dagger \ddagger$

Impulse generator.
Transformer rectifier.-Max about 2 Mev.
Electrostatic generator, belt type.-Originated by R. J. Van de Graaff at M.I.T. Developed for use in nuclear physics at M.I.T. by Van de Graaff and at Carnegie Institution in Washington by M. A. Tuve. About 1-3 Mev. Performance improved at Wisconsin, by enclosing equipment in pressure chamber (with freon added to air), up to 4-5 Mev (under pressure) $100 \mathrm{lb} / \mathrm{in}^{2}{ }^{2}$ This device can accelerate any kind of charged particle. Under construction (M.I.T., Los Alamos) 12 Mev .

Cyclotron.-Originated at Berkeley by E. O. Lawrence. For accelerating any heavy charged particles (not electrons). 44 Mev alpha-particles, 22 Mev deuterons, 9.5 Mev protons.

Betatron.-Originated at Illinois by D. W. Kerst. For accelerating electrons. 300 Mev , Illinois; 100 Mev , General Electric Co.

Synchro-cyclotron.-Developed at Berkeley. 390 Mev alpha-particles, 400 Mev protons, 195 Mev deuterons.

Synchrotron (electron).-Berkeley, 335 Mev electrons; General Electric Co., Cornell, Michigan, Perdue, Berkeley, about 300 Mev ; Harvard, 125 Mev .

Linear accelerator.-Berkeley, 32 Mev protons; Stanford, 5.7 Mev electrons (under construction, 1000 Mev ) ; M.I.T., 20-30 Mev electrons.

Proton synchrotron.-Berkeley, 3-6 Mev (under construction) ; Brookhaven, 3 Mev (under construction).

Some of the smaller cyclotrons at various laboratories have been converted to F. M. cyclotrons. There are now in use, or under construction in this country, over 100 devices for producing particles of over 1 Mev energy.

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TABLE 719.-ATOMIC WEIGHTS AND OTHER CHARACTERISTICS OF ISOTOPES ${ }^{22}$
Part 1.-The neutron to fluorine ${ }^{a}$

| $z$ | Element | Isotope | Atomic mass | Spin ${ }^{\text {d }}$ | Magnetic moment 0 | Quadrupole $\underset{\left(10^{-24} \mathrm{~cm}^{2}\right)^{\text {moment }}}{ }$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | n | 1 | 1.008977 | 1/2 | $-1.91280 \pm 9$ |  |
| 1 | H | 1 | 1.0081374 | 1/2 | $+2.79254 \pm 0$ |  |
|  |  | 2 | 2.014719 | 1 | $+.857352 \pm 9$ | $+.002766 \pm 25$ |
|  |  |  | 3.016971 | 1/2 | $+2.978624 \pm 28$ |  |
| 2 | He | 3 | 3.016951 | 1/2 | $(-) 2.127414 \pm 3$ |  |
|  |  | 4 | 4.003910 | 0 |  |  |
| 3 | Li | 6 | 6.017043 | 1 | $+.82189 \pm 4$ | $\left\|<9 \times 10^{-4}\right\|$ |
|  |  | 7 | 7.018242 | 3/2 | $+3.25586 \pm 11$ | +(.02) $\pm 2$ |
|  |  | 8 | 8.025031 |  |  |  |
| 4 | Be | 7 | 7.019169 | $\ldots$ | ....... |  |
|  |  | 8 | 8.007916 |  |  |  |
|  |  | 9 | 9.015098 | 3:2 | (-). $7849 \times 1 * \pm 5$ |  |
|  |  | 10 | 10.016774 |  |  |  |
| 5 | B | 9 | 9.016246 | . |  |  |
|  |  | 10 | 10.016173 | 3 | $+1.8004 \pm 7$ | $+.06 \pm 4$ |
|  |  | 11 |  | 3/2 | $+2.68858 \pm 28$ | $+.03 \pm 2$ |
| 6 | C | 12 |  |  |  | ...... |
|  |  | 13 | 13.007554 | 1/2 | $+.70225 \pm 14$ |  |
|  |  | 14 | 14.007733 | 0 |  |  |
| 7 | N | 13 | 13.009941 |  |  |  |
|  |  | 14 | 14.007565 | 1 | $+.40365 \pm 3$ | +. 02 |
|  |  | 15 |  | 1/2 | $-.28299 \pm 3$ |  |
| 8 | O | 17 | 17.004515 | $\begin{gathered} 0 \\ (1 / 2) \end{gathered}$ | ....... |  |
|  |  | 18 |  | (0) |  | $\left\|<4 \times 10^{-8}\right\|$ |
| 9 | F | 19 | 19.004486 | 1/2 | +2.6285 $\pm 7$ |  |

${ }^{227}$ References and other footnotes at end of table, p. 663. Superior letters ( ${ }^{a}$, ${ }^{b}$, etc) refer to authorities cited in footnote.

Part 2.-Fluorine to thallium ${ }^{\text {b }}$


TABLE 719.-ATOMIC WEIGHTS AND OTHER CHARACTERISTICS OF ISOTOPES (continued)

| $z$ | Element | Isotope | Atomic mass | Spin ${ }^{\text {a }}$ | Magnetic moment ${ }^{\prime}$ | Quadrupole moment $\dagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 30 | 29.9832 | (0) | ..... | $\sim 0$ |
|  |  | 31 | 30.9862 | (a) | $\ldots$ |  |
|  |  | 32 | (31.9849) | ... | ..... |  |
| 15 | P | 29 | 28.9919 | $\ldots$ |  |  |
|  |  | 30 | 29.9873 | - |  |  |
|  |  | 31 | 30.9843 | $1 / 2$ | $+1.13165 \pm 20$ | $\ldots$ |
|  |  | 32 | 31.9827 | $\ldots$ | . |  |
|  |  | 33 | 32.9826 | $\ldots$ |  |  |
|  |  | 34 | 33.9826 | $\ldots$ |  |  |
| 16 | S | 31 | 30.9899 |  |  |  |
|  |  | 32 | 31.98089 | 0 |  |  |
|  |  | 33 | 32.9800 | 3/2 | (+)(.3土.2, .9) | - ${ }^{\text {. }} \times 8$ |
|  |  | 34 | 33.97710 | (0) | (1)... | $\mid<2 \times 10^{-3}$ \| |
|  |  | 35 | 34.9788 | 3/2 | .... | + 06 |
|  |  | 36 | 35.978 | (0) | ...... | < 01 |
|  |  | 37 | 36.982 |  |  |  |
| 17 | Cl | 33 | 32.9860 | $\ldots$ |  |  |
|  |  | 34 | 33.9801 |  |  |  |
|  |  | 35 | 34.97867 | $3 / 2$ | $+.82191 \pm 22$ | $-.0795 \pm 5$ |
|  |  | 36 | 35.9788 | 2 |  | -. $0172 \pm 4$ |
|  |  | 37 | 36.97750 | $3 / 2$ | +.68414 $\pm 24$ | $-.0621 \pm 5$ |
|  |  | 38 | 37.981 | ... |  | .... |
|  |  | 39 | (38.9794) | $\ldots$ | ..... | .... |
| 18 | A | 35 | 34.9850 |  |  | .... |
|  |  | 36 | 35.98780 | (0) | $\sim 0$ | $\ldots$ |
|  |  | 37 | 36.9777 | (a) | ..... | .... |
|  |  | 38 | 38.974 | ... | ..... | .... |
|  |  | 39 | (38.9755) |  |  | .... |
|  |  | 40 | 39.9756 | (0) | $\sim 0$ | .... |
|  |  | 41 | 40.9770 | ... |  |  |
| 19 | K | 37 | (36.9830) | $\cdots$ | ..... | $\ldots$ |
|  |  | 38 | 37.9795 38 | $3 / 2$ | $391 \pm 1$ | $\ldots$ |
|  |  | $40 \ddagger$ | 39.9760 | 4 | $-1.291 \pm 4$ | $\ldots$ |
|  |  | 41 | 40.974 | 3/2 | $-.215 \pm 1$ | $\ldots$ |
| 20 | Ca | 40 | 39.97530 | (0) | $\sim 0$ | .... |
|  |  | 42 | 41.9711 | (0) |  | $\ldots$ |
|  |  | 43 | 42.9723 |  |  | .... |
| 21 | Sc | 45 | 44.9669 | 7/2 | $-4.7556 \pm 10$ | $\ldots$ |
| 22 | Ti | 46 | 45.9661 | $\ldots$ | ..... | $\ldots$ |
|  |  | 47 | 46.9647 |  |  |  |
|  |  | 48 | 47.9631 | ... | ..... | $\ldots$ |
|  |  | 49 | 48.9646 | ... | $\ldots$ | $\ldots$ |
|  |  | 50 | 49.9621 | ... |  |  |
|  |  | 51 | 50.5887 |  |  |  |
| 23 | V | 51 | 50.9577 | 7/2 | $(+) 5.1478 \pm 5$ | $\ldots$ |
| 24 | Cr | 51 | 50.958 | ... | ..... | $\ldots$ |
|  |  | 52 | 51.956 | $\ldots$ |  |  |
|  |  | 53 | 52.956 |  |  |  |
| 25 | $\mathrm{Me}^{\mathrm{Mn}}$ | 55 | 54.957 | 5/2 | $+3.4677 \pm 4$ | $\ldots$ |
| 26 | Fe | 54 56 | 53.957 55.9568 | ... | ..... | $\cdots$ |
|  |  | 57 | 56.957 |  | $\sim 0$ |  |
| 27 | Co | 59 | 58.94 | 7/2 | +4.6482 | $\ldots$ |
| 28 | Ni | 58 | 57.9594 | ... | ..... | .... |
|  |  | 60 | 59.9495 | ... |  |  |
|  |  | 61 | 60.9537 | $\ldots$ | $\sim 0$ | $\ldots$ |
|  |  | 62 | 61.9493 | $\ldots$ | $\ldots$ | $\ldots$ |
| 29 | Cu | 64 | 63.9471 | $3 / 2$ |  | - . $26 \pm 10$ |
|  | Cu | 65 | 64.955 | 3/2 | $\begin{aligned} & +2.3845 \pm 4 \end{aligned}$ | $-.14 \pm 10$ |
| 30 | Zn | 64 | 63.955 | (0) | $\sim 0$ | .... |
|  |  |  |  | inued) |  |  |

TABLE 719.-ATOMIC WEIGHTS AND OTHER CHARACTERISTICS OF ISOTOPES (continued)

| $z$ | Element | Isotope | Atomic mass | Spin 0 | Magnetic moment ${ }^{g}$ | Quadrupole moment $\dagger$ g |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 66 | 65.954 | (0) | $\sim 0$ | ..... |
|  |  | 67 | 66.954 | 5/2 | $+.9$ |  |
|  |  | 68 | 67.955 | (0) | $\sim 0$ |  |
|  |  | 70 | 69.954 |  |  |  |
| 31 | Ga | 69 | 68.952 | 3/2 | $+2.0167 \pm 11$ | $+.2318 \pm 23$ |
|  |  | 71 | 70.952 | 3/2 | $+2.5614 \pm 10$ | $+.1461 \pm 15$ |
| 32 | Ge | 70 | ..... | (0) |  | $\left\|<7 \times 10^{-8}\right\|$ |
|  |  | 72 |  | (0) | $\ldots$ | \|<7×10-31 |
|  |  | 73 | $\ldots$ | $9 / 2,>9 / 2$ |  | $-.21 \pm 10$ |
|  |  | 74 |  | (0) |  | $\left\|<7 \times 10^{-8}\right\|$ |
|  |  | 76 |  | (0) |  | $\left\|<7 \times 10^{-8}\right\|$ |
| 33 | As | 75 | 74.91 | 3/2 | +1.4 | + . $3 \pm 2$ |
| 34 | Se | 74 |  | (0) |  |  |
|  |  | 76 | ..... | (0) | $\sim 0$ | $1<2 \times 10^{-3}$ \| |
|  |  | 77 | . | $7 / 2 \pm 1,(1 / 2)$ |  | <2×10 $0^{-3}$ |
|  |  | 78 | . | (0) | $\sim 0$ | <2×10-3 |
|  |  | 80 | ..... | 0 |  | $1<2 \times 10^{-3}$ |
|  |  | 82 |  | (0) | $\sim 0$ |  |
| 35 | Br | 79 | $\ldots$ | 3/2 | $+2.10576 \pm 37$ | +.26 $\pm 8$ |
|  |  | 81 | ..... | 3/2 | $+2.2696 \pm 5$ | $+.21+7$ |
| 36 | Kr | 82 | ...... | (0) | $\sim 0$ |  |
|  |  | 83 | ..... | 9/2 | -. 9704 | +. 15 |
|  |  | 84 |  | (0) | $\sim 0$ |  |
|  |  | 86 | . | (0) | $\sim 0$ |  |
| 37 | Rb | 85 | ..... | 5/2 | $+1.3532 \pm 4$ | .... |
|  |  | $87 \pm$ | ..... | 3/2 | $+2.7501 \pm 5$ | $\ldots$ |
| 38 | Sr | 86 | ..... | (0) |  | $\ldots$ |
|  |  | 87 |  | 9/2 | -1.1 |  |
|  |  | 88 | ...... | (0) | $\sim 0$ |  |
| 39 | Y | 89 | ..... | 1/2 | $-.14$ | .... |
| 40 | Zr | 91 |  | 5/2 |  |  |
| 41 | Nb | 93 |  | 9/2 | $+6.165 \pm 32$ | $\sim 0$ |
| 42 | Mo | 92 |  | (0) | $\sim 0$ |  |
|  |  | 94 | 93.945 | (0) | $\sim 0$ | $\ldots$ |
|  |  | 95 | 94.946 | (5/2) |  |  |
|  |  | 96 | 95.944 |  | $\sim 0$ | $\ldots$ |
|  |  | 97 | 96.945 | (5/2) |  |  |
|  |  | 98 | 97.943 | (0) | $\sim 0$ | $\ldots$ |
| 44 | Ru | 96 | 95.945 | $\ldots$ | $\ldots$ |  |
|  |  | 98 | 97.943 | $\ldots$ | ..... |  |
|  |  | 99 | 98.944 | ... | ..... | $\ldots$ |
|  |  | 100 | 99.942 | ... | $\ldots$ | $\ldots$ |
|  |  | 101 | 100.946 | ... | ..... | .... |
|  |  | 102 | 101.941 |  |  |  |
| 45 | Rh | 102 | 102.941 |  |  |  |
|  |  | 103 |  | $>(1 / 2 ?)$ | <0 |  |
| 46 | Pd | 102 | 101.941 | ... | ..... | $\ldots$ |
|  |  | 104 | 103.941 | ... | ..... |  |
|  |  | 105 | 105.941 | $\ldots$ | . | $\ldots$ |
|  |  | 108 | 107.941 | $\ldots$ |  |  |
|  |  | 110 | 109.941 |  |  |  |
| 47 | Ag | 107 | 106.945 | 1/2 | $-.086$ |  |
|  |  | 109 | 108.944 | 1/2 | $-.160$ |  |
| 48 | Cd | 110 |  | (0) | $\sim 0$ | $\ldots$ |
|  |  | 111 | ..... | 1/2 | $-.59492 \pm 8$ |  |
|  |  | 112 | ..... | (0) | $\sim 0$ | .. |
|  |  | 113 |  | 1/2 | -. $62238 \pm 8$ |  |
|  |  | 114 |  | (0) | $\sim 0$ |  |
| 49 | In | 116 113 | $\ldots .$. | 9/2 | $\sim 00$ |  |
|  |  | 115 | $\ldots$ | 9/2 | $+5.500 \pm 3$ | 1.161 |
| 50 | Sn | 115 | 114.940 | 1/2 | $-.9177 \pm 2$ |  |
|  |  |  |  | (ontinued) |  |  |

TABLE 719.-ATOMIC WEIGHTS AND OTHER CHARACTERISTICS OF ISOTOPES (continued)

| $Z$ | Element | Isotope | Atomic mass | Spin ${ }^{\text {a }}$ | Magnetic moment | Quadrupole moment $\dagger$ g |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 116 | 115.939 | (0) | $\sim 0$ |  |
|  |  | 117 | 116.937 | 1/2 | -. $9997 \pm 2$ |  |
|  |  | 118 | 117.937 | (0) | $\sim 0$ |  |
|  |  | 119 | 118.938 | 1/2 | $-1.0459 \pm 2$ |  |
|  |  | 120 | 119.937 | (0) | $\sim 0$ |  |
|  |  | 122 | 121.945 | (0) |  |  |
|  |  | 124 | 123.944 |  |  |  |
| 51 | Sb | 121 | ..... | $5 / 2$ | $+3.3591 \pm 5$ | $-.3 \pm 2$ |
|  |  | 123 |  | 7/2 | $+2.5465 \pm 5$ | $-1.2 \pm 2$ |
| 52 | Te | 123 | ..... | 1/2 |  |  |
|  |  | 125 | . . . . | 1/2 |  |  |
|  |  | 126 | . . . . | (0) | $\sim 0$ |  |
|  |  | 128 |  | (0) | $\sim 0$ |  |
|  |  | 130 |  | (0) | $\sim 0$ |  |
| 53 | I | 127 | 126.92 | 5/2 | $+2.8086 \pm 8$ | -. $59 \pm 20$ |
|  |  | 129 |  | $7 / 2$ | $(+) 2.74 \pm 14 \mathrm{~h}$ | -. $43 \pm 15$ |
| 54 | Xe | 129 |  | 1/2 | -. $7766 \pm 1$ |  |
|  |  | 131 |  | 3/2 | $+.7$ | $1<.1 \mid$ |
|  |  | 132 | . . . . | (0) | $\sim 0$ |  |
|  |  | 134 |  | (0) | $\sim 0$ | ... |
|  |  | 136 |  | (0) | $\sim 0$ |  |
| 55 | Cs | 133 | 13291 | 7/2 | $+2.5771 \pm 9$ | $\|\leqslant .3\|$ |
|  |  | 135 |  | $7 / 2$ | $+2.7271 \pm 33$ |  |
|  |  | 137 |  | 7/2 | $+2.8397 \pm 30$ |  |
| 56 | Ba | 134 |  | (0) | $\sim 0$ | ... |
|  |  | 135 | ..... | 3/2 | $+.8346 \pm 25$ | . . . |
|  |  | 136 |  | (0) | $\sim 0$ |  |
|  |  | 137 |  | 3/2 | +. $9351 \pm 27$ |  |
|  |  | 138 |  | (0) | $\sim 0$ |  |
| 57 | La | 139 | 138.953 | $7 / 2$ | $+2.7769 \pm 28$ | $\neq 0$ |
| 58 | Ce |  |  |  |  |  |
| 59 | Pr | 141 | 140.95 | 5/2 | +4.5938 |  |
| 60 | Nd | 145 | 144.962 | ... | ..... | . . . |
|  |  | 146 | 145.962 | . . . | . . . . | . |
|  |  | 148 | 147.962 | . . . | . . . . | ... . |
|  |  | $150 \ddagger$ | 149.964 | -•• | -•... |  |
| 61 | Pr |  |  | ( |  |  |
| 62 | Sm | 147 |  | $(>1 / 2)$ | ..... |  |
|  |  | 149 | . . . . | $(>1 / 2)$ |  |  |
| 63 | Eu | 151 | , | $5 / 2$ | $+3.4$ | $+1.2$ |
|  |  | 153 |  | 5/2 | +1.5 | +2.5 |
| 64 | Gd | 154 | 153.971 | , | + | + |
|  |  | 155 | 154.971 | ... | ..... | . . . |
|  |  | 156 | 155.972 | ... | ..... | .... |
|  |  | 157 | 156.973 | ... | . . . . . | $\ldots$ |
|  |  | 158 | 157.973 | ... | ..... | .... |
|  |  | 160 | 159.974 | $\cdots$ | . . . . | .... |
| 65 | Tb | 159 | 159.2 | 3/2 |  | . . . |
| 66 | Dy |  |  |  |  |  |
| 67 | Ho | 165 | 164.94 | 7/2 | . . . $\cdot$ | . $\cdot$. |
| 68 69 | $\mathrm{Er}_{\mathrm{Tm}}$ |  |  |  |  |  |
| 70 | Yb | 169 171 | 169.4 | 1/2 | $+.45$ |  |
|  |  | 173 | . . . . | 5/2 | -. 65 | $+3.9 \pm 4$ |
| 71 | Lu | 175 |  | 7/2 | +2.6 | $+5.9$ |
|  |  | 176 $\ddagger$ | . | $\geq 7$ | +3.8 | $+7 \pm 1$ |
| 72 | Hf | 177 | ..... | (1/2,3/2) |  | .... |
|  |  | 178 |  | (0) | $\sim 0$ | . . . |
|  |  | 179 180 |  | (1/2,3/2) | $\sim 0$ | . . . |
| 73 | Ta | 181 | 180.88 | $7 / 2$ | +2.1 | +6 |
| 74 | W | 182 |  | (0) | ..... | .... |
|  |  | 183 | . . . . | 1/2 | . . . . | . $\cdot$. |

(continued)

TABLE 719.-ATOMIC WEIGHTS AND OTHER CHARACTERISTICS OF ISOTOPES (continued)

| $Z$ | Element | Isotope | Atomic mass | Spin ${ }^{\text {a }}$ | Magnetic moment ${ }^{g}$ | Quadrupole moment $\dagger s$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 184 |  | (0) |  |  |
| 75 | Re | 186 |  | (0) |  |  |
|  |  | 185 | ..... | 5/2 | +3.3 | $(+2.8)$ |
|  |  | 186 |  | 5/2 |  |  |
| 76 | Os | $187 \ddagger$ |  | 5/2 | $+3.3$ | +2.6 |
|  |  | 189 | 189.04 | 1/2 | ..... | .... |
|  |  | 190 | 190.03 | 1/2 |  |  |
| 77 | Ir | 192 | 192.04 |  |  |  |
|  |  | 191 | 191.04 | $(>1 / 2)$ |  |  |
|  |  | 193 | 193.04 | $(3 / 2)$ |  |  |
| 78 | Pt | 194 | 194.039 |  | $\sim 0$ |  |
|  |  | 195 | 195.039 | 1/2 | -. $60592 \pm 8$ | .... |
|  |  | 196 | 196.039 | (0) | $\sim 0$ | .... |
|  |  | 198 | 198.05 |  |  |  |
| 79 | $\mathrm{Al}^{1}$ | 197 | 197.04 | 3/2 | +. 20 | $\cdots$ |
| 80 | Hg | 198 |  | (0) |  |  |
|  |  | 199 |  | 1/2 | . $50413 \pm 13$ |  |
|  |  | 200 | $\ldots$ | (0) |  |  |
|  |  | 201 |  | 3/2 | $+.5590 \pm 1$ | $+.5$ |
|  |  | 202 |  | (0) | $\sim 0$ |  |
|  |  | 204 |  | (0) | $\sim 0$ |  |

Part 3.-Thallium to curium (1950) §
The masses have been derived as outlined by Stern. ${ }^{d}$ The mass of the a-particle is assumed to be 4.00389 mass units and the mass of $\mathrm{Pb}^{206}$ is 206.04519 mass units. The masses of thallium, lead, and bismuth isotopes are determined from the following neutron binding energies (in Mev):

| T1 ${ }^{\text {pos }}$ | $6.52 \pm 0.03$ | $\mathrm{Pb}^{208}$ | $8.15 \pm 0.05$ | $\mathrm{Pb}^{200}$ | $3.87 \pm 0.05$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T1 ${ }^{108}$ | $7.48 \pm 0.15$ | $\mathrm{Pb}^{207}$ | $6.719 \pm 0.016$ | $\mathrm{Bi}^{200}$ | $7.44 \pm 0.05$ |
| T1 ${ }^{20}$ | $6.30 \pm 0.03$ | $\mathrm{Pb}^{288}$ | $7.38 \pm 0.008$ | $\mathrm{Bi}^{210}$ | $4.62 \pm 0.015$ |

The decay energies are taken from a paper by Wapstra ${ }^{\circ}$ except for two corrections. The decay energy of $\mathrm{Ra}^{223}$ is taken to be 170 Kev higher than that given by Wapstra as was assumed by Stern. Also, it is assumed that the decay of $\mathrm{Ra}^{225}$ is 700 Kev , and the masses based on this assumption are in parentheses. A few other disintegration energies not given by Wapstra were taken from Perlman, et al. ${ }^{\prime}$


TABLE 719.-ATOMIC WEIGHTS AND OTHER CHARACTERISTICS OF ISOTOPES (concluded)


[^288]
## TABLE 720.-SOME FUNDAMENTAL PARTICLES OF MODERN PHYSICS *

Electron.-A negatively charged stable particle. The negative charge surrounding the nuclei in all neutral atoms consists entirely of electrons.

Positron.-A particle of the same mass, $M_{e}$, as an ordinary electron. It has a positive electrical charge of exactly the same amount as that of an ordinary electron (which is sometimes called negatron). Positrons are created either by the radioactive decay of certain unstable nuclei or, together with a negatron, in a collision between an energetic (more than one Mev ) photon and an electrically charged particle (or another photon). A positron does not decay spontaneously but on passing through matter it sooner or later collides with an ordinary electron and in this collision the positron-negatron pair is annihilated. The rest energy of the two particles, which is given by Einstein's relation $E=\mathrm{mc}^{2}$ and amounts to 1.0216 Mev altogether, is converted into electromagnetic radiation in the form of one or more photons.

Proton.-This is the nucleus of an ordinary hydrogen atom. It has a positive charge of exactly the same amount as that of an electron and a mass $M_{P}$ which is 1837 times larger than $M_{e}$ and is a stable particle. No experimental evidence of negative protons has been found as yet.

Neutron.-An electrically neutral particle of mass only very slightly greater (by a factor of 1.0013) than that of the proton. Neutrons are produced in various nuclear reactions. In the free state a neutron is unstable, decaying spontaneously with a half-life of about 10 minutes into a proton, and electron and (presumably) a neutrino. When passing through matter a neutron can also be captured by atomic nuclei.

Deuteron. $\dagger$-Nucleus of $\mathrm{H}^{2}$.
a-particle, $\dagger$-Nucleus of $\mathrm{He}^{\dagger}$.
Meson.-Two types of particles of mass intermediate between that of the electron and proton have been discovered in cosmic radiation and in the laboratory. The one particle with mass about $215 m_{e}$ is called $\mu$-meson, the other with about $280 m_{e} \pi$-meson. Mesons of both positive and negative charge have been found and there is now reasonably good evidence for neutral mesons. Both types of mesons decay spontaneously. Some evidence exists for a meson of mass about $1000 \mathrm{~m}_{\text {e }}$.

Neutrino.-An electrically neutral particle of mass very much smaller than that of the electron and possibly zero. There exists as yet no direct experimental evidence for the existence of neutrinos since they interact extremely weakly with matter (e.g., only a small fraction of neutrinos passing through a body of solar mass would be absorbed). There exist, however, extensive measurements on the momentum and energy of the parent and daughter nucleus and of the emitted $\beta$-particle in a $\beta$-decay process. These measurements show that energy and momentum (as well as spin and charge) in such a process can be conserved if, and only if, a light neutral particle such as the neutrino is emitted together with the $\beta$-particle.
Photon.-A photon (or $\gamma$-ray) is a quantum of electromagnetic radiation which has zero rest mass and an energy of $h$ (Planck's constant) times the frequency of the radiation. Photons are generated in collisions between nuclei or electrons and in any other process in which an electrically charged particle changes its momentum. Conversely photons can be absorbed (i.e., annihilated) by any charged particle.
There have been some reports of other particles than those listed above.


[^289]If a neutron or proton (or a light nucleus) approaches a nucleus at a distance less than the range of nuclear forces it may interact with the nucleus in various ways. If the kinetic energy of the incident particle is not more than a few Mev it is usually first captured by the nucleus, forming a compound nucleus. This compound nucleus is in an excited state (having an excess energy due to the extra binding energy of the additional particle as well as its initial kinetic energy) and in a short time either (a) makes a transition to its groundstate releasing the excess energy in the form of photons, (b) re-emits the incident particle returning to the ground-state or an excited state of the original nucleus (elastic or inelastic scattering), or (c) emits some other particle (neutron, proton, deuteron or $a$-particle usually).

A neutron does not experience any Coulomb repulsion on approaching a nucleus and hence can react with a nucleus however low its kinetic energy. However, if the incident particle is a proton or deuteron (and even more so if it is an $\alpha$-particle) it has to overcome an energy barrier due to the electrostatic Coulomb repulsion of the nucleus. For a proton incident on a light nucleus (small Z) this barrier is a few hundred Kev and increases almost proportionately with $Z$. If the kinetic energy of an incident proton is larger than this barrier it can react about as easily as a neutron. If its energy is lower it can still react due to a purely quantum phenomenon called barrier penetration, but the probability of such a reaction's taking place decreases extremely rapidly as the kinetic energy is decreased relative to the barrier.

Nuclear processes in stars.-There are no free neutrons in stellar interiors (any produced are quickly captured by nuclei), but there is a large proportion of ionized hydrogen and helium (protons and $a$-particles). At a stellar temperature of, say, $2 \times 10^{7}{ }^{\circ} \mathrm{C}$ the mean thermal kinetic energy of a proton is less than 2 Kev which is appreciably less than the Coulomb barrier of even light nuclei. This means that the reaction rate for protons being captured by a nucleus in stars is in general low and decreases very rapidly with increasing charge $Z$ of the nucleus, reactions with nuclei of $Z$ greater than 8 (oxygen) being negligible for practical purposes in stars.

Two different cycles (the carbon and proton-proton cycle respectively) are of importance in connection with nuclear energy production in stars. In each of these cycles four protons are captured, separately, by certain light nuclei, two of the compound nuclei thus formed, beta-decay, emitting a positron and neutrino. Each positron subsequently finds an electron and the pair is annihilated, accompanied by the emission of photons. The net effect in each of these cycles is that four protons and two electrons have disappeared, an a-particle has appeared in their place and two neutrinos have been emitted. The energy generated is the total binding energy of an a-particle plus the rest-energy of two electrons which amounts to about 29 Mev per cycle. About 7 percent of this energy is lost in the form of kinetic energy of neutrinos, which escape without interacting any further. The remaining 93 percent of the energy is converted into thermal kinetic energy and radiation. The photons created in the original nuclear processes are absorbed after traversing only a short distance in the star and a larger number of photons of lower frequency are emitted, etc., so that the radiation finally leaving the star has approximately the spectral distribution of blackbody radiation. The rate at which these cycles take place and hence the rate of energyproduction increases very much for even a small increase in the stellar temperature.

- Prepared by E. E. Salpeter.

TABLE 722.-THE THEORETICAL DE BROGLIE WAVELENGTHS ASSOCIATED WITH VARIOUS PARTICLES AND BODIES OF GROSS MATTER ${ }^{226}$

$$
(\lambda=h /(m v))
$$

|  |  | Melocity | Energy | De Broglie <br> wavelengths <br> Particle |
| :--- | :---: | :---: | :---: | :---: |
| ergs |  |  |  |  |

[^290]TABLE 723.-RATES OF NUCLEAR REACTIONS IN STARS AND OF ENERGY PRODUCTION AT VARIOUS TEMPERATURES * ${ }^{225}$

| Reaction Temperature: |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10 \times 10^{6}$ | $15 \times 10^{6}$ | $17.5 \times 10^{6}$ | $20 \times 10^{6}$ | $25 \times 10^{\text {e }}$ | $30 \times 10^{8}$ |
| $\mathrm{H}^{1}+\mathrm{H}^{1} \rightarrow \mathrm{H}^{2}+e^{+}$ | $6 \times 10^{10} \mathrm{yr}$ | $1.2 \times 10^{10} \mathrm{yr}$ | $6 \times 10^{9} \mathrm{yr}$ | $4 \times 10^{0} \mathrm{yr}$ | $2 \times 10^{9} \mathrm{yr}$ | $1 \times 10^{9} \mathrm{yr}$ |
| $\mathrm{H}^{2}+\mathrm{H}^{1} \rightarrow \mathrm{He}^{3}+\gamma$ | 15 sec | 2 sec | 1 sec | . 5 sec | . 2 sec | .1 sec |
| $\mathrm{He}^{3}+\mathrm{He}^{4} \rightarrow \mathrm{Be}^{7}+\gamma$ | $2 \times 10^{12} \mathrm{yr}$ | $1.5 \times 10^{9} \mathrm{yr}$ | $1.2 \times 10^{8} \mathrm{yr}$ | $1.5 \times 10^{7} \mathrm{yr}$ | $5 \times 10^{5} \mathrm{yr}$ | $5 \times 10^{4} \mathrm{yr}$ |
| $\mathrm{Be}^{7} \rightarrow \mathrm{Li}^{7}-\mathrm{c}^{-}$ | 70 days | 70 days | 70 days | 70 days | 70 days | 70 days |
| $\mathrm{Li}^{7}+\mathrm{H}^{1} \rightarrow \mathrm{He}^{4}+\mathrm{He}^{4}$ | 10 hr | 50 min | 50 sec | 15 sec | 2 sec | .4 sec |
| Mean life of hydrogen | $6 \times 10^{10} \mathrm{yr}$ | $3 \times 10^{9} \mathrm{yr}$ | $1.5 \times 10^{8} \mathrm{yr}$ | $1 \times 10^{9} \mathrm{yr}$ | $5 \times 10^{8} \mathrm{yr}$ | $3 \times 10^{8} \mathrm{yr}$ |
| Energy production in ergs/(g sec) | . 75 | 40 | 80 | 120 | 250 | 400 |

Part 2.-Carbon cycle, temperatures in ${ }^{\circ} \mathrm{K}$

| Reaction | ture: |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10 \times 10^{6}$ | $15 \times 10^{0}$ | $17.5 \times 10^{6}$ | $20 \times 10^{6}$ | $25 \times 10^{8}$ | $30 \times 10^{8}$ |
| $\mathrm{C}^{12}+\mathrm{H}^{7} \rightarrow \mathrm{~N}^{13}+\gamma$ | $2 \times 10^{9} \mathrm{yr}$ | $1 \times 10^{6} \mathrm{yr}$ | $6 \times 10^{4} \mathrm{yr}$ | $7 \times 10^{3} \mathrm{yr}$ | 200 yr | 15 yr |
| $\mathrm{N}^{13} \rightarrow \mathrm{C}^{13}+\mathrm{c}^{+}$ | 10 min | 10 min | 10 min | 10 min | 10 min | 10 min |
| $\mathrm{C}^{12}+\mathrm{H}^{2} \rightarrow \mathrm{~N}^{14}+\gamma$ | $\leq 5 \times 10^{8} \mathrm{yr}$ | $\leq 2.5 \times 10^{5} \mathrm{yr}$ | $\leq 1.5 \times 10^{4} \mathrm{yr}$ | $\leq 1.5 \times 10^{3} \mathrm{yr}$ | $\leq 50 \mathrm{yr}$ | $\Sigma 3 \mathrm{yr}$ |
| $\mathrm{N}^{14}+\mathrm{H}^{4} \rightarrow \mathrm{O}^{15}+\gamma$ | $2 \times 10^{11} \mathrm{yr}$ | $4 \times 10^{7} \mathrm{yr}$ | $1.7 \times 10^{6} \mathrm{yr}$ | $1.5 \times 10^{5} \mathrm{yr}$ | $3 \times 10^{3} \mathrm{yr}$ | 150 yr |
| $\mathrm{O}^{15} \rightarrow \mathrm{~N}^{15}+\mathrm{c}^{+}$ | 2 min | 2 min | 2 min | 2 min | 2 min | 2 min |
| $\mathrm{N}^{15}+\mathrm{H}^{1} \rightarrow \mathrm{C}^{12}+\mathrm{He}^{4}$ | $4 \times 10^{7} \mathrm{yr}$ | $8 \times 10^{3} \mathrm{yr}$ | 300 yr | 30 yr | . $6 \times \mathrm{yr}$ | ${ }_{3} .1 \mathrm{yr}$ |
| Mean life of hydrogen | $5 \times 10^{13} \mathrm{yr}$ | $1 \times 10^{10} \mathrm{yr}$ | $4 \times 10^{8} \mathrm{yr}$ | $4 \times 10^{7} \mathrm{yr}$ | $7 \times 10^{5} \mathrm{yr}$ | $3 \times 10^{4} \mathrm{yr}$ |
| Energy production in ergs/ (g sec) | . 0025 | 12 | 300 | 3,000 | 200,000 | 4,000,000 |

Relative abundances of $\mathrm{N}^{14}: \mathrm{C}^{12}: \mathrm{C}^{13}: \mathrm{N}^{15}$ at a temperature of $17.5 \times 10^{0}{ }^{\circ} \mathrm{K}$ are in the approximate ratios of 5,000: 200: 50: 1.

Note that the energy-production for the carbon cycle increases much more rapidly with temperature than for the proton-proton cycle. At very "low" temperatures ( $\leq 10^{7}{ }^{\circ} \mathrm{K}$ ) the protonproton reactions are the only ones of importance. The net result at these temperatures is the formation of $\mathrm{He}^{3}$ and a positron out of three $\mathrm{H}^{1}$ nuclei, since the reaction between $\mathrm{He}^{3}$ and $\mathrm{He}^{4}$ is then too slow to be important. In Table 724 the reaction times of a few other nuclear reactions are given merely to show the rapid increase of the reaction time with increasing charge of the interacting muclei especially at lower temperatures. None of the reactions listed in Table 724 are of importance as sources of stellar energy.

* Tables 723 and 724 prepared by E. E. Salpeter.
${ }^{225}$ Bethe, Phys. Rev., vol. 55, p. 434, 1939; Astrophys. Journ., vol. 92, p. 118, 1940
Gamow and Critchfield, Theory of atome nucleus and nuclear energy sources, Oxford Univ. Press, 1940. Fowler, W. A., and Hall, R. N., Phys. Rev., vol. 77, p. 197, 1950, and private communication. Christy, R. F., and O'Reilly, J., unpublished work.

TABLE 724.-TIMES REQUIRED FOR SOME OTHER REACTIONS

| Reaction | Temperature: $15 \times 10^{6}{ }^{\circ} \mathrm{K}$ | $20 \times 10^{\circ}{ }^{\circ} \mathrm{K}$ | $30 \times 10^{\circ}{ }^{\circ} \mathrm{K}$ |
| :---: | :---: | :---: | :---: |
| $\mathrm{F}^{19}+\mathrm{H}^{1} \rightarrow \mathrm{O}^{16}+\mathrm{He}^{4}$ | $5 \times 10^{9} \mathrm{yr}$ | $1 \times 10^{7} \mathrm{yr}$ | $5 \times 10^{8} \mathrm{yr}$ |
| $\mathrm{N}^{15}+\mathrm{H}^{1} \rightarrow \mathrm{O}^{18}+\gamma$ | $1 \times 10^{8} \mathrm{yr}$ | $5 \times 10^{8} \mathrm{yr}$ | $5 \times 10^{3} \mathrm{yr}$ |
| $\mathrm{O}^{16}+\mathrm{H}^{2} \rightarrow \mathrm{~F}^{17}+\gamma$ | $5 \times 10^{18} \mathrm{yi}$ | $2 \times 10^{11} \mathrm{yr}$ | $1 \times 10^{8} \mathrm{yr}$ |
| $\mathrm{Ne}^{22}+\mathrm{H}^{1} \rightarrow \mathrm{Na}^{23}+\gamma$ | $5 \times 10^{15} \mathrm{yr}$ | $5 \times 10^{12} \mathrm{yr}$ | $5 \times 10^{8} \mathrm{yr}$ |
| $\mathrm{Li}^{7}+\mathrm{He}^{4} \rightarrow \mathrm{~B}^{11}+\gamma$ | $2 \times 10^{17} \mathrm{yr}$ | $2 \times 10^{24} \mathrm{yr}$ | $2 \times 10^{10} \mathrm{yr}$ |
| $\mathrm{Be}^{7}+\mathrm{He}^{4} \longrightarrow \mathrm{C}^{11}+\gamma$ | $5 \times 10^{23} \mathrm{yr}$ | $1 \times 10^{20} \mathrm{yr}$ | $2 \times 10^{15} \mathrm{yr}$ |


#### Abstract

All mean reaction times are proportional to the density $\rho$ of the stellar material and to $C_{n}$, the percentage by weight of hydrogen (except the reactions in which one of the colliding nuclei is $\mathrm{He}^{+}$instead of $\mathrm{H}^{1}$ in which case $C_{\# e}$ replaces $C_{\prime \prime}$ ). The figures in the above tables are for $C_{H}=67$ percent, $C_{H e}=30$ percent, and for $\rho=160 \mathrm{~g} / \mathrm{cm}^{3}$. The calculations of Christy and O'Reilly* for the interior of the sun give these values for $C_{H}, C_{I I}$ and $\rho$ as wcll as a concentration of 1.5 percent for carbon, nitrogen, and oxygen combined and of 1.5 percent for all other elements combined. Their calculations predict a temperature of about $17 \times 10^{\prime \circ} \mathrm{K}$ in the interior of the sun. The mean life of all the hydrogen now present and the total energy production due to the proton-proton cycle and the carbon cycle are also given in Table 723 . For the carbon cycle the mean life of hydrogen and the energy production depend on the concentration of the isotopes of carbon and nitrogen. These elements play the role of a "catalyst" controlling the speed of the reaction and are reproduced at the end of each cycle. The figures in Part 2 of Table 723 are for a concentration of 1 percent by weight for $\mathrm{N}^{14}$.


[^291]TABLE 725.-SLOW NEUTRON PRODUCED RADIOACTIVITIES OF LONG HALF-LIFE * ${ }^{220}$

| Radioactive isotope | Half-life | $\begin{gathered} \text { Max energy } \\ \beta-\text { particles } \\ \text { emited } \\ M \mathrm{Mev} \end{gathered}$ | $\begin{gathered} \text { Max energy } \\ \gamma-\text { rays } \\ \text { emitted } \\ \text { Mev } \end{gathered}$ | Thermal neutron cross section in barns | Percent abundance of parent nucleus |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{1} \mathrm{H}^{3}$ | 12.1 yr | . 0179 | none | $6.5 \times 10^{-4}$ | . 016 |
| ${ }_{1} \mathrm{H}^{3}$ | 12.1 yr | . 0179 | none | 860 ( $n, a$ ) | 7.5 |
| ${ }_{1} \mathrm{H}^{3}$ | $12.1 \mathrm{yr}^{\circ}$ | . 0179 | none | 5000 ( $n, p$ ) | $1.2 \times 10^{-4}$ |
| ${ }_{4} \mathrm{Be}^{10}$ | $2.7 \times 10^{\circ} \mathrm{yr}$ | . 6 | none | . 0085 | 100. |
| ${ }_{-} \mathrm{C}^{14}$ | 5700 yr | . 156 | none | $1.7(n, p)$ | 99.6 |
| ${ }_{0} \mathrm{C}^{14}$ | 5700 yr | . 156 | none | . 1 | 1.12 |
| ${ }_{11} \mathrm{Na}^{24}$ | 14.8 hr | 1.39 | 2.76 | . 4 | 100. |
| ${ }_{14} \mathrm{Si}^{31}$ | 170 min | 1.8 | none | . 11 | 3.05 |
| ${ }_{15} \mathrm{~S}^{35}$ | 14.3 d | 1.72 | none | . 23 | 100. |
| ${ }_{10} \mathrm{~S}^{35}$ | 87.1 d | . 169 | none | . 26 | 4.15 |
| ${ }_{17} \mathrm{Cl}^{36}$ | $2 \times 10^{\circ} \mathrm{yr}$ | . 64 | none | 53. | 75.4 |
| ${ }_{17} \mathrm{C}^{198}$ | 37.5 min | 4.94 | 2.15 | . 6 | 24.6 |
| ${ }_{18} \mathrm{~A}^{41}$ | 1.83 hr | 2.55 | 1.37 | 1.2 | 99.6 |
| ${ }_{19} \mathrm{~K}^{42}$ | 12.4 hr | 3.5 | 1.5 | 1.0 | 6.6 |
| ${ }_{20} \mathrm{Ca}^{45}$ | 152 d | . 260 | none | . 63 | 2.06 |
| ${ }_{20} \mathrm{Ca}^{48}$ | 2.5 hr | 2.3 | . 8 | . 2 | . 19 |
| ${ }_{21} \mathrm{Sc}^{48}$ | 85 d | 1.49 | 1.12 | 22. | 100. |
| ${ }_{22} \mathrm{Ti}^{\text {i }}$ | 72 d | . 36 | 1.0 | . 04 | 5.34 |
| ${ }_{24} \mathrm{Cr}^{51}$ | 26.5 d | K capture | . 32 | 16.2 | 4.49 |
| ${ }_{25} \mathrm{Mn}^{58}$ | 2.59 hr | 2.81 | 2.06 | 12.8 | 100. |
| ${ }_{28} \mathrm{Fe}^{55}$ | 4 yr | K capture | . 07 | 2.1 | 5.8 |
| ${ }_{20} \mathrm{Fe}^{59}$ | 47 d | . 46 | 1.30 | . 32 | . 28 |
| ${ }_{27} \mathrm{Co}^{\text {a0 }}$ | 5.3 yr | . 3 | 1.3 | 22.5 | 100. |
| ${ }_{28} \mathrm{Ni}^{\text {as }}$ | 2.6 hr | 1.9 | 1.1 | 2.6 | . 88 |
| ${ }_{29} \mathrm{Cu}^{\text {es }}$ | 12.8 hr | . 66 | 1.35 | 4.3 | 69.1 |
| ${ }_{30} \mathrm{Zn}^{\text {es }}$ | 250 d | . 4 | 1.14 | . 51 | 50.9 |
| ${ }_{30} \mathrm{Zn}^{\text {®0 }}$ | 13.8 hr | I.T. | . 44 | . 09 | 17.4 |
| ${ }_{30} \mathrm{Zn}^{\text {e9 }}$ | 57 min | 1.0 | none | . 9 | 17.4 |
| ${ }_{31} \mathrm{Ga}^{72}$ | 14.1 hr | 3.17 | 2.5 | 3.4 | 39.8 |
| ${ }_{32} \mathrm{Ge}^{71}$ (?) | 40 hr | 1.2 |  | . 073 | 21.2 |
| ${ }_{32} \mathrm{Ge}^{71}$ | 11.4 d | K capture | . 32 | . 45 | 21.2 |
| ${ }_{32} \mathrm{Ge}^{75}$ | 89 min | 1.2 |  | . 60 | 36.7 |
| ${ }_{32} \mathrm{Ge}^{77}$ | 12 hr | 2.0 |  | . 085 | 7.7 |
| ${ }_{33} \mathrm{As}^{78}$ | 26.8 hr | 3.0 | 1.2 | 4.6 | 100.87 |
| ${ }_{34} \mathrm{Se}^{75}$ | 127 d . | K capture | . 5 | 24. | . 87 |
| ${ }_{34} \mathrm{Se}^{81}$ | 58 min | I.T. | . 10 | . 03 | 49.8 |
| ${ }_{35} \mathrm{Br}^{80}$ | 4.4 hr | I.T. | . 049 | 3.0 | 50.6 |
| ${ }_{35} \mathrm{Br}^{82}$ | 34 hr | . 47 | 1.35 | 2.25 | 49.4 |
| ${ }_{36} \mathrm{Kr}^{79}$ | 34 hr | . 9 | . 2 | . 27 | . 34 |
| ${ }_{30} \mathrm{Kr}^{\text {88 }}$ | 4.5 hr | . 94 | . 37 | . 96 | 57. |
| ${ }_{36} \mathrm{Kr}^{88}$ | 9.4 yr | . 74 | none | . 06 | 57. |
| ${ }_{33} \mathrm{Kr}^{87}$ | 74 min | 4. |  | . 06 | 17.4 |
| ${ }_{37} \mathrm{Rb}^{88}$ | 19.5 d | 1.8 | 1.08 | . 72 | 72.8 |
| ${ }_{3 \times} \mathrm{Sr}^{57}$ | 2.7 hr | I.T. | . 386 | 1.3 | 9.9 |
| ${ }_{3} \mathrm{Sr}^{88}$ | 55 d | 1.5 | none | . 005 | 82.6 |
| ${ }_{38} \mathrm{Y}^{90}$ | 62 hr | 2.35 | none | 1.2 | 100. |
| ${ }^{\circ} \mathrm{Zr}{ }^{\text {05 }}$ | 65 d | 1.0 | . 92 | . 1 | 17. |
| ${ }^{10} \mathrm{Z} \mathrm{r}^{97}$ | 17 hr | 2.1 | . 8 | . 29 | 2.8 |
| ${ }^{12} \mathrm{Mo}^{\text {m8 }}$ | 6.7 hr | 3.7 | 1.6 | . 2 | 15.9 |
| ${ }_{42} \mathrm{Mo}^{08}$ | 67 hr | 1.5 | . 75 |  | 24. |
| ${ }_{43} \mathrm{Tc}^{98}$ | 6.6 hr | I.T. | . 136 | from $\mathrm{Mo}^{\text {ox }}$ decay |  |
| ${ }_{\text {14 }} \mathrm{Ru}^{177}{ }^{103}$ | $2.8{ }_{41} \mathrm{~d}$ | K capture | . 23 | .01 .2 | 5.7 31.3 |
| ${ }_{4} \mathrm{Ru}^{105}$ | 4 hr | 1.35 | . 76 | 1.67 | 18.3 |
| ${ }_{45} \mathrm{Rh}^{105}$ | 35 hr | . 78 | . 3 | from Ru ${ }^{105}$ decay |  |
| ${ }_{46} \mathrm{Pd}^{109}$ | 13 hr | 1.1 | none | 12.1 | 27. |
| ${ }_{60} \mathrm{Pd}^{111}$ | 26 min | 3.5 |  | . 39 | 13.5 |
| ${ }_{\text {* }} \mathrm{Ag}^{110}$ | 225 d | . 59 | 1.40 | 2.3 | 48.7 |
| ${ }_{4}^{47} \mathrm{Ag}^{111}$ | 7.5 48.6 din | I. 1.0 | none | from $\mathrm{Pd}_{2}^{111}$ decay | 12.8 |

[^292]\begin{tabular}{|c|c|c|c|c|c|}
\hline Radioactive
isotope \& Half-life \& Max energy $\beta$-particles emitted
Mev \& $$
\begin{gathered}
\text { Max energy } \\
\gamma-\text {-ays } \\
\text { emited } \\
\text { Mev }
\end{gathered}
$$ \& Thermal neutron cross section in barns \& Percent
abundance
of parent
nucleus <br>
\hline ${ }_{48} \mathrm{Cd}^{115}$ \& 43 d \& 1.7 \& . 5 \& . 14 \& 28. <br>
\hline ${ }_{48} \mathrm{Cd}{ }^{115}$ \& 2.33 d \& 1.13 \& . 55 \& 1.1 \& 28. <br>
\hline ${ }_{88} \mathrm{Cd}^{177}$ \& 2.8 hr \& 1.7 \& \& 1.4 \& 7.3 <br>
\hline ${ }_{40} \mathrm{Cn}^{114}$ \& 48 d . \& I.T. \& . 19 \& 61. \& 4.5 <br>
\hline ${ }_{40} \mathrm{In}^{113}$ \& 53.9 min \& . 85 \& 2.32 \& 56. \& 95.77 <br>
\hline ${ }_{50} \mathrm{Sn}^{113}$ \& 105 d \& . 080 \& . 085 \& 1.1 \& 1.1 <br>
\hline ${ }_{51} \mathrm{Sb}^{122}$ \& 2.8 d \& 1.94 \& . 57 \& 6.8 \& 57. <br>
\hline ${ }_{51} \mathrm{Sb}^{124}$ \& 60 d \& 2.37 \& 2.06 \& 2.5 \& 44. <br>
\hline ${ }_{52} \mathrm{Te}^{27}$ \& 9.3 hr \& . 70 \& none \& . 78 \& 18.7 <br>
\hline ${ }_{62} \mathrm{~T}^{1289}$ \& 72 min \& 1.8 \& . 8 \& . 13 \& 31.8 <br>
\hline ${ }_{63} \mathrm{I}^{128}$ \& 25 min \& 2.02 \& . 428 \& 6.8 \& 100. <br>
\hline ${ }_{53} \mathrm{I}^{131}$ \& 8 d \& . 687 \& . 37 \& from $\mathrm{Te}^{131}$ decay \& <br>
\hline ${ }_{54} \mathrm{Xe}^{138}$ \& 5.27 d \& . 35 \& . 085 \& . 2 \& 26.9 <br>
\hline ${ }_{\text {65 }} \mathrm{CS}^{184}$ \& 3.1 hr \& 2.4 \& . 7 \& . 016 \& 100. <br>
\hline ${ }_{65} \mathrm{Cs}^{134}$ \& 2.3 yr \& . 66 \& 1.40 \& 26. \& 100. <br>
\hline ${ }_{60} \mathrm{Ba}^{131}$ \& 11.7 d \& K capture \& 1.2 \& 24. \& . 09 <br>
\hline ${ }_{58} \mathrm{Ba}^{139}$ \& 85 min \& 2.27 \& . 163 \& . 5 \& 71.7 <br>
\hline ${ }_{5:} \mathrm{La}^{140}$ \& 40 hr \& 2.12 \& 2.3 \& 9. \& 99.9 <br>
\hline ${ }_{58} \mathrm{Ce}^{141}$ \& 30 d \& . 6 \& . 2 \& . 95 \& 88.5 <br>
\hline ${ }_{88} \mathrm{Ce}^{143}$ \& 33 hr \& 1.35 \& . 5 \& . 31 \& 11.1 <br>
\hline ${ }_{69} \mathrm{Pr}^{142}$ \& 19.3 hr \& 2.14 \& 1.9 \& 11. \& 100. <br>
\hline ${ }^{60} \mathrm{Nd}^{147}$ \& 11.0 d \& . 90 \& . 58 \& 1.5 \& 16.5 <br>
\hline ${ }_{00} \mathrm{Nd}^{149}$ \& 1.7 hr \& 1.5 \& \& 2.4 \& 6.8 <br>
\hline ${ }_{82} \mathrm{Sm}^{153}$ \& 47 hr \& . 78 \& . 61 \& 280. \& 26.6 <br>
\hline ${ }_{72} \mathrm{Sm}_{\mathrm{E}}{ }^{1505}$ \& 25 min \& 1.9 \& . 3 \& 6. \& 22.5 <br>
\hline ${ }_{93} \mathrm{Eu}^{182}$ \& 9.2 hr \& 1.88 \& . 725 \& 1530. \& 49.1 <br>
\hline ${ }_{83} \mathrm{Eu}^{154}$ \& 7 yr \& . 9 \& 1.2 \& 1000. \& 52.2 <br>
\hline ${ }_{84} \mathrm{Gd}^{150}$ \& 18 hr \& . 95 \& . 38 \& 1.1 \& 24.8 <br>
\hline ${ }_{\text {as }} \mathrm{Tb}^{180}$ \& 3.9 hr \& \& \& 11. \& 100. <br>
\hline ${ }^{59} \mathrm{~Tb}^{180}{ }^{108}$ \& 75 d \& ${ }_{1} .88$ \& 1.15 \& 22. \& 100. <br>
\hline ${ }_{07}^{88} \mathrm{Ho}^{188}$ \& 27.2 hr \& 1.6 \& . 8 \& 2700.
67. \& 100. <br>
\hline ${ }_{08} \mathrm{Er}^{180}$ \& 9.4 d \& . 33 \& none \& \& 27.1 <br>
\hline ${ }_{88} \mathrm{Er}^{171}$ \& 7.5 hr \& 1.5 \& . 81 \& 7. \& 14.9 <br>
\hline ${ }_{08} \mathrm{Tm}^{170}$ \& 127 d \& . 98 \& . 833 (?) \& 118. \& 100. <br>
\hline ${ }_{78} \mathrm{Yb}^{189}$ \& 33 d \& K capture \& . 4 \& 18,000. \& . 14 <br>
\hline ${ }_{70} \mathrm{Y}^{7} \mathrm{Yb}^{177}$ \& 4.1
2.1 d

hr \& .50
1.2 \& . 35 \& 50. \& 31.8
127 <br>
\hline ${ }_{71} \mathrm{Lu}^{178}$ \& 3.7 hr \& 1.15 \& none \& 30. \& 97.5 <br>
\hline ${ }_{71} \mathrm{Lu}^{177}$ \& 6.6 d \& . 47 \& . 2 \& 3200. \& 2.5 <br>
\hline ${ }_{72} \mathrm{Hf}^{181}$ \& 46 d \& . 46 \& . 47 \& 10. \& 35.1 <br>
\hline ${ }_{73} \mathrm{Ta}^{182}$ \& 120 d \& . 53 \& 1.22 \& 20.6 \& 100. <br>
\hline ${ }_{74} \mathrm{~W}^{188}$ \& 73 d \& . 43 \& none \& 2.1 \& 30.7 <br>
\hline ${ }_{74} \mathrm{~W}^{187}$ \& 24.1 hr \& 1.33 \& . 69 \& 37.2 \& 29.2 <br>
\hline ${ }_{75} \mathrm{Re}^{188}$ \& 90 hr \& 1.05 \& none \& 101. \& 38.2 <br>
\hline ${ }_{75} \mathrm{Re}^{188}$ \& 18 hr \& 2.05 \& 1.43 \& 75. \& 61.8 <br>
\hline ${ }_{78} \mathrm{Os}^{191}$ \& 15 d \& . 142 \& . 129 \& 3.4 \& 26.4 <br>
\hline ${ }_{76} \mathrm{Os}^{193}$ \& 32 hr \& 1.2 \& 1.58 \& 3.9 \& 41.0 <br>
\hline ${ }_{77 \text { IT }}{ }^{192}$ \& 70 d \& . 67 \& . 607 \& 740. \& 38.5 <br>
\hline ${ }_{77} \mathrm{Ir}^{109}$ \& 19 hr \& 2.2 \& 1.4 \& 130. \& 61.5 <br>
\hline ${ }_{78} \mathrm{Pt}^{107}$ \& 3.3 d \& \& \& 4.5 \& 25.4 <br>
\hline ${ }_{78} \mathrm{PP}^{107}$ \& 18 hr \& . 7 \& \& 1.1 \& 25.4 <br>
\hline ${ }_{79} \mathrm{Pt}^{198}{ }^{198}$ \& 31 min \& 1.8 \& \& 3.9 \& 7.2 <br>
\hline ${ }_{79} \mathrm{Au}^{198}$ \& 2.7 d \& . 96 \& . 411 \& 96. \& 100. <br>
\hline ${ }_{80} \mathrm{Hg}^{208}{ }^{208}$ \& 51.5 d \& . 21 \& . 3 \& 2.4 \& 29.6 <br>
\hline ${ }_{81}{ }_{82} \mathrm{Tl}^{204} \mathrm{~Pb}^{208}$ \& ${ }_{3.32}^{3.5 \mathrm{yr}}$ \& . 87 \& none \& 7.5 \& 29.2 <br>
\hline ${ }_{83}{ }_{83} \mathrm{~PB}^{210}{ }^{200}$ \& $5.0{ }^{3.32 \mathrm{dr}}$ \& .68
1.17 \& none \& .00045
.015 \& 52.3
100. <br>
\hline ${ }_{38} \mathrm{PO}^{210}$ \& 138 d \& \& ${ }_{\text {or }}{ }^{\text {nine }}$ decay \& \& <br>
\hline ${ }_{00} \mathrm{Th}^{238}$ \& 23.5 min \& 1.6 \& none \& \& 100. <br>
\hline ${ }_{01} \mathrm{PP}^{238}$ \& 25 d \& . 23 \& . 30 \& from $\mathrm{Th}^{288}$ decay \& <br>
\hline ${ }_{93}^{02} \mathrm{U}^{239} \mathrm{~N}^{239}$ \& 23.5
2.3 dmin
d \& 1.20
1.18 \& . 076 \& from $\underline{U}^{2 s}{ }^{\text {d }}$ dec \& 99. <br>
\hline
\end{tabular}

When various materials are bombarded with the high－speed particles produced by one of the de－ vices given in Table．718，disintegrations，or the building up of elements higher in the atomic table，result．Some examples of these reactions are given in the table．

Part 1．－Some values of the energy of artificial disintegration for different isotopes and for different reactions ${ }^{277}$

| Neutron bombardment |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{H}^{1}(n, \gamma) \mathrm{H}^{2}$ | $-2.320$ | Mev | $\mathrm{B}^{11}\left(n, H^{3}\right) \mathrm{Be}^{9}$ | $-9.57$ | Mev | $\mathrm{N}^{14}(n, a) \mathrm{B}^{11}$ | －． 28 | Mev |
| $\mathrm{He}^{3}(n, p) \mathrm{H}^{3}$ | ． 764 |  | $\mathrm{B}^{11}(n, \gamma) \mathrm{B}^{12}$ | 2.6 |  | $\mathrm{N}^{14}(n, p) \mathrm{C}^{14}$ | ． 60 |  |
| $\mathrm{Li}^{8}(n, p) \mathrm{He}^{8}$ | $-2.9$ |  | $\mathrm{Be}^{19}(n, \gamma) \mathrm{Be}^{10}$ | 6.69 |  | $\mathrm{O}^{16}(n, 2 n) \mathrm{O}^{15}$ | －15．6 |  |
| $\mathrm{Li}^{0}(n, a) \mathrm{H}^{3}$ | 4.785 |  | $\mathrm{Be}^{( }(n, a) \mathrm{He}^{8}$ | －． 80 |  | $\mathrm{O}^{18}(n, a) \mathrm{C}^{13}$ | $-2.31$ |  |
| $\mathrm{Li}^{7}(\boldsymbol{n}, \boldsymbol{\gamma}) \mathrm{Li}^{8}$ | 1.98 |  | $\mathrm{Be}^{0}(n, 2 n) \mathrm{Be}^{8}$ | $-1.63$ |  | $\mathrm{O}^{17}(n, a) \mathrm{C}^{14}$ | 1.73 |  |
| $\mathrm{B}^{10}(n, a) \mathrm{Li}^{7}$ | 2.79 |  | $\mathrm{C}^{12}(n, n) 3 a$ | － 7.43 |  | $\mathrm{N}^{14}\left(n, H^{3}\right) \mathrm{C}^{12}$ | － 4.10 |  |
| $\mathrm{B}^{10}\left(n, H^{3}\right) \mathrm{Be}^{8}$ | ． 22 |  | $\mathrm{C}^{12}(n, 2 n) \mathrm{C}^{11}$ | －18．68 |  | $\mathrm{N}^{14}(n, p) \mathrm{C}^{14}$ | ． 626 |  |
| $\mathrm{B}^{10}(n, p) \mathrm{Be}^{10}$ | ． 20 |  | $\mathrm{C}^{18}(n, a) \mathrm{B}^{10}$ | － 3.94 |  | $\mathrm{N}^{14}\left(n, H^{3}\right) 3 \mathrm{a}$ | $-11.43$ |  |
| $\mathrm{B}^{11}(n, a) \mathrm{Li}^{8}$ | － 6.66 |  |  |  |  | $\mathrm{N}^{15}\left(n, H^{3}\right) \mathrm{C}^{13}$ | － 9.97 |  |
| Proton bombardment |  |  |  |  |  |  |  |  |
| $\underline{L i}{ }^{0}(p, \gamma) \mathrm{Be}^{7}$ | 5.53 | Mev | $\mathrm{Be}^{9}(p, d) \mathrm{Be}^{8}$ | ． 558 |  | $\mathrm{N}^{14}(p, a) \mathrm{C}^{11}$ | － 3.00 |  |
| $\mathrm{Li}^{\text {e }}$（ $\left.p, a\right) \mathrm{He}^{8}$ | 4.021 |  | $\mathrm{B}^{10}(p, \gamma) \mathrm{C}^{11}$ | 8.70 |  | $\mathrm{N}^{15}(p, a) \mathrm{C}^{12}$ | 4.92 |  |
| $\mathrm{Li}^{7}(p, n) \mathrm{Be}^{7}$ | － 1.645 |  | $\mathrm{B}^{10}(p, n) \mathrm{C}^{10}$ | － 5.2 |  | $\mathrm{C}^{12}(p, \gamma) \mathrm{N}^{18}$ | 1.92 |  |
| $\mathrm{Li}^{7}(p, \gamma) \mathrm{Be}^{8}, \mathrm{Be}^{8}$ | 17.21 |  | $\mathrm{B}^{10}(p, a) \mathrm{Be}^{7}$ | 1.146 |  | $\mathrm{C}^{13}(p, \gamma) \mathrm{N}^{14}, \mathrm{~N}^{16}$＊ | 7.56 |  |
| $\mathrm{Li}^{7}(p, a) \mathrm{He}^{4}$ | 17.28 |  | $\mathrm{B}^{11}(p, a) \mathrm{Be}^{8}$ | 8.57 |  | $\mathrm{C}^{13}(p, n) \mathrm{N}^{13}$ | 2.96 |  |
| $\mathrm{Be}^{9}(p, d) \mathrm{Be}^{8}$ | ． 559 |  | $\mathrm{B}^{11}(p, n) \mathrm{C}^{11}$ | $-2.762$ |  | $\mathrm{F}^{19}(p, a) \mathrm{O}^{18}$ | 8.113 |  |
| $\mathrm{Be}^{9}(p, \gamma) \mathrm{B}^{10}, \mathrm{~B}^{10}$＊ | 6.49 |  | $\mathrm{B}^{11}(p, \gamma) \mathrm{C}^{12}, \mathrm{C}^{12}$＊ | 15.96 |  | $\mathrm{F}^{19}(p, n) \mathrm{Ne}^{19}$ | $-3.84$ |  |
| $\mathrm{Be}^{9}(p, n) \mathrm{B}^{9}$ | － 1.84 |  |  |  |  | $\mathrm{O}^{18}(p, n) \mathrm{F}^{18}$ | － 2.455 |  |
| $\mathrm{Be}^{9}(p, a) \mathrm{Li}^{8}$ | $2.125$ | Mev |  |  |  |  |  |  |
| Deuteron bombardment |  |  |  |  |  |  |  |  |
| $\mathrm{Li}^{\text {® }}$（ ${ }^{\text {d，a }}$ ） $\mathrm{He}^{4}$ | 22.23 | Mev | $\mathrm{B}^{11}($ d，a $) \mathrm{Be}^{\text {e }}$ | 8.03 | Mev | $\mathrm{C}^{13}(d, p) \mathrm{C}^{14}$ | 5.99 | Mev |
| $\underline{\mathrm{Li}}{ }^{6}(d, n) \mathrm{Be}^{8}$ | 3.54 |  | $\mathrm{B}^{11}(d, n) \mathrm{C}^{12}, \mathrm{C}^{12}$＊ | 13.78 |  | $\mathrm{N}^{14}(d, a) \mathrm{C}^{12}$ | 13.50 |  |
| $\underline{L} \mathrm{i}^{i}(d, p) \mathrm{Li}^{7}$ | 5.012 |  | $\mathrm{B}^{11}(d, p) \mathrm{B}^{12}$ | ． 7.4 |  | $\mathrm{N}^{14}(d, p) \mathrm{N}^{15}$ | 8.57 |  |
| $\mathrm{Li}^{\mathbf{8}}(d, n) \mathrm{Be}^{7}$ | 3.34 |  | $\mathrm{Be}^{9}(d, a) \mathrm{Li}^{7}, \mathrm{Li}^{7}{ }^{*}$ | 7.09 |  | $\mathrm{N}^{14}(d, n) \mathrm{O}^{15}$ | 5.1 |  |
| $\mathrm{Li}^{\mathbf{8}}(d, a) \mathrm{He}^{4}$ | 22.29 |  | $\mathrm{Be}^{9}\left(d, H^{3}\right) \mathrm{Be}^{8}$ | 4.53 |  | $\mathrm{N}^{14}\left(d, H^{3}\right) \mathrm{N}^{18}$ | $-4.36$ |  |
| $\underline{L^{17}}(d, p) \mathrm{Li}^{8}$ | － .193 |  | $\mathrm{Be}^{\theta}(d, p) \mathrm{Be}^{10}$ | 4.52 |  | $\mathrm{N}^{14}(d, a) 3 a$ | 6.16 |  |
| $\mathrm{Li}^{7}(d, a) \mathrm{He}^{5}$ | 14.3 |  | $\mathrm{C}^{12}(d, p) \mathrm{C}^{18}$ | 2.726 |  | $\mathrm{N}^{18}(d, a) \mathrm{C}^{13}$ | 7.62 |  |
| $\mathrm{B}^{10}($ d，a $) \mathrm{Be}^{8}, \mathrm{Be}^{8}$ | 17.81 |  | $\mathrm{C}^{12}(d, n) \mathrm{N}^{13}$ | －． 279 |  | $\mathrm{O}^{18}(d, a) \mathrm{N}^{14}$ | 3.07 |  |
| $\mathrm{B}^{10}(d, p) \mathrm{B}^{11}, \mathrm{~B}^{11}$＊ | 9.24 |  | $\mathrm{C}^{13}(d, a) \mathrm{B}^{11}$ | 5.10 |  |  |  |  |
| $\mathrm{B}^{10}(d, n) \mathrm{C}^{11}$ | 6.53 |  |  |  |  |  |  |  |
| $a$－ray bombardment |  |  |  |  |  |  |  |  |
| $\mathrm{Be}^{9}\left(a, a^{\prime}\right) \mathrm{Be}^{8}+n$ | $-1.63$ | Mev | $\mathrm{Li}^{7}(\mathrm{a}, n) \mathrm{B}^{10}, \mathrm{~B}^{10} *$ | $-2.78$ | Mev | $\mathrm{Be}^{9}\left(a, a^{\prime}\right) \mathrm{Be}^{9}{ }^{*}$ | $-1.63$ | Mev |
| $\mathrm{Be}^{\theta}\left(a, a^{\prime}\right) \mathrm{Be}^{8}{ }^{*}$ | $-1.63$ |  | $\mathrm{B}^{10}(\mathrm{a}, \mathrm{d}) \mathrm{C}^{12}$ | 1.44 |  | $\mathrm{B}^{11}(a, n) \mathrm{N}^{14}$ | ． 28 |  |
| $\mathrm{Be}^{0}\left(a, a^{\prime}\right) \mathrm{He}^{5}+a$ | $-2.4$ |  | $\mathrm{B}^{10}(a, p) \mathrm{C}^{13} \mathrm{C}^{13}{ }^{*}$ | 4.14 |  | $\mathrm{B}^{11}(a, p) \mathrm{C}^{14}$ | ． 88 |  |
| $\mathrm{Be}^{9}\left(a, a^{\prime}\right) 2 a+n$ | － 1.58 |  | $\mathrm{B}^{10}(a, n) \mathrm{N}^{18}$ | 1.18 |  | $\mathrm{C}^{12}(a, n) \mathrm{O}^{15}$ | $-8.4$ |  |
| $\mathrm{Li}^{\text {® }}$（ $\left.a, p\right) \mathrm{Be}^{9}$ | $-2.12$ |  | ${ }^{1} \mathrm{e}^{9}(\mathrm{a}, n) \mathrm{C}^{12}, \mathrm{C}^{12}$＊ | 5.75 |  |  |  |  |

[^293] p．372， 1950.

Part 2．－Photo－nuclear reactions，threshold values ${ }^{228}$

| $\mathrm{H}^{2}(\boldsymbol{\gamma}, n) \mathrm{H}^{1}$ | $2.20 \pm .05 \mathrm{Mev}$ | $\mathrm{Ca}^{40}(\gamma, n) \mathrm{Ca}^{30}$ | $15.9 \pm .4 \mathrm{Mev}$ | $\mathrm{Cd}^{113}(\gamma, n) \mathrm{Cd}^{112}$ | $6.44 \pm .15 \mathrm{Mev}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Be}^{0}(\gamma, n) \mathrm{Be}^{8}$ | 1．63 $\ddagger .3$ | $\mathrm{Fe}^{54}(\gamma, n) \mathrm{Fe}^{53}$ | $13.8 \pm .2$ | $\mathrm{Sn}^{119}(\gamma, n) \mathrm{Sn}^{118}$ | $6.51 \pm .15$ |
| $\mathrm{Lij}^{7}(\gamma, p) \mathrm{He}^{8}$ | $9.8 \pm .5$ | $\mathrm{Mn}^{55}(\gamma, n) \mathrm{Mn}^{54}$ |  | $\mathrm{Sn}^{124}(\gamma, n) \mathrm{Sn}^{123}$ | $8.50 \pm .15$ |
| $\mathrm{C}^{12}(\gamma, n) \mathrm{C}^{11}$ | $18.7 \pm 1.0$ | $\mathrm{Cu}^{13}(\gamma, n) \mathrm{Cu}^{02}$ | $10.9 \pm .2$ | $\mathrm{Sb}^{121}(\gamma, n) \mathrm{Sb}^{120}$ | $9.25 \pm .2$ |
|  | $10.65 \pm .2$ | $\mathrm{Cu}^{65}(\gamma, n) \mathrm{Cu}^{\text {ad }}$ | 10.2 士 ． 2 | ${ }_{\mathrm{P}^{127}}^{127}(\gamma, n){ }^{128}(\gamma){ }^{128}$ | $9.3 \pm .2$ |
| $\mathrm{Mg}^{24}(\gamma, n) \mathrm{Mg}^{23}$ | 16.2 ¥．3 | $\mathrm{Zn}^{\text {²4 }}\left(\gamma, n, \mathrm{Zn}^{\text {²3 }}\right.$ | $11.80 \pm .20$ | ${ }^{\operatorname{Pr}^{141}(\gamma, n)} \operatorname{Pr}^{140}$ | $9.40 \pm .10$ |
| $\mathrm{Mg}^{25}(\boldsymbol{\gamma}, \boldsymbol{p}) \mathrm{Na}^{24}$ | $11.5 \pm 1.0$ | $\mathrm{Zn}^{70 *}(\gamma, n) \mathrm{Zn}^{\text {®9 }}$ | 9．20士． 20 | $\mathrm{Nd}^{150}(\gamma, n) \mathrm{Nd}^{148}$ | $7.40 \pm .20$ |
| $\mathrm{Mg}^{28}\left(\boldsymbol{\gamma}, p\right.$ ） $\mathrm{Na}^{28}$ | $14.0 \pm 1.0$ |  | $10.7 \pm .20$ | $\mathrm{Ta}^{181}(\boldsymbol{\gamma}, n) \mathrm{Ta}^{180}$ $\mathrm{Au}^{197}(\boldsymbol{\gamma}, n) \mathrm{Au}^{180}$ | ${ }_{8.00}^{7.7} \pm .2$ |
|  |  |  |  |  | $8.00 \pm .15$ |
| ${ }^{\text {P }}$ | $12.35 \pm .2$ | $\mathrm{Zr}^{91}(\gamma, n) \mathrm{Zr}^{90}$ | $7.20 \pm .40$ | $\mathrm{T}^{205}(\gamma, n) \mathrm{T} \mathrm{P}^{204}$ | $7.38 \pm .15$ |
| $\mathrm{S}^{32}(\gamma, n) \mathrm{S}^{31}$ | $14.8 \pm .4$ | $\mathrm{Mo}^{82}(\boldsymbol{\gamma}, n) \mathrm{Mo}^{91}$ | 13．28 | $\mathrm{Pb}^{207}(\gamma, n) \mathrm{Pb}^{208}$ | $6.85 \pm .20$ |
| $\mathrm{K}^{39}(\gamma, n) \mathrm{K}^{38}$ | 13.2 士 ． 2 | $\mathrm{Mo}^{87}(\gamma, n) \mathrm{Mo}^{88}$ | $7.10 \pm .30$ | $\mathrm{Bi}^{208}(\boldsymbol{\gamma}, n) \mathrm{Bi}^{208}$ | $7.45 \pm .2$ |

[^294]The heavier elements, $\mathrm{Np}, \mathrm{Pu}, \mathrm{Am}, \mathrm{Cm}, \mathrm{Bk}$, and Cf may be produced by artificial transformation of $U$, followed by radioactive breakdown. A few examples follow :

$$
\begin{aligned}
& { }_{43} \mathrm{~N}_{\mathrm{p}}{ }^{20} \rightarrow{ }_{{ }_{4} \mathrm{Pu}^{23 n}}+\beta^{-} \text {(2.3 days) }
\end{aligned}
$$

For quantity production:

$$
\begin{aligned}
& { }_{94} \mathrm{Pu}^{241} \rightarrow{ }_{{ }_{5}} \mathrm{Am}^{241}+\beta^{-} \\
& { }_{06} \mathrm{Pu}^{239}+{ }_{2} \mathrm{He}^{4} \rightarrow \frac{{ }_{n P} \mathrm{Cm}^{242}}{}+\underset{{ }_{00} \mathrm{Cm}^{201}}{ }+{ }^{1} n^{2}+{ }^{2} n^{1}+{ }_{0} n^{1}
\end{aligned}
$$

For quantity production:

$$
\begin{aligned}
& { }_{93} \mathrm{Am}^{241}+{ }_{2} \mathrm{He}^{4} \rightarrow{ }_{n i} \mathrm{Bk}^{243}+{ }_{o n}{ }^{1}+{ }_{0} n^{1} \\
& { }_{90} \mathrm{Cm}^{242}+{ }_{2} \mathrm{He}^{4} \rightarrow \overline{{ }^{4}} \mathrm{Cf}^{24+}+{ }_{0} n^{1}+{ }_{0} n^{1}
\end{aligned}
$$

[^295]TABLE 728.-PILE YIELDS OF SOME ISOTOPES*
Calculated for 10 liters of material exposed to $10^{10}$ neutrons $\mathrm{cm}^{-3} \mathrm{sec}^{-1}$

| Radioactive isotope | Cross section in units of $10^{-24} \mathrm{~cm}^{2}$ times relative isotope abundance | Density material $\mathrm{g} / \mathrm{cm}^{3}$ | Half-life in hours | Atomic weight of material | Mean free path cm | Yields $\mathrm{mc} / \mathrm{hr}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{H}^{3}$ | $10^{-7}$ | 1 | $1.1 \times 10^{5}$ | 9 | $7 \times 10^{7}$ | $10^{-7}$ |
| $\mathrm{Be}^{10}$ | . 0086 | 1.85 | $2.4 \times 10^{10}$ | - 9 | 570 | $7 \times 10^{-8}$ |
| $\mathrm{C}^{14}$ | 1.7 | 1.6 | $4 \times 10^{7}$ | 30 | 12 | $2 \times 10^{-3}$ |
| $\mathrm{Na}^{24}$ | . 4 | . 97 | 14.8 | 23 | 60 | 1100 |
| $\mathrm{P}^{22}$ | . 23 | 2.2 | 343 | 31 | 60 | 45 |
| $\mathrm{K}^{+2}$ | . 066 | . 86 | 12.4 | 39 | 680 | 120 |
| $\mathrm{Ca}^{45}$ | . 012 | 1.54 | 3650 | 40 | 2220 | . 12 |
| $\mathrm{Fe}^{50}$ | . 001 | 4.86 | 1110 | 56 | 7000 | . 1 |
| $\mathrm{Zn}^{65}$ | . 26 | 7.14 | 6000 | 65 | 65 | 4.5 |
| $\mathrm{As}^{78}$ | 4.6 | 5.7 | 26.8 | 75 | 2.86 | 1300 |
| $\mathrm{Br}^{\mathrm{N}_{2}}$ | 1.12 | 3.12 | 34 | 80 | 22.8 | 1300 |
| $\mathrm{Rb}^{83}$ | . 52 | 1.53 | 469 | 85 | 106 | 20 |
| $\mathrm{Sr}^{89}$ | . 0041 | 2.6 | 1770 | 88 | 8000 | . 1 |
| $\mathrm{Ag}^{110}$ | 1.1 | 10.5 | 5400 | 108 | . 41 | 200 |
| In ${ }^{144 m}$ | 2.74 | 7.3 | 1150 | 115 | 5.7 | 150 |
| Ta ${ }^{182}$ | 20.6 | 16.6 | 2800 | 181 | . 48 | 680 |
| $B i^{210}$ | . 015 | 9.8 | 120 | 209 | 1420 | 6 |

[^296]TABLE 729.-COMPARATIVE PROPERTIES OF ORDINARY AND HEAVY WATER*

| Property | $\mathrm{H}_{2} \mathrm{O}$ | $\mathrm{H}_{2}{ }^{2} \mathrm{O}$ |
| :---: | :---: | :---: |
| Specific gravity at $25^{\circ} \mathrm{C}$ relative to ordinary water at $25^{\circ} \mathrm{C}$ | 1.0000 | 1.1079 |
| Temperature of maximum density | $4.0{ }^{\circ} \mathrm{C}$ | $11.6{ }^{\circ} \mathrm{C}$ |
| Dielectric constant | 81.5 | 80.7 |
| Surface tension | 72.75 dynes/cm | 67.8 |
| Viscosity at $10^{\circ} \mathrm{C}$ | 13.10 millipoises | 16.85 |
| Melting point | $.000^{\circ} \mathrm{C}$ | $3.802^{\circ} \mathrm{C}$ |
| Boiling point ( 76 cmHg pressure) | $100.00^{\circ} \mathrm{C}$ | $101.42^{\circ} \mathrm{C}$ |
| Heat of fusion. | $1436 \mathrm{cal} / \mathrm{mole}$ | 1510 |
| Heat of vaporization at $25^{\circ} \mathrm{C}$ | $10484 \mathrm{cal} / \mathrm{mole}$ | 10743 |
| Refractive index at $20^{\circ} \mathrm{C}$ for NaD line. | 1.33300 | 1.32828 |

* For reference, see footnote 224, p. 665.

TABLE 730.-THE MECHANICAL EFFECTS OF RADIATION ${ }^{230}$


[^297]A number of elements ( $12 ; 43$ isotopes) of high atomic weight, now found in the earth, and one of the isotopes of each of six lighter elements (Table 732) are unstable in that they spontaneously break down into other elements, emitting $a, \beta$ or $\gamma$ rays. The study of artificial radioactivity shows some other types of breakdown. Some of the artificial radioactive nuclei break down by the emission of positive electrons or of neutrons; a $K$ electron may be captured (designated by $K^{\prime}$ ) ; some internal conversion of electrons may take place ( $e^{-}$) or there may be some isomeric transition of the nucleus (I.T.).

The characteristics of the three rays- $a, \beta$, and $\gamma$-are quite different. A $3 \mathrm{Mev} a$-particle has a velocity of about $1 / 25$ that of light, a range in air of 1.7 cm , and produces some 4,000 ion pairs per mm in air at 760 mmHg at $15^{\circ} \mathrm{C}$. A $3 \mathrm{Mev} \beta$-ray has a velocity of nearly 99 percent of that of light and a range in air of about 13 meters, and produces only about 4 ion pairs per mm in air. The energy of a $\gamma$-ray, which is very short-wavelength radiant energy, is $E=h \nu$, and it has the velocity of light. Thus a $3 \mathrm{Mev} \gamma$-ray has a wavelength of 4.1 XU. However, the $\gamma$-rays given by the natural radioactive materials have much less energy than this ( 4 Mev ), generally about 1 Mev . [Some artificial radioactive materials emit $\gamma$-rays with very high energy (See Tables 750-752.).] The wavelengths of the $\gamma$-rays from natural radioactivity particles range from about 4.5 to about $4,000 \mathrm{XU}$. $\gamma$-rays have a very long range. A $\gamma$-ray produces directly no ions along its path but spends almost its entire energy in producing a photoelectron. Rutherford ${ }^{2300}$ says that the $\beta$-rays are about 100 times as penetrating as the $a$-rays, and the $\gamma$-rays 10 to 100 times as penetrating as the $\beta$-rays.

Today it should be stated that, in general, the radioactive isotopes (about 43 in number) of these 12 elements change into other isotopes, either smaller or of the same weight, depending upon the type of breakdown. The nucleus of the resulting isotope may be smaller in weight by about four units and have a charge two units smaller than the parent due to the emission of an $\alpha$-particle, or it may be of almost the same weight and have a charge one unit greater due to the emission of a $\beta$-ray. There are several changes in both the weight and charge that may take place for some of the artificial radioactive nuclei.

The character of these changes varies with the element and seems to be determined by some probability law. It does not seem possible, by any ordinary physical or chemical means, to change these characteristics. (See artificial disintegration, Table 726.)

[^298]
## TABLE 731.-UNITS FOR THE RATE OF RADIOACTIVE DISINTEGRATION

The curie, the adopted unit of the rate of radioactive decay, is defined as the number of disintegrations of 1 gram of radium $\left(3.61 \times 10^{10}\right)$ in 1 second. As a working value for the curie the National Bureau of Standards some years ago adopted the value $3.700 \times 10^{10}$ disintegrations per second.

The rutherford (abbreviated $r d$ ) $=10^{6}$ disintegrations per second, has been suggested as a smaller working standard. Then, 1 millirutherford ( mrd ) $=10^{3}$ disintegrations per second and 1 microrutherford $(\mu r d)=1$ disintegration per second.
The rate of disintegration of an isotope that emits gamma-rays may be determined by a measure of the $\gamma$-ray emission in roentgens.

A committee of the National Research Council ${ }^{281}$ recommended that the curie be defined as $3.70 \times 10^{10}$ disintegrations per second; the rutherford ( $r d$ ) as just given. For quantitative comparison of radioactive sources emitting gamma-rays, for which disintegration rates cannot be determined, the roentgen per hour at 1 meter ( rhm ) is recommended.

[^299]TABLE 732.-NATURAL RADIOACTIVE MATERIALS


[^300]TABLE 732.-NATURAL RADIOACTIVE MATERIALS (concluded)






TABLE 733.-THE ORIGINAL NAMES OF CERTAIN RADIOACTIVE MATERIALS*

| Radioactive name | Element and isotope | Radioactive name | Element and isotope |
| :---: | :---: | :---: | :---: |
| Actinium | 89 Actinium 227 | " D | 82 Lead 210 |
| Actinium A | 84 Polonium 215 | Radium E | 83 Bismuth 210 |
| " B | 82 Lead 211 | F | 84 Polonium 210 |
| " C | 83 Bismuth 211 | " G | 82 Lead 206 |
| " C' | 84 Polonium 211 | Radon $\dagger$ | 86 Radon 222 |
| " C" | 81 Thallium 207 | Actinon | 86 Radon 219 |
| " D | 82 Lead 207 | Emanation | 86 Radon 222 |
| " K | 87 Francium 223 | Niton | 86 Radon 222 |
| " X | 88 Radium 223 | Thoron | 86 Radon 220 |
| Actinouranium | 92 Uranium 235 | Thorium | 90 Thorium 232 |
| Brevium (see <br> Uranium $\mathrm{X}_{2}$ ) | 91 Protactinium 234m | Thorium ${ }_{\text {" }}^{\text {A }}$ | 84 Polonium 216 82 Lead 212 |
| Emanation | 86 Radon 222 | " ${ }^{\prime}$ ' | 84 Polonium 212 |
| Mesothorium I | 88 Radium 228 | " C" | 81 Thallium 208 |
| " II | 89 Actinium 228 | * D | 82 Lead 208 |
| Niton | 86 Radon 222 | " X | 88 Radium 224 |
| Radioactinium | 90 Thorium 227 | Thoron | 86 Radon 220 |
| Radiothorium | 90 Thorium 228 | Uranium I | 92 Uranium 238 |
| Radium | 88 Radium 226 | " II | 92 Uranium 234 |
| Radium A | 84 Polonium 218 | " $\mathrm{X}_{1}$ | 90 Thorium 234 |
| " B | 82 Lead 214 | " $\mathrm{X}_{2}$ | 91 Protactinium 234 m |
| " C | 83 Bismuth 214 | " Y | 90 Thorium 231 |
| " C' | 84 Polonium 214 | " Z | 91 Protactinium 234 |
| " C" | 81 Thallium 210 | Uranium lead | 82 Lead 206 |

* At times the prefix cca was used to designate the element following certain elements either in the periodic table or in radioactive series. $\dagger$ At one time all these materials were called Emanation, i.e., RaEm, AcEm, ThEm.


## TABLE 734.-THE FOUR RADIOACTIVE FAMILIES

The radioactive isotopes of the heavy materials arrange themselves into four families, or series, that are known either by the parent of the family or by the member of the series with the longest life. Before the various isotopes had been established some of the different members of the families had special names. (See Table 733.) These families or series are also designated by the numerical relation of the particular isotopes of the family involved and the number 4. Thus the four families or series are: (1) Thorium, or $4 n$ series; (2) Neptunium,* or $4 n+1$; (3) Uranium, or $4 n+2$; (4) Actinium, or $4 n+3$.

Generally, tables of these families show the type of radiation emitted, the energy of the radiation, the end product, and two or three factors that describe the time characteristics of the disintegrations; i.e., $T$ the half-life (that is, the time it takes for one-half of the given material to disintegrate, which can be accurately measured $T_{a}$, the average life, and $\lambda$, the decay constant. From the law of disintegration which radioactive materials have been found to follow, the three constants are shown to be related as follows: $\lambda=\frac{0.693}{T}$ and $T_{a}=\frac{1}{\lambda}$.
There are a number of isomers ${ }^{232}$ in the series as shown in Table 742, as for instance, see Uranium $\mathrm{X}_{1}$, Radium C, Actinium, etc. As a result of recent work on the artificial production of radioactive isotopes many more isomers could be given. Also, the first member of some of the series might be different. Thus, the $4 n+3$ series (the Actinium group) might start in this manner:

| Element | Rays and <br> end products | $T$ <br> (half-period) | Decay constant <br> sec $^{-1}$ |
| :---: | :---: | :---: | :---: |
| 92 Uranium 239 | $\beta^{-}, \mathrm{Np}^{238}$ | 23.5 min | $4.9 \times 10^{-8}$ |
| 93 Neptunium 239 | $\beta^{-}, \mathrm{Pu}^{238}$ | 2.3 days | $3.5 \times 10^{-7}$ |
| 94 Plutonium 239 | $a, \mathrm{U}^{298}$ | $2.4 \times 10^{4} \mathrm{yr}$ | $9.2 \times 10^{-18}$ |

To be sure, any trace of such members of this family would no longer be found in the earth.

[^301]TABLE 734.-THE FOUR RADIOACTIVE FAMILIES (continued)

| Part 1.-Thorium series (4n) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Atomic | Element | Isotope | Radioactive name | Rays and end product |  | $\underset{\text { (half period) }}{T}$ | $\begin{aligned} & \text { Decay } \\ & \text { constant } \\ & \lambda \text { sec }^{-1} \end{aligned}$ | Energy of radiation $\alpha$ or $\beta$ <br> in Mev |  |
| 90 | Thorium | 232 | Thorium | $a$ | MsTh 1 | $1.39 \times 10^{10} \mathrm{yr}$ | $1.58 \times 10^{-19}$ | 4.0 |  |
| 88 | Radium | 228 | Mesothorium 1 | $\beta^{-}$ | MsTh 2 | 6.7 yr | $3.28 \times 10^{-0}$ | . 05 | - |
| 89 | Actinium | 228 | Mesothorium 2 | $\beta^{-}, \gamma$ | RaTh | 6.13 hr | $3.14 \times 10^{-5}$ | 1.5 |  |
| 90 | Thorium | 228 | Radiothorium | a, $\gamma$ | ThX | 1.90 yr | $1.16 \times 10^{-8}$ | 5.4 |  |
| 88 | Radium | 224 | Thorium X | ${ }_{a}$ | Tn | 3.64 days | $2.20 \times 10^{-8}$ | 5.7 | - |
| 86 | Radon | 220 | Thoron | a | ThA | 54.5 sec | $1.27 \times 10^{-2}$ | 6.3 | - |
| 84 | Polonium | 216 | Thorium A | a | ThB | . 158 sec | 4.4 | 6.8 | - |
| 82 | Lead | 212 | Thorium B | $\beta^{-}, \gamma$ | ThC | 10.6 hr | $1.8 \times 10^{-5}$ | . 36 | - |
| 83 | Bismuth | 212 | Thorium C | ${ }_{\boldsymbol{a}}{ }^{\text {a }}$ | ThC" | 60.5 min | $1.91 \times 10^{-3}$ | 6.1 | - |
|  | Polonium | 212 | Thorium C' | $\underset{a}{\beta-\gamma}$ | ThC' | $3 \times 10^{-7} \mathrm{sec}$ | $2.3 \times 10^{-8}$ | 8.8 |  |
| 81 | Thallium | 208 | Thorium C" | $\beta^{-}, \gamma$ | ThD | 3.10 min | $3.72 \times 10^{-3}$ | 1.7 | 2.6 |
| 82 | Lead | 208 | Thorium D |  | Stable |  |  |  |  |

Part 2.-Neptunium series $(4 n+1)$

| Energy of radiation in Mev |  |
| :---: | :---: |
|  |  |
| .01-.02 | - |
| 5.46 | . 06 |
| 23 | . 2 |
| 4.7 |  |
| . 4 | . 3 |
| 4.8 | . 3 |
| 5. | - |
| 5.8 |  |



$\dagger$ Not isolated from ores, artificially produced by bombarding uranium with a-particles.
TABLE 734.-THE FOUR RADIOACTIVE FAMILIES (continued)

Part 3.-Uranium series $(4 n+2)$


$\begin{gathered}\text { Decay } \\ \text { constant } \\ \lambda \text { sec } \\ 2 \text { sec }\end{gathered}$
$2.3 \times 10^{-3}$
33.
$2.5 \times 10^{1}$
$1.6 \times 10^{-5}$
$5.2 \times 10^{-3}$
$5.8 \times 10^{-5}$
(half period)
5 min
.021 sec
$46^{2} \mathrm{~min}$
$4.2 \times 10^{-0} \mathrm{sec}$
2.2 ming
3.3 hr
 ,


| Isotope | Rays and end product |  | $\begin{gathered} T \\ \text { (half period) } \end{gathered}$ | $\begin{gathered} \text { Decay } \\ \text { constant } \\ \lambda \sec ^{-1} \end{gathered}$ | Energy of radiation |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 221 | a | At | 5 min | $2.3 \times 10^{-3}$ | 6.31 | - |
| 217 | a | Bi | . 021 sec | 33. | 7.0 | - |
| 213 | $\beta^{-}$ | $\mathrm{Po}^{\text {o }}$ | 46 min | $2.5 \times 10^{1}$ | 1.3 | - |
|  | a | T1 |  |  | 5.8 | - |
| 213 | $\alpha$ | Pb | $4.2 \times 10^{-9} \mathrm{sec}$ | $1.6 \times 10^{-3}$ | 8.4 | - |
| 209 | $\beta^{-}$ | Pb | 2.2 min | $5.2 \times 10^{-3}$ | 1.8 | - |
| 209 | $\beta^{-}$ | ${ }_{\text {Bi }}$ | 3.3 hr | $5.8 \times 10^{-8}$ | . 70 | - |
| 209 |  | Stable |  |  |  |  |


$\qquad$

| Atomic | Element | Isotope | Radioactive name name | Rays and end product |  | $\stackrel{T}{\text { (half period) }}$ | $\begin{gathered} \text { Decay } \\ \text { constant } \\ \lambda \sec ^{-1} \end{gathered}$ | Energy of radiation in Mev |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 92 | Uranium | 238 | Uranium I | a | UX 1 | $4.5 \times 10^{\mathrm{n}} \mathrm{yr}$ | $4.9 \times 10^{-18}$ | 4.2 | - |
| 90 | Thorium | 234 | Uranium $\mathrm{X}_{1}$ | $\begin{aligned} & \beta^{-}, \gamma \\ & \text { I.T. } \end{aligned}$ | $\begin{aligned} & \text { UX } 2 \\ & \text { UZ } \end{aligned}$ | 24.1 days | $3.3 \times 10^{-7}$ | . 15 | . 09 |
|  | Protactinium |  | Uranium $\mathrm{X}_{2}$ |  |  |  |  |  |  |
| 91 |  | 234 m |  | $\beta^{-}, \gamma$ | U II | 1.14 min | $1.01 \times 10^{-}$ | 2.0 | . 8 |
| 91 |  | 234 | Uranium Z | $\underset{a}{\beta^{-}, \gamma}$ | U II | 6.7 hr | $2.9 \times 10^{-5}$ | 1.0 | . 70 |
| 92 | Uranium | 234 | Uranium II |  | Io | $2.5 \times 10^{-5} \mathrm{yr}$ | $8.8 \times 10^{-14}$ | 4.7 | - |
| 90 | Thorium | 230 | Ionium | ${ }_{a, \gamma}$, | Ra | $8.0 \times 10^{1} \mathrm{yr}$ | $3.1 \times 10^{-11}$ | 4.7 | - |
| 88 | Radium | 226 | Radium |  | $\begin{aligned} & \mathrm{Rnn} \\ & \mathrm{RaA} \end{aligned}$ | 1620 yr | $1.355 \times 10^{-14}$ | 4.8 | . 19 |
| 86 | Radon | 222 | Emanation | $\underset{a}{a, \gamma}$ |  | 3.825 days | $2.10 \times 10^{-9}$ | 5.5 | - |
| 84 | Polonium | 218 | Radium A | ${ }_{\text {a }}{ }^{-}$ | RaB | 3.05 min | $3.85 \times 10^{-2}$ | 6.0 | - |
|  |  |  |  |  | AcRaC | 26.8 min |  |  |  |
| 82 | Lead | 214 | Radium B | $\beta^{-}$ |  |  | $4.3 \times 10^{-4}$ | 5.4 | 1.8 |
| 83 | Bismuth | 214 | Radium C | $\underset{\beta^{-}}{a, \gamma}$ | RaC" | 19.7 min | $5.85 \times 10^{-4}$ | 3.1 | - |
|  |  |  |  |  | $\mathrm{RaC}^{\text {RaD }}$ |  | $4.5 \times 10^{3}$ | 7.7 |  |
| 81 | Thallium | 210 | Radium C" | ${ }^{\beta^{-}, \gamma}$ | $\begin{aligned} & \mathrm{RaD} \\ & \mathrm{RaD} \end{aligned}$ | $1.5 \times 10^{-4} \mathrm{sec}$ 1.32 min | $9.8 \times 10^{-2}$ | 1.80 |  |
| 82 | Lead | 210 | Radium D |  | RaE | 22 yr | $1.0 \times 10^{-0}$ | . 025 | . 05 |
| 83 | Bismuth | 210 | Radium E | $\begin{gathered} \beta^{\prime} \\ a, \gamma \end{gathered}$ | RaF | 5.0 days | $1.6 \times 10^{-0}$ | 1.17 |  |
| 84 | Polonium | 210 | Radium F |  | RaG Stable | 138 days | $5.35 \times 10^{-9}$ | 5.3 | . 77 |
| 82 | Lead | 206 | Radium G <br> (uranium lead) | a, $\gamma$ |  |  |  |  |  |


| Atomic | Element | Isotope | Radioactive name name | Rays and end product |  | $\stackrel{T}{\text { (half period) }}$ | $\begin{gathered} \text { Decay } \\ \text { constant } \\ \lambda \sec ^{-1} \end{gathered}$ | Energy of radiation in Mev |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 92 | Uranium | 238 | Uranium I | a | UX 1 | $4.5 \times 10^{\mathrm{n}} \mathrm{yr}$ | $4.9 \times 10^{-18}$ | 4.2 | - |
| 90 | Thorium | 234 | Uranium $\mathrm{X}_{1}$ | $\begin{aligned} & \beta^{-}, \gamma \\ & \text { I.T. } \end{aligned}$ | $\begin{aligned} & \text { UX } 2 \\ & \text { UZ } \end{aligned}$ | 24.1 days | $3.3 \times 10^{-7}$ | . 15 | . 09 |
|  | Protactinium |  | Uranium $\mathrm{X}_{2}$ |  |  |  |  |  |  |
| 91 |  | 234 m |  | $\beta^{-}, \gamma$ | U II | 1.14 min | $1.01 \times 10^{-}$ | 2.0 | . 8 |
| 91 |  | 234 | Uranium Z | $\underset{a}{\beta^{-}, \gamma}$ | U II | 6.7 hr | $2.9 \times 10^{-5}$ | 1.0 | . 70 |
| 92 | Uranium | 234 | Uranium II |  | Io | $2.5 \times 10^{-5} \mathrm{yr}$ | $8.8 \times 10^{-14}$ | 4.7 | - |
| 90 | Thorium | 230 | Ionium | ${ }_{a, \gamma}$, | Ra | $8.0 \times 10^{1} \mathrm{yr}$ | $3.1 \times 10^{-11}$ | 4.7 | - |
| 88 | Radium | 226 | Radium |  | $\begin{aligned} & \mathrm{Rnn} \\ & \mathrm{RaA} \end{aligned}$ | 1620 yr | $1.355 \times 10^{-14}$ | 4.8 | . 19 |
| 86 | Radon | 222 | Emanation | $\underset{a}{a, \gamma}$ |  | 3.825 days | $2.10 \times 10^{-9}$ | 5.5 | - |
| 84 | Polonium | 218 | Radium A | ${ }_{\text {a }}{ }^{-}$ | RaB | 3.05 min | $3.85 \times 10^{-2}$ | 6.0 | - |
|  |  |  |  |  | AcRaC | 26.8 min |  |  |  |
| 82 | Lead | 214 | Radium B | $\beta^{-}$ |  |  | $4.3 \times 10^{-4}$ | 5.4 | 1.8 |
| 83 | Bismuth | 214 | Radium C | $\underset{\beta^{-}}{a, \gamma}$ | RaC" | 19.7 min | $5.85 \times 10^{-4}$ | 3.1 | - |
|  |  |  |  |  | $\mathrm{RaC}^{\text {RaD }}$ |  | $4.5 \times 10^{3}$ | 7.7 |  |
| 81 | Thallium | 210 | Radium C" | ${ }^{\beta^{-}, \gamma}$ | $\begin{aligned} & \mathrm{RaD} \\ & \mathrm{RaD} \end{aligned}$ | $1.5 \times 10^{-4} \mathrm{sec}$ 1.32 min | $9.8 \times 10^{-2}$ | 1.80 |  |
| 82 | Lead | 210 | Radium D |  | RaE | 22 yr | $1.0 \times 10^{-0}$ | . 025 | . 05 |
| 83 | Bismuth | 210 | Radium E | $\begin{gathered} \beta^{\prime} \\ a, \gamma \end{gathered}$ | RaF | 5.0 days | $1.6 \times 10^{-0}$ | 1.17 |  |
| 84 | Polonium | 210 | Radium F |  | RaG Stable | 138 days | $5.35 \times 10^{-9}$ | 5.3 | . 77 |
| 82 | Lead | 206 | Radium G <br> (uranium lead) | a, $\gamma$ |  |  |  |  |  |


| Atomic | Element | Isotope | Radioactive name name | Rays and end product |  | $\stackrel{T}{\text { (half period) }}$ | $\begin{gathered} \text { Decay } \\ \text { constant } \\ \lambda \sec ^{-1} \end{gathered}$ | Energy of radiation in Mev |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 92 | Uranium | 238 | Uranium I | a | UX 1 | $4.5 \times 10^{\mathrm{n}} \mathrm{yr}$ | $4.9 \times 10^{-18}$ | 4.2 | - |
| 90 | Thorium | 234 | Uranium $\mathrm{X}_{1}$ | $\begin{aligned} & \beta^{-}, \gamma \\ & \text { I.T. } \end{aligned}$ | $\begin{aligned} & \text { UX } 2 \\ & \text { UZ } \end{aligned}$ | 24.1 days | $3.3 \times 10^{-7}$ | . 15 | . 09 |
|  | Protactinium |  | Uranium $\mathrm{X}_{2}$ |  |  |  |  |  |  |
| 91 |  | 234 m |  | $\beta^{-}, \gamma$ | U II | 1.14 min | $1.01 \times 10^{-}$ | 2.0 | . 8 |
| 91 |  | 234 | Uranium Z | $\underset{a}{\beta^{-}, \gamma}$ | U II | 6.7 hr | $2.9 \times 10^{-5}$ | 1.0 | . 70 |
| 92 | Uranium | 234 | Uranium II |  | Io | $2.5 \times 10^{-5} \mathrm{yr}$ | $8.8 \times 10^{-14}$ | 4.7 | - |
| 90 | Thorium | 230 | Ionium | ${ }_{a, \gamma}$, | Ra | $8.0 \times 10^{1} \mathrm{yr}$ | $3.1 \times 10^{-11}$ | 4.7 | - |
| 88 | Radium | 226 | Radium |  | $\begin{aligned} & \mathrm{Rnn} \\ & \mathrm{RaA} \end{aligned}$ | 1620 yr | $1.355 \times 10^{-14}$ | 4.8 | . 19 |
| 86 | Radon | 222 | Emanation | $\underset{a}{a, \gamma}$ |  | 3.825 days | $2.10 \times 10^{-9}$ | 5.5 | - |
| 84 | Polonium | 218 | Radium A | ${ }_{\text {a }}{ }^{-}$ | RaB | 3.05 min | $3.85 \times 10^{-2}$ | 6.0 | - |
|  |  |  |  |  | AcRaC | 26.8 min |  |  |  |
| 82 | Lead | 214 | Radium B | $\beta^{-}$ |  |  | $4.3 \times 10^{-4}$ | 5.4 | 1.8 |
| 83 | Bismuth | 214 | Radium C | $\underset{\beta^{-}}{a, \gamma}$ | RaC" | 19.7 min | $5.85 \times 10^{-4}$ | 3.1 | - |
|  |  |  |  |  | $\mathrm{RaC}^{\text {RaD }}$ |  | $4.5 \times 10^{3}$ | 7.7 |  |
| 81 | Thallium | 210 | Radium C" | ${ }^{\beta^{-}, \gamma}$ | $\begin{aligned} & \mathrm{RaD} \\ & \mathrm{RaD} \end{aligned}$ | $1.5 \times 10^{-4} \mathrm{sec}$ 1.32 min | $9.8 \times 10^{-2}$ | 1.80 |  |
| 82 | Lead | 210 | Radium D |  | RaE | 22 yr | $1.0 \times 10^{-0}$ | . 025 | . 05 |
| 83 | Bismuth | 210 | Radium E | $\begin{gathered} \beta^{\prime} \\ a, \gamma \end{gathered}$ | RaF | 5.0 days | $1.6 \times 10^{-0}$ | 1.17 |  |
| 84 | Polonium | 210 | Radium F |  | RaG Stable | 138 days | $5.35 \times 10^{-9}$ | 5.3 | . 77 |
| 82 | Lead | 206 | Radium G <br> (uranium lead) | a, $\gamma$ |  |  |  |  |  |

 Radioactive
 $-$

TABLE 734.-THE FOUR RADIOACTIVE FAMILIES (concluded)

| Atomic | Element | Isotope | Radioactive name | $\begin{aligned} & \text { Rays and end } \\ & \text { product } \end{aligned}$ |  | $\underset{\text { (half period) }}{T}$ | $\begin{gathered} \text { Decay } \\ \text { constant } \\ \lambda \sec ^{-1} \end{gathered}$ | Energy of radiation $a$ or $\beta$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 92 | Uranium | 235 | Actinouranium | $a, \gamma$ | UY | $8 \times 10^{\text {e }} \mathrm{yr}$ | $3.1 \times 10^{-17}$ | 4.6 | . 16 |
| 90 | Thorium | 231 | Uranium Y | $\beta^{-}, \gamma, c^{-}$ | Pa | 25.6 hr | $7.52 \times 10^{-5}$ | . 2 | . 04 |
| 91 | Protactinium | 231 | Protactinium | $a, \gamma$ | Ac | $3.4 \times 10^{4} \mathrm{yr}$ | $6.5 \times 10^{-13}$ | 5.0 | . 3 |
| 89 | Actinium | 227 | Actinium | $\beta^{-}$ | RdAc |  |  | 4.9 | . 04 |
|  |  |  |  | $\gamma$ | Ack | 21.7 yr | $\begin{aligned} & 1.01 \times 10^{-9} \\ & 4.3 \times 10^{-7} \end{aligned}$ |  |  |
| 90 87 | Thorium | 227 | Radioactinium Actinium K | $a_{1}, \gamma$ $\beta^{-}, \gamma$ | AcX AcX | 18.6 days | $5.5 \times 10^{-4}$ | 1.2 | . 1 |
| 87 88 | Francium Radium | 223 | ${ }_{\text {Actinum }} \mathrm{K}$ | ${ }_{a, \gamma}{ }^{\prime}$ | Acx An | 11.2 days | $7.2 \times 10^{-7}$ | 5.7 | . |
| 86 | Radon | 219 | Actinon | a | AcA | 3.9 sec | . 178 | 6.8 |  |
| 84 | Polonium | 215 | Actinium A | a | AcB | $1.8 \times 10^{-3} \mathrm{sec}$ | $3.9 \times 10^{-1}$ | 7.4 | - |
|  |  |  |  | $\beta^{-}$ $a$ | $\mathrm{At}_{\mathrm{AcC}}$ |  | $6.9 \times 10^{3}$ |  |  |
| 85 82 | Astatine Lead | 215 | Astatine Actinium B | $\stackrel{a}{\beta^{-}, \gamma}$ | AcC AcC | 36 min | $3.2 \times 10^{-4}$ | 1.5 | . 8 |
| 83 | Bismuth | 211 | Actinium C | $\beta^{-}, \gamma$ | $\mathrm{AcC}^{\prime}$ ', | 2.2 min | $5.2 \times 10^{-3}$ | 6.6 | - |
|  | Polonium | 211 | Actinium $\mathrm{C}^{\prime}$ | a | AcC AcD | $5 \times 10^{-3} \mathrm{sec}$ | $1.4 \times 10^{2}$ | 7.4 | - |
| 81 | Thallium | 207 | Actinium C" | $\beta^{-}, \gamma$ | AcD | 4.8 min | $2.4 \times 10^{-3}$ | 1.5 | - |
| 82 | Lead | 207 | Actinium D |  | Stable |  |  |  |  |


| Atomic | Element | Isotope | Radioactive name | $\begin{aligned} & \text { Rays and end } \\ & \text { product } \end{aligned}$ |  | $\underset{\text { (half period) }}{T}$ | $\begin{gathered} \text { Decay } \\ \text { constant } \\ \lambda \sec ^{-1} \end{gathered}$ | Energy of radiation $a$ or $\beta$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 92 | Uranium | 235 | Actinouranium | $a, \gamma$ | UY | $8 \times 10^{\text {e }} \mathrm{yr}$ | $3.1 \times 10^{-17}$ | 4.6 | . 16 |
| 90 | Thorium | 231 | Uranium Y | $\beta^{-}, \gamma, c^{-}$ | Pa | 25.6 hr | $7.52 \times 10^{-5}$ | . 2 | . 04 |
| 91 | Protactinium | 231 | Protactinium | $a, \gamma$ | Ac | $3.4 \times 10^{4} \mathrm{yr}$ | $6.5 \times 10^{-13}$ | 5.0 | . 3 |
| 89 | Actinium | 227 | Actinium | $\beta^{-}$ | RdAc |  |  | 4.9 | . 04 |
|  |  |  |  | $\gamma$ | Ack | 21.7 yr | $\begin{aligned} & 1.01 \times 10^{-9} \\ & 4.3 \times 10^{-7} \end{aligned}$ |  |  |
| 90 87 | Thorium | 227 | Radioactinium Actinium K | $a_{1}, \gamma$ $\beta^{-}, \gamma$ | AcX AcX | 18.6 days | $5.5 \times 10^{-4}$ | 1.2 | . 1 |
| 87 88 | Francium Radium | 223 | ${ }_{\text {Actinum }} \mathrm{K}$ | ${ }_{a, \gamma}{ }^{\prime}$ | Acx An | 11.2 days | $7.2 \times 10^{-7}$ | 5.7 | . |
| 86 | Radon | 219 | Actinon | a | AcA | 3.9 sec | . 178 | 6.8 |  |
| 84 | Polonium | 215 | Actinium A | a | AcB | $1.8 \times 10^{-3} \mathrm{sec}$ | $3.9 \times 10^{-1}$ | 7.4 | - |
|  |  |  |  | $\beta^{-}$ $a$ | $\mathrm{At}_{\mathrm{AcC}}$ |  | $6.9 \times 10^{3}$ |  |  |
| 85 82 | Astatine Lead | 215 | Astatine Actinium B | $\stackrel{a}{\beta^{-}, \gamma}$ | AcC AcC | 36 min | $3.2 \times 10^{-4}$ | 1.5 | . 8 |
| 83 | Bismuth | 211 | Actinium C | $\beta^{-}, \gamma$ | $\mathrm{AcC}^{\prime}$ ', | 2.2 min | $5.2 \times 10^{-3}$ | 6.6 | - |
|  | Polonium | 211 | Actinium $\mathrm{C}^{\prime}$ | a | AcC AcD | $5 \times 10^{-3} \mathrm{sec}$ | $1.4 \times 10^{2}$ | 7.4 | - |
| 81 | Thallium | 207 | Actinium C" | $\beta^{-}, \gamma$ | AcD | 4.8 min | $2.4 \times 10^{-3}$ | 1.5 | - |
| 82 | Lead | 207 | Actinium D |  | Stable |  |  |  |  |

## Part 4.-Actinium series $(4 \boldsymbol{n}+3)$

TABLE 735.-VAR!ATIONS IN THE ISOTOPIC COMPOSITION OF COMMON LEAD *


* For reference, see footnote 45, p. 136.

TABLE 736.—LEAD RATIOS OF SELECTED RADIOACTIVE MINERALS*


[^302]TABLE 737.-ANALYSIS OF THORIUM C" (THALLIUM 208) BETA-RAY SPECTRUM ${ }^{233}$

|  |  | $\begin{gathered} \stackrel{5}{6} \\ \stackrel{y}{0} \\ \hline 0 \end{gathered}$ | Energy of $\beta$-ray line + absorption nergy in Mev | $\begin{gathered} \text { Energy } \\ \text { of } \begin{array}{c} \text { r-ray } \\ \text { Mev } \end{array} \end{gathered}$ |  | $\stackrel{\text { 立 }}{\stackrel{y}{E}}$ | $\begin{aligned} & \text { 霝 } \end{aligned}$ | Energy of $\beta$-rav line + absorption energy Mev Mev | $\begin{gathered} \text { Energy } \\ \text { of } \begin{array}{c} \text { Yray } \\ \text { Mev } \end{array} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | v.s. | $L_{\text {I }}$ | . $0252+.0158$ | . 0410 | 23 | m . | $L_{1}$ | $.2446+.0158$ | . 2604 |
| 2 | s. | $l^{\prime \prime}$ | $.0259+.0152$ | . 0411 | 18 | v.s. | K | $.1915+.0875$ | . 2790 |
| 3 | m. | $L_{\text {III }}$ | $.0278+.0133$ | . 0411 | 25 | m | $L_{1}$ | $.2640+.0158$ | . 2798 |
| 4 | v.s. | $M_{1}$ | $.0369+.0038$ | . 0407 | 20 | s. | K | $.2042+.0875$ | . 2917 |
| 5 | m. | $M_{v}$ | $.0380+.0025$ | . 0406 | 26 | m.s. | $L_{1}$ | $.2756+0158$ | . 2914 |
| 6 | . | $N_{t}$ | . $0398+.0009$ | . 0407 | 29 | v.s. | K | $.4281+.0875$ | . 5156 |
| 7 | m. | $N \mathrm{~N}$ or O | . $0404+.0001$ | . 0405 | 30 | v.s. | $L_{1}$ | $.5025+.0158$ | . 518.3 |
| 8 | f. | K | $.0577+.0875$ | . 1452 | 31 | m.f. | $M_{t}$ | $.5150+.0038$ | . 5188 |
| 13 | f. | $L_{t}$ | $.1283+.0158$ | . 1441 | 30 | v.s. | K | $.5025+.0875$ | . 5900 |
| 12 | m.s. | K | $.1231+.0875$ | . 2106 | 33 | m.s. | Ll | $.5729+.0158$ | . 5887 |
| 19 | m.f. | $I_{1}$ | $.1954+.0158$ | . 2112 | 35 | m.f. | K | $.6990+.0875$ | . 786 |
| 14 | m.s. | $K$ | . $1458+.0875$ | . 2333 | 36 | f. | $L_{1}$ | $.770+.0158$ | . 786 |
| 21 | m.f. | $L_{1}$ | . $2165+.0158$ | . 2323 | 40 | s. | K | $2.558+.0875$ | 2.646 |
| 16 | m.s. | K | $.1661+.0875$ | . 2536 | 41 | m . | $L_{1}$ | $2.635+.0158$ | 2.651 |
| 22 | f. | $L_{1}$ | $.2369+.0158$ | . 2527 | 42 | f | $M_{r}$ | $2.646+.0034$ | 2.649 |
| 17 | m. | K | $.1706+.0875$ | . 2581 |  |  |  |  |  |

[^303]
## TABLE 738.-ALPHA-RAY SPECTRA OF SOME NATURAL RADIOACTIVE MATERIALS

It is sometimes stated that all alpha-particles from any one source are emitted with the same energy or velocity. This is in the main true for most of the particles but careful measurements have shown that this is not always the case. For some time it was known that occasionally an alpha-particle had a range much longer than average, which, of course, means a high initial velocity.

| $\begin{aligned} & \text { Atomic } \\ & \text { No. } \end{aligned}$ | Element and isotope | a-ray | Mean range in air, cm | Velocity <br> ( $\mathrm{cm} / \mathrm{sec}$ ) $\times 10^{-v}$ | $\begin{gathered} \text { a-ray } \\ \text { energy } \end{gathered}$ $\mathrm{Mev}$ | Disintegration energy Mev | Energy differences from main group Mev | Relative number of particles |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 92 | Uranium 238 <br> (Uranium I) |  | 2.92 | 1.420 | 4.20 | 4.28 | . . . |  |
|  | Uranium 234 (Uranium II) |  | 3.5 | 1.515 | 4.76 | 4.85 | .... | .... |
| 91 | Protactinium 231 |  | 3.8 | 1.553 | 5.01 | 5.11 |  |  |
| 90 | Thorium 232 |  | 2.90 | 1.390 | 4.00 | 4.75 |  |  |
|  | Thorium 230 (Ionium) |  | 3 | $1.500$ | 4.66 | 4.67 | ... | .... |
|  | Thorium 228 <br> (Radiothorium) <br> Thorium 227 <br> (Radioactinium) | $a_{0}$ |  | 1.6150 | 5.418 | 5.517 | 0 | 5 |
|  |  | $a_{1}$ |  | 1.6020 | 5.335 | 5.431 | . 086 | 1 |
|  |  | $a_{0}$ |  | 1.7063 | 6.049 | 6.159 | 0 | 80 |
|  |  | $a_{1}$ | .... | 1.7021 | 6.019 | 6.127 | . 32 | 15 |
|  |  | $\alpha_{2}$ | . . . | 1.6979 | 5.990 | 6.097 | . 62 | 100 |
|  |  | $a_{3}$ |  | 1.6948 | 5.986 | 6.075 | . 84 | 15 |
|  |  | $a_{4}$ |  | 1.6885 | 5.924 | 6.030 | 1.29 | 5 |
|  |  | $a_{5}$ |  | 1.6806 | 5.870 | 5.975 | 1.84 | 10 |
|  |  | $a_{6}$ | .... | 1.6729 | 5.817 | 5.921 | 2.38 | 5 |
|  |  | $a_{3}$ | .... | 1.6558 | 5.766 | 5.869 | . 290 | 80 |
|  |  | $a_{8}$ |  | 1.6627 | 5.744 | 5.847 | . 312 | 15 |
|  |  | $\alpha_{9}$ |  | 1.6589 | 5.719 | 5.822 | . 337 | 60 |
|  |  | $\alpha_{10}$ | $\ldots$ | 1.6524 | 5.674 | 5.776 | . 383 | 10 |
| 88 | Radium 226 | $a_{0}$ | $\begin{aligned} & 3.5 \\ & 3.4 \end{aligned}$ | 1.520 | 4.793 | 4.879 | 0 | . . |
|  |  |  |  | 1.492 | 4.612 | 4.695 | . 184 |  |
|  | Radium 224 <br> (Thorium X) |  | .... | 1.653 | 5.681 5.719 | 5.786 5.823 | . .18 |  |
|  | Radium 223 <br> (Actinium X) | $a_{0}$$a_{1}$ |  | $\begin{aligned} & 1.6589 \\ & 1.6424 \end{aligned}$ | $\begin{aligned} & 5.719 \\ & 5.607 \end{aligned}$ | $\begin{aligned} & 5.823 \\ & 5.709 \end{aligned}$ | 0 |  |
|  |  |  |  |  |  |  | . 114 | 6 4 |
|  |  | Radon 222 <br> (Emanation) |  |  | 1.6316 | 5.533 | 5.634 | . 186 | 1 |
| 86 |  |  |  | 4.3 | 1.626 | 5.486 | 5.58867 | .... | . . . . |
|  | Radon 220 <br> (Thoron) |  | 4.967 | 1.7387 | 6.2872 | 6.3995 | $\cdots$ | 10 |
|  | Radon 219 | $a_{0}$ | 5.655 | 1.8117 | 6.824 | 6.953 | 0 | 10 |
|  | (Actinon) | $a_{1}$ | (5.308) | 1.7763 | 6.561 | 6.683 | . 270 | 1 |
|  |  | $a_{2}$ | 5.147 | 1.7593 | 6.436 | 6.556 | . 397 | 1 |
| 84 | Polonium 218 <br> (Radium A) |  | 4.9 | 1.700 | 6.00024 | 6.11239 | . . . | ... |
|  | Polonium 216 <br> (Thorium A) |  | 5.601 | 1.8054 | 6.774 | 6.9038 | .... | .... |
|  | Polonium 215 <br> (Actinium A) <br> Polonium 214 <br> (Radium C') |  | 6.420 | 1.8824 | 7.368 | 7.508 | $\cdots$ | $\cdots$ |
|  |  |  | $6.870$ | 1.9220 | 7.68300 | $7.82934$ | $0$ | $10^{8}$ |
|  |  |  | 7.755 | 1.9550 2.0729 | 8.280 | $\begin{aligned} & 8.437 \\ & 9.112 \end{aligned}$ | .608 1.283 | $\begin{gathered} .43 \\ (.45) \end{gathered}$ |
|  |  |  | 9.00 | 2.0876 | 9.068 | 9.242 | 1.412 | 22 |
|  |  |  |  | 2.1157 | 9.315 | 9.493 | 1.663 | . 38 |
|  |  |  |  | 2.1356 | 9.492 | 9.673 | 1.844 | 1.35 |
|  |  |  |  | 2.1543 | 9.660 | 9.844 | 2.015 | . 35 |
|  |  |  | .... | 2.1678 | 9.781 | 9.968 | 2.138 | 1.06 |
|  |  |  |  | 2.1817 | 9.908 | 10.097 | 2.268 | . 36 |
|  |  |  | .... | 2.2001 | 10.077 | 10.269 | 2.439 | 1.67 |
|  |  |  |  | 2.2079 | 10.149 | 10.342 | 2.513 | . 38 |
|  |  |  |  | 2.2274 | 10.329 | 10.526 | 2.697 | 1.12 |
|  |  |  | 11.47 | 2.2466 | 10.509 | 10.709 | 2.880 | . 23 |
|  | Polonium 213 |  | 3.805 | 1.59715 | 5.3006 | 5.4033 | ... | ... |

TABLE 738.-ALPHA-RAY SPECTRA OF SOME NATURAL RADIOACTIVE MATERIALS (concluded)

| Atomic No. | Element and isotope | a-ray | Mean range in air, cm | Velocity <br> ( $\mathrm{cm} / \mathrm{sec}$ ) $\times 10^{-9}$ | a-ray energy Mev | Disintegration Mev | Energy differences from main group Mev | Relative number of particles |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Polonium 212 |  | 8.533 | 2.05405 | 8.7783 | 8.9476 | 0 | $10^{6}$ |
|  | (Thorium C') |  | 9.687 | 2.1354 | 9.4912 | 9.6736 | . 726 | 34 |
|  |  |  | 11.543 | 2.2501 | 10.5418 | 10.7447 | 1.797 | 190 |
|  | Polonium 211 <br> (Actinium C') |  | 6.518 | 1.8911 | 7.434 | 7.581 |  |  |
| 83 | Bismuth 214 | $a_{0}$ | (4.039) | 1.630 | 5.5068 | 5.6117 | 0 | 94 |
|  | (Radium C) | $a_{1}$ | (3.969) | 1.620 | 5.4458 | 5.5495 | . 062 | 113 |
|  | Bismuth 212 | $a_{1}$ |  | 1.7108 | 6.081 | 6.20069 | 0 | 27.2 |
|  | (Thorium C) | $a_{2}$ |  | 1.7053 | 6.044 | 6.16069 | . 0400 | 69.8 |
|  |  | $a_{3}$ |  | 1.6651 | 5.762 | 5.8729 | . 3278 | 1.80 |
|  |  | $\alpha_{4}$ | .... | 1.6446 | 5.620 | 5.7283 | . 4724 | . 16 |
|  |  | $a_{5}$ |  | 1.6418 | 5.610 | 5.7089 | . 4918 | 1.10 |
|  | Bismuth 211 | $a_{0}$ | 5.392 | 1.7832 | 6.619 | 6.739 | 0 | 100 |
|  | (Actinium C) | $a_{1}$ | 4.947 | 1.7356 | 6.262 | 6.383 | . 356 | 19 |

TABLE 739.-CHARACTERISTICS OF SOME HIGH-SPEED ALPHA-PARTICLES FROM NATURAL RADIOACTIVE SOURCES*

| $\begin{aligned} & \text { Atomic } \\ & \text { No. } \end{aligned}$ | Element | Isotope | Common name | Velocity | Energy Mev | Range $\dagger$ cm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 92 | Uranium | 234 | Uranium II | $1.516 \times 10^{0}$ | 4.76 | 3.4 |
|  |  | 235 | Actinouranium | 1.483 | 4.56 | 3.2 |
|  |  | 238 | Uranium I | 1.43 | 4.18 | 2.9 |
| 91 | Protactinium | 231 |  | 1.555 | 5.01 | 3.7 |
| 90 | Thorium | 227 | Radioactinium |  | 6.05 | 4.8 |
|  |  | 228 | Radiothorium | 1.616 | 5.42 | 4.1 |
|  |  | 230 | Ionium | 1.500 | 4.66 | 3.3 |
|  |  | 232 | Thorium | 1.498 | 3.98 | 2.7 |
| 89 | Actinium | 227 | Actinium | 1.537 | 4.94 | 3.6 |
| 88 | Radium | 223 | Actinium X | 1.660 | 5.72 | 4.4 |
|  |  | 224 | Thorium X | 1.657 | 5.68 | 4.4 |
|  |  | 226 | Radium | 1.520 | 4.79 | 3.5 |
| 86 | Radon | 219 | Actinon | 1.814 | 6.82 | 5.8 |
|  |  | 220 | Thoron | 1.729 | 6.28 | 5.1 |
|  |  | 222 | Radon | 1.628 | 5.49 | 4.2 |
| 85 | Astatine | 215 | Rador | 1.964 | 8.00 | 7.4 |
|  |  | 216 |  | 1.937 | 7.79 | 7.1 |
|  |  | 218 |  | 1.802 | 6.72 | 5.7 |
| 84 | Polonium | 210 | Polonium | 1.599 | 5.30 | 4.0 |
|  |  | 211 | Actinium $\mathrm{C}^{\prime}$ | 1.894 | 7.43 | 6.6 |
|  |  | 212 | Thorium C' | 2.058 | 8.78 | 8.7 |
|  |  | 214 | Radium $\mathrm{C}^{\prime}$ | 1.925 | 7.68 | 7.0 |
|  |  | 215 | Actinium A | 1.886 | 7.37 | 6.5 |
|  |  | 216 | Thorium A | 1.805 | 6.77 | 5.8 |
|  |  | 218 | Radium A | 1.701 | 6.00 | 4.8 |
| 83 | Bismuth | 211 | Actinium C | 1.787 | 6.62 | 5.6 |
|  |  | 212 | Thorium C | 1.713 | 6.08 | 4.9 |
|  |  | 214 | Radium C | 1.630 | 5.51 | 4.2 |

[^304]TABLE 740.-CHARACTERISTICS OF SOME HIGH-SPEED ALPHA-PARTICLES FROM ARTIFICIAL RADIOACTIVE SOURCES *

| Atomic No. | Element | Isotope | Velocity $\mathrm{cm} / \mathrm{sec}$ | Energy Mev | Range in air, $\dagger \mathrm{cm}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 96 | Curium | . 238 | $1.77 \times 10^{9}$ | 6.50 | 5.4 |
|  |  | 240 | 1.74 | 6.26 | 5.1 |
|  |  | 241 | 1.71 | 6.08 | 4.9 |
|  |  | 242 | 1.72 | 6.1 | 4.9 |
| 95 | Americium | 239 | 1.67 | 5.77 | 4.5 |
|  |  | 241 | 1.62 | 5.48 | 4.2 |
| 94 | Plutonium | . 232 | 1.78 | 6.6 | 5.5 |
|  |  | 234 | 1.73 | 6.2 | 5.0 |
|  |  | 236 | 1.66 | 5.75 | 4.5 |
|  |  | 238 | 1.63 | 5.51 | 4.2 |
|  |  | 239 | 1.57 | 5.15 | 3.8 |
|  |  | 240 | 1.57 | 5.1 | 3.8 |
| 93 | Neptunium | . 231 | 1.73 | 6.2 | 5.0 |
|  |  | 235 | 1.56 | 5.06 | 3.8 |
|  |  | 237 | 1.51 | 4.77 | 3.4 |
| 92 | Uranium | . 228 | 1.80 | 6.72 | 5.7 |
|  |  | 229 | 1.76 | 6.42 | 5.3 |
|  |  | 230 | 1.68 | 5.85 | 4.6 |
| 91 | Protactinium | 226 | 1.81 | 6.81 | 5.8 |
|  |  | 227 | 1.76 | 6.46 | 5.4 |
|  |  | 228 | 1.71 | 6.09 | 4.9 |
|  |  | 229 | 1.66 | 5.69 | 4.4 |
| 90 | Thorium | . 224 | 1.86 | 7.20 | 6.3 |
|  |  | 225 | 1.78 | 6.57 | 5.5 |
|  |  | 226 | 1.74 | 6.30 | 5.1 |
|  |  | 227 | 1.71 | 6.05 | 4.8 |
|  |  | 229 | 1.56 | 5.02 | 3.7 |
| 89 | Actinium |  | 1.83 | 6.96 | 6.0 |
|  |  | 223 | 1.79 | 6.64 | 5.6 |
|  |  | 224 | 1.73 | 6.17 | 5.0 |
|  |  | 225 | 1.67 | 5.80 | 4.5 |
| 88 | Radium | . 220 | 1.90 | 7.49 | 6.7 |
|  |  | 221 | 1.80 | 6.71 | 5.6 |
|  |  | 222 | 1.77 | 6.51 | 5.4 |
|  |  | 224 | 1.65 | 5.68 | 4.4 |
| 87 | Francium | 218 | 1.94 | 7.85 | 7.2 |
|  |  | 219 | 1.88 | 7.30 | 6.4 |
|  |  | 220 | 1.80 | 6.69 | 5.6 |
|  |  | 221 | 1.74 | 6.30 | 5.2 |
| 86 | Radon | . 216 | 1.97 | 8.07 | 7.6 |
|  |  | 217 | 1.93 | 7.74 | 7.1 |
|  |  | 218 | 1.85 | 7.12 | 6.2 |
| 85 | Astatine | 207 | 1.67 | 5.76 | 4.5 |
|  |  | 208 | 1.65 | 5.66 | 4.4 |
|  |  | 211 | 1.69 | 5.89 | 4.6 |
|  |  | 214 | 2.06 | 8.78 | 8.4 |
|  |  | 217 | 1.84 | 7.02 | 6.1 |
| 84 | Polonium | 208 | 1.57 | 5.14 | 3.8 |
|  |  | 205 | 1.61 | 5.35 | 4.0 |
|  |  | 206 | 1.58 | 5.2 8.34 | 3.9 8.0 |
|  |  | 213 197 | 2.01 | 8.34 | 8.0 5.0 |
| 83 | Bismuth | - 197 | 1.73 1.68 | 6.20 5.83 | 5.0 4.6 |
|  |  | 198 | 1.68 1.62 | 5.83 5.47 | 4.6 |
|  |  | 200 | 1.58 | 5.15 | 3.8 |

[^305]TABLE 741.-VAPOR PRESSURE OF THE RADIUM EMANATION IN $\mathbf{c m H g}$
$\begin{array}{llrrrrrrrrrrrr}\text { Temperature }{ }^{\circ} \mathrm{C} & \ldots \ldots \ldots & -127 & -101 & -65 & -56 & -10 & +17 & +49 & +73 & +100 & +104 \\ \text { Vapor pressure } \ldots . . . & .9 & 5 & 76 & 100 & 500 & 1000 & 2000 & 3000 & 4500 & 4745 & \end{array}$

TABLE 742.-BETA-RAYS FROM RADIOACTIVE MATERIALS—BOTH NATURAL (MARKED WITH *) AND ARTIFICIAL

| $\begin{aligned} & \text { Atomic } \\ & \text { No. } \end{aligned}$ | Element | Isotope | Radioactive | Energy in Mev |
| :---: | :---: | :---: | :---: | :---: |
| 95 | Americium | 242 m | ..... | . 8 |
| 93 | Neptunium | 239 | $\ldots$ | . 68 |
| 92 | Uranium | 238 |  | 1.20 |
| 91 | Protactinium | 234 m* | Uranium $\mathrm{X}_{2}$ | 2.32 |
|  |  | 230 |  | $\sim 1.1$ |
| 90 | Thorium | 233 |  | 1.2 |
| 89 | Actinium | 228* | Mesothorium 2 | 1.55 |
| 87 | Francium | 223* | Actinium K | 1.20 |
| 83 | Bismuth | 213 |  | $\sim 1.3$ |
|  |  | 210* | Radium E | 1.17 |
| 82 | Lead | 211* | Actinium B | 1.40 |
|  |  | 209 | .... | . 7 |
| 81 | Thallium | 209 |  | 1.8 |
|  |  | 208* | Thorium C" | 1.82 |
|  |  | 207* | Actinium C" | 1.47 |
|  |  | 206 | . | 1.70 |
|  |  | 204 | .... | . 8 |
| 80 | Mercury | 205 | .... | 1.62 |
| 79 | Gold | 200-202 | .... | 2.5 |
|  |  | 198 |  | . 96 |
| 78 | Platinum | 199 | .... | 1.8 |
|  |  | 197 |  | . 65 |
| 77 | Iridium | 194 | $\ldots$ | 2.2 |
|  |  | 192 | .... | . 67 |


| Atomic No. No. | Element | Isotope | Energy in Mev | $\begin{aligned} & \text { Atomic } \\ & \text { No. } \end{aligned}$ | Element | Isotope | Energy in Mev |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 76 | Osmium | 193 | 1.5 | 54 | Xenon | 137 | 4.0 |
| 75 | Rhenium | 188 | 2.5 | 53 |  | 135 | . 93 |
|  |  | 186 | 1.07 |  | Iodine | 136 | 6.5 |
| 74 | Tungsten | 187 | . 63 |  |  | 135 | 1.4 |
| 73 | Tantalum | 182 | 1.0 |  |  | 133 | 1.4 |
| 71 | Lutetium | 176 m | 1.15 |  |  | 128 | 1.59 |
|  |  | 170 | $1.7 \beta^{+}$ | 52 | Tellurium | 129 | 1.8 |
| 7069 | Ytterbium | 177 | 1.3 |  |  | 127 | . 76 |
|  | Thulium | 170 | 1.0 | 51 | Antimony | 126 | 2.8 |
| 6867 | Erbium | 171 | 1.49 |  |  | 124 m | 3.2 |
|  | Holmium | 166 | $1.8{ }^{1.8}{ }^{+}$ |  |  | 124 | 2.37 1.36 |
| 656463 | Terbium Gadolinium Europium | ${ }_{154}^{162-161}$ | $\begin{array}{lll}2.0 & \beta^{+} \\ 2.6 & \beta^{+}\end{array}$ |  |  | 122 | ${ }_{1}^{1.36}{ }^{+}$ |
|  |  | 161 | 1.5 |  |  | 118 | $3.1 \beta^{+}$ |
|  |  | $>154$ | $\sim 2.5$ | 50 | Tin | $>120$ | 1.8 |
| 63 |  | 157 154 | $\sim_{9}$ |  |  | 125 | $\sim 2.6$ |
|  |  | 152 | 1.88 | 49 | Indium | 117 | 1.73 |
| 62 | Samarium | 155 | 1.9 |  |  | 116 | 2.8 |
|  |  | 153 | . 78 |  |  | 114 | 1.5 |
| 61 | Promethium | 149 148 | 1.1 |  |  | 112 | $1.5{ }^{1.2} \beta^{+}$ |
|  |  |  | 1.7 | 48 | Cadmium | 115 m | 1.8 |
|  |  |  | 2.0 | 47 | Silver | 113 | 2.2 |
| 60 | Neodymium | 149 | 1.6 |  |  | 112 | 3.6 |
|  |  | 141 | . $78 \beta^{+}$ |  |  | 110 | 2.6 |
| 59 | Praseodymium | 145 | 3.2 |  |  | 108 |  |
|  |  | 144 140 | ${ }_{2.5}^{3.0} \beta^{+}$ | 46 | Palladium | 106 | $2.04 \beta^{+}$ |
| 5857 | Cerium Lanthanum | 143 | 1.36 |  |  | 101 | $2.3 \beta^{+}$ |
|  |  | 141 | 2.9 | 45 | Rhodium | 106 | 3.55 |
|  |  | <139 | 2.1 | 44 | Ruthenium | 104 | -4.3. |
|  |  | 139 | 2.27 |  |  | 105 | 1.4 |
| 55 | Cesium | 138 | 2.6 |  |  | 95 | $1.1 \beta^{+}$ |

TABLE 742.-BETA-RAYS FROM RADIOACTIVE MATERIALS—BOTH NATURAL (MARKED WITH *) AND ARTIFICIAL (concluded)

| $\begin{aligned} & \text { Atomic } \\ & \text { No. } \end{aligned}$ | Element | Isotope | Energy in Mev | Atomic No. | Element | Isotope | Energy <br> in Mev |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 43 | Technetium | 101 | 1.3 | 28 | Nicke1 | 65 | 1.9 |
|  |  | 100 | 2.3 |  |  | 57 | . $67 \beta^{+}$ |
|  |  | 95 | 1.3 | 27 | Cobalt | 62 |  |
|  |  | 94 | $2.47 \beta^{+}$ |  |  | 56 | $1.5 \beta^{+}$ |
|  |  | 92 | $4.3 \beta^{+}$ | 26 | Iron | 52 | . 55 \% |
| 42 | Molybdenum | 101 | 2.0 | 25 | Manganese | 52 m | $2.66 \beta^{+}$ |
|  |  | 99 | 1.3 |  |  | 51 | $2.0 \beta^{+}$ |
|  |  | 93 | $2.65 \beta^{+}$ | 24 | Chromium | 49 | $1.45{ }^{+}$ |
| 41 | Niobium | 97 | 1.4 | 23 | Vanadium | 52 | 2.05 |
|  |  | 96 | 1.8 |  |  | 47 | $1.9 \beta^{+}$ |
|  |  | 92 | 1.38 | 22 | Titanium | 51 m |  |
| 40 | Zirconium | 97 | 2.2 |  |  | 45 | $1.2{ }^{+}$ |
| 39 | Yttrium | 89 93 | $1.07{ }^{\text {d }}{ }^{+}$ | 21 | Scandium | 49 | 1.8 1.5 |
|  | Ytrium | 92 | 3.5 |  |  | 41 | $4.94{ }^{\text {/ }}$ |
|  |  | 91 | 1.5 | 20 | Calcium | 49 | 2.3 |
|  |  | 90 | 2.35 | 19 | Potassium | 42 | 2.04 |
|  |  | 88 | . $83 \beta^{+}$ |  |  | 40* | 1.9 |
| 38 | Strontium | 91 | 1.3 |  |  | 38 | $2.5{ }^{+}$ |
| 37 | Rubidium | 88 | 1.5 4.6 | 18 | Argon | 41 35 | ${ }_{4.1}^{1.18} \beta^{+}$ |
|  |  | 86 | 1.8 | 17 | Chlorine | 38 | 1.19 |
|  |  | 81 | . $9 \beta^{+}$ |  |  | 34 | $2.5 \beta^{+}$ |
| 36 | Krypton | 87 | $\sim 4$. |  |  | 33 | $4.1 \beta^{+}$ |
|  |  | 85 | 1.0 | 16 | Sulfur | 37 |  |
| 35 | Bromine | 85 | 2.5 |  |  | 31 | $3.85 \beta^{+}$ |
|  |  | 84 | 5.3 | 15 | Phosphorus | 34 | 5.1 |
|  |  | 80 78 | 2.0 |  |  | 32 | $1.7$ |
|  |  | 78 76 78 | $2.3 \beta^{+}$ |  |  | 30 29 | $\begin{array}{lll}3.0 & \beta^{+} \\ 3.6 & \beta^{+}\end{array}$ |
|  |  | 75 | $1.6 \beta^{+}$ | 14 | Silicon | 31 |  |
| 34 | Selenium | 83 | 1.5 |  |  | 27 | $3.74 \beta^{+}$ |
|  |  | 83 m | 3.4 | 13 | Aluminum | 29 | 2.5 |
|  |  | 81 | 1.5 |  |  | 28 | 3.0 |
| 33 | Arsenic | 78 | 1.4 |  |  | 26 | $3.0{ }^{+}$ |
|  |  | 74 | 1.3 | 12 | Magnesium | 23 | $2.82 \beta^{+}$ |
| 32 |  | 72 77 | $2.78 \beta^{+}$ | 11 | Sodium | 24 | 1.4 |
| 32 | Germanium | ${ }_{77}^{77}$ | 2.8 | 10 | Neon | 23 19 | $4.12 \beta^{+}$ |
|  |  | 71 | $1.2 \beta^{+}$ | 9 | Fluorine | 20 | 5.0 |
| 31 | Gallium | 73 | 1.4 |  |  | 17 | $2.1 \beta^{+}$ |
|  |  | 70 | 1.68 | 8 | Oxygen | 19 | 4.5 |
|  |  | 68 | $1.9 \beta^{+}$ |  |  | 14 | $1.8 \beta^{+}$ |
|  |  | 66 | $3.1{ }^{+}{ }^{+}$ | 7 | Nitrogen | 17 | 3.75 |
| 30 | Zinc | 69 | 1.0 |  |  | 16 |  |
| 29 | Copper | 66 | 2.9 | 6 | Carbon | $\sim 10$ | $2{ }^{\text {}}$ |
|  |  | 62 | $2.6 \beta^{+}$ | 5 | Boron | 12 | 12 |
|  |  | 61 | $1.2 \beta^{+}$ |  | Lithium | 8 | 12 |
|  |  | 60 | $1.8 \beta^{+}$ | 2 | Helium | 6 | 3.7 |

TABLE 743.-RELATIVE STOPPING POWER OF SELECTED SUBSTANCES FOR a-PARTICLES ${ }^{234}$

${ }^{234}$ Rasetti, Franco, Elements of nuclear physics. Copyright 1936 by Prentice-Hall, Inc., New York.

|  | $\begin{aligned} & \text { N} \\ & \stackrel{\rightharpoonup}{5} \\ & \stackrel{y}{E} \end{aligned}$ |  | Energy of $\beta$－ray line + absorption nergy Mev | $\begin{gathered} \text { Energy } \\ \text { of } \begin{array}{c} \text {-ray } \\ \text { Mev } \end{array} \end{gathered}$ |  |  |  | $\begin{gathered} \text { Energy of } \beta \text {-ray } \\ \text { line +ahorption } \\ \text { energy } \\ \text { Mev } \end{gathered}$ $\mathrm{Mev}$ | $\begin{aligned} & \text { Energy } \\ & \text { of } \begin{array}{c} \text { Y-ray } \\ \text { Mev } \end{array} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 20 | $L_{1}$ | $.0125+.0192$ | ． 0317 | 26 | 40 | $L_{1}$ | ． $0813+.0192$ | ． 1005 |
| 3 | 20 | $L_{\text {III }}$ | $.0160+.0154$ | ． 0314 | 29 | 30 | $M_{t}$ | ． $0965+.0048$ | ． 1013 |
| 6 | 15 | $M_{1}$ | $.0262+.0048$ | ． 0310 | 30 | 30 | $N_{1}$ | $.0990+.0012$ | ． 1002 |
| 7 | 10 | $M_{\text {II }}$ | $.0271+.0044$ | ． 0315 | 18 | 100 | K | $.0454+.1035$ | ． 1489 |
| 9 | 15 | Mv | $.0290+.0031$ | ． 0321 | 35 | 80 | $L_{1}$ | $.1305+.0192$ | ． 1497 |
| 10 | 30 | $N_{t}$ | $.0299+.0012$ | ． 0311 | 36 | 30 | $M_{1}$ | $.1445+.0048$ | ． 1493 |
| 11 | 20 | $N_{v i}$ | $.0305+.0003$ | ． 0308 | 28 | 50 | K | $.0936+.1035$ | ． 1971 |
| 12 | 15 |  | ． 0320 | ． 0320 | 38 | 30 | $L_{1}$ | $.1753+.0192$ | ． 1945 |
| 4 | 50 | $L_{1}$ | $.0246+.0192$ | ． 0438 | 40 | 20 | $M_{1}$ | $.1899+.0048$ | ． 1947 |
| 5 | 20 | $L_{\text {II }}$ | $.0255+.0185$ | ． 0440 | 37 | 60 | $K$ | $.1501+.1035$ | ． 2536 |
| 8 | 25 | $L_{\text {III }}$ | $.0281+.0154$ | ． 0435 | 46 | 40 | $L_{1}$ | $.2348+.0192$ | ． 2540 |
| 16 | 10 | $M_{t}$ | $.0388+.0048$ | ． 0436 | 47 | 30 | $M_{t}$ | $.2488+.0048$ | ． 2536 |
| 14 | 40 | $L_{1}$ | $.0340+.0192$ | ． 0532 | 39 | 60 | $K$ | $.1796+.1035$ | ． 2831 |
| 19 | 20 | $M_{t}$ | $.0486+.0048$ | ． 0534 | 48 | 20 | $L_{1}$ | $.2618+.0192$ | ． 2810 |
| 17 | 90 | $L_{1}$ | $.0425+.0192$ | ． 0617 | 41 | 50 | K | ． $1976+.1035$ | ． 3011 |
| 20 | 70 | $M_{\text {t }}$ | $.0567+.0048$ | ． 0615 | 49 | 20 | $L_{I}$ | $.2800+.0192$ | ． 2992 |
| 21 | 50 | $N_{1}$ | $.0598+.0012$ | ． 0610 |  |  |  |  |  |

[^306]TABLE 745．－ANALYSIS OF BETA．RAY SPECTRUM OF MESOTHORIUM 2 （ACTINIUM 228）＊

| 点单 |  | $\begin{aligned} & \underline{E} \\ & \stackrel{y}{E x} \\ & \hline 0 \end{aligned}$ | Energy of $\beta$－ray line + absorption nergy Mey Mev | $\begin{gathered} \text { Energy } \\ \text { of } \begin{array}{c} \text {-ray } \\ \text { Mev } \end{array} \end{gathered}$ |  |  |  | $\begin{gathered} \text { Energy of } \beta \text {-ray } \\ \text { line + absorption } \\ \text { energy } \\ \text { Mev } \end{gathered}$ $\mathrm{Mev}$ | $\begin{gathered} \text { Energy } \\ \text { of } \begin{array}{c} \text { orgay } \\ \text { Mev } \end{array} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 100 | $L_{1}$ | $.0381+.0204$ | ． 0585 | 18 | 6 | $M_{1}$ | $.1782+.0052$ | ． 1834 |
| 2 | 85 | $L_{H I}$ | $.0416+.0162$ | ． 0578 | 16 | 18 | K | $.1406+.1092$ | ． 2498 |
| 3 | 65 | $M_{1}$ | $.0523+.0052$ | ． 0584 | 20 | 8 | $L_{1}$ | $.2291+.0204$ | ． 2495 |
| 4 | 45 | $N_{\text {I }}$ | $.0566+.0012$ | ． 0579 | 19 | 16 | K | ． $2099+.1092$ | ． 319 |
| 5 | 6 | $L_{1}$ | $.0593+.0204$ | ． 0797 | 21 | 6 | $L_{I}$ | $.299+.0204$ | ． 319 |
| 6 | 4 | $L_{\text {HII }}$ | $.0631+.0162$ | ． 0793 | 22 | 2 | $N_{t}$ | $.318+.001$ | ． 319 |
| The $M$ and $N$ lines would be masked exactly by the intense lines 8 and 9 ． |  |  |  |  | $\begin{array}{r}23 \\ 24 \\ \hline\end{array}$ | 8 | $K$ <br> $L_{I}$ | ． $352+.109$ | ． 461 |
|  |  |  |  |  | 25 | 2 | $M_{\text {I }}$ | $.458+.005$ | ． 463 |
| 12 | 25 | $L_{\text {III }}$ | ． $1129+.0162$ | ． 1291 | 26 | 6 | K | $.804+.109$ | ． 913 |
| 13 | 22 | $M_{1}$ | ． $1245+.0052$ | ． 1297 | 28 | 3 | $L_{K}$ | ． $897+.020$ | ． 917 |
| 14 | 6 | $N_{t}$ | $.1279+.0013$ | ． 1292 | 27 | 3 | K | ． $8619+.109$ | ． 970 |
| 8 | 50 | K | ． $0749+.1092$ | ． 1841 | 29 | 2 | $L_{t}$ | ． $949+.020$ | ． 969 |
| 17 | 20 | $L_{1}$ | $.1644+.0204$ | ． 1848 |  |  |  |  |  |

＊For reference，see footnote 233，p． 679.

TABLE 746．－ANALYSIS OF THE BETA．RAY SPECTRUM OF PROTACTINIUM＊

|  |  | 品 | $\begin{aligned} & \text { Energy of } \beta \text {-ray } \\ & \text { line + alsorption } \\ & \text { energy } \\ & \text { Mev } \end{aligned}$ | $\underset{\substack{\text { Energy } \\ \text { of } \begin{array}{c} \text { Mev } \\ \text { Mev } \end{array}}}{ }$ |  |  |  | $\begin{aligned} & \text { Energy of } \beta \text {-ray } \\ & \text { line + absorption } \end{aligned}$ $\begin{aligned} & \text { energy } \\ & \text { Mev } \end{aligned}$ | $\begin{gathered} \text { Energy } \\ \text { of } \begin{array}{c} \text { ray } \end{array} \\ \text { Mev } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 60 | $L_{1}$ | ． $0753+.0198$ | ． 0951 | 10 | 30 | $M_{\text {I }}$ | $.2869+.0050$ | ． 2919 |
| 2 | 40 | $L_{\text {III }}$ | $.0788+.0158$ | ． 0946 | 6 | 70 | $K$ | $.2194+.1064$ | ． 3258 |
| 3 | 40 | $M_{1}$ | $.0905+.0050$ | ． 0950 | 11 | 40 | $L_{\text {r }}$ | $.3016+.0198$ | ． 3214 |
| 5 | 100 | K | $.1896+.1064$ | ． 2960 | 12 | 20 | $M_{1}$ | $.3182+.0050$ | ． 3232 |
| 9 | 60 | $L_{1}$ | ． $2746+.0198$ | ． 2944 |  |  |  |  |  |

[^307]TABLE 747.-GAMMA-RAY ENERGY OF SOME HEAVY ISOTOPES, NATURAL AND ARTIFICIAL


* Natural radioactive source.


## TABLE 748.-THE GAMMA-RAY SPECTRUM OF ThC" *

These differences of energies, or velocities, of the $a$-ray from thorium $C$ are sometimes explained on the encrgy-level basis of the nucleus. The agreement with the energies of the $\gamma$-rays emitted from $\mathrm{ThC}^{\prime \prime}$, the daughter of ThC , and these apparent differences of disintegration energy of a-ray of ThC , given in the table show one agreement with this theory.


* For reference, see footnote 225, p. 666.

TABLE 749.-DANGER RANGES FOR PERSONS WHO ARE WORKING WITH RADIUM, FOR DIFFERENT AMOUNTS OF RADIUM, PROVIDING THE RADIUM IS ENCLOSED IN NOT LESS THAN 1 mm LEAD OR ITS EQUIVALENT

| Amount of radium element milligrams | Daily exposure (in hours) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 4 | 8 | 16 |
|  | Danger range (in meters) |  |  |  |  |
| 100 | . 9 | 1.3 | 1.8 | 2.5 | 3.6 |
| 200 | 1.3 | 1.8 | 2.6 | 3.6 | 5.1 |
| 400 | 1.8 | 2.5 | 3.5 | 5 | 7.1 |
| 1000 | 2.9 | 4 | 5.7 | 8 | 11.3 |

TABLE 750.-GAMMA-RAY ENERGY OF SOME ARTIFICIAL RADIOACTIVE ISOTOPES OF LOW ATOMIC WEIGHT

| $\begin{aligned} & \text { Atomic } \\ & \text { No. } \end{aligned}$ | Element | Isotope | $\begin{gathered} \gamma-\text { ray } \\ \text { enery } \\ \text { Mev } \end{gathered}$ | $\begin{aligned} & \text { Atomic } \\ & \text { No. } \end{aligned}$ | Elenient | Isotope | $\begin{gathered} \gamma \cdot \mathrm{ray} \\ \text { eneryy } \\ \text { Mev } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | Beryllium | 7 | . 49 | 40 | Zirconium | 95 | . 73 |
| 7 | Nitrogen | 15 | 6.7 | 41 | Niobium | 92 | 1.0 |
| 8 | Oxygen | 14 | 2.3 |  |  | 96 | 1.0 |
|  |  | 19 | 1.6 | 42 | Molybdenum | 93 | 1.6 |
| 11 | Sodium | 20 | 2.2 | 43 | Technetium | 92,93 | 2.4 |
|  |  | 22 | 1.3 | 45 | Rhodium | 100 | 1.2 |
|  |  | 24 | 1.38 |  |  | 106 | 1.25 |
| 12 | Magnesium | 27 | 1.0 | 47 | Silver | 110 | 1.40 |
| 13 | Sulfur | 28 | 1.80 | 48 | Cadmium | 107 | . 84 |
| 16 |  | 37 | 2.6 | 49 | Indium | 116 | 2.32 |
| 17 | Chlorine | 34 | 3.4 | 50 | Tin | 126 | 1.2 |
|  |  | 38 | 1.60 | 51 | Antimony | 118 | 1.5 |
| 1819 | Argon <br> Potassium * | 41 | 1.37 |  |  | 124 | 2.04 |
|  |  | 38 | 2.15 | 52 | Tellurium | 119 | 1.4 |
|  |  | 40 | 1.54 | 53 | Iodine | 135 | 1.6 |
|  |  | 42 | 1.4 |  |  | 136 | 2.9 |
| 20 | Calcium | 47 | 1.3 | 54 | Xenon | 127 | . 9 |
|  |  | 48 | . 8 | 55 | Cesium | 136 | 1.2 |
| 21 | Scandium | 43 | 1.65 |  |  | 138 | 1.2 |
|  |  | 44 | 1.33 | 56 | Barium | 140 | . 53 |
|  |  | 48 | 1.3 | 57 | Lanthanum | 140 | 1.63 |
| 222325 | Titanium | 51 | 1.0 | 58 | Cerium | 139 | 1.8 |
|  | Vanadium | 52 | 1.46 | 59 | Praseodymium | 142 | 1.9 |
|  | Manganese | 52 m | 1.46 |  |  | 146 | 1.4 |
|  |  | 56 | 2.06 | 61 | Promethium | 143 | . 67 |
| 26 | Iron | 59 | 1.10 | 63 | Europium | 156 | 2.0 |
| 27 | Cobalt | 60 | 1.16 | 65 | Terbium | 154 | 1.4 |
|  |  | 62 | 1.3 | 67 | Holmium | 162 | 1.1 |
| 28 | Nickel Copper | 65 | 1.1 | 69 | Thulium | 166 | 1.5 |
|  |  | 60 | 1.5 | 71 | Lutetium | 170 | 1.5 |
|  |  | 64 | 1.35 | 72 | Hafnium | 175 | 1.5 |
|  |  | 66 | 1.32 | 73 | Tantalum | 176 | 1.7 |
| 30 |  | 65 | 1.11 |  |  | 182 | 1.2 |
| 32 | Germanium | 75 | 1.1 | 75 | Rhenium | 182 | 1.5 |
|  | Arsenic | 72 | 2.4 | 76 | Osmium | 193 | 1.58 |
| 33 | Bromine | 76 | 2.0 | 77 | Iridium | 194 | 1.35 |
|  |  | 82 | 1.35 | 78 | Platinum | 193 | 1.5 |
| 37 | Rubidium | 81 | . 8 | 79 | Gold | 192 | 2.3 |
|  |  | 82 | 1.0 | 81 | Thallium | 198 | 1.3 |
|  |  | 86 | 1.08 | 82 | Lead | 204 m | 1.1 |
| 3839 | Strontium Yttrium | 91 | 1.3 | 83 | Bismuth | 206 | . 74 |
|  |  | $\begin{aligned} & 88 \\ & 93 \end{aligned}$ | $2.76$ |  |  |  |  |

* Natural radioactive source.

TABLE 751.-TOTAL MASS ABSORPTION COEFFICIENT, $\mu / \rho$, FOR $\gamma$-RAYS IN VARIOUS ELEMENTS (IN CM ${ }^{2} / \mathrm{G}$ )

| Wavelength |  |  |  |  | Cu |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A | C | Cr | Ag | Pb |  |
| .1 | .15 | .16 | .36 | 1.4 | 3.8 |
| .2 | .16 | .28 | 1.5 | 5.6 | 4.9 |
| .3 | .19 | .47 | 4.3 | 17. | 14. |
| .4 | .35 | 2.1 | 9.8 | 38. | 31. |
| .5 |  | 19. | 71. | 54. |  |

TABLE 752.-GAMMA SPECTRUM FOR SOME RADIOACTIVE BREAKDOWNS *


[^308](continued)

TABLE 752.-GAMMA SPECTRUM FOR SOME RADIOACTIVE BREAKDOWNS (concluded)
$\gamma$-rays ${ }^{295}$ from $82 \underset{(\operatorname{RaD})}{\text { Lead }} 210 \rightarrow 83 \underset{(\mathrm{RaE})}{\text { Bismuth }} 210$

| $\gamma$-ray line | $E$ (kev) | $\boldsymbol{\gamma}$-ray line | $E$ (kev) |
| :---: | :--- | :---: | :---: |
| $(X)$ | $65 \pm 5.1$ | $D$ | $32 . \pm 1$ |
| $A$ | $46.7 \pm .1$ | $E$ | $23.2 \pm .6$ |
| $B$ | $43 \pm 1$ | $F$ | $7.3 \pm .7$ |

${ }^{235}$ San Tsiang Tsien, Phys. Rev., vol. 69, p. 38, 1946.

# TABLE 753.-THE ENERGY RADIATED BY A NUMBER OF RADIOACTIVE MATERIALS * 

| Material | Half-life | Radiation | Energy of radiation in Mev |  | DisintegrationsNo $\mathrm{g}^{-1} \mathrm{sec}^{-1}$ | Radiation Mev $\mathrm{g}^{-1} \mathrm{sec}^{-1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $a$ or $\beta$ | $\boldsymbol{\gamma}$ |  |  |
| 92 Uranium 238 | $4.5 \times 10^{\circ} \mathrm{yr}$ | $a$ | 4.2 | . | $1.23 \times 10^{4}$ | $5.2 \times 10^{4}$ |
| 90 Thorium 232 | $1.39 \times 10^{10} \mathrm{yr}$ | $a$ | 4.1 |  | $4.1 \times 10^{3}$ | $1.70 \times 10^{4}$ |
| 88 Radium 226 | 1620 yr | $a \gamma$ | 4.79 | . 19 | $3.6 \times 10^{10}$ | $1.80 \times 10^{12}$ |
| 86 Radon 222 | 3.825 d | $a$ | 5.486 |  | $5.7 \times 10^{18}$ | $3.1 \times 10^{18}$ |
| 86 Radon 220 | 54.5 sec | a | 6.282 | . | $3.5 \times 10^{19}$ | $2.2 \times 10^{20}$ |
| $86 \begin{gathered}\text { Radon } 219 \\ \text { (Actinon) }\end{gathered}$ | 3.92 sec | $a$ | 6.824 |  | $4.8 \times 10^{20}$ | $3.3 \times 10^{21}$ |
| 86 Radon 217 | $10^{-3} \mathrm{sec}$ | $a$ | 7.74 | . | $1.93 \times 10^{24}$ | $1.50 \times 10^{28}$ |
| $84 \begin{gathered}\text { Polonium } 214 \\ \text { (Radium C') }\end{gathered}$ | $1.5 \times 10^{-6} \mathrm{sec}$ | a | 7.680 | . | $1.30 \times 10^{25}$ | $1.0 \times 10^{28}$ |
| 84 Polonium 212 <br> (Thorium C') | $3.1 \times 10^{-7} \mathrm{sec}$ | $a$ | 8.776 |  | $6.4 \times 10^{27}$ | $5.6 \times 10^{28}$ |
| 84 Polonium 211 <br> (Actinium $\mathrm{C}^{\prime}$ ) | $5 \times 10^{-8} \mathrm{sec}$ | $a$ | 7.434 |  | $3.9 \times 10^{23}$ | $2.9 \times 10^{24}$ |
| 84 Polonium 210 | 138 d | $a \gamma$ | 5.3 | . 77 | $1.57 \times 10^{15}$ | $1.2 \times 10^{18}$ |
| 83 Bismuth 214 | $19.7 \mathrm{~min}$ | a ${ }^{\text {r }}$ | 5.5 | 1.8 | $1.65 \times 10^{18}$ |  |
| 81 Thallium 210 (Radium C") | 1.32 min | $\beta^{-}$ | 1.8 | . | $2.51 \times 10^{10}$ | $4.5 \times 10^{10}$ |
| 81 Thallium 208 (Thorium C") | 3.1 min | $\beta^{-} \gamma$ | 1.7 | 2.6 | $1.08 \times 10^{19}$ | $4.7 \times 10^{10}$ |
| 81 Thallium 207 <br> (Actinium C") | 4.76 min | $\beta^{-\gamma}$ | 1.47 | . | $7.1 \times 10^{18}$ | $1.04 \times 10^{19}$ |
| 59 Praseodymium 142 | 19.3 hr | $\beta^{-\gamma}$ | 2.1 | 1.9 | $4.28 \times 10^{17}$ | $8 \times 10^{17}$ |
| 53 Iodine 136 | 1.8 min | $\beta^{-} \gamma$ | 6.5 | 2.9 | $2.85 \times 10^{20}$ | $8 \times 10^{20}$ |
| 19 Potassium 40 ** | $1.8 \times 10^{\circ} \mathrm{yr}$ | $\beta^{-} \gamma$ | 1.9 | 1.54 | $1.84 \times 10^{5}$ | $3.9 \times 10^{5}$ |

[^309] thorium, in part due to its greater number of atoms per gram.

TABLE 754.-SAFE WORKING DISTANCES FOR DIFFERENT EXPOSURE
TIMES TO DIFFERENT AMOUNTS OF RADIUM

| Daily exposure <br> milligram-hr | Safe distance <br> meters | Daily exposure <br> milligram-hr | Safe distance <br> meters |
| :---: | :---: | :---: | :---: |
| 100 | 1 | 800 | $2 \frac{1}{2}$ |
| 200 | $1 \frac{1}{2}$ | 1600 | $3 \frac{1}{2}$ |
| 400 | 2 | 3200 | 5 |

## TABLE 755.-COMBINATION OF LEAD SHIELD THICKNESS AND DISTANCE FOR ADEQUATE PROTECTION FOR EXPOSURES TO DIFFERENT AMOUNTS OF RADIUM, NOT EXCEEDING 8 HOURS PER DAY

Workers with radioactive materials must observe certain precautions to avoid being burned by the emitted radiations. Tables 749, 751, 754, 755, taken from the National Bureau of Standards Handbook H 23 on Radium Protection, give some of the necessary precautions. These precautions are for radium; if some other radioactive product is being worked with, care must be taken to increase these precautions if the materials are more active than radium. See Table 732.

The $\alpha$-rays are much more easily stopped than the $\beta$ - or $\gamma$-rays. The most energetic a-rays are stopped by an ordinary sheet of paper or a sheet of aluminum .06 mm thick. The $\beta$-rays are stopped by a few millimeters of aluminum, while many of the $\gamma$-rays will penetrate a block of lead a number of inches thick.

| Amount of radium milligrams | Thickness of lead cm | Distance | Amount of radium milligrams | Thickness of lead cm | $\begin{aligned} & \text { Distance } \\ & \text { cm } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 10.100. | . 5 | . 70 | 1000. | 1 | . 570 |
|  | 1 |  |  | 3 | 340 |
|  | 2 | . 45 |  | 6 | 160 |
|  | 1 | . 185 | 5000. | . 4 | . 550 |
|  | 2 | . 140 |  | 6 | 160 |
|  | 3 | . . 105 |  | 10 | 220 |

## TABLE 756.-CONSTANTS FOR CATHODE-RAY SPEEDS IN MATTER

Cathode rays whose direction of motion is perpendicular to the direction of a uniform magnetic field $(H)$ describe a circular path of radius ( $r$ ) according to the formula corrected for relativity change of mass of electron.

$$
H r=1704\left[\beta\left(1-\beta^{2}\right)^{-1 / 2}\right]
$$

where $H$ is expressed in gauss and $r$ in cm .
When cathode rays impinge on matter they are deflected from their original direction of motion. These deflections grade all the way from $180^{\circ}$ "reflections" to the "diffusion" corresponding to deflections through very small angles. The large-angle deflections are ordinarily comparatively infrequent. However, when the substance struck by the cathode rays is crystalline, certain directions may be preferred by the deflections. Here the beam of cathode rays behaves as though it consisted of a train of waves of wavelength $\lambda_{e}=0.02426 / \beta$, where $\lambda_{e}$ is in angstroms. The preferred directions for the "reflected" cathode-ray beams may be calculated from the Bragg formula (see Siegbahn's "X-ray Spectroscopy"). The simple Bragg formula is quite limited in application here, however, since refraction in the crystal is very appreciable for the cathode-ray beams. In general, the cathode rays which have been deflected bv matter will have lost speed, but the rays which have undergone these "preferred" deflections remain of the same speed as the primary cathode beam.

Cathode rays lose speed on penetrating matter. The losses of speed by individual cathode particles grade from complete stoppage to no loss of speed. The maiority of the cathode particles, however, lose speed according to the relation (Thomas-WhiddingtonBohr law)

$$
\beta_{0}{ }^{4}-\beta^{4}=a x
$$

where $\beta_{0}$ is the initial speed, and $\beta$ the speed after traversing a path length $x$ in the material ( $x$ to be measured in cm along the actual curved path), and $a$ is a constant roughly equal to $6.5 \rho$ where $\rho$ is the density of the material in $\mathrm{g} / \mathrm{cm}^{3}$. A convenient form for the expression is the following. Note that the two forms are not equivalent except at very low speeds (experiment has not yet decided between the two) :

$$
V_{0}{ }^{2}-V^{2}=b x
$$

where $V_{0}$ and $V$ are the initial and final "equivalent voltages" (see above) of the cathode rays, in kv, and $b$ is a constant roughly equal to $40 \times 10^{\prime} \rho$. A tabulation of experimental values of $a$ and $b$ for various materials follows:


TABLE 757.-ENERGY IN CALORIES/HR DEVELOPED BY ONE GRAM OF RADIUM IN EQUILIBRIUM WITH ITS PRODUCTS*


Total energy radiated ( $a, \beta^{-}, \gamma$ in Mev $)=144.46 \times 10^{10}=199 \mathrm{cal} / \mathrm{hr}$.
The total heating effect developed by one gram of radium in equilibrium with its products in $199 \mathrm{cal} / \mathrm{hr}$.

[^310]
## TABLE 758.-CATHODE RAYS

Owing to the growth of the subject, electrons are treated under three separate headings; cathode rays, the swiftly moving electrons from the cathode in a discharge tube ; beta rays, from radioactive breakdown; and the general field, electrons. The velocity of the cathode rays (electrons) depends upon the applied voltage. At comparatively low pressures the cathode rays have a nearly uniform velocity. Free electrons are emitted from hot bodies (Table 683-689), especially if the heated substance is coated with barium, calcium, or strontium oxide (Wehnelt cathode). These electrons can be given any desired speed, always less than that of light, if the heated substance (usually in the form of a wire) be enclosed in an evacuated tube and the difference of potential $(V)$ applied between the wire (cathode) and another electrode (anode, anticathode, or target). The speed of the electron and also its kinetic energy is often designated by giving the applied voltage, i.e., a 10 kv electron has a speed of 10 kv , about .2 that of light, and an energy of $10,000 \mathrm{ev}$, or $1.602 \times 10^{-8}$ ergs. (See Table 713.) The speed ( $v$ ) of the cathode rays, expressed as a fractional part $(\beta)$ of the speed of light $(\beta=v / c$, where $c$ is the speed of light), when they have fallen through the entire potential difference, is given by the formula (which is corrected for the relativity change of mass)

$$
V=510.8\left[\left(1-\beta^{2}\right)^{-1 / 2}-1\right]
$$

where $V$ is in kilovolts.
A tabulation of the corresponding values of $V$ (kilovolts) and $\beta$ follows.

| $\beta$ | $V(\mathrm{kv})$ | $\beta$ | $V(\mathrm{kv})$ | $\beta$ | $V(\mathrm{kv})$ |
| :--- | :---: | :--- | :---: | :--- | ---: |
| .01 | .0255 | .40 | 46.5 | .90 | 661. |
| .02 | .1022 | .50 | 79.0 | .942 | 1000. |
| .05 | .639 | .548 | 100 | .95 | 1085. |
| .10 | 2.574 | .80 | 127.7 | .98 | 2045. |
| .20 | 10.53 |  | 80 | 340.4 |  |

X-rays, which are short wavelength (. $06-1020 \mathrm{~A}$ ) radiant energy, are, in general, generated whenever swiftly moving electrons are suddenly stopped by striking any material substance. The electrons may come from a cold cathode (gas-filled tube) and the current increased by ionization of the gas in the tube, or they may come from a hot cathode (Coolidge tube) in a tube of very low gas pressure. Soft and hard X-rays are terms applied to X-rays produced by low or high applied voltage respectively.

Two types of X-rays are generated when the electrons hit the target-continuous spectrum (over a limited wavelength) and the radiation that is characteristic of the material of which the anode is made. The continuous X-ray spectrum has a very definite short-wave limit that depends upon the voltage applied to the tube. Thus

$$
V_{0} e=h \nu_{0}=h c / \lambda_{0}
$$

If $V_{0}$ is given in volts, this wavelength $\lambda_{0}$ will be in angstroms if the other units are properly chosen.

$$
\lambda_{0}(\text { in } A)=\frac{12395}{V_{0}}
$$

The characteristic spectra are designated $K, L, M, N, O$, etc., where these letters refer to the various electron shells (Table 658).
X-rays, like any type of radiant energy, have two characteristics ; intensity (i.e., the rate of energy transfer), and wavelength. These two quantities are connected thus: the energy $E=h \nu=h c / \lambda$.
This, of course, assumes monochromatic radiation or the energy for a narrow wavelength interval, which is not always the case ; all electrons do not hit the anode with the same energy nor do all materials react alike to electron bombardment. Some of the characteristics of X-rays and the reaction of X -rays to various materials are given in the following tables.

TABLE 759.—X-RAY PRODUCTION ${ }^{283}$
Quantity of X-rays emitted by a tungsten-target tube per kilowatt of energy in cathode-ray beam.**

| Operating <br> potential <br> kilovolts | Power in total <br> X-rays from <br> focal spot <br> watts | Effective <br> wavelenghth <br> (unfiltered | Roentgens ( $r$ ) <br> per second at <br> meter from <br> target |
| :---: | :---: | :---: | :---: |
| 50 | 2.5 | .56 | units <br> (unfiltered) |
| 70 | 3.5 | .40 | 1.2 |
| 100 | 5. | .28 | .62 |
| 200 | 10. | .14 | .34 |
| 500 | 25. | .056 | .39 |
| 1000 | 48. | .028 | 1.1 |
| 2000 | 95. | .014 | 2.1 |

\footnotetext{
${ }^{238}$ Clark, George L., Applied X-rays, McGraw-Hill Book Company, Inc., 1940. Used by permission of the publishers.

* Compiled by A. H. Compton.

TABLE 760.-CRITICAL ABSORPTION WAVELENGTHS (A), K SERIES*

| 12 Mg | 9.5112 | 35 Br | . 9182 | 74 W | . 17807 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 13 Al | 7.9470 | 40 Zr | . 6874 | 78 Pt | . 1581 |
| 17 Cl | 4.3938 | 42 Mo | . 61842 | 79 Au | . 1534 |
| 24 Cr | 2.0663 | 47 Ag | . 4852 | 82 Pb | . 1410 |
| 26 Fe | 1.7405 | 53 I | . 3738 | 92 U | . 1075 |
| 29 Cu | 1.3780 | 56 Ba | . 3308 |  |  |

[^311]TABLE 761.-RELATIVE IONIZATION PRODUCED IN VARIOUS GASES BY HETEROGENEOUS X-RAYS*

| Gas or vapor | Density relative to air $=1$ | Ionization relative to air $=1$ |  |
| :---: | :---: | :---: | :---: |
|  |  | Soft X-rays | Hard X-rays |
| Hydrogen, $\mathrm{H}_{2}$ | . 07 | . 01 | . 18 |
| Carbon dioxide, $\mathrm{CO}_{2}$ | . 1.53 | 1.57 | 1.49 |
| Ethyl chloride, $\mathrm{C}_{2} \mathrm{H}_{6} \mathrm{Cl}$ | . 2.24 | 18.0 | 17.3 |
| Carbon tetrachloride, $\mathrm{CCl}_{4}$ | . 5.35 | 67 | 71 |
| Nickel carbonyl, $\mathrm{Ni}(\mathrm{CO})$ | . 5.90 | 89 | 97 |
| Ethyl bromide, $\mathrm{C}_{2} \mathrm{H}_{5} \mathrm{Br} .$. | . 3.78 | 72 | 118 |
| Methyl iodide, $\mathrm{CH}_{3} \mathrm{I}$. | . 4.96 | 145 | 125 |
| Mercury methyl, $\mathrm{Hg}\left(\mathrm{CR}_{3}\right)_{2}$. | . 7.93 | 425 | ... |

* For refcrence, see foot note 236, p. 692.


# TABLE 762.-WAVELENGTHS OF FLUORESCENT RADIATION EXCITED BY X-RAYS * 

| Material | Region | $\underset{A}{\text { of } \underset{\text { Pasition }}{\text { maximum }}}$ |
| :---: | :---: | :---: |
| Fluorspar | 3640-2400 | 2840 |
| Fluorspar and iron spar. | 3900-2310 | 2800 |
| Scheelite (Ca tungstate). | 4800-3750 | 4330 |
| Zinc sulfide | 5090-4120 | 4500 |
| K platinocyanide | 4900-4120 | 4500 |
| Ba platinocyanide | 5090-4420 | 4800 |
| Ca platinocyanide | 5090-4550 | 4800 |
| U NH، fluoride. | 4400-3800 | 4100 |
| X-ray tube glass | 5090-3000 | 3750 |

[^312]
## TABLE 763.-THE ABSORPTION OF X-RAYS

The absorption of X -rays by materials follows the same law as the absorption of radiant energy, i.e.,

$$
I=I_{0} \times e^{-\mu x}
$$

where $I_{0}$ is the initial intensity and $I$ the intensity after a distance $x$, and $\mu$ the absorption coefficient. $\mu / \rho$ is the mass absorption ( $\rho$ density) of the material. $\mu / \rho$ is really the sum of two coefficients- $\tau / \rho$ the true or fluorescent X-ray mass-absorption coefficient-and $\sigma / \rho$ the mass-absorption due to scattering. For light elements $\sigma / \rho$ has a practically constant value of 0.17 independent of the wavelength for intermediate ranges.
The following relations may be written

$$
\mu / \rho=\tau / \rho+\sigma / \rho=K \lambda^{8}+\sigma / \rho
$$

The constants for this absorption equation for several materials follow: *

|  | Mo 42 | Ag 47 | Sn 50 | W 74 | Au 79 | Pb 82 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| $K_{K}$ | 375 | 545 | 595 | 1870 | 2230 | 2570 |
| $K_{L}$ | 50 | 70 | 90 | 330 | 395 | 476 |
| $K_{K} / K_{L}$ | 7.5 | 7.8 | 6.6 | 5.65 | 5.65 | 5.40 |
| $\tau A\left(10^{-21}\right)$ | 13.3 | 11.0 | 8.90 | 3.19 | 2.57 | 2.37 |

* For reference, see footnote 236, p. 692.

TABLE 764.-APPROXIMATE LEAD THICKNESS REQUIRED TO REDUCE RADIATION DOSAGE RATE TO 5 PERCENT OF USEFUL BEAM ${ }^{237}$

| Kilovolts _........... | 50 | 75 | 100 | 150 | 200 | 250 | 400 | 500 | 1000 | 2000 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Lead thickness, mm..... | .1 | .3 | .4 | .7 | 1.0 | 1.3 | 3.0 | 7 | 32 | 50 |

[^313] MATERIALS FOR DIFFERENT WAVELENGTHS *

| Wavelength <br> angstroms | C | Al | Cu | Sn |
| :---: | :---: | :---: | :---: | :---: |
| .010 |  |  |  |  |

*For reference, see footnote 236, ก. 692.

TABLE 766.-EXPONENTIAL FORMULAE FOR THE TOTAL MASS-ABSORP. TION VALUES, $\mu / \rho$, FOR SEVERAL ELEMENTS*

| Absorber | $\lambda(A)$ | $\mu / \rho$ | Absorber | $\lambda(A)$ | $\mu / \rho$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Al | . 1 to . 4 | $14.45 \times \lambda^{3}+.15$ | Mo | . 1 to . 35 | $450 \times \lambda^{3}+.4$ |
| A1 | .4 to . 7 | $14.30 \times \lambda^{3}+.16$ | Mn | $>\lambda_{\kappa_{\mathrm{abs}}}$ | $51.5 \times \lambda^{3}+1.0$ |
| Fe | .1 to . 3 | $110 \times \lambda^{3}+.18$ | Ag | . 1 to . 4 | $603 \times \lambda^{3}+.7$ |
| Co. | .1 to . 3 | $124 \times \lambda^{3}+.18$ | Ag | $>\lambda_{K_{\text {atix }}}$ | $86 \times \lambda^{3}+.6$ |
| $\stackrel{\mathrm{Ni}}{\mathrm{Cu}}$. | . 1 to 1 to .6 | $145 \times \lambda^{3}+.20$ | Pb | $>\lambda_{K_{\text {abs }}}$ | $510 \times \lambda^{3}+.75$ |

* For reference, see footnote 236, p. 692.


## TABLE 766A.-X-RAY DOSAGE UNITS

The international unit of quantity or dose of X-rays (and gamma-rays), one roentgen, $r$, is obtained from that X-ray (or gamma-ray) energy which, when the secondary electrons are fully utilized and secondary radiation from the walls of the chamber avoided, under standard conditions $0^{\circ} \mathrm{C}$ and 760 mmHg , produces in a cubic centimeter of atmospheric air such a degree of conductivity that thé quantity of electricity, measured at saturation, equals 1 esu.

## TABLE 767.-PROTECTIVE POWERS OF MATERIALS RELATIVE TO LEAD*

A lead screen is very effective in protecting against X -rays. The data in the table show the thickness of lead is as effective as 1 mm of certain other materials that are in common use for protection against X-rays generated by a 100,000 -volt Coolidge tube.

| Lead glass | . 12 to . 20 | Wood |  |
| :---: | :---: | :---: | :---: |
| Lead rubber | . 25 to . 45 | Barium | . 05 |
| Bricks and | . 01 |  |  |

[^314]TABLE 768.-THE MINIMUM THICKNESS OF LEAD RECOMMENDED FOR PROTECTION FOR VARIOUS INTENSITIES OF X-RAYS

| X-rays generated <br> by peak voltage <br> not in exess of <br> (kilovolts): | Minimum equivalent <br> thickness of lead <br> millimeters | X-rays generated <br> by peak voltage <br> not in excess of <br> (kilovolts) | Minimum equivalent <br> thickness of lead <br> millimeters |
| :---: | :---: | :---: | :---: |
| 75 | 1.0 | 225 | 5.0 |
| 100 | 1.5 | 300 | 9.0 |
| 125 | 2.0 | 400 | 15.0 |
| 150 | 2.5 | 500 | 22.0 |
| 175 | 3.0 | 600 | 34.0 |
| 200 | 4.0 |  |  |

The National Bureau of Standards Handbook 41 on X-ray protection gives as the permissible dosage rate $0.3 r$ per week. On the basis of a 48 -hour week of uniform exposure the permissible dosage rate is $0.00625 r$ per hr ( 6.25 mr per hr ).
This booklet also gives safety rules for operating X-ray equipment and the thickness of lead or concrete necessary for protection against X -ray tubes operated at various intensities.

TABLE 769.-DISTANCE PROTECTION*

| Distance $\dagger$ for various applied voltages (kilovolts) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Target current | 50 | 75 | 100 | 150 | 200 | 250 | 400 | 500 | 1000 | 2000 |
| ma |  |  |  |  | feet |  |  |  |  |  |
| . 005 | 15 | 20 | 20 | 25 | 25 | 25 | 25 | 30 | 90 | 195 |
| . 05 | 40 | 50 | 60 | 60 | 65 | 70 | 70 | 75 | 220 | 400 |
| . 5 | 85 | 115 | 145 | 145 | 165 | 170 | 170 | 200 | 460 | 850 |
| 2.5 | 120 | 185 | 235 | 245 | 270 | 285 | 295 | 340 | 690 | . . . |
| 10 | 160 | 250 | 330 | 350 | 390 | 420 |  |  | ... | ... |
| 25 | 195 | 300 | 390 | 420 | 480 | 510 |  |  |  |  |

* For reference, see footnote 237, p. 693.
$\dagger$ These distances were computed by taking into account distance and air absorption. The air absorption was determined by assuming the radiation was monochromatic and of double the minimum wavelength of the polychromatic radiation given off by the tube at the indicated potential.


## TABLE 770.-PRIMARY PROTECTIVE-BARRIER REQUIREMENTS FOR 10 MILLIAMPERES AT THE PULSATING POTENTIALS* AND DISTANCES INDICATED $\dagger$

|  | Lead thickness with peak kilovolts of - |  |  |  |  | Target distance | Lead thickness with peak kilovolts of 一 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Target distanc | 75 | 100 | 150 | 200 | 250 |  | 75 | 100 | 150 | 200 | 250 |
| $f t$ |  |  | mm |  |  |  |  |  | mm |  |  |
| 2 ( .61 m ) | 2.2 | 3.4 | 4.3 | 6.7 | 11.8 | 20 ( 6.1 m ) | 1.0 | 1.7 | 2.4 | 3.6 | 6.4 |
| 5 ( 1.52 m ) | 1.7 | 2.7 | 3.6 | 5.5 | 9.6 | $50(15.2 \mathrm{~m})$ | . 5 | 1.1 | 1.7 | 2.4 | 4.3 |
| 10 ( 3.05 m ) | 1.3 | 2.2 | 3.0 | 4.5 | 8.1 |  |  |  |  |  |  |

[^315]TABLE 771.-PRIMARY PROTECTIVE-BARRIER REQUIREMENTS FOR 400-KILOVOLTS PEAK PULSATING POTENTIAL WITH REFLECTION TARGET*

| Target distance ft | Lead thickness with target current of 一 |  |  | Target distance ft | Lead thickness with target current of - |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 ma | 3 ma <br> mm | 5 ma |  | 1 ma | $\begin{aligned} & 3 \mathrm{ma} \\ & \mathrm{~mm} \end{aligned}$ | 5 ma |
| 5 ( 1.52 m ) | 16.5 | 20 | 22 | $20(6.1 \mathrm{~m})$ | 9.5 | 11.5 | 13.0 |
| 10 ( 3.05 m ) | 12.5 | 15.5 | 17.0 | $50(15.2 \mathrm{~m})$ | 5.5 | 8.0 | 9.0 |

* For reference, see footnote 237 , p. 693.

TABLE 772.-PRIMARY PROTECTIVE-BARRIER REQUIREMENTS FOR 1000-KILOVOLT CONSTANT POTENTIAL WITH TRANSMISSION TARGET *

| Target distance ft | Barrier thicknesses with target current of- |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 ma |  | 2 ma |  | 3 ma |  |
|  | Lead mm | Concrete $\dagger$ in. | Lead mm | Concrete in. | Lead mm | Concrete in. |
| 5 ( 1.52 m ) | 123 | 30.5 | 131 | 32.5 | 136 | 33.5 |
| 10 ( 3.05 m ) | 107 | 27.0 | 115 | 28.5 | 120 | 29.5 |
| 20 ( 6.1 m ) | 91 | 23.0 | 99 | 25.0 | 103 | 26.0 |
| $100(30.5 \mathrm{~m})$ | 53 | 15.0 | 61 | 17.0 | 66 | 18.0 |

* For reference, see footnote 237, p. 693.
$\dagger$ These concrete thicknesses are for a concrete density of 147 pounds per cubic foot.

TABLE 773.-FILTERS FOR OBTAINING MONOCHROMATIC X-RAYS *

| Target | Lowest approximate voltage for $K$ series kilovolts | $\lambda$ for K n doublet | Filter | Thickness, millimeters | $\mathrm{g} / \mathrm{cm}^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Chromium | 6 | 2.287 | Vanadium | . 0084 | . 0048 |
| Iron | 7 | 1.935 | Manganese | . 0075 | . 0055 |
| Copper | 9 | 1.539 | Nickel | . 0085 | . 0076 |
| Molybdenum | 20 | . 710 | Zirconium | . 037 | . 024 |
| Silver | 25 | . 560 | Palladium | . 03 | . 036 |

* For reference, see footnote 236, p. 692.

TABLE 774.—CRITICAL ABSORPTION WAVELENGTHS (A), L SERIES*

| Element | $\begin{gathered} L_{1} \\ \left(L_{11}\right) \end{gathered}$ | $\underset{\left(L_{21}\right)}{L_{11}}$ | $\stackrel{L_{111}}{\left(L_{22}\right)}$ | Element | $\begin{aligned} & L_{1} \\ & \left(L_{11}\right) \end{aligned}$ | $\underset{\left(L_{21}\right)}{L_{11}}$ | $\underset{\left(L_{22}\right)}{L_{111}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 47 Ag | 3.2474 | 3.5067 | 3.6908 | 78 Pt | . 8921 | . 9321 | 1.0709 |
| 53 I | 2.3839 | 2.5475 | 2.7139 | 82 Pb | . 7806 | . 8136 | . 9500 |
| 56 Ba | 2.0620 | 2.1993 | 2.3568 | 92 U | . 5687 | . 5920 | . 7216 |
| 74 W | 1.0205 | 1.0713 | 1.2116 |  |  |  |  |

* For reference, see footnote 236, p. 692.

TABLE 775.-CRITICAL ABSORPTION WAVELENGTHS (A), M SERIES *

| Element | $M_{\mathrm{I}}$ | $M_{\mathrm{II}}$ | $M_{\mathrm{III}}$ | $M_{\mathrm{IV}}$ | $M_{\mathrm{V}}$ | Element | $M_{\mathrm{I}}$ | $M_{\mathrm{II}}$ | $M_{\mathrm{III}}$ | $M_{\mathrm{IV}}$ | $M_{\mathrm{V}}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| W | $\ldots$ | 4.38 | 4.83 | 5.45 | 6.62 | 6.85 | Th | $\ldots$ | 2.338 | 2.571 | 3.058 |
| Bi | $\ldots$ | 3.100 | 3.342 | 3.889 | 4.574 | 4.763 | U | $\ldots$ | 2.228 | 2.385 | 2.873 |

* For reference, see footnote 236, p. 692.

TABLE 776.-CHARACTERISTIC EMISSION WAVELENGTHS (A). K SERIES*

| Element | $\gamma\left(\beta_{2}\right)$ | $\beta_{1}$ | $\beta_{2}$ | $a_{1}$ | $a_{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 24 Cr | $\left.2.0667^{( } \beta_{\mathrm{s}}\right)$ | 2.0806 |  | 2.28503 | 2.28891 |
| 26 Fe | $1.74080\left(\beta_{5}\right)$ | 1.753013 | 1.75646 | 1.932076 | 1.936012 |
| 28 Ni | 1.48561 | 1.49705 |  | 1.65450 | 1.65835 |
| 29 Cu | 1.37824 | 1.38935 |  | 1.53739 | 1.54123 |
| 42 Mo | . 619698 | . 630978 | . 631543 | . 707831 | . 712105 |
| 45 Rh | . 53396 | . 54449 | . 54509 | . 61202 | . 61637 |
| 47 Ag | . 486030 | . 496009 | . 49665 | . 55828 | . 56267 |
| 74 W | . 17899 † | . 18397 | . 18477 | . 20860 | . 21341 |
| 78 Pt | . 15887 | . 16370 |  | . 18523 | . 19004 |

[^316]TABLE 777.-WAVELENGTHS IN ANGSTROMS OF K-SERIES LINES REPRESENTING TRANSITIONS IN THE ORDINARY X-RAY ENERGY LEVEL DIAGRAM * ALLOWED BY THE SELECTION PRINCIPLES ${ }^{288}$

| Siegbahn Sommerfeld transition | $\begin{aligned} & K a_{2} \\ & K a^{2} \\ & K \cdot L_{11} \end{aligned}$ | $\begin{aligned} & K a_{1} \\ & K \cdot \\ & K \cdot L_{1 I I} \end{aligned}$ | $\begin{aligned} & K \beta \\ & K \beta_{3} \\ & K-M_{1 I} \end{aligned}$ | $\begin{aligned} & K \beta_{1} \\ & K \cdot \beta_{1} \\ & K \cdot M_{11} \end{aligned}$ | $\begin{aligned} & { }_{l}^{K} \beta_{2} \\ & K \cdot \mathcal{L}_{\mathrm{HI}} N_{\mathrm{HI}} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 4 Be | 115.7 |  |  |  |  |
| 5 B | 67.71 |  |  |  |  |
| 6 C | 44.54 |  |  |  |  |
| 7 N | 31.557 |  |  |  |  |
| 8 O | 23.567 |  |  |  |  |
| 9 F | 18.275 |  |  |  |  |
| 11 Na | 11.885 |  | 11.594 |  |  |
| 12 Mg | 9.869 |  | 9.539 |  |  |
| 13 Al | 8.3205 |  | 7.965 |  |  |
| 14 Si | 7.11106 |  | 6.7545 |  |  |
| 15 P | 6.1425 |  | 5.7921 |  |  |
| 16 S | 5.3637 | 5.3613 | 5.0211 |  |  |
| 17 Cl | 4.7212 | 4.7182 | 4.3942 |  |  |
| 19 K | 3.73707 | 3.73368 | 3.4468 |  |  |
| 20 Ca | 3.35495 | 3.35169 | 3.0834 |  |  |
| 21 Sc | 3.02840 | 3.02503 | 2.7739 |  |  |
| 22 Ti | 2.74681 | 2.74317 | 2.5090 |  |  |
| 23 V | 2.50213 | 2.49835 | 2.2797 |  |  |
| 24 Cr | 2.28891 | 2.28503 | 2.0806 |  |  |
| 25 Mn | 2.10149 | 2.09751 | 1.90620 |  |  |
| 26 Fe | 1.936012 | 1.932076 | 1.753013 |  |  |
| 27 Co | 1.78919 | 1.78529 | 1.61744 |  |  |
| 28 Ni | 1.65835 | 1.65450 | 1.47905 |  | 1.48561 |
| 29 Cu | 1.541232 | 1.537395 | 1.38935 |  | 1.37824 |
| 30 Zn | 1.43603 | 1.43217 | 1.29255 |  | 1.28107 |
| 31 Ga | 1.34087 | 1.33715 | 1.20520 |  | 1.1938 |
| 32 Ge | 1.25521 | 1.25130 | 1.12671 |  | 1.11459 |
| 33 As | 1.17743 | 1.17344 | 1.05510 |  | 1.04281 |
| 34 Se | 1.10652 | 1.10248 | . 993013 |  | . 97791 |
| 35 Br | 1.04166 | 1.03759 | . 93087 |  | . 91853 |
| 36 Kr | . 9821 | . 9781 | . 8767 |  | . 8643 |
| 37 Rb | . 92776 | . 92364 | . 82749 | . 82696 | 81476 |
| 38 Sr | . 87761 | . 87345 | . 78183 | . 78130 | .76921 |
| 39 Y | .83132 | . 82712 | . 73072 | . 73919 | . 72713 |
| ${ }_{41}^{40 \mathrm{Zr}} \mathrm{Nb}$ | . 788889 | . 784465 | . 70083 | . 600238 | . 685280 |
| 42 Mo | . 712105 | . 707831 | . 631543 | . 630978 | . 619698 |
| 43 Tc | . 675 | . 672 | . 601 |  |  |
| 44 Ru | . 64606 | . 64174 | . 57193 | . 57131 | . 56051 |
| 45 Rh | . 61637 | . 61202 | . 54509 | . 54449 | . 53396 |
| 46 Pd | . 58863 | . 58427 | . 52009 | . 51947 | . 50918 |
| 47 Ag | . 56267 | . 55828 | . 49665 | . 49601 | . 48603 |
| 48 Cd | . 53832 | . 53390 | . 47471 | . 47408 | . 46420 |
| 49 In | . 51548 | . 51106 | . 45423 | . 45358 | . 44428 |
| 50 Sn | . 49402 | . 48957 | . 43495 | . 43430 | . 42499 |
| 51 Sb | . 47387 | . 46931 | . 41623 |  | . 40710 |
| 52 Te | . 45491 | . 45037 | 3822.39926 |  | . 39037 |
| 53 I | . 43703 | . 43249 | . 38292 | . 38315 | . 37471 |
| ${ }_{55}^{54 \mathrm{Cs}}$ | . 417 |  | 35436.360 |  |  |
| 55 Cs 56 Ba | . 40411 | . 39959 | .35436 .34089 | .35360 .34022 | . 34516 |
| 57 La | . 37466 | . 37004 | . 32809 | . 32726 | . 31966 |
| 58 Ce | . 36110 | . 35647 | . 31572 | . 31501 | . 30770 |
| 59 Pr | . 34805 | . 34340 | . 30439 | . 30360 | . 29625 |
| 60 Nd | . 33595 | . 33125 | . 29351 | . 29275 | . 28573 |
| 62 Sm | . 31302 | . 30833 | . 27325 | . 27250 | . 26575 |
| 63 Eu | . 30265 | . 29790 | . 26386 | . 26307 | . 25645 |

[^317]TABLE 777.-WAVELENGTHS IN ANGSTROMS OF K-SERIES LINES REPRE-
SENTING TRANSITIONS IN THE ORDINARY X-RAY ENERGY LEVEL
DIAGRAM ALLOWED BY THE SELECTION PRINCIPLES
(concluded)

| Siegbahn Sommerfeld transition | $\begin{aligned} & K a_{2} \\ & K a^{\prime} \\ & K \cdot \dot{L}_{\mathrm{II}} \end{aligned}$ | $\begin{aligned} & K a_{1} \\ & K \\ & K-L_{I I I} \end{aligned}$ | $\begin{aligned} & K \beta \\ & K \beta_{3} \\ & K-M_{\mathrm{II}} \end{aligned}$ |  | $\begin{aligned} & K \beta_{1} \\ & K \beta-M_{1 I I} \\ & K \end{aligned}$ | $\begin{aligned} & K \beta_{2} \\ & K \cdot \mathcal{L}_{\mathrm{II}} N_{\mathrm{III}} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 64 Gd | . 29261 | . 28782 | . 25471 |  | . 25394 | . 24762 |
| 65 Tb | . 28286 | . 27820 | . 24629 |  | . 24551 | . 23912 |
| 66 Dy | . 27375 | . 26903 | . 23787 |  | . 23710 | . 23128 |
| 67 Ho | . 26499 | . 26030 |  |  |  |  |
| 68 Er | . 25664 | . 25197 | . 22300 |  | . 22215 | . 21671 |
| 69 Tm | . 24861 | . 24387 | . 21558 |  | . 21487 |  |
| 70 Yb | . 24098 | . 23628 | . 20916 |  | . 20834 | . 20322 |
| 71 Lu | . 23358 | . 2282 | . 20252 |  | . 20171 | . 19649 |
| 72 Hf | . 22653 | . 22173 | . 19583 |  | . 19515 | . 19042 |
| 73 Ta | . 21973 | . 21488 |  | . 18991 |  | . 18452 |
| 74 W | . 21337 | . 20856 | . 18475 |  | . 18397 | . 17906 |
| 76 Os | . 20131 | . 19645 |  | . 17361 |  | . 16875 |
| 77 Ir | . 19550 | . 19065 |  | . 16850 |  | . 16376 |
| 78 Pt | . 19004 | . 18223 |  | . 16370 |  | . 15887 |
| 79 Au | . 18483 | . 17996 |  | . 15902 |  | . 15426 |
| 81 Tl | . 17466 | . 16980 |  | . 15011 |  | . 14539 |
| 82 Pb | . 17004 | . 16516 |  | . 14606 |  | . 14125 |
| 83 Bi | . 16525 | . 16041 |  | . 14205 |  | . 13621 |
| 92 U | . 13095 | . 12640 |  | . 11187 |  | . 10842 |

TABLE 778.-WAVELENGTHS, TUNGSTEN L SERIES*

| $\gamma_{4}$ | $L_{11}-O_{22}$ | 1.02647 | $\beta_{7}$ | $L_{22}-N_{43}, 4$ | 1.2208 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $\gamma_{0}$ | $L_{11}-N_{33}$ | 1.0439 | $\beta_{11}, 12$ | $L_{22} \cdots N_{32}$ | 1.2354 |
| $\gamma_{3}$ | $L_{11}-N_{22}$ | 1.05965 | $\beta_{2}$ | 1.24191 |  |
| $\gamma_{2}$ | $L_{11}-N_{21}$ | 1.06584 | $\beta_{3}$ | $L_{11}-M_{22}$ | 1.26000 |
| $\gamma_{8}$ | $L_{21}-O_{32}$ | 1.0720 | 1.079 | $\beta_{1}$ | $L_{21}-M_{32}$ |
| $\gamma_{8}$ | $L_{21}-O_{11}$ | 1.09553 | $\beta_{0}$ | $L_{12}-N_{11}$ | 1.27971 |
| $\gamma_{1}$ | $L_{21}-N_{32}$ | 1.2971 |  |  |  |
| $\gamma_{5}$ | $L_{21}-N_{11}$ | 1.1292 | $\beta_{4}$ | $L_{11}-M_{21}$ | 1.29874 |
| $\beta_{0}$ | $\cdots \cdots{ }_{31}$ | 1.2021 | $\beta_{11}$ | $L_{11}-M_{11}$ | 1.3344 |
| $\beta_{8}$ | $L_{11}-M_{33}$ | 1.2034 | $\eta$ | $L_{12}-M_{11}$ | 1.4177 |
| $\beta_{10}$ | $\cdots \cdots$ | 1.2094 | $a_{1}$ | $L_{22}-M_{33}$ | 1.47348 |
| $\beta_{5}$ | $L_{22}-O_{32}, 33$ | 1.2125 | $a_{2}$ | $L_{22}-M_{32}$ | 1.48452 |

* For reference, see footnote 236, p. 692.

TABLE 779.-TYPICAL SAFE RATINGS OF DIAGNOSTIC X-RAY TUBES

General Electric Company Benson-type X-ray tube Westinghouse Corporation WL-355 tube

| Effective focal area |  | wave | $\begin{aligned} & \text { Half } \\ & \mathrm{Hv}^{*} \end{aligned}$ |  |  |  | Effective focal area | $\begin{aligned} & \text { Full wave } \\ & \text { kv ma } \end{aligned}$ | $\underset{\text { kv malf wa }}{\text { kave }}$ | Self. rectified kv ma |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Stationary target : 1 second |  |  |  |  |  |  | Stationary target: 1 second |  |  |  |
| $1.5 \mathrm{~mm}^{2}$ | 110 | 20 | 110 | 15 |  |  | $1.5 \mathrm{~mm}^{2}$ | 2770 | 2025 | 1520 |
| 3.7 | 110 | 60 | 95 | 50 |  |  | 2.1 | 4830 | 3410 | 2570 |
| 5.2 | 90 | 150 | 100 | 100 | 78 | 100 | 2.6 | 6500 | 4730 | 3400 |
|  | 1/60 second |  |  |  |  |  | 3.0 | 7680 | 5915 | 4150 |
| 5.2 | 72 | 500 |  |  |  |  | 4.2 | 11900 | ${ }_{1 / 60 \text { second }}^{9650}$ |  |
|  | 104 | 350 |  |  |  |  | 4.2 | 25000 |  |  |
| Rotating target: 1 second |  |  |  |  |  |  |  |  | ... |  |
|  | 80 | 280 |  |  |  |  |  |  |  |  |
| 1/60 second |  |  |  |  |  |  |  |  |  |  |

[^318]TABLE 780.-WAVELENGTHS OF THE MORE PROMINENT L-GROUP LINES IN ANGSTROMS*


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TABLE 780.-WAVELENGTHS OF THE MORE PROMINENT L-GROUP LINES IN ANGSTROMS (concluded)

| Siegbahn Sommerfeld transition | $\begin{aligned} & a_{3} \\ & \stackrel{a}{z}^{L_{\mathrm{II}}} \mathrm{M}_{\mathrm{IV}} \end{aligned}$ | $\begin{aligned} & a_{1} \\ & \stackrel{a}{L_{111}} \cdot M_{\mathrm{v}} \end{aligned}$ | $\begin{aligned} & \beta_{1} \\ & \stackrel{\beta}{1 I}^{L_{11}} M_{\mathrm{v}} \end{aligned}$ | $\begin{aligned} & \beta_{2} \\ & \stackrel{L}{L I I I}^{-N} \end{aligned}$ | $\begin{aligned} & \gamma_{1} \\ & {\underset{L}{1 I}}^{L_{11}} N_{\mathrm{IV}} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 80 Hg | 1.24951 | 1.23863 | 1.04652 | 1.03770 | . 8946 |
| 81 Tl | 1.21626 | 1.20493 | 1.01299 | 1.00822 | . 86571 |
| 82 Pb | 1.18408 | 1.17258 | . 98083 | . 98083 | . 83801 |
| 83 Bi | 1.15301 | 1.14150 | . 95002 | . 95324 | . 81143 |
| 90 Th | . 96585 | . 95405 | . 76356 | . 79192 | . 65176 |
| 91 Pa | . 9427 | . 9309 | . 7407 | . 7721 | . 6325 |
| 92 U | . 92062 | . 90874 | . 71851 | . 75307 | . 61359 |

TABLE 781.-WAVELENGTHS OF M-SERIES LINES IN ANGSTROMS FROM
73 Ta TO $92 U^{*}$

| Transition | 73 Ta | 74 W | 75 Re | 76 Os | 77 Ir | 78 Pt | 79 Au | 81 Tl | 82 Pb | 83 Bi | 90 Th | 92 U |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $M_{11} O_{2 v}$ |  |  |  |  |  |  |  |  |  |  | 2.613 | 2.440 |
| $M_{1} N_{111}$ |  | 5.163 |  |  |  | 4.451 | 4.291 | 4.005 | 3.864 | 3.732 | 2.938 | 2.745 |
| $M_{\text {II }} N_{\text {IV }}$ | 5.558 | 5.342 |  | 4.944 | 4.770 | 4.590 | 4.424 | 4.110 | 3.964 | 3.829 | 3.006 | 2.813 |
| $\mathrm{MuH}_{\mathrm{H}} \mathrm{O}$ |  |  |  |  | 4.859 | 4.682 | 4.514 | 4.207 | 4.063 | 3.926 | 3.124 | 2.941 |
| $\mathrm{MiHI}^{\text {O }}$ |  | 5.620 |  |  |  |  |  |  | 4.235 | 4.096 |  | 3.114 |
| $M_{11} N_{\text {I }}$ |  |  |  |  |  |  |  |  |  |  |  | 3.322 |
| $\boldsymbol{\gamma}^{\prime}$ |  |  |  |  |  |  |  | 4.800 | 4.650 | 4.506 | 3.661 | 3.463 |
| $M_{\text {III }} N_{V}$ | 6.299 | 6.076 | 5.875 | 5.670 | 5.490 | 5.309 | 5.135 | 4.815 | 4.665 | 4.522 | 3.672 | 3.473 |
| $M_{\text {III }} N_{\text {IV }}$ | 6.340 | 6.121 | 5.919 | 5.712 | 5.529 | 5.346 | 5.175 | 4.855 | 4.705 | 4.560 | 3.710 | 3.514 |
| $\mathrm{Miv}_{\text {IV }} \mathrm{O}_{11}$ | 7.083 | 6.794 |  |  |  |  |  |  |  | 4.813 | 3.804 | 3.570 |
| $\beta^{\prime}$ | 6.984 | 6.718 |  | 6.233 | 6.009 | 5.796 | 5.595 | 5.220 | 5.045 | 4.881 | 3.924 | 3.698 |
| $M_{\text {Iv }} N_{\text {vi }}$ | 7.008 | 6.743 | 6.491 | 6.254 | 6.025 | 5.8168 | 5.612 | 5.239 | 5.065 | 4.899 | 3.934 | 3.708 |
| $\mathrm{MvO}_{\text {HiI }}$ |  |  |  |  |  | 5.975 | 5.755 |  |  |  |  |  |
| $a^{\prime \prime}$ | 7.201 | 6.932 |  | 6.440 | 6.215 | 5.997 | 5.794 | 5.416 | 5.239 |  |  |  |
| $a^{\prime}$ | 7.219 | 6.948 |  | 6.459 | 6.231 | 6.011 | 5.811 | 5.433 | 5.256 | 5.087 | 4.112 | 3.886 |
| $M_{\mathrm{v}} \mathrm{Nvir}^{\text {rem }}$ | 7.237 | 6.969 | 6.715 | 6.477 | 6.249 | 6.034 | 5.828 | 5.450 | 5.274 | 5.108 | 4.130 | 3.902 |
| $M_{\mathrm{v}} N_{\text {vi }}$ |  |  |  |  | 6.262 | 6.045 | 5.842 | 5.461 | 5.288 | 5.119 | 4.143 | 3.916 |
| $M_{111} N_{1}$ | 7.596 | 7.346 |  |  | 6.653 | 6.442 | 6.241 | 5.870 | 5.694 | 5.526 | 4.554 | 4.322 |
| $M_{\text {IV }} N_{\text {III }}$ |  | 8.559 | 8.222 |  | 7.629 | 7.356 | 7.086 |  | 6.371 | 6.149 | 4.901 | 4.615 |
| $M_{\text {V }} N_{\text {III }}$ | 9.297 | 8.943 | 8.612 | 8.293 | 8.002 | 7.722 | 7.451 | 6.960 | 6.726 | 6.508 | 5.229 | 4.937 |
| $M_{\text {IV }} N_{\text {II }}$ | 9.311 | 8.977 | 8.646 | 8.344 | 8.048 | 7.774 | 7.507 | 7.017 | 6.788 | 6.571 | 5.329 | 5.040 |

* E. Lindberg, Dissertation, Uppsala (1931). In addition to the values listed here, measurements have been made in the range from Ce 58 to 72 Hf . The wavelengths may be found in the dissertation, or in Siegbalin, Spektroskopie der Röntgenstrahlen (1931). For reference, see footnote 238, p. 697.

TABLE 782.-X-RAY TERMS FOR VARIOUS ELEMENTS *
$\nu^{\prime} R$ values; $\nu$ in $\mathrm{cm}^{-1}, R=109,737 \mathrm{~cm}^{-1}$

| Term | 13 Al | 20 Ca | 29 Cu | 42 Mo | 47 Ag | 74 W | 92 U |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| K | 10.71 | 297.4 | 661.6 | 1473.4 | 1880.9 | 5120.7 | 8474 |
| $L_{1}$ |  |  | 81.0 | 211.3 | 282.7 | 890.8 | 1602.6 |
| $L_{11}$ | 2.30 | 25.8 | 70.3 | 193.7 | 260.9 | 849.9 | 1542.7 |
| $L_{\text {III }}$ | 2.30 | 25.5 | 68.9 | 186.0 | 248.6 | 751.3 | 1264.2 |
| $M_{1}$ | . |  | 8.9 | 37.5 | 54.4 | 207.3 | 408.5 |
| $M_{11}$ | . 63 | 1.9 | 5.7 | 30.5 | 46.7 | 189.3 | 381.5 |
| $M_{\text {III }}$ | . 63 | 1.9 | 5.7 | 29.2 | 44.4 | 167.5 | 316.8 |
| $M_{\text {Iv }}$ | . . . | . 4 | . 4 | 17.3 | 29.2 | 137.5 | 274.2 |
| $M_{V}$ | . . . | . 4 | . 4 | 17.1 | 28.8 | 132.9 | 261.2 |
| $N_{1}$ |  |  |  | 5.1 | 8.7 | 43.3 | 106.0 |
| $N_{\text {II }}$ | .... | . . . | ... | 2.9 | 6.5 | 36.0 | 93.5 |
| $N_{111}$ |  |  |  | 2.9 | 6.5 | 31.0 | 76.6 |
| $N_{\text {Iv }}$ |  |  |  |  | 1.1 | 18.7 | 57.5 |
| $N_{V}$ |  |  |  | . 4 | 2.0 | 17.6 | 54.3 |
| $N \mathrm{vi}$ |  |  |  |  | . . . | 2.3 | 28.5 |
| $N \mathrm{vil}$ |  | . . . . |  | .... | . . . | 2.0 | 27.6 |
| $\mathrm{O}_{1}$ |  |  |  |  |  | 5.4 | 23.7 |
| $O_{11}$ |  |  |  |  | . . . | 2.9 | 18.3 |
| $O_{\text {IIf }}$ |  |  |  |  | . . . | 2.9 | 13.9 |
| $O_{\text {Iv }} O_{\mathrm{v}}$ |  |  |  |  |  | . . . | 7.0 |
| $P_{\text {II }} P_{\text {III }}$ |  | . . . |  | . . . | . . . |  | . 8 |

[^320]Longer wavelengths
$M_{\mathrm{v}}$
zก্ড
722.08
$M_{\text {IV }}$
708.18
$M_{\text {III }}$
786.8
$\ldots$

$\ldots$
M
$\begin{array}{ll}\infty & \vdots \\ \infty\end{array}$
$M_{1}$
$M_{\text {IV }}$
13.15
$\ldots$
$L_{\text {III }}$
TABLE 783.-CRITICAL ABSORPTION WAVELENGTHS IN ANGSTROMS*

TABLE 783.-CRITICAL ABSORPTION WAVELENGTHS IN ANGSTROMS*

（continued）
（
Longer wavelengths

$$
\begin{gathered}
N_{\mathrm{III}} \\
855.63
\end{gathered}
$$

令三N゙

$$
\begin{array}{rllll}
\Xi & \vdots & \vdots & \vdots & \vdots \\
\vdots & \vdots & \vdots
\end{array}
$$



[^321]TABLE 783.-CRITICAL ABSORPTION WAVELENGTHS IN ANGSTROMS (concluded)
Longer wavelengths
2
0
$-\infty$
$=-\infty$
$=1$ N
$\infty$
$\infty$
ヘN
${ }_{1153.52}^{P_{\text {II, }} \text { III }}$

$N$
N
M
M


$\begin{array}{ll}\circ & \text { N } \\ \text { M } \\ \text { N }\end{array}$

| $M_{\text {III }}$ |
| :--- |
|  |
|  |
| 5.427 |
|  |
| 5.027 |
| 4.851 |
| 4.676 |
| 4.508 |
| 4.340 |
| 4.184 |
| 4.034 |
| 3.893 |
|  |
|  |





|  | 8 | $\infty$ |
| :--- | :--- | :--- |
|  |  |  |




|  |
| :---: |
|  |  |
|  |  |
|  |  |





| 8 |
| :--- |
| + |






$\stackrel{\rightharpoonup}{\underset{\sim}{7}}$

$$
\begin{aligned}
& \stackrel{7}{7}
\end{aligned}
$$

TABLE 784.-CALCULATED MASS ABSORPTION COEFFICIENTS (concluded)
8


| $\stackrel{8}{+}$ |  |
| :---: | :---: |




Material
Molybdenum
Palladium
Silver
Tin
Tellurium
Iodine
Xenon
Barium
Cerium
Neodymium
Terbium
Tantalum
Tungsten
Platinum
Gold
Mercury
Lead
Bismuth
Thorium
Uranium


Artificial disintegration is generally considered in two parts: the first when the bombarded atom suffers a change not greater than the loss (or gain) of an alpha particle, and the second when the change in the bombarded atom is much greater-the bombarded atom being at times split into two nearly equal parts. This latter is called fission : the former, artificial disintegration. Fission was at first brought about by bombardment with neutrons but it can be caused by bombardment by almost any particle with the proper energy (see Table 726). This effect can be produced in a number of isotopes of the heavier atoms such as $\mathrm{Np}, \mathrm{U}, \mathrm{Pa}, \mathrm{Th}, \mathrm{Pb}, \mathrm{Sn}, \mathrm{Eu}$, and Ni . Some other atoms such as $\mathrm{Bi}, \mathrm{Rb}, \mathrm{Tl}$, $\mathrm{Hg}, \mathrm{Au}, \mathrm{Pt}, \mathrm{W}$, and many others show no fission; at least if such an effect exists it is less than $1 / 1000$ that of Th . There are a great many products of fission as shown by a paper by scientists of the Plutonium Project. ${ }^{240}$ One example of fission is

$$
{ }_{92} \mathrm{U}^{235}+{ }_{0} n^{1} \rightarrow{ }_{40} \mathrm{Zr}^{97}+{ }_{52} \mathrm{Te}^{137}+{ }_{0} n^{1}+{ }_{0} n^{1}
$$

There is a considerable release of energy when fission takes place. Complete data are not available but such as are available give values of about 200 Mev per fission per atom of the heavier elements. (See Table 790.) It is also to be noted that there are two neutrons given as a result of the above reaction; thus, it is self-sustaining.
${ }^{240}$ Journ. Amer. Chem. Soc., vol. 68, p. 2411, 1946.

TABLE 785.-FISSION DATA*


* For reference, see footnote 226, p. 667.

TABLE 786.-FISSION THRESHOLDS *

|  | Threshold energy for exciting fission |  |  |  | Threshold energy for exciting fission |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{90} \mathrm{Th}^{282}$ | $5.40 \pm .22 \mathrm{Mev}$ | $\gamma$ | ${ }_{90} \mathrm{Th}^{232}$ | ${ }_{92} \mathrm{U}^{238}$ | $5.08 \pm .15 \mathrm{Mev}$ | $\gamma$ | ${ }_{92} \mathrm{U}^{298}$ |
| ${ }_{00} \mathrm{Th}^{233}$ | $1.10 \pm .05$ | $n$ | ${ }_{90} \mathrm{Th}^{232}$ | ${ }_{92} \mathrm{U}^{239}$ | $1.0 \pm .1$ | $n$ | ${ }_{92} \mathrm{U}^{298}$ |
| ${ }_{11} \mathrm{~Pa}^{232}$ | $\sim 1$ | $n$ | ${ }_{91} \mathrm{~Pa}^{231}$ | ${ }_{93} \mathrm{~Np}^{258}$ | <0 | slow $n$ | ${ }_{93} \mathrm{~Np}^{237}$ |
| ${ }_{91} \mathrm{~Pa}^{233}$ | <6.9 | $p$ | ${ }_{80} \mathrm{Th}^{232}$ | ${ }_{93} \mathrm{~N} \mathrm{p}^{238}$ | <6.9 | $p$ | ${ }_{92} \mathrm{U}^{238}$ |
| ${ }_{91} \mathrm{~Pa}^{294}$ | $\sim 8$ | $d$ | ${ }_{90} \mathrm{Th}^{232}$ | ${ }_{33} \mathrm{~N} \mathrm{p}^{240}$ | $\sim 8$ | d | ${ }_{92} \mathrm{U}^{298}$ |
| ${ }_{92} \mathrm{U}^{233}$ | $5.18 \pm .27$ | $\gamma$ | ${ }_{92} \mathrm{U}^{233}$ | ${ }_{94} \mathrm{Pu}^{239}$ | $5.31 \pm .27$ | $\gamma$ | ${ }_{04} \mathrm{Pu}^{239}$ |
| ${ }_{92} U^{2235}$ | $5.31 \pm .25$ | $\gamma$ | ${ }_{22} U^{235}$ | ${ }_{94} \mathrm{Pu}^{240}$ | <0 | slow $n$ | ${ }_{40} \mathrm{Pu}^{239}$ |
| ${ }_{92} \mathrm{U}^{238}$ | <0 | slow $n$ | ${ }_{02} \mathrm{U}^{235}$ |  |  |  |  |

[^322]TABLE 787.-ESTIMATED VALUES OF THE NEUTRON BINDING ENERGY OF THE DIVIDING NUCLEUS *

| Compound nucleus | Neutron binding energy | Compound nucleus | Neutron binding energy |
| :---: | :---: | :---: | :---: |
| ${ }_{90} \mathrm{Th}^{232}$ | 6.2 Mev | ${ }_{82} \mathrm{U}^{237}$ | 5.2 Mev |
| ${ }_{90} \mathrm{Th}^{238}$ | 5.2 | ${ }_{92} \mathrm{U}^{238}$ | 6.1 |
| ${ }_{91} \mathrm{~Pa}^{231}$ | 6.4 | ${ }_{92} \mathrm{U}^{239}$ | 5.1 |
| ${ }_{81} \mathrm{~Pa}^{232}$ | 5.4 | ${ }_{93} \mathrm{~Np}^{239}$ | $\sim 6.3$ |
| ${ }_{92} \mathrm{U}^{234}$ | 6.5 | ${ }_{33} \mathrm{~Np}^{249}$ | $\sim 5.3$ |
| ${ }_{92} \mathrm{U}^{235}$ | 5.4 | ${ }_{94} \mathrm{Pu}^{239}$ | $\sim 5.4$ |
| ${ }_{92} \mathrm{U}^{236}$ | 6.4 | ${ }_{04} \mathrm{Pu}^{240}$ | $\sim 6.4$ |

* For reference, see footnote 226 , p. 667.


## TABLE 788.-THE CRITICAL ENERGY FOR FISSION *

The experimental values of the critical energy for fission of a number of isotopes have been determined by Koch, McElhinney, and Gasteiger ${ }^{241}$ who give the following photofission threshold energies. (The work of Shoupp and Hill ${ }^{242}$ on the fast neutron fission energies for $\mathrm{Th}^{232}$ and $\mathrm{U}^{238}$ was used for the values given for $\mathrm{Th}^{233}$ and $\mathrm{U}^{230}$.)


* Prepared by J. L. Rhodes, University of Pennsylvania.
${ }^{241}$ Phys. Rev., vol. 77, p. 329, 1950.
242 Phys. Rev., vol. 75, p. 785, 1949.

TABLE 789.-HALF-LIVES FOR SPONTANEOUS FISSION ${ }^{243}$
These half-lives are calculated on the basis of a half-life of $10^{15}$ years for $\mathrm{U}^{235}$

${ }^{243}$ Turner, Rev. Mod. Phys., vol. 17, p. 292, 1945.

TABLE 790.-THE ENERGY RELEASED BY FISSION ON DIVISION OF SOME ATOMS INTO EQUAL PARTS *

| Original | Two products | Energy released on division | Energy released in subsequent beta decay |
| :---: | :---: | :---: | :---: |
| ${ }_{2 \times} \mathrm{Ni}^{01}$ | ${ }_{14} \mathrm{Si}^{\text {co, }}{ }^{31}$ | -11 Mev | 2 Mev |
| ${ }_{50} \mathrm{Sn}^{117}$ | ${ }_{25} \mathrm{Mn}^{38,54}$ | 10 | 12 |
| ${ }_{68} \mathrm{Er}^{167}$ | ${ }_{34} \mathrm{Se}^{83,84}$ | 94 | 13 |
| ${ }_{82} \mathrm{~Pb}^{208}$ | ${ }_{41} \mathrm{Nb}^{103,104}$ | 120 | 32 |
| ${ }_{92} \mathrm{U}^{239}$ | ${ }_{41} \mathrm{Pd}^{110}{ }^{120}$ | 200 | 31 |

[^323]|  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{30} \mathrm{Kr}^{\text {85 }}$ | 9.4 yr | . 74 | none | . 24 | ${ }_{52} \mathrm{Sb}^{127}$ | 93 hr | 1.2 | . 72 |  |
| ${ }_{32} \mathrm{Rb}^{88}$ | 19 d | 1.82 | 1.08 | . 00016 | ${ }_{52} \mathrm{Te}^{129}$ | 90 d | I.T. |  | . 033 |
| ${ }_{38} \mathrm{Sr}^{89}$ | 55 d | 1.5 | none | 4.6 | ${ }_{52} \mathrm{Te}^{128}$ | 32 d | I.T. |  | . 19 |
| ${ }_{38} \mathrm{Sr}^{20}$ | 25 yr | . 65 | none | $\sim 5$ | ${ }_{52} \mathrm{Te}^{132}$ | 77 hr | . 28 | . 22 | 3.6 |
| ${ }_{39} \mathrm{Y}^{20}$ | 62 hr | 2.35 | none |  | ${ }_{63}{ }^{191}$ | 8 d | . 687 | . 37 | 2.8 |
| ${ }_{38} \mathrm{Y}^{91}$ | 61 d | 1.6 | none | 5.9 | ${ }_{44} \mathrm{Xe}^{138}$ | 5.3 d | . 35 | . 085 | 6 |
| * $\mathrm{Zr}^{\text {a5 }}$ | 65 d | 1.0 | . 92 | 6.4 | ${ }_{55} \mathrm{Cl}^{188}$ | 13 d | . 28 | 1.2 | . 008 |
| ${ }_{41} \mathrm{Nb}^{\text {958 }}$ | 35 d | . 15 | . 77 |  | ${ }_{55} \mathrm{CS}^{137}$ | 37 yr | . 8 | . 75 | $\sim 6$ |
| ${ }_{41} \mathrm{Nb}^{88}$ | 90 hr | I.T. |  |  | ${ }_{56} \mathrm{Ba}^{140}$ | 12.8 d | 1.05 | . 53 | 6.1 |
| ${ }_{42} \mathrm{Mo}^{90}$ | 67 hr | 1.5 | . 75 | 6.2 | ${ }_{58} \mathrm{Ce}^{141}$ | 30 d | . 6 | . 2 | 5.7 |
| ${ }_{48} \mathrm{Ru}^{108}$ | 41 d | . 67 | . 55 | 3.7 | ${ }_{\text {ss }} \mathrm{Ce}^{144}$ | 275 d | . 35 | none | 5.3 |
| ${ }_{48} \mathrm{Ru}^{108}$ | 1.0 yr | $\sim .03$ | none | . 5 | ${ }_{50} \mathrm{Pr}^{1 / 3}$ | 13.8 d | 1.0 | none | 6 |
| ${ }_{42} \mathrm{Ag}^{111}$ | 7.5 d | 1.0 | none | . 018 | ${ }_{00} \mathrm{Nd}^{147}$ | 11 d | . 90 | . 58 | 2.6 |
| ${ }_{48} \mathrm{Cd}^{1115}$ | 43 d | 1.7 |  | . 0008 | ${ }_{61} \mathrm{Pm}^{147}$ | 3.7 yr | . 23 | none | 2.6 |
| ${ }_{48} \mathrm{Cd}^{115}$ | 43 d | 1.7 | . 5 | . 0008 | ${ }_{83} \mathrm{Eu}^{155}$ | 2 yr | . 2 | . 084 | . 03 |
| ${ }_{\text {50 }}{ }_{\text {60 }} \mathrm{Sn}^{128} \mathrm{Sb}^{128}$ | 130 d | 1.3 | . 69 | . 02 | ${ }_{93} \mathrm{Eu}^{150}$ | 15.4 d | 2.4 | 2.0 | . 013 |

* Revised by J. L. Rhodes, University of Pennsylvania. For reference, see footnote 226, p. 667.

TABLE 792.-CROSS SECTIONS OF FISSIONABLE NUCLEI FOR NEUTRONS (IN UNITS OF $10^{-2 t} \mathrm{~cm}^{2}$ ) *

| $\begin{gathered} \text { Target } \\ \text { substance } \end{gathered}$ | Process | Cross section for energy ranges |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Thermal | Resonance | Fast $\dagger$ |
| ${ }_{82} \mathrm{U}^{235}$ | fission | $420 \pm 100$ | 30 | 2.4 |
| ${ }_{88} \mathrm{U}^{238}$ | scattering | 17 | 17 | 6 |
|  | fission | 0 | 0 | . 5 |
|  | scattering | 17 | 17 |  |
|  | absorption (resonance) | 3 | $5000 \ddagger$ | 0 |
| Ordinary uranium | fission. | 3 (ave) | . 2 (ave) | . 5 |
|  | scattering | 17 | 17 | 6 |
|  | absorption | 3 | $5000 \pm$ | 0 |
| $\begin{aligned} & { }_{84} \mathrm{P}^{\mathrm{U}^{298}} \\ & { }_{25} \mathrm{~T}^{282} \end{aligned}$ | fission | \}assumed same as for ${ }_{92} \mathrm{U}^{235}$ |  |  |
|  | scattering |  |  |  |
|  | fission. | 0 | 0 | . 1 |
|  | scattering | 17 | 17 | 6 |
|  | absorption | 8.3 |  |  |
| ${ }_{91} \mathrm{~Pa}^{281}$ | fission | 0 | 0 | 3 |
|  | scattering | 17 | 17 | 6 |
| ${ }_{00} \mathrm{Th}^{230}$ | fission | 0 | 0 | . 3 |
|  | scattering | 17 | 17 | 6 |

[^324]TABLE 793.-CROSS SECTIONS OF SOME FISSION PRODUCTS FOR THERMAL NEUTRONS*

| Atomic number | Element | "Average nucleus" |  | Isotope (in units of $\underbrace{10^{-12} \mathrm{~cm}^{2} \text { ) }}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Absorption $\sigma a$ | $\underset{\substack{\text { Total } \\ \sigma 1}}{ }$ | $\begin{gathered} \text { Mass } \\ \text { number } \end{gathered}$ | $\underset{\sigma a}{\text { Absorption }}$ | $\begin{gathered} \text { Relative } \\ \text { natural } \\ \text { abundance } \end{gathered}$ |
| 35 | Br | 7 | 9.5 | $\begin{aligned} & 79 \\ & 81 \end{aligned}$ | $\begin{gathered} 12 \\ 2.25 \end{gathered}$ | $\begin{array}{ll} 50.6 \\ 49.4 \end{array}$ |
| 36 | Kr | . 1 | 27 | $\begin{aligned} & 78 \\ & 84 \\ & 86 \end{aligned}$ | $\begin{aligned} & .27 \\ & .16 \\ & .061 \end{aligned}$ | $\begin{array}{r} .34 \\ 57.0 \\ 17.4 \end{array}$ |
| 37 | Rb | . 7 | 12 | $\begin{aligned} & 85 \\ & 87 \end{aligned}$ | $\begin{aligned} & .724 \\ & .135 \end{aligned}$ | $\begin{aligned} & 72.8 \\ & 27.2 \end{aligned}$ |
| 38 | Sr | 1.5 | 11 | $\begin{aligned} & 86 \\ & 88 \end{aligned}$ | $\stackrel{1.3}{.005}$ | $\begin{gathered} 9.8 \\ 82.56 \end{gathered}$ |
| 39 | Y | 1.1 | ... | 89 | 1.1 | 100 |
| 40 | Zr | . 4 | 15 | $\begin{aligned} & 90 \\ & 91 \\ & 92 \\ & 94 \\ & 96 \end{aligned}$ | $\begin{array}{r} .12 \\ 1.54 \\ .27 \\ .53 \\ 1.07 \end{array}$ | $\begin{array}{r} 51.5 \\ 11.2 \\ 17.1 \\ 17.4 \\ 2.8 \end{array}$ |
| 41 | Nb | 1.0 | 6.9 | 93 | 1.0 | 100 |
| 42 | Mo | 3.9 | 7.9 | $\begin{array}{r} 95 \\ 97 \\ 98 \\ 100 \end{array}$ | $\begin{aligned} & 13 \\ & 2.3 \\ & .37 \\ & .23 \end{aligned}$ | $\begin{array}{r} 15.7 \\ 9.5 \\ 24.1 \\ 9.25 \end{array}$ |
| 51 | Sb | 4.7 | 9 | $\begin{aligned} & 121 \\ & 123 \end{aligned}$ | $\begin{aligned} & 6.8 \\ & 2.5 \end{aligned}$ | $\begin{aligned} & 56 \\ & 44 \end{aligned}$ |
| 52 | Te | 5 | 10 | $\begin{aligned} & 126 \\ & 128 \\ & 130 \end{aligned}$ | $\begin{aligned} & .88 \\ & .2 \\ & \hline \end{aligned}$ | $\begin{aligned} & 18.7 \\ & 31.86 \\ & 34.52 \end{aligned}$ |
| 53 | I | 6.1 | 9.4 | 127 | 6.1 | 100 |
| 54 | Xe | ... | 35 | $\begin{aligned} & 132 \\ & 136 \end{aligned}$ | $.2$ | $\begin{array}{r} 26.9 \\ 8.9 \end{array}$ |
| 56 | Ba | 1.25 | 9.25 | 138 | . 56 | 71.66 |
| 57 | La | 9 | 25 | 139 | 9 | 99.9 |
| 62 | Sm | 8000 | $\ldots$ | 149 | 53,000 | 15.5 |
| 63 | Eu | 2500 | 4500 | $\begin{aligned} & 151 \\ & 153 \end{aligned}$ | $\begin{array}{r} 5200 \\ 240 \end{array}$ | $\begin{aligned} & 49.1 \\ & 50.9 \end{aligned}$ |
| 64 | Gd | 38,000 | $\cdots$ | $\begin{aligned} & 155 \\ & 157 \end{aligned}$ | $\begin{array}{r} 50,000 \\ 180,000 \end{array}$ | $\begin{aligned} & 14.8 \\ & 15.7 \end{aligned}$ |

* Revised by J. L. Rhodes, University of Pennsylvania. For reference, see footnote 226, p. 667.

Cosmic rays are an ionizing radiation that has been discovered in the atmosphere of the earth. As generally discussed these rays are divided into primary and secondary cosmic rays, the primary rays being the high-energy particles that fall upon the outer atmosphere of the earth. In general, the intensity of cosmic radiation is given as the number of rays per $\mathrm{cm}^{2}$ per second. The intensity (i.e., number of particles per $\mathrm{cm}^{2}$ ) increases for about the first onetenth of the atmosphere where it is about 5 times the initial intensity and from there down to sea level the intensity decreases. These primary rays appear to come from all directions from outer space and to consist almost entirely, if not altogether, of particles charged positively ${ }^{245}$ (i.e., protons, alpha-particles, and probably other nuclei). Several theories have been advanced for the origin of this primary radiation: (1) Annihilation of matter; (2) speeding up of stripped atoms in outer space either by electrical fields or by changing magnetic fields; (3) from some activity in stars in distant space; or even (4) that it is radiation remaining from the original explosion some $10^{9}-10^{10}$ years ago when the present known universe was started. These assumptions are based upon the theory that this radiation comes from the cosmos or outer space. Some ${ }^{246}$ present arguments for the sun as the source of the cosmic rays and argue that the magnetic field of the sun traps at least a part of the radiation from the sun, which give the results as now found on the earth. There are seemingly very great difficulties to explain away in establishing any one of these theories.

Owing to the effect of the earth's magnetic field there is less of this energy that reaches even the outer atmosphere at or near the magnetic equator than in higher latitudes, the lower-energy particles being screened off by the strong magnetic fields of the earth near the magnetic equator. The energy of the cosmic-ray particles that strike the upper atmosphere extends from about $10^{\circ}$ to $10^{17} \mathrm{ev}$, or even higher, with a maximum number for about $6 \times 10^{3} \mathrm{ev}$. The average energy of all particles entering the atmosphere at the equator is about $3 \times 10^{10} \mathrm{ev}$ and for geomagnetic latitudes above about 40 the average is about $6 \times 10^{3} \mathrm{ev}$.

In Tables 794 and 797 are given some data on the primary radiation reaching the outer atmosphere for different geomagnetic latitudes.

[^325]
## TABLE 794.-PROBABLE CHARACTERISTICS OF COSMIC RAYS FALLING UPON THE TOP OF THE ATMOSPHERE AT VARIOUS MAGNETIC LATITUDES

All energies are given in electron volts.

|  | Geomagnetic latitude |  |  |
| :---: | :---: | :---: | :---: |
|  | $3{ }^{\circ}$ | $39^{\circ}$ | $52^{\circ}$ |
| Energy falling per sec un each $\mathrm{cm}^{2}$ of the atmosphere.. | $1 \times 10^{9}$ | $1.7 \times 10^{0}$ | $3.2 \times 10^{9}$ |
| Total number of ions formed per sec below each $\mathrm{cm}^{2}$ of the upper surface of the atmosphere. | $3 \times 10^{7}$ | $5.4 \times 10^{7}$ | $7.4 \times 10^{7}$ |
| Low energy limit of oncoming particles imposed by the earth's magnetic field | $15 \times 10^{9}$ | $8 \times 10^{3}$ | $2 \times 10^{9}$ |
| Average energy per particle striking the atmosphere.. | $3 \times 10^{10}$ | $1.6 \times 10^{10}$ | . $88 \times 10^{10}$ |
| Probable number of particles striking each $\mathrm{cm}^{2}$ of outer surface of the atmosphere per min. | 1.9 | 6.5 | 21.8 |

The secondary cosmic rays, which are due to the ionization and other actions of the highenergy particles of the primary cosmic rays, have been studied by various methods for various positions with respect to the geomagnetic latitude on the earth's surface and for different elevations up to such heights that only about 0.5 percent of the atmosphere, by weight, is above the measuring instrument. The secondary rays consist of all sorts of particles such as electrons, both positive and negative; protons, and other heavy particles; mesons; neutrons, traveling with various speeds, and radiant energy of very short wavelength.

At the surface of the earth (sea level) the cosmic rays are of such intensity that they produce 1.63 ion pair $\mathrm{cm}^{-3} \mathrm{sec}^{-1}$. The intensity is about constant, within a very few percent, for geomagnetic latitudes higher than above 40 and from this point to the equator the intensity drop-off is about 9 percent.

The ionization increases with altitude up to about $16,000 \mathrm{~m}$ for geomagnetic latitudes $>40$, where it is about $150-200$ times as large as at sea level. Above this altitude the intensity of ionization drops off until, at an elevation where the amount of the atmosphere above the measuring instrument :s only about 0.5 percent ( $35,300 \mathrm{~m}$ ), the intensity is about 0.2 percent of that at the maximum, or about the same as that observed at 0.4 atmosphere above the earth. The variation with altitude is much less at the geomagnetic equator.

Cosmic rays react with the atoms of the atmosphere and produce a variety of effects; the production of a simple ion pair, the production of neutrons and electrons, the production of mesons, the production of extensive showers, where the released energy is so great that the cosmic ray must be only the cause of some explosion or some artificial disintegration. Mesons are particles that may have a unit positive or negative charge or they may be neutral as to charge. The mass of the meson is about 200 times that of an electron; it is very penetrating and is radioactive, with a life of about $2 \times 10^{-8} \mathrm{sec}$. Some evidence exists for mesons with a mass of about 1000 m .

Thus, there are formed bursts, an extensive production of ionization, and stars when a group of particles have a common origin as shown by cloud-chamber pictures. Stars are probably so named because these pictures show a number of tracks that have a common origin. These tracks vary from 2 to 10 with an average of about 4. The number of stars increases with the elevation above sea level. At an elevation of about $4,500 \mathrm{~m}$ the average energy ionization star particle was about 12 Mev .

Cosmic-ray showers, extensive ionizations of exceedingly complex reactions taking place in the atmosphere, extend over distances up to several hundred meters. These showers contain millions of particles and represent a total of about $10^{18} \mathrm{ev}$.

These secondary rays may be roughly divided into a hard and a soft component. The separation is generally made by filtering out the soft component with about 10 to 12 cm of lead. The hard component consists of mesons, a small number of protons, possibly some fast-moving electrons, and short-wavelength photons. The soft component consists of electrons, photons, and some slow-moving mesons, protons, and neutrons. The number of rays of the hard component does not reach a maximum with height but seems to increase to as great a height as measurements have been made, i.e., up to a height where the pressure is above 0.8 mmHg , where it is about 15 times as intense as at sea level. The soft component increases in intensity down from the top of the atmosphere to a pressure of 75 mmHg , then decreases to sea level, where the intensity is about 1 percent of that at its maximum. At its maximum intensity the soft component is about 5 times that of the hard component, in the vertical direction. At the earth's surface this hard component makes up about 75 percent of the cosmic radiation and a much smaller part at high altitudes. This hard component is very penetrating, since it will pass through many meters of water or lead. Cosmic rays have been detected in a mine at a depth of 384 meters, and by tipping the apparatus, the thickness through which the cosmic rays passed was equivalent to 1,408 meters of water (about 124 meters of lead!). Another observer detected this radiation in a coal mine at a depth of 610 meters, which is equivalent to 1,600 meters of water! In this case, the intensity measured at the depth corresponding to 1,600 meters of water was only about $1 / 20000$ of that at the surface! These highly penetrating rays are thought to be mesons, produced by the primary cosmic rays.

TABLE 796.-MEAN IONIZATION ENERGY OF $\gamma$-RAY NECESSARY TO PRODUCE AN ION PAIR*
(See Table 799.)

| Gas |  | ev | Gas |  | ev | Gas |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{H}_{2}$ | $\ldots \ldots$ | 33.0 | $\mathrm{~N}_{2}$ | $\ldots \ldots$ | $\ldots$ | 35.0 | Nev |
| He | $\ldots \ldots$ | 27.8 | $\mathrm{O}_{2}$ | $\ldots \ldots \ldots$ | 32.3 | $\ldots$ | 27.4 |

[^326]TABLE 797.-THE CRITICAL ENERGY* AND THE TOTAL ENERGY OF COSMIC RAYS ENTERING THE ATMOSPHERE AT FOUR LOCATIONS

| Location |  |  |  | Location |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Saskatoon | $60^{\circ}$ | 1.4 | 2.36 | San Antonio | $38^{\circ}$ | 6.7 | 1.81 |
| Omaha | $51^{\circ}$ | 2.9 | 2.25 | Madras | $3^{\circ}$ | 17.0 | . 94 |

* The energy of a cosmic ray which enables it to enter the earth's atmosphere.


## TABLE 798.—ESTIMATED COSMIC RAY INTENSITIES AT 50응 GEOMAGNETIC LATITUDE

In this table are given some data on cosmic rays for various altitudes for geomagnetic latitudes of $50^{\circ}$

| Altitude |  | Total intensity |  |  | Hard component |  |  | Soft component |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Omnidirec. tional | Vertical | Latitude effect | Omni-directional | Vertical | Latitude effect | Omnidirec. tional | Vertical | Latitude effect |
| meters | atm | sec $\mathrm{cm}^{2}$ | $\underline{\sec \mathrm{cm}^{2} \omega}$ | cent | $\frac{\mathrm{sec} \mathrm{cm}^{2}}{}$ | $\frac{\sec \mathrm{cm}^{2} \omega}{}$ | cent | sec cm ${ }^{2}$ | $\frac{\mathrm{sec} \mathrm{cm}^{2} \omega}{}$ | per- <br> cent |
| 0 | 1.000 | . 020 | . 015 | 10 | . 013 | . 009 | 10 | . 007 | . 006 | 10 |
| 2,000 | . 784 | . 035 | . 025 | 15 | . 018 | . 012 | 15 | . 017 | . 013 | 15 |
| 4,500 | . 570 | . 10 | . 07 | 25 | . 03 | . 020 | 25 | . 07 | . 05 | 25 |
| 10,000 | . 261 | . 7 | . 3 | 45 | . 10 | . 05 | 30 | . 6 | . 25 | 30 |
| 16,100 | . 100 | 1.5 | . 5 | 75 | . 25 | . 08 | ? | 1.25 | . 42 | 80 |
| 30,000 | . 0115 | . 5 | . 15 | 85 | . 4 | . 13 | ? | . 06 | . 02 | ? |
| $\infty$ | 0 | . 3 | . 1 | 90 | ? | ? | ? | ? | ? | ? |

TABLE 799.-SOME COSMIC-RAY DATA

| Total number of rays at top of the atmos | $8 \times 10^{17} \mathrm{sec}^{-1}$ |
| :---: | :---: |
| Total energy carried to earth per second (outer atmosphere) <br> $9 \times 10^{18} \mathrm{Bev} / \mathrm{sec}, 1.4 \times 10^{9}$ watts |  |
|  |  |
| a current of | .13 amp |
| Average number of rays ${ }^{\dagger}$ at top of atmosph | $.16 \mathrm{~cm}^{-2} \mathrm{sec}^{-1}$ |
| Average energy of all incident particles, latitude $>40$ | 7 Bev |
| Average energy of all incident particles, all areas, about | 11 Bev |
| Cosmic energy reaching earth's outer atmosphere, high latitude |  |
| Average energy of the cosmic rays entering the atmosphere is about | $7 \times 10^{9} \mathrm{ev}$ |
| The spectrum extends from about | $1 \times 10^{91}$ to $10^{17} \mathrm{ev}$ and probably higher |
| The energy required for the ionization found in a column |  |
| $1 \mathrm{~cm}^{2}$ in cross section extending to top of atmosphere |  |
| at 60 N geomagnetic latitude | $3.8 \times 10^{-8} \mathrm{erg} \mathrm{cm}^{-2} \mathrm{sec}^{-1}$ |
| Thus in this column there are for | $7.4 \times 10^{7}$ ion pairs |
| This means about...... | 90 ion pair, $\mathrm{cm}^{-1} \mathrm{sec}^{-1}$ |
| Total number of rays at sea level from all directio | 1.2 ray $\mathrm{min}^{-1} \mathrm{~cm}^{-2}$ |
| Cosmic ray at sea level produces $\ddagger$ | 1.63 ion pair, $\mathrm{cm}^{-3} \mathrm{sec}^{-1}$ |
| Total cosmic energy reaching earth per second at sea level. | 40 joules |
| Radiant energy flux reaching earth from all st | $3.02 \times 10^{-8} \mathrm{erg} \mathrm{cm}^{-2} \mathrm{sec}^{-1}$ |

[^327]TABLE 800.-RADIATION AT EARTH'S SURFACE, MASS AND RADIATION DENSITY IN OUR GALAXY, AND IN THE UNIVERSE

| Our galaxy: |  |
| :---: | :---: |
| Total number of stars | $30 \times 10^{\text {a }}$ |
| Average mass of stars | $2 \times 10^{38} \mathrm{~g}$ |
| Total mass of galaxy | $3.27 \times 10^{44} \mathrm{~g}$ |
| Total volume | $10^{08} \mathrm{~cm}^{3}$ |
| Diameter (disk) | $5 \times 10^{22} \mathrm{~cm}$ |
| Average mass density | $3 \times 10^{-24} \mathrm{~g} \mathrm{~cm}^{-3}$ |
| Total mass energy... | $2.95 \times 10^{88} \mathrm{ergs}$ |
| Total kinetic energy | $1.6 \times 10^{00} \mathrm{ergs}$ |
| Average mass-energy-density | $3 \times 10^{-8} \mathrm{erg} \mathrm{cm}^{-3}$ |
| Average kinetic energy-density | $1.6 \times 10^{-8} \mathrm{erg} \mathrm{cm}^{-8}$ |
| Universe: |  |
| Mass density | $3 \times 10^{-30} \mathrm{~g} \mathrm{~cm}^{-3}$ |
| Mass-energy-density | $3 \times 10^{-9} \mathrm{erg} \mathrm{cm}^{-8}$ |
| Radiant-energy-density | $6 \times 10^{-18} \mathrm{erg} \mathrm{cm}{ }^{-8}$ |
| Cosmic ray energy-density | $1.7 \times 10^{-11} \mathrm{erg} \mathrm{cm}^{-8}$ |
| At earth's surface (top of atmosphere) : |  |
| Total radiant energy from all stars. | $1.78 \times 10^{-8} \mathrm{erg} \mathrm{cm}^{-2} \mathrm{sec}^{-1}$ |
| Total radiant energy density (our galaxy) | $5.8 \times 10^{-14} \mathrm{erg} \mathrm{cm}^{-3}$ |
| Total radiant energy (sun directly overhead)* | $1.2 \times 10^{8} \mathrm{erg} \mathrm{cm}^{-2} \mathrm{sec}^{-1}$ |
| Cosmic ray energy | $3.8 \times 10^{-8} \mathrm{erg} \mathrm{cm}^{-2} \mathrm{sec}^{-1}$ |
| Cosmic ray energy-density | $10^{-18} \mathrm{erg} \mathrm{cm}{ }^{-8}$ |

[^328]
## TABLE 801.-COMPOSITION OF COSMIC RADIATION AT GEOMAGNETIC LATITUDE $30^{\circ} 247$

| Nuclei | Relative No. of particles |  |  | Nuclei | Relative No. of particles |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Sun | $\tau$ Sco | Cosmic rays |  | Sun | $\tau$ Sco | Cosmic rays |
| H |  | $1.6 \times 10^{8}$ | $1.6 \times 10^{8}$ | $11 \leqslant Z \leqslant 14$ | 157 | 215 | $\sim 2600$ |
| He |  | $2.9 \times 10^{5}$ | $4.0 \times 10^{5}$ | $16 \leqslant 2 \leqslant 20$ | 28 | 5 | $\sim 1000$ |
| $6 \leqslant 2 \leqslant 8$ | 3200 | 2500 | 14000 | Fe | 150 |  | $\sim 400$ |

[^329]
## TABLE 802.-ACCELERATION OF GRAVITY

For sea-level and different latitudes. Calculated from the International Gravity Formuia:
$g=978.0490\left[1+0.0052884 \sin ^{2} \phi-0.0000059 \sin ^{2} 2 \phi\right]$

| $\begin{gathered} \text { Latitude } \\ \hline \end{gathered}$ | $\stackrel{g}{\mathrm{~cm} / \mathrm{sec}^{2}}$ | $\log g$ | $\stackrel{g}{\mathrm{ft} / \mathrm{sec}^{2}}$ | $\underset{\phi}{\text { Latitude }}$ | $\stackrel{g}{\mathrm{~cm} / \mathrm{sec}^{2}}$ | $\log g$ | $\stackrel{g}{\mathrm{ft} / \mathrm{sec}^{2}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | 978.0490 | 2.9903607 | 32.08 | $50^{\circ}$ | $981.0786^{2}$ | 2.9917038 | 32.19 |
| 5 | . 0881 | . 9903780 | . 09 | 51 | . 1673 | . 9917431 | . 19 |
| 10 | . 2043 | . 9904296 | . 09 | 52 | . 2554 | . 9917821 | . 19 |
| 12 | . 2716 | . 9904594 | . 09 | 53 | . 3427 | . 9918207 | . 20 |
| 14 | . 3504 | . 9904944 | . 10 | 54 | . 4291 | . 9918589 | . 20 |
| 15 | 978.3940 | . 9905138 | 32.10 | 55 | 981.5146 | . 9918968 | 32.20 |
| 16 | . 4404 | . 9905344 | . 10 | 56 | . 5990 | . 9919341 | . 20 |
| 17 | . 4893 | . 9905561 | . 10 | 57 | . 6822 | . 9919709 | -. 21 |
| 18 | . 5409 | . 9905790 | . 10 | 58 | . 7642 | . 9920072 | . 21 |
| 19 | . 5951 | . 9906031 | . 11 | 59 | . 8448 | . 9920428 | . 21 |
| 20 | 978.6517 | . 9906281 | 32.11 | 60 | 981.9239 | . 9920778 | 32.21 |
| 21 | . 7107 | . 9906543 | . 11 | 61 | 982.0015 | . 9921122 | . 22 |
| 22 | . 7721 | . 9906815 | . 11 | 62 | . 0773 | . 9921457 | . 22 |
| 23 | . 8357 | . 9907098 | . 11 | 63 | . 1515 | . 9921785 | . 22 |
| 24 | . 9015 | . 9907390 | . 12 | 64 | . 2238 | . 9922105 | . 22 |
| 25 | 978.9694 | . 9907691 | 32.12 | 65 | 982.2941 | . 9922415 | 32.23 |
| 26 | 979.0394 | . 9908001 | . 12 | 66 | . 3624 | . 9922718 | . 23 |
| 27 | . 1113 | . 9908321 | . 12 | 67 | . 4287 | . 9923010 | . 23 |
| 28 | . 1850 | . 9908648 | . 12 | 68 | . 4927 | . 9923293 | . 23 |
| 29 | . 2606 | . 9908983 | . 13 | 69 | . 5545 | . 9923567 | . 24 |
| 30 | 979.3378 | . 9909325 | 32.13 | 70 | 982.6139 | . 9923829 | 32.24 |
| 31 | . 4165 | . 9909674 | . 13 | 71 | . 6709 | . 9924081 | . 24 |
| 32 | . 4968 | . 9910030 | . 14 | 72 | . 7254 | . 9924322 | . 24 |
| 33 | . 5785 | . 9910392 | . 14 | 73 | . 7774 | . 9924552 | . 24 |
| 34 | . 6614 | . 9910760 | . 14 | 74 | . 8267 | . 9924769 | . 24 |
| 35 | 979.7455 | . 9911133 | 32.14 | 75 | 982.8734 | . 9924976 | 32.25 |
| 36 | . 8308 | . 9911511 | . 15 | 76 | . 9173 | . 9925170 | . 25 |
| 37 | . 9170 | . 9911893 | . 15 | 77 | . 9585 | . 9925351 | . 25 |
| 38 | 980.0041 | . 9912279 | . 15 | 78 | . 9968 | . 9925521 | . 25 |
| 39 | . 0919 | . 9912668 | . 15 | 79 | 983.0322 | . 9925678 | . 25 |
| 4.1 | 980.1805 | . 9913060 | 32.15 | 80 | 983.0647 | . 9925821 | 32.25 |
| 41 | . 2696 | . 9913455 | . 16 | 81 | . 0942 | . 9925951 | . 25 |
| 42 | . 3591 | . 9913852 | . 16 | 82 | . 1207 | . 9926068 | . 25 |
| 43 | . 4490 | . 9914250 | . 17 | 83 | . 1442 | . 9926172 | . 25 |
| 44 | . 5391 | . 9914649 | . 17 | 84 | . 1645 | . 9926262 | . 26 |
| 45 | 980.6294 | . 9915049 | 32.17 | 85 | 983.1818 | . 9926338 | 32.26 |
| 46 | . 7197 | . 9915449 | . 18 | 86 | . 1960 | . 9926402 | . 26 |
| 47 | . 8098 | . 9915848 | . 18 | 87 | . 2071 | . 9926450 | . 26 |
| 48 | . 8998 | . 9916246 | . 18 | 88 | . 2150 | . 9926485 | . 26 |
| 49 | . 9894 | . 9916643 | . 18 | 90 | 983.2213 | . 9926513 | . 26 |

## TABLE 803.-FREE-AIR CORRECTION OF ACCELERATION OF GRAVITY FOR ALTITUDE

To reduce $\log g$ ( cm per sec per sec) to $\log g$ ( ft per sec per sec) add $\log 0.03280833=$ $8.5159842-10$.

The standard value of gravity, used in barometer reductions, etc., is 980.665 . It was adopted by the International Committee on Weights and Measures in 1901. It corresponds nearly to latitude $45^{\circ}$ sca-level.
$-0.0003086 \mathrm{~cm} \mathrm{sec}^{-2} \mathrm{~m}^{-1}$ when altitude is in meters.
$-0.000003086 \mathrm{ft} \mathrm{sec}^{-2} \mathrm{ft}^{-1}$ when altitude is in feet.

| Altitude | Correction | Altitude | Correction |
| :---: | :---: | :---: | :---: |
| 200 m | $-.0617 \mathrm{~cm} / \mathrm{sec}^{2}$ | 200 ft | $-.000617 \mathrm{ft} / \mathrm{sec}^{2}$ |
| 300 | .0926 | 300 | .000926 |
| 400 | .1234 | 400 | .001234 |
| 500 | .1543 | 500 | .001543 |
| 600 | .2162 | 600 | .001852 |
| 700 | .2469 | 700 | .002160 |
| 800 | .2777 | 800 | .002469 |
| 900 |  | 900 | .002777 |

[^330]TABLE 804.-ACCELERATION OF GRAVITY, VARIOUS WORLD STATIONS

| Name | Latitude | Longitude | Elevation meters | Gravity, ${ }_{\text {cm } / \mathrm{sec}^{2}}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Observed | Reduced to sea level |
| Santiago, Chile | 33²7.1 S | $70^{\circ} 39^{\prime} 8 \mathrm{~W}$ | 541.3 | 979.429 | 979.596 |
| Rio, Brazil | 2253.7 S | 4313.4 W | 29.0 | 978.805 | 978.814 |
| Tacna, Peru | 1801.0 S | 7015.0 W | 557.1 | 978.298 | 978.470 |
| Chala, Peru | 1549.0 S | 7418.5 W | 14.0 | 978.452 | 978.456 |
| Lima, Peru | 1201.1 S | 7702.3 W | 143.6 | 978.289 | 978.333 |
| Minkindani, E. Africa | 1016.6 S | 4007.6 E | , | 978.224 | 978.225 |
| Timor Sea | 936 S | 12807 E | - 340 | 978.233 | 978.233 |
| Trujillo, Peru | 807.0 S | 7902.3 W | 29.4 | 978.095 | 978.104 |
| Mafia, E. Afric | 754.9 S | 3939.4 E | 5 | 978.168 | 978.169 |
| Indian Ocean | 735 S | 10655 E | - 230 | 978.292 | 978.292 |
| Kaliwa, E. Afri | 504.2 S | 3147.5 E | 1080 | 977.783 | 978.116 |
| Banda Sea | 145 S | 12657 E | -1390 | 978.058 | 978.058 |
| Limuru, E. Africa | 107 S | 3640 E | 2193 | 977.412 | 978.089 |
| Marigal, E. Africa | 028 N | 3559 E | 1036 | 977.664 | 977.984 |
| Kanifuri, India | 522.2 N | 7319.2 E | 1 | 978.107 | 978.107 |
| Indian Ocean | 756 N | 6846 E | -4390 | 978.102 | 978.102 |
| Punalur, India | 901.0 N | 7655.8 E | 34 | 978.107 | 978.117 |
| Pacific Ocean | 952 N | 13246 E | -6050 | 978.212 | 978.212 |
| Pacific Ocean | 1335 N | 9527 W | -3870 | 978.360 | 978.360 |
| Dharwar, India | 1527.6 N | 7500.2 E | 728 | 978.183 | 978.407 |
| Musmar, E. Africa | 1813.0 N | 3558. | 493 | 978.399 | 978.551 |
| Tacubaya, Mexico | 1924.3 N | 9911.7 W | 2299 | 977.941 | 978.650 |
| Pacific Ocean . . | 1958 N | 16456 W | -4960 | 978.660 | 978.660 |
| Atlantic Ocean | 2044 N | 6537 W | -5510 | 978.704 | 978.704 |
| Santiago, Cuba | 2230.9 N | 8030.4 W | 67 | 978.826 | 978.847 |
| Atlantic Ocean | 2321 N | 4705 W | -3550 | 978.880 | 978.880 |
| Key West, Fla | 2433.6 N | 8148.4 W |  | 978.973 | 978.973 |
| Dholpur, India | 2642.0 N | 7754.8 E | 176 | 978.999 | 979.054 |
| Nagasaki, Japan | 3244.7 N | 12952.2 E | 30 | 979.594 | 979.603 |
| Mount Wilson, Ca | 3413.4 N | 11803.4 W | 1719.4 | 979.253 | 979.783 |
| Batna, Algeria | 3533.0 N | 610 E | 1050 | 979.468 | 979.792 |
| Atlantic Ocean | 3623 N | 2643 W | -3610 | 979.890 | 979.890 |
| Sevilla, Spain | 3723.0 N | 559.5 W | 11 | 979.965 | 979.968 |
| Denver, Colo. | 39406 N | 10457.1 W | 1639.5 | 979.612 | 980.118 |
| Buffalo, N. Y | 4257.1 N | 7849.3 W | 210 | 980.363 | 980.428 |
| Atlantic Ocean | 4314 N | 1936 W | -4100 | 978.520 | 978.520 |
| Ottawa, Ontario | 4523.6 N | 7543.0 W | 83 | 980.622 | 980.648 |
| Müchen, Germany | 4809 N | 1137 E | 525 | 980.733 | 980.895 |
| Greenwich, England | 5128.6 N | 000.3 E | 47 | 981.189 | 981.204 |
| Saskatoon, Saskatchewan | 5207.8 N | 10638.1 W | 497 | 981.138 | 981.291 |
| Vladimirskaja, Siberia | 5457 N | 8559 E | 265 | 981.424 | 981.506 |
| Tomsk, Siberia ........ | 5628 N | 8457 E | 125 | 981.582 | 981.621 |
| Oslo, Norway | 5954.7 N | 1043.5 E | 28 | 981.927 | 981.936 |
| St. Michael, Alaska | 6328.5 N | 16202.4 W | 1 | 982.197 | 982.197 |
| Arctic Red River. N. T | 6726.6 N | 13344.3 W | 41 | 982.438 | 982.451 |
| Whales Point, Spitzbergen | 7730.4 N | 2058.8 E | 458 | 982.897 | 983.038 |
| Hellwald, Spitzbergen | 7844.1 N | 2050.2 E | 660 | 982.871 | 983.075 |
| Ile de Rosse ........ | 8049.6 N | 2020.6 E | 31 | 983.145 | 983.155 |
| Arctic Ocean | 8148 N | 1925 E | -3402 | 983.096 | 983.096 |

[^331]
## TABLE 805.-ACCELERATION OF GRAVITY ( $g$ ) IN THE UNITED STATES

The following table is abridged from the table of Principal Facts in U. S. Coast and Geodetic Survey Special Publication No. 244, Pendulum Gravity Data in the United States. The observed values depend on relative determinations and on an adopted value of 980.118 for the Commerce Building Base in Washington, D. C.

There are also given two types of gravity anomalies. The free-air anomaly is the difference between the observed value of gravity and the theoretical values of gravity for the latitude of the station corrected for the elevation of the station. The isostatic anomaly is the difference between the observed values of gravity and the theoretical value of gravity for the latitude of the station corrected for the elevation of the station, topography and isostatic compensation in the earth's crust to a depth of 113.7 kilometers.

| Station | Latitude | Longitude | Elevation | Observed gravity gal | $\begin{aligned} & \text { Free-air } \\ & \text { anomaly } \end{aligned}$ gal | Isostatic anomaly gal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Atlanta, Ga. | $33^{\circ} 45.3$ | $84^{\circ} 23.5$ | 324.0 | 979.527 | -. 014 | -. 030 |
| Austin, Tex. (university) | 3017.2 | 9744.2 | 189 | 979.286 | -. 016 | -. 017 |
| Baltimore, Md. | 3917.8 | 7637.3 | 30.5 | 980.114 | +. 005 | +. 002 |
| Beaufort, N. | 3443.1 | 7639.8 | 1.5 | 979.732 | +. 011 | -. 026 |
| Birmingham, Ala | 3330.8 | 8648.8 | 179 | 979.539 | -. 027 | -. 038 |
| Bismarck, N. Da | 4648.5 | 10047.1 | 514.4 | 980.628 | -. 006 | -. 001 |
| Boise, Idaho | 4337.2 | 11612.3 | 822.0 | 980.215 | -. 036 | +. 010 |
| Boston, Mass | 4221.6 | 7103.8 | 22 | 980.399 | $+.014$ | +. 002 |
| Burbank, Okla | 3642.2 | 9641.0 | 345 | 979.788 | $+.003$ | -. 001 |
| Calais, Maine | 4511.2 | 6716.9 | 38 | 980.634 | . 000 | -. 008 |
| Cambridge, Mas | 4222.8 | 7107.8 | 14 | 980.401 | +. 012 | +. 001 |
| Charleston, S. C. | 3247.2 | 7956.0 | 6.1 | 979.549 | -. 010 | -. 026 |
| Charlottesville, Va. | 3802.0 | 7830.3 | 166 | 979.941 | -. 015 | -. 017 |
| Chicago, IIl. | 4147.4 | 8735.9 | 182 | 980.281 | -. 003 | -. 004 |
| Cincinnati, Ohio | 3908.3 | 8425.3 | 245 | 980.007 | -. 022 | -. 024 |
| Cleveland, Ohio | 4130.4 | 8136.6 | 210 | 980.244 | -. 006 | -. 006 |
| Cloudland, Tenn. | 3606.2 | 8207.9 | 1890 | 979.386 | +. 129 | -. 001 |
| Colorado Springs, Colo | 3850.8 | 10449.5 | 1841.8 | 979.493 | -. 017 | -. 008 |
| Columbus, Ga. | 3227.0 | 8457.6 | 73.5 | 979.526 | +. 015 | +. 014 |
| Columbus, Ohio | 3957.8 | 8259.4 | 231.0 | 980.092 | -. 014 | -. 014 |
| Denver, Colo. | 3940.6 | 10457.1 | 1639.5 | 979.612 | -. 034 | -. 016 |
| Duluth, Minn. | 4647.0 | 9206.4 | 215.8 | 980.761 | +. 037 | +. 048 |
| Durham, N. | 3600.2 | 7856 | 126 | 979.838 | +. 046 | $+.034$ |
| El Paso, Te | 3146.3 | 10629.0 | 1146.0 | 979.127 | +. 002 | +. 009 |
| Empire State Building, | 4044.9 | 7359.2 | 16.2 | 980.269 | +. 027 | +. 020 |
| Eugene, Oreg | 4402.7 | 12305.6 | 129 | 980.493 | -. 010 | +. 005 |
| Fort Dodge, Iowa | 4230.8 | 9411.4 | 340.1 | 980.314 | +. 014 | +. 011 |
| Grand Canyon, Ariz | 3605.3 | 11206.8 | 847.0 | 979.466 | -. 111 | -. 014 |
| Grand Canyon, Wyo | 4443.7 | 11029.7 | 2386.0 | 979.902 | +. 033 | -. 002 |
| Grand Rapids, Mich | 4258.0 | 8539.5 | 235.8 | 980.375 | +. 002 | -. 004 |
| Green River, Uta | 3859.4 | 11009.9 | 1243 | 979.639 | -. 068 | -. 025 |
| Iowa City, Iowa | 4139.6 | 9132.2 | 212.3 | 980.250 | -. 013 | -. 012 |
| Ithaca, N. Y. | 4227.1 | 7629.0 | 246.9 | 980.303 | $-.020$ | -. 022 |
| Key West, Fla. | 2433.6 | 8148.4 | 1 | 978.973 | $+.034$ | -. 011 |
| Knoxville, Tenn. | 3557.7 | 8355 | 280 | 979.715 | -. 027 | -. 026 |
| Lancaster, N. H. | 4429.5 | 7134.3 | 261.8 | 980.489 | -. 014 | -. 014 |
| Las Vegas, N. Me | 3535.8 | 10513.1 | 1959.6 | 979.207 | $+.015$ | -. 003 |
| Little Rock, Ark | 3444.9 | 9216.4 | 89.0 | 979.724 | +. 027 | +. 028 |
| Madison, Wis. | 4304.6 | 8924.0 | 270 | 980.368 | -. 005 | -. 008 |
| Memphis, Tenn. | 3508.7 | 9003.3 | 80.3 | 979.743 | +. 010 | +. 008 |
| Miles City, Mon | 4624.2 | 10550 | 718 | 980.542 | +. 008 | +. 028 |
| Minneapolis, Minn | 4458.7 | 9313.9 | 256.1 | 980.600 | +. 052 | +. 055 |
| Mitchell, S. Dak | 4341.8 | 9801.8 | 408 | 980.378 | -. 003 | -. 002 |
| Mount Hamilton, Calif | 3720.4 | 12138.6 | 1281.7 | 979.663 | +. 112 | -. 004 |
| New Orleans, | 2956.9 | 9004.3 | 2.4 | 979.326 | -. 007 | -. 020 |
| New York, N. | 4048.5 | 7357.7 | 38.1 | 980.270 | +. 029 | +. 019 |
| Oberlin, Ohio | 4117.5 | 8213.2 | 248 | 980.208 | -. 011 | -. 013 |
| Philadelphia, Pa | 3957.1 | 7511.7 | 15.8 | 980.199 | +. 028 | +. 018 |
| Pike's Peak, Col | 3850.4 | 10502.5 | 4293.1 | 978.957 | +. 203 | +. 018 |
| Pittsburgh, Pa. | 4027.4 | 8000.6 | 235 | 980.121 | -. 027 | -. 027 |
| Prestonsburgh, Ky. | 3740.6 | 8245.6 | 193 | 979.884 | -. 032 | -. 028 |
| Princeton, N. J.. | 4021.0 | 7439.5 | 64.0 | 980.181 | -. 011 | -. 025 |

(continued)

# TABLE 805.-ACCELERATION OF GRAVITY (g) IN THE UNITED STATES (concluded) 

| Station | Latitude | Longitude | $\begin{gathered} \text { Elevation } \\ m \end{gathered}$ | Observed gravity gal | Free-air anomaly anomal | Isostatic anomaly <br> ga! |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Richmond, Va. | $37^{\circ} 32.2$ | $77^{\circ} 26{ }^{\prime} 1$ | 29.9 | 979.963 | +. 009 | . 000 |
| St. Louis, Mo. | 3838.0 | 9012.2 | 153.9 | 980.004 | -. 008 | -. 007 |
| St. Petersburg, F | 2748.9 | 8240.2 | 15 | 979.191 | $+.025$ | +.006 |
| Salt Lake City, Utah | 4046.1 | 11153.8 | 1322 | 979.806 | -. 035 | +. 006 |
| San Francisco, Calif. | 3737.5 | 12225.7 | 114.3 | 979.968 | +. 018 | -. 022 |
| Seattle, Wash. (university) | 4739.6 | 12218.3 | 58 | 980.736 | -. 115 | -. 095 |
| Sheridan, Wyo. | 4448.0 | 10658.7 | 1149.9 | 980.244 | -. 012 | +. 010 |
| Smith College, Mas | 4219.0 | 7238.2 | 54.6 | 980.376 | $+.005$ | +. 006 |
| State College, Pa. | 4047.9 | 7751.8 | 357.8 | 980.127 | +. 014 | $\pm .014$ |
| Terre Haute, Ind. | 3928.7 | 8723.8 | 150.9 | 980.075 | -. 013 | -. 011 |
| Traverse City, Mich. | 4445.8 | 8537.2 | 180.1 | 980.553 | +. 001 | $+.001$ |
| Washington, D. C.: |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Geophysical Laboratory | 3856.6 | 7703.4 | 88.1 | 980.104 | $\dot{+} .044$ | $+.036$ |
| National Bureau of Standar | 3856.5 | 7703.9 | 95.1 | 980.100 | $+.042$ | +. 034 |
| Smithsonian Institution | 3853.3 | 7701.5 | 10.4 | 980.118 | +. 039 | +. 038 |
| Wheeling, W. Va... | 4004.0 | 8043.3 | 205 | 980.088 | -. 035 | -. 032 |
| Winnemucca, Nev. | 4058.4 | 11743.8 | 1311 | 979.847 | -. 016 | -. 012 |
| Worcester, Mass. | 4216.5 | 7148.5 | 170.0 | 980.328 | -. 003 | -. 022 |
| Wright Field, Ohio | 3946.6 | 8405.9 | 247.8 | 980.094 | +. 010 | +. 008 |
| Yuma, Ariz. . | 3243.3 | 11437.0 | 53.9 | 979.532 | -. 007 | +. 006 |

TABLE 806.-LENGTH OF SECONDS PENDULUM AT SEA LEVEL AND FOR DIFFERENT LATITUDES

|  | Length <br> cm | Log | Length <br> in. | Log | Lat <br> Lathgth <br> cm | Log | Length <br> in. | Log |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ}$ | 99.097 | 1.996061 | 39.014 | 1.591221 | $50^{\circ}$ | 99.404 | 1.997404 | 39.135 | 1.592565 |
| 5 | 99.101 | 1.996078 | 39.016 | 1.591243 | 55 | 99.449 | 1.997597 | 39.153 | 1.592765 |
| 10 | 99.113 | 1.996131 | 39.020 | 1.591287 | 60 | 99.490 | 1.99778 | 39.169 | 1.592943 |
| 15 | 99.132 | 1.996215 | 39.028 | 1.591376 | 65 | 99.527 | 1.997942 | 39.184 | 1.593109 |
| 20 | 99.158 | 1.996329 | 39.038 | 1.591488 | 70 | 99.560 | 1.998084 | 39.196 | 1.593242 |
| 25 | 99.190 | 1.996469 | 39.051 | 1.591632 | 75 | 99.586 | 1.998198 | 39.207 | 1.593364 |
| 30 | 99.228 | 1.996633 | 39.066 | 1.591799 | 80 | 99.605 | 1.998283 | 39.214 | 1.593441 |
| 35 | 99.269 | 1.996814 | 39.082 | 1.591977 | 85 | 99.618 | 1.998335 | 39.219 | 1.593497 |
| 40 | 99.313 | 1.997006 | 39.099 | 1.592166 | 90 | 99.622 | 1.998352 | 39.221 | 1.593519 |
| 45 | 99.359 | 1.997205 | 39.117 | 1.592366 |  |  |  |  |  |

Calculated from Table 802 by the formula $l=g / \pi^{2}$. For each 100 ft of elevation subtract 0.000953 cm or 0.000375 in . or 0.0000313 ft . This table could also have been computed by either of the following formulas derived from the gravity formula at the top of Table 802.
$l=0.990961\left(1+0.0052884 \sin ^{2} \phi-0.0000059 \sin ^{2} 2 \phi\right)$ meters.
$l=0.990961+.0052406 \sin ^{2} \phi-0.0000058 \sin ^{2} 2 \phi$, meters.
$l=39.014135\left(1+0.0052884 \sin ^{2} \phi-0.000059 \sin ^{2} 2 \phi\right)$ inches.
$l=39.014135+0.203214 \sin ^{2} \phi-0.0002302 \sin ^{2} 2 \phi$, inches.

The departures are from values of gravity normally expected, from Table 802.

| Latitude | Longitude | Elevation meters * | Gravity $\mathrm{cm} / \mathrm{sec}^{2}$ | Departure from values of table | Place |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $19^{\circ} 29.8 \mathrm{~N}$ | $155^{\circ} 34.8 \mathrm{~W}$ | 3970 | 978.096 | +698 | Mauna Loa |
| 1942.2 N | 155 27.9 W | 2030 | 978.504 | $+495$ | Kalaieha |
| 1925.4 N | 15515.7 W | 1211 | 978.673 | $+428$ | Kilavea |
| 2347.0 N | 16612.5 W | 2 | 979.201 | +315 | East Island |
| 3221 N | 6440 W | 2 | 979.806 | $+282$ | St. Georges |
| 3730.0 N | 2 45.0 W | 858 | 979.669 | +265 | Baza |
| 3806.7 N | 304.5 W | 805 | 979.792 | $+248$ | Villacarrillo |
| 4255.8 N | 008 E | 2877 | 979.779 | +224 | Pic du Midi |
| 3711.0 N | 3 36.0 W | 669 | 979.669 | +206 | Granada |
| 4550 N | 652 E | 4807 | 979.401 | +180 | Mont Blanc |
| 4557.5 N | 748.9 E | 2797 | 980.019 | +166 | Bétempshütte |
| 4559.5 N | 742.7 E | 2582 | 980.080 | +157 | Schwarzsee |
| 6753.6 N | 1302.0 E | 19 | 982.622 | +142 | Sörvaagen |
| 3348.5 N | 7433.3 E | 3338 | 978.752 | +133 | Korag |
| 5148 N | 1037 E | 1140 | 981.015 | +129 | Brocken |
| 3544.5 N | 1539.5 E | - 460 | 979.926 | +118 | Mediterranean Sea |
| 4038 N | 1757 E | 16 | 980.337 | +107 | Brindisi |
| 2306.1 N | 7458.5 W | 2 | 978.941 | +100 | Clarence Town |
| 4208 N | 4142 E | 3 | 980.317 | -53 | Poti |
| 4621.9 N | 907.6 E | 1030 | 980.374 | -61 | Augio |
| 5608.0 N | 9118.0 E | 339 | 981.435 | - 70 | Kosulka |
| 814 S | 3035 E | 783 | 977.835 | - 78 | Moliro |
| 3019.5 N | 7803.4 E | 683 | 979.063 | - 89 | Dehra Dun |
| 5030.2 N | 11603.4 W | 828 | 980.767 | -100 | Invermere |
| 150 N | 3119 E | 623 | 977.753 | -109 | Butiaba |
| 750 S | 12048 E | -5140 | 978.024 | -121 | Java Sea |
| 512 N | 9412 E | -2555 | 977.962 | -129 | Indian Ocean |
| 4026 N | 5000 E | 57 | 980.065 | -136 | Surachany |
| 848 S | 12826 E | -2120 | 978.019 | -151 | Timor Sea |
| 2641.8 N | 8824.8 E | 118 | 978.887 | -166 | Siliguri |
| 209 N | 12659 E | -2200 | 977.877 | -179 | Celebes Sea |
| 1017 N | 12641 E | -8740 | 978.013 | -200 | Philippine Sea |
| 029 S | 12559 E | -2390 | 977.833 | -216 | Celebes Sea |
| 536 S | 13108 E | -7330 | 977.843 | -255 | Banda Sea |
| 1932 N | 6646 W | -8040 | 978.284 | -341 | Atlantic Ocean |

[^332]
## TABLE 808.-THE SOLAR CONSTANT

A long series of measurements has been made ${ }^{289}$ at widely separated, selected stations by the astrophysicists of the Smithsonian Institution on both the total intensity of the solar radiation and the spectral distribution of this radiation. One result of these measurements is the value of the solar constant, that is, the total solar radiation (cal $\mathrm{cm}^{-2} \mathrm{~min}^{-1}$ ) at normal incidence outside the atmosphere at the mean solar distance. As a result of the work up to 1913 the solar constant was found to be $1.9408 \mathrm{ly} . \mathrm{min}^{-1}$ (langley ; see Table 2, Part 2). .Later investigations ${ }^{250}$ showed that the standard used in these measurements was somewhat in error. Observations showed that the correction employed for the unmeasured ultraviolet radiation was too low; also solar radiation in the infrared region beyond about $2.5 \mu$ introduced some error. As a final result of all the corrections it was found that this 1913 value of the solar constant was very good. It should be pointed out that there is evidence ${ }^{240}$ that the solar constant fluctuates as much as $\pm 1.5$ percent. In addition, the varying distance between the sun and earth (see Table 827) produces a change in the actual solar radiation at the top of the atmosphere of about $\pm 3.5$ percent from the mean value. Now in 1951 the value of the solar constant (amount of energy falling at normal incidence on one square centimeter per minute on body at earth's mean distance) $=1.946$ calories $=$ mean 6430 determinations 1924-47. Subject to variations, usually within the range of 2.8 percent, and occurring irregularly in periods of a week or 10 days. New data on the ultraviolet and infrared corrections to the solar constant given by F. S. Johnson (in press) indicate that the value 1.946 should be increased by 2.6 percent. Johnson's best value is $2.00 \pm 2$ percent.
Computed effective temperature of the sun: from form of blackbody curves, $6000^{\circ}$ to $7000^{\circ}$ Absolute; from $\lambda_{\text {max }} T=2930$ and $\max =0.470 \mu, 6230^{\circ}$; from total radiation, $J=$ $76.8 \times 10^{-12} \times T^{4}, 5830$ :

| Sun radiates | $\begin{aligned} & 3.8 \times 10^{38} \mathrm{erg} / \mathrm{sec}^{-1} \mathrm{coc}^{-2} \times 10^{10} \mathrm{erg} \mathrm{sec}^{-1} \mathrm{~cm}^{-2} \end{aligned}$ |
| :---: | :---: |
| of this | $1.72 \times 10^{24} \mathrm{erg} / \mathrm{sec}$ strikes the eart |

[^333]TABLE 809.-ATMOSPHERIC TRANSMISSION COEFFICIENTS

| $\underset{\mu}{\substack{\text { Wave. } \\ \text { length } \\ \mu}}$ | Montezuma, Chile |  | Table Mt., Calif. |  | $\begin{gathered} \text { Miami, } \\ \text { Fla. } \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | High | Low | High | Low | High | Low |
| . 34 | . 620 | . 568 | . 605 | . 552 | . 512 | . 464 |
| . 35 | . 656 | . 600 | . 641 | . 585 | . 541 | . 492 |
| . 36 | . 687 | . 630 | . 672 | . 615 | . 567 | . 519 |
| . 37 | . 714 | . 657 | . 701 | . 643 | . 593 | . 545 |
| . 38 | . 738 | . 681 | . 726 | . 668 | . 617 | . 571 |
| . 39 | . 759 | . 703 | . 749 | . 692 | . 642 | . 595 |
| . 40 | . 778 | .722 | . 769 | . 712 | . 662 | . 615 |
| . 45 | . 848 | . 792 | . 840 | . 783 | . 755 | . 709 |
| . 50 | . 890 | . 838 | . 883 | . 831 | . 818 | . 764 |
| . 55 | . 900 | . 849 | . 890 | . 838 | . 850 | . 788 |
| . 60 | . 913 | . 863 | . 905 | . 854 | . 873 | . 814 |
| . 65 | . 936 | . 884 | . 933 | . 880 | . 925 | . 872 |
| . 70 | . 963 | . 924 | . 961 | . 922 | . 935 | . 890 |
| . 75 | . 972 | . 936 | . 970 | . 934 | . 943 | . 902 |
| . 80 | . 980 | . 945 | . 978 | . 943 | . 949 | . 911 |
| . 85 | . 984 | . 952 | . 983 | . 950 | . 954 | . 917 |
| . 90 | . 985 | . 956 | . 984 | . 954 | . 957 | .922 |
| . 95 | . 986 | . 957 | . 985 | . 956 | . 960 | . 925 |
| 1.00 | . 987 | . 958 | . 986 | . 957 | . 962 | . 928 |
| 1.25 | . 989 | . 960 | . 989 | . 959 | . 964 | . 933 |
| 1:50 | . 994 | . 965 | . 994 | . 968 | . 969 | .942 |
| 1.75 | . 997 | . 970 | . 997 | . 970 | . 973 | . 946 |
| 2.00 | . 996 | . 975 | . 996 | . 974 | . 969 | . 945 |
| 2.25 | . 988 | . 970 | . 987 | . 965 | . 955 | . 930 |

High transmissions are for every clear day and low precipitable water, 2 mm for Montezuma and Table Mt., and 3.5 mm for Miami.
Low transmissions are for very hazy days and high precipitable water, 10 mm for Montezuma and Table Mt., and 25 mm for Miami.
Transmission coefficients in the range $.70-2.25 \lambda$ are all smooth-curve values drawn over the tops of the water-vapor bands.
Unit air mass.

TABLE 810.-THE SOLAR CONSTANT, MONTHLY AND YEARLY MEANS*

Jan. Feb. Mar. Apr. May June July Aug. Sept. Oct. Nov. Dec. mean

| 1920 |  |  |  |  |  |  |  | 1.945 | 1.950 | 1.953 |  |  |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 21 | 1.957 | 1.955 | 1.949 | 1.947 | 1.950 | 1.939 | 1.950 | 1.943 | 1.950 | 55 | 57 | 52 | 1.950 |
| 22 | 47 | 46 | 36 | 30 | 30 | 18 | 14 | 21 | 17 | 25 | 26 | 24 | 28 |
| 23 | 42 | 29 | 32 | 31 | 36 | 28 | 36 | 34 | 53 | 45 | 44 | 43 | 38 |
| 24 | 44 | 41 | 47 | 42 | 50 | 52 | 51 | 46 | 47 | 52 | 53 | 50 | 48 |
| 25 | 46 | 55 | 50 | 50 | 48 | 48 | 49 | 47 | 49 | 48 | 46 | 48 | 49 |
| 26 | 45 | 38 | 40 | 38 | 40 | 41 | 42 | 46 | 43 | 38 | 36 | 37 | 40 |
| 27 | 39 | 39 | 40 | 44 | 43 | 46 | 44 | 43 | 48 | 42 | 46 | 44 | 43 |
| 28 | 41 | 42 | 46 | 44 | 48 | 49 | 43 | 42 | 42 | 43 | 46 | 47 | 44 |
| 29 | 48 | 41 | 41 | 43 | 43 | 37 | 41 | 39 | 40 | 39 | 43 | 46 | 42 |
| 1930 | 44 | 44 | 43 | 42 | 47 | 50 | 50 | 49 | 46 | 46 | 48 | 52 | 47 |
| 31 | 48 | 46 | 47 | 46 | 51 | 47 | 48 | 47 | 49 | 47 | 45 | 46 | 47 |
| 32 | 45 | 39 | 39 | 41 | 39 | 42 | 44 | 41 | 41 | 39 | 39 | 46 | 41 |
| 33 | 50 | 48 | 42 | 40 | 41 | 43 | 46 | 43 | 49 | 49 | 50 | 50 | 46 |
| 34 | 48 | 45 | 47 | 43 | 44 | 48 | 47 | 44 | 48 | 51 | 51 | 50 | 47 |
| 35 | 48 | 45 | 47 | 46 | 47 | 47 | 47 | 49 | 45 | 47 | 50 | 51 | 47 |
| 36 | 47 | 46 | 44 | 46 | 47 | 49 | 47 | 47 | 48 | 49 | 52 | 51 | 48 |
| 37 | 49 | 48 | 43 | 41 | 43 | 47 | 44 | 46 | 48 | 46 | 48 | 51 | 46 |
| 38 | 47 | 46 | 48 | 44 | 44 | 43 | 44 | 45 | 46 | 49 | 52 | 51 | 47 |
| 39 | 47 | 42 | 44 | 43 | 42 | 41 | 42 | 40 | 46 | 44 | 51 | 47 | 44 |
| 1940 | 47 | 45 | 43 | 48 | 48 | 48 | 49 | 47 | 49 | 46 | 45 | 49 | 47 |
| 41 | 48 | 48 | 50 | 47 | 51 | 48 | 52 | 50 | 48 | 50 | 49 | 51 | 49 |
| 42 | 49 | 48 | 43 | 45 | 47 | 48 | 48 | 45 | 44 | 44 | 48 | 44 | 46 |
| 43 | 42 | 44 | 43 | 45 | 46 | 51 | 48 | 49 | 47 | 46 | 43 | 48 | 46 |
| 44 | 48 | 52 | 44 | 44 | 46 | 44 | 45 | 43 | 40 | 43 | 46 | 46 | 45 |
| 45 | 39 | 46 | 44 | 48 | 47 | 44 | 47 | 41 | 42 | 42 | 47 | 43 | 44 |
| 46 | 46 | 39 | 38 | 46 | 53 | 52 | 51 | 48 | 50 | 48 | 53 | 54 | 48 |
| 47 | 53 | 49 | 45 | 49 | 50 | 51 | 47 | 49 | 47 | 52 | 53 | 54 | 50 |
| 48 | 51 | 53 | 49 | 51 | 52 | 56 | 57 | 53 | 56 | 52 | 56 | 55 | 53 |
| 49 | 55 | 56 | 47 | 49 | 51 | 44 | 49 | 49 | 47 | 50 | 52 | 54 | 50 |
| 1950 | 56 | 49 | 47 | 45 | 49 | 49 | 47 | 50 | 47 | 52 | 51 | 49 | 49 |
| 1951 | 50 | 52 | 55 | 43 | 40 | 44 | 46 | 48 | 47 | 47 | 42 | 46 | 46 |
| 1952 | 45 | 41 | 36 | 44 | 46 | 47 | 40 | 43 | 42 | 43 | 40 | 47 | 43 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |

* Calories per cm per min.


## TABLE 811.-AIR MASSES

The transmission, both total and spectral, of the atmosphere depends upon several varying factors besides the actual air masses, that is, the length of the path of the rays in the atmosphere ; thus, corrections must always be determined for different tests.

Values of the transmission of the atmosphere for any position of the sun except when it is directly overhead are calculated from measurement when the sun is in the zenith, i.c., $\epsilon_{m}=e_{0} a^{m}$ when $\epsilon_{m}$ is the intensity of the radiation at air mass $m, e_{0}$ the intensity for the sun in the zenith, and $a$ the transmission for unit air mass. $m$ is unity when the sun is in the zenith and approximately equals the secant of the zenith distance for the other positions.

Besides values derived from the pure secant formula, the table contains those derived from various other more complex formulas, taking into account the curvature of the earth, refraction, etc. The most recent is that of Bemporad.

| Zenith dist | $0^{\circ}$ | $20^{\circ}$ | $40^{\circ}$ | $60^{\circ}$ | $70^{\circ}$ | $75^{\circ}$ | $80^{\circ}$ | $85^{\circ}$ | $88^{\circ}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Secant | 1.00 | 1.064 | 1.305 | 2.000 | 2.924 | 3.864 | 5.76 | 11.47 | 28.7 |
| Forbes | 1.00 | 1.065 | 1.306 | 1.995 | 2.902 | 3.809 | 5.57 | 10.22 | 18.9 |
| Bouguer | 1.00 | 1.064 | 1.305 | 1.990 | 2.900 | 3.805 | 5.56 | 10.20 | 19.0 |
| Laplace | 1.00 | - | - | 1.993 | 2.899 | - | 5.56 | 10.20 | 18.8 |
| Bemporad | 1.00 | - | - | 1.995 | 2.904 | -- | 5.60 | 10.39 | 19.8 |

TABLE 812.-THE AMOUNT OF SOLAR RADIATION IN DIFFERENT SECTIONS OF THE SPECTRUM, ULTRAVIOLET, VISIBLE, AND INFRARED

Calories, $\mathrm{min}^{-1} \mathrm{~cm}^{-2}$, Smithsonian scale of 1913

| ${ }_{\mu}^{\text {Wavelength }}$ | 0 | Miami, Fla. <br> Air mass |  |  |  |  | Montezuma, Chile Air mass |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1 | 2 | 3 | 4 | 5 | 1 | 2 | 3 | 4 | 5 |
| . 00 to .400 | . 151 | . 070 | . 036 | . 018 | . 010 | . 005 | . 094 | . 061 | . 041 | . 028 | . 019 |
| . 400 to . 770 | . 925 | . 740 | . 591 | . 476 | . 386 | . 314 | . 813 | . 734 | . 664 | . 603 | . 549 |
| . 770 to $\sim$ | . 874 | . 606 | . 517 | . 450 | . 398 | . 359 | . 742 | . 695 | . 657 | . 630 | . 608 |
| .00 to ${ }^{\sim}$ | 1.950 | 1.416 | 1.144 | . 944 | . 794 | . 678 | 1.649 | 1.490 | 1.362 | 1.261 | 1.176 |

Average clear day at Miami, Fla. (sea level) precipitable water about 2.00 cm .
Average clear day at Montezuma, Chile (altitude 9,000 feet) precipitable water 0.25 cm .

## TABLE 813.-SPECTRAL DISTRIBUTION OF SOLAR RADIATION OUTSIDE THE ATMOSPHERE

On the bases of the Smithsonian and other observations, Moon ${ }^{251}$ in 1940 proposed a spectral solar-radiation curve at normal incidence outside the atmosphere at the mean solar distance and also a like curve for solar radiation at the earth's surface for air mass 2 (Table 815). More recently a rocket observation ${ }^{252}$ has given a direct measurement (at 55 km ) of the ultraviolet spectrum of the sun at wavelengths below $0.34 \mu$. Since less than 1 percent of atmospheric ozone is above this level, this observation should be closely representative of ultraviolet solar radiation at wavelengths above $0.22 \mu$ at the top of the atmosphere. Moon's values for wavelengths above $0.33 \mu$ and data from the rocket observation for wavelengths below $0.33 \mu$ were used in constructing the table.

Part 1.-Intensity of solar radiation outside the atmosphere

| Wave- <br> length <br> $\mu$ | Intensity <br> Relative <br> units | Wave-- <br> length <br> $\mu$ | Intensity <br> Relative <br> units | Wave- <br> length <br> $\mu$ | Intensity <br> Relative <br> units | Wave- <br> length <br> $\mu$ | Intensity <br> Relative <br> units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| .220 | 14 | .420 | 1766 | .68 | 1473 | 2.5 | 50 |
| .230 | 33 | .424 | 1742 | .69 | 1439 | 2.6 | 43 |
| .240 | 40 | .430 | 1788 | .70 | 1405 | 2.7 | 38 |
| .250 | 55 | .44 | 1939 | .71 | 1371 | 2.8 | 33 |
| .260 | 126 | .45 | 2036 | .72 | 13337 | 2.9 | 30 |
| .265 | 174 | .46 | 2096 | .73 | 1304 | 3.0 | 26 |
| .270 | 162 | .47 | 2119 | .74 | 1270 | 3.1 | 23 |
| .275 | 136 | .48 | 2127 | .75 | 1236 | 3.2 | 21 |
| .280 | 145 | .49 | 2103 | .80 | 1097 | 3.3 | 19 |
| .290 | 378 | .50 | 2061 | .85 | 976 | 3.4 | 17 |
| .295 | 418 | .51 | 2000 | .90 | 871 | 3.5 | 15 |
| .300 | 386 | .52 | 1954 | .95 | 781 | 3.6 | 14 |
| .310 | 538 | .53 | 1912 | 1.0 | 706 | 3.7 | 12 |
| .320 | 621 | .54 | 1894 | 1.1 | 590 | 3.8 | 11 |
| .330 | 796 | .55 | 1878 | 1.2 | 488 | 3.9 | 10 |
| .335 | 826 | .56 | 1861 | 1.3 | 395 | 4.0 | 9 |
| .340 | 856 | .57 | 1841 | 1.4 | 319 | 4.1 | 8 |
| .345 | 886 | .58 | 1819 | 1.5 | 260 | 4.2 | 8 |
| .350 | 916 | .59 | 1795 | 1.6 | 214 | 4.3 | 7 |
| .360 | 976 | .60 | 1762 | 1.7 | 177 | 4.4 | 6 |
| .370 | 1046 | .61 | 1727 | 1.8 | 148 | 4.5 | 0 |
| .380 | 1121 | .62 | 1690 | 1.9 | 124 | 4.6 | 5 |
| .390 | 1202 | .63 | 1653 | 2.0 | 105 | 4.7 | 5 |
| .400 | 1304 | .64 | 1616 | 2.1 | 89 | 4.8 | 5 |
| .405 | 1427 | .65 | 1579 | 2.2 | 76 | 4.9 | 4 |
| .410 | 1728 | .66 | 1543 | 2.3 | 66 | 5.0 | 4 |
| .413 | 1803 | .67 | 1508 | 2.4 | 57 |  |  |

[^334]TABLE 813.-SPECTRAL DISTRIBUTION OF SOLAR RADIATION OUTSIDE THE ATMOSPHERE (concluded)

Part 2.-Energy distribution of solar radiation outside the atmcsphere

| Wavelength <br> interval <br> $\mu$ | Energy <br> cal $\mathrm{cm}^{-2}$ <br> $\mathrm{~min}^{-1}$ | Wavelength <br> interval <br> $\mu$ | Energy <br> cal $\mathrm{cm}^{-2}$ <br> $\mathrm{~min}^{-1}$ | Wavelength <br> interval <br> $\mu$ | Energy <br> cal $\mathrm{cm}^{-2}$ <br> $\mathrm{~min}^{-1}$ | Wavelength <br> interval <br> $\mu$ | Energy <br> cal $\mathrm{cm}^{-2}$ <br> $\mathrm{~min}^{-1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $.22-.23$ | .0004 | $.45-.46$ | .0303 | $.68-.69$ | .0213 | $.91-.92$ | .0123 |
| $.23-.24$ | .0006 | $.46-.47$ | .0309 | $.69-.70$ | .0208 | $.92-.93$ | .0121 |
| $.24-.25$ | .0010 | $.47-.48$ | .0312 | $.70-.71$ | .0203 | $.93-.94$ | .0118 |
| $.25-.26$ | .0011 | $.48-.49$ | .0311 | $.71-.72$ | .0198 | $.94-.95$ | .0116 |
| $.26-.27$ | .0025 | $.49-.50$ | .0306 | $.72-.73$ | .0194 | $.95-.96$ | .0113 |
| $.27-.28$ | .0021 | $.50-.51$ | .0299 | $.73-.74$ | .0189 | $.96-.97$ | .0111 |
| $.28-.29$ | .0029 | $.51-.52$ | .0290 | $.74-.75$ | .0183 | $.97-.98$ | .0109 |
| $.29-.30$ | .0059 | $.52-.53$ | .0283 | $.75-.76$ | .0179 | $.98-.99$ | .0107 |
| $.30-.31$ | .0067 | $.53-.54$ | .0279 | $.76-.77$ | .0175 | $.99-1.0$ | .0105 |
| $.31-.32$ | .0085 | $.54-.55$ | .0277 | $.77-.78$ | .0171 | $1.0-1.1$ | .0948 |
| $.32-.33$ | .0107 | $.55-.56$ | .0274 | $.78-.79$ | .0167 | $1.1-1.2$ | .0792 |
| $.33-.34$ | .0121 | $.56-.57$ | .0271 | $.79-.80$ | .0163 | $1.2-1.3$ | .0643 |
| $.34-.35$ | .0130 | $.57-.58$ | .0268 | $.80-.81$ | .0159 | $1.3-1.4$ | .0518 |
| $.35-.36$ | .0138 | $.58-.59$ | .0264 | $.81-.82$ | .0155 | $1.4-1.5$ | .0424 |
| $.36-.37$ | .0149 | $.59-.60$ | .0260 | $.82-.83$ | .0152 | $1.5-1.6$ | .0348 |
| $.37-.38$ | .0159 | $.60-.61$ | .0255 | $.83-.84$ | .0148 | $1.6-1.7$ | .0288 |
| $.38-.39$ | .0171 | $.61-.62$ | .0251 | $.84-.85$ | .0145 | $1.7-1.8$ | .0240 |
| $.39-.40$ | .0184 | $.62-.63$ | .0245 | $.85-.86$ | .0142 | $1.8-1.9$ | .0197 |
| $.40-.41$ | .0212 | $.63-.64$ | .0240 | $.86-.87$ | .0138 | $1.9-2.0$ | .0168 |
| $.41-.42$ | .0262 | $.64-.65$ | .0234 | $.87-.88$ | .0135 | $2.0-3.0$ | .0719 |
| $.42-.43$ | .0256 | $.65-.66$ | .0229 | $.88-.89$ | .0132 | $3.0-4.0$ | .0227 |
| $.43-.44$ | .0276 | $.66-.67$ | .0224 | $.89-.90$ | .0129 | $4.0-5.0$ | .0084 |
| $.44-.45$ | .0292 | $.67-.68$ | .0219 | $.90-.91$ | .0126 |  |  |

## TABLE 814.-DISTRIBUTION OF INTENSITY (RADIATION) OVER SOLAR DISC

Fraction of radius

| Wavelength | . 00 | . 30 | . 50 | . 60 | . 70 | . 80 | . 90 | . 95 | . 975 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 3149 | 1.000 | . 959 | . 857 | . 760 | . 721 | . 607 | . 446 | . 337 | . 251 |
| . 3518 | 1.000 | . 977 | . 895 | . 841 | . 785 | . 679 | . 524 | . 407 | . 328 |
| . 3665 | 1.000 | . 980 | . 881 | . 841 | . 787 | . 703 | . 546 | . 437 | . 359 |
| . 4030 | 1.000 | . 959 | . 877 | . 859 | . 767 | . 664 | . 533 | . 423 | . 346 |
| . 4487 | 1.000 | . 977 | . 912 | . 859 | . 804 | . 720 | . 594 | . 500 | . 389 |
| . 5186 | 1.000 | . 975 | . 929 | . 877 | . 832 | . 759 | . 644 | . 551 | . 466 |
| . 5485 | 1.000 | . 967 | . 919 | . 884 | . 832 | . 756 | . 650 | . 565 | . 487 |
| . 6151 | 1.000 | . 980 | . 936 | . 900 | . 853 | . 790 | . 687 | . 600 | . 528 |
| . 6980 | 1.000 | . 983 | . 946 | . 916 | . 872 | . 812 | . 722 | . 644 | . 574 |
| . 8384 | 1.000 | . 984 | . 952 | . 926 | . 893 | . 843 | . 766 | . 695 | . 640 |
| . 9920 | 1.000 | . 987 | . 957 | . 933 | . 903 | . 860 | . 788 | . 727 | . 670 |
| 1.1973 | 1.000 | . 988 | . 965 | . 944 | . 918 | . 880 | . 814 | . 758 | . 702 |
| 1.5397 | 1.000 | . 993 | . 973 | . 960 | . 940 | . 912 | . 863 | . 811 | . 763 |
| 1.7093 | 1.000 | . 994 | . 980 | . 967 | . 950 | . 925 | . 878 | . 832 | . 786 |
| 2.0664 | 1.000 | . 994 | . 980 | . 970 | . 955 | . 929 | . 888 | . 849 | . 811 |
| 2.2870 | 1.000 | . 995 | . 980 | . 968 | . 953 | . 931 | . 891 | . 850 | . 814 |
| 3.5 | 1.000 | . 996 | . 988 | . 980 | . 969 | . 952 | . 928 | . 902 | . 875 |
| 8.3 | 1.000 | . 998 | . 992 | . 990 | . 986 | . 977 | . 960 | . 942 | . 928 |
| 10.2 | 1.000 | . 998 | . 994 | . 991 | . 988 | . 982 | . 966 | . 953 | . 946 |

[^335]TABLE 815.-SOLAR IRRADIATION AT SEA LEVEL WITH SURFACE
PERPENDICULAR TO SUN'S RAYS $m=2 *$
(Watts per square meter per micron)

| $\underset{\text { microns }}{\lambda}$ | $J_{\lambda}$ | $\underset{\text { microns }}{\lambda}$ | $J_{\lambda}$ | $\underset{\text { microns }}{\lambda}$ | $J_{\lambda}$ | $\underset{\text { microns }}{\lambda}$ | $J_{\lambda}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 295 | 2.09 * | . 60 | 1167 | 1.15 | 216 | 1.65 | 173 |
| . 296 | $2.35{ }^{\text {* }}$ | . 61 | 1168 | 1.16 | 271 | 1.66 | 163 |
| . 297 | $2.87{ }^{\text {b }}$ | . 62 | 1165 | 1.17 | 328 | 1.67 | 159 |
| . 298 | $9.87{ }^{\text {b }}$ | . 63 | 1176 | 1.18 | 346 | 1.68 | 145 |
| . 299 | . 0346 | . 64 | 1175 | 1.19 | 344 | 1.69 | 139 |
| . 300 | . 0810 | . 65 | 1173 | 1.20 | 373 | 1.70 | 132 |
| . 301 | . 177 | . 66 | 1166 | 1.21 | 402 | 1.71 | 124 |
| . 302 | . 342 | . 67 | 1160 | 1.22 | 431 | 1.72 | 115 |
| . 303 | . 647 | . 68 | 1149 | 1.23 | 420 | 1.73 | 105 |
| . 304 | 1.16 | . 69 | 978 | 1.24 | 387 | 1.74 | 97.1 |
| . 305 | 1.91 | . 70 | 1108 | 1.25 | 328 | 1.75 | 80.2 |
| . 306 | 2.89 | . 71 | 1070 | 1.26 | 311 | 1.76 | 58.9 |
| . 307 | 4.15 | . 72 | 832 | 1.27 | 381 | 1.77 | 38.8 |
| . 308 | 6.11 | . 73 | 965 | 1.28 | 382 | 1.78 | 18.4 |
| . 309 | 8.38 | . 74 | 1041 | 1.29 | 346 | 1.79 | 5.70 |
| . 310 | 11.0 | . 75 | 867 | 1.30 | 264 | 1.80 | . 920 |
| . 311 | 13.9 | . 76 | 566 | 1.31 | 208 | 1.81 |  |
| . 312 | 17.2 | . 77 | 968 | 1.32 | 168 | 1.82 | ... |
| . 313 | 21.0 | . 78 | 907 | 1.33 | 115 | 1.83 | ... |
| . 314 | 25.4 | . 79 | 923 | 1.34 | 58.1 | 1.84 | ... |
| . 315 | 30.0 | . 80 | 857 | 1.35 | 18.1 | 1.85 | ... |
| . 316 | 34.8 | . 81 | 698 | 1.36 | . 660 | 1.86 | $\ldots$ |
| . 317 | 39.8 | . 82 | 801 | 1.37 | ... | 1.87 | $\ldots$ |
| . 318 | 44.9 | . 83 | 863 | 1.38 | $\ldots$ | 1.88 |  |
| . 319 | 49.5 | . 84 | 858 | 1.39 | ... | 1.89 | ... |
| . 32 | 54.0 | . 85 | 839 | 1.40 |  | 1.90 |  |
|  |  | . 86 | 813 | 1.41 | 1.91 | 1.91 | . 705 |
|  |  | . 87 | 798 | 1.42 | 3.72 | 1.92 | 2.34 |
| . 33 | 101 | . 88 | 614 | 1.43 | 7.53 | 1.93 | 3.68 |
| . 34 | 151 | . 89 | 517 | 1.44 | 13.7 | 1.94 | 5.30 |
| . 35 | 188 | . 90 | 480 | 1.45 | 23.8 | 1.95 | 17.7 |
| . 36 | 233 | . 91 | 375 | 1.46 | 30.5 | 1.96 | 31.7 |
| . 37 | 279 | . 92 | 258 | 1.47 | 45.1 | 1.97 | 37.7 |
| . 38 | 336 | . 93 | 169 | 1.48 | 83.7 | 1.98 | 22.6 |
| . 39 | 397 | . 94 | 278 | 1.49 | 128 | 1.99 | 1.58 |
| . 40 | 470 | . 95 | 487 | 1.50 | 157 | 2.00 | 2.66 |
| . 41 | 672 | . 96 | 584 | 1.51 | 187 | 2.01 | 19.5 |
| . 42 | 733 | . 97 | 633 | 1.52 | 209 | 2.02 | 47.6 |
| . 43 | 787 | . 98 | 645 | 1.53 | 217 | 2.03 | 55.4 |
| . 44 | 911 | . 99 | 643 | 1.54 | 226 | 2.04 | 54.7 |
| . 45 | 1006 | 1.00 | 630 | 1.55 | 221 | 2.05 | 38.3 |
| . 46 | 1080 | 1.01 | 620 | 1.56 | 217 | 2.06 | 56.2 |
| . 47 | 1138 | 1.02 | 610 | 1.57 | 213 | 2.07 | 77.0 |
| . 48 | 1183 | 1.03 | 601 | 1.58 | 209 | 2.08 | 88.0 |
| . 49 | 1210 | 1.04 | 592 | 1.59 | 205 | 2.09 | 86.8 |
| . 50 | 1215 | 1.05 | 551 | 1.60 | 202 | 2.10 | 85.6 |
| . 51 | 1206 | 1.06 | 526 | 1.61 | 198 | 2.11 | 84.4 |
| . 52 | 1199 | 1.07 | 519 | 1.62 | 194 | 2.12 | 83.2 |
| . 53 | 1188 | 1.08 | 512 | 1.63 | 189 | 2.13 | 20.7 |
| . 54 | 1198 | 1.09 | 514 | 1.64 | 184 | 2.14 | ... |
| . 55 | 1190 | 1.10 | 252 |  |  |  |  |
| . 56 | 1182 | 1.11 | 126 |  |  |  |  |
| . 57 | 1178 | 1.12 | 69.9 |  |  |  |  |
| . 58 | 1168 | 1.13 | 98.3 |  |  |  |  |
| . 59 | 1161 | 1.14 | 164 |  |  |  |  |

* For reference, see footnote 251, p. 721.
$\cdot \times 10^{-4} \quad b \times 10^{-8}$

TABLE 816.-THE BIOLOGICALLY EFFECTIVE COMPONENT OF ULTRAVIOLET, SOLAR, AND SKY RADIATION PER MONTH PER CM² (UVQ IN WATT MINUTES) AND THE TOTAL SOLAR AND SKY RADIATION (Q IN CALORIES PER MONTH PER CM ${ }^{2}$ ) INCIDENT IN WASHINGTON, D. C., 1941-1946, MONTHLY AVERAGE ${ }^{263}$

| Month | $\begin{gathered} U V Q \\ \begin{array}{c} \text { watt min } \\ \text { month } \\ \text { min } \\ \mathrm{cm}^{-2} \end{array} \end{gathered}$ | $\underset{\substack{\text { cal } \\ \text { month } \\ \mathrm{cm}^{-1}}}{\substack{\text { and }}}$ | Month | $\begin{gathered} U V Q \\ \text { watt min } \\ \text { month }^{-1} \mathrm{~cm}^{-2} \end{gathered}$ | $\begin{gathered} \begin{array}{c} \text { cal } \\ \text { month } \\ \mathrm{m}^{-1} \end{array} \mathrm{~cm}^{-2} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Jan. | . 112 | 4,982 | July | 1.091 | 15,239 |
| Feb. | . 209 | 6,987 | Aug. | 1.012 | 14,470 |
| Mar. | . 466 | 10,847 | Sept. | . 721 | 11,158 |
| Apr. | . 692 | 12,916 | Oct. | . 406 | 8,767 |
| May | . . 990 | 15,203 | Nov. | . 177 | 6,085 |
| June | . 1.108 | 16,019 | Dec. | . 087 | 4,690 |

${ }^{253}$ Coblentz, W. W., Bull. Amer. Meteorol. Soc., vol. 28, p. 465, 1947.

TABLE 817.-DURATION OF SUNSHINE *

| Approx declination of sun: | $-23^{\circ} 27^{\prime}$ | $-15^{\circ}$ | $-10^{\circ}$ | $-5^{\circ}$ | $0^{\circ}$ | $+5^{\circ}$ | $+10^{\circ}$ | +15 ${ }^{\circ}$ | +20 | $+23^{\circ} 27^{\prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approx date: | Dec. 22 | Feb. 9 Nov. 3 | Feb. 23 <br> Oct. 19 | Mar. 8 <br> Oct. 6 | Mar. 21 <br> Sept. 23 | Apr. 3 <br> Sept. 10 | Apr. 16 <br> Aug. 28 | $\begin{gathered} \text { May } 1 \\ \text { Aug. } 13 \end{gathered}$ | $\begin{aligned} & \text { May } 20 \\ & \text { July } 24 \end{aligned}$ | June 21 |
| Latitude | h m | h m | h m | h m | h m | $h \mathrm{~m}$ | h m | $h \mathrm{~m}$ | h m | h m |
| $0^{\circ}$ | 1207 | 1207 | 1207 | 1207 | 1207 | 1207 | 1206 | 1206 | 1207 | 1207 |
| $10^{\circ}$ | 1132 | 1145 | 1153 | 1200 | 1207 | 1214 | 1221 | 1229 | 1237 | 1243 |
| $20^{\circ}$ | 1055 | 1123 | 1138 | 1152 | 1207 | 1222 | 1237 | 1253 | 1308 | 1321 |
| $30^{\circ}$ | 1012 | 1058 | 1121 | 1144 | 1208 | 1231 | 1254 | 1319 | 1345 | 1405 |
| $40^{\circ}$ | 920 | 1026 | 1101 | 1135 | 1209 | 1243 | 1316 | 1353 | 1432 | 1501 |
| $50^{\circ}$ | 804 | 943 | 1035 | 1123 | 1212 | 1259 | 1347 | 1439 | 1537 | 1623 |
| $55^{\circ}$ | 710 | 915 | 1016 | 1114 | 1212 | 1311 | 1408 | 1511 | 1624 | 1723 |
| $60^{\circ}$ | 552 | 836 | 953 | 1103 | 1215 | 1325 | 1435 | 1554 | 1730 | 1853 |
| $65^{\circ}$ | 334 | 742 | 921 | 1050 | 1217 | 1345 | 1514 | 1658 | 1916 | 2203 |
| $70^{\circ}$ |  | 614 | 832 | 1029 | 1221 | 1414 | 1613 | 1844 |  |  |
| $80^{\circ}$ |  |  | 310 | 846 | 12. 38 | 1644 |  |  |  |  |

[^336]
## TABLE 818.-RELATIVE DISTRIBUTION IN NORMAL SPECTRUM OF SUNLIGHT AND SKY LIGHT AT MOUNT WILSON

Zenith distance about $50^{\circ}$
This table is abstracted in modified form from the Annals of the Smithsonian Astrophysical Observatory. The observations, which were visual, made on October 17, 1906, probably represent the most ideal sky conditions on Mount Wilson.

|  |  |  |  |  |  |  | $C$ | $D$ | $b$ | $F$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Place in spectrum $(\mu) \ldots \ldots \ldots$ | .422 | .457 | .491 | .566 | .614 | .660 |  |  |  |  |
| Intensity sunlight $\ldots \ldots \ldots \ldots$. | 186 | 232 | 227 | 211 | 191 | 166 |  |  |  |  |
| Intensity sky light.......... | 642 | 986 | 701 | 395 | 231 | 174 |  |  |  |  |
| Ratio at Mount Wilson........ | - | - | 309 | 187 | 121 | 105 | 102 | 143 | 246 | 316 |
| Ratio computed by Rayleigh... | - | - | - | - | - | - | 102 | 164 | 258 | 328 |
| Ratio observed by Rayleigh... | - | - | - | - | 102 | 168 | 291 | 369 |  |  |

TABLE 819.-ILLUMINATION DUE TO DIRECT SUNLIGHT, SKY LIGHT, AND TOTAL ON HORIZONTAL AND VERTICAL PLANES ${ }^{254}$

| $\begin{gathered} \text { Solar } \\ \text { altitude } \\ h \end{gathered}$ | $\underset{\substack{\text { mass } \\ m}}{\operatorname{Ain}_{2}}$ | Direct sunlight |  | Skylight |  | Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Ind | $I_{p d}$ | TA, | $I_{p}$ | TIA | $I_{p}$ |
|  |  | $\mathrm{ft}-\mathrm{c}$ |  | $\mathrm{ft}-\mathrm{c}$ |  | $\mathrm{ft}-c$ |  |
| 3 | 15.36 | 19.6 | 374 | 256 | 587 | 277 | 961 |
| 5 | 10.39 | 100 | 1150 | 325 | 746 | 425 | 1900 |
| 7 | 7.77 | 252 | 2050 | 395 | 848 | 647 | 2900 |
| 10 | 5.60 | 590 | 3350 | 491 | 953 | 1080 | 4300 |
| 15 | 3.82 | 1310 | 4910 | 629 | 1070 | 1940 | 5980 |
| 20 | 2.90 | 2130 | 5860 | 750 | 1140 | 2880 | 7000 |
| 25 | 2.36 | 2980 | 6390 | 856 | 1180 | 3840 | 7570 |
| 30 | 2.00 | 3820 | 6620 | 945 | 1210 | 4760 | 7830 |
| 35 | 1.74 | 4650 | 6640 | 1020 | 1220 | 5670 | 7860 |
| 40 | 1.55 | 5440 | 6490 | 1090 | 1220 | 6530 | 7710 |
| 45 | 1.41 | 6170 | 6170 | 1160 | 1220 | 7330 | 7390 |
| 50 | 1.30 | 6850 | 5750 | 1210 | 1200 | 8060 | 6950 |
| 55 | 1.22 | 7450 | 5220 | 1270 | 1180 | 8720 | 6400 |
| 60 | 1.15 | 8000 | 4620 | 1310 | 1150 | 9310 | 5770 |
| 65 | 1.10 | 8470 | 3950 | 1350 | 1090 | 9820 | 5040 |
| 70 | 1.06 | 8860 | 3230 | 1390 | 1020 | 10250 | 4250 |
| 75 | 1.04 | 9160 | 2450 | 1420 | 930 | 10580 | 3380 |
| 80 | 1.02 | 9380 | 1650 | 1440 | 834 | 10820 | 2480 |
| 85 | 1.01 | 9510 | 833 | 1460 | 728 | 10970 | 1560 |
| 90 | 1.00 | 9570 | 00 | 1480 | 615 | 11050 | 615 |

The solar altitude, $h$, is expressed in angular units, the illumination, $I$, in foot-candles. The subscripts $p$ and $h$ designate the evaluation of illumination on the perpendicular (facing the sun) and horizontal planes. The additional subscripts, $d, s$, and $t$, designate direct sunlight, sky light and total light (direct sunlight plus sky light).

[^337]TABLE 820.-MEAN INTENSITY J FOR 24 HOURS OF SOLAR RADIATION ON A HORIZONTAL SURFACE AT THE TOP OF THE ATMOSPHERE AND THE SOLAR RADIATION A, IN TERMS OF THE SOLAR RADIATION, A., AT EARTH'S MEAN DISTANCE FROM THE SUN

| Date | $\begin{gathered} \text { Motion of } \\ \text { the sun } \\ \text { inn } \\ \text { longi. } \\ \text { tude } \end{gathered}$ | Relative mean vertical intensity $\frac{J}{A_{0}}$Latitude north Latitude north |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $0^{\circ}$ | $10^{\circ}$ | $20^{\circ}$ | $30^{\circ}$ | $40^{\circ}$ | $50^{\circ}$ | $60^{\circ}$ | $70^{\circ}$ | ${ }^{80}$ | $90^{\circ}$ | $\frac{A}{A_{0}}$ |
| Jan. 1 | 0:99 | . 303 | . 265 | . 220 | . 169 | . 117 | . 066 | . 018 |  |  |  | 1.0335 |
| Feb. 1 | 31.54 | . 312 | . 282 | . 244 | . 200 | . 150 | . 100 | . 048 | . 006 |  |  | 1.0288 |
| Mar. 1 | 59.14 | . 320 | . 303 | . 279 | . 245 | . 204 | . 158 | . 108 | . 056 | . 013 |  | 1.0173 |
| Apr. 1 | 89.70 | . 317 | . 319 | . 312 | . 295 | . 269 | . 235 | . 195 | . 148 | . 101 | . 082 | 1.0009 |
| May 1 | 119.29 | . 303 | . 318 | . 330 | . 329 | . 320 | . 302 | . 278 | . 253 | . 255 | . 259 | . 9841 |
| June 1 | 149.82 | . 287 | . 315 | . 334 | . 345 | . 349 | . 345 | . 337 | . 344 | . 360 | . 366 | . 9714 |
| July 1 | 179.39 | . 283 | . 312 | . 333 | . 347 | . 352 | . 351 | . 345 | . 356 | . 373 | . 379 | . 9666 |
| Aug. 1 | 209.94 | . 294 | . 316 | . 330 | . 334 | . 330 | . 318 | . 300 | . 282 | . 295 | . 300 | . 9709 |
| Sept: 1 | 240.50 | . 310 | . 318 | . 316 | . 305 | . 285 | . 256 | . 220 | . 180 | . 139 | . 140 | . 9828 |
| Oct. 1 | 270.07 | . 317 | . 308 | . 289 | . 261 | . 225 | . 183 | . 135 | . 084 | . 065 |  | 9995 |
| Nov. 1 | 300.63 | . 312 | . 286 | . 251 | . 211 | . 164 | . 114 | . 063 | . 018 |  |  | 1.0164 |
| Dec. 1 | 330.19 | . 304 | . 267 | . 224 | . 175 | . 124 | . 072 | . 024 |  |  |  | 1.0288 |
| Year |  | . 305 | . 301 | . 289 | . 268 | . 241 | . 209 | . 173 | . 144 | . 133 | . 126 |  |

Average annual solar energy received per square dekameter of horizontal surface in kilowatt hours. U. S.: Lincoln, 160,906; Mount Weather, 148,824; Washington, 145,403; New York, 106,460; Chicago, 97,856 . Other countries: Toronto, 139,523; Johannesburg, 175,696; Davos Platz, 174,043; South Kensington, 78,569; Stockholm, 79,267.

Mean temperatures of a few selected American stations, also of one station of very high and two of very low temperature, and one of very great and one of very small range of temperature.


Lat., Long., Alt. respectively : $(1)+58.5,63 \circ 0 \mathrm{~W},-:(2)+49.9,97.1 \mathrm{~W}, 233 \mathrm{~m} ;(3)+45.5$, $73.6 \mathrm{~W}, 57 \mathrm{~m} ;(4)+42.3,71.1 \mathrm{~W}, 38 \mathrm{~m} ;(5)+41.9,87.6 \mathrm{~W}, 251 \mathrm{~m} ;(6)+39.7,105.0 \mathrm{~W}, 1613 \mathrm{~m}$; $(7)+38.9,77.0 \mathrm{~W}, 34 \mathrm{~m} ;(8)+38.8,105.0 \mathrm{~W}, 4308 \mathrm{~m} ;(9)+38.6,90.2 \mathrm{~W}, 173 \mathrm{~m} ;(10)+37.8$, $122.5 \mathrm{~W}, 47 \mathrm{~m}:(11)+32.7,114.6 \mathrm{~W}, 43 \mathrm{~m} ;(12)+30.0,90.1 \mathrm{~W}, 16 \mathrm{~m} ;(13)+15.6,37.5 \mathrm{E}, 9 \mathrm{~m}$; $(14)+81.7,64.7 \mathrm{~W},-;(15)+67.6,133.8 \mathrm{E}, 140 \mathrm{~m}$; (16) $-6.2,106.8 \mathrm{E}, 7 \mathrm{~m}$.
Note.-Highest recorded temperature in world $=57^{\circ} \mathrm{C}$ in Death Valley, California, July 10, 1913. Lowest recorded temperature in world $=-68^{\circ} \mathrm{C}$ at Verkhoyansk, Feb. 1892.

TABLE 822.-TEMPERATURE VARIATION OVER EARTH'S SURFACE (HANN)
Maximum values for month in italics.

| Latitude | Temperatures ${ }^{\circ} \mathrm{C}$ |  |  |  |  |  | Mean ocean temp | $\begin{gathered} \text { Land } \\ \text { surface } \\ \% \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Jan. | Apr. | July | Oct. | Year | Range |  |  |
| North pole | -41.0 | -28.0 | - 1.0 | -24.0 | -22.7 | 40.0 | - 1.7 | - |
| +80 ${ }^{\circ}$ | -32.2 | -22.7 | + 2.0 | -19.1 | -17.1 | 34.2 | -1.7 | 20 |
| 70 | -26.3 | -14.0 | 7.3 | $-9.3$ | -10.7 | 33.6 | + 7 | 53 |
| 60 | -16.1 | $-2.8$ | 14.1 | + . 3 | - 1.1 | 30.2 | 4.8 | 61 |
| 50 | - 7.2 | + 5.2 | 17.9 | 6.9 | + 5.8 | 25.1 | 7.9 | 58 |
| 40 | + 5.5 | 13.1 | 24.0 | 15.7 | 14.1 | 18.5 | 14.1 | 45 |
| 30 | 14.7 | 20.1 | 27.3 | 21.8 | 20.4 | 12.6 | 21.3 | 43.5 |
| 20 | 21.9 | 25.2 | 28.0 | 26.4 | 25.3 | 6.1 | 25.4 | 31.5 |
| +10 | 25.8 | 27.2 | 27.0 | 26.9 | 26.8 | 1.4 | 27.2 | 24 |
| Equator | 26.5 | 26.6 | 25.7 | 26.5 | 26.3 | . 9 | 27.1 | 22 |
| -10 | 26.4 | 25.9 | 23.0 | 25.7 | 25.5 | 3.4 | 25.8 | 20 |
| 20 | 25.3 | 24.0 | 19.8 | 22.8 | 23.0 | 5.5 | 24.0 | 24 |
| 30 | 21.6 | 18.7 | 14.5 | 18.0 | 18.4 | 7.1 | 19.5 | 20 |
| 40 | 15.4 | 12.5 | 8.8 | 11.7 | 11.9 | 6.6 | 13.3 | 4 |
| 50 | 8.4 | 5.4 | 3.0 | 4.8 | 5.4 | 5.4 | + +6.4 | 2 |
| 60 | 3.2 | - | - 9.3 | - | $-3.2$ | 12.5 | . 0 | 0 |
| 70 | - 1.2 | - | -21.0 | - | -12.0 | 19.8 | $-1.3$ | 71 |
| 80 | (-4.3) | - | (-28.7) | - | (-20.6) | (24.4) | - | 100 |
| South pole | ( -6.0 ) | - | (-33.0) | - | (-25.0) | (27.0) | - | (100) |

Table illustrates temperature changes underground at moderate depths due to surface warming (read from plot for Tiflis, Lehrbuch der Meteorologie, Hann and Süring, 1915). Below $20-30 \mathrm{~m}$ (nearer the surface in Tropics) there is no annual variation. Increase downward at greater depths, $0.03 \pm{ }^{\circ} \mathrm{C}$ per $\mathrm{m}\left(1^{\circ}\right.$ per 35 m$)$ 1.c. At Pittsburgh, 1524 m , $49.4^{\circ}$, 0294 per m; Oberschlesien, $2003 \mathrm{~m}, 70^{\circ}, .0294$ per m; or West Virginia, 2200 m ; $70^{\circ}, .034^{\circ}$ per m (Van Orstrand). Mean value outflow heat from earth's center, 0.00000172 g cal $\mathrm{cm}^{-2} \mathrm{sec}^{-1}$, or $54 \mathrm{~g} \mathrm{cal} \mathrm{cm}^{-2} \mathrm{yr}^{-1}$ ( 39 Laby ). Open ocean temperatures: Greatest mean annual range (Schott) $40^{\circ} \mathrm{N} ., 4.2^{\circ} \mathrm{C} ; 30^{\circ} \mathrm{S} ., 5.1^{\circ}$; but $10^{\circ} \mathrm{N}$., only $2.2^{\circ} ; 50^{\circ} \mathrm{S} ., 2.9^{\circ}$. Mean surface temp. whole ocean (Krümmel) $17.4^{\circ}$ : all depths, 3.9 :. Below 1 km nearly isothermal with depth. In Tropics, surface $28^{\circ}$; at $183 \mathrm{~m}, 11^{\circ}, 80$ percent water less than $4.4^{\circ}$. Deep-sea (bottom) temps. range $-0.5^{\circ}$ to $+2.6^{\circ}$. Soundings in South Atlantic: $0 \mathrm{~km}, 18.9^{\circ} ; .25 \mathrm{~km}, 15^{\circ} ; .5 \mathrm{~km}, 8.3^{\circ} ; 1 \mathrm{~km}, 3.3^{\circ} ; 3 \mathrm{~km}, 1.7^{\circ} ; 4.5 \mathrm{~km}, 0.6^{\circ}$.

Maximum values in boldface.

| Depth. | Tan. | Feb. | Mar. | Apr. | May | June | July | Aug. | Sept. | Oct. | Nov. | Dec. |
| :---: | ---: | ---: | ---: | ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\boldsymbol{m}$ | Jat |  |  |  |  |  |  |  |  |  |  |  |
| 0 | 1 | 4 | 10 | 14 | 21 | 29 | 32 | 32 | 24 | 16 | 9 | 4 |
| .5 | 4 | 4 | 9 | 13 | 18 | 23 | 26 | 28 | 24 | 18 | 12 | 6 |
| 1.0 | 6 | 6 | 8 | 12 | 15 | 20 | 24 | 26 | 23 | 18 | 14 | 10 |
| 1.5 | 9 | 8 | 9 | 11 | 14 | 18 | 21 | 23 | 22 | 18 | 15 | 12 |
| 20 | 11 | 10 | 10 | 11 | 13 | 16 | 19 | 21 | 21 | 18 | 16 | 14 |
| 3.0 | 14 | 12 | 12 | 11 | 13 | 14 | 16 | 17 | 18 | 18 | 17 | 15 |
| 4.0 | 15 | 13 | 12 | 12 | 12 | 13 | 14 | 16 | 16 | 17 | 17 | 16 |
| 5.0 | 15 | 14 | 13 | 13 | 13 | 13 | 14 | 14 | 15 | 16 | 16 | 16 |
| 6.0 | $\mathbf{1 5}$ | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 15 | 15 | 15 |

## TABLE 824.-WOLF'S SUNSPOT NUMBERS, ANNUAL MEANS* ${ }^{255}$

Sunspot number $=k(10 \times$ number of groups and single spots observed + total number of spots in groups and single spots). $k$ depends on observer and telescope, equaling unity for Wolf with 3 -in. telescope and power of 64 . Wolf's numbers are closely proportional to spotted area on sun, 100 corresponds to about $1 / 600$ of visible disk covered (umbras and penumbras). Periodicity: successive outbursts about 11 years apart, extremes 7.3 years and 17.1 years. See references for daily and monthly values.
Smoothed monthly numbers are formed from monthly means of observed number by weighting the sixth months preceding and following 1 , all 11 intervening months 2.

Smoothed monthly sunspot numbers, annual means
Maximunn and minimum values for period in boldface

| Year | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1750 | 83.1 | 52.2 | 45.9 | 28.9 | 13.5 | 9.3 | 12.2 | 31.9 | 47.2 | 54.5 |
| 1760 | 64.7 | 80.2 | 60.1 | 48.5 | 36.7 | 21.4 | 14.2 | 35.9 | 66.8 | 103.4 |
| 1770 | 98.5 | 86.7 | 65.7 | 39.7 | 27.5 | 8.8 | 21.7 | 92.2 | 151.3 | 123.4 |
| 1780 | 89.2 | 66.5 | 38.7 | 22.5 | 10.3 | 26.7 | 81.2 | 128.2 | 133.3 | 117.0 |
| 1790 | 90.6 | 67.6 | 59.8 | 47.3 | 38.5 | 24.0 | 15.6 | 6.5 | 4.6 | 6.9 |
| 1800 | 15.0 | 33.7 | 44.1 | 43.0 | 46.8 | 42.5 | 27.3 | 11.6 | 7.6 | 3.1 |
| 1810 | . 0 | 1.7 | 4.5 | 12.1 | 15.5 | 35.1 | 46.1 | 39.8 | 30.0 | 23.4 |
| 1820 | 16.6 | 6.6 | 4.0 | 2.6 | 8.3 | 16.9 | 35.3 | 51.6 | 62.1 | 67.1 |
| 1830 | 67.2 | 50.5 | 26.3 | 9.4 | 13.3 | 59.1 | 121.1 | 137.0 | 103.4 | 83.4 |
| 1840 | 61.9 | 38.5 | 23.0 | 13.2 | 17.7 | 38.4 | 59.7 | 97.3 | 125.0 | 95.4 |
| 1850 | 69.8 | 63.2 | 52.8 | 38.6 | 21.0 | 7.7 | 5.2 | 23.0 | 56.3 | 90.3 |
| 1860 | 94.9 | 77.7 | 61.1 | 45.4 | 45.2 | 31.4 | 14.7 | 8.8 | 36.9 | 78.6 |
| -1870 | 131.8 | 113.8 | 99.7 | 67.9 | 43.1 | 18.9 | 11.7 | 11.0 | 3.9 | 7.7 |
| 1880 | 31.6 | 54.4 | 58.1 | 65.4 | 63.3 | 51.3 | 25.1 | 12.6 | 7.0 | 6.3 |
| 1890 | 8.4 | 37.7 | 70.0 | 83.7 | 79.1 | 61.5 | 43.1 | 28.1 | 24.6 | 13.8 |
| 1900 | 8.8 | 3.4 | 5.7 | 23.0 | 44.1 | 58.7 | 60.3 | 56.0 | 51.2 | 40.6 |
| 1910 | 21.0 | 6.5 | 3.4 | 2.2 | 11.8 | 46.4 | 59.1 | 96.2 | 83.1 | 65.5 |
| 1920 | 36.9 | 27.0 | 13.0 | 6.3 | 16.8 | 43.7 | 66.5 | 70.0 | 74.5 | 62.0 |
| 1930 | 38.8 | 21.1 | 12.1 | 5.9 | 9.4 | 36.5 | 79.6 | 113.2 | 103.9 | 89.6 |
| 1940 | 66.8 | 50.5 | 30.3 | 15.3 | 11.1 | 36.4 | 91.7 | 145.6 | 141.2 | 134.7 |
| 1950 | 83.9 | 69.4 |  |  |  |  |  |  |  |  |

[^338]
## 728 TABLES 825-884.-ASTRONOMY AND ASTROPHYSICS *

Astronomy, including astrophysics, is a study of the geometry and physics of the heavenly bodies and the material in the intervening space. This experimental science requires some very special apparatus-in general, used in connection with large telescopes. Table 825 gives a list of the larger telescopes that are now (1949) in active scientific use. Some definitions and standards and other data on astronomy follow.

[^339]$\dagger$ Prepared by J. J. Nassau, Case Institute of Technology.

## TABLE 826.-APPROXIMATE EQUATION OF TIME**

The equation of time in this table is to be added algebraically to local apparent solar time to obtain local mean solar time.

Accurate values of the equation of time may be obtained from the American Ephemeris and Nautical Almanac.

|  | 1 nin |  | min |  | min |  | min |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Jan. 1 | $+3$ | Apr. 1 | + 4 | July 1 | + 4 | Oct. 1 | -10 |
|  | + 8 | 11 | +1 | 11 | + 5 | 11 | -13 |
| 21 | +11 | 21 | $-1$ | 21 | + 6 | 21 | -15 |
| Feb. 1 | +14 | May 1 | - 3 | Aug. 1 | +6 | Nov. 1 | -16 |
| 11 | +14 | 11 | -4 | 11 | + 5 | 11 | -16 |
| 21 | +14 | 21 | -4 | 21 | + 3 | 21 | -14 |
| Mar. 1 | +13 | June 1 | -2 | Sept. 1 | 0 | Dec. 1 | -11 |
| 11 | +10 | ${ }^{\text {J }} 11$ | -1 | ${ }^{11}$ | -3 | Dec 11 | -7 |
| 21 | + 8 | 21 | $+1$ | 21 | -7 | 21 | -2 |

[^340]Aberration constant. $-20^{\prime \prime} 47$ (conventional value; work of Doolittle, Spencer Jones, and others, indicates a value of $20: 50$ ).
Aphelion.-Point where earth is farthest from sun $=1.520 \times 10^{18} \mathrm{~cm}$.
Astronomical unit (A. U.)-Distance: mean distance earth to sun, $149,500,000 \mathrm{~km}$. (Conventional value, solar parallax 8 " 79 would give $149,700,000$.) Mass: the combined mass of the sun and earth which means, practically, the sun's mass $=1.987 \times 10^{28} \mathrm{~g}$.

Color index.-Ordinary stellar magnitudes are supposed to correspond to observations with the normal eye. This is by no means easy to define, for the brightness of a red star compared with a white, appears greater when the amount of light entering the eye is increased for both in the same ratio (Purkinje effect) for low brightness.

Owing to differences in the actual distribution of the energy with wavelength, the relative brightness of stars of different temperatures and colors measured with receptors sensitive to different spectral regions vary greatly.

On ordinary photographs, red stars appear much fainter than to the eye. If the measures are calibrated so that the visual and photographic magnitudes average the same for spectral class $A$, the difference for any other group of stars is called color index. This ranges from about $-0^{m} .3$ to +1.8 for class $M$ and reaches $5^{m}$ for the reddest stars of class $N$.
The difference in color index between the two standard types, e.g., $A O$ and $K O$ is called the color-equation. It varies over a wide range with the spectral sensitivity of the receiver, very large and positive for the violet and ultraviolet and negative for the red and infrared.

Photoelectric devices, combined with screens and measurable transmission have at last provided standard systems for stellar photometry of at least approximately definite physical significance for spectral regions ranging from the ultraviolet to the infrared. Radiometric magnitudes correspond to the measures of the whole observable energy radiztion.

Bolometric magnitudes are supposed to represent the total energy radiation of all wavelengths, and must be found bv calculation.

Date line.-Established by convention not far from the 180th meridian from Greenwich. Where the line runs across a group of islands, the change of the date line is diverted to one side so that the group has the same day. Ships crossing from the east, skip a day ; going east, count the same day twice.

Day.-Mean solar day $=1,440$ minutes $=86,400$ seconds $=1.0027379$ sidereal day. Sidereal day (ordinary, two successive transits of vernal equinox, might be called equinoctial day $)=86,164.09054$ mean solar seconds $=23 \mathrm{hr}, 56 \mathrm{~min}, 4.09054 \mathrm{sec}$ mean solar time.

Two successive transits of same fixed star $=86,164.09967$ mean solar seconds.
Declination.-If $\delta=$ declination, $t$, hour angle measured west from meridian, $h$, altitude, $\phi$, latitude and $A$, azimuth measured from S. point through W . Then

$$
\left.\begin{array}{rl}
\sin h & =\sin \phi \sin \delta+\cos \phi \cos \delta \cos t \\
\cos h \cos A & =-\cos \phi \sin \delta+\sin \phi \cos \delta \cos t \\
\cos h \sin A & = \\
\cos \delta \sin t
\end{array}\right\} \text { given } \delta, t, \phi
$$

Delaunay's $\gamma=\sin 1 / 2 I=0.04488716$ (Brown).
Dip of horizon.-In minutes of arc $=\sqrt{\text { eievation in } \mathrm{ft}}$ (approximately).
Earth.-Mean $r=6.3712 \times 10^{8} \mathrm{~cm}$. Equatorial diameter $=12,756.78 \mathrm{~km}$; polar diameter $=12,713.82 \mathrm{~km}$. Area $=5.101 \times 10^{18} \mathrm{~cm}^{2}$. Angular velocity $=72.9 \times 10^{-6}$ radians $/ \mathrm{sec}$. Volume $=1.083 \times 10^{27} \mathrm{~cm}^{3}$. Mass $=5.975 \times 10^{27} \mathrm{~g}$. Density $=5.517 \mathrm{~g} / \mathrm{cm}^{3}$. Mean distance to sun $=$ $1.495 \times 10^{13} \mathrm{~cm}$. Distance to the moon $=3.844 \times 10^{19} \mathrm{~cm}$. Light traverses mean radius of earth's orbit in 498.6 sec . Semimajor axis orbit $=1.4950 \times 10^{13} \mathrm{~cm}$; semi ninor axis $=$ $1.4948 \times 10^{18} \mathrm{~cm}$. Viscosity $=10.9 \times 10^{16} \mathrm{cgs}$. Velocity of equatorial point on earth, because of rotation: $1,050 \mathrm{mi} / \mathrm{hr}=1,550 \mathrm{ft} / \mathrm{sec}=1,650 \mathrm{~km} / \mathrm{hr}=460 \mathrm{~m} / \mathrm{sec}$. In orbit: $18 / 5 \mathrm{mi} / \mathrm{sec}$ $=30 \mathrm{~km} / \mathrm{sec}$. See Tables 831 and 833 . Rotational energy $=2.16 \times 10^{30} \mathrm{erg}$.

Earth's orbital velocity $=18.5$ miles $/ \mathrm{second}$. $1,550 \mathrm{ft} / \mathrm{sec}$ (rotation at Equator).
Eccentricity of earth's orbit $=e=0.01675104-4.180 \times 10^{-7}(t-1900)-1.26 \times 10^{-11}$ $(t-1900)^{2}$ :

Eccentricity of moon's orbit $=e_{2}=0.05490056$ (Brown).
Gal.-Unit of gravity acceleration $=1 \mathrm{~cm} \mathrm{sec}-{ }^{-2}$.
General precession (westward movement of the equinoxes) $=50: 2564+0 " 000222$ $\left.{ }^{( } t-1900\right)$ per year (Newcomb). Probably requires correction of about $+0 \% 01$. See Table 838.
Gravitation constant $=(6.670 \pm 0.005) \times 10^{-8}$ dyne $\mathrm{cm}^{2} \mathrm{~g}^{-2}($ Heyl, 1930 $)$.
Gravity, acceleration due to, $g=978.0495 \mathrm{~cm} \mathrm{sec}^{-2}$ (conventional value at sea level at equator. See Table 802). Unit, gal $=1 \mathrm{~cm} \mathrm{sec}{ }^{-2}$.

[^341](continued)

## TABLE 827.-MISCELLANEOUS ASTRONOMICAL DATA (continued)

Heat index.-Radiometric (heat or bolometric), zero taken to agree with Class $A O$, (radiometric - visual magnitude) $=$ heat index, + for red stars.
Horizon.-Distance at sea is approximately, miles $=\sqrt{(3 / 2)}$ height in feet. Local refraction (mirage) may introduce large percentage changes in either direction for observations from altitudes of 30 feet or less.
Inclination of moon's orbit $=I=5^{\circ} 8^{\prime} 43.5^{\prime \prime}$ (Brown).
Julian period, $1950=6663$.-January 1, 1950, Julian-day number $=2433283$.
Latitude variation.-The direction of the axis of the earth in space changes approximately $20 " 5$ per year owing to precession. The change is roughly periodic in 25,800 years with an amplitude of $23: 5$. This does not affect terrestrial latitudes, but a variation in them is caused by a shift of the earth's body about this axis. The two ascertained components of the polar motion have periods of 1.00 and nearly 1.20 years (the annual and Chandlerian components, respectively), so that the oscillations in $X$ and $Y$, as well as the resultant total motion have variations in amplitude with a "beat period" of about 6 years. In contrast to the annual terms, Chandler's term shows striking variations in amplitude. There is, further, a variation in the period of the Chandlerian term (1.18, 1.20, 1.17, 1.15, 1.19 years) which appears nearly proportional to the corresponding amplitude variations according to the relation $P=0.185 A+1.128$, where $P$ is the period in years and $A$ the amplitude in 0"01 units. (See T. Nicolini, appendix to Commission 19 Report, Trans. Int. Astron. Union, Zurich, 1948.)
Light, velocity of.-(Mean value) in vacuo, $299773 \pm 10 \mathrm{~km} \mathrm{sec}^{-1}$ (Dorsey).
$299792.5 \pm 0.8 \mathrm{~km} \mathrm{sec}^{-1}$ (Bearden).
$299776 \pm 0.00004 \mathrm{~km} \mathrm{sec}^{-1}$ (Birge).
Light year.-The distance light travels in 1 year $=9.5 \times 10^{12}$ kilometers $=5.9 \times 10^{18}$ miles. Light traverses mean radius of earth's orbit in 498.6 sec .
Lunar inequality of earth $=L=6.454$.'
Lunar node $d=$ daily motion $=-0.052954$.
Lunar parallax $=3422.70^{\prime \prime}$ (Brown).
Lunar perigee, daily motion $=+0.111404$.
Lunar-solar precession $=p^{\prime}=50.3714^{\prime \prime}$ per year (De Sitter, 1927). Of this 0.0191", Einstein, orbital motion earth.
Magnitudes.-The observed intensity of light received on the earth from astronomical bodies ranges over a factor exceeding $10^{19}$. It is therefore expressed on a logarithmic scale-the system of stellar magnitudes. This system, which was adopted by Hipparchus more than 2,000 years ago, is closely represented by the equation

$$
m=2.5 \log _{10}\left(l_{0} / l\right)
$$

where $l$ is the observed light and $l_{0}$ a standard value corresponding roughly to the light of Arcturus or Vega. Decrease of light by a factor of 100 increases the stellar magnitude by 5.00 ; hence the brightest objects have negative magnitudes. (Sun: -26.8 ; mean full moon: - 12.5 ; Venus at brightest: - 4.3 ; Jupiter at opposition: -2.3 ; Sirius: -1.6 ; Vega: +0.2 ; Polaris: +2.1 ). The faintest stars visible to the naked eye on a clear dark night are of about the sixth magnitude (though on a perfectly black background the limit for a single luminous point approaches the eighth magnitude). The faintest stars visible with a telescope of aperture $A$ (in inches) is one approximately of magnitude $9+5$ $\log _{10} A$. The magnitude of the faintest stars which can be photographed with the 200 -inch telescope is about +22.7 . The apparent magnitude of a standard candle at a distance of 1 meter is -14.2 .
Absolute magnitude, $M$, is that which the body would exhibit if placed at a distance of 10 parsecs, and corresponds to its actual luminosity. For a star of magnitude $m$, and parallax $p$, in seconds of arc

$$
M=m+5+5 \log p
$$

For the sun, $M=+4.7$. The brightest stars probably exceed $M=-7$ and the faintest observed value is $M=+18$, a range of $10^{20}$. The full moon (could it be observed without interference from the standard distance) would have $M=+32$ and a standard candle +72.8 .
Mean distance earth to moon $=60.2678$ terrestrial radii.
$=384,411$ kilometers $=238,862$ miles. (See Table 834.)
Mean distance earth to sun $=149,500,000$ kilometers $=92,900.000$ miles. (See Astronomical unit.) See Table 833.
Month.-Sidereal $=27.321661$ days, synodical (ordinary) $=29.530588$ days $($ Brown $)$.
Nutation constant (periodic motion of celestial pole) $=9.21^{\prime \prime}$ : conventional value ; 9.207". Principal in long $=\Delta \phi=\left(-17.234^{\prime \prime}-.017^{\prime \prime} T\right)$ sin $\Omega$; principal term in obliquity $=\Delta \epsilon=(+9.210+.0009 T) \cos \Omega$ (Newcomb). $T$ centuries from 1900.
Obliquity of ecliptic $=23^{\circ} 27^{\prime} 8.26^{\prime \prime}-0.4684(t-1900)^{\prime \prime}($ Newcomb $)$.
(continued)

TABLE 827.-MISCELLANEOUS ASTRONOMICAL DATA (concluded)
Parallactic inequality moon $=Q=124.785^{\prime \prime}$ (Brown.)
Parsec.-Distance of star whose parallax is $1 \mathrm{sec}=31 \times 10^{12} \mathrm{~km}=19.2 \times 10^{12}$ miles $=3.263$ light years.
Perihelion-Point where earth is nearest sun $=1.4700 \times 10^{18} \mathrm{~cm}$.
Planetary precession $=\lambda=0.1247^{\prime \prime}$ (Newcomb).
Pole of Milky Way = R. A., $12 \mathrm{hr} 48 \mathrm{~min} ;$ Dec., $+27^{\circ}$ :
Refraction. $r$ in. (") $=\left[983 \times\left(\right.\right.$ barometer in in.) $\left./\left(460+t^{\circ} \mathrm{F}\right)\right]$ tan $Z$, where $Z=$ zenith distance. Error $<1^{\prime \prime}, Z<75^{\circ}$, ordinary $t$ and pressure.

Solar diameter $=864,408$ miles .
Solar parallax $=8.80$ (conventional value), 8 ".79 (Newcomb, Spencer Jones).
Sun. $-r=6.965 \times 10^{10} \mathrm{~cm}$. Area $=6.093 \times 10^{24} \mathrm{~cm}^{2}$. Volume $=1.412 \times 10^{38} \mathrm{~cm}^{3}$. Mass $=1.987 \times 10^{33} \mathrm{~g}$. Density $=1.41 \mathrm{~g} / \mathrm{cm}^{3}$. Mean distance to earth $1.495 \times 10^{13} \mathrm{~cm}$. See Table 831.

Twilight.-There are three definitions of twilight: civil, nautical, and astronomical. Civil twilight lasts until the sun is about $6^{\circ}$ below the horizon, after which motor-car lights must be turned on. Nautical twilight lasts until the sun is about $12^{\circ}$ below the horizon. This is the limit for observations of stars with the sea horizon. Astronomical twilight is considered to end when the sky is dark in the zenith. It lasts until the sun is about $18^{\circ}$ below the horizon. For latitudes $>50^{\circ}$ there is a faint twilight at midnight in midsummer.

Year.-Anomalistic (two successive passages of the perihelion) $=365.25964134+3.04$ $\times 10^{-8}(t-1900)$ days. Eclipse (time taken by sun to pass from a node of the moon's orbit to the same node) $=346.620031+3.2 \times 10^{-7}(t-1900)$ days. Sidereal (from given star to same star again) $=365.25636042+1.1 \times 10^{-9}(t-1900)$ days. Tropical (ordinary) (two successive passages of vernal equinox by sun) $=365.24219879-6.14 \times 10^{-8}$ ( $t-1900$ ) days.

## TABLE 828.-ELEMENTS OF SOLAR MOTION *

Because of the asymmetry in stellar motions (Table 876), determinations of the speed and direction of the sun's motion are very sensitive to the selection of stars to which it is referred. Ideally we wish to refer the sun's motion to the circular velocity with respect to the galactic center; this may be called the basic solar motion. It is possible to determine this basic solar motion from detailed studies of the distribution of motions among nearby stars and it is found that such a determination made from the giant $K$ stars is in excellent agreement with an independent determination from the $A$ stars (Janssen and Vyssotsky). This value is given in the last line of the table. The figures listed for the first five groups are smoothed values obtained from a combination of the best observational results. ${ }^{288}$ The values for the next four groups come from investigations made at Leiden, Mount Wilson, and McCormick Observatories. The solar motion with respect to $B$ stars, $c$-stars, and Cepheids is difficult to determine satisfactorily because of uneven distribution in space, very small proper motions, etc.

|  |  | Coordinates of the apex |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Stellar group of reference | Solar velocity | R A | Dec | $\begin{aligned} & \text { Gal } \\ & \text { long } \end{aligned}$ | $\begin{aligned} & \text { Gal } \\ & \text { lat } \end{aligned}$ |
| B8 to A3. | $16 \mathrm{~km} / \mathrm{sec}$ | $263{ }^{\circ}$ | $+20^{\circ}$ | $11^{\circ}$ | $+24^{\circ}$ |
| A5 to F2. | 17 | 266 | $+23$ | 15 | $+22$ |
| F5 to G0. | 18 | 269 | +26 | 18 | $+21$ |
| K 0 to K2. | 20 | 273 | +29 | 23 | $+19$ |
| gK5 to gM8. | 22 | 276 | +31 | 27 | $+17$ |
| dK8 to dM5. | 23 | 275 | $+44$ | 39 | $+22$ |
| Irregular var | 35 | 265 : | +38: | 30 : | +28: |
| Long-period var | 54 | 295 | +46 | 47 | $+10$ |
| Gluster-type var | 130 | 297 | $+52$ | 53 | $+12$ |
| Basic solar motion. | 15 | 260 | $+17$ | 7 | +25 |

[^342]This calendar gives the day of the week for any known date from the beginning of the Christian Era down to the year 2400.

Dominical letters


To find the calendar for any year of the Christian Era, first find the Dominical letter for the year in the upper section of the table. Two letters are given for leap years; the first is to be used for January and February, the second for the other months. In the lower section of the table, find the column in which the Dominical letter for the year is in the same line with the month for which the calendar is desired; this column gives the days of the week that are to be used with the month.
E.g., in the table of Dominical Letters we find that the letter for 1951 is G ; in the line with July, this letter occurs in the first column; hence July 4, 1951, is Wednesday.

[^343]Days are numbered consecutively, beginning with the number 0 , from Greenwich mean noon on Jan. 1, 4713 B.C. The number of days since that time that have elapsed at Greenwich mean noon on any given date is the Julian Day Number of that day.

For A.D. 0 to A.D. 1580 inclusive, the Julian Day Numbers in this table are the days elapsed at Greenwich mean noon up to January 0 of the Julian Calendar in each leap year.

For 1584 to 2096 inclusive, the Julian Day Numbers are for January 0 of the Gregorian Calendar, except that in 1700, 1800, and 1900, which were not leap years, they are for January -1 .

| A.D. | 0 | 100 | 200 | 300 | 400 | 500 | 600 | 700 | 800 | 900 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 1721057 | 1757582 | 1794107 | 1830632 | 1867157 | 1903682 | 1940207 | 1976732 | 2013257 | 782 |
| 4 | 1722518 | 1759043 | 1795568 | 1832093 | 1868618 | 1905143 | 1941668 | 1978193 | 2014718 | 2051243 |
| 8 | 1723979 | 1760504 | 1797029 | 1833554 | 1870079 | 1906604 | 1943129 | 1979654 | 2016179 | 2052704 |
| 12 | 1725440 | 1761965 | 1798490 | 1835015 | 1871540 | 1908065 | 1944590 | 1981115 | 2017640 | 2054165 |
| 16 | 1726901 | 1763426 | 1799951 | 1836476 | 1873001 | 1909526 | 1946051 | 1982576 | 2019101 | 2055626 |
| 20 | 1728362 | 1764887 | 1801412 | 1837937 | 1874462 | 1910987 | 1947512 | 1984037 | 2020562 | 2057087 |
| 24 | 1729823 | 1766348 | 1802873 | 1839398 | 1875923 | 1912448 | 1948973 | 1985498 | 2022023 | 2058548 |
| 28 | 1731284 | 1767809 | 1804334 | 1840859 | 1877384 | 1913909 | 1950434 | 1986959 | 2023484 | 2060009 |
| 32 | 1732745 | 1769270 | 1805795 | 1842320 | 1878845 | 1015370 | 1951895 | 1988420 | 2024945 | 2061470 |
| 36 | 1734206 | 1770731 | 1807256 | 1843781 | 1880306 | 1916831 | 1953356 | 1989881 | 2026406 | 2062931 |
| 40 | 1735667 | 1772192 | 1808717 | 1845242 | 1881767 | 1918292 | 1954817 | 1991342 | 2027867 | 2064392 |
| 44 | 1737128 | 1773653 | 1810178 | 1846703 | 1883228 | 1919753 | 1956278 | 1992803 | 2029328 | 2065853 |
| 48 | 1738589 | 1775114 | 1811639 | 1848164 | 1884689 | 1921214 | 1957739 | 1994264 | 2030789 | 2067314 |
| 52 | 1740050 | 1776575 | 1813100 | 1849625 | 1886150 | 1922675 | 1959200 | 1995725 | 2032250 | 2068775 |
| 56 | 1741511 | 1778036 | 1814561 | 1851086 | 1887611 | 1924136 | 1960661 | 1997186 | 2033711 | 2070236 |
| 60 | 1742972 | 1779497 | 1816022 | 1852547 | 1889072 | 1925597 | 1962122 | 1998647 | 2035172 | 2071697 |
| 64 | 1744433 | 1780958 | 1817483 | 1854008 | 1890533 | 1927058 | 1963583 | 2000108 | 2036633 | 2073158 |
| 68 | 1745894 | 1782419 | 1818944 | 1855469 | 1891994 | 1928519 | 1965044 | 2001569 | 2038094 | 2074619 |
| 72 | 1747355 | 1783880 | 1820405 | 1856930 | 1893455 | 1929980 | 1966505 | 2003030 | 2039555 | 2076080 |
| 76 | 1748816 | 1785341 | 1821866 | 1858391 | 1894916 | 1931441 | 1967966 | 2004491 | 2041016 | 2077541 |
| 80 | 1750277 | 1786802 | 1823327 | 1859852 | 1896377 | 1932902 | 1969427 | 2005952 | 2042477 | 2079002 |
| 84 | 1751738 | 1788263 | 1824788 | 1861313 | 1897838 | 1934363 | 1970888 | 2007413 | 2043938 | 2080463 |
| 88 | 1753199 | 1789724 | 1826249 | 1862774 | 1899299 | 1935824 | 1972349 | 2008874 | 2045399 | 2081924 |
| 92 | 1754660 | 1791185 | 1827710 | 1864235 | 1900760 | 1937285 | 1973810 | 2010335 | 2046860 | 2083385 |
| 96 | 1756121 | 1792646 | 1829171 | 1865696 | 1902221 | 1938746 | 1975271 | 2011796 | 2048321 | 2084846 |
| A.D. | 1000 | 1100 | 1200 | 1300 | 1400 | 1500 | 1600 | 1700 | 1800 | 1900 |
| 0 | 2086307 | 2122832 | 2159357 | 2195882 | 2232407 | 2268932 | 2305447 | 23+1971† | $2378495 \dagger$ | $2415019 \dagger$ |
| 4 | 2087768 | 2124293 | 2160818 | 2197343 | 2233868 | 2270393 | 2306908 | 2343432 | 2379956 | 2416480 |
| 8 | 2089229 | 2125754 | 2162279 | 2198804 | 2235329 | 2271854 | 1308369 | 2344893 | 2381417 | 2417941 |
| 12 | 2090690 | 2127215 | 2163740 | 2200265 | 2236790 | 2273315 | 2309830 | 2346354 | 2382878 | 2419402 |
| 16 | 2092151 | 2128676 | 2165201 | 2201726 | 2238251 | 2274776 | 2311291 | 2347815 | 2384339 | 2420863 |
| 20 | 2093612 | 2130137 | 2166662 | 2203187 | 2239712 | 2276237 | 2312752 | 2349276 | 2385800 | 2422324 |
| 24 | 2095073 | 2131598 | 2168123 | 2204648 | 2241173 | 2277698 | 2314213 | 2350737 | 2387261 | 2423785 |
| 28 | 2096534 | 2133059 | 2169584 | 2206109 | 2242634 | 2279159 | 2315674 | 2352198 | 2388722 | 2425246 |
| 32 | 2097995 | 2134520 | 2171045 | 2207570 | 2244095 | 2280620 | 2317135 | 2353659 | 2390183 | 2426707 |
| 36 | 2099456 | 2135981 | 2172506 | 2209031 | 2245556 | 2282081 | 2318596 | 2355120 | 2391644 | 2428168 |
| 40 | 2100917 | 2137442 | 2173967 | 2210492 | 2247017 | 2283542 | 2320057 | 2356581 | 2393105 | 2429629 |
| 44 | 2102378 | 2138903 | 2175428 | 2211953 | 2248478 | 2285003 | 2321518 | 2358042 | 2394566 | 2431090 |
| 48 | 2103839 | 2140364 | 2176889 | 2213414 | 2249939 | 2286464 | 2322979 | 2359503 | 2396027 | 2432551 |
| 52 | 2105300 | 2141825 | 2178350 | 2214875 | 2251400 | 2287925 | 2324440 | 2360964 | 2397488 | 2434012 |
| 56 | 2106761 | 2143286 | 2179811 | 2216336 | 2252861 | 2289386 | 2325901 | 2362425 | 2398949 | 2435473 |
| 60 | 2108222 | 2144747 | 2181272 | 2217797 | 2254322 | 2290847 | 2327362 | 2363886 | 2400410 | 2436934 |
| 64 | 2109683 | 2146208 | 2182733 | 2219258 | 2255783 | 2292308 | 2328823 | 2365347 | 2401871 | 2438395 |
| 68 | 2111144 | 2147669 | 2184194 | 2220719 | 2257244 | 2293769 | 2330284 | 2366808 | 2403332 | 2439856 |
| 72 | 2112605 | 2149130 | 2185655 | 2222180 | 2258705 | 2295230 | 2331745 | 2368269 | 2404793 | 2441317 |
| 76 | 2114066 | 2150591 | 2187116 | 2223641 | 2260166 | 2296691 | 2333206 | 2369730 | 2406254 | 2442778 |
| 80 | 2115527 | 2152052 | 2188577 | 2225102 | 2261627 | $2298152 \ddagger$ | 2334667 | 2371191 | 2407715 | 2444239 |
| 84 | 2116988 | 2153513 | 2190038 | 2226563 | 2263088 | $2299603 \S$ | 2336128 | 2372652 | 2409176 | 2445700 |
| 88 | 2118449 | 2154974 | 2191499 | 2228024 | 2264549 | 2301064 | 2337589 | 2374113 | 2410637 | 2447161 |
| 92 | 2119910 | 2156435 | 2192960 | 2229485 | 2266010 | 2302525 | 2339050 | 2375574 | 2412098 | 2448622 |
| 96 | 2121371 | 2157896 | 2194421 | 2230946 | 2267471 | 2303986 | 2340511 | 2377035 | 2413559 | 2450083 |
|  | 2000 | 2451544 | 2020 | 2458849 | 2040 | 2466154 | 2060 | 2473459 | 2080 | 2480764 |
|  | 2004 | 2453005 | 2024 | 2460310 | 2044 | 2467615 | 2064 | 2474920 | 2084 | 2482225 |
|  | 2008 | 2454466 | 2028 | 2461771 | 2048 | 2469076 | 2068 | 2476381 | 2088 | 2483686 |
|  | 2012 | 2455927 | 2032 | 2463232 | 2052 | 2470537 | 2072 | 2477842 | 2092 | 2485147 |
|  | 2016 | 2457388 | 2036 | 2464693 | 2056 | 2471998 | 2076 | 2479303 | 2096 | 2486608 |

Days to be added to reduce to the beginning of each month: For dates from 1582 October 15 to 1583 December 31, inclusive, Gregorian Calendar, diminish all numbers in this table by 10.

In 1700, 1800, and 1900, Gregorian Calendar, for January 0 use the number 1 instead of the tabular value 0 , and for February 0 use 32 instead of 31.

| Year | Jan. 0 | Feb. 0 | Mar. 0 | Apr. 0 | May 0 | June 0 | July 0 | Aug. 0 | Sept. 0 | Oct. 0 | Nov. 0 |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | Dec. 0

[^344]TABLE 831.-PHYSICAL DATA; PLANETS AND PRINCIPAL SATELLITES
(From unpublished compilation by G. P. Kuiper and D. L. Harris, Yerkes Observatory.)

| Planet or satellite | $\begin{gathered} \text { Mass * } \\ (\text { Earth }=1) \end{gathered}$ | $\begin{gathered} \text { Mean } \\ \begin{array}{c} \text { diameter } \\ (E=1) \end{array} \dagger \end{gathered}$ | $\begin{gathered} \text { Mean } \\ \text { density } \\ \mathrm{H}_{2} \mathrm{O}=1 \end{gathered}$ | Surface gravity ( $E=1$ ) | Velocity of escape $\mathrm{km} / \mathrm{sec}$ | Rotation period (days) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mercury | . 0543 | . 38 | 5.46 | . 38 | 4.3 | 88.0 |
| Venus . | . 8136 | . 967 | 4.96 | . 87 | 10.4 | 15-30? |
| Farth | 1.0000 | 1.000 | 5.52 | 1.00 | 11.3 | 1.00 |
| Mars | . 1069 | . 523 | 4.12 | . 39 | 5.1 | 1.03 |
| Jupiter | 318.35 | 10.97 | 1.33 | 2.65 | 61.0 | . 41 |
| Saturn | 95.3 | 9.03 | . 71 | 1.17 | 36.7 | . 43 |
| Uranus | 14.58 | 3.72 | 1.56 | 1.05 | 22.4 | . 45 |
| Neptune | 17.26 | 3.38 | 2.47 | 1.23 | 25.6 | . 66 |
| Pluto . . | < 1 ? | . 45 | $<5.5$ ? | $<.5$ ? | $<5.3$ ? | ? |
| Moon | . 0123 | . 273 | 3.33 | . 16 | 2.4 | 27.3 |
| Jupiter I | . 0121 | . 255 | 4.03 | . 19 | 2.5 | 1.77 |
| Jupiter II | . 0079 | . 226 | 3.78 | . 16 | 2.1 | 3.55 |
| Jupiter III | . 0261 | . 394 | 2.35 | . 17 | 2.9 | 7.15 |
| Jupiter IV | . 0160 | . 350 | 2.06 | . 13 | 2.4 | 16.69 |
| Titan . | . 0235 | . 371 | 2.54 | . 17 | 2.8 | 15.95 |
| Triton | . 022 | . 35 ? | 2.8? | .18? | 2.8? | 5.88 |

[^345]TABLE 832._PLANETARY TEMPERATURES


All temperatures are given on the absolute scale. To change to centigrade, sibtract 273. The column headed "measured" presents values determined by Coblentz and Lampland, and by Pettit and Nicholson. The column headed " $A$ " gives black sphere temperatures; " $B$ " gives these multiplied by $\sqrt{2}$ or the calculated maximum temperatures of the center of the illuminated hemisphere of atmosphereless black plancts. The observed values lie, as expected, between $A$ and $B$ in nearly pwery case.

TABLE 833.-PLANETARY ORBITS * 257

| Body | Mean distance to Sun |  | Sidereal period |  | Inclination | Eccentricity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\overparen{A Y^{\circ}}$ | km | Mean <br> days | Tropical years |  |  |
| Mercury | . 387 | $57.9 \dagger$ | 87.97 | . 241 | $7: 004$ | . 2056 |
| Venus | . 723 | 108.1 | 224.70 | . 615 | 3.394 | . 0068 |
| Earth | 1.000 | $149.5 \ddagger$ | 365.26 | 1.000 | . 000 | . 0167 |
| Mars | 1.524 | 227.8 | 686.98 | 1.881 | 1.850 | . 0934 |
| Jupiter | 5.203 | 777.8 | 4332.58 | 11.862 | 1.306 | . 0484 |
| Saturn | 9.539 | 1426.1 | 10759.20 | 29.458 | 2.490 | . 0557 |
| Uranus | 19.191 | 2869.1 | 30685.91 | 84.015 | . 773 | . 0472 |
| Neptune | 30.071 | 4495.6 | 60187.60 | 164.788 | 1.774 | . 0086 |
| Pluto | 39.457 | 5898.9 | 90469.27 | 247.697 | 17:143 | . 2485 |

[^346]| Body | Mean distance from planet ( km ) | Sidereai period (days) | $V$ is magnitude at mean opp | Direction of motion $\dagger$ |
| :---: | :---: | :---: | :---: | :---: |
| Earth |  |  |  |  |
| Moon | 384,400 | 27.322 | $-12.7$ | D |
| Mars |  |  |  |  |
| Phobos | 9,400 | . 319 | 11.5 | D |
| Deimos | 23,500 | 1.262 | 13.0 | D |
| Jupiter |  |  |  |  |
| V | 181,200 | . 498 | 13.0 | D |
| I Io | 421,400 | 1.769 | 5.0 | D |
| II Europa | 670,500 | 3.551 | 5.3 | D |
| III Ganymede | 1,069,500 | 7.155 | 4.6 | D |
| IV Callisto . | 1,881,200 | 16.689 | 5.6 | D |
| VI | 11,500,000 | 250.6 | 137 | D |
| VII | 11,750,000 | 259.6 | 16. | D |
| X | 11,750,000 | 260. | 17.8 | D |
| VIII | 23,500,000 | 739. | 16. | R |
| IX | 23,700,000 | 758. | 17.6 | R |
| XI | 22,500,000 | 692. | 17.4 | R |
| Saturn |  |  |  |  |
| Mimas | 185,500 | . 942 | 12.1 | D |
| Enceladus | 238,000 | 1.370 | 11.6 | D |
| Tethys | 294,600 | 1.888 | 10.5 | D |
| Dione | 377,300 | 2.737 | 10.7 | D |
| Rhea | 526,900 | 4.518 | 9.7 | D |
| Titan | 1,220,800 | 15.945 | 8.2 | D |
| Hyperion | 1,482,000 | 21.277 | 13.0 | D |
| Iapetus . | 3,558,000 | 79.330 | 10.1-11.8 | D |
| Phoebe | 12,950,000 | 550.48 | 16. | R |
| Uranus |  |  |  |  |
| Miranda | 129,700 | 1.413 | 16.8 | D |
| Ariel | 190,700 | 2.520 | 14.8 | D |
| Umbriel | 265,700 | 4.144 | 15.4 | D |
| Titania | 435,800 | 8.706 | 13.9 | D |
| Oberon | 582,800 | 13.463 | 14.3 | D |
| Neptune |  |  |  |  |
| Triton | 353,700 | 5.877 | 13.5 | R |
| Nereid | 5,580,000 | 368. | 18.5 | ? |

[^347] direct motion, $R=$ retrograde motion.

TABLE 835.—NUMBER OF STARS [ $\phi$ (M)] PER CUBIC PARSEC NEAR THE SUN WITH ABSOLUTE (PHOTOGRAPHIC AND VISUAL) MAGNITUDES $M-1 / 2$ TO $M+1 / 2$ * ${ }^{259}$

|  | $\log \phi(M)+10$ |  |  | $\log \phi(M)+10$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | M | Phot | Visual | M | Phot | Visual |
|  | $-6.0$ | 2.10 | 1.63 | $+5.0$ | 7.35 | 7.40 |
|  | $-5.0$ | 3.07 | 2.77 | + 6.0 | 7.49 | 7.45 |
| - | $-4.0$ | 3.65 | 3.58 | + 7.0 | 7.53 | 7.45 |
|  | $-3.0$ | 4.25 | 4.12 | +8.0 | 7.46 | 7.55 |
|  | $-2.0$ | 4.75 | 4.71 | + 9.0 | 7.49 | 7.75 |
|  | $-1.0$ | 5.07 | 5.32 | $+10.0$ | 7.64 | 7.84 |
|  | . 0 | 5.68 | 5.98 | +11.0 | 7.81 | 7.99 |
|  | $+1.0$ | 6.34 | 6.59 | +12.0 | 7.97 | 8.02 |
|  | + 2.0 | 6.77 | 6.71 | +13.0 | 8.01 | 8.05 |
|  | + 3.0 | 6.86 | 6.98 | $+14.0$ | 8.06 | . . . |
|  | + 4.0 | 7.19 | 7.29 |  |  |  |

[^348]Relationship between diameter and depth of terrestrial explosion craters, terrestrial meteoritic craters and lunar craters. (All explosions occurred slightly below the surface.)

$$
D=0.1083 d^{2}+0.6917 d+0.75
$$

where

$$
\begin{aligned}
D & =\log \text { diameter (feet) } \\
d & =\log \text { depth (feet) }
\end{aligned}
$$

Examples:

|  | Diameter | Observed depth | $\begin{gathered} \text { Calculated } \\ \text { depth } \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| Shell crater | 10 ft | $3 \mathrm{ft}+$ | 2.20 ft |
| Arizona meteorite crater | 4150 ft | 700 ft (originally) | 732 ft |
| Lunar crater Moretus | 77 mi | $14,600 \mathrm{ft}$ | $16,900 \mathrm{ft}$ |

Relationship between diameter of crater and rim height above ground level for terrestrial explosion craters, terrestrial meteoritic craters, and lunar craters.

$$
E=-0.097 D^{2}+1.542 D-1.841
$$

where
$E=\log$ rim height (feet)
$D=\log$ diameter (feet)
Examples:

| Examples. | Diameter | Observed rim height | Calculated rim height |
| :---: | :---: | :---: | :---: |
| Shell crater | 10 ft | $.4 \mathrm{ft} \pm$ | 40 ft |
| Arizona meteorite crater | 4150 ft | 165 ft (past erosion | 295 ft |
| Lunar crater Cleomedes | 80 mi | 5200 ft | 5830 ft |

Terrestrial meteoritic craters

|  | $\underset{(\mathrm{ft})}{\text { Diameter }}$ | Present depth (ft) | Original depth (ft) | $\begin{aligned} & \text { Present } \\ & \text { rim height } \end{aligned}$ | Discovered |
| :---: | :---: | :---: | :---: | :---: | :---: |
| American craters: 4150 |  |  |  |  |  |
| Arizona ........ | 4150 | 570 | 700 | 165 | 1891 |
| Odessa 1, near Odessa, Tex. | 550 | 14 | 130 | 12 | 1921 |
| Odessa 2 | 70 | shallow | 17 | 0 | 1921 |
| At least one other small crater identified nearby |  |  |  |  |  |
|  | d $56 \times 36$ | shallow | >10 | 0 | 1933 |
| Chubb (Quebec) | $2 \frac{1}{2} \mathrm{mi}$ | filled-i | overed lake | 550 | 1950 |
| South American craters: |  |  |  |  | Pits known |
| Campo del Cielo, Argentine; many craters | . 20 to 254 |  | $\ldots$ |  | since 1576 |
| Australian craters: |  |  |  |  |  |
| Henbury 1, near Henbury cattle station | 75 | shallow |  | 0 | 1930 |
| 2 2................................... | 90 | shallow | $\ldots$ | 0 | 1930 |
| 3 | 135 | 18 | $\ldots$ | 2 | 1930 |
| 4 | 135 | 18 |  | 2 | 1930 |
| 5 | 75 | 6 | $\cdots$ | 4 | 1930 |
| 6 | 240 | 25 | ... | 12 | 1930 |
| 7 (probably double) | $660 \times 360$ | 60 | $\ldots$ | high | 1930 |
| $8 . .$. | 175 | 15 |  | high | 1930 |
| 9 ...................................... . . | small |  |  |  | 1930 |
| 10 | 60 | shallow |  | low | 1930 |
| 11 | 45 |  |  |  | 1930 |
| 12 | 60 |  |  | 12 | 1930 |
| 13 ............................ | 30 | 3 | 10 | low | 1930 |
| Boxhole crater, 200 miles N. E. of |  |  |  |  |  |
| Dalgaranga crater ................... | . 230 | 16 | ... | prominent | 1923 |

[^349](continued)


The 1947 meteorite probably disintegrated high in the air. The 1908 meteorite exploded violently either just before striking the ground or immediately after a ricochet. All others seem to have struck the ground, penetrated a short distance, and then exploded.

It will be noticed that there is a tendency for several craters to be formed simultaneously as if the meteorites traveled in clusters.

Only authenticated craters are here listed. Possible or doubtful cases have been omitted.

TABLE 837.-ALBEDOS

| Object | $m$ | ${ }^{9}$ | $\sigma$ | $p$ | $q$ | Visual albedo | Color index | Photographic albedo |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Moon | -12.66 | +. 29 | 2".40 | . 104 | . 694 | . 072 | $+.75$ | . 059 |
| Mercury | - 2.20 | -. 14 | 3.34 | . 080 | . 72 | . 058 | $+1.00$ | . 038 |
| Venus | - 5.12 | -4.41 | 8.50 | . 630 | 1.20 | . 76 | $+.62$ | . 70 |
| Mars | - 1.88 | -1.39 | 4.60 | . 133 | 1.11 | . 148 | $+1.00$ | . 088 |
| Jupiter | $-2.53$ | $-9.23$ | 95.19 | . 424 | 1.2: | . 51 | +. 67 | . 45 |
| Saturn | + .76 | -8.80 | 78.95 | . 416 | 1.2 : | . 50 | +. 90 | . 36 |
| Uranus | + 5.55 | -7.17 | 32.4 | . 548 | 1.2 : | . 66 | + . 42 | . 73 |
| Neptune | + 7.80 | -6.91 | 29.7 | . 514 | 1.2: | . 62 | +. 42 | . 68 |
| Pluto | +14.74 | -1.17 | 4.0 | . 146 | 1.1 : | . 16 | +. 67 | . 14 |

Table compiled by D. L. Harris on the basis of measures by G. Müller and E. S. King and reduced to the International Photovisual System. Long-period variations of the outer planets have been suspected by W. Becker ${ }^{\text {zand }}$ but are subject to confirmation.

The albedo, according to Pond, is defined as follows: "Let a sphere $S$ be exposed to parallel light. Then its albedo is the ratio of the whole amount reflected from $S$ to the whole amount of light incident on it." In the above table, $m=$ the stellar magnitude at mean opposition: $y=$ magnitucle it would have at full phase and unit distance from earth and sun; $\sigma=$ assumed mean semidiameter at unit distance; $p=$ ratio of observed brightness at full phase to that of a flat disk of same size and same position, illuminated and viewed normally and reflecting all the incident light according to Lambert's law ; q depends on law of variation of light with phase; albedo $=p q$.
Albeds of the earth: $0.39 .^{\text {2an }}$

[^350]




[^351]

## Part 1.-Density and pressure

The density distribution in the earth's interior is obtained by a series of approximations made to conform with known data as boundary conditions. These known facts, with which any density distribution must harmonize, include the following:
(1) The average density is 5.522 , obtained by comparing the attraction of the earth with that of a known mass. Dr. Heyl's value for the constant of gravitation is used, $6.664 \times 10^{-8}$ dyne $\mathrm{cm}^{2} g^{-2}$ (Table 27).
(2) The precession constant and other astronomic and geodetic data (Table 827) give the earth's moments in inertia. $I=0.33344 \mathrm{Er}^{2}$ where $I$ is the moment of inertia about the polar axis, $r$ the equatorial radius, and $E$ the mass of the earth; further

$$
I=\frac{8 \pi}{15} \int \rho d\left(a r^{4}\right)
$$

where $a$ is the polar semi-axis and $\rho=f(a, r)$, the density. If the earth were a homogeneous sphere its moment of inertia would be $0.4 \mathrm{Mr}^{2}$ and density 4.6 .
(3) The known flattening of the earth from geodetic data is $1 / 297$. If the earth were homogeneous the flattening would be larger. These should be sufficient to give a unique density distribution but, as Lambert of the Coast and Geodetic Survey pointed out, a distribution satisfying condition (2) also satisfies condition (3).
(4) The last boundary condition results by comparing the elastic behavior at various depths with the known elastic constants of rocks. Time-distance curves of earthquake impulses enable one to calculate the velocities of the compressional, $V_{p}$, and distortional, $V_{s}$, waves at various depths in the earth. Assuming isotropy there are simple relations between $K, R, E$ (moduli of compression, rigidity, Young's respectively), $\sigma$ (Poisson's ratio), $V_{p}$ and $V$ such that if the density and any two of them are known the others can be had. The variation in elastic constants for different rocks is small but sufficient to permit discrimination when compared with the elastic properties at different depths computed by means of the equations

$$
V_{s}^{2}=R / \rho, \quad V_{p}^{2}-4 / 3 V_{s}^{2}=K / \rho, \quad\left(V_{p} / V_{s}\right)^{2}=\frac{2(1-\sigma)}{1-2 \sigma}
$$

The uncertainties result from extrapolating low pressure and temperature laboratory data to high pressures and temperatures.

Whence we deduce: "granitic" material to a depth of 10 to 30 km ; below this the rock is denser, about 3.0 , and corresponds to a basalt or gabbro. At about 45 km depth a discontinuity occurs; the change in elastic properties corresponds with a transition to peridotite, density 3.4 . From this depth to $1,600 \mathrm{~km}$ the variation is uniform, the density increasing slowly with pressure. From 1,600 to $2,900 \mathrm{~km}$ the earthquake velocities remain somewhat constant and could be accounted for by a slow addition of iron and nickel to the material, the density changing from 3.4 to 9.0 . Below. $2,900 \mathrm{~km} V_{p}$, begins to decrease slightly and the assumption is that this core consists of nickel-iron with a density at the center of about 10.7.

| Depth | Density | Pressure | Rock type |
| :---: | :---: | :---: | :---: |
| 0 km | $2.7 \mathrm{~g} / \mathrm{cm}^{3}$ |  | Granitic |
| 10 | 2.7 | . $0027 \times 10^{6} \mathrm{~kg} / \mathrm{cm}^{2}$ |  |
| 30 | 3.0 | . 0067 | Basaltic |
| 60 | 3.4 | . 0171 | Peridotitic |
| 120 | 3.5 | . 0381 |  |
| 400 | 3.75 | . 131 |  |
| 800 | 4.0 | . 30 |  |
| 1200 | 4.25 | 47 |  |
| 1700 | 4.4 | . 68 |  |
| 2000 | 5.8 | . 84 |  |
| 2450 | 7.25 | 1.135 |  |
| 2900 | 9.0 | 1.5 | Transition layer |
| 3200 | 9.6 | 1.7 |  |
| 4800 | 10.25 | 2.8 | Ni -Fe core |
| 6370 | 10.7 | 3.1 |  |

[^352](continued)

TABLE 839.-CHARACTERISTICS OF EARTH'S INTERIOR (concluded)
Part 2.-Elastic constants of earth's interior

| Depth km | $\begin{aligned} & \text { Bulk modulus } \\ & \times 10^{-12} \\ & \text { dynes } / \mathrm{cm}^{2} \end{aligned}$ | $\begin{gathered} \text { Rigidity } \\ \times 10^{-12} \\ \text { dynes } / \mathrm{cm}^{2} \end{gathered}$ | $\begin{gathered} \text { Depth } \\ \mathbf{k m} \end{gathered}$ | $\begin{gathered} \text { Bulk modulus } \\ \times 10^{-12} \\ \text { dynes } / \mathrm{cm}^{2} \end{gathered}$ | $\begin{gathered} \text { Rigidity } \\ \times 10^{-12} \\ \text { dynes } / \mathrm{cm}^{2} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | . 415 | . 26 | 1200 | $3.6 \pm .3$ | $2.2 \pm .3$ |
| 0-20 | . $5 \pm .05$ | . $3 \pm .05$ | 1700 | $4.2 \pm .3$ | $2.7 \pm .3$ |
| 20-45 | . $7 \pm .1$ | $.4 \pm .1$ | 2850 | $8 \pm 2$ | $4.0 \pm 1.0$ |
| 45-120 | $1.4 \pm .2$ | . $6 \pm .1$ | 2900 | $7 \pm 1$ ? | Smaller than at |
| 120-400 | $1.6 \pm .2$ | $1.0 \pm .2$ | 6370 | $12 \pm 10$ ? | surface, perhaps zero. |

## Part 3.-Velocities of earthquake waves

$V_{n}^{\prime}$ is the velocity in $\mathrm{km} / \mathrm{sec}$ of the primary or condensational wave, $V_{s}$, of the secondary or distortional wave. Turner speaks of them as the push and shake waves.

| Layer | $V_{p}, \mathrm{~km} / \mathrm{sec}$ | $V_{*}, \mathrm{~km} / \mathrm{sec}$ |
| :---: | :---: | :---: |
| 0 to $20 \pm 10 \mathrm{~km}$ depth, depending on locality | 5.4 to 5.6 , depending on locality. May reach 6.1 | $3.2 \pm .3$ |
| $20 \pm 10$ to $45 \pm 10 \mathrm{~km}$ depth, depending on locality | 6.25 to 6.75 , depending on locality | $3.5 \pm .3$ |
| Between $45 \pm 10$ and 2900 km depth: |  |  |
| $45 \pm 10$ 1300 | $\begin{array}{r}8.0 \\ 12.5 \pm .1 \\ \hline .1\end{array}$ | $4.4 \pm .2$ $6.9 \pm .2$ |
| 2400 | $13.5 \pm .1$ | $7.5 \pm .2$ |
| $<2900$ | $13.5 \pm .1$ | $7.4 \pm .2$ |
| Core, 2700 to 6370 km (center) : $\begin{aligned} & >2900 \\ & 6000 \end{aligned}$ | $\begin{array}{r} 8.7 \pm .2 \\ 10.9 \pm .2 \end{array}$ | $\begin{aligned} & 7 \\ & ? \end{aligned}$ |

## TABLE 840.—BULK MODULI OF ROCK-FORMING MINERALS*

The bulk modulus, $K$, of a compact holocrystalline rock can be obtained with a fair degree of accuracy except for low pressures by adding the proportionate bulk moduli of the constituent minerals.

Pressure, $P$, and $K \times 10^{-8}$ are in bars.

|  | Pressure in bars |  |  |
| :---: | :---: | :---: | :---: |
| Mineral | 1 | 2,000 | 10,000 |
| Feldspar: Orthoclase | . 527 | . 538 | . 603 |
| Oligoclase, $\mathrm{Ab}_{7 \times} \mathrm{An}_{122}$ | . 582 | . 592 | . 641 |
| Labradorite, $\mathrm{Ab}_{4} \mathrm{An}_{52}$ | . 654 | . 671 | . 758 |
| Pyroxene: Orthorhombic ..... |  | 1.00 | 1.00 |
| Diopside .... | . 935 | . 935 | . 935 |
| Augite .. | . 981 | . 981 | . 981 |
| Hornblende: Actinolite | . 769 | . 769 | . 769 |
| Mica: Phlogopite .... | . 431 | . 451 | . 516 |
| Quartz ......... | . 373 | . 383 | .437 |
| Calcite | . 736 | . 741 | . 758 |
| Magnetite | 1.818 |  |  |
| Corundum | 2.44 | - | - |
| Tourmaline | 1.22 | - | - |
| Rutile | 1.72 | - | - |

[^353]$P$ (pressure), and $K, R . E$ (bulk, rigidity, and Young's moduli resp), are given in bars ( 1 bar $=10^{0}$ dynes $\left./ \mathrm{cm}^{2}\right) . V_{p}$ and $V_{s}^{\prime}$ (compressional and distortional wave velocities respectively), are in $\mathrm{km} / \mathrm{sec} . \sigma$ is Poisson's ratio and $\rho$ is the density. $\rho$ is in $\mathrm{g} / \mathrm{cm}^{3}$.
Dynamically determined elastic constants are surrounded by parentheses (single parenthesis represents seismic data) ; the others are static determinations. Italicized figures are calculated. In places where insufficient data were present to complete the calculations, figures in square brackets have been assumed. In the " $P$ " column m.s. denotes mean stress.

The basis of this table includes data of L. H. Adams and Williamson, F. D. Adams and Coker, Bridgman and others.

| Name | $P$ | $K \times 10^{-18}$ | $\stackrel{\sigma}{0}$ | $R \times 10^{-0}$ | $E \times 10^{-8}$ | ${ }^{\rho}$ | $V_{p}$ | $V$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Granite |  | (.439) | (.32) | (.18) | (.46) | 2.62 | (5.05) | (2.62) |
|  | m.s. 350 | . 303 | . 23 | . 20 | . 50 |  |  |  |
|  | 2000 | . 472 | [.28] | . 26 | . 62 | 2.62 | 5.53 | 3.05 |
|  | 10000 | . 552 | [.28] | . 29 | . 73 | 2.67 | 5.91 | 3.26 |
| Basalt | 200 | (.476) | (.30) | (.22) | (.58) | 2.91 | (5.06) | (2.72) |
|  | 2000 | . 538 | [.28] | . 28 | . 71 | 2.91 | 5.59 | 3.08 |
|  | 10000 | . 654 | [.28] | . 34 | . 86 | 2.95 | 6.11 | 3.38 |
|  |  | . 606 | . 24 | . 35 | . 84 | 2.85 |  |  |
| Gabbro, norite, diabase. | 12 | (.041) | (.27) | (.35) | $\begin{gathered} (.88) \\ (. .911)) \end{gathered}$ | 2.85 | (6.22) | (3.49) |
|  | 600 | . 641 |  |  | (.91)) |  |  |  |
|  | 2000 | . 700 | [.27] | . 38 | . 97 | 2.85 | 6.50 | 3.65 |
|  | 10000 | . 714 | [.27] | . 39 | . 99 | 2.89 | 6.54 | 3.67 |
| Olivine diabase, olivine gabbro | $1\{$ | . 736 | . 28 | . 38 | $\stackrel{1.01}{(.985))}$ | $\stackrel{3.00}{-}$ - | 6.46 | 3.57 |
|  | m.s. 350 | . 741 | . 28 | . 37 | . 95 | 3.00 |  |  |
|  | 600 | . 752 | - | - |  |  |  |  |
|  | 2000 | . 806 | [.28] | . 42 | 1.06 | 3.01 | 6.7 | 3.7 |
|  | 10000 | . 826 | [.28] | . 43 | 1.09 | 3.08 | 6.7 | 3.7 |
| Peridotite dunite | 1 | 1.064 | [.27] | . 58 | 1.47 | 3.28 | 7.5 | 4.2 |
|  | 2000 | 1.191 | [.27] | . 65 | 1.64 | 3.28 | 7.9 | 4.4 |
|  | 10000 | 1.265 | [.27] | . 69 | 1.74 | 3.29 | 8.15 | 4.57 |
| Obsidian | 1 | . 345 | . 17 | - | ( (.682)) | 2.34 | - |  |
|  | 2000 | . 352 |  | - | - | 2.35 |  |  |
| Basalt glass | 10000 | . 352 |  | - | - | 2.41 |  |  |
| Cryst limestone, parallel bed | $\left.\begin{array}{r}2000 \\ 10000\end{array}\right\}$ | . 690 | $\{1 . \overline{27}]$ |  | 95 | 2.85 | 6.4 |  |
|  | $\begin{array}{r} 100005 \\ \text {.m.s. } 350 \end{array}$ | . 437 | [1.27] | . 37 | . 95 | 2.89 | 6.4 | 3.6 |
|  | 7000 | . 715 | [.28] | . 37 | . 94 | 2.71 | 6.68 | 3.69 |
|  | 1 | (.439) | (.29) | (.17) | (.55) | 2.71 | (5.2) | (2.81) |
|  |  | . 402 | . 26 | . 23 | . 57 | 2.69 |  | - |
| Quartzitic sandstone | 1 | . 374 | . 21 | . 27 | . 65 | 2.64 | 5.3 | 1.9 |
|  | 2000 10000 | .383 .437 | [. $\overline{27}]$ | 24 | . 60 | 2.70 | 5.4 | 2.9 |

* Compiled by R. W. Goranson.


## TABLE 842.-AGE OF EARTH, MOON, AND STRATA

The age of the earth is probably from ( 1.3 to 3 ) $\times 10^{8}$ years (radioactive data). Its liquefaction was probably complete within 5,000 years, solidification within 15,000 years from start. The age of the earth's crust may be taken as roughly 2,000 million years.

Ages of geologic strata

| Late Oligocene .... | $37,000,000 \mathrm{yr}$ | Late pre-Cambrian (?). $\quad 587,000,000 \mathrm{yr}$ |
| :---: | :---: | :---: |
| Permian-Carboniferous | 204,000,000 | Middle pre-Cambrian ... 987,000,000 to |
| Permian to Devonian... | $\begin{aligned} & 239,000,000 \text { to } \\ & 374,000,000 \mathrm{yr} \end{aligned}$ | Lower pre-Cambrian ... $1,087,000,000 \mathrm{yr}$ |

The diagram, figure 31, prepared by the U. S. Naval Observatory, shows the paths of total and total-annular eclipses in the United States during the twentieth century. The following data for total United States solar eclipses betwcen 1950 and 2000 are taken from the complete table of eclipses from A.D. 1900-A.D. 2000, given by D. H. Menzel. ${ }^{202}$

| Date | Beginning |  | "Noon" |  | End |  | Maximum duration |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Lati- tude | Longitude | Latitude | Longitude | Latitude | Longitude |  |  |
| June 30, 1954. | $+42^{\circ}$ | + $99^{\circ}$ | $+62^{\circ}$ | + $5^{\circ}$ | $+26^{\circ}$ | $-74^{\circ}$ | $2{ }^{\text {m }}$ | $40^{\circ}$ |
| October 2, 1959 | +42 | + 72 | $+23$ | + 6 | + 7 | -56 | 3 |  |
| July 20, 1963. | +43 | -143 | +62 | +126 | +33 | +44 | 1 |  |
| March 7, 1970 | -2 | +149 | +25 | + 88 + | +55 | +23 | 3 |  |
| February 26, 1979 | +47 | +140 | +61 | + 77 | +77 | +34 | 3 |  |

[^354]

Fig. 31.-Curves showing the paths of solar eclipses during the twentieth century.

TABLE 843.-SPECTRUM CLASS AND PROPER MOTIONS*

| Limits of pm | 0 | B | $A$ | $F$ | G | K | M | $N$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ".00 to "02. | 13 | 238 | 392 | 97 | 107 | 218 | 48 | 3 |
| . 02 to . 04 | 6 | 164 | 533 | 115 | 91 | 327 | 54 | 4 |
| . 04 to . 10. | 1 | 88 | 476 | 231 | 168 | 393 | 99 | 2 |
| . 10 to . 20. |  |  | 160 | 245 | 70 | 242 | 27 | 1 |
| . 20 to . 45. | $\cdots$ | 1 | 31 | 168 | 56 | 88 | 8 |  |
| .45 to .80 |  |  | 1 | 46 | 20 | 23 | 1 |  |
| . 80 to 2.00 . |  |  | 1 | 12 | 19 | 13 | . |  |
| Over 2"00 |  |  |  | 1 | 6 | 6 |  |  |
| Mean pm | "22 | " 03 | "06 | "17 | ."18 | ".12 | ".07 | ".04 |
| Percentage of $\mu>": 20$ | 0 | . 2 | 5 | 25 | 18 | 10 | 4 | 0 |

[^355]|  | Mean area in <br> $10^{-6}$ of sun's <br> hemisphere | Mean <br> duration | Class | Mean area in <br> $10^{-6}$ of sun's <br> hemisphere | Mean <br> duration |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Class | 217 | 17 min | 3 | 1266 | 62 min |
| 1 | 570 | 29 | $4+$ | 2350 | 3 hr |

The following paragraphs are reprinted from F. Hoyle, "Some Recent Researches in Solar Physics," p. 36, Cambridge Lniversity Press, $1949 . \dagger$

Flares are a particular class of bright reversal characterized by sudden commencements. The properties of flares are:
(a) They are roughly classified in order of increasing importance as $1,2,3$, and $3+$. The area of the flare, seen in projection against the solar disk, is, at present, used as the criterion of importance. Flares of class $3+$ are rare, occurring on an average only once or twice per year. At the other extreme, flares of class 1 occur every few hours during periods of marked solar activity.
(b) The effective line width in $H$ a at peak intensity varies between 1.75 A and 16 A . being approximately proportional to the importance of the flare. $H \beta, H \gamma$ show lesser widths, but the data for these are somewhat meager.
(c) The contour of the bright emission is nearly symmetrical about the normal position of $H a$ and is independent of the position of the flare upon the disk (there is invariably a greater extension in the red wing than in the blue wing, which increases with the importance of the flare, reaching 0.7 A for those of the greatest intensity). Doppler displacements of the contour indicating large-scale turbulence of the emitting material in the line of sight have not been observed in excess of $\pm 10 \mathrm{~km} / \mathrm{sec}$.
(d) Flares are associated with sunspots, and in particular with complicated spot groups. The size of a sunspot, however, is not always a criterion of flare activity, some large spots being relatively inactive. The emitting material is mainly situated either in the reversing layer or the lower chromosphere, and the emission occurs in a region with fixed position relative to the position of the spot group. The areas of flares projected on the solar disk vary from a few hundred millionths up to the values exceeding 10,000 millionths of the area of the disk. The duration of a flare is usually of the order of an hour or less, but lifetimes $>5$ hours occasionally occur.
(e) Flares are strongly correlated with a number of terrestrial effects. Radio fadeouts, due to increased ionization in the $D$-layer, occur simultaneously with the visible appearance of intense flares. Great magnetic storms are associated with flares of classes 3 and $3+$. The magnetic disturbances commence about 26 hours after the appearance of the flare, and are most marked when the flare is near the center of the disk. Finally, there is a growing body of evidence that the sun emits cxceptionally high intensities in the radio meter wave-band during flares.

[^356]TABLE 845.-CONSTELLATION ABBREVIATIONS (Astron. Union, 1922)

| Andromeda ... And | Circinus ...... Cir | Lacerta ...... Lac | Pisces Austr . . PsA |
| :---: | :---: | :---: | :---: |
| Antlia .... .... Ant | Columba ...... Col | Leo ........... Leo | Puppis ........ Pup |
| Apus ......... Aps | Coma Beren . . Com | Leo Minor .... LMi | Pyxis ........ Pyx |
| Aquarius ..... Aqr | Corona Aust . . CrA | Lepus ......... Lep | Reticulum .... Ret |
| Aquila ........ Aql | Corona Bor ... CrB | Libra ......... Lib | Sagitta ....... Sge |
| Ara.......... Ara | Corvus ........ Cry | Lupus ........ Lup | Sagittarius .... $\mathrm{Sgr}_{\text {Sc }}$ |
| Aries .......... Ari | Crater ......... Crt | Lynx ......... Lyn | Scorpius ...... Sco |
| Auriga ....... Aur | Crux .......... Cru | Lyra ......... Lyr | Sculptor ...... Scl |
| Roötes ....... Boo | Cygnus ....... Cyg | Mensa ........ Men | Scutum ........ Sct |
| Caelum ....... Cae | Delphinus ..... Del | Microscopium . Mic | Serpens ...... Ser |
| Camelopardalis. Cam | Dorado ....... Dor | Monoceros .... Mon | Sextans ......S Sex |
| $r_{\text {ancer }}$....... Cnc | Draco ........ Dra | Musca ........ Mus | Taurus .......T Tau |
| Canes Venatici. CVn | Equaleus ..... Equ | Norma . ...... Nor | Telescopium . . Tel |
| Canis Major .. CMa | Eridanus ...... Eri | Octans ....... Oct | Triangulum ... Tri |
| " Minor .. CMi | Fornax ....... For | Ophiuchus .... Oph | " Austr ... TrA |
| Capricornus ... Cap | Gemini ....... Gem | Orion ........ Ori | Tucana |
| Carina ........ Car | Grus ......... Gru | Pavo ......... Pav | Ursa Major ... UMa |
| Cassiopeia .... Cas | Hercules . . . . Her | Pegasus .......Peg | " Minor ... UMi |
| Centaurus . . . . . Cen | Horologium .. Hor | Perseus ...... Per | Vela $\ldots . . . . . V{ }^{\text {Vel }}$ |
| Cepheus ...... Cep | Hydra ........ Hya | Phoenix ...... Phe | Virgo ........Vir |
| Cetus ......... Cet | Hydrus ....... Hyi | Pictor ........ Pic | Volans .......V Vol |
| Chamaeleon ... Cha | Indus ......... Ind | Pisces ........ Psc | Vulpecula .... Vul |

The following table was taken from Edlén's paper. ${ }^{283}$ It summarizes the results of the identification of 19 of the coronal lines caused by forbidden transitions. Fe X, XI, XIII, XIV, XV; Ni XII, XIII, XV, XVI ; Ca XII, XIII, XV; A X, XIV. Two of these identifications, namely $\lambda 4359$ attributed to A XIV and $\lambda 5694$ attributed to Ca XV, are somewhat questionable and therefore these two identifications are given with a (?) in the table. All these identified lines are caused by magnetic dipole radiation.

The first column gives the wavelengths of the coronal lines taken from Mitchell's compilation ${ }^{24}$ and reduced values from later work by Lyot. ${ }^{2 n 5}$. The second column gives the corresponding wave numbers. The third and fourth columns give the intensities as measured by Grotrian and Lyot respectively. The proposed identification is given in column five and the transition probabilities in column six. The seventh and eighth columns give the excitation potential and ionization potentials of the next preceding ionization stages.

| A | $\mathrm{cm}^{-1}$ | Intensity | Identification | ${ }_{\text {sec }}{ }_{\text {amm }}{ }^{\text {m }}$ | EP | $1 P^{\dagger}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3328 | 30039 | 1.0 | Ca XII $2 s^{2} 2 \mathrm{p}^{5}{ }^{2} \mathrm{P}_{1 / 2}-{ }^{2} \mathrm{P}_{11 / 2}$ | 488 | 3.72 | 589 |
| 3388.1 | 29507 | 16 | Fe XIII $3 \mathrm{~s}^{2} 3 \mathrm{p}^{21} \mathrm{D}_{2}-{ }^{3} \mathrm{P}_{2}$ | 87 | 5.96 | 325 |
| 3454.1 | 28943 | 2.3 |  |  |  |  |
| 3601.0 | 27762 | 2.1 | Ni XVI $3 \mathrm{~s}^{2} 3 \mathrm{p}{ }^{2} \dot{\mathrm{P}}_{11 / 2}-{ }^{2} \mathrm{P}_{1 / 2}$ | 193 | 3.44 | 455 |
| 3642.9 | 27443 |  | Ni XIII $3 \mathrm{~s}^{3} 3 \mathrm{p}^{4} \mathrm{D}_{2}-{ }^{3} \mathrm{P}_{1}$ | 18 | 5.82 | 350 |
| 3800.8 | 26303 |  |  |  |  |  |
| 3986.9 4086.3 | 25075 24465 | . 7 | Fe XI $3 \mathrm{~s}^{2} \mathrm{sp}^{4}{ }^{1} \mathrm{D}_{2}-{ }^{3} \mathrm{P}_{5}$ | ${ }_{319}^{9.5}$ | 4.68 | 261 |
| 4231.4 | 23626 | 2.6 | Ni XII $3 \mathrm{~s}^{2} 3 \mathrm{p}^{5} \mathrm{P}^{1 / 2}-{ }^{2} \mathrm{P}_{11 / 2}$ | 237 | 2.93 | 6 |
| 4311 | 23190 |  |  |  |  |  |
| 4359 | 22935 |  | ? A XIV 2s ${ }^{2} 2 \mathrm{p}{ }^{2} \mathrm{P}_{11 / 2}-{ }^{2} \mathrm{P}_{1 / 2}$ | 108 | 2.84 | 682 |
| 4567 | 21890 | 1.1 |  |  |  |  |
| 5116.03 | 19541.0 | $4.3 \quad 2.2$ | Ni XIII $3 \mathrm{~s}^{2} 3 \mathrm{p}^{4} \mathrm{P}_{1}-{ }^{3} \mathrm{P}_{2}$ | 157 | 2.42 | 350 |
| 5302.86 | 18852.5 | 100100 | Fe XIV 3s $\mathrm{s}^{2} 3 \mathrm{p}^{2}{ }^{2} \mathrm{P}_{11 / 2}-{ }^{2} \mathrm{P}_{1 / 2}$ | $\epsilon 0$ | 2.34 | 355 |
| 5536 | 18059 |  | A X ${ }^{\text {c }} \mathrm{s}^{2} 2 \mathrm{p}^{5} \mathrm{~S}^{2} \mathrm{P}_{1 / 2}-{ }^{2} \mathrm{P}_{1 / 2}$ | 106 | 2.24 | 421 |
| 5694.42 | 17556.2 | 1.2 | ? Ca XV $\mathrm{s}^{2} 2 \mathrm{p}^{2}{ }^{3} \mathrm{P}_{1}-{ }^{3} \mathrm{P}_{0}$ | 95 | 2.18 | 814 |
| 6374.51 | 15683.2 | 8.118 | Fe X ${ }^{\text {d }}{ }^{2} \mathrm{Sp}^{5}{ }^{2} \mathrm{P}_{1 / 2}-{ }^{2} \mathrm{P}_{1 / 2}$ | 69 | 1.94 | 233 |
| 6701.83 | 14917.2 | 5.42 .0 | Ni XV $3 \mathrm{~s}^{2} 3 \mathrm{p}^{2}{ }^{3} \mathrm{P}_{1}-{ }^{3} \mathrm{P}_{0}$ | 57 | 1.85 | 422 |
| 7059.62 | 14161.2 | 2.2 | $\mathrm{Fe} \mathrm{XV} \quad 3 \mathrm{~s}{ }^{3} \mathrm{p}{ }^{3} \mathrm{P}_{2}-{ }^{3} \mathrm{P}_{1}$ |  | 31.7 | 390 |
| 7891.94 | 12667.7 | 13 | Fe XI $3 \mathrm{~s}^{2} 3 \mathrm{p}^{4}{ }^{3} \mathrm{P}_{1}-{ }^{3} \mathrm{P}_{2}$ | 44 | 1.57 | 261 |
| 8024.21 | 12458.9 |  | $\mathrm{Ni} \mathrm{XV} \quad 3 \mathrm{~s}^{2} 3 \mathrm{p}^{2}{ }^{3} \mathrm{P}_{2}-{ }^{3} \mathrm{P}_{1}$ | 22 | 3.39 | 422 |
| 10746.80 | 9302.5 | 55 | Fe XIII $3 \mathrm{~s}^{2} 3 \mathrm{p}^{2}{ }^{3} \mathrm{P}_{1}-{ }^{3} \mathrm{P}_{0}$ | 14 | 1.15 | 325 |
| 10797.95 | 9258.5 | 35 | Fe XIII $3 \mathrm{~s}^{2} 3 \mathrm{p}^{2}{ }^{3} \mathrm{P}_{2} \rightarrow{ }^{3} \mathrm{P}_{1}$ | 9.7 | 2.30 | 325 |

* Prepared by Edith J. Tebo, Harvard College Observatory.
${ }_{28}{ }^{26}$ Zeitschr. Astrophys., vol, 22, p. 30, 1943.
${ }^{204}$ Handbook d' $\mathbf{A}$ strophys., vol. 4, p. 324, 1929; vol. 7, p. 401, 1936.
285 Monthly Notices, Roy. Astron. Soc., vol. 99, p. 580, 1939.
$\dagger$ The ionization polential refers to the next lower stage.

TABLE 847.-THE CEPHEID PERIOD-LUMINOSITY CURVE*

|  |  |  |  |  | 镸 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 0 | F 2.5 | -. 31 | -. 85 | 1.2 | G 6 | -2.39 | $-3.77$ |
| . 2 | $F 5.5$ | -. 68 | -1.26 | 1.4 | G 8 | $-2.80$ | -4.31 |
| . 4 | F 7.5 | -1.01 | $-1.74$ | 1.6 | K. 5 | $-3.25$ | -4.99 |
| . 6 | G 0 | -1.33 | -2.25 | 1.8 | K 2.5 | -3.73 | $-5.87$ |
| . 8 | G 2 | -1.66 | -2.74 | 2.0 | M 0 | -4.24 | -7.52 |
| 1.0 | $G 4$ | -2.02 | -3.26 |  |  |  |  |

[^357]| $\lambda$ | Classification | Excitation potential | Intensity |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | 7027 | 7662 |
| H I |  |  |  |  |
| 4340.5 | $2{ }^{2} \mathrm{~S}, \mathrm{P}-5^{2} \mathrm{~S}, \mathrm{P}, \mathrm{D}$ | 13.0 | 39 | 40 |
| 4861.3 | $2{ }^{2} \mathrm{~S}$, P $-4{ }^{2} \mathrm{~S}$ S, P, D | 12.7 | 100 | 100 |
| 6562.8 | $2{ }^{2} \mathrm{~S}, \mathrm{P}-3{ }^{2} \mathrm{~S}, \mathrm{P}, \mathrm{D}$ | 12.0 | 580 | 500 |
| He I |  |  |  |  |
| 3888.6 | $2 \mathrm{~s}{ }^{3} \mathrm{~S}-3 \mathrm{p}{ }^{8} \mathrm{P}$ | 22.9 | $<13$ | <25 |
| 4471.5 | $2 \mathrm{p}{ }^{3} \mathrm{P}-4 \mathrm{~d}^{3} \mathrm{D}$ | 23.6 | 6 | 5 |
| 5015.7 | $2 \mathrm{~s}{ }^{1} \mathrm{~S}-3 \mathrm{p}{ }^{1} \mathrm{P}$ | 23.0 | $5 \pm$ |  |
| 5875.6 | $2 \mathrm{p}{ }^{3} \mathrm{P}-3 \mathrm{~d}^{8} \mathrm{D}$ | 23.0 | 50 | 30 |
| 6678.1 | $2 \mathrm{p}{ }^{1} \mathrm{P}-3 \mathrm{~d}^{1} \mathrm{D}$ | 23.0 | 8 | 6 |
| He II |  |  |  |  |
| 4541.6 | $4{ }^{2} \mathrm{~S}, \mathrm{P}, \mathrm{D}, \mathrm{F}-9{ }^{2} \mathrm{~S}, \mathrm{P}, \mathrm{D}, \mathrm{F}, \mathrm{G}$ | 53.5 | 4 | 3 |
| 4685.8 | $3{ }^{2} \mathrm{~S}, \mathrm{P}, \mathrm{D}-4{ }^{2} \mathrm{~S}, \mathrm{P}, \mathrm{D}, \mathrm{F}$ | 50.8 | 39 | 60 |
| 5411.6 | $4{ }^{2} \mathrm{~S}, \mathrm{P}, \mathrm{D}, \mathrm{F}-7{ }^{2} \mathrm{~S}, \mathrm{P}, \mathrm{D}, \mathrm{F}, \mathrm{G}$ | 53.1 | 25 | 10 |
| C II |  |  |  |  |
| 4267.2 | $3 \mathrm{~d}^{2} \mathrm{D}-4 \mathrm{f}{ }^{2} \mathrm{~F}$ | 20.9 | 3 | 1 |
| N II |  |  |  |  |
| 5755.0 | $\left[2 \mathrm{p}^{2}{ }^{1} \mathrm{D}-2 \mathrm{p}^{21} \mathrm{~S}\right]$ | 4.0 | 30 |  |
| 6548.4 | $\left[2 \mathrm{p}^{2}{ }^{3} \mathrm{P}_{1}-2 \mathrm{p}^{2}{ }^{1} \mathrm{D}\right]$ | 1.9 | 150 | $5 \pm$ |
| 6583.9 | $\left[2 \mathrm{p}^{23} \mathrm{P}_{2}-2 \mathrm{p}^{21} \mathrm{D}\right]$ | 1.9 | 260 | $10 \pm$ |
| O I |  |  |  |  |
| O II |  |  |  |  |
| 3726.2 | $\left[2 p^{24} \mathrm{~S}-2 \mathrm{p}^{32} \mathrm{D}_{1 / 2}\right]$ | 3.3 | 20 | 8 |
| 3729.1 | $\left[2 \mathrm{p}^{3}{ }^{4} \mathrm{~S}-2 \mathrm{p}^{8}{ }^{2} \mathrm{D}^{21 / 3}\right]$ | 3.3 | 11 | 5 |
| 7319.0 | $\left[2 \mathrm{p}^{3}{ }^{2} \mathrm{D}_{2 / /}-2 \mathrm{p}^{3{ }^{3 / 2} \mathrm{P}}\right.$ ] | 5.0 | P |  |
| 7330.4 | $\left[2 p^{3}{ }^{2} \mathrm{D}_{11 /}-2 \mathrm{p}^{3} \mathrm{P}\right.$ ] | 5.0 | P |  |
| O III |  |  |  |  |
| 4363.2 | [ $2 \mathrm{p}^{21} \mathrm{D}-2 \mathrm{p}^{2} \mathrm{~S}$ ] |  |  |  |
| 4959.5 | $\left[2 \mathrm{p}^{2} \mathrm{P}^{3} \mathrm{P}_{1}-2 \mathrm{p}^{2} 1{ }^{1} \mathrm{D}\right]$ | 2.5 | 430 | 350 |
| 5007.6 | $\left[2 \mathrm{p}^{23} \mathrm{P}_{2}-2 \mathrm{p}^{21} \mathrm{D}\right]$ | 2.5 | 1200 | 1000 |
| Ne III |  |  |  |  |
| 3868.7 | [ $2 \mathrm{p}^{4}{ }^{3} \mathrm{P}_{2}-2 \mathrm{p}^{4} \mathrm{D}$ ] | 3.2 | 95 | 80 |
| 3967.5 | $\left[2 p^{4} P_{1}-2 p^{4} \mathrm{D}\right]$ | 3.2 | 24 | <80 |
| Ne IV |  |  |  |  |
| 4714.1 | $\left[2 p^{3}{ }^{2} \mathrm{D}_{21 / 2}-2 \mathrm{p}^{3}{ }^{2} \mathrm{P}\right]$ | 7.7 | <6 | <10 |
| 4719.7 | $\left[2 p^{3}{ }^{2} \mathrm{D}_{1 / 2}-2 \mathrm{p}^{3} \mathrm{P}\right.$ ] | 7.7 | ... |  |
| Ne V |  |  |  |  |
| 3345.8 34258 | $\left[2 \mathrm{p}^{2}{ }^{3} \mathrm{P}_{1}-2 \mathrm{p}^{2}{ }^{1} \mathrm{D}\right]$ | 3.8 | 43 | P |
| 3425.8 | [ $\left.2 \mathrm{p}^{2} \mathrm{P}_{2}-2 \mathrm{p}^{21} \mathrm{D}\right]$ | 3.8 | 109 | P |
| S II |  |  |  |  |
| 4068.5. | $\left[3 p^{34} \mathrm{~S}-3 \mathrm{p}^{3}{ }^{2} \mathrm{P}_{1} /{ }^{1 / 3}\right]$ | 3.0 |  |  |
| 4076.5 6717.3 |  | 3.0 1.8 | 5 6 6 | ${ }_{5} .5$ |
| 6731.5 | $\left[3 \mathrm{p}^{3} \mathrm{~S}\right.$ S $3 \mathrm{p}^{\left.3{ }^{3} \mathrm{D}^{2 / 1 / 2}\right]}$ | 1.8 | 12 ) | 5 |
| A 1 V |  |  |  |  |
| 4711.4 | $\left[3 p^{34} \mathrm{~S}-3 p^{3}{ }^{2} \mathrm{D}_{21 / 2}\right.$ ] | 2.6 | <6 | <10 |
| 4740.3 | $\left[3 \mathrm{p}^{3} \mathrm{~S}-3 \mathrm{p}^{3} \mathrm{D}_{11 / 2}\right]$ | 2.6 | 10 | 10 |
| $\begin{aligned} & \mathrm{Fe} \mathrm{XII} \\ & 3871.9 \end{aligned}$ | $\left[3 p^{48} \mathrm{P}_{1}-3 \mathrm{p}^{4} \mathrm{D}\right.$ ] | 4.7 | <<95 | <<80 |

The above table, containing most of the strongest and/or important lines under nebular conditions, is taken from a more complete list." ${ }^{\text {"19 }}$ The brackets [] about a classification indicate a forbidden transition. These wavelengths are in all cases except Ne III and Ne V the values calculated from series analyses of the ions concerned. The last two columns give the observed intensities in the objects NGC 7027 and 7662. P indicates the line is present but out of the range covered by the observations and intensity estimates; $<$ represents a blend with a line classified otherwise, transition indicated probably an appreciable contributor; 《 is also a blend with a line classified otherwise, transition indicated probably is not an appreciable contributor.

[^358]The solar neighborhood distance of 50 light-ycars, explored chiefly through the motions of nearby stars. A large majority are of less than solar luminosity, most below naked-eye visibility. Only 40 percent of the stars known to be nearer than 16 light-years are brighter than the sixth magnitude. Exploring the solar neighborhood therefore involves a search for telescopic dwarf stars. Any body $1 / 100$ of sun's mass within 1,000 astronomical units ( .015 light year) would be detected by its disturbance on Neptune and Uranus even if invisible (Russell). Nearest known star is 4 light-years distant (Proxima Centauri, $m=11, M=15.5$ ).

Region of brighter stars extending 500 light-ycars. The great majority of naked-eye stars lie in this region, though some of unusually high intrinsic luminosity are farther away. It includes probably 500,000 telescopic stars. Studied by proper motions, trigonometric and spectroscopic parallaxes, and photometry.

The Milky Way with a radius of about 50,000 light-ycars. The stars within 5,000 light-years of the sun are a trifling part of the galactic system outlined by the globular clusters and Milky Way clouds. The stars are so remote that proper motions and spectroscopic analyses hopelessly fail. Statistical counts are of some help in the nearer parts. But most of our knowledge comes from eclipsing binaries, long-period variables, and Cepheids. The period-luminosity relation for Cepheid variables is the key to practically all distances $>$ a few 1,000 light-years.

The Clouds of Magellan, nearly 100,000 light-ycars distant, nearest of all external galaxies and the most easily studied. Great advantage, all of its varied manifestations are seen at practically the same distance. These phenomena include gaseous nebulae, star clusters, giant and supergiant stars, some 1,500 known Cepheids in the Larger Cloud. In this cloud 750 stars brighter than -5.0 abs mag and over 200,000 brighter than the 0.0 have been estimated.

The Supergalaxies, $1,000,000$ to $500,000,000$ light-years distant. Composed of clusters of extragalactic nebulae. The relative diameters and brightnesses have been determined for some of the supergalaxies. The most conspicuous is the Coma-Virgo cloud $A$, a stream of several hundred bright spiral, spheroidal, and irregular galaxies, about $10^{7}$ light-years distant ; its greatest length about one-half this. One of the richest and most distinct supergalaxies is in Centaurus.

## TABLE 850.-STELLAR SPECTRA AND RELATED CHARACTERISTICS*

The one-dimensional classification system.-The spectra of almost all the stars can be arranged in a continuous sequence, the various types connected in a series of imperceptible gradations. With two unimportant exceptions, the sequence is linear. According to the now generally accepted Harvard (or Draper) system of classification, certain principal types of spectrums are designated by letters- $P, W, O, B, A, F, G, K, M, R, N$, and $S$-and the intermediate types of suffixed numbers. A spectrum halfway between $B$ and $A$ is denoted by $B 5$ while those differing slightly from class $A$ in the direction of Class $B$ are called $B 8$ or $B 9$. Classes $R$ and $N$ apparcntly form one side chain, and class $S$ another chain, both branching from the main series near class $K$.

The two-dimensional classification system.-In addition to the larger characteristics used to determine the spectral class (temperature differences) there are smaller luminosity effects that depend mainly on differences in densities in the atmospheres of the stars. Thus one can distinguish betwcen dwarfs, giants, and supergiants. At Harvard, in 1897, Miss Maury was actually the first to denote certain stars by prefixing the letter " $c$ " to the spectral class. These stars are now known to be supergiants. Mount Wilson observers still use this letter "c" to denote supergiants, "g" for giants, and "d" for dwarfs. This $d M 5$ denotes a dwarf star of spectral type M5 (see Table 874). Morgan, Keenan, and Kellman have extended the classification even further. ${ }^{\text {T0 }}$ ) Their luminosity classes include not only giants (III) and dwarfs (V) but subgiants (IV) and several classes of supergiants (I: Ia, and Ib) and intermediates (II).

Almost all the stars can be classified on the above system. In addition to individual peculiar stars there are, however, groups of stars that cannot be given specific classifications, such as the $A$-type spectrum variables ${ }^{271}$ and the "metallic-line" stars. ${ }^{272}$

The colors of the stars, the degree to which they are concentrated into the region of the sky, including the Milky Way (Table 854), and the average magnitudes of their peculiar velocities in space (Tables 828 and 876 ) all show important correlations with spectral type. In the case of colors, the correlation is so close as to indicate that both spectrum and color depend almost entirely on the surface temperature of the stars. The correlation in the other two cases, though statistically important, is by no mean so close.

[^359]Part 1.-The Harvard spectrum classification

| Class | Principal spectral lines <br> (absorption unless otherwise stated) | Example | Number than 6.25, | $\begin{gathered} \text { Percent } \\ \text { in } \\ \text { galactic } \\ \text { region } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| $P$ | Gaseous nebulae. Emission lines and bands of H, He I and II, and O II. |  | .... |  |
| W | Wolf-Rayet objects divided into two sequences: carbon, WC, have emission lines attributed to He I and II, C II, III, and IV, and O II, III, IV, have emission lines attributed to He I and II, and N III, IV, and V. | $\gamma$ Velorum | 5 | 100 |
| O | Lines of H, He I and II, O II and III, and N II and III. | $\xi$ Puppis | 20 | 100 |
| B | Neutral H and He, N II, and O II, and a few ionized lines of metals. | $\epsilon$ Orionis | 696 | 82 |
| A | H series at maximum, Ca II ( H and K ), and weak ionized metallic lines. | Sirius | 1885 | 66 |
| F | Ca II ( H and K ) strong, H lines fainter, metallic lines more abundant. | Canopus | 720 | 57 |
| G | H lines faint, Ca II ( H and K ) strong, many fine metallic lines. | The sun | 609 | 58 |
| $K$ | Ca II ( H and K ) very strong, many neutral metallic lines. Spectrum faint in the violet. | Arcturus | 1719 | 56 |
| M | Molecular bands of TiO , lines of Ca I and II, and other metals. Long-period variables have emission H lines. | Antares | 457 | 54 |
| $S$ | ZrO bands and metallic lines. Longperiod variables have emission H lines. | $r_{1}$ Gruis | 0 | $\ldots$ |
| $R$ | Bands of $\mathrm{C}_{2}, \mathrm{CN}$, and CH ; many metallic lines. | $\begin{gathered} \mathrm{BD} \mathrm{D} \\ -10^{\circ} 5057 \end{gathered}$ | 0 | 63 |
| $N$ | Bands of $\mathrm{C}_{2}, \mathrm{CN}$, and CH ; very little violet light. | 19 Piscium | 8 | 87 |
| $Q$ | Novae. Rapid spectral changes from early. supergiant type near maximum, through nebular stage, and finally to a Wolf-Rayet type. | $\ldots$ | $\ldots$ | $\ldots$ |

Part 2.-Prototypes for luminosity classification ${ }^{273}$

| Class | Supergiants | Giants | Main sequence | Class | Supergiants | Giants | Main sequence |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| B 0 | $\epsilon$ Ori | $\kappa$ Ori | $\zeta \mathrm{Oph}$ | G 5 | 9 Peg | $\gamma \mathrm{Hya}$ | $\kappa$ Cet |
| B 5 | 67 Oph | $\delta$ Per | $\kappa$ Hya | K2 | 56 Ori | $\kappa$ Oph | $\epsilon$ Eri |
| A 2 | a Cyg | $\lambda$ UMa | $\zeta$ Vir | M 1 | a Sco | 75 Cyg | $B D+42.2296$ |
| F0 | a Lep | $\zeta$ Leo | $\mu$ Cap | M 5 | a Her | 56 Leo | $B D+4.3561$ |
| F 8 | $\gamma$ Cyg | 1 Com | $\beta$ Vir |  |  |  |  |

For description of classification of Wolf-Rayet stars see reference, footnote 274. The "galactic region" here means the zone between galactic latitudes $\pm 30^{\circ}$, and including half the area of the heavens. 96 percent of the stars of known spectra belong to classes $A, F, G, K, 99.7$ percent including $B$ and $M$ (Innes, 1919). Henry Draper Catalog, 9 vols., 1918-24, and H. D. Extension, 2 vols., 1925-49, give positions, magnitudes, and spectra of nearly 360,000 stars. See also Yale Zone Catalogs, and the Bergedorf and Potsdam Spectral-Durchmusterungen.

[^360]TABLE 852．－PERCENTAGE OF STARS OF VARIOUS SPECTRAL CLASSES＊


The data are taken from the publications of the Harvard，McCormick，and Bergedorf Observ－ atories．The discontinuity in trend appearing between the visual and photographic groupings is in the sense to be expected．Ninety－nine percent of the stars brighter than magnitude 8.5 belong to the six classes listed；less than one percent have spectra of classes $P, W R, O, R, N, S$ ，and Peculiar，and such stars are even more uncommon among the fainter groupings．

Among stars brighter than sixth magnitude the percentages of dwarfs are as follows（Öpik et al．）：
F5
F． 8
G 0
G 5
15
K 0
5
$K 2$
3
K 5
$M$
0

A limited sampling in the Milky Way yields the following percentages of dwarfs among fainter stars（Nassau and McCrae）：

| Photographic <br> magnitude | $F 8$ to $G 2$ | $G 5$ | $G 8$ to K 3 |
| :---: | :---: | :---: | :---: |
| 8 to 10 | 75 | 23 | 7 |
| 10 to 11 | 77 | 31 | 8 |
| 11 to 12 | 82 | 42 | 10 |

In higher galactic latitudes the percentages of dwarfs are higher ；thus in latitudes $31^{\circ}$ to $90^{\circ}$ dwarfs constitute about 17 percent of the $K 0$ and $K 2$ stars of visual magnitude 10.4 （Janssen and Vyssotsky）．Among the $M 0$ and $M 8$ stars of all latitudes between visual magnitudes 8.5 and 10.53 percent are dwarfs（Dyer and Vyssotsky）．

[^361]TABLE 853．－THE LOCAL FAMILY OF GALAXIES ${ }^{275}$

| Member | Type | Modulus $\dagger$ |  | Distance （corrected for <br> Lat effect） | $M_{p g}$ | Diameter |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Ohs | Corr |  |  | $\overbrace{\text { pparent }}$ | Linear |
| Our galaxy | Sb |  |  |  |  |  | 24 kpc |
| M 31 ．．．． | Sb | 22.4 | 21.8 | 231 kpc | －17．9 | $3.2{ }^{\circ}$ | 12.9 |
| LMC | I | 17.1 | 16.7 | 22 kp | －15．9 | $12^{\circ}$ | 4.6 |
| M 33 | Sc | 22.3 | 21.9 | 239 | －14．9 | $62^{\prime}$ | 4.3 |
| SMC | I | 17.3 | 17.0 | 25 | －14．5 | $8^{\circ}$ | 3.6 |
| M 32 | E 2 | 22.4 | 21.8 | 231 | －12．9 |  |  |
| Fornax system | E | 21.0 ： | 20.8 ： | 142： | －11．9： | $50^{\prime}$ | 2.1 ： |
| NGC 205 | E 5p | 22.4 | 21.8 | 231 | －11．5 | 15.8 | 1.1 |
| NGC 6822 | I | 21.6 | 21.0 | 161 | －10．8 | $20^{\prime}$ | ． 94 |
| IC 1613 | I | 22.0 | 21.8 | 225 | －10．8 | $17^{\prime}$ | 1.1 |
| Sculptor system |  | 19.4 | 19.2 | 69 | －10．6 | $45^{\prime}$ | ． 90 |
| NGC 185 | E | $22.4 \pm$ | 21．5土 | 204士 | －10．6 | 14.5 | ． 86 |
| NGC $147 \ldots$ |  | $22.4 \pm$ | $21.5 \pm$ | 204土 | －10．3 | 14.1 | ． 83 |

[^362]
# TABLE 854.-GALACTIC CONCENTRATION OF STARS OF VARIOUS SPECTRAL CLASSES* 

Part 1.-Number of stars per 100 square degrees


The data are taken from the publications of the Harvard, McCormick, and Bergedorf Observatories. The spectral groupings are the same as in the preceding table. Absorption accounts for the apparent discrepancy in low latitudes between the numbers of early type stars in the last line of the visual magnitudes and those in the first line of the photographic magnitudes.

A measure of apparent galactic concentration may be found from the ratios of the star numbers in low latitudes to those in high latitudes. We obtain the figures given in Part 2:

Part 2.-Index of apparent galactic concentration

| Visual magnitude | $B$ | A | F | G | K | M |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $<6.0$ | 22 | 2.8 | 2.3 | 2.1 | 1.2 | 1.9 |
| 6.0 to 7.0 |  | 4.0 | 1.9 | 1.2 | 1.5 | 3.7 |
| 7.0 to 8.25 |  | 10 | 1.5 | 1.3 | 1.7 | 2.2 |
| 8.5 to 9.4 |  | 24 | 4.2 | 1.2 | 2.7 |  |
| 9.5 to 10.4 |  | 76 | 12 | 1.8 | 2.3 | 9 |
| Photographic magnitude |  |  |  |  |  |  |
| 9.5 to 10.5 | . | 56 | 4.8 | 1.8 | 2.4 | 2.1 |
| 10.5 to 11.5 |  | 97 | 16 | 2.5 | 2.9 | 3.5 |
| 11.5 to 12.5 | . | 99 | 35 | 2.9 | 3.5 | 5.5 |

The irregularities here are attributable in part to inadequate sampling.
Among the stars of the main sequence the true concentration increases with the stellar mass; the true concentration of the red giants is relatively low. The $W, O$, and $N$ stars show high apparent concentration to the Milky Way as do the Cepheids, and planetary nebulae; on the other hand, the long-period variables show little concentration and the cluster-type variables even less.

[^363]TABLE 855.-MEAN ANNUAL PARALLAX FOR STARS*
Part 1.-Stars of given visual magnitude and galactic latitude

| Mag | $0^{\circ}-20^{\circ}$ | $20^{\circ}-40^{\circ}$ | $40^{\circ}-90^{\circ}$ | Mag | $0^{\circ}-20^{\circ}$ | $20^{\circ}-40^{\circ}$ | $40^{\circ}-90^{\circ}$ |
| :---: | :---: | :---: | :---: | ---: | :---: | :---: | :---: |
| 3.0 | $\because 027$ | $\because 036$ | $\because .036$ | 9.0 | $\because 0043$ | $\because 0047$ | $\because 0073$ |
| 4.0 | .020 | .025 | .027 | 10.0 | .0032 | .0037 | .0057 |
| 5.0 | .015 | .017 | .020 | 11.0 | .0023 | .0030 | .0045 |
| 6.0 | .011 | .012 | .015 | 12.0 | .0018 | .0024 | .0034 |
| 7.0 | .0080 | .0086 | .0117 | 13.0 | .0014 | .0020 | .0027 |
| 8.0 | .0059 | .0062 | .0092 | 14.0 | .0011 | .0016 | .0021 |

These tabular values have been obtained by combining and smoothing the secular parallaxes derived at Groningen and McCormick together with mean parallaxes for fainter stars derived at Leiden. To obtain annual parallaxes from secular parallaxes a solar velocity of 19 kilometers per second has been assumed. Similarly the leiden figures rest on certain assumptions as to the peculiar motions of faint stars. Recent studies of the space motions of stars more than 500 parsecs from the plane of the galaxy indicate that the annual parallaxes listed here may well be systematically too large for stars fainter than tenth magnitude in the higher latitudes.

Some idea of the dependence of the mean parallaxes on the spectral type may he gained from Part 2. Here the probable error of a secular parallax is approximately 0.001 .

Part 2.-Mean parallaxes according to spectral class for stars of visual magnitude 10.0 (latitude $0^{\circ}$ to $90^{\circ}$ )

| Spectral class | Secular parallax | Solar velocity | $\begin{gathered} \text { Innual } \\ \text { parallax } \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| $B 8$ to $A 3$ | ".007 | $16 \mathrm{~km} / \mathrm{sec}$ | "0021 |
| $A 5$ to $F 2$ | . 011 | 17 | . 0031 |
| F 5 to $G 0$ | . 022 | 18 | . 0058 |
| K0 to K2 | . 014 | 20 | . 0033 |
| $g M 0$ to $g M 8$ | . 005 | 22 | . 0011 |

* Prepared by A. N. Vyssotsky, University of Virginia.

TABLE 856.-SPECTRUM CLASSES AND TEMPERATURES OF STARS*

| ${ }_{\substack{\text { Spectral } \\ \text { type }}}^{\text {cen }}$ | Observed |  | Temperature by several methods, ${ }^{\circ} \mathrm{K}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Heat | Water-cell | Heat | index |  |  |  |
|  | index | al) sorption Mag | $\lambda 0.555 \mu$ | $\lambda 0.529 \mu$ | Water-cell absorption | $\text { index }{ }^{276}$ | Ioniza tion |
| B 0 | . 05 | . 20 |  |  |  | $25000^{\circ}$ | 20000 |
| B 5 | . 01 | . 23 |  |  |  | 15500 | 15000 |
| $A 0$ | . 00 | . 26 |  |  |  | 10700 | 10000 |
| A 5 | . 02 | . 30 |  |  | $7500^{\circ}$ | 8530 | 8400 |
| F0 | . 15 | . 36 | $6750^{\circ}$ | $7300^{\circ}$ | 6200 | 7500 | 7500 |
| F 5 | . 30 | . 41 | 5760 | 6160 | 5450 | 6470 | 7000 |
| $d G 0$ | . 32 | . 42 | 5700 | 6100 | 5350 | 6000 |  |
| $d G 5$ | . 39 | . 47 | 5350 | 5750 | 4920 | 5360 |  |
| DK 0 | . 55 | . 54 | 4820 | 5100 | 4460 | 4910 |  |
| $d K 5$ | 1.10 | . 76 | 3720 | 3980 | 3550 | 4150 † |  |
| dM 0 | 1.40 | . 87 | 3400 | 3650 | 3260 | $3600 \ddagger$ |  |
| $d M 2$ | 2.1 | 1.14 | 2870 | 3060 | 2780 | 3200 |  |
| $g G 0$ | . 47 | . 50 | 5000 | 5450 | 4700 | 5200 | 5600 |
| gG 5 | . 65 | . 60 | 4550 | 4870 | 4140 | 4620 | 5000 |
| gK 0 | . 90 | . 70 | 4020 | 4300 | 3750 | 4230 | 4000 |
| gK 5 | 1.57 | . 93 | 3240 | 3480 | 3130 | 3580 | 3000 |
| g $M 0$ | 1.86 | 1.01 | 3030 | 3250 | 2980 | 3400 | 3000 |
| gM 2 | 2.2 | 1.14 | 2810 | 3000 | 2810 | 3200 |  |
| gM 4 | 3.1 | 1.30 | 2400 | 2590 | 2550 | 2930 |  |
| $g M 6$ | 4.2 | 1.46 | 2050 | 2200 | 2390 | 2750 |  |
| gM 8 | 5.2 | 1.62 | 1780 | 2000 | 2250 |  |  |
| Mc Max | 4.4 | 1.5 | 1990 | 2160 | 2350 |  |  |
| Mc Min | 8.9 | 2.2 |  |  | 1830 |  |  |

[^364]TABLE 857.—STARS KNOWN TO BE WITHIN 5 PARSECS OF THE SUN *

|  | $\begin{aligned} & \text { R A } 1950 \text { Dec } \\ & \text { h m } \end{aligned}$ | $m$ v | St | $\stackrel{ }{\prime \prime}$ | M | ${ }^{\mu}$ | $\theta$ | $V \mathrm{rad}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| a Cen A | $1436.2-60^{\circ} 38^{\prime}$ | . 3 | dG 3 | . 755 | 4.7 | 3.68 | $281{ }^{\circ}$ | - 22 |
| a Cen B | 14 36.2-60 38 | 1.7 | dK 2 | . 755 | 6.1 | 3.68 | 281 | - 22 |
| a Cen C | 14 26.3-62 29 | 11.5 | $d M$ : | . 778 | 16.0 | 3.85 | 282 |  |
| + 4:3561 | $1755.4+433$ | 9.4 | dM 5 | . 544 | 13.1 | 10.26 | 356 | -110 |
| W 359 | $1054.1+719$ | 13.8 | dM 6 | . 402 | 16.8 | 4.70 | 235 | +13 |
| L 726-8 A | $136.4-1813$ | 12.4 | dM 6 c | . 4 : | 15.4 | 3.38 | 80 | + 30 |
| L 726-8 B, | $136.4-1813$ | 12.9 | dM $6 e$ | . 4 : | 15.9 | 3.38 | 80 | + 30 |
| $+36: 2147 \mathrm{~A} \dagger$ | $1100.6+3618$ | 7.5 | dM 2 | . 390 | 10.5 | 4.78 | 187 | -87 |
| a CMa A. | $642.9-1639$ | $-1.6$ | A 0 | . 378 | 13 | 1.32 | 203 | - 8 |
| a CMa B | 6 42.9-16 39 | 8.5 | $F$ | . 378 | 11.4 | 1.32 | 203 | 8 |
| R 154 | 18 46.7-23 54 | 10.5 | dM 5 | . 354 | 13.2 | . 74 | 106 | 0 |
| R 248 | $2339.4+4355$ | 12.2 | dM 6 | . 318 | 14.7 | 1.82 | 176 | -81 |
| $\epsilon$ Eri | $330.6-938$ | 3.8 | dK2 | . 301 | 6.2 | . 97 | 271 | + 15 |
| 61 Cyg A | $2104.7+3830$ | 5.6 | dK 5 | . 298 | 8.0 | 5.21 | 52 | - 64 |
| 61 Cyg B | $2104.7+3830$ | 6.3 | dK 7 | . 298 | 8.7 | 5.21 | 52 | -64 |
| $\tau \mathrm{Cet}$ | 1 41.7-16 12 | 3.6 | $d G 7$ | . 298 | 6.0 | 1.92 | 296 | -16 |
| a CMi A | $736.7+521$ | . 5 | $d F 4$ | . 294 | 2.8 | 1.25 | 214 | - 4 |
| a CMi B | $736.7+521$ | 10.8 |  | . 294 | 13.1 | 1.25 | 214 |  |
| L 789-6 | $2235.7-1536$ | 12.3 | dM 6 | . 293 | 14.6 | 3.27 | 46 | - 60 |
| $\epsilon$ Ind | 21 59.6-5700 | 4.7 | $d K^{\prime} 5$ | . 288 | 7.0 | 4.69 | 123 | - 40 |
| R 128 | $1145.1+107$ | 11.0 | dM 5 | . 288 | 13.3 | 1.39 | 153 | $-12$ |
| + 59:1914 A | $1842.2+5933$ | 8.9 | dM 3 | . 285 | 11.2 | 2.28 | 324 | + 2 |
| $+59: 1915$ B | $1842.2+5933$ | 9.7 | dM 4 | . 285 | 12.0 | 2.28 | 324 |  |
| +43:44 A $\dagger$ | $015.4+4344$ | 8.1 | dM 3 | . 279 | 10.3 | 2.90 | 82 | + 8 |
| $+43: 44 \mathrm{~B}$ | $015.4+4344$ | 10.8 | $\operatorname{sd} M 14 \mathrm{c}$ | . 279 | 13.0 | 2.90 | 82 | + 8 |
| -36:9694 | 23 02.6-36 09 | 7.3 | dM 1 | . 277 | 9.5 | 6.91 | 79 | + 10 |
| -44:612 | 5:09.7-45:00 | 9.0 | sdM 0 | . 262 | 11.1 | 8.74 | 131 | +242 |
| + 5:1668 | $724.7+528$ | 10.1 | dM 5 | . 262 | 12.2 | 3.76 | 171 | + 27 |
| -39:8920 | 21 14.3-39 04 | 6.6 | dM 0 | . 257 | 8.8 | 3.46 | 251 | + 22 |
| +56:2783 A | $2226.6+5726$ | 9.8 | dM 4 | . 256 | 11.8 | . 86 | 246 | - 24 |
| +56:2783 B | $2226.6+5726$ | 11.2 | dM 6 | . 256 | 13.2 | . 86 | 246 | - 24 |
| R 614 AB $\dagger$ | $626.8-246$ | 11.6 | $d M 6 e$ | . 256 | 13.6 | 1.00 | 131 | + 25 : |
| -12:4523 | $1627.5-1232$ | 9.9 | dM 4 | . 253 | 11.9 | 1.18 | 182 | -18. |
| vMa 1 | $046.6+510$ | 12.3 | I) $F$ | . 245 | 14.2 | 2.98 | 155 | +238 |
| W 424 A | $1230.8+918$ | 12.7 | dM 7 | . 225 | 14.5 | 1.80 | 279 |  |
| W 424 B | $1230.8+918$ | 12.7 | dM 7 | . 225 | 14.5 | 1.80 | 279 |  |
| Co-46: 11540 | 17 24.9-46 51 | 9.7 | dM 3 | . 224 | 11.5 | 1.04 | 147 |  |
| -37:9435 | 0 02.5-37 36 | 8.5 | dM 3 | . 222 | 10.2 | 6.07 | 113 | + 24 |
| +68:946 | $1736.7+6823$ | 92 | dM 3 | . 218 | 10.8 | 1.31 | 197 | -17 |
| + $50: 1725$ | $1008.3+4942$ | 6.7 | $d K 8$ | . 218 | 8.4 | 1.45 | 249 | - 27 |
| -49:11439 | 21 30.3-49 14 | 9.0 | dM 2 | . 212 | 10.6 | . 81 | 185 |  |
| -15:6290 | 22 50.7-14 31 | 10.2 | dM 5 | . 211 | 11.8 | 1.11 | 123 | + 10 |
| CO-44: 11909 | 17 33.4-44 16 | 10.5 | dM15 | . 210 | 12.1 | 1.15 | 217 |  |
| a Aql | $1948.3+844$ | . 9 | A 4 | . 206 | 2.5 | . 66 | 55 | - 26 |
| L 145-141 | $1142.7-6434$ | 12.1 | I) $A$ | . 204 | 13.6 | 2.68 | 97 |  |
| +43:4305 | $2244.7+4405$ | 10.1 | dM 5 | . 203 | 11.6 | . 86 | 237 |  |
| $\mathrm{o}_{2} \mathrm{Erj}$ A | $413.0-744$ | 4.5 | dK 0 | . 200 | 6.0 | 4.08 | 213 | - 42 |
| $0_{2}$ Eri B | $413.0-744$ | 9.4 | DA | . 200 | 10.9 | 4.08 | 213 | - 42 |
| $c_{2}$ Eri C | 4 13.0-7 44 | 11.1 | dM 5c | . 200 | 12.6 | 4.08 | 213 | - 42 |
| Grw+79:3888 | $1145.4+7858$ | 11.0 | dM 4 | . 200 | 12.5 | 87 | 57 | -120 |

The stars have been designated by their $R I$ or $C P D$ numbers and only if neither of these was available, by their Cordoba Durchmusterung numbers: for very faint stars the discoverer's numbers have had to be used. $p=$ parallax, $\mu=$ proper motion, $m=$ magnitude, $M=$ absolute magnitude, $V_{\text {rad }}=$ radial velocity, $S_{p}=$ spectrum, $\theta=$ position angle.

[^365]
## TABLE 858.-MASSES OF STARS FOR BINARIES WITHIN 10 PARSECS FROM THE SUN*

This table contains all visual binary stars within 10 parsecs for which the orbital elements and parallax are well determined.
The sum of the masses follows from the harmonic relation:

$$
M_{1}+M_{2}=\frac{a^{3}}{P^{2}}
$$

where $a$ is the semimajor axis of the relative orbit, expressed in astronomical units, $P$ the period in years; the masses are referred to the sun's mass as unit. For the majority of these binaries the mass-ratio is known, thus permitting a determination of the masses of the individual component.

| Star | Parallax | A ${ }_{\text {U }}$ | $\underset{\text { years }}{P}$ | $\begin{gathered} \text { Sum of } \\ \text { masses } \\ M_{1}+M_{2} \end{gathered}$ | Separate masses |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | $M_{1}$ | $M_{2}$ |
| $\eta$ Cas | "184 | 67.9 | 526 | 1.13 | . 69 | . 44 |
| $p$ Eri | . 161 | 52 | 251 | 2.22 |  |  |
| $\mathrm{O}_{2}$ Eri B, C | . 202 | 34.1 | 248 | . 64 | . 44 | . 20 |
| Sirius | . 381 | 20.0 | 49.94 | 3.21 | 2.15 | 1.06 |
| Procyon | . 287 | 15.8 | 40.65 | 2.37 | 1.74 | . 63 |
| $\xi$ UMa | . 129 | 19.7 | 59.86 | 2.13 | . 98 | 1.15 |
| $a$ Cen A, B | . 756 | 23.2 | 80.09 | 1.92 | 1.06 | . 86 |
| $\xi$ Boo | . 142 | 34.4 | 149.95 | 1.81 | . 96 | . 85 |
| $\zeta$ Her | . 102 | 13.24 | 34.42 | 1.96 | 1.12 | . 84 |
| $-8^{\circ} 4352$ | . 148 | 1.28 | 1.72 | . 70 |  |  |
| Fu 46 | . 155 | 4.58 | 13.12 | . 56 | . 31 | . 25 |
| HR 6416 | . 132 | 37.4 | 242 | . 89 | . |  |
| HR 6426 | . 147 | 12.5 | 42.2 | 1.09 | . | . |
| $\mu$ Her B, C | . 109 | 11.8 | 43.0 | . 87 |  |  |
| $7^{\circ} \mathrm{Oph} . .$. | . 197 | 23.14 | 87.85 | 1.61 | . 89 | . 72 |
| 61 Cyg | . 294 | 83.5 | 720 | 1.12 | . 69 | . 43 |
| Krü 60 | . 256 | 9.23 | 44.52 | . 40 | . 26 | . 14 |

[^366]
## TABLE 859.-THE FIRST-MAGNITUDE STARS ARRANGED IN ORDER OF BRIGHTNESS *

| Name | $\underset{\mathrm{h}}{\mathrm{R}} \underset{\mathrm{~m}}{\mathrm{~A}} 1950$ | Dec | ${ }_{m}^{m_{v}}$ | $s p$ | $\mu$ | $\theta$ | $\underset{\mathrm{km} / \mathrm{s}}{V}$ | $p$ | $M_{\text {abs }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sirius ${ }^{\dagger}$ | 642.9 | $-16^{\circ} 39^{\prime}$ | $-1.6$ | $A 0$ | $1: 32$ | $203{ }^{\circ}$ | -8 | "378 | +1.3 |
| Canopus | 622.8 | -52 40 | -. 9 | $c F 0$ | . 02 | 47 | +20 | . 012 | -5.5 |
| a Centauri $\dagger \ddagger$ | 1436.2 | -60 38 | . 1 | $d G 3$ | 3.68 | 281 | -22 | . 755 | $+4.5$ |
| Vega ${ }^{\text {8 }}$ | 1835.2 | +38 44 | . 1 | A 0 | . 34 | 36 | -14 | . 122 | $+.5$ |
| Capella II | 513.0 | +4557 | . 2 | G 1 | . 44 | 168 | $+30$ | . 073 | $-.5$ |
| Arcturus | 14134 | +1927 | . 2 | K 0 | 2.28 | 209 | -5 | . 091 | . 0 |
| Rigel $\dagger 11$ | 512.1 | -815 | . 3 | cB8 | . 00 |  | +24 | . 002 : | -8. : |
| Procyon ${ }^{\dagger}$ | 736.7 | + 521 | . 5 | $d F 4$ | 1.25 | 214 | -4 | . 294 | +2.8 |
| Achernar | 135.9 | -5729 | . 6 | B 7 | . 10 | 110 | +19 | . 032 | -1.9 |
| $\beta$ Centauri $\dagger \\|$ | 1400.3 | -60 08 | . 9 | $B 3$ | . 04 | 217 | -12: | . 036 : | -1.3 : |
| Altair \% | 1948.3 | + 844 | . 9 | A 4 | . 66 | 55 | -26 | . 206 | +2.5 |
| Betelgeuse \|| $\delta$ | 552.4 | + 724 | . 9 : | M 2 | . 03 | 75 | +21 | . 013 | -3.5 |
| Aldebaran $\ddagger$ | 433.0 | +1625 | . 8 | K 5 | . 20 | 160 | +54 | . 058 | $-.4$ |
| a Crucis $\dagger \ddagger ⿻$ | 1223.8 | -62 49 | 1.1 | B1 | . 04 | 235 | -8: | . 03 : | -1.5 |
| Spica II | 1322.6 | -10 54 | 1.2 | B 2 | . 06 | 230 | + 2 : | . 011 : | -2.6: |
| Pollux 8 | 742.3 | +28 09 | 1.2 | $G 8$ | . 62 | 265 | + 3 | . 100 | +1.2 |
| Antares $\dagger$ | 1626.3 | -26 19 | 1.2 | M 1 | . 03 | 200 | - 3 | . 020 : | -2.3: |
| Fomalhaut | 2254.9 | -29 53 | 1.3 | A 3 | . 37 | 116 | $+6$ | . 145 | +2.1 |
| Deneb ${ }^{\text {8 }}$ | 2039.7 | +4506 | 1.3 | $c A 2$ | . 0 |  | - 5 : | . 002 : | -7.: |
| Regulus $\dagger \ddagger$ | 1005.7 | +1213 | 1.3 | B 8 | . 25 | 270 | + 3: | . 042 | -. 6 |
| $\beta$ Crucis \|| | 1244.8 | -59 25 | 1.5 | B1 | . 05 | 235 | +20 | . 006 : | -4.4: |

[^367]| Main sequence | Sp | $p$ | Mv | $T$ | $R$ | d | $\mu$ | $\rho$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\beta$ Centauri ...... . 9 | B 3 | "036 | -1.3 | $21,000^{\circ} \mathrm{K}$ | 11 | ".001 | (25) | . 018 |
| $\nu$ Scorpii ........ 4.3 | B 3 | . 009 | - . 8 | 21,000 | 3.2 | . 0003 | (5.2) | . 16 |
| $\beta$ Aurigae A .... 2.8 | A0 | . 034 | . 6 | 10,700 | 2.4 | . 0008 | 2.2 | . 13 |
| a Lyrae ......... . 1 | A 0 | . 122 | . 5 | 10,700 | 2.4 | . 003 | (3.0) | . 11 |
| a Can Maj A ...-1.6 | A 0 | . 378 | 1.3 | 10,700 | 1.8 | . 006 | 2.4 | . 42 |
| a Aquilae ....... . 9 | $A 4$ | . 206 | 2.5 | 8,800 | 1.4 | . 003 | (1.7) | . 6 |
| a Can Min ...... . 5 | $d F 4$ | . 294 | 2.8 | 6,100 | 1.9 | . 006 | 1.1 | . 16 |
| a Centauri A .... . 1 | $d G 3$ | . 755 | 4.5 | 5,850 | 1.0 | . 007 | 1.1 | 1.1 |
| 70 Ophiuchi A ... 4.3 | dK 0 | . 192 | 5.7 | 5,740 | 1.0 | . 002 | . 9 | . 9 |
| 61 Cygni A ..... 5.6 | $d K 5$ | . 298 | 8.0 | 4,300 | . 7 | . 003 | (.45) | 1.3 |
| Krüger 60 A .... 9.8 | $d M 4$ | . 256 | 11.8 | 3,180 | . 34 | . 0008 | . 26 | 9. |
| Barnard's Star ... 9.4 | $d M 5$ | . 544 | 13.1 | 3,020 | . 16 | . 0008 | (.18) | $45:$ |
| Giants |  |  |  |  |  |  |  |  |
| a Aurigae A .... . 2 | $g G 1$ | . 073 | - . 5 | 5,150 | 12 | . 007 | 4.2 | . 0024 |
| a Boötis ........ . 2 | $g K 0$ | . 091 | . 0 | 4,620 | 30 | . 023 | (8) | . 0003 |
| a Tauri ......... . 8 | $g K 5$ | . 058 | $-.4$ | 3,940 | 70 | . 034 | (5) | $1.4 \times 10^{-5}$ |
| $\beta$ Pegasi ........ 2.2 | $g M 3$ | . 016 | $-1.0$ | 3,390 | 160 | . 025 | (6) | $1.5 \times 10^{-6}$ |
| a Orionis ......... ${ }^{\text {a }} 9$ | cM 2 | . 017 | -4.0 | 3,060 | 480 | . 048 | (35) | $3 \times 10^{-7}$ |
| a Scorpii A ..... 1.2 | cM 2 | . 0095 | -3.5 | 3,060 | 380 | . 042 | (22) | $5 \times 10^{-7}$ |
| White dwarfs |  |  |  |  |  |  |  |  |
| a Can Maj B ... 8.5 | F | . 378 | 11.4 | 7,500 | . 034 | . 00012 | . 96 | $5 \times 10^{4}$ |
| 40 Eridani B .... 9.4 | A | . 200 | 10.9 | 11,000 | . 018 | . 00004 | . 44 | $7 \times 10^{4}$ |
| van Maanen's Star. 12.3 | F | . 245 | 14.2 | 7,500 | . 009 | : 00002 | (.14) | $10^{5}-10^{8}$ |

Many of the data were taken from the reference given in footnote 277. The spectra, magnitudes, radii, parallaxes, and densities have been revised for some of the stars. The letters $A$ and $B$ denote the brighter and fainter components, respectively, of binary stars.

Apparent (visual) magnitude is denoted by $m_{v}$, spectral class by $S p$, parallax in seconds of arc, $p$, absolute (visual) magnitude by $M_{v}$, radius in terms of the sun by $R$, apparent diameter in seconds of arc by $d$, mass in terms of the sun by $\mu$, and density by $\rho$ (in $\mathrm{g} / \mathrm{cm}^{3}$ ).

[^368]TABLE 861.-SPECTRUM TYPE AND MEAN VISUAL ABSOLUTE MAGNITUDE*

| Type | Main <br> sequence | Super- <br> giants | Type | Main <br> sequence | Giants | Super- <br> giants | Sub- <br> giants |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $O$ | -3.8 | ..- | $F 5$ | +3.7 | +1.2 | -4.2 | $\cdots$ |
| $B 0$ | -3.1 | -5.4 | $F 8$ | +4.1 | +.8 | -4.0 | $\cdots$ |
| $B 1$ | -2.6 | -5.4 | $G 0$ | +4.4 | +.6 | -3.8 | $\cdots$ |
| $B 2$ | -2.2 | -5.3 | $G 2$ | +4.7 | +.6 | -3.6 | $\cdots$ |
| $B 3$ | -1.7 | -5.3 | $G 5$ | +5.1 | +.5 | -3.2 | +3.0 |
| $B 5$ | -.8 | -5.2 | $G 8$ | +5.5 | +.5 | -2.8 | $\cdots$ |
| $B 8$ | +.2 | -5.0 | $K 0$ | +5.9 | +.5 | -2.6 | +3.0 |
| $B 9$ | +.4 | -5.0 | $K 2$ | +6.3 | +.5 | -2.3 | $\cdots$ |
| $A 0$ | .+ .7 | -4.9 | $K 5$ | +7.1 | +.2 | -2.0 | $\cdots$ |
| $A 2$ | +1.2 | -4.8 | $K 8$ | +7.7 | .0 | -.5 | $\cdots$ |
| $A 3$ | +1.5 | -4.8 | $M 0$ | +8.4 | -.2 | -4.5 | $\cdots$ |
| $A 5$ | +1.7 | -4.7 | $M 1$ | +9.0 | $\cdots$ | $\cdots$ | $\cdots$ |
| $A 8$ | +2.3 | -4.5 | $M 2$ | +9.6 | $\cdots$ | $\cdots$ | $\cdots$ |
| $F 0$ | +2.6 | -4.4 | $M 3$ | +10.4 | $\cdots$ | $\cdots$ | $\cdots$ |
| $F 2$ | +3.1 | -4.3 | $M 4$ | +11.5 | $\cdots$ | $\cdots$ | $\cdots$ |

For Type $R, \overline{\mathrm{M}}=-0.5$; and for Type $N, \overline{\mathrm{M}}=-2.0$.

[^369]
## TABLE 862.-REDUCTION OF VISUAL TO BOLOMETRIC MAGNITUDE*

The bolometric corrections (B C) given in the table are added algebraically to visual magnitudes. From tables by G. P. Kuiper, ${ }^{278}$ slightly revised for $O$ and $B$ stars by same author. The (effective) temperature, Te, scale of the $O$ and early $B$ stars is still to be regarded as provisional. The corrections for $O_{5}-F_{0}$ stars are based on the stellar temperature scale and on theoretical spectral-energy curves. For $F_{0}-M_{5}$ stars they are based on radiometric observations by Pettit and Nicholson.

| Type | $\mathrm{C}^{\text {Main seq }}$ |  | Type | ${ }^{\text {Main }}$ seq |  | $\begin{gathered} \text { Giants } \\ (M \stackrel{1}{=} 0) \end{gathered}$ |  | $\begin{aligned} & \text { Supergiants } \\ & (M=-4) \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | B C | Te |  | B C | $T$ 。 | B C | $T$ e | B C | $T$ 。 |
| O 5 | -5.3: | 100,000: | F. 0 | . 0 | 6500 | . 0 | 6500 | . 0 | 6500 |
| 06 | -4.8 | 70,000: | F 2 | -. 04 | 6100 | -. 04 | 6100 | -. 04 | 6100 |
| 07 | -4.3 | 50,000 | F 5 | -. 04 | 6100 | -. 08 | 5850 | -. 12 | 5720 |
| O 8 | -3.9 | 41,600 | F 8 | -. 05 | 6050 | -. 17 | 5500 | -. 28 | 5150 |
| $\bigcirc 9$ | -3.5 | 35,000 | G 0 | -. 06 | 6000 | -. 25 | 5240 | -. 42 | 4830 |
| $B 0$ | -3.0 | 28,500 | G 2 | -. 07 | 5900 | -. 31 | 5070 | -. 52 | 4650 |
| B 1 | -2.8 | 26,300 | $G 5$ | $-.10$ | 5770 | -. 39 | 4880 | -. 65 | 4480 |
| B 2 | -2.5 | 23,000 | G 8 | -. 10 | 5770 | -. 47 | 4720 | -. 80 | 4330 |
| B 3 | -2.3 | 21,000 | K0 | $-.11$ | 5740 | -. 54 | 4620 | -. 93 | 4240 |
| B 4 | -2.1 | 19,300 | K 2 | $-.15$ | 5580 | $-.72$ | 4420 | -1.20 | 4060 |
| B 5 | -1.9 | 17,800 | K 3 | $-.31$ | 5070 | -. 89 | 4260 | $-1.35$ | 3940 |
| B 6 | -1.6 | 15,600 | $K 4$ | $-.55$ | 4600 | -1.11 | 4120 | $-1.56$ | 3780 |
| B 7 | -1.4 | 14,300 | $K 5$ | $-.85$ | 4300 | -1.35 | 3940 | -1.86 | 3590 |
| B 8 | -1.2 | 13,100 | K 6 | -1.14 | 4100 |  |  |  |  |
| B 9 | -. 9 | 11,600 | M 0 | $-1.43$ | 3880 | $-1.55$ | 3800 | -2.2 | 3420 |
| A 0 | $-.7$ | 10,700 | M 1 | $-1.70$ | 3700 | -1.72 | 3680 | -2.6 | 3230 |
| A 1 | $-.6$ | 10,150 | M 2 | -2.03 | 3540 | -1.95 | 3560 | -3.0 : | 3060 |
| A 2 | -. 5 | 9,600 | M 3 | -2.4 : | 3320 | -2.26 | 3390 | -3.6 : | 2840 |
| A 3 | -. 4 | 9,000 | M 4 | -2.7: | 3180 | -2.72 | 3160 |  |  |
| A 5 | $-.3$ | 8,500 | M 5 | -3.1: | 3020 | -3.4: | 2920 : |  |  |
| A 7 | -. 2 | 7,900 |  |  |  |  |  |  |  |
| F0 | -. 0 | 6,500 |  |  |  |  |  |  |  |

* Prepared by G. P. Kuiper, Yerkes Observatory.
278 Astrophys. Journ., vol. 88, p. 446, 1938.


## TABLE 862A.-RUSSELL-HERTZSPRUNG DIAGRAM*

Absolute magnitudes (ordinates) of 3,915 stars of different spectrum types (abscissae) determined by the spectroscopic method by W. S. Adams and his associates (courtesy of Mount Wilson Observatory, 1932). The diagram shows distinctly the division of types $G$, and later, into giants (high-luminosity stars) and dwarfs (low-luminosity) with few intermediate stars. The curve simulates the mirror image of the figure 7 , and with the addition of much new material confirms fully that first drawn by Russell in 1913.

The majority of the stars may be divided into dwarfs, giants, and supergiants (a few stars do appear to have luminosities intermediate between these classifications). The luminosity of the dwarfs decreases regularly with advancing spectral type (reduced surface temperature) ; it drops abruptly for the coolest. Among the giants the luminosity decreases until about class $F 5$ and then increases with decreasing temperature at least as far as the early subdivisions of class $M$. For supergiants, the luminosity does not appear to change appreciably with spectral class.

In the diagram, the concentration into vertical columns is purely an effect of rough spectral classification. Most of the stars on this diagram belong to Population Type I (Table 874). The white dwarfs occupy the lower left corner (Table 872).

Kuiper ${ }^{279}$ has more recently derived the empirical mass luminosity relation for (1) the visual binaries. (2) some selected spectroscopic binaries, and (3) Trumpler's massive stars in clusters. His diagram is reproduced in figure 33. Morgan, Keenan, and Kellman ${ }^{250}$ have presented a preliminary calibration of their luminosity classes in terms of visual absolute magnitudes, which includes $B$ stars as well as subclasses (intermediates between giants and dwarfs and between giants and supergiants).

[^370]Fig. 32.-The Russell-Hertzsprung Diagram

TABLE 863.-LOG (NO. STARS)/(SQ. DEGREE) BRIGHTER THAN PHOTOGRAPHIC MAGNITUDE, m, AT STATED GALACTIC LATITUDES*

|  |  |  |  |  |  |  |  |  |  | Ratio Nos. successive magnitudes |  |  | $\begin{gathered} \text { Ratio } \\ \text { Nos. at } \\ 0^{\circ} \pm 90^{\circ} \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $m$ | $+90^{\circ}$ | $+40^{\circ}$ | $+20^{\circ}$ | $+10^{\circ}$ | $0^{\circ}$ | $-10^{\circ}$ | $-20^{\circ}$ | $-40^{\circ}$ | $90^{\circ}$ | $+90^{\circ}$ |  | -90 ${ }^{\circ}$ | +90 | $-90^{\circ}$ |
| 5.0 | 8.15 | 8.24 | 8.37 | 8.49 | 8.77 | 8.65 | 8.50 | 8.25 | 8.07 |  |  |  | 4.1 | 5.0 |
| 6.0 | 8.59 | 8.72 | 8.85 | 8.95 | 9.22 | 9.10 | 8.94 | 8.71 | 8.62 | 2.8 | 2.8 | 3.5 | 4.3 | 4.0 |
| 7.0 | 9.02 | 9.18 | 9.31 | 9.41 | 9.64 | 9.51 | 9.35 | 9.16 | 9.08 | 2.7 | 2.6 | 2.9 | 4.1 | 3.6 |
| 8.0 | 9.44 | 9.62 | 9.77 | 9.87 | . 09 | 9.93 | 9.79 | 9.60 | 9.50 | 2.6 | 2.8 | 2.6 | 4.5 | 3.9 |
| 9.0 | 9.86 | . 05 | . 21 | . 33 | 55 | . 37 | . 23 | . 04 | 9.92 | 2.6 | 2.9 | 2.6 | 4.9 | 4.3 |
| 10.0 | . 25 | . 47 | . 65 | . 77 | 1.02 | . 82 | . 67 | . 47 | . 32 | 2.5 | 3.0 | 2.5 | 5.9 | 5.0 |
| 11.0 | . 63 | . 87 | 1.08 | 1.21 | 1.49 | 1.26 | 1.11 | . 89 | . 72 | 2.4 | 3.0 | 2.5 | 7.2 | 5.9 |
| 12.0 | 1.01 | 1.26 | 1.50 | 1.64 | 1.95 | 1.70 | 1.54 | 1.29 | 1.12 | 2.4 | 2.9 | 2.5 | 8.7 | 6.8 |
| 13.0 | 1.38 | 1.63 | 1.90 | 2.05 | 2.39 | 2.14 | 1.95 | 1.68 | 1.48 | 2.3 | 2.8 | 2.3 | 10 | 8.1 |
| 14.0 | 1.70 | 1.97 | 2.28 | 2.45 | 2.82 | 2.57 | 2.34 | 2.03 | 1.78 | 2.1 | 2.7 | 2.0 | 13 | 11 |
| 15.0 | 1.98 | 2.30 | 2.66 | 2.85 | 3.22 | 2.99 | 2.72 | 2.34 | 2.02 | 1.9 | 2.5 | 1.7 | 17 | 16 |
| 16.0 | 2.26 | 2.61 | 3.02 | 3.25 | 3.60 | 3.39 | 3.07 | 2.64 | 2.26 | 1.9 | 2.4 | 1.7 | 22 | 22 |
| 17.0 | 2.53 | 2.90 | 3.36 | 3.64 | 3.96 | 3.76 | 3.40 | 2.92 | 2.48 | 1.9 | 2.3 | 1.7 | 27 | 30 |
| 18.0 | 2.79 | 3.15 | 3.67 | 3.97 | 4.32 | 4.10 | 3.68 | 3.18 | 2.70 | 1.8 | 2.3 |  | 34 | 42 |
| 19.0 |  |  |  |  |  |  |  |  |  | 1.6 | 2.0 |  |  |  |
| 20.0 |  |  |  |  |  |  |  |  | es. |  | 1.9 |  |  |  |
| 21.0 |  |  |  |  |  |  |  |  |  | 1.4 | 1.9 |  |  |  |

## (Characteristic 8. or 9. means, of course, -2 . or -1 .)

For values averaged over all galactic longitudes see reference, footnote 281. An excess of stars, relative to the averages, between longitudes $230^{\circ}$ and $50^{\circ}$, and a deficit elsewhere, reflect the eccentric position of the sun within the stellar system, which, in a first approximation, may be regarded as a greatly flattened spheroid. For more detailed values for both longitude and latitude see references, footnote 282 . The Groningen numbers are generally larger than the Mount Wilson values, notably so in low galactic latitudes. This defference arises partly from the irregular influence of the highly complex structure of the stellar system and especially of the obscuring dust clouds in and near the Milky Way. Mount Wilson results were derived from counts of stars in small areas at and north of declination $-15^{\circ}$; Groningen results from sample counts over the whole sky. The Groningen magnitude scale for faint stars south of declination $-15^{\circ}$ is, however, somewhat in doubt and may also affect the totals.

[^371]TABLE 864.-STARS OF LARGE PROPER MOTION*

| Star | $m$ | Sp |  | $\theta$ | Star |  | Sp |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| + 4:3561 | 9.4 | $d M 5$ | 10"26 | $356^{\circ}$ | W 489 | 14.8 | DC | 3"92 | $252^{\circ}$ |
| -44:612 | 9.0 | sdM 0 | 8.74 | 131 | Proxima Cen | 11.5 | dM | 3.85 | 282 |
| +38:2285 | 6.4 | $d G 6$ | 7.04 | 145 | + 5:1668 | 10.1 | $d M 5$ | 3.76 | 171 |
| -36:9694 | 7.3 | dM 1 | 6.91 | 79 | $\mu$ Cassiopeiae | 5.3 | $d G 5$ | 3.75 | 115 |
| -37:9435 | 8.5 | dM 3 | 6.07 | 113 | a Centauri | . 3 | $d G 3$ | 3.68 | 281 |
| R 619 | 12.6 | dM 6 | 5.40 | 167 | -15:4041/2 | 9.3 | sdG 6 | 3.68 | 235 |
| 61 Cygni | 5.6 | $d K 5$ | 5.21 | 52 | -39:8920 | 6.6 | dM 0 | 3.46 | 251 |
| +36:2147 | 7.5 | dM 2 | 4.78 | 187 | L 726-8 | 12.4 | $d M 6{ }^{\text {c }}$ | 3.38 | 80 |
| W 359 | 13.8 | dM 6 | 4.70 | 235 | L 789-6 | 12.3 | dM 6 | 3.27 | 46 |
| $\epsilon$ Indi | 4.7 | $d K 5$ | 4.69 | 123 | R 451 | 12.7 | sdK 8 | 3.20 | 174 |
| +44:2051 | 8.7 | $d M 1$ | 4.49 | 282 | -43:354 | 4.3 | $d G 5$ | 3.15 | 76 |
| $\mathrm{o}_{2}$ Eridani | 4.5 | $d K 0$ | 4.08 | 213 | R 578 | 14.1 | sdM 2 | 3.06 | 152 |

$m=$ magnitude, $S p=$ spectrum, $\mu=$ proper motion, $\theta=$ position angle.
Stars have been identified with their B.D. or C.P.D. numbers. In case of multiple stars the magnitudes and spectra of the brightest component are given. For further information on stars possessing large proper motions see references, footnote 283.

[^372]| Photographic magnitude | Number stars | Equivalent no. 1st mag stars (photogr) | Totals to mag m | Photographic magnitude | Number of stars | Equivalent no. 1st mag stars (photogr) | Totals to mas m |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -1.6 | Sirius | 11 | 11 | $8.0-9.0$ | 40,600 | 40 | 258 |
| -. 9 | a Carinae | 6 | 17 | $9.0-10.0$ | 116,000 | 46 | 304 |
| . 0 | a Centauri | 2 | 19 | 10.0-11.0 | 304,000 | 48 | 352 |
| .0-1.0 | 8 | 14 | 33 | $11.0-12.0$ | 789,000 | 50 | 402 |
| $1.0-2.0$ | 24 | 15 | 48 | $12.0-13.0$ | 2,000,000 | 50 | 452 |
| $2.0-3.0$ | 66 | 17 | 65 | $13.0-14.0$ | 4,950,000 | 50 | 502 |
| $3.0-4.0$ | 188 | 19 | 84 | $14.0-15.0$ | 11,500,000 | 46 | 548 |
| $4.0-5.0$ | 767 | 31 | 115 | $15.0-16.0$ | 25,400,000 | 40 | 588 |
| $5.0-6.0$ | 2,000 | 32 | 147 | $16.0-17.0$ | 56,000,000 | 35 | 623 |
| 6.0-7.0 | 5,360 | 34 | 181 | $17.0-18.0$ | 115,000,000 | 29 | 652 |
| $7.0-8.0$ | 14,800 | 37 | 218 | 18.0 - | . . . . . | 48 | 700 |

This table derived from van Rliijn's counts (Table 7 of reference 281) shows that to photographic magnitude 18.0 the total of starlight received is equivalent to 652 stars of photographic magnitude 1.0. If all the remaining stars are included, the equivalent addition is only 481 st -magnitude stars, giving a total of 700 , equal to about a hundredth part of full moonlight. The corresponding total of stars of visual magnitude 1.0 would be about 1,320 , which agrees reasonably well with the equivalent total of 1,440 stars (zenith) found by van Rhijn from direct measurement of the visual brightness of the sky; or 1,674 stars outside the earth's atmosphere. Density of stellar radiation $=0.8 \times 10^{-13} \mathrm{erg} / \mathrm{cm}^{3}$. Cosmic radiation density $=1.3 \times 10^{-13} \mathrm{erg} / \mathrm{cm}^{3}$ (near the earth).

The number of stars in each magnitude interval is still increasing rapidly at $m=18$, but the run in the numbers in the second column of the table indicates that somewhere about $m=30$ the numbers begin to decrease and eventuaily to approach zero as the limit of the stellar system is reached. The extrapolated total number of stars in the system given by different investigations ranges from 30 to 100 billion. The great inherent uncertainty of this total is further increased by the unknown influence of interstellar absorption.

Practically all the stars visible to the naked eye lie within 1,000 parsecs of the sun, and most of them are more than 100 parsecs distant. In the vicinity of the sun, the majority of the stars lie within 200 or 300 parsecs of the galactic plane; but along this plane the star-filled region extends far beyond 1,000 parsecs in all directions, and may reach 30,000 parsecs in the great southern star clouds (Shapley).

[^373]TABLE 866.—BRIGHT OR WELL.OBSERVED NOVAE*

| Nova and year | Apparent magnitures |  |  | Dura. tion 3 maks decline days | $\begin{aligned} & \text { Dis. } \\ & \text { tance } \\ & \text { parsecs } \end{aligned}$ | . Absolute magnitudes |  |  | Expansion velocities in $\mathrm{km} / \mathrm{sec}$ (absorption lines) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Max | Al in |  |  | Max | Min |  | $\begin{aligned} & \text { Prin- } \\ & \text { cinal } \end{aligned}$ | Diffuse enhanced | Orion |
| Aquilae | 1918 | -1.1 | 10.8 v | 8 | 430 | -9.3 | +2.6 | $1{ }^{\prime \prime} 0$ | $+1500^{\text {a }}$ | -2200 | -4000 |
| T Aurigae | 1891 | 3.8 | 14.8 | 100 | 800 | $-5.3$ | +5.7 | . 12 | - 400 | - 870 | -1200 |
| Carinae | 1843 | $-.8$ | 7.9 | 6000: | $170{ }^{\text {b }}$ | -7: $\ddagger$ | +1.7: |  |  |  |  |
| T Coronae B | 1946 ${ }^{\circ}$ | 3.0 | 11 :v | 9 | 850 | $-7.0$ | +1: |  | $-1100$ | -4360 |  |
| Cygni | 1920 | 2.0 | 15.5 | 16 | 1470 | -8.9 | $+4.6$ | . 09 | - 725 | -1400 | -2500 |
| Geminorum | 1912 | 3.5 | 14.7 | 37 | $790{ }^{\text {d }}$ | -6. 4 | $+4.8$ |  | - 800 | -1400 | -2100 |
| DQ Herculis | 1934 | 1.4 | 15 :v | 100 | 230 | -5.5 | $+7.5$ | . 27 | - 318 | - 800 | -1100 |
| CP Lacertae | 1936 | 2.1 | 15.3 | 9 | 1350 | -8.6 | $+4.6$ | . 25 | $-1500^{\dagger}$ | -3200 | -3800 |
| RS Ophiuchi | $1933{ }^{\text {c }}$ | 4.3 | 11.0 v | 9 | $1150{ }^{\text {² }}$ | -8.0 $\ddagger$ | $-1.3$ |  | Note |  |  |
| Persei | 1901 | . 2 | 13 : v | 13 | 470 | -8.4 | +4:v | . 4 | -1300 | -3500 | -3700 |
| RR Pictoris | 1925 | 1.2 | 12.7 | 150 | 500 | $-7.3$ | +4.2 | . 17 | - 320 | - 750 | -1500 |
| CP Puppis | 1942 | . 4 | 117 | 7 | 500 : ${ }^{\text {d }}$ | -8: | $1+8.5$ | . . | $-1000$ |  |  |
| RT Serpentis | $1909{ }^{\text {c }}$ | 10.5 | [16) | 8000: | $3300{ }^{\text {b }}$ | +3.6 ${ }^{\text {b }}$ |  |  | small |  |  |
| T Pyxidis | $1944^{\circ}$ | 6.4 | 13.6 | 130 | $1370{ }^{\text {" }}$ | $-5.4{ }^{\prime \prime}$ | $+1.6$ |  | - 940 | $-1800$ | -1900 |
| Tauri | $1054{ }^{\text {f }}$ | -5: | 15.9 |  | 1180 | $-16$ | $+4.3$ | . 20 | -1100 |  |  |

[^374]The mass-luminosity relation is shown in figure 33, which is based on data by G. P. Kuiper. ${ }^{284}$ Dots and open circles represent visual and spectroscopic binaries, each component being shown separately. Crosses represent several visual binaries in the cluster of the Hyades. Squares represent the white dwarfs. The symbol $\odot$ stands for the sun.

[^375]

Fig. 33.-The mass luminosity relation for stars.

TABLE 867.-CLASSIFICATION OF NEBULAE


Radiometric magnitude of any star = visual (or photographic) magnitude of a spectral class $A^{\circ}$ star giving the same radiometric deflection. If $m_{r}, m_{p r}$, and $m_{p g}$ are, respectively, radionetric, photovisual, and photographic magnitude, then Color Index, $C I=\left(m_{p g}-\right.$ $\left.m_{p v}\right)$; heat index, $H I_{p v}=m_{p v}-m_{r} ; H I_{p g}=m_{p g}-m_{r}$. Spectral class: Henry Draper, revised by 1). Hoffleit (DH) ; by W. W. Morgan (WWM). All measures reduced to zenith at Mount Wilson; two reflections from fresh silver; zinc-antimony black thermojunction; rock salt window. Stars of known or suspected variability are rejected from this list.
All the stars were in both the Mount Wilson and Harvard observing programs. ${ }^{285}$
The reduction of the Mount Wilson and Harvard data to a common basis has been rather difficult. The following are the principal factors that differ between the Mount Wilson and Harvard observations.
(1) The Atmosphere.-There was more water vapor over Oak Ridge than Mount Wilson ; hence, early-type stars would be too faint at Oak Ridge.
(2) The thermocouple blacking.-Probably the surfaces were equally "black" in the ultraviolet and visible regions; the Harvard surfaces were blacker in the infrared; hence, late-type stars would be too faint at Mount Wilson.
(3) The cell winduw.-Ruck salt was used at Mount Wilson; fluorite was used at Harvard. These are equally good throughout the ultraviolet, visible, and infrared to the region of 6 to 8 microns. For longer wavelengths, rock salt is better. The effect of this difference is in the opposite direction to the thermocouple blacking in (2) above. However, the very small percentage of stellar energy beyond 8 microns and absorption bands in the earth's atmosphere means that the difference in the cell windows has a very much smaller effect than the thermocouple blacking and, therefore, (2) above dominates.
A systematic difference exists between the Mount Wilson and Harvard observations which follows a pattern predicted in accordance with factors (1) and (2) above. Therefore, corrections which are usually less than 0.1 magnitudes have been applied. The largest, 0.16 magnitudes, is for 51 Gem . This correction brings the two sets of data into better agreement but there remains an apparent difference in zero-point of about 0.13 magnitudes. Since it is impossible to determine which of these two sets of observations is in error, the mean of the Mount Wilsen and Harvard data has been taken, corrected as indicated for factors (1) and (2) above. These mean values are the data given in the $m_{r}$ column.

| Star | Magnitude |  |  | Speciral class |  | Star | Magnitude |  |  | Spectral class |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $m_{p v}$ | $m_{p g}$ | $m_{r}$ | DH | . WWM |  | $m_{p v}$ | $m_{p o}$ | $m_{r}$ | DH | WWM |
| a And | 2.11 | 2.08 | 2.12 | $\mathrm{B}_{\text {в }}$ |  | 51 Gem | 4.85 |  | 2.17 | $\mathrm{M}_{8}$ |  |
| $\beta$ Cas | 2.34 | 2.82 | 2.11 | $\mathrm{F}_{3}$ | $\mathrm{F}_{2}$ III | a CMi | . 40 | . 83 | . 10 | $\mathrm{F}_{5}$ | $\mathrm{F}_{4} \mathrm{~V}$ |
| $\gamma \mathrm{Peg}$ | 3.00 | 2.67 | 2.83 | $\mathrm{B}_{2}$ |  | $\beta$ Gem | 1.13 | 2.31 | . 37 | $\mathrm{K}_{0}$ | $\mathrm{K}_{0}$ III |
| $\beta$ And | 2.07 | 3.94 | . 28 | $\mathrm{K}_{8}$ | $\mathrm{K}_{5}$ III | $\epsilon$ Leo | 2.96 |  | 2.44 | $\mathrm{G}_{0}$ | $\mathrm{G}_{1}$ II |
| $\boldsymbol{\alpha}$ Cet | 2.54 | 4.47 | . 53 | M | $\mathrm{M}_{n}$ III | $\pi$ Leo | 4.52 |  | 2.77 | $\mathrm{M}_{2}$ |  |
| a Per | 1.78 | 2.43 | 1.47 | $\mathrm{F}_{3}$ | Fs I | $\beta$ UMa | 2.34 | 2.40 | 2.50 | $\mathrm{A}_{1}$ |  |
| $\eta$ Tau | 2.90 | 2.92 | 2.86 | $\mathrm{B}_{5}$ : |  | a UMa | 1.70 | 3.09 | 1.02 | $\mathrm{G}_{7}$ | K ${ }_{0}$ III |
| a Tau | . 77 | 2.70 | $-.80$ | $\mathrm{K}_{5}$ | $\mathrm{K}_{5}$ III | a Cyg | 1.24 | 1.40 | 1.17 | $\mathrm{A}_{2 \mathrm{p}}$ |  |
| a Aur | . 14 | 1.03 | $-.53$ | $\mathrm{G}_{2}$ | $\mathrm{G}_{2}$ I | $\beta$ Peg | 2.25 | 4.39 | . 11 | $\mathrm{M}_{3}$ |  |
| $\beta$ Tau | 1.68 | 1.52 | 1.66 | $\mathrm{B}_{8}$ |  | a Peg | 2.56 | 2.53 | 2.59 | $\mathrm{A}_{1}$ |  |

[^376]
## TABLE 869.-NONGALACTIC NEBULAE

Some 400 considered. Distribution of magnitudes appears uniform throughout sequence. For each stage in the sequence the total magnitude ( $M_{r}$ ) is related to the max diameter ( $d$ ) by the formula: $M_{T}=\mathrm{C}-5 \log d$. When minor diameter is used, $C$ approx constant throughout sequence $(C=10.1)$. Mean absolute visual magnitude -15.2 . The statistical expression for distance in parsecs is $\log D=4.04+0.2 M_{\text {r }}$. Masses appear to be of the order of $2.6 \times 10^{8} \times$ our sun's. Apparently nebulae as far as measured are distributed uniformly in space, one to $10^{18}$ parsecs ${ }^{3}$ or $1.5 \times 10^{-31}$ in cgs units.

Corresponding radius of curvature of the finite universe of general relativity is of order of $2.7 \times 10^{10}$ parsecs, about 600 times the distance at which normal nebulae can be detected with the Mount Wilson 100 -inch reflector.

The task of cataloging and naming variable stars was delegated in 1946 by the International Astronomical Union to the Sternberg Astronomical Institute in Moscow. The 1948 General Catalogue lists 10,912 variable stars; a supplement lists 265 additional variables discovered in 1948. Several thousands of variable stars in globular clusters, in the Magellanic Clouds, and in the nearest galaxies are not included in this catalog, nor are thousands of stars whose variability has been announced, but which are not officially recognized pending confirmation. The total number of variable-star discoveries announced until 1950 probably amount to 20,000 .
Classification.-Variable stars, with the exception of eclipsing binaries (see Table 879), can be divided roughly into three major groups: (1) Pulsating stars. The variables of this group are all giants, located above the main sequence in the Russell diagram. (2) Explosive stars. The variables of this group are, as far as is known, dwarfish; located below the main sequence in the Russell diagram. (3) Erratic variables, whose light, fluctuations, mostly of an erratic nature, are produced by external causes (nebulosity) or by peculiar phenomena in their atmospheres.

Pulsating stars.-Cepheids. Usually divided into cluster-type variables, with periods shorter than one day, and classical Cepheids, with periods longer than one day, although at least five subgroups are indicated.

Cluster-type variables belong to Population II, have spectra ranging from $A$ to $F$, absolute magnitudes close to zero: most variables found in globular clusters belong to this group. Periods range from $0^{d} .061$ (CY Aquarii) to $1^{4} .35$ (a star in the $\omega$ Centauri cluster), with the greatest concentration around $0^{d} .53$. Typical variable: RR Lyrae ( $7^{\mathrm{m}} .1$ $-8^{\mathrm{m}} .0$; period $0^{d} .57$; spectrum $.42-F 0$ ). About 1,700 galactic objects and 600 stars in globular clusters are known to belong to this group.

Classical Cepheids belong to Population I, have spectra ranging from $F$ to $K$, with marked dependence on period, and intrinsic luminosities increasing with the period (periodluminosity law) from $-0^{\mathrm{M}} .5$ to $-3^{\mathrm{M}}$ (absolute visual magnitudes). Periods range from $1^{d} .13$ (BQ Coronae Austrinae) to $45^{\mathrm{d}} .2$ (SV Vulpeculae), with the greatest concentration around $2^{\mathrm{a}} .7$. Typical variable: $\delta$ Cephei ( $3^{\mathrm{m}} .8-4^{\mathrm{m}} .6$, period $5^{\mathrm{d}} .37$, spectrum $F 5-G 2$ ). About 500 galactic stars and 2,500 stars in the Magellanic Clouds and other extragalactic systems are known to belong to this group.

For both cluster-type and classical Cepheids the shape of the light curve is a function of the period; the rise to maximum is always faster than the decline. Average visual amplitude $0^{\mathrm{m}} .75$; photographic amplitudes 50 percent larger. Radial-velocity curves are in phase with light curves (maximum approach at maximum light); Average amplitude $30-40 \mathrm{~km} / \mathrm{sec}$.

Long-period variables. Typical variable: o (Mira) Ceti ( $2^{\mathrm{m}} .0-10^{\mathrm{m}} .1$ : period $331^{\mathrm{d}}$; spectrum $M G c$ ). Characterized by very large amplitudes (from 4 to 10 magnitudes, visual), late spectra ( $M, S, R, N$ ) with bright hydrogen emission lines near maximum light, unstable light curves and periods ranging from $120^{1}$ (W Puppis) to $1379^{\circ}$ (BX Monocerotis). Greatest concentration of periods around $275^{\circ}$. Long-period variables seem to fall into two major groups, whose periods overlap to a great extent. Stars of the first group have nearly symmetrical light curves with moderate amplitudes and periods ranging from $120^{d}$ to $450^{\text {d }}$; they seem to belong to Population II. Stars of the second group have strongly asymmetrical light curve (rise faster than decline), large amplitudes and periods upward of $200^{\text {d }}$; they seem to belong to Population I.

The enormous visual (and photographic) amplitudes are accounted for by a shift in the effective wavelength of the radiation with phase and by the formation of strong absorption bands at minimum light in the visual region of the spectrum. The total (bolometric) radiation has an amplitude of only one magnitude. Absolute bolometric magnitudes near -4. About 2,600 stars are known to belong to this group.

Semiregular red variables. Typical variables: Af Cygni ( $6^{\mathrm{m}} .3-8^{\mathrm{m}} .0$; period $89^{\text {d }}$; spectrum $M 6$ ). Spectra similar th those of long-period variables, except for much weaker, or entirely absent, hydrogen emission lines. Amplitude mostly comprised between 1 and 3 magnitudes (both visual and photographic). Light curves very irregular, often erratic; periods ranging from $42^{4}$ (TX Tauri) to $810^{\circ}$ (S Persei), but mostly comprised between $100^{4}$ and $200^{4}$; several unrelated periods often occur in the same star and for many variables periods have only a statistical significance. Then mean brightness often changes slowly, with cycles of $1,000-2,000$ days. Absolute visual magnitudes high, between 0 and -4. Their galactic distribution suggests Population II. Total number of recognized variables 600 .
$R V$ Tauri stars. Typical variable: RV Tauri ( $8^{\mathrm{m}} .7-11^{\mathrm{m}} .8$; period $39^{\mathrm{d}} .3$; spectrum $K$ IV). Spectra Cepheid-like, but light curves similar to those of the preceding group. Deep and shallow minima often alternate. Periods (intervals between two successive

[^377]TABLE 870.—VARIABLE STARS, GENERAL CHARACTERISTICS (concluded)
minima, irrespective of principal and secondary) range from $16^{d .5}$ (SX Centauri) to $73^{\text {d }}$ ( R Scuti). Galactic distribution suggests Population I. Only 60 stars can be safely assigned to this group.
Explosive stars.-U Geminorum stars. Typical variable: U Geminorum ( $8^{\mathrm{m}} .8$ $14^{\mathrm{m}} .0$; average cycle $97^{\mathrm{d}}$ ). Characterized by long permanence at minimum light, interrupted by brief, sudden explosions which bring the star almost always to the same maximum magnitude; the time between explosions might vary as from 1 to 4 for an individual star, but the average length of cycles over long periods of time are constant for each star. Average cycle length ranges from $13^{4}$ (AB Draconis) to $340^{4}$ (AW Geminorum). A few stars undergo temporary spells of continuous, irregular fluctuations. The amplitude increases from 3 magnitudes for short-cycle stars to 5 magnitudes for long-cycle stars. Spectra are of early type and peculiar; hydrogen lines in emission at minimum in absorption at maximum galactic concentration low for short-cycle variables, greater for long-cycle ones. Group numbers about 70 stars.
$Z$ Camclopardalis stars. Typical variable: Z Camelopardalis ( $10^{\mathrm{m}} .5-13^{\mathrm{m}} .3$; average cycle $22^{d} .1$ ). Similar to the preceding, but with shorter minima and smaller amplitudes; erratic variation is the rule rather than the exception: Less than a dozen stars are known of this type.
Novae, repeating novae, and novaelike stars. Novae are stars that suddenly blaze up with startling rapidity and then gradually fade out again. For data on bright or wellobserved novae see Table 866. A repeating (or recurrent) nova, such as T Pyx, has several outbursts, any one of which would have identified it as a nova. A novalike star, e.g., $Z$ Andromeda, from time to time shows novalike characteristics with the formation of a shell spectrum and displaced absorption lines and later emission lines. Nebular lines are often associated with these objects.
Erratic variables.- $R$ Coronae Borcalis stars. Supergiants with $G$ and $R$ spectra and an abnormal abundance of carbon in their atmospheres. For long periods of time (often years) the light remains constant at maximum. At entirely irregular intervals the light is dimmed, probably by a carbon veil, with resulting fluctuations which may reach 9 or 10 magnitudes. Typical stars: R Coronae Borealis (variable from $5^{\mathrm{m}} .8$ to $15^{\mathrm{m}} .0$ ), RY Sagittarii (variable from $5^{\mathrm{m}} .9$ to $15^{\prime \prime \prime} .0$ and probably fainter). Only 23 stars are known to belong to this type.
l'ariables associated zevith nebulosities. Stars in gaseous nebulae of the diffuse or of the cometary type, or even in dark nebulac, often show erratic variations with various amplitudes and speeds. At least three subtypes are indicated, typified by the following stars: T Orionis ( $9^{\mathrm{m}} .6-11^{\mathrm{m}} .9$; rapid; often constant at maximum) ; R Monocerotis ( $10^{\mathrm{mm}}-14^{\mathrm{m}}$; slow) ; RW Aurigae ( $9^{\text {m }} .0-13^{\text {m }} .5$; very rapid, no constant light at any time). About 200 stars can be attributed to one or the other of these groups.
$P C y g n i$ and $B e$ Stars. These early-type giants are normally quiescent, but occasionally some of them undergo slow fluctuations of moderate amplitude $\left(1^{m}-4^{m}\right)$ which last over a series of years. Typical: P Cygni ( $3^{\prime \prime \prime}-6^{m}$ ), active in the 17 th century $; \gamma$ Cassiopeiae $\left(1^{\mathrm{m}} .6-3^{\mathrm{m}} .0\right)$, active after 1936.

## TABLE 871.-VISUAL BINARY STARS*

A. Visual binary stars are cataloyed as follows:

1. "New General Catalog of Double Stars within $120^{\circ}$ of the North Pole" (abbreviated: $A D S=$ Aitken Double Stars), by R. G. Aitken, Carnegie Inst. Washington Publ. 417, 1932 ( 2 vols.) ; contains 17,180 objects.
2. $A D S$ is the successor to $B D S=$ "A General Catalog of Double Stars within $121^{\circ}$ of the North Pole," by S. W. Burnham, Carnegie Inst. Washington Publ. 5, 1906 ( 2 vols.) ; this catalog contains 13,665 pairs. About one-third of these (mostly wide objects) are not repeated in $A D S$.
3. SDS or "Southern Double Star Catalog," from $-19^{\circ}$ to $-90^{\circ}$ declination, by R. T. A. Innes, B. H. Dawson, and W. H. van den Bos, Union Observatory, Johannesburg, South Africa, 1927 (4 vols.).
4. Many zeide double stars of interest are contained in "Measures of Proper Motion Stars," by S. W. Burnham, Carnegie Inst. Washington Publ. 168, 1913.
B. A full discussion of mass determinations of visual binary stars is found in "The Masses of the Stars with a General Catalog of Dynamical Parallaxes," by H. N. Russell and C. E. Moore, Univ. Chicago Press, 1940.
C.. Orbits of visual binaries are listed in W. H. Finsen, "Second Catalog of Orbits of Visual Binary Stars," Union Obs. Circ. 100, 1938. Supplementary orbits are found in later Union Observatory Circulars and in the Astronomical Journal.
[^378]| Star | $m_{0}$ | CI | Sp | $\mu$ | $p$ | $M_{v}$ | $\odot^{r} \stackrel{r}{=}$ | $\begin{gathered} \rho \\ \text { cgs } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V Ma 1 | 12.3 | m + +69 | DF | 2"98 | "245 | 14.2 | . 009 : | $10^{5}-10^{6}$ |
| $o_{2}$ Eridani B | 9.4 | . 0 : | DA | 4.08 | . 200 | 10.9 | . 018 | $7 \times 10^{\text {c }}$ |
| Sirius B | 8.5 |  | DF | 1.32 | . 378 | 11.4 | . 034 | $5 \times 10^{\text {s }}$ |
| He 3 | 12.0 | -. 80 | $D B$ | . 90 | . 066 | 11.1 | . 002 : | $10^{8}-10^{7}$ |
| LDS 275 A | 14.7 | +. 15 | $D C$ | . 35 | ... | ... | . 012 : | $10^{5}-10^{6}$ |
| LDS 275 B | 15.0 | +. 15 | DC | . 35 |  |  | . 012 : | $10^{5}-10^{8}$ |
| L 39-44 ... | 17.2 | +.2: |  | . 57 |  |  | . 005 : | $10^{\text {b }}$ |
| W 489 | 14.8 | +. 77 | DC | 3.92 | . 129 | 15.4 | . 012 : | $10^{5}-10^{6}$ |
| LDS 678 A | 12.0 | -. 14 | DA | . 20 |  |  | . 014 | $10^{5}$ |

$p=$ parallax, $\mu=$ proper motion, $S p=$ spectrum, $m=$ magnitude, $M=$ absolute magnitude.
A representative selection of white dwarfs is given above, including the two stars for which the masses are known ( $o_{2}$ Eri B and Sirius B), the bluest white dwarf ( He 3 ), the reddest degenerate star ( W 489), the only known double white dwarf (LDS 275), the faintest known white dwarf ( $\mathrm{L} 39-44$ ) and a typical example of a white component of red-white dwari double (LDS 678 which has a red component of 13.7 vis with a color index of +1.81 ).

The values given for the radii and the densities ( $\rho$ ) are in most cases very uncertain estimates based on very approximate parallaxes and estimated masses.

* Prepared by W. Luyten, University of Minnesota.

TABLE 873.-LOW-DENSITY STARS, GIANTS *

| Star | Type | Visual <br> abs mag | Density <br> sun $=1$ | $\begin{gathered} \text { Radius } \\ \text { sun }=1 \end{gathered}$ | $\begin{gathered} \text { Mass } \\ \text { sun }=1 \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| a Orionis | cM 2 | -4.0 | $3 \times 10^{-7}$ | 480 | (35) |
| a Scorpii A | $c M 2$ | -3.5 | $5 \times 10^{-7}$ | 380 | (22) |
| $\beta$ Pegasi | ${ }_{\text {g }} M 3$ | -1.0 | $1.5 \times 10^{-6}$ | 160 | (6) |
| a Tauri | g $K 5$ | $-.4$ | $1.4 \times 10^{-5}$ | 70 | (5) |

* Prepared by W. S. Adams, Mount Wilson Observatory.


## TABLE 874.-GIANT AND DWARF STARS*

The table gives a list of typical supergiants, giants, and main-sequence stars. The relations between the absolute magnitudes and spectral types of the stars are conspicuous and complicated. Along the main sequence $M$ (visual) falls very rapidly from about -4 for class $O$ to +14 for $M 6$. For identical spectra, the scatter about the mean is of the order of $\pm 1^{m}$. The normal giants form a sequence with $M$ ranging from about 0 for class $G 2$ to -1.5 for $M 8$ with a somewhat greater scatter. Supergiants, with $M$ from -4 to -7 , are found sparingly in all spectral classes. The white dwarfs, of which nearly 100 are now known, form a widely separated group with spectra from $A$ (or perhaps $B$ ) to $G$ and with $M$ from +10 to +15 . Subgiants, one or two magnitudes fainter than the normal giants, are recognizable and the existence of other sequences is indicated by recent precise work.
The above discussion applies to stars of Population Type I, which is found in many parts of the galaxy, the arms of spiral nebulae, and other regions where absorbing interstellar material is present. Population 1I, in regions far from such matter, includes no supergiants or bright blue stars and the relation of the sequences are different. This type is found in the globular clusters, the elliptical nebulae, and the central regions of spiral nebulae and the galaxy. Both types occur near the sun.

The majority of the stars visible to the naked eye are giants, since these, being brighter, can be seen at much greater distances. Classes $F$ and $G$ comprise the greatest percentage of dwarf stars among those visible to the eye. The dwarf stars of classes $K$ and $M$ are actually much more numerous per unit of volume, but are so faint that few of the former, and none of the latter, are visible to the naked eye.

[^379](continued)

Typical supergiants, giants, and main-sequence stars

| $\begin{gathered} \text { Mount } \\ \text { Wilson } \\ \text { type } \end{gathered}$ | Star | Boss | Vis mag | 1950 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| cB 0 | $\epsilon$ Ori | 1370 | 1.8 | $\begin{array}{lll}\text { h m } \\ 5 & 3 \\ 5\end{array}$ | - $1^{\circ} 14^{\prime}$ |
| $g B 0$ | ${ }_{\kappa}^{\epsilon}$ Ori | 1435 | 2.2 | 545.4 | - 941 |
| $d B 1$ | $\eta$ Ori | 1301 | 3.4 | 522.0 | -226 |
| $d B 3$ | $\eta$ Aur | 1204 | 3.3 | 503.0 | +4110 |
| c ${ }^{5}$ | $\eta$ CMa | 1934 | 2.4 | 722.7 | -29 12 |
| $g B^{5}$ | $\delta$ Per | 838 | 3.1 | 339.4 | +4738 |
| $d B 5$ | $\tau$ Her | 4162 | 3.9 | 1618.2 | +4626 |
| c ${ }^{8} 8$ | $\beta$ Ori | 1250 | . 3 | 512.8 | -815 |
| g $B 8$ | $\beta$ Tau | 1304 | 1.8 | 523.1 | +28 34 |
| dB9 | ${ }_{\boldsymbol{a}} \mathrm{Peg}$ | 5944 | 2.6 | 2302.3 | +1456 |
| $g A 0$ | $\delta \mathrm{Cyg}$ | 5048 | 3.0 | 1943.4 | +4500 |
| d $A 1$ | a Lyr | 4722 | . 1 | 1835.2 | +3844 |
| cA 2 | $a \mathrm{Cyg}$ | 5320 | 1.3 | 2039.7 | +4506 |
| dA 2 | a CMa | 1732 | 1.6 | 642.9 | -1639 |
| gA 5 | $\beta$ Tri | 482 | 3.1 | 206.6 | +34 45 |
| dA 5 | $\beta$ Ari | 428 | 2.7 | 151.9 | +2034 |
| g $A 7$ | $\gamma$ Воо | 3722 | 3.0 | 1430.1 | +38 42 |
| $d F 0$ | $\gamma$ Vir | 3307 | 2.9 | 1239.1 | - 111 |
| gF 2 | $\beta$ Cas | 12 | 2.4 | 006.5 | +5852 |
| dF 3 | a CMi | 2008 | . 5 | 736.7 | + 521 |
| cF 5 | a Per | 772 | 1.9 | 320.7 | +49 41 |
| Df 5 | $\gamma \mathrm{Ser}$ | 4055 | 3.9 | 1554.1 | +1549 |
| cF 8 | $\gamma \mathrm{Cyg}$ | 5229 | 2.3 | 2020.4 | +4006 |
| gF 8 | $\epsilon$ Hya | 2354 | 3.5 | 844.1 | +636 |
| dF 8 | $\beta$ Vir | 3105 | 3.8 | 1148.1 | +203 |
| $d G 0$ | $\delta \mathrm{Tri}$ | 514 | 5.4 | 214.0 | $+3400$ |
| $g G 1$ | a Aur | 1246 | . 2 | 513.0 | +4557 |
| $c G 2$ | GC10756 | 2099 | 4.4 | 754.7 | -22 45 |
| gG 5 | $\gamma$ Hya | 3449 | 3.3 | 1316.2 | -2255 |
| $d G 5$ | $\kappa$ Cet | 752 | 5.0 | 316.7 | + 311 |
| cG 8 | $\epsilon$ Gem | 1717 | 3.3 | 640.8 | +25 11 |
| $g K 0$ | a Boo | 3662 | . 2 | 1413.4 | +1927 |
| $d K 0$ | 70 Oph | 4571 | 4.3 | 1802.9 | +231 |
|  | $\xi \mathrm{Cyg}$ | 5431 | 3.9 | 2103.1 | +43 44 |
| $g K 5$ | a Tau | 1077 | 1.1 | 433.0 | +1625 |
| dK 6 | 61 Cyg A | 5433 | 5.6 | 2004.7 | +3830 |
| dM0 | 61 Cyg B | 5434 | 6.3 | $20 \cdot 04.7$ | +3830 |
| $g M 0$ | $\beta$ And | 259 | 2.4 | 106.9 | +3521 |
| cM 1 | a Sco | 4193 | 1.2 | 1626.3 | -2619 |
| cM 2 | a Ori | 1468 | . 9 | 552.5 | +724 |
| gM2 | ${ }^{\text {a }}$ Cet | 691 | 2.8 | 259.7 | +354 |
| $d M 2$ | GC15183 | 2935 | 7.6 | 11.6 | +3618 |
| cM 5 | ${ }_{5}{ }_{5} \mathrm{Her}$ | 4373 | 3.6 | 1712.4 | +1427 |
| gM 5 | 56 Leo | 2915 | 6.0 | 1053.4 | +627 |
| dM 5 | GC923 |  | 9.2 | 1516.9 | -732 |

TABLE 875.-TEMPERATURE IN INTERSTELLAR SPACE*287
Because interstellar matter is far from being in thermodynamic equilibrium, the temperature of space will depend on the measuring process used.

```
Temperature from energy density of starlight.......... \(3^{\circ} \mathrm{K}\)
Color temperature of starlight........................... \(10,000-15,000^{\circ} \mathrm{K}\)
                                    dilution factor \(10^{-14}\)
Temperature of gas (kinetic)
    H I region (hydrogen neutral) .................... \(60^{\circ} \mathrm{K}\)
    H II region (hydrogen ionized) ................... \(10,000^{\circ} \mathrm{K}\)
Temperature of цrains (internal energy) ................ \(20^{\circ} \mathrm{K}\)
```

[^380]The motions of the stars show various well-marked features, of which the ellipsoidal distribution and the asymmetry are a conscquence of the rotation of the galaxy; the significance of certain other features is not yet fully understood. If we assume the circular velocity around the galactic center (Table 828) as our origin, and plot the individual motions of the stars of any group as vectors from this origin, the ends of these vectors do not form a spherical distribution (as they would if the motions of the stars were at random) but rather an elongated distribution which is more or less asymmetrical and in which the area of highest concentration of the vector points is centered about the origin. If for the moment we ignore the asymmetry, the distribution may be characterized as roughly ellipsoidal and the approximate extent and shape of the distribution may be inferred from the dispersions of the velocity components along each of the three principal axes, $\sigma_{a}, \sigma_{b}$, and $\sigma_{c}$, in $\mathrm{km} / \mathrm{sec}$.

| Spectral group 288 <br> (main sequence) | $\sigma_{a}$ | $\sigma_{b}$ | $\sigma_{c}$ | $\bar{M}_{\sigma_{o}{ }^{2}}$ |
| :---: | :---: | :---: | :---: | :---: |
| $A 0$ to $A 9$ | 17 | 12 | $8 \frac{1}{2}$ | 180 |
| $F 0$ to $F 9$ | $24 \frac{1}{2}$ | 16 | $12 \frac{1}{2}$ | 250 |
| $F 5$ to $G 0$ | 27 | 17 | $13 \frac{1}{2}$ | 240 |
| $G 0$ to $K 6$ | 32 | 16 | $16 \frac{1}{2}$ | 270 |
| $K 8$ to $M 5$ | 37 | 25 | 17 | 170 |
| (Giant branch) |  |  |  |  |
| $K 0$ to $K 9$ | $23 \frac{1}{2}$ | 17 | 20 | 1300 |
| $M 0$ to $M 9$ | 27 | $19:$ | $19:$ | $1800:$ |

The direction of the $a$-axis is called the direction of the preferential motion; the two opposite points on the sky at the extremities of this axis are called the vertices. The $a$-axis for any group of stars is always nearly parallel to the plane of the galaxy. In the case of most groups of stars fainter than eighth magnitude, it appears that the $a$-axis is directed approximately toward the galactic center at longitude 325\%. Among stars brighter than sixth magnitude the direction deviates from the direction of the galactic center toward greater longitudes and the deviation is most marked in the case of the $A$ stars, for which the longitude of the vertex is close to $350^{\circ}$. In every case the $c$-axis is directed toward some point close to the galactic pole. The asymmetry referred to above characterizes the distribution of the components parallel to the $b$-axis. It is relatively slight when the dispersions are small as with the $A$ stars, but becomes very pronounced in the case of groups with large dispersions, there being practically no large motions in the direction of the galactic rotation (longitude $55^{\circ}$ ).

The last column in the table contains the product of the mean stellar mass (in terms of the sun's mass) and the square of the dispersion along the $c$-axis. This quantity (analogous to kinetic energy) is practically constant for the various groups of the main sequence but is much larger for the giant branch.

The dispersions of velocities for the $B$ stars, the $c$ stars, and the Cepheids are of the order of $10 \mathrm{~km} / \mathrm{sec}$ and difficult to determine accurately. For long-period variables the dispersions average about $50 \mathrm{~km} / \mathrm{sec}$ and for the cluster-type variables $90 \mathrm{~km} / \mathrm{sec}$.

A general card catalog of radial velocities is kept at Mount Wilson Observatory. It now contains approximately 14,000 entries and will be published in the near future. The proper motions of all stars brighter than magnitude 7.0 and of many fainter stars may be found in the Albany General Catalog. The Transactions of the Yale Observatory contain the proper motions of many thousands of stars down to magnitude 9.5 and north of declination $-30^{\circ}$ and two catalogs of the Cape Observatory contain 40,000 proper motions in the zone $-40^{\circ}$ to $-52^{\circ}$.

[^381]TABLE 877.-STARS WITH LARGE SPACE VELOCITY GREATER THAN $20.0 \mathrm{~km} / \mathrm{sec}$, BASED ON PARALLAXES $\geqslant \because 005 * 220$

| Star | $V$ is mag | Spec | Par | Rad vel $\mathrm{km} / \mathrm{sec}$ | Apex |  | $\begin{aligned} & \mathrm{Vel} \\ & \mathrm{~km} / \mathrm{sec} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | $1 a$ | $b_{a}$ |  |
| 20 C 1321 | 10.8 | $d G 1$ | ".005 | -178 | $163^{\circ}$ | $-29^{\circ}$ | 699 |
| 20 C 879 | 10.2 | $d G 2$ | . 008 | -138 | 190 | +13 | 546 |
| HD 134439 | 9.4 | d ${ }^{\prime} 2$ | . 040 | +295 | 273 | -3 | 521 |
| HD 104800 | 9.3 | $d G 0$ | . 006 | +11 | 286 | $-17$ | 488 |
| HD 111980 | 8.3 | dF 6 | . 009 | +144 | 296 | -26 | 472 |
| HD 177095 | 9.4 | dG 3 | . 009 | + 78 | 246 | - 6 | 433 |
| HD 160693 | 8.4 | $d F 8$ | . 011 | + 40 | 299 | +18 | 432 |
| HD 224618 | 9.0 | $d G 6$ | . 014 | - 44 | 178 | -4 | 388 |
| 18 C 560 | 8.9 | dA 8 | . 007 | +338 | 187 | 0 | 380 |
| HD 179626 | 9.3 | $d F 4$ | . 007 | -71 | 264 | $+10$ | 358 |
| HD 6755. | 7.8 | $d G 0$ | . 018 | -325 | 248 | + 7 | 352 |
| HD 64090 | 8.2 | $s d G 0$ | . 038 | -242 | 294 | $-15$ | 345 |
| 20 C 825 | 10.2 | $s d A 4 p$ | . 009 | -164 | 289 | -18 | 324 |
| HD 230409 | 10.0 | $d G 4$ | . 009 | - 19 | 288 | $-1$ | 316 |
| HD 222766 | 9.7 | $d G 4$ | . 009 | - 98 | 188 | $+1$ | 307 |
| 18 C 3002 | 8.4 | $d K 0$ | . 023 | - 26 | 162 | -10 | 304 |
| HD 103095 | 6.5 | $s d G 5$ | . 108 | - 98 | 299 | $-12$ | 296 |
| 18 C 2348 | 9.1 | $d F 1$ | . 008 | -240 | 231 | +2 | 276 |
| HD 113083 | 8.2 | $d F 4$ | . 014 | $+227$ | 242 | +18 | 275 |
| HD 33793 | 9.2 | $s d K^{2} 2$ | . 262 | +242 | 243 | -8 | 273 |
| 20 C 58 | 12.3 | stl: 3 | . 243 | $+263$ | 97 | $-66$ | 264 |
| HD 134113 | 8.7 | dF 8 | . 009 | - 60 | 197 | +21 | 263 |
| HD 193901 | 8.2 | $d F 5$ | . 027 | -179 | 341 | -13 | 258 |
| 18 C 756 | 9.2 | dF 8 | . 031 | -191 | 307 | $+12$ | 243 |
| HD 5223 | 8.8 | $R 3$ | . 019 | -234 | 275 | +41 | 235 |
| HD 148816 | 7.4 | $d F 7$ | . 029 | - 52 | 256 | $-16$ | 223 |
| HD 219175 | 8.3 | $d F 5$ | . 011 | - 32 | 173 | $-13$ | 223 |
| HI) 102158 | 8.0 | $d G 0$ | . 014 | + 24 | 162 | $+21$ | 221 |
| HD 74000 | 9.4 | $d F 5$ | . 005 | +200 | 238 | +13 | 215 |
| HD 25329 | 8.6 | dK 0 | . 047 | - 30 | 229 | +88 | 214 |
| HD 140283 | 7.3 | sdA 5p | . 033 | $-170$ | 179 | $-5$ | 214 |
| HD 219962 | 6.4 | $g K 1$ | . 006 | $+23$ | 161 | $-10$ | 210 |
| HD 219617 | 9.0 | $\operatorname{sd} A 88$ | . 030 | + 6 | 293 | $-6$ | 202 |

[^382]|  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

[^383]| Star | $\begin{gathered} \text { Period } \\ \text { days } \end{gathered}$ | $\underset{\text { App }}{\text { bright }}$ | Sp 1 | Sp 2 | Radius |  | Mass |  | Ref ${ }^{200}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | $\overbrace{\left(i_{1}^{R_{1}}\right)}$ | $\begin{aligned} & \text { (in } \left.{ }_{2}^{R_{2}}\right) \end{aligned}$ | $\overbrace{\left(i^{M_{1}}\right)}$ | (in ${ }_{\text {¢ }}^{\text {¢ }}$ ) |  |
| V 444 Cyg | 4.212 | ${ }^{\text {m }} 8.4$ | 06 | WN 6 | 13 |  | 35 | 20 | a |
| AO Cas.. | 3523 | 5.8 | O 8.5 | O 8.5 | 16 | 10 | 31 | 29 | b |
| $\gamma \mathrm{Cyg}$ | 2.996 | 7.0 | $\bigcirc 9$ | $\bigcirc 9$ | 5.9 | 5.9 | 17.4 | 17.2 | c |
| SZ Cam | 2.698 | 7.0 | B 0 | ( $B^{2}$ ) | 12.7 | 5.6 | 36 | 10.3 | d |
| AH Cep | 1.775 | 6.6 | $B 0$ | B 0 | 6.1 | 6.1 | 16.5 | 14.2 | e |
| $\delta$ Ori | 5.733 | 2.4 | B 0 | (B2) | 17 | 10 | 26 | 10 | f |
| V 478 Cyg | 2.881 | 8.9 | B . 5 | B . 5 | 7.1 | 7.1 | 15.4 | 15.2 | g |
| VV Cep.. | 7430 | 6.6 | $B$ | cM 2 | 13 | 1200 | 33 | 47 | h |
| V Pup | 1.454 | 4.5 | B 1 | B 3 | 6.1 | 5.5 | 16.6 | 9.8 | i |
| V 470 Cyg | 1.873 | 8.7 | B 2 | B 2 | 6.0 | 7.2 | 13 | 11 | j |
| $\mu^{\prime}$ Sco | 1.446 | 3.0 | B 3 | B6 | 5.2 | 5.7 | 14.0 | 9.2 | k |
| TT Aur | 1.333 | 8.1 | B 3 |  | 3.8 | 3.4 | 6.7 | 5.3 | 1 |
| EO Aur | 4.066 | 7.6 | B 3 | ( $B 8$ ) | 13 | 16 | 27 | 27 | m |
| $v$ Her | 2.051 | 4.6 | B 3 | B 7 | 4.4 | 4.4 | 6.8 | 5.4 | n |
| CW Cep | 2.729 | 7.6 | B 3 | B 3 | 4.5 | 4.0 | 10.0 | 9.8 | j |
| AG Per | 2.029 | 6.5 | B 3 | B 4 | 2.7 | 2.6 | 5.0 | 4.4 | $\bigcirc$ |
| SX Aur | 1.210 | 8.2 | B 3.5 | B 3.5 | 5.1 | 4.4 | 10.7 | 5.6 | i |
| $\xi$ Aur | 972.15 | 6.6 | B6 | cK 4 | 2.8 | 200 | 10 | 22 | p |
| U CrB | 3.452 | 7.6 | B 5 | ( $A 2$ ) | 3.4 | 5.5 | 6.4 | 2.4 | q |
| U Oph | 1.677 | 5.8 | B 5 | $B 5$ | 3.1 | 3.0 | 5.3 | 4.6 | r |
| V 599 Ag 1 | 1.849 | 6.5 | B 5 | B 8 | 7.8 | 4.4 | 12 | 6.4 | s |
| Z Vul | 2.455 | 7.0 | B 3 |  | 4.6 | 4.3 | 5.3 | 2.4 | t |
| 6 Agl | 1.950 | 5.0 | B 8 | B 8 | 3.6 | 3.6 | 6.8 | 5.4 | u |
| TX UMa | 3.063 | 6.8 | B 8 | $g F 2$ | 2.1 | 3.4 | 2.8 | . 9 | v |
| $\beta$ Per | 2.867 | 2.2 | B 8 | (G) | 2.7 | 2.8 | 2.3 | . 6 | w |
| AR Aur | 4.135 | 5.8 | B 9 | A 0 | 1.8 | 1.8 | 2.6 | 2.3 | c |
| $\beta$ Lyr | 12.908 | 3.4 | cB9 |  | 47 | 31 | 52 | 43 | w |
| U Sge | 3.381 | 6.4 | B 9 | G 2 | 4.5 | 5.8 | 6.7 | 2.0 | x |
| GO Cyg | . 718 | 8.3 | $B 9$ |  | 2.0 | 1.4 | 1.6 | 1.3 | y |
| $\beta$ Aur | 3.960 | 2.1 | A 0 | A 0 | 2.6 | 2.6 | 2.4 | 2.4 | z |
| TV Cas | 1.813 | 7.3 | A 0 |  | 2.4 | 2.5 | 1.7 | 1.0 | a 1 |
| RX Her | 1.779 | 7.1 | A 0 | $A 0$ | 2.3 | 1.8 | 2.1 | 1.9 | b 1 |
| MR Cyg | 1.677 | 8.5 | A 0 | (A0) | 3.2 | 3.6 | 3.0 | 2.6 | c 1 |
| WX Cep | 3.378 | 9.1 | A 2 | (A5) | 3 | 3 | 1.0 | 1.0 | d 1 |
| TX Her | 2.060 | 8.3 | A 2 | A 2 | 1.6 | 1.6 | 2.0 | 1.8 | e 1 |
| CM Lac | 1.605 | 8.3 | A 2 | A 8 | 1.3 | 1.7 | 2.0 | 1.5 | $f 1$ |
| UX Mon | 5.905 | 8.7 | A 3 | G 2 | 1.8 | 6.6 | 3.4 | 1.5 | g 1 |
| RX Gem | 12.208 | 8.5 | A 4 | K 0 | 2.2 | 5.5 | 3.1 | . 6 | $h 1$ |
| WW Aur | 2.525 | 5.7 | A 7 | A 7 | 2.2 | 2.2 | 2.2 | 1.9 |  |
| S Aut | . 648 | 8.8 | A 8 | A 8 | 1.4 | 1.1 | 1.0 | . 9 | i 1 |
| Z Her | 3.993 | 7.2 | F 2 | (F2) | 1.5 | 3.1 | 1.5 | 1.3 |  |
| RS CV | 4.798 | 8.0 | $F 4$ | G 8 | 1.6 | 5.3 | 1.9 | 1.7 | j 1 |
| VZ Hya | 2.904 | 9.2 | $F 5$ | $F 9$ | 1.3 | 1.0 | 1.2 | 1.1 | k 1 |
| WUMa | . 334 | 8.3 | F 8 | F 8 | . 8 | . 6 | 1.0 | . 9 | 11 |
| WZ Oph | 4.183 | 9.7 | G 0 | G 0 | 1.3 | 1.2 | 1.4 | 1.3 | m 1 |
| UV Leo | . 600 | 8.5 | G0 | G 2 | 1.1 | 1.2 | 1.3 | 1.2 | n 1 |
| RT And | . 629 | 9.0 | G 0 | $K 1$ | . 8 | 1.4 | 1.5 | 1.0 | - 1 |
| \& Boo | . 268 | 6.6 | G 2 | G 2 | . 7 | . 6 | 1.0 | . 5 | p 1 |
| WW Dra | 4.630 | 8.8 | $g G 2$ | $g K 0$ | 4.8 | 8.3 | 3.5 | 2.5 | q 1 |
| Ar Lac | 1.983 | 7.3 | G 5 | K 0 | 1.8 | 3.0 | 1.4 | 1.4 | k 1 |
| RT Lac | 5.074 | 8.8 | G 9 | K 1 | 4.9 | 4.9 | 1.0 | 1.9 | r 1 |
| AH Vir | . 408 | 9.7 | $K 0$ | K 0 | 1.3 | . 8 | 1.4 | . 6 | s 1 |
| YY Gem | . 814 | 8.6 | M 1 | M 1 | . 6 | . 6 | 1.0 | . 9 | t 1 |

[^384]Huffer and Eggen, Astrophys. Journ., vol. 106, p. 313, 1947. f, Luyten-Struve-Morgan, Yerkes Publ., vol. 7, pt. 4, 1939. g, McDonald, Publ. Dominion Istrophys. Obs., vol. 7, p. 135, 1949. h, Geodicke, Michigan Publ., vol. 8, No. 1, $1939 . \quad$ i, Popper, Astrophys. Journ., vol. 97, p. 394, 1943. j, Gaposchkin, $\Lambda$ stron. Journ., vol. 53, p. 112, 1948 . k, Stibbs, Monthly Notices, Roy. Astron. Soc., vol. 108, p. 398, 1948.1 , Joy and Sitterly, Astrophys. Journ., vol. 73, p. 77, 1931. m, Gaposchkin, Publ. Astron. Soc. Pacific, vol. 55, p. 192, 1943. n, Baker, Lick Obs. Bull., vol. 12, p. 130, 1926. o, Eggen (private communication). Kopal, Astrophys. Journ., vol. 103, p. 310, 1946. q, Shapley, Princeton Contr., No. 3, 1915. r, Huffer and Kopal, Istrophys. Journ. (in press). s, Gaposchkin, Harvard Bull., No. 917, 1943. i, Baker, Laws Bull., No. 2, p. 173,1916 . t. Wylie, Astrophys. Journ., vol. 56, p. 232,1922 . v, Huffer and Eggen, Astrophys. Journ., vol. 105, p. 217, 19.f7. w, Kopal, Astrophys. Journ., vol. 93, p. 92, 1941. x, Joy, Astrophys. Journ., vol. 71, p. 336, 1930. y, Pierce, istron. Journ., vol. 48, p. 113, 1939. z, Piotrowski, Astrophys. Journ., vol. 108, p. 510, 1948; Smith. Astrophys. Journ., vol. 108, p. 504, 1948. a 1, McDiarmid, Princeton Contr., No. 7, $1924 . \quad$ h 1, Wood, Astrophys. Journ., vol. 110, p. 465, 1949. c 1, Fracastaro, Arcetri Publ., vol. 55, p. 37, 1937. d 1, Sahade and Cesco, Astrophys. Journ., vol. 102, p. $128,1945$. e 1, Baker, Laws Bull., No. 31, 1921. f 1, Wachmann, Astron. Journ., vol. 259, p. 323, 1936. g $]$, Struve, Astrophys. Journ., vol. 106, p. 255, 1947. h 1, Gaposchkin, Astrophys. Journ., vol. 104, p. $376,1946$. i 1, Joy. Astrophys. Journ., vol. 64, p. 293, 1926. J1, Sitterly, Princeton Contr., No. 11, 1930. k 1 , Wood, Princeton Contr., No. 21, 1946. 11,' Huffer, Astrophys. Journ., vol. 79, p. 369, 1934.1 m 1, Gaposch' kin, Harvard Bull., No. 907, 1938. n 1, Gaposchkin, Astrophys. Journ., vol., 104, p. 370, $1946 . \mathrm{p} 1$, Eggen, Astrophys. Journ., vol. 108, p. 15, 1948. q 1, Plant, Diss. Leiden. 1939. r 1, Fowler, Astrophys. Journ., vol. 52, p. 261, 1920. s 1, Chang, Istrophys. Journ., vol. 107, p. 96, 1948. t 1, Kuiper, Astrophys. Journ., vol. 88, p. 456, 1938.

## TABLE 880.—SPECTROSCOPIC BINARY STARS*

These binary systems were discovered and investigated by measuring the Doppler displacements of the spectrum lines. All except the widest systems are too close to each other to be observed as double stars through the telescope. The data given are from J. H. Moore's "Fifth Catalogue of Spectroscopic Binaries." ${ }^{2011}$ In the table a designates the semimajor axis of the orbit in kilometers and refers to the center of gravity of the system; $i$ is the inclination of the orbit plane to the plane of the sky; and $m$ designates the mass of each component. When both components of a binary system are bright enough to record their spectral lines, individual mass functions can be derived and these are shown in column 8. When only the spectrum of one star is visible a more complicated mass function is obtained involving the total mass of the system and the mass ratio. Several systems in the table are eclipsing stars and for them the inclination is nearly 90 : Hence for them the quantity $\sin ^{3} i$ in columns 8 and 9 is nearly equal to 1 .


[^385]
## TABLE 881.-PROPERTIES AND CLASSIFICATION OF STAR CLUSTERS*

Star clusters fall into two distinctly different types:
Globular.-Typical, Messier 13; open, Messier 4; elongated, Messier 19. Have strong central condensations, rich in faint stars. Scattered widely in latitude, restricted in longitude. Many variables-nearly 1,300 in 62 clusters. Radial velocities $>100 \mathrm{~km} / \mathrm{sec}$. All more than 5,000 , and one-third more than 50,000 light-years away. Very few new ones found-about 100 known. Very definitely part of galaxy. Although concentrated toward its plane, only 2 within $4^{\circ}$ of it (obstruction by interstellar dust clouds). Diameters about 35 parsecs. Many stars, tens and hundreds of thousands. Many giants and supergiants with maximum luminosity about -2.5 .

Galactic.-Very varied: rich, M11; irregular, M 35; nebulous, Pleiades; accidental, M 103. Almost exclusively in Milky Way, all longitudes : apparently no variables. Radial velocities rarely $>40 \mathrm{~km} / \mathrm{sec}$, generally less. Almost all less than 4,000 light-years distant. Almost exclusively in galactic region devoid of globulars. Tens and hundreds, rarely thousands of stars. Hyades type, yellow stars as dominant as $A$ type. Pleiades type, almost all $B$ 's and $A$ 's, on Russell's main sequence.

* Prepared by H. Shapley, Harvard University.


## Part 1.-Globular star clusters

This table contains those with galactic latitudes $>20^{\circ}$, for which space absorption can be evaluated and distance correctly estimated (also the giant cluster Omega Centauri in lower latitude). ${ }^{292}$

| NGC | RA (1900) | ) Dec | Galactic |  | Apparent magnitude | Distance (kiloparsecs) | Absolute magnitude | No. of variables |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Long | Lat |  |  |  |  |
|  | ${ }^{\text {h }} \mathrm{m}$ |  |  |  |  |  |  |  |
| 104 (47 Tuc) | $\begin{array}{ll}0 & 19.6\end{array}$ | $-72^{\circ} 38^{\prime}$ | $272^{\circ}$ | $-45^{\circ}$ | (4.5) | 7.6 | $-10.2$ | 8 |
| 288 .... | 047.8 | $-2708$ | 157 | -88 | 8.96 | 14.5 | - 6.8 | 2 |
| 362 | 058.9 | -71 23 | 268 | -47 | 8.0 | 10.0 | $-7.3$ | 14 |
| 1261 | 39.5 | -55 36 | 237 | -51.5 | 9.5 | 22 | $-7.2$ | 0 |
| 1851 | 510.8 | -40 09 | 212 | -34.5 | 7.72 | 14 | $-8.1$ | 3 |
| 2419 | 731.4 | +39 06 | 148 | $+26$ | 11.51 | 56.2 | $-7.7$ | 36 |
| 4147 | 125.0 | +1906 | 226 | +79 | 11.01 | 20.0 | $-5.5$ | 4 |
| 4590 (M 68) | 1234.2 | $-2612$ | 269 | $+36$ | 9.12 | 13.5 | $-6.8$ | 28 |
| 5024 (M 53) | 138.0 | +1842 | 305 | +79 | 8.68 | 20.2 | $-7.8$ | 42 |
| 5053 ..... | 1311.5 | +1813 | 310 | +78 | 10.9 | 17.4 | $-5.3$ | 10 |
| 5139 ( $\omega$ Cen) | 1320.8 | -46 47 | 277 | $+15$ | (4.7:) | 6.8 | -10: | 168 |
| 5272 (M3). | 1337.6 | +28 53 | 8 | $+78$ | 7.21 | 12.2 | $-8.2$ | 186 |
| 5466 . | 141.0 | +2900 | 8 | +72.5 | 10.39 | 17.0 | - 5.8 | 18 |
| 5634 | 1424.4 | - 532 | 310 | +48.5 | 10.8 | 32 | - 6.7 | 7 |
| 5694 | 1433.8 | -26 36 | 299 | +29 | 10.87 : | 33.1 | - 7.1: | 0 |
| 5897 | 1511.7 | -20 39 | 312 | +29 | 9.61 | 13.8 | - 6.5 | 0 |
| 5904 (M 5) | 1513.5 | +227 | 332 | $+46$ | 7.04 | 10.1 | - 8.0 | 97 |
| 6205 (M 13) | 1638.1 | +36 39 | 27 | +40 | 6.78 | 9.5 | $-8.1$ | 15 |
| 6218 (M 12) | 1642.0 | -146 | 344 | $+25$ | 7.95 | 8.3 | $-7.3$ | 1 |
| 6229 ..... | 1644.2 | +47 42 | 40 | +40 | 10.26 | 30 | $-7.1$ | 21 |
| 6254 (M 10) | 1651.9 | - 357 | 343 | +22 | 7.64 | 8.3 | $-7.6$ | 2 |
| 6341 (M 92) | 1714.1 | +4315 | 36 | +35 | 7.30 | 10.3 | $-7.8$ | 16 |
| 6752 … | 192.0 | -60 48 | 303 | -26.5 | 7.2 : | 5.8 | -7.4 : | 1 |
| 6809 (M 55) | 1933.7 | $-3110$ | 336 | -25 | 7.08 | 5.8 | -7.7 | 2 |
| 6864 (M 75) | 20.2 | $-2212$ | 347 | -27 | 9.50 | 42 | -8.9 : | 11 |
| 6934 | 2029.3 | + 704 | 20 | $-20$ | 10.01 | 18 | $-7.0$ | 51 |
| 6981 (M 72) | 2048.0 | -12 55 | 3 | -34 | 10.24 | 16.6 | $-6.6$ | 31 |
| 7006 … | 2056.8 | +1548 | 32 | -21 | 11.45 | 44 | $-7.3$ | 20 |
| 7078 (M 15) | 2125.2 | +1144 | 33 | $-28$ | 7.33 | 11.5 | $-8.3$ | 66 |
| 7089 (M 2) | 2128.3 | -116 | 21 | -36 | 7.30 | 13.8 | - 8.5 | 17 |
| 7492 .... | 233.1 | $-1610$ | 22 | -64 | 12.33 | 25.1 | $-4.7$ | , |

[^386]TABLE 881.-PROPERTIES AND CLASSIFICATION OF STAR CLUSTERS (concluded)

## Part 2.-Galactic star clusters

Columns 2 through 6 from Shapley. ${ }^{203}$ Distances from R. J. Trumpler, unpublished. Linear diameters computed on basis of revised distances. 1 kiloparsec $=31 \times 10^{15} \mathrm{~km}=$ $3 \times 10^{3}$ light-years.


## TABLE 882.-OUR GALAXY, ITS CENTER AND ROTATION*

The center of the galaxy apparently lies among the dense Milky Way clouds in Sagittarius, at a distance of about 9,000 to 10,000 parsecs from the sun. About this center the sun revolves with a period of some 200 million years at an orbital speed of nearly $300 \mathrm{~km} / \mathrm{sec}$. The amount of matter within the sun's orbit is probably more than 200 billion times the sun's mass. In the table, $A$ is the differential orbital radial velocity per kiloparsec of distance from the sun, $r A$ is the maximum group velocity for a distance $r$, and $l_{0}$ is the longitude of the galactic center. The sun is about 33 parsecs above the galactic plane. ${ }^{214}$

| Stars | No. | $\begin{gathered} \text { Vis } \\ \text { mag } \\ \text { limit } \end{gathered}$ | Distance kpc | $\begin{gathered} \frac{\mathrm{Max}}{r} A \\ \mathrm{~km} / \mathrm{sec} \end{gathered}$ | $\underset{\mathrm{km} \mathrm{sec}^{-1} \mathrm{kpc}^{-1}}{A}$ | 10 | $\begin{aligned} & \text { Dist } \\ & \text { to } \\ & \text { center } \\ & \text { kpc } \end{aligned}$ | Source ${ }^{295}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{O}-\mathrm{M}$ | 210 | 8.0 | .2-1.1 | 35 | 19.0 | 324 | 6.3 | a |
| O-B 7 | 849 | 7.5 | .2-1.4 | 22.2 | 15.0 | 324.4 | 10.0 | b |
| Interstellar | 261 | 8.6 | . $4-1.2$ | 13.5 | 16.6 | 331.7 |  | c |
| B-K | 3786 |  |  |  | 15.0 | 324 | 6.5 | d |
| PGC and 18 C | 4233 |  |  |  | 15.0 |  | 8.8 | e |
| K | 392 | 7.5 | 2 |  | 17.0 | 17 |  | f |
| Plan Neb | 110 |  | .5-12.0 | 264 | 14.0 | 333.0 | 9.4 | g |
| Cepheids | 156 | 14.1 | . $4-2.3$ | 39.4 | 20.9 | 325.3 | 10.0 | h |
| O B, Ceph, c, gas |  |  | .2-10.0 | 39.6 | 17.7 | 326.0 | 9.4 | i |
| - | 205 | 8.4 | .2-1.3 | 26.6 |  | 324.4 | . . | j |
| O 5-B 5 | 987 | 6.4 | . $3-1.1$ | 18.8 |  |  | $\cdots$ | k |
| Irreg var | 116 | . . | . 5 | 9.5 | ... | 325.7 |  | 1 |

[^387]The maximum component ( $v \sin i$ ) along the line of sight of the equatorial velocity $v$ of rotation is found from the distortion of an absorption line produced by differential Doppler effect across the observed hemisphere. For stars in the following groups, v> $50 \mathrm{~km} / \mathrm{sec}$ very rarely, and $v \ll 50 \mathrm{~km} / \mathrm{sec}$ usually: supergiants, giants; main-sequence stars later than $I: 5$ and not close spectroscopic binaries. For main-sequence stars of early type, and not spectroscopic binaries or cluster members, the distribution function $f(v)$ is found to be well represented by the formula

$$
f(v)=(j / \sqrt{v \pi})\left\{\exp \left[-j^{2}\left(v-v_{1}\right)^{2}\right]+\exp \left[-j\left(v+v_{1}\right)^{2}\right]\right\},
$$

where the parameters $j^{-1}, v_{1}$, and $\bar{v}$ have the following values:

|  | $\overbrace{B e}$ | $O-B$ | $A$ | $F 0 \cdot F 2$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| $j^{-1}(\mathrm{~km} / \mathrm{sec})$ | 70 | 63 | 107 | 90 |
| $\frac{v_{1}}{v}(\mathrm{~km} / \mathrm{sec})$ | 350 | 95 | 107 | 0 |
| $\frac{v}{v}(\mathrm{~km} / \mathrm{sec})$ | 348 | 94 | 112 | 51 |

In an idealized Roche model, rotational instability sets in at $v=560 \mathrm{~km} / \mathrm{sec}$. The Be stars are surmised to be rotationally unstable $B$ 's. Number of $B 8$ 's per $B 8 e=123$; number of $(B 0-B 5$ )'s per $(B 0 c-B 5 e)=15$. In the Pleiades and in $h$ and $\chi$ Persei, $v$ for $B$ 's is $\sim 2 \times \overline{v^{\prime}}$ for noncluster $B$ 's. For 13 Pleiades earlier than $B 9$, number of $B$ 's per $B e=$ 3. In many close spectroscopic binaries of both late and early types, the components rotate with the orbital period. In some eclipsing systems, the sense of rotation is found from the Doppler shift of an absorption line at partial phrase. The sense is always that of the orbital motion. For the sun, $v=2.1 \mathrm{~km} / \mathrm{sec}$.

* Prepared by A. J. Deutsch, Harvard University.


## TABLE 884.-TRANSMISSION OF LIGHT THROUGH SPACE*

The obscuring matter in space is too irregularly distributed to be described by a mean extinction coefficient for the galaxy. For bright Milky Way regions a minimum value of $0.2 \mathrm{~m} / \mathrm{kpc}$ has been found. ${ }^{210}$

Photoelectric measurements by Stebbins and Whitford ${ }^{207}$ indicate that the wavelength dependence of the interstellar extinction is essentially the same throughout the galaxy. Their results are given with the table. See references to Oort ${ }^{208}$ and Strohmeier ${ }^{2010}$ for possibility of variations in bright and obscured regions.

| $\lambda(A)$ | $\frac{1}{\lambda}\left(\mu^{-1}\right)$ | $m(\mathrm{mag})$ | $\lambda(A)$ | $\frac{1}{\lambda}\left(\mu^{-1}\right)$ | $m(\mathrm{mag})$ |
| :---: | :---: | :---: | ---: | :---: | :---: |
| 3200 | 3.12 | $1.30 \dagger$ | 5700 | 1.75 | .64 |
| 3550 | 2.83 | 1.18 | 7190 | 1.39 | .35 |
| 4220 | 2.37 | 1.00 | 10300 | .97 | .00 |
| 4880 | 2.05 | .81 | 21000 | .48 | $-.25 \dagger$ |

An unknown constant must be added to these values to give the actual extinction. The scale has been adjusted arbitrarily to give 1 mag differential extinction between $\lambda 4200$ and 10,300 .

A value of 4 for the ratio of total photographic absorption to international color excess [ $\left.R=A_{44 \times} /\left(A_{\text {tum }}-A_{\text {stan }}\right)\right]$ is obtained by extrapolation of the above table to $1 / \lambda=0$. Most observational determinations are between 3 and $5 .{ }^{300}$

Light from distant stars shows polarization up to 5 percent, approximately proportional to reddening. Plane of polarization variable but generally perpendicular to galactic plane. ${ }^{301}$

[^388]
# TABLE 885.-SOME DATA ON THE EARTH AND ITS SURFACE <br> Part 1.—Dimensions 

'The earth is a great oblate spheroid with the oceans making up about 71 percent of the area. The dimensions of the earth are as follows :

| Equatorial radiu <br> Polar radius <br> Area of surface. <br> Volume of geoid | 6378.388 km <br> 6356.912 km <br> $510,100,934 \mathrm{~km}^{2}$ <br> $1,083,319,780,000 \mathrm{~km}^{8}$ |
| :---: | :---: |
| The surface consists of: |  |
| Oceans and seas Land | $\begin{aligned} & 351.059 \times 10^{9} \mathrm{~km}^{2} \text { or } 70.8 \text { percent } \\ & 148.892 \times 10^{9} \mathrm{~km}^{2} \text { or } 29.2 \text { percent } \end{aligned}$ |

The land surface is of various elevations above sea level, the mean being about 840 m , while the average depth of the three great oceans and adjacent seas is about 3800 m (Table 886). The highest elevation and the lowest elevation in each continent are given in Part 2.

Part 2.-Area and elevation of continents

|  | $\begin{gathered} \text { Area } \\ 10^{n} \mathrm{~km}^{2} \end{gathered}$ | Highest mountain | Height | Lowest | $\begin{gathered} \text { Depth } \\ m \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Africa | 298 | Kibo | 5970 | Libian Desert | 133 |
| North America | 21.5 | McKinley | 6150 | Death Valley | 85 |
| South America | 17.6 | Aconcagua | 6960 | Sea level |  |
| Asia .......... | 44.0 | Fverest | 8880 | Dead Sea | 392 |
| Europe | 9.7 | Elbrus | 5640 | Caspian Sea | 28 |
| Australia | 7.7 | Korciusko | 2230 | Lake Eyre | 12 |

TABLE 886.-SEA.WAVE HEIGHT IN FEET FOR VARIOUS WIND VELOCITIES AND DURATIONS

| Wind <br> duration <br> in hours | $\overbrace{10}$ | 20 | 30 | 40 | 50 | 60 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 2 | 5 | 10 | 14 | 20 | 25 |
| 12 | 2 | 7 | 13 | 20 | 30 | 35 |
| 24 | 2 | 9 | 17 | 30 | 40 | 55 |
| 48 | 2 | 10 | 22 | 35 | 45 | 70 |

Waves consistently higher than the values given are not found because stronger winds blow the tops of the waves off. Isolated waves up to 80 feet are due to the addition of two or more crests.
One of the longest swell periods recorded was 23 seconds. According to the relations given, its length in deep water would equal 2,650 feet, and its velocity 69 knots. A 28 -second swell has been recorded near Cape of Good Hope. Its length must have been almost three-quarters of a mile and its speed 84 knots.

## TABLE 887.-APPROXIMATE HEIGHT OF SWELL IN FEET AT VARIOUS DISTANCES FROM THE STORM AREA

| Distance from storm |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | area in nautical miles |  |  |  |
| 40 | 500 | 1000 | 2000 | 3000 |
| 30 | 19 | 20 | 12 | 8 |
| 20 | 12 | 14 | 8 | 5 |
| 15 | 8 | 8 | 5 | 3 |
| 10 | 5 | 5 | 3 | 2 |
| 5 | 2 | 3 | 2 | 1 |

[^389]| Body | $\begin{gathered} \text { Area } \\ 10^{8} \mathrm{~km}^{2} \end{gathered}$ | Volume $10^{6} \mathrm{~km}^{3}$ | Mean depth m |
| :---: | :---: | :---: | :---: |
| Atlantic Ocean | 82.441 | 323.613 | 3,926 |
| Pacific Ocean $\}$ excluding adjacent seas | 165.246 | 707.555 | 4,282 |
|  | 73.443 | 291.030 | 3,963 |
| All oceans (excluding adjacent seas). | 321.130 | 1,322.198 | 4,117 |
| Arctic Mediterranean . . | 14.090 | 16.980 | 1,205 |
| American Mediterranean | 4.319 | 9.573 | 2,216 |
| Mediterranean Sea and Black Sea | 2.966 | 4.238 | 1,429 |
| Asiatic Mediterranean | 8.143 | 9.873 | 1,212 |
| Large Mediterranean seas | 29.518 | 40.664 | 1.378 |
| Baltic Sea .............. | . 422 | . 023 | 55 |
| Hudson Bay | 1.232 | . 158 | 128 |
| Red Sea ... | . 438 | . 215 | 491 |
| Persian Gulf | . 239 | . 006 | 25 |
| Small Mediterranean seas. | 2.331 | . 402 | 172 |
| All Mediterianean seas. | 31.849 | 41.066 | 1,289 |
| North Sea | . 575 | . 054 | 94 |
| English Channel | . 075 | . 004 | 54 |
| Irish Sea | . 103 | . 006 | 60 |
| Gulf of St. Lawrence. | . 238 | . 030 | 127 |
| Andaman Sea | . 798 | . 694 | 870 |
| Bering Sea | 2.268 | 3.259 | 1,437 |
| Okhotsk Sea | 1.528 | 1.279 | 838 |
| Japan Sea | 1.008 | 1.361 | 1,350 |
| East China Sea. | 1.249 | . 235 | 188 |
| Gulf of California. | . 162 | . 132 | 813 |
| Bass Strait | . 075 | . 005 | 70 |
| Marginal seas | 8.079 | 7.059 | 874 |
| All adjacent seas | 39.928 | 48.125 | 1,205 |
| Atlantic Ocean $7 . . . . . . . . . . . .$. | 106.463 | 354.679 | 3,332 |
| Pacific Ocean $\}$ including adjacent seas. | 179.679 | 723.699 | 4,028 |
| Indian Ocean $\}$. . . . . . . . . . . . . . . . . . . | 74.917 | 291.945 | 3,897 |
| All oceans (including adjacent seas) | 361.059 | 1,370.323 | 3,795 |

$$
\begin{array}{ll}
\text { Mean elevation of land } & =840 \mathrm{~m} \\
\text { Mean depth of oceans } & =3,800 \mathrm{~m} \\
\text { Mean sphere depth } & =2,440 \mathrm{~m}
\end{array}
$$

Continental shelves extend out with small gradients to depths of about 100 to 150 m . Average width about 30 miles but varies from zero to several hundred. Continental slopes have about $2^{\circ}$ to $3^{\circ}$ inclination. Volcanic islands, fault scarps, etc., may have slopes as steep as similar features on land.

| Greatest depths known are in the Pacific Ocean-10,800 m |
| :--- |
| Deepest sounding in the Atlantic Ocean is |
| Deepest sounding in the Indian Ocean is |
| , 200 m |
| $7,450 \mathrm{~m}$ |

Greatest depths occur in troughs or trenches paralleling mountainous coasts and insular arcs. These areas are centers of seismic and volcanic activity.

Topography of the ocean floor is in general similar to major features found on land. Submerged features such as the Mid-Atlantic Ridge are comparable in size and extent to the combined Rockies and Andes Mountains. In the Pacific are hundreds of isolated guyots, flat-topped seamounts rising thousands of feet from the ocean bed with minimum depths of $1,000-2,000 \mathrm{~m}$. Many isolated seamounts rise more than $3,000 \mathrm{~m}$ from the sea floor. Continental and insular shelves and slopes are not regular but generally show topographic relief such as shoals, terraces, canyons and valleys. Certain areas such as the Mediterranean, Black Sea, Sea of Japan, Red Sea, etc., are isolated at depth by ridges separating the deep water from the adjacent sea or ocean.

[^390]| Depth interval ( $m$ ) | Including adjacent seas |  |  | $\begin{gathered} \text { All } \\ \text { oceans } \end{gathered}$ | Excluding adjacent seas |  |  | $\underset{\text { oceans }}{\text { All }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Atlantic | Pacific | Indian |  | Atlantic | Pacific | Indian |  |
| 0-200 | 13.3 | 5.7 | 4.2 | 7.6 | 5.6 | 1.7 | 3.2 | 3.1 |
| 200-1000 | 7.1 | 3.1 | 3.1 | 4.3 | 4.0 | 2.2 | 2.7 | 2.8 |
| 1000-2000 | 5.3 | 3.9 | 3.4 | 4.2 | 3.6 | 3.4 | 3.1 | 3.4 |
| 2000-3000 | 8.8 | 5.2 | 7.4 | 6.8 | 7.6 | 5.0 | 7.4 | 6.2 |
| 3000-4000 | 18.5 | 18.5 | 24.0 | 19.6 | 19.4 | 19.1 | 24.4 | 20.4 |
| 4000-5000 | 25.8 | 35.2 | 38.1 | 33.0 | 32.4 | 37.7 | 38.9 | 36.6 |
| 5000-6000 | 20.6 | 26.6 | 19.4 | 23.3 | 26.6 | 28.8 | 19.9 | 26.2 |
| 6000-7000 | . 6 | 1.6 | . 4 | 1.1 | . 8 | 1.8 | . 4 | 1.2 |
| $>7000$ |  | . 2 |  | . 1 |  | . 3 |  | . 1 |

*For reference, see footnote 302, p. 773.

## TABLE 890.-PHYSICAL PROPERTIES OF SEA WATER (Fig. 34)

Temperatures in the sea range from $-2^{\circ}$ to $30^{\circ} \mathrm{C}$. The lower limit is set by the formation of ice and the higher limit by the balance between incoming radiation, back radiation, and evaporation.

Pressures in the sea vary from zero at the sea surface to about $1,000 \mathrm{~atm}$ in the greatest depths $(10,000 \mathrm{~m})$. Standard unit is the bar $=10^{6}$ dynes $/ \mathrm{cm}^{2}$. Approximately 10 m of sea water $=1 \mathrm{~atm}$.

Concentration of the dissolved constituents varies from nearly zero in river mouths to $40^{\circ} \%$ (parts per thousand) in isolated seas in arid regions. In most ocean waters the total solids are between 33 and $37 \%$. In addition, sea water contains dissolved gases, dissolved organic matter, and variable amounts of particulate material of biological or terrigenous origin.

Salinity is defined as the total amount of solid material in grams in one kg of sea water when all carbonates are converted to oxides, the bromine and iodine replaced by chlorine, and all organic matter completely oxidized.

Chlorinity, determined by titration with $\mathrm{AgNO}_{3}$, is essentially equal to the amount of chlorine in grams in one kg of sea water when all the bromine and iodine have been replaced by chlorine.

$$
\text { Salinity }=0.03+1.805 \times \text { Chlorinity }(\% / \text { oo })
$$

Distribution of temperature and salinity is most variable in the surface layers. Low temperatures occur in high latitudes with relatively low salinities. In the Tropics surface temperatures and salinities are high. The great ocean basins are filled with highdensity water produced in high latitudes during the winter when ice forms or when water of high salinity is cooled. Deep temperatures are therefore generally between $0^{\circ}$ and $2^{\circ} \mathrm{C}$. Convection and wind mixing produce a surface layer in which uniform conditions prevail. This may be as thick as several hundred meters. Immediately beneath this there is a rapid change in temperature called the thermocline. Diurnal variations of temperature at the surface rarely exceed $1^{\circ} \mathrm{C}$. Annual variations of surface temperature are greatest in midlatitudes (about $10^{\circ} \mathrm{C}$ ). Annual variations diminish with depth and rarely extend below 200 m .

Density of sea water is a function of salinity as well as temperature and pressure. The range in values is from 1.00 to about $1.04 \mathrm{~g} / \mathrm{cm}^{3}$. Most of the other properties are functions of temperature, salinity, and pressure. The difference from the values for pure water depends then on the effects of the dissolved organic compounds. Light absorption and color will also be primarily determined by suspended or dissolved debris. Processes of heat conduction, diffusion, and transfer of momentum are dominated by turbulent water movements and consequently the laboratory coefficients of conductivity, diffusion, and viscosity have to be replaced by "eddy" coefficients of vastly greater magnitude.

Absorption of light.-Water is essentially opaque to electromagnetic radiation except in the visible spectrum. Below several hundred meters, even in the clearest water, all the solar radiation is absorbed. (See Tabic 891 and fig. 35.) In coastal waters that contain suspended debris, the radiation may be absorbed in only a few meters. The rapid absorption of radiation limits photosynthesis to the surface layers.

Evaporation.-The principal source of heat is radiation from sun and sky. The chief heat losses are due to long-wave radiation to space and evaporation. Evaporation is greatest when the air is dry and colder than the water. Regional variations are generally between 50 and $150 \mathrm{~cm} /$ year.


Fig. 34.-Osomotic pressure, vapor pressure, of sea water, relative to that of pure water, freezing point, and temperature of maximum density as functions of chlorinity and salinity.

TABLE 891.-PERCENTAGE OF RADIATION OF GIVEN WAVELENGTH TRANSMITTED BY 1 M OF WATER *

| Type of water | Wavelength ( $\mu$ ) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | . 46 | . 48 | . 515 | . 53 | . 565 | . 60 | . 66 |
| Pure water | 98.5 | 98.5 | 98.2 | 97.9 | 96.8 | 88.3 | 75.9 |
| [ highest | 96.4 | 97.5 | 96.6 | 96.3 | 92.9 | 81.8 |  |
| Oceanic water highest | 91.8 | 92.7 | 92.5 | 91.8 | 89.8 | 75.9 |  |
| average | 85.1 | 85.7 | 86.7 | 86.9 | 84.5 | 71.6 |  |
| ¢ average | 80.0 | 79.4 | 82.6 | 84.5 | . . | 68.7 | 62.0 |
| Coastal water lowest . |  | 71.6 | 75.9 | 76.4 |  | 64.6 | 53.6 |
| lowest . | 60.0 | 63.5 | 67.1 | 70.6 |  | 61.4 | 46.7 |

* For reference, see footnote 302, p. 773.


Fig. 35.-Extinction coefficients of radiation of different wavelengths in pure water and in different types of sea water.

## TABLE 892.-COMPOSITION OF SEA WATER*

The major ions present (over 99.9 percent of dissolved solids) are given in the table for $\mathrm{Cl}=19.00 \%$.

| Ion | \% $\%$ | Cl-ratio | Equiv/kg | Ion | \% $\%$ | Cl-ratio | Equiv/kg |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Cl}^{-}$ | 18.9799 | . 99894 | . 5353 | $\mathrm{Na}^{+}$ | 10.5561 | . 5556 | . 4590 |
| $\mathrm{SO}_{4}{ }^{-}$ | 2.6486 | . 1395 | . 0551 | $\mathrm{Mg}^{++}$ | 1.2720 | . 06695 | . 1046 |
| $\mathrm{HCO}_{3}{ }^{--}$ | . 1397 | . 00735 | . 0023 | $\mathrm{Ca}^{++}$ | . 4001 | . 02106 | . 0200 |
| $\mathrm{Br}^{-}$ | . 0646 | . 00340 | . 0008 | $\mathrm{K}^{+}$ | . 3800 | . 02000 | . 0097 |
| $\mathrm{F}^{-}$ | . 0013 | . 00007 | . 0001 | $\mathrm{Sr}^{++}$ | . 0133 | . 00070 | . 0003 |
| $\mathrm{H}_{3} \mathrm{BO}_{3}$ | . 0260 | . 00137 |  |  |  |  |  |
|  |  |  | . 5936 |  |  |  | . 5936 |

$$
\text { Salinity }=34.325 \% \text { Total solids }=34.48 \%
$$

The Cl -ratios are constants for oceanic waters except for $\mathrm{HCO}_{3}{ }^{--}$and $\mathrm{Ca}^{++}$which are affected by biological activity. Ratios are not valid in areas of river dilution.

* For reference, see footnote 302 , p. 773.


## TABLE 893.-GEOCHEMISTRY OF THE OCEANS

The oceans contain about $5 \times 10^{16}$ metric tons of dissolved solids. The amount in tons of any element can be estimated by multiplying the values in Table 894 by $1.42 \times 10^{12}$. Rivers each year add about $2.7 \times 10^{9}$ metric tons.

TABLE 894.-ELEMENTS PRESENT IN SOLUTION IN SEA WATER*
Elements present in solution in sea water in terms of $\mathrm{Cl}=19 \%$ are listed in order of abundance in the table. Adding the dissolved gases $\mathrm{H}_{2}, \mathrm{~N}_{2}, \mathrm{O}_{2}, \mathrm{He}$, and A, a total of some 49 elements are known to occur.

Ranges are indicated for $\mathrm{Si}, \mathrm{N}, \mathrm{P}, \mathrm{As}, \mathrm{Fe}, \mathrm{Mn}$, and Cu . The distribution of these elements, present in small quantities, is affected by biological activity. Lower values are usually near surface.

All atmospheric gases are found in the sea. Their solubility decreases with increasing temperature and salinity. At $0^{\circ} \mathrm{C}, \mathrm{Cl}=19 \%$, surface water contains $8.08 \mathrm{~m} / / l$ of $\mathrm{O}_{2}$ and $14.40 \mathrm{ml} / \mathrm{l}$ of $\mathrm{N}_{2}$. At $20^{\circ} \mathrm{C}$ corresponding values are 5.38 and 9.65 . Distribution of dissolved $\mathrm{N}_{2}$ is determined by temperatures and salinity. Oxygen at middepths is reduced, but only in the waters of isolated basins such as the Black Sea is there stagnation and $\mathrm{H}_{2} \mathrm{~S}$ present. Plant activity near the surface may increase $\mathrm{O}_{2}$ above saturation values. Carbon dioxide is present in large quantities (about $50 \mathrm{ml} / \mathrm{l}$ ) chiefly as $\mathrm{HCO}_{3}{ }^{-}$and $\mathrm{CO}_{3}{ }^{--}$ balanced against basic cations. Strong acid must be added to drive off all $\mathrm{CO}_{2}$. The pH in the sea varies between 7.4 and 8.4 depending upon the $\mathrm{O}_{2} \rightleftarrows \mathrm{CO}_{2}$ changes due to respiration or photosynthesis.
(Dissolved gases not included)

| Element | $c l=19.00 \%$ | Element | $\mathrm{Cl}=19.00 \%$ |
| :---: | :---: | :---: | :---: |
| Chlorine | . 18980 | Copper | . $001-.01$ |
| Sodium | 10561 | Zinc | . 005 |
| Magnesium | 1272 | Lead | . . 004 |
| Sulfur | 884 | Selenium | . . 004 |
| Calcium | 400 | Cesium | . . 002 |
| Potassium | 380 | Uranium | . . 0015 |
| Bromine | 65 | Molybdenum | . . 0005 |
| Carbon | 28 | Thorium | . . 0005 |
| Strontium | 13 | Cerium | . . 0004 |
| Boron | 4.6 | Silver | . . 0003 |
| Silicon | . $02-4.0$ | Vanadium | . . 0003 |
| Fluorine | 1.4 | Lanthanum | . . 0003 |
| Nitrogen ${ }^{\dagger}$ | . $01-.7$ | Yttrium | . . 0003 |
| Aluminum | . 5 | Nickel | . . 0001 |
| Rubidium | . 2 | Scandium | . . 00004 |
| Lithium |  | Mercury | . . 00003 |
| Phosphorus | . $001-.10$ | Gold | . 000006 |
| Barium | . 05 | Radium | . $2-3 \times 10^{-10}$ |
| Iodine | . 05 | Cadmium | . traces |
| Arsenic | . $01-.02$ | Chromium | . traces |
| Iron | .002-. 02 | Cobalt | traces |
| Manganese | . .001-. 01 | Tin | traces |

[^391]TABLE 895.-WAVE VELOCITY IN VERY SHALLOW WATER

| Denth <br> of water <br> feet | Speed <br> of wave <br> knots |
| :---: | :---: |
| 15 | 13 |
| 10 | 11 |
|  | 8 |

TABLE 896.-VELOCITY OF EARTHQUAKE WAVES WITH DEPTH OF WATER

| Depth in feet. . . . . . . . . . . . | 500 | 1,000 | 2,000 | 5,000 | 10,000 | 15,000 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Velocity in knots. . $\ldots \ldots \ldots \ldots$ | 70 | 100 | 150 | 240 | 340 | 420 |

If a large swell or an earthquake wave approaches a shoreline great damage may be done before the energy of the moving water is absorbed.

The permanent currents of the ocean are maintained by differential heat and cooling and by the indirect effects of the wind. They may extend to depths as great as $1,000 \mathrm{~m}$ and their speed is usually less than $50 \mathrm{~cm} / \mathrm{sec}$. In the Gulf Stream and Kuroshio, speeds may exceed $250 \mathrm{~cm} / \mathrm{sec}$. Volume transparents of the large current systems exceed 50 million tons $/ \mathrm{sec}$.

Wind-driven currents induced by the drag of the wind are generally shallow, less than 100 m , flow with speeds about 2 percent of wind, and deviate about $30^{\circ}$ from the wind direction, to the right in the Northern Hemisphere and to the left in the Southern Hemisphere.

Tidal currents follow elliptical orbits during each tidal cycle. Motion probably extends to the bottom. In restricted coastal channels the currents are reversing and sometimes exceed $250 \mathrm{~cm} / \mathrm{sec}$.
WAVES AT SEA *

Whenever the wind blows over the water, the surface is formed into waves which grow under the influence of the wind and form a most irregular surface known as a sea. Such waves traveling out from a storm area are called swells. As waves break near the shore surfs are formed.

Waves may also be formed by earthquakes, fault movements, submarine landslides, or volcanic eruptions beneath the sea.
The height of a wave, $H$, is the vertical distance from crest to trough. The length, $L$, is the horizontal distance between adjacent crests. The wave period, $P$, is the time interval between passage of successive crests at a fixed point. The velocity, $V$, of a wave is the speed with which the wave travels along the sea surface.

The following relations hold for depths greater than one-quarter wavelength with good approximation:

$$
L=5 P^{2}, V=3 P
$$

where the wavelength, $L$, is in feet, the period, $P$, in seconds, and the velocity, $V$, in knots. The waves move along the surface of the water but the water, on the other hand, advances very little-about one percent only of the wave velocity.

The height of the sea is determined by three factors:
Wind velocity, average speed of wind over fetch.
Fetch, distance over wind blows.
Wind duration, how long the wind blows.
Tables 886 and 898 show the wave heights for some conditions.

[^392]TABLE 898.-WAVE HEIGHT IN FEET FOR VARIOUS WIND VELOCITIES AND FETCHES

| Fetch in <br> nautical <br> miles | $\overbrace{10}^{5}$ | 20 | 30 | 40 | 50 | 60 |
| :---: | :---: | ---: | ---: | ---: | ---: | ---: |
| 10 | 2 | 3 | 5 | 7 | 9 | 10 |
| 20 | 2 | 4 | 7 | 9 | 12 | 14 |
| 50 | 2 | 6 | 10 | 14 | 18 | 22 |
| 100 | 2 | 7 | 13 | 17 | 25 | 30 |
| 500 | 2 | 10 | 20 | 31 | 45 | 55 |
| 1000 | 2 | 10 | 21 | 35 | 50 | 70 |

(See also Tables 886, 887, and 895.)
(Nat. Res. Council Bull. 78, 1931.)
Spring tides.-When moon (new or full) is in line with sun (large tide).
Neap tide. -When moon is in quadrature with sun (small tide).
Generally two high and two low each day. Variation in heights of two high and two low $=$ "diurnal inequality."

River-type tide, steep short-period graph for flood, more inclined and longer for ebb. Extreme case = "bore", tide rises so rapidly it assumes form of wall several feet high. Most famous bores, Tsientang Kiang, China; Turnagain Arm, Alaska; Severn and the Wye, England; Seine in France; Hoogly, India; Petitcodiac, Canada.
Mean sea level (geodetic).-The equipotential surface which the oceans woud assume if undisturbed by the tides and effects of wind and weather. Starting with mean sea level at any given initial point the geodesist can determine by precise spirit leveling, the equipotential surface.
Mean sea level (geographic).-Determined by averaging actual tidal heights over a sufficient period. It is a local or geographic value. It is much disturbed by prevalent winds and local contours. Note difference between average of hourly readings (mean sea level) and half-tide point (because of the shape of the tide height as related to time). On Atlantic coast $\frac{1}{2}$ tide level lies below mcan by about $1 / 10 \mathrm{ft}$ : on Pacific above by $1 / 20 \mathrm{ft}$. Mean tide near rivers varies with rainfall. Nineteen years' observation used for full tide cycle. A fundamental level net has been connected with mean sea level at Portland, Me., via Boston, Mass., Ft. Hamilton, N. Y., Sandy Hook and Atlantic City, N. J., Old Point Comfort and Norfolk, Va., Brunswick, Ga., Fernandina, St. Augustine, and Cedar Keys, Fla., Biloxi, Miss., Galveston, Tex., San Diego, San Pedro, San Francisco, Calif., Ft. Stevens, Oreg., and Seattle, Wash. The accuracy of high precision leveling is measured by the correction necessary to close circuits, about 0.00063 foot/mile. Mean sea level difference indicated by special adjustment of leveling network in 1929: Portland, Maine, 9 cm higher than Ft. Hamilton; Vancouver, 2 cm higher than Seattle; Galveston, 27 cm higher than St. Augustine; San Diego, 33 cm higher than Galveston; Fort Stevens, 26 cm higher than San Diego; Isthmus of Panama, Pacific coast, 20 cm higher than Atlantic; Death Valley, 280 ft ( 84.1 ) below sea level ; Mount Whitney, $14,495 \mathrm{ft}(4418.1 \mathrm{~m}$ ) above.

From observations, Spencer Jones (Monthly Notices, Roy. Astron. Soc., vol. 99, p. 541, 1939) deduces as the best value of the apparent solar acceleration $2.5^{\prime \prime} /$ (century) ${ }^{2}$. Lunar theory predicts $12.0^{\prime \prime} /$ (century $)^{2}$ leaving part attributable to tidal friction $10^{\prime \prime \prime}$ ( century) ${ }^{2}$.
Estimates of tidal friction losses (Jeffreys, Philos. Trans., A, vol. 221, p. 239, 1920) :


Other contributions are small. Total for spring tides $22 \times 10^{18} \mathrm{erg} / \mathrm{sec} .1 .1 \times 10^{20} \mathrm{erg} / \mathrm{sec}$ average, corresponding to about $7^{\prime \prime}$ secular acceleration per century per century. If $\Omega$ is earth's angular velocity of rotation, $d \Omega / d t=-2.5 \times 10^{-22} / \mathrm{sec}^{2} . \Omega=7.3 \times 10^{-5} \mathrm{rad} . / \mathrm{sec}$. $\Omega$ changes by $10^{-5}$ of its amount in $3 \times 10^{12} \mathrm{sec}$ or $10^{5}$ years. The day should have lengthened by 1 sec in 120,000 years.

The fluctuations in the earth's rate of rotation indicated by astronomical evidence are of a quite greater order of magnitude. Moreover the changes vary in sign whereas frictional effects should not. The observations come from deviations of the sun and moon from their gravitational orbits, the transits of Mercury, and eclipses of Jupiter's satellites. Changes in the speed of rotation of the earth rotation seem the only explanation. This may be due to shifts of matter within or on the earth. The following figure by Brown indicates that in 1928 the earth was about 25 sec ahead of its average rotational motion during the last three centuries. The greatest apparent change in the loss or gain of one sec in a whole year. (1 part in $30,000,000$.)


Fig. 36.-Irregularities in the earth's rotation derived from the moon's motions.

Tidal friction should make the earth rotate more slowly and the moon recede from the earth. The rate of dissipation of energy by friction is about $1.4 \times 10^{18} \mathrm{erg} / \mathrm{sec}$. The earth's rotation from this cause should have slowed by 4 hours during geologic time. The moon should continue to recede until its period of revolution and that of the earth's rotation are equal to 47 of our present days. The moon should then gradually approach the earth, ultimately coming within Roche's limit (about twice the earth's radius) breaking up possibly into a ring like Saturn's.

[^393]| Area (See Tables 31-33) |  |  | Density |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Multiply | by | to obtain | Multiply | by | to obtain |
| acre | 40.47 | are | $\mathrm{g} / \mathrm{ft}^{\text {3 }}$ | 35.31 | $\mathrm{g} / \mathrm{m}^{3}$ |
|  | $1.60 \times 10^{2}$ | $\mathrm{rod}^{2}$ | $\mathrm{g} / \mathrm{liter}$ | $8.345 \times 10^{-8}$ | lb/gal |
|  | $4.356 \times 10^{4}$ | $\mathrm{ft}^{2}{ }^{2}$ | $\mathrm{g} / \mathrm{cm}^{3}$ | 62.43 | $\mathrm{lb} / \mathrm{ft}^{3}$ |
| are | $10^{2}$ | $\mathrm{m}^{2}$ | $\mathrm{g} / \mathrm{cm}^{3}$ | 1.94 | slug/ $\mathrm{ft}^{\text {8 }}$ |
| cir mils | $5.067 \times 10^{-6}$ | $\mathrm{cm}^{2}$ | $\mathrm{lb} / 1000 \mathrm{ft}^{8}$ | 1.602 | $\mathrm{kg} / 100 \mathrm{~m}^{3}$ |
| $\mathrm{ft}^{2}$ | $9.290 \times 10^{2}$ | $\mathrm{cm}^{2}$ | $\mathrm{lb} / \mathrm{ft}^{8}$ | $1.602 \times 10^{-2}$ | $\mathrm{g} / \mathrm{cm}^{3}$ |
| in. ${ }^{3}$ | 6.452 | $\mathrm{cm}^{2}$ | $\mathrm{lb} / \mathrm{in}^{\text {. }}$ | 27.68 | $\mathrm{g} / \mathrm{cm}^{8}$ |
| Capacity units (See Tables 31-33) |  |  | siug/ft ${ }^{3}$ | $32.17{ }^{.} 5153$ | $\begin{aligned} & \mathrm{g} / \mathrm{cm}^{2} \\ & \mathrm{lb} / \mathrm{ft}^{3} \end{aligned}$ |
| barrel | 31.5 | gal |  | Electrical units (See Tables 6-8) |  |
| bushei | 1.244 | $\mathrm{ft}^{3}$ |  |  |  |
|  | $2.1504 \times 10^{3}$ | in. ${ }^{3}$ | amu |  | $\mathrm{Mev}$ |
|  | $3.524 \times 10^{-2}$ | $\mathrm{m}^{3}$ |  | $1.492 \times 10^{-8}$ | ergs |
|  | 4 64 | pecks pt (dry) |  | Energy units (See Tables 7, |  |
|  | 32 | qt (dry) | cal | $4.185 \times 10^{7}$ |  |
| chaldrons (U.S., dry) | 36 | bu | erg | $9.4801 \times 10^{-11}$ $2.389 \times 10^{-8}$ | Btu* ${ }_{\text {cal }}{ }^{\text {a }}$ |
| firkin | 9 | gal |  | $1.0197 \times 10^{-8}$ | g-cm |
| $\mathrm{ft}^{3}$ | 7.48 | gal |  | $7.376 \times 10^{-8}$ | ft-lbs |
| $\mathrm{ft}^{\text {² }}$ | 28.32 | liter |  | $2.373 \times 10^{-6}$ | ft-poundals |
| gallon | $3.7854 \times 10^{3}$ | $\mathrm{cm}^{3}$ |  | $6.24 \times 10^{5}$ | Mev |
|  | .1337 | $\mathrm{ft}^{3}$, | electron-volt <br> $\mathrm{ft}^{3}$-atm <br> ft-lb | $1.602 \times 10^{-12}$ | erg |
|  | $2.31 \times 10^{2}$ | in. ${ }^{3}$ |  | 28.32 | liter-atm |
|  | 3.7853 | liter |  | $1.356 \times 10^{7}$ | ergs |
|  | 8 | pt (liquid) |  | $3.766 \times 10^{-7}$ | kw-hr |
|  | 4 | qt (liquid) |  | ${ }_{32} .3238$ | cal |
| hogsheads | 8.423 | $\mathrm{ft}^{3}$ |  | 32.17 - ${ }^{-3}$ | ft-poundal |
|  | ${ }^{63} 1.000028 \times 10^{3}$ | $\mathrm{gal}^{3}$ | ft-poundal | $1.285 \times 10^{-3}$ | Btu |
| $l \mathrm{liter}{ }_{\text {l }} \mathrm{H}$ of $\mathrm{H}_{2} \mathrm{O}$ | $1.000028 \times 10^{3}$ | $\mathrm{cm}^{3}$ |  | $4.214 \times 10^{5}$ | ergs |
| lb of $\mathrm{H}_{2} \mathrm{O}$ | $1.602 \times 10^{-2}$ | $\mathrm{ft}^{3}$ of $\mathrm{H}_{2} \mathrm{O}$ |  | $3.108 \times 10^{-2}$ | $\mathrm{ft}-1 \mathrm{~b}$ |
|  | 27.72 | in. ${ }^{3}$ of $\mathrm{H}_{2} \mathrm{O}$ | g-cm | $9.806 \times 10^{2}$ | erg |
| pt (liquid) | 28.88 | in. ${ }^{\text {gal }}$ | hp-hr | $2.545 \times 10^{3}$ | Btu Btal |
| qt (dry) | 67.20 | in. ${ }^{3}$ |  | $6.413 \times 10^{2}$ | kg-cal |
| qt (liquid) | 57.75 | in. ${ }^{3}$ |  | . 7457 | kw-hrs |
|  | 1.164 | qt (dry) |  |  |  |

* In this table the calorie $=4.185$ joules and the Btu $=252$ calorics $($ See Table 7).
TABLE 901.-GENERAL CONVERSION FACTORS (continued)


| Energy units (continued) |  |  |
| :---: | :---: | :---: |
| Multiply | by | to obtain |
| joule | $10^{7}$ | ergs |
|  | $9.482 \times 10^{-4}$ | Btu |
|  | 23.73 | ft-poundals |
|  | . 7376 | ft -lbs |
|  | $3.021 \times 10^{18}$ | quanta ( $\lambda=.6 \mu$ ) |
| kg -cm | $9.807 \times 10^{5}$ | ergs |
| kw-hr | $7.233 \times 10^{-2}$ | $\mathrm{ft}-1 \mathrm{~b}$ |
|  | $3.6 \times 10^{6}$ | joule |
|  | $3.414 \times 10^{3}$ | Btu |
|  | $8.602 \times 10^{5}$ | cal |
| Mev <br> pound-foot poundal-foot quantum ( $\lambda=.6 \mu$ ) | $1.602 \times 10^{-6}$ | ergs |
|  | $1.3553 \times 10^{7}$ | ergs |
|  | $4.2130 \times 10^{5}$ | ergs |
|  | $3.310 \times 10^{-12}$ | ergs |
| Energy flow (See Tables 129-130) |  |  |
| $\mathrm{ft}^{3} / \mathrm{min}$ | Flow |  |
|  | $4.720 \times 10^{2}$ | $\mathrm{cm}^{3} / \mathrm{sec}$ |
|  | . 1247 | $\mathrm{gal} / \mathrm{sec}$ |
|  | . 47200 | liter/sec |
| $\mathrm{gal} / \mathrm{min}$ | $2.228 \times 10^{-3}$ | $\mathrm{ft}^{3} / \mathrm{sec}$ |
| liter/min | $5.885 \times 10^{-4}$ | $\mathrm{ft}^{3} / \mathrm{sec}$ |
|  | $4.403 \times 10^{-3}$ | gal/sec |
| dyne | Force |  |
|  | $7.233 \times 10^{-5}$ | poundal |
|  | $2.248 \times 10^{-6}$ | poundweight |
|  | $1.0197 \times 10^{-6}$ | kg weight |
| newton $\dagger$ <br> pound (see lb) | $10^{5}$ | dyne |
| poundal | $1.3827 \times 10^{4}$ | dyne |
| pound (weight) | $4.448 \times 10^{5}$ | dyne |
| gram (weight) | $9.81 \times 10^{2}$ | dyne |
| grav (gal) | Gravitational |  |
|  | $9.80665 \times 10^{2}$ | $\mathrm{cm} / \mathrm{sec}^{2}$ |
|  | 32.174 | $\mathrm{ft} / \mathrm{sec}^{2}$ |

$\dagger$ The unit of force in the MKS system.
TABLE 901.-GENERAL CONVERSION FACTORS (continued)
(U)


|  | กั๊ | \% | $\underset{\text { E }}{\underset{E}{\sim}}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |

Metric system prefixes (continucd)
(continucd)
to obtain
by
.01
.1
10
$1.00 \times 10^{2}$
$1.00 \times 10^{3}$
$1.00 \times 10^{4}$
$1.00 \times 10^{6}$
Paper measure
$5.00 \times 10^{2}$
Photometric units (See Tables 66 and $69-74$ )
Multiply
centi
deci
deka
hecto
kilo
myra
$\ldots$.
mega reams $_{\text {Btu/min }}^{\text {cal/min }} \begin{aligned} & \text { ft-lb/sec } \\ & \text { hp } \\ & \text { hp } \\ & \text { kw } \\ & \text { atm }\end{aligned}$

$\underset{\mathrm{Btu} / \mathrm{ft}^{3}}{\mathrm{Btu} / \mathrm{lb}}$ 정
等
year ${ }^{8}$ day
$\mathrm{kg} / \mathrm{m}^{2}$
$\mathrm{~kg} / \mathrm{cm}^{2}$
$\mathrm{kips} / \mathrm{in}^{2}{ }^{2}$
$\mathrm{lb} / \mathrm{ft}^{2}$
$\mathrm{lb} / \mathrm{in}^{2}{ }^{2}$
mmHg

$$
\begin{aligned}
& \text { It of wa } \\
& \mathrm{kg} / \mathrm{m}^{2} \\
& \mathrm{lb} / \mathrm{ft}^{2}
\end{aligned}
$$

$$
\begin{aligned}
& \text { to obtain } \\
& \text { grains } \\
& \mathrm{kg} \\
& \mathrm{mg} \\
& \mathrm{oz} \\
& \mathrm{lb} \\
& \mathrm{lb} \\
& \text { grains } \\
& \mathrm{g} \\
& \mathrm{oz} \\
& \mathrm{lb} \text { (av) } \\
& \text { gee lb } \\
& \mathrm{lb} \\
& \mathrm{~g}
\end{aligned}
$$

$$
\begin{aligned}
& \mathrm{m}^{3} \text { of gas } / 100 \mathrm{~kg} \\
& \mathrm{lb} .
\end{aligned}
$$

4
n

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[^0]:    ${ }^{1}$ Because of its greater psychological and physical simplicity, and the desirability that the unit chosen should have extensive magnitude, it has been proposed to choose as the fourth fundamental quantity a quantity of electrical charge, $e$. The standard units of electrical charge would then be the electronic charge. For thermal needs, entropy has been proposed. While not generally so psychologically easy to grasp as temperature, entropy is of fundamental importance in thermodynamics and has extensive magnitude. (Tolman, R. C., The measurable quantities of physics, Phys. Rev., vol. 9, p. 237, 1917.)

[^1]:    ${ }^{2}$ Buckingham, E., Phys. Rev., vol. 4, p. 345, 1914 ; also Philos. Mag., vol. 42, p. 696, 1921.
    ${ }^{3}$ Philos. Mag., ser. 4, vol. 41, p. 107, 1871. See also Robertson, Dimensional analysis, Gen. Electr. Rev., vol. 33, p. 207, 1930.

[^2]:    ${ }^{4}$ For dimensional formula see Table 30, part 2.
    4a Some writers have used this term for 1 dyne $/ \mathrm{cm}^{2}$.

[^3]:    ${ }^{6}$ Gen. Electr. Rev., vol. 47, p. 26, 1944.

[^4]:    ${ }^{8}$ Circular 60 of the National Bureau of Standards, Electric Units and Standards, 1916. The subsequent matter in this introduction is based upon this circular.
    ${ }^{9}$ For example, A. G. Webster, Theory of electricity and magnetism, 1897; J. H. Jeans, Electricity and magnetism, 1911; H. A. Lorentz, The theory of electrons, 1909; and O. W. Richardson, The electron theory of matter, 1914.

[^5]:    ${ }^{10}$ There was, however, some slight error in these values that had to be taken into account for accurate work. (See Table 5.)

[^6]:    12 Nat. Bur. Standards Circ. C-459, 1947.

[^7]:    *Where 3 occurs it is to be taken as 2.99776 (from velocity of light). Where 9 occurs (not as an exponent), it is the square of this number.

[^8]:    * Arlapterl from National Bureau of Standards Tables.
    $\ddagger$ Is defined for International Steam Tables.
    § init atomic weight energy equivalent.

[^9]:    *This table is now superseded by the adoption of the new system of electrical units in January 1948 and is given for reference only.

[^10]:    *Taken from B. O. Peirce's Short table of integrals, Ginn \& Co.

[^11]:    * Prepared by the late A. G. Worthing. of the C'niversity of Pittsurgh.

[^12]:    ${ }^{13}$ Worthing, A. G., and Geffner, J., Treatment of experimental data, p. 259, John Wiley and Sons, New York, 1943. Used by permission.

[^13]:    ${ }^{14}$ Birge, R. T., and Shea, J. D., Univ. California Publ. Math., vol. 2, p. 67, 1921 ; Worthing, A. G., and Geffner, J., Treatment of experimental data, p. 250, John Wiley and Sons, New York, 1943.
    ${ }^{15}$ Baily, J. L., Ann. Math. Statistics, vol. 2, p. 355, 1931.
    ${ }^{16}$ Cox, G. C., and Matuschak, Margaret, Journ. Phys. Chem., vol. 45, p. 362, 1941.

[^14]:    ${ }^{17}$ Phys. Rev. Suppl., vol. 1, p. 1, 1929 ; Rev. Mod. Phys., vol. 13, p. 233, 1941 ; Amer. Journ. Phys., vol. 13, p. 63, 1945.

    18 Phys. Rev., vol. 58, p. 457, 1940; Rev. Mod. Phys., vol. 20, p. 82, 1948.
    ${ }^{18:}$ Bearden, J. A., and Watts, H. M., Phys. Rev., vol. 81, p. 73, 1951.
    ${ }^{18}$ bearden, Earle, Minkowski, and Thomsen, private communication from J. A. Bearden.

[^15]:    * Unless otherwise specified, all quantities in this table that involve the mol or the gram equivalent are on the chemical scale of atomic weights.

[^16]:    ** $J_{\lambda}$ may be defined in several ways and this determines the value of $c_{1}$. If $J_{\lambda} d \lambda$ gives the energy density of unpolarized radiation in range $d \lambda$, then $c_{1}=8 \pi h c$. If $J_{\lambda} d \lambda$ gives the emission of linearly polarized light, in range $d \lambda$ per unit solid angles perpendicular to the surface, then $c_{1}=h c^{2}$. If this expression $J_{\lambda} d \lambda$ denotes the emission of radiation in range $d \lambda$, per unit surface from one side in all directions ( $2 \pi$ solid angle) then $c_{2}=2 \pi h c^{2}$. See Table 53.

    + For $2 \pi$ solid angle.

[^17]:    : The binding energy of the electron in the hydrogen atom has been included in the quantity. The mass of the electron when found in the hydrogen atom is not $m$ but more correctly $m\left(1-1 / 2 a^{2}+\cdots\right)$.

[^18]:    ${ }^{\mathrm{b}}$ The numerical constant 4.96511423 is the root of the transcendental equation $x=5\left(1-c^{-x}\right)$.

[^19]:    c These formulas apply only to non-relativistic velocities. If the velocity of the particle is not negligible compared to the velocity of light, $c$, or the energy not negligible compared to the rest mass energy, we must use $\lambda_{D}=\lambda_{c}[\epsilon(\epsilon+2)]^{-1 / 2}$ where $\lambda_{c}$ is the appropriate Compton wavelength and $\epsilon$ is the kinetic energy measured in units of the particle rest mass.

[^20]:    * For reference, see footnote 18a, p. 46.
    $\dagger$ Private communication by J. A. Bearden. Data presented at May 1953 meeting of Physical Society at Washington by Bearden, Earle, Minkowski, Thomsen, Johns Hopkins University.

[^21]:    * For these formulæ the numbers in the last column are the exponents of $F$ where $F$ refers to the luminous Hux. For definitions of these quantities see Tables 70 and 72.

[^22]:    * As adopted by Imerican Institute of Electrical Engineers, 1915.
    $+c$ is the velocity of an electromagnetic wave in the ether $=3 \times 10^{10}$ approximately.
    $\ddagger$ This conversion factor should include $\left[A^{-1}\right]$.

[^23]:    * Quoted from sheets issued by the National Bureau of Standards.

[^24]:    ${ }^{10}$ Taken from Circular 47 of the National Bureau of Standards, 1915, which see for more complete tables. .

[^25]:    * In accordance with the schedule adopted under the Weights and Measures (metric system) Act, 1897.

[^26]:    ${ }_{21} 20$ Nat. Bur. Standards Journ. Res., vol. 42, p. 209, 1949.
    ${ }^{21}$ The General Conference, held in October 1948, decided to discontinue the use of the words "Centesimal" and "Centigrade" and to replace them by "Celsius." See also Nat. Bur. Standards Techn. News Bull., vol. 33, p. 110, 1949.
    *See footnote 5a, p. 7.

[^27]:    ${ }^{22 a}$ Bull. Nat. Bur. Standards, vol. 8, p. 239, 1912.

[^28]:    * These values are now superseded by the introduction of the 1948 International Temperature Scale and are given for reference only.
    ${ }^{23}$ Taken from Nat. Bur. Standards Res. Papers RP 1080, RP 767, and RP 530.

[^29]:    * Hoskins Thermocouple.

[^30]:    ${ }^{23 a}$ Rev. Sci. Instr., vol. 7, p. 322, 1936. "These terms apply only to a source. The term "radiance" is not recommended as a substitute for radiant flux; however, if a single term is desired to express the radiant flux from a source, the word "radiance" is suggested as the most logical. † See footnote 5a, p. ${ }^{7}$
    ${ }^{24}$ For a more extensive list of values of $J_{\lambda}$ reference sbould be made to two papers by Parry Moon: Journ. Math. and Phys., vol. 16, p. 133, 1937; Publ. Electr. Eng., Massachusetts Institute of Technology, 1947.

[^31]:    * Energy radiated from $3000^{\circ} \mathrm{K}$ can be obtained from the value for this temperature by multiplying it by $10^{4}$. Likewise for other temperatures that are 10 times the
    values given in the table.

[^32]:    *For reference, see footnote 23, p. 74.

[^33]:    ${ }^{25}$ Blanchard, Phys. Rev., vol. 11, 1. 81, 1918; Stiles and Crawford, Proc. Roy. Soc. London, ser. B, vol. 112, p. 428, 1933 ; Lowry, Journ. Opt. Soc. Amer., vol. 18, p. 29, 1929.

[^34]:    ${ }^{25}$ I.E.S. Nomenclature and photometric standards, American Standards Association. ASA C.42. 1941.

[^35]:    ** For reference, see foot note 25, p. 87.

    * The field brightnesses are values ohtained hy mechanically increasing or reducing values measured at photopic levels. † Taken from smooth curve drawn through Blanchard's data. The unit will depend upon definition. As these figures stand they are brightnesses for this radiation measured at photopic levels and reduced mechanically to values given. $\ddagger$ For radiation from a source at a color temperature of $2680{ }^{\circ} \mathrm{K}$. § This is the ratio of the eye sensitivity to that of the eye adapted to the next lower (one-tenth) field brightness for this radiation. \| Minimum threshold from Taylor's value.

[^36]:    ${ }^{28}$ Judd, D. B., Journ. Opt. Soc. Amer., vol. 23, p. 359, 1933.

[^37]:    * The lumens within a unit solid angle around the normal from a plane blackbody is equal to 0.92 times the normal intensity.

[^38]:    1 candle per $\mathrm{ft}^{2}{ }^{2}=3.142$ foot-lamberts.
    1 stilb $=1$ candle per $\mathrm{cm}^{2}$
    1 apostilb $=0.1$ millilambert.

[^39]:    so Wensel, Roeser, Barbrow, and Caldwell, Nat. Bur. Standards Journ. Res., vol. 6, p. 1103, 1931.
    ${ }^{31}$ Nat. Bur. Standards Circ. C.459, 1947.

[^40]:    32 Weaver, K. S., Journ. Opt. Soc. Amer., vol. 38, p. 278. 1949; vol. 40, p. 60, 1950.
    ${ }^{39}$ Terrien, Journ. Opt. Soc. Amer., vol. 39, p. 888, 1949.

    * Platinum point.

[^41]:    * Calculated, $\sigma=5.6724 \times 10^{-12}$, watts $\mathrm{cm}^{-2} \mathrm{deg}^{-4}$.
    $\dagger$ Brightness, Waidner-Burgess standard. See Table 69.

[^42]:    ${ }^{\text {s }}$ Worthing, A. G., Tenperature radiation emissivities and emittances, Temperature, Its Measurement and Control, p. 1184, Reinhold Publishing Co., 1941.

[^43]:    ${ }^{\text {st }}$ Private communication from Wahlin, taken from data by Wahlin and Knop, L. V. Whitney, Wahlin and Wright, Worthing, Fiske, Phys. Rev.

[^44]:    * The values given in this table also give the correction for a window having a transmission given in column 1 for different temperatures of the source when this window is used between the source and the pyrometer.

[^45]:    ${ }^{3}$ Barnes, B. T., Forsythe, W. E., and Adams, E. Q. Journ. Opt. Soc. Amer., vol. 37, p. 804, 1947.

    * Assuming no radiation transmitted through sample from heater and no temperature gradient.
    $\dagger$ Assuming all of sample at heater temperature. $\ddagger$ Between front and hack surfaces.

[^46]:    * As observed with total radiation pyrometer sighted on the platinum.

[^47]:    * Data furnished by W. W. Lozier of National Carbon Co. $\dagger$ All direct-current power. $\ddagger$ "National" white fiame photographic carbons, rare earth cored. \& "National" 2 F carbon, neutral cored.

[^48]:    ${ }^{42}$ Forsythe, W. E., and Adams, E. Q., Bull. Denison Sci. Lab., vol. 32, p. 70, 1937.

[^49]:    * Data furnished by W. E. Forsvthe and E. M. Watson, of the General Electric Co. t These values furnished by W. H. Fisher, Nela Park. $\ddagger$ Vacuum lamps, all others are gas-filled. \& Temperature at junction of base and bulb. II Area of coil in $\mathrm{mm}^{2}$. II Candlepower in direction used. - Color temperature.

[^50]:    * Data furnished by H. C. Froelich, of Nela Park. $\dagger 2200$ A was lower limit of measurements.

[^51]:    
    A, $120^{\circ}$ cylindrical shield to side of filament. B, Hemispherical shield in front of filament masking all direct light. C, $90^{\circ}$ spherical shield in front of filament
    masking all upward direct light. masking all upward direct light.

[^52]:    Note.-Rated lives of black-light and general-lighting lamps listed above are based on specified test conditions with the lamps turned off and restarted no of tener than
     ife of the A-H5 is 5,000 hours, and the $\mathrm{E}-\mathrm{Hi} 4,000$ hours. If the $\mathrm{A}-\mathrm{H} 9$ lamp is started once every base down.

    * Prepared by C. L. Amick, General Electric Co., Nela Park.

[^53]:    ＊Data taken from reports by General Electric Lamp Department and from reports by Sylvania Electric Products．$\quad$ Add auxiliary watts for total．$\ddagger$ Nominal length includes the lamp and two standard lamp－ holders．\＆Approximate．｜｜See Table 96.

[^54]:    ＊The data given for the light and time characteristics and for the color temperature of the lamps are average values for a large number of lamps．Individual lamps may differ considerably from these averages．Prepared by Adelaide Easley，General Electric Lamp Division．$\dagger$ Milliseconds．$\ddagger \times 10^{3}$ ．$\& \times 10^{6}$ ．

[^55]:    * Data furnished by L. R. Benjamin, General Electric Co., Nela Park, Cleveland, Ohio. t With approximately 0.5 millihenry of inductance in series with each 100 microfarads of capacity. $\ddagger$ Data taken from circular of Amglo Corporation, Chicago, Ill.

[^56]:    * See Table 80.

[^57]:    * Computed with $\sigma=5.32$, blackbody efficiency of platinum as follows (Lummer and Kurlbaum): $492^{\circ} \mathrm{K}, .039 ; 654^{\circ}, .060 ; 795^{\circ}, .075 ; 1108^{\circ}, .112 ; 1481^{\circ}, .154 ; 1761^{\circ} \mathrm{K}, .180 . \quad \dagger$ Weighted mean.

[^58]:    ${ }^{45}$ Bridgman, P. W., Proc. Amer. Acad. Arts and Sci., vol. 70, p. 25, 1935.

[^59]:    ${ }^{44}$ Bridgman, P. W., Journ. Phys. Chem., vol. 9, p. 795, 1941.

    * Second modification of the solid.

[^60]:    *Prepared by F. C. Kracek, Geophysical Laboratory, Carnegie Institution of Washington. $\dagger$ Decomposes. $\ddagger$ At 2.5 atm pressure. $\delta$ At 5.2 atm pressure.

[^61]:    || At 10.5 mmHg pressure.

[^62]:    * See Table 201.

[^63]:    * Arranged by F. C. Kracek, Geophysical Laboratory, Carnegie Institution. All other footnotes at end of table.

[^64]:    $\ddagger$ Third modification at room temperature. $\ddagger$ Acetone. § Five cther modifications; not accurately located. $\quad$ Very heautiful for demonstration purnoses. a Leucite. $b$ Prohably pentamorphic, inv. at $1150^{\circ}$ and $1300^{\circ} \mathrm{C}$. $\quad$ Acetate. $\quad d$ Sluggish. $e$ Quartz. $f$ Cristobalite. $g$ Zincblende and wurtzite. $h$ Tridymite.

[^65]:    ＊The majority of these determinations are by G．A．Rankin．
    $\dagger$ The accuracy of the melting points is 5 to 10 units．（Geophysical Laboratory．）

[^66]:    * Lowest temperature obtained.

[^67]:    * Copper: $100-197^{\circ} \mathrm{C}, k_{t}=1.043 ; 100-268^{\circ}, 0.969 ; 100-370^{\circ}, 0.931 ; 100-541^{\circ}, 0.902$.
    $\dagger$ Iron: $100-727^{\circ} \mathrm{C}, k_{t}=0.202 ; 100-912^{\circ}, 0^{\prime} .184 ; 100.1245^{\circ}, 0.191$.

[^68]:    * Compiled from the International Critical Tables, which see for more complete data.

[^69]:    ${ }^{46}$ Griffiths, E., Journ. Inst. Fuel, vol. 15, p. 111, 1942.

[^70]:    * Air: $k_{n}=5.22\left(10^{-5}\right) \mathrm{cal} \mathrm{cm}^{-1} \mathrm{sec}^{-1} \mathrm{deg} \mathrm{C}^{-1} ; 5.74$ at $22^{\circ}$; temp. coef. $=.0029$.

[^71]:    47 Bridgman, P. W., Proc. Amer. Acad. Arts and Sci., vol. 59, p. 158, 1923

    * $1.2,6,8,12,13$, extreme purity ; $3,4,5,7,9,10,11$, very pure; 14,15 , commercial.
    $\dagger$ Toluol freezes at $9900 \mathrm{~kg} / \mathrm{cm}^{2}$ at $30^{\circ}$. The figure at 11000 is for the solid.

[^72]:    ${ }^{48}$ Harper, D. R., Journ. Washington Acad. Sci., vol. 18, p. 469, 1928.

    * Substances marked with the asterisk vary widely in thermal conductivity according to composition. For limits of such variation, consult International Critical Tables, vol. 2. The figure listed above for any such material represents the author's estimate of the "best guess" for use in those cases where the composition of the material is not specified.

    In preparing this table, the author has consulted vol. 2, I.C.T. For still other materials, grateful acknowledgment is made to the staff of the National Bureau of Standards for advice in selecting most probable values in the light of present information.

[^73]:    *Compiled by Peter Hidnert and H. S. Krider, of the National Bureau of Standards.
    $\dagger$ The coefficient of cubical expansion of an isotropic solid element may be taken as 3 times the coefficient of linear expansion within a high degree of approximation (See Part 3 for determined coefficients of cubical expansion of some chemical elements.)
    **Numbers refer to authorities given at end of table.
    $\ddagger$ The coefficients of expansion depend upon the orientation of the constituent crystals.
    § The coefficients of expansion depend upon coarseness of grains and treatment of metal.

[^74]:    Compiled by Peter Hidnert and H. S. Krider, National Bureau of Standards.
    $\ddagger$ Chemical composition is given in percent by weight. $\ddagger$ Coefficient of expansion varies with coms. position and treatment. ** Numbers refer to authorities given at end of table.

[^75]:    $\S$ Composition of Kanthal: A: 68.5 Fe, 23.4 Cr, $6.2 \mathrm{Al}, 1.9 \mathrm{Co}, 0.06 \mathrm{C}$; A-1: $69.0 \mathrm{Fe}, 23.4 \mathrm{Cr}, 5.7 \mathrm{Al}$, $1.9 \mathrm{Co}, 0.06 \mathrm{C}$; $\mathrm{D}: 70.9 \mathrm{Fe}, 22.6 \mathrm{Cr}, 4.5 \mathrm{Ai}, 2.0 \mathrm{Co}, 0.09 \mathrm{C}$.
    (continued)

[^76]:    *Compiled hy Peter Hidnert and H. S. Krider, National Bureau of Standards. "* Numbers refer to authorities given helow. $\ddagger$ With load of $30 \mathrm{lh} / \mathrm{in}^{2}{ }^{2} \ddagger$ includes terms "ebonite" and "vulcanite." \& Vari-

[^77]:    * Allotropic heat of transformation: $\mathrm{Mn}, 1070-1130^{\circ} ; \mathrm{Ni}, 320-330^{\circ} ; \mathrm{Co}, 950-1100^{\circ} ; \mathrm{Fe}, 725-785^{\circ} ; 919^{\circ} \pm 1$; $1404.5^{\circ} \pm 0.5$.

[^78]:    ** For reference, see footnote 45, p. 136.

    * The heat capacity of an ideal monatomic gas (at constant pressure) is equal to (5/2) $R$.

[^79]:    ${ }^{51}$ From Slater, John C., Introduction to chemical physics, McGraw•Hill Book Co., copyright 1939. Iised by permission.

[^80]:    * Abridred from Steam tables and Mollier's diagram, by Keenan, 1930. Printed by permission of publisher, The American Society of Mechanical Engineers.

[^81]:    *See also Table 175.

[^82]:    ＊Prepared by E．W．Dean，Standard Oil Co．of New Jersey．†API（American Petroleum Industry）unit $=\frac{141.5}{\text { sp．g．} 60^{\circ} / 60^{\circ}}-131.5 . \quad \ddagger$ Spec．gravity $15^{\circ} \mathrm{C} . \quad$ \＆Calories per gram．

[^83]:    I Prepared by G. Stegeman, University of Pittsburgh.

[^84]:    * Because of volatility and oxidation of some, these liquids should be kept in well-stoppered bottles when not in use.

[^85]:    $n$, failure to explode in twenty minutes.
    *The decomposition of nitrocellulose in celluloid commences at about $100^{\circ} \mathrm{C}$; above that the heat of decomposition may raise the mass to the ignition point if loss of heat is prevented. Above $170^{\circ}$, decomposition occurs with explosive violence as with nitrocellulose. Rate of combustion is 5 to 10 times that of poplar, pine, or paper of the same size and conditions. $\dagger$ Measured by contact with porcelain tube of given temperature. Average. $\ddagger$ Measured by contact with molten lead. Average.

[^86]:    am =amorphous: $d i=$ diamond; $\mathrm{cr}=$ crystal $; \mathrm{g}=\mathrm{gas} ; \mathrm{gr}=\mathrm{graphite} ; \mathrm{l}=$ liquid; $\mathrm{rh}=$ rhombic (sulfur); $\mathrm{s}=$ solid; $\mathrm{y}=$ yellow (gold).

    * Heats of formation not from elements but as indicated.

[^87]:    ${ }^{* 5}$ Everhart, Lindlief, Kanegis, Weissler, and Siegel, Nat. Bur. Standards Circ. C-447, 1943.
    ${ }^{56}$ Selected from Nat. Bur. Standards Circ. C-447, Mechanical properties of metals and alloys, and from Alcoa's circular, Aluminum and its alloys.
    ${ }^{57}$ Chase Brass \& Copper Co.'s circular, Copper and commercially important copper alloys, 1948 ; American Brass Co., Copper and copper alloys, 1945.

[^88]:    * Data furnished by the W. S. Tyler Co., Cleveland.

[^89]:    Element Samarium
    Scandium
    Selenium
    Silicon .....
    Silver
    Sodium ...
    Strontium
    Sulfur (rh
    Tantalum
    Technetium
    Tellurium
    Terbium
    Thallium
    Thorium
    Tin
    Titanium
    Tungsten
    Uranium
    Vanadium
    Xenon
    Ytterbium
    Yttrium
    Zinc
    Zirconium

[^90]:    (continued)

[^91]:    

[^92]:    * For 4.55 mm wire drawn cold to indicated sizes.
    $\dagger$ For 4.55 mm (. 018 in. ) wire annealed in $\mathrm{H}_{2}$ at $850^{\circ} \mathrm{C}$.

[^93]:    Recommended allowable load for wire rope running over sheave is onefifth of specified minimum strength.

[^94]:    * Commercial composition for some incandeseent electric lamp filaments containing thoria ( $\mathrm{ThO}_{2}$ ) approx. 0.75 percent.
    $\dagger$ Ordinary annealing treatment makes $W$ hrittle, and severe working, below recrystallization or equiaxing temperature, produces ductility. W rods which have been worked and recrystallized are stronger than sintered rods. The equiaxing temperature of worked tungsten, with a 5 -min exposure, varies from $2200^{\circ} \mathrm{C}$ for a work rod with 24 percent reduction, to $1350^{\circ} \mathrm{C}$ for a fine wire with 100 percent reduction. Tungsten wire, $\mathrm{D}=0.635$ mm or 0.025 in .
    $\ddagger$ Compression on cylinder 25.4 mm ( 1 in .) hy 65.1 mm ( 2.6 in .), at 20 percent deformation:
    For spelter (cast zinc) free from Cd, av. $17.2 \mathrm{~kg} / \mathrm{mm}^{2}$ or $24,500 \mathrm{lb} / \mathrm{in} .^{2}$
    For spelter with Cd 0.26 , av. $27.4 \mathrm{~kg} / \mathrm{mm}^{2}$ or $39,000 \mathrm{Hb} / \mathrm{in} .^{2}$
    Modulus of rupture averages twice the corresponding tensile strength.
    Shearing strength: rolled, averages $13.6 \mathrm{~kg} / \mathrm{mm}^{2}$ or $194,000 \mathrm{ib} / \mathrm{in}^{2}{ }^{2}$
    Modulus of elasticity: cast, $7,750 \mathrm{~kg} / \mathrm{mm}^{2}$ or $11,025,000 \mathrm{lb} / \mathrm{in}^{2}$
    Modulus of elasticity: rolled, $8450 \mathrm{~kg} / \mathrm{mm}^{2}$ or $12,000,000 \mathrm{lb} / \mathrm{in}^{2}$

[^95]:    * See also Table 123.

[^96]:    * U. S. Navy Spec. $46 \mathrm{M} 2 \mathrm{~b}(\mathrm{Cu} 3$ to $4.5, \mathrm{Sn} 88$ to $89.5, \mathrm{Sb} 7.0$ to 8.0$)$ covers manufacture of antifrictionmetal castings. (Composition W.)

[^97]:    ${ }^{62}$ Walker and Bloem, Journ. Amer. Concrete Inst., vol. 42, p. 629, 1946.

    * Strengths given are for mixes in which full advantage was taken of the sand and water-content reductions made possible by the increased workability resulting from entrained air.

[^98]:    ${ }^{63}$ McBurney and Lovewell, Proc. Amer. Soc. Test. Mat., vol. 33, p. 1, 1933.

[^99]:    * Prepared by R. Hobbs, National Bureau of Standards.
    ${ }^{65}$ Beek, J., and Hobbs, R. B., Journ. Amer. Leather Chem. Assoc., vol. 36, p. 190, 1941.
    ${ }_{68}$ Federal specification for leather and leather products, $\mathrm{K}_{\mathrm{k}}$-L-311. Government Printing Office, Washington, D. C., March 1945.

[^100]:    ${ }^{67}$ Wilson, J. A., Modern practice in leather manufacture, Reinhold Publishing Co., New York, 1941.

[^101]:    ex Progress in leather science, 1920-1945, British Leather Manufacturers' Res. Assoc., London, 1948.

[^102]:    ${ }^{6 n}$ Kanagy, J. R., and Wallace, E. I.., Journ. Amer. I.eather Chem. Assoc., vol. 38, p. 314, 1943 ; Rose, H., ibid., p. 107.

[^103]:    * For reference, see foot note 68, p. 232.

[^104]:    * Prepared by Lawrence A. Wood, National Bureau of Standards.

[^105]:    ${ }^{73}$ Bridgman, P. W., Proc. Amer. Acad. Mrts and Sci., vol. 74, p. 50, 1940.

[^106]:    ${ }^{74}$ Bridgman, P. W., Proc. Amer. Acad. Arts and Sci., vol. 76, p. 22, 1942.

[^107]:    ${ }^{75}$ Taken from Technical data on plastics，Plastic Mfg．Assoc．，Inc．，May 1948．For trade names see original reference．
    ＊Compression．
    $\dagger$ To fracture．

[^108]:    ${ }^{76}$ Polaroid Corporation, NDRC Report, Library of Congress PB 28553.

    * See Table 523.

[^109]:    * Acetate rayon or estron. $\dagger$ Including regular and high-tenacity varieties. $\ddagger$ "Denier" is the weight in grams of 9000 meters of the fiber. \& The value given for stiff ness is a measure of the ability of the fiber substance to resist deformation. || The toughness index is a measure of the ability of the fiber substance to absorb work.

[^110]:    * Data from the Plymouth Rope Co. and Mr. Axelsson of Columbian Rope Co. Data on cotton rope furnished by Mr. Moss, Southeastern Cordage Co. †Excellent resistance to acids, alkalis, and most chemicals.

[^111]:    * Table prepared by W. N. Watkins, U. S. National Museum.

[^112]:    * Adapted from data furnished by J. Hilsenrath, National Bureau of Standards.
    ${ }^{78}$ Woolley, Scott, and Brickwedde, Nat. Bur. Standards Res. Pap. RP 1932, vol. 41, 1948.

[^113]:    ${ }^{79}$ Slater, J. C., Introduction to chemical physics, page 408, 1939, McGraw-Hill Book Co. Used by permission of the publishers.
    (continued)

[^114]:    * Abridged from Nat. Bur. Standards Circ. ${ }^{2} 79,1926$.

[^115]:    * Taken from Nat. Bur. Standards Circ. 279, 1926.

[^116]:    * For reference, see footnote 45, p. 136.
    * At 710 mmHg .

[^117]:    ** For reference, see footnote 45, p. 136.

    * Plait point. † Critical point of contact.

[^118]:    * The material on the Joule-Thomson effect was supplied by J. R. Roebuck, of the University of Wisconsin.

[^119]:    ${ }^{84}$ Phys. Rev., vol. 43, p. 60, 1933 (corrected).

[^120]:    ${ }^{86}$ Phys. Rev., vol. 48, p. 45, 1935 (corrected).

[^121]:    88 Journ. Amer. Chem. Soc., vol. 64, p. 400, 1942.

[^122]:    89 Journ. Amer. Chem. Soc., vol. 60, p. 341, 1938 (corrected).

[^123]:    ${ }^{\infty}$ Bridgman, P. W., Proc. Amer. Acad. Arts and Sci., vol. 47, p. 345, 1911; vol. 48, p. 309, 1912; vol.

[^124]:    * $-\Delta V / V_{0}$.

[^125]:    Qs Bridgman, P. W., Proc. Amer. Acad. Arts and Sci., vol. 76, p. 75, 1948.

    * Transition at 23,300. Compressions . 3716 and . 3776 . $\dagger$ Transition at 23,370 . Compressions .0755 and .0781. $\ddagger$ Transition at 12,430 . Compressions .0736 and .1504 .

    TABLE 275.-VARIATION OF THE VOLUME ( $\Delta V / V_{0}$ ) FOR A NUMBER OF COMPOUNDS WITH PRESSURE FOR TWO TEMPERATURES ${ }^{\circ}$

[^126]:    ${ }^{04}$ Bridgman, P. W., Proc. Amer. Acad. Arts and Sci., vol. 74, October 1940.

    * Transition below this point.

[^127]:    ** For reference, see footnote 45, p. 136.

[^128]:    * Dynamical measurements.

[^129]:    ${ }^{95}$ Bridgman, P. W., Proc. Amer. Acad. Arts and Sci., vol. 76, p. 68, 1948.

    * Glass $A$ is a potash lead silicate of very high lead content. $\dagger$ Glass $C$ is a soda potash lime silicate. $\ddagger$ Glass $D$ is a lead zinc borosilicate.

[^130]:    * Where the temperature is not given, ordinary temperature is understood.

[^131]:    * According to P. Chappuis, Bureau International des Poids et Mesures.

[^132]:    * Cf. Table 269.

[^133]:    (continued)

[^134]:    95 References: a, Weissler, A., Journ. Amer. Chem. Soc., 1948 and 1949 ; also unpublished work with V. A. Del Grosso, b, Bergmann, L., Ultrasonics, 3d ed., p. 175, Edwards Brothers, Ann Arbor, Mich., 1944. c, Rao, M. R., Ind. Journ. Phys., vol. 14, p. 109, 1940. d, Lagemann, R. J., et al., Journ. Chem. Phys., vol. 16, p. 247, 1948; Journ. Amer. Chem. Soc., vol. 70, p. 2994, 1948. e, Kandall, C. R., Nat. Bur. Standards Journ. Res., vol. 8, p. 95, 1932.

[^135]:    * Data selected and arranged by Cyril M. Harris, Bell Telephone Laboratories.
    ${ }_{100}$ Fletcher, H., Speech and hearing, p. 74, D. VanNostrand, 1929. French, Carter, and Koenig, Bell System Techn. Journ., vol. 9, p. 290, 1930.

[^136]:    $\dagger$ The bel is a dimensionless unit for expressing the ratio of two values of power, the number of bels being the logarithm to the base 10 of the power ratio.

    The decibel, abbreviated db , is one-tenth of a bel. When conditions are such that scalar ratios of pressure amplitudes or particle velocities are the square roots of the corresponding power ratios, the number of decibels by which the corresponding powers differ is expressed by
    $20 \log \left(p_{1} / p_{2}\right) \mathrm{db}$
    where $p_{1} / p_{2}$ represents the scalar ratio. This relationship is frequently applied where the scalar ratio is not the square root of the corresponding power ratio, but such usage should be accompanied by a specific statement of application.

[^137]:    ${ }^{101}$ Dunn, H. K., and White, S. D., Journ. Accoust. Soc. Amer., vol. 11, p. 278, 1940.

[^138]:    102 Sivian, L. J., Dunn, H. K., and White, S. D., Journ. Acoust. Soc. Amer., vol. 2, p. 330, 1931.

[^139]:    ${ }^{106}$ Sivian, L. J., and White, S. D., Journ. Acoust. Soc. Amer., vol. 4, p. 228, 1933.

[^140]:    ${ }^{107}$ Taken from Acoustical designing in architecture, by V. O. Knudsen and C. M. Harris, John Wiley \& Sons, 1949. Used by permission of the publishers.

[^141]:    * The data on viscosity were selected and arranged by George V. McCauley, Corning Glass Works.
    ${ }^{100}$ L.illie, H. R., Journ. Amer. Cer. Soc., vol. 12, p. 505, 1929.
    ${ }^{100}$ Hunter, R. G., Journ. Amer. Cer. Soc., vol. 17, p. 123, 1934 ; Ann. d. Phys., ser. 4, vol. 22, p. 287, 1907 ; vol. 23, p. 447, 1907.

[^142]:    * Tables 314 and 315 tiken from Nat. Bur. Standards Techn. Pap. No. 112, 1918. Gilycerol data,

    Table 314, from Archbutt. Deeley, and Gerlack; castor oil data, Table 315, from Kahlbaum and Raber. Archhutt and Deeley give for the density and viscosity of castor oil at $65.6^{\circ} \mathrm{C}, 0.9284$ and 0.605 , respectively; at $100^{\circ} \mathrm{C}, 0.9050$ and 0.169 .
    $\dagger$ The kinematic viscosity is the ordinary viscosity in cys units (poises) divided by the density in $\mathrm{g} / \mathrm{cm}^{3}$. The cgs unit of kinematic viscosity is the stoke.

[^143]:    ${ }_{115}$ Herschel, Nat. Bur. Standards Techn. Pap. No. 125, 1919.

[^144]:    ${ }^{117}$ Babcock, C. L., Journ. Amer. Cer. Soc., vol. 17, p. 319, 1934. Lillie, H. R., Journ. Amer. Cer. Soc., vol. 22, p. 367, 1939.

[^145]:    118 Volarovich, M. P., and Leontieva, A. A., Journ. Soc. Glass Techn., vol. 20, p. 139, 1936.

[^146]:    ${ }^{121}$ Landolt and Börnstein, 1935. Based on data by Esser, Greis, and Brundgart. Arch. Eisenhütten, vol. 7, p. 385, 1934. Viscosity in centipoises. Data on tin by Stott, Proc. Phys. Soc., vol. 45, p. 530, 1933, included.
    *Esser, Greis, and Brundgart. $\dagger$ Stott.

[^147]:    * American mineral oils; based on water as .01028 at $20^{\circ} \mathrm{C}$. $\dagger$ Based on water as per 1 st footnote. $\ddagger$ Densities.

[^148]:    ${ }^{128}$ Lipkin, M. R., Davison, J. A., and Kurtz, S. S., Ind. Eng. Chem., vol. 34, p. 976, 1942.

[^149]:    ${ }^{124}$ Babcock, C. L., Journ. Amer. Cer. Soc., vol. 17, p. 329, 1934 ; English Journ. Soc. Glass Techn., vol. 7, p. 25,1923 ; vol. 8, p. 205,1924 ; vol. 9 , p. 83,1925 ; vol. 10 , p. 52,$1926 ;$ Lillie, H. R., Journ. Amer. Cer. Soc., vol. 14. p. 502, 1931; Hunter, Journ. Amer. Cer. Soc., vol. 17, n. 121, 1934; Lillie, H. R., unpublished data. * $\mathrm{R}_{2} \mathrm{O}_{3}$. Glasses 11 and 12 contained 0.50 and 0.34 nercent BaO, respectively. $\dagger$ Glass 14 contains 20 percent liaU. $\ddagger$ Data by H. R. Lillie, Corning Glass Works Laburatory.

[^150]:    ${ }^{125}$ Dushman, S., Vacuum technique, p. 37. John Wiley \& Sons, New York, 1949 ; Banerjea, G. B., and Plattanaik, B., Zeit. Physik, vol. 110, p. 676, 1938; Partington, J. R., Phys. Zeit., vol. 34, p. 289, 1933; Fisher, Phys. Rev., vol. 24, 1907.

[^151]:    ${ }^{127}$ Bridgman, P. W., Proc. Acad. Arts and Sci., vol. 61, p. 59, 1926.

[^152]:    ${ }^{130}$ Metals Handbook, 1948 ed., p. 69, American Society for Metals, Cleveland.
    Symbols: $D r y=$ no cutting fluid, $E m=$ soluble or emulsifiable oils and compounds, $K=$ kerosene, $L=$ lard oil, $M L=$ mineral-lard oils, $M O=$ mineral oils, Sulf $=$ sulfurized oils.

[^153]:    *Tables 339 to 346 and figures 6 to 15 were prepared under the direction of C. H. Helms, assistant director of aeronautical research, National Advisory Committee for Aeronautics.

[^154]:    ${ }^{131}$ Authorities: 1, Eiffel G., Resistance de 1'air et l'aviation, 2d ed., p. 231, Dunod et Pinat, Paris. 2, Dines, Proc. Roy. Soc. London, A, Math. and Phys. Sci., vol. 48, p. 233, 1890. 3, Föppl, Jahrb. Motor-luftschiff-Studiengesellsch., vol. 4, p. 51, 1910. 4, Riabouchinski, Bull. Inst. Aerodynam. de Koutchino, Petrograd, vol. 4, p. 113, 1912. 5, Stanton, T. E. Air resistance of plane surfaces, Minutes of Proc. Inst. Civil Eng., vol. 156, p. 78, 1903. 6 and 6 a , National Bureau of Standards, private communication. 7, Knight, Montgomery, and Wenzinger, Carl J., Wind tunnel tests on a series of wing models through a large angle of attack range, Pi. 1, Force tests. NACA Rep. No. 317, 1929.

[^155]:    132 Wieselberger, C., New data on the laws of fluid resistance. NACA TN No. 84, 1922. Relf, E. F., Discussion of the results of measurements of the resistance of wires with some additional tests on the resistance of wires of small diameter. R. \& M. No. 102, British ACA, March 1914. Wieselsberger, C., Further information on the laws of fluid resistance. NACA TN No. 121, December 1922.

[^156]:    ${ }^{133}$ Allen, H. S., The motion of a sphere in a viscous fluid, Phil. Mag., vol. 50, p. 323, 1900. Wieselberger, C., Further information on the laws of fuid resistance, NACA TN No. 121 , Decemher 1922. Millikan, C. B., and Klein, A. L.. The effect of turbulence, Aircraft Eng., vol. 5, p. 169, 1933. Platt, Robert C., Turbulence factors of NACA wind lunnels as determined by sphere tests, NACA Rep. No. 558, 1936. Dryden, Hugh L., Schubauer, G. B., Mock, W. C., Jr., and Skramstad, H. K., Measurements of intensity and scale of wind-tunnel turbulence and their relation to the critical Reynolds number of spheres, NACA Rep. No. 581, 1937. Ferri, Antonio, The influence of Reynolds numbers at high Mach numbers, Atti di Guidonia, n. 67/69, Mar. 10, 1942.

[^157]:    ${ }^{184}$ Tetervin, Neal, A method for the rapid estimation of turbulent boundary-layer thickness for calculating profile drag, NACA 1 CR No. L.4G14, July 1944

[^158]:    195 Aiken, William S.. Tr.. Standard nomenclature for airsneeds with tables and charts for use in calculation of airspeed, NACA Rep. No. $837,1947$. Warfield, Calvin N., Tentative tables for the properties of the upper atmosphere, NACA TN No. 1200, January 1947.

[^159]:    * For metric values see Table 628.

[^160]:    ${ }^{106}$ Burcher. Marie $\Lambda$., Compressible flow tables for air, N.\C. $\overline{\text { T N No. 1592, August }} 1948$.

[^161]:    137 Abbott, Ira H., von Doenhoff, Albert E., and Stivers, Louis S., Jr., Summary of airfoil data. NACA Rep. No. 824, 1945. Stack, John, and von Doenhoff, Albert E., Tests of 16 related airfoils at high speeds, NACA Rep. No. 492, 1934.

[^162]:    ＊Table by J．W．H．Randall，reprinted with permission of Chemical Catalog Co．

[^163]:    $p=K . T^{-1} e^{-\lambda 0 / R T}$ dynes $/ \mathrm{cm}^{2}$ (Egerton)
    $\mathrm{Zn}, \lambda_{0}=3.28 \times 10^{4} ; K=1.17 \times 10^{14} ; \mathrm{Cd}, \lambda_{0}=2.77 \times 10^{4} ; K=5.27 \times 10^{13} ;$
    $\mathrm{Hg}, \lambda_{0}=1.60 \times 10^{4} ; K=3.72 \times 10^{13}$ (Knudsen).

[^164]:    * Prepared by Saul Dushman, General Electric Research Laboratory, Schenectady, N. Y.

[^165]:    138a Cromwell, J. C., Origins and prevention of laboratory accidents, 1950; Bell Laboratories Rec., p. 318 , June 1936; Johns Hopkins University, Report of Electrician, November 1934; Journ. Franklin Inst., vol. 215, p. 1, 1933.

[^166]:    * Everett, Units and physical constants: Table of Ayrton and Perry's results, prepared by Ayrton.

[^167]:    ${ }^{140}$ Nat. Bur. Standards Circ. 346, 1927.

[^168]:    * Amalgamated. $\ddagger$ Not constant. $\ddagger$ After some time. $\$$ A quantity of bromine was used corresponding to $\mathrm{NaOH}=1$.

[^169]:    (continued)

[^170]:    * Electrical conductivity of $T e_{\beta}=0.04, T e_{a}=1.7 \mathrm{emu}$.

[^171]:    * See note to Table 377

[^172]:    ${ }^{142}$ Bridgman, Proc. Amer. Acad. Arts and Sci., vol. 72, p. 174, 1938.

[^173]:    * For reference, see footnote 142, above.

[^174]:    * This line gives the specific mass resistance at $25^{\circ}$, the other lines, the specific volume resistance.

    The use of mercury as ahove has the advantage of beng perfectly reproducihle so that at any time a pressure can be measured without recourse to a fundamental standard. However, at $0^{\circ} \mathrm{C}$ mercury freezes at $7500 \mathrm{~kg} / \mathrm{cm}^{2}$. Manganin is suitahle over a much wider range. Over a temperature range 0 to $50^{\circ} \mathrm{C}$ the pressure resistance relation is linear within $1 / 10$ percent of the change of resistance up to $13,000 \mathrm{~kg} / \mathrm{cm}^{2}$. The coefficient varies slightly with the sample. Bridgman's samples (German) had values of ( $\Delta R / p R_{0}$ ) $\times 10^{0}$ from 2295 to 2325. These are + instead of - , as with most of the above metals.

[^175]:    ${ }^{13}$ Smith, G. H., and W'ilhelm, J. O., Rev. Mod. Phys., vol. 7, p. 240, 1935.

[^176]:    * For reference, see footnote 45, p. 136.

[^177]:    ${ }^{147}$ Corning Glass Co. publication, Properties of selected commercial glasses, 1949. General Electric Co. publication, Fused quartz, 1947.

[^178]:    * Acids and alkaline salts show peculiar irregularities.

[^179]:    * These values are at the concentration 80.0.

[^180]:    *The American wire gage sizes have been rounded off to the usual limits of commercial accuracy. They are given to four significant figures in Tables 420 to 423 . They can be calculated with any desired accuracy, being based upon a simple mathematical law. The diameter of No. 0000 is defined as 0.4600 inch and of No. 36 as 0.0050 inch. The ratio of any diameter to the diameter of the next greater number $\sqrt[39]{\frac{.4600}{.0050}}=1.1229322$.
    $\dagger$ The steel wire, gage is the same gage that has been known by the various names: "Washburn and Moen," "Roebling," "American Steel and Wire Co.'s." Its abbreviation should he written "Stl. W. G." to distinguish it from "S. W. G.," the usual abbreviation for the (British) Standard Wire Gage.

[^181]:    * These values are for voltages in the range up to 5,000 or 7,000 and for 75 to 100 percent time load, ambient temperature $30^{\circ} \mathrm{C}$ and copper temperature $75-80^{\circ} \mathrm{C}$. Adapted from Publication No. P-29-226 of the Insulated Power and Cable Engineers' Association. For other values see these tables

[^182]:    * Prepared by F. W. Grover, Nat. Bur. Standards.

[^183]:    148 Danforth, Phys. Rev., vol. 38, p. 1224, 1931.

[^184]:    ＊For reference，see footnote 45，p． 136.

[^185]:    * Prepared by Hans Jaffe, Brush Development Co., Cleveland, Ohio.
    $n$, e Letters refer to references, p. 431 .

[^186]:    ** Table from Corning Glass Works publication on Properties of Selected Commercial Glasses (B-83).
    *Values of P. H. Moon and A. S. Norcross, Trans. Amer. Inst. Electr. Engr., vol. 49, p. 775 (1930).
    $\dagger$ Values of S. Whitehead. World Power, p. 72, September 1936.

[^187]:    *Tables 444, 450, and 451 prepared by Hans Jaffe, Brush Development Co., Cleveland, Ohio. † All data refer to room temperature unless otherwise noted.

[^188]:    149 For authorities, see references, p. 431.
    $\ddagger$ Synthetic, Linde Air Products Company.

[^189]:    * The coefficient $d_{14}$ of Rochelle salt is extremely dependent on temperature and on amplitude. The ratio of $d_{14}$ to dielectric constant $K$ (for the latter see figure 16 ) is, however, nearly constant; $4 \pi d_{14} / K=$ $g_{14}=6.4 \times 10^{-7}$ statvolt $\mathrm{cm} /$ dyne
    m Letters refer to references, p. 431

[^190]:    Range of 9 samples. $\dagger$ Range of 27 samples $\ddagger$ Range of 10 samples. $f$ Range of a of samples from different localities. || Range of several samples. $\quad$ A After drying 48 hours at $80^{\circ} \mathrm{C}$.

[^191]:    * Data arranged by Newbern Smith and Marcella Phillips, Central Radio Propagation Laboratory, National Bureau of Standards.

[^192]:    ${ }^{160}$ Jelatis, J. G., Journ. Appl. Phys., vol. 19, p. 419, 1948; Hecter, L. G., and Woernley, D. C., Phys. Rev., vol. 69, p. $101,1946$.

[^193]:    ${ }^{151}$ These data were selected from Tables of Dielectric Materials, volume 3, Laboratory of Insulation Research, Massachusetts Institute of Technology, Cambridge, Mass., June 1948.
    $\epsilon$ is used for dielectric constant in this table in the place of K .

    * Numbers refer to notes at end of table.
    ** Not corrected for variations of density.
    $\dagger$ Rod stock in $\mathrm{H}_{11}$ ( $\mathrm{TE}_{11}$ ) made of circular wave guide.

[^194]:    Notes: 1, From conductivity water. 2, Fresh crystals (Harshaw). Audio frequency loss decreases with time. For a discussion of low-frequency dispersion in ionic crystals see R. G. Breckenridge, Bull. Amer. Phys. Soc., vol. 23, p. 33, 1948. 3, Magnesium silicate (American Lava). 4, Muscovite. 5, Mica, glass, TiO (Mycalex) 6, Knox. 7, $96 \% \mathrm{SiO}_{2}$. ${ }^{8}$ Iron sealing glass. ${ }^{2}$, Soda-lime (Pittsburgh-Corning) ${ }^{2}$ $10, \mathrm{SiO}_{2}$ (General Electric). 11, Eastman Kodak; recryst. and resubl. Lab. Ins. Res. 12, Mica-filled (Bakelite). 13, $50 \%$ paper laminate (Formica). $14,58 \%$ mica, $2 \%$ misc. (Monsanto). $15,55 \%$ filler (Formica). 16, Mineral filler (American Cyanamid). 17, a-cellulose (Libbey-Owens-Ford). 18, DuPont. 19, 5-15\% plasticizer, pigments, dyes (Tennessee Eastman). 20, $25 \%$ camphor (DuPont). 21, 2.73 ethoxy groups/glucose, plast. (Dow). $\quad 2$, Cross-linked organo siloxane polymer (Dow Corning). 23 .

[^195]:    ${ }^{152}$ Smith-Rose, Journ. Inst. Electr. Eng., London, vol. 75, p. 221, 1934.

[^196]:    ${ }^{153}$ Norton, K. A.. The calculation of ground wave ficld intensity over a finitely conducting spherical earth, Proc. Inst. Radio Eng., December 1941; Van der Pol. Balth, and Bremmer, H., Philos. Mag., vol. 24, p. 141, 1937 ; vol. 24, p. 825, supplement. November 1937.

[^197]:    ${ }^{154}$ Adapted from Becker and Autler, Phys. Rev., vol. 70, p. 303, September 1946.

[^198]:    * Prepared by C. R. Burrows.

    157 For references, see p. 450.

[^199]:    References: a, Bolton, J. G., Nature, vol. 162, p. 141, 1948; b, Bolton, J. G., Stanley, G. J., and Slee, O. B., Nature, vol. 164, p. 101, 1949; c, Unpublished; d, Ryle, M., and Śmith, F. G., Nature, vol. 162, p. 462, 1948; e, Hey, J. S., Parsons, S. J., and Phillips, J. W., Nature, vol. 158, p. 234, 1946; f, Bolton, J. G., and Stanley, G. J., Nature, vol. 161, P. 312, 1948; g, Hey, J. S., Parsons, S. J., and Phillips, J. W., Proc. Roy. Soc. London, vol. 192, p. 425, 1948; h, Bolton, J. G., and Stanley, G. J., Australian Journ. Sci. Res., vol. 2, p. 139, 1949; i, Williamson, R. E., Journ. Roy. Astron. Soc. Canada, vol. 42, p. 9, 1948; j, Pawsey, J L., and Yabsley, D. E., Australian Journ. Sci. Res., vol. 2, p. 198, 1949.

[^200]:    * See pages 16-18.

[^201]:    * $Q$, quench or controlled cooling.

[^202]:    

[^203]:    * Much of the data on magnetism was corrected by W. E. Ruder, of the General Electric Co.

[^204]:    158 Hicks, Laurence C., Nickel-iron alloys for magnetic circuits, Electrical Manufacturing, January 1946.

[^205]:    * Prepared by E. H. Vestine, Carnegie Institution of Washington, and David G. Knapp, U. S. Coast and Geodetic Survey.
    ${ }^{150}$ For references, see bibliography following Table 511, p. 501.

[^206]:    * East declination. $\dagger$ Values on this line are west, except those marked (*).

[^207]:    * Melting point.

[^208]:    ${ }^{160}$ Adapted from data from Bausch \& Lomb (BL) and Corning Glass Works (CG). F. A. Molby, West Virginia University, assisted in selecting and arranging these data. For reference see Molby, Journ. Opt. Soc. Amer., vol. 39, p. 600, 1949.

[^209]:    * Abbreviated from a list of results of measurements on freshly polished samples of Bausch \& Lomb glasses. Data supplied by the Bausch \& Lomb Optical Co.

[^210]:    Fig. 26.-Spectral transmission of a number of infrared materials. Curves: 1, Fluorite, $\mathrm{CaF}_{2}, 1 \mathrm{~cm}$ thick. 2, Rocksalt, $\mathrm{NaCl}, 1 \mathrm{~cm} .3$, SilBaird Associates, Engineering Research Development Laboratories, Rep. W-44-009 Eng. 473, 1949.

[^211]:    ${ }^{162}$ Baird Associates, Infrared optical materials, Engineer Research and Development Laboratories, Fort Belvoir, Va.

[^212]:    ${ }^{163}$ Schonrock, Zeitschr. Instrumentenkunde, vol. 40, p. 94, 1920; vol. 41, p. 104, 1921.

[^213]:    * Types of glass in class 1 or 2 are not likely to stain even when used as exposed surfaces in tropical climates. Glasses in class 5 are liable to stain when exposed to rain, moisture condensation, or fingerprints in any climate. Other glasses are intermediate in stain resistance.

[^214]:    * Corning Glass Works. $\dagger$ Second max at 2.55 with transmission at 5.0 percent. $\ddagger$ Second max at .605 with transmission at 1.0 percent.

[^215]:    ${ }^{185}$ b, Tsukamoto, K., Rev. d'Optique, vol. 7, p. 89, 1929. c, Dawson, L. H., and Hulburt, E. O., Journ. Opt. Soc. Amer., vol. 24, p. 175, 1934. d,'Hulburt, E. O., Journ. Opt. Soc. Amer., vol. 35, p. 698, 1945. e, Collins, J. R., Phys. Rev., vol. 26, p. 771, 1925.

[^216]:    * Adapted from data furnished by J. W. Forrest, Bausch \& Lomb Optical Co.
    $\dagger t=2.0 \mathrm{~mm}$.

[^217]:    See Table 77.
    100 "Temperature, Its Measurement and Control," a symposium prepared by the American Institute of Physics, p. 1115, Reinhold Publishing Co.

[^218]:    * Data furnished by I. H. Godlove, General Aniline \& Film Corporation.

[^219]:    107 Barnes, Phys. Rev., vol. 39, p. 562, 1932.
    *On celluloid $1 \mu$ thick.

[^220]:    ${ }^{170}$ Cartwright, Phys. Rev., vol. 35, p. 415, 1930; Pfund, Rev. Sci. Instr., vol. 1, p. 397, 1930, and Journ. Opt. Soc. Amer., vol. 23, p. 375, 1933.

[^221]:    *This column gives the degree of polarization. †Columns 5 and 6 furnish a means of determining $A$ and $B$ for other values of $n$. They represent the change in these quantities for a change of $n$ of 0.01 .

[^222]:    *The smoke of magnesium turnings freely burning in air and deposited on a satisfactory base forms a uniform fine-grained diffusing surface of high reflectance. This oxide should be deposited so as not to be affected by the heat from the burning Mg. A satisfactory base may be Al, silver-plated Cu , block porcelain. The oxide adheres better to depolished surfaces. Surfaces of high and uniform reflectance throughout the spectrum are best. † Revised values.

[^223]:    ${ }^{171}$ Coblentz, Stair, Nat. Bur. Standards Journ. Res., vol. 4, p. 189, 1930.

[^224]:    ＊Nonmonochromatic means from Coblentz．
    A surface of plate glass，ground uniformly with the finest emery and then silvered，used at an angle of $75^{\circ}$ ，reflected 90 percent at $4 \mu$ ，approached 100 for longer waves，only 10 at $1 \mu$ ，less than 5 in the visible＇red and approached 0 for shorter waves．Similar results were obtained with a plate of rock salt for transmitted energy when roughened merely by breathing on it．In both cases the finer the surface， the more suddenly it cuts off the short waves．

[^225]:    *Restrahlung from KBr . $\dagger$ Isolated with quartz lens.

[^226]:    ${ }^{178}$ Hulburt, Journ. Opt. Soc. Amer., vol. 17. p. 23, 1928.

    * Yellow-white grains of many kinds. $\dagger$ Very white. $\ddagger$ Anhydrous. \& Handkerchief.

[^227]:    ${ }^{174}$ Strong, Phys. Rev., vol. 38, p. 1818, 1931.
    *The use of a paraffin window about 3 mm thick stops the short wavelength restrahlung of quartz at $8.7 \mu$ and of calcite at $6.7 \mu$. Weak reflection at $41 \mu$.

[^228]:    * Degrees per dm . The above values are for a near normal solution, i.e., approximately 26 g of sucrose per $100 \mathrm{~cm}^{3}$.

[^229]:    * See footnote 5, p. 7.

[^230]:    * The material on photography was prepared by L. A. Jones, of the Eastman Kodak Co.

[^231]:    - $S_{i}=10 / i$, where $i$ is the inertia value at $\gamma=1.0$. Reciprocal inertia was originally proposed by Hurter and D'riffeld as a sensitometric measure of the speed of photographic materials. It bears no direct relation to their effective speed as determined by camera exposures, however. It is useful for comparing different types of materials which have no common basis of application in practice.

[^232]:    ${ }^{175}$ Mees, C. E. K., The theory of the photographic process, chap. 21, Macmillan, 1942.
    ${ }^{176}$ Mees, C. E. K., Proc. Roy. Soc. London, vol. 83, p. 10, 1909.

[^233]:    * This value was obtained by direct exposure to a line interference pattern. With conventional methods of measurement, the value is limited by the optical system rather than by the characteristics of the emulsion.

[^234]:    New values of 20 krypton lines as secondary standards of wavelength were adopted in 1935 by the International Astronomical Union. ${ }^{184}$ See Table 614.

[^235]:    ${ }^{184}$ For reference, see p. 578.

[^236]:    ${ }^{182}$ For reference, see p. 578.

[^237]:    180-191 For references, see p. 578.

[^238]:    102 For reference, see p. 578.

[^239]:    - Band lines due to molecular oxygen in the earth's atmosphere. The wavelength of the first line of the band is recorded here.
    $\dagger$ Jahoratory wavelengths listed. He lines are conspicuous in the spectrum of the chromosphere.
    $\ddagger$ Rowland assigns the index letter " $g$ " to this line.

[^240]:    ${ }^{198}$ For more detailed discussions of atomic spectra and complete compilations of atomic energy levels, see the list of references, page 585.

[^241]:    * Prepared by G. Herzberg, National Research Council of Canada.

[^242]:    ${ }^{185}$ Grimminger, G., Analysis of temperature, pressure and density of the atmosphere extending to extreme altitudes, p. 18, Rand Corporation, November 1948.

[^243]:    $\left.\begin{array}{l}\text { - For reference. see } \\ \dagger 1 \text { millibar }(\mathrm{mb})\end{array}\right)=10^{2}$ dynes $/ \mathrm{cm}^{2}=0.750 \mathrm{mmHg}$.

[^244]:    ${ }^{106}$ The tables on densities and humidities have been adapted from the sixth edition of the Smithsonian Meteorological Tables, which see for more extensive data.

[^245]:    - 1.7

[^246]:    * The height of the barometer is affected by the relative thermal expansion of the mercury and the glass, in the case of instruments graduated on the glass tube, and by the relative expansion of the mercury and the metallic enclosing case, usually of brass, in the case of instruments graduated on the brass case. This relative expansion is practically proportional to the first power of the temperature. The above tables of values of the coefficient of relative expansion will be found to give corrections almost identical with those given in the International Meteorological Tables. The numbers tabulated under a are the values of $a$ in the equation $H_{t}=H_{t^{\prime}}-a\left(t^{\prime}-t\right)$ where $H_{t}$ is the height at the standard temperature, $H t^{\prime}$ the observed height at the temperature $t^{\prime}$, and $a\left(t^{\prime}-t\right.$ ) the correction for temperature. The standard temperature is $0^{\circ} \mathrm{C}$ for the metric system and $28^{\circ}: 5 \mathrm{~F}$ for the English system. The English barometer is correct for the temperature of melting ice at a temperature of approximately $28^{\circ} .5 \mathrm{~F}$, because of the fact that the brass scale is graduated so as to be standard at $62^{\circ} \mathrm{F}$, while mercury has the standard density at $32^{\circ} \mathrm{F}$.

    EXAMPLE.-A barometer having a brass scale gave $H=765 \mathrm{~mm}$ at $25^{\circ} \mathrm{C}$; required, the corresponding reading at $0^{\circ} \mathrm{C}$. Here the value of $a$ is the mean of .1235 and 1251 , or $.1243 ; \therefore a\left(t^{\prime}-t\right)=.1243 \times$ $25=3.11$. Hence $H_{0}=765-3.11=761.89$.

    Note.-Although $a$ is here given to three and sometimes to four significant figures, it is seldom worth while to use more than the nearest two-figure number. In fact, all barometers have not the same values for $a$, and when great accuracy is wanted the proper coefficients have to be determined by experiment.

[^247]:    * $980.665 \mathrm{~cm} \mathrm{sec}^{-2}$

[^248]:    * 32.17 in. $\mathrm{sec}^{-2}$

[^249]:    ${ }^{1209}$ Seaborg and Perlman, Rev. Mod. Fhys., vol. 20, p. 585, 1948.
    ${ }^{200}$ Bethe, H. A., Elementary nuclear theory, John Wiley \& Sons, Inc., 1947. Reprinted by permission.

[^250]:    *This table adapted from data furnished by the National Bureau of Standards.
    $\dagger$ This means $h \nu /$ molecule where the values given are for $\nu=$ unity.

[^251]:    201 Wichers, Edward Journ. Amer. Chem. Soc., vol. 74, p. 2447, 1952

    * A value given in brackets denotes the mass number of the isotope of longest known half life.

    Because of natural variations in the relative abundance of the isotopes of sulfur, the atomic weight of this element has a range of $\pm .003$.

[^252]:    202 Meggers, W. F., Science, vol. 105, p. 514, 1947; G. T. Seaborg, private communication.

    - Rare earths:
    71 Lu
    174.99
    ${ }_{169.4}^{69 \mathrm{Tm}} \stackrel{170 \mathrm{Yb}}{173.04}$
    $\begin{array}{rr}67 \mathrm{Ho} & 68 \mathrm{Er} \\ 164.94 & 167.2\end{array}$
    $\begin{array}{cccc}\begin{array}{c}63 \mathrm{Eu} \\ 152.0\end{array} & \begin{array}{c}64 \mathrm{Gd} \\ 156.9\end{array} & \begin{array}{c}65 \mathrm{~Tb} \\ 159.2\end{array} & \begin{array}{c}66 \mathrm{Dy} \\ 162.46\end{array} \\ & & & \\ 95 \mathrm{Am} & 96 \mathrm{Cm} & 97 \mathrm{Bk} & 98 \mathrm{Cf}\end{array}$
    $\begin{array}{ll}{ }_{1471}^{61} \mathrm{Pm} & \begin{array}{c}62 \mathrm{Sm} \\ 150.43\end{array} \\ & \\ 93 \mathrm{~Np} & 94 \mathrm{Pu}\end{array}$
    
    $\begin{array}{lll}57 \mathrm{La} & 58 \mathrm{Ce} & 59 \mathrm{Pr} \\ 138.92 & 140.13 & 140.92\end{array}$
    $\quad 57 \mathrm{La} \quad \begin{gathered}58 \mathrm{Ce} \\ 138.92 \\ 140.13\end{gathered}$
    + Actinide rare earths
    
    05 Am 96 Cm -
    ${ }_{238.17}^{92}$
    $\dagger$ Actinide rare earths: 91 Pa

[^253]:    * See column 3, Table 623. G. T. Seaborg, private communication.

[^254]:    *This table was selected from several sources including the report by Brown (see footnote 204) and data furnished by Ingerson of the U. S. Geological Survey. †The lithosphere, 10 miles of earth crust, makes up 93 percent, the hydrosphere makes up 7 percent, and the atmosphere makes up 0.03 percent of the part of the earth considered. Proc. Nat. Acad. Sci., vol. 8, p. 114, 1922.

[^255]:    * Prepared by B. Bell.
    ${ }^{205}$ Brown. Rev. Mod. Phys., vol. 21, p. 625, 1949; Russell-Dugan-Stewart, Astronomy, vol. 2, p. 503, 1938: Unsöld, Zeitschr. f. Astrophys., vol. 24, p. 307, 1948. $\dagger$ Brown. $\ddagger$ Russell. §Unsöld.

[^256]:    * For reference, see footnote 204, p. 625.

[^257]:    * Prepared by Charlotte E. Moore, National Bureau of Standards.
    ${ }^{200}$ The sources used are as follows:
    2935 A-3062A, Babcock, H. D., Moore, C. E., and Coffeen, M. F., Astrophys. Journ., vol. 107, p. 287, 1948 (Mount Wilson Contr. No. 745).
    3062A-6600A, St. John, C. C. ., and others, Revised Rowland Table, Carnegie Inst. Washington Publ. 396, 1928, with unpublished corrections and revisions by C. E. Moore (September 1949).
    6600.1-13495A, Babcock, H. D., and Moore, C. E., Carnegie Inst. Washington Publ. 579, 1947.

    The counts included also the raic ultime of $\mathrm{Mg} 1(2852 \mathrm{~A})$; the ultimate lines of Mg 11 (2795A, 2802A) and the strong Si i line at 2881 A . These lines, ainong others, have been identified in the ultraviolet solar spectrum photographed from a V-2 rocket. Intensities in parentheses are quoted from the paper on this subject by Durand, E., Oherly. J. J., and Tousey, R., Astrophys. Journ., vol. 109, p. 1, 1949. (See also Hopfield, J. J., and Clearman, H. E., Phys. Rev., vol. 73 , p. $877,1948$.

    For lines of H and He see Menzel, D. H., Lick Obs. Publ. 17, p. 1, 1931; Mitchell, S. A., Astrophys. Journ., vol. 105, p. 1, 1947.
    ** These counts refer to lines not present in disk spectrum. † Lines of $H$ and He are prominent in the spectrum of the chromosphere. $\ddagger B$ and $F$ are identified only from their presence in compounds (see Part 2 ).

[^258]:    207 Babcock, H. D., Astrophys. Journ., vol. 102, p. 154, 1945 (Mount Wilson Contr. No. 708).

[^259]:    ${ }^{208}$ Unsöld, Zeitschr. f. Astrophys., vol. 21, p. 1, 1941.
    200 Aller, Astrophys. Journ., vol. 104, p. 347, 1946.

[^260]:    * Prepared by B. Donn.
    ${ }^{210}$ Adams, Astrophys. Journ., vol. 109, 1949; Publ. Astron. Soc. Pacific, vol. 60, p. 354, 1948; Dunham, Proc. Amer. Philos. Soc., vol. 81, p. 277, 1939. Ledoux, Pop. Astr., vol. 49, p. 513, 1941. Stromgren, Astrophys. Journ., vol. 108, p. 242, 1948. Struve, Journ. Washington Acad. Sci., vol. 31, p. 217, 1941; Astrophys. Journ., vol. 89. p. 517, 1939.
    $\dagger$ Values for apparently abnormally dense cloud.

[^261]:    * Prepared by B. Donn.
    ${ }^{212}$ Greenstein, Harvard Circ. 422, 1938. Spitzer, Astrophys. Journ., vol. 93, p. 369, 1941. Van de Hulst, Rech. Astron. de l'Obs. d'Utrecht, vol. 11, pt. 1, 1946, pt. 2, 1949. Schalen, Publ. of Uppsala Oliservatory, 1930 on. Oort, Astron. Inst. Netherlands Bull. No. 283, 1932.

[^262]:    ${ }^{212 a}$ Alexander, J., Colloid chemistry, vol. 2, Chemical Publishing Co. Used by permission.

[^263]:    ${ }_{213}$ Neurath, Journ. Arer. Chem. Soc., vol. 61, p. 1841, 1939.

[^264]:    216 Thomas, Arthur W., Colloid chemistry, McGraw-Hill Book Co., 1934. Used by permission of the author.

    * These are the permanent saturated solutions. The more concentrated solutions, obtained from contact with the more finely ground particles, slowly revert to the normally saturated solutions and the particles grow to $2 \mu$ in size.

[^265]:    ${ }^{215}$ Weiser, H. B., Colloid chemistry, 2d ed., John Wiley \& Sons, Inc., 1949. Reprinted by permission.

    * Further activation reduces the granules to a fine powder.

[^266]:    * For reference, see \{ootnote 215 , above.

[^267]:    ${ }^{216}$ Lewis, Squires, and Broughton, Industrial chemistry of colloidal and amorphous materials, Macmillan Co., 1942. Used by permission of the publishers.

[^268]:    * For the energy per atom, divide these values by the Avogadro number, $6.023 \times 10^{23}$.
    ${ }_{217}$ Pauling, Linus, The nature of the chemical bond. Used by permission of the author.

[^269]:    * For reference, see footnote 214, p 631.

[^270]:    *Prepared by Saul Dushman, General Electric Research Laboratory, Schenectady, N. Y.

[^271]:    ${ }_{218}$ Herring, C., and Nichols, M. H., Rev. Mod. Phys., vol. 21, p. 185, 1949. R_imann, A. L., Thermionic emission, John Wiley \& Sons, Inc., 1934. Dushman, S., Rev. Mod. Phys., vol. 2, p. 381, 1930.

[^272]:    ${ }^{210}$ Dushman, Saul, The scientific foundations of vacuum technique, John Wiley \& Sons, Inc., 1949. Reprinted by permission.

    * Layer of thorium on tungsten.

[^273]:    * Prepared by Saul Dushman, General Electric Co. The formulae and calculations in this section are based on a more comprehensive discussion in chapter 1 of his "Scientific Foundations of Vacuum Technique" (John Wiley \& Sons, New York, 1949).

[^274]:    * For reference, see footnote 219, p. 636.
    ${ }^{* *} P_{m n t}=$ vapor pressure at $t^{\circ} \mathrm{C}$. ${ }^{+}{ }^{+} \dot{N}_{n}=$ number of molecules $/ \mathrm{cm}^{2}$ for monomolecular layer.
    In the case of $\mathrm{H}_{2} \mathrm{O}$, for which the values of $L$ (path length) and $\delta$ (diameter) for a series of temperatures are given in the table, the Sutherland relation was used with $C=650$ and $\eta_{15}=926 \times 10^{-5} \mathrm{cgs}$ units.

    In the case of Hg the values of $\eta$ (viscosity) used are based on $t=219.4^{\circ} \mathrm{C}$. Values at other temperatures were derived by means of Sutherland's relations, with $C=942.2$

[^275]:    ${ }^{220}$ Newman and Searle, The gencral properties of matter, Edward Arnold \& Co., London.

[^276]:    * Tables $698-700$ and 702 prepared by J. D. Cobine, General Electric Co., Schenectady, N. Y. ${ }_{221}$ Cobine, J. D., Gaseous conductors, 2d ed., McGraw-Hill Book Co. Used by permission of the publishers.

[^277]:    * For reference, see foot note 221 , above.
    ${ }^{* *} D$ in $\mathrm{cm}^{2} / \mathrm{sec}$. $\dagger D={ }^{*} D_{0}\left(T / T_{0}\right)^{m}\left(p_{0} / p\right)$, where $D_{o}$ is the value of $D$ in the table, $T_{0}=0^{\circ} \mathrm{C}$, $p_{0}=1 \mathrm{~atm}$.

[^278]:    * For reference, see footnote 220, p. 640.
    $\dagger$ Viscosity. $\ddagger$ Van der Waal's equation.

[^279]:    * For reference, see footnote 219, p. 636.

[^280]:    *For reference, see foctnote 203, p. 624.

[^281]:    * For reference, see footnote 203, p. 624.

[^282]:    ** For reference, see footnote 203, p. 624.

[^283]:    

[^284]:    * For reference, see footnote 203, p. 624.

[^285]:    * For reference, see footnote 224, p. 665.

[^286]:    (continued)

[^287]:    * This list was prepared by R. G. Herb, University of Wisconsin, and W. W. Brobeck, University of California. See Brookhaven National Laboratory Publication BNL-L-101, Particle accelerators, 1948.
    $\dagger$ High-speed neutrons cannot, of course, be produced directly by any of these devices. Neutrons are produced by bombarding certain materials with one of the high-speed particles produced by these devices. If beryllium, boron, or lithium are bombarded by a-particles neutrons are produced thus:

    $$
    \begin{gathered}
    { }^{{ }^{\mathrm{Be}}{ }^{\theta}+2 \mathrm{He}^{4} \rightarrow{ }_{0} \mathrm{C}^{12}+{ }_{0} n^{1}} \\
    \mathrm{~B}^{11}+2 \mathrm{He}^{4} \rightarrow{ }_{7} \mathrm{~N}^{14}+{ }_{0} n^{1} \\
    { }_{1} \mathrm{H}^{2}+h \nu \rightarrow \mathrm{H}^{1}+{ }_{0} n^{1}
    \end{gathered}
    $$

    $\ddagger$ Machines up to about 6 Mev now produced commercially.

[^288]:    ${ }^{223}$ References: a, Tollestrup, Fowler, and Lauritsen, Phys. Rev., vol. 78, p. 372, 1950. b, Bethe, H. A Elementary nuclear theory, John Wiley \& Sons, Inc., 1947; Rasetti, F.. Elements of nuclear physics. PrenticeHall, Inc. 1936 ; Poss, H. L., Phys. Rev., vol. 75, D. 600, 1949. c, Harvey, J. A., Bull. Amer. Phys. Soc., vol. 25, p. U4, 1950 . d, Stern, M. O., Rev. Mod. Phys.. Anril 19.49. e, Wapstra, A. H.. Phvsica, vol. 16, p. 33, 1950. f, Perlman, I., Ghiorso, A., and Seaborg, G. T., Phys. Rev., vol. 77, p. 26, 1950; Kinsey, B. B. et al., Phys. Rev., vol. 78, f. 77,1950 ; also private communications; Hanson, et al., Phys. Rev., vol. 76, p. 578 , 1949. g, Ramsey, Norman, Experimental nuclear physics (forthcoming), John Wilev \& Srns. Inc.

    Note added in proof, 1953 .- Because of recent mass measurements, the mass of Pb 200 should be taken as 206.03859. All mass values should be lowered 0.00660 mass units. See Stone, Martin O., Rep. Univ. California Radiation Lab., April 1952.
    ${ }^{*} I=$ spin. $\quad{ }^{*}$ Quadrupole moment $=-0.4 . \quad \dagger\left(10^{-24} \mathrm{~cm}^{2}\right) . \quad \ddagger$ Radioactive series.
    § Prepared by J. A. Harvey, Massachusetts Institute of Technology (see footnote 223, above, reference c).

[^289]:    - Prepared by E. E. Salpeter and W. K. H. Wolfgang. quantum), $h \nu: \gamma ;$ value $(\lambda=.6 \mu)=3.310 \times 10^{-12}$ ergs.

[^290]:    ${ }^{24}$ Stranathan, J. D., The particles of modern physics, Blakiston Co., 1942. Used by permission of the publishers.

[^291]:    * For reference, see footnote 225 above.

[^292]:    * Revised by Jacol L. Rhodes, I'niversity of Pennsylvania.
    ${ }_{200}$ Stephens, W. E.. (editor), Nuclear fission and atomic energy, Science Press. Used by permission of the editor.

[^293]:    ${ }^{227}$ Hornyak，W．F．，and Lauritsen，T．，Rev．Mod．Phys．，vol．20，p．191，1948；Phys．Rev．，vol．78，

[^294]:    ${ }_{228}$ McElhinney，J．，Hanson，A．O．，Becker，R．A．，Duffield，R．B．，and Diven，B．C．，Phys．Rev．，vol．75， p． $542,1949$.

[^295]:    ${ }^{22 y}$ G. T. Seaborg, private communication.

    * Sixteen-hour +100 -year isomers.

[^296]:    - Revised by J. L. Rhodes. For reference, see footnote 226, p. 667.

[^297]:    ${ }^{280}$ Nat. Res. Council Bull. 80, 1931.

[^298]:    * For reference, see footnote 199, p. 618.
    ${ }^{2200}$ Rutherford, E., Chadwick, J., and Ellis, C. D., Radiation from radioactive substances, Cambridge Univ. Press, 1930.

[^299]:    ${ }^{231}$ Physics Today, vol. 3, p. 5, 1950.

[^300]:    (continued)
    (cefore it was known that they were isotopes of other elements.

[^301]:    * Almost all the isotopes of this family are artificial products and arc not now found in the earth.
    ${ }^{232}$ Sergè, Emilio, and Helmholtz, A. C., Rev. Mod. Phys., vol. 21, p. 271, 1949.

[^302]:    * For reference, see footnote 45, p. 136.

[^303]:    ${ }^{233}$ Rutherford, E., Chadwick, J., and Ellis. C. D., Radiation from radioactive substances, Cambridge University Press, 1930.

[^304]:    * For reference, see foolnole 199. 1). 618.
    $\dagger$ Approximate range in air (from curve).

[^305]:    * For reference, see footnote 199, p. 618.
    $\dagger$ Approximately, from curve.

[^306]:    ＊For reference，see footnote 233，p． 679.

[^307]:    ＊For reference，see footnote 233，p． 679.

[^308]:    * For reference, see fool note 234, p. 684.

[^309]:    * For reference, see footnote 199, p. 618.
    * The radiation from potassium may seem to be too intense as compared to that from thorium 232 or uranium 238 but it must be remembered that the active isotope of potassium constitutes only . 01 percent of ordinary potassium while the active isotopes of uranium and thorium constitute about 100 percent of the material. It is also to be noted that the active isotope of potassium has more disintegration than either uranium or

[^310]:    * For reference, see footnote 199, p. 618.

[^311]:    - For reference, see footnote 236, above.

[^312]:    * For reference, see footnote 236, p. 692.

[^313]:    ${ }^{237}$ National Bureau of Standards Handbook 41, Medical X-ray protection up to two million volts.

[^314]:    * For reference, see footnote 236, p. 692.

[^315]:    * Direct-current potentials require the order of 10 percent greater thickness than those given here for pulsating potential.
    $\dagger$ For reference, see footnote 237, p. 693.

[^316]:    *For reference, see footnote 236, p. 692.
    $\dagger \delta=0.17803, \delta_{2}=0.17917$ (Duane, 1933).

[^317]:    *This criterion cannot be strictly applied to the $K$ a line from 4 Be to 9 F , nor to the $K \beta_{1}$ line from 11 Na to 29 Cu as reported in this table.
    ${ }_{228}$ Compton, A. H., and Allison, S. K., X-rays in theory and experiment, D. Van Nostrand Co., Inc., New York, 1935. Courtesy of the publishers.

[^318]:    * Peak kilovolts.

[^319]:    *For reference, see footnote 238, p. 697.

[^320]:    * For reference, see footnote 238, p. 697.

[^321]:    
    

[^322]:    * Revised by J. L. Rhodes, University of Pennsylvania. For reference, see footnote 226, p. 667.

[^323]:    * For reference, see foot note 226, p. 667.

[^324]:    *For reference, see footnote 226, p. 667.
    $\dagger$ Most of the scattering of fast neutrons is inelastic scattering, resulting in large energy losses (as much as 90 percent). $\ddagger$ The resonance peak for $U^{238}$ occurs at approximately 5 ev and is taken to have an effective width of 0.16 .

[^325]:    ${ }^{244}$ Rev. Mod. Phys., vol. 21, p. 1, 1949 ; Stranathan, The "particle" of modern physics, D. Blakiston Co.; Montgomery, D. J. X., Cosmic ray physics, Princeton University Press; Johnson, T. R., Rev. Mod. Phys., vol. 10, p. 193, 1938; Swann, W. F. G., Reports on progress in physics, vol. 10. p. 1, 1946.
    ${ }^{245}$ Korff, Physics Today, vol. 3, p. 9, 1950.
    ${ }^{246}$ Teller, Edward, Physics Today, vol. 2, p. 6, 1949.

[^326]:    * For reference, see footnote 203, p. 624.

[^327]:    * If there were no compensating effects the potential of the earth would increase about $180 \mathrm{~V} / \mathrm{sec}$. $\dagger$ The number varies with the geomagnetic latitude, being about 0.33 particles $\mathrm{cm}^{-2} \mathrm{sec}^{-1}$ at high latitudes ( $>40^{\circ}$ ) and about 0.032 particles $\mathrm{cm}^{-2} \mathrm{sec}^{-1}$ at the equator. This data is based upon an energy of 32 ev necessary to produce one ion pair. $\ddagger$ Thus the average ray entering the $\mathrm{cm}^{3}$ at sea level has an energy of about $10^{8} \mathrm{ev}$.

[^328]:    * Astrophysical data.

[^329]:    ${ }^{247}$ Bradt and Peters, Phys. Rev., vol. 77, p. 54, 1950.

[^330]:    * Prepared under the direction of K. T. Adams, U. S. Coast and Geodetic Survey.

[^331]:    *For sea stations, the depth is recorded in this column; the observations were made in submarines and reduced to sea level.

[^332]:    ${ }^{248}$ Heiskanen, W., Catalogue of the isostatically reduced gravity stations, Helsinki, 1939.
    *For sea stations, the depth is recorded in this column; the observations were made in submarines and reduced to sea level.

[^333]:    * Prepared by L. B. Aldrich and W. H. Hoover, Astrophysical Ohservatory, Smithsonian Institution.
    ${ }_{249}$ Abbot, C. G., Solar radiation and weather studies, Smithsonian Misc. Coll., vol. 94, No. 10. 1935.
    250 Aldrich, L. B., and Abbot, C. G., Smithsonian pyrheliometry and the standard scale of solar radiation, Smithsonian Misc. Coll., vol. 110, No. 5, 1948. See also Annals, Smithsonian Astrophysical Observatory, vol. 7, ch. 3 (in press).

[^334]:    ${ }^{251}$ Moon, P., Journ. Franklin Inst., vol. 230, p. 583, 1940.
    ${ }^{252}$ Hulbert, E. O., Journ. Opt. Soc. Amer., vol. 37, p. 405, 1947.

[^335]:    * Values . 3149 through . $4487 \mu$ from Cavanaggia and Chalonge, Ann. d'Astrophys., vol. 9, p. 143 1946; . 5186 through $10.2 \mu$ from Pierce, McMath, Goldberg, and Mohler, Astrophys. Journ., vol. 112, p. 289, 1950.

[^336]:    * Prepared by G. M. Clemence, U. S. Naval Observatory. For more extensive tables, see "Tables of Sunrise, Sunset, and Twilight," Supplement to the American Ephemeris, 1946.

[^337]:    251 Jones, L. A., and Condit, H. R., Journ. Opt. Soc. Amer., vol. 38, p. 147, 1948.

[^338]:    * Prepared hy Allan F. Cook II
    ${ }^{2555}$ Astron. Mitt. Zürich, No. 145. 1945; Tourn. Geophys. Res., vol. 54. p. 347, 1949: Waldmeier, M., Astron. Mitt Zürich; Terr, Mag.; Tourn. Geophys. Res., Trans. Int. Astron. Vnion Quart. Bull. Solar Activity; Imerican Sunspot Number Reductions, Central Radio Propagation Laboratory, National Bureau of Standards.

[^339]:    *These tables were prepared under the supervision of D. H. Menzel, of Harvard University, and Edith Janssen Tebo, of Harvard College Observatory.

    # TABLE 825.-THE LARGEST TELESCOPES IN ACTIVE SCIENTIFIC USE (1949) $\dagger$ 

    ## Reflectors <br> ( 60 -inch mirrors and larger)

    Hale Telescope, Palomar Mountain, Calif., U. S. A.............................. 200 -inch
    Hooker Telescope, Mount Wilson, Calif., U. S. A.................................. . . . 100-inch
    MacDonald Observatory, Mount Locke, Tex., U. S. A............................... . . 82-inch
    Radcliffe Observatory, Pretoria, South Africa...................................... 76-inch
    David Dunlap Observatory, Richmond Hill, Ontario, Canada................... 74-inch
    Dominion Astrophysical Observatory, Victoria, B. C., Canada.................... 72-inch
    Perkins Observatory, Delaware, Ohio, U. S. A..................................... 69 -inch
    Wyeth Reflector, Harvard Jbservatory, Oak Ridge, Mass., U. S. A.............. 61-inch
    Southern Station of the Harvard Observatory, Bloemfontein, South Africa..... 60-inch
    Mount Wilson Observatory, Mount Wilson, Calif., U. S. A........................ 60 -inch
    Cordoba Observatory, Bosque Alegre, Argentina................................... 60 -inch

    ## Refractors <br> (30-inch lenses and larger)

    Yerkes Observatory, Williams Bay, Wis., U. S. A............................... 40 -inch
    Lick Observatory, Mount Hamilton, Calif., U. S. A................................. 36-inch
    Astrophysical Section, Observatory of Paris, Mundon, France.................... 33-inch
    Allegheny Observatory, Pittsburgh, Pa., U. S. A.................................... . . . 30-inch
    University of Paris Observatory, Nice, France....................................... . 30-inch
    Schmidt-type telescopes
    (of large aperture)
    48 -inch correction plate, 72 -inch mirror, Palomar Observatory, Calif., U. S. A.
    24 -inch correction plate, 36 -inch mirror (Burrell Telescope), Warner \& Swasey Observatory, Case Institute of Technology, Cleveland, Ohio, U. S. A.
    24 -inch correcting plate, 33 -inch mirror (Jewett Telescope) Harvard Observatory, Oak Ridge, Mass., U. S. A.

[^340]:    ** Prepared by G. M. Clemence, U. S. Naval Observatory.

[^341]:    * Prepared by G. M. Clemence, U. S. Naval Observatory.

[^342]:    * Prepared by A. N. Vyssotsky, University of Virginia.
    ${ }_{250}$ Astron. Journ., vol. 53, p. 87, 1948.

[^343]:    * Prepared by G. M. Clemence, U. S. Naval Observatory, $\dagger$ On and before 1582, Oct. 4 only. $\ddagger$ On and after 1582 , Oct. 15 only.

[^344]:    * Prepared by G. M. Clemence, U. S. Naval Observatory.
    $\dagger$ For January - 1.
    $\ddagger$ Julian Calendar. § Gregorian Calendar.

[^345]:    * Mass of the Earth is $5.975 \times 10^{27}$ grams; of the Sun $332,488(1 \pm 0.00013) E=1.987 \times 10^{33}$ grams; of the Moon $(0.012289 \pm 0.000004) E=7.343 \times 10^{25}$ grams. $\quad \dagger$ Equatorial diameter of the Earth $=12,756.78 \mathrm{~km}$; polar diameter $12 \overline{, 7} 13.82 \mathrm{~km}$; "mean diameter" $12,742.46 \mathrm{~km}$. See Table 827

[^346]:    *Prepared G. P. Kuiper, Yerkes Observatory
    ${ }^{257}$. Imerican Ephemeris and Nautical Almanac for 1950.
    $+\times 10^{n}$. $\ddagger$ Mean distance in km computed from earth's equatorial radius ( 6378.388 km ) and solar parallax of $8 . " 80$. Recent determinations by Spencer Jones (Monthly Notices, Roy. Astron. Soc. vol. 101, P. 356, 1941) and Rabe ( $\lambda$ stron. Journ., vol. 55, p. 112, 1950) give $8 . " 790 \pm 0 . " 001$ and $8 . " 7984 \pm 0 . " 0004$, respectively.

[^347]:    * Compiled by D. L. Harris, Yerkes Olservatory. † With respect to rotation of planet. $D=$

[^348]:    * Prepared by S. W. McCuskey, Case Institute of Technology.
    ${ }^{258}$ van Rhijn, Groningen Publ. No. 47, 1936.

[^349]:    * Prepared by R. B. Baldwin, Oliver Machinery Co., Grand Rapids, Mich.

[^350]:    275 13ecker, W., Astron. Nachs., wot. 277, p. 65, $19+9$.
    ${ }^{260}$ Dinjon, . Inn. Sirashourg, vol. 3, sit. 3, 1. $168,1937$.

[^351]:    - Selected by Edith J. Tebo, Harvard Observatory.

    2ai The Observer's Handbook for 1949, Royal /lstronomical Society of Canada.

[^352]:    * Compiled by R. W. Goranson.

[^353]:    * Compiled by R. W. Goranson.

[^354]:    ${ }^{202}$ Menzel, D. H., Our Sun, p. 260, Harvard Univ. Press, 1949. U'sed by permission.

[^355]:    *This table, after Boss, gives the number of stars in his catalog brighter than $6^{m} .5$ which have proper motions between given limits. For reference, see footnote 272, p. 746.

[^356]:    * Prepared by Edith J. Tebo, Harvard College Observatory. † Used with permission of the author.

[^357]:    * Prenared by H. Shapley, Harvard University.
    ${ }^{200}$ Shapley, Harvard Bull., vol. 861, 1928.
    207 Shapley, Proc. Nat. Acad. Sci., vol. 26, n. 544. 1940.
    ${ }^{268}$ Kuiper, Astrophys. Journ., vol. 88, p. 453, 1938.

[^358]:    * Prepared hy Edith J. Teho. Harvard College Observatory.
    ${ }^{200}$ Bowen, I. S., and W$\dot{\text { Wen }}$. A. B., Lick Obs. Mull., vol. 19, p. 1, 1939.

[^359]:    * Prepared hy Fidith J. Tebo. Harvard College Observatory.
    ${ }_{270}$ An Atlas of Stellar Spectra. Tniversity of Chicago Press, 1943.
    ${ }^{271}$ Deutsch, Istrophys. Journ., vol. 105, n. 283, 1947.
    ${ }^{272}$ Roman. Morgan, and Eggen, Astrophys. Journ., vol. 107, p. 107, 1948. Gireenstein, Astrophys. Journ., vol. 107, p. 151, 1948; vol. 109, ก. 121, 1949.

[^360]:    * Prepared by M. W. Mayall, Harvard College Observatory.
    ${ }^{273}$ Trans. Int. Astron. Union, vol. 7, p. 408, 1950.
    274 Trans. Int. Astron. Union, vol. 6, p. 248, 1938.

[^361]:    ＊Prepared by A．N．Vyssotsky，University of Virginia．

[^362]:    ${ }_{275}$ Baade，Walter，Astrophys．Journ．，vol．100，n．150， 1944.
    $\dagger$ Modulus in stellar magnitude is $m-M=5(\log d-1)$ ，where $d$ is distance in parsecs and $M$ is absolute magnitude．

[^363]:    * Prepared by A. N. Vyssotsky, University of Virginia.

[^364]:    * Prepared liy S. B. Nicholson, Mount Wilson Observatory.
    ${ }_{270}$ Kuiper, G. P., Astrophys. Journ., vol. 88, p. 464, 1938.
    $\ddagger$ Payne, Stellar atmospheres, 1925 . $\ddagger$ Interpolated.

[^365]:    * Prepared by W. I.uyten, University of Minnesota. †These stars have invisible companions.

[^366]:    * Prepared by Peter van de Kamp, Swarthmore College.

[^367]:    *Prepared by W. Luyten, University of Minnesota. † Visual binary. $\ddagger$ Has distant companion. § Has an optical companion. The magnitude shown is the combined visual magnitude. I| Spectroscopic binary. $m=$ magnitude, $S p=$ spectrum, $\mu=$ proper motion, $\theta=$ position angle, $V=$ radial velocity, $p=$ parallax, $M=$ absolute magnitude.

[^368]:    * Prepared by Edith J. Tebo, Harvard College Observatory.
    ${ }_{277}$ Russell, Dugan, and Stewart, Istronomy, p. 740, Ginn \& Co., 1926. Used by permission.

[^369]:    * Prepared by R. E. Wilson, Mount Wilson Observatory

[^370]:    * Prepared by Edith J. Tebo, Harvard College Observatory.
    ${ }_{279}$ Astrophys. Journ., vol. 88, p. 472, 1938.
    280 An atlas of stellar spectra, p. 34, University of Chicago Press, 1943.

[^371]:    * Prepared by F. H. Seares, Mount Wilson Observatory
    ${ }^{281}$ van Rhijn, Groningen Publ. No. 43, Table 6, 1929.
    ${ }^{282}$ van Rhijn, Groningen Publ. No. 43, Table 10; Seares and Joyner, Mount Wilson Contributions Nos. 346, 347; Astrophys. Journ., vol. 67, p. 24, 123, 1928; Publ. $\Lambda$ stron. Soc. Pacific, vol. 40, p. 303, 1928.

[^372]:    * Prepared by W. Luyten, University of Minnesota.
    ${ }^{288}$ Lick Obs. Bull. No. 344 ; Harvard Circ. 283; Publ. Cincinnati Obs. LO 18; Publ. Astronomical Ohs. Univ. Minnesota, vol. 3, No. 1.

[^373]:    * Prepared by F. H. Seares, Mount Wilson Observatory.

[^374]:    * Prepared hy D. B. Mclaughlin. ['niversity of Michigan. a. Shsorption velocities increased with time: N $\backslash$ (q), to $-1700 \mathrm{~km} / \mathrm{sec}$; (PP 1.ac, to $-2500 \mathrm{~km} / \mathrm{sec}$. D. Absolute magnitude assumed; distance based on asamed alisolute magnitude. c, Recurrent novae: T CrB; RS Oph, 1898; T Pyx, 1890, $1902,1920$. T (rB: distance based on spectroscopic parallax of class $M$ companion, i, Nova Gem and CP Pup: distances bised on strength of interstellar calcium lines. e, RT Serpentis reached maximum in 1919. f , Nova Tauri 1054; a super novz; now the (rab) Nebula. Note on velocity of RS Ophiuchi: there was no system of ahsorption lines at the short-wavelength edge of the emissions as in other novae.

[^375]:    * Prepared by O. Struve, University of California, Berkeley.

    284 Astrophys. Journ., vol. 88, p. 472, 1938.

[^376]:    * Prepared by R. M. Emberson, Research and Development Board, Washington, D. C.
    ${ }_{245}$ Pettit and Nicholson, Astrophys. Journ., vol. 56, p. 295, 1922; vol. 68, p. 279, 1928; vol. 78, p. $320,1933$. Stern and Emberson, \strophys. Journ., vol. 94, p. 412, 1941.

[^377]:    * Prepared by L. Tacchia, Massachusetts Institute of Technology.
    ${ }^{288}$ Kukarkin, B. V., and Parenago, P. P., Fizičeskic Peremennye Zvjozdy, 1937; Gaposchkin, C. P., and Gaposchkin, S., Variable stars, 1938; Camphcll, I.., and Jacchia, I.., The story of variable stars, 1941.

[^378]:    * Prepared by G. P. Kuiper, Yerkes Observatory.

[^379]:    * Prepared by R. E. Wilson, Mount Wilson Observatory, and E. M. Janssen, Harvard College Observatory.

[^380]:    * Prepared by B. Donn, Harvard University
    ${ }^{287}$ Dunham, Proc. Amer. Philos. Soc., vol. 81, p. 277, 1939; Eddington, Proc. Roy. Soc. London, vol. A 111, p. 424, 1926; Spitzer, Astrophys. Journ., vol. 107, p. 6, 1948; vol. 109, p. 337, 1949; vol. 111, p. 593, 1950; van de Hulst, Rech. Astron. Obs. Utrecht, vol. 11, pt. 1, 1946.

[^381]:    * Prepared by A. N. Vyssotsky, University of Virginia.

    289 Astron. Journ., vol. 53, p. 94, 1948.

[^382]:    * Revised by R. E. Wilson, Mount Wilson Observatory.
    ${ }^{284}$ Miczaika, G., Astron. Nachs., vol. 271, p. 265, 1940.

[^383]:    * Prepared by R. E. Wilson, Mount Wilson Observatory.

[^384]:    * Prepared by Z. Kopal, Harvard College Observatory.
    ${ }^{290}$ References: a, Keeping, Publ. Dominion Astrophys. Obs., vol. 7, p. 349, 1947. b, Wood, Astrophys. Journ., vol. 108, p. 28, 1948. c, Dugan, Princeton Contr., No. 12, 1931. d, Kopal (unpublished). e,

[^385]:    * Prepared by O. Struve, University of California, Berkeley.

    201 Lick Obs. Bull. No. 521, 1949.
    $\dagger$ System of Castor.

[^386]:    292 Shapley, Proc. Nat. Acad. Sci., vol. 30, p. 63, 1944; Pop. Astron., vol. 57, p. 9, 1949. For number of variables see Sawyer, Helen B., Publ. David Dunlap Obs., vol. 1, p. 388, 1947.

[^387]:    * Prepared by A. H. Joy, Mount Wilson Observatory.
    ${ }^{204}$ Gerasimič, Luyten, Proc. Nat. Acad. Sci., vol. 13, p. 180, 1927.
    245 a, Oort, Bull. Astron. Inst. Netherlands, vol. 4, p. 80, 1927. b, Plaskett, Pearce, Publ. Dominion Astrophys. Olss.. vol. 5. n. 241, 193 G. C, Plaskett, Pearce, Publ. Dominion Astrophys. Obs., vol. 5, p. 167, 1933. d, Lindlhad, Monthly Notices, Roy. Astron. Soc., vol. 90, p. 503, 1930. e, Wilson, R., Astron. Tourn., vol. 40, p. 121, 1930. f, Relman, Publ. Dominion Astrophys. Obs., vol. 6, p. 27, 1931. G. Berman, Lick Obs. Bull.. vol. 18, p. 57, 1937. h, Jov, Astrophys. Journ., vol. 89, p. 356, 1939. i, Wilson, Astrophys. Journ., vol. 93, p. 212, 194i. k, Wilson, Astrophys. Journ., vol. 94, p. 12, 1941. 1, Wilson, Astrophys. Journ., vol. 96, p. 371, 1942.

[^388]:    * Prepared by B. Donn, Harvard University.
    $\dagger$ Preliminary values, currently under investigation by Whitford.
    ${ }_{2016}$ Stebbins, Huffer, and Whitford, Astrophys. Journ., vol. 96, p. 209, 1939; Bok, Pop. Astron., vol. 52. p. $261,1944$.
    ${ }_{297}$ Stebbins and Whitford, Astrophys. Journ., vol. 98, p. 323, 1943; Whitford, Astrophys. Journ., vol. 107, p. 102, 1948.
    ${ }_{298}$ Oort. Ann. d'Astrophys., vol. 1, p. 91, 1938.
    ${ }_{299}$ Strohmeier, Zeitschr. Astrophys., vol. 17, p. 83, 1939.
    300 Greenstein, Astrophys. Journ., vol. 87, p. 151, 1938; Oort, Bull. Astron. Inst. Netherlands, vol. 8, p. 308, 1938; Stehbins, Astrophys. Journ., vol. 90, P. 209, 1939; van Rhijn, Groningen Publ. 51, 1946; Weaver, Astrophys. Journ., vol. 110, p. 190.1949.

    302 Hall, Science, vol. 109, p. 166, 1949; Hiltner, Science. vol. 109, p. 165, 1949, Astrophys. Journ., 1949.

[^389]:    * Tables 888 to 894 , and 897 prepared by R. H. Fleming, U. S. Hydrographic Office.

[^390]:    ${ }^{302}$ Reprinted by permission of the publishers from The oceans; their physics, chemistry, and general biology, by H. U. Sverdrup, Martin W. Johnson, and Richard H. Fleming. Copyright 1942 by PrenticeHall, Inc.

[^391]:    * For reference, see footnote 302, p. 773.
    $\dagger$ Computed.

[^392]:    * Absiracted from an article prepared for the Encyclopedia Britannica, by Walter Munk, Scripps Institute of Occanography. Used by permission.

[^393]:    ${ }^{503}$ Jeffreys, The earth, Macmillan, 1929 , Innes, Changes in the length of the day, Scientia, vol. 42 , p. 69, 1927; Brown, Nature, vol. 119, P. 200, 1927; Jo rrn. Roy. Astron. Soc. Canada, vol. 24, p. 177, 1930. Kevised by G. M. Clemence, U. S. Naval Observatory.

